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COMPLETE

ENGINEERING CHANGE NOTICE			1. ECN NO 622103
Page 1 of <u>4</u>			Proj. ECN

2. ECN Category (mark one) Supplemental <input type="checkbox"/> Direct Revision <input checked="" type="checkbox"/> <i>4/21/95</i> Change ECN <input checked="" type="checkbox"/> Temporary <input type="checkbox"/> Standby <input type="checkbox"/> Supersedure <input type="checkbox"/> Cancel/Void <input type="checkbox"/>	3. Originator's Name, Organization, MSIN, and Telephone No. Tejpal S. Basra, Tank Farms Environmental Engineering, 7C420, R1-51, 373-5039		
	4. Date 04/19/95		
	5. Project Title/No./Work Order No. 242-A Evaporator Waste Analysis Plan		
	6. Bldg./Sys./Fac. No. N/A		
	7. Impact Level EQ		
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10. Related PO No. N/A			

11a. Modification Work <input type="checkbox"/> Yes (fill out Blk. 11b) <input checked="" type="checkbox"/> No (NA Blks. 11b, 11c, 11d)	11b. Work Package No. N/A	11c. Modification Work Complete N/A Cog. Engineer Signature & Date	11d. Restored to Original Condition (Temp. or Standby ECN only) N/A Cog. Engineer Signature & Date
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12. Description of Change <p>The entire document, WHC-SD-WM-EV-060, REV. 4, is being replaced with WHC-SD-WM-EV-060, Rev. 5, ECN# 622103.</p> <p>Synopsis of significant changes:</p> <p style="text-align: center;"><i>et 4/21/95</i></p> <p>1) Entire Section 4.2, Process condensate process criteria, deleted. 2) Table 4-3, Process condensate limits for LERF liner compatibility, deleted. 3) Entire Section 6.0, Process condensate sampling and analysis, deleted.</p>			
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13a. Justification (mark one) As-Found <input type="checkbox"/>	Criteria Change <input checked="" type="checkbox"/>	Design Improvement <input type="checkbox"/>	Environmental <input type="checkbox"/>
	Facilitate Const. <input type="checkbox"/>	Const. Error/Omission <input type="checkbox"/>	Design Error/Omission <input type="checkbox"/>

13b. Justification Details <p>The revision of this document implements the deletion of RCRA sampling of process condensate while discharging into the LERF during evaporator operations. Rationale for deletion of process condensate sampling requirements is documented in the Evaporator Data Quality Objective, WHC-SD-WM-DQO-014, Rev. 1.</p>

14. Distribution (include name, MSIN, and no. of copies) See attached distribution	RELEASE STAMP OFFICIAL RELEASE BY WHC DATE APR 21 1995 <i>2</i> <i>STA 4</i>
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1. ECN (use no. from pg. 1)

622103

15. Design Verification Required	16. Cost Impact				17. Schedule Impact (days)	
	ENGINEERING		CONSTRUCTION		Improvement	N/A
<input type="checkbox"/> Yes	Additional	<input type="checkbox"/> \$	Additional	<input type="checkbox"/> \$	Delay	<input type="checkbox"/>
<input checked="" type="checkbox"/> No	Savings	<input checked="" type="checkbox"/> \$	Savings	<input checked="" type="checkbox"/> \$		

18. Change Impact Review: Indicate the related documents (other than the engineering documents identified on Side 1) that will be affected by the change described in Block 12. Enter the affected document number in Block 19.

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Functional Design Criteria	<input type="checkbox"/>	Stress/Design Report	<input type="checkbox"/>	Health Physics Procedure	<input type="checkbox"/>
Operating Specification	<input type="checkbox"/>	Interface Control Drawing	<input type="checkbox"/>	Spares Multiple Unit Listing	<input type="checkbox"/>
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Conceptual Design Report	<input type="checkbox"/>	Installation Procedure	<input type="checkbox"/>	Component Index	<input type="checkbox"/>
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Const. Spec.	<input type="checkbox"/>	Engineering Procedure	<input type="checkbox"/>	Human Factor Consideration	<input type="checkbox"/>
Procurement Spec.	<input type="checkbox"/>	Operating Instruction	<input type="checkbox"/>	Computer Software	<input type="checkbox"/>
Vendor Information	<input type="checkbox"/>	Operating Procedure	<input type="checkbox"/>	Electric Circuit Schedule	<input type="checkbox"/>
OM Manual	<input type="checkbox"/>	Operational Safety Requirement	<input type="checkbox"/>	ICRS Procedure	<input type="checkbox"/>
FSAR/SAR	<input type="checkbox"/>	IEFD Drawing	<input type="checkbox"/>	Process Control Manual/Plan	<input type="checkbox"/>
Safety Equipment List	<input type="checkbox"/>	Cell Arrangement Drawing	<input type="checkbox"/>	Process Flow Chart	<input type="checkbox"/>
Radiation Work Permit	<input type="checkbox"/>	Essential Material Specification	<input type="checkbox"/>	Purchase Requisition	<input type="checkbox"/>
Environmental Impact Statement	<input type="checkbox"/>	Fac. Proc. Samp. Schedule	<input type="checkbox"/>		<i>✓/A</i>
Environmental Report	<input type="checkbox"/>	Inspection Plan	<input type="checkbox"/>		<input type="checkbox"/>
Environmental Permit	<input type="checkbox"/>	Inventory Adjustment Request	<input type="checkbox"/>		<input type="checkbox"/>

19. Other Affected Documents: (NOTE: Documents listed below will not be revised by this ECN.) Signatures below indicate that the signing organization has been notified of other affected documents listed below.

