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*Title:*

RESULTS OF EXPLOSIVELY-DRIVEN ISENTROPIC  
COMPRESSION EXPERIMENTS (HEPP-ICE)

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## **Results of Explosively-Driven Isentropic Compression Experiments (HEPP-ICE)\***

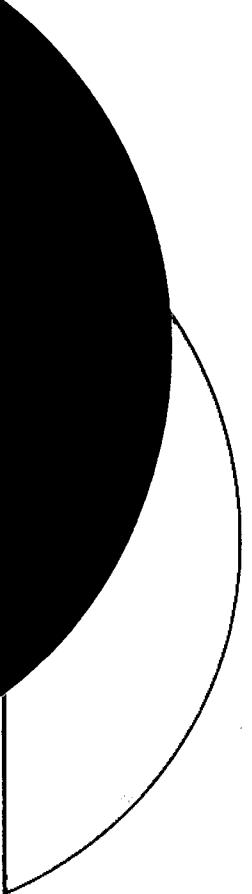
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Using the Los Alamos high explosive pulsed power (HEPP) system, isentropic equation of state (EOS) data may be obtained for a wide range of materials. Current pulses with risetimes of  $\sim$ 500 ns and current densities exceeding 400 MA/m, create continuous magnetic loading of samples at megabar pressures. We will summarize the technique and the problems that had to be overcome to perform the HEPP-ICE experiments at these pressures. We will then present our EOS results obtained with the conventional Lagrangian analysis and the Hayes' "Backward" integration method,<sup>1</sup> and compare the data with the published principal isentrope of OFHC copper.

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\* This work was supported by the U.S. Department of Energy, LA-UR-04-0157

<sup>1</sup> "Backward Integration of the Equations of Motion ...," Dennis Hayes, Sandia National Labs., SAND2001-1440, May 2001



# Results of Explosively-Driven Isentropic Compression Experiments (HEPP-ICE)

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ICOPS 2004  
July 1

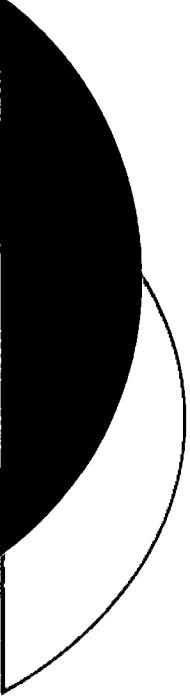
**Doug Tasker**, Jim Goforth, Hank Oona, Paulo Rigg,  
Darcie Dennis-Koller, Jim King, Dave Torres, Dennis Herrera,  
Pancho Sena, Frank Abeyta, Lenny Tabaka\*  
DX-2, \*P-22

Los Alamos National Laboratory

# Overview

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- What is HEPP-ICE?
- Technique described, physics, circuit specifications
- Experimental design
- Timing issues
- Results compared to principal isentrope of OFHC copper
- Future capabilities
- Summary



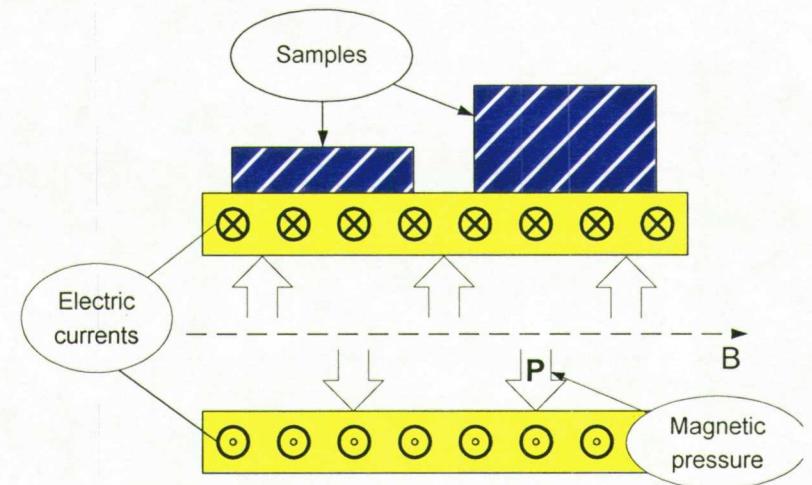
# What is HEPP-ICE?

