Features, Events, and Processes in UZ Flow and Transport

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11. Remarks
G.X. Zhang and J.E. Houseworth contributed Appendix D.

Change History

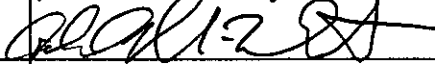| 12. Revision No.	13. Description of Change
REV 00	Initial Issue
REV 01	Revision addresses bases for assumptions, disposition descriptions, secondary FEPs, and provides more detailed exclusion arguments. Entire analysis was extensively revised such that change bars are not prudent.
REV 02	Entire scientific analysis documentation was revised. Changes were too extensive to use side bars (per Step 5.6c)1) of AP-SIII.9Q/Rev. 1/ICN 3). Revision addresses changes in the FEP list and updates to the include/exclude status and associated discussions based on revisions to technical inputs.
REV 03	Revised to qualify direct input data (Appendix C). Revised calculations of transport with fracture apertures changed by seismic activity (Sections 6.8.6, 6.8.7, and Appendix D). Changed Acceptance Criteria (Sections 4.2 and 7.2). Revised Section 6.8.2 to fulfill KTI agreement. Entire analysis was extensively revised such that change bars are not used.

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ACRONYMS AND ABBREVIATIONS

Acronyms

DOE	U.S. Department of Energy
EBS	engineered barrier system
ECRB	enhanced characterization of the repository block
EDZ	excavation disturbed zone
ESF	Exploratory Studies Facility
FEHM	finite element heat and mass
FEP	feature, event, or process
LA	license application
NRC	U.S. Nuclear Regulatory Commission
NSP	Nevada State Plane
RMEI	reasonably maximally exposed individual
RTTF	residence time transfer function
SR	site recommendation
SZ	saturated zone
TH	thermal-hydrologic
THC	thermal-hydrologic-chemical
THM	thermal-hydrologic-mechanical
THMC	thermal-hydrologic-mechanical-chemical
TSPA	total system performance assessment
UZ	unsaturated zone
YMP	Yucca Mountain Project
YMRP	*Yucca Mountain Review Plan, Final Report*

Abbreviations

CHn	Calico Hills nonwelded hydrogeologic unit
Ma	million years ago
PTn	Paintbrush Tuff nonwelded hydrogeologic unit
TSw	Topopah Spring welded hydrogeologic unit

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1. PURPOSE

The purpose of this report is to evaluate and document the inclusion or exclusion of the unsaturated zone (UZ) features, events, and processes (FEPs) with respect to modeling that supports the total system performance assessment (TSPA) for license application (LA) for a nuclear waste repository at Yucca Mountain, Nevada. A screening decision, either *Included* or *Excluded*, is given for each FEP, along with the technical basis for the screening decision. This information is required by the U.S. Nuclear Regulatory Commission (NRC) in 10 CFR 63.114 (d, e, and f) [DIRS 156605].

The FEPs deal with UZ flow and radionuclide transport, including climate, surface water infiltration, percolation, drift seepage, and thermally coupled processes. This analysis summarizes the implementation of each FEP in TSPA-LA (that is, how the FEP is included) and also provides the technical basis for exclusion from TSPA-LA (that is, why the FEP is excluded). This report supports TSPA-LA.

1.1   PLANNING AND DOCUMENTATION

Development of this report follows the technical work scope, content, and management in *Technical Work Plan for: Regulatory Integration Team Revision of Features, Events, and Processes (FEPs) Analysis Reports Integration* (BSC 2004 [DIRS 170408]), with the following deviations: FEP 2.2.07.21.0A, Drift shadow forms below repository, previously assigned to this report in Appendix A of the technical work plan, has been reassigned to *Engineered Barrier System Features, Events, and Processes* (BSC 2004 [DIRS 169898]). FEPs 2.2.08.05.0A, Diffusion in the UZ, and 2.2.07.06.0A, Episodic or pulse release from repository, defined in the technical work plan as included FEPs, were determined to be excluded during this analysis.

1.2   SCOPE

The scope of this report is to describe, evaluate, and document screening decisions and technical bases for the UZ FEPs for TSPA-LA. TSPA-LA dispositions are provided in Section 6.2 for FEPs that are included in the TSPA-LA. The disposition is a consolidated summary of how each FEP has been included and addressed in the TSPA-LA model, based on supporting technical analysis reports and model reports that describe the inclusion of the FEP. This report also provides, in Section 6.1.3, a list, or reference roadmap, of the specific supporting technical AMRs that provide more detailed discussions of the FEP. This report in turn is used as input to MDL-WIS-PA-000004, *Total System Performance Assessment Model/Analysis for License Application.*

This report provides, in Sections 6.3 through 6.9, a screening argument for each FEP that is excluded from the TSPA-LA, which identifies the basis for the screening decision (that is, low probability, low consequence, or by regulation) and discusses the technical basis that supports that decision. Appropriate references to Yucca Mountain Project (YMP) and non-Project information support the exclusion.

In cases where a FEP covers multiple technical areas and is shared with other FEP reports, only a partial technical basis is provided for the screening decision as it relates to UZ concerns. The full technical basis for these shared FEPs is addressed collectively by all of the sharing FEP

reports. This information is provided with the individual FEP discussions in Sections 6.2 through 6.9.

The YMP FEP analysis and scenario development process is explained in *The Development of the TSPA-LA Features, Events, and Processes* (BSC 2004 [DIRS 168706], Sections 2.4, 3, and 4). As part of that process, the TSPA-LA FEP list (DTN: MO0407SEPFEPLA.000 [DIRS 170760]) was developed. This DTN was used as an initial input to the UZ FEP analysis. The list of UZ TSPA-LA FEPs, which is a subset of the LA FEP list, is presented in Table 1-1, including the designation of shared FEPs. This list was derived from DTN: MO0407SEPFEPLA.000 [DIRS 170760] with subsequent modifications to the FEP list, FEP names, and/or FEP descriptions. These modifications are documented in the "FEP History File" in the FEP database (BSC 2004 [DIRS 168706], Table 6-2). Changes in the FEP list, FEP names, and FEP descriptions also can be traced through that report. Section 4 lists direct inputs supporting the screening decisions. FEP discussions providing identification (FEP number, name, and description) and screening (screening decision, screening argument or TSPA disposition) information are in Section 6.2 for included FEPs and in Sections 6.3 through 6.9 for excluded FEPs.

Table 1-1.   Unsaturated Zone FEPs for TSPA-LA

FEP Number	FEP Name	Addressed in Section	Sharing FEP Report [a]
1.1.01.01.0A	Open site investigation boreholes	6.3.1	(none)
1.1.01.01.0B	Influx through holes drilled in drift wall or crown	6.3.2	(none)
1.1.02.01.0A	Site flooding (during construction and operation)	6.3.3	(none)
1.1.02.02.0A	Preclosure ventilation	6.2.1	EBS
1.1.04.01.0A	Incomplete closure	6.3.4	(none)
1.1.11.00.0A	Monitoring of the repository	6.3.5	SYS
1.2.02.01.0A	Fractures	6.2.2	SZ
1.2.02.02.0A	Faults	6.2.3	SZ
1.2.04.02.0A	Igneous activity changes rock properties	6.8.1	DE SZ
1.2.06.00.0A	Hydrothermal activity	6.8.2	SZ
1.2.07.01.0A	Erosion/denudation	6.5.1	(none)
1.2.07.02.0A	Deposition	6.5.2	(none)
1.2.09.02.0A	Large-scale dissolution	6.5.3	SZ
1.2.10.01.0A	Hydrologic response to seismic activity	6.8.3	DE SZ
1.2.10.02.0A	Hydrologic response to igneous activity	6.8.4	DE SZ
1.3.01.00.0A	Climate change	6.2.4	Bio
1.3.04.00.0A	Periglacial effects	6.4.1	Bio
1.3.05.00.0A	Glacial and ice sheet effect	6.4.2	Bio
1.3.07.01.0A	Water table decline	6.4.3	SZ
1.3.07.02.0B	Water table rise affects UZ	6.2.5	(none)
1.4.01.00.0A	Human influences on climate	6.6.1	Bio
1.4.01.01.0A	Climate modification increases recharge	6.2.6	(none)
1.4.01.02.0A	Greenhouse gas effects	6.6.2	Bio
1.4.01.03.0A	Acid rain	6.6.3	Bio
1.4.01.04.0A	Ozone layer failure	6.6.4	Bio
1.4.06.01.0A	Altered soil or surface water chemistry	6.6.5	(none)
2.1.05.01.0A	Flow through seals (access ramps and ventilation shafts)	6.3.6	(none)
2.1.05.02.0A	Radionuclide transport through seals	6.3.7	(none)
2.1.05.03.0A	Degradation of seals	6.3.8	(none)
2.1.08.01.0A	Water influx at the repository	6.2.7	(none)
2.1.08.02.0A	Enhanced influx at the repository	6.2.8	(none)
2.1.09.12.0A	Rind (chemically altered zone) forms in the near-field	6.9.1	(none)
2.1.09.21.0C	Transport of particles larger than colloids in the UZ	6.4.4	(none)
2.2.01.01.0A	Mechanical effects of excavation and construction in the near-field	6.2.9	(none)
2.2.01.01.0B	Chemical effects of excavation and construction in the near-field	6.9.2	(none)

Table 1-1.   Unsaturated Zone FEPs for TSPA-LA (Continued)

FEP Number	FEP Name	Addressed in Section	Sharing FEP Report [a]
2.2.01.02.0A	Thermally-induced stress changes in the near-field	6.9.3	EBS
2.2.01.03.0A	Changes in fluid saturations in the excavation disturbed zone	6.9.4	(none)
2.2.01.04.0A	Radionuclide solubility in the excavation disturbed zone	6.9.5	(none)
2.2.01.05.0A	Radionuclide transport in the excavation disturbed zone	6.9.6	(none)
2.2.03.01.0A	Stratigraphy	6.2.10	SZ
2.2.03.02.0A	Rock properties of host rock and other units	6.2.11	SZ
2.2.06.01.0A	Seismic activity changes porosity and permeability of rock	6.8.5	DE SZ
2.2.06.02.0A	Seismic activity changes porosity and permeability of faults	6.8.6	DE SZ
2.2.06.02.0B	Seismic activity changes porosity and permeability of fractures	6.8.7	DE SZ
2.2.06.03.0A	Seismic activity alters perched water zones	6.8.8	DE
2.2.06.04.0A	Effects of subsidence	6.5.4	(none)
2.2.07.01.0A	Locally saturated flow at bedrock/alluvium contact	6.2.12	(none)
2.2.07.02.0A	Unsaturated groundwater flow in the geosphere	6.2.13	(none)
2.2.07.03.0A	Capillary rise in the UZ	6.2.14	(none)
2.2.07.04.0A	Focusing of unsaturated flow (fingers, weeps)	6.2.15	(none)
2.2.07.05.0A	Flow in the UZ from episodic infiltration	6.4.5	(none)
2.2.07.06.0A	Episodic or pulse release from repository	6.4.6	EBS
2.2.07.06.0B	Long-term release of radionuclides from the repository	6.2.16	EBS
2.2.07.07.0A	Perched water develops	6.2.17	(none)
2.2.07.08.0A	Fracture flow in the UZ	6.2.18	(none)
2.2.07.09.0A	Matrix imbibition in the UZ	6.2.19	(none)
2.2.07.10.0A	Condensation zone forms around drifts	6.2.20	(none)
2.2.07.11.0A	Resaturation of geosphere dry-out zone	6.2.21	(none)
2.2.07.15.0B	Advection and dispersion in the UZ	6.2.22	(none)
2.2.07.18.0A	Film flow into the repository	6.2.23	(none)
2.2.07.19.0A	Lateral flow from Solitario Canyon Fault enters drifts	6.2.24	(none)
2.2.07.20.0A	Flow diversion around repository drifts	6.2.25	(none)
2.2.08.01.0B	Chemical characteristics of groundwater in the UZ	6.2.26	(none)
2.2.08.03.0B	Geochemical interactions and evolution in the UZ	6.9.7	(none)
2.2.08.04.0A	Re-dissolution of precipitates directs more corrosive fluids to waste packages	6.2.27	EBS
2.2.08.05.0A	Diffusion in the UZ	6.9.17	(none)
2.2.08.06.0B	Complexation in the UZ	6.2.28	(none)
2.2.08.07.0B	Radionuclide solubility limits in the UZ	6.9.8	(none)
2.2.08.08.0B	Matrix diffusion in the UZ	6.2.29	(none)
2.2.08.09.0B	Sorption in the UZ	6.2.30	(none)

Table 1-1.   Unsaturated Zone FEPs for TSPA-LA (Continued)

FEP Number	FEP Name	Addressed in Section	Sharing FEP Report [a]
2.2.08.10.0B	Colloidal transport in the UZ	6.2.31	(none)
2.2.08.12.0A	Chemistry of water flowing into the drift	6.2.32	(none)
2.2.09.01.0B	Microbial activity in the UZ	6.2.33	(none)
2.2.10.01.0A	Repository-induced thermal effects on flow in the UZ	6.9.9	(none)
2.2.10.03.0B	Natural geothermal effects on flow in the UZ	6.2.34	(none)
2.2.10.04.0A	Thermo-mechanical stresses alter characteristics of fractures near repository	6.9.10	SZ
2.2.10.04.0B	Thermo-mechanical stresses alter characteristics of faults near repository	6.9.11	SZ
2.2.10.05.0A	Thermo-mechanical stresses alter characteristics of rocks above and below the repository	6.9.12	SZ
2.2.10.06.0A	Thermo-chemical alteration in the UZ (solubility, speciation, phase changes, precipitation/dissolution)	6.9.13	(none)
2.2.10.07.0A	Thermo-chemical alteration of the Calico Hills unit	6.9.14	(none)
2.2.10.09.0A	Thermo-chemical alteration of the Topopah Spring basal vitrophyre	6.9.15	(none)
2.2.10.10.0A	Two-phase buoyant flow/heat pipes	6.2.35	(none)
2.2.10.11.0A	Natural air flow in the UZ	6.7.1	(none)
2.2.10.12.0A	Geosphere dry-out due to waste heat	6.2.36	(none)
2.2.10.14.0A	Mineralogic dehydration reactions	6.9.16	(none)
2.2.11.02.0A	Gas effects in the UZ	6.7.2	(none)
2.2.11.03.0A	Gas transport in geosphere	6.7.3	(none)
2.2.12.00.0A	Undetected features in the UZ	6.8.9	(none)
2.3.01.00.0A	Topography and morphology	6.2.37	(none)
2.3.11.01.0A	Precipitation	6.2.38	Bio
2.3.11.02.0A	Surface runoff and flooding	6.2.39	(none)
2.3.11.03.0A	Infiltration and recharge	6.2.40	(none)
3.1.01.01.0A	Radioactive decay and ingrowth	6.2.41	WF SZ Bio

[a] Bio=biosphere; DE= disruptive events; EBS=engineered barrier system; FEP=feature, event, or process; LA=license application; SYS=system level FEPs report; SZ=saturated zone; TSPA=total system performance assessment; WF= waste form

1.3   SCIENTIFIC ANALYSIS AND LIMITATIONS

This report provides FEP screening information for the LA project-specific FEP database and promotes traceability and transparency for both included and excluded UZ FEPs. The report is intended for use as the documentation for inclusion or exclusion of UZ FEPs within or from the TSPA-LA model. The following limitations apply to this report:

- Because this report cites other reports and controlled documents as direct input, limitations inherently include any limitations or constraints described in the cited reports or controlled documents.

- In cases where FEPs are shared (that is, where the FEP affects more than one model area), the scope is limited to effects of the FEP on UZ flow and transport. The full technical basis for each shared FEP is addressed, collectively, by this report and all sharing FEP reports.

- For screening purposes, mean values of probabilities, mean amplitude of events, or mean value of consequences (e.g., mean time to waste package degradation) are used as a basis for reaching an include or exclude decision. Mean values are determined based on the range of possible values.

- The results of the FEP screening are specific to the repository design and processes for YMP available at the time of the TSPA-LA. Changes in direct inputs listed in Section 4.1, in baseline conditions used for this evaluation, or in other subsurface conditions, will need to be evaluated to determine whether the changes are within the limits stated in the FEP evaluations. Engineering and design changes are subject to evaluation to determine whether there are any adverse impacts to safety, as codified at 10 CFR 63.73 and in Subparts F and G [DIRS 156605]. See also the requirements at 10 CFR 63.44.

2. QUALITY ASSURANCE

Development of this analysis report and the supporting modeling activities are subject to the Yucca Mountain Project quality assurance (QA) program, as indicated in *Technical Work Plan for: Regulatory Integration Team Revision of Features, Events, and Processes (FEPs) Analysis Reports Integration* (BSC 2004 [DIRS 170408], Section 8.1). Approved QA procedures identified in Section 4 of the technical work plan have been used to conduct and document the activities described in this report. Section 8.4 of the technical work plan also identifies applicable controls for the electronic management of data during the analysis and documentation activities. This report was developed under AP-SIII.9Q, *Scientific Analyses*.

This analysis report provides information about radionuclide transport through the UZ above and below the repository, which are natural barriers classified in *Q-List* (BSC 2004 [DIRS 168361]) as Safety Category because they are important to waste isolation, as defined in AP-2.22Q, *Classification Analyses and Maintenance of the Q-List*. The results of this report are important to the demonstration of compliance with the postclosure performance objectives prescribed in 10 CFR 63.113 [DIRS 156605]. The report contributes to the analysis and modeling data used to support postclosure performance assessment; the conclusions do not directly impact engineered features important to safety, as defined in AP-2.22Q.

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3. USE OF SOFTWARE

Calculations to support exclusion arguments presented in Sections 6.8.6 and 6.8.7 and Appendix D used software listed in Table 3-1. These are appropriate for the intended application and were used only within the range of validation. These codes were obtained from software configuration management in accordance with LP-SI.11Q-BSC, *Software Management.*

Table 3-1.   Qualified Software Used in This Report

Software Name, Codes	Version	Software Tracking Number (STN)	DIRS Reference Number	Platform/Operating System
TOUGH2	1.4	10007-1.4-01	146496	SUN / OSF1 V4.0
T2R3D	1.4	10006-1.4-00	146654	SUN / UNIX

TOUGH2 V1.4 (LBNL 2000 [DIRS 146496]) and T2R3D (LBNL 1999 [DIRS 146654]) were used in Appendix D for modeling UZ flow and radionuclide transport in the UZ, respectively. The results of those calculations are the basis for FEP exclusion arguments presented in Sections 6.8.6 and 6.8.7. The selection of TOUGH2 and T2R3D to evaluate UZ flow and transport is based on the fact that these software codes have been developed on the Yucca Mountain Project specifically for this purpose.

Pre- and postprocessing were performed using Microsoft Excel (v. 97-SR-1 and 2000), and visual display graphics were developed using Tecplot v. 7.0-4.0 for Microsoft Windows. No other software requiring qualification in accordance with LP-SI.11Q-BSC was used for the development of this report. Standard functions of Excel (v. 97-SR-1) and visual display graphics programs (Tecplot v. 7.0-4.0 for Microsoft Windows) were used. All information required for an independent person to reproduce the work using these standard software programs, including the input, computation, and output, is included in this report. Excel calculations are documented in Appendices A and B.

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4. INPUTS

AP-3.15Q, *Managing Technical Product Inputs,* categorizes technical product input usage as either direct input or indirect input. Direct input is used to develop the results or conclusions in a technical product. Indirect input is used to provide additional information, often corroborative, that is not directly used in the development of results or conclusions. This section describes and lists direct inputs.

Section 4.1 identifies all direct inputs used in this FEP report. The direct inputs were obtained from controlled source documents and other appropriate sources in accordance with the controlling procedure AP-3.15Q. Section 4.2 identifies the FEP screening criteria described in 10 CFR Part 63 [DIRS 156605] along with the FEP screening criteria derived directly from 10 CFR Part 63 [DIRS 156605].

The direct inputs listed in Section 4.1 are appropriate for use, as discussed below:

Established facts: Richards 1931 [DIRS 104252], pp. 319-321 presents the commonly used conservation law for unsaturated single-phase flow based on the fact that for air and water in the unsaturated zone, capillary forces dominate the liquid pressure and the gas phase rapidly equilibrates such that a constant gas-phase pressure is suitable.

Perry and Chilton (1973 [DIRS 104946], Equation 5-215) presents Stokes' law, which is the standard relationship used for settling of particles for which the Reynolds number is less than 0.1 (Vanoni 1977 [DIRS 164901], p. 23). The Reynolds number is sufficiently small for particles on the order of 1 μm in diameter, as used in Section 6.4.4 (Vanoni 1977 [DIRS 164901], Figure 2.2).

Repository design information: Repository design information is presented in controlled design drawings and requirements (BSC 2004 [DIRS 168370]; BSC 2004 [DIRS 168489]; BSC 2004 [DIRS 169058]; BSC 2004 [DIRS 164519]; BSC 2004 [DIRS 170058]; BSC 2004 [DIRS 171676], Sections 3.1.1.13.1 through 3.1.1.13.3), which represent the best available information concerning repository system characteristics.

Site characterization information: Information on site characterization boreholes are provided in input DTNs: SNF40060298001.001 [DIRS 107372], MO9906GPS98410.000 [DIRS 109059], MO0004QGFMPICK.000 [DIRS 152554], and MO0010CPORGLOG.003 [DIRS 155959]. This is the best available information pertaining to location, stratigraphic units encountered and contact depths, and total borehole depth for the site characterization boreholes evaluated in Section 6.3.1.

Data qualified within this report: Unqualified data used as direct input for this report are qualified in Appendix C, where their appropriateness for the intended purpose is documented.

All remaining direct inputs: All remaining direct inputs are from model and analysis reports qualified for use to support the Yucca Mountain license application. The information used as inputs from these reports pertain directly to the TSPA dispositions or screening arguments presented in Sections 6.2 through 6.9 and, therefore, are suitable for their intended use.

4.1   DIRECT INPUTS

The LA FEP list (DTN: MO0407SEPFEPLA.000 [DIRS 170760]) was used as a direct input to provide the initial list of UZ FEPs for screening in this report. The LA FEP list identifies a FEP report or a set of sharing FEP reports for each FEP. Subsequent additions or deletions from that FEP list (numbers, names, or descriptions) are described in Section 6.1.1 and can be traced through the "FEP History File" in the FEP database (BSC 2004 [DIRS 168706], Table 6-2). Direct inputs used for the FEP inclusion and exclusion are listed in Tables 4-1 and 4-2, respectively. Several direct inputs in Table 4-2 have been qualified for use in accordance with AP-SIII.2Q, *Qualification of Unqualified Data*, or AP-SIII.9Q. The qualification reports are presented in Appendix C.

Table 4-1. Direct Inputs for Inclusion of FEPs

Source (in order of DIRS number)	Category	Used in Section Number	Description
LL000122051021.116 [DIRS 142973]	Data	6.2.31	Summary of analyses of glass dissolution filtrates
LB0205REVUZPRP.001 [DIRS 159525]	Data	6.2.2, 6.2.11, 6.2.14, 6.2.18	Fracture properties
LB0207REVUZPRP.001 [DIRS 159526]	Data	6.2.2, 6.2.11	Fracture properties
LB0302DSCPTHCS.002 [DIRS 161976]	Data	6.2.1, 6.2.2, 6.2.4, 6.2.6, 6.2.7, 6.2.10, 6.2.11, 6.2.13, 6.2.15, 6.2.18, 6.2.19, 6.2.20, 6.2.21, 6.2.26, 6.2.27, 6.2.32, 6.2.34, 6.2.35, 6.2.36	Drift-scale coupled processes (THC seepage) model: data summary
LB0302SCMREV02.002 [DIRS 162273]	Data	6.2.23	Seepage calibration model capillary strength parameter results
LB0302PTNTSW9I.001 [DIRS 162277]	Data	6.2.4, 6.2.6, 6.2.7	PTn/TSw flux maps from UZ flow model
LA0408AM831341.001 [DIRS 171584]	Data	6.2.26, 6.2.28, 6.2.30	UZ distribution coefficients (K_ds) for U, Np, Pu, Am, Pa, Cs, Sr, Ra, and Th
LA0303HV831352.002 [DIRS 163558]	Data	6.2.31	Colloid retardation factors for the saturated zone fractured volcanics
LB0304SMDCREV2.002 [DIRS 163687]	Data	6.2.2, 6.2.8, 6.2.11, 6.2.13, 6.2.15, 6.2.18, 6.2.25	Seepage model look-up tables for TSPA
LB0301DSCPTHSM.002 [DIRS 163689]	Data	6.2.1, 6.2.2, 6.2.8, 6.2.11, 6.2.13, 6.2.15, 6.2.18, 6.2.20, 6.2.21, 6.2.25, 6.2.35, 6.2.36	TH seepage model results
LB0305PTNTSW9I.001 [DIRS 163690]	Data	6.2.4, 6.2.6, 6.2.7	PTn/TSw flux maps from UZ flow model – alternative model
SN0306T0504103.006 [DIRS 164131]	Data	6.2.30, 6.2.31	Colloid concentration and radionuclide sorption coefficients onto colloids
LB0307SEEPDRCL.002 [DIRS 164337]	Data	6.2.2, 6.2.8, 6.2.11, 6.2.13, 6.2.15, 6.2.18, 6.2.25	Seepage results for collapsed drift scenario
BSC 2004 [DIRS 164500], Appendix A	Data	6.2.30	Treatment of sorption in TSPA-LA

Table 4-1. Direct Inputs for Inclusion of FEPs (Continued)

Source (in order of DIRS number)	Category	Used in Section Number	Description
BSC 2004 [DIRS 164500], Section A4	Data	6.2.26	Treatment of sorption in TSPA-LA
BSC 2004 [DIRS 164500], Section A5	Data	6.2.26, 6.2.28, 6.2.30, 6.2.33	Treatment of sorption in TSPA-LA
BSC 2004 [DIRS 164500], Section A8	Data	6.2.26, 6.2.28, 6.2.33	Treatment of sorption in TSPA-LA
BSC 2004 [DIRS 164500], Section I8	Data	6.2.26, 6.2.30	Treatment of sorption in TSPA-LA
BSC 2004 [DIRS 164500], Sections 6.1.3, 6.18	Data	6.2.28	Treatment of complexation in TSPA-LA
BSC 2004 [DIRS 164500], Sections 6.1, 6.2.3, 6.18	Data	6.2.30	Treatment of sorption in TSPA-LA
BSC 2004 [DIRS 164500], Sections 6.1.3, 6.1.4	Data	6.2.33	Treatment of microbial effect on transport in TSPA-LA
LB0307DSTTHCR2.002 [DIRS 165541]	Data	6.2.1, 6.2.2, 6.2.4, 6.2.6, 6.2.7, 6.2.10, 6.2.11, 6.2.13, 6.2.18, 6.2.19, 6.2.20, 6.2.21, 6.2.26, 6.2.27, 6.2.32, 6.2.34, 6.2.35, 6.2.36	Drift-scale coupled processes (DST seepage) model: Data summary
LB0305TSPA18FF.001 [DIRS 165625]	Data	6.2.2, 6.2.3, 6.2.4, 6.2.6, 6.2.7, 6.2.10, 6.2.11, 6.2.13, 6.2.15, 6.2.17, 6.2.18, 6.2.19, 6.2.24, 6.2.38, 6.2.39, 6.2.40	Flow fields for present-day and future climates, converted from TOUGH2 to FEHM format.
SN0308T0503100.008 [DIRS 165640]	Data	6.2.2, 6.2.4, 6.2.11, 6.2.12, 6.2.18, 6.2.37, 6.2.39, 6.2.40	Frequency distributions for net infiltrations and weighting factors applied to lower, mean, and upper climates
BSC 2003 [DIRS 165991], Section 7.1	Data	6.2.2, 6.2.4, 6.2.11, 6.2.12, 6.2.18, 6.2.37, 6.2.38, 6.2.39	Treatment of infiltration uncertainty in TSPA-LA
BSC 2003 [DIRS 165991], Section 1.1	Data	6.2.40	Treatment of infiltration uncertainty in TSPA-LA
BSC 2003 [DIRS 165991], Section 6.1.2	Data	6.2.38, 6.2.39	Model parameters for infiltration analysis
BSC 2003 [DIRS 165991], Figure 1-1	Data	6.2.40	Repository footprint
BSC 2003 [DIRS 165991], Table 6-1	Data	6.2.2	Model parameters for infiltration analysis
BSC 2003 [DIRS 165991], Table 6-2	Data	6.2.2, 6.2.11	Treatment of infiltration uncertainty
BSC 2003 [DIRS 165991], Table 6-3	Data	6.2.2, 6.2.11, 6.2.38, 6.2.39	Treatment of infiltration uncertainty

Table 4-1. Direct Inputs for Inclusion of FEPs (Continued)

Source (in order of DIRS number)	Category	Used in Section Number	Description
LB0311ABSTHCR2.003 [DIRS 166713]	Data	6.2.1, 6.2.2, 6.2.4, 6.2.6, 6.2.7, 6.2.10, 6.2.11, 6.2.13, 6.2.18, 6.2.19, 6.2.20, 6.2.21, 6.2.26, 6.2.27, 6.2.32, 6.2.34, 6.2.35, 6.2.36	Microsoft Excel 97 spreadsheets summarizing geochemical speciation at the original drift wall, and in and around the rubble zone. These data were used to generate time profiles for predicted TH parameters, aqueous species, and CO_2 gas concentrations
LB0311ABSTHCR2.001 [DIRS 166714]	Data	6.2.1, 6.2.2, 6.2.4, 6.2.6, 6.2.7, 6.2.10, 6.2.11, 6.2.13, 6.2.15, 6.2.18, 6.2.19, 6.2.20, 6.2.21, 6.2.26, 6.2.27, 6.2.32, 6.2.34, 6.2.35, 6.2.36	Summary statistics of predicted aqueous species and CO_2 gas concentrations
LA0311BR831229.001 [DIRS 166924]	Data	6.2.29	Transfer function calculation files for UZ transport abstraction model
LA0311AM831341.001 [DIRS 167015]	Data	6.2.26, 6.2.28, 6.2.30	Correlation matrix for sampling of sorption coefficient probability distributions
BSC 2004 [DIRS 167652], Section 6.3	Data	6.2.2, 6.2.8	Process model of seepage from fractures into drift; treatment of enhanced influx at the repository for drift seepage in TSPA
BSC 2004 [DIRS 167652], Section 6.3.6	Data	6.2.4, 6.2.6, 6.2.7	Climate change and resulting change in percolation flux included in drift seepage model
BSC 2004 [DIRS 167652], Sections 6.3.2, 6.4	Data	6.2.9	Mechanical effects of excavation are included in the seepage model
BSC 2004 [DIRS 167652], Sections 6.3.2, 6.3.3, 6.3.4	Data	6.2.10, 6.2.11	Seepage simulated in Tptpmn and Tptpll layers of TSw
BSC 2004 [DIRS 167652], Sections 6.2.1, 6.3	Data	6.2.13	Conceptual and numerical model of unsaturated groundwater flow used for seepage calculations
BSC 2004 [DIRS 167652], Section 6.8	Data	6.2.15	Treatment of flow focusing in the seepage model
BSC 2004 [DIRS 167652], Sections 6.3.2, 6.3.3	Data	6.2.18	Treatment of fracture flow in the seepage model
BSC 2004 [DIRS 167652], Section 6.3	Data	6.2.19	Matrix imbibition is neglected in the seepage model
BSC 2004 [DIRS 167652], Section 6.3	Data	6.2.23	Film flow is included in the seepage model
BSC 2004 [DIRS 167652], Sections 6.2.1, 6.3.2, 6.7	Data	6.2.25	Flow diversion around opening is included in the seepage model.
BSC 2004 [DIRS 168489]	Data	6.2.1	Heat output from emplaced waste
BSC 2004 [DIRS 169131], Sections 6.4.3.1, 6.5.2	Data	6.2.1	Effect of preclosure ventilation on seepage
BSC 2004 [DIRS 169131], Sections 6.3.1, 6.4, 6.6	Data	6.2.2	Method of deriving seepage-relevant parameters, and probability distributions describing their spatial variability and uncertainty. Abstraction methodology. Effects of THC and THM processes on seepage.

Table 4-1. Direct Inputs for Inclusion of FEPs (Continued)

Source (in order of DIRS number)	Category	Used in Section Number	Description
BSC 2004 [DIRS 169131], Section 6.6.5	Data	6.2.4, 6.2.6, 6.2.7	Percolation flux distributions from flow fields output by UZ flow model
BSC 2004 [DIRS 169131], Section 6.4.1, 6.4.2, 6.4.3	Data	6.2.8	Calculation of ambient seepage, using drift scale model with distributions of seepage-relevant parameters.
BSC 2004 [DIRS 169131], Sections 6.6.2, 6.6.3; Tables 6.6-1 and 6.6-3	Data	6.2.9	Permeability and capillary-strength values, and their probability distributions, for fracture continuum
BSC 2004 [DIRS 169131], Section 6.4	Data	6.2.10	Drift-scale seepage process model.
BSC 2004 [DIRS 169131], Sections 6.4, 6.6.1, 6.6.2, 6.6.5.1	Data	6.2.11	Rock properties used in seepage calculation and seepage abstraction.
BSC 2004 [DIRS 169131], Sections 6.4, 6.6.5.1	Data	6.2.13	Method of calculating seepage. Distribution of values of seepage-relevant parameters. Effects of THC and THM processes on seepage
BSC 2004 [DIRS 169131], Sections 6.4, 6.6.5.2	Data	6.2.15	Flow focusing factor distribution and effect of heterogeneous permeability field
BSC 2004 [DIRS 169131], Sections 6.3.1, 6.4, 6.5.1.4, 6.5.2, 6.6.5, 6.7.1	Data	6.2.18	Inclusion of fracture-flow processes in seepage abstraction.
BSC 2004 [DIRS 169131], Sections 6.4, 6.6.5.1	Data	6.2.19	Matrix imbibition is not included in calculation of seepage from fractures, but is included in calculation of percolation flux.
BSC 2004 [DIRS 169131], Sections 6.3.2, 6.4.3.3, 6.5.2	Data	6.2.20	Inclusion of condensation zone in seepage abstraction.
BSC 2004 [DIRS 169131], Sections 6.4.3, 6.5.2	Data	6.2.21	Inclusion of re-saturation and reflux in seepage abstraction.
BSC 2004 [DIRS 169131], Section 6.4.1.1, Table 6.6-1	Data	6.2.23	Inclusion of film flow in fractures in seepage abstraction.
BSC 2004 [DIRS 169131], Sections 6.4.1, 6.4.2, 6.4.3	Data	6.2.25	Inclusion of flow diversion around drifts, and of drift collapse, in seepage abstraction.
BSC 2004 [DIRS 169131], Sections 6.4.3, 6.4.4	Data	6.2.34	Inclusion of natural geothermal gradient
BSC 2004 [DIRS 169131], Sections 6.3.2, 6.4.3.3, 6.5.2	Data	6.2.35	Inclusion of heat pipe effect
BSC 2004 [DIRS 169131], Sections 6.4.3.3, 6.5.2	Data	6.2.36	Inclusion of geosphere dryout
BSC 2004 [DIRS 169565], Section 5.1.4	Data	6.2.4	Timing of climate change for TSPA
BSC 2004 [DIRS 169855], Entire	Data	6.2.2, 6.2.3, 6.2.10, 6.2.11, 6.2.37	Stratigraphic sequence
BSC 2004 [DIRS 169856], Section 4.1.7, 6.5	Data	6.2.1	Treatment of preclosure ventilation in THC modeling
BSC 2004 [DIRS 169856], Sections 6.2.1, 6.4.3, 6.4.4, 6.4.7	Data	6.2.2, 6.2.18	Treatment of fracture flow in THC modeling

Table 4-1. Direct Inputs for Inclusion of FEPs (Continued)

Source (in order of DIRS number)	Category	Used in Section Number	Description
BSC 2004 [DIRS 169856], Sections 6.2.1.3, 6.5.2	Data	6.2.4, 6.2.6	Treatment of climate change in THC modeling
BSC 2004 [DIRS 169856], Sections 6.2.1, 6.2.1.3, 6.5.2, 6.5.5.2	Data	6.2.7	Percolation flux increases caused by climate change and by contribution of reflux to percolation flux
BSC 2004 [DIRS 169856], Sections 4.1.2, 6.5.1	Data	6.2.10	Treatment of stratigraphy in THC modeling
BSC 2004 [DIRS 169856], Sections 6.4.7, 6.5.5.3, Table 6.4-1	Data	6.2.11	Treatment of rock properties for THC modeling
BSC 2004 [DIRS 169856], Section 6.2.1	Data	6.2.13	Treatment of unsaturated flow and matrix imbibition in THC modeling
BSC 2004 [DIRS 169856], Section 6.3	Data	6.2.15	Treatment of matrix imbibition in THC modeling
BSC 2004 [DIRS 169856], Section 6.2.1; Figure 6.2.3	Data	6.2.19	Treatment of matrix imbibition in THC modeling
BSC 2004 [DIRS 169856], Sections 6.2, 6.5, 6.6	Data	6.2.20	Treatment of condensation in THC modeling
BSC 2004 [DIRS 169856], Sections 6.2.1, 6.5.5	Data	6.2.21	Treatment of resaturation of the rock following dryout in THC modeling
BSC 2004 [DIRS 169856], Sections 6.2.2, 6.5.5; Table 6.2-1	Data	6.2.26	Treatment of variability of groundwater chemistry in THC modeling
BSC 2004 [DIRS 169856], Sections 6.4.4, 6.4.5, 6.5.5.2	Data	6.2.27	Treatment of redissolution of precipitates in THC modeling
BSC 2004 [DIRS 169856], Sections 6.2.1.2, 6.2.2.1, 6.2.2.2	Data	6.2.32	Treatment of THC processes leading to simulation of seepage chemistry
BSC 2004 [DIRS 169856], Section 6.5.2	Data	6.2.34	Treatment of natural geothermal gradient in THC modeling
BSC 2004 [DIRS 169856], Sections 6.2.1.1, 6.2.1.2, 6.5.5.2.2	Data	6.2.35	Treatment of heat pipes and buoyant flow in THC modeling
BSC 2004 [DIRS 169856], Sections 6.2.1, 6.5.5.1	Data	6.2.36	Treatment of geosphere dryout in THC modeling
BSC 2004 [DIRS 169856], Table 6.2-1, Fig. 6.2-4	Data	6.2.40	Treatment of infiltration and recharge in THC modeling
BSC 2004 [DIRS 169857], Section 6.3	Data	6.2.2	Calibration of fracture properties
BSC 2004 [DIRS 169857], Section 6.3.4	Data	6.2.3	Calibration of fault properties
BSC 2004 [DIRS 169857], Section 6.1.4	Data	6.2.10	Treatment of stratigraphy on calibration of flow model
BSC 2004 [DIRS 169857], Section 6.3	Data	6.2.11	Calibration of rock properties
BSC 2004 [DIRS 169857], Section 6.1.4, 6.3.2	Data	6.2.15	Treatment of flow focusing in model calibration, calibration of active-fracture parameter
BSC 2004 [DIRS 169857], Section 6.1.4, 6.3	Data	6.2.13	Calibration of unsaturated flow parameters

Table 4-1. Direct Inputs for Inclusion of FEPs (Continued)

Source (in order of DIRS number)	Category	Used in Section Number	Description
BSC 2004 [DIRS 169857], Section 6.1.4, 6.3	Data	6.2.18	Calibration of parameters to simulate fracture flow
BSC 2004 [DIRS 169857], Section 6.1.5	Data	6.2.19	Treatment of matrix imbibition in model calibration
BSC 2004 [DIRS 169858], Section 6.2	Data	6.2.20	Treatment of condensation zone in post processing of THC simulations
BSC 2004 [DIRS 169858], Section 6.2.3.1	Data	6.2.21	Treatment of resaturation of dryout zone in post processing of THC simulations
BSC 2004 [DIRS 169858], Section 6.2.3	Data	6.2.27	Treatment of re-dissolution of precipitates in post processing of THC simulations
BSC 2004 [DIRS 169858], Section 6.2	Data	6.2.32	Treatment of seepage chemistry in post processing of THC simulations
BSC 2004 [DIRS 169861], Sections 6.1.5, 6.2.3	Data	6.2.2	Treatment of fractures in the UZ flow model
BSC 2004 [DIRS 169861], Sections 6.1.5, 6.2.2, 6.3.3, 6.7.3	Data	6.2.3	Treatment of faults, water influx at the repository, and diffusion in the UZ flow model
BSC 2004 [DIRS 169861], Sections 6.1.4, 6.2.5	Data	6.2.4	Treatment of climate change in UZ flow model
BSC 2004 [DIRS 169861], Section 6.6.3	Data	6.2.5	Effects of water table rise on UZ flow
BSC 2004 [DIRS 169861], Section 6.6	Data	6.2.6	Treatment of climate modification and increased recharge in the UZ flow model
BSC 2004 [DIRS 169861], Section 6.6.3	Data	6.2.7	Development of flow fields representing water influx at repository
BSC 2004 [DIRS 169861], Section 6.1.1, 6.1.2	Data	6.2.10	Treatment of stratigraphy in the UZ flow model
BSC 2004 [DIRS 169861], Section 6.1.5	Data	6.2.11	Treatment of rock properties in the UZ flow model
BSC 2004 [DIRS 169861], Sections 6.1.3, 6.1.4	Data	6.2.12	Effects of infiltration are linked to UZ flow model
BSC 2004 [DIRS 169861], Sections 6.2, 6.6, 6.7	Data	6.2.13	Treatment of unsaturated groundwater flow in the UZ flow model
BSC 2004 [DIRS 169861], Section 6.2.5	Data	6.2.14	Treatment of capillary rise in the UZ flow model
BSC 2004 [DIRS 169861], Sections 6.1.2, 6.6.3, 6.7.3	Data	6.2.15	Treatment of flow focusing in the UZ flow model
BSC 2004 [DIRS 169861], Sections 6.2.2, 6.2.3, 6.2.5, 6.6.2, 6.6.3	Data	6.2.17	Treatment of perched water in the UZ flow model
BSC 2004 [DIRS 169861], Section 6.6.3	Data	6.2.18	Fracture-continuum flow fields output by the UZ flow model
BSC 2004 [DIRS 169861], Section 6.6	Data	6.2.19	Treatment of matrix imbibition in the UZ flow model
BSC 2004 [DIRS 169861], Section 6.6.3	Data	6.2.24	Treatment of lateral flow from Solitario Canyon Fault
BSC 2004 [DIRS 169861], Section 6.3	Data	6.2.34	Treatment of natural geothermal effects in the UZ flow model
BSC 2004 [DIRS 169861], Section 6.1.1	Data	6.2.37	Incorporation of topography and morphology in UZ flow model through the grid.