Document Number/Revision	Document Number/Revision	Document Number Revision
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✓/A

20. Approvals

Signature	Date	Signature	Date
OPERATIONS AND ENGINEERING		ARCHITECT-ENGINEER	
Cog Engineer * Tejpal S Basra <i>Tejpal S. Basra</i>	<u>4/14/94</u>	PE	
Cog. Mgr. * R.D. Gustavson <i>R.D. Gustavson</i>	<u>4/20/95</u>	QA	
QA *Roger True <i>R. True</i>	<u>4-20-95</u>	Safety	
Safety		Design	
Security		Environ.	
Environ. <i>M.W. Bowman</i>	<u>4-20-95</u>	Other	
Projects/Programs			
Tank Waste Remediation System			
Facilities Operations			
Restoration & Remediation			
Operations & Support Services			
IRM			
Other			
Treatment System Plant Engineering * Brian Von Bargen <i>Brian Von Bargen</i>	<u>4/21/95</u>	DEPARTMENT OF ENERGY Signature or Letter No.	
		ADDITIONAL	

WASTE TANKS ADMINISTRATION	Manual	WHC-IP-0842
UNREVIEWED SAFETY QUESTIONS	Section	15.9, REV 1
	Page	15 of 25
	Effective Date	September 3, 1993

APPENDIX B

Unreviewed Safety Question Forms

Figure B-1. Unreviewed Safety Question - Changes Screening Form. (1 Sheet)

REFERENCE ITEM # ECN #622103TITLE 242-A Evaporator Waste Analysis Plan, WHC-SD-WM-EV-060, Rev. 5

Does the referenced item:

A. Make PROPOSED CHANGES to the facility or procedures which differ from conditions described in the AUTHORIZATION BASIS documentation?

N/A NO X Yes/Maybe

Basis: ECN #622103 does not make proposed changes to the facility or procedures which differ from conditions described in WHC-SD-WM-SAR-023, "242-A Evaporator/Crystallizer Safety Analysis Report", Rev. 1-B, or WHC-SD-W105-SAR-001, Final Safety Analysis Report 242-A Evaporator Liquid Effluent Retention Facility", Rev. 0-C. The ECN implements the Waste Analysis Plan (part of the Part B Permit Application) which provides guidance necessary to meet environmental compliance objectives only. Implementation of this document has no effect on the accidents described in Table 9-1, "Summary of Radiological Consequences".

B. Make PROPOSED CHANGES that represent conditions that have not been analyzed in the AUTHORIZATION BASIS?

N/A NO X Yes/Maybe

Basis: ECN #622103 does not make proposed changes that represent conditions that have not been analyzed in WHC-SD-WM-SAR-023, "242-A Evaporator/Crystallizer Safety Analysis Report", Rev. 1-B, Chapter 9 or WHC-SD-W105-SAR-001, Final Safety Analysis Report 242-A Evaporator Liquid Effluent Retention Facility", Rev. 0-C. The ECN implements the Waste Analysis Plan (part of the Part B Permit Application) which provides guidance necessary to meet environmental compliance objectives only. Implementation of this document has no effect on the accidents described in Table 9-1, "Summary of Radiological Consequences".

C. Describe tests or experiments which differ from those described in the AUTHORIZATION BASIS documentation?

N/A NO X Yes/Maybe

Basis: ECN #622103 does not describe any tests or experiments at all. The ECN implements the Waste Analysis Plan (part of the Part B Permit Application) which provides guidance necessary to meet environmental compliance objectives only. Implementation of this document has no effect on the accidents described in Table 9-1, "Summary of Radiological Consequences".

WASTE TANKS ADMINISTRATION	Manual	WHC-IP-0842
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D. Is a change in a TSR, OSR, or compliance plan to OSR involved?

N/A NO x Yes/Maybe

Basis: ECN #622103 does not change any TSR, OSR, or compliance plan to OSR as described in WHC-SD-WM-SAR-023, "242-A Evaporator/Crystallizer Safety Analysis Report", Rev. 1-B, Chapter 9 or WHC-SD-W105-SAR-001, Final Safety Analysis Report 242-A Evaporator Liquid Effluent Retention Facility", Rev. 0-C. The ECN implements the Waste Analysis Plan (part of the Part B Permit Application) which provides guidance necessary to meet environmental compliance objectives only. Implementation of this document has no effect on the accidents described in Table 9-1, "Summary of Radiological Consequences".

USQE #1 Brian Von Bargen

Print Name

Brian Von Bargen
Signature

USQE #2 Elvis Le

Print Name

Elvis Le
Signature

4/13/95
Date

4/13/95
Date

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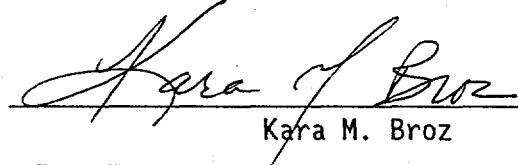
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Release Date: April 21, 1995

This document was reviewed following the procedures described in WHC-CM-3-4 and is:

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WHC Information Release Administration Specialist:



Kara M. Broz

April 21, 1995

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SUPPORTING DOCUMENT

1. Total Pages 30

2. Title <i>ch</i> 242-A Evaporator Waste Analysis Plan, WHC-SD-WM-EV-060, Rev. 5	3. Number WHC-SD-WM-EV-060	4. Rev No. Rev. 5
5. Key Words Waste characterization of candidate feed tank(s) at the evaporator.	6. Author Name: Tejpal S. Basra <i>Tejpal S. Basra 4/14/95</i> Signature	Organization/Charge Code 7C42D/71151
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9. Impact Level		

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REVISION

(1) Document Number

WHC-SD-WM-EV-060

(2) Title

242-A Evaporator Waste Analysis Plan

CHANGE CONTROL RECORD

(3) Revision	(4) Description of Change - Replace, Add, and Delete Pages	Authorized for Release		
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3 RS	WHC-SD-WM-EV-060, REV. 2 ECN 192267 Revise per ECN 161468	C.M. Bell	R.D. Gustavson	4/15/93
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5 RS	WHC-SD-WM-EV-060, Rev. 4 ECN 613528 Revise per ECN 622103	Mark A. Miller Taypal Bassra	R.D. Gustavson	4/21/95

