

OFFICE OF CIVILIAN RADIOACTIVE WASTE MANAGEMENT CALCULATION COVER SHEET

1. QA: QA

Page: 1

Of: 15

2. Calculation Title

Horizontal Lifting of 5 DHLW/DOE - Long, 12-PWR Long and 24-BWR Waste Packages

3. Document Identifier (including Revision Number)

CAL-EBS-ME-000010 REV 00

4. Total Attachments

7

5. Attachment Numbers - Number of pages in each

I-4, II-4, III-4, IV-9, Attachments V through VII are on one CD (See Remarks).

	Print Name	Signature	Date
6. Originator	Valérie de la Brosse	<i>V. de la Brosse</i>	05/17/01
7. Checker	Sreten Mastilovic	<i>Sreten Mastilovic</i>	05/17/2001
8. Lead	Scott M. Bennett	<i>Scott M. Bennett</i>	05/18/01

9. Remarks

Attachments V through VII are electronic media attachments (compact disc) containing ANSYS V5.4 electronic files. The name, size, date and time of creation of each file are listed in section 8 of this document.

Revision History

10. Revision No.	11. Description of Revision
00	Initial Issue

CONTENTS

	Page
1. PURPOSE	4
2. METHOD	4
3. ASSUMPTIONS	4
4. USE OF COMPUTER SOFTWARE AND MODELS	6
4.1 SOFTWARE	6
4.2 SOFTWARE ROUTINES	6
4.3 MODELS	6
5. CALCULATION	7
5.1 MATERIAL PROPERTIES	7
5.2 MASS OF PWR FUEL ASSEMBLIES	8
5.3 MASS OF BWR FUEL ASSEMBLIES	8
5.4 FINITE ELEMENT REPRESENTATIONS	8
6. RESULTS	10
7. REFERENCES	12
8. ATTACHMENTS	14

TABLES

Page

1. Maximum Stress Intensities for the 5 DHLW/DOE - Long Waste Package at Three Different Temperatures.....	10
2. Maximum Stress Intensities for the 12-PWR Long Waste Package at 316°C	11
3. Maximum Stress Intensities for the 24-BWR Waste Package at 316°C	11
4. Name, Size, Date and Time of Creation of the Files in Attachments V to VII	15

1. PURPOSE

The objective of this calculation was to determine the structural response of a 12-Pressurized Water Reactor (PWR) Long, a 24-Boiling Water Reactor (BWR) and a 5-Defense High Level Waste/Department of Energy (DHLW/DOE) - Long spent nuclear fuel waste packages lifted in a horizontal position (see Ref. 8, Section 1.2.1.18). The scope of this calculation was limited to reporting the calculation results in terms of maximum stress intensities in the trunnion collar sleeves. In addition, the maximum stress intensities in the inner and outer shells of the waste packages were presented for illustrative purposes. The information provided by the sketches (Attachments I, II and III) is that of the potential design of the types of waste packages considered in this calculation, and all obtained results are valid for these designs only. This calculation is associated with the waste package design and was performed by the Waste Package Design Section in accordance with the *Technical work plan for: Waste Package Design Description for LA* (Ref. 7). AP-3.12Q, *Calculations* (Ref. 13), was used to perform the calculation and develop the document.

2. METHOD

The finite element calculations were performed using the commercially available ANSYS version (V) 5.4 (Ref. 6) finite element code. The results of these calculations are provided in terms of stress intensities.

With regard to the development of this calculation, the control of the electronic management of data was accomplished in accordance with the *Technical work plan for: Waste Package Design Description for LA* (Ref. 7) and evaluated in accordance with AP-SV.1Q, *Control of the Electronic Management of Information* (Ref. 14). The evaluation (Addendum B of Ref. 7) determined that current work processes and procedures are adequate for the control of electronic management of data for this activity.

3. ASSUMPTIONS

In the course of developing this document, the following assumptions were made regarding the structural calculations for the waste packages.

- 3.1 Some of the temperature-dependent material properties were not available for SB-575 N06022 (Alloy 22) and SA-240 S31600 (316 nuclear grade [NG] stainless steel [SS]). Therefore, room-temperature (RT) (20°C) density and RT Poisson's ratio were assumed for both materials used. The impact of using RT density and RT Poisson's ratio was anticipated to be small. The rationale for this assumption was that the mechanical properties of these materials do not change significantly at the temperatures experienced during handling and lifting operations. This assumption was used in Section 5.1.
- 3.2 The Poisson's ratio of Alloy 22 was not available in literature. Therefore, the Poisson's ratio of Alloy 625 (SB-443 N06625) was assumed for Alloy 22. The impact of this assumption

was anticipated to be negligible. The rationale for this assumption was that the chemical compositions of Alloy 22 and Alloy 625 are similar (see Ref. 2 and Ref. 1, respectively). This assumption was used in Section 5.1.

- 3.3 The masses of the BWR and PWR fuel assemblies were increased by 25 lbs. The rationale for this assumption was to take into account potential variations in fuel assembly weight while providing a set of bounding results. This assumption was used in Section 5.2 and 5.3.

4. USE OF COMPUTER SOFTWARE AND MODELS

4.1 SOFTWARE

The finite element analysis (FEA) computer code used for this calculation is ANSYS V5.4 (see Ref. 6), which was obtained from Software Configuration Management in accordance with appropriate procedures, and is identified by the Computer Software Configuration Item number 30040 V5.4. ANSYS V5.4 is a commercially available FEA code and is appropriate for structural calculations of waste packages as performed in this calculation. The calculations using the ANSYS V5.4 software were executed on the Hewlett-Packard (HP) 9000 series workstation identified with YMP (Yucca Mountain Project) tag number 117161. The software qualification of ANSYS V5.4 was summarized in reference 6. The ANSYS evaluation performed for this calculation is fully within the range of the validation performed for the ANSYS V5.4 code. Access to the code was granted by the Software Configuration Secretariat in accordance with the appropriate procedures.

The input files (identified by .inp file extensions) and output files (identified by .out file extensions) for ANSYS V5.4 are provided in Attachments V, VI and VII.

4.2 SOFTWARE ROUTINES

None used.

4.3 MODELS

None used.

5. CALCULATION

5.1 MATERIAL PROPERTIES

Material properties used in this calculation are listed in this section. Some of the temperature-dependent material properties were not available for Alloy 22 and 316NG SS. Therefore, RT density and RT Poisson's ratio were used for Alloy 22 and 316NG SS (see Assumption 3.1).

SB-575 N06022 (Alloy 22) (outer shell, outer shell lids, extended outer shell lid, upper and lower trunnion collar sleeves, and inner shell support ring):

- Density = 8690 kg/m^3 (0.314 lb/in^3) (at RT) (Ref. 2, SB-575 Section 7.1)
- Yield strength = 310 MPa (45 ksi) (at RT) (Ref. 2, Table Y-1)
Yield strength = 236 MPa (34.3 ksi) (at $400^\circ\text{F} = 204^\circ\text{C}$) (Ref. 2, Table Y-1)
Yield strength = 211 MPa (30.6 ksi) (at $600^\circ\text{F} = 316^\circ\text{C}$) (Ref. 2, Table Y-1)
- Poisson's ratio = 0.278 (at RT) (Ref. 1, p. 143; see Assumption 3.2)
- Modulus of elasticity = 206 GPa (at RT) (Ref. 12, p. 14)
Modulus of elasticity = 196 GPa (at $400^\circ\text{F} = 204^\circ\text{C}$) (Ref. 12, p. 14)
Modulus of elasticity = 190 GPa (at $600^\circ\text{F} = 316^\circ\text{C}$) (Ref. 12, p. 14)

SA-240 S31600 (316NG SS, which is 316 SS with tightened control on carbon and nitrogen content and has the same material properties as 316 SS [see Ref. 2, page 931 and Ref. 2, Section II, SA-240 Table 1]) (Inner shell and inner shell lids):

- Density = 7980 kg/m^3 (at RT) (Ref. 4, Table X1, p. 7)
- Yield strength = 207 MPa (30 ksi) (at RT) (Ref. 2, Table Y-1)
Yield strength = 148 MPa (21.4 ksi) (at $400^\circ\text{F} = 204^\circ\text{C}$) (Ref. 2, Table Y-1)
Yield strength = 130 MPa (18.9 ksi) (at $600^\circ\text{F} = 316^\circ\text{C}$) (Ref. 2, Table Y-1)
- Poisson's ratio = 0.298 (at RT) (Ref. 1, Figure 15, p. 755)
- Modulus of elasticity = 195 GPa ($28.3 \cdot 10^6 \text{ psi}$) (at RT) (Ref. 2, Table TM-1)
Modulus of elasticity = 183 GPa ($26.5 \cdot 10^6 \text{ psi}$) (at $400^\circ\text{F} = 204^\circ\text{C}$) (Ref. 2, Table TM-1)
Modulus of elasticity = 174 GPa ($25.3 \cdot 10^6 \text{ psi}$) (at $600^\circ\text{F} = 316^\circ\text{C}$) (Ref. 2, Table TM-1)

5.2 MASS OF PWR FUEL ASSEMBLIES

This calculation was performed by using the following mass of the PWR fuel assemblies (Ref. 8, Table 2, p. 10 and Assumption 3.3):

$$\text{Total mass} = 1920 + 25 = 1945 \text{ lbs (882.2 kg)}$$

5.3 MASS OF BWR FUEL ASSEMBLIES

This calculation was performed by using the following mass of the BWR fuel assemblies (Ref. 8, Table 1, p. 10 and Assumption 3.3):

$$\text{Total mass} = 699 + 25 = 724 \text{ lbs (328.4 kg)}$$

5.4 FINITE ELEMENT REPRESENTATIONS

A three-dimensional FER of each waste package was developed in ANSYS V5.4 using the dimensions provided in Attachments I, II and III.

The internal structure of the waste packages was simplified as follow: The fuel plates and tubes, the basket sideguides and stiffeners and the fuel assemblies were not taken into account in the FER representation of the 12-PWR long and 24-BWR waste packages. The FER representation of the 5 DHLW/DOE - long does not include the divider plates, brackets, support tubes, HLW glass assemblies and canister. Nevertheless, the mass of those elements were taken into account in the mass of the inner shell of the corresponding waste package. The lid lifting features were not represented in the FER either. Their mass was taken into account in the mass of the lid they are attached to. Furthermore, the densities of all components of the waste packages were adjusted so that the masses of the waste packages match the masses given in Attachment I, II and III.

Besides, the inner and outer shells were represented with solid connections at their adjacent surfaces, although reference 9 specifies loose fit between those two components. However, since the structural performance of the trunnion collar sleeves was the main objective of this calculation and total force acting on the trunnion collar sleeves remained unchanged, this had no impact on the results for the trunnion collar sleeves.

Due to the geometry and loadings of these calculations, half-symmetry models were used.

The benefit of using this approach was to reduce the computer execution time while preserving all features of the problem relevant to the structural calculation.

The mesh of each FER was appropriately generated and refined in the contact region according to standard engineering practice. Thus, the accuracy and representativeness of the results of this calculation were deemed acceptable. The meshes of the 5 DHLW/DOE - long, 12-PWR long and 24-BWR waste packages are presented in Figures 1, 5 and 7 of Attachment IV, respectively.

Each FER was then used in ANSYS V5.4 to perform the static analysis for the 5 DHLW/DOE - long,

Waste Package Project

Title: Horizontal Lifting of 5 DHLW/DOE - Long, 12-PWR Long and 24-BWR Waste Packages
Document Identifier: CAL-EBS-ME-000010 REV 00

Page 9 of 15

12-PWR long and 24-BWR waste packages horizontal lifting (See Ref. 8) at RT, 204 °C , and 316 °C .

6. RESULTS

The maximum stresses were found by examining the results of the calculations for each part of the waste packages. Table 1 lists the maximum stress intensities in the outer and inner shells, as well as in the trunnion collar sleeves of the 5 DHLW/DOE - long waste package at three different temperatures: RT, 204 °C, and 316 °C. Figures 2, 3 and 4 of Attachment IV show the stress intensities in the 5 DHLW/DOE - long waste package at those temperatures.

Table 1. Maximum Stress Intensities for the 5 DHLW/DOE - Long Waste Package at Three Different Temperatures

Temperature	5 DHLW/DOE - Long		
	Inner Shell and Lids	Outer Shell and Lids	Trunnion Collar Sleeves
RT	3.4 MPa (see Att. V, post5DRT.out, line 483)	5.1 MPa (see Att. V, post5DRT.out, line 395)	5.1 MPa (see Att. V, post5DRT.out, line 294)
204 °C	3.4 MPa (see Att. V, post5D400.out, line 483)	5.1 MPa (see Att. V, post5D400.out, line 395)	5.0 MPa (see Att. V, post5D400.out, line 294)
316 °C	3.4 MPa (see Att. V, post5D600.out, line 483)	5.2 MPa (see Att. V, post5D600.out, line 395)	5.0 MPa (see Att. V, post5D600.out, line 294)

The above table shows that for each temperature condition, the maximum stress intensities in the outer and inner shells, as well as in the trunnion collar sleeves, of the 5 DHLW/DOE - long were far lower than the yield strength of the corresponding materials (see Sections 5.1). Furthermore, it shows that the increase of temperature has a negligible influence on the results. Therefore, for the two other waste package designs -12-PWR long and 24-BWR-, the behavior of the waste package was studied only at 316°C.

Remark: As noted in Section 5.4, the inner and outer shells were represented with solid connections at their adjacent surfaces, although reference 9 specifies loose fit between those two components. Although this approach had no impact on the results in the trunnion collar sleeves, this could affect the results in the inner and outer shells of the waste packages. Nevertheless, considering that the level of the maximum stress intensities in these components were low, and that these components were of secondary importance in this study, the representation of the connection between inner and outer shell in the FER was deemed acceptable for the purpose of this calculation.

The maximum stress intensities in the outer and inner shells, as well as in the trunnion collar sleeves, of the 12-PWR long waste package at 316°C are presented in Table 2. Figure 6 of Attachment IV shows the stress intensities in the 12-PWR long waste package at this temperature.

Waste Package Project

Title: Horizontal Lifting of 5 DHLW/DOE - Long, 12-PWR Long and 24-BWR Waste Packages
Document Identifier: CAL-EBS-ME-000010 REV 00

Page 11 of 15

Table 2. Maximum Stress Intensities for the 12-PWR Long Waste Package at 316°C

Temperature	12-PWR Long		
	Inner Shell and Lids	Outer Shell and Lids	Trunnion Collar Sleeves
316 °C	4.0 MPa (see Att. VI, post12PWR.out, line 483)	6.1 MPa (see Att. VI, post12PWR.out, line 395)	5.7 MPa (see Att. VI, post12PWR.out, line 294)

The maximum stress intensities in the outer and inner shells, as well as in the trunnion collar sleeves of the 24-BWR waste package at 316°C are presented in Table 3. Figure 8 of Attachment IV shows the stress intensities in the 24-BWR waste package at this temperature.

Table 3. Maximum Stress Intensities for the 24-BWR Waste Package at 316°C

Temperature	24-BWR		
	Inner Shell and Lids	Outer Shell and Lids	Trunnion Collar Sleeves
316 °C	3.4 MPa (see Att. VII, post24BWR.out, line 483)	5.2 MPa (see Att. VII, post24BWR.out, line 395)	5.0 MPa (see Att. VII, post24BWR.out, line 294)

The values of the stress intensities were far lower than the yield strength of the corresponding material in both inner and outer shell, and in the trunnion collar sleeves, for the 12-PWR long and 24-BWR waste package designs.

7. REFERENCES

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3. ASME (American Society of Mechanical Engineers) 1998. *1998 ASME Boiler and Pressure Vessel Code*. 1998 Edition with 1999 and 2000 Addenda. New York, New York: American Society of Mechanical Engineers. TIC: 247429.
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10. DOE (U.S. Department of Energy) 1998. "Design Specification." Volume 1 of *Preliminary Design Specification for Department of Energy Standardized Spent Nuclear Fuel Canisters*. DOE/SNF/REP-011, Rev. 1. Washington, D.C.: U.S. Department of Energy, Office of Spent Fuel Management and Special Projects. TIC: 241528.
11. DOE (U.S. Department of Energy) 1999. *Waste Acceptance System Requirements Document*. DOE/RW-0351, Rev. 03. Washington, D.C.: U.S. Department of Energy, Office of Civilian Radioactive Waste Management. ACC: HQO.19990226.0001.
12. Haynes International 1997. *Hastelloy C-22 Alloy*. Kokomo, Indiana: Haynes International. TIC: 238121.

Waste Package Project

Title: Horizontal Lifting of 5 DHLW/DOE - Long, 12-PWR Long and 24-BWR Waste Packages

Document Identifier: CAL-EBS-ME-000010 REV 00

Page 13 of 15

13. AP-3.12Q, Rev. 0, ICN 4. *Calculations*. Washington, D.C.: U.S. Department of Energy, Office of Civilian Radioactive Waste Management. ACC: MOL.20010404.0008
14. AP-SV.1Q, Rev. 0, ICN 2. *Control of the Electronic Management of Information*. Washington, D.C.: U.S. Department of Energy, Office of Civilian Radioactive Waste Management. ACC: MOL.20000831.0065

8. ATTACHMENTS

- Attachment I: Design sketches (*5 DHLW/DOE SNF - long waste package configuration for Site Recommendation* [SK-0200 REV 04] and *5 DHLW/DOE SNF - long weld configuration* [SK-0201 REV 00]. This attachment uses Ref. 10 and 11)
- Attachment II: Design sketches (*12-PWR long waste package configuration for Site Recommendation* [SK-0183 REV 01] and *12-PWR long waste package weld configuration* [SK-0205 REV 00]. This attachment uses Ref. 5)
- Attachment III: Design sketches (*24-BWR waste package configuration for Site Recommendation* [SK-0184 REV 00] and *24-BWR waste package assembly weld configuration* [SK-0202 REV 00]. This attachment uses Ref. 5)
- Attachment IV: Figures obtained from ANSYS V5.4 for the horizontal lifting of the 5 DHLW/DOE - long, 12-PWR long and 24-BWR waste packages
- Attachments V to VII (Compact Disc):
ANSYS V5.4 electronic files for the horizontal lifting of the 5 DHLW/DOE - long, 12-PWR long and 24-BWR waste packages
- Table 4 contains the name, size, date and time of creation of each file in Attachments V to VII.