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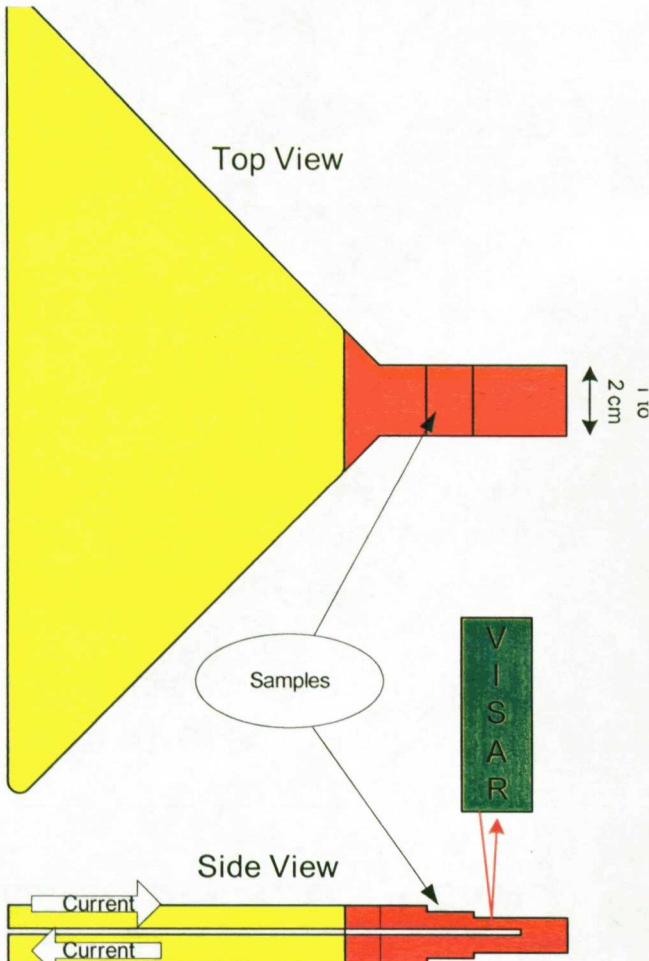
- Purpose:
  - To obtain isentropic equation-of-state (EOS) data for various materials at megabar pressures.
- Why?
  - At megabar pressures isentropic EOS data are significantly different to shock (Hugoniot) EOS data.
- Concept:
  - Use magnetic pressure to achieve shock-free loading of materials.
- Method:
  - Use high explosive pulsed power (HEPP) to develop current densities  $\geq 5\text{MA/cm}$  with risetimes of  $\sim 500\text{ ns}$ .

# Magnetic compression - parallel plates

- Magnetic pressure  $P = 2\pi$  GPa (63 kbar) for  $J = 10^8$  A/m (1 MA/cm) -
  - $P = \frac{1}{2}\mu_0 J^2$  Pa (J: current density, A/m), SI units,
  - $P = \sim 3$  Mbar @ 7 MA/cm ( $B = 880$  T).



# HEPP ICE load section



- Planar design (not coaxial).
- Tapered to minimize inductance.



