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Solid Explosive Plane-Wave  
Lenses Pressed-to-Shape with Dies



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Edited by Mable Amador, Group IRM-CAS.  
Photocomposition by Deidré A. Plumlee, Group IRM-CAS.

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**Solid Explosive Plane-Wave  
Lenses Pressed-to-Shape with Dies**

B. Olinger





# SOLID EXPLOSIVE PLANE-WAVE LENSES PRESSED-TO-SHAPE WITH DIES

by  
Bart Olinger

## ABSTRACT

Solid-explosive plane-wave lenses 1", 2" and 4½" in diameter have been mass-produced from components pressed-to-shape with aluminum dies. The method used to calculate the contour between the solid plane-wave lens components pressed-to-shape with the dies is explained. The steps taken to press, machine, and assemble the lenses are described. The method of testing the lenses, the results of those tests, and the corrections to the dies are reviewed. The work on the ½", 8", and 12" diameter lenses is also discussed.

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## INTRODUCTION

Most shock and detonation waves used in physics and engineering experiments are unidirectional and planar in order to avoid divergent effects. This is achieved by planar initiation of the explosive that generates the detonation wave. The most practical planar initiators are solid explosive plane-wave lenses because of the quality of their planar simultaneity, and that they can be manufactured in mass and stored for long periods.

## CALCULATING THE INTERFACE SURFACES

If an explosive is initiated at a point, the explosive reaction, or detonation, propagates spherically from that point. If a cone of slower detonating explosive is overlaid with a coating of faster detonating explosive so that the detonation down the surface of the cone reaches its base at the same time as the detonation down the axis of the cone, then a planar detonation wave will propagate along that axis. The length of the sides of the cone are proportional to the detonation velocity of the fast-detonating explosive,  $V_f$ , and the height of the cone is proportional to the detonation velocity of the slow-detonating explosive,  $V_s$ . This is the basic concept of the solid explosive plane-wave lens.

In Figure 1, the initiation occurs at the apex. Using cylindrical coordinates, the planar detonation front reaches a depth of  $Z_d$  for all values of the radius at the same time,  $t_d$ . The coordinates of the interface between the fast detonating explosive and the slow are  $Z_c(r)$  and  $r$ . Therefore,

$$t_d = \frac{\left[ Z_c(r)^2 + r^2 \right]^{1/2}}{V_f} + \frac{[Z_d - Z_c(r)]}{V_s}. \quad (1)$$

Solving for  $Z_c(r)$ ,

$$Z_c(r) = Z_d - \left( \frac{V_s}{V_f^2 - V_s^2} \right) \times \left( V_f^2 \times t_d - V_s \times Z_d - \left[ V_f^2 \times \left\{ Z_d^2 - 2V_s \times Z_d \times t_d + V_s^2 \times t_d^2 \right\} + r^2 \times \left\{ V_f^2 - V_s^2 \right\} \right]^{1/2} \right). \quad (2)$$

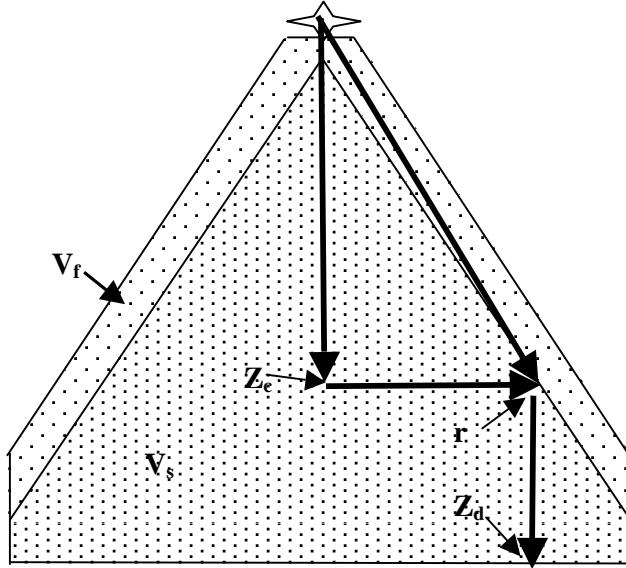


Figure 1. The initiation of the plane-wave lens is in the detonator above the explosive. The detonation front reaches  $Z_d$  by traveling through a fast detonating explosive a distance of  $(Z_c^2 + r^2)^{1/2}$  at velocity  $V_f$  and then by traveling through the slow detonating explosive a distance of  $(Z_d - Z_c)$  at velocity  $V_s$ . The total times required to reach  $Z_d$  for all values of  $r$  are the same,  $t_d$ .

The depth of the interface,  $Z_c(r)$ , is found for all values of  $r$  to the maximum  $r$  of interest. The depth or thickness of fast-detonating explosive above the slow at the apex is determined by the choices of  $Z_d$  and  $t_d$  along the axis. The aspect ratio of lens is determined by  $V_f$  and  $V_s$ .

PBX 9501 and TNT are the fast and slow detonating explosives currently used for the manufacture of plane-wave lenses. Because TNT is a single component explosive and the quality control for the production of PBX 9501 is tightly controlled, their detonation velocities depend only on their compacted densities.

$$V_f(PBX9501) = 1.88 + 3.76\rho \text{ mm/\mu s}, \quad (3)$$

$$V_s(TNT) = 1.88 + 3.76\rho \text{ mm/\mu s}. \quad (4)$$

The standard densities for pressed PBX 9501 and TNT are  $1.83 \text{ g/cm}^3$  ( $8.76 \text{ mm/\mu s}$ ) and  $1.64 \text{ g/cm}^3$  ( $6.94 \text{ mm/\mu s}$ ), respectively. The detonator currently used for plane-wave lens production is the SE-1, or the commercially available RP-1. This detonator has an apparent center-of-initiation 7.2 mm above its face when the detonation wave is measured at some depth

in PBX 9501. Because the face of the detonator is usually set 10 mm above the slow detonating component apex on the fast in order to smooth out detonation wave irregularities caused by the detonator, the value of  $Z_c(r = 0)$  becomes 17.2 mm.

## PRESSING, MACHINING, AND ASSEMBLY

The steel-die press cylindrical diameters available are 1", 1 $\frac{5}{8}$ ", 2", 2 $\frac{1}{2}$ ", and 3" (Savage press), and 4 $\frac{1}{4}$ ", 6", 8", 10", and 12" (Accudyne press). We selected the 4 $\frac{1}{4}$ " diameter for the initial lens. Dies were machined based on the contours calculated using equation 2 above, the components pressed and assembled, and the lens was tested for simultaneity. (PowerPoint presentation, about Sept. 2005, titled Planarity Measurements of Pressed, High-Explosive Lenses, by Russ Olson, et al.) Based on those results the 4 $\frac{1}{4}$ " diameter lens dies were corrected and 1", 2", and 4 $\frac{1}{4}$ " diameter lens dies were machined based on that correction. The tests of the lenses made with these dies and their corrections are now discussed.

The dies consist of convex and concave mandrels machined from 7075 aluminum. The explosive TNT components are pressed using flaked TNT, heated to 65°C, and compacted at 5,000 psi for 5 min., using the concave mandrel. The concave surface is the contour between the faster and slower detonating explosives first calculated and then corrected. The PBX 9501 components were pressed from the stock of PBX 9501 maintained at the Laboratory, heated to 90°C, and compacted twice at 20,000 psi for 5 min. with a brief rest between using the convex mandrel. The concave and convex surfaces have the same contour, line-to-line. Those contours used for the 1", 2" and 4 $\frac{1}{4}$ " lenses are listed in the "Old" column in the table at the end of this report. The outer conical surface of the PBX 9501 is formed at the same time with a second concave mandrel used with the convex mandrel.

Next, the pressed TNT components' faces are machined flat and perpendicular to their axes using pot chucks machined to match the TNT components contoured surfaces. The components are also machined to specified heights. Those heights are measured and recorded.

The next step is to bond the PBX 9501 and TNT components together. The contour surfaces are first cleaned with isopropyl alcohol. The PBX 9501 components are then inverted and set in cardboard tube pedestals. Their concave contoured surfaces are thinly painted with Aralhex adhesive. The TNT components' convex contoured surfaces are inserted into the PBX 9501 components. Padded weights are placed on the TNT faces until the adhesive sets, after 12 hours. The weights used are 250 g, 1 kg, and 4 kg Cu cylinders for the 1", 2", and 4 $\frac{1}{4}$ " diameter lenses.

The final step is to machine a surface flat-and-parallel to the TNT face 1 cm above the apex of the slow component whose height was recorded. This surface is for mounting a detonator locator using Aralhex adhesive. The locator must be precisely centered on the lenses' axes. Diagrams of the three assembled lenses are attached.

## TESTING AND CORRECTING

Lenses are tested at Chamber 8, TA-40, DE-9. The 1", 2" and 4 $\frac{1}{4}$ " lenses were bonded to plate glass with 3-mil shim stock sandwiched between. The air gap flashes when the detonation wave arrives at the surface of the lens. A set of slits are placed across the image of the explosive lens face and a Cordin camera sweeps that slit image over the recording film at 12 mm/ $\mu$ s.

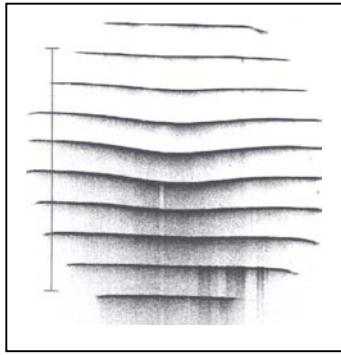


Figure 2. Slit image of a 1" lens. Scale on the left is 12 mm.

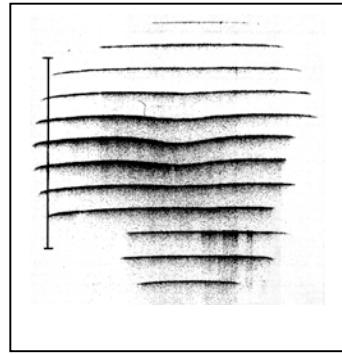


Figure 3. Slit image of a 2" lens. Scale on the left is 12 mm.

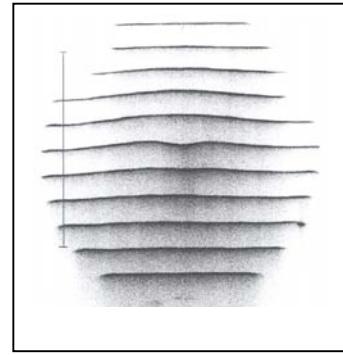


Figure 4. Slit image of a 4 1/4" lens. Scale on the left is 12 mm.

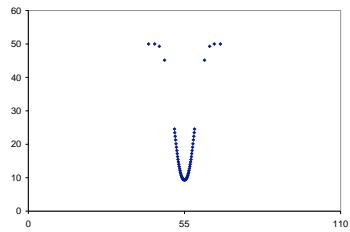


Figure 5. Time of arrival of the detonation wave for the 1" lens. The vertical scale is ns, the horizontal is mm.