Table 4. Name, Size, Date and Time of Creation of the Files in Attachments V to VII

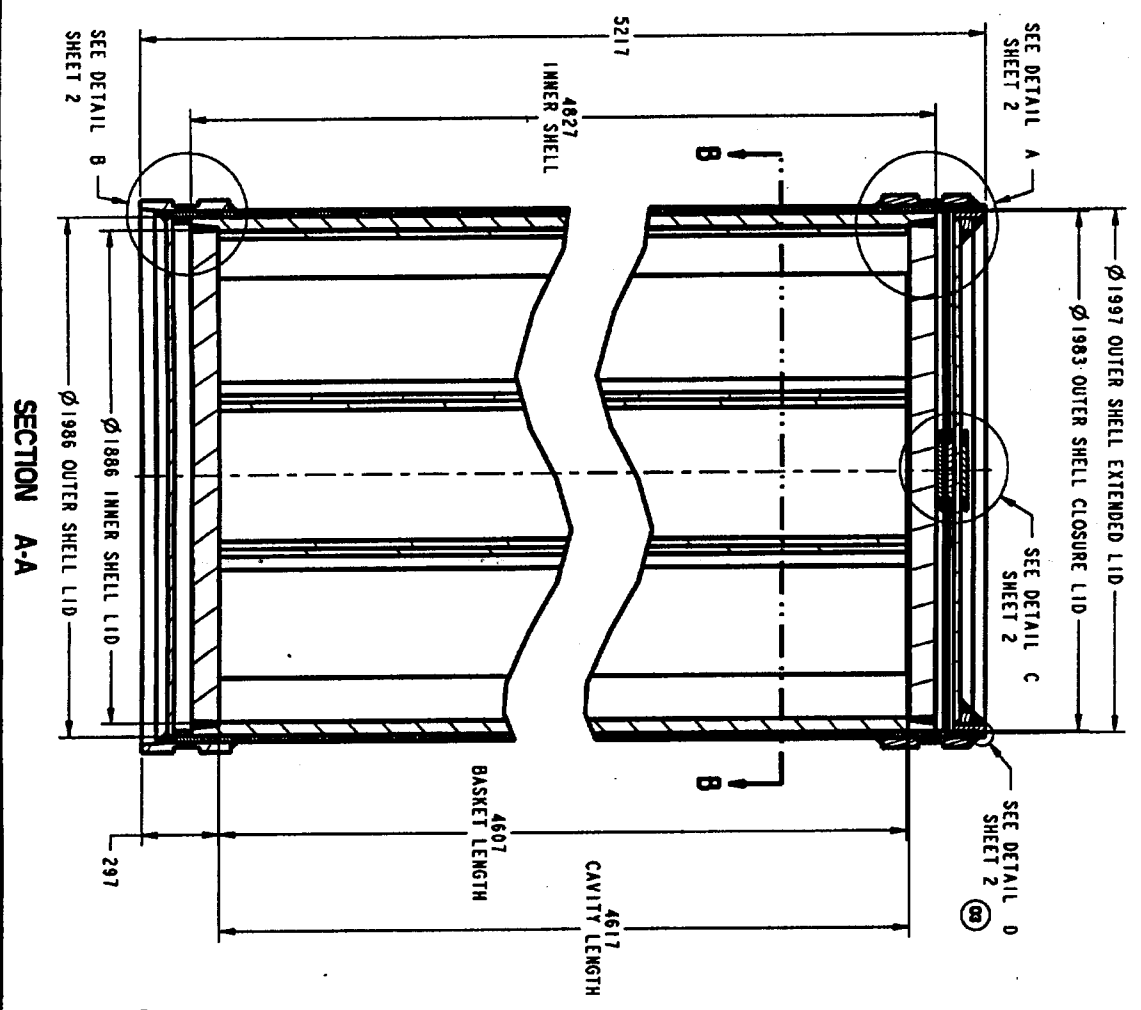
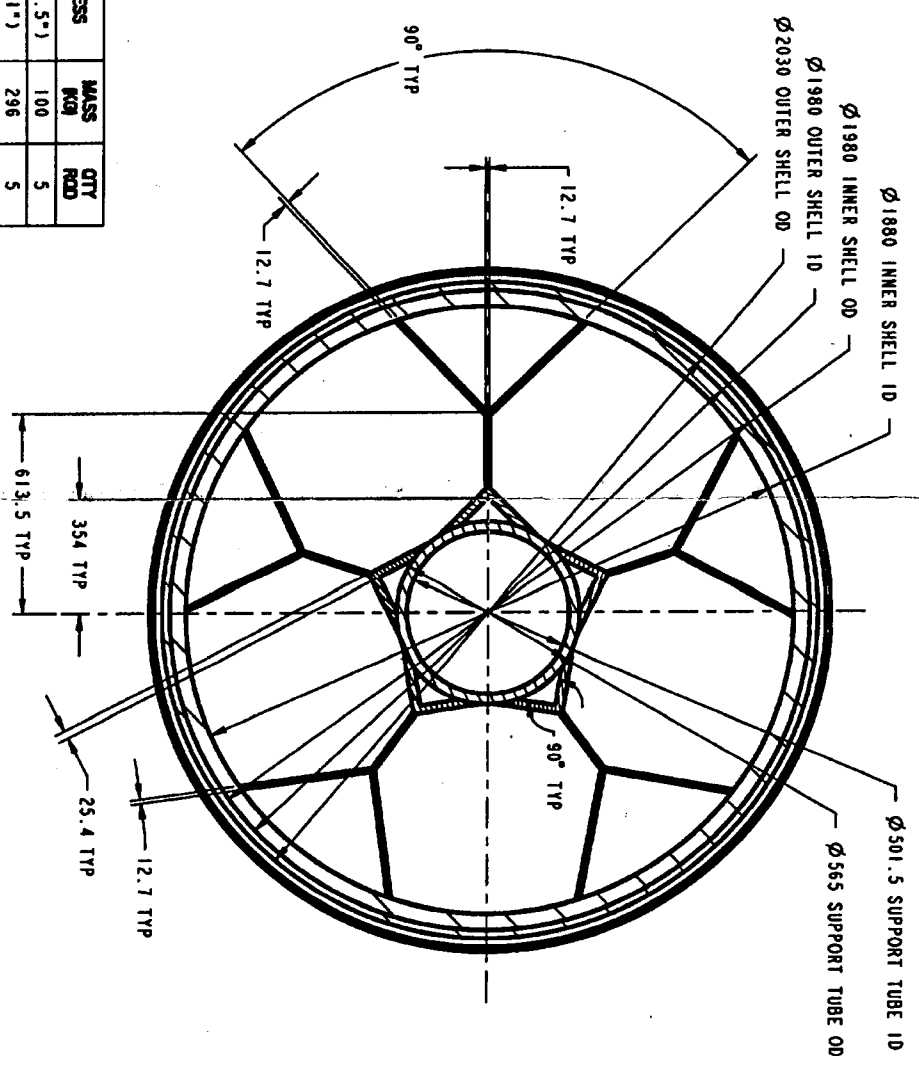
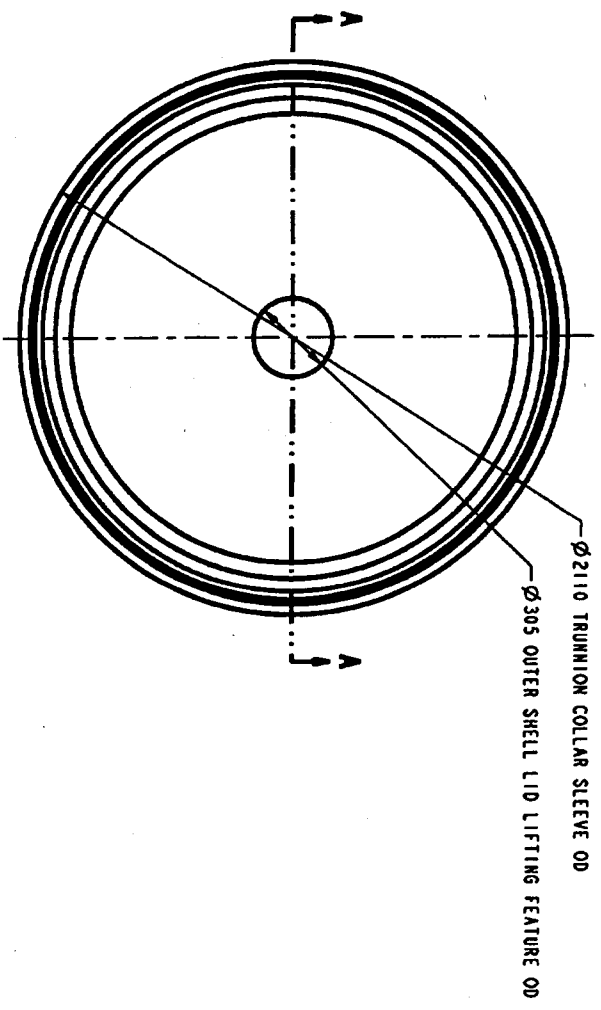
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	horiz_5D600.inp	2	4/10/01	5:08 pm
	horiz_5D600.out	72	4/10/01	5:08 pm
	horiz_5DRT.inp	2	4/10/01	5:08 pm
	horiz_5DRT.out	71	4/10/01	5:08 pm
	mesh5DHLW.inp	22	4/10/01	5:08 pm
	mesh5DHLW.out	961	4/10/01	5:08 pm
	post5D400.inp	2	4/10/01	5:09 pm
	post5D400.out	23	4/10/01	5:09 pm
	post5D600.inp	2	4/10/01	5:08 pm
	post5D600.out	23	4/10/01	5:08 pm
	post5DRT.inp	2	4/10/01	5:09 pm
	post5DRT.out	23	4/10/01	5:09 pm
VI: Horizontal lifting of the 12-PWR long waste package at 316°C	horiz_12PWR.inp	2	4/10/01	3:18 pm
	horiz_12PWR.out	24	4/10/01	3:18 pm
	mesh12PWR.inp	22	4/10/01	3:18 pm
	mesh12PWR.out	846	4/10/01	3:18 pm
	post12PWR.inp	2	4/10/01	3:18 pm
	post12PWR.out	23	4/10/01	3:18 pm
VII: Horizontal lifting of the 24-BWR waste package at 316°C	horiz24BWR.inp	2	4/10/01	4:02 pm
	horiz24BWR.out	24	4/10/01	4:02 pm
	mesh24BWR.inp	22	4/10/01	4:02 pm
	mesh24BWR.out	830	4/10/01	4:02 pm
	post24BWR.inp	2	4/10/01	4:02 pm
	post24BWR.out	23	4/10/01	4:02 pm

ATTACHMENT I

Design sketches

*5 DHLW/DOE SNF - Long Waste Package Configuration
for Site Recommendation [SK-0200 REV 04]*

*5 DHLW/DOE SNF - Long Weld Configuration
[SK-0201 REV 00]*



COMPONENT NAME	MATERIAL	THICKNESS	MASS KG	QTY REQ
DIVIDER PLATE	SA-516 K02100	12.7 (0.5")	100	5
INNER BRACKET	SA-516 K02100	25.4 (1")	296	5
OUTER BRACKET	SA-516 K02100	12.7 (0.5")	375	5
SUPPORT TUBE	SA-516 K02100	31.75 (1.25")	1924	1
INNER SHELL	SA-240 S31600	50	11507	1
INNER SHELL LID	SA-240 S31600	105	2314	2
INNER LID LIFTING FEATURE	SA-240 S31600	27	12	1
OUTER SHELL	SB-575 N06022	25	6918	1
EXTENDED OUTER SHELL LID	SB-575 N06022	25	172	1
EXTENDED OUTER SHELL LID BASE	SB-575 N06022	25	629	1
EXTENDED LID REINFORCEMENT RING	SB-575 N06022	50	129	1
OUTER LID LIFTING FEATURE	SB-575 N06022	27	13	2
OUTER SHELL FLAT CLOSURE LID	SB-575 N06022	10	268	1
OUTER SHELL FLAT BOTTOM LID	SB-575 N06022	25	669	1
UPPER TRUNNION COLLAR SLEEVE	SB-575 N06022	40	655	1
LOWER TRUNNION COLLAR SLEEVE	SB-575 N06022	40	642	1
INNER SHELL SUPPORT RING	SB-575 N06022	20	53	1
TOTAL ALLOY 22 WELDS	SFA-5.14 N06022	-	325	***
TOTAL 316 WELDS	SFA-5.9 S31680	-	194	***
WASTE PACKAGE ASSEMBLY	-	-	32610	1
HLW GLASS ASSEMBLY	-	-	4200**	5
18" CANISTER LONG	-	-	2721*	1
WP ASSEMBLY WITH SNF	-	-	56331	-

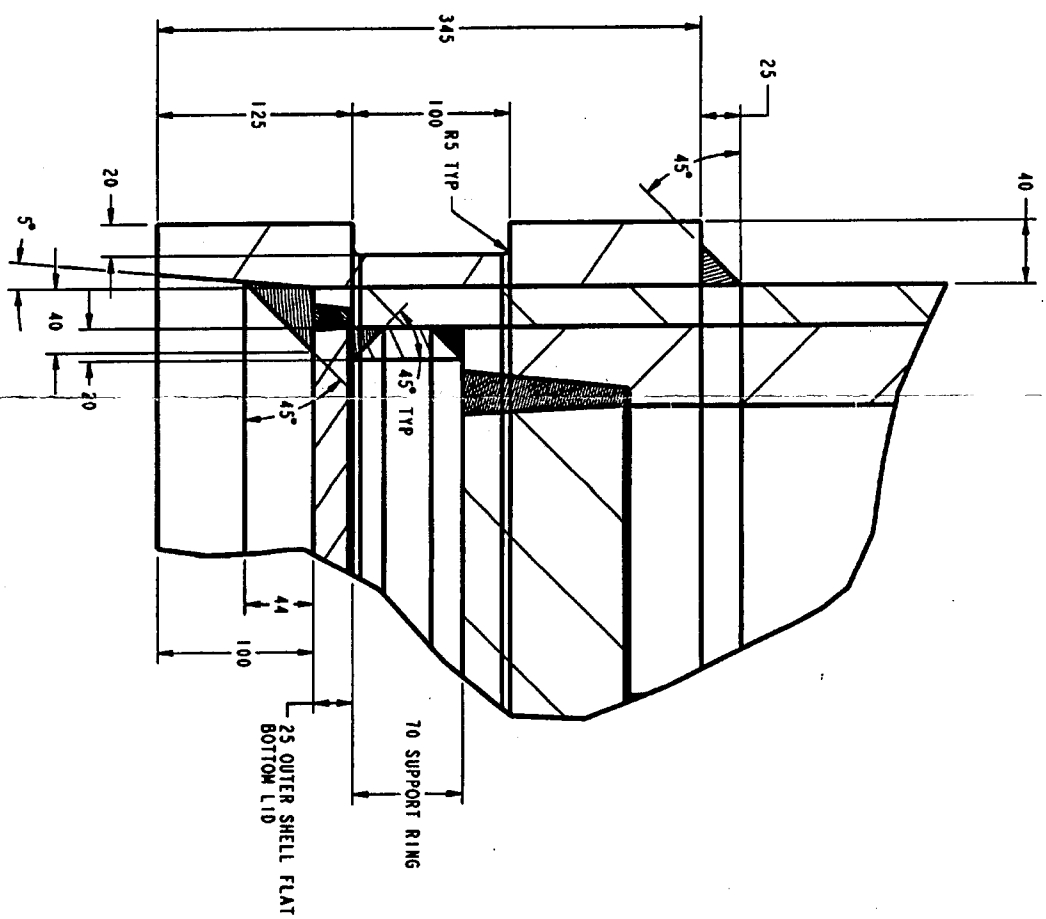
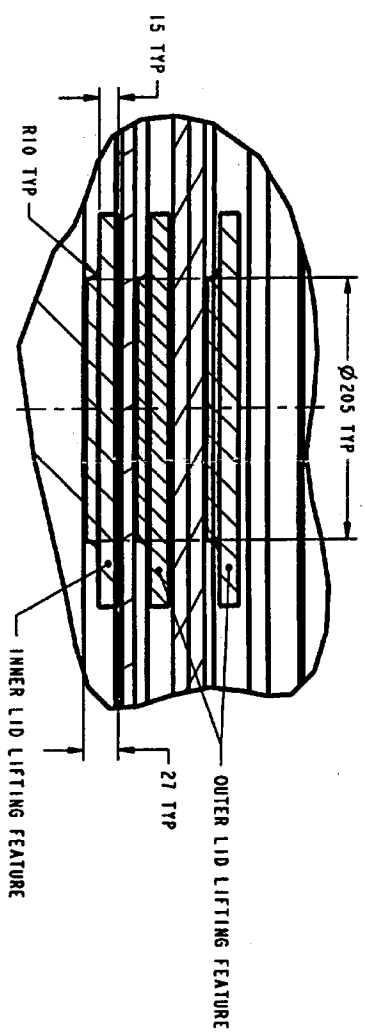
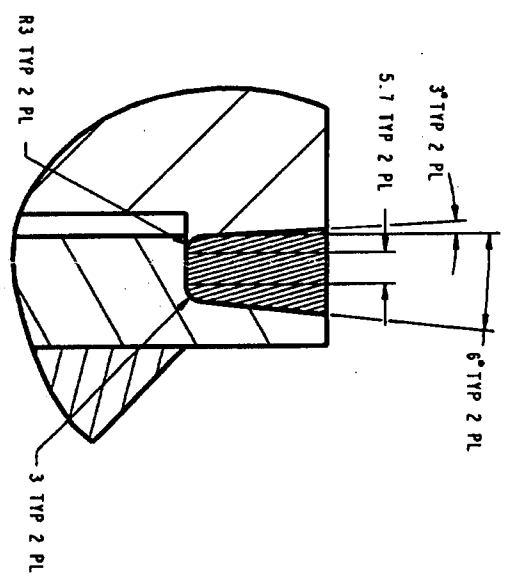
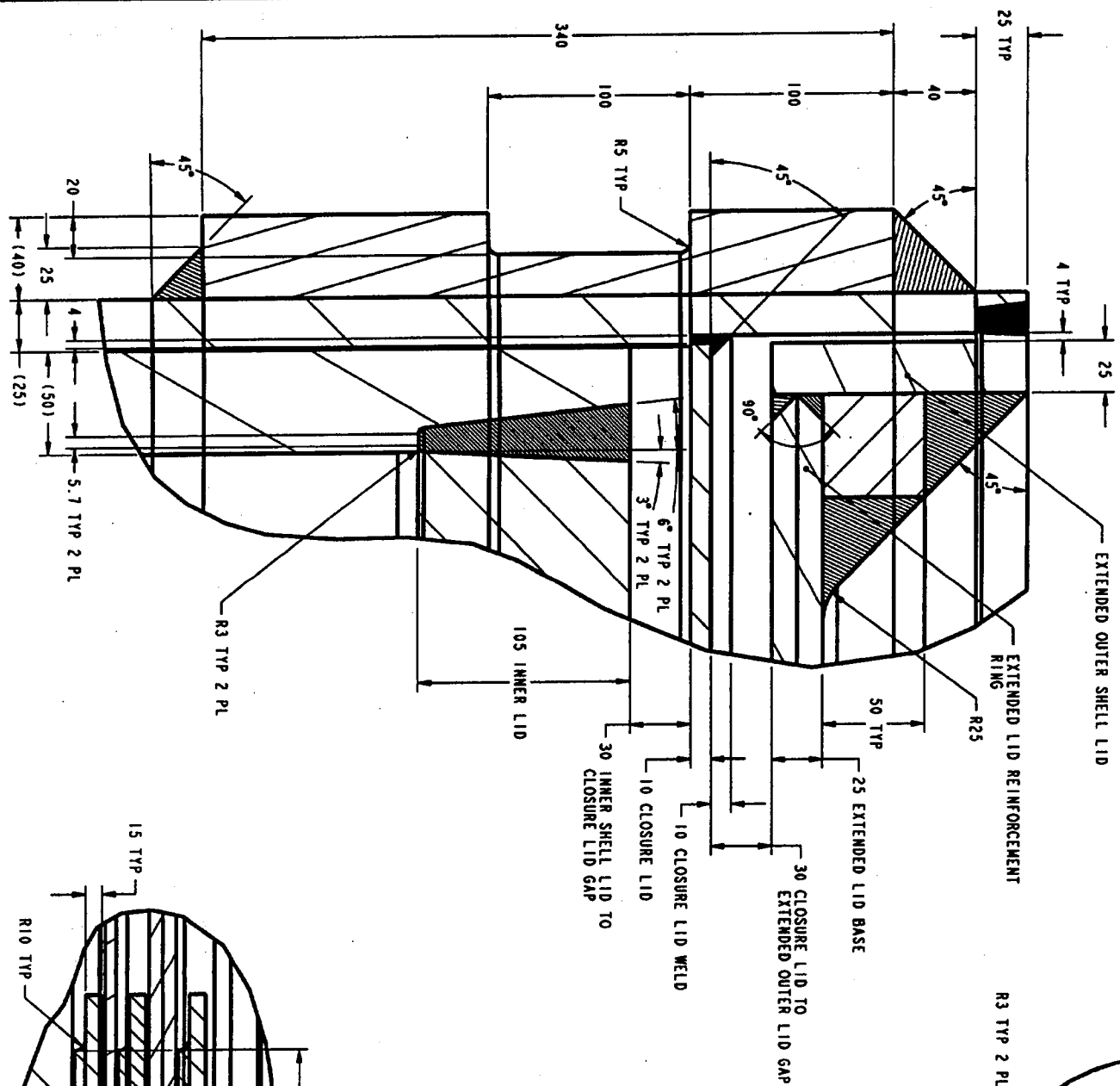
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 *** SEE SK-0201 FOR WELD CONFIGURATION AND MASSES