HEPP-ICE gap exaggerated, is  $\sim \frac{1}{2}$  mm

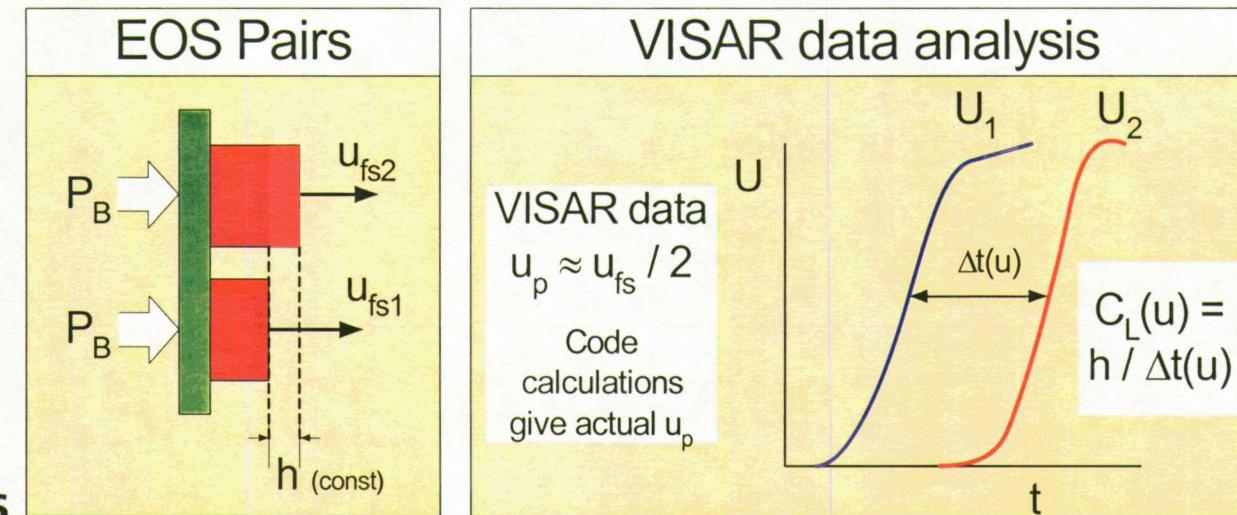
# EOS data recovery – standard method

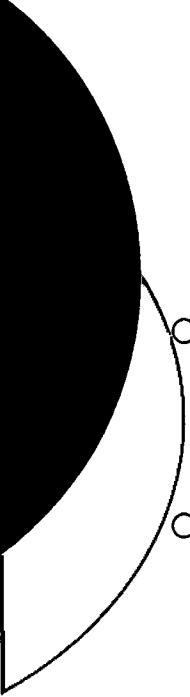
- 2 or more sample thickness compressed in each experiment
  - Note: Pressures ( $P_B$ ) must be equal so B field MUST be uniform.
- VISARs used to measure particle velocities at back faces
  - with or without windows.
- Lagrangian analysis gives pressure etc., with  $h = \text{constant}$ .