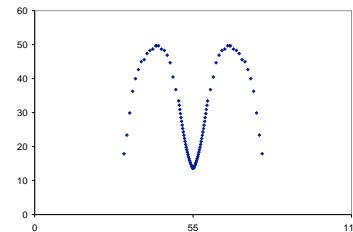


Figure 6. Time of arrival of the detonation wave for the 2" lens. The vertical scale is ns, the horizontal is mm.

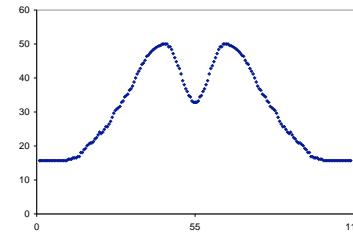


Figure 7. Time of arrival of the detonation wave for the 4 1/4" lens. The vertical scale is ns, the horizontal is mm.

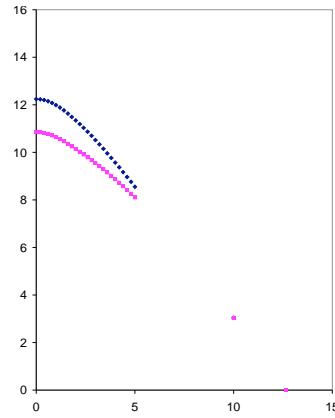


Figure 8. Contour for 1" explosive lens dies. Dark blue is the original contour, pink is the corrected. The vertical axis is the axis of the contour in mm; the horizontal is the contour radius in mm.

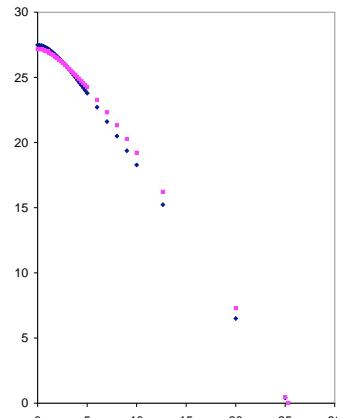


Figure 9. Contour for 2" explosive lens dies. Dark blue is the original contour, pink is the corrected. The vertical axis is the axis of the contour in mm; the horizontal is the contour radius in mm.

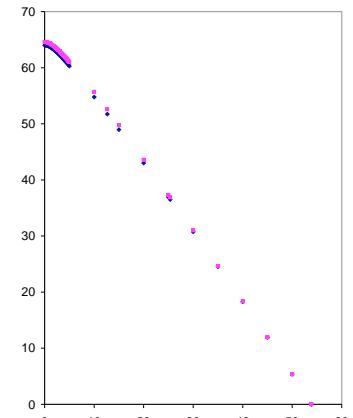


Figure 10. Contour for 4 1/4" explosive lens dies. Dark blue is the original contour, pink is the corrected. The vertical axis is the axis of the contour in mm; the horizontal is the contour radius in mm.

Figures 2, 3, and 4 are the slit images from a 1", 2" and 4¼" lenses. Two lenses of each size were tested and they were reproducible. Group DE-9 normally analyzes the slit images, but at this time they are developing new software and training a new analyzer. While waiting for their analyses, I blew-up the film images with a microfiche printer and read the central lines with an eye-loupe with an internal scale. During the shot setup, no effort was made to place the central slit on the diameter; therefore, the results are not the true maxima.

In Figures 5, 6, and 7 are plotted the times of arrival of the detonation fronts as a function of the diameter position centered at 55 mm. The initial arrivals are plotted at 50 ns. All three lens sizes were based on the same contour, for the 4¼" lens, therefore, the deviations display the same pattern. The first arrival for all three lens sizes occurs at a radius of about ½" or 12.7 mm. The center of the lens lags behind the first arrival by 40 ns (1"), 37 ns (2"), and 17 ns (4¼"). These data are the deviations from simultaneity,  $\Delta t_d$ , as a function of the radius,  $r$ , of the lenses.

Differentiating  $Z_c(r)$  with respect to  $t_d$  in Equation 2, deviations from the interface that will create a simultaneous detonation wave as a function of the radius can be calculated,

$$\Delta Z_c(r) = \Delta t_d(r) \div \left[ \frac{1}{V_f} \times \left\{ \frac{Z_c(r)}{\left[ Z_c(r)^2 + r^2 \right]^{1/2}} \right\} - \frac{1}{V_s} \right]. \quad (5)$$

These deviations are now used to adjust the interface for the final lens design. Figures 8, 9, and 10 show the corrected contours. The corrected contours are listed in the "New" column in the table below.

### THE ½", 8", AND 12" DIAMETER LENSES

Dies for a 1" diameter lenses initiated with RP-3 detonators (the P-25B drawings) were also made. The lenses have 2 mm, rather than 10 mm, of PBX 9501 between the detonator platform and the top of the slow component. Lens components made from these dies were pressed and assembled. The detonator locator for the RP-3 was then attached. The lenses were then reduced in height to 0.45" and in diameter to 0.75", producing a ½" diameter lens. This lens is to be test-fired at Chamber 8.

The 8"-diameter dies were used to press PBX 9501 and TNT components. The TNT components cracked parallel to the flat base. The problem appears to be that the pressure used was too high. Before we could press additional components at lower pressure, the HE pressing facility was closed. The new press, the Accudyne, will begin operation in early 2008. Attempts at pressing the 12" components were postponed until successful 8" components were produced.

### DRAWINGS

Engineering drawings of the dies, the pot chucks, and the finished lenses, both tested and not yet tested, are appended to this report.

## **ACKNOWLEDGEMENTS**

Tim Cash, PF-TDI, LANL, created the engineering drawings of the dies and pot chucks. Steve Rivera created the engineering drawings of the lenses. John Morris, Larry, Vaughan, and Bob Meir set up and fired the lens tests with the Cordin sweep camera at the enclosed firing chamber of DE-9, LANL. They were mentored by Larry Hill of the same group. This research is funded by the HE Science Project led by Dan Hooks, DE-9, under LANL's NNSA Campaign 2 Dynamic Materials Properties Program, David J. Funk, DE-DO, Program Manager.

## Old and New Contours of the Dies for the 1", 2" and 4¼" Lenses

1" lens			2" Lens			4¼" Lens		
Old	New		Old	New		Old	New	
X	X	Y	X	X	Y	X	X	Y
mm	mm	mm	mm	mm	mm	mm	mm	mm
12.245	10.852	0.000	27.486	27.163	0.000	63.985	64.569	0.000
12.234	10.841	0.200	27.475	27.163	0.200	63.974	64.561	0.200
12.203	10.814	0.400	27.444	27.146	0.400	63.943	64.534	0.400
12.151	10.770	0.600	27.392	27.110	0.600	63.891	64.485	0.600
12.079	10.711	0.800	27.320	27.056	0.800	63.819	64.418	0.800
11.991	10.640	1.000	27.232	26.988	1.000	63.731	64.334	1.000
11.886	10.556	1.200	27.127	26.905	1.200	63.626	64.235	1.200
11.767	10.462	1.400	27.008	26.809	1.400	63.507	64.121	1.400
11.635	10.359	1.600	26.876	26.703	1.600	63.375	63.995	1.600
11.492	10.248	1.800	26.733	26.587	1.800	63.232	63.859	1.800
11.344	10.137	2.000	26.585	26.468	2.000	63.084	63.718	2.000
11.194	10.027	2.200	26.435	26.348	2.200	62.934	63.575	2.200
11.035	9.911	2.400	26.276	26.220	2.400	62.775	63.424	2.400
10.870	9.793	2.600	26.111	26.088	2.600	62.610	63.267	2.600
10.698	9.671	2.800	25.939	25.950	2.800	62.438	63.104	2.800
10.520	9.547	3.000	25.761	25.807	3.000	62.260	62.935	3.000
10.338	9.421	3.200	25.579	25.662	3.200	62.078	62.763	3.200
10.152	9.295	3.400	25.393	25.513	3.400	61.892	62.587	3.400
9.961	9.155	3.600	25.202	25.360	3.600	61.701	62.407	3.600
9.768	9.016	3.800	25.009	25.207	3.800	61.508	62.225	3.800
9.571	8.872	4.000	24.812	25.050	4.000	61.311	62.040	4.000
9.372	8.726	4.200	24.613	24.892	4.200	61.112	61.853	4.200
9.170	8.574	4.400	24.411	24.732	4.400	60.910	61.664	4.400
8.966	8.420	4.600	24.207	24.571	4.600	60.706	61.473	4.600
8.761	8.262	4.800	24.002	24.410	4.800	60.501	61.282	4.800
8.553	8.099	5.000	23.794	24.246	5.000	60.293	61.088	5.000
3.043	3.031	10.000	22.715	23.288	6.000	54.783	55.710	10.000
0.000	0.000	12.650	21.608	22.306	7.000	51.730	52.604	12.650
			20.494	21.325	8.000	48.976	49.779	15.000
			19.372	20.273	9.000	43.002	43.602	20.000
			18.284	19.230	10.000	36.911	37.313	25.000
			15.231	16.226	12.650	36.499	36.889	25.336
			6.503	7.288	20.000	30.747	30.990	30.000
			0.412	0.476	25.000	24.540	24.678	35.000
			0.000	0.000	25.336	18.287	18.333	40.000
						11.936	11.944	45.000
						5.361	5.361	50.000
						0.000	0.000	53.885

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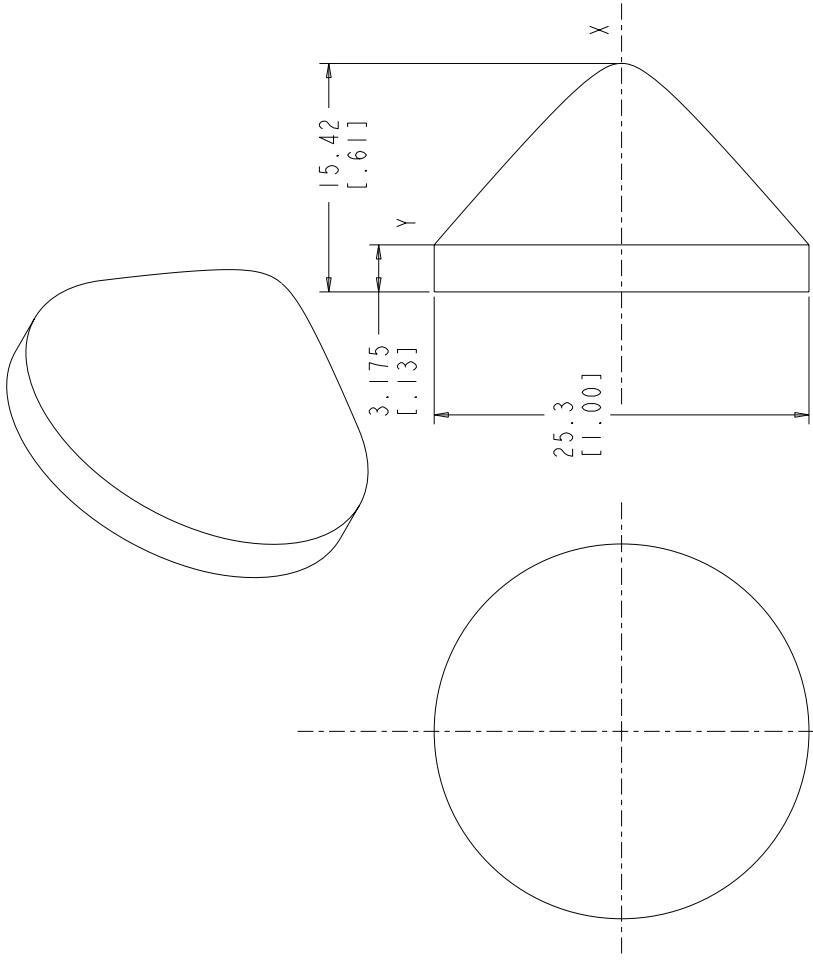
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PART NUMBER		REVISIONS			
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NA 9300000					
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Los Alamos					
National Laboratory					
METRIC		UNCLASSIFIED			
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CHECKED:	DATE	DRAWING NUMBER			
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APPROVED:	APPROVING	5056 Lens Mandrel			
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LA - CKW -					