242-A EVAPORATOR WASTE ANALYSIS PLAN
April 13, 1995

WHC-SD-WM-EV-060
Rev. 5

242-A EVAPORATOR WASTE ANALYSIS PLAN

By

Tejpal S. Basra

April 13, 1995

MASTER

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ABBREVIATIONS & ACRONYMS

ASTM	AMERICAN SOCIETY FOR TESTING AND MATERIALS
CFR	CODE OF FEDERAL REGULATIONS
DOE	U.S. DEPARTMENT OF ENERGY
DQO	DATA QUALITY OBJECTIVE
DSC	DIFFERENTIAL SCANNING CALORIMETER
DST	DOUBLE SHELL TANKS
Ecology	WASHINGTON STATE DEPARTMENT OF ECOLOGY
EPA	U.S. ENVIRONMENTAL PROTECTION AGENCY
ETF	EFFLUENT TREATMENT FACILITY
Evaporator	242-A EVAPORATOR
HDPE	HIGH DENSITY POLYPROPYLENE
LDR	LAND DISPOSAL RESTRICTION
LERF	LIQUID EFFLUENT RETENTION FACILITY
PC	PROCESS CONDENSATE
QA	QUALITY ASSURANCE
QAPjP	QUALITY ASSURANCE PROJECT PLAN
QAPP	QUALITY ASSURANCE PROGRAM PLAN
QC	QUALITY CONTROL
RSD	RELATIVE STANDARD DEVIATION
SD	SUPPORTING DOCUMENT
TCLP	TOXICITY CHARACTERISTIC LEACHING PROCEDURE
TC	TOTAL CARBON
TIC	TOTAL INORGANIC CARBON
TOC	TOTAL ORGANIC CARBON
TSD	TREATMENT, STORAGE, DISPOSAL
WAC	WASHINGTON ADMINISTRATIVE CODE
WAP	WASTE ANALYSIS PLAN
WHC	WESTINGHOUSE HANFORD COMPANY
WM	WASTE MANAGEMENT (WHC)

1.0 INTRODUCTION

1.1 PURPOSE

This Waste Analysis Plan (WAP) provides the plan for obtaining information needed for proper waste handling and processing in the 242-A Evaporator (Evaporator) located on the Hanford Site. In particular it addresses analysis necessary to manage the waste according to *Washington Administrative Code* (WAC) 173-303 and Parts 264 and 265 of the *Code of Federal Regulations* (CFR). Regulatory and safety issues are addressed by establishing boundary conditions for waste received and treated at the 242-A Evaporator. The boundary conditions are set by establishing limits for items such as potential exothermic reactions, waste compatibility, and control of vessel vent organic emissions. Boundary conditions are also set for operational considerations and to ensure waste acceptance at receiving facilities.

1.2 SCOPE

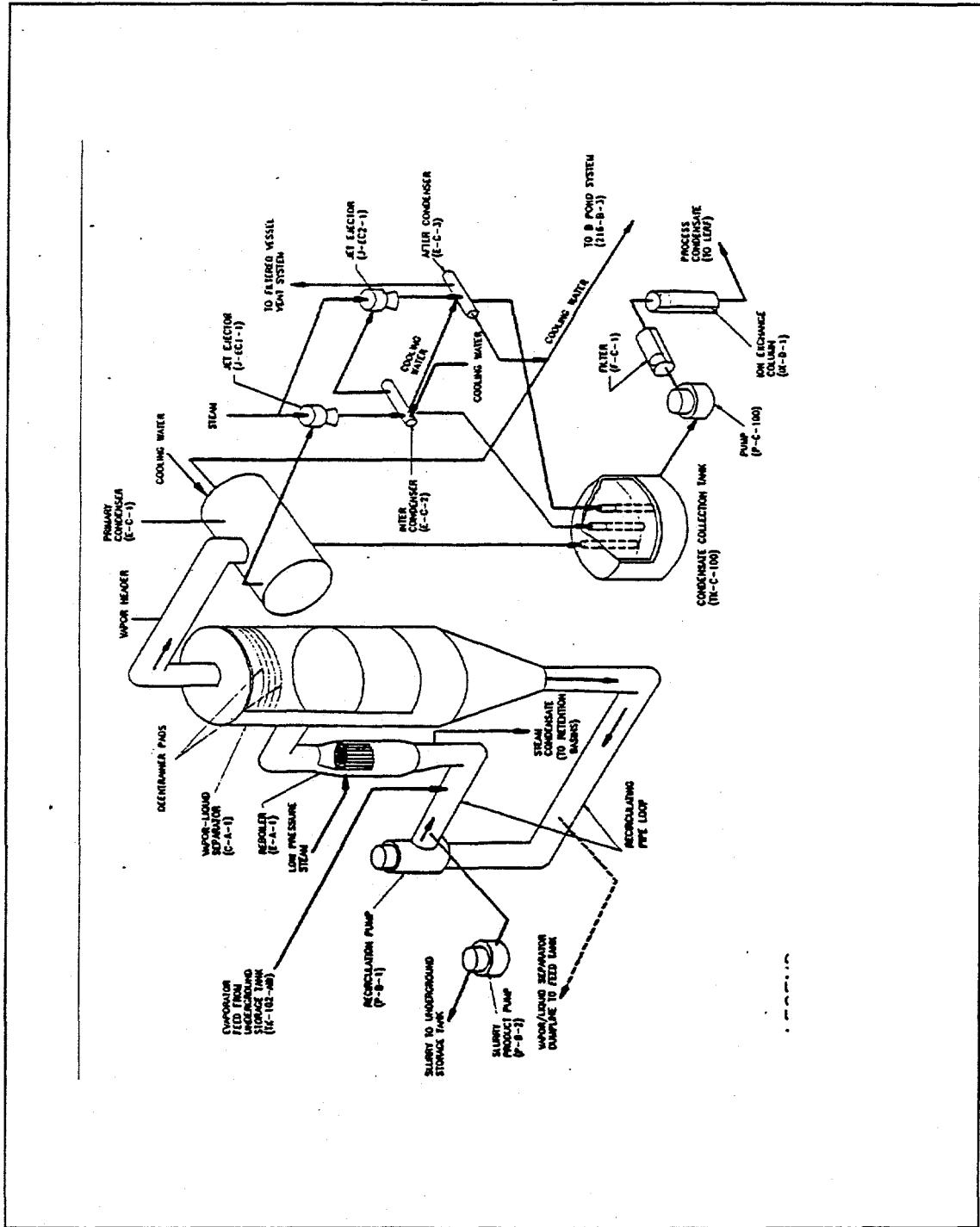
The issues that are addressed in this plan include prevention of exotherms in the waste, waste compatibility, and vessel vent emissions. Samples from the other streams associated with the Evaporator are taken as required by Process Control Plans but are excluded from this plan because either the streams do not contain dangerous waste or the analyses are not required by WAC 173-303-300.

2.0 FACILITY AND PROCESS DESCRIPTION

The 242-A Evaporator is located in the 200 East Area of the Hanford Site. This Evaporator separates the waste into three components as described in the following paragraph. Also associated with this Evaporator are utility waste streams such as cooling water and steam condensate. The types of wastes processed by the Evaporator are described in Section 3.0.