Table 4-1. Direct Inputs for Inclusion of FEPs (Continued)

Source (in order of DIRS number)	Category	Used in Section Number	Description
BSC 2004 [DIRS 169861], Sections 6.1.3, 6.1.4	Data	6.2.38	Treatment of precipitation through the infiltration model in the UZ flow model
BSC 2004 [DIRS 169861], Sections 6.1.3, 6.1.4	Data	6.2.39	Treatment of surface runoff and flooding through the infiltration model in the UZ flow model
BSC 2004 [DIRS 169861], Section 6.1.4	Data	6.2.40	Treatment of infiltration and recharge in the UZ flow model
BSC 2004 [DIRS 170002], Section 6.6	Data	6.2.4	Treatment of climate change
BSC 2004 [DIRS 170004], Section 6.1, 6.2	Data	6.2.2, 6.2.13	Data used to derive seepage-relevant parameters
BSC 2004 [DIRS 170004], Section 6.6	Data	6.2.2	Data describing fracture-matrix interaction
BSC 2004 [DIRS 170004], Section 6.1	Data	6.2.9	Measurements that include the effects of construction
BSC 2004 [DIRS 170004], Sections 6.1, 6.2	Data	6.2.13	Data describing unsaturated flow
BSC 2004 [DIRS 170004], Sections 6.2, 6.6	Data	6.2.18	Data from fracture flow tests
BSC 2004 [DIRS 170004], Section 6.4	Data	6.2.19	Data from matrix imbibition tests
BSC 2004 [DIRS 170004], Section 6.2	Data	6.2.23, 6.2.25	Measurements that demonstrate flow diversion around niches and include the effects of film flow into niches
BSC 2004 [DIRS 170004], Section 6.12	Data	6.2.40	Infiltration test data
BSC 2004 [DIRS 170006], Section 6.4.3	Data	6.2.31	Colloid retardation factors
BSC 2004 [DIRS 170007], Section 6.1, Appendix B	Data	6.2.2	Treatment of fractures in infiltration model
BSC 2004 [DIRS 170007], Section 6.9	Data	6.2.4	Inclusion of future climate states in infiltration model
BSC 2004 [DIRS 170007], Section 6.3.4	Data	6.2.12	Treatment of saturated flow at bedrock/alluvium contact in infiltration model
BSC 2004 [DIRS 170007], Section 6.11	Data	6.2.6, 6.2.7	Percolation flux and increased percolation due to climate change in infiltration model
BSC 2004 [DIRS 170007], Section 6.4	Data	6.2.10	Treatment of stratigraphy in infiltration model
BSC 2004 [DIRS 170007], Section 6.6.4, Appendix B	Data	6.2.11	Treatment of rock properties in infiltration model
BSC 2004 [DIRS 170007], Sections 6.1.2, 6.11	Data	6.2.13	Treatment of unsaturated flow in infiltration model
BSC 2004 [DIRS 170007], Sections 6.1.2, 6.3.4	Data	6.2.18	Treatment of fracture flow in infiltration model
BSC 2004 [DIRS 170007], Sections 6.5.3, 6.6.1, Appendix D	Data	6.2.37	Treatment of topography and morphology in infiltration model
BSC 2004 [DIRS 170007], Sections 6.4, 6.9	Data	6.2.38	Treatment of precipitation in infiltration model
BSC 2004 [DIRS 170007], Section 6.4	Data	6.2.39	Treatment of surface runoff and flooding in infiltration model

Table 4-1. Direct Inputs for Inclusion of FEPs (Continued)

Source (in order of DIRS number)	Category	Used in Section Number	Description
BSC 2004 [DIRS 170007], Section 6.11	Data	6.2.40	Treatment of infiltration and recharge in infiltration model
BSC 2004 [DIRS 170035], Section 6.2.2	Data	6.2.29	Scale dependency of matrix diffusion
BSC 2004 [DIRS 170035], Sections 6.3, 7	Data	6.2.13	Active-fracture model
BSC 2004 [DIRS 170035], Sections 6.1.7, 6.3.7, 7	Data	6.2.15	Treatment of focusing of unsaturated flow
BSC 2004 [DIRS 170035], Section 6.3	Data	6.2.18	Treatment of fracture flow
BSC 2004 [DIRS 170035], Section 6.2.3	Data	6.2.30	Treatment of sorption
BSC 2004 [DIRS 170035], Section 6.2.4	Data	6.2.31	Treatment of colloid transport
BSC 2004 [DIRS 170041], Sections 6.4, 6.4.1, 6.4.2, 6.5.1	Data	6.2.22	Particle-tracking methodology
BSC 2004 [DIRS 170041], Sections 6.4.3, 6.5.4, 6.5.8, 6.5.12	Data	6.2.30	Treatment of sorption in particle-tracking model
BSC 2004 [DIRS 170041], Section 6.4.4	Data	6.2.41	Treatment of radioactive decay and ingrowth in particle-tracking model
BSC 2004 [DIRS 170041], Section 6.5.1	Data	6.2.3, 6.2.6, 6.2.10, 6.2.13, 6.2.17, 6.2.18, 6.2.19	Use of pregenerated flow fields output by UZ flow model for particle-tracking simulations
BSC 2004 [DIRS 170041], Sections 6.5.1, 6.5.7	Data	6.2.2, 6.2.3	Treatment of fractures for radionuclide transport in the rock
BSC 2004 [DIRS 170041], Sections 6.4.6, 6.4.7	Data	6.2.16	Treatment of radionuclide transport in TSPA
BSC 2004 [DIRS 170041], Entire	Data	6.2.2, 6.2.5, 6.2.11, 6.2.17, 6.2.30, 6.2.31	Treatment of perched water, diffusion and radioactive decay for radionuclide transport in the rock
BSC 2004 [DIRS 170041], Section 6.5.15	Data	6.2.7	Tracked-particle releases dependent upon percolation flux
BSC 2004 [DIRS 170041], Section 6.4.5	Data	6.2.29, 6.2.30, 6.2.31	Treatment of colloid-facilitated radionuclide transport in the rock
BSC 2004 [DIRS 170041], Entire	Data	6.2.22	Treatment of advection and dispersion for radionuclide transport in the rock
BSC 2004 [DIRS 170041], Sections 6.4.4, 6.5.1.4	Data	6.2.41	Treatment of radioactive decay and ingrowth
BSC 2004 [DIRS 170041], Sections 6.5.4	Data	6.2.26, 6.2.28, 6.2.33	Matrix adsorption coefficient used in particle tracking model for TSPA
BSC 2004 [DIRS 170041], Sections 6.4.5, 6.5.9	Data	6.2.31	Fraction of unretarded colloids
BSC 2004 [DIRS 170338], Sections 6.1.1, 6.2.1.4	Data	6.2.8	Grid for simulation of thermal seepage includes drift geometry
BSC 2004 [DIRS 170338], Sections 4.1.1.3, 6.2.1.3.3	Data	6.2.1	Simulation of thermal seepage includes heat removal by preclosure ventilation
BSC 2004 [DIRS 170338], Section 6.2	Data	6.2.4, 6.2.20, 6.2.21	Simulation of thermal seepage includes condensation zone and changes in percolation flux resulting from climate change

Table 4-1. Direct Inputs for Inclusion of FEPs (Continued)

Source (in order of DIRS number)	Category	Used in Section Number	Description
BSC 2004 [DIRS 170338], Section 6.2.2.2	Data	6.2.7	Refluxing condensate contributes to percolation flux
LB0406U0075FCS.002 [DIRS 170712]	Data	6.2.7	Flow focusing distribution
LA0407BR831371.001 [DIRS 170806]	Data	6.2.2, 6.2.11, 6.2.29, 6.2.30	UZ transport abstraction model, transport parameters and base case simulation results
BSC 2004 [DIRS 171764], Sections 6.3, 6.5	Data	6.2.2	Development of seepage relevant parameters for fracture continuum
BSC 2004 [DIRS 171764], Sections 6.3, 6.6, 6.8	Data	6.2.8	Treatment of enhanced influx in the seepage calibration model
BSC 2004 [DIRS 171764], Sections 6.3, 6.5.2, 6.6	Data	6.2.9	Mechanical effects of construction are included in the seepage calibration model
BSC 2004 [DIRS 171764], Section 6.5.2	Data	6.2.11	Location-specific rock properties are included in seepage calibration model
BSC 2004 [DIRS 171764], Sections 6.3.2, 6.6.1.1	Data	6.2.13	Unsaturated flow processes are accounted for in the seepage calibration model
BSC 2004 [DIRS 171764], Sections 6.3, 6.6	Data	6.2.15	Flow focusing developed from heterogeneity
BSC 2004 [DIRS 171764], Sections 6.3, 6.6	Data	6.2.18	Fracture flow is included in the seepage calibration model
BSC 2004 [DIRS 171764], Sections 6.3.3.2	Data	6.2.19	Matrix imbibition is neglected in the seepage calibration model
BSC 2004 [DIRS 171764], Sections 6.1.2, 6.3.3, 6.6.3	Data	6.2.23	Film flow is included in the seepage calibration model
BSC 2004 [DIRS 171764], Sections 6.3, 6.6, 6.8	Data	6.2.25	Flow diversion is included in the seepage calibration model

Table 4-2. Direct Inputs Used for Exclusion of FEPs

Source (in order of DIRS number)	Type	Used in Section Number	Description
DOE 1988 [DIRS 100282], Section 1.1.3.3.2	Data qualified in accordance with AP-SIII.2Q; see Appendix C, Section C10.	6.5.1	Mass wasting at Yucca Mountain
YMP 1993 [DIRS 100520], Section 3.4	Data qualified in accordance with AP-SIII.2Q; see Appendix C, Section C10.	6.4.1, 6.5.1	Erosion rate
YMP 1993 [DIRS 100520], Section 3.4	Data qualified in accordance with AP-SIII.2Q; see Appendix C, Section C10.	6.5.2	Deposition rate
Carrigan et al. 1991 [DIRS 100967], p. 1,159	Data qualified in accordance with AP-SIII.2Q; see Appendix C, Section C2.	6.8.3	Water table excursions due to a fault slip

Table 4-2. Direct Inputs Used for Exclusion of FEPs (Continued)

Source (in order of DIRS number)	Type	Used in Section Number	Description
Stock and Healy 1988 [DIRS 101022], Entire	Data qualified in accordance with AP-SIII.2Q; see Appendix C, Section C1.	6.8.3	Interpretation of stress measurements at Yucca Mountain
Stock et al. 1985 [DIRS 101027], Entire	Data qualified in accordance with AP-SIII.2Q; see Appendix C, Section C1.	6.8.3	Residual stress field at Yucca Mountain
YMP 1995 [DIRS 102215], Sections 2.5.2 and 4.2	Data qualified in accordance with AP-SIII.2Q; see Appendix C, Section C10.	6.5.1	Effects of debris flows on erosion processes
CRWMS M&O 1999 [DIRS 103618], Entire	Data qualified in accordance with AP-SIII.2Q; see Appendix C, Section C5.	6.9.9	Thermal effects on vegetation
Richards 1931 [DIRS 104252], pp. 319-321	Established fact	6.7.1	Unsaturated flow mathematical approximation
Perry and Chilton 1973 [DIRS 104946], Equation 5-215	Established Fact	6.4.4	Stokes' law
SNF40060298001.001 [DIRS 107372]	Data	Table 6-4	Stratigraphic contact depths
MO9906GPS98410.000 [DIRS 109059]	Data	6.3.1; Table 6-4	Surface borehole coordinates
Valentine et al. 1998 [DIRS 119132], Chapter 5	Data qualified in accordance with AP-SIII.2Q; see Appendix C, Section C3	6.8.1, 6.8.4	Mineral alteration resulting from hydrothermal activity
LB990801233129.009 [DIRS 118717]	Data	Appendix D	Fracture continuum hydraulic properties (k and α)
Smyth 1982 [DIRS 119483], p. 201	Data qualified in accordance with AP-SIII.2Q; see Appendix C, Section C8	6.9.16	Zeolitic alteration temperature
LB990801233129.001 [DIRS 122753]	Data	Appendix D	Grid for calculations of transport sensitivity to fracture aperture
LB990801233129.003 [DIRS 122757]	Data	Appendix D	Fracture continuum hydraulic properties (k and α)
LB9908T1233129.001 [DIRS 147115]	Data	Appendix D	Grid for transport simulations
MO0004QGFMPICK.000 [DIRS 152554]	Data	6.3.1; Table 6-4	Stratigraphic contact depths in boreholes
CRWMS M&O 2000 [DIRS 153246], Figure 4.1-7	Output from canceled document qualified in accordance with AP-SIII.9Q; see Appendix C, Section C14	6.7.3	Aqueous-phase dose for ^{14}C

Table 4-2. Direct Inputs Used for Exclusion of FEPs (Continued)

Source (in order of DIRS number)	Type	Used in Section Number	Description
CRWMS M&O 2000 [DIRS 153246], Figures 4.1-5 and 4.1-7	Output from canceled document qualified in accordance with AP-SIII.9Q; see Appendix C, Section C14	6.9.6	Change in dose rates over 10,000 years
CRWMS M&O 2000 [DIRS 153246], Figure 4.1-9	Output from canceled document qualified in accordance with AP-SIII.9Q; see Appendix C, Section C14	6.9.6	Waste package failures as a function of time
BSC 2001 [DIRS 155950], Section 5.3.2.4.4	Output from cancelled document qualified in accordance with AP-SIII.9Q; see Appendix C, Section C13	6.9.4	Sensitivity of temperature to preclosure ventilation
MO0010CPORGLOG.003 [DIRS 155959]	Data	Table 6-4	Borehole design information for USW UZ-7a
DOE 2002 [DIRS 155970], Section I.7	Data qualified in accordance with AP-SIII.2Q; see Appendix C, Section C9	6.7.3	Gas-phase dose for ^{14}C
BSC 2002 [DIRS 157928], Figures 17 through 19	Data	6.3.3	Flooding at Yucca Mountain: Map of flood-prone areas on the site surface
BSC 2001 [DIRS 158726], Sections 6.2.2 and 6.2.5	Output from superseded document qualified in accordance with AP-SIII.9Q; see Appendix C, Section C12.	6.8.9	Alternative perched water models
BSC 2001 [DIRS 158726], Section 6.7.2; Figures 6-54 through 6-56	Output from superseded document qualified in accordance with AP-SIII.9Q; see Appendix C, Section C12.	6.8.9	Transport sensitivity to perched water models
BSC 2003 [DIRS 161727],	Output from superseded document qualified in accordance with AP-SIII.9Q; see Appendix C, Section C15	Appendix A	Emplacement drift end point coordinates
LB0302DSCPTHCS.002 [DIRS 161976]	Data	6.7.2	Drift-scale coupled processes (THC seepage) model: Data summary
Zhou et al. 2003 [DIRS 162133]	Data qualified in accordance with AP-SIII.2Q; see Appendix C, Section C11	6.8.4	Effects of small-scale heterogeneity on flow and transport
LB03023DSSCP9I.001 [DIRS 163044]	Data	Appendix A, Appendix B, Figures A-1, A-2, B-1	Fracture and matrix saturation in gridblocks where perched water occurs; used to estimate potential quick release of perched water and to calculate how many years of flux this corresponds to; also to confirm that the PTn overlies the entire repository.

Table 4-2. Direct Inputs Used for Exclusion of FEPs (Continued)

Source (in order of DIRS number)	Type	Used in Section Number	Description
Wilson et al. 2003 [DIRS 163589], Section 8	Data qualified in accordance with AP-SIII.2Q; see Appendix C, Section C7.	6.8.2	Two-phase fluid inclusions
BSC 2004 [DIRS 164500], Section 6.18.4	Data	6.4.4	Colloid transport time in the UZ
BSC 2004 [DIRS 164500], Equation 6-23	Data	6.4.4	Stokes-Einstein Equation
BSC 2004 [DIRS 164500], Section A4	Data	6.9.6	Treatment of sorption in TSPA
BSC 2004 [DIRS 164500], Appendix A	Data	6.9.7, 6.9.13	Effects of pH on radionuclide sorption
BSC 2004 [DIRS 164500], Appendix A	Data	6.9.15	Effects of rock type on radionuclide sorption
BSC 2004 [DIRS 164500], Appendix A	Data	6.9.14	Effects of rock type on radionuclide sorption
BSC 2004 [DIRS 164500], Appendix I	Data	6.9.13	Effects of temperature on radionuclide sorption
BSC 2004 [DIRS 164519]	Data	6.3.1, Table 6-4	Repository layout information
Vanoni 1977 [DIRS 164901], Figure 2.51	Data qualified in accordance with AP-SIII.9Q; see Appendix C, Section C4	6.4.4	Entrainment of cohesive sediments in flowing water
BSC 2004 [DIRS 166107], Appendix R	Data	6.5.4	Effects of drift collapse
BSC 2004 [DIRS 166107], Sections 6.3 and 6.4	Data	6.9.3	Effects of temperature on fracturing, block size, rockfall, and drift degradation
MO0401MWDRPSHA.000 [DIRS 166962]	Data	6.8.6	Future fault movement for Solitario Canyon Fault
BSC 2004 [DIRS 167652], Table 6-4	Data	6.3.2, 6.9.2	Effects of boreholes on drift seepage
BSC 2004 [DIRS 167652], Section 6.5	Data	6.3.2, 6.9.2	Effects of rock bolt holes on drift seepage
BSC 2004 [DIRS 168180]	Data	6.3.1, Table 6-4	Borehole location relative to waste emplacement
BSC 2004 [DIRS 168370]	Data	6.3.1, Table 6-4	Repository layout information
BSC 2004 [DIRS 168370]	Data	6.8.8	Waste emplacement area
BSC 2004 [DIRS 168489]	Data	6.5.4	Drift spacing
BSC 2004 [DIRS 169058]	Data	6.5.4, 6.9.2	Drift diameter; ground support materials
BSC 2004 [DIRS 169131], Section 6.4.2.5	Data	6.3.2, 6.9.2	Effects of rock bolt holes on drift seepage
BSC 2004 [DIRS 169131], Section 6.4.4.2	Data	6.9.1	THC effects on drift seepage
BSC 2004 [DIRS 169131], Section 6.4.4.1	Data	6.9.3, 6.9.10	Effects of temperature-induced stress changes on permeability

Table 4-2. Direct Inputs Used for Exclusion of FEPs (Continued)

Source (in order of DIRS number)	Type	Used in Section Number	Description
BSC 2004 [DIRS 169131], Section 6.5.1.4	Data	6.9.1, 6.9.10	Effects of temperature-induced stress changes on permeability
BSC 2004 [DIRS 169131], Sections 6.4.4.1.2, 6.5.1.5	Data	6.8.6	Effects of drift collapse on seepage-relevant hydrologic properties.
BSC 2004 [DIRS 169425], Section 6.3.3.3	Data	6.9.8	Solubility of actinides at elevated temperature
LB0306DRSCLTHM.001 [DIRS 169733]	Data	6.5.4	Subsidence calculations for drifts
BSC 2004 [DIRS 169734], Section 6.4.1.4	Data	6.4.2	Information on glaciation near Yucca Mountain
BSC 2004 [DIRS 169734], Section 3.3.2	Data	6.5.3	Bulk mineral composition of Yucca Mountain
BSC 2004 [DIRS 169734], Section 4.2.3.5	Data	6.8.2, 6.8.4	Spatial extent of contact metamorphism
BSC 2004 [DIRS 169734], Section 3.6.2	Data	6.8.2	Evidence for hydrothermal activity
BSC 2004 [DIRS 169855], Section 5.2	Data	6.9.16	Location of zeolites in the UZ
BSC 2004 [DIRS 169855], Figures 6-6 through 6-8	Data	6.9.16	Location of zeolites in the UZ
BSC 2004 [DIRS 169856], Section 6.5.5.3	Data	6.9.1, 6.9.7, 6.9.13	Changes in fracture permeability due to THC processes
BSC 2004 [DIRS 169856], Figures 6.5-39 and 6.5-40	Data	6.9.1, 6.9.7, 6.9.13	Changes in fracture permeability due to THC processes
BSC 2004 [DIRS 169856]	Data	6.9.7	Effects of THC processes on water composition
BSC 2004 [DIRS 169856], Figures 6.5-12, 6.5-25, 6.5-58	Data	6.9.7, 6.9.13	Effects of THC processes on pH
BSC 2004 [DIRS 169856], Table 6.2-1	Data	6.9.7, 6.9.13	Range of variability in pH for porewater compositions
BSC 2004 [DIRS 169856], Figure 6.5-16	Data	6.9.7, 6.9.13	Effects of THC processes on water aqueous silica, Ca, Na, and Cl
BSC 2004 [DIRS 169860], Table 6.6-4	Data	6.9.2	Seepage water composition
BSC 2004 [DIRS 169860], Tables 6.6-8 through 6.6-12	Data	6.9.2	Seepage water composition
BSC 2004 [DIRS 169860], Section 6.8	Data	6.9.2	Effects of stainless steel on water composition
BSC 2004 [DIRS 169860], Section 6.12.4.1	Data	6.9.2	Effects of stainless steel on water composition
BSC 2004 [DIRS 169860], Section 6.12.4.1.3	Data	6.9.2	Effects of stainless steel on water composition
BSC 2004 [DIRS 169861], Figure H-2	Data	6.3.6, 6.3.7, 6.3.8	Breakthrough curve at repository horizon for ^{36}Cl infiltrating at surface
BSC 2004 [DIRS 169861] Appendix G	Data	6.4.5	Damping effect of PTn on episodic infiltration

Table 4-2. Direct Inputs Used for Exclusion of FEPs (Continued)

Source (in order of DIRS number)	Type	Used in Section Number	Description
BSC 2004 [DIRS 169861], Section 6.9	Data	6.8.7	Effects of infiltration uncertainty on transport uncertainty
BSC 2004 [DIRS 169861], Sections 6.2.2.1 and 6.6.3	Data	6.8.9	Flow and transport patterns in the UZ
BSC 2004 [DIRS 169861], Sections 6.2.2.2 and 6.6.3	Data	6.8.9	Effects of perched water on lateral diversion
BSC 2004 [DIRS 169861], Tables 6.1-2, 6.6-3	Data	6.9.17	Percolation flux and fraction of flux in fractures and faults
BSC 2004 [DIRS 169864], Section 6.6.1	Data	6.9.6	Effects of stress relief
BSC 2004 [DIRS 169864], Sections 6.6.2, 6.9	Data	6.9.3, 6.9.10	Effects of temperature-induced stress changes in permeability on the flow field
BSC 2004 [DIRS 169864], Section 6.7	Data	6.9.3	Effect of thermal stress on fracture permeability in low quality rock.
BSC 2004 [DIRS 169864], Figure 6.4.5-1	Data	6.9.3	Changes in fracture permeability resulting from thermal stress
BSC 2004 [DIRS 169864], Section 7.4.2; Table 4.1-3a, Table 6.4.5-1	Data	6.9.3	Rock strength and fracture spacing modeled as independent of temperature
BSC 2004 [DIRS 169864], Section 8.1	Data	6.5.4	Effects of drift subsidence
BSC 2004 [DIRS 169864], Table 4.1-3c, Table 4.1-3d	Data	6.5.4	Model domain for mechanical calculations
BSC 2004 [DIRS 169864], Section 6.2	Data	6.8.5, 6.8.6, 6.8.7	Thermal-mechanical simulations with fracture spacing and rock strength unaffected by temperature
BSC 2004 [DIRS 169864], Section 6.10.5	Data	6.9.11	Effects of THM coupled processes on permeability
BSC 2004 [DIRS 169864], Section 6.5	Data	6.9.3, 6.9.10,	Effects of stress relief on fracture permeability
BSC 2004 [DIRS 169864], Section 6.5.1	Data	6.5.4, 6.9.6	Treatment of drift collapse
BSC 2004 [DIRS 169864], Sections 6.5.5, 6.6	Data	6.9.3, 6.9.10	Effects of thermal-mechanical stress on rock matrix properties; effects of THM coupled processes on temperature and flow; effects of temperature-induced stress changes in permeability on the flow field, effects of THM processes on temperature and flow
BSC 2004 [DIRS 169866], Section 6.5	Data	6.9.12	Effects of THM processes on flow away from the waste emplacement drifts
BSC 2004 [DIRS 169866], Sections 6.4.3.3.3, 6.4.3.3.4	Data	6.9.14	Mineral alteration and hydrogeologic effects of precipitation or dissolution in the CHn
BSC 2004 [DIRS 169866], Section 6.4.3.3.2; Figure 6.4-17	Data	6.9.7, 6.9.13	pH, bicarbonate, and chloride variations under perturbed THC conditions

Table 4-2. Direct Inputs Used for Exclusion of FEPs (Continued)

Source (in order of DIRS number)	Type	Used in Section Number	Description
BSC 2004 [DIRS 169866], Figure 6.3.1-6	Data	6.9.8	Mountain-scale temperature profiles
BSC 2004 [DIRS 169866], Section 6.1.2; Figures 6.2-10a and b, 6.3.1-16a and b, 6.3.1-18	Data	6.9.9	Effects of TH processes on flow
BSC 2004 [DIRS 169866], Sections 6.4.3.3.3, 6.4.3.3.4; Figures 6.4-20 through 6.4-26	Data	6.9.15	Mineral alteration and hydrogeologic effects of precipitation or dissolution in the TSw vitrophyre
BSC 2004 [DIRS 169866], Figure 6.2-6c	Data	6.9.16	Peak temperatures in zeolitic units
BSC 2004 [DIRS 169866], Section 6.3.1	Data	6.9.16	Peak temperatures in zeolitic units
BSC 2004 [DIRS 169868], Entire	Data	6.4.6	Treatment of episodic or pulse release from repository
BSC 2004 [DIRS 169980], Section 6.3.1	Data	6.8.1, 6.8.4	Dike thicknesses
BSC 2004 [DIRS 169980], Table C-7	Data	6.8.4	Ash deposit grain sizes
BSC 2004 [DIRS 169989], Table 7-1	Data	6.8.1, 6.8.2, 6.8.4	Probability of a volcanic event
BSC 2004 [DIRS 169989], Figure 6-1	Data	6.8.2	Spatial relationship between Yucca Mountain and the associated caldera
BSC 2004 [DIRS 169989], Section 6.2	Data	6.8.1	Decline in eruptive volume in the southwestern Nevada volcanic fluid
BSC 2004 [DIRS 169989], Section 6.2	Data	6.8.2	Silicic magmatism at Yucca Mountain
BSC 2004 [DIRS 170002], Section 6.6.2	Data	6.4.1	Mean annual temperatures for glacial-transition climate
BSC 2004 [DIRS 170002], Section 6.6	Data	6.4.2, 6.4.3	Future climates
BSC 2004 [DIRS 170007], Appendix B	Data	6.8.4	Soil permeability
BSC 2004 [DIRS 170025], Section 6.3.1	Data	6.9.5, 6.9.8	Source of colloids
BSC 2004 [DIRS 170025], Section 6.3.1	Data	6.9.5, 6.9.8	Formation of true colloids from waste form
BSC 2004 [DIRS 170025], Section 6.3.1	Data	6.9.13	Source of colloids
BSC 2004 [DIRS 170025], Sections 6.3.2.1, 6.5.2.3	Data	6.9.13	Effects of temperature on colloidal stability
BSC 2004 [DIRS 170028], Figure D-1	Data	6.8.1, 6.8.4	Spatial extent of boiling near dikes
BSC 2004 [DIRS 170037], Section 6.4.5	Data	6.8.8	Water table rise

Table 4-2. Direct Inputs Used for Exclusion of FEPs (Continued)

Source (in order of DIRS number)	Type	Used in Section Number	Description
BSC 2004 [DIRS 170038], Table 6-5	Data	6.3.1, 6.9.7, 6.9.13	Fracture area per unit volume
BSC 2004 [DIRS 170040], Table E-2	Data	6.9.17	Effects of fracture aperture on fracture-matrix partitioning of radionuclides entering the UZ
BSC 2004 [DIRS 170041], Section 6.4.5	Data	6.9.13	Treatment of colloid-facilitated transport
BSC 2004 [DIRS 170041], Tables 6-2 and 6-13	Data	6.9.17	Values for dispersivity and fracture porosity
BSC 2004 [DIRS 170041], Table 6-6	Data	6.8.8	Minimum average water content of rock in the UZ within 100 m of the water table.
BSC 2004 [DIRS 170058]	Data	6.9.2	Use of cementitious materials for ground support
BSC 2004 [DIRS 170338], Section 6.2.2.1	Data	6.9.9	Diversion of water around thermal dryout zone
BSC 2004 [DIRS 170338], Section 6.2.1.3.3	Data	6.9.4	Effects of preclosure dryout on thermal seepage
BSC 2004 [DIRS 170338], Section 6.2.2.1.1	Data	6.9.9	Effects of thermal dryout and drift shadow on radionuclide transport
BSC 2004 [DIRS 170505], Sections 3.3.1.4, 3.3.2	Data	6.3.5	Effects of monitoring activities on repository performance
LB0308DRSCLTHM.001 [DIRS 171567]	Data	6.5.4	Subsidence calculations for drift in Tptpll low-quality rock
LB0408RITSSCPF.001 [DIRS 171593]	Data	6.3.1, 6.4.5	Episodic flow behavior in the PTn
BSC 2004 [DIRS 171676], Sections 3.1.1.13.1 through 3.1.1.13.3	Data	6.3.3, 6.3.7, 6.3.8	Design requirement concerning surface water inundation of the subsurface facilities
LB0408CMATUZFT.004 [DIRS 171706]	Data qualified in accordance with AP-SIII.2Q; see Appendix C, Section C6	6.9.2	Diffusion and dispersion of plumes of leachate from altered cementitious materials.
LB0408CMATUZFT.003 [DIRS 171705]	Data qualified in accordance with AP-SIII.2Q; see Appendix C, Section C6	6.9.2	Chemistry of leachate from altered cementitious materials

LA = license application; TH = thermal hydrologic; THC = thermal-hydrologic-chemical; THM = thermal-hydrologic-mechanical; TSPA = total system performance assessment; UZ = unsaturated zone.

Table 4-3   Regulations Used as Direct Inputs

Section Number	Input	Type	Description
6.6.1, 6.6.2, 6.6.3, 6.6.4	10 CFR 63.305(b) [DIRS 156605]	Established Fact	Regulatory exclusion of human effects on climate
6.6.1, 6.6.2, 6.6.3, 6.6.4	66 FR 55732 [DIRS 156671], p. 55,757	Established fact	Rationale for regulatory position excluding human influences on climate
6.6.1	67 FR 62628 [DIRS 162317]	Established fact	Rationale for regulatory position excluding human influences on climate
6.3.4 6.6.5	10 CFR 63.305(b) [DIRS 156605]	Established fact	Rationale for regulatory position excluding human influences on soil and water

Regulation 10 CFR Part 63 [DIRS 156605] and a portion of the Federal Register containing the preamble to 10 CFR Part 63 [DIRS 156605], 66 FR 55732 [DIRS 156671], and 67 FR 62628 [DIRS 162317], provide the regulatory requirements and the background information for licensing and operating the repository. These requirements and definitions were used throughout Section 6.6 to construct FEP exclusion arguments. Information from 10 CFR Part 63 [DIRS 156605] and the background information can be considered established fact and is appropriate for use in this analysis. In particular, human influences on climate are excluded on the basis of requirements of 10 CFR 63.305(b) [DIRS 156605]. The licensing rule and the supplemental information (66 FR 55732 [DIRS 156671] indicate that only natural evolution of the reference biosphere is to be included in the performance assessment and that the changes caused by the future human behaviors are not to be included. Furthermore, 10 CFR 63.305(b) [DIRS 156605] states that "DOE should not project changes in society, the biosphere (other than climate), human biology, or increases or decreases in human knowledge or technology. In all analyses done to demonstrate compliance with this part, the DOE must assume that all of those factors remain constant as they are at the time of submission of the license application." Therefore, human activities (changes in the social and institutional attributes of society, lifestyle, land use, and water use) that would alter soil or surface water chemistry are excluded on the basis of the regulatory requirements (10 CFR 63.305(b) [DIRS 156605]). The NRC has indicated that the natural systems of the biosphere should be allowed to vary consistent with the geologic records, which provide basis for predicting future biosphere changes (66 FR 55732 [DIRS 156671], p. 55,757). Because human behavior cannot be similarly predicted, such an approach cannot be used for the reasonably maximally exposed individual (66 FR 55732 [DIRS 156671], p. 55,757) and, extending this reasoning, for the human-induced changes to the environment. Therefore, the geological, hydrological and climatological factors that the DOE must vary under 10 CFR 63.305(b) [DIRS 156605], are limited to naturally occurring FEPs.

4.2   CRITERIA

This section addresses the criteria relevant to the FEP screening process. These criteria stem from the applicable regulations at 10 CFR Part 63 [DIRS 156605], as identified in *Project Requirements Document* (PRD) (Canori and Leitner 2003 [DIRS 166275]). These criteria find expression as specific acceptance criteria presented by the NRC in *Yucca Mountain Review Plan, Final Report* (NRC 2003, [DIRS 163274], Sections 2.2.1.2.1.3 and 2.2.1.2.2.3). The correlation of the regulations and Yucca Mountain Review Plan (YMRP) acceptance criteria are shown in Table 4-4. Satisfaction of the criteria is discussed in Section 7.1.

Table 4-4.   Relationships of Regulations to the YMRP Acceptance Criteria

Description of the Applicable Regulatory Requirement or Acceptance Criterion	10 CFR Part 63 [DIRS 156605] Regulatory Citation	Canori and Leitner 2003 [DIRS 166275] Associated PRD	Associated Criteria in the YMRP [DIRS 163274]
General Requirements and Scope Pertinent to FEP Screening			
Include data related to geology, hydrology, geochemistry, and geophysics	63.114(a)	PRD-002/T-015	2.2.1.2.1.3 Acceptance Criterion 1
Include information of the design of the engineered barrier system used to define parameters and conceptual models	63.114(a)	PRD-002/T-015	2.2.1.2.1.3 Acceptance Criterion 1
Account for uncertainties and variabilities in parameter values and provide the technical basis for parameter ranges, probability distributions, or bounding values	63.114(b)	PRD-002/T-015	2.2.1.2.2.3 Acceptance Criteria 2 and 3
FEP Screening Criteria			
Provide the justification and technical basis for excluding FEPs specifically excluded by regulation.	Not Applicable	Not Applicable	2.2.1.2.1.3 Acceptance Criterion 2
Provide the technical basis for either inclusion or exclusion of FEPs. Provide the justification and technical basis for those excluded based on probability.	63.114(d) 63.342	PRD-002/T-015 PRD-002/T-034	2.2.1.2.1.3 Acceptance Criterion 2 2.2.1.2.2.3 Acceptance Criteria 1 and 2
Provide the technical basis for either inclusion or exclusion of FEPs. Provide the justification and the technical basis for those excluded based on lack of significant change in resulting radiological exposure or release to the accessible environment.	63.114 (e and f) 63.342	PRD-002/T-015 PRD-002/T-034	2.2.1.2.1.3 Acceptance Criterion 2 2.2.1.2.2.3 Acceptance Criteria 1 and 2

FEPs = features, events, and processes, PRD = Project Requirements Document.

4.2.1   Project Requirements Document

Project Requirements Document (PRD) (Canori and Leitner 2003 [DIRS 166275]) documents and categorizes the regulatory requirements and other project requirements and provides a crosswalk to the various YMP organizations that are responsible for ensuring that the criteria have been addressed in the LA.   The regulatory requirements include criteria relevant to performance assessment activities, in general, and to FEP-related activities as they pertain to performance assessment, in particular. Table 4-4 provides a crosswalk between the regulatory requirements, the PRD (Canori and Leitner 2003 [DIRS 166275]), and the acceptance criteria provided in *Yucca Mountain Review Plan, Final Report* (YMRP) (NRC 2003 [DIRS 163274], Sections 2.2.1.2.1.3 and 2.2.1.2.2.3).

4.2.2   Yucca Mountain Review Plan

The acceptance criteria for the NRC review of the LA are described in the *Yucca Mountain Review Plan, Final Report* (YMRP) (NRC 2003 [DIRS 163274], Section 2.2.1.2). In Table 4-4,

YMRP acceptance criteria are correlated to the corresponding regulations as they pertain to FEP-related criteria.

The cited YMRP (NRC 2003 [DIRS 163274]) criteria are provided in Table 4-5. The YMRP acceptance criteria for FEP screening echo the regulatory screening criteria of low probability and low consequence, but also allow for exclusion of a FEP if the process is specifically excluded by the regulations (Section 4.2.3).

Table 4-5.   Relevant YMRP Acceptance Criteria

YMRP Section	Acceptance Criterion	Description
Scenario Analysis and Event Probability: Scenario Analysis (from Section 2.2.1.2.1.3 NUREG-1804 [DIRS 163274])	1. The Identification of a List of FEPs Is Adequate	The safety analysis report contains a complete list of FEPs related to the geologic setting or the degradation, deterioration, or alteration of engineered barriers (including those processes that would affect the performance of natural barriers), that have the potential to influence repository performance. The list is consistent with the site characterization data. Moreover, the comprehensive features, events, and processes list includes, but is not limited to, potentially disruptive events related to igneous activity (extrusive and intrusive); seismic shaking (high-frequency-low magnitude, and rare large-magnitude events); tectonic evolution (slip on existing faults and formation of new faults); climatic change (change to pluvial conditions); and criticality.
	2. Screening of the Initial List of Features, Events, and Processes Is Appropriate	(1) The DOE has identified all FEPs related to either the geologic setting or to the degradation, deterioration, or alteration of engineered barriers (including those processes that would affect the performance of natural barriers) that have been excluded.
		(2) The DOE has provided justification for those FEPs that have been excluded. An acceptable justification for excluding FEPs is that either the FEP is specifically excluded by regulation; probability of the FEP (generally an event) falls below the regulatory criterion; or omission of the feature, and process does not significantly change the magnitude and time of the resulting radiological exposures to the reasonably maximally exposed individual, or radionuclide releases to the accessible environment.
		(3) The DOE has provided an adequate technical basis for each FEP, excluded from the performance assessment, to support the conclusion that either the FEP is specifically excluded by regulation; the probability of the FEP falls below the regulatory criterion; or omission of the FEP does not significantly change the magnitude and time of the resulting radiological exposures to the reasonably maximally exposed individual, or radionuclide releases to the accessible environment.