$$c_L(u) = \frac{h}{\Delta t(u)}$$

$$d\sigma = \rho_0 c_L(u) du$$

$$c_E = \left( \frac{\rho_0}{\rho} \right) c_L$$





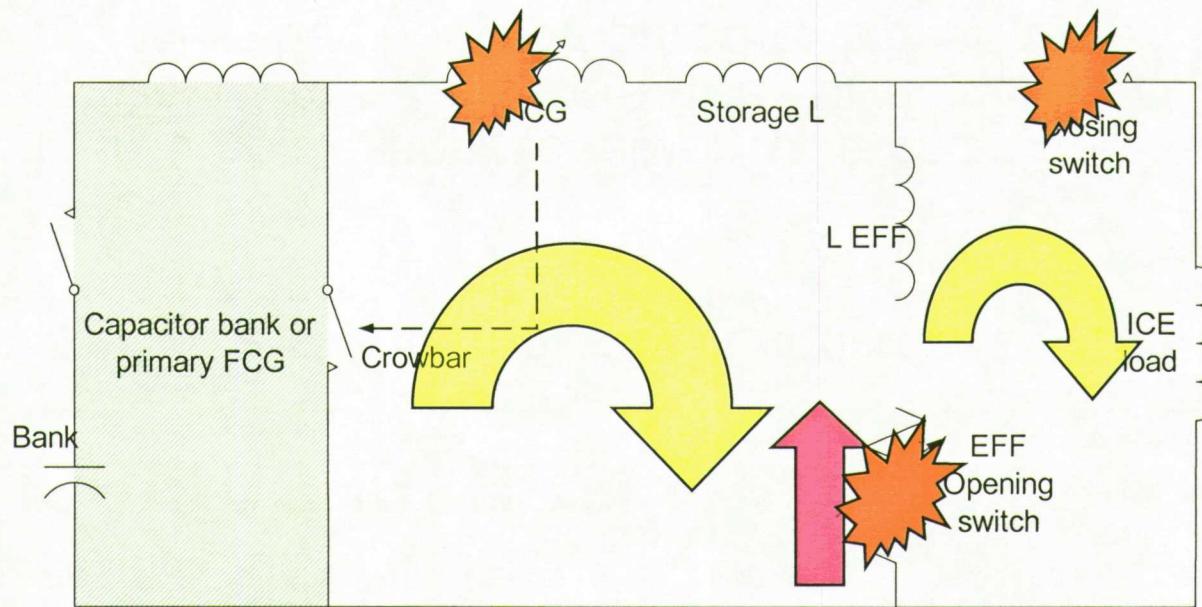
# Risetime issues

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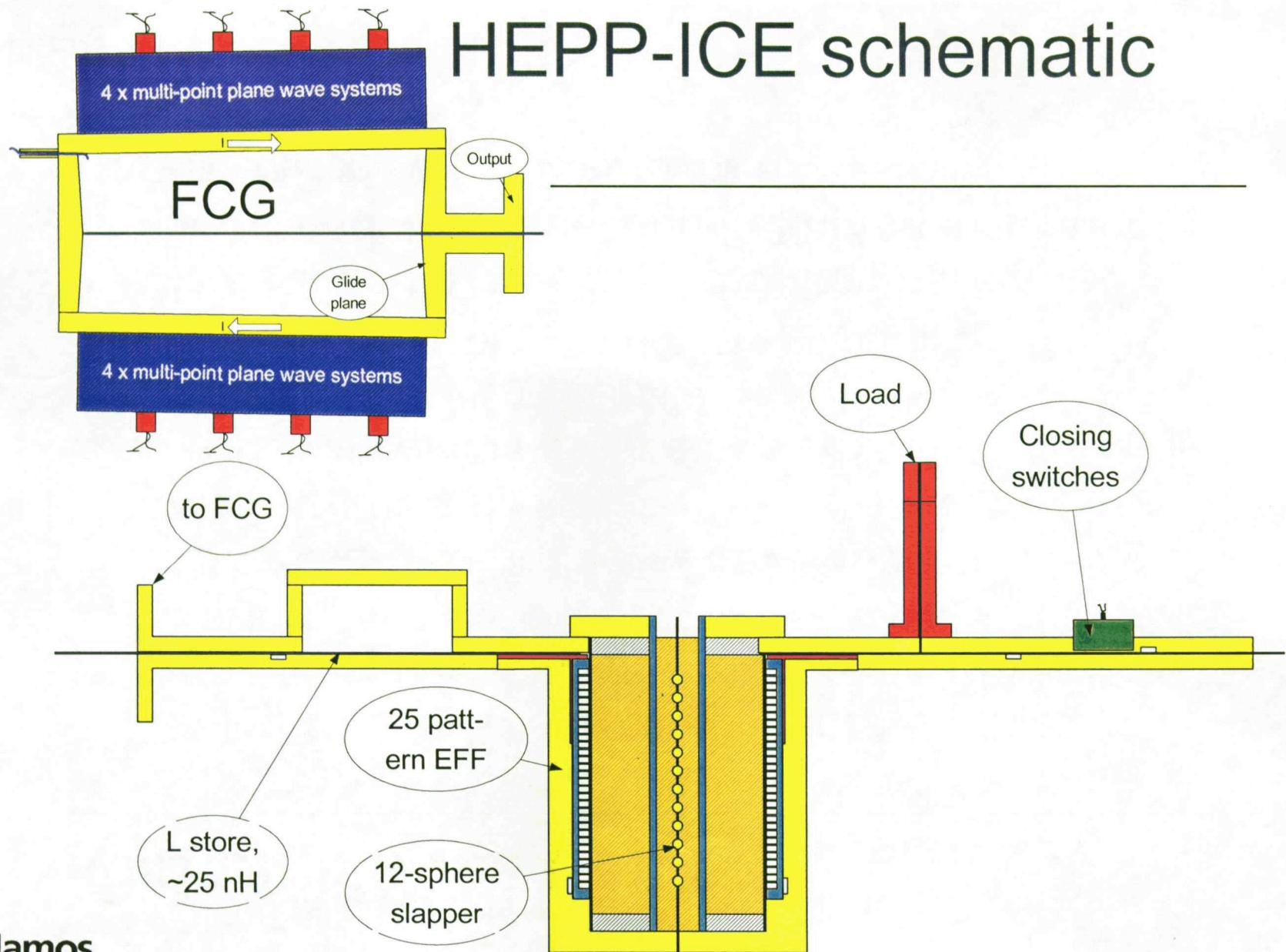
- Pressure  $P_B \gg$  strength of any conductor (1 - 10 kbar), so conductors fly apart.
- ONLY inertia holds them together for a short time (i.e., time for relief waves to return from free surface). So current risetimes must be short compared to transit time.
- BUT if risetime is too short than shocks develop prematurely
  - 300 to 600 ns optimum for ICE for mm-thick samples.
- This is a challenge for HEPP, 5  $\mu$ s is more typical.
- Have developed a “baseline” system to meet this requirement.

