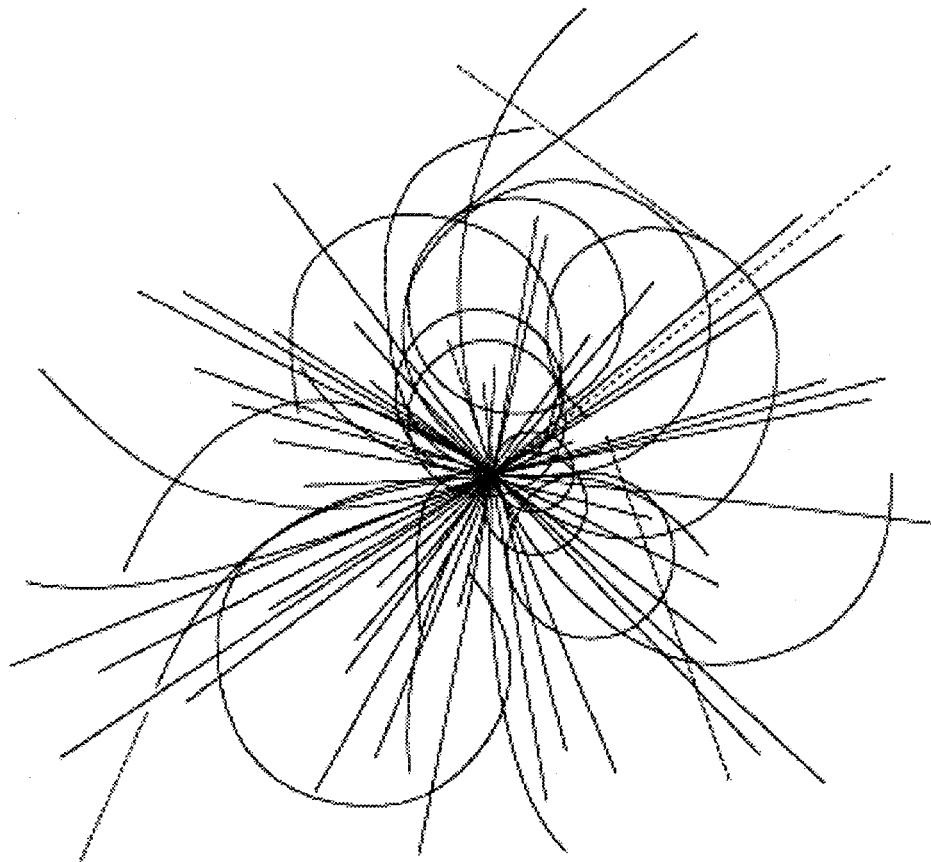


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Superconducting Super Collider
Laboratory

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CORRECTOR MAGNETS: COMBINED STRUCTURAL ANALYSIS OF COLLIDER 50MM APERTURE ORDERED WOUND SEXTUPOLES INTERIOR SECTION

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ABSTRACT

The 50mm aperture prototype collider ordered wound sextupole corrector magnets have been modeled with finite element techniques considering the individual and combined load cases of the preloading from keys, cooldown to 4 K and the effect of magnetic forces during energizing. Results of the analysis are presented as longitudinal, transverse and shear stresses for the ordered wound coils and as maximum von Mises stress for the carbon steel outer laminations, the stainless steel inner lamination, the carbon steel floating pole tips and the carbon steel keys.

INTRODUCTION

The sextupole corrector magnets are members of the collider ring correctors which are responsible for linear chromaticity control of the proton beams. These corrector magnets are located inside of the spool piece. This paper presents results from a finite element stress analysis of the 50mm aperture prototype collider ordered wound sextupole corrector magnets. This analysis considers only the interior cross-sections along the length of the structure - which differ greatly from the end sections. The coils for this sextupole magnet structure are manufactured using ordered wound techniques. Load cases involved in the analysis include preloading from keys, cooldown to 4 K and magnetic (Lorentz) forces from energizing. The objectives of this stress analysis for the corrector magnet sextupole structure are to determine the stress in the ordered wound coils, the necessary shim thickness around the coils and to evaluate the capability of the outer laminations, inner laminations, floating pole tips and keys to resist the stress induced by reaction with the coils. The results of this analysis will be used as reference for further design of the sextupole structure members - including the coils, the inner laminations, the outer laminations and the keys.

The sextupole magnet structures consist of magnetic coils held in place by a series of thin, interlocking carbon steel outer laminations. Figure 1 shows two consecutive cross-sections of the sextupole. The outer laminations are configured such that each cross-section of the magnetic structure along the longitudinal axis of the coils contains four interlocking outer lamination pieces. Each outer lamination piece is joined to the pieces immediately in front of and behind it by two continuous pins. Continuous longitudinal carbon steel alignment keys (on the right and left sides) and lock keys (on the top and bottom sides) provide the "preload" forces necessary to hold the outer laminations in