The 242-A Evaporator process uses a conventional forced circulation and vacuum evaporation system to concentrate mixed waste solutions. The 242-A Evaporator feed stream is separated into two liquid streams: a concentrated slurry stream and a process condensate. A gaseous exhaust stream is also produced. The slurry contains the majority of the radionuclides and inorganic constituents. This stream is pumped back to the double shell tanks (DSTs) and stored for further treatment after being concentrated to target levels. The process condensate (PC) is primarily water that contains trace amounts of organic material and a greatly reduced concentration of radionuclides. Currently, the PC is stored in the Liquid Effluent Retention Facility (LERF) until it can be further processed in the Effluent Treatment Facility (ETF) once it is operational. The process exhaust or vessel vent stream is filtered for fine particulate and discharged through an exhaust stack. Figure 2-1 shows a simplified schematic of the Evaporator. A more detailed description of the Evaporator is contained in the *242-A Evaporator Part B Dangerous Waste Permit Application* (DOE-RL 1991a).

Figure 2-1 242-A Evaporator Simplified Schematic



3.0 WASTE STREAM IDENTIFICATION

All of the waste accepted by the Evaporator comes from double-shell tanks (DSTs). The waste in the DSTs is received from onsite generators, which characterize the waste before transfer to the DSTs. Waste characterization is based on actual analytical knowledge and/or process knowledge. Based on this and other available information, certain DSTs are selected as "candidates" for being processed in the Evaporator. The contents of these candidate feed tanks are subjected to closer scrutiny and evaluated against processing criteria before the final tank selection is made. In order to meet processing criteria, the contents of several tanks may be blended together in the Evaporator Feed Tank (TK-241-AW-102) prior to actually being processed in the Evaporator.

3.1 IDENTIFICATION OF WASTE

The waste processed in the evaporator is classified as a mixed waste because it contains both radioactive and hazardous chemical components. Historical analytical data for the three dangerous waste streams (feed, slurry, and process condensate) are presented in Chapter 3.0 of the 242-A *Evaporator Part B Dangerous Waste Permit Application* (DOE-RL 1991a). The candidate feed tanks, feed stream, and slurry stream are classified as extremely hazardous waste as specified in WAC 173-303-100 (5). Most of the radionuclides and dangerous waste constituents remain in the slurry after being processed in the Evaporator. Because some radionuclides and dangerous waste constituents may carry over into the process condensate, the PC remains classified as a dangerous waste per WAC 173-303-100. Table 3-1 lists the waste codes which are applied to the feed and slurry streams at the 242-A Evaporator.

Analysis of utility streams including cooling water and steam condensate are conducted. These analyses are not discussed in this plan because these streams are not considered dangerous wastes under WAC 173-303.

3.2 GENERAL CONSTITUENT DESCRIPTION

The waste sent to the Evaporator contains water as a major constituent of the waste. The pH of the waste can be 12.5 or higher due to the quantity of hydroxide used as corrosion protection for the DSTs. Qualitatively, the other major constituents of the mixed waste are sodium salts of nitrate, nitrite, fluoride, phosphate, carbonate, and sulfate. Additionally other salts including calcium, aluminum, and potassium salts may be present. Detectable levels of halogenated and non-

halogenated organic compounds may also be present. The mixed waste in some tanks has detectable levels of heavy metals such as lead, chromium, and cadmium. The radionuclide content includes fission products such as the isotopes ^{90}Sr and ^{137}Cs , and actinide series elements such as uranium and plutonium.

3.3 WASTE CHARACTERISTICS

Due to the blending which occurs in the Evaporator Feed Tank, the composition of waste actually sent to the Evaporator is more homogenized than the waste in the candidate feed tanks. Generally, this waste is a stable aqueous liquid with a low organic content. The waste has been designated as characteristically ignitable, corrosive, reactive, and TCLP toxic per WAC 173-303-090. It has also been designated as an extremely hazardous waste because it meets the toxic, carcinogenic, and persistent criteria described in WAC 173-303-100. The waste has also been assigned the nonspecific waste codes F001 to F005 due to the presence of spent halogenated and nonhalogenated solvents. The Evaporator may also process waste from leachate systems that has been assigned the nonspecific waste code F039.

The Evaporator separates the waste into two streams (slurry and the process condensate) which are sent to other treatment, storage, or disposal (TSD) units. Process knowledge and historical data indicate that the slurry stream exhibits the same dangerous waste properties as the waste feed, so the same dangerous waste codes are applicable to the slurry. The process condensate exhibits different dangerous waste characteristics because most of the nonvolatile toxic compounds have remained in the slurry. The process condensate has still been assigned the nonspecific source codes F001 to F005 and F039 because it has been derived from the treatment of a listed waste. The PC is also designated state characteristically toxic (WT02) due to the potential ammonia concentration.

Table 3-1 contains a list of the dangerous waste codes assigned to the feed and slurry streams of the 242-A Evaporator in the Hanford Facility Dangerous Waste Part A Permit Application (DOE/RL-88-21). Table 3-2 contains a listing of the dangerous waste codes which have been assigned to the process condensate in the LERF portion of the Hanford Facility Dangerous Waste Part A Permit Application (DOE/RL-88-21). A detailed description of waste designation is contained in Chapter 3.0 of the Evaporator Part B permit application (DOE-RL 1991a).

The DST waste was designated ignitable due to the presence of nitrates and nitrites, which are classified as oxidizers in 49 CFR 173. However the concentrations of these nitrogen compounds in the waste are normally so dilute that ignitability is not an issue. DSTs which contain concentrated quantities of these materials, such as tank 101-SY, will not be processed in the Evaporator without an evaluation of the potential ignitability problem.

To confirm that a waste will not produce an exothermic or spontaneous reaction that would result in a violent change, a differential scanning calorimetry (DSC) check is performed on samples from the candidate feed tanks. This is used to indicate that the waste is not reactive.

A detailed discussion of the assertion that the DST waste processed in the Evaporator is not physically ignitable or reactive is given in Chapter 3.0 of the Evaporator Part B permit application (DOE-RL 1991a).