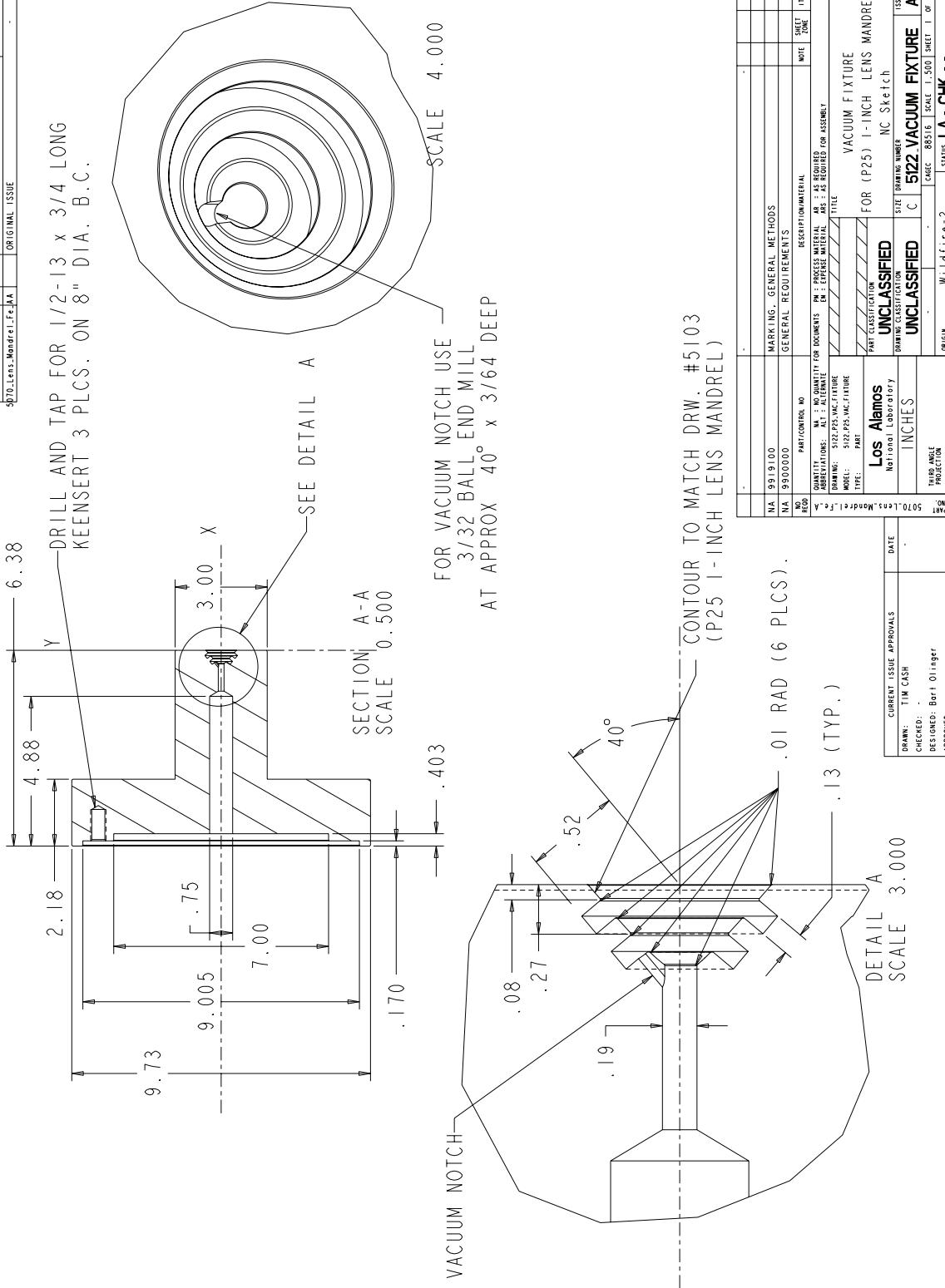
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PTS-P25-VACFIX-#5122

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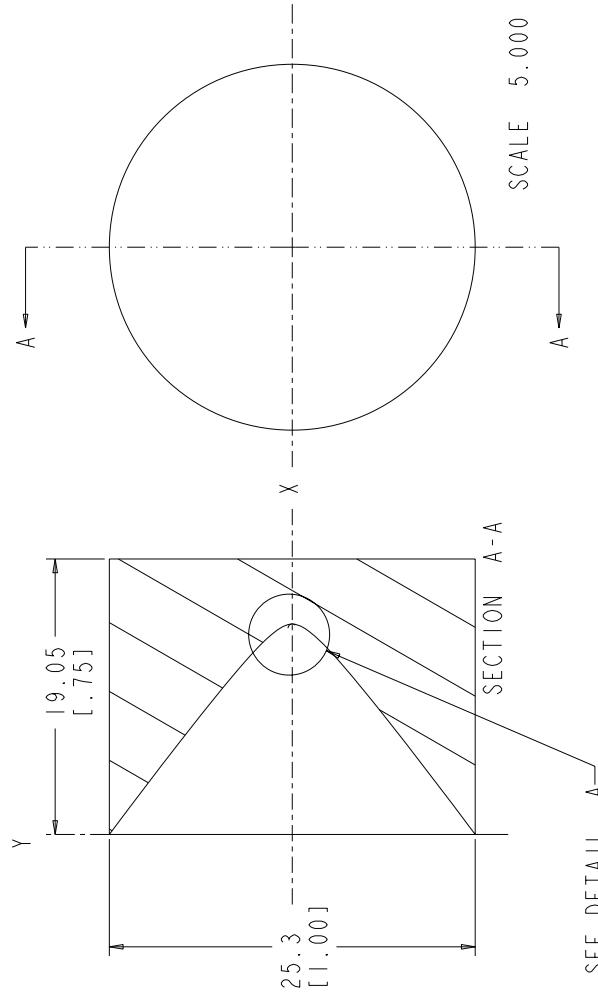
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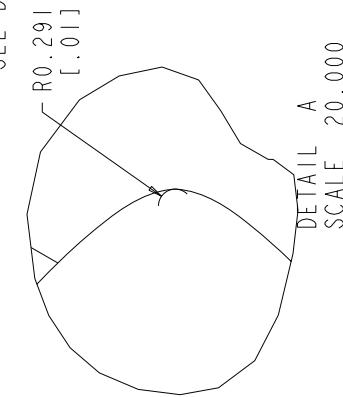
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SEE DETAIL

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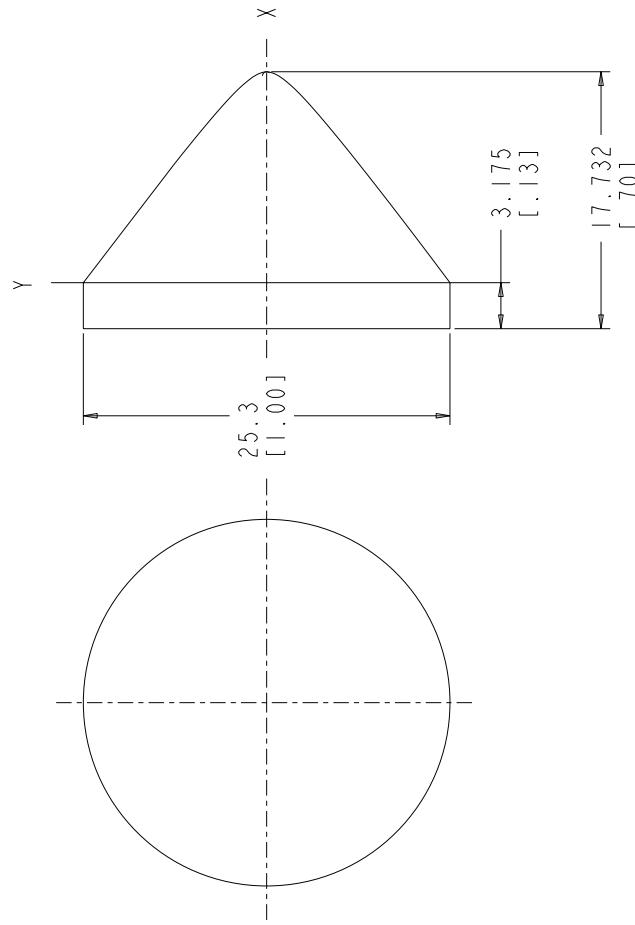
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13.92235	1.299948	0
13.81208	1.441836	0
13.69334	1.583646	0
13.56194	1.725098	0
13.43812	1.866312	0
13.30312	2.007249	0
13.16369	2.147949	0
13.0213	2.288489	0
12.81596	2.428871	0
12.72693	2.569055	0
12.51641	2.0916	0
12.42295	2.849106	0
12.268	2.988972	0
12.11084	3.12872	0
11.9522	3.268389	0
11.79382	3.408018	0
11.63123	3.547527	0
11.362366	7.022987	0
5.001832	8.859721	0
2.874085	10.48667	0
0	12.65	0