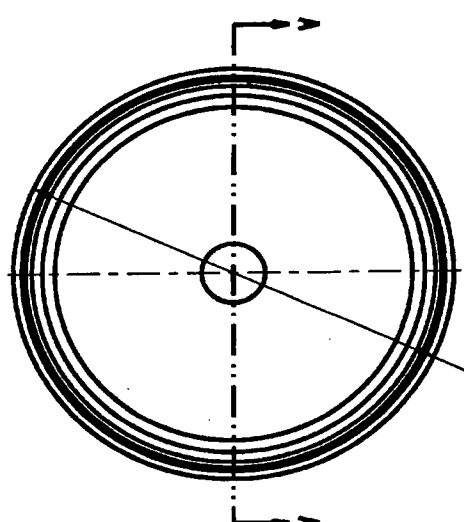
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01	INNER SHELL LID THICKNESS 105 "WAS" 80 IN TABLE	1/26/00	DCM
02	OUTER SHELL THICKNESS 25 "WAS" 20 IN TABLE	2/9/00	DCM
03	SKETCHED BY "WAS" ORIGINATOR, "REDESIGNED" REVISION BLOCK, SDHLW LONG "WAS" NEW LONG, "ADDED" VIEW "D" TO SHEET 2	3/2/00	EJC
04	IN NOTE **, DOE/RW-0351 "WAS" DOE/RW-315P	6/5/00	EJC

SECTION B-B

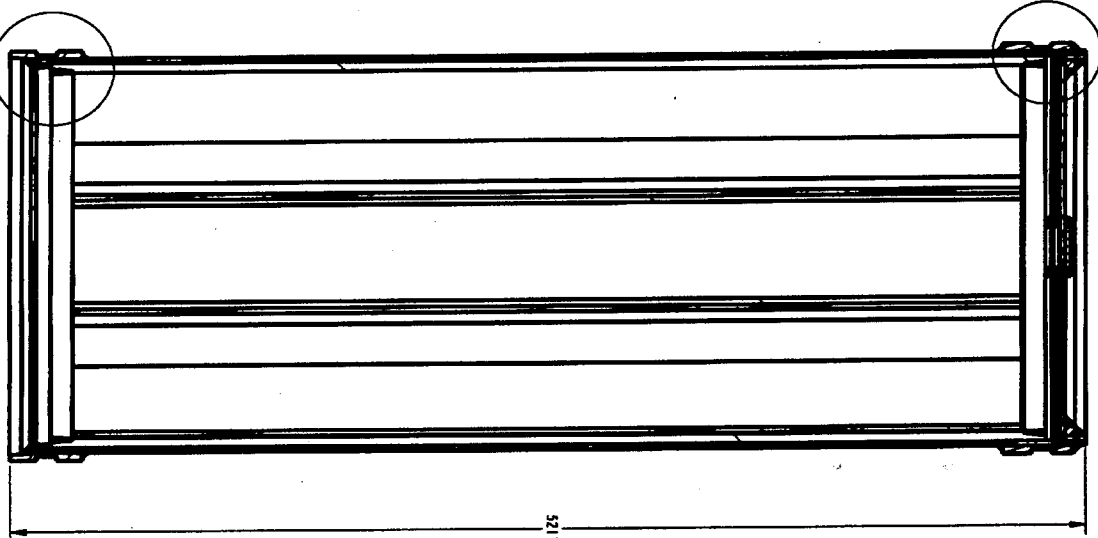
FOR INFORMATION ONLY

5 DRLW/DOE SNF - LONG WASTE PACKAGE CONFIGURATION FOR SITE RECOMMENDATION
 SKETCH NUMBER: SK-0200 REV 04
 SKETCHED BY: EUGENE CONNELL
 DATE: 06/05/00
 SHEET 1 OF 2
 89C 6/6/00 sub 501.5
 04/06/00

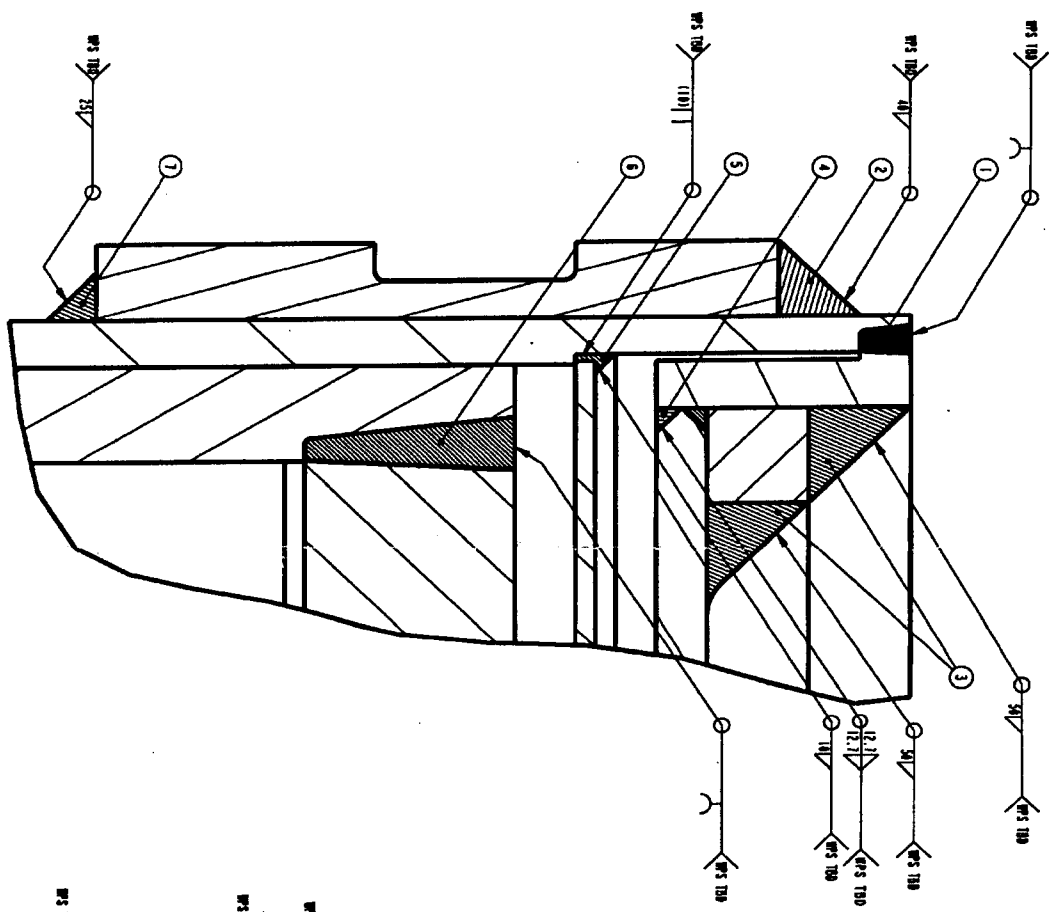




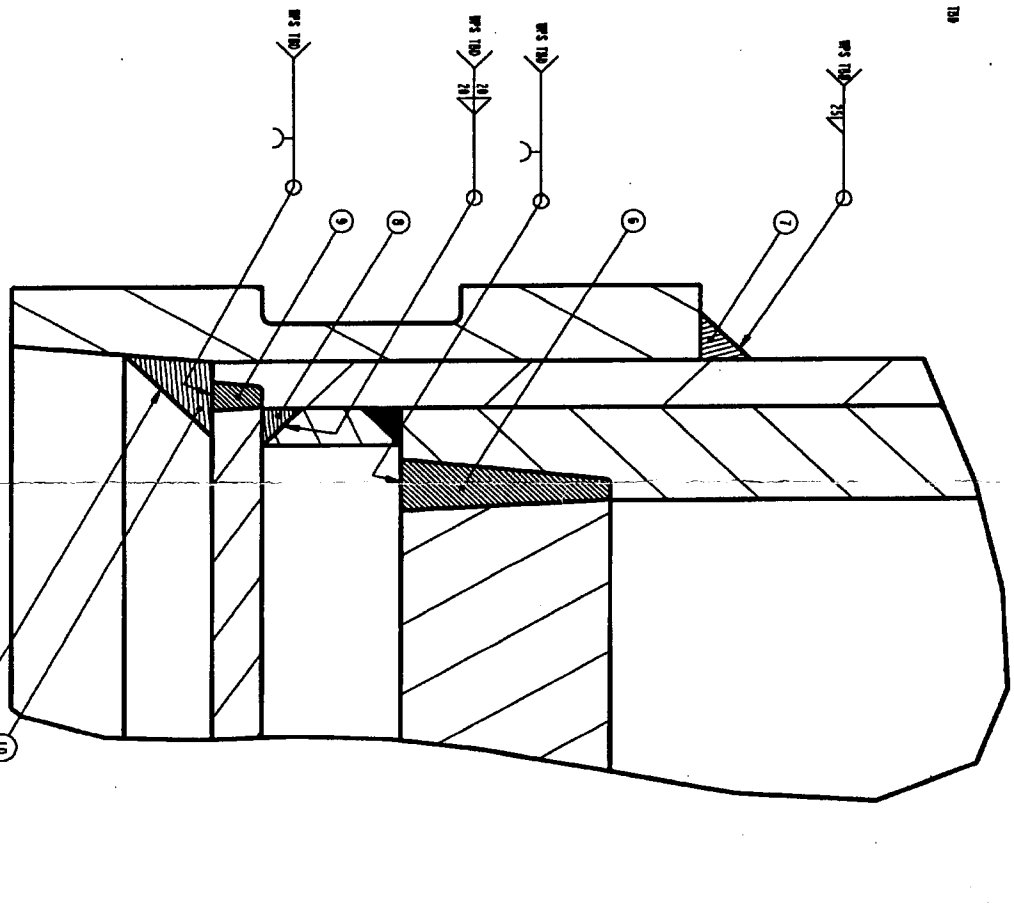
Ø2110 TRUNNION COLLAR SLEEVE OD



SECTION A-A
SCALE 0.062



DETAIL A
SCALE 0.609



DETAIL B
SCALE 0.609

WELD	MATERIAL	WPS	WPS	WPS
1	SFA-5.14 NO5022	18	1	1
2	SFA-5.14 NO5022	45	1	1
3	SFA-5.14 NO5022	127	1	1
4	SFA-5.14 NO5022	4.1	2	2
5	SFA-5.14 NO5022	4.9	1	1
6	SFA-5.9 S31680	97	2	2
7	SFA-5.14 NO5022	17	2	2
8	SFA-5.14 NO5022	11	2	2
9	SFA-5.14 NO5022	18	1	1
10	SFA-5.14 NO5022	46	1	1
TOTAL ALLOY 22 WELDS	SFA-5.14 NO5022	325	-	-
TOTAL 316 WELDS	SFA-5.9 S31680	194	-	-

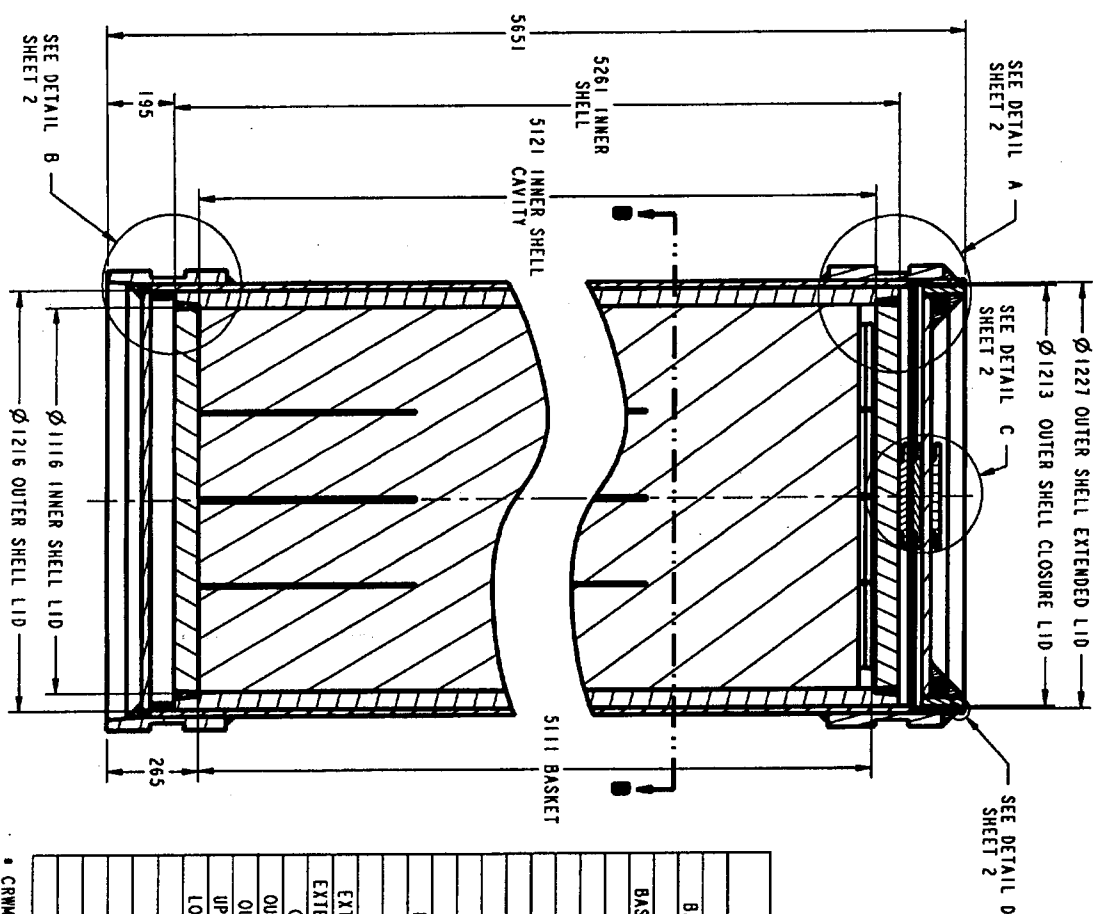
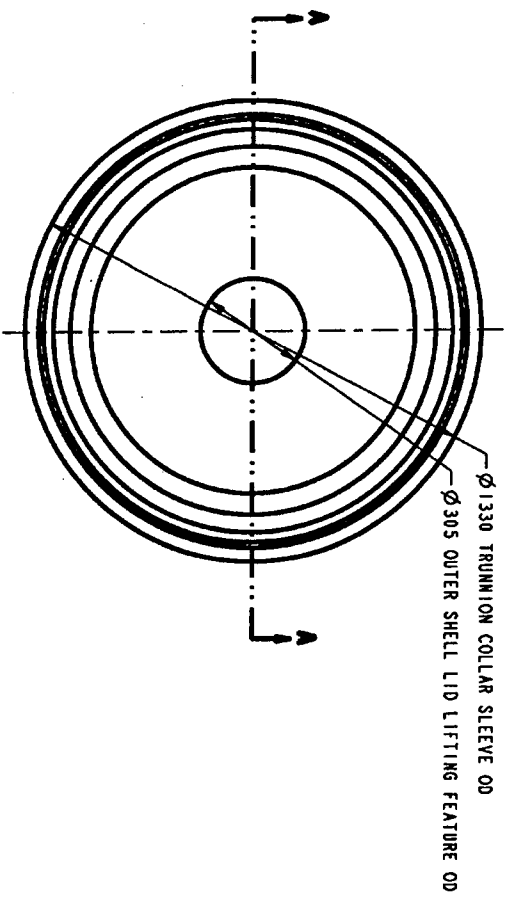
FOR INFORMATION ONLY		APPROVALS	
THIRD ANGLE PROJECTION		DESIGNED BY BRYAN HARRIS	
DRAWN BY SCOTT BENNETT		INITIAL DATE 05/11/00	
CHECKED BY JERRY COOK		DATE 05/11/00	
DESIGNED BY THOMAS DOUGLAS		DATE 05/11/00	
DO NOT SCALE FROM SKETCH		SCALE 0.062	
TITLE 5 DILW/DOE SNF - LONG WELD CONFIGURATION		REVISION 00	
SHEET NUMBER SK-0201		SHEET 1 OF 1	