Table 4-5.   Relevant YMRP Acceptance Criteria (Continued)

YMRP Section	Acceptance Criterion	Description
Scenario Analysis and Event Probability: Identification of Events with Probability Greater than 10^{-8} per Year (from Section 2.2.1.2.2.3 NUREG-1804 [DIRS 163274])	2. Probability Estimates for Future Events Are Supported by Appropriate Technical Bases	(1) Probabilities for future natural events are based on past patterns of the natural events in the Yucca Mountain region, considering the likely future conditions and interactions of the natural and engineered repository system. These probability estimates have specifically included igneous events, faulting and seismic events, and criticality events.
	3. Probability Model Support is Adequate	(1) Probability models are justified through comparison with output from detailed process level models and/or empirical observations (e.g., laboratory testing, field measurements, or natural analogs, including Yucca Mountain site data). Specifically: (a) For infrequent events, the U.S. Department of Energy justifies, to the extent appropriate, proposed probability models with data from reasonably analogous systems. Analog systems should contain significantly more events than the Yucca Mountain system, to provide reasonable evaluations of probability model performance; (b) The U.S. Department of Energy justifies, to the extent appropriate, the ability of probability models to produce results consistent with the timing and characteristics (e.g., location and magnitude) of successive past events in the Yucca Mountain system; and (c) The U.S. Department of Energy probability models for natural events use underlying geologic bases (e.g., tectonic models) that are consistent with other relevant features, events, and processes evaluated.

DOE = U.S. Department of Energy; FEP=feature, event, and process; YMRP=*Yucca Mountain Review Plan, Final Report*

4.2.3   FEPs Screening Criteria

The criteria for determining low probability, low consequence, or by regulation exclusions are described below.

Low Probability

The low-probability criterion is stated in 10 CFR 63.114(d) [DIRS 156605]:

> *Consider only events that have at least one chance in 10,000 of occurring over 10,000 years.*

and supported by 10 CFR 63.342 [DIRS 156605]:

> *The Department of Energy's (DOE) performance assessments shall not include consideration of very unlikely features, events, or processes, i.e., those that are estimated to have less than one chance in 10,000 of occurring within 10,000 years of disposal.*

As noted in Assumption 5.1, the low-probability criterion for very unlikely events corresponds to an annual-exceedance probability of 10^{-8}.

Low Consequence

The low consequence criterion is stated in 10 CFR 63.114 (e and f) [DIRS 156605]:

> *(e) Provide the technical basis for either inclusion or exclusion of specific features, events, and processes in the performance assessment. Specific features, events, and processes must be evaluated in detail if the magnitude and time of the resulting radiological exposures to the reasonably maximally exposed individual, or radionuclide releases to the accessible environment, would be significantly changed by their omission.*

> *(f) Provide the technical basis for either inclusion or exclusion of degradation, deterioration, or alteration processes of engineered barriers in the performance assessment, including those processes that would adversely affect the performance of natural barriers. Degradation, deterioration, or alteration processes of engineered barriers must be evaluated in detail if the magnitude and time of the resulting radiological exposures to the reasonably maximally exposed individual, or radionuclide releases to the accessible environment, would be significantly changed by their omission.*

and supported by 10 CFR 63.342 [DIRS 156605]:

> *DOE's performance assessments need not evaluate the impacts resulting from any features, events, and processes or sequences of events and processes with a higher chance of occurrence if the results of the performance assessments would not be changed significantly.*

Some FEPs have a beneficial effect on the TSPA, as opposed to an adverse effect. As identified in 10 CFR 63.102(j) [DIRS 156605], the concept of a performance assessment includes:

> *The features, events, and processes considered in the performance assessment should represent a wide range of both beneficial and potentially adverse effects on performance (e.g., beneficial effects of radionuclide sorption; potentially adverse effects of fracture flow or a criticality event). Those features, events, and processes expected to materially affect compliance with [10 CFR] 63.113(b) or be potentially adverse to performance are included, while events (event classes or scenario classes) that are very unlikely (less than one chance in 10,000 over 10,000 years) can be excluded from the analysis. ...*

Yucca Mountain Review Plan, Final Report (NRC 2003, Section 2.2.1 [DIRS 163274]), states:

> *In many regulatory applications, a conservative approach can be used to decrease the need to collect additional information or to justify a simplified modeling approach. Conservative estimates for the dose to the reasonably maximally exposed individual may be used to demonstrate that the proposed repository meets U.S. Nuclear Regulatory Commission regulations and provides adequate protection of public health and safety. ...The total system performance assessment is a complex analysis with many parameters, and the U.S. Department of Energy may use conservative assumptions to simplify its approaches and data collection needs. However, a technical basis ... must be provided.*

On the basis of these statements, those FEPs that are demonstrated to have only beneficial effects on the radiological exposures to the reasonably maximally exposed individual, or radionuclide releases to the accessible environment, can be excluded on the basis of low consequence because they have no adverse effects on performance.

By Regulation

Yucca Mountain Review Plan, Final Report (NRC 2003, [DIRS 163274], Section 2.2.1.2.1.3, Acceptance Criterion 2) allows for exclusion of a FEP if the process is specifically excluded by the regulations. To wit:

> The DOE has provided justification for those FEPs that have been excluded. An acceptable justification for excluding FEPs is that either the FEP is specifically excluded by regulation; probability of the FEP (generally an event) falls below the regulatory criterion; or omission of the feature, and process does not significantly change the magnitude and time of the resulting radiological exposures to the reasonably maximally exposed individual (RMEI), or radionuclide releases to the accessible environment.

4.3   CODES, STANDARDS, AND REGULATIONS

No codes, standards, or regulations, other than those identified in the *Project Requirements Documents* (Canori and Leitner 2003 [DIRS 166275], Table 2-3) and determined to be applicable in Table 4-5, were used in this analysis/model report.

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5. ASSUMPTIONS

Assumption 5.1–A regulation expressed as a probability criterion also can be expressed as an annual exceedance probability, which is defined as "the probability that a specified value will be exceeded during one year." More specifically, a stated probability screening criterion for very unlikely FEPs of 1 chance in 10,000 in 10,000 years ($10^{-4}/10^4$ yr) is assumed equivalent to a 10^{-8} annual exceedance probability or annual exceedance frequency.

Justification–The assumption of equivalence of annual exceedance probability is appropriate if the possibility of an event is equal for any given year (10 CFR 63.114(d) [DIRS 156605]). Geologic events such as earthquakes are considered independent events with regard to size, time, and location. Consequently, assuming annual equivalence is reasonable. No further confirmation is required.

Use–This assumption is used in FEPs 2.2.06.02.0A and 2.2.06.02.0B.

Assumption 5.2–It is assumed that the repository will be constructed, operated, and closed according to the regulatory requirements applicable to the construction operation and closure period. Deviations from design will be detected and corrected.

Justification–Inherent in the FEPs evaluation approach is the assumption that the repository will be constructed, operated, and closed according to the design used as the basis for the FEP screening and in accordance with NRC license requirements. This is inherent in performance evaluation of any engineering project, and design verification and performance confirmation are required as part of the construction and operation processes. Therefore, no further confirmation of the assumption is required.

Engineering and design changes are subject to evaluation to determine if there are any adverse manner impacts to safety as codified at 10 CFR 63.73 and in Subparts F and G [DIRS 156605]. See also the requirements at 10 CFR 63.32, 10 CFR 63.44, and 10 CFR 63.131 [DIRS 156605].

These requirements require the periodic and special reports regarding:

(1) Progress of construction

(2) Any data about the site, obtained during construction, that are not within the predicted limits on which the facility design was based

(3) Any deficiencies in design and construction that, if uncorrected, could adversely affect safety at any future time

(4) Results of research and development programs being conducted to resolve safety questions.

Use–Any changes in direct inputs listed in Section 4.1, in baseline conditions used for this evaluation, or in other subsurface conditions, will need to be evaluated to determine if the changes are within the limits stated in the FEP evaluations. This assumption is specifically used in FEPs 1.1.04.01.0A and 1.1.11.00.0A.

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6. SCIENTIFIC ANALYSIS DISCUSSION

The following sections discuss the UZ FEP analyses. Section 6.1 of this report discusses the methods and approach used for the FEP screening. Section 6.2 provides the screening documentation for included FEPs (those that are screened into TSPA) and Sections 6.3 through 6.9 provide the screening documentation for excluded FEPs (those that are screened out of TSPA).

6.1 METHODS AND APPROACH

The identification and screening process of a comprehensive list of FEPs potentially relevant to the postclosure performance of the Yucca Mountain repository is an ongoing, iterative process based on site-specific information, design, and regulations. FEP analysis uses the following definitions from *Yucca Mountain Review Plan, Final Report* (NRC 2003 [DIRS 163274], Glossary):

Feature   An object, structure, or condition that has a potential to affect disposal system performance.

Event   A natural or human-caused phenomenon that has a potential to affect disposal system performance and that occurs during an interval that is short compared to the period of performance.

Process   A natural or human-caused phenomenon that has a potential to affect disposal system performance and that operates during all or a significant part of the period of performance.

FEP analysis for TSPA-LA is described in *The Development of the TSPA-LA Features, Events, and Processes* (BSC 2004 [DIRS 168706]), which is summarized in the following sections.

6.1.1 Identification of Features, Events, and Processes

The first step of FEP analysis is the FEP identification and classification process, which addresses Acceptance Criterion 1 of the YMRP (NRC 2003 [DIRS 163274], Section 2.2.1.2.1.3). The TSPA-LA FEP identification and classification process is described in Section 3 of *The Development of the TSPA-LA Features, Events, and Processes* (BSC 2004 [DIRS 168706]). This classification process resulted in the LA FEP list (DTN: MO0407SEPFEPLA.000 [DIRS 170760]), which was used as initial input in this UZ FEP analysis. Subsequent modifications to the FEP list from the information shown in DTN: MO0407SEPFEPLA.000 [DIRS 170760], aside from editorial corrections to FEP descriptions, are discussed later in this section. All subsequent modifications are also documented in the "FEP History File" in the FEP database (BSC 2004 [DIRS 168706], Table 6-2). As part of the TSPA-LA FEP evaluation, FEP 2.2.07.21.0A (Drift shadow forms below repository), which was initially assigned to this report in the LA FEP list (DTN: MO0407SEPFEPLA.000 [DIRS 170760]), has been reassigned to the engineered barrier system FEPs report (BSC 2004 [DIRS 169898]). This report addresses the other 93 FEPs that are identified as UZ FEPs for TSPA-LA as noted and derived from the YMP FEPs database.

6.1.2 Feature, Event, and Process Screening Process

The second step of FEP analysis is FEP screening, which addresses Acceptance Criterion 2 of the YMRP (NRC 2003 [DIRS 163274], Section 2.2.1.2.1.3). The TSPA-LA FEP screening process is described in Section 4 of *The Development of the TSPA-LA Features, Events, and Processes* (BSC 2004 [DIRS 168706]).

For the purposes of this report, the FEPs are divided into two broad categories: included and excluded FEPs. Each FEP is screened against the specified exclusion criteria (Section 4.2.1) summarized in the following FEP screening statements:

- FEPs having less than 1 chance in 10,000 of occurring over 10,000 years may be excluded (screened out) from the TSPA on the basis of low probability (as per 10 CFR 63.114(d) [DIRS 156605])

- FEPs whose omission would not significantly change the magnitude and time of the resulting radiological exposures to the reasonably maximally exposed individual, or radionuclide releases to the accessible environment, may be excluded (screened out) from the TSPA on the basis of low consequence (as per 10 CFR 63.114 (e) and (f) [DIRS 156605])

- FEPs that are inconsistent with the characteristics, concepts, and definitions specified in 10 CFR Part 63 [DIRS 156605] may be excluded (screened out) from the TSPA by regulation.

A FEP need only satisfy one of the exclusion screening criteria to be excluded from TSPA. A FEP that does not satisfy any of the exclusion screening criteria must be included (screened in) in the TSPA-LA model.

This report documents the screening decisions for the UZ FEPs. In cases where a FEP covers multiple technical areas and is shared with other FEP reports, this report provides only a partial technical basis for the screening decision as it relates to UZ issues. The full technical basis for these shared FEPs is addressed, collectively, by all of the sharing FEP reports.

For UZ Flow and Transport there are 41 included FEPs and 52 excluded FEPs. Included FEPs are those directly (or, in some cases, implicitly) represented in TSPA-LA models. Included FEPs are identified and the method for inclusion is summarized, with reference to the reports that document how the FEP is represented in TSPA-LA. Section 6.2 discusses FEPs that are included in TSPA-LA.

Excluded FEPs are those excluded due to low probability, low consequence, or by regulation and therefore not modeled in TSPA-LA. In particular, low-probability means that the occurrence of a FEP has a probability lower than 10^{-4} in 10^4 years. Low-consequence arguments in this analysis are based on the UZ subsystem performance. UZ subsystem performance is defined by the release of radionuclides at the water table for SZ radionuclide transport, or water seepage into waste emplacement drifts. A UZ subsystem low-consequence argument for exclusion is always conservative with respect to a total system argument, because the other components of the total

system that contribute to performance are not amplified by changes in UZ performance. The performance of the waste package outer barrier and drip shield over 10,000 years depends on temperature, relative humidity, and water chemistry derived from seepage water chemistry, but is not a strong function of drift seepage quantity (BSC 2004 [DIRS 169984], Figure 6-1; BSC 2004 [DIRS 169845], Figure 1). Seepage water chemistry is determined mainly by water–rock interaction and evaporative concentration in the near-field, and the uncertainty in seepage water chemistry determined by the uncertainty in initial water chemistry, as discussed in *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]), Section 6.6.2). Also, the rate of radionuclide transport in the saturated zone is independent of the source-term strength. Therefore, some FEPs may have a significant effect on radionuclide transport or drift seepage in the UZ and yet have an insignificant effect on total system performance, because of the contributions of the other system components to total system performance. Thus, if a FEP can be shown to have minimal consequence on the UZ subsystem performance, and is not included by any other FEP report, then it will also have a minimal consequence on total system performance in terms of the time or magnitude of the resulting radiological exposures to the reasonably maximally exposed individual, or radionuclide releases to the accessible environment. The rationale for exclusion is given in the screening argument presented for each excluded FEP. Sections 6.3 through 6.9 discuss FEPs that are excluded from TSPA-LA.

The following standardized format is used to present the status of each FEP as presented in the third-order subsections of this chapter. Documentation of the screening for each FEP is provided in Sections 6.2 through 6.9. The following standardized format is used.

Third-Order Subsection Heading: FEP Name (FEP Number)

FEP Description: This field describes the nature and scope of the FEP under consideration.

Screening Decision: Identifies the screening decision as one of:

- "Included"
- "Excluded–Low Probability"
- "Excluded–Low Consequence"
- "Excluded–By Regulation."

A few FEPs are excluded by a combination of two criteria (e.g., Low Probability and Low Consequence).

Screening Argument: This field is used only for excluded FEPs. It provides the discussion for why a FEP has been excluded from TSPA-LA.

TSPA Disposition: This field is used only for included FEPs. It provides the consolidated discussion of how a FEP has been included in TSPA-LA, making reference to more detailed documentation in other supporting technical reports, as applicable.

Supporting Reports: This field is only used for included FEPs. It provides the list of supporting technical reports that identified the FEP as an included FEP and contain information relevant to the implementation of the FEP within the TSPA-LA model. This list of supporting

technical reports provides traceability of the FEP through the document hierarchy. For excluded FEPs, it is indicated as "Not applicable."

6.1.3   Supporting Reports and Inputs

For included FEPs, the model reports develop the models or parameters. These are passed to abstraction reports and then to the TSPA model. In some cases, process model reports pass outputs directly to the TSPA model (e.g., in the flow fields that are output from *UZ Flow Models and Submodels* [BSC 2004 (DIRS 169861)]). Reports that discuss the subject matter of a FEP, but do not develop any input that is eventually used in, or abstracted for use in, the TSPA model are not listed as supporting reports in the disposition of included FEPs. Supporting reports are listed below.

- *Abstraction of Drift Seepage*   (BSC 2004 [DIRS 169131])

- *Analysis of Hydrologic Properties Data*   (BSC 2004 [DIRS 170038])

- *Analysis of Infiltration Uncertainty*   (BSC 2004 [DIRS 165991])

- *Calibrated Properties Model*   (BSC 2004 [DIRS 169857])

- *Conceptual Model and Numerical Approaches for UZ Flow and Transport*   (BSC 2004 [DIRS 170035])

- *Development of Numerical Grids for UZ Flow and Transport Modeling*   (BSC 2004 [DIRS 169855])

- *Drift Scale THM Model*   (BSC 2004 [DIRS 169864])

- *Drift-Scale Coupled Processes (DST and TH Seepage) Models*   (BSC 2004 [DIRS 170338])

- *Drift-Scale THC Seepage Model*   (BSC 2004 [DIRS 169856])

- *Future Climate Analysis*   (BSC 2004 [DIRS 170002])

- *In Situ Field Testing of Processes*   (BSC 2004 [DIRS 170004])

- *Mountain-Scale Coupled Processes (TH/THC/THM)*   (BSC 2004 [DIRS 169866])

- *Particle Tracking Model and Abstraction of Transport Processes*   (BSC 2004 [DIRS 170041])

- *Post-Processing Analysis for THC Seepage*   (BSC 2004 [DIRS 169858])

- *Radionuclide Transport Models Under Ambient Conditions*   (BSC 2004 [DIRS 164500])

- *Saturated Zone Colloid Transport* (BSC 2004 [DIRS 170006])

- *Seepage Calibration Model and Seepage Testing Data* (BSC 2004 [DIRS 171764])

- *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652])

- *Simulation of Net Infiltration for Present-Day and* (BSC 2004 [DIRS 170007])
  Potential Future Climates

- *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861])

Direct inputs to this report are listed in Tables 4-1 and 4-2; indirect inputs are cited within the discussions of individual FEPs.

6.1.4   Qualification of Unqualified Direct Inputs

Direct inputs are listed in Section 4.1, which identifies several inputs that are qualified in this report in accordance with AP-SIII.2Q or AP-SIII.9Q. The qualification reports for those inputs are included in Appendix C.

6.1.5   Assumptions, Simplifications, and Uncertainties

For included FEPs, the TSPA dispositions may include statements regarding assumptions made to implement the FEP within the TSPA-LA model. Such statements are descriptive of the manner in which the FEP has been included and are not used as the basis of the screening decision to include the FEP with the TSPA-LA model.

Because the individual FEPs are specific in nature, any discussion of applicable mathematical formulations, equations, algorithms, numerical methods, idealizations, or simplifications are provided within the individual FEP discussions in Sections 6.2 through 6.9.

For included FEPs, uncertainty is captured in the treatment of the processes as implemented in TSPA-LA. Therefore, uncertainty from the standpoint of the FEPs evaluation is concerned only with uncertainty in the exclusion of FEPs. Because there is no mechanism to capture uncertainty in the FEPs analysis in TSPA-LA, uncertainty leads to conservatism in the FEPs exclusion analyses (i.e., exclusions are based on conservative arguments that are unlikely to change with more detailed or accurate input information). The only restrictions for subsequent use that result from this approach is that worst-case or conservative analyses may overemphasize the importance of FEPs included on that basis.

6.1.6   Intended Use and Limitations

The intended use of this report is to provide FEP screening information for a project-specific FEP database and to promote traceability and transparency regarding FEP screening. This report is the documentation for the FEP database described in *The Development of the Total System Performance Assessment License Application Features, Events, and Processes* (BSC 2004 [DIRS 168706]). For included FEPs, this document summarizes and consolidates the method of

implementation of the FEP in TSPA-LA in the form of TSPA Disposition statements, based on more detailed implementation information in the listed supporting technical reports. For excluded FEPs, this document provides the technical basis for exclusion in the form of screening arguments.

The results of the FEP screening are specific to the repository design evaluated in this report for TSPA-LA, as presented in several reports (BSC 2004 [DIRS 168489]; BSC 2004 [DIRS 168180]; BSC 2004 [DIRS 169058]; and BSC 2004 [DIRS 170058]). Any changes in direct inputs listed in Section 4.1, in baseline conditions used for this evaluation, or in other subsurface conditions, will need to be evaluated to determine whether the changes are within the limits stated in the FEP evaluations.

6.2 INCLUDED FEPS

Table 6-1 gives the section numbers, FEP numbers, and names of Included FEPs.

Table 6-1.   Included UZ FEPs

Section Number	FEP Number	FEP Name
6.2.1	1.1.02.02.0A	Preclosure ventilation
6.2.2	1.2.02.01.0A	Fractures
6.2.3	1.2.02.02.0A	Faults
6.2.4	1.3.01.00.0A	Climate change
6.2.5	1.3.07.02.0B	Water table rise affects UZ
6.2.6	1.4.01.01.0A	Climate modification increases recharge
6.2.7	2.1.08.01.0A	Water influx at the repository
6.2.8	2.1.08.02.0A	Enhanced influx at the repository
6.2.9	2.2.01.01.0A	Mechanical effects of excavation and construction in the near-field
6.2.10	2.2.03.01.0A	Stratigraphy
6.2.11	2.2.03.02.0A	Rock properties of host rock and other units
6.2.12	2.2.07.01.0A	Locally saturated flow at bedrock/alluvium contact
6.2.13	2.2.07.02.0A	Unsaturated groundwater flow in the geosphere
6.2.14	2.2.07.03.0A	Capillary rise in the UZ
6.2.15	2.2.07.04.0A	Focusing of unsaturated flow (fingers, weeps)
6.2.16	2.2.07.06.0B	Long-term release of radionuclides from the repository
6.2.17	2.2.07.07.0A	Perched water develops
6.2.18	2.2.07.08.0A	Fracture flow in the UZ
6.2.19	2.2.07.09.0A	Matrix imbibition in the UZ
6.2.20	2.2.07.10.0A	Condensation zone forms around drifts
6.2.21	2.2.07.11.0A	Resaturation of geosphere dry-out zone
6.2.22	2.2.07.15.0B	Advection and dispersion in the UZ
6.2.23	2.2.07.18.0A	Film flow into the repository
6.2.24	2.2.07.19.0A	Lateral flow from Solitario Canyon fault enters drifts
6.2.25	2.2.07.20.0A	Flow diversion around repository drifts
6.2.26	2.2.08.01.0B	Chemical characteristics of groundwater in the UZ
6.2.27	2.2.08.04.0A	Re-dissolution of precipitates directs more corrosive fluids to waste packages
6.2.28	2.2.08.06.0B	Complexation in the UZ

Table 6-1. Included UZ FEPs (Continued)

Section Number	FEP Number	FEP Name
6.2.29	2.2.08.08.0B	Matrix diffusion in the UZ
6.2.30	2.2.08.09.0B	Sorption in the UZ
6.2.31	2.2.08.10.0B	Colloidal transport in the UZ
6.2.32	2.2.08.12.0A	Chemistry of water flowing into the drift
6.2.33	2.2.09.01.0B	Microbial activity in the UZ
6.2.34	2.2.10.03.0B	Natural geothermal effects on flow in the UZ
6.2.35	2.2.10.10.0A	Two-phase buoyant flow/heat pipes
6.2.36	2.2.10.12.0A	Geosphere dry-out due to waste heat
6.2.37	2.3.01.00.0A	Topography and morphology
6.2.38	2.3.11.01.0A	Precipitation
6.2.39	2.3.11.02.0A	Surface runoff and flooding
6.2.40	2.3.11.03.0A	Infiltration and recharge
6.2.41	3.1.01.01.0A	Radioactive decay and ingrowth

Source: LA FEP list (DTN: MO0407SEPFEPLA.000 [DIRS 170760]).

6.2.1   Preclosure Ventilation (1.1.02.02.0A)

FEP Description: The duration of preclosure ventilation acts together with waste package spacing (as per design) to control the extent of the boiling front (zone of reduced water content).

Screening Decision: Included.

TSPA Disposition: Preclosure ventilation in drifts will remove a considerable amount of the heat output from the waste canisters. The ventilation period following emplacement is 50 years, during which, for an 800-m-long drift, 86% ± 3% of the heat energy supplied to the rock by the waste is removed from the drifts by ventilation (BSC 2004 [DIRS 169862], Table 8-2). This effect of preclosure ventilation on the thermal load provided to the rock is explicitly simulated in *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338], Sections 4.1.1.3 and 6.2.1.3.3), which bases its simulations on 86.3% heat removal by ventilation. Those results are incorporated into the seepage abstraction by using time-dependent boundary conditions for the thermal load (BSC 2004 [DIRS 169131], Section 6.4.3.1). These boundary conditions reflect the current emplacement design (waste package spacing, average heat output of waste canisters, etc.), as provided in design drawing *D&E/PA/C IED Emplacement Drift Configuration and Environment* (BSC 2004 [DIRS 168489]). Thus, the TH-modeling results from the TH seepage model (DTN: LB0301DSCPTHSM.002 [DIRS 163689]) directly account for the impact of preclosure ventilation and waste package spacing on two-phase flow and the TH conditions in the near-drift rock. As discussed in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.5.2), the abstraction of thermal seepage utilizes these modeling results to develop an appropriate thermal seepage abstraction methodology. Preclosure ventilation also causes initial rock drying in the drift vicinity because of evaporation effects. The reduced relative humidity in the emplacement drifts leads to evaporation of water at the drift surfaces and development of a small zone of reduced saturation in the drift vicinity. This early dryout because of evaporation is neglected in the TH seepage model, because seepage into ventilated drifts is highly unlikely (BSC 2004

[DIRS 169131], Section 6.5.2). The effects of preclosure ventilation on dryout of the rock are the same for the THC model as for the TH model.

The effect of preclosure ventilation on the thermal load provided to the rock is also explicitly simulated with the THC seepage model that feeds into the drift-scale coupled processes abstraction model, by using time-dependent boundary conditions for the thermal load (BSC 2004 [DIRS 169856], Sections 4.1.7 and 6.5). These boundary conditions reflect the current emplacement design (waste package spacing, average heat output of waste canisters, etc.), provided in the design drawings (BSC 2004 [DIRS 168489]).

The results from the THC seepage model, and their abstraction (BSC 2004 [DIRS 169858], Section 6.2), account for the impact of preclosure ventilation and waste package spacing on the THC conditions in the near-drift rock. Summary tables of concentrations through time are presented in DTNs: LB0302DSCPTHCS.002 [DIRS 161976]; LB0307DSTTHCR2.002 [DIRS 165541]; LB0311ABSTHCR2.003 [DIRS 166713], and summary statistics through time are presented in LB0311ABSTHCR2.001 [DIRS 166714]. These data are used to feed and/or provide technical basis for *Engineered Barrier System: Physical and Chemical Environment Model* (BSC 2004 [DIRS 169860]), which generates look-up tables used in the TSPA-LA model.

Supporting Reports: *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]); *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]); *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]).

6.2.2 Fractures (1.2.02.01.0A)

FEP Description: Groundwater flow in the Yucca Mountain region and transport of any released radionuclides may take place along fractures. The rate of flow and the extent of transport in fractures are influenced by characteristics such as orientation, aperture, asperity, fracture length, connectivity, and the nature of any linings or infills.

Screening Decision: Included.

TSPA Disposition: This FEP on "Fractures" is included in process models for UZ flow and transport. The UZ flow model is based on a dual-permeability concept, with fractures and matrix each represented by a continuum in the dual permeability mesh (BSC 2004 [DIRS 169855]). The fracture continuum represents the spatially averaged flow through discrete fractures. The fracture continuum interacts with the matrix continuum, which represents matrix blocks separated by fractures.

Fracture continuum properties include permeability, porosity, interface area per unit volume, van Genuchten α and m parameters for the saturation-capillary pressure and relative permeability functions, and an active fracture parameter. These parameters and associated range of values are obtained as described in *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861], Section 6.1.5) and adjusted as described in *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861], Section 6.2.3) for each UZ model layer (DTN: LB0205REVUZPRP.001 [DIRS 159525] and LB0209DSSCFPR.002 [DIRS 162128]).

Fracture permeability is based on field measurements, which integrate the discrete fracture characteristics such as orientation, aperture, asperity, fracture length, connectivity, and the nature of any linings or infills. Permeabilities and other properties are further calibrated as described in *Calibrated Properties Model* (BSC 2004 [DIRS 169857], Section 6.3) and *Analysis of Hydrologic Properties Data* (BSC 2004 [DIRS 170038]). The fracture continuum properties are used as inputs to the UZ flow model, and their effects are incorporated into the output flow fields developed for use in TSPA-LA (output flow fields are in DTN: LB0305TSPA18FF.001 [DIRS 165625]).

The permeability of bedrock (either unfractured PTn or fractured TCw depending on location) is a major contributor to the simulation of net infiltration (BSC 2004 [DIRS 170007], Section 6.1.2). *Simulation of Net Infiltration for Present-Day and Potential Future Climates* (BSC 2004 [DIRS 170007], Section 6.1) discusses conceptual treatment of fractures in the infiltration model and numerical values used (BSC 2004 [DIRS 170007], Appendix B).

The influence of fractures on radionuclide transport through UZ is investigated through the dual permeability model (BSC 2004 [DIRS 170041], Section 6.4.3). The influences of fracture characteristics on UZ flow are included through the pregenerated flow fields (BSC 2004 [DIRS 170041], Section 6.5.1; DTN: LB0305TSPA18FF.001 [DIRS 165625]). Fracture aperture, porosity, and frequency (DTNs: LB0205REVUZPRP.001 [DIRS 159525] and LB0207REVUZPRP.001 [DIRS 159526]) affecting UZ radionuclide transport are summarized in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.5.7). Fracture porosity and frequency data will be statistically sampled during TSPA-LA multirealization runs using the distribution given in DTN: LA0407BR831371.001 [DIRS 170806].

Flow processes in fractures or other channels are important for seepage because the amount of seepage is determined by the diversion capacity of the fracture flow in the drift vicinity. This process is modeled in *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652], Section 6.3). Seepage-relevant parameters are determined in *Seepage Calibration Model and Seepage Testing Data* (BSC 2004 [DIRS 171764] Sections 6.3 and 6.5), based upon data acquired in *In Situ Field Testing of Processes* (BSC 2004 [DIRS 170004], Sections 6.1 and 6.2). Data relevant to modeling of fracture-matrix interaction are acquired in *In Situ Field Testing of Processes* (BSC 2004 [DIRS 170004], Section 6.6). The seepage simulation results in *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652] are abstracted for use in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.3.1). These flow processes are influenced by fracture characteristics such as orientation, aperture, asperity, length, connectivity, and fillings. All seepage process models that feed into seepage abstraction explicitly simulate the flow processes in fractures, using appropriate continuum properties that represent these characteristics (BSC 2004 [DIRS 169131], Section 6.4).

For ambient seepage, the relevant continuum properties are the continuum permeability and the effective fracture capillary-strength in the drift vicinity. For seepage abstraction, probability distributions describing the spatial variability and uncertainty of these parameters have been developed in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.6), based on air-permeability measurements and liquid-release tests combined with inverse modeling (BSC 2004 [DIRS 169131], Sections 6.6 and 6.4). Ambient seepage calculations will be

conducted within the TSPA-LA by sampling from these probability distributions and interpolating seepage rates from the look-up tables given in DTNs: LB0304SMDCREV2.002 [DIRS 163687] and LB0307SEEPDRCL.002 [DIRS 164337]. During the thermal period, the ambient seepage rates will be adjusted based on the TH-modeling results from *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]), which explicitly simulates the thermally perturbed fracture flow conditions. Results are given in DTN: LB0301DSCPTHSM.002 [DIRS 163689]. THM and THC effects on fracture characteristics are evaluated with process models that explicitly account for fracture flow affected by THM and THC parameter alterations (BSC 2004 [DIRS 169131], Section 6.4.4; see FEPs 2.1.09.12.0A and 2.2.10.04.0A). It was demonstrated that these potential alterations can be neglected in the TSPA-LA, because the expected changes would lead to less seepage (BSC 2004 [DIRS 169131], Section 6.5.1.4), and therefore would result in predictions that underestimate repository performance.

Flow processes in fractures or other channels affect modeled THC coupled processes because of (1) their strong effect on TH behavior (BSC 2004 [DIRS 169131], Sections 6.4.4.1 and 6.4.4.2), and (2) their strong effect on water and gas chemistry (BSC 2004 [DIRS 169856], Section 6.2.1). The latter is primarily due to volatilization of steam and CO_2 from the rock matrix-water and subsequent transport and condensation in fractures. The amount of mobilized CO_2 with steam directly affects the pH of the condensate, which in turn affects the degree of water–rock interaction and water chemistry. These THC processes are influenced by the fracture characteristics, such as orientation, aperture, asperity, length, connectivity, and fillings. The THC seepage model that feeds into the drift scale coupled processes abstraction model explicitly simulates the flow processes in fractures using appropriate continuum properties that represent these characteristics (BSC 2004 [DIRS 169856], Sections 6.4.3, 6.4.4, and 6.4.7).

Thus, the results from the THC seepage model and their abstraction (BSC 2004 [DIRS 169858], Section 6.2), and tables of concentrations and summary statistics through time, implicitly account for the effect of climate change on THC processes. Summary tables of concentrations through time are presented in DTNs: LB0302DSCPTHCS.002 [DIRS 161976]; LB0307DSTTHCR2.002 [DIRS 165541]; and LB0311ABSTHCR2.003 [DIRS 166713]; and summary statistics through time are presented in LB0311ABSTHCR2.001 [DIRS 166714]. These data are used to feed and/or provide technical basis for *Engineered Barrier System: Physical and Chemical Environment Model* (BSC 2004 [DIRS 169860]), which generates look-up tables used in the TSPA-LA model.

The effects of fractures are also included in the treatment of infiltration uncertainty for TSPA-LA (BSC 2003 [DIRS 165991]. Infiltration uncertainty is represented through three discrete infiltration scenarios (lower, mean, and upper), which are sampled in TSPA-LA according to weighting factors (BSC 2003 [DIRS 165991], Section 7.1). Fractures are included in the infiltration uncertainty analysis by incorporation of the fracture parameters for bedrock permeability (BRPERM) and bedrock porosity (BRPOROS) that are included implicitly in the determination of the weighting factors. *Analysis of Infiltration Uncertainty* (BSC 2003 [DIRS 165991], Table 6-1) defines these fracture parameters and their uncertainties (BSC (2003 [DIRS 165991], Tables 6-2 and 6-3). These uncertainties are propagated through the infiltration numerical model and so are implicitly included in the output (weighting factors)

that is passed to TSPA-LA (BSC 2003 [DIRS 165991]; DTN: SN0308T0503100.008 [DIRS 165640]).

Supporting Reports: *Simulation of Net Infiltration for Present-Day and Potential Future Climates* (BSC 2004 [DIRS 170007]); *Development of Numerical Grids for UZ Flow and Transport Modelin*g (BSC 2004 [DIRS 169855]); *In Situ Field Testing of Processes* (BSC 2004 [DIRS 170004]); *Calibrated Properties Model* (BSC 2004 [DIRS 169857]); *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]); *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]); *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652]); *Seepage Calibration Model and Seepage Testing Data* (BSC 2004 [DIRS 171764]); *Analysis of Hydrologic Properties Data* (BSC 2004 [DIRS 170038]), *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]), *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]), *Analysis of Infiltration Uncertainty* (BSC 2003 [DIRS 165991].

6.2.3   Faults (1.2.02.02.0A)

FEP Description: Numerous faults of various sizes have been noted in the Yucca Mountain region and specifically in the repository area. Faults may represent an alteration of the rock permeability and continuity of the rock mass, an alteration or short-circuiting of the flow paths and flow distributions close to the repository, and/or unexpected pathways through the repository.

Screening Decision: Included

TSPA Disposition: The stratigraphic units/layers and fault geometries are defined in *Geological Framework Model (GFM2000)* (BSC 2004 [DIRS 170029]) and DTN: MO0012MWDGFM02.002 [DIRS 153777]). This provides the basis the UZ model grid in *Development of Numerical Grids for UZ Flow and Transport Modeling* (BSC 2004 [DIRS 169855]). Major displacement, dip-slip, strike-slip, and detachment faults within the model domain are explicitly discretized in the mountain-scale UZ flow and transport models described in *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861], Sections 6.1.5, 6.2.2, 6.6.3, 6.7.3) and *Development of Numerical Grids for UZ Flow and Transport Modeling* (BSC 2004 [DIRS 169855], Sections 6.4 and 6.6.1). These faults are represented in the UZ model grid developed in *Development of Numerical Grids for UZ Flow and Transport Modeling* (BSC 2004 [DIRS 169855] as vertical or inclined discrete zones 30 m wide, and include existing displacements that affect the relative geometry of the hydrogeologic model units. Specific hydrogeologic properties are assigned to the fault zones. Fault properties (matrix and fracture parameters) are in DTN: LB02092DSSCFPR.002 [DIRS 162128] and in *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861], Table 4.1-1). These properties have been calibrated as described in *Calibrated Properties Model* (BSC 2004 [DIRS 169857], Section 6.3.4) and *Analysis of Hydrologic Properties Data* (BSC 2004 [DIRS 170038]). The fault properties are used as inputs to the UZ flow model, and their effects are incorporated into the output flow fields developed for use in TSPA-LA (output flow fields are in DTN: LB0305TSPA18FF.001 [DIRS 165625]).

The influence of faults on radionuclide transport is implicitly included through the use of a dual permeability model, the use of pregenerated flow fields that include the faults in the three-dimensional model in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.5.1; DTN: LB0305TSPA18FF.001 [DIRS 165625]), and the characteristics of fractures within the faults (BSC 2004 [DIRS 170041], Section 6.5.7). In TSPA-LA runs, the influence of faults is included through the use of fault properties and the pregenerated flow fields under different climate conditions as described in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Sections 6.5.1 and 6.5.7); however, *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]) provides a model for use in TSPA-LA, but does not generate a direct data feed to TSPA-LA pertaining to this FEP.

Supporting Reports: *Development of Numerical Grids for UZ Flow and Transport Modeling* (BSC 2004 [DIRS 169855]); *Analysis of Hydrologic Properties Data* (BSC 2004 [DIRS 170038]); *Calibrated Properties Model* (BSC 2004 [DIRS 169857]); *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]); *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]).

6.2.4   Climate Change (1.3.01.00.0A)

FEP Description: Climate change may affect the long-term performance of the repository. This includes the effects of long-term change in global climate (e.g., glacial/interglacial cycles) and shorter-term change in regional and local climate. Climate is typically characterized by temporal variations in precipitation and temperature.

Screening Decision: Included.

TSPA Disposition: Global climate change is addressed in TSPA-LA, using a climate analysis based on paleoclimate information. That is, the record of climate changes in the past is used to predict the expected changes in climate for the future. Future climates are described in terms of discrete climate states that are used to approximate continuous variations in climate. The effects of seasonality are included in the climate analysis through the use of climate analogues with specific seasonal meteorological records. Climate analyses are incorporated into TSPA-LA through the UZ flow fields that have different surface water infiltration as a result of different climates corresponding to three distinct different climates (climate change timing in parentheses): present day (from 0 to 600 years after present), monsoon (from 600 to 2,000 years after present), and glacial transition (from 2,000 years after present to the end of the period simulated) (BSC 2004 [DIRS 169565], Section 5.1.4). The nine infiltration rates are summarized in Table 6-2 for average values over the model domain.

Table 6-2.   Infiltration Rates (mm/year) Averaged over the UZ Model Domain

Scenario	Lower-Bound Infiltration	Mean Infiltration	Upper-Bound Infiltration
Present-Day/Modern	1.25	4.43	10.74
Monsoon	4.43	11.83	19.23
Glacial Transition	2.35	17.02	31.69

NOTE: Values averaged from DTN: GS000308311221.005 [DIRS 147613].