Table 3-1 Waste Designation For 242-A Evaporator Feed And Slurry

EPA/State Waste Code	Characteristic	Basis for designation
D001	Ignitable	Presence of constituents classified as ignitable. Waste itself will not exhibit the characteristic of ignitability
D002	Corrosive	pH > 12.5
D003	Reactive	Presence of constituents classified as reactive. Waste itself will not exhibit the characteristic of reactivity.
D004	TCLP toxic	Arsenic
D005	TCLP toxic	Barium
D006	TCLP toxic	Cadmium
D007	TCLP toxic	Chromium
D008	TCLP toxic	Lead

Table 3-1 Waste Designation For 242-A Evaporator Feed And Slurry

EPA/State Waste Code	Characteristic	Basis for designation
D009	TCLP toxic	Mercury
D010	TCLP toxic	Selenium
D011	TCLP toxic	Silver
D018	TCLP toxic	Benzene
D019	TCLP toxic	Carbon Tetrachloride
D022	TCLP toxic	Chloroform
D028	TCLP toxic	1,2-Dichloroethane
D029	TCLP toxic	1,1-Dichloroethylene
D030	TCLP toxic	2,4-Dinitrotoluene
D033	TCLP toxic	Hexachloro-1,3-butadiene
D034	TCLP toxic	Hexachloroethane

Table 3-1 Waste Designation For 242-A Evaporator Feed And Slurry

EPA/State Waste Code	Characteristic	Basis for designation
D035	TCLP toxic	Methyl ethyl ketone
D036	TCLP toxic	Nitrobenzene
D038	TCLP toxic	Pyridine
D039	TCLP toxic	Tetrachloroethylene
D040	TCLP toxic	Trichloroethylene
D041	TCLP toxic	2,4,5-Trichlorophenol
D043	TCLP toxic	Vinyl chloride
WT01/WT02	Toxicity	Sodium hydroxide, Sodium nitrite, Sodium nitrate, Sodium fluoride, Ammonium hydroxide, Tributyl phosphate
WC01/ WC02	Carcinogenic	Not determined
WP01/ WP02	Persistent	Not determined

Table 3-1 Waste Designation For 242-A Evaporator Feed And Slurry

EPA/State Waste Code	Characteristic	Basis for designation
F001	Spent halogenated solvents	Carbon Tetrachloride and others
F002	Spent halogenated solvents	Methylene chloride, 1,1,1 Trichloroethane, and others
F003	Spent nonhalogenated solvents	Acetone, Methyl Isobutyl ketone, and others
F004	Spent nonhalogenated solvents	Cresylic acid, Cresols (o- or p-cresols) and others
F005	Spent nonhalogenated solvents	Methyl ethyl ketone, and others
F039	Leachate from hazardous waste disposal operations	Receipt of waste with the F039 code, derived from F001 through F005.

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Table 3-2 Waste Designation For 242-A Evaporator Process Condensate/LERF Waste

EPA/State Waste Code	Characteristic	Basis for designation
F001	Spent halogenated solvents	Derived from F001 waste
F002	Spent halogenated solvents	Derived from F002 waste
F003	Spent nonhalogenated solvents	Acetone, Methyl Isobutyl ketone and others Derived from F003 waste
F004	Spent nonhalogenated solvents	Derived from F004 waste
F005	Spent nonhalogenated solvents	Methyl ethyl ketone
F039	Leachate from hazardous waste disposal operations	Derived from and/ or contains F039 designated waste
WT02	Toxicity	Ammonia

4.0 EVAPORATOR PROCESSING CRITERIA

Processing criteria have been established from regulatory requirements, operating experience, process knowledge, analyses, and calculations. Processing criteria are maximum and/or minimum values of a waste analyte that, if exceeded, alert the operator that the waste requires further attention before proceeding. Prior to each evaporator campaign, candidate feed tank analyses in conjunction with processing criteria are used to develop a control plan which is used to ensure that established limits will not be exceeded. The criteria selection process is discussed in detail in the 242-A Evaporator/LERF DQO Document (Von Bargen 1995). The reason for selecting a given analyte for inclusion in this WAP as required by WAC 173-303, is indicated in Sections 4.1 and 4.2 of this plan.

Additional analyses of the Evaporator streams (feed, slurry, and PC) via process control sampling are conducted for the purpose of monitoring the evaporation process and ensuring that all streams will meet all established operating criteria. This type of sampling is considered outside the scope of this plan and is addressed by the latest editions of the 242-A Evaporator Process Control Plan (the plan for each campaign has a unique number beginning with WHC-SD-WM-PCP-), and the DST WAP (Mulkey and Jones 1995).

4.1 CANDIDATE FEED TANK WASTE ACCEPTANCE AND PROCESS CRITERIA

Sections 4.1.1 through 4.1.4 discuss waste acceptance analysis issues and the assurances that processing criteria will not be exceeded when waste from the candidate feed tanks is processed in the Evaporator.

4.1.1 Exothermic Reactions

To evaluate the probability of an uncontrolled reaction, a differential scanning calorimeter (DSC) test is performed on all waste to be processed in the Evaporator. Waste exhibiting exotherms below 335 °F (168°C), or with an absolute value of the exotherm-to-endotherm ratio greater than one, will not be processed in the Evaporator without further technical evaluation.

4.1.2 Compatibility

A compatibility evaluation is performed on wastes from the candidate feed tanks in order to verify that there will be no adverse affects due to mixing the contents of different waste tanks in the 242-A Evaporator feed tank. The evaluation uses information gained from a mixing and compatibility study. As part of the mixing and compatibility study, samples of waste from the candidate feed tanks are taken to the

laboratory where they are combined, mixed, and then observed for any unusual changes in color, temperature, clarity, solids formation, or other visual characteristic. If any changes are observed, further compatibility evaluations will be conducted or the wastes will not be processed.

4.1.3 Organic Constituents

The levels of volatile organics in the candidate feed tanks must be limited to prevent organic vessel vent emissions from exceeding 3 lbs/hr and 3.1 tons/yr during processing (40 CFR 265). To ensure that these limits are not exceeded, equilibrium calculations were performed in the *242-A Evaporator Part B Dangerous Waste Permit Application* (DOE/RL 1991a) to determine limits for individual organic constituents. These limits, shown in Table 4.1, include a modifier "R-1/R", which adjusts the limits based on the campaign's planned boil-off rate (R is the ratio of feed flow rate to slurry flow rate).