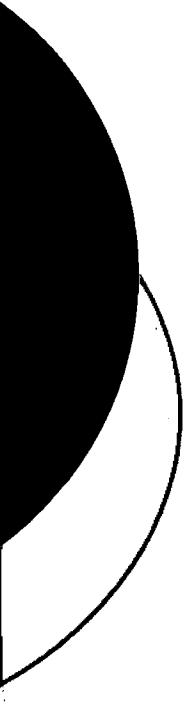
# LANL HEPP-ICE Circuit

- Plate flux compression generator (FCG) and pulse conditioning
  - FCG produces large current at low voltage,
  - Then explosively-formed fuse (EFF) produces high voltage,
    - for fast risetime,
  - At peak voltage, current switched to load by staged closing switch,
    - for shaped (controlled) current rise.



# HEPP-ICE schematic





# Circuit issues (timing)

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- Timing of the various components is critical
  - Desired jitter of the flux compressor, opening switch, and closing switches is  $\sim 50\text{ns}$ .
- We had serious problems developing a closing switch to these specs.
  - Original switch was based on explosively-driven jet puncture of insulation,
  - Jitter was as high as **600 ns** with this switch.
- We designed a new closing switch based on shock-induced conduction in Kapton insulation
  - Reduced switch jitter to **20 ns**.

# Progress with HEPP-ICE system - 1

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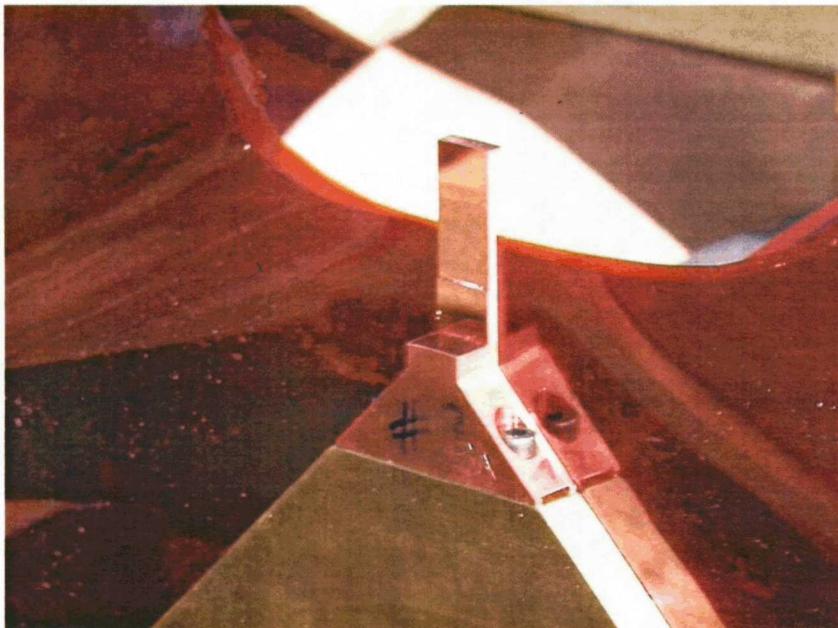
- We systematically eliminated various problems associated with insulation systems, corona, and closing switches.
- From ICE-10 on there have been **six successful shots in a row – the design has been reliable.**
- Having achieved reliability we were able to build accurate circuit models to analyze and optimize HEPP-ICE performance
  - These models incorporate all the physics of the FCG, EFF, closing switches, AND the load (including acoustic wave interactions).
- Performance of complete experiment can now be modeled
  - Allows accurate predictions of HEPP-ICE capabilities.
  - More on this later ...