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place and to exert pressure on the coils. The outer laminations sections immediately in front of and behind each individual outer laminations section are identical in geometry but are rotated 180 degrees about the vertical axis (y-axis), yielding the same external shape but a different configuration at the alignment and lock keys. The alternating orientation of the outer lamination pieces permits the "elbow" section of each outer lamination piece keyway to be alternately placed above or below the alignment keys and placed on the left or right side of the lock keys. There are two floating pole tips located on the left and right sides of the inner laminations. Layer of Kapton are placed around the coil to act as a shim. Therefore, one of the design criteria in this analysis is to provide enough shim thickness to have the minimum stress in the coil after cooldown to be at least greater than the maximum stress in the coil due to magnetic forces only. This criteria should be applied to each coil's local longitudinal, transverse and shear direction stresses in the coils. The ordered wound coil structure consists of continual loops of 0.381 mm (15.0 mil)-diameter superconducting Cu:Nb-Ti (2.2:1) wire insulated with a 0.076 mm (3.0 mil)-thick layer of Kapton and Dupont XMPI adhesive.

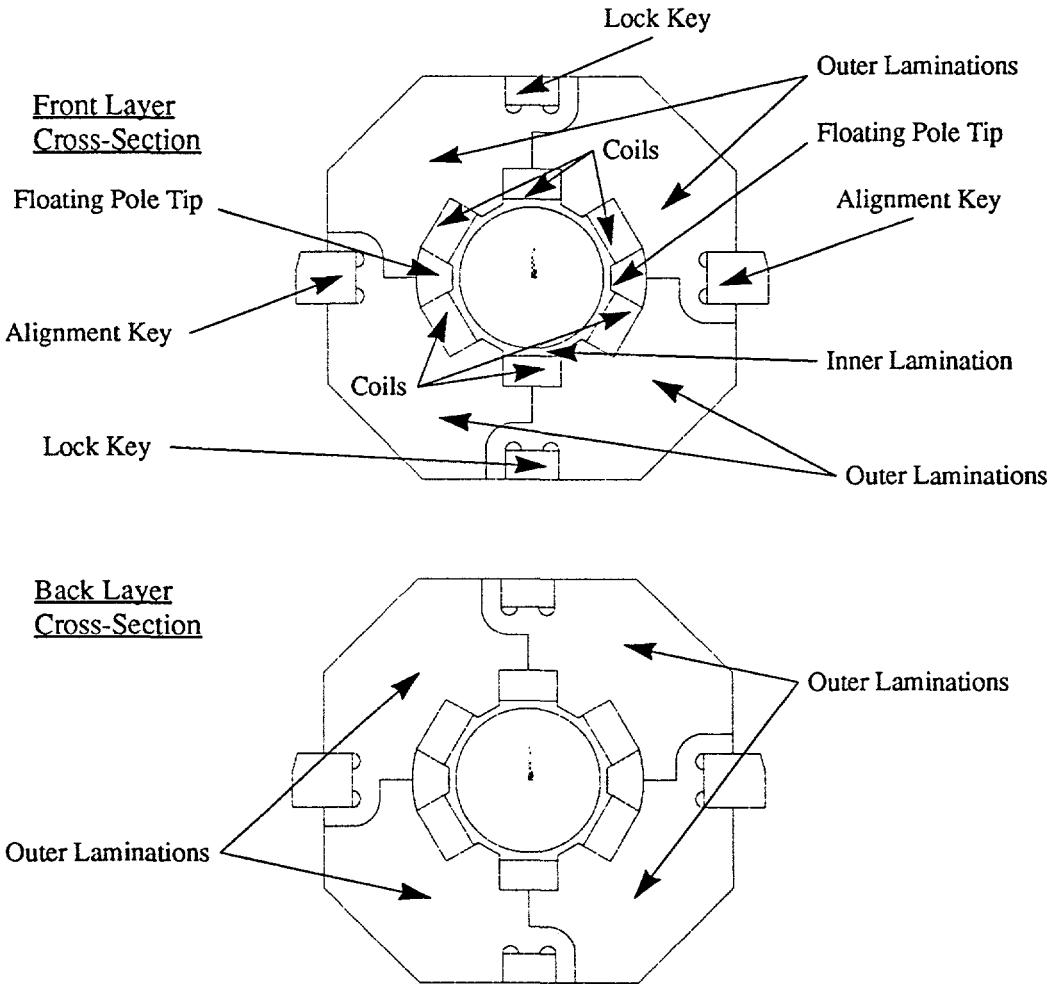


Figure 1. Collider 50mm Aperture Ordered Wound Sextupoles - Front and Back Layer Cross-Sections

MODEL CONSTRUCTION

The magnet assembly is modeled as a two-dimensional finite element system using ANSYS finite element code. The model consists of two adjacent layers of outer laminations (each consisting of four outer lamination pieces from the same cross-section) hereafter referred to as the "front" and "back" outer laminations. To get the correct loading from the keys, the two layers of the outer laminations are modeled with two-dimensional plane stress elements. The front and back outer laminations are linked together by the coupled nodes at each of the eight continuous pin locations. Gap elements having a positive gap distance to act as an interference are used to join the coils to the outer laminations (gap elements only transmit compression load not tension load). These positive gap distance represent the thickness of the shim around the coils. All other gap elements between various

parts are given a zero value. The coils, inner lamination, floating pole tips and keys are constructed from two-dimensional plane stress elements. Material properties used in this model are shown in Table 1. Material properties for the ordered wound coils are obtained from testing and analysis.