The organic limits in the permit application were based on twelve months of continuous operation each year. These limits were adjusted to six months continuous operation each year for this plan. The six months operating is a realistic limit because the Evaporator must shut down during the year for maintenance outages, candidate feed tank analysis, and establishing transfer routes for staging the waste into the feed tank. Since the limits are based on a calendar year and they depend on operating time, the limits in Table 4.1 may need to be adjusted to reflect actual operation. The total carbon (TC) minus the total inorganic carbon (TIC) is used as a screening tool to account for all organic species (Von Bargen 1995). If the TC-TIC limit is exceeded, a more detailed evaluation will be conducted to determine organic emissions out of the vessel vent. This limit of 87 mg/L is based on the assumption that all organic species are volatile and are calculated as acetone (as if all organic species were acetone) due to its relatively low carbon percentage (Von Bargen 1995).

In addition to the organics with limits shown in Table 4.1, analyses for 2-hexanone, 2-pentanone, methyl isobutyl ketone, and tetrahydrofuran will be conducted to ensure they are not routinely present in the waste. In the future, characterizations of candidate feed tank waste (if these compounds are regularly seen) feed limits will be added for these organics as well.

The level of volatile organics in the feed must be limited to ensure PC is compatible with the LERF liner. The HDPE liner used at the LERF is exposed to PC that may contain trace quantities of chemicals, which in turn may cause degradation of the liner material. Based on the liner manufacturer's data, the concentration limits in Table 4.2 are imposed on those classes of constituents that could potentially degrade the liner (Von Bargen 1995). To ensure that these limits are

not exceeded in the process condensate, the concentration limits are applied to the candidate feed tanks as well and modified by "R-1/R," as appropriate.

4.1.4 **Ammonia**

The candidate feed tanks must be sampled for ammonia so that processing can be adjusted to ensure the process condensate does not exceed 1 wt% ammonia, which is the limit for Washington State extremely hazardous waste as indicated in WAC 173-303-100. The 1 wt% limit equates to a concentration of 0.58M ammonia in the process condensate. This assumes a typical 50% waste volume reduction per pass (R equals 2) through the Evaporator and conservatively assumes all the ammonia transfers with the process condensate, processing adjustments such as candidate feed tank blending are made to ensure the ammonia concentration in the feed stream remains below 0.29M (5,000 mg/L).

Table 4-1 Candidate Waste Tank Limits for Vessel Vent Organic Discharge^a

Feed Constituent	Limit (mg/L) ^{b,c}
Acetone	174.4 x (R-1)/R
1-Butanol	452 x (R-1)/R
2-Butoxyethanol	190.4 x (R-1)/R
2-Butanone	116 x (R-1)/R
Tri-Butyl Phosphate	2.030 E+4 x (R-1)/R
2-Hexanone	N/A (see discussion)
2-Pentanone	N/A (see discussion)
Methyl Isobutyl Ketone	N/A (see discussion)
Tetrahydrofuran	N/A (see discussion)
TC and TIC	(TC-TIC) < 174.4 x (R-1)/R (as acetone)

^aLimits in this table are based on a maximum continuous operating time equivalent to six months per year. If total operating time is expected to exceed six months per year, the limits must be evaluated.

^bThe limits are applied using the sum of the fraction technique:

$$\sum_{n=1}^i \left(\frac{\text{Conc}_n}{\text{LIMIT}_n} \right) \leq 1$$

where i is the number of organic constituents detected in analysis of the waste feed tank. TC and TIC are not part of the summation.

^cR is the ratio of feed flowrate to slurry flowrate (typically R = 2).

Table 4-2 Candidate Feed Tank Limits for LERF Liner Compatibility

Chemical Family/Parameter	Current Target Compounds	Limit (mg/L) ^{a,b,e}
Alcohol/Glycol	1-butanol	500,000 x (R-1)/R
Alkanone ^c	sum of acetone, 2-pentanone, 2-butanone, 2-hexanone, methyl isobutyl ketone	200,000 x (R-1)/R
Alkenone ^d	none targeted	2000 x (R-1)/R
Aromatic/Cyclic Hydrocarbon	tetrahydrofuran	2000 x (R-1)/R
Halogenated Hydrocarbon	none targeted	2000 x (R-1)/R
Aliphatic Hydrocarbon	none targeted	500,000 x (R-1)/R
Ether	2-Butoxyethanol	2000 x (R-1)/R
Other Hydrocarbons	Tri-butyl Phosphate	2000 x (R-1)/R
Oxidizers	none targeted	1000 x (R-1)/R
Acids, Bases, and Salts	ammonia	100,000 x (R-1)/R
TC and TIC	N/A	(TC-TIC) < 1240 x (R-1)/R

^aR is the ratio of feed flowrate to slurry flowrate (typically R = 2).

^bThe limits are applied using the sum of the fraction technique:

$$\sum_{n=1}^i \left(\frac{\text{Conc}_n}{\text{LIMIT}_n} \right) \leq 1$$

where i is the number of organic constituents detected in analysis of the waste feed tank. TC and TIC are not part of the summation.

^cKetone containing saturated alkyl group(s)

^dKetone containing unsaturated alkyl group(s)

^eIf a chemical fits in more than one chemical family, the more restrictive limit applies.

5.0 CANDIDATE FEED TANK SAMPLING AND ANALYSIS

This section discusses parameters associated with the candidate feed tanks. The parameters include tank selection, sampling frequency, and selection of analytes. Due to the highly radioactive nature of the samples, it is anticipated that all analyses will be conducted at one of the laboratories on the Hanford Site because they are equipped to handle such samples. Laboratory selection will be dependent on the analysis needed and the availability and capability of the laboratories at the time of sampling.

It is recognized that analytical data from candidate feed tanks may be available from other programs. Data from other programs which meets the criteria contained in the 242-A Evaporator DQO (Von Bargen 95) can be substituted for the sampling and analysis required by this document.

5.1 SELECTION OF CANDIDATE FEED TANKS

The Evaporator feed stream originates from the DSTs. For each campaign of the 242-A Evaporator, DSTs will be selected based on process knowledge of waste characteristics (components) with respect to waste acceptability criteria provided in Section 4.0 of this plan. If the waste is suitable for evaporation, it will be transferred to the evaporator feed tank, TK-241-AW-102.