Future climate conditions are addressed in the infiltration model (BSC 2004 [DIRS 170007], Section 6.9) through the selection of analogues at other locations with present day climates that are representative of the range of future climate conditions at Yucca Mountain (BSC 2004 [DIRS 170002], Section 6.6). The meteorological data from these analogues are then used for modeling infiltration under future climate conditions at Yucca Mountain. A description of the modeling methods used for infiltration, and of how infiltration is affected by climate, is given in *Simulation of Net Infiltration for Present-Day and Potential Future Climates* (BSC 2004 [DIRS 170007], Section 6.9). The results of the infiltration model are then used for computing UZ flow throughout the UZ flow-model domain, which includes the repository waste emplacement zone. The UZ flow model uses the infiltration results as top boundary conditions for UZ flow calculations (BSC 2004 [DIRS 169861], Section 6.1.4). The UZ flow fields are used directly in TSPA-LA (BSC 2004 [DIRS 169861], Section 6.2.5). The output flow fields are in DTN: LB0305TSPA18FF.001 [DIRS 165625], developed for use in Performance Assessment (BSC 2003 [DIRS 166296]); the conversion of flow fields to the format needed for use in TSPA is documented in *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861], Appendix D).

Climate change is implicitly included in the treatment of radionuclide transport for TSPA-LA as discussed in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.4.8). The effect of climate change on repository performance was studied by using pregenerated flow fields under different climates (DTN: LB0305TSPA18FF.001 [DIRS 165625]). For TSPA-LA, the pregenerated flow fields are used by the FEHM model as described in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.4.9). *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]) transmits software and parameters, which incorporate climate change through the flow fields for use in TSPA-LA, but does not generate a direct data feed to TSPA-LA pertaining to this FEP.

Potential effects of climate change on the amount of infiltration and percolation at Yucca Mountain are taken implicitly into account in the THC seepage model by considering different climate stages and climate scenarios when setting infiltration rates at the top model boundary (BSC 2004 [DIRS 169856], Sections 6.2.1.3 and 6.5.2). Thus, the results from the THC seepage model and their abstraction (BSC 2004 [DIRS 169858], Section 6.2), and tables of concentrations and summary statistics through time, implicitly account for the effect of climate change on THC processes. Summary tables of concentrations through time are presented in DTNs: LB0302DSCPTHCS.002 [DIRS 161976], LB0307DSTTHCR2.002 [DIRS 165541] and LB0311ABSTHCR2.003 [DIRS 166713], and summary statistics through time are presented in LB0311ABSTHCR2.001 [DIRS 166714). These data are used to feed and/or provide technical basis for *Engineered Barrier System: Physical and Chemical Environment Model* (BSC 2004 [DIRS 169860]), which generates look-up tables used in the TSPA-LA model. Note that seepage is calculated in the TSPA-LA using percolation flux distributions based on results from the UZ flow and transport model (BSC 2004 [DIRS 169131], Section 6.6.5.1), given in DTNs: LB0302PTNTSW9I.001 [DIRS 162277] and LB0305PTNTSW9I.001 [DIRS 163690]. These flux distributions are based on the same varying climate stages and scenarios identified and used in the THC seepage model.

Potential effects of climate change on the amount of infiltration and percolation at Yucca Mountain are taken into account in the seepage abstraction by considering different climate

stages and climate scenarios in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.6.5; and in *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338], Section 6.2). Seepage is calculated in the TSPA-LA using percolation flux distributions based on results from the UZ flow and transport model (BSC 2004 [DIRS 169131], Section 6.6.5.1), given in DTNs: LB0302PTNTSW9I.001 [DIRS 162277] and LB0305PTNTSW9I.001 [DIRS 163690]. These flux distributions include different climate stages and scenarios.

The effects of climate change are also included in the treatment of infiltration uncertainty for TSPA-LA (BSC 2003 [DIRS 165991]). Infiltration uncertainty is represented through three discrete infiltration scenarios (lower, mean, and upper), which are sampled in TSPA-LA according to weighting factors (BSC 2003 [DIRS 165991], Section 7.1). Climate change is incorporated through the use of the analogue climate (lower-bound, mean, and upper-bound) infiltration rate maps (BSC 2003 [DIRS 165991], Table 6-7; DTN: GS000308311221.005 [DIRS 147613]) developed in *Simulation of Net Infiltration for Present-Day and Potential Future Climates* (BSC 2004 [DIRS 170007]) by using the climate analogue data as direct input. It is incorporated implicitly by inclusion of the spatial average analogue net infiltration rate maps in the calculation of the weighting factors passed to TSPA-LA (BSC 2003 [DIRS 165991]; DTN: SN0308T0503100.008 [DIRS 165640]).

The effects of climate change are also included in the treatment of seepage in *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652], Section 6.3.6) and *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]) through the use of percolation fluxes taken from flow fields calculated for present and future climate states; and in *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]) through the use of varying flux boundary conditions applied at the top of the model.

Supporting Reports: *Future Climate Analysis* (BSC 2004 [DIRS 170002]); *Simulation of Net Infiltration for Present-Day and Potential Future Climates* (BSC 2004 [DIRS 170007]); *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]); *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]); *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]); *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]); *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652]); *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]); *Analysis of Infiltration Uncertainty,* (BSC 2003 [DIRS 165991]).

6.2.5   Water Table Rise Affects UZ (1.3.07.02.0B)

FEP Description: Climate change could produce increased infiltration, leading to a rise in the regional water table, possibly affecting radionuclide release from the repository by altering flow and transport pathways in the UZ. A regionally higher water table and change in UZ flow patterns might flood the repository.

Screening Decision: Included.

TSPA Disposition: The water table will be higher in future climates with greater infiltration (see Table 6-2). To include this water table rise in TSPA-LA calculations, the water table elevation is

instantaneously increased by 120 m when the climate changes from present-day to monsoon climate. The same water table elevation is also used for glacial-transition climate. This is conservative and is consistent with the instantaneous change of UZ flow fields (see FEP 1.3.01.00.0A).

Water table changes are implemented in the TSPA-LA by allowing the water table to change elevation instantaneously upon change in climate, concurrent with changes in infiltration (implemented by the postprocessor software WTRISE (V2.0, STN: 105372.000) (LBNL 2003 [DIRS 163453]) for radionuclide transport), thus affecting the unsaturated flow and pathways in the UZ. WTRISE allows the user to specify a water table location and removes all the particles in the gridblocks below the specified water table instantaneously by setting full saturation to the submerged gridblocks (BSC 2004 [DIRS 169861], Section 6.6.3). The particles removed from the UZ gridblocks enter the SZ transport model. WTRISE is implemented in the TSPA-LA model.

Paleoclimate data indicates that the historical water table has never risen to the level of the repository (Forester et al. 1999 [DIRS 109425], pp. 46 and 56). Based on analysis of mineralogic alteration (zeolitization and tridymite distribution) and strontium isotope ratios, and groundwater flow modeling, the water table for future climates (both monsoon and glacial transition) is specified in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.4.8). Future climate flow fields have been generated using WTRISE for three monsoon and three glacial-transition climate flow fields, which are given in DTN: LB0312TSPA06FF.001 [DIRS 166671].

The effect of water table rise on the thermal regime is not included in the TSPA because the exact boundary condition values for temperature, gas pressure, and saturation are not important for TH seepage model results. The temperature and gas pressure values that define the initial temperature and pressure fields, respectively, are soon significantly altered in the near-field rock once the drifts are heated up. The thermal perturbation of the temperature and pressure fields is so strong in the near field that the initial distribution of these parameters has little effect (BSC 2004 [DIRS 170338], Section 4.1.1.2).

Supporting Reports: *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]); *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]).

6.2.6   Climate Modification Increases Recharge (1.4.01.01.0A)

FEP Description: Climate modification causes an increase in recharge in the Yucca Mountain region. Increased recharge might lead to increased flux through the repository, perched water, or water table rise.

Screening Decision: Included.

TSPA Disposition: The effects of climate changes (BSC 2003 [DIRS 166296], Section 5.2) on UZ flux through the repository are incorporated through the explicit simulations of UZ flow fields corresponding to the upper-bound, mean, and lower-bound infiltrations of three distinct different climates: present-day, monsoon, and glacial transition. The flow boundary conditions at the top of the UZ flow model are set by nine infiltration maps developed in *Simulation of Net*

Infiltration for Present-Day and Potential Future Climates (BSC 2004 [DIRS 170007], Section 6.11). The nine base-case flow fields and nine alternative flow fields are presented in *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861], Section 6.6). The output flow fields are in DTN: LB0305TSPA18FF.001 [DIRS 165625], developed for use in performance assessment (BSC 2003 [DIRS 166296]); the conversion of flow fields to the format needed for use in TSPA is documented in *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861], Appendix D).

Above the repository, perched water bodies were neither observed in the field nor predicted by the UZ flow model. The potential effect of perched water above the repository is indirectly related to lateral diversion of percolation flux in the PTn above the repository. PTn effects on the flow field are discussed in *UZ Flow Models and Submodels* (BSC 2004 [DIRS169861], Section 6.6). The potential for water table rise caused by climate change is included in TSPA-LA calculations by adjusting the flow fields to the higher water tables (implemented by software WTRISE (LBNL 2003 [DIRS 163453]).

The effect of climate changes in the form of increased recharge is implicitly included in the transport model for TSPA-LA through the use of pregenerated flow fields (BSC 2004 [DIRS 170041], Section 6.5.1 and DTN: LB0305TSPA18FF.001 [DIRS 165625]). In multirealization TSPA-LA runs, different climate patterns are applied and the effect of climate change is included through FEHM's use of pregenerated flow fields for the corresponding climates as described in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.5.1). *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]) provides a model for use in TSPA-LA, but does not generate a direct data feed to TSPA-LA pertaining to this FEP.

Potential effects of climate change on the amount of infiltration and percolation at Yucca Mountain are taken into account in the THC seepage model by implicitly considering different climate stages and climate scenarios when setting infiltration rates at the top model boundary (BSC 2004 [DIRS 169856], Sections 6.2.1.3 and 6.5.2).

Thus, the results from the THC seepage model, and their abstraction in *Post-Processing Analysis for THC Seepage* (BSC 2004 [DIRS 169858], Section 6.2), implicitly account for the effect of climate change on predicted water and gas chemistry. Summary tables of concentrations through time are presented in DTNs: LB0302DSCPTHCS.002 [DIRS 161976], LB0307DSTTHCR2.002 [DIRS 165541], and LB0311ABSTHCR2.003 [DIRS 166713], and summary statistics through time are presented in LB0311ABSTHCR2.001 [DIRS 166714]. These data are used to feed and/or provide technical basis for *Engineered Barrier System: Physical and Chemical Environment Model* (BSC 2004 [DIRS 169860]), which generates lookup tables used in the TSPA-LA model. Potential effects of climate change on the amount of flux through the repository are taken into account in the seepage modeling and abstraction by considering different climate stages and climate scenarios (BSC 2004 [DIRS 169131], Section 6.6.5). The method for calculating seepage in the TSPA-LA (BSC 2004 [DIRS 167652], Section 6.3.6); BSC 2004 [DIRS 170338]; BSC 2004 [DIRS 169131], Section 6.6.5.1) uses percolation flux distributions based on results from *UZ Flow Model and Submodels* (BSC 2004 [DIRS 169861]), given in DTNs: LB0302PTNTSW9I.001 [DIRS 162277] and LB0305PTNTSW9I.001

[DIRS 163690]. These flux distributions are based on the same varying climate stages and scenarios as identified and used in the THC seepage model.

Supporting Reports: *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]); *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652]); *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]); *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]); *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]); *Simulation of Net Infiltration for Present-Day and Potential Future Climates* (BSC 2004 [DIRS 170007]); *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]).

6.2.7 Water Influx at the Repository (2.1.08.01.0A)

FEP Description: An increase in the unsaturated water flux at the repository may affect thermal, hydrologic, chemical, and mechanical behavior of the system. Increases in flux could result from climate change, but the cause of the increase is not an essential part of the FEP.

Screening Decision: Included.

TSPA Disposition: This FEP is considered to be included implicitly in the TSPA-LA. Changes in UZ flow in response to climate changes are incorporated in the infiltration maps developed in *Simulation of Net Infiltration for Present-Day and Future Climates* (BSC 2004 [DIRS 170007], Section 6.11) and in output flow fields developed for use in the TSPA-LA by *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861], Section 6.6.3); the output flow fields are in DTN: LB0305TSPA18FF.001 [DIRS 165625]). Furthermore, the outputs from *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]) are also used by other models and evaluations that are intermediate between the UZ flow model and the TSPA-LA model. For example, the flow fields are used to calculate seepage flux in *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652], Section 6.3.6) and *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]).

In TSPA-LA multirealization runs, climate changes and the change of water influx at the repository on radionuclide transport are addressed through the use of corresponding pregenerated flow fields. Release of tracked particles (the transport modeling method used for TSPA-LA) is related to the percolation flux at the repository as described in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.5.15).

The thermal model output from *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]) is used for setting initial conditions for the downstream mountain-scale coupled process evaluation. The effects of changes in UZ flow caused by climate change are also included in the calculations for the thermal-hydrologic (TH) behavior of the repository system in *Mountain-Scale Coupled Processes (TH/THC/THM)* (BSC 2004 [DIRS 169866], Section 6); however, the results are not implemented in TSPA because they are used only to support arguments for the exclusion of certain FEPs. The effects of transient flow driven by thermal-hydrologic processes are also included in TSPA-LA calculations for drift seepage in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]). The effects of THC and THM on seepage are also addressed in the seepage abstraction report.

The potential increase in the magnitude of percolation flux at the repository, as a result of climate changes or flow focusing effects, is accounted for in the seepage abstraction by considering different climate stages, climate scenarios, and introducing flow-focusing factors (BSC 2004 [DIRS 169131], Section 6.6.5). Seepage is calculated in the TSPA-LA using percolation flux distributions based on results from the UZ flow and transport model (BSC 2004 [DIRS 169131], Section 6.6.5.1), given in DTNs: LB0302PTNTSW9I.001 [DIRS 162277] and LB0305PTNTSW9I.001 [DIRS 163690]. These flux distributions include different climate stages and scenarios. The potential focusing of flow towards individual drift sections is accounted for by a distribution of flow-focusing factors, as discussed in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.6.5.2). This distribution is given in DTN: LB0406U0075FCS.002 [DIRS 170712]. The local percolation flux distribution used for the seepage calculations in the TSPA-LA is derived by multiplying the percolation flux values from the site-scale model with the randomly sampled flow-focusing factors (BSC 2004 [DIRS 169131], Section 6.7.1).

The potential increase in the magnitude of percolation flux at the repository, as a result of climate changes, is accounted for in the THC seepage model by implicitly considering different climate stages, and climate scenarios when setting infiltration rates at the top model boundary (BSC 2004 [DIRS 169856], Sections 6.2.1.3 and 6.5.2). Also, flux increases caused by reflux of water upon boiling are explicitly accounted for by the modeling of coupled THC processes (BSC 2004 [DIRS 169856], Sections 6.2.1 and 6.5.5.2). Therefore, these effects are directly accounted for in results from the THC seepage model and their abstraction (BSC 2004 [DIRS 169858], Section 6.2). Summary tables of concentrations through time are presented in DTNs: LB0302DSCPTHCS.002 [DIRS 161976], LB0307DSTTHCR2.002 [DIRS 165541], and LB0311ABSTHCR2.003 [DIRS 166713], and summary statistics through time are presented in LB0311ABSTHCR2.001 [DIRS 166714]. DTNs: LB0302DSCPTHCS.002 [DIRS 161976] and LB0311ABSTHCR2.001 [DIRS 166714] are used to feed and/or provide technical basis for *Engineered Barrier System: Physical and Chemical Environment Model* (BSC 2004 [DIRS 169860]), which generates lookup tables used in the TSPA-LA model. Note that seepage is calculated in the TSPA-LA using percolation flux distributions that are based on results from the UZ flow and transport model (BSC 2004 [DIRS 169131], Section 6.6.5.1), given in DTNs: LB0302PTNTSW9I.001 [DIRS 162277] and LB0305PTNTSW9I.001 [DIRS 163690]. These flux distributions include the same climate stages and scenarios as used in the THC seepage model.

Waste heat causes water to boil and move as vapor to a cooler region where it condenses. This condensation is then available to increase the percolation flux. The effect of this increased percolation flux at the repository as a result of this refluxing flow was examined in *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338], Section 6.2.2.2. Despite the refluxing of condensate, no seepage into intact drifts was found to occur as long as the temperature at the drift wall remains above 100°C. The thermal seepage abstraction for TSPA-LA consists of setting the thermal seepage for intact drifts equal to zero for the period of above-boiling temperatures at the drift wall. (For collapsed drifts and intact drifts with wall temperatures below 100°C, seepage is set equal to the estimated ambient seepage.)

Supporting Reports: *Simulation of Net Infiltration for Present-Day and Future Climates* (BSC 2004 [DIRS 170007]); *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]);

Seepage Model for PA Including Drift Collapse (BSC 2004 [DIRS 167652]); *Drift-Scale THC Seepage Model,* BSC 2004 [DIRS 169856]); *Abstraction of Drift Seepage,* BSC 2004 [DIRS 169131]); *Particle Tracking Model and Abstraction of Transport Process* (BSC 2004 [DIRS 170041]); *Drift-Scale Coupled Processes (DST and TH Seepage) Models,* (BSC 2004 [DIRS 170338]).

6.2.8   Enhanced Influx at the Repository (2.1.08.02.0A)

FEP Description: An opening in unsaturated rock may alter the hydraulic potential, affecting local saturation around the opening and redirecting flow. Some of the flow may be directed to the opening where it is available to seep into the opening.

Screening Decision: Included.

TSPA Disposition: The impact of an underground opening on the unsaturated flow field (including capillary barrier effect and flow diversion around the drifts) and its relevance for seepage is explicitly captured in the seepage process models used for the seepage abstraction *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652], Section 6.3), *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Sections 6.4.1, 6.4.2, and 6.4.3); and *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338] Sections 6.1.1 and 6.2.1.4). Parameters used in the process models are developed from inverse modeling in *Seepage Calibration Model and Seepage Testing Data,* BSC 2004 [DIRS 171764], Sections 6.3, 6.6, and 6.8). From these model simulations, seepage predictions are available in the form of look-up tables in DTNs: LB0304SMDCREV2.002 [DIRS 163687] and LB0307SEEPDRCL.002 [DIRS 164337]. These will be used in the TSPA-LA to calculate ambient seepage, by sampling parameter cases of seepage-relevant parameters from the probability distributions that are defined in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.7.1). These seepage-relevant parameters are the effective capillary-strength parameter, the permeability, and the local percolation flux. The percolation flux distributions include flow-focusing effects, as discussed in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.6.5.2). During the thermal period, the ambient seepage rates will be adjusted based on the TH-modeling results from DTN: LB0301DSCPTHSM.002 [DIRS 163689], using the abstraction methodology developed in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Sections 6.5.2 and 6.5.3).

Supporting Reports: *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652]); *Seepage Calibration Model and Seepage Testing Data* (BSC 2004 [DIRS 171764]); *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]); *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]).

6.2.9   Mechanical Effects of Excavation and Construction in the Near-Field (2.2.01.01.0A)

FEP Description: Excavation will produce some disturbance of the rocks surrounding the drifts due to stress relief. Stresses associated directly with excavation (e.g., boring and blasting operations) may also cause some changes in rock properties. Properties that may be affected include rock strength, fracture spacing and block size, and hydrologic properties such as permeability.

Screening Decision: Included.

TSPA Disposition: Excavation effects, including mechanical effects of excavation on excavation-disturbed zone (EDZ) fractures, near-field fractures, and seepage, are taken into account in the fracture permeability measurements reported in *In Situ Field Testing of Processes* (BSC 2004 [DIRS 170004], Section 6.1). Seepage-relevant parameters are derived from those measurements in *Seepage Calibration Model and Seepage Testing Data* (BSC 2004 [DIRS 171764], Sections 6.3, 6.5.2, and 6.6) and used in *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652], Sections 6.3.2 and 6.4). These results are included in the seepage abstraction through the use of postexcavation air-permeability data (BSC 2004 [DIRS 169131], Section 6.6.3 and Table 6.6-3) and the estimation of a capillary-strength parameter determined from seepage tests (BSC 2004 [DIRS 169131], Section 6.6.2 and Table 6.6-1). These data reflect the impact of excavation around a large opening (niche or drift). The THM modeling results are supported by the measured postexcavation air-permeability data (BSC 2004 [DIRS 169131], Section 6.6.3.1). The probability distributions for permeability and capillary strength given in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.7.1) are based on the values given in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Tables 6.6-3 and 6.6-1), respectively, and thus account for such excavation effects. These distributions will be used in the TSPA-LA to calculate seepage from the seepage look-up tables, using the methodology defined in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.7.1). Simulation results presented in *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338], Sections 6.2.2 and 6.2.3) also incorporate the effects of excavation. The seepage abstraction model also captures the effects of drift collapse (BSC 2004 [DIRS 169131], Sections 6.4.2.4 and 6.7.1.2) in terms of the larger drift profile that results.

Supporting Reports: *In Situ Field Testing of Processes* (BSC 2004 [DIRS 170004]); *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652]); *Seepage Calibration Model and Seepage Testing Data* (BSC 2004 [DIRS 171764]); *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]); *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]).

6.2.10 Stratigraphy (2.2.03.01.0A)

FEP Description: Stratigraphic information is necessary information for the performance assessment. This information should include identification of the relevant rock units, soils and alluvium, and their thickness, lateral extents, and relationships to each other. Major discontinuities should be identified.

Screening Decision: Included.

TSPA Disposition: This FEP is included in the UZ flow model (BSC 2004 [DIRS 169861], Sections 6.1.1 and 6.1.2) by use of the grids developed with the information contained in *Geologic Framework Model (GFM2000)* (BSC 2004 [DIRS 170029]) and DTN: MO0012MWDGFM02.002 [DIRS 153777]. The stratigraphic unit and layers are developed into a model grid in *Development of Numerical Grids for UZ Flow and Transport Modeling* (BSC 2004 [DIRS 169855]). Because the assignment of hydrologic properties is

associated with the grid used for the UZ flow model, the stratigraphy information is implicitly embedded in the TSPA-LA through the output flow fields. Aspects that affect hydrogeologic properties for flow are further discussed in *Development of Numerical Grids for UZ Flow and Transport Modeling* (BSC 2004 [DIRS 169855], Section 6) and *Calibrated Properties Model* (BSC 2004 [DIRS 169857], Section 6.1.4). See also FEP 2.2.03.02.0A.

This FEP is also implicitly included for radionuclide transport in the UZ through the use of pregenerated flow fields (DTN: LB0305TSPA18FF.001 [DIRS 165625]) as used by FEHM in TSPA-LA UZ multirealization runs as described in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.5.1). However, *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]) provides a model for use in TSPA-LA, but does not generate a direct data feed to TSPA-LA pertaining to this FEP.

Ambient seepage as a result of incomplete flow diversion around drifts is a local process simulated by drift-scale seepage process models (BSC 2004 [DIRS 169131], Section 6.4). In these models, the stratigraphy below and above the repository unit can be neglected. In contrast, the UZ flow and transport model (which provides the percolation flux distributions used for seepage calculations) explicitly accounts for the various geological units and major faults in the UZ (BSC 2004 [DIRS 169861], Sections 6.1.1 and 6.1.2). This is because the overall distribution of percolation flux at the repository horizon is influenced by stratigraphic layering and by major discontinuities. For example, the PTn unit overlying the Topopah Spring welded tuff units can divert a fraction of percolating water to intercepting faults and fault zones, thereby changing the spatial distribution of fluxes (BSC 2004 [DIRS 169861], Section 6.6.3), which could affect water–rock interaction and seepage water chemistry. The drift-scale process models addressing TH, THM, and THC processes (BSC 2004 [DIRS 169131], Sections 6.4.3.1, 6.4.4.1, and 6.4.4.2) also represent the stratigraphy in the UZ at Yucca Mountain in an explicit manner. This is needed because the thermal perturbation of the unsaturated rock extends far into the overlying and underlying geological units. Thus, the stratigraphy information is inherently embedded in the respective model results from the UZ flow and transport model and the TH, THM, and THC drift-scale models. Also, the mineralogy of stratigraphic intervals affects seepage water chemistry. For example, the presence of fluorite in the Tptpll hydrogeologic unit may affect fluoride concentrations in porewaters in this unit (BSC 2004 [DIRS 169856], Section 6.5.5.2). Finally, the thermal perturbation of the unsaturated rock extends far into the geologic units overlying and underlying the emplacement drifts. For these reasons, the THC seepage model includes explicitly the Yucca Mountain stratigraphy (BSC 2004 [DIRS 169856], Sections 4.1.2 and 6.5.1), using stratigraphic information from DTN: LB990501233129.004 [DIRS 111475] and mineralogical information from DTNs: LA9908JC831321.001 [DIRS 113495], LA9912SL831151.001 [DIRS 146447], LA9912SL831151.002 [DIRS 146449], and LA0009SL831151.001 [DIRS 153485]. Therefore, the results from the THC seepage model, and their abstraction in *Post-Processing Analysis for THC Seepage* (BSC 2004 [DIRS 169858], Section 6.2), explicitly account for the effect of stratigraphy on predicted water and gas chemistry. Summary tables of concentrations through time are presented in DTNs: LB0302DSCPTHCS.002 [DIRS 161976], LB0307DSTTHCR2.002 [DIRS 165541], and LB0311ABSTHCR2.003 [DIRS 166713], and summary statistics through time are presented in LB0311ABSTHCR2.001 [DIRS 166714]. These data are used to feed and/or provide technical basis for *Engineered Barrier System: Physical and Chemical Environment Model* (BSC 2004 [DIRS 169860]), which generates look-up tables used in the TSPA-LA model.

The bases for the UZ and SZ stratigraphic models are different. The UZ uses the geologic framework model, GFM2000 (BSC 2004 [DIRS 170029]); DTN: MO0012MWDGFM02.002 [DIRS 153777]) and the SZ uses the hydrogeologic framework model, HFM (BSC 2004 [DIRS 170008]; DTN: GS000508312332.002 [DIRS 150136]). These different models for stratigraphy are used as a result of the different domains treated by the UZ and SZ models. The UZ model encompasses rock above the water table over a region around the repository that is roughly 5 km × 9 km (BSC 2004 [DIRS 169861], Figure 6.1-1). The SZ model encompasses rock below the water table over an area that is roughly 30 km × 45 km (BSC 2004 [DIRS 170037], Figure 6-1).

Stratigraphy is implicitly incorporated in the output from reports that develop different data sets for drifts in the Tptpll and Tptpmn. This includes *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]) and *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652], Sections 6.3.2 through 6.3.4). Stratigraphy is also explicitly incorporated in *Analysis of Hydrologic Properties Data* (BSC 2004 [DIRS 170038]). Stratigraphy is implicitly incorporated in *Simulation of Net Infiltration for Present-Day and Future Climates* (BSC 2004 [DIRS 170007], Section 6.4) because different strata form the bedrock at different locations.

Supporting Reports: *Development of Numerical Grids for UZ Flow and Transport Modeling* (BSC 2004 [DIRS 169855]); *Calibrated Properties Model* (BSC 2004 [DIRS 169857]); *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]); *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652]); *Analysis of Hydrologic Properties Data* (BSC 2004 [DIRS 170038]); *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]); *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]); *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]); *Simulation of Net Infiltration for Present-Day and Potential Future Climate* (BSC 2004 [DIRS 170007]); *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]).

6.2.11   Rock Properties of Host Rock and Other Units (2.2.03.02.0A)

FEP Description: Physical properties such as porosity and permeability of the relevant rock units, soils, and alluvium are necessary for the performance assessment. Possible heterogeneities in these properties should be considered. Questions concerning events and processes that may cause these physical properties to change over time are considered in other FEPs.

Screening Decision: Included.

TSPA Disposition: This FEP is similar to FEP 2.2.03.01.0A, Stratigraphy (Section 6.2.10). Rock properties used are defined for each of the stratigraphic units/layers classified in the geological framework model (GFM2000; MO0012MWDGFM02.002 [DIRS 153777]), which is further developed into model grid in *Development of Numerical Grids for UZ Flow and Transport Modeling* (BSC 2004 [DIRS 169855]). However, rock properties are not developed in the grid development report. For the UZ flow model rock properties are modeled in terms of the sequence of hydrogeologic units and discrete faults (BSC 2004 [DIRS 169861], Section 6.1.5). Therefore, rock properties are implicitly embedded in the TSPA-LA through the output flow fields, with site-scale layering and faults explicitly taken into account. Rock properties used as

input for *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]) are developed in *Calibrated Properties Model* (BSC 2004 [DIRS 169857], Section 6.3). On the drift scale, the effects of rock heterogeneity on seepage are discussed in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]). Percolation-flux distributions provided by *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]) are used in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.6.5.1), which accounts for rock properties and their variation on a larger scale (e.g., stemming from stratigraphy effects).

Rock properties of host rock and other units are included and used in the simulations of radionuclide transport through the UZ. *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Sections 6.5.3 and 6.5.7) documents the matrix porosity, rock density, fracture porosity, fracture spacing, and aperture data (DTNs: LB0305TSPA18FF.001 [DIRS 165625], LB0210THRMLPRP.001 [DIRS 160799], LB0205REVUZPRP.001 [DIRS 159525], and LB0207REVUZPRP.001 [DIRS 159526]). The generated distributions of fracture porosity and fracture frequency are given in (DTN: LA0407BR831371.001 [DIRS 170806]) and will be used by TSPA-LA in multirealization runs as described in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Sections 6.5.3 and 6.5.7).

All the seepage process models that feed into seepage abstraction explicitly represent the physical properties of the unsaturated rock and their heterogeneity (BSC 2004 [DIRS 169131], Section 6.4). Small-scale heterogeneity is accounted for by a stochastic continuum representation of fracture permeability. Thus, heterogeneity on this scale is implicitly embedded in the model output from the seepage calibration model (BSC 2004 [DIRS 171764], Section 6.5.2), the seepage model for performance assessment (BSC 2004 [DIRS 167652], Sections 6.3.2 through 6.3.4), and the TH seepage model (BSC 2004 [DIRS 170338]) provided respectively in DTNs: LB0304SMDCREV2.002 [DIRS 163687]; LB0307SEEPDRCL.002 [DIRS 164337]; and LB0301DSCPTHSM.002 [DIRS 163689]. The intermediate-scale spatial variability and uncertainty of seepage-relevant rock properties are accounted for by appropriate probability distributions that were developed in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Sections 6.6.1 and 6.6.2). Potential alterations of these properties, as a result of THM or THC processes, have been assessed using drift-scale process models (BSC 2004 [DIRS 169131], Sections 6.4.4.1 and 6.4.4.2). It was demonstrated that these potential alterations can be neglected in the TSPA-LA, because the expected changes would lead to less seepage (BSC 2004 [DIRS 169131], Section 6.5.1.4; see FEPs 2.1.09.12.0A and FEP 2.2.10.04.0A). The THC seepage model feeding into the drift-scale coupled process abstraction model explicitly represents the physical properties of the unsaturated rock (BSC 2004 [DIRS 169856], Section 6.4.7 and Table 6.4-1). Therefore, these effects are explicitly accounted for in the results from the THC seepage model, and their abstraction in *Post-Processing Analysis for THC Seepage* (BSC 2004 [DIRS 169858], Section 6.2). Summary tables of concentrations through time are presented in DTNs: LB0302DSCPTHCS.002 [DIRS 161976], LB0307DSTTHCR2.002 [DIRS 165541], and LB0311ABSTHCR2.003 [DIRS 166713], and summary statistics through time are presented in LB0311ABSTHCR2.001 [DIRS 166714]. These data are used to feed and/or provide technical basis for *Engineered Barrier System: Physical and Chemical Environment Model* (BSC 2004 [DIRS 169860]), which generates lookup tables used in the TSPA-LA model. Small-scale fracture permeability heterogeneity was also investigated and determined not to significantly affect seepage water chemistry (BSC 2004

[DIRS 169856], Section 6.3). The THC seepage model includes rock properties from DTNs: LB0205REVUZPRP.001 [DIRS 159525], LB0208UZDSCPMI.002 [DIRS 161243], LB0207REVUZPRP.002 [DIRS 159672] and LB0210THRMLPRP.001 [DIRS 160799]. Potential alterations of these properties as a result of THC processes are explicitly accounted for by the modeling of coupled THC processes, and result in reducing fracture permeability (BSC 2004 [DIRS 169856], Section 6.5.5.3). The effects of rock properties are also included in the treatment of infiltration uncertainty for TSPA-LA (BSC 2003 [DIRS 165991]). Infiltration uncertainty is represented through three discrete infiltration scenarios (lower, mean, and upper), which are sampled in TSPA-LA according to weighting factors (BSC 2003 [DIRS 165991], Section 7.1). Rock properties are included through the fracture parameters bedrock permeability (BRPERM) and bedrock porosity (BRPOROS). The uncertainties for these parameters are described in *Analysis of Infiltration Uncertainty* (BSC 2003 [DIRS 165991], Tables 6-2 and 6-3). These uncertainties are propagated through the infiltration numerical model and so are implicitly included in the output (weighting factors) that is passed to TSPA-LA (BSC 2003 [DIRS 165991]; DTN: SN0308T0503100.008 [DIRS 165640]). Heterogeneities in these properties are included in the input used in the analysis reported in *Simulation of Net Infiltration for Present-Day and Potential Future Climates* (BSC 2004 [DIRS 170007], Section 6.6.4 and Appendix B).

Rock properties are implicitly incorporated in the output from reports that develop different data sets for drifts in the Tptpll and Tptpmn. This includes *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]) and *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652], Sections 6.3.2 through 6.3.4). Rock properties are also explicitly incorporated in *Analysis of Hydrologic Properties Data* (BSC 2004 [DIRS 170038]). Rock properties are implicitly incorporated in *Simulation of Net Infiltration for Present-Day and Potential Future Climate* (BSC 2004 [DIRS 170007], Section 6.6.4 and Appendix B) and *Analysis of Infiltration Uncertainty* (BSC 2003 [DIRS 165991]) because different rocks form the bedrock at different locations.

Supporting Reports: *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]); *Simulation of Net Infiltration for Present-Day and Potential Future Climates* (BSC 2004 [DIRS 170007]); *Calibrated Properties Model* (BSC 2004 [DIRS 169857]); *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]); *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]); *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652]); *Seepage Calibration Model and Seepage Testing Data* (BSC 2004 [DIRS 171764]); *Analysis of Hydrologic Properties Data* (BSC 2004 [DIRS 170038]); *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]); *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]); *Analysis of Infiltration Uncertainty* (BSC 2003 [DIRS 165991]).

6.2.12 Locally Saturated Flow at Bedrock/Alluvium Contact (2.2.07.01.0A)

FEP Description: In washes in arid areas, infiltration can descend to the alluvium/bedrock interface and then proceed down the wash at that interface as a saturated flow system distinct from the surface and distinct from the local water table.

Screening Decision: Included.

TSPA Disposition: The phenomenon of infiltration resulting in a saturated condition at the bedrock/alluvium contact, with water then either infiltrating into fractures or contributing to lateral drainage, is indirectly included in the infiltration model. Although not explicitly modeled, runoff at the bedrock–alluvium contact is accounted for in the overall model water balance through the calibration process (using runoff measurements). The assumptions underlying this calibration are given in *Simulation of Net Infiltration for Present-Day and Potential Future Climates* (BSC 2004 [DIRS 170007], Section 6.3.4). The impacts of runoff processes on preferential flow–percolation in the UZ is incorporated into the TSPA-LA through the UZ flow fields that use the infiltration model results (DTN: GS000308311221.005 [DIRS 147613]) as upper-boundary conditions (BSC 2004 [DIRS 169861], Sections 6.1.3 and 6.1.4).

The effects of rock properties are also included in the treatment of infiltration uncertainty for TSPA-LA (BSC 2003 [DIRS 165991]). Infiltration uncertainty is represented through three discrete infiltration scenarios (lower, mean, and upper), which are sampled in TSPA-LA according to weighting factors (BSC 2003 [DIRS 165991], Section 7.1). Flow through the alluvium–bedrock interface is incorporated into the uncertainty analysis using the uncertain parameters such as soil depth (SOILDEPM), the soil permeability (SOILPERM), and the effective bedrock permeability (BRPERM). The flow is incorporated implicitly by inclusion of uncertainty in the soil depth, the soil permeability, and the effective bedrock permeability in the calculation of the weighting factors which are passed to TSPA-LA (BSC 2003 [DIRS 165991]; DTN: SN0308T0503100.008 [DIRS 165640]).

Supporting Reports: *Simulation of Net Infiltration for Present-Day and Potential Future Climates* (BSC 2004 [DIRS 170007]); *Analysis of Infiltration Uncertainty* (BSC 2003 [DIRS 165991]); *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]).

6.2.13 Unsaturated Groundwater Flow in the Geosphere (2.2.07.02.0A)

FEP Description: Groundwater flow occurs in unsaturated rocks in most locations above the water table at Yucca Mountain, including at the location of the repository. See related FEPs for discussions of specific issues related to unsaturated flow.

Screening Decision: Included.

TSPA Disposition: This FEP is included in the UZ process models for mountain-scale flow, drift seepage, mountain-scale radionuclide transport, drift-scale radionuclide transport, and seepage chemistry. The flow model is for three-dimensional, steady flow in a heterogeneous dual-permeability system that includes discrete fault zones (BSC 2004 [DIRS 169861], Sections 6.2, 6.6, and 6.7), which allow for a realistic description of flow pathways in the UZ. The flow fields (DTN: LB0305TSPA18FF.001 [DIRS 165625]) generated by the UZ flow model are used directly by the TSPA-LA and are also implicitly included in the TSPA-LA via the abstractions for drift seepage (BSC 2004 [DIRS 169131], Section 6.6.5.1) and radionuclide transport simulations (BSC 2004 [DIRS 170041], Section 6.5.1). The infiltration model provides the flux boundary condition at the top of the UZ flow model (BSC 2004 [DIRS 170007], Section 6.11) and includes the effects of soil depth on UZ flow at Yucca Mountain (BSC 2004 [DIRS 170007], Section 6.1.2).

Unsaturated groundwater flow in the UZ is the driving force for radionuclide transport through the UZ. This FEP is implicitly addressed through the use of pregenerated flow fields (BSC 2004 [DIRS 170041], Section 6.5.1; DTN: LB0305TSPA18FF.001 [DIRS 165625]) in TSPA-LA multirealization runs. The pregenerated flow fields are directly used by FEHM as described in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.5.1). *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]) provides a model for use in TSPA-LA, but does not generate a direct data feed to TSPA-LA pertaining to this FEP.

Parameter values needed to describe unsaturated flow are developed in supporting reports. Data input for model calibration are developed in *Analysis of Hydrologic Properties Data,* BSC 2004 [DIRS 170038]. The van Genuchten α and m values and the active-fracture parameter γ value for each model layer of the fracture and matrix continua are developed in *Calibrated Properties Model* (BSC 2004 [DIRS 169857], Sections 6.1.4 and 6.3). The active fracture model is described and validated in *Conceptual Model and Numerical Approaches for UZ Flow and Transport* (BSC 2004 [DIRS 170035], Sections 6.3 and 7). Seepage-relevant parameters for the drift-scale seepage model are based on measurements reported in *In Situ Field Testing of Processes* (BSC 2004 [DIRS 170004, Sections 6.1 and 6.2) and developed in *Seepage Calibration Model and Seepage Testing Data* (BSC 2004 [DIRS 171764], Sections 6.3.2 and 6.6.1.1). Unsaturated flow processes are accounted for in the seepage abstraction by using results from process models that explicitly account for various relevant aspects of unsaturated groundwater flow. All the seepage process models that feed into seepage abstraction simulate groundwater flow processes in unsaturated rock (BSC 2004 [DIRS 169131], Section 6.4). For ambient seepage, the fracture flow processes in the drift vicinity and the resulting seepage rates are predicted by model simulations from the seepage model for performance assessment (BSC 2004 [DIRS 167652], Sections 6.2.1 and 6.3.4), and abstracted in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.4.2). Results are available as look-up tables in DTNs: LB0304SMDCREV2.002 [DIRS 163687] and LB0307SEEPDRCL.002 [DIRS 164337]. These will be used in the TSPA-LA to calculate ambient seepage, by sampling parameter cases of seepage-relevant parameters from the probability distributions defined in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.7.1). During the thermal period, the ambient seepage rates will be adjusted based on the TH-modeling results from *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]), which explicitly simulates thermally perturbed groundwater flow processes. Results are given in DTN: LB0301DSCPTHSM.002 [DIRS 163689]. THM and THC effects on fracture flow processes are evaluated with process models that explicitly account for groundwater flow processes affected by THM and THC parameter alterations (BSC 2004 [DIRS 169131], Sections 6.4.4.1 and 6.4.4.2). It was demonstrated that these potential alterations can be neglected in the TSPA-LA, as the expected changes would lead to less seepage (BSC 2004 [DIRS 169131], Section 6.5.1.4). See also FEPs 2.1.09.12.0A and 2.2.10.04.0A. Percolation flux distributions are provided by the UZ flow model (BSC 2004 [DIRS 169131], Section 6.6.5.1), which accounts for groundwater flow on a larger scale, influenced by climate changes, infiltration variability, and stratigraphy effects.