REVISI0NS			
PART NUMBER	ISS	SHEET ZONE	DESCRIPTION
5070-Lens, Mandrel, F-6, A		ORIGINAL ISSUE	

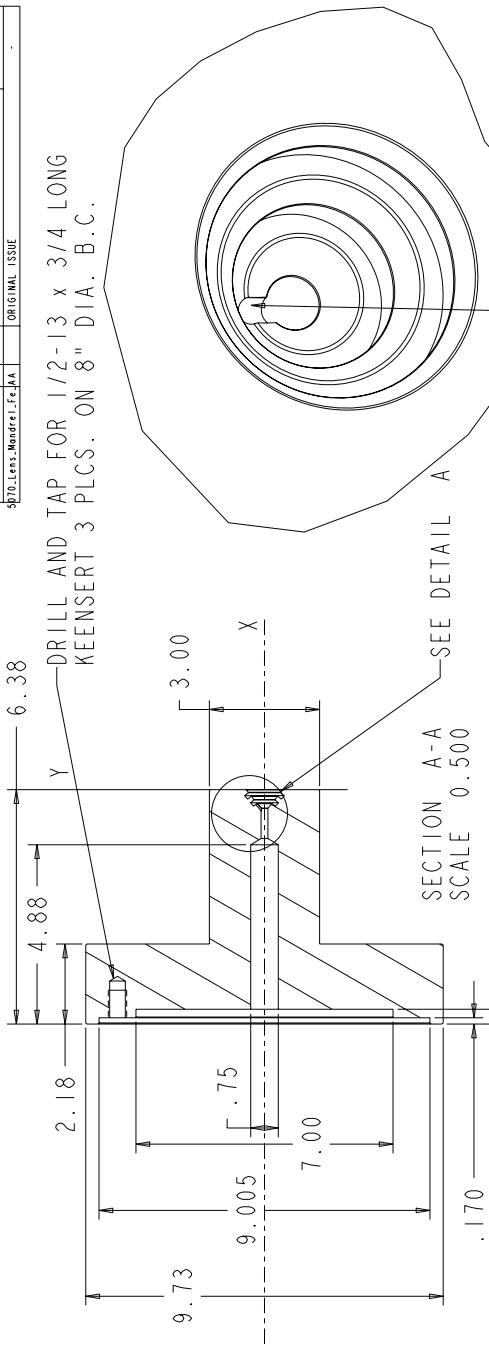
GENERAL REQUIREMENTS			
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GENERAL REQUIREMENTS			
ITEM	NOTE	ITEM	NOTE
1		2	
3		4	
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61		62</td	

UNCLASSIFIED

UNCLASSIFIED

PART NUMBER	155	REVISIONS	
		Sheet Zone	DESCRIPTION
SD-70-Lens-Mondrel-Set A		ORIGINAL	ISSUE
			-



DRILL AND TAP FOR 1/2-13 x 3/4 LONG  
KEESENSERT 3 PLCS. ON 8" DIA. B.C.

FOR VACUUM NOTCH USE  
3/32 BALL END MILL  
AT APPROX 40° x 3/64 DEEP  
SCALE 4.000

DETAIL A  
SCALE 4,000

UNCLASSIFIED

PTS-P25B-VACFIX-#5123

UNCLASSIFIED

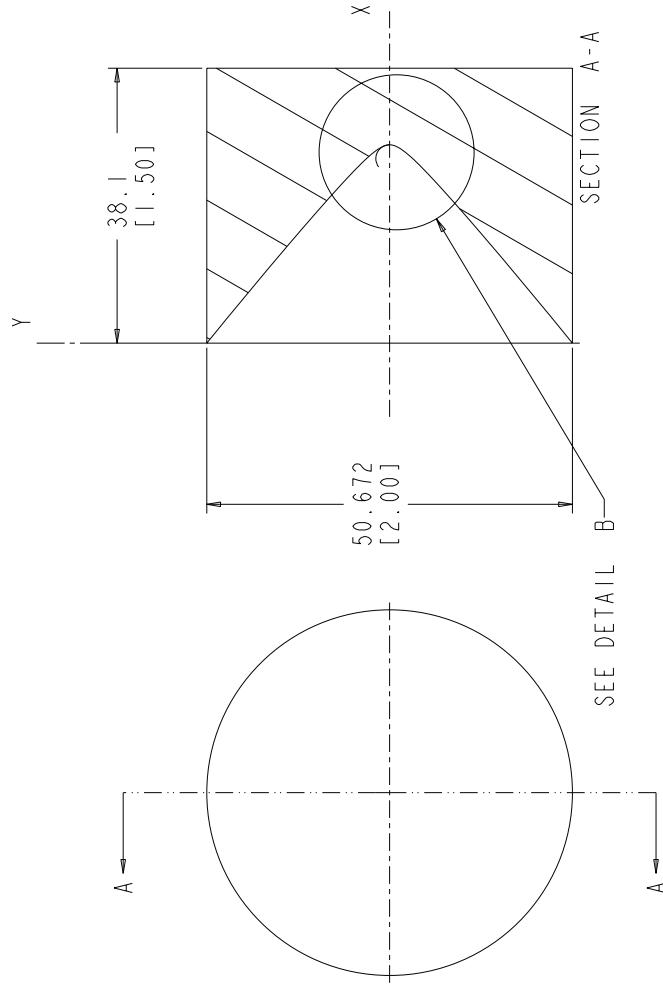
Coordinates of spline points:

CARTESIAN COORDINATES:

UNCLASSIFIED

Coordinates of spline points:

## CARTESIAN COORDINATES:



PTS-P50-CONCAVE-#5072

UNCLASSIFIED

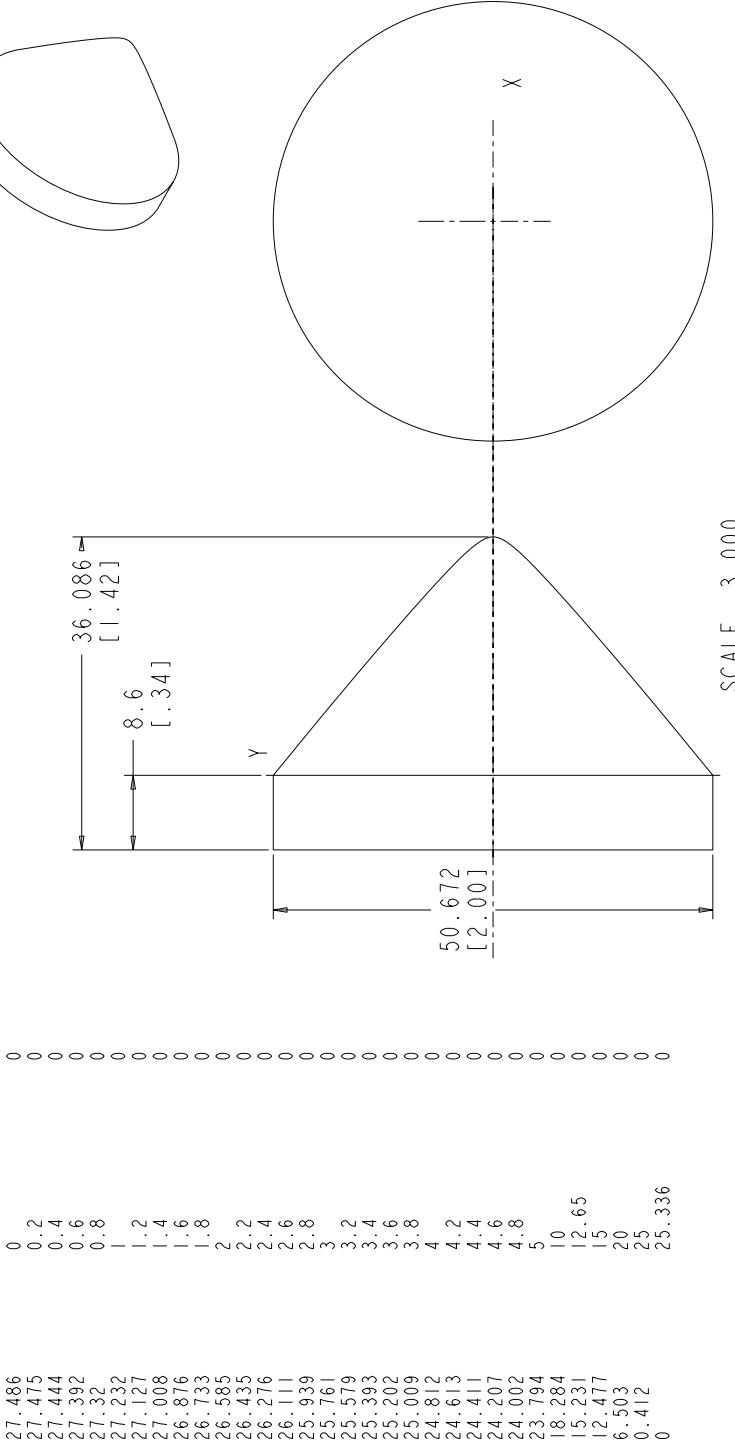
UNCLASSIFIED

Coordinates of spline points:

CARTESIAN COORDINATES:

×

7 Y



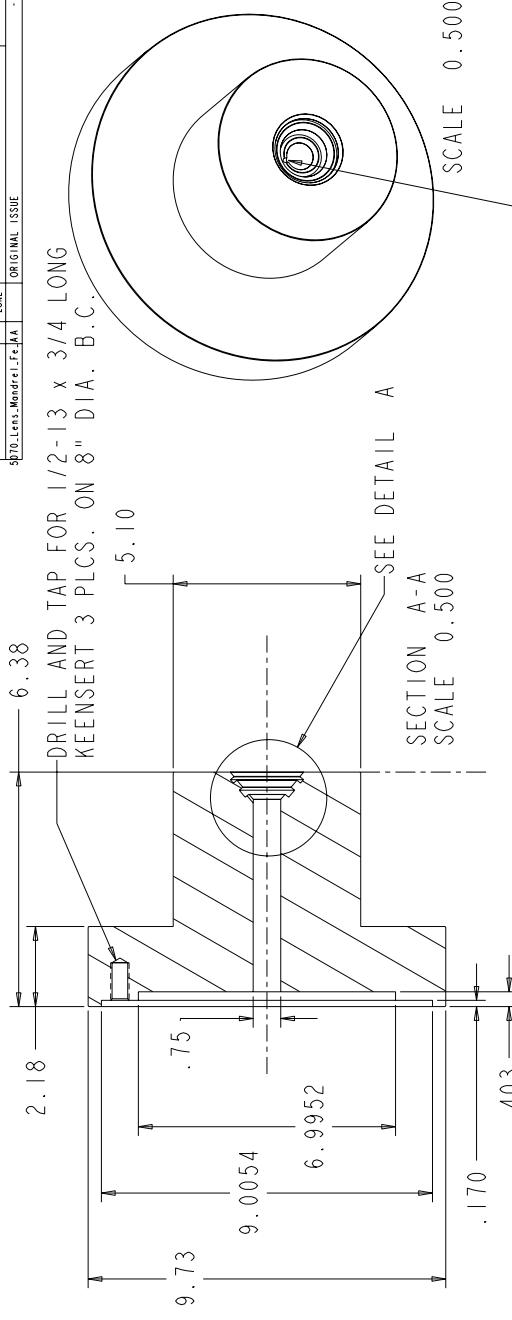
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UNCLASSIFIED

UNCLASSIFIED

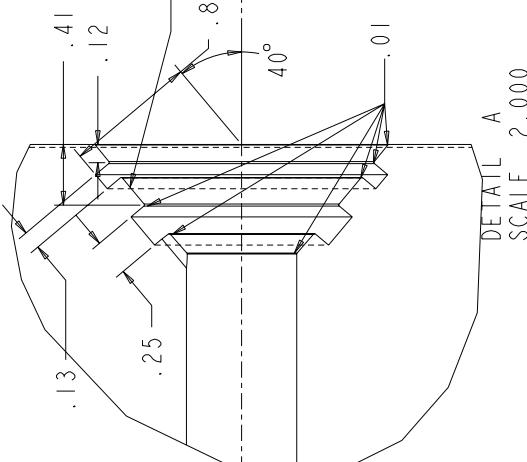
UNCLASSIFIED

PART NUMBER	ISS	REVISIONS		DATE
		SHEET ZONE	DESCRIPTION	
070-Lens-Molded-Fc-AA			ORIGINAL ISSUE	-



FOR VACUUM NOTCH USE -  
1/8 BALL END MILL  
AT APPROX 40° X 1/16 DEEP

- CONTOUR TO MATCH DRW. #5072  
(2 INCH P50 LENS MANDREL)