ATTACHMENT II

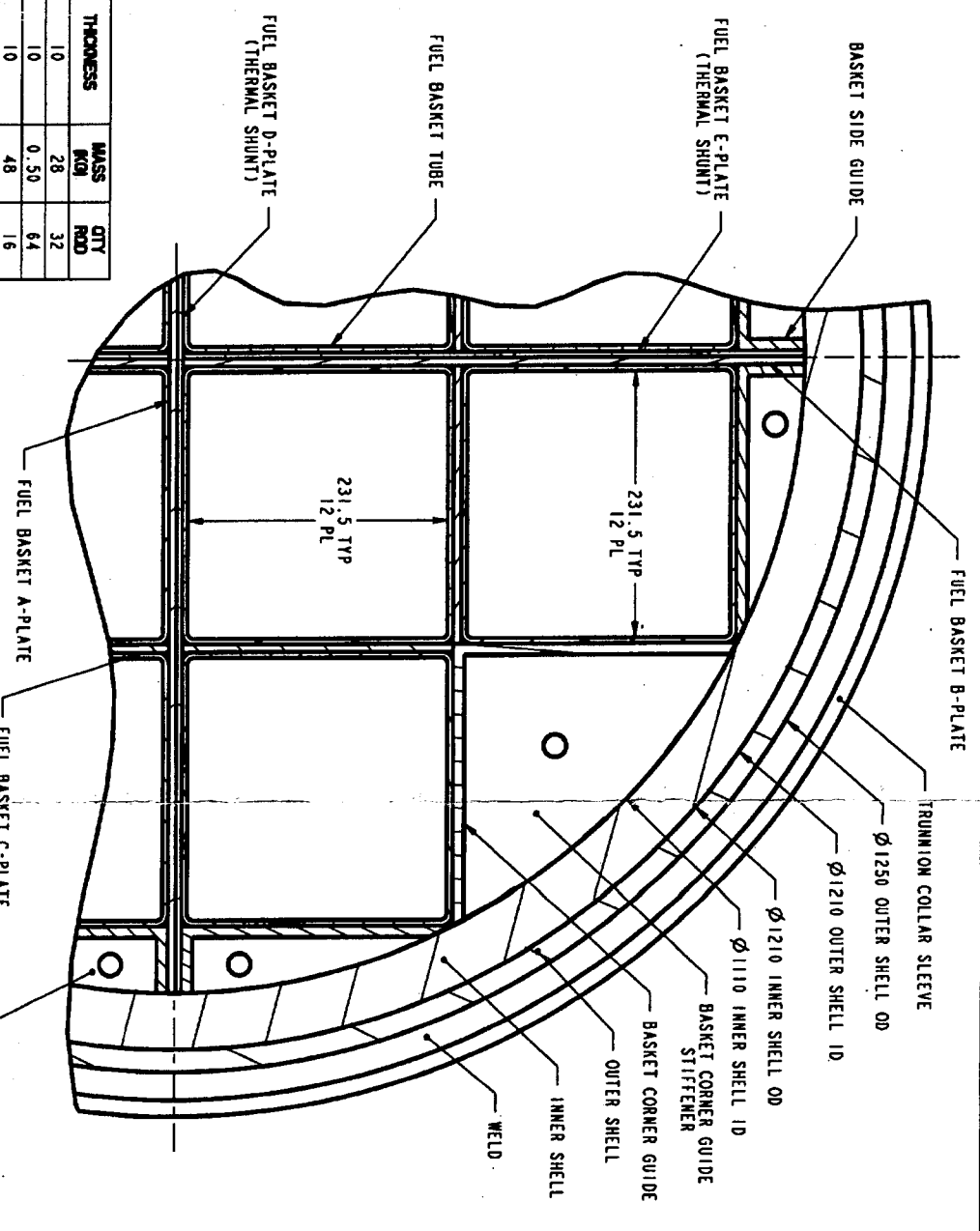
Design sketches

*12-PWR Long Waste Package Configuration
for Site Recommendation [SK-0183 REV 01]*

*12-PWR Long Waste Package Weld Configuration
[SK-0205 REV 00]*



SECTION A-A



SECTION B-B

COMPONENT NAME	MATERIAL	THICKNESS	MASS KG	QTY RCD
BASKET SIDEGUIDE	SA-516 K02700	10	28	32
BASKET SIDEGUIDE STIFFENER	SA-516 K02700	10	0.50	64
BASKET CORNER GUIDE	SA-516 K02700	10	48	16
BASKET CORNER GUIDE STIFFENER	SA-516 K02700	10	2.5	32
FUEL BASKET A-PLATE	NEUTRONIT A 978	7	76	4
FUEL BASKET B-PLATE	NEUTRONIT A 978	7	76	4
FUEL BASKET C-PLATE	NEUTRONIT A 978	7	34	16
FUEL BASKET D-PLATE	SB-209 A96061 T4	5	19	4
FUEL BASKET E-PLATE	SB-209 A96061 T4	5	19	4
FUEL BASKET TUBE	SA-516 K02700	5	187	12
INNER SHELL	SA-240 S31600	50	7589	1
INNER SHELL LID	SA-240 S31600	70	538	2
INNER LID LIFTING FEATURE	SA-240 S31600	27	12	1
OUTER SHELL	SB-575 N06022	(10) 20	3666	1
EXTENDED OUTER SHELL LID	SB-575 N06022	25	104	1
EXTENDED OUTER SHELL LID BASE	SB-575 N06022	25	226	1
EXTENDED LID REINFORCEMENT RING	SB-575 N06022	50	76	1
OUTER LID LIFTING FEATURE	SB-575 N06022	27	13	2
OUTER SHELL FLAT CLOSURE LID	SB-575 N06022	10	100	1
OUTER SHELL FLAT BOTTOM LID	SB-575 N06022	25	250	1
UPPER TRUNNION COLLAR SLEEVE	SB-575 N06022	40	408	1
LOWER TRUNNION COLLAR SLEEVE	SB-575 N06022	40	400	1
INNER SHELL SUPPORT RING	SFA-5.14 N06022	20	32	1
TOTAL ALLOY 22 WELDS	SFA-5.9 S31680	-	196	**
WASTE PACKAGE ASSEMBLY	-	-	67	**
WASTE PACKAGE ASSEMBLY	-	-	19341	1
WASTE PACKAGE ASSEMBLY	-	-	882.2*	12
WASTE PACKAGE ASSEMBLY	-	-	30127	1

* CRMS MDO 1997, WASTE CONTAINER CAVITY SIZE DETERMINATION. BBAA00000-01717-0200-00028 REV 00
LAS VEGAS, NEVADA: CRMS MDO. ACC: MOL. 19980106-0081
** REFER TO SK-0205 REV 00 "12-PWR LONG PACKAGE WELD CONFIGURATION"

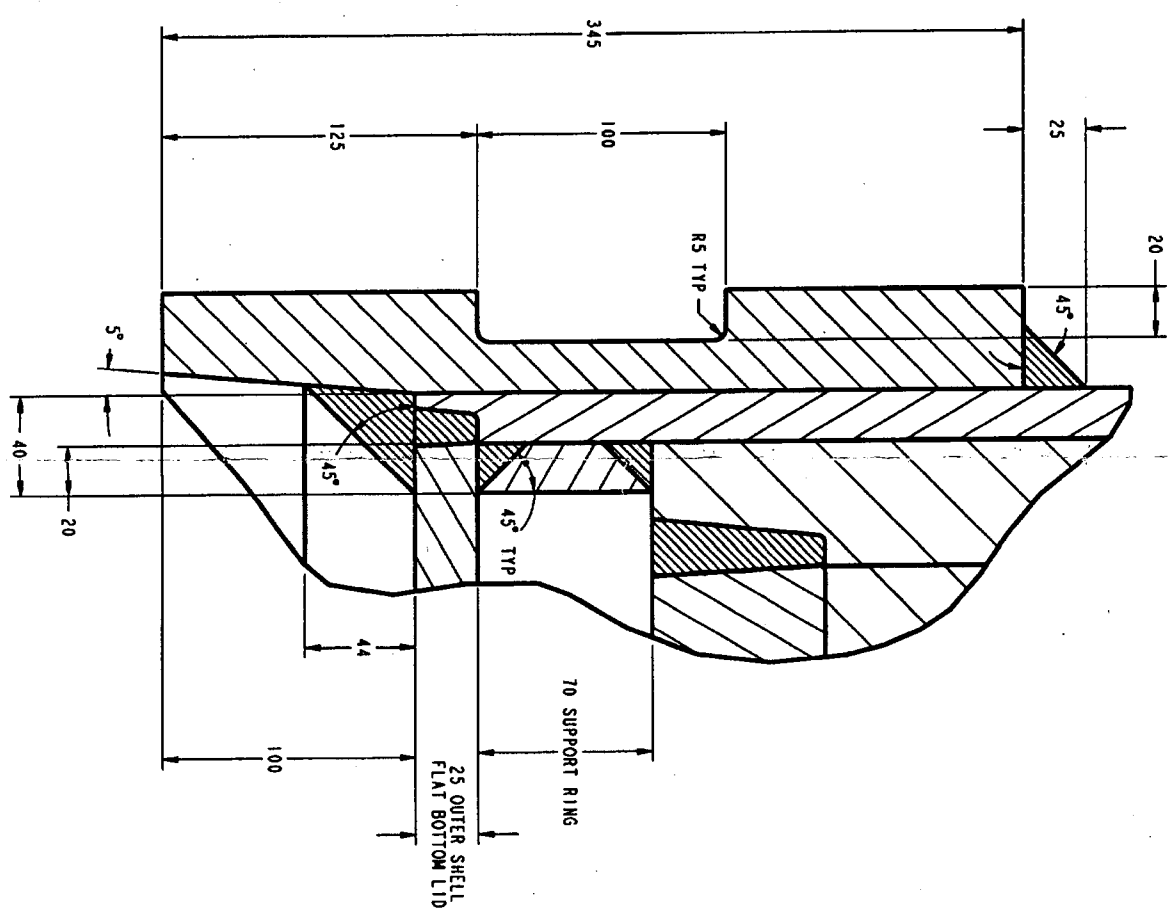
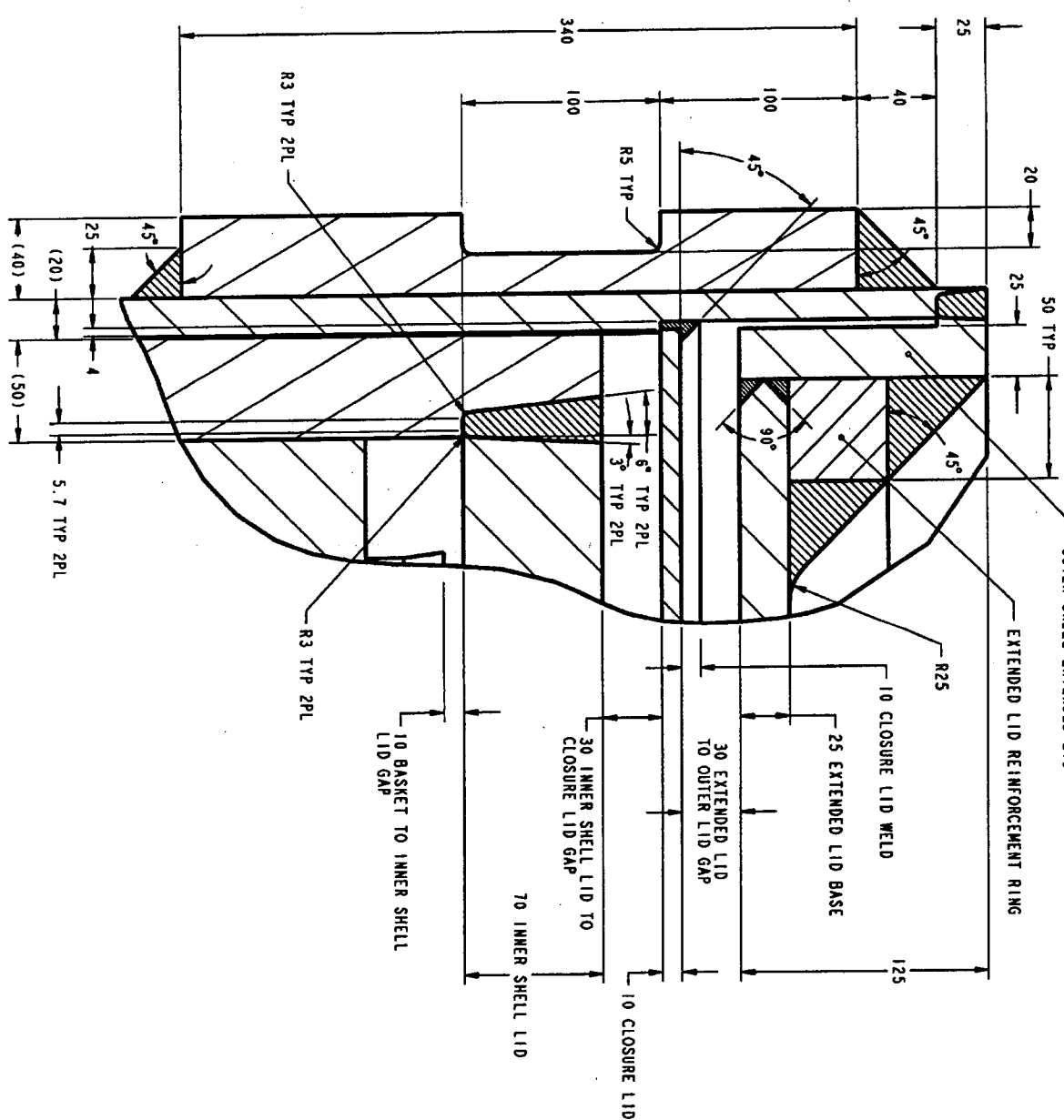
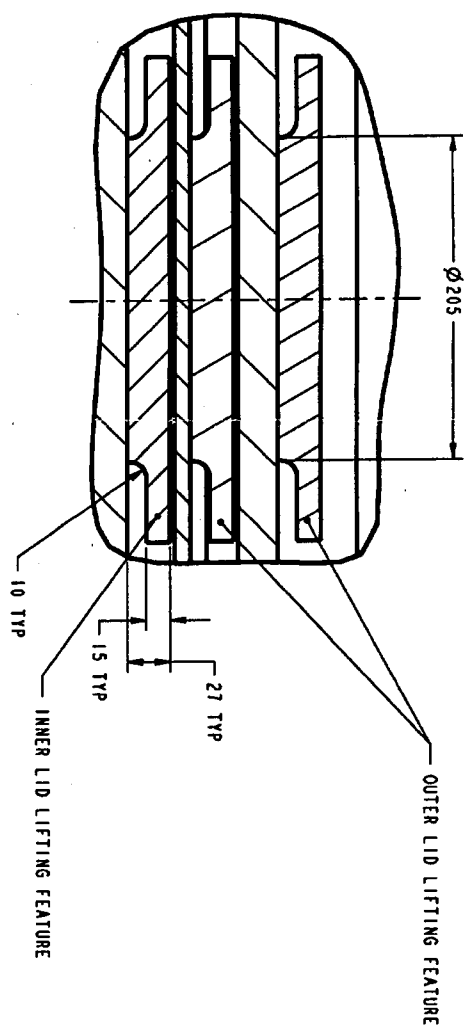
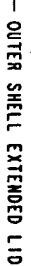
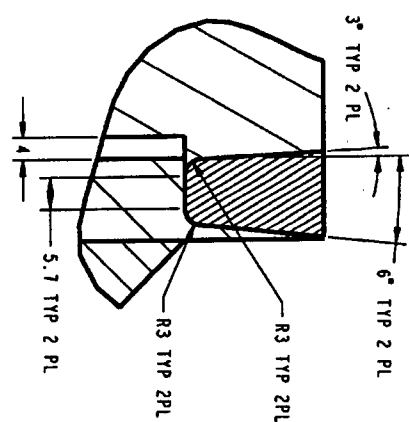
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02	22 OUTER SHELL THICKNESS "MAX" 25. REVISION TABLE "ADDED"	02/23/98

"FOR INFORMATION ONLY"
12-PWR LONG WASTE PACKAGE CONFIGURATION
FOR SITE RECOMMENDATION

SKETCH NUMBER: SK-0183 REV 01
SKETCHED BY: BRYAN HARKINS
DATE: 03/23/00
FILE: /home/pep/lib/rev/sketches/12pwr/12pwr_100g/sk-0183.dwg