# Progress with HEPP-ICE system - 2

ICE	Seed MA	FCG MA	Veff kV	Load	Load MA	Risetime ns	P mag Mbar
4	1.90	6.90		OFHC Cu	3.00		
5	1.90	6.90	120	OFHC Cu	3.00		
6	1.92	9.14	100	OFHC Cu	3.00		
7	1.92	9.14	90	W	3.30		
8	1.90	9.00	102	OFHC Cu	3.10	1812	0.37
9	1.90	9.70	96	Brass	5.30	2074	1.09
10	<b>1.90</b>	<b>9.95</b>	<b>60</b>	<b>Brass</b>	<b>5.70</b>	<b>680</b>	<b>1.27</b>
11	<b>1.95</b>	<b>9.05</b>	<b>100</b>	<b>Brass</b>	<b>4.87</b>	<b>860</b>	<b>0.92</b>
12	<b>1.88</b>	<b>9.05</b>	<b>91</b>	<b>OFHC Cu</b>	<b>5.96</b>	<b>964</b>	<b>1.38</b>
14	<b>1.88</b>	<b>9.06</b>	<b>82</b>	<b>OFHC Cu</b>	<b>5.00</b>	<b>648</b>	<b>0.97</b>
15	<b>1.95</b>	<b>9.85</b>	<b>125</b>	<b>OFHC Cu</b>	<b>5.39</b>	<b>662</b>	<b>1.13</b>
16	<b>1.95</b>	<b>9.91</b>	<b>80</b>	<b>OFHC Cu</b>	<b>5.15</b>	<b>670</b>	<b>1.03</b>