UNCLASSIFIED

UNCLASSIFIED

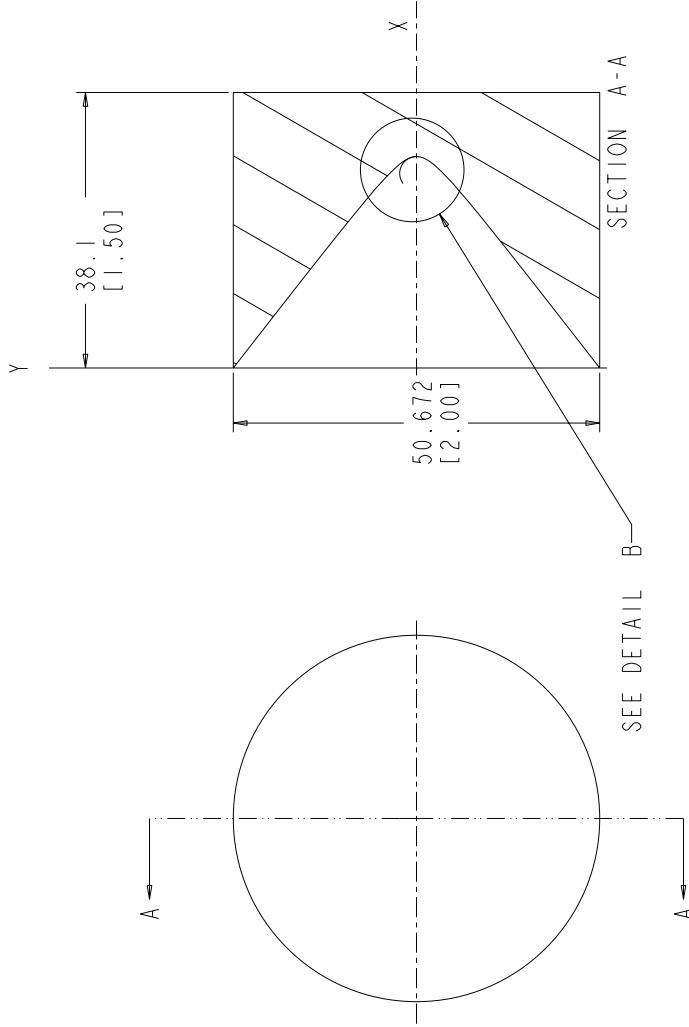
PTS-P50-VACFIX-#5124

UNCLASSIFIED

Coordinates of spline points:

CARTESIAN COORDINATES:

X	Y	Z
29.239	0	0
29.23	0.2	0
29.204	0.4	0
29.16	0.6	0
29.1	0.8	0
29.024	-1	0
28.933	1.2	0
28.829	1.4	0
28.711	1.6	0
28.581	1.8	0
28.44	2	0
28.289	2.2	0
28.129	2.4	0
27.961	2.6	0
27.786	2.8	0
27.604	3	0
27.416	3.2	0
27.222	3.4	0
27.023	3.6	0
26.82	3.8	0
26.613	4	0
26.403	4.2	0
26.189	4.4	0
25.972	4.6	0
25.752	4.8	0
25.53	5	0
19.539	10	0
13.24	15	0
6.854	20	0
0.432	25	0
0	25.336	0

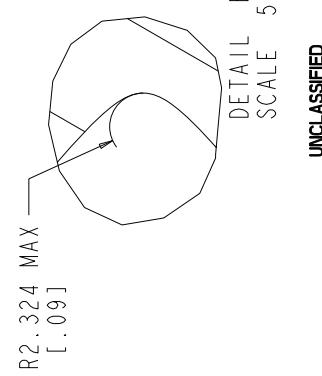


UNCLASSIFIED

PART NUMBER		REVISONS		DATE	
5010 Lens, Mandrel, Fe. A		ISS	SHEET	DESCRIPTION	ORIGINAL ISSUE

PTS-P50B-CONCAVE-#5105

PART CLASSIFICATION		DRAWING CLASSIFICATION		DRAWING NUMBER		NOTE	
UNCLASSIFIED	UNCLASSIFIED	UNCLASSIFIED	UNCLASSIFIED	P50B	(2 INCH) LENS	ITEM	
Los Alamos	Los Alamos	Los Alamos	Los Alamos	5105 Lens, Mandrel, Fe. A	5105 Lens, Mandrel, Fe. A	AS DRAWN	
NO. 100	NO. 100	NO. 100	NO. 100	5105 P50B FEMALE	5105 P50B FEMALE	AS DRAWN	
4.00	4.00	4.00	4.00	AS DRAWN:	AS DRAWN:	AS DRAWN:	
ABREVIATIONS: AY : AS DRAWN							
TYPE: PART							
5105 P50B FEMALE							
APPROVED: -							
DATE: -							
DRAWN: TIM CASH							
CHECKED: -							
DESIGNED: Gary Olinger							
APPROVED: -							