5.2 SAMPLE COLLECTION

The number of lateral sampling locations in candidate feed tanks is limited by the availability of tank risers providing access into the tank. Generally, only a few risers in each tank are actually available for sampling because some of the risers are dedicated to instrumentation or other uses. Sampling within a vertical column is generally limited only by the depth of waste in the tank. The number of available sample locations, information on the proximity of expected tank analyte concentration to a decision point or target threshold, and information from previous Evaporator runs will be used to statistically determine the number of samples necessary to verify the composition of the tank. The statistical analysis includes the generation of power curves as indicated in the 242-A Evaporator/LERF DQO Document (Von Bargen 1995). The number of samples required are based on the criteria action level (target threshold), estimated or known concentrations, and the required confidence levels (which are based on the consequences of a wrong decision). If concentration of a critical analyte approaches the target threshold (criteria) then more samples are required to minimize sampling anomalies. Figure

5-1 illustrates the decision logic path which can be used to determine the number of samples needed for a given tank. Generally three to five samples will be taken from each candidate feed tank.

Samples will be obtained by using a grab sampling (e.g. "bottle on a string method") method approved for use on the Hanford Site. Normally only one set of samples will be needed for each candidate feed tank. Additional samples may be taken if needed to confirm that processing criteria will be met. Table 5.1 should be used when determining the specific sampling locations:

Table 5-1 Sample Point Selection

Number of Samples	Location of Sample Points
Two Samples	One sample taken from the upper half of the waste from one riser and the other sample taken from the lower half of the waste from another riser.
Three Samples	Two Samples taken from one riser (one from the top half and the other from the bottom half of the waste) and one sample from another riser (determined by random number generator).
Four Samples	Two samples taken from each of two separate risers. One sample is to be taken from the top half of the waste and one from the bottom half of the waste from each of the selected risers.
Five Samples	Same as for four samples except one sample from either the top or bottom half of the tank will be taken from a third riser

Riser selection will be made by numbering the available risers which are at least 15 feet from each other and using a random number generator to select which risers will be used. Sample depth will be determined by dividing the tank level into one foot

increments and then by using a random number generator to determine a depth which meets the criteria given in Table 5-1.

Presence of a separable organic layer is determined by collection of one additional surface grab sample from each of the candidate feed tanks. The samples are analyzed for TOC as well as a visual determination and compared to the TOC for the supernate layer in the tanks to determine if a separable organic layer is present. Analytical data taken for other purposes (such as from a compatibility study) can be used for the determination of the presence of a separable organic layer if it is available and meets the evaporator program requirements.

The requirements contained in the latest editions of the 242-A Evaporator/LERF DQO (Von Bargen 1995) and the 242-A Evaporator Quality Assurance Project Plan (Basra 1995) regarding QA/QC requirements, sample size, and holding times must be met. A chain of custody must also be completed for all samples required to be taken by this plan. The chain of custody must include a discrete sample number, date and time sample was taken, shipment number, and signature.

5.3 ANALYTE SELECTION AND RATIONALE

The 242-A Evaporator/LERF DQO Document (Von Bargen 1995) examined the data needs for sampling the candidate feed tanks and determined that the analyses in Table 5-2 should be conducted in order to satisfy WAC 173-303-300 (b) requirements. The 242-A Evaporator/LERF DQO Document (Von Bargen 1995) contains additional information on how and why these analytes were selected.

5.4 ANALYTICAL METHODS AND QA/QC

Performance based specifications rather than procedure based specifications were used for determining appropriate analytical methods due to problems associated with analysis of waste with high radioactivity and the sample matrix. This allows adjustments for Hanford site-specific issues while ensuring acceptable data quality. The test methods which must be followed are included in Table 5-2. The analyses will in some cases deviate from SW-846 specifications for holding times, sample preservation, and other specific analytical procedures. These deviations are discussed in *Analytical Methods for Mixed Waste Analysis at the Hanford Site* (DOE/RL 1994). All analytical and sampling methods conducted as part of this plan must meet the data quality requirements contained in the latest editions of the 242-A Evaporator/LERF DQO (Von Bargen 1995) and the 242-A Evaporator Quality Assurance Project Plan (Basra 1995).

Figure 5-1 Strategy for Determining the Number of Candidate Feed Tank Samples.