The THC seepage model that feeds into the drift-scale coupled processes abstraction model simulates groundwater flow and water-gas-rock interactions in unsaturated rock and explicitly accounts for various relevant aspects of unsaturated groundwater flow (BSC 2004

[DIRS 169856], Section 6.2.1). Therefore, the results from the THC seepage model, and their abstraction in *Post-Processing Analysis for THC Seepage* (BSC 2004 [DIRS 169858], Section 6.2), explicitly account for the effect of unsaturated groundwater flow on predicted water and gas chemistry. Summary tables of concentrations through time are presented in DTNs: LB0302DSCPTHCS.002 [DIRS 161976], LB0307DSTTHCR2.002 [DIRS 165541], and LB0311ABSTHCR2.003 [DIRS 166713]), and summary statistics through time are presented in LB0311ABSTHCR2.001 [DIRS 166714]. These data are used to feed and/or provide technical basis for *Engineered Barrier System: Physical and Chemical Environment Model* (BSC 2004 [DIRS 169860]), which generates look-up tables used in the TSPA-LA model.

Supporting Reports: *In Situ Field Testing of Processes* (BSC 2004 [DIRS 170004]); *Simulation of Net Infiltration for Present-Day and Potential Future Climates* (BSC 2004 [DIRS 170007]); *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]); *Conceptual Model and Numerical Approaches for UZ Flow and Transport* (BSC 2004 [DIRS 170035]); *Calibrated Properties Model* (BSC 2004 [DIRS 169857]); *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652]); *Seepage Calibration Model and Seepage Testing Data* (BSC 2004 [DIRS 171764]); *Analysis of Hydrologic Properties Data* (BSC 2004 [DIRS 170038]); *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]); *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]); *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]; *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]).

6.2.14 Capillary Rise in the UZ (2.2.07.03.0A)

FEP Description: Capillary rise involves the drawing up of water, above the water table or above locally saturated zones, in continuous pores of the unsaturated zone until the suction gradient is balanced by the gravitational pull downward.

Screening Decision: Included.

TSPA Disposition: Capillary forces are included in the UZ flow model. These forces affect the distribution of water in the UZ through capillary effects on water flow, also known as capillary wicking. Parameters used for capillarity modeling are incorporated within the matrix properties (DTN: LB02091DSSCP3I.002 [DIRS 161433]) and fracture properties (DTN: LB0205REVUZPRP.001 [DIRS 159525]) as described in *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861], Section 6.2.5). These parameters are used as direct input to the UZ flow model and are implicitly incorporated into the output flow fields used in the TSPA-LA (output flow fields are in DTN: LB0305TSPA18FF.001 [DIRS 165625]).

Supporting Reports: *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]).

6.2.15 Focusing of Unsaturated Flow (Fingers, Weeps) (2.2.07.04.0A)

FEP Description: Unsaturated flow can differentiate into zones of greater and lower saturation (fingers) that may persist as preferential flow paths. Heterogeneities in rock properties, including fractures and faults, may contribute to focusing. Focused flow may become locally saturated.

Screening Decision: Included.

TSPA Disposition: The UZ flow fields represent the redistribution of infiltration through UZ layers, with faults explicitly taken into account (BSC 2004 [DIRS 169861], Sections 6.1.2, 6.6.3, and 6.7.3). The flux redistribution is based on tuff layer properties including fracture and matrix interaction. Faults are included in the UZ flow model as discrete features; therefore, flow in faults is also included in the UZ flow model (BSC 2004 [DIRS 169861]). Flow model results indicate that as flow moves downward through the UZ, the flow tends to focus into fault zones, with the fraction of flow in the faults increasing from about 30–40 percent at the repository to about 60 percent at the water table (BSC 2004 [DIRS 169861], Section 6.6.3).

For radionuclide transport, the effect of focusing unsaturated flow is implicitly included through the use of pregenerated flow fields contained in DTN: LB0305TSPA18FF.001 [DIRS 165625] for simulations (BSC 2004 [DIRS 170041], Sections 6.5.1, 6.6.2). In TSPA-LA runs, pregenerated flow fields are used directly by the transport model FEHM (LANL 2003 [DIRS 165741]). *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]) provides a model for use in TSPA-LA, but does not generate a direct data feed to TSPA-LA pertaining to this FEP.

Intermediate-scale focusing of flow from the site scale to the drift scale is accounted for in the seepage abstraction by using appropriate flow-focusing factors (BSC 2004 [DIRS 169131], Section 6.6.5.2). The distribution of flow-focusing factors used for seepage calculations is developed in *Seepage Calibration Model and Seepage Testing Data* (BSC 2004 [DIRS 171764], Sections 6.3 and 6.6), using property values calibrated in *Calibrated Properties Model* (BSC 2004 [DIRS 169857], Sections 6.1.4 and 6.3.2). Small-scale preferential flow is explicitly simulated in the seepage process model, developed in *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652], Section 6.8) that feeds into the abstraction by use of heterogeneous fracture-permeability fields (BSC 2004 [DIRS 169131], Sections 6.4.1.1, 6.4.2.1, and 6.4.3.1). Thus, preferential flow is inherently embedded in the seepage look-up tables for ambient seepage given in DTNs: LB0304SMDCREV2.002 [DIRS 163687] and LB0307SEEPDRCL.002 [DIRS 164337], and in the thermal seepage results provided in DTN: LB0301DSCPTHSM.002 [DIRS 163689]. The abstraction methodology for both ambient and thermal seepage is described in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.7.1). The possibility of episodic finger flow is accounted for with an alternative conceptual model analyzed in the thermal seepage model report (BSC 2004 [DIRS 170338], Section 6.3). Results from this alternative conceptual model are consistent with results from the TH seepage model used for this abstraction (BSC 2004 [DIRS 169131], Section 6.4.3.2).

Intermediate-scale focusing of flow from the site scale to the drift scale is implicitly accounted for in *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338] by using appropriate flow-focusing factors (BSC 2004 [DIRS 169131], Section 6.6.5.2). However, flow focusing is not taken into account in the THC seepage model results or their abstraction (BSC 2004 [DIRS 169858], Section 6.2. This is because fracture permeability heterogeneity was determined to not significantly affect seepage water chemistry (BSC 2004 [DIRS 169856],   Section 6.3).   DTNs: LB0302DSCPTHCS.002   [DIRS 161976]   and LB0311ABSTHCR2.001 [DIRS 166714] are used to feed and/or provide technical basis for *Engineered Barrier System: Physical and Chemical Environment Model* (BSC 2004

[DIRS 169860]), which generates look-up tables used in the TSPA-LA model. Another aspect of flow focusing is the channeling of fracture flow into a relatively few fractures. This is captured in the active fracture model described and validated in *Conceptual Model and Numerical Approaches for UZ Flow and Transport* (BSC 2004 [DIRS 170035], Sections 6.1.7 and 6.3.7, description; Section 7, validation). The active-fracture parameter values for different model layers are calibrated in the *Calibrated Properties Model* (BSC 2004 [DIRS 169857], Tables 6-8, 6-9, 6-10, and 6-14).

Supporting Reports: *Conceptual Model and Numerical Approaches for UZ Flow and Transport* (BSC 2004 [DIRS 170035]); *Calibrated Properties Model* (BSC 2004 [DIRS 169857]); *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]); *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652]); *Seepage Calibration Model and Seepage Testing Data* (BSC 2004 [DIRS 171764]); *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]); and *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]); *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]); *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]).

6.2.16 Long-Term Release of Radionuclides from the Repository (2.2.07.06.0B)

FEP Description: The release of radionuclides from the repository may occur over a long period of time, as a result of the timing and magnitude of the waste packages and drip shield failures, waste form degradation, and radionuclide transport through the invert.

Screening Decision: Included.

TSPA Disposition: The effects of long-term waste package failures over a long period of time are included in the source term model for TSPA-LA (BSC 2003 [DIRS 166296], Section 5.1). This is done by modeling the environmental conditions of the waste packages in different parts of the repository and by modeling corrosion processes under these environmental conditions that lead to waste package failure. Releases from the waste package and engineered barrier system serve as a time-dependent boundary condition to the mountain-scale radionuclide transport model, which allows for a general time-dependent radionuclide source term that accounts for long-term releases (BSC 2004 [DIRS 170041], Section 6.4.7). For each GoldSim-FEHM run, GoldSim passes radionuclide mass releases to FEHM and FEHM simulates the transport process through the UZ. Long-term radionuclide release because of the failure of waste packages in the repository is implicitly included in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Sections 6.4.6 and 6.4.7). *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]) provides a model for use in TSPA-LA, but does not generate a direct data feed to TSPA-LA pertaining to this FEP.

Supporting Reports: *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]).

6.2.17 Perched Water Develops (2.2.07.07.0A)

FEP Description: Zones of perched water may develop above the water table. If these zones occur above the repository, they may affect UZ flow between the surface and the waste

packages. If they develop below the repository, e.g. at the base of the Topopah Spring welded unit, they may affect flow pathways and radionuclide transport between the waste packages and the saturated zone.

Screening Decision: Included.

TSPA Disposition: The seepage abstraction model contains a wide range of seepage possibilities, including flow focusing and spatial variability (BSC 2004 [DIRS 169131], Section 6). Therefore, the potential for effects of perched water above the repository are indirectly captured in the seepage abstraction model through cases with high percolation flux (DTN: LB0305TSPA18FF.001 [DIRS 165625]), as described in the model report *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6). However, above the repository, no perched water bodies were observed in the fields predicted by the UZ flow model. The effects of existing perched water zones below the repository are also included, and potential changes in these perched-water zones caused by climate changes are also included in the mountain-scale UZ flow model (BSC 2004 [DIRS 169861], Sections 6.2.2, 6.2.3, 6.2.5, 6.6.2, and 6.6.3). The potential for this effect is captured in the output flow fields developed for use in TSPA-LA (output flow fields are in DTN: LB0305TSPA18FF.001 [DIRS 165625]).

This FEP is also implicitly included through the use of pregenerated flow fields (DTN: LB0305TSPA18FF.001 [DIRS 165625]) for radionuclide transport in the UZ. In TSPA-LA runs, pregenerated flow fields are used by FEHM and used in UZ transport simulations as described in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.5.1). *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]) provides a model for use in TSPA-LA, but does not generate a direct data feed to TSPA-LA pertaining to this FEP.

Supporting Reports: *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]), *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]).

6.2.18 Fracture Flow in the UZ (2.2.07.08.0A)

FEP Description: Fractures or other analogous channels may act as conduits for fluids to move into the subsurface to interact with the repository and as conduits for fluids to leave the vicinity of the repository and be conducted to the SZ. Water may flow through only a portion of the fracture network, including flow through a restricted portion of a given fracture plane.

Screening Decision: Included.

TSPA Disposition: The UZ flow model is based on the dual-permeability concept, with the fractures represented by a continuum (BSC 2004 [DIRS 169861], Section 6.1.2). The fracture continuum represents the spatially averaged flow through discrete fractures. The fracture continuum interacts with the matrix continuum, which represents matrix blocks separated by fractures. Fracture continuum properties, including permeability, porosity, interface area per unit volume, van Genuchten α and m parameters for the saturation-capillary pressure and relative permeability functions, and active fracture parameter γ, for each UZ model layer are used as input to the UZ flow model (DTN: LB0205REVUZPRP.001 [DIRS 159525] listed in *UZ Flow*

Models and Submodels (BSC 2004 [DIRS 169861], Table 4.1-1). These fracture continuum properties are developed from data acquired in *In Situ Field Testing of Processes* (BSC 2004 [DIRS 170004], Sections 6.2 and 6.6). Permeabilities and other properties are calibrated as described in the *Analysis of Hydrologic Properties Data* (BSC 2004 [DIRS 170038]) and *Calibrated Properties Model* (BSC 2004 [DIRS 169857], Sections 6.1.4 and 6.3). The fracture-continuum properties are used as inputs to the UZ flow model, and their effects are incorporated into the output flow fields developed for use in TSPA-LA (output flow fields are in DTN: LB0305TSPA18FF.001 [DIRS 165625]). Output flow fields for the fracture continuum are presented in *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861], Section 6.6.3)

The top boundary condition for the UZ flow model is set by the infiltration maps output by *Simulation of Net Infiltration for Present-Day and Potential Future Climates* (BSC 2004 [DIRS 170007], Section 6.11). When the soil/bedrock contact reaches near-saturated conditions, fracture flow is initiated in the bedrock (BSC 2004 [DIRS 170007]) Sections 6.1.2 and 6.3.4). Channeling in the UZ fracture continuum is captured as discussed for FEP 2.2.07.04.0A, including the use of the active fracture model in *Conceptual Model and Numerical Approaches for UZ Flow and Transport* (BSC 2004 [DIRS 170035], Section 6.3); and the development of the distribution of flow-focusing factors in *Seepage Calibration Model and Seepage Testing Data* (BSC 2004 [DIRS 171764], Sections 6.3 and 6.6).

In the UZ, fracture flow plays an important role in the transport of radionuclides. In TSPA-LA runs, the effect of fracture flow on radionuclide transport (advection) is implicitly included through FEHM's use of pregenerated flow fields (DTN: LB0305TSPA18FF.001 [DIRS 165625]) in UZ transport simulations as described in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.5.1). *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]) provides a model for use in TSPA-LA, but does not generate a direct data feed to TSPA-LA pertaining to this FEP.

Flow processes in fractures or other channels are important for the seepage abstraction, because the amount of seepage is determined by the capacity of the fracture network to divert flow around the drifts as a result of capillary forces (*Abstraction of Drift Seepage,* BSC 2004 [DIRS 169131], Section 6.3.1). All the seepage process models that feed into seepage abstraction simulate flow processes in fractured rock (BSC 2004 [DIRS 169131], Section 6.4). Spatial variability in the fracture flow, potentially leading to water flow through only a portion of the fracture network, is accounted for by using a stochastic continuum representation. For ambient seepage, the fracture flow processes in the drift vicinity and the resulting seepage rates are predicted by model simulations from the seepage model for PA (BSC 2004 [DIRS 167652], Sections 6.3.2 and 6.3.3) and abstracted in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.4.2). Results are available as look-up tables in DTNs: LB0304SMDCREV2.002 [DIRS 163687] and LB0307SEEPDRCL.002 [DIRS 164337]. These will be used in the TSPA-LA to calculate ambient seepage, by sampling parameter cases of seepage-relevant parameters from the probability distributions defined in Section 6.7.1 of *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]). During the thermal period, the ambient seepage rates will be adjusted based on the TH-modeling results from *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]), which explicitly simulates thermally perturbed fracture flow conditions. Results are given in

DTN: LB0301DSCPTHSM.002 [DIRS 163689]. The abstraction methodology for thermal seepage is developed in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]), Section 6.5.2). THM and THC effects on fracture flow processes are evaluated with process models that explicitly account for fracture flow affected by THM and THC parameter alterations (BSC 2004 [DIRS 169131], Section 6.4.4). It was demonstrated that these potential alterations can be neglected in the TSPA-LA, because the expected changes would lead to less seepage (BSC 2004 [DIRS 169131], Section 6.5.1.4; Sections 6.9.1 (FEP 2.1.09.12.0A) and 6.9.10 (FEP 2.2.10.04.0A). Percolation flux distributions are provided by the UZ flow model for use in the seepage abstraction model (BSC 2004 [DIRS 169131], Section 6.6.5.1), which accounts for fracture flow on a larger scale (influenced by climate changes), infiltration variability, and stratigraphy effects. Flow focusing effects (channeling) are included as discussed in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.6.5.2).

Flow processes in fractures or other channels affect modeled THC coupled processes because of (1) their strong effect on TH behavior (BSC 2004 [DIRS 169131], Section 6.4.4) and (2) their strong effect on water and gas chemistry (BSC 2004 [DIRS 169856], Section 6.2.1). The latter is primarily due to volatilization of steam and CO_2 from the rock matrix-water and subsequent transport and condensation in fractures. The amount of mobilized CO_2 with steam directly affects the pH of the condensate, which in turn affects the degree of water–rock interaction and water chemistry. These THC processes are influenced by the fracture characteristics, such as orientation, aperture, asperity, length, connectivity, and fillings. The THC seepage model that feeds into the drift scale coupled processes abstraction model explicitly simulate the flow processes in fractures using appropriate continuum properties that represent these characteristics as shown in *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856], Sections 6.4.3, 6.4.4, and 6.4.7). Thus, the results from the THC seepage model and their abstraction (BSC 2004 [DIRS 169858], Section 6.2), and tables of concentrations and summary statistics through time, implicitly account for the effect of climate change on THC processes. Summary tables of concentrations through time are presented in DTNs: LB0302DSCPTHCS.002 [DIRS 161976], LB0307DSTTHCR2.002 [DIRS 165541], and LB0311ABSTHCR2.003 [DIRS 166713], and summary statistics through time are presented in LB0311ABSTHCR2.001 [DIRS 166714]. These data are used to feed and/or provide technical basis for *Engineered Barrier System: Physical and Chemical Environment Model* (BSC 2004 [DIRS 169860) that generates lookup tables used in the TSPA-LA model. The effects of fracture flow are also included in the treatment of infiltration uncertainty for TSPA-LA (BSC 2003 [DIRS 165991]). Infiltration uncertainty is represented through three discrete infiltration scenarios (lower, mean, and upper), which are sampled in TSPA-LA according to weighting factors (BSC (2003 [DIRS 165991], Section 7.1). This FEP is implicitly included in the determination of the weighing factors fed to TSPA-LA (BSC 2003 [DIRS 165991]; DTN: SN0308T0503100.008 [DIRS 165640]). This FEP is incorporated in the uncertain parameters describing the bedrock permeability multiplier (BRPERM) and bedrock porosity (BRPOROS).

Supporting Reports: *In Situ Field Testing of Processes* (BSC 2004 [DIRS 170004]); *Simulation of Net Infiltration for Present-Day and Potential Future Climates* (BSC 2004 [DIRS 170007]); *Conceptual Model and Numerical Approaches for UZ Flow and Transport* (BSC 2004 [DIRS 170035]); *Analysis of Hydrologic Properties Data* (BSC 2004 [DIRS 170038]); *Calibrated Properties Model* (BSC 2004 [DIRS 169857]); *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]); *Seepage Model for PA Including Drift Collapse*

(BSC 2004 [DIRS 167652]); *Seepage Calibration Model and Seepage Testing Data* (BSC 2004 [DIRS 171764]); *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]); *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]); *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]); *Analysis of Infiltration Uncertainty* (BSC 2003 [DIRS 165991]); *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]).

6.2.19   Matrix Imbibition in the UZ (2.2.07.09.0A)

FEP Description: Water flowing in fractures or other channels in the unsaturated zone may be imbibed into the surrounding rock matrix. This may occur during steady flow, episodic flow, or into matrix pores that have been dried out during the thermal period.

Screening Decision: Included.

TSPA Disposition: Matrix imbibition is included in the process model for UZ flow at the mountain scale (BSC 2004 [DIRS 169861], Section 6.1.2). Matrix imbibition refers to the movement of water into the matrix as a result of capillary forces. This process affects the distribution of flow between fractures and matrix in a dual-permeability flow model for fractured rock. The flow simulations in *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861], Section 6.6) are for steady-state flow. Imbibition is captured in the UZ flow model through capillarity modeling, which uses matrix and fracture properties as model input. Therefore, the effect of imbibition is implicitly incorporated in the output flow fields (DTN: LB0305TSPA18FF.001 [DIRS 165625]) used in the TSPA-LA. Matrix imbibition is implicit in the increase in matrix saturation that is simulated when changing to a wetter climate state. Matrix imbibition is also important in damping the effect of episodic infiltration, as discussed in Appendix G of *UZ Flow Models and Submodel* (BSC 2004 [DIRS 169861]). Also see FEP 2.2.07.05.0A, Flow in the UZ from episodic infiltration.

For TSPA-LA runs, the pregenerated flow fields (DTN: LB0305TSPA18FF.001 [DIRS 165625]) are used by FEHM in UZ transport simulations as described in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.5.1). Therefore, the effects of matrix imbibition are implicitly included in the treatment of UZ radionuclide transport. However, *Particle Tracking Model and Abstraction of Transport Processes* provides a model for use in TSPA-LA, but does not generate a direct data feed to TSPA-LA.

The THC seepage model similarly explicitly accounts for matrix imbibition using appropriate dual-permeability modeling concepts as reported in *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856], Section 6.2.1). This is needed because heating and dryout of the unsaturated rock transfers liquid and gas from the matrix into the fractures; upon rewetting water and solutes are imbibed from fracture to matrix (see, for example, BSC 2004 [DIRS 169856], Figure 6.2-3). Therefore, these effects are directly accounted for in the results from the THC seepage model, and in their abstraction in *Post-Processing Analysis for THC Seepage* (BSC 2004 [DIRS 169858], Section 6.2). Summary tables of concentrations through time are presented in DTNs: LB0302DSCPTHCS.002 [DIRS 161976], LB0307DSTTHCR2.002 [DIRS 165541], and LB0311ABSTHCR2.003 [DIRS 166713], and summary statistics through time are presented in

LB0311ABSTHCR2.001 [DIRS 166714. These data are used to feed and/or provide technical basis for *Engineered Barrier System: Physical and Chemical Environment Model* (BSC 2004 [DIRS 169860]), which generates look-up tables used in the TSPA-LA model.

Ambient seepage is mainly governed by flow in the fractures, as discussed in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.4). Thus, in the predictive model for ambient seepage, that is, the seepage calibration model (BSC 2004 [DIRS 171764], Section 6.3.3.2) and the seepage model for PA (BSC 2004 [DIRS 167652], Section 6.3), matrix imbibition is neglected. In contrast, the drift-scale process models addressing TH, THM, and THC processes, including *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]), *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]), and *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Sections 6.4.3.1, 6.4.4.1, and 6.4.4.2), explicitly account for matrix imbibition using appropriate dual-permeability modeling concepts. This is needed because the thermal perturbation of the unsaturated rock results in significant transfer of liquid and gas from the matrix into the fractures and vice versa. The UZ flow model (which provides the percolation flux distributions used for seepage calculations) also accounts for the impact of matrix imbibition in an explicit manner (BSC 2004 [DIRS 169131], Section 6.6.5.1). Thus, matrix imbibition effects are inherently embedded in the respective model results used for this abstraction.

Matrix imbibition tests are reported in *In Situ Field Testing of Processes* (BSC 2004 [DIRS 170004], Section 6.4). The matrix properties used to simulate matrix imbibition are developed in *Calibrated Properties Model* (BSC 2004 [DIRS 169857], Section 6.1.5).

Supporting Reports: *In Situ Field Testing of Processes* (BSC 2004 [DIRS 170004]); *Calibrated Properties Model* (BSC 2004 [DIRS 169857]); *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]); *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652]); *Seepage Calibration Model and Seepage Testing Data* (BSC 2004 [DIRS 171764]); *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]); *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]); *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]); *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]).

6.2.20 Condensation Zone Forms around Drifts (2.2.07.10.0A)

FEP Description: Condensation of the two-phase flow generated by repository heat may form in the rock where the temperature drops below the local vaporization temperature. Waste package emplacement geometry and thermal loading may affect the scale at which condensation caps form (over waste packages, over panels, or over the entire repository), and the extent to which "shedding" will occur as water flows from the region above one drift to the region above another drift or into the rock between drifts.

Screening Decision: Included.

TSPA Disposition: The coupled processes of vapor condensation forming a condensation zone (or "condensation cap") in the fractured rock above the drifts are explicitly simulated with the TH seepage model (BSC 2004 [DIRS 170338], Sections 6.2 and 7.4) that feeds into the seepage

abstraction. Using this model, the impact of condensation and shedding on seepage is assessed for various simulation cases (BSC 2004 [DIRS 169131], Section 6.4.3.3). Thus, the TH-modeling results from DTN: LB0301DSCPTHSM.002 [DIRS 163689] inherently include these effects. As discussed in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.5.2), the abstraction of thermal seepage uses these modeling results to develop an appropriate thermal-seepage abstraction methodology.

The coupled processes of vapor condensation forming a condensation cap above the drifts and occurrence of "shedding" between drifts (that is, diversion of vapor to cooler regions and drainage of condensation through the cooler region between drifts) are explicitly simulated with the THC seepage model (BSC 2004 [DIRS 169856], Sections 6.2.1, 6.5.5.1, 6.5.5.3, and 6.5.5.2.2). Using this model, the impact of condensation and drainage on seepage water chemistry is assessed for various simulation cases (BSC 2004 [DIRS 169856], Sections 6.2, 6.5, and 6.6). Therefore, the results from the THC seepage model, and their abstraction in *Post-Processing Analysis for THC Seepage* (BSC 2004 [DIRS 169858], Section 6.2), explicitly include these effects. Summary tables of concentrations through time are presented in DTNs: LB0302DSCPTHCS.002 [DIRS 161976], LB0307DSTTHCR2.002 [DIRS 165541], and LB0311ABSTHCR2.003 [DIRS 166713], and summary statistics through time are presented in LB0311ABSTHCR2.001 [DIRS 166714]. These data are used to feed and/or provide technical basis for *Engineered Barrier System: Physical and Chemical Environment Model* (BSC 2004 [DIRS 169860]), which generates look-up tables used in the TSPA-LA model.

Supporting Reports: *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]); *Abstraction of Drift Seepage;* (BSC 2004 [DIRS 169131]); *Post-Processing Analysis for THC Seepage* (BSC 2004 [DIRS 169858]); *Drift-Scale Coupled Processes (DST and TH Seepage) Models;* (BSC 2004 [DIRS 170338]).

6.2.21 Resaturation of Geosphere Dry-Out Zone (2.2.07.11.0A)

FEP Description: Following the peak thermal period, water in the condensation cap may flow downward into the drifts. Influx of cooler water from above, such as might occur from episodic flow, may accelerate return flow from the condensation cap by lowering temperatures below the condensation point. Percolating groundwater will also contribute to resaturation of the dry-out zone. Vapor flow, as distinct from liquid flow by capillary processes, may also contribute.

Screening Decision: Included.

TSPA Disposition: Resaturation of the dryout zone around drifts, and the potential of return flow from the condensation zone back to the drifts, are explicitly simulated with the TH seepage model (BSC 2004 [DIRS 170338], Section 6.2), which feeds into seepage abstraction. Using this model, the impact of resaturation and reflux (on) seepage is assessed for various simulation cases (BSC 2004 [DIRS 169131], Section 6.4.3.3). Thus, the TH-modeling results from DTN: LB0301DSCPTHSM.002 [DIRS 163689] inherently include these effects. As discussed in *Abstraction of Drift Seepage* (BSC (2004 [DIRS 169131], Section 6.5.2), the abstraction of thermal seepage utilizes these modeling results to develop an appropriate thermal-seepage abstraction methodology. The impact of potential episodic flow was addressed with an alternative conceptual model for thermal seepage, as discussed in *Abstraction of Drift Seepage*

(BSC 2004 [DIRS 169131], Section 6.4.3). It was shown that results from this alternative conceptual model are consistent with the process model results from the TH seepage model used for this abstraction.

Resaturation of the dryout zone around drifts, and the potential of return flow from the condensation zone back to the drifts, are explicitly simulated with the THC seepage model (BSC 2004 [DIRS 169856], Sections 6.2.1 and 6.5.5). Using this model, the impact of resaturation on reflux chemistry is assessed as part of the abstraction methodology (that is, the compositions of abstracted "FRONT" waters reflect concentration increases because of the dissolution of salts precipitated during dryout; see *Post-Processing Analysis for THC Seepage* (BSC 2004 [DIRS 169858], Section 6.2.3.1). Therefore, the results from the THC seepage model, and their abstraction in *Post-Processing Analysis for THC Seepage* (BSC 2004 [DIRS 169858], Section 6.2), explicitly include these effects. Summary tables of concentrations through time are presented in DTNs: LB0302DSCPTHCS.002 [DIRS 161976], LB0307DSTTHCR2.002 [DIRS 165541], and LB0311ABSTHCR2.003 [DIRS 166713], and summary statistics through time are presented in LB0311ABSTHCR2.001 [DIRS 166714]. These data are used to feed and/or provide technical basis for *Engineered Barrier System: Physical and Chemical Environment Model* (BSC 2004 [DIRS 169860]), which generates look-up tables used in the TSPA-LA model.

Supporting Reports: *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]); *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]); *Post-Processing Analysis for THC Seepage* (BSC 2004 [DIRS 169858]); *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]).

6.2.22   Advection and Dispersion in the UZ (2.2.07.15.0B)

FEP Description: Advection and dispersion processes may affect radionuclide transport in the UZ.

Screening Decision: Included.

TSPA Disposition: Radionuclide transport through the UZ by advection is simulated using the RTTF (Residence Time Transfer Function) method documented in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.4.1). Dispersion is incorporated into the RTTF algorithm through the use of a transfer function based on an analytical solution to the advection–dispersion equation (BSC 2004 [DIRS 170041], Section 6.4.2). In TSPA–LA runs, advection and dispersion are implicitly included through the use of FEHM RTTF model and the pregenerated flow fields as described in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Sections 6.4 and 6.5.1). *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]) provides a model for use in TSPA-LA, but does not generate a direct data feed to TSPA-LA pertaining to this FEP.

Supporting Reports: *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]).

6.2.23   Film Flow into the Repository (2.2.07.18.0A)

FEP Description: Water may enter waste emplacement drifts by a film flow process. This differs from the traditional view of flow in a capillary network where the wetting phase exclusively occupies capillaries with apertures smaller than some level defined by the capillary pressure. A film flow process could allow water to enter a waste emplacement drift at non-zero capillary pressure. Dripping into the drifts could also occur through collection of the film flow on the local minima of surface roughness features along the crown of the drift.

Screening Decision: Included.

TSPA Disposition: The potential impact of film flow is represented in the data acquired in *In Situ Field Testing of Processes* (BSC 2004 [DIRS 170004], Section 6.2) and developed by *Seepage Calibration Model and Seepage Testing Data* (BSC 2004 [DIRS 171764], Sections 6.1.2, 6.3.3, and 6.6.3), into results that are used for the seepage abstraction; that is, the calibrated values of the capillary-strength parameter given in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Table 6.6-1 and DTN: LB0302SCMREV02.002 [DIRS 162273]). If water originating from film flow seeps into the opening during a liquid-release test, it is reflected in the corresponding seepage data point used for model calibration. Film flow is thus inherently accounted for in the estimated seepage-related capillary-strength parameter from the seepage calibration model (BSC 2004 [DIRS 171764]), and thus in the prediction of seepage into waste emplacement drifts in *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652], Section 6.3) and the abstraction in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.4.1.1). In theory, film-flow behavior may be influenced by the elevated temperatures in the drift vicinity during the first several thousand years after emplacement. This effect is not included in the ambient liquid-release tests. However, the potential changes in film flow as a result of temperature increase are not expected to be significant for drift seepage.

Supporting Reports: *In Situ Field Testing of Processes* (BSC 2004 [DIRS 170004]); *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]); *Seepage Calibration Model and Seepage Testing Data* (BSC 2004 [DIRS 171764]); *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652]).

6.2.24   Lateral Flow from Solitario Canyon Fault Enters Drifts (2.2.07.19.0A)

FEP Description: Water movement down Solitario Canyon Fault could enter waste emplacement drifts through lateral flow mechanisms in the Topopah Spring welded hydrogeologic unit. This percolation pathway is more likely to transmit episodic transient flow to waste emplacement locations due to the major fault pathway through the overlying units.

Screening Decision: Included.

TSPA Disposition: The UZ flow model contains potential hydrogeologic connections between the Solitario Canyon Fault and the waste emplacement horizon. The potential connection is captured using a property set of the PTn unit with calibrated fracture-matrix properties that favor lateral flow (BSC 2004 [DIRS 169861], Sections 6.2.2.1 and 6.2.3). Therefore, flow from this fault to waste emplacement locations is addressed. This water may seep into waste emplacement

drifts if the flux is sufficient to overcome the capillary barrier represented in the drift seepage model (BSC 2004 [DIRS 169131]); however, this FEP is not explicitly represented in that report. The lateral flow effect is implicitly incorporated in the output flow fields developed in *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861], Section 6.6.3) and submitted to the TDMS (DTN: LB0305TSPA18FF.001 [DIRS 165625]) for use in TSPA-LA. Other aspects of flow focusing in faults (preferential flow in faults) are discussed in FEP 2.2.07.04.0A. Perched water is discussed in FEP 2.2.07.07.0A.

Supporting Reports: *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]).

6.2.25   Flow Diversion around Repository Drifts (2.2.07.20.0A)

FEP Description: Flow in unsaturated rock tends to be diverted by openings such as waste emplacement drifts due to the effects of capillary forces. The resulting diversion of flow could have an effect on seepage into the repository. Flow diversion around the drift openings could also lead to the development of a zone of lower flow rates and low saturation beneath the drift, known as the drift shadow.

Screening Decision: Included.

TSPA Disposition: The impact of flow diversion around the drifts and its relevance for seepage is explicitly captured in the data acquired in *In Situ Field Testing of Processes* (BSC 2004 [DIRS 170004], Section 6.2) and in the seepage process models (BSC 2004 [DIRS 171764], Sections 6.3, 6.6, and 6.8; BSC 2004 [DIRS 167652], Sections 6.2.1, 6.3.2, and 6.7; BSC 2004 [DIRS 170338]; BSC 2004 [DIRS 169856]) and the seepage abstractions (BSC 2004 [DIRS 169131], Sections 6.4.1, 6.4.2, and 6.4.3). From these model simulations, seepage predictions are available in the form of look-up tables in DTNs: LB0304SMDCREV2.002 [DIRS 163687] and LB0307SEEPDRCL.002 [DIRS 164337]. These will be used in the TSPA-LA to calculate ambient seepage, by sampling parameter cases of seepage-relevant parameters from the probability distributions defined in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.7.1). These seepage-relevant parameters are the effective capillary-strength parameter permeability and local percolation flux. During the thermal period, the ambient rates will be adjusted based on the TH-modeling results from DTN: LB0301DSCPTHSM.002 [DIRS 163689], using the abstraction methodology developed in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.5.2.1). The drift seepage model also captures the effects of drift collapse (BSC 2004 [DIRS 169131], Sections 6.4.2.4 and 6.7.1.2) in terms of the larger drift profile that results.

Supporting Reports: *In Situ Field Testing of Processes* (BSC 2004 [DIRS 170004]); *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652]); *Seepage Calibration Model and Seepage Testing Data* (BSC 2004 [DIRS 171764]); *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]); *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]); *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]).

6.2.26   Chemical Characteristics of Groundwater in the UZ (2.2.08.01.0B)

FEP Description: Chemistry and other characteristics of groundwater in the unsaturated zone may affect groundwater flow and radionuclide transport of dissolved and colloidal species.

Groundwater chemistry and other characteristics, including temperature, pH, Eh, ionic strength, and major ionic concentrations, may vary spatially throughout the system as a result of different rock mineralogy.

Screening Decision: Included.

TSPA Disposition: THC seepage model simulations feeding the drift scale coupled processes abstraction were run explicitly using five different input water compositions representing the range of compositions at Yucca Mountain (BSC 2004 [DIRS 169856], Table 6.2-1, Sections 6.2.2 and 6.5.5). This variability of porewater compositions in repository host units implicitly reflects spatial variations in rock mineralogy and infiltration rates. Therefore, the results from the THC seepage model, and their abstraction in *Post-Processing Analysis for THC Seepage* (BSC 2004 [DIRS 169858], Section 6.2), explicitly reflect the natural variability of porewater compositions and implicitly reflect the natural variability of rock mineralogy. Summary tables of concentrations through time are presented in DTNs: LB0302DSCPTHCS.002 [DIRS 161976], LB0307DSTTHCR2.002 [DIRS 165541], and LB0311ABSTHCR2.003 [DIRS 166713], and summary statistics through time are presented in LB0311ABSTHCR2.001 [DIRS 166714]. These data are used to feed and/or provide technical basis for *Engineered Barrier System: Physical and Chemical Environment Model* (BSC 2004 [DIRS 169860]), which generates look-up tables used in the TSPA-LA model.

The effects of groundwater chemical characteristics are included in the radionuclide sorption coefficients under ambient conditions. The sorption coefficient data on which the distributions are based are obtained in laboratory experiments in which crushed rock samples from the Yucca Mountain site are contacted with groundwaters (or simulated groundwaters) representative of the site, spiked with one or more of the elements of interest (BSC 2004 [DIRS 164500], Sections A4 and A5). The chemistry of porewaters and perched waters in the UZ along potential flowpaths to the accessible environment is discussed in *Yucca Mountain Site Description* (BSC 2004 [DIRS 169734]). In the UZ, two distinct water types exist in the ambient system. One is perched water and the other is porewater. Perched water is generally more dilute than porewater. The J-13 and UE p#1 waters were used in sorption experiments as end-member compositions intended to bracket the impact of water composition on sorption coefficients (BSC 2004 [DIRS 164500], Section A4). Some spatial trends in water composition through the TSw and CHn geologic units have been noted (BSC 2003 [DIRS 169734], Section 5.2.2.4.2). However, the uncertainty in these spatial variations (BSC 2004 [DIRS 169856], Section 6.2.2.1) and the uncertainty with respect to the effects of the bounding water compositions on sorption (BSC 2004 [DIRS 164500], Sections A8.3, A8.4, and A8.9) have led to the treatment of natural variability in water composition as uncertainty. Sorption experiments have been carried out as a function of time, element concentration, atmospheric composition, particle size, and temperature. In some cases, the solids remaining from sorption experiments were contacted with unspiked groundwater in desorption experiments. The experimental data used to determine the sorption K_ds are provided in the following DTNs: LA0305AM831341.001 [DIRS 163789], LA0407AM831341.001 [DIRS 170623], LA0407AM831341.002 [DIRS 170621], LA0407AM831341.004 [DIRS 170622], LA0407AM831341.005 [DIRS 170625], LA0407AM831341.003 [DIRS 170626], LA0407AM831341.006 [DIRS 170628], and LA0310AM831341.001 [DIRS 165865]. The sorption and desorption experiments together provide information on the equilibration rates of the forward and backward sorption reactions.

For elements that sorb primarily through surface complexation reactions, the experimental data are augmented with the results of modeling calculations using PHREEQC (V2.3, STN: 10068-2.3-00) (BSC 2001 [DIRS 155323]). The inputs for the modeling calculations include groundwater compositions, surface areas, binding constants for the elements of interest, and thermodynamic data for solution species. These modeling calculations provide a basis for interpolation and extrapolation of the experimentally derived sorption coefficient dataset. The effects of nonlinear sorption are approximated by capturing the effective K_d range (BSC 2004 [DIRS 164500], Section A8).