SHEET 1 OF 2
3/23/00
3/23/00
3/23/00

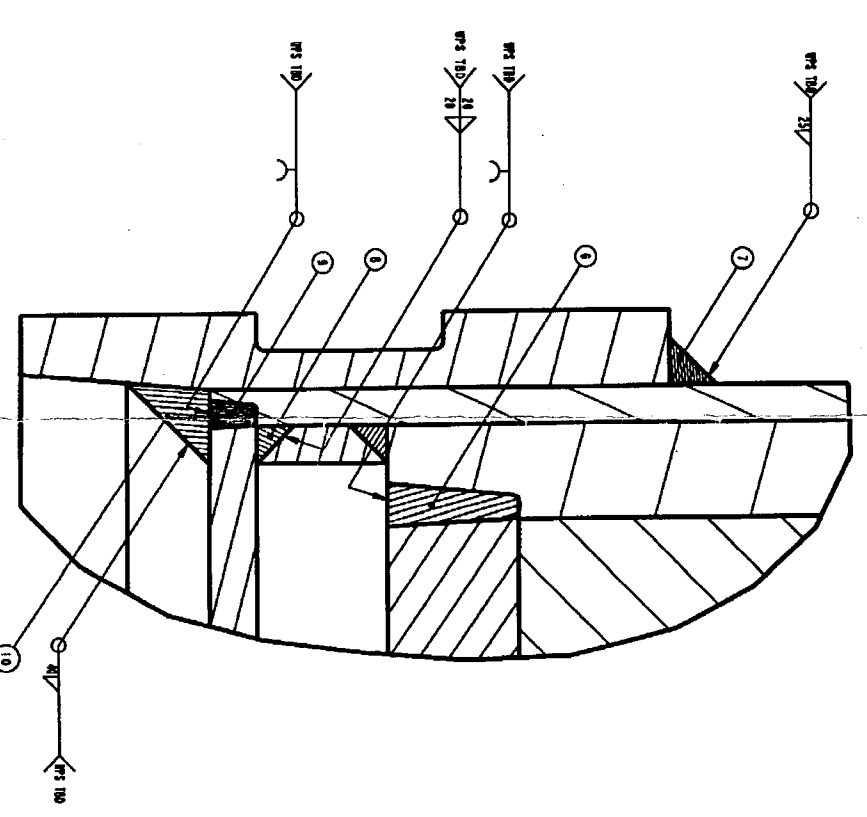
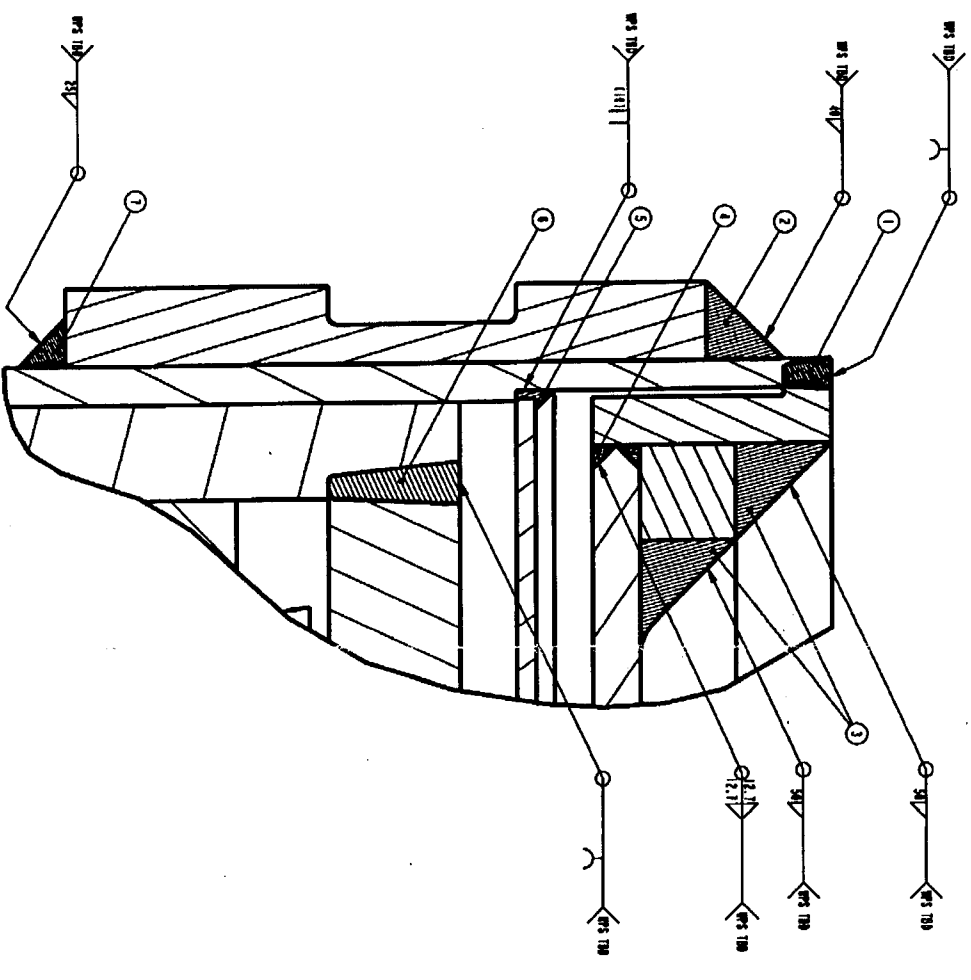
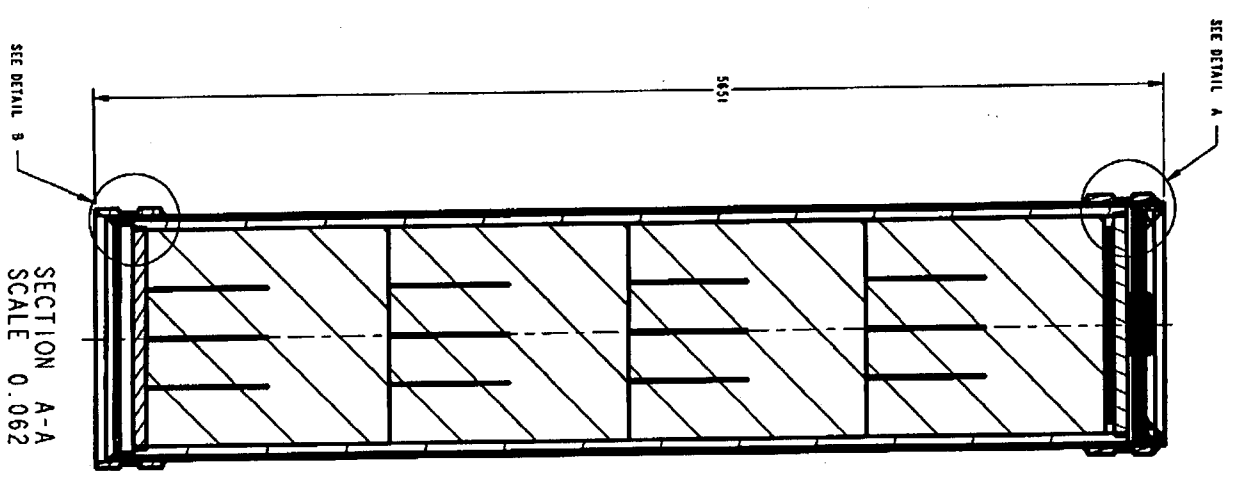
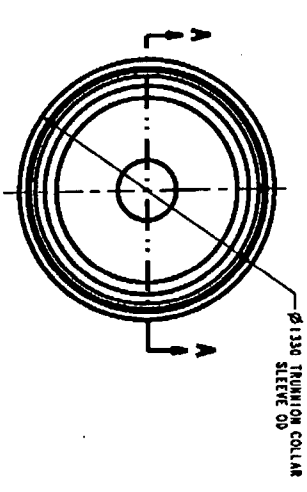


SK-0183 REV 01 SHEET 2 OF 2

Illegibility does not impact the technical meaning or content of the record. 18.0517101

ALL SHEETS ARE THE SAME REVISION STATUS

08	1	40	1	5020-15	REVISION HISTORY	DATE	APPROVED
NO. 1	1	1	1	REVISION	DESCRIPTION		



WELD	MATERIAL	WELD	WELD	QTR
WELD 1	SFA-5.14 W00022	11	1	
WELD 2	SFA-5.14 W00022	26	1	
WELD 3	SFA-5.14 W00022	74	1	
WELD 4	SFA-5.14 W00022	2.5	2	
WELD 5	SFA-5.14 W00022	3.0	1	
WELD 6	SFA-5.9 S31600	34	2	
WELD 7	SFA-5.14 W00022	11	2	
WELD 8	SFA-5.14 W00022	6.5	2	
WELD 9	SFA-5.14 W00022	11	1	
WELD 10	SFA-5.14 W00022	29	1	
TOTAL ALLOY 22 WELDS	SFA-5.14 W00022	198	-	
TOTAL 316 WELDS	SFA-5.9 S31600	67	-	

For Information and Completeness. No Approvals Required. 5/18/12/06/100

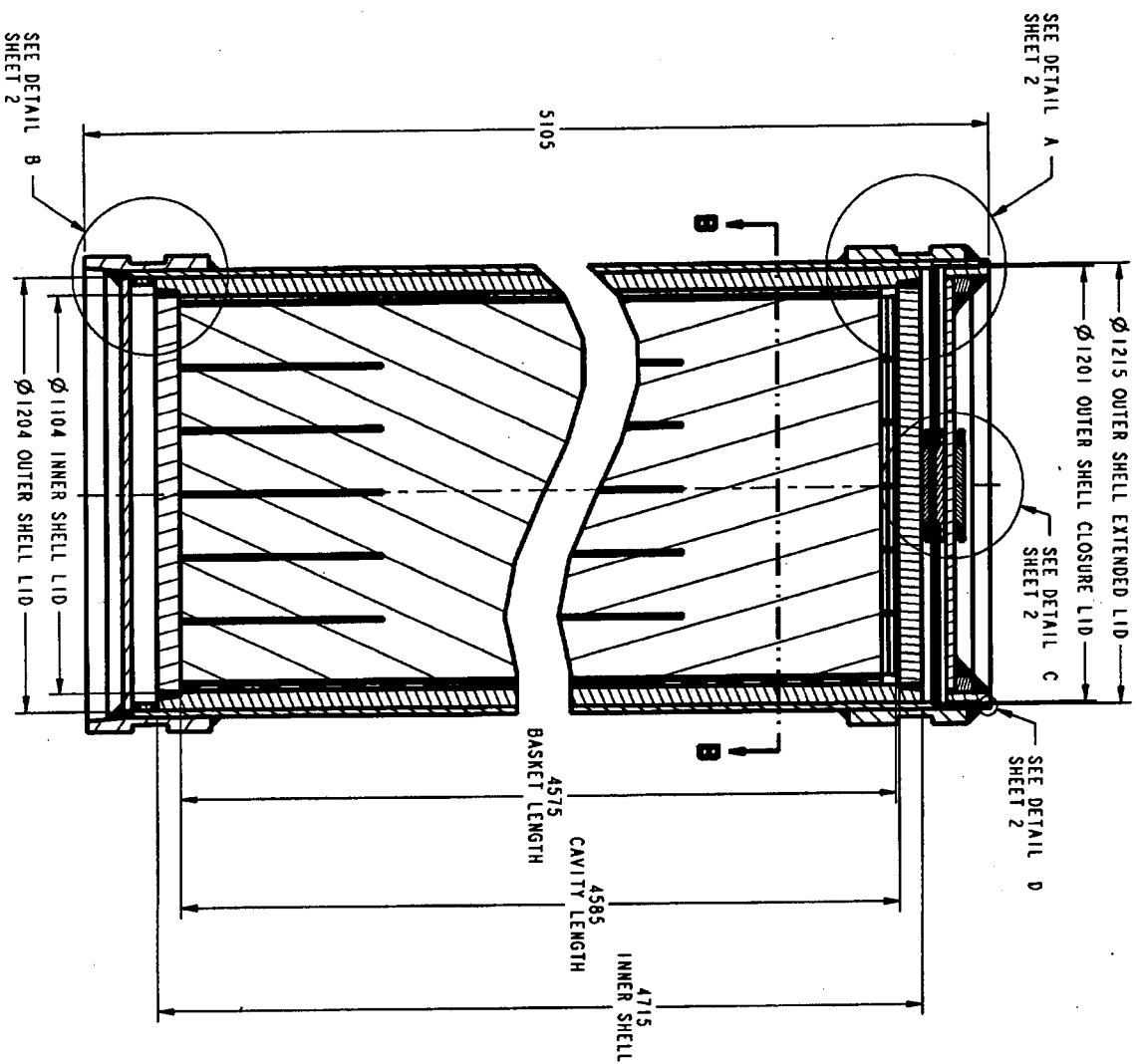
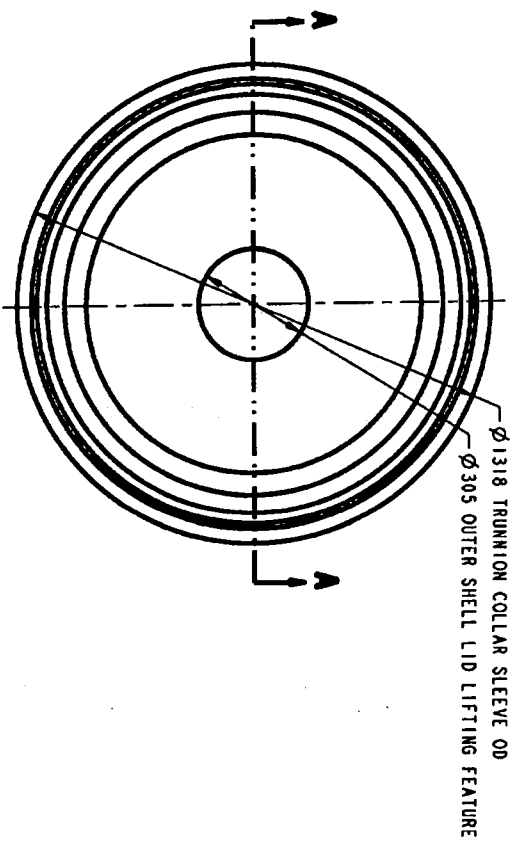
THIRD ANGLE PROJECTION	APPROVALS	INITIAL/DATE	WASTE PACKAGE COMPONENT
	DRAWN BY	SCOTT BENNETT	12-PWR LONG WASTE PACKAGE WELD CONFIGURATION
	CHECKED BY	JERRE COOK	
	DESIGNED BY	THOMAS DORRIS	
	SCALE	0.0625	
DO NOT SCALE FROM SKETCH		REVISION	SHEET 1 OF 1