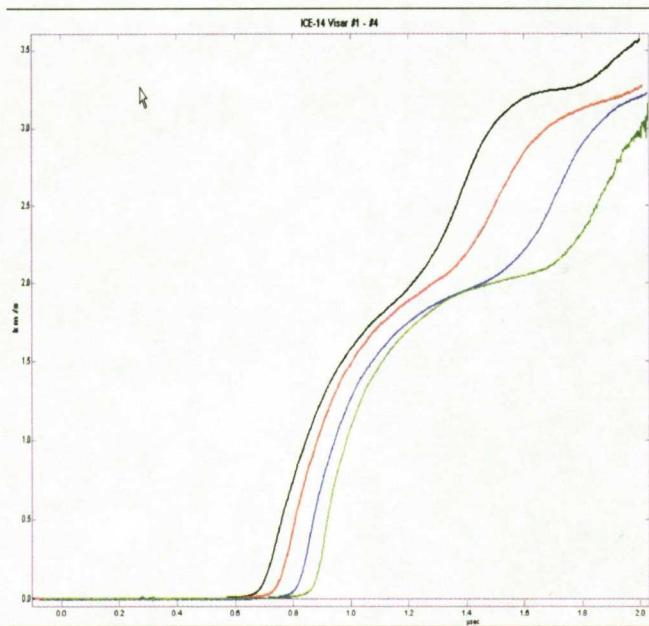
## RESULTS: For ICE-14 copper load

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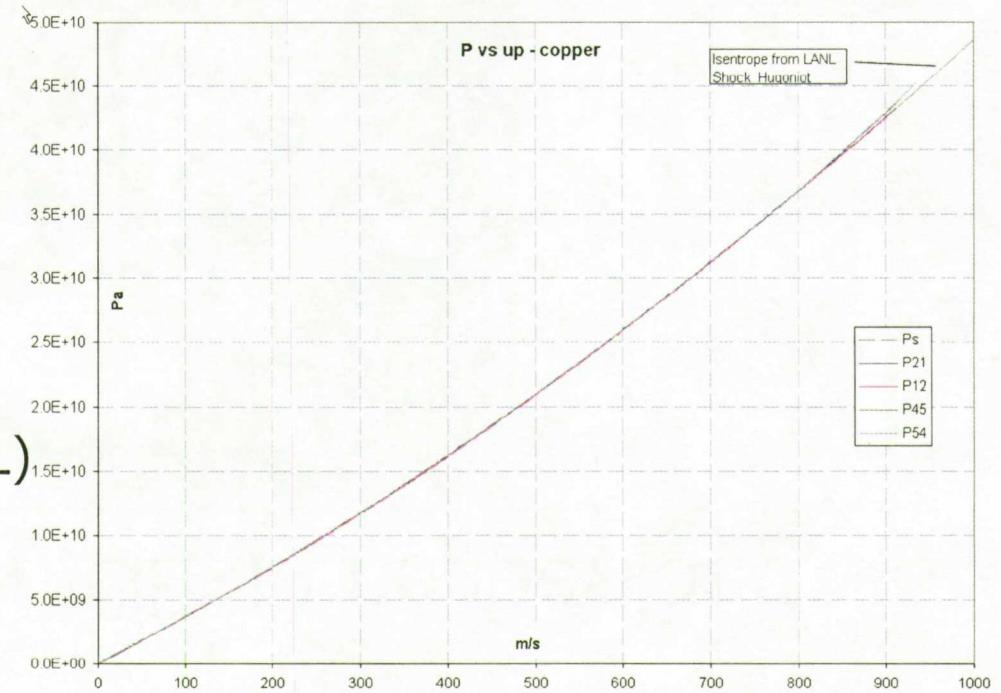


- 4 OFHC copper samples, 2 on each face with different thicknesses (1.8 – 2.5 mm thick).
- Width here 1.27 cm.

# ICE-14 Visar data and EOS results



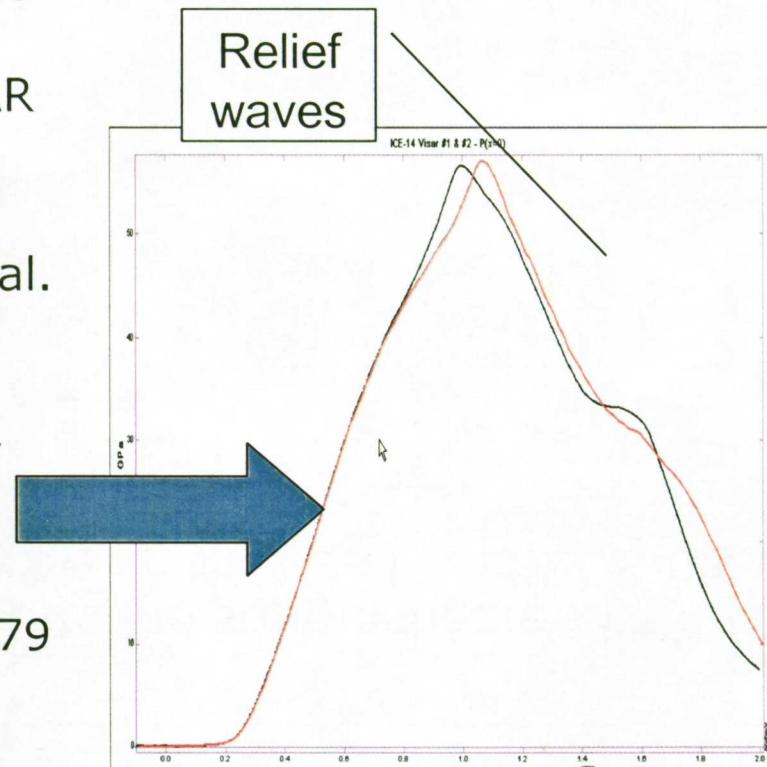
- Free surface velocities at back faces of samples 1 to 4 in OFHC copper
  - Thicknesses: 1791, 2005, 2283, 2517  $\mu\text{m}$ .