Table 1. Material Properties

Materials		Carbon Steel	304L Stainless Steel ¹	Ordered Wound Coil
Young's Modulus (psi)	T = 293 K	30.0×10^6	27.6×10^6	200,000
	T = 4 K	30.6×10^6	29.2×10^6	300,000
Poisson's Ratio	T = 293 K	0.292	0.29	0.346
	T = 4 K	0.292	0.2788	0.339
Thermal Expansion ² Coefficients, (K ⁻¹)		0.685×10^{-5}	1.059×10^{-5}	1.4×10^{-5}
Yield Tensile Strength (psi)	T = 293 K	25,000	58,900	N/A
	T = 4 K	54,000	79,400	N/A
Ultimate Tensile Strength (psi)	T = 293 K	42,000	95,500	N/A
	T = 4 K	65,000	241,000	N/A

LOADING CASES

Preload Case

As mentioned previously, the preloading case experienced upon assembly is simulated by assigning to all the gap elements around the four coils an overlapping gap distance to represent the shim thickness. All material properties for the preload case are referenced to 293 K.

Preload and Cooldown Case

The combined analysis of the preload and the cooldown uses the same model as does the preload alone except that the model is assigned an initial temperature of 293 K and a final temperature of 4 K to represent the cryogenic state after the cooldown has occurred. All material properties for the combined analysis are given at the reference temperature of 4 K.

Magnetic Forces Case

To complete a magnetic stress analysis of the model, a separate magnetic analysis must first be conducted. The magnetic analysis is performed using a somewhat simplified version of the sextupole model. The magnetic analysis is concerned only with the location and the magnetic properties of sextupole structure components; therefore, the model used in the said analysis contains only the geometric and physical description of the individual components and does not require the use of gap elements. The wire in the coils are given a current density of 4.3884×10^8 A/m² at 100% of short sample current, but only 66% is required for operation current. The forces on the nodes of the coils are computed in the magnetic analysis and then inserted into the standard sextupole model. A finite element analysis is then performed on the standard model with the magnetic forces alone to determine the influence of the magnetic forces on the sextupole structure.

Preload, Cooldown and Magnetic Forces Case

To complete the final combined analysis, the standard sextupole model is subjected to the simultaneous loadings of the preload, cooldown and magnetic forces. Once again, a finite element analysis is performed to determine the stresses on the individual components of the coil structure due to the three combined loading cases.

STRESS ANALYSIS RESULTS

In order to have the minimum stresses in the coils after cooldown to be at least greater than the maximum stresses in the coils due to magnetic forces only, the finite element analysis shows that shim thickness of 3 and 6 mils must be used along the two shorter and one longer lengths of all the coils, respectively. These results are shown on Table 2. As shown in Table 2 for the coils the first value is the minimum and the second is the maximum, thus showing the range of stresses in the coils. The longitudinal and transverse directions are defined along the longer and shorter length of the coils, respectively.

Table 2. Stress Levels for Collider Ordered Wound Sextupoles

Loading Cases		Preload of Keys shim1 = 3 mils * shim2 = 6 mils **	Preload of Keys & Cool Down to 4 K	Magnetic Forces Only $I = 66\% I_{ss}$ or $110\% I_{op}$	Preload of Keys & Cool Down & Magnetic Forces
Coils Min : Max Stress (psi)	$\sigma_{transverse}$	-1,187 : -954	-877 : -657	-505 : -80	-927 : -478
	$\sigma_{longitudinal}$	-672 : -515	-586 : -426	-372 : -17	-618 : -282
	τ_{shear}	-34 : 34	-33 : 33	-38 : 20	-14 : 21
C.S. Outer Laminations Max. von Mises Stress (psi)		57,200	44,000	18,000	45,300
C.S. Floating Pole Tips Max. von Mises Stress (psi)		4,500	4,000	50	3,000
C.S. Keys Max. von Mises Stress (psi)		31,300	23,100	10,800	23,700
S.S. Inner Laminations Max. von Mises Stress (psi)		15,500	10,900	700	6,800
* shim1 = shim thickness between the two shorter lengths of coils and outer laminations ** shim2 = shim thickness between the longer length of coils and outer laminations					

CONCLUSION

The finite element analysis for the 50mm aperture collider ordered wound sextupole corrector magnets shows that at shim thickness of 3 and 6 mils, there are sufficient stresses in the coils to restrain movement. The stresses in the coils have peak values of maximum and minimum, therefore, further design of the sextupoles should try to reduce these peak values and get an evenly distributed stresses in the coils. It should be noted that different values for the material properties of coils will greatly effect the design and analysis. Therefore, accurate values of coils material properties must be obtained for further design and analysis. It should also be remembered that this analysis considers only cross-sections from the interior of the structure in a two-dimensional frame. As the cross-sections at the ends of the sextupole structure differ significantly from those in the interior, additional analyses must be performed to evaluate their behavior.

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