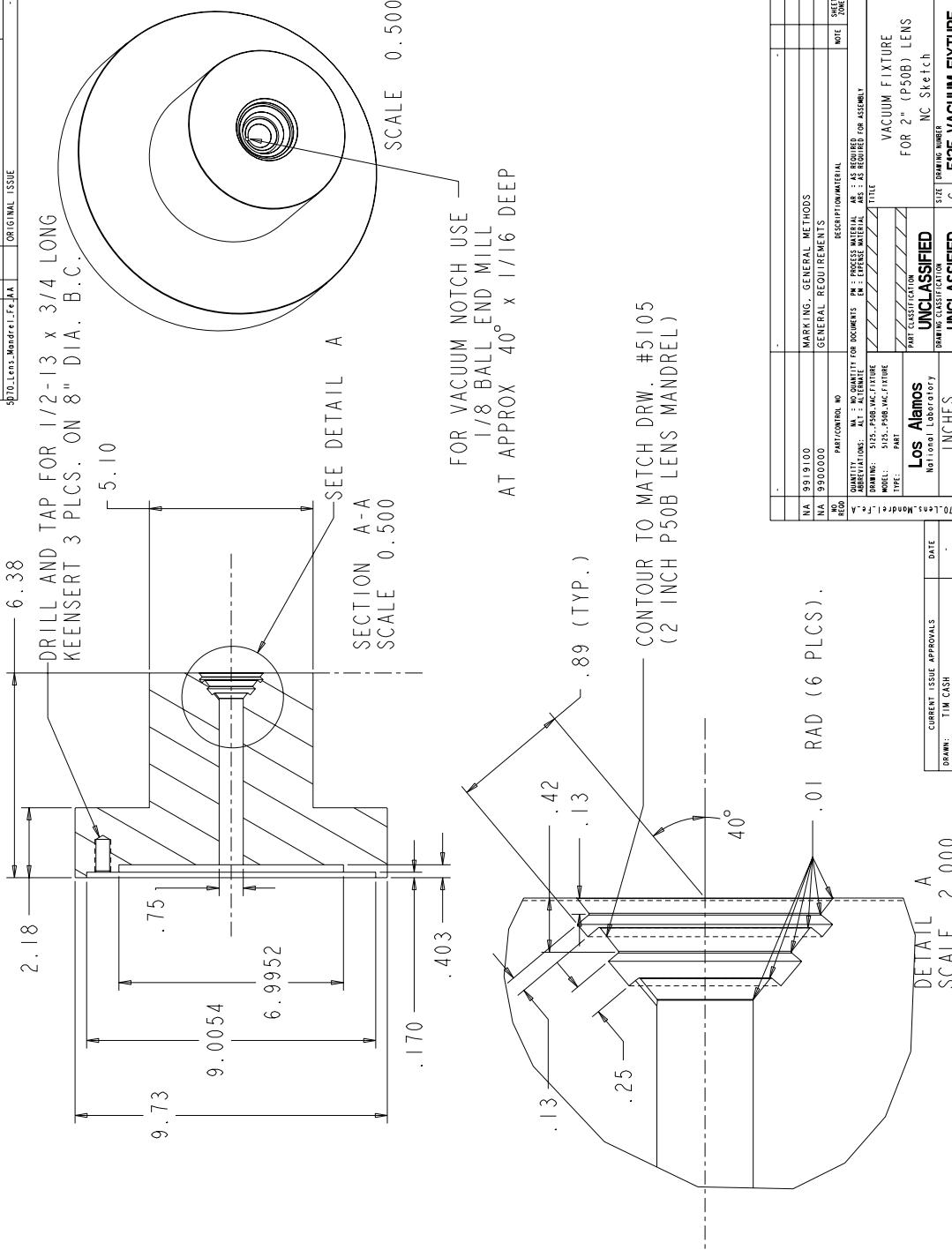
UNCLASSIFIED



UNCLASSIFIED

UNCLASSIFIED

PART NUMBER	ISS	REVISIONS	
		SHEET ZONE	DESCRIPTION
505010-Lens, Mandrel, Fe, AA			ORIGINAL ISSUE



UNCLASSIFIED

UNCLASSIFIED

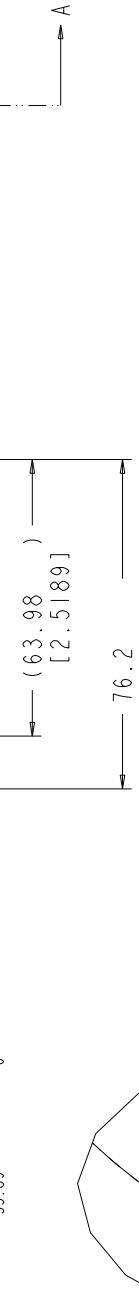
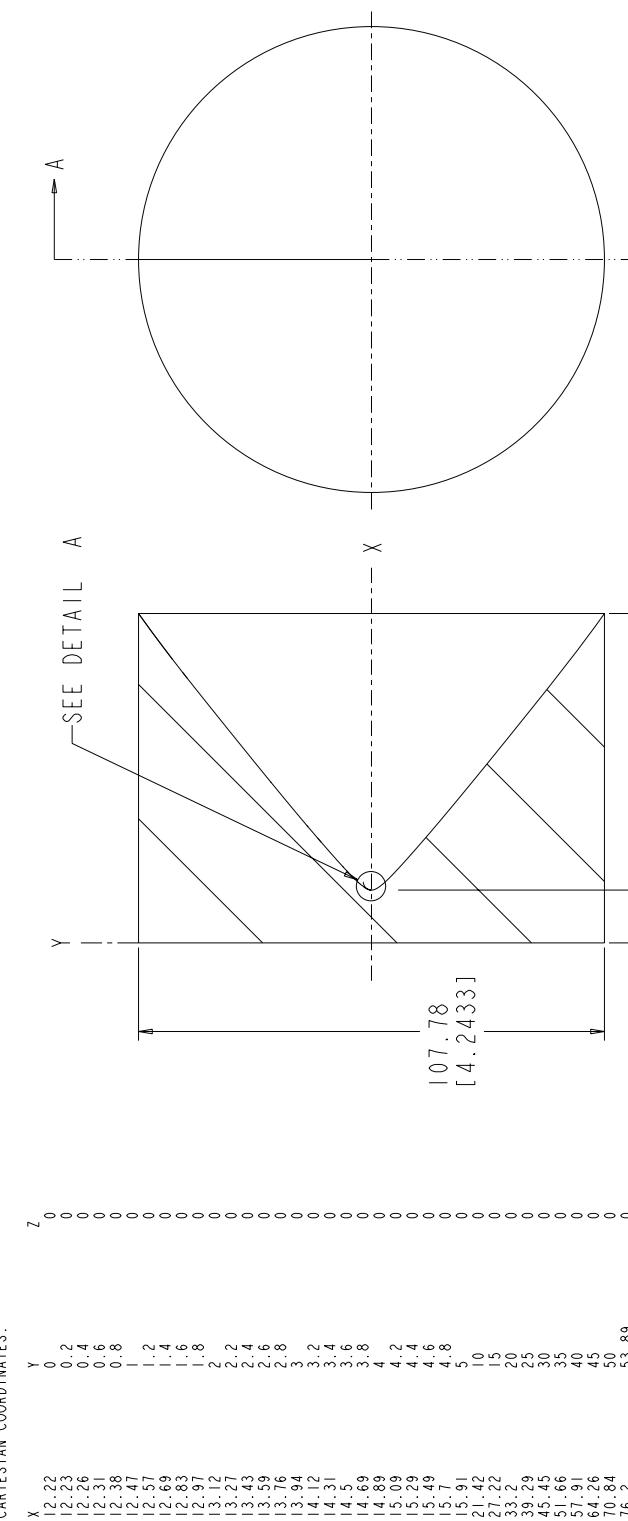
PTS-P50B-VACFIX-#5125

UNCLASSIFIED

UNCLASSIFIED

Coordinates of spline points:

CARTESIAN COORDINATES:



PART NUMBER		REVISONS	
ISSUE	STL	ZONE	DESCRIPTION
5070.Lens, Mandrel, Fe, A	1	ORIGINAL ISSUE	DATE
-			
-			

GENERAL REQUIREMENTS		DESCRIPTION MATERIAL	
ITEM	NOTE	ITEM	NOTE
NA 9919100	MARKING, GENERAL METHODS	NA	
NA 9900000	GENERAL REQUIREMENTS	NA	
NO. 1020	PART/CONTROL NO.	NA	
ABRASION:	NA : AS PERMANENT	NA : AS PERMANENT	
ABRASION:	NA : AS PERMANENT	NA : AS PERMANENT	
DRAWING:	5070.Lens, Mandrel, Fe, A	4.25 inch Lens Mandrel	4.25 inch Lens Mandrel
MODEL:	5070.Lens, Mandrel, Fe, A	Female A	Female A
TYPE:	NC Sketch	NC Sketch	NC Sketch

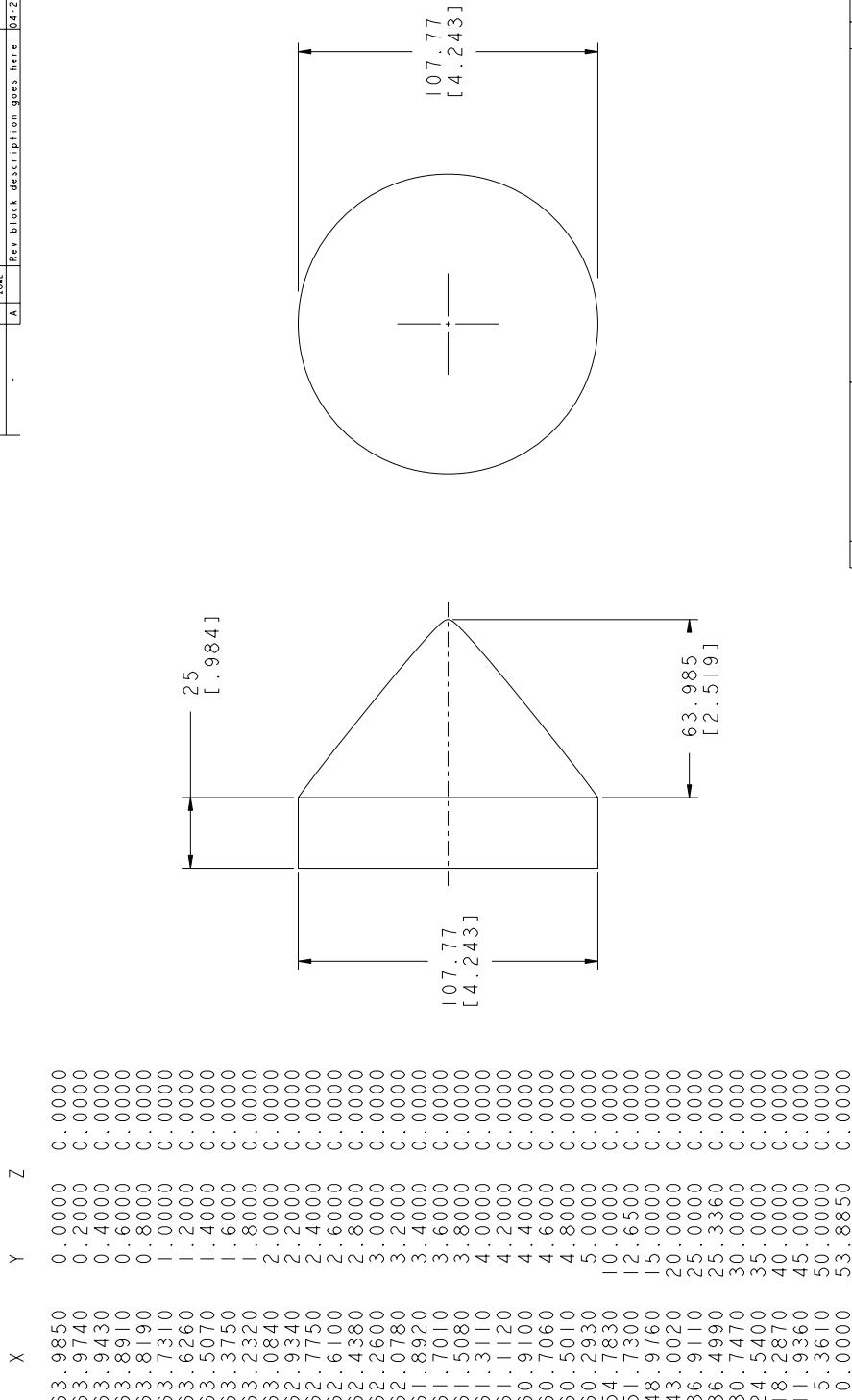
PART CLASSIFICATION		DRAWING NUMBER	
ITEM	NOTE	ITEM	NOTE
Los Alamos	UNCLASSIFIED	5070.Lens, Mandrel, Fe, A	5070.Lens, Mandrel, Fe, A
National Laboratory	UNCLASSIFIED	5070.Lens, Mandrel, Fe, A	5070.Lens, Mandrel, Fe, A
DRAWN:	Jacob Talyor	DATE	DATE
CHECKED:	-	APPROVED:	-
DESIGNED:	Burt Oliver	APPROVED:	-
APPROVED:	-	APPROVED:	-

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

PART NUMBER	REVISIONS		
	ISS	SHEET ZONE	DESCRIPTION
-	A	Rev block	description goes here



NA	99191000	MARKING GENERAL METHODS					
NA	99000000	GENERAL REQUIREMENTS					
NO		PART/CONTROL NO					
REF ID:		DESCRIPTION/MATERIAL					
QUANTITY	NA	NO QUANTITY	ART	AS REQUIRED	NOTE	ITEM	
ABBR/ATIONS:	NA	ALL	PI	PROCESS MATERIAL	ZONE		
		EM	EM	EXPENSE MATERIAL			
DRAWING:	0571	EM	EM	ART	AS REQUIRED	FOR ASSEMBLY	
MODEL:	0571						
TYPE:	(PART)						
		PART CLASSIFICATION					
		UNCLASSIFIED					
		DRAWING CLASSIFICATION					
		UNCLASSIFIED					
SI	METRIC	SIZE	DRAWING NUMBER			ISSUE	
		C	5071-LENS MANDREL A				
		SCALE	1/1				
		DATE	04-26-2000				
THREE ANGLE	PRO/E WILDFIRE	STATUS	-				
ROT. NO.	PART	ITEM	-				

CONFIRMED TO BE UNCLASSIFIED  
CLASSIFIER: -  
TITLER: -  
ORG: -

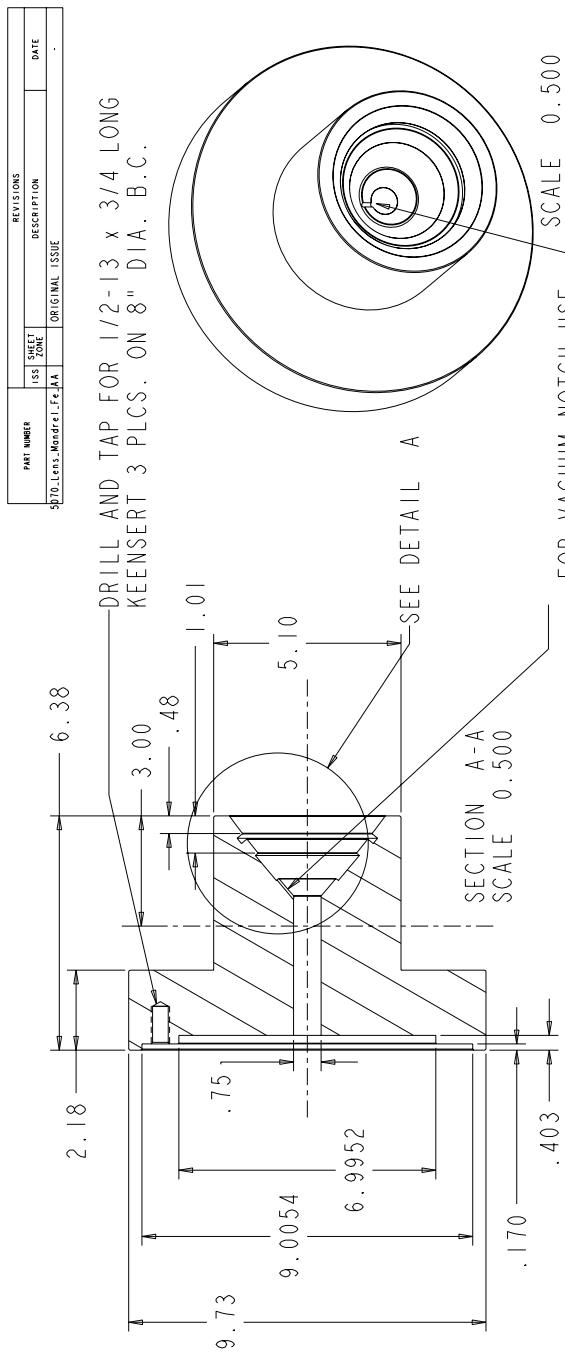
NEXT ASY:	FINAL ASY:
PROJECT NAME:	DRAWING LEVEL:
UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN MILLIMETERS.	
DECIMALS	ANGULAR $\pm$ 0.5°
XX	0.76
XX	0.754
XX	0.254
XX	32

LAW

PTS-P108-CONVEX-#5071

UNCLASSIFIED

UNCLASSIFIED



DRILL AND TAP FOR 1/2"-13 X 3/4" LONG  
KEENERT 3 PLCS. ON 8" DIA. B.C.