- Excellent agreement between published (LANL) EOS and ICE-14
  - Within 0.2%

# Verification of results with “Backward” calculation

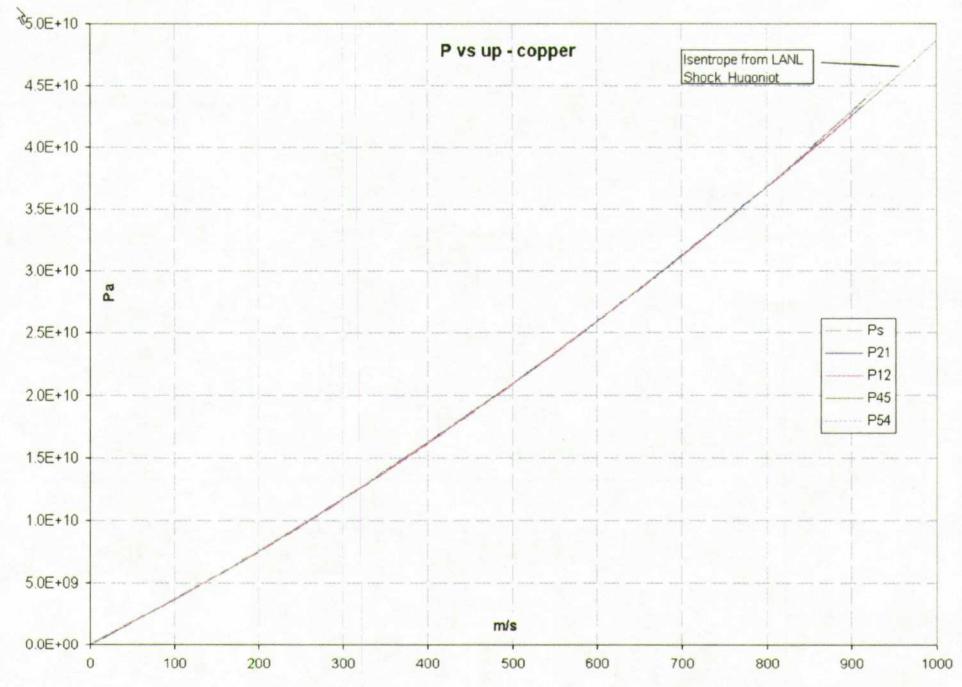
- If we have the correct EOS (and the loading is shock-free) we can calculate backwards from the VISAR surface to the magnetic drive surface.
- There the pressures should be equal.
- Stresses obtained with “Backward” and principle isentrope from published data, for OFHC copper
  - RMS deviation between samples 79 MPa, or 0.2% of 40 GPa,
  - Results indistinguishable from published data.



# Summary

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- Good data obtained. Results indistinguishable, within experimental error of  $\sim 0.2\%$ , from published EOS data for OFHC copper, up to 40 GPa.
- Further improvements are possible.

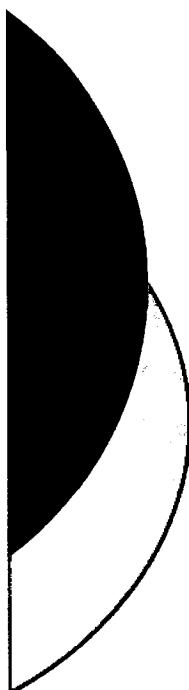




# Future work

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- This baseline system, based on a 12-MA flux compressor, is limited to ~2.5 Mbar.
- Tandem or parallel flux compression generator (FCG) modifications can extend pressure range beyond 4 Mbar.
- A scaled-up design, based on the 90-MA Ranchero FCG, will allow us to reach significantly higher pressures.



# Acknowledgements

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- We truly appreciate the invaluable assistance and support of the LANL DX-2 shock physics group who provided and fielded the VISAR diagnostics.
- We are extremely grateful to Rendell Carver (LANL X-division) for his continued encouragement, enthusiasm, and financial support.
- We are indebted to Dennis Hayes for invaluable contributions to the data analysis.