ATTACHMENT III

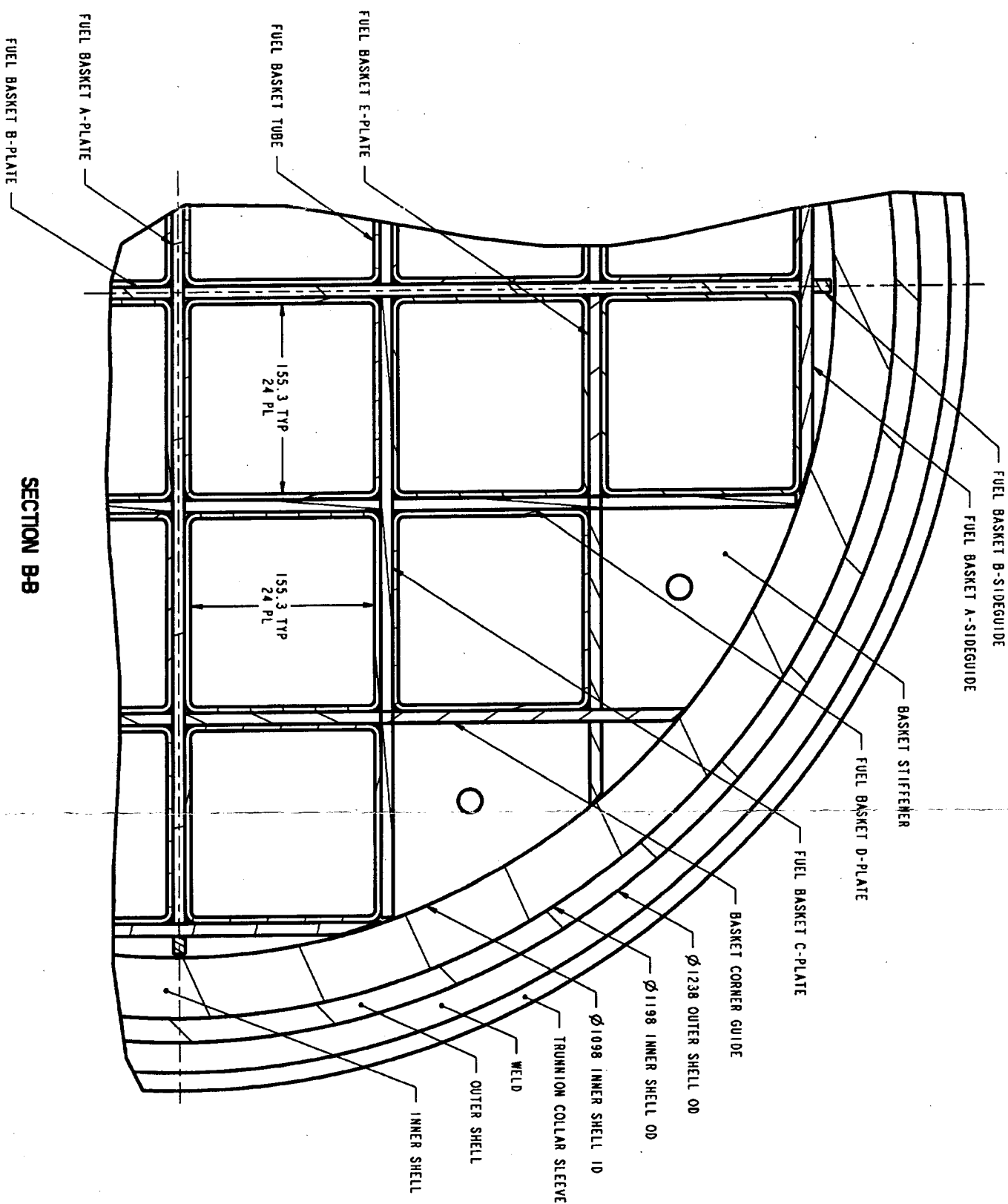
Design sketches

*24-BWR Waste Package Configuration
for Site Recommendation [SK-0184 REV 00]*

*24-BWR Waste Package Assembly Weld Configuration
[SK-0202 REV 00]*



SECTION A-A



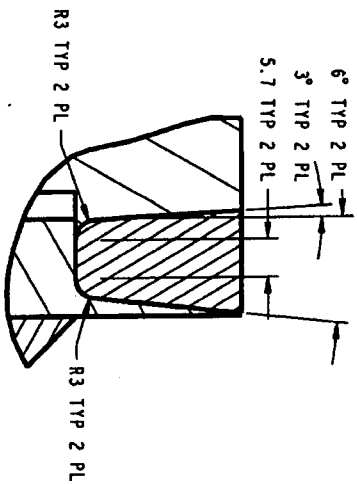
SECTION B-B

FOR INFORMATION ONLY

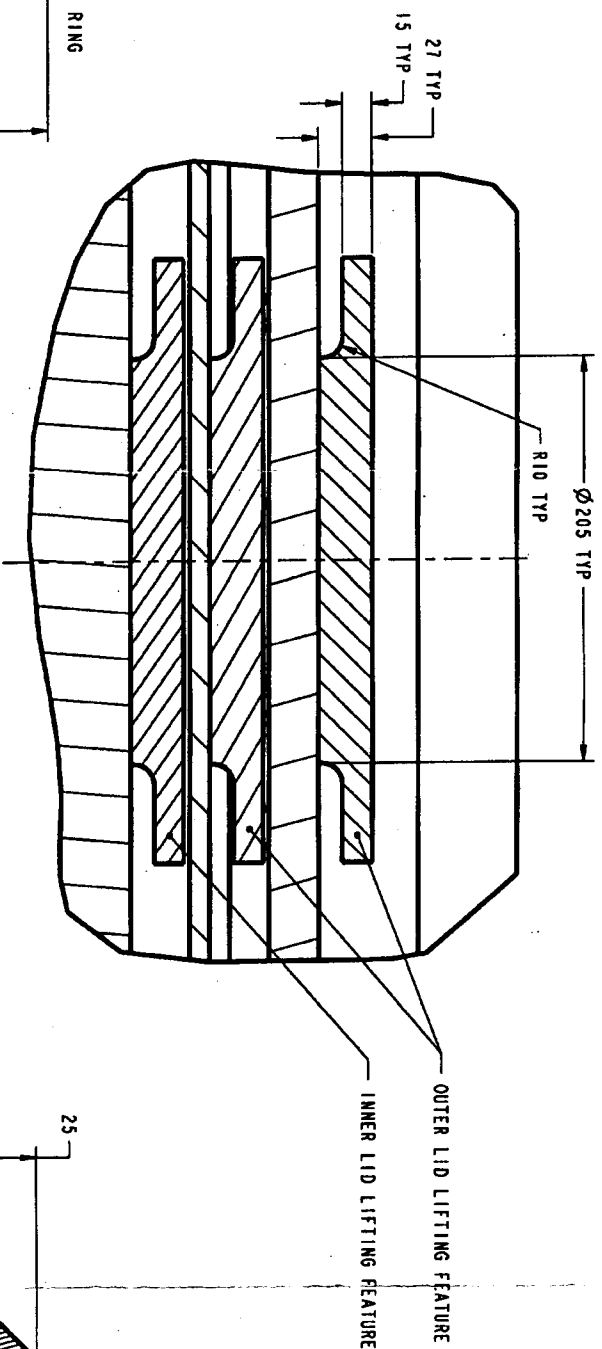
24-BWR WASTE PACKAGE CONFIGURATION FOR SITE RECOMMENDATION

SHEET NUMBER	SM-0184 REV 00	SHEET 1 OF 2
SKETCHED BY:	BRYAN HARKINS	DATE 01/25/00
FILE	/home/pro.library/checkout/sketches/24-bwr/st-0184.dwg	

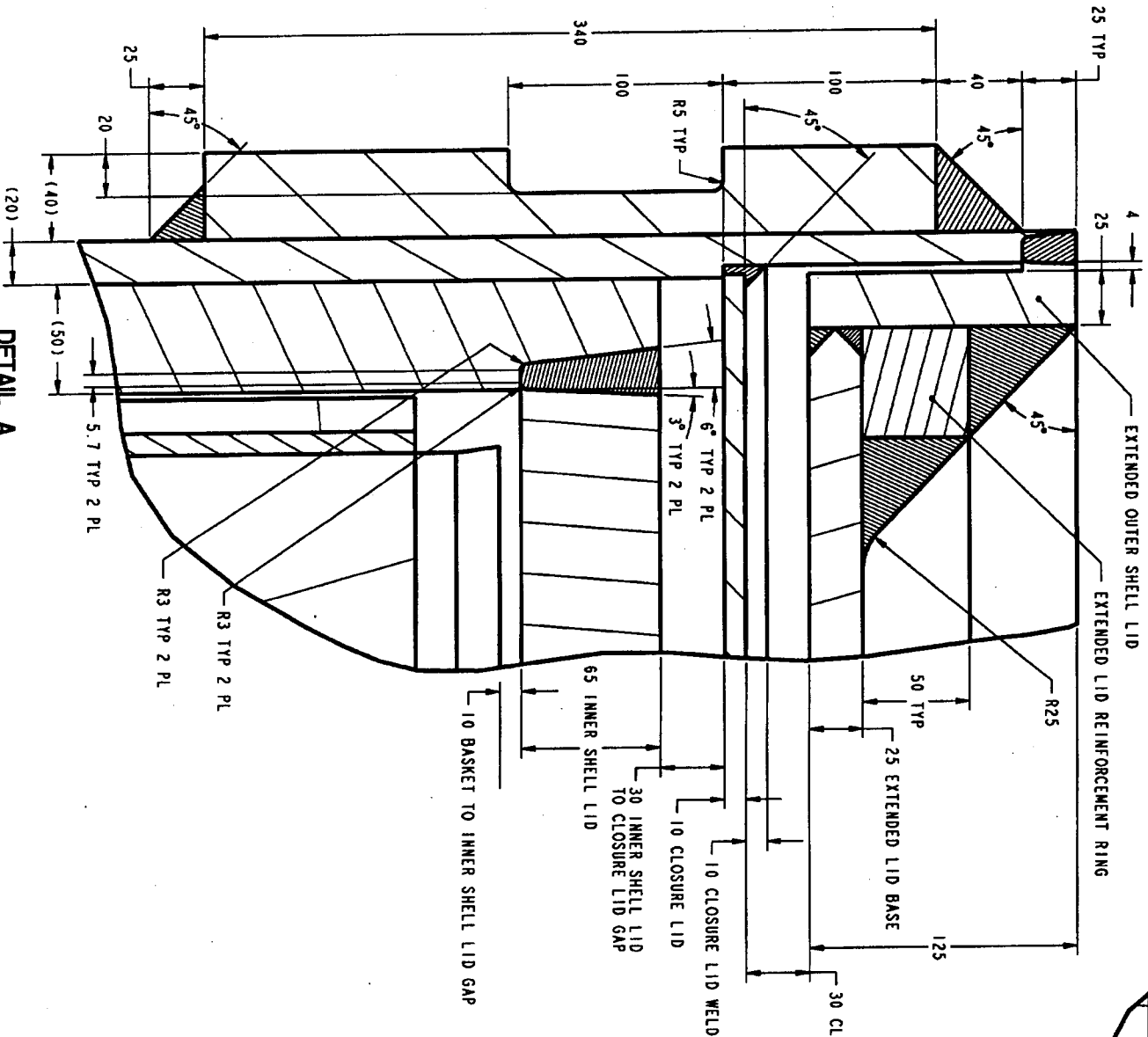
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DETAIL D

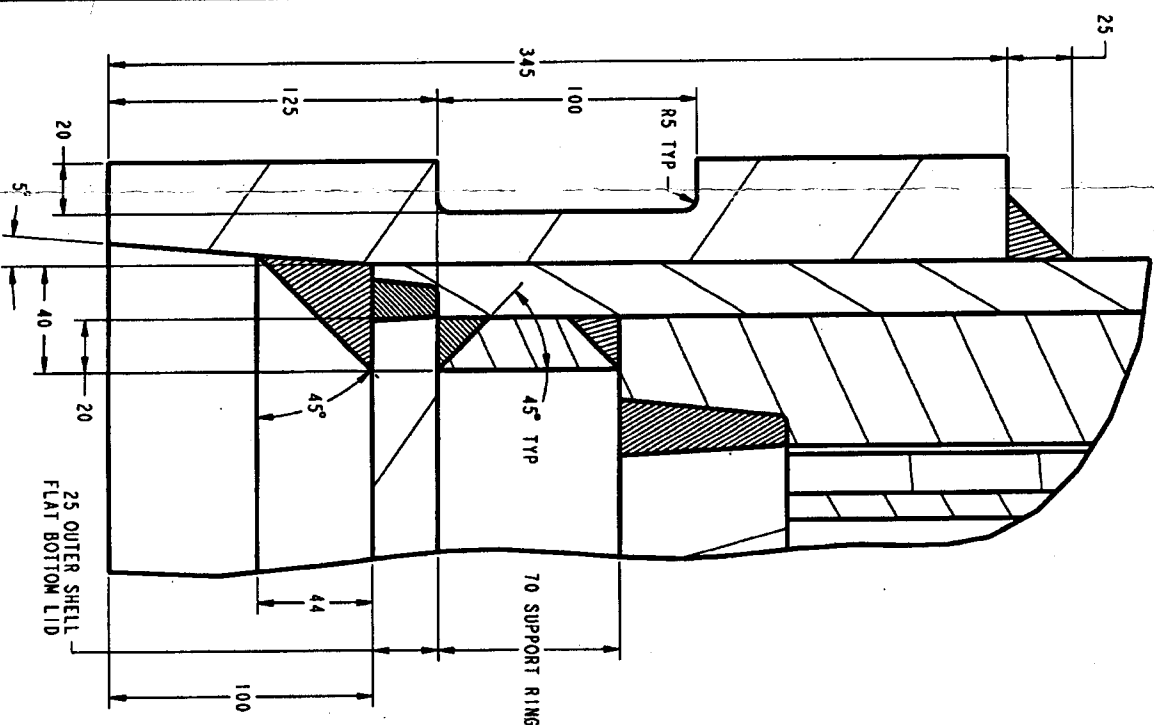


DETAIL C



DETAIL A

COMPONENT NAME	MATERIAL	THICKNESS	MASS KG	QTY RCD
BASKET A-GUIDE	SA-516 K02700	10	27	16
BASKET B-GUIDE	SA-516 K02700	10	1.3	16
BASKET CORNER GUIDE	SA-516 K02700	10	22	32
BASKET STIFFENER	SA-516 K02700	10	1.6	64
FUEL BASKET A-PLATE	NEUTRONIT A 978	10	89	4
FUEL BASKET B-PLATE	NEUTRONIT A 978	10	89	4
FUEL BASKET C-PLATE	NEUTRONIT A 978	10	90	8
FUEL BASKET D-PLATE	NEUTRONIT A 978	10	90	8
FUEL BASKET E-PLATE	NEUTRONIT A 978	10	30	16
FUEL BASKET TUBE	SA-516 K02700	5	113	24
INNER SHELL	SA-240 S31600	50	6131	1
INNER SHELL LID	SA-240 S31600	65	489	2
INNER SHELL LID LIFTING FEATURE	SA-240 S31600	27	12	1
OUTER SHELL	SB-575 N06022	20	3268	1
EXTENDED OUTER SHELL LID	SB-575 N06022	25	103	1
EXTENDED OUTER SHELL LID BASE	SB-575 N06022	25	221	1
OUTER SHELL LID LIFTING FEATURE	SB-575 N06022	27	13	2
EXTENDED LID REINFORCEMENT RING	SB-575 N06022	50	75	1
OUTER SHELL FLAT CLOSURE LID	SB-575 N06022	10	98	1
OUTER SHELL FLAT BOTTOM LID	SB-575 N06022	25	245	1
UPPER TRUNNION COLLAR SLEEVE	SB-575 N06022	40	404	1
LOWER TRUNNION COLLAR SLEEVE	SB-575 N06022	40	396	1
INNER SHELL SUPPORT RING	SB-575 N06022	20	32	1
TOTAL ALLOY 22 WEIDS	SFA-5.14 N06022	-	194	**
TOTAL 316 WEIDS	SFA-5.9 S31680	-	59	**
WASTE PACKAGE ASSEMBLY	-	-	19437	1
BWR FUEL ASSEMBLY	-	-	4328.4	24
WASTE PACKAGE ASSEMBLY WITH SNF	-	-	27318	1

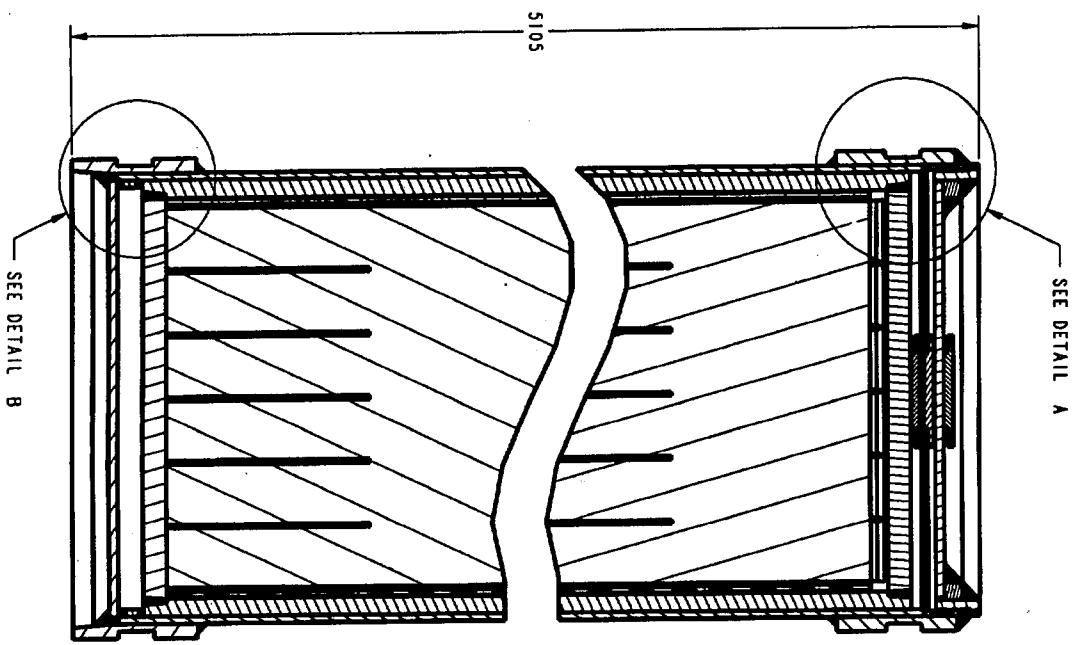
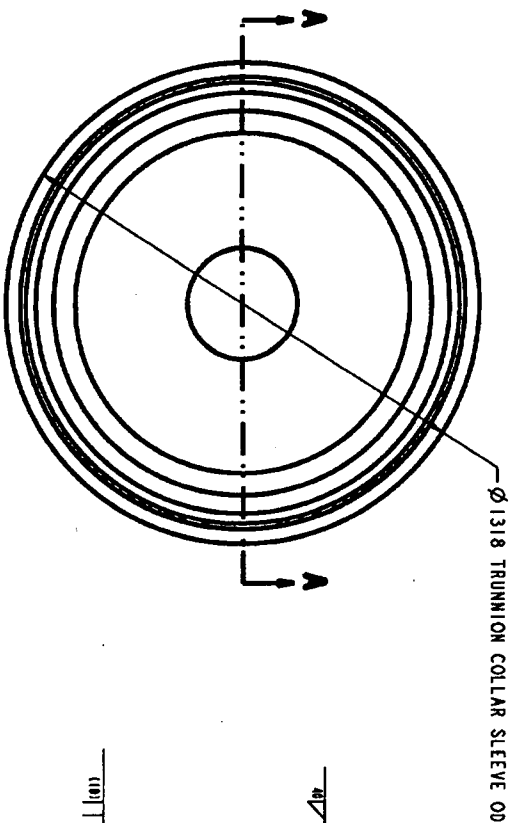


DETAIL B

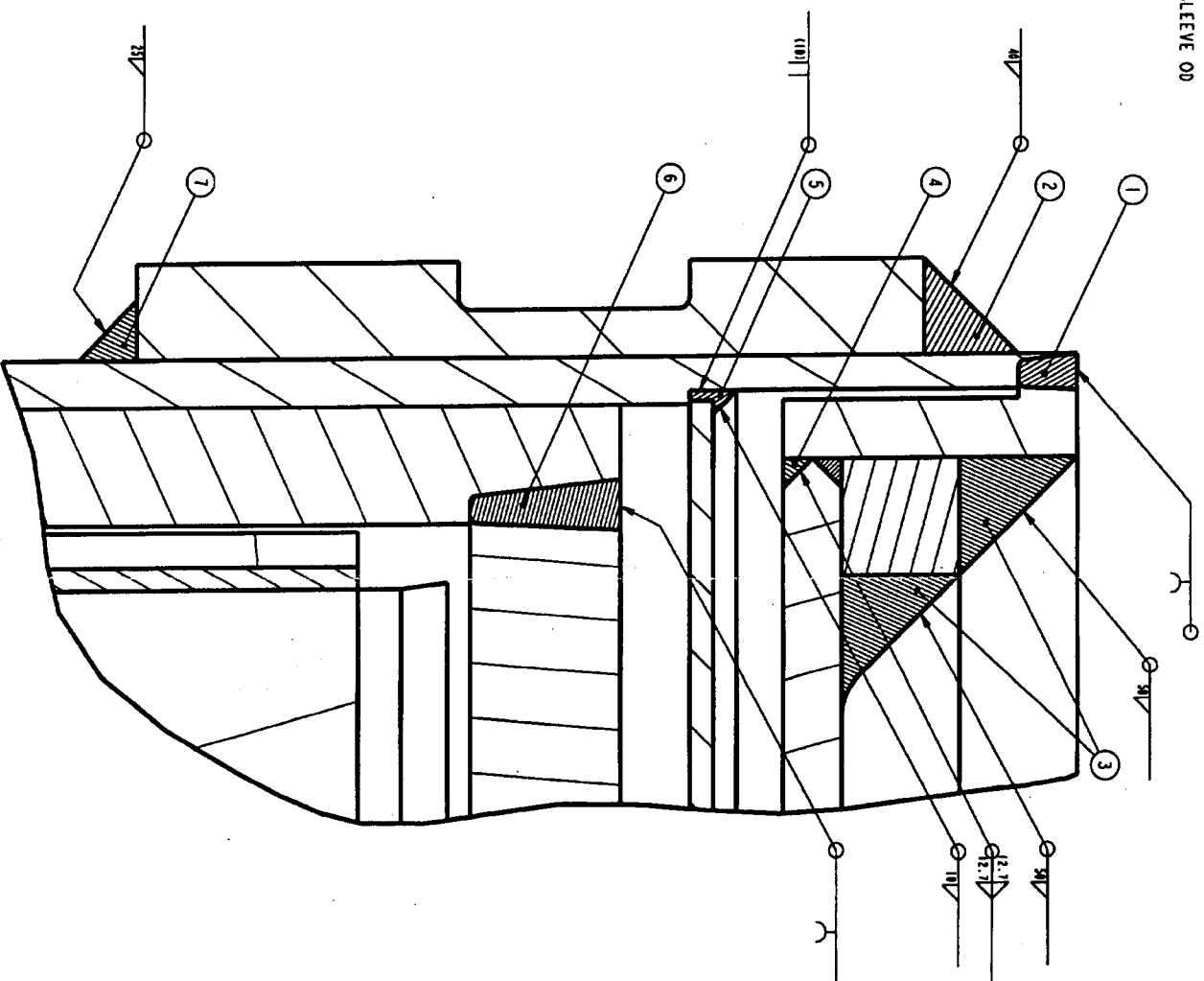
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 LAS VEGAS, NV: CRWMS M&O, ACC: MOL 19980106, 0081
 ** REFER TO SK-0202 REV 00 *24-BWR WASTE PACKAGE ASSEMBLY WELD CONFIGURATION*