The effects of groundwater composition with respect to sorption coefficients are provided in terms of probability distributions for the sorption coefficient of each element of interest among the three major rock types (devitrified, zeolitic, and vitric) found in the UZ. The influence of expected variations in water chemistry, radionuclide concentrations, and variations in rock surface properties within one of the major rock types are incorporated into these probability distributions. These distributions are specified for each radionuclide–rock type combination (BSC 2004 [DIRS 164500], Section I8) and are sampled in the TSPA-LA to account for the effects of natural variations in porewater chemistry and mineral surfaces on sorption. Correlations for sampling sorption coefficient probability distributions have been derived for the elements investigated (BSC 2004 [DIRS 164500], Appendix B). To derive the correlations, a rating system was first developed to rate the impact of six different variables on the sorption coefficient for a given element in each of the three major rock types. The six variables are pH, Eh, water chemistry, rock composition, rock surface area, and radionuclide concentration. Water chemistry refers to the major ion concentrations and silica. Rock composition refers to both the mineralogical composition of the rocks and the chemical composition of the minerals (for example, zeolite compositions). The output DTNs for the sorption K_ds and correlations are LA0408AM831341.001 [DIRS 171584] and LA0311AM831341.001 [DIRS 167015]. These K_ds, which include the effects of the chemical characteristics of groundwater, are used in the simulation of radionuclide transport for TSPA-LA, as described in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.5.4).

Supporting Reports: *Radionuclide Transport Models Under Ambient Conditions* (BSC 2004 [DIRS 164500]); *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]); *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]).

6.2.27 Re-dissolution of Precipitates Directs More Corrosive Fluids to Waste Packages (2.2.08.04.0A)

FEP Description: Re-dissolution of precipitates that have plugged pores as a result of evaporation of groundwater in the dry-out zone, may produce a pulse of fluid reaching the waste packages when gravity-driven flow resumes, which is more corrosive than the original fluid in the rock.

Screening Decision: Included.

TSPA Disposition: The THC seepage model simulations feeding *Post-Processing Analysis for THC Seepage* (BSC 2004 [DIRS 169858]) explicitly consider the formation of salt precipitates upon dryout (BSC 2004 [DIRS 169856], Sections 6.4.5 and 6.5.5.2) and their dissolution during

rewetting around drifts (BSC 2004 [DIRS 169856], Section 6.5.5.2) and the resulting effect on percolation water chemistry (BSC 2004 [DIRS 169858], Section 6.2.3; BSC 2004 [DIRS 169856], Section 6.4.4). Therefore, the results from the THC seepage model, and their abstraction in *Post-Processing Analysis for THC Seepage* (BSC 2004 [DIRS 169858], Section 6.2), explicitly reflect the effect of salt redissolution upon rewetting. The effect results in an increase in both salinity and variability (BSC 2004 [DIRS 169858], Section 6.2.3). Summary tables of concentrations through time are presented in DTNs: LB0302DSCPTHCS.002 [DIRS 161976], LB0307DSTTHCR2.002 [DIRS 165541], and LB0311ABSTHCR2.003 [DIRS 166713], and summary statistics through time are presented in LB0311ABSTHCR2.001 [DIRS 166714]. These data are used to feed and/or provide technical basis for *Engineered Barrier System: Physical and Chemical Environment Model* (BSC 2004 [DIRS 169860]), which generates look-up tables used in the TSPA-LA model.

Supporting Reports: *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]); *Post-Processing Analysis for THC Seepage* (BSC 2004 [DIRS 169858]).

6.2.28   Complexation in the UZ (2.2.08.06.0B)

FEP Description: Complexing agents such as humic and fulvic acids present in natural groundwaters could affect radionuclide transport in the UZ.

Screening Decision: Included.

TSPA Disposition: Complexation on mobile complexing agents such as humic and fulvic acids is treated as part of colloid transport in *Radionuclide Transport Models Under Ambient Conditions* (BSC 2004 [DIRS 164500], Sections 6.1.3 and 6.18). Complexation on mineral surfaces is treated as part of sorption in *Radionuclide Transport Models Under Ambient Conditions* (BSC 2004 [DIRS 164500], Section A7). Therefore, the effects of complexation are implicitly included in the radionuclide sorption coefficients under ambient conditions. For TSPA-LA, radionuclide transport is simulated by a particle-tracking model that includes the effects of complexation, as described in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.5.4).

The sorption coefficient data on which the distributions are based are obtained in laboratory experiments in which crushed rock samples from the Yucca Mountain site are contacted with groundwaters (or simulated groundwaters) representative of the site (BSC 2004 [DIRS 164500], Section A4), spiked with one or more of the elements of interest (BSC 2004 [DIRS 164500], Section A5). As such, the sorption experiments contain representative ligands responsible for complex formation, such as carbonates (Triay et al. 1997 [DIRS 100422], p. 85, 133). Sorption experiments have been carried out as a function of time, element concentration, atmospheric composition, particle size, and temperature. In some cases, the solids remaining from sorption experiments were contacted with unspiked groundwater in desorption experiments. The experimental data used to determine the sorption K_ds are provided in the following DTNs: LA0305AM831341.001 [DIRS 163789], LA0407AM831341.001 [DIRS 170623], LA0407AM831341.002 [DIRS 170621], LA0407AM831341.004 [DIRS 170622], LA0407AM831341.005 [DIRS 170625], LA0407AM831341.003 [DIRS 170626], LA0407AM831341.006 [DIRS 170628], and LA0310AM831341.001 [DIRS 165865]. The

sorption and desorption experiments together provide information on the equilibration rates of the forward and backward sorption reactions. For elements that sorb primarily through surface complexation reactions, the experimental data are augmented with the results of modeling calculations using PHREEQC V2.3 (BSC 2001 [DIRS 155323]). The inputs for the modeling calculations include groundwater compositions, surface areas, binding constants for the elements of interest, and thermodynamic data for solution species. These modeling calculations provide a basis for interpolation and extrapolation of the experimentally derived sorption coefficient dataset. The effects of nonlinear sorption are approximated by capturing the effective K_d range (BSC 2004 [DIRS 164500], Section A.8).

The effects of organics on sorption were also investigated by Triay et al. (1997 [DIRS 100422], Section IV.B). Their experiments tested the effects of organic materials (dihydroxyphenylalanine and Nordic Aquatic Fulvic Acid) on the sorption of Pu and Np on tuff materials. The results of these tests showed very little effect of the organic materials for sorption of these radionuclides in tuffs. The effects of complexation with respect to sorption coefficients are provided in terms of probability distributions for the sorption coefficient of each element of interest among the three major rock types (devitrified, zeolitic, and vitric) found in the UZ. The influence of expected variations in water chemistry, radionuclide concentrations, and variations in rock surface properties within one of the major rock types are incorporated into these probability distributions. These distributions are specified for each radionuclide–rock type combination (BSC 2004 [DIRS 164500], Section A8) and are sampled in the TSPA-LA to account for the effects of natural variations in porewater chemistry and mineral surfaces on sorption. Correlations for sampling sorption coefficient probability distributions have been derived for the elements investigated (BSC 2004 [DIRS 164500], Appendix B). To derive the correlations, a rating system was first developed to rate the impact of six different variables on the sorption coefficient for a given element in each of the three major rock types. The six variables are pH, Eh, water chemistry, rock composition, rock surface area, and radionuclide concentration. Water chemistry refers to the major ion concentrations and silica. Rock composition refers to both the mineralogic composition of the rocks and the chemical composition of the minerals (for example, zeolite compositions). The output DTNs for the sorption K_ds and correlations are LA0408AM831341.001 [DIRS 171584] and LA0311AM831341.001 [DIRS 167015].

Supporting Reports: *Radionuclide Transport Models Under Ambient Condition* (BSC 2004 [DIRS 164500]); *Particle Tracking Model and Abstraction of Transport Process* (BSC 2004 [DIRS 170041]).

6.2.29 Matrix Diffusion in the UZ (2.2.08.08.0B)

FEP Description: Matrix diffusion is the process by which radionuclides and other species transported in the UZ by advective flow in fractures or other pathways move into the matrix of the porous rock by diffusion. This includes osmotic processes in response to chemical gradients. Matrix diffusion can be a very efficient retarding mechanism, especially for strongly sorbed radionuclides, due to the increase in rock surface accessible to sorption.

Screening Decision: Included.

TSPA Disposition: Migration of radionuclides from fast flow fracture into surrounding slow flow matrix blocks by diffusion could play an important role in delaying the transport process of radionuclides in fractures. Scale dependency of matrix diffusion is analyzed in *Conceptual Model and Numerical Approaches for UZ Flow and Transport* (BSC 2004 [DIRS 170035], Section 6.2.2). The role of matrix diffusion is included through the development of the particle tracking approach as described in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.4.3). Transfer function curves (DTN: LA0311BR831229.001 [DIRS 166924]) that are generated are fed directly to TSPA-LA. These curves are used by FEHM in simulating the effect of matrix diffusion on radionuclide transport in TSPA-LA runs as described in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.4.3 and Appendix C). This particle tracking approach was used to simulate matrix diffusion of dissolved radionuclides. This treatment of matrix diffusion includes the effects of partial saturation of the matrix, radionuclide sorption in the matrix, and finite spacing of fractures. Osmosis would tend to cause water from fractures to flow into the matrix, if the matrix presents a suitable barrier to the migration of dissolved salts. Matrix diffusion of colloids was assumed not to occur because its effects would be small and would only retard transport (BSC 2004 [DIRS 170041], Section 6.4.5). Therefore, the approximation of no diffusion for colloids results in predictions that underestimate repository performance. One important factor affecting the strength of matrix diffusion is matrix diffusion coefficient. Matrix diffusion coefficient is related to matrix water content and matrix effective permeability through the relationship developed by Reimus et al. (2002 [DIRS 163008], Eq. 2.5). The distributions of matrix water content and matrix effective permeability are outputs from *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.5.5 and Table 6-6; DTN: LA0407BR831371.001 [DIRS 170806]). TSPA-LA uses these distributions in multiple realization runs to randomly generate matrix diffusion coefficients (DTN: LA0407BR831371.001 [DIRS 170806]. Related FEP 2.1.09.08.0A, Diffusion of dissolved radionuclides in EBS, is discussed in *Engineered Barrier System Features, Events, and Processes* (BSC 2004 [DIRS 169898], Section 6.2.51).

Supporting Reports: *Conceptual Model and Numerical Approaches for UZ Flow and Transport* (BSC 2004 [DIRS 170035]); *Particle Tracking Model and Abstraction of Transport Process* (BSC 2004 [DIRS 170041]).

6.2.30 Sorption in the UZ (2.2.08.09.0B)

FEP Description: Sorption of dissolved and colloidal radionuclides in the UZ can occur on the surfaces of both fractures and matrix in rock or soil along the transport path. Sorption may be reversible or irreversible, and it may occur as a linear or nonlinear process. Sorption kinetics and the availability of sites for sorption should be considered. Sorption is a function of the radioelement type, mineral type, and groundwater composition.

Screening Decision: Included.

TSPA Disposition: Sorption is identified in *Conceptual Model and Numerical Approaches for UZ Flow and Transport* (BSC 2004 [DIRS 170035], Section 6.2.3) as a process to be included in transport modeling. It is included in the TSPA-LA model for mountain-scale UZ radionuclide transport as a linear equilibrium sorption (K_d) model in *Radionuclide Transport Models Under*

Ambient Conditions (BSC 2004 [DIRS 164500], Section 6.1); K_d values and their basis in experimental data are presented in *Radionuclide Transport Models Under Ambient Conditions* (BSC 2004 [DIRS 164500], Appendix A). In TSPA-LA runs, sorption coefficients are sampled and fed into FEHM. Sorption onto fracture surfaces is neglected because of few data available in supporting such a retardation mechanism in the UZ. Thus, a fracture surface retardation factor of 1 is set for use in TSPA-LA runs (BSC 2004 [DIRS 170041], Section 6.5.8; DTN: LA0407BR831371.001 [DIRS 170806]).

Sorption is only accounted for in the matrix continuum; there is no sorption modeled in the fracture continuum. Sorption characteristics of the rock minerals are assumed to be static in time. Sorption K_ds have been derived for the elements Am, Cs, Np, Pa, Pu, Ra, Sr, Th, and U as dissolved radionuclides; other dissolved radionuclide elements treated by TSPA-LA (for example, Tc) are modeled as nonsorbing.

The sorption coefficient data on which the distributions are based are obtained in laboratory experiments in which crushed rock samples from the Yucca Mountain site are contacted with groundwaters (or simulated groundwaters) representative of the site, spiked with one or more of the elements of interest (BSC 2004 [DIRS 164500], Sections A4 and A5). Sorption experiments have been carried out as a function of time, element concentration, atmospheric composition, particle size, and temperature. In some cases, the solids remaining from sorption experiments were contacted with unspiked groundwater in desorption experiments. The experimental data used to determine the sorption K_ds are provided in the following DTNs: LA0305AM831341.001 [DIRS 163789], LA0309AM83341.002 [DIRS 170623], LA0309AM83341.003 [DIRS 170621], LA0309AM83341.004 [DIRS 170622], LA0309AM83341.005 [DIRS 170625], LA0309AM83341.006 [DIRS 170626], LA0309AM83341.007 [DIRS 170628], and LA0310AM831341.001 [DIRS 165865]. The sorption and desorption experiments together provide information on the equilibration rates of the forward and backward sorption reactions. For elements that sorb primarily through surface complexation reactions, the experimental data are augmented with the results of modeling calculations using PHREEQC V2.3 (BSC 2001 [DIRS 155323]). The inputs for the modeling calculations include groundwater compositions, surface areas, binding constants for the elements of interest, and thermodynamic data for solution species. These modeling calculations provide a basis for interpolation and extrapolation of the experimentally derived sorption coefficient dataset. The effects of nonlinear sorption are approximated by capturing the effective K_d range (BSC 2004 [DIRS 164500], Section I8).

Sorption coefficients are provided in terms of probability distributions for the sorption coefficient of each element of interest among the three major rock types (devitrified, zeolitic, and vitric) found in the UZ. The influence of expected variations in water chemistry, radionuclide concentrations, and variations in rock surface properties within one of the major rock types are incorporated into these probability distributions. These distributions are specified for each radionuclide–rock type combination (BSC 2004 [DIRS 164500], Section I8) and are sampled in the TSPA-LA to account for the effects of natural variations in porewater chemistry and mineral surfaces on sorption. Correlations for sampling sorption coefficient probability distributions have been derived for the elements investigated (BSC 2004 [DIRS 164500], Appendix B). To derive the correlations, a rating system was first developed to rate the impact of six different variables on the sorption coefficient for a given element in each of the three major rock types. The six variables are pH, Eh, water chemistry, rock composition, rock surface area, and

radionuclide concentration. Water chemistry refers to the major ion concentrations and silica. Rock composition refers to both the mineralogic composition of the rocks and the chemical composition of the minerals (for example, zeolite compositions). The output DTNs for the sorption K_ds and correlations are LA0408AM831341.001 [DIRS 171584] and LA0311AM831341.001 [DIRS 167015].

Sorption in the UZ is treated as a linear process in the radionuclide transport abstraction model (BSC 2004 [DIRS 170041], Section 6.5.4). In the matrix, sorption is incorporated in the generation of transfer function curves and expressed as part of the defined dimensionless parameters (BSC 2004 [DIRS 170041], Section 6.4.3). For colloid facilitated radionuclide transport, radionuclide sorption onto colloids and its effect on transport is simulated through the colloid K_c factor (BSC 2004 [DIRS 170041], Section 6.4.5). The K_c factor is the product of the radionuclide sorption coefficient onto colloids and the colloid concentration (BSC 2004 [DIRS 170041], Section 6.5.12). Radionuclide sorption coefficients that were used in the simulation of radionuclide transport in the UZ are documented in *Radionuclide Transport Models Under Ambient Conditions* (BSC 2004 [DIRS 170041], Section 6.5.4); the data are presented in DTN: LA0408AM831341.001 [DIRS 171584]). Colloid concentration and radionuclide sorption coefficients onto colloids are documented in *Waste Form and In-Drift Colloids-Associated Radionuclide Concentrations: Abstraction and Summary* (BSC 2004 [DIRS 170025], Section 6.3) and used in *Radionuclide Transport Models Under Ambient Conditions* (BSC 2004 [DIRS 170041], Section 6.5.12); the data are presented in DTNs: SN0306T0504103.005 [DIRS 164132] and SN0306T0504103.006 [DIRS 164131]). Sorption on colloids and resulting colloid transport are addressed in *Radionuclide Transport Models Under Ambient Conditions* (BSC 2004 [DIRS 164500], Sections 6.1.3 and 6.2.3), with simulation results presented in *Radionuclide Transport Models Under Ambient Conditions* (BSC 2004 [DIRS 164500], Section 6.18).

Supporting Reports: *Conceptual Model and Numerical Approaches for UZ Flow and Transport* (BSC 2004 [DIRS 170035]); *Radionuclide Transport Models Under Ambient Conditions* (BSC 2004 [DIRS 164500]); *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]).

6.2.31 Colloidal Transport in the UZ (2.2.08.10.0B)

FEP Description: Radionuclides may be transported in groundwater in the UZ as colloidal species. Types of colloids include true colloids, pseudo colloids, and microbial colloids.

Screening Decision: Included.

TSPA Disposition: Colloidal transport of radionuclides is identified in *Conceptual Model and Numerical Approaches for UZ Flow and Transport* (BSC 2004 [DIRS 170035], Section 6.2.4) as a process to be included in transport modeling. The influence of colloid transport on radionuclide migration through the UZ is implicitly included and discussed in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.4.5). *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]) provides a model for use in TSPA-LA, but does not generate a direct data feed to TSPA-LA pertaining to this FEP. Parameters that can impact colloid transport in the UZ include colloid

size (DTN: LL000122051021.116 [DIRS 142973]), colloid concentration (DTN: SN0306T0504103.005 [DIRS 164132]), radionuclide sorption coefficient onto colloid (DTN: SN0306T0504103.006 [DIRS 164131]), and colloid retardation factors (DTN: LA0303HV831352.002 [DIRS 163558]). The colloid concentration data and sorption-onto-colloid data are documented in *Waste Form and In-Drift Colloids-Associated Radionuclide Concentrations: Abstraction and Summary* (BSC 2004 [DIRS 170025], Section 6.3). Colloid retardation factors are documented in *Saturated Zone Colloid Transport* (BSC 2004 [DIRS 170006], Section 6.4.3). These data are used in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Sections 6.5.9 through 6.5.13). Colloid transport processes include advection and dispersion. In addition, colloids that undergo reversible filtration in fractures (BSC 2004 [DIRS 170041, Sections 6.4.5 and 6.5.9) are simulated through the use of the colloid retardation factor, R_c, which is evaluated based on field experiments in the C-Wells complex using microspheres as analogues. Field experiments have also shown that a small percentage of colloidal particles are transported through the groundwater system essentially unretarded (BSC 2004 [DIRS 170006], Section 6.6). The fractions of unretarded colloids have been developed based on field data (BSC 2004 [DIRS 170006]). Sorption of colloids is addressed in FEP 2.2.08.09.0B. Colloid matrix diffusion was assumed not to occur because its effect would be small and would only retard transport (BSC 2004 [DIRS 170041], Section 6.5.5). Therefore, the approximation of no diffusion for colloids will result in predictions that underestimate repository performance. In TSPA-LA runs, colloid facilitated radionuclide transport is investigated through the FEHM colloid transport model and variations of colloid transport parameters.

Supporting Reports: *Conceptual Model and Numerical Approaches for UZ Flow and Transport* (BSC 2004 [DIRS 170035]); *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]); *Saturated Zone Colloid Transport* (BSC 2004 [DIRS 170006])

6.2.32 Chemistry of Water Flowing into the Drift (2.2.08.12.0A)

FEP Description: Inflowing water chemistry may be used in analysis or modeling that requires initial water chemistry in the drift. Chemistry of water flowing into the drift is affected by initial water chemistry in the rock, mineral and gas composition in the rock, and thermal-hydrologic-chemical processes in the rock.

Screening Decision: Included.

TSPA Disposition: The THC seepage model was designed specifically to investigate the effect of thermal-hydrologic-chemical processes in the host rock (BSC 2004 [DIRS 169856], Section 6.2.1.2), including the effects of initial water chemistry (BSC 2004 [DIRS 169856], Section 6.2.2.1), and mineral and gas compositions in the rock (BSC 2004 [DIRS 169856], Section 6.2.2.2). Therefore, these effects are explicitly accounted for in the results from the THC seepage model, and their abstraction in *Post-Processing Analysis for THC Seepage* (BSC 2004 [DIRS 169858], Section 6.2). Summary tables of concentrations through time are presented in DTNs: LB0302DSCPTHCS.002 [DIRS 161976], LB0307DSTTHCR2.002 [DIRS 165541], and LB0311ABSTHCR2.003 [DIRS 166713], and summary statistics through time are presented in LB0311ABSTHCR2.001 [DIRS 166714]. These data are used to feed and/or provide technical

basis for *Engineered Barrier System: Physical and Chemical Environment Model* (BSC 2004 [DIRS 169860]), which generates look-up tables used in the TSPA-LA model. Because in the analysis of seepage water chemistry no water is predicted to actually seep into the modeled drift, the abstraction method was specifically designed to consider waters deemed most representative of potential in-drift seepage (BSC 2004 [DIRS 169858], Section 6.2.1; DTN: LB0311ABSTHCR2.001 [DIRS 166714]). The evaluation of seepage flow rates into the drifts is discussed in FEP 2.2.07.20.0A.

Supporting Reports: *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]); *Post-Processing Analysis for THC Seepage* (BSC 2004 [DIRS 169858]).

6.2.33 Microbial Activity in the UZ (2.2.09.01.0B)

FEP Description: Microbial activity in the UZ may affect radionuclide mobility in rock and soil through colloidal processes, by influencing the availability of complexing agents, or by influencing groundwater chemistry. Changes in microbial activity could be caused by the response of the soil zone to changes in climate.

Screening Decision: Included.

TSPA Disposition: The effects of microbes on sorption are included in the distributions for sorption coefficients used in TSPA-LA. The sorption coefficient data on which the distributions are based are obtained in laboratory experiments in which crushed rock samples from the Yucca Mountain site are contacted with groundwaters (or simulated groundwaters) representative of the site, spiked with one or more of the elements of interest (BSC 2004 [DIRS 164500], Section A5). These K_d values, which include the effects of microbial activity, are used in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.5.4).

The basic technique for the laboratory determination of sorption coefficients involved the contact of a groundwater sample, spiked with the radionuclide of interest, with a crushed sample of tuff or alluvium. The rock sample was generally obtained as a core sample. The rock and water samples were not sterilized and, therefore, contain representative microbial biota from the UZ. Sorption experiments have been carried out as a function of time, element concentration, atmospheric composition, particle size, and temperature. In some cases, the solids remaining from sorption experiments were contacted with unspiked groundwater in desorption experiments. The effects of microbial activity with respect to sorption coefficients are provided in terms of probability distributions for the sorption coefficient of each element of interest among the three major rock types (devitrified, zeolitic, and vitric) found in the UZ. The influence of expected variations in water chemistry, radionuclide concentrations, and variations in rock surface properties within one of the major rock types are incorporated into these probability distributions. These distributions are specified for each radionuclide–rock type combination (BSC 2004 [DIRS 164500], Section A8) and are sampled in the TSPA-LA to account for the effects of natural variations in porewater chemistry and mineral surfaces on sorption. Correlations for sampling sorption coefficient probability distributions have been derived for the elements BSC 2004 [DIRS 164500], Appendix B).

Supporting Reports: *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]); *Radionuclide Transport Models Under Ambient Conditions* (BSC 2004 [DIRS 164500]).

6.2.34   Natural Geothermal Effects on Flow in the UZ (2.2.10.03.0B)

FEP Description: The existing geothermal gradient, and spatial or temporal variability in that gradient, may affect groundwater flow in the UZ.

Screening Decision: Included.

TSPA Disposition: Natural geothermal effects are included in the models of thermal-hydrologic processes used to describe the effects of waste heat in the repository (BSC 2004 [DIRS 169866]) The initial and boundary temperature conditions represent the natural geothermal gradient (BSC 2004 [DIRS 169866], Section 6.1.3). This temperature profile is primarily determined by the ground surface temperature, the water table temperature, water flux through the UZ, and the thermal conductivity from layer to layer. Natural geothermal effects on unsaturated flow in the absence of repository thermal effects have been investigated in the models of natural thermal processes in the UZ (BSC 2004 [DIRS 169861], Section 6.3). The results of these models indicate that the effects of the natural temperature gradient on UZ flow are insignificant.

The natural geothermal gradient at Yucca Mountain is explicitly included in starting conditions of the TH seepage model in *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]) and thereby included in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.4.3). The natural geothermal gradient is also included in the THC seepage model in *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]), and in the abstraction of drift seepage (BSC 2004 [DIRS 169131], Section 6.4.4) by setting the ground surface temperature (top model boundary) and the temperature at the water table (bottom boundary) to measured values (BSC 2004 [DIRS 169856], Section 6.5.2). The effect of this temperature gradient on flow is explicitly accounted for by the coupled heat–flow transport algorithms implemented in the THC simulator (TOUGHREACT V3.0 LBNL 2002 [DIRS 161256]). Therefore, this effect is explicitly taken into account in the results of the THC seepage model; summary tables of concentrations through time submitted under DTNs: LB0302DSCPTHCS.002 [DIRS 161976], LB0307DSTTHCR2.002 [DIRS 165541], and LB0311ABSTHCR2.003 [DIRS 166713], and tables of concentrations and summary statistics through time submitted under DTN: LB0311ABSTHCR2.001 [DIRS 166714]). DTNs: LB0302DSCPTHCS.002 [DIRS 161976] and LB0311ABSTHCR2.001 [DIRS 166714] are used to feed and/or provide technical basis for *Engineered Barrier System: Physical and Chemical Environment Model* (BSC 2004 [DIRS 169860]), which generates look-up tables used in the TSPA-LA model.

Natural geothermal effects on unsaturated flow in the absence of repository thermal effects have been investigated in the models of natural thermal processes in the UZ (BSC 2004 [DIRS 169861], Section 6.3). The results of these models have found indicate that the effects of the natural temperature gradient on UZ flow are insignificant.

Supporting Reports: *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]); *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]); *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]); *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]).

6.2.35 Two-Phase Buoyant Flow/Heat Pipes (2.2.10.10.0A)

FEP Description: Heat from waste can generate two-phase buoyant flow. The vapor phase (water vapor) could escape from the mountain. A heat pipe consists of a system for transferring energy between a hot and a cold region (source and sink respectively) using the heat of vaporization and movement of the vapor as the transfer mechanism. Two-phase circulation continues until the heat source is too weak to provide the thermal gradients required to drive it. Alteration of the rock adjacent to the drift may include dissolution that maintains the permeability necessary to support the circulation (as inferred for some geothermal systems).

Screening Decision: Included.

TSPA Disposition: The coupled processes causing heat-pipe behavior (BSC 2004 [DIRS 169131], Section 6.3.2) are explicitly simulated with the TH seepage model (BSC 2004 [DIRS 170338]) that feeds into the seepage abstraction. Using this model, the impact of heat-pipe behavior on seepage is assessed for various simulation cases (BSC 2004 [DIRS 169131], Section 6.4.3.3) Thus, the TH-modeling results from DTN: LB0301DSCPTHSM.002 [DIRS 163689] inherently include the effect of heat pipes. As discussed in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.5.2), the abstraction of thermal seepage utilizes these modeling results to develop an appropriate thermal-seepage abstraction methodology.

The coupled processes causing heat-pipe behavior are explicitly simulated with the THC seepage model (BSC 2004 [DIRS 169856], Section 6.2.1.1). The continuous boiling and refluxing of water in this zone affects water–rock interactions (BSC 2004 [DIRS 169856], Section 6.2.1.2). The resulting water chemistry in the heat pipe is captured by the HISAT waters (BSC 2004 [DIRS 169858], Section 6.2.3; BSC 2004 [DIRS 169856], Section 6.5.5.2.2). Therefore, the effect of heat pipes on predicted water and gas chemistries is explicitly taken into account in the results of the THC seepage model and their abstraction (BSC 2004 [DIRS 169858], Section 6.2; summary tables of concentrations through time submitted under DTNs: LB0302DSCPTHCS.002 [DIRS 161976], LB0307DSTTHCR2.002 [DIRS 165541], and LB0311ABSTHCR2.003 [DIRS 166713]; and tables of concentrations and summary statistics through time submitted under DTN: LB0311ABSTHCR2.001 [DIRS 166714]). DTNs: LB0302DSCPTHCS.002 [DIRS 161976] and LB0311ABSTHCR2.001 [DIRS 166714] are used to feed and/or provide technical basis for *Engineered Barrier System: Physical and Chemical Environment Model* (BSC 2004 [DIRS 169860]), which generates look-up tables used in the TSPA-LA model.

Supporting Reports: *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]); *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]); *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338]).

6.2.36   Geosphere Dry-Out due to Waste Heat (2.2.10.12.0A)

FEP Description: Repository heat evaporates water from the UZ rocks near the drifts as the temperature exceeds the vaporization temperature. This zone of reduced water content (reduced saturation) migrates outward during the heating phase (about the first 1000 years) and then migrates back to the waste packages as heat diffuses throughout the mountain and the radioactive sources decay. This FEP addresses the effects of dry-out within the rocks.

Screening Decision: Included.

TSPA Disposition: The coupled processes of vaporization, dryout, and resaturation are explicitly simulated with the TH seepage model (BSC 2004 [DIRS 170338]) that feeds into the seepage abstraction. Using this model, the impact of such coupled processes on seepage is assessed for various simulation cases (BSC 2004 [DIRS 169131], Section 6.4.3.3). Thus, the TH-modeling results from DTN: LB0301DSCPTHSM.002 [DIRS 163689] inherently include these effects. As discussed in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.5.2), the abstraction of thermal seepage utilizes these modeling results to develop an appropriate thermal-seepage abstraction methodology.

The coupled processes of vaporization, dryout, and resaturation are explicitly simulated with the THC seepage model, including the formation of a dry (or nearly dry) zone around drifts, expanding and then receding through time following the pulse of heat released from the waste packages (BSC 2004 [DIRS 169856], Sections 6.2.1 and 6.5.5.1). Therefore, these effects are explicitly accounted for in the results from the THC seepage model, and in their abstraction in *Post-Processing Analysis for THC Seepage* (BSC 2004 [DIRS 169858], Section 6.2). Summary tables of concentrations through time are presented in DTNs: LB0302DSCPTHCS.002 [DIRS 161976], LB0307DSTTHCR2.002 [DIRS 165541], and LB0311ABSTHCR2.003 [DIRS 166713], and summary statistics through time are presented in LB0311ABSTHCR2.001 [DIRS 166714]. These data are used to feed and/or provide technical basis for *Engineered Barrier System: Physical and Chemical Environment Model* (BSC 2004 [DIRS 169860]), which generates look-up tables used in the TSPA-LA model. The effects of dryout on surface infiltration are discussed in FEP 2.2.10.01.0A.

Supporting Reports: *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856]); *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131]); *Drift-Scale Coupled Processes (DST and TH Seepage) Models* (BSC 2004 [DIRS 170338].

6.2.37   Topography and Morphology (2.3.01.00.0A)

FEP Description: This FEP is related to the topography and surface morphology of the disposal region. Topographical features include outcrops and hills, water-filled depressions, wetlands, recharge areas and discharge areas. Topography, precipitation, and surficial permeability distribution in the system will determine the flow boundary conditions (i.e., location and amount of recharge and discharge in the system).

Screening Decision: Included.

TSPA Disposition: Topographical features (such as hillslopes, washes, and ridges), precipitation, and surficial permeability distribution are included in *Simulation of Net Infiltration for Present-Day and Potential Future Climates* (BSC 2004 [DIRS 170007] Sections 6.5.3 and 6.6.1 and Appendix D), and are incorporated into the INFIL V2.0 (USGS 2001 [DIRS 139422]) model. Precipitation and surficial permeability distribution are also incorporated into the uncertainty analysis (*Analysis of Infiltration Uncertainty* (BSC 2003 [DIRS 165991]). Topography is also captured in INFIL V2.0 (USGS 2001 [DIRS 139422]; BSC 2004 [DIRS 170007]) model using data from the digital elevation model (DEM). The impacts of topography and morphology on preferential flow/percolation in the UZ is incorporated into the TSPA-LA through the UZ flow fields that use the infiltration model results (DTN: GS000308311221.005 [DIRS 147613]) as upper boundary conditions (*UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861], Section 6.1.4). Topographical features from GFM2000 [DIRS 153777] are captured in the UZ model grid developed in *Development of Numerical Grids for UZ Flow and Transport Modeling* (BSC 2004 [DIRS 169855]) and used in *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861], Section 6.1.1). The incorporation of UZ flow fields into the TSPA-LA is described in *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861], Section 6.2.5).

The effects of rock properties are also included in the treatment of infiltration uncertainty for TSPA-LA (*Analysis of Infiltration Uncertainty;* BSC 2003 [DIRS 165991]). Infiltration uncertainty is represented through three discrete infiltration scenarios (lower, mean, and upper), which are sampled in TSPA-LA according to weighting factors (BSC 2003 [DIRS 165991], Section 7.1). Precipitation and the surficial permeability distributions are captured in the uncertainty analysis using the precipitation multiplier (PRECIPM), the soil permeability multiplier (SOILPERM), and the effective bedrock permeability multiplier (BRPERM). They are incorporated implicitly by inclusion of uncertainty in the precipitation multiplier, soil permeability multiplier, and effective bedrock permeability multiplier in the calculation of the weighting factors, which are passed to TSPA-LA (BSC 2003 [DIRS 165991], DTN: SN0308T0503100.008 [DIRS 165640]).

Supporting Reports: *Development of Numerical Grids for UZ Flow and Transport Modeling* (BSC 2004 [DIRS 169855]); *Simulation of Net Infiltration for Present-Day and Potential Future Climates* (BSC 2004 [DIRS 170007]); *Analysis of Infiltration Uncertainty* (BSC 2003 [DIRS 165991]); *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]).

6.2.38 Precipitation (2.3.11.01.0A)

FEP Description: Precipitation is an important control on the amount of recharge. It transports solutes with it as it flows downward through the subsurface or escapes as runoff. Precipitation influences agricultural practices of the receptor. The amount of precipitation depends on climate.

Screening Decision: Included.

TSPA Disposition: Precipitation affects the net infiltration. Water balance, climate and snowpack are included in *Simulation of Net Infiltration for Present-Day and Potential Future Climate* (BSC 2004 [DIRS 170007], Section 6.4), and precipitation under future climates is

represented in *Simulation of Net Infiltration for Present-Day and Potential Future Climate* (BSC 2004 [DIRS 170007], Section 6.9). The net infiltration map outputs (DTN: GS000308311221.005 [DIRS 147613]) are used as a boundary condition for the UZ flow model (BSC 2004 [DIRS 169861], Sections 6.1.3 and 6.1.4). Flow fields developed for use in TSPA-LA (DTN: LB0305TSPA18FF.001 [DIRS 165625]) using the UZ flow model, therefore, include the effects of precipitation and changes of precipitation under future climate conditions, including low, mean, and upper bounds of infiltrations in glacial, monsoon, and present-day (or modern) climatic scenarios.

The effects of precipitation are also included in the treatment of infiltration uncertainty for TSPA-LA (*Analysis of Infiltration Uncertainty*, BSC 2003 [DIRS 165991]). Infiltration uncertainty is represented through three discrete infiltration scenarios (lower, mean, and upper), which are sampled in TSPA-LA according to weighting factors (BSC 2003 [DIRS 165991], Section 7.1). Precipitation is incorporated in the infiltration uncertainty analysis through the precipitation-rate multiplier (PRECIPM) (BSC 2003 [DIRS 165991], Table 6-3 and Section 6.1.2). PRECIPM operates on the precipitation rate, as prescribed in the input file TULELAKE.INP, which contains the precipitation record for the selected "mean glacial transition-climate" analogue site, within the infiltration model software, INFIL VA_2.a1 (SNL 2001 [DIRS 147608]) and INFIL V2.0 (USGS 2001 [DIRS 139422]).

Supporting Reports: *Simulation of Net Infiltration for Present-Day and Potential Future Climates* (BSC 2004 [DIRS 170007]); *Analysis of Infiltration Uncertainty* (BSC 2003 [DIRS 165991]); *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]).

6.2.39 Surface Runoff and Flooding (2.3.11.02.0A)

FEP Description: Surface runoff and evapotranspiration are components in the water balance, together with precipitation and infiltration. Surface runoff produces erosion, and can feed washes, arroyos, and impoundments, where flooding may lead to increased recharge.

Screening Decision: Included.

TSPA Disposition: Evapotranspiration and surface runoff affect the net infiltration, as discussed in *Simulation of Net Infiltration for Present-Day and Potential Future Climates* (BSC 2004 [DIRS 170007], Section 6.4). The net infiltration map outputs (DTN: GS000308311221.005 [DIRS 147613]) are used as a boundary condition for the UZ flow model (BSC 2004 [DIRS 169861], Sections 6.1.3 and 6.1.4). Flow fields developed for use in TSPA-LA (DTN: LB0305TSPA18FF.001 [DIRS 165625]) using the UZ flow model, therefore, include the effects of precipitation and changes of precipitation under future climate conditions, including low, mean, and upper bounds of infiltrations in glacial, monsoon, and present-day (or modern) climatic scenarios.

The effects of evapotranspiration are included in the treatment of infiltration uncertainty for TSPA-LA (BSC 2003 [DIRS 165991]). Infiltration uncertainty is represented through three discrete infiltration scenarios (lower, mean, and upper), which are sampled in TSPA-LA according to weighting factors in *Analysis of Infiltration Uncertainty* (BSC 2003 [DIRS 165991], Section 7.1). Evapotranspiration is incorporated in the infiltration uncertainty analysis through the two evapotranspiration coefficient-rate multipliers ETCOEFFA and ETCOEFFB (BSC 2003

[DIRS 165991], Table 6-3 and Section 6.1.2.). The evapotranspiration-rate multiplier POTETMUL operates on the evapotranspiration rate, as calculated within the infiltration model software, INFIL VA_2.a1 (SNL 2001 [DIRS 147608]) (and also INFIL V2.0; USGS 2001 [DIRS 139422]). Surface runoff is incorporated through the inclusion of a parameter (FLAREA) that defines the fraction of each grid cell in the infiltration model that is affected by overland flow and channel flow during the routing of runoff. It is incorporated implicitly by inclusion of uncertainty in the fraction of each grid cell in the infiltration model that is affected by overland flow and channel flow during the routing of runoff in the calculation of the weighting factors that are passed to TSPA-LA (BSC 2003 [DIRS 165991] and DTN: SN0308T0503100.008 [DIRS 165640]).

Supporting Reports: *Simulation of Net Infiltration for Present-Day and Potential Future Climates* (BSC 2004 [DIRS 170007]); *Analysis of Infiltration Uncertainty* (BSC 2003 [DIRS 165991]); *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]).

6.2.40 Infiltration and Recharge (2.3.11.03.0A)

FEP Description: Infiltration into the subsurface provides a boundary condition for groundwater flow. The amount and location of the infiltration influences the hydraulic gradient and the height of the water table. Different sources of recharge water could change the composition of groundwater passing through the repository. Mixing of these waters with other groundwaters could result in precipitation, dissolution, and altered chemical gradients.

Screening Decision: Included.

TSPA Disposition: The hydrological effects of infiltration and recharge are included in the infiltration model (FEP 1.3.01.00.0A). This model includes the effects of seasonal and climate variations, climate change, surface-water runoff, and site topography such as hillslopes and washes to simulate the spatial distribution of infiltration as described in *Simulation of Net Infiltration for Present-Day and Potential Future Climates* (BSC 2004 [DIRS 170007], Section 6.11). The time dependence of infiltration results is linked to the timing of climate change as discussed in Section 6.2.4; FEP 1.3.01.00.0A. This is incorporated into the TSPA-LA through the UZ flow fields that use the infiltration model results (DTN: GS000308311221.005 [DIRS 147613]) as upper boundary conditions (BSC 2004 [DIRS 169861], Section 6.1.4). Flow fields for TSPA-LA are in DTN: LB0305TSPA18FF.001 [DIRS 165625]. Data for calibrating the infiltration model were acquired in experiments at Alcove 1, as reported in *In Situ Field Testing of Processes* (BSC 2004 [DIRS 170004], Section 6.12).

The effects of present-day water composition infiltrating from the ground surface are accounted for in the analysis of seepage-water chemistry by using the measured porewater chemistry in the UZ (BSC 2004 [DIRS 169856], Table 6.2-1). However, porewater chemistry varies by hydrologic unit (BSC 2004 [DIRS 169856], Figure 6.2-4). Variation in the quality of infiltrating water is dominated by rock–water interaction.