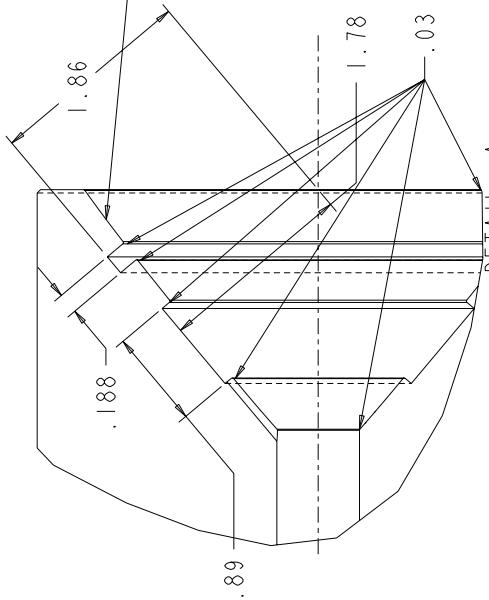
SEE DETAIL A

SECTION A-A  
SCALE 0.500

FOR VACUUM NOTCH USE  
1/8 BALL END MILL  
AT APPROX 40° x 1/16 DEEP

SEE DETAIL A  
SCALE 0.500

CONTOUR TO MATCH DRW. #5070  
(4.25 inch Lens Mandrel 1)



DETAIL A  
SCALE 1.500

SECTION A-A  
SCALE 1.500

SECTION A-A  
SCALE 1.500

PART CLASSIFICATION		DRAWING CLASSIFICATION		DRAWING NUMBER		ITEM	
UNCLASSIFIED		UNCLASSIFIED		5070-1.500		-	
DRAWN BY: TIM CASH		CHECKED:		DESIGNED: Gary Olinger		APPROVED:	
DATE: -		DATE: -		DATE: -		DATE: -	
REV: 0		REV: 0		REV: 0		REV: 0	

UNCLASSIFIED

UNCLASSIFIED

PART CLASSIFICATION		DRAWING CLASSIFICATION		DRAWING NUMBER		ITEM	
UNCLASSIFIED		UNCLASSIFIED		5070-1.500		-	
DRAWN BY: NC		CHECKED: NC		DESIGNED: NC		APPROVED: NC	
DATE: -		DATE: -		DATE: -		DATE: -	
REV: 0		REV: 0		REV: 0		REV: 0	

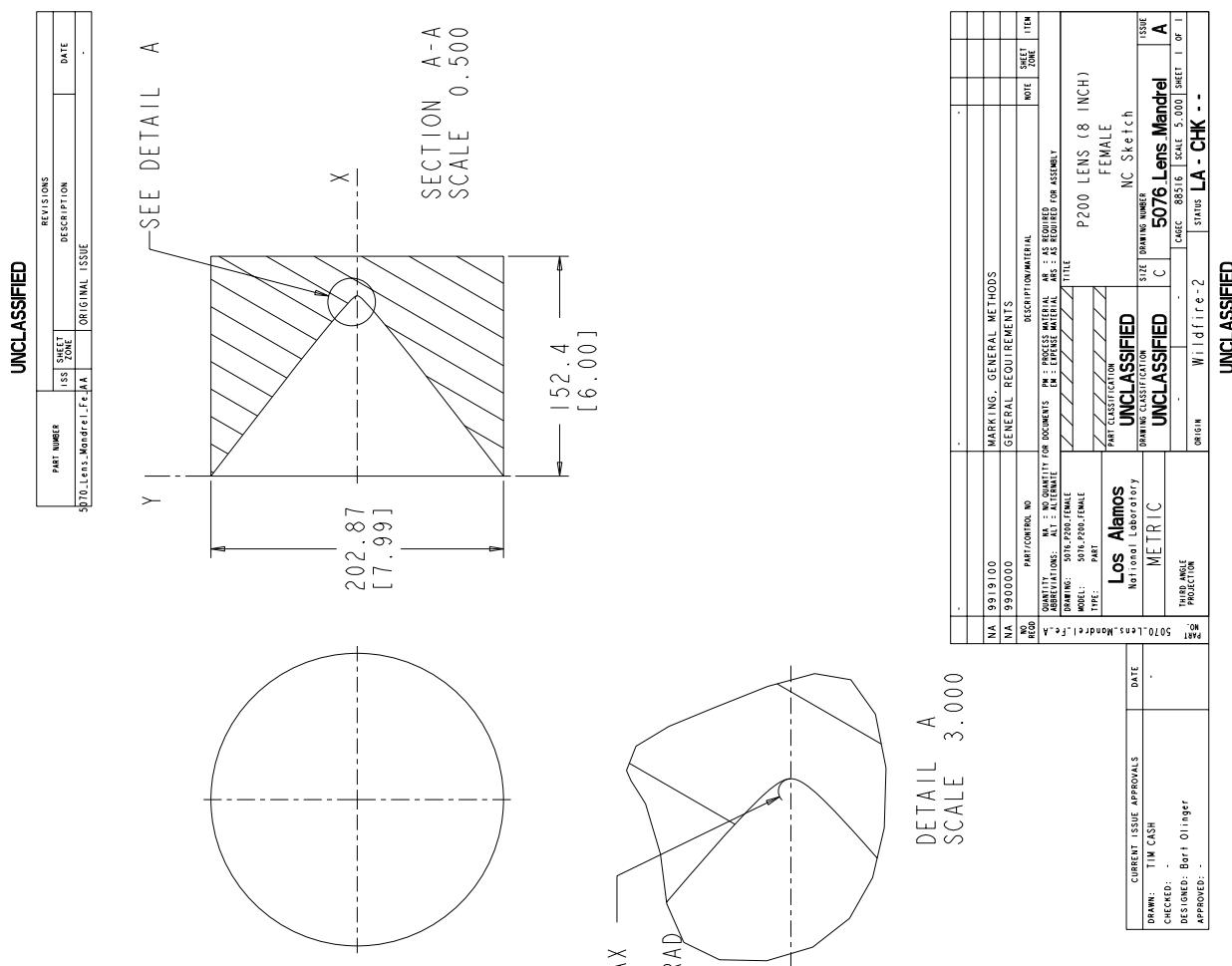
UNCLASSIFIED

**UNCLASSIFIED**  
Coordinates of spline points:

**CARTESIAN COORDINATES:**

X	Y	Z
125.027	0	0
125.016	0.2	0
124.985	0.4	0
124.933	0.6	0
124.861	0.8	0
124.773	-1	0
124.688	1.2	0
124.549	1.4	0
124.417	1.6	0
124.274	1.8	0
124.126	2	0
123.96	2.2	0
123.817	2.4	0
123.652	2.6	0
123.48	2.8	0
123.302	3	0
123.12	3.2	0
122.934	3.4	0
122.743	3.6	0
122.55	3.8	0
122.353	4	0
122.154	4.2	0
121.952	4.4	0
121.748	4.6	0
121.543	4.8	0
121.335	5	0
115.825	10	0
110.018	15	0
104.044	20	0
97.953	25	0
91.789	30	0
85.582	35	0
79.329	40	0
72.978	45	0
66.403	50	0
59.966	55	0
53.523	60	0
47.074	65	0
40.622	70	0
34.166	75	0
27.708	80	0
21.247	85	0
14.785	90	0
8.321	95	0
1.856	100	0
0	101.435	0

**UNCLASSIFIED**



PTS-P200-CONCAVE-#5076

**UNCLASSIFIED**

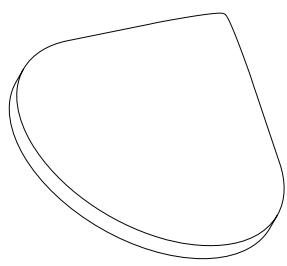
Coordinates of spline points:

CARTESIAN COORDINATES:

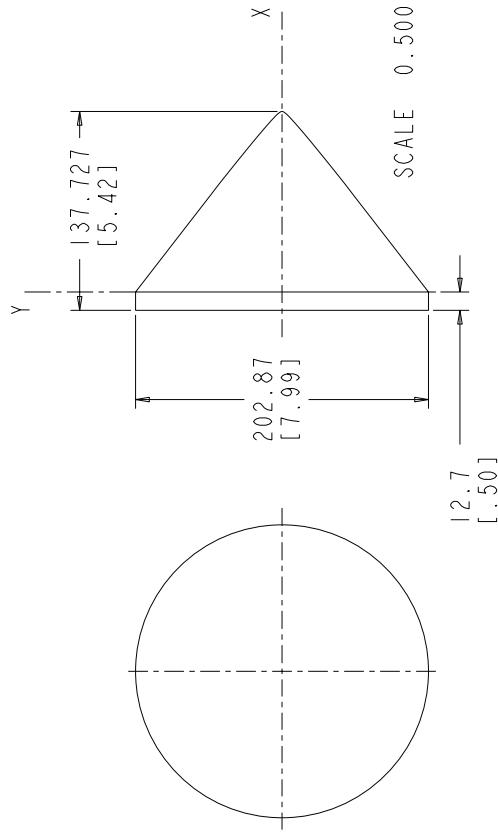
X	Y	Z
25.027	0	0
25.016	0.2	0.2
24.985	0.4	0.4
24.933	0.6	0.6
24.861	0.8	0.8
24.773	1	1
24.668	1.2	1.2
24.549	1.4	1.4
24.417	1.6	1.6
24.274	1.8	1.8
24.126	2	2
23.976	2.2	2.2
23.817	2.4	2.4
23.652	2.6	2.6
23.48	2.8	2.8
23.302	3	3
23.12	3.2	3.2
22.934	3.4	3.4
22.743	3.6	3.6
22.55	3.8	3.8
22.353	4	4
22.154	4.2	4.2
21.952	4.4	4.4
21.748	4.6	4.6
21.543	4.8	4.8
21.335	5	5
21.154	5.0	5.0
21.018	5.5	5.5
104.044	20	20
97.953	25	25
91.789	30	30
85.382	35	35
79.329	40	40
72.978	45	45
66.403	50	50
59.966	55	55
53.523	60	60
47.074	65	65
40.622	70	70
34.166	75	75
27.708	80	80
21.247	85	85
14.785	90	90
8.321	95	95
1.856	100	100
0	101.435	0