SK-0184 REV 00

SHEET 2 OF 2

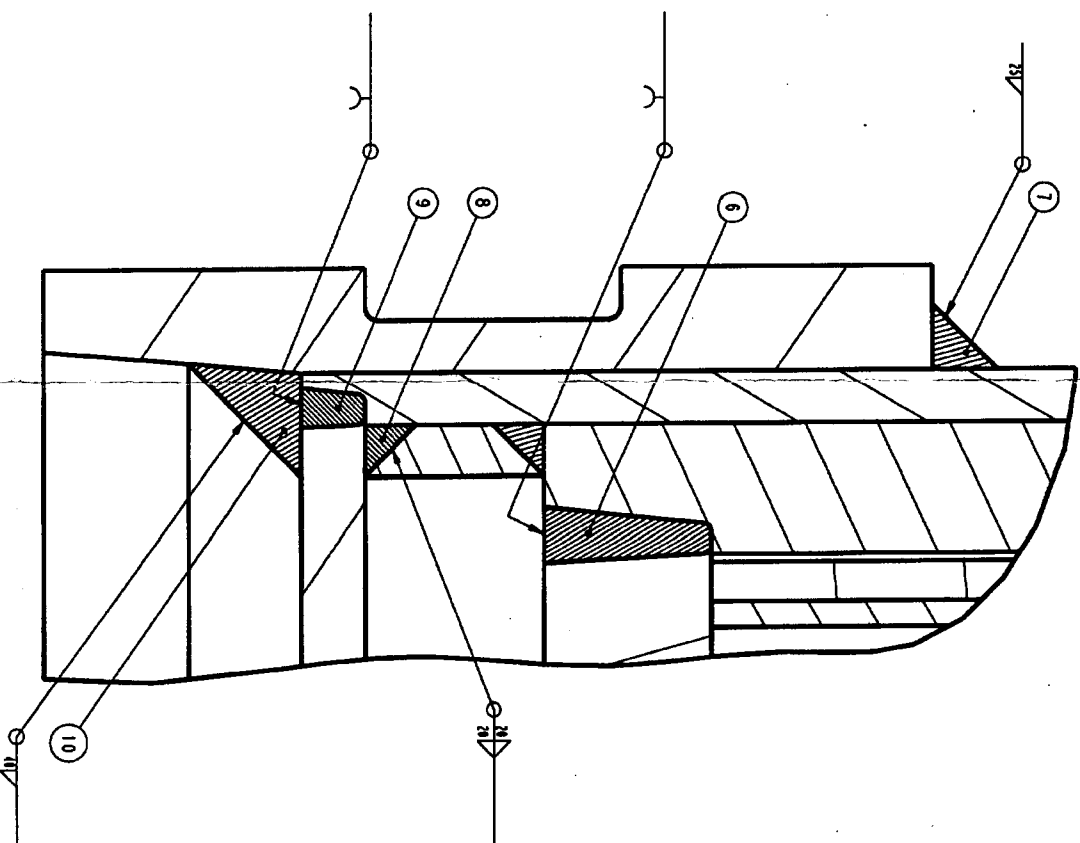


SECTION A-A



DETAIL A

WELD	MATERIAL	MASS KG	QTY ROD
1	SFA-5.14 N06022	11	1
2	SFA-5.14 N06022	28	1
3	SFA-5.14 N06022	73	1
4	SFA-5.14 N06022	2.4	2
5	SFA-5.14 N06022	3.0	1
6	SFA-5.9 S31680	30	2
7	SFA-5.14 N06022	11	2
8	SFA-5.14 N06022	6.5	2
9	SFA-5.14 N06022	11	1
10	SFA-5.14 N06022	29	1
TOTAL ALLOY 22 WELDS	SFA-5.14 N06022	194	-
TOTAL 316 WELDS	SFA-5.9 S31680	59	-



DETAIL B

FOR INFORMATION ONLY

24-BWR WASTE PACKAGE ASSEMBLY WELD CONFIGURATION

SKETCH NUMBER: SK-0202 REV 00

SKETCHED BY:

BRYAN HARRIS

DATE:

03/07/00

FILE:

/home/pro-libray/checkouts/sketches/24bwr/sk-0202.dwg

UNITS: mm
DO NOT SCALE FROM SKETCH

REV	DESCRIPTION	DATE
00	ISSUED APPROVED	03/07/00

ATTACHMENT IV

Figures obtained from ANSYS V 5.4 for the Horizontal Lifting
of the 5DHLW/DOE - Long, 12-PWR Long and 24-BWR Waste Packages