Infiltration uncertainty, as it applies to the determination of weighting factors used in TSPA-LA (DTN: SN0308T0503100.008 [DIRS 165640]), is documented in *Analysis of Infiltration Uncertainty* (BSC 2003 [DIRS 165991]. The way it is handled is summarized in *Analysis of Infiltration Uncertainty* (BSC 2003 [DIRS 165991], Section 1.1). TSPA-LA has included three

distinct climate regimes in the comprehensive repository performance analysis for Yucca Mountain: present-day, monsoon, and glacial-transition. Each climate regime was characterized using three infiltration-rate maps, including a lower- and upper-bound and a mean value (equal to the average of the two boundary values). For each of these maps, which were obtained based on analogue site climate data, a spatially averaged value was also calculated. For a more detailed discussion of these infiltration-rate maps, see *Simulation of Net Infiltration for Present-Day and Potential Future Climates* (BSC 2004 [DIRS 170007]). Spatially averaged values were calculated for the lower-bound, mean, and upper-bound climate analogues only for the glacial transition climate regime, within the simulated multirectangular region approximating the repository footprint, shown in *Analysis of Infiltration Uncertainty* (BSC 2003 [DIRS 165991], Figure 1-1).

Supporting Reports: *Simulation of Net Infiltration for Present-Day and Potential Future Climates* (BSC 2004 [DIRS 170007]); *Analysis of Infiltration Uncertainty* (BSC 2003 [DIRS 165991]); *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861]); *In Situ Field Testing of Processes* (BSC 2004 [DIRS 170004]).

6.2.41 Radioactive Decay and Ingrowth (3.1.01.01.0A)

FEP Description: Radioactivity is the spontaneous disintegration of an unstable atomic nucleus that results in the emission of subatomic particles. Radioactive isotopes are known as radionuclides. Radioactive decay of the fuel in the repository changes the radionuclide content in the fuel with time and generates heat. Radionuclide quantities in the system at any time are the result of the radioactive decay and the growth of daughter products as a consequence of that decay (i.e., ingrowth). Over a 10,000-year performance period, these processes will produce daughter products that need to be considered in order to adequately evaluate the release and transport of radionuclides to the accessible environment.

Screening Decision: Included.

TSPA Disposition: Decay and ingrowth are implicitly included through the development of an effective integration algorithm described in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.4.4). This algorithm can handle multiple species decay and ingrowth processes. Radionuclide half lives and daughter products considered in the UZ transport abstraction model are documented in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Section 6.5.14). In TSPA-LA runs, 36 species of radionuclides are simulated through the UZ using the FEHM (V2.21; LANL 2003 [DIRS 165741]) decay/ingrowth model over a specified time period as described in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Sections 6.4.4 and 6.5.14). *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]) provides a model for use in TSPA-LA, but does not generate a direct data feed to TSPA-LA pertaining to this FEP. The output of the UZ radionuclide transport model is a boundary condition for the SZ radionuclide transport model, which accounts for decay and ingrowth during radionuclide transport as described in *Saturated Zone Flow and Transport Model Abstraction* (BSC 2004 [DIRS 170042], Section 6.3).

Supporting Reports: *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041]).

6.3   BOREHOLE SEALS AND REPOSITORY DRIFT SEALS

These excluded FEPs concern the effects of boreholes and repository drifts as pathways for fluid and radionuclide migration.   The implicit treatment of boreholes in the TSPA-LA is that boreholes are sealed so that the borehole region is indistinguishable from the natural rock in terms of fluid flow and radionuclide transport.   However, the specific properties of the seals and their evolution over time are not accounted for in the flow and transport modeling.   Similarly, repository drifts will be assumed to be sealed such that liquids or gases cannot migrate between emplacement drifts (other than through geosphere pathways).   Arguments are presented here to demonstrate that the potential effects of borehole seal or repository seal leakage have a negligible effect on the potential performance of the repository.   Therefore, these FEPs are excluded from the TSPA-LA calculation, based on low consequence.

Table 6-3 gives the FEP numbers and names categorized under borehole and repository seals.

Table 6-3.   Excluded FEPs: Repository Seals and Borehole Seals

Section Number	FEP Number	FEP Name
6.3.1	1.1.01.01.0A	Open site investigation boreholes
6.3.2	1.1.01.01.0B	Influx through holes drilled in drift wall or crown
6.3.3	1.1.02.01.0A	Site flooding (during construction and operation)
6.3.4	1.1.04.01.0A	Incomplete closure
6.3.5	1.1.11.00.0A	Monitoring of the repository
6.3.6	2.1.05.01.0A	Flow through seals (access ramps and ventilation shafts)
6.3.7	2.1.05.02.0A	Radionuclide transport through seals
6.3.8	2.1.05.03.0A	Degradation of seals

Source: DTN: MO0407SEPFEPLA.000 [DIRS 170760].

6.3.1   Open Site Investigation Boreholes (1.1.01.01.0A)

FEP Description: Site investigation boreholes that have been left open, degraded, improperly sealed, or reopened, could modify flow and transport properties and produce enhanced pathways between the surface and the repository.

Screening Decision: Excluded–Low Consequence

Screening Argument: The implicit treatment of boreholes in the TSPA-LA is that boreholes are sealed so that the borehole region is indistinguishable from the natural rock in terms of fluid flow and radionuclide transport. However, the specific properties of the seals and their evolution over time are not accounted for in the flow and transport modeling. Similarly, repository drifts will be assumed to be sealed such that liquids or gases cannot migrate between emplacement drifts (other than through geosphere pathways).

The consequence of site-investigation boreholes depends on several factors, such as location and depth of the boreholes. The following arguments demonstrate that, based on a number of factors and considerations, the existing test boreholes will not have a significant impact on either radionuclide transport or the performance of the repository.

Only boreholes within or close to the repository block are important to the performance of the UZ.   Boreholes well outside the footprint of the repository block will not influence water

movement to the waste emplacement drifts or radionuclide transport from the waste emplacement drifts to the water table. Table 6-4 lists 8 deep boreholes in the repository block and 7 deep boreholes near the repository block. The definition for deep borehole in the repository block is a borehole that penetrates the TSw. The definition for deep borehole near the repository block is a borehole that penetrates below the elevation of waste emplacement (DTNs: MO9906GPS98410.000 [DIRS 109059], MO0004QGFMPICK.000 [DIRS 152554], and *D&E/PA/C IED Subsurface Facilities* (BSC 2004 [DIRS 164519]). Boreholes that terminate in or above the PTn will have a negligible effect on percolation flux at the repository because flow through these boreholes will tend to be homogenized by matrix flow in the underlying Paintbrush nonwelded hydrogeologic unit (*UZ Flow Models and Submodels*, BSC 2004 [DIRS 169861], Appendix G; DTN: LB0408RITSSCPF.001 [DIRS 171593]; CRWMS M&O 1998 [DIRS 100356], Section 2.4.2.8; Wu et al. 2000 [DIRS 154918], Section 4.1). The locations of the boreholes listed in Table 6-4 relative to waste emplacement locations are shown in *D&E/PA/C IED Subsurface Facilities* (BSC 2004 [DIRS 168180]).

Many of the boreholes penetrate the UZ entirely and terminate at or below the water table. Based on the design layout (BSC 2004 [DIRS 164519]) and borehole locations in Table 6-4, none of the existing boreholes will intersect with a waste emplacement drift. Therefore, water entering these boreholes would continue to flow through these boreholes to the water table, bypassing waste emplacement locations. One of the deep boreholes within the waste emplacement footprint, USW UZ-1, only partially penetrates the UZ. USW UZ-1 has a total depth of 1,270 ft, but terminates near the TSw vitrophyre beneath waste emplacement locations. Therefore, none of the deep boreholes in the repository block terminates above potential waste emplacement locations. In the event that a drift unexpectedly encounters a borehole during repository construction, such boreholes will either be sealed or waste packages will have a stand-off distance from the location of the borehole penetration into the waste emplacement drift, or both.

The other aspect of this problem is the movement of dissolved radionuclides and radionuclides associated with mobile colloids between the repository and the water table. Fractures and faults represent continuous rapid-transport pathways from the repository to the water table. Any significant lateral flow beneath the repository eventually finds one of these high-permeability pathways to the water table. The principal difference between these high-permeability pathways and boreholes is that the cross-sectional area of the boreholes available to intercept lateral flow is much smaller than the area associated with fractures and faults. The 15 boreholes in Table 6-4 with depths greater than 1,000 ft present a total cylindrical area (available to intercept lateral flow) per unit depth that may be calculated by the product of the borehole diameter times the number of boreholes. The average borehole diameter is bounded by a value of 1 m (Table 6-4), given that borehole diameters can exceed the size of the drill bit. This gives a total borehole sidewall area per unit depth of 15π m^2/m. The fractured rock between the repository and the water table has a fracture area per unit volume of 0.1 m^{-1} or more (BSC 2004 [DIRS 170038], Table 6-5). Multiplying this by the 5×10^6 m^2 footprint of the repository (BSC 2004 [DIRS 168370]) gives a minimum fracture area per unit depth of about 5×10^5 m^2/m. Therefore, the contribution of boreholes to the steady state flow and transport pattern between the repository and the water table is negligible. A potential scenario that could lead to greater radionuclide releases is the migration of perched water through the borehole pathways if a borehole seal should fail.

Table 6-4. Deep Boreholes in or Close to the Repository Block

Borehole Identifier	Surface Elevation (feet)	Lowest Stratigraphic Contact Depth (feet)[16] (except as noted)	Tptpv3[‡] Depth (feet)[16] (except as noted)	Nominal Borehole Diameter (inches)[†]	NSP Easting (feet)	NSP Northing (feet)
UE-25 WT #18**	4,384	1,620	1,501	8.75[1]	564,854	771,167
USW G-1*	4,350	3,558	1,287	3.875[2]	561,001	770,502
USW G-4**	4,166	2,950	1,317	12.25[3]	563,082	765,808
USW H-1*	4,274	3,661	1,410	13.25[4]	562,388	770,255
USW H-5*	4,851	3,422	1,582	14.75[5]	558,908	766,634
USW NRG-7a**	4,207	1,498	1,415	5.5[6]	562,984	768,880
USW SD-7*	4,472	2,612	1,182	8.75[7]	561,240	758,950
USW SD-9*	4,273	2,016	1,358	8.5[8]	561,818	767,998
USW SD-12*	4,343	2,138	1,278	12.25[9]	561,606	761,957
USW UZ-1*	4,425	1,145	979[17]	17.5[10]	560,222	771,277
USW UZ-6**	4,925	1,829	1,333	17.5[11]	558,325	759,730
USW UZ-7a**	4,228	759[18]	629[17]	12.25[12]	562,270	760,693
USW UZ-14*	4,425	2,072	1,279	12.25[13]	560,142	771,310
USW WT-2**	4,268	1,794	1,179	8.75[14]	561,924	760,662
USW SD-6**	4,905[20]	2,506[19]	1,456[19]	12.25[15]	558,608[20]	762,421[20]

NOTE: DTN: MO9906GPS98410.000 [DIRS 109059] except where other source noted; NSP easting and northing and elevation values have been rounded to the nearest foot.

NSP = Nevada State Plane.

*In repository block .
**close to repository block .
[†]based on drill bit size used to create borehole in the repository host rock .
[‡]Top contact of Tptpv3, or lower contact of Tptpln (BSC 2004 [DIRS 169855]). Tptpln is the lowest stratigraphic unit that was identified for waste emplacement (BSC 2004 [DIRS 168370]).
[1] Fenix and Scisson (1986 [DIRS 101238], p. 63).
[2] Fenix and Scisson (1987 [DIRS 103102], p. 3).
[3] Fenix and Scisson (1987 [DIRS 103102], p. 109).
[4] Fenix and Scisson (1987 [DIRS 126415], p. 3).
[5] Fenix and Scisson (1987 [DIRS 126415], p. 51).
[6] DTN: TMUSWNRG7A0096.002 ([DIRS 166424], MOL.19971023.0323, Attachment VII).
[7] CRWMS M&O (1996 [DIRS 129957], p. 13).
[8] CRWMS M&O (1996 [DIRS 114799], p. 11).
[9] DTN: TM000000SD12RS.012 ([DIRS 105627], p. 9).
[10] Fenix and Scisson (1987 [DIRS 165939], p. 3).
[11] Fenix and Scisson (1987 [DIRS 165939], p. 35).
[12] CRWMS M&O (1996 [DIRS 130425], p. 2).
[13] CRWMS M&O (1996 [DIRS 130429], p. 9).
[14] Fenix and Scisson (1986 [DIRS 101238], p. 75).
[15] YMP (1999 [DIRS 166080], Attachment 8).
[16] DTN: MO0004QGFMPICK.000 [DIRS 152554], note that borehole UE-25 WT#18 is designated as USW WT#18 in this DTN.
[17] nearest repository waste emplacement depth, also uses information from BSC 2004 [DIRS 164519] and 800-IED-WIS0-00104-000-00A (BSC 2004 [DIRS 168180]).
[18] maximum depth of borehole data, DTN: MO0010CPORGLOG.003 [DIRS 155959].
[19] DTN: SNF40060298001.001 [DIRS 107372].
[20] DTN: MO9912GSC99492.000 [DIRS 165922].

A bounding calculation was performed that assessed the potential for radionuclides in the perched water to be suddenly released to the water table (Appendix A; FEP 2.2.06.03.0A). The calculation considers the volume of perched water contained in the fractures to be available for rapid release. This volume is restricted to fractures with permeability greater than 1 millidarcy. In no case (of the nine UZ flow scenarios) does this volume represent more than three months of percolation flux. Therefore, the potential effects of these boreholes on flow and percolation in the UZ or as preferential pathways for radionuclide transport, even if the borehole seals should fail completely, are negligible. It follows that any effects on repository performance are negligible, given that these are the factors associated with boreholes that could affect repository performance.

Test boreholes drilled in the underground facility are all relatively short (they remain within the TSw hydrogeologic unit) and are only present in access and observation drifts, not in the waste emplacement drifts (FEP 1.1.01.01.0B). Therefore, these boreholes will not have any significant effect on radionuclide transport between the repository and the water table. This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.3.2 Influx through Holes Drilled in Drift Wall or Crown (1.1.01.01.0B)

FEP Description: Holes may be drilled through the drift walls or crown for a variety of reasons including, but not limited to, rock bolt and ground support, monitoring and testing, or construction related activities. These openings may promote flow or seepage into the drifts and onto the waste packages.

Screening Decision: Excluded–Low Consequence.

Screening Argument: Detailed simulations were made using the predictive seepage model for PA (*Seepage Model for PA Including Drift Collapse*, BSC 2004 [DIRS 167652], Section 6.5) to study the effect of rock bolts in the drift crown. In a sensitivity analysis, several combinations of capillarity and permeability were examined, including cases representing both grouted and ungrouted rock bolts and an open hole. These features were found to have only a minor effect on seepage (less than 2 percent according to *Seepage Model for PA Including Drift Collapse* (BSC 2004 [DIRS 167652], Table 6-4), due to the small area for water to enter the boreholes from the surrounding formation (BSC 2004 [DIRS 169131], Section 6.4.2.5). These conclusions are not dependent on the activity that creates a hole in the drift wall or crown (that is, ground support, monitoring, testing, or construction activities). From these results, the presence of holes drilled in drift wall or crown is not considered significant for seepage into drifts. This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.3.3 Site Flooding (During Construction and Operation) (1.1.02.01.0A)

FEP Description: Flooding of the site during construction and operation could introduce water into the underground tunnels, which could affect the long-term performance of the repository.

Screening Decision: Excluded–Low Consequence.

Screening Argument: This FEP describes an issue related to preclosure operations. Areas that would be inundated in the probable maximum flood in the vicinity of the north portal pad were calculated in *Preliminary Hydrologic Engineering Studies for the North Portal Pad and Vicinity* (BSC 2002 [DIRS 157928], Figures 17 through 19). These maps show that flooding is not expected to reach the main portals of the Exploratory Studies Facility or the intake and exhaust shafts. Design requirements also address the issue of surface water inundation of subsurface facilities (BSC 2004 [DIRS 171676], Sections 3.1.1.13.1 through 3.1.1.13.3). Very little of the flood zone overlies waste emplacement zones. A small region of the expected flood zone overlies the repository footprint in the upper part of Drill Hole Wash (DTN: MO0004YMP98132.004 [DIRS 149806]). Boreholes USW NRG-7a, USW G-1, and USW H-1 lie close to or within the potential flood zone of Drill Hole Wash, which overlies the repository footprint (DTN: MO0011YMP00114.000 [DIRS 171565]). As discussed for FEP 1.1.01.01.0A (Section 6.3.1), if water should enter these boreholes, it is not expected to enter waste emplacement locations. Flooding during storm events is not unusual and leads to infiltration and runoff. The effects of flooding are addressed in the infiltration model (FEP 2.3.11.02.0A). This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.3.4 Incomplete Closure (1.1.04.01.0A)

FEP Description: Disintegration of society could result in incomplete closure, sealing, and decommissioning of the disposal vault.

Screening Decision: Excluded – Low Consequence and By Regulation

Screening Argument: This FEP is similar in content to the ones discussed in Sections 6.3.1 (FEP 1.1.01.01.0A) and 6.3.6 (FEP 2.1.05.01.0A). In these FEPs, the effects of boreholes on water movement between the surface and the repository and transport of radionuclides between the repository and the water table were argued to be negligible. Also, the effects of short test boreholes drilled in the underground test facility were found (FEP 1.1.01.01.0A) to be negligible with respect to repository performance. The effects of drift seals on water or gas movement through the drifts were also assessed (FEP 2.1.05.01.0A) to have a negligible effect on repository performance under nominal case performance modeling. With regard to sealing of the access portals, *Preliminary Hydrologic Engineering Studies for the North Portal Pad and Vicinity* (BSC 2002 [DIRS 157928], Figures 17 through 19) shows that flooding is not expected to reach the main portals of the Exploratory Studies Facility or the intake and exhaust shafts (at least under present-day climate), even if not sealed. This FEP is, therefore, excluded because it will

not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance. 10 CFR 63.305(b) [DIRS 156605] specifies that "DOE should not project changes to society..." This FEP is predicated on an assumption of a disintegration of society (i.e., a projected change) and is, therefore, also excluded by regulation.

Supporting Reports: Not applicable.

6.3.5 Monitoring of the Repository (1.1.11.00.0A)

FEP Description: Monitoring that is carried out during or after operations, for either operational safety or verification of long-term performance, has the potential to detrimentally affect long-term performance. For example, monitoring boreholes could provide enhanced pathways between the surface and the repository.

Screening Decision: Excluded–Low Consequence.

Screening Argument: This FEP is similar to the ones discussed in Sections 6.3.1 (FEP 1.1.01.01.0A), 6.3.2 (FEP 1.1.01.01.0B), and 6.3.6 (FEP 2.1.05.01.0A). The effect of rock-bolt boreholes drilled in the drift wall or crown was analyzed (BSC 2004 [DIRS 167652], Section 6.5) and found to increase seepage less than 2 percent (BSC 2004 [DIRS 167652], Table 6-4). The effects of repository drift seals on water or gas movement through the drifts were also assessed (FEP 2.1.05.01.0A) to have a negligible effect on repository performance. Therefore, this FEP is excluded on the basis of low consequence. These conclusions are not dependent on the activity that creates a hole in the drift wall or crown (i.e. ground support, monitoring, testing, or construction activities).

Planned UZ monitoring activities, including testing of transport properties and field sorptive properties of the host rock, are described in *Performance Confirmation Plan* (BSC 2004 [DIRS 170505], Section 3.3.1.4). These activities began during site characterization and will continue during construction and emplacement. They are not expected to adversely affect the ability of the repository to meet performance objectives because the alcoves and drilling to obtain samples is very limited and occurs in a very small portion of the repository. Planned geotechnical and construction effects monitoring activities, including subsurface mapping, and instrumenting mined openings to detect construction deformation, are described in *Performance Confirmation Plan* (BSC 2004 [DIRS 170505], Section 3.3.2). These activities also are not expected to adversely affect the ability of the repository to meet performance objectives because the instrumentation is very small and covers an insignificant portion of the rock in the repository. This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Other activities associated with performance confirmation are given in *Performance Confirmation Plan* (BSC 2004 [DIRS 170505], Section 5). These include air permeability and gas and liquid tracer tests prior to waste emplacement and monitoring, sampling, and laboratory testing of condensation water quantities, composition, and ionic characteristics, including microbial effects, from a thermally accelerated emplacement drift. These activities do not present any disturbance greater than the creation of test boreholes or other similar activities conducted during site characterization.

Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.3.6   Flow through Seals (Access Ramps and Ventilation Shafts) (2.1.05.01.0A)

FEP Description: Long-term fluid flow through the shaft seal system, and uncertainty about long-term properties of the shaft seal system, may influence cumulative radionuclide releases from the disposal system.

Screening Decision: Excluded–Low Consequence.

Screening Argument: The host rock in the repository is highly fractured; hence seals for repository access drifts are of little consequence for water movement in the repository environment.   There is only a small driving force for water to move along the relatively horizontal access drifts or emplacement drifts. Water is expected to move in a general vertical flow pattern through the waste emplacement horizon relative to the length scale of these drifts, with some flow diversion around the drifts caused by the capillary barrier effect. This flow pattern is consistent with the drift-scale seepage model having no-flow lateral boundary conditions (BSC 2004 [DIRS 167652], Section 6.3.1). The ventilation shafts connect to access drifts at the waste emplacement level and, therefore, represent pathways for water to enter the waste emplacement drifts. For postclosure, the ventilation shafts will be backfilled. The hydrogeologic effects of ventilation shafts provide high-permeability pathways similar to smaller fault features with respect to flow from the surface to the repository. The design for the shafts will account for the effects of flooding (BSC 2004 [DIRS 171676], Sections 3.1.1.13.1 through 3.1.1.13.3). Therefore, the quantity of water available to flow through the ventilation shafts is limited to rainfall and should not exceed infiltration that occurs in smaller fault features. Although fault features are suspected pathways for rapid migration of water from the surface to the repository (as observed from ^{36}Cl measurements), the amount of water that can bypass matrix flow in the Paintbrush nonwelded hydrogeologic unit is a only a small fraction (generally less than 5 percent in fault zones) of the total infiltration, based on transport calculations for ^{36}Cl between the ground surface and the repository horizon, which show 5 percent breakthrough at several hundred years (BSC 2004 [DIRS 169861], Figure H-2). Similarly, flow through the backfilled ventilation shafts is expected to have a large component of matrix flow, greatly reducing the amount of transient water pulses penetrating from the surface to the waste emplacement drifts, regardless of the specific characteristics or evolution of the backfill over time. Therefore, the effect of the ventilation shafts on flow from the surface to the repository is negligible. Gas flow could potentially move through the drifts, so drift seals could affect the nature of this flow. However, the fractured nature of the host rock ensures that gas will be able to move between drifts if there is a driving force for this flow pattern. Given these conditions, the seals in the repository access drifts and ventilation shafts are expected to have very little effect on the movement of gas or water in the repository environment and, therefore, have little effect on repository performance.   This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

The effects of borehole seal failure can also be excluded on the basis of low consequence, as discussed in FEP 1.1.01.01.0A.

Supporting Reports: Not applicable.

6.3.7 Radionuclide Transport through Seals (2.1.05.02.0A)

FEP Description: Groundwater flow through seals in the access ramps, ventilation shafts, and exploratory boreholes could affect long-term performance of the disposal system. Radionuclide transport through seals should be considered.

Screening Decision: Excluded–Low Consequence.

Screening Argument: This FEP is similar in content to the ones discussed in Sections 6.3.1 (FEP 1.1.01.01.0A) and 6.3.6 (FEP 2.1.05.01.0A). The host rock in the repository is highly fractured; hence seals for ramps, ventilation shafts, and exploratory boreholes are of little consequence for water movement in the repository environment. The ventilation shafts connect to access drifts at the waste emplacement level and, therefore, represent pathways for water to enter the waste emplacement drifts. For postclosure, the ventilation shafts will be backfilled. The hydrogeologic effects of ventilation shafts provide high-permeability pathways similar to smaller fault features with respect to flow from the surface to the repository. The design for the shafts will account for the effects of flooding (BSC 2004 [DIRS 171676], Sections 3.1.1.13.1 through 3.1.1.13.3). Therefore, the quantity of water available to flow through the ventilation shafts is limited to rainfall and should not exceed infiltration that occurs in smaller fault features. Although fault features are suspected pathways for rapid migration of water from the surface to the repository (as observed from ^{36}Cl measurements), the amount of water that can bypass matrix flow in the Paintbrush nonwelded hydrogeologic unit is a only a small fraction (generally less than 5 percent in fault zones) based on transport calculations for ^{36}Cl between the ground surface and the repository horizon, which show 5 percent breakthrough at several hundred years (BSC 2004 [DIRS 169861], Figure H-2). Similarly, flow through the backfilled ventilation shafts is expected to have a large component of matrix flow, greatly reducing the amount of transient water pulses penetrating from the surface to the waste emplacement drifts, regardless of the specific characteristics or evolution of the backfill over time. Therefore, the effect of radionuclide transport through seals is negligible. This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.3.8 Degradation of Seals (2.1.05.03.0A)

FEP Description: Degradation of seals in the access ramps, ventilation shafts, and exploratory boreholes could modify flow and transport properties. Physical properties of the seals emplaced in the access ramps, ventilation shafts, and exploratory boreholes may affect the long-term performance of the disposal system. These properties include the location of the seals (and the openings they seal), and the physical and chemical characteristics of the sealing materials.

Possible mechanisms for seal degradation include: chemical alteration from water interactions, wetting associated with condensation, and thermally-induced stress-strain changes.

Screening Decision: Excluded–Low Consequence.

Screening Argument: The host rock in the repository is highly fractured; hence seals for ramps, ventilation shafts, and exploratory boreholes, whether intact or degraded, are of little consequence for water movement in the repository environment. The ventilation shafts connect to access drifts at the waste emplacement level and, therefore, represent pathways for water to enter the waste emplacement drifts. For postclosure, the ventilation shafts will be backfilled. The hydrogeologic effects of ventilation shafts provide high-permeability pathways similar to smaller fault features with respect to flow from the surface to the repository. The design for the shafts will account for the effects of flooding (BSC 2004 [DIRS 171676], Sections 3.1.1.13.1 through 3.1.1.13.3). Therefore, the quantity of water available to flow through the ventilation shafts in case of degraded seals is limited to rainfall and should not exceed infiltration that occurs in smaller fault features. Although fault features are suspected pathways for rapid migration of water from the surface to the repository (as observed from ^{36}Cl measurements), the amount of water that can bypass matrix flow in the Paintbrush nonwelded hydrogeologic unit is a only a small fraction (generally less than 5 percent in fault zones) of the total infiltration based on transport calculations for ^{36}Cl between the ground surface and the repository horizon, which show 5 percent breakthrough at several hundred years (BSC 2004 [DIRS 169861], Figure H-2). Similarly, flow through the backfilled ventilation shafts is expected to have a large component of matrix flow, greatly reducing the amount of transient water pulses penetrating from the surface to the waste emplacement drifts, regardless of the specific characteristics or evolution of the backfill over time. Therefore, the effect of radionuclide transport through seals is negligible. This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.4 EXTREME CLIMATE/ALTERNATIVE FLOW PROCESSES

These excluded FEPs concern the effects of climate and alternative flow processes on hydrological conditions, flow, and radionuclide transport in the UZ. Episodic (or short duration) transient flows are found to have a negligible effect and an average steady flow is used to represent the effects of flow.   The rationale for this approximation is discussed below. Longer-term changes in climate are addressed in TSPA-LA using a quasi-steady flow approximation; in other words, the flow fields instantaneously adjust to steady conditions for a given climate (infiltration). However, certain aspects of climate discussed in this section are excluded based on low probability and others on low consequence.

Table 6-5 gives the FEP numbers and names categorized under extreme climate/alternative flow processes.

Table 6-5. Excluded FEPs: Climate and Episodic Transient Flow

Section Number	FEP Number	FEP Name
6.4.1	1.3.04.00.0A	Periglacial effects
6.4.2	1.3.05.00.0A	Glacial and ice sheet effect
6.4.3	1.3.07.01.0A	Water table decline
6.4.4	2.1.09.21.0C	Transport of particles larger than colloids in the UZ
6.4.5	2.2.07.05.0A	Flow in the UZ from episodic infiltration
6.4.6	2.2.07.06.0A	Episodic or pulse release from repository

Source: DTN: MO0407SEPFEPLA.000 [DIRS 170760].

6.4.1 Periglacial Effects (1.3.04.00.0A)

FEP Description: This FEP addresses the physical processes and associated landforms in cold but ice-sheet-free environments. Permafrost and seasonal freeze/thaw cycles are characteristic of periglacial environments. These effects could include erosion and deposition.

Screening Decision: Excluded–Low Consequence and Low Probability.

Screening Argument: This FEP refers to climate conditions that could produce a cold, but glacier-free environment. Results of such a climate could include permafrost (permanently frozen ground). Paleoclimate records indicate that the climate conditions necessary to form permafrost are not credible at Yucca Mountain over the next 10,000 years (BSC 2004 [DIRS 170002], Section 6.6.2). The glacial-transition climate (identified as "intermediate" in Sharpe 2003 [DIRS 161591], Table 6-6) has the lowest predicted mean annual temperatures for the 10,000-year period (BSC 2004 [DIRS 170002], Section 6.6.2; Sharpe 2003 [DIRS 161591], Section 6.3.2). For the glacial-transition climate, the estimated range of mean annual temperatures is 8.3°C to 10.1°C (Sharpe 2003 [DIRS 161591], Table 6-3), which is too warm to sustain permafrost. Only the coldest scenario for the full glacial climate (Oxygen Isotope Stage 6/16) is expected to have a mean annual temperature of 0°C (Sharpe 2003 [DIRS 161591], Table 6-3). The expected return for such a climate is 200,000 years after present (Sharpe 2003 [DIRS 161591], Table 6-5). Therefore, soil erosion and deposition at Yucca Mountain as a result of permafrost are not credible. Freeze–thaw mechanical erosion will likely increase as the climate cools. However, the magnitude of erosion will not likely be significant even during the cooler climate condition. The time-averaged erosion over a 10,000-year period is expected to be less than 10 cm (YMP 1993 [DIRS 100520], Section 3.4), which is within the range of existing surface irregularities. This is based on estimates for erosion rates that have occurred at Yucca Mountain over the last 12 million years (YMP 1993 [DIRS 100520], Section 3.4) and, therefore, includes the effects of cooler climates. This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance. This FEP is also excluded because climate conditions necessary to form permafrost are not credible at Yucca Mountain over the next 10,000 years.

Supporting Reports: Not applicable.

6.4.2   Glacial and Ice Sheet Effect (1.3.05.00.0A)

FEP Description: This FEP addresses the effects of glaciers and ice sheets occurring within the region of the repository, including direct geomorphologic effects and hydrologic effects. These effects include changes in topography (due to glaciation and melt water), changes in flow fields, and isostatic depression and rebound. These effects could include erosion and deposition.

Screening Decision: Excluded–Low Probability.

Screening Argument: This FEP refers to the local effects of glaciers and ice sheets. Paleoclimate records indicate that during the next 10,000 years, the existence of glaciers or ice sheets at Yucca Mountain is not credible (BSC 2004 [DIRS 170002], Section 6.6). The closest alpine glaciers to Yucca Mountain during the Pleistocene were in the White Mountains in California (BSC 2004 [DIRS 169734], Section 6.4.1.4), too far from Yucca Mountain to have any effect on site geomorphology or hydrology. Given the relatively low elevation of Yucca Mountain, there is no credible mechanism by which a glacier could form at the site over the next 10,000 years. The geomorphologic and hydrological effects associated with glaciers, such as changes in topography resulting from erosion, deposition, and glacial transport, changes in flow fields, and isostatic depression and rebound, are not credible processes at Yucca Mountain. Therefore, this FEP is excluded from TSPA-LA on the basis of low probability.

Supporting Reports: Not applicable.

6.4.3   Water Table Decline (1.3.07.01.0A)

FEP Description: Climate change could produce decreased infiltration (e.g., an extended drought), leading to a decline in the water table in the saturated zone, which would affect the release and exposure pathways from the repository.

Screening Decision: Excluded–Low Consequence.

Screening Argument: This FEP refers to the effects of a climate change that leads to much drier climate conditions. Some of the consequences of this type of climate change are a decrease in infiltration rate over time, water table decline, and desertification of the surface environment. However, the Yucca Mountain region is already a desert environment, and future climates are only expected to have increased precipitation (BSC 2004 [DIRS 170002], Section 6.6). In any case, a decline in the water table and lower infiltration rates would increase the distance, and reduce the velocity of transport, from the repository to the water table and, therefore, would only enhance the UZ as a barrier to radionuclide movement. This FEP is, therefore, excluded because it will have no adverse affects on the radiological exposures to the RMEI, or radionuclide release to the accessible environment.   Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.4.4 Transport of Particles Larger Than Colloids in the UZ (2.1.09.21.0C)

FEP Description: Particles of radionuclide-bearing material larger than colloids could be entrained in suspension and then be transported in water flowing through the UZ.

Screening Decision: Excluded – Low Consequence.

Screening Argument: Particles larger than colloids are not expected to show much mobility in the UZ because of the large gravitational settling that occurs relative to diffusive movement for such particles. A relevant velocity scale for particle diffusion is the particle diffusion coefficient divided by the particle diameter. The colloid diffusion coefficient is given by the Stokes-Einstein equation (BSC 2004 [DIRS 164500], Equation 6-23). The gravitational settling velocity for a colloid may be computed from Stokes' law (Perry and Chilton 1973 [DIRS 104946], Equation 5-215). The particle diameter, d_p, at which these velocities are equal is given by:

$$d_p = \left[\frac{6kT}{\pi g(\rho_c - \rho_w)} \right]^{\frac{1}{4}}$$

(Eq. 6-1)

where k is the Boltzmann constant (1.38×10^{-23} J/K), T is the temperature in Kelvin (300 K), g is the gravitational acceleration (9.81 m/s^2), ρ_c is the colloid grain density (2,650 kg/m^3), and ρ_w is the density of water (1,000 kg/m^3). This equation indicates that for a value of d_p equal to 0.836 μm, gravitational settling and diffusion will be roughly in balance. For particles larger than colloids (greater than 1 μm) gravitational settling will dominate particle movement. Therefore, particles larger than colloids are not mobile.

The effects of perturbed TH conditions or other perturbed flow conditions (e.g., "groundwater rinse") on colloid movement (or movement of particles larger than colloids) are expected to be negligible because of the limited entrainment expected. Tests with fine, cohesive sediments presented by Vanoni (1977 [DIRS 164901], Figure 2.51) show that although entrainment does occur, for a wide variety of conditions this appears to be a very limited transient response. Entrainment is observed for a few days, and then the system stabilizes with no further initiation of motion, as compared with unretarded colloid transport, which has a 10 percent breakthrough in about 5 years (BSC 2004 [DIRS 164500], Section 6.18.4). The limited time frame for enhanced colloid movement is negligible with respect to the time frames for waste release and transport. This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.4.5   Flow in the UZ from Episodic Infiltration (2.2.07.05.0A)

FEP Description: Episodic flow could occur in the UZ as a result of episodic infiltration. Episodic flow may affect radionuclide transport.

Screening Decision: Excluded–Low Consequence.

Screening Argument: The process that drives infiltration in the UZ is precipitation, which is clearly episodic in nature.   Studies of episodic infiltration and percolation have found, however, that matrix-dominated flow in the Paintbrush Tuff nonwelded hydrogeologic unit (PTn) damps out the transient nature of the percolation such that UZ flow below the PTn is essentially steady (BSC 2004 [DIRS 169861], Appendix G).

The PTn primarily consists of nonwelded to partially welded tuffs and extends from the base of the densely to moderately welded Tiva Canyon welded tuff (TCw) to the top of the densely welded Topopah Spring welded (TSw) hydrogeologic unit.   Within the repository area, the thickness of the PTn unit ranges from approximately 30 to 60 m. As a whole, the PTn unit exhibits different hydrogeologic properties than the TCw and TSw units that bound it above and below.   Both the TCw and the TSw units display the low porosity and intense fracturing typical of the densely welded tuffs at Yucca Mountain.   In contrast, with its high porosity and low fracture intensity, the matrix of the PTn has a large capacity for storing groundwater and effectively damps percolation flux at the base of the TCw unit.   Water imbibing into the PTn matrix from rapid fracture flow of the TCw results in a more uniform distribution of flux at the base of the PTn after traveling through the entire PTn unit.

Calculations with infiltration boundary conditions of 5 mm/yr and 20 mm/yr (BSC 2004 [DIRS 169861], Figures G-11 and G-12; DTN: LB0408RITSSCPF.001 [DIRS 171593]) show the flow damping effect. This conclusion is supported by additional calculations (Wu et al. 2000 [DIRS 154918], Section 4.1; Wu et al. 2002 [DIRS 161058]). Furthermore, the PTn overlies the entire repository block (Appendix B). This damping of transient flow is due to capillary forces and high matrix permeability in the PTn that lead to matrix imbibition of water from fractures to the matrix. This is also supported by carbon-14 data collected in bedded tuffs of the PTn unit (BSC 2004 [DIRS 169861], Appendix G) as well as by results of a water-release test at Alcove 4 and the results of line surveys of fracture minerals in the ESF and ECRB Cross-Drift (BSC 2004 [DIRS 170004], Sections 6.7 and 6.14.1). Therefore, this FEP is excluded on the basis that the UZ flow is steady at the repository and along radionuclide transport pathways.

Very small amounts of fracture flow do appear to penetrate as fast pathways through fault zones between the ground surface and the repository elevation as evidenced by high [36]Cl concentrations in samples taken from the Exploratory Studies Facility (ESF).   Higher concentrations of this isotope found in the ESF can only be explained through surface deposition of [36]Cl from nuclear weapons testing and subsequent aqueous transport to certain ESF sampling locations in a period of approximately 50 years. The flow responsible for rapid transport could occur either as steady flow or as episodic transient flow. In either case, the key to fast transport through the PTn is for solute to move through fractures and bypass transport through the rock matrix. However, the flow and transport models indicate that the quantity of water and dissolved constituents that do penetrate the PTn as a result of fast pathways (generally less than 1 percent

of the total infiltration is negligible with respect to repository performance (CRWMS M&O 1998 [DIRS 100356], Section 2.4.2.8). This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.4.6 Episodic or Pulse Release from Repository (2.2.07.06.0A)

FEP Description: Episodic or pulse release of radionuclides from the repository and radionuclide transport in the UZ may occur both because of episodic flow into the repository, and because of pulse releases from failed waste packages.

Screening Decision: Excluded–Low Consequence.

Screening Argument: Precipitation and infiltration are episodic, percolation flux in the UZ at the repository horizon (below the PTn) is steady. Seepage, if it occurs, will also be steady. Radionuclide release from failed waste packages is modeled in EBS radionuclide transport abstraction (BSC 2004 [DIRS 169868]) as a "flow-through" process, where, for any waste package that has been breached by corrosion, the geometry of the openings does not present any barrier to flow. Section 6.6.1 of the abstraction also examines an alternative "bathtub flow" model, where an opening at the top of a waste package allows water to enter, but the package retains mobilized radionuclides until either it overflows or a second opening is formed below the water line, suddenly releasing water with mobilized radionuclides. Waste packages also fail at different times in the TSPA model, resulting in step increases of release rate. Transport would then proceed with matrix imbibition, diffusion, and retardation by sorption.

The analysis in *EBS Radionuclide Transport Abstraction* (BSC 2004 [DIRS 169868], Section 6.6.1) also examined the effect of step changes in seepage chemistry, such that the solubility of radionuclides might increase or decrease. The conclusion is that the effect of episodic or pulse releases from waste packages is not significant because of the potential mitigation from sorption and diffusion and because the variability of corrosion rates provides large uncertainty in radionuclide release rates from the waste package. This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.5 EROSION/DISSOLUTION/SUBSIDENCE

These excluded FEPs concern the effects of surface erosion, mineral dissolution, and subsidence on hydrological conditions, flow, and radionuclide transport in the UZ. All of these processes are expected to occur at Yucca Mountain at low rates. These FEPs are all excluded on the basis of low consequence given conservative bounds on the extent that these processes can affect the hydrogeologic system at Yucca Mountain in a 10,000-year period.