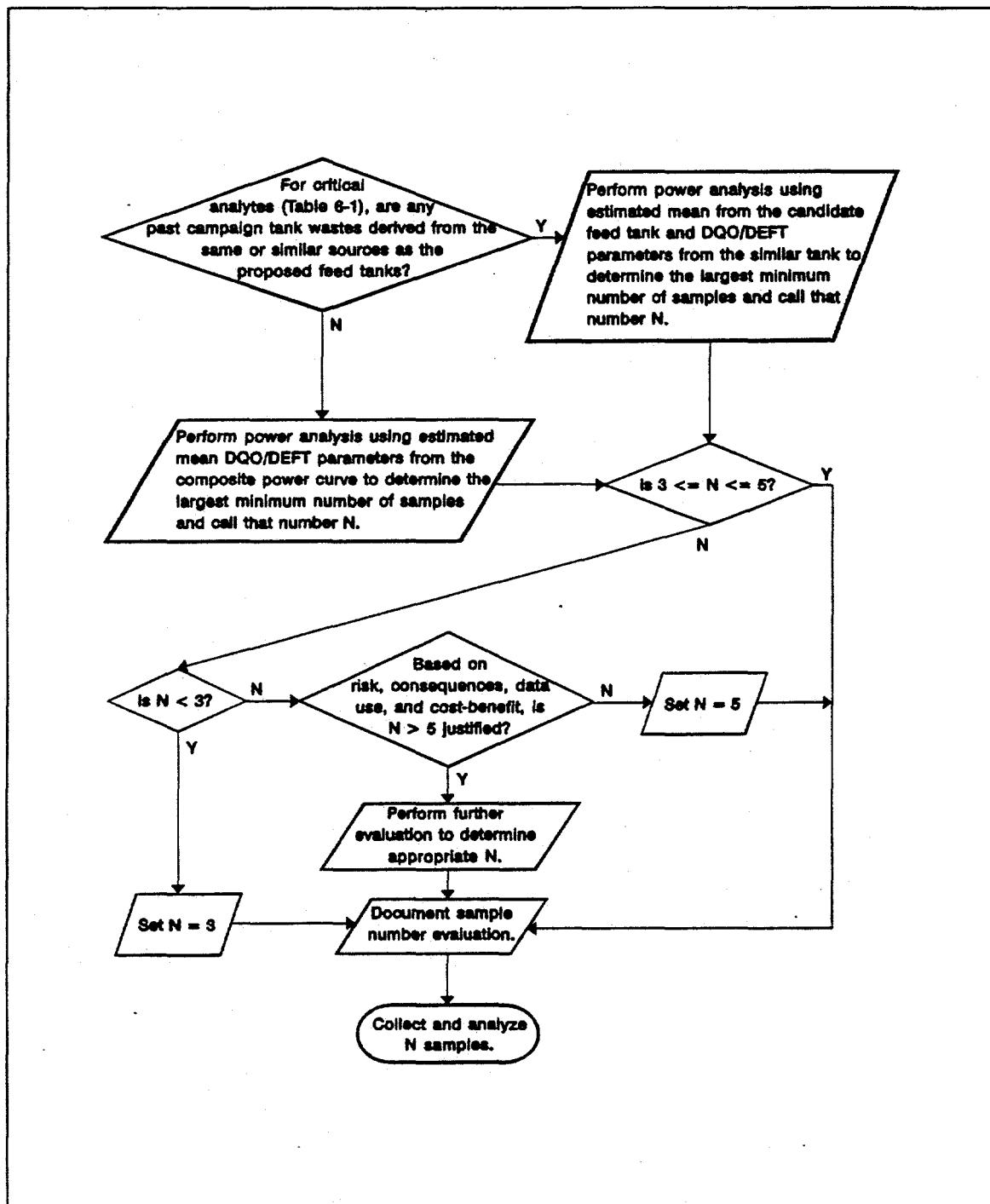


Figure 5-2 Strategy for Verifying the Number of Candidate Feed Tank Samples.

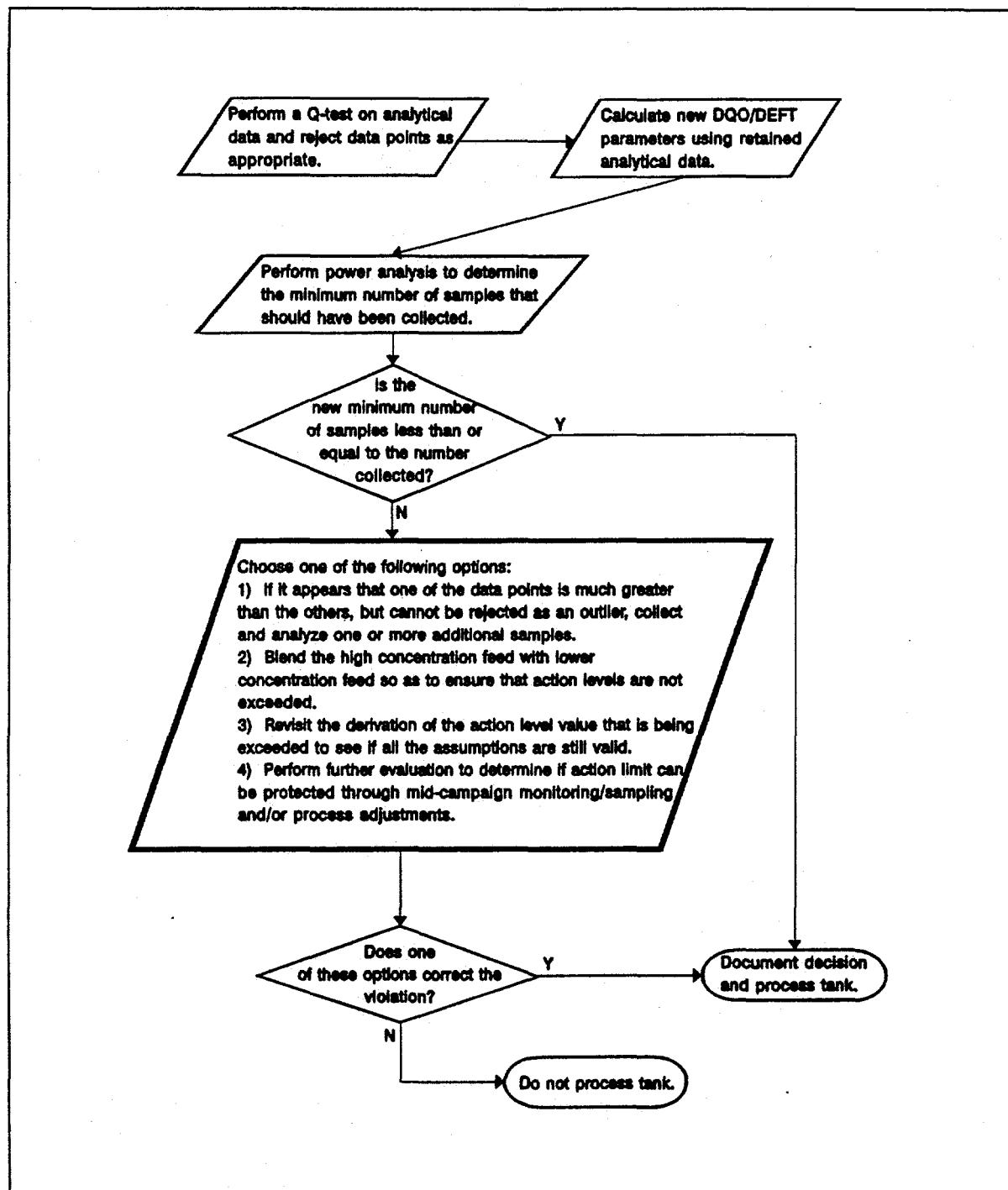


Table 5-2 Analytes for Candidate Feed Tanks

Parameter	Test Method	Analyte	Rationale
Exotherm	Differential Scanning Calorimeter	Temperature and Energy	Verify that the waste will not undergo an exothermic reaction.
Compatibility Test	Mixing and compatibility study	Visual physical changes	Verify that the wastes are chemically compatible.
Organic Compounds	GC/MS, or GC/FID, or Heated Headspace GC or GC/MS	Acetone, 1-Butanol, 1-Butoxyethanol, 1-Butanone, 2-Hexanone, 2-Pentanone, Tetrahydrofuran, Methyl isobutyl ketone, Tri-butyl phosphate	Used in calculations to verify that Vessel Vent emissions will not exceed regulatory limits and to prevent compatibility problems with the LERF liner.
Ammonia	Kjeldahl Distillation/ Autotitration, or Ion Selective Electrode	Ammonia	Verify that the ammonia content of the process condensate will be below the Extremely Hazardous Waste levels.

6.0 REFERENCES

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