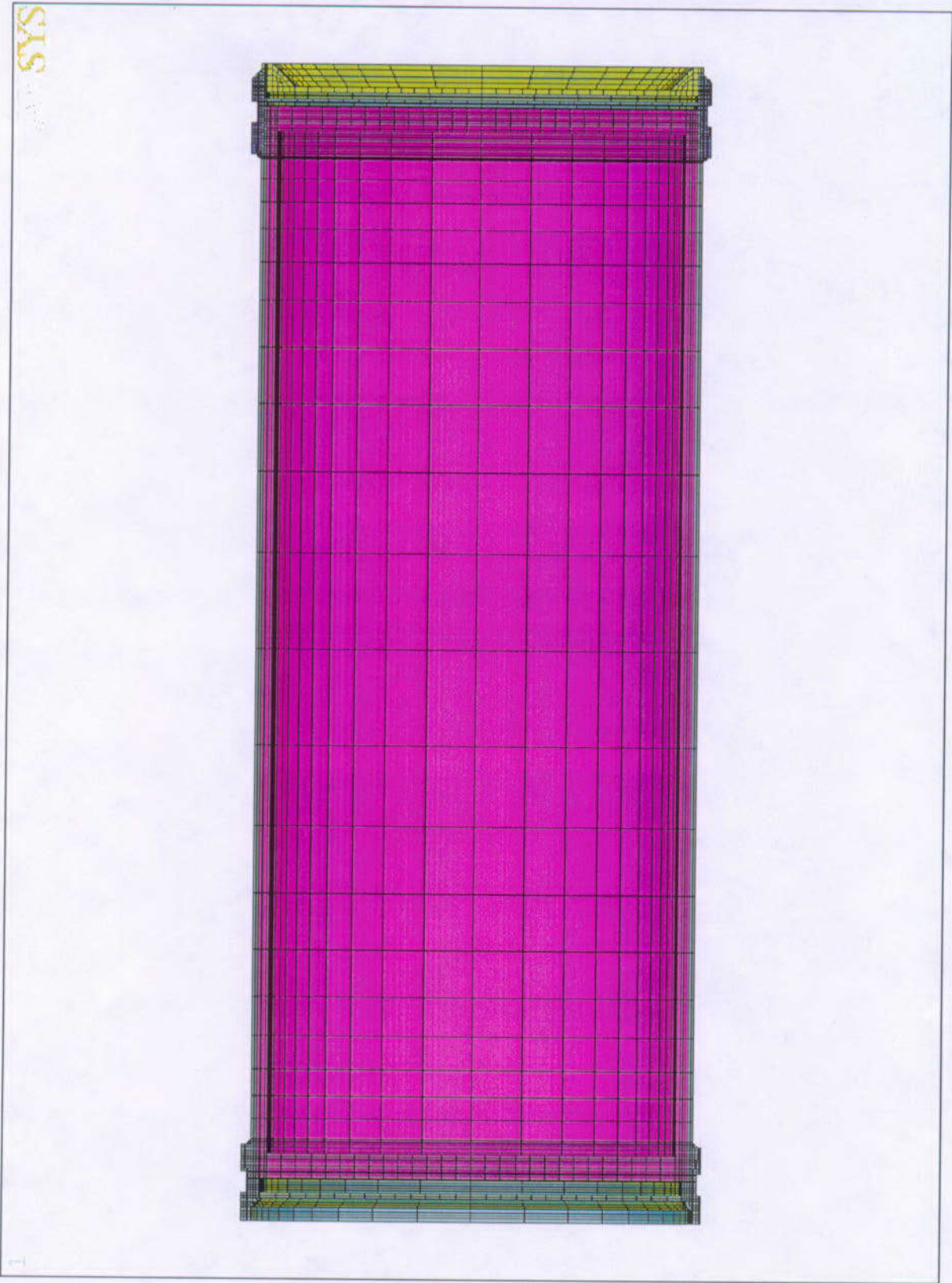


Figure 1: Mesh of the 5 DHLW/DOE - Long Waste Package

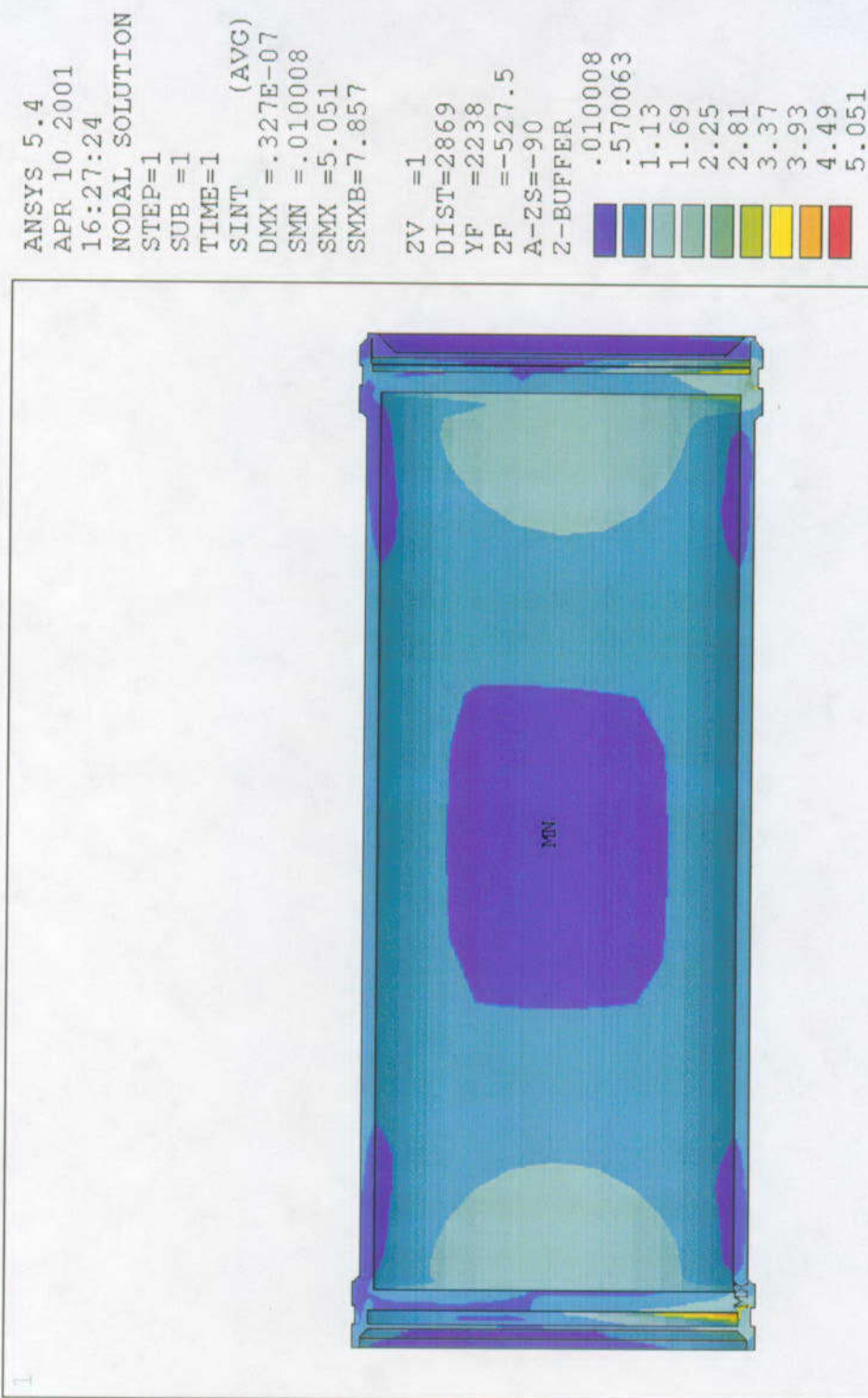


Figure 2: Stress Intensity in the 5 DHLW/DOE - Long Waste Package at RT

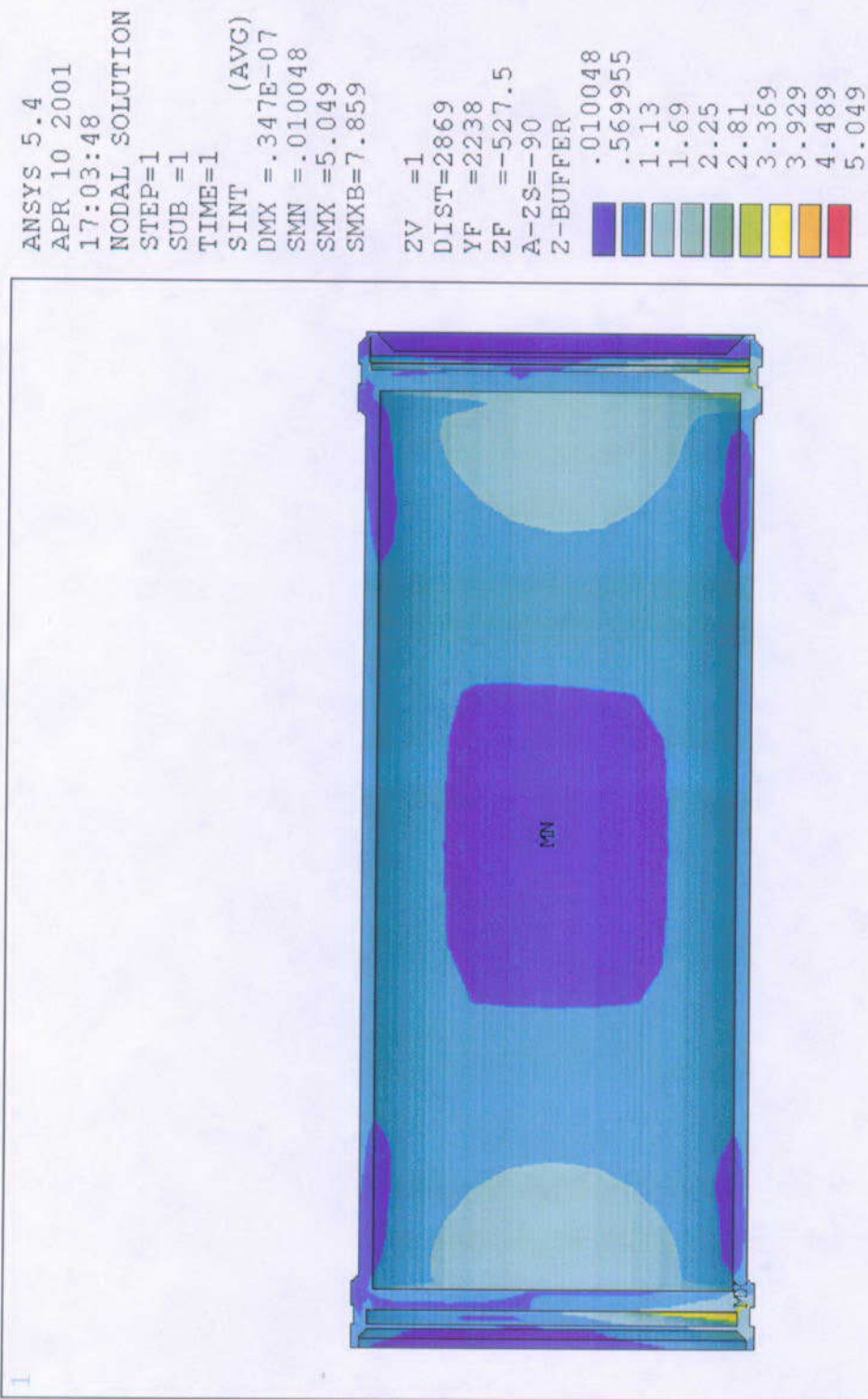


Figure 3: Stress Intensity in the 5 DHLW/DOE - Long Waste Package at 204°C

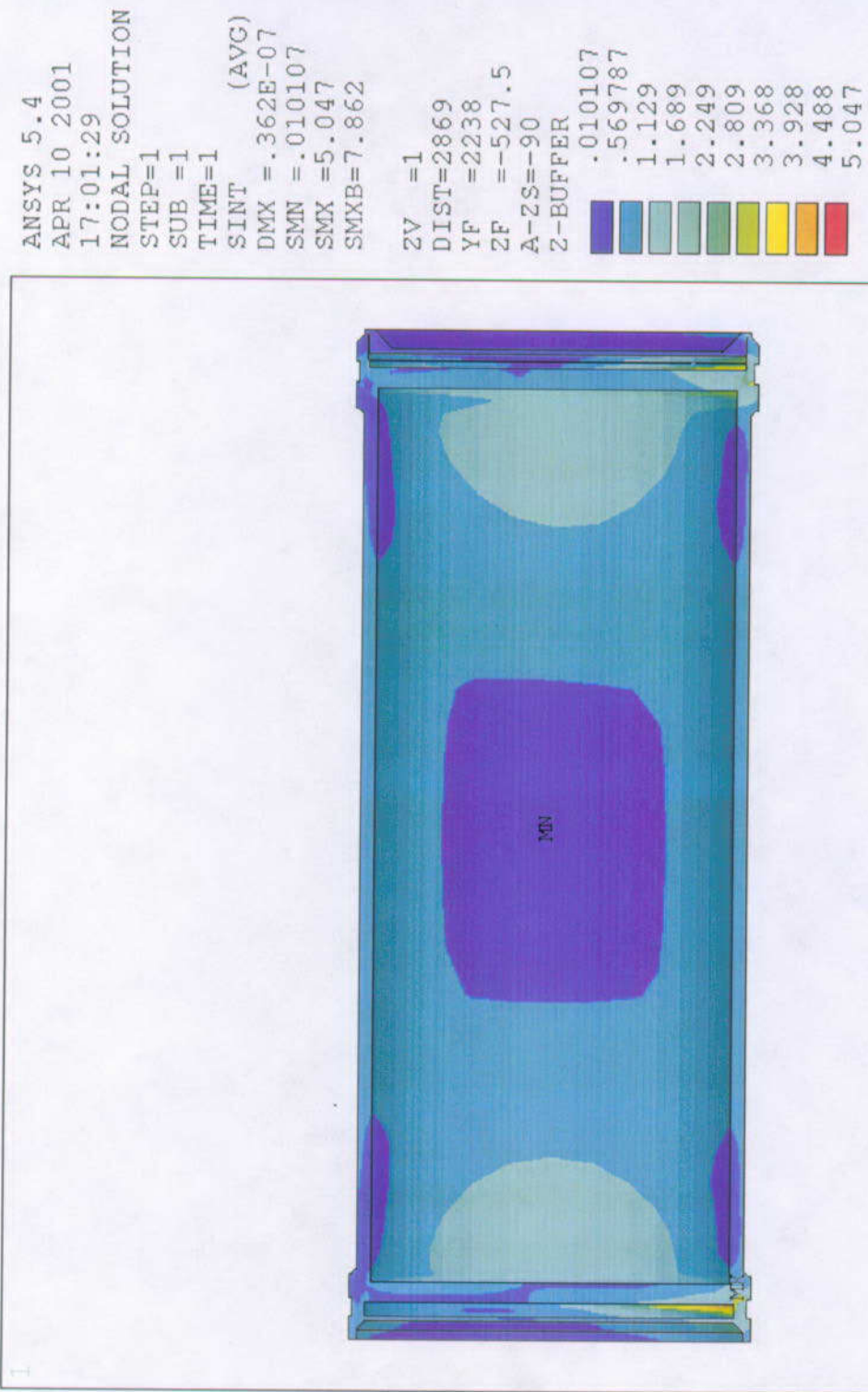


Figure 4: Stress Intensity in the 5 DHLW/DOE - Long Waste Package at 316°C

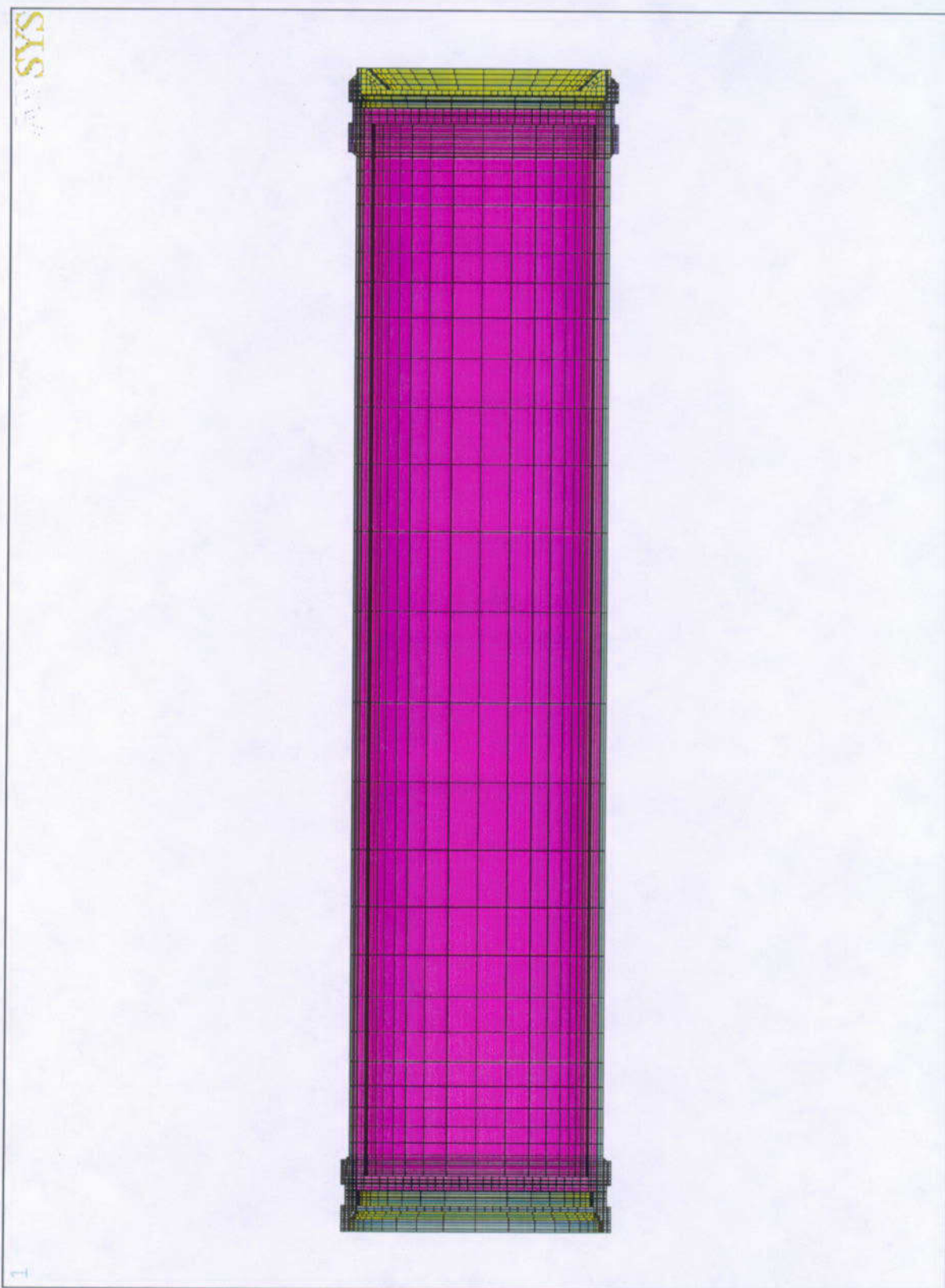


Figure 5: Mesh of the 12-PWR Long Waste Package

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 APR 9 2001
 18:09:53
 NODAL SOLUTION
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 SUB =1
 TIME=1
 SINT (AVG)
 DMX =.771E-07
 SMN =.002311
 SMX =5.734
 SMXB=9.36
 ZV =1
 DIST=3108
 YF =2455
 ZF =-332.5
 A-ZS=-90
 Z-BUFFER
 .002311
 .639204
 1.276
 1.913
 2.55
 3.187
 3.824
 4.461
 5.097
 5.734

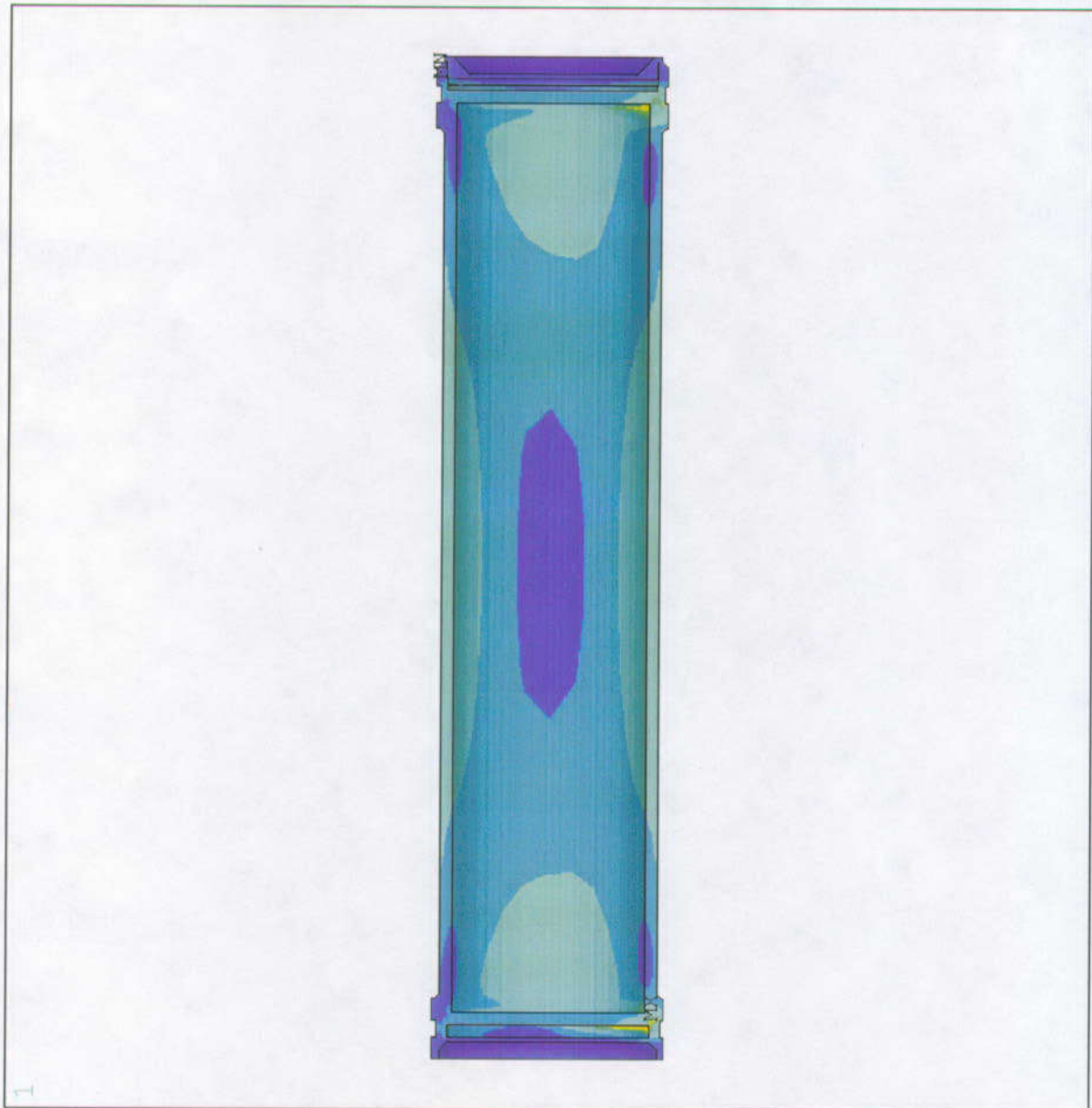


Figure 6: Stress Intensity in the 12-PWR Long Waste Package at 316°C

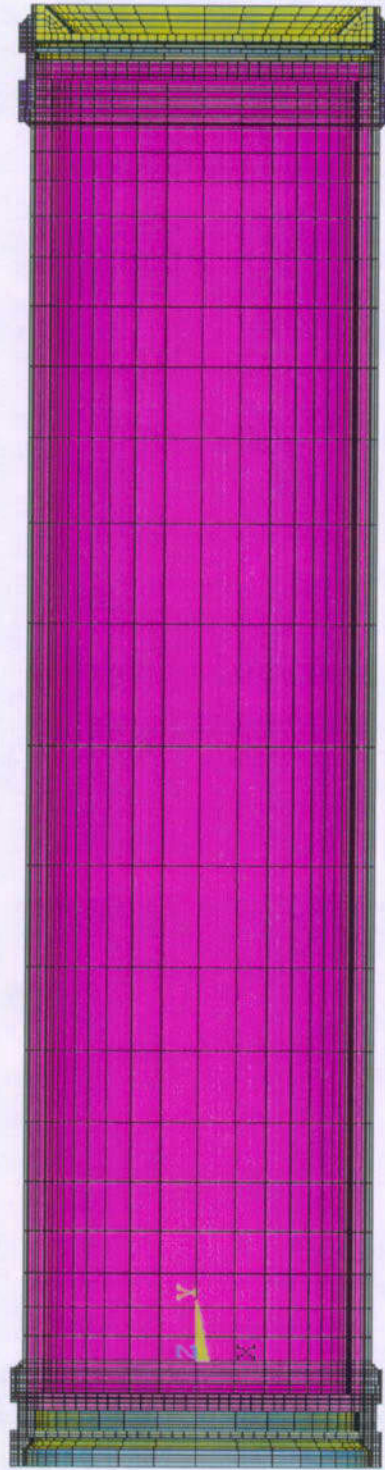


Figure 7: Mesh of the 24-BWR Waste Package

```

ANSYS 5.4
APR 10 2001
16:04:10
NODAL SOLUTION
STEP=1
SUB =1
TIME=1
SINT      (AVG)
DMX =.556E-07
SMN =.002417
SMX =4.952
SMXB=8.365

ZV =1
DIST=2808
YF =2182
ZF =-329.5
A-ZS=-90
Z-BUFFER
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.552377
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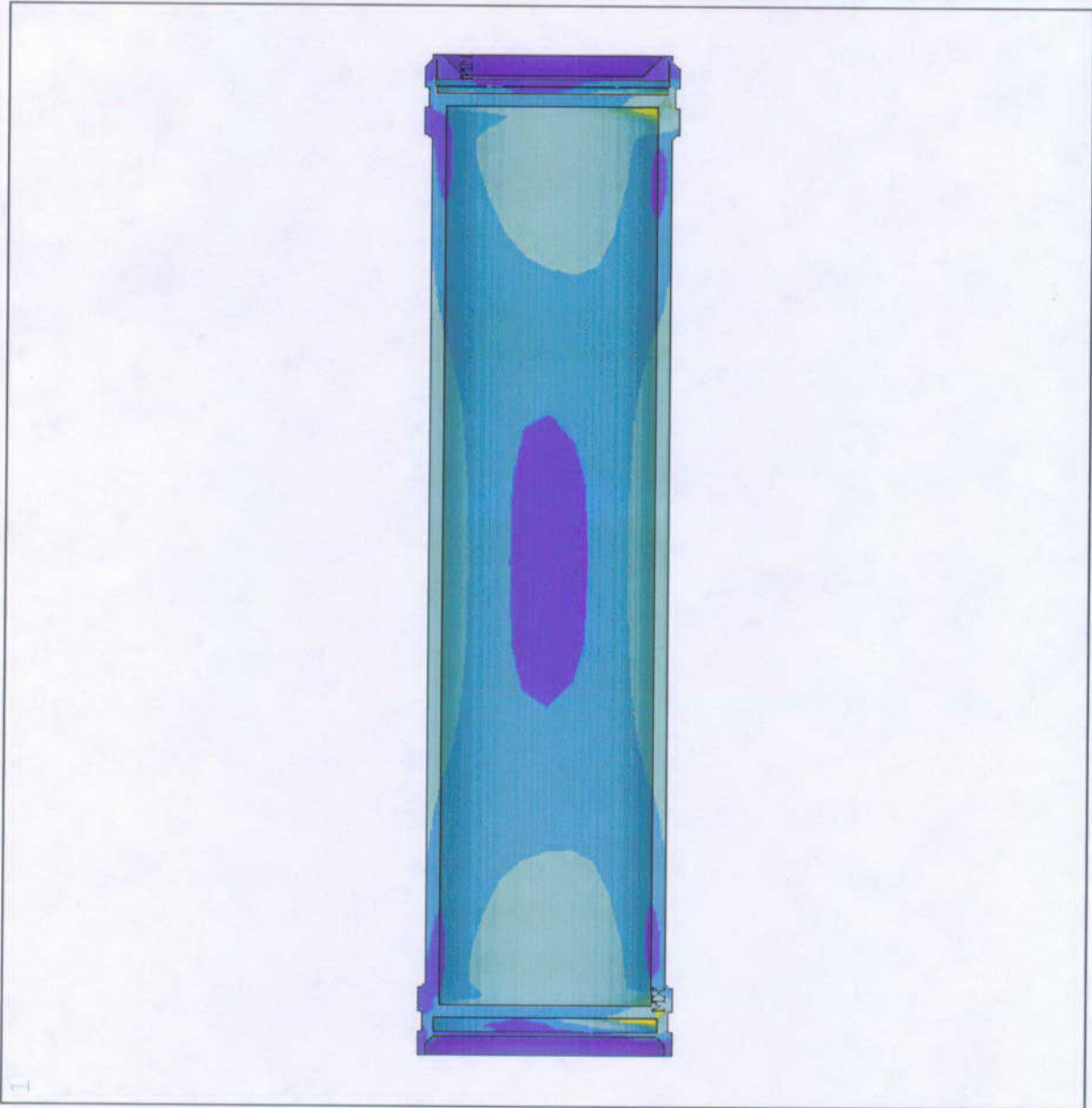


Figure 8: Stress Intensity in the 24-BWR Waste Package at 316°C

✓ file list 5/30/01 PC

OFFICE OF CIVILIAN RADIOACTIVE WASTE MANAGEMENT
SPECIAL INSTRUCTION SHEET

1. QA: QA

Page: 1 of: 1

Complete Only Applicable Items

This is a placeholder page for records that cannot be scanned.

2. Record Date 05/24/2001		3. Accession Number ATT-10 MOL-20010530.0143	
4. Author Name(s) VALERIE DE LA BROSSE		5. Author Organization N/A	
6. Title/Description HORIZONTAL LIFTING OF 5 DHLW/DOE - LONG, 12-PWR LONG AND 24 BWR WASTE PACKAGES ATTACHMENT V, VI, VII			
7. Document Number(s) CAL-EBS-ME-000010			8. Version Designator REV. 00
9. Document Type CD-ROM		10. Medium DATA	
11. Access Control Code PUB			
12. Traceability Designator DC #26242			

AB 5/30/01

13. Comments
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