**UNCLASSIFIED**

PART NUMBER		REVISIONS	
5070-Lens-Mondrel-Ft. A		ISSUE	DATE
		ORIGINAL ISSUE	



SCALE 0.500



SCALE 0.500

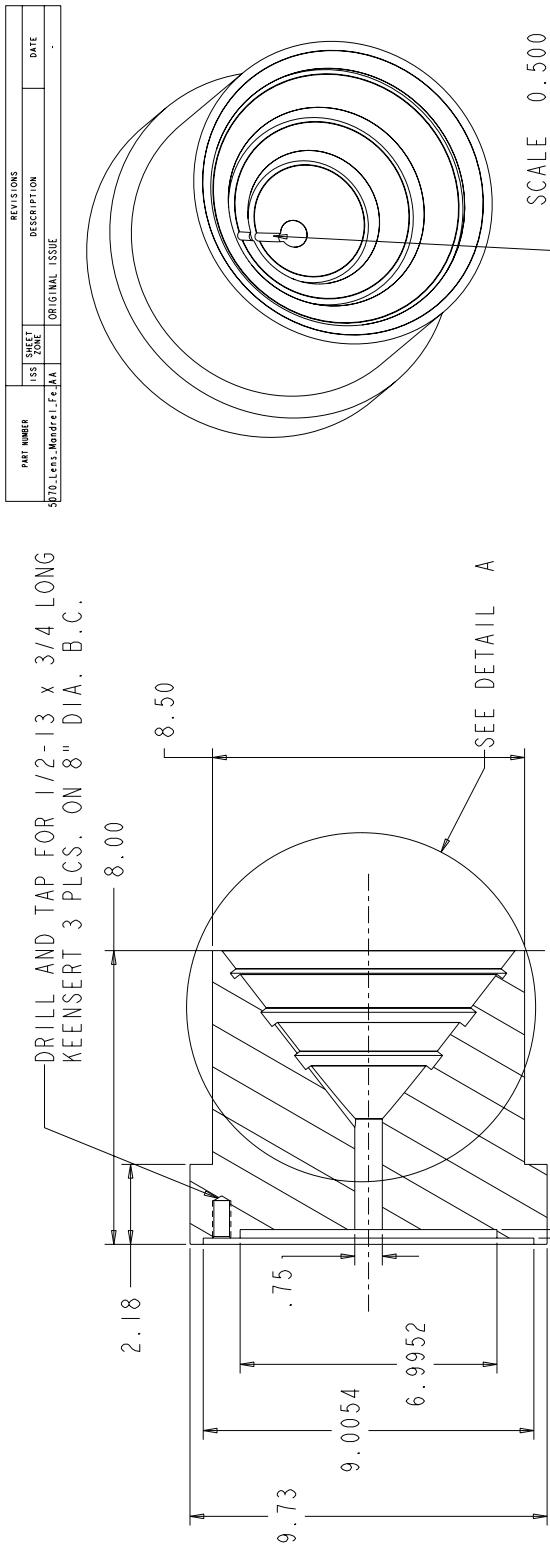
PART NUMBER		REVISIONS	
5070-Lens-Mondrel		ISSUE	DATE
		ORIGINAL ISSUE	
NA 9919100		MARKING, GENERAL METHODS	
NA 9930000		GENERAL REQUIREMENTS	
NA		DESCRIPTION/MATERIAL	
ABBRIVIATIONS:	NA : NO ABBRIVIATE	EM : EXPRESSED METHODS	NOTE
ABBREV:	AS : AS IS	AS : AS IS ASSEMBLED	ITEM
DRAWING:	AL : AS DRAWN	AS : AS DRAWN	
TYPE:	3017 P200 Male	3017 P200 Male	
MODEL:	3017 P200 Male	3017 P200 Male	
PART:	Los Alamos	Los Alamos	
LABORATORY:	UNCLASSIFIED	UNCLASSIFIED	
MATERIAL:	UNCLASSIFIED	UNCLASSIFIED	
MANUFACTURER:	C	C	
PROJECTION:	W/ Line	W/ Line	
ON:	LA - C	LA - C	
DESIGNED:	Tim Cash	Tim Cash	
CHECKED:			
APPROVED:	Bar + Longer	Bar + Longer	
SCALE:	1/2.7	1/2.7	
DATE:	1-1-85	1-1-85	
PROJECTION:	LA - C	LA - C	
ON:	LA - C	LA - C	
DESIGNED:	Bar + Longer	Bar + Longer	
CHECKED:			
APPROVED:	Bar + Longer	Bar + Longer	
SCALE:	1/2.7	1/2.7	
DATE:	1-1-85	1-1-85	
PROJECTION:	LA - C	LA - C	
ON:	LA - C	LA - C	

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FOR VACUUM NOTCH USE  
 1/4 BALL END MILL  
 AT APPROX 38° X 1/16 DEEP

SECTION A-A  
 SCALE 0.500  
 .49 (TYP. 2 PLCS.)

CONTOUR TO MATCH DRW. #5076

(8 INCH P200 LENS MANDREL)

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RAD (6 PLCS.)

3.35 (TYP.)

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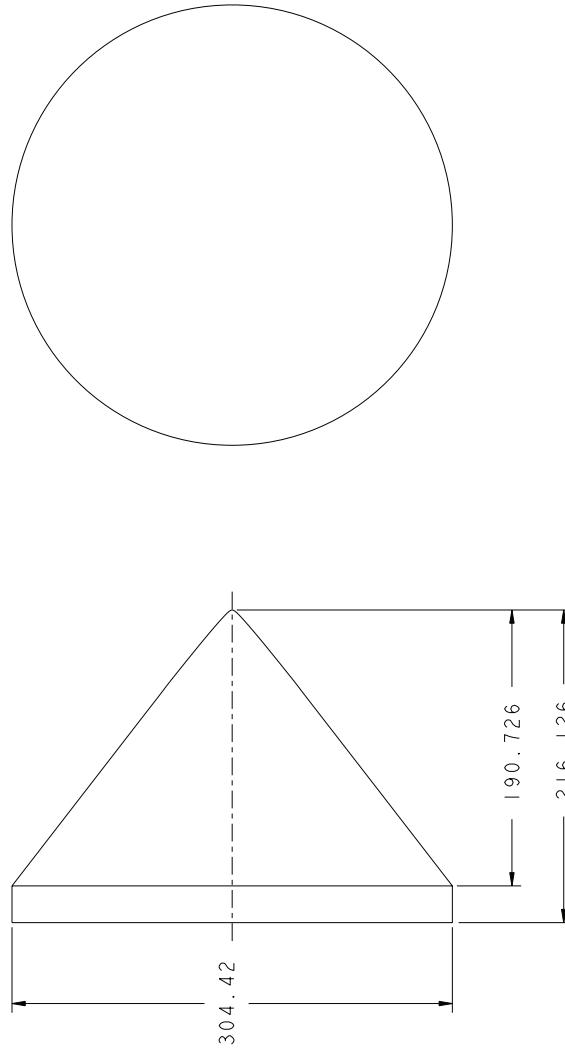
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190.7260	0.0000	0.0000
190.7150	0.2000	0.0000
190.6840	0.4000	0.0000
190.6320	0.6000	0.0000
190.5600	0.8000	0.0000
190.4720	1.0000	0.0000
190.3670	1.2000	0.0000
190.2480	1.4000	0.0000
190.1660	1.6000	0.0000
189.9730	1.8000	0.0000
189.8250	2.0000	0.0000
189.6750	2.2000	0.0000
189.5160	2.4000	0.0000
189.3510	2.6000	0.0000
189.1790	2.8000	0.0000
189.0010	3.0000	0.0000
188.8190	3.2000	0.0000
188.6330	3.4000	0.0000
188.4420	3.6000	0.0000
188.2490	3.8000	0.0000
188.0520	4.0000	0.0000
187.8530	4.2000	0.0000
187.6510	4.4000	0.0000
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187.2420	4.8000	0.0000
187.0340	5.0000	0.0000
187.5240	10.0000	0.0000
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175.7170	15.0000	0.0000
69.7430	20.0000	0.0000
63.6520	25.0000	0.0000
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51.2810	35.0000	0.0000
45.0280	40.0000	0.0000
38.6770	45.0000	0.0000
32.1020	50.0000	0.0000
25.6650	55.0000	0.0000
19.2220	60.0000	0.0000
12.7730	65.0000	0.0000
10.3210	70.0000	0.0000
9.8650	75.0000	0.0000
9.3407	80.0000	0.0000
8.6946	85.0000	0.0000
8.0484	90.0000	0.0000
7.4020	95.0000	0.0000
6.7550	100.0000	0.0000
6.0890	105.0000	0.0000
5.4621	110.0000	0.0000
4.8153	115.0000	0.0000
4.1685	120.0000	0.0000
3.5215	125.0000	0.0000
2.8745	130.0000	0.0000
2.2275	135.0000	0.0000
1.5804	140.0000	0.0000
9.3320	45.0000	0.0000
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0.0000	152.2100	0.0000
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-10.0840	160.0000	0.0000



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PTS-P300-CONVEX-#5079

PART NUMBER		REVISONS		DATE	
ISSUE	SHEET ZONE	ORIGINAL ISSUE		05-13-2005	
B					
CONFIRMED TO BE UNCLASSIFIED					
CLASSIFIER: -		TITLE: -		REDO	
DRAWING: A5079		PART CONTROL NO: A5079		PART NUMBER: A5079	
MODEL: A5079		TYPE: PART		TITLE: 1 INCH MALE LENS	
UNCLASSIFIED		UNCLASSIFIED		PROG A5079	
DRAWING CLASSIFICATION		DRAWING CLASSIFICATION		SIZE DRAWING NUMBER	
S / I METRIC		S / I METRIC		C 5079 LENS, MANDREL B	
DRAWN: RMONTA		DRAWN: RMONTA		SIZE: 88516 SCALE: 1/2	
CHECKED: -		CHECKED: -		NOTE: NC SKETCH	
DESIGNED: -		DESIGNED: -		ISSUE: LA-CHIK-05-13-2005	
APPROVED: -		APPROVED: -		RELEASE DATE: 05-13-2005	
TOLERANCES: UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN MILLIMETERS		TOLERANCES: UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN MILLIMETERS		DRAWING NUMBER: LA-CHIK-05-13-2005	
DECIMALS: .XX : ± 0.76		DECIMALS: .XX : ± 0.76		DRAWING LEVEL: CURRENT ISSUE APPROVALS	
ANGULAR: ± 0.5°		ANGULAR: ± 0.5°		DRAWING NUMBER: RMONTA	
MACHINED: 32		MACHINED: 32		DRAWING NUMBER: RMONTA	
FINISH: 0.254		FINISH: 0.254		DRAWING NUMBER: RMONTA	
PROJECT NAME: NEXT ASSY: DRAWING LEVEL: FINAL ASSY: DRAWING NUMBER: DATE: 05-13-2005					
PROJ. REVISION VERSION RELEASE DATE: 05-13-2005					
NOTE: 3					
DRAWING: -					

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