Table 6-6 gives the FEP numbers and names categorized under Erosion/Dissolution/Subsidence.

Table 6-6.   Excluded FEPs: Erosion/Dissolution/Subsidence

Section Number	FEP Number	FEP Name
6.5.1	1.2.07.01.0A	Erosion/denudation
6.5.2	1.2.07.02.0A	Deposition
6.5.3	1.2.09.02.0A	Large-scale dissolution
6.5.4	2.2.06.04.0A	Effects of subsidence

Source: DTN: MO0407SEPFEPLA.000 [DIRS 170760].

6.5.1   Erosion/Denudation (1.2.07.01.0A)

FEP Description: Erosion and denudation are processes which cause significant changes in the present-day topography and thus affect local and regional hydrology. Erosion of surficial materials can occur by a variety of means, including physical weathering (including glacial and fluvial erosion), chemical weathering, erosion by wind (aeolian erosion), and mass wasting (e.g., landslide) processes. The extent of erosion depends to a large extent on climate and uplift.

Screening Decision: Excluded–Low Consequence.

Screening Argument: Erosion is a process that will be ongoing at Yucca Mountain over the 10,000-year performance period. The time-averaged erosion due to various processes (e.g., fluvial erosion, aeolian erosion, chemical weathering) over a 10,000-year period is expected to be less than 10 cm (YMP 1993 [DIRS 100520], Section 3.4), even in high-erosion rate environments such as canyons. Erosion of 10 cm is within the range of existing surface irregularities. DOE (1988 [DIRS 100282], Section 1.1.3.3.2) indicates that mass wasting, such as landslides, does not play a significant role in the present erosional regime at Yucca Mountain.

Debris flows are the primary mechanism for hillslope erosion of unconsolidated deposits in the Yucca Mountain region (YMP 1995 [DIRS 102215], Section 2.5.2). However, the effects of debris flows are generally restricted to channelized areas (YMP 1995 [DIRS 102215], Section 4.2) and are not an effective erosion mechanism for unweathered bedrock. Therefore, debris flows have a limited influence on the evolution of surficial materials at Yucca Mountain. The effects of debris flows, over a 10,000-year period, are captured within the maximum expected erosion of 10 cm or less and are, therefore, insignificant.

The effects of surface construction and characterization activities at the ground surface on future erosion will also be negligible because of the planned reclamation of the site ground surface. As stated in *Reclamation Implementation Plan* (YMP 2001 [DIRS 154386], Section 5.2.2.1), "Recontouring and erosion control practices include backfilling spoil material and grading disturbed sites, so that a stable land form is created that blends with the surrounding topography. Following site decommissioning, disturbed areas will be graded such that the natural drainage pattern (predisturbance drainage) is restored. The sites will be stabilized and recontoured to blend into the natural topography of the area." This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.5.2   Deposition (1.2.07.02.0A)

FEP Description: Deposition is a process that causes significant changes in the present-day topography and thus affects local and regional hydrology. Deposition of surficial materials can occur by a variety of means, including fluvial, aeolian, and lacustrine deposition and redistribution of soil through weathering and mass wasting processes.

Screening Decision: Excluded–Low Consequence.

Screening Argument: Like erosion, deposition is a process that will be ongoing at Yucca Mountain over the 10,000-year performance period. However, given the topographic relief of Yucca Mountain, erosion is expected to dominate over deposition. Deposition is believed to be a dominant process in Fortymile Wash (YMP 1993 [DIRS 100520], Section 3.4). However, this drainage channel has no effect on UZ flow and transport at Yucca Mountain due to its lateral offset. This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance. The effects of igneous disruptive events and possible ash deposition are addressed in FEP 1.2.10.02.0A.

Supporting Reports: Not applicable

6.5.3   Large-Scale Dissolution (1.2.09.02.0A)

FEP Description: Dissolution can occur when any soluble mineral is removed by flowing water. Large-scale dissolution is a potentially important process in rocks that are composed predominantly of water-soluble evaporite minerals, such as salt.

Screening Decision: Excluded–Low Consequence.

Screening Argument: This FEP is principally concerned with the dissolution of highly soluble evaporite rocks such as halite or carbonates. Evaporitic minerals are present, but the UZ at Yucca Mountain is primarily composed of vitric high-silica rhyolite and quartz latite (or trachyte) (BSC 2004 [DIRS 169734], Section 3.3.2). Solubilities of these minerals are too low to produce large dissolution cavities, breccia pipes, or solution chimneys over the time scales of interest and expected water flow rates. Local dissolution processes, for example those that affect fracture-filling minerals, are discussed in FEP 2.2.08.03.0B. This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.5.4   Effects of Subsidence (2.2.06.04.0A)

FEP Description: Subsidence above the mined underground facility or other openings may affect the properties of the overlying rocks and surface topography. Changes in rock properties, such as enhanced permeability, may alter flow paths from the surface to the repository. Changes in surface topography may alter run-off and infiltration, and may perhaps create impoundments.

Screening Decision: Excluded–Low Consequence.

Screening Argument: Subsidence can occur as a result of underground excavations. Subsidence calculations for Yucca Mountain were done as the first step in analysis of drift-scale THM effects (BSC 2004 [DIRS 169864]). The model domain extends upward to the ground surface (BSC 2004 [DIRS 169864], Tables 4.1-3c and 4.1-3d). The simulation was conducted by first excavating the drift and then implementing a thermal line load into the drift opening (BSC 2004 [DIRS 169864], Section 6.5.1). Subsidence at the drift crown and at the ground surface   directly   above   the   drift   were   extracted   from   model   results   in DTNs: LB0306DRSCLTHM.001   [DIRS   169733]   and   LB0308DRSCLTHM.001 [DIRS 171567], and entered in a scientific notebook (Tsang 2004 [DIRS 171673], pp. 38 and 39). These results show that the simulated subsidence from excavation of a single drift, without input of heat, is greater at the drift crown than at the ground surface. The maximum subsidence predicted was 1.3 cm at the drift crown and 1.6 mm at the ground surface, for a drift in Tptpll low-quality rock. These calculated subsidence distances are too small to affect run-off or infiltration, or to create impoundments (Tsang 2004 [DIRS 171673], pp. 38 and 39). Therefore, subsidence is expected to have a negligible impact on large-scale UZ flow or surface topography, and is excluded from TSPA-LA modeling.

Corroborative evidence comes from mining experience. In coal mining, subsidence has been found to occur when more than 50 percent of the coal bed was removed (Keller 1992 [DIRS 146831], p. 142). In the case of Yucca Mountain, the percent of earth removal is very small. The emplacement drift diameter is less than 10 percent of the drift spacing (BSC 2004 [DIRS 168489]; BSC 2004 [DIRS 169058]).

Brady and Brown (1985 [DIRS 126811], Figure 16.18) present an empirical correlation of maximum subsidence S with width w of a rectangular opening, the extraction thickness m (height of the opening), and depth d. A circular drift, being smaller, will be less likely to cause subsidence; that is, the empirical correlation represents an upper bound. For repository drifts, $w=m=$ 5.5 m and d = 300 m. For this combination of variables, the maximum subsidence is off the chart on the low side; that is, S/m is less than 1%, or less than 5.5 cm.

Further corroboration comes from modeling of drift collapse (BSC 2004 [DIRS 166107], Appendix R). Collapse, separation of blocks from the roof of the drift, is distinct from subsidence, which is downward displacement without separation. A typical realization of drift collapse is shown in *Drift Degradation Analysis* (BSC 2004 [DIRS 166107], Figure 6-173). This figure shows collapse extending about 7 m above the original elevation of the drift crown, with uncollapsed rock above the drift being displaced downward 6 to 10 cm (subsidence at the ground surface is not shown).

The effects of changes to fracture characteristics around emplacement drifts caused by stress relief have been found to be small to moderate and to have no adverse effects on seepage (BSC 2004 [DIRS 169864], Section 8.1). Therefore, subsidence is expected to have a negligible impact on large-scale UZ flow or surface topography. This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.6   HUMAN INFLUENCES ON CLIMATE AND SOIL

This group of FEPs is excluded from the TSPA-LA calculation because they postulate a human influence on climatic effects. The licensing rule and supplemental information (66 FR 55732 [DIRS 156671]) indicate that only natural evolution of the reference biosphere is to be included in the performance assessment. Naturally occurring climate change effects are addressed in the TSPA-LA through climate modeling and ranges of parameters used to characterize UZ water chemistry.

Table 6-7 gives the FEP numbers and names categorized under Human Influences on Climate and Soil.

Table 6-7.   Excluded FEPs: Human Influences on Climate and Soil

Section Number	FEP Number	FEP Name
6.6.1	1.4.01.00.0A	Human influences on climate
6.6.2	1.4.01.02.0A	Greenhouse gas effects
6.6.3	1.4.01.03.0A	Acid rain
6.6.4	1.4.01.04.0A	Ozone layer failure
6.6.5	1.4.06.01.0A	Altered soil or surface water chemistry

Source: DTN: MO0407SEPFEPLA.000 [DIRS 170760].

6.6.1   Human Influences on Climate (1.4.01.00.0A)

FEP Description: Future human actions, either intentional or accidental, could influence global, regional, or local climate.

Screening Decision: Excluded–By Regulation.

Screening Argument: Human influences on climate are excluded on the basis of requirements of 10 CFR 63.305(b) [DIRS 156605]. The licensing rule and the supplemental information (66 FR 55732 [DIRS 156671]) indicate that only natural evolution of the reference biosphere is to be included in the performance assessment and that the changes caused by the future human behaviors are not to be included. In response to comments on climate change (66 FR 55732 [DIRS 156671], p. 55,757), the NRC emphasized the importance of including "climate change in both the geosphere and biosphere performance assessment calculations to ensure that the conceptual model of the environment is consistent with our scientific understanding of reasonably anticipated *natural* events [emphasis added]." Similarly, in the background

discussion of the 2002 amendment to the rule the NRC stated "DOE's performance assessments are required to consider the *naturally occurring* features, events and processes that could affect the performance of a geologic repository…[emphasis added]" (67 FR 62628 [DIRS 162317]). As the part of the response to the comments, the NRC also stated that considering future economic growth trends and human behaviors would add inappropriate speculation into the requirements and would lead to problems deciding which alternative futures are credible and which are unrealistic (66 FR 55732 [DIRS 156671], p. 55,757). The NRC stated further that the natural systems of the biosphere should be allowed to vary consistent with the geologic records, which provide basis for predicting future biosphere changes (66 FR 55732 [DIRS 156671], p. 55,757). Because human behavior cannot be similarly predicted, such an approach cannot be used for the reasonably maximally exposed individual (66 FR 55732 [DIRS 156671], p. 55,757) and, extending this reasoning, for the human-induced changes to the environment. Prediction of the human-induced climate changes would not only involve speculations about the local population, but also introduce inherently large uncertainties in prediction of the global population behaviors and their consequences. In their discussion of consideration of future economic growth trends the NRC concluded that inclusion of such future predictions would not only add inappropriate speculation, but also would not enhance public safety and would likely be inconsistent with the Environmental Protection Agency standards. Based on these statements, the FEPs associated with the characteristics of the reference biosphere and their change are limited to naturally occurring FEPs and exclude those related to human activities. Likewise, the geological, hydrological and climatological factors that the DOE must vary under 10 CFR 63.305(b) [DIRS 156605], are also limited to naturally occurring FEPs. In general, the exclusion of anthropogenic effects on climate is believed to be conservative, because global warming would increase temperature and reduce precipitation in the Yucca Mountain region (NRC 2004 [DIRS 170243], Section 4.3.5.1).

Supporting Reports: Not applicable.

6.6.2 Greenhouse Gas Effects (1.4.01.02.0A)

FEP Description: The greenhouse effect refers to the presence in the atmosphere of carbon dioxide and other gases that tend to allow solar radiation through to the earth's surface and reflect heat back. Thus, these gases act much as the glass of a greenhouse, with the earth as the greenhouse. Human activities, such as burning fossil fuels, clearing forests, and industrial processes, produce these greenhouse gases. The greenhouse effect could increase concentrations of carbon dioxide and other gases in the atmosphere, and lead to changes in climate such as global warming.

Screening Decision: Excluded–By Regulation.

Screening Argument: Human influences on climate are excluded on the basis of requirements of 10 CFR 63.305(b) [DIRS 156605]. The licensing rule and the supplemental information (66 FR 55732 [DIRS 156671]) indicate that only natural evolution of the reference biosphere is to be included in the performance assessment and that the changes caused by the future human behaviors are not to be included (FEP 1.4.01.00.0A). In general, the exclusion of anthropogenic effects on climate is believed to be conservative, because global warming would increase

temperature and reduce precipitation in the Yucca Mountain region (NRC 2004 [DIRS 170243], Section 4.3.5.1).

Supporting Reports: Not applicable.

6.6.3   Acid Rain (1.4.01.03.0A)

FEP Description: Human actions may result in acid rain on a local to regional scale. Acid rain can detrimentally affect aquatic and terrestrial life by interfering with the growth, reproduction, and survival of organisms. It can influence the behavior and transport of contaminants in the biosphere, particularly by affecting surface water and soil chemistry.

Screening Decision: Excluded–By Regulation.

Screening Argument: Human influences on climate are excluded on the basis of requirements of 10 CFR 63.305(b) [DIRS 156605]. The licensing rule and the supplemental information (66 FR 55732 [DIRS 156671]) indicate that only natural evolution of the reference biosphere is to be included in the performance assessment and that the changes caused by the future human behaviors are not to be included (FEP 1.4.01.00.0A).

Supporting Reports: Not applicable.

6.6.4   Ozone Layer Failure (1.4.01.04.0A)

FEP Description: Human actions (i.e., the use of certain industrial chemicals) may lead to destruction or damage to the earth's ozone layer. This may lead to significant changes to the climate, affecting properties of the geosphere such as groundwater flow patterns.

Screening Decision: Excluded–By Regulation.

Screening Argument: Human influences on climate are excluded on the basis of requirements of 10 CFR 63.305(b) [DIRS 156605]. The licensing rule and the supplemental information (66 FR 55732 [DIRS 156671]) indicate that only natural evolution of the reference biosphere is to be included in the performance assessment and that the changes caused by the future human behaviors are not to be included (FEP 1.4.01.00.0A).

Supporting Reports: Not applicable.

6.6.5   Altered Soil or Surface Water Chemistry (1.4.06.01.0A)

FEP Description: Human activities (e.g., industrial pollution, agricultural chemicals) may produce local changes to the soil chemistry or to the chemistry of water infiltrating Yucca Mountain and could provide a plume of unspecified nature to interact with the repository and possibly with waste packages.

Screening Decision: Excluded–By Regulation.

Screening Argument: Human activities may affect soil and surface water chemistry because of agricultural activities or pollution from industrial activities. Current land use at Yucca Mountain does not include activities such as these that may lead to large-scale changes in soil or water chemistry. It is not credible that such activities would occur at Yucca Mountain, because the site does not offer known mineral resources (BSC 2004 [DIRS 169734], Section 3.6), commercial or industrial land uses (BSC 2004 [DIRS 169734], Section 3.2), or land that is suitable for agricultural development due to the rough terrain, thin soils, low rainfall, and deep water table. The nearest agriculture to the repository site is currently well outside the footprint of the UZ model (CRWMS M&O 1997 [DIRS 101090], Tables 3-10 through 3-12, Figure 3-10, Appendix A). Furthermore, 10 CFR 63.305(b) [DIRS 156605] states that "DOE should not project changes in society, the biosphere (other than climate), human biology, or increases or decreases in human knowledge or technology. In all analyses done to demonstrate compliance with this part, the DOE must assume that all of those factors remain constant as they are at the time of submission of the license application." Therefore, human activities (changes in the social and institutional attributes of society, lifestyle, land use, and water use) that would alter soil or surface water chemistry are excluded on the basis of the regulatory requirements (10 CFR 63.305(b) [DIRS 156605]).

Supporting Reports: Not applicable.

6.7 GAS PHASE EFFECTS

This group of FEPs is excluded from the TSPA-LA calculation. These FEPs concern the effects of gas generation caused by chemical reactions in the repository, the intrusion of naturally occurring gases such as methane, gas-phase radionuclide transport, and natural air flow. These FEPs are all excluded on the basis of low consequence to performance.

Table 6-8 gives the FEP numbers and names categorized under Natural Gas/Gas Generation Effects.

Table 6-8. Excluded FEPs: Natural Gas/Gas Generation Effects

Section Number	FEP Number	FEP Name
6.7.1	2.2.10.11.0A	Natural air flow in the UZ
6.7.2	2.2.11.02.0A	Gas effects in the UZ
6.7.3	2.2.11.03.0A	Gas transport in geosphere

Source: DTN: MO0407SEPFEPLA.000 [DIRS 170760].

6.7.1 Natural Air Flow in the UZ (2.2.10.11.0A)

FEP Description: Natural convective air circulation has been observed at a borehole at the top of the mountain. Repository heat may increase this flow.

Screening Decision: Excluded–Low Consequence.

Screening Argument: Natural air flow is expected to have a negligible impact on TH processes, owing to the large volume of thermally generated flow, including water vapor. The effects of repository heat on air flow are discussed in Section 6.2.35 (FEP 2.2.10.10.0A). The effects of

natural air flow have little consequence on water movement in the UZ because of the high mobility of the gas phase; hence, little dynamic interaction occurs between the phases. The standard practice when modeling unsaturated liquid flow is to neglect the effects resulting from flow in the gas phase (Richards 1931 [DIRS 104252], pp. 319-321). All unsaturated zone flow results supporting TSPA-LA were performed using the EOS9 module of TOUGH2 V1.4 (LBNL 2000 [DIRS 146496]), which solves Richards' equation for unsaturated flow calculations (BSC 2004 [DIRS 169861], Section 6.2.4). In this method, air–gas flow dynamics are ignored by using a constant gas-phase pressure in an isothermal system. This simplified two-phase flow solution for the three-dimensional model calibrations and TSPA flow field simulations is the most computationally efficient approach, while giving accurate results for isothermal two-phase flow. Two-phase flow problems are solved with one equation per gridblock instead of solving two or three equations, as required by the EOS3 module. Numerical tests have shown that for unsaturated flow at steady state, the EOS9 solutions are nearly identical to EOS3, "true two-phase" flow solutions (BSC 2004 [DIRS 169861], Section 6.2.4).

The effects of natural air flow due to barometric pumping and the associated removal of water through vapor transport has been investigated. Estimates of the rate of water removal from Yucca Mountain through this mechanism range from 0.001 mm/yr to an upper limit of 0.1 mm/yr (Tsang and Pruess, 1990, [DIRS 172018] p. iii; Martinez and Nilson, 1994, [DIRS 172023], p. 26). These rates are negligible in comparison with the estimates for average infiltration at Yucca Mountain, which range from 1.25 to 31.69 mm/yr (BSC 2004 [DIRS 169861], Table 6.1-2), and would likely be even smaller under future climate scenarios. Regardless of magnitude, excluding this effect of natural air flow will not result in an underestimation of dose in TSPA.

This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.7.2   Gas Effects in the UZ (2.2.11.02.0A)

FEP Description: Pressure variations due to gas generation may affect flow patterns and contaminant transport in the UZ or may intrude into the repository. Degassing could affect flow and transport of gaseous contaminants. Gases could also affect other contaminants if water flow is driven by large gas bubbles forming in the repository. Potential gas sources include degradation of repository components and naturally occurring gases from clathrates, microbial degradation of organic material, or deep gases in general.

Screening Decision: Excluded–Low Consequence.

Screening Argument: In the Yucca Mountain UZ, the build-up of any significant gas pressure is unlikely, because of the permeable fracture pathways (BSC 2004 [DIRS 169861], Appendix A). Furthermore, sealing of fractures due to precipitation in the thermally perturbed repository environment has a negligible effect on hydrogeologic properties of the fractures

relative to gas pressure effects. This can be seen by comparing the gas-phase pressures in fractures for TH calculations (no mineral precipitation) with those for THC calculations (mineral precipitation included) (DTN: LB0302DSCPTHCS.002 [DIRS 161976]; BSC 2004 [DIRS 169856]). These analyses include the effects the phase change of water to vapor under the higher temperatures caused by waste heat from the repository. This FEP also addresses the effects of gas bubbles. Because the repository at Yucca Mountain is located in the UZ with high aqueous to gas-phase contact, bubbles would quickly be absorbed into the gas phase and could not drive substantial water flow. Therefore, the bubble-release mechanism is negligible. This argument is valid regardless of the specific potential sources of gas generation (e.g., degradation of repository components or microbial degradation of organic matter). This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.7.3   Gas Transport in Geosphere (2.2.11.03.0A)

FEP Description: Gas released from the drifts and gas generated in the near-field rock will flow through fracture systems in the near-field rock and in the geosphere. Certain gaseous or volatile radionuclides may be able to migrate through the far-field faster than the groundwater advection rate.

Screening Decision: Excluded–Low Consequence.

Screening Argument: All radionuclides in the nominal scenario for TSPA-LA are transported from the repository to the accessible environment into the aqueous phase (DOE 2002 [DIRS 155970], Section I.7). This is expected to bound any dose effects of gas-phase transport in the geosphere. The only radionuclides that would have a potential for gas transport are ^{14}C and ^{222}Rn. ^{129}I can exist in a gas phase, but it is highly soluble and, therefore, would be more likely to dissolve in groundwater rather than migrate as a gas. Other gas-phase isotopes have been eliminated in a screening analysis (DOE 2002 [DIRS 155970], Section I.3.3), usually because they have short half-lives and are not decay products of long-lived isotopes. Note that for ^{14}C and ^{222}Rn, the process of inhalation dose in the biosphere model is included (BSC 2004 [DIRS 169826], Section 6.2.45)

An analysis of the potential dose from gas-phase geosphere transport of carbon-14 shows that the individual maximum radiological dose rate was found to be 1.8×10^{-10} mrem per year (DOE 2002 [DIRS 155970], Section I.7). This may be compared with doses from ^{14}C in *Total System Performance Assessment for the Site Recommendation* (TSPA-SR) CRWMS M&O 2000 [DIRS 153246], Figure 4.1-7), which found peak doses from aqueous ^{14}C release to be in excess of 10^{-4} mrem/yr. Because gas-phase releases comprise approximately 2 percent of the ^{14}C inventory (DOE 2002 [DIRS 155970], Section I.7), this fraction should result in a maximum dose rate of about 10^{-6} mrem/yr, given aqueous release. Therefore, the dose from aqueous geosphere transport of carbon-14 bounds the dose from gas-phase geosphere transport pathways.

Radon is a decay product of uranium and would be generated for as long as any uranium remained in the repository. Based on gas flow studies, radon released from the repository in the gas phase is expected to decay before reaching the ground surface (DOE 2002 [DIRS 155970], Section I.7.3). Therefore, aqueous geosphere transport pathway will also bound the dose from ^{222}Rn, primarily through aqueous transport of the parent uranium radionuclide and generation of ^{222}Rn as a decay product at the accessible environment.

In summary, all radionuclides are transported in the aqueous phase between the repository and the accessible environment for the nominal scenario. The effects of gas phase geosphere transport on radiological exposures and radionuclide releases are bounded by aqueous phase geosphere transport. Therefore, this FEP may be excluded because including gas-phase radionuclide transport in the geosphere would result in lower predicted doses in TSPA. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.8 SEISMIC/IGNEOUS/ROCK CHARACTERISTICS

This group of FEPs is excluded from the TSPA-LA calculation. These FEPs concern the potential effects of seismic and igneous events and processes on existing rock properties and characteristics. Table 6-9 gives the FEP numbers and names categorized under Seismic/ Igneous/Rock Characteristics.

Table 6-9. Excluded FEPs: Seismic/Igneous/Rock Characteristics

Section Number	FEP Number	FEP Name
6.8.1	1.2.04.02.0A	Igneous activity changes rock properties
6.8.2	1.2.06.00.0A	Hydrothermal activity
6.8.3	1.2.10.01.0A	Hydrologic response to seismic activity
6.8.4	1.2.10.02.0A	Hydrologic response to igneous activity
6.8.5	2.2.06.01.0A	Seismic activity changes porosity and permeability of rock
6.8.6	2.2.06.02.0A	Seismic activity changes porosity and permeability of faults
6.8.7	2.2.06.02.0B	Seismic activity changes porosity and permeability of fractures
6.8.8	2.2.06.03.0A	Seismic activity alters perched-water zones
6.8.9	2.2.12.00.0A	Undetected features in the UZ

Source: DTN: MO0407SEPFEPLA.000 [DIRS 170760].

6.8.1 Igneous Activity Changes Rock Properties (1.2.04.02.0A)

FEP Description: Igneous activity near the underground facility may cause extreme changes in rock stress and the thermal regime, and may lead to rock deformation, including activation, creation, and sealing of faults and fractures. This may cause changes in the rock hydrologic and mineralogic properties. Permeabilities of dikes and sills and the heated regions immediately around them can differ from those of country rock. Mineral alterations can also change the chemical response of the host rock to contaminants.

Screening Decision: Excluded–Low Consequence.

Screening Argument: Volcanism and igneous activity in the Yucca Mountain region was principally silicic until about 11 Ma (million years ago); since then the igneous activity has been basaltic, at a much lower level of activity (BSC 2004 [DIRS 169989], Section 6.2). Basaltic igneous activity typically has minimal physical and mineralogical effects on local rock properties. Basaltic magma chills rapidly against country rock, forming a nonvesicular aphanitic border facies having low thermal conductivity and low chemical reactivity. The country rock itself may be baked to form a thin rind or hornfels. Any such alteration in the welded tuff units would be minimal, owing to the dearth of hydrous minerals and the large component of high-temperature feldspars in the tuff. Furthermore, studies of analogue sites suggest that the consequences of hydrothermal activity in terms of the amount and extent of mineral alteration are small (Valentine et al. 1998 [DIRS 119132], p. 5-74; CRWMS M&O 1998 [DIRS 105347]; Carter-Krogh and Valentine 1996 [DIRS 160928], pp. 7 and 8).

Dikes are expected to range between about 0.5 m to 4.5 m in thickness, with an average of 1.5 m (BSC 2004 [DIRS 169980], Section 6.3.1). A simple conduction-only, dike-cooling model indicates that a dike of 5.5 m thickness will cool to sub-boiling in less than 60 years, with boiling temperatures no more than 20 m from the dike (BSC 2004 [DIRS 170028], Figure D-1). A period of 200 to 300 years to cool to 500°C was estimated by Ratcliff et al. (1994 [DIRS 106634] for the 150-m-thick Paiute Ridge lopolith, but thinner intrusions would cool much faster. Contact metamorphism resulting from dikes at a vadose-zone analogue site, Paiute Ridge, is confined to distances of a few meters from the dike (Valentine et al. 1998 [DIRS 119132], Chapter 5). With significant thermal perturbations limited to less than 100 years and alteration limited to zones of a few meters around the dike, the effects of basaltic magmatism on transport pathways, advective velocities, and sorption coefficients (K_ds) is negligible.

On the basis of these confined and short-duration features and processes, this FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Furthermore, the probability for the occurrence of a volcanic event at Yucca Mountain is 1.7×10^{-8} per year (BSC 2004 [DIRS 169989], Table 7-1), which results in a greatly reduced expected consequence from a probability-weighted perspective. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable

6.8.2 Hydrothermal Activity (1.2.06.00.0A)

FEP Description: Naturally-occurring high-temperature groundwater may induce hydrothermal alteration of minerals in the rocks through which the high-temperature groundwater flows.

Screening Decision: Excluded–Low Consequence.

Screening Argument: The earliest volcanism in the Yucca Mountain region was dominated by a major episode of caldera-forming, silicic volcanism that occurred primarily between ~15 and 11 million years ago (Ma), forming the southwestern Nevada volcanic field (Sawyer et al. 1994

[DIRS 100075]).   Silicic volcanism was approximately coincident with a major period of extension, which occurred primarily between 13 and 9 million years ago (Sawyer et al. 1994 [DIRS 100075], Figure 4).   The southwestern Nevada volcanic field is considered to have virtually ceased eruptive activity of silicic magmas since about 7.5 Ma (BSC 2004 [DIRS 169989], Section 6.2).   The commencement of basaltic volcanism occurred during the latter part of the caldera-forming phase, as extension rates waned, and small-volume basaltic volcanism has continued into the Quaternary (BSC 2004 [DIRS 169989], Section 6.2).   The focus of igneous-related FEPs is on the potential for small scale basaltic volcanism and the mean probability of a basaltic dike intersecting the repository footprint has been calculated to be 1.7×10^{-8} per year (BSC 2004 [DIRS 169989], Table 7-1)

Yucca Mountain is an uplifted, erosional remnant of voluminous ash-flow tuff deposits formed during the early phase of silicic volcanism (BSC 2004 [DIRS 169989], Section 6.2). Hydrothermal alteration and mineralization that followed the deposition of the Paintbrush Group are present within a few kilometers of the Yucca Mountain site in the Calico Hills and in Claim Canyon.   However, no clear evidence for hydrothermal activity exists in the repository area (BSC 2004 [DIRS 169734], Section 3.6.2).   Yucca Mountain is located outside the caldera margin, (BSC 2004 [DIRS 169989], Figure 6-1), and the level of heating at Yucca Mountain associated with the Timber Mountain volcanic center (and its associated hydrothermal system) was relatively minor, with peak fluid inclusion temperatures of around 80°C to 90°C occurring at around 9 to 10 Ma, so that the heating event at Yucca Mountain did not result in pervasive hydrothermal alteration of the tuffs. Studies of secondary minerals at Yucca Mountain using petrography, fluid-inclusion thermometry, and U–Pb dating indicate that temperatures have remained close to the current ambient values over the past 2 to 5 million years (Wilson et al. 2003 [DIRS 163589], Section 8).

Mineral coatings composed primarily of calcite, opal, chalcedony, and quartz provide evidence of the thermal-hydrothermal history of Yucca Mountain. The minerals were deposited under unsaturated conditions, because they are found only on fracture footwalls and lithophysal cavity bottoms (Marshall and Whelan 2000 [DIRS 154415]).   Various lines of evidence, including (i) stable isotope oxygen data of calcite, which indicates the temperature of mineral precipitation (ii) homogenization temperatures of fluid inclusions which indicates the temperature at which the inclusions were trapped (iii) Uranium and lead isotope ratios in opal associated with the calcite (Neymark et al. 2003 [DIRS 163681]), which constrain the age of deposited minerals, combine to indicate that temperatures in the UZ decreased over time from approximately 90°C at 10 Ma to near ambient temperatures at 2 Ma. These secondary minerals were interpreted to have been deposited from downward percolating meteoric water, and not from upwelling groundwaters (Whelan et al. 2003 [DIRS 163590]).

Marshall and Whelan (2001 [DIRS 163591]) present a conceptual model of heat transfer from the Timber Mountain magma chamber to explain the temperature history of Yucca Mountain that was inferred from geological evidence. This was implemented in a numerical model using the program HEAT (Wohletz et al. 1999 [DIRS 164597], Appendix B); model results are presented in Marshall and Whelan (2001 [DIRS 171061]). In a sensitivity study, the conditions above the magma chamber were varied: 5 or 2.5 km from the top of the magma chamber to the ground surface (shallower depth causes faster cooling of the magma), presence or absence of an UZ (with a UZ the magma cools slower because saturated rock is more thermally conductive), and

presence or absence of a hydrothermal regime, which would allow heat loss by convection (Ziegler 2004 [DIRS 171590], Section H.4.2). Conditions that caused the magma to cool off more rapidly also caused a target location 4 km from the edge of the magma chamber and 250-m deep (approximately representing the near edge of the repository location) to get hot sooner and to reach a higher maximum temperature. That is, applying conditions of convective heat transfer and shallow burial resulted in more heat transfer to the target location. The simulations presented by Marshall and Whelan (2001 [DIRS 171061]) agree with the temperature history inferred from the geologic evidence (Whelan et al. 2003 [DIRS 163590], Figure 4) since 5 Ma, but before that time, the geologic evidence indicates hotter temperatures than predicted by the model.

In simulations conducted by Marshall and Whelan (2001 [DIRS 171061]), the magma chamber is maintained at constant magmatic temperature from 15 Ma to 11 Ma. One way to possibly reconcile the model and data would be to extend the magmatic activity of the Timber Mountain system beyond 11 Ma (Ziegler 2004 [DIRS 171590], Section H.4.2). While only minor volcanic activity is associated with Timber Mountain after 11.4 Ma, it is possible that the system received continued injections of mantle-derived mafic magmas that would have provided additional heating to the region (Farmer et al. 1991 [DIRS 153024]). Continuing silicic volcanism at the Black Mountain caldera (9.4 Ma) and Stonewall Mountain volcanic center (7.5 Ma), both located northwest of the Timber Mountain caldera, indicates that regional silicic magmatism and associated heating persisted beyond 11 Ma (Sawyer et al. 1994 [DIRS 100075]).

The Long Valley caldera in California provides a natural analogue to test the caldera-heating model proposed by Marshall and Whelan (2001 [DIRS 163591]). This is a younger caldera than Timber Mountain, so that the thermal gradient away from the caldera is still detectable. Data presented by Lachenbruch et al. (1976 [DIRS 171203], Table 1) show a horizontal thermal gradient decreasing with distance from the caldera, analogous to the results provided by Marshall and Whelan (2001 [DIRS 171061]).

Additional evidence of elevated paleotemperatures at Yucca Mountain may be provided by observations of thick twinned calcite samples in discrete narrow faults (2 to 20 cm) (Gray et al. 2000 [DIRS 171202]). Thick twinned calcite was interpreted to indicate deformation at temperature above 170°C (Ferrill et al 2004, [DIRS 171196], which is higher than the temperatures indicated by calcite fluid inclusions reported by Whelan et al. (2003 [DIRS 163590]) and by Wilson et al. (2003 [DIRS 163589], Section 8). If the higher temperatures indicated by thick twins (which have not been confirmed by studies of fluid inclusions in the same samples) are correct, they may indicate that the twinned calcite was formed during a very early, higher-temperature event. Such temperatures would most likely have occurred shortly after emplacement of the ash-flow tuff deposits at Yucca Mountain, when degassing and cooling of the ash-flow tuff can result in devitrification, vapor-phase alteration, and development of localized meteoric-hydrothermal activity in the upper parts of ash-flow sheets (Holt 2002 [DIRS 162326]). Gray et al. (2000 [DIRS 171202]) note that the calcite mineralization observed in the narrow faults is not encountered in the intrablock and block-bounding faults, which would be likely candidates for fluid flow and mineralization in the event of widespread hydrothermal alteration. The absence of pervasive hydrothermal mineralization of the Yucca Mountain tuffs is consistent with the interpretation that large-scale hydrothermal activity has not occurred in the Yucca Mountain area.

Since the cessation of silicic magmatism about 11.4 Ma, basaltic igneous activity has been characteristic of the Yucca Mountain region. Silicic volcanism during the regulatory period is, therefore, not credible and analysis of this FEP is focused on the probability and consequence of basaltic magmatism (Reamer 1999 [DIRS 119693], p. 5). Although basaltic magmatism could occur during the regulatory period, the effects of any related hydrothermal system would be of limited scale as described in Section 6.8.1 (FEP 1.2.04.02.0A) where the effects of basaltic magmatism are addressed. Due to the limited scale of effects from basaltic dikes, the potential effects of hydrothermal alteration are excluded because they will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. With significant thermal perturbations limited to less than 100 years and alteration limited to zones of a few meters around the dike, the effects of basaltic magmatism on transport pathways, advective velocities, and sorption coefficients (K_ds) is also negligible. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.8.3   Hydrologic Response to Seismic Activity (1.2.10.01.0A)

FEP Description: Seismic activity, associated with fault movement, may create new or enhanced flow pathways and/or connections between stratigraphic units, or it may change the stress (and, therefore, fluid pressure) within the rock. These responses have the potential to significantly change the surface and groundwater flow directions, water level, water chemistry, and temperature.

Screening Decision: Excluded–Low Consequence and Low Probability.

Screening Argument: This FEP addresses the effects of seismic activity on UZ flow and transport at the mountain scale and for drift seepage. It also addresses the possible water table rise in response to seismic activity. The aspects of this FEP related to flow and transport are addressed in Sections 6.8.5 (FEP 2.2.06.01.0A), 6.8.6 (FEP 2.2.06.02.0A), and 6.8.7 (FEP 2.2.06.02.0B). This FEP assesses the effects of seismically induced water table rise caused by seismic pumping and changes in the large hydraulic gradient. The effect of seismic activity on transport is addressed in a sensitivity study in Sections 6.8.5, 6.8.6, 6.8.7, and in Appendix D.

Seismic pumping (Szymanski 1989 [DIRS 106963], pp. 3 through 22) is the temporary increase in height of the water table caused by fault movement. This movement of the water table is caused by the opening and closing of fractures during an earthquake cycle. Longer-term changes result from complex strain adjustments, but these changes are dissipated under the influence of regional stress field, which brings the state of the SZ fracture network back to an ambient, preseismic state as postseismic relaxation occurs. Numerical simulations by Carrigan et al. (1991 [DIRS 100967]) of tectonohydrological coupling involving earthquakes typical of the Basin and Range province (~ 1 m slip) produced 2 to 3 m excursions of a water table 500 m below ground surface. Extrapolation to an event of about 4-m slip would result in a transient rise of 17 m near the fault (Carrigan et al. 1991 [DIRS 100967], p. 1,159). As discussed in Section 6.8.6, seismic activity can also change fault permeability. Carrigan et al. (1991 [DIRS 100967]) modeled a 100-m-wide fracture zone centered on a vertical fault, with vertical

permeability increased by a factor of 1,000. Water level excursions in the fracture zone were twice as great as in the adjacent block. For a fault-fracture zone with 1-m slip, transient excursions of about 12 m can occur.

The significance of a rise in the water table is that it reduces the barrier capability of the UZ by shortening the flow path from the repository to the SZ. Regardless, data and modeling results indicate that changes in water table elevation at Yucca Mountain are not likely to exceed several meters and are likely to be transient. What seems most reasonable is that the water table excursions caused by earthquakes do not cause sufficient water table level fluctuations to threaten, even temporarily, the repository horizon, which in the current design is approximately 300 m above the water table. Given this limited water table movement, changes to surface- and groundwater-flow directions, water level, water chemistry, and temperature would also be negligible. Therefore, the seismic effects on water table rise resulting from seismic pumping are excluded because they will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment.

Another aspect of the water-table rise issue concerns the large hydraulic gradient that exists north of the repository. North of the repository, the water table elevation decreases by about 250 m as one moves from north to south towards the repository. If this gradient were to migrate southward, the resulting water table below the repository could be much higher than present-day conditions.

The work of Davies and Archambeau (1997 [DIRS 103180], p. 28) presents a hypothesis that the gradient is a result of stress variations in the rock that are residual stress effects induced by the Timber Mountain caldera. Furthermore, they suggest that moderate earthquakes in this area could induce a sufficient change in geomechanical strain downstream of the current large hydraulic gradient to induce a similar gradient downstream of the repository. This would result in a large (150 m to 250 m) rise in the water table beneath the repository. However, the hypothesis regarding the residual stress effects of the 10 million-year (Ma) Timber Mountain caldera contradicts extensive previous experience in the region of the Nevada Test Site (Stock et al. 1985 [DIRS 101027]). This composite experience is compiled from 14 sources reporting results from diverse methods, including hydraulic fracturing, overcoring stress measurements, earthquake focal mechanisms, borehole breakouts, orientations of explosion-produced fractures, and study of Quaternary faults and cinder-cone alignments. These studies show a reasonably uniform direction of extension between northwest and west, with a mixed potential-slip regime of normal faulting (mainly for shallow indicators) and strike-slip faulting (mainly for deep indicators). The Davies and Archambeau discussion is also inconsistent with actual stress measurements in G-2 as reported by Stock and Healy (1988 [DIRS 101022]), which is cited, though erroneously, as a source of "slug-test" data. Stock and Healy (1988 [DIRS 101022]) characterize G-2 as being within the same ("combined normal and strike-slip") faulting regime as that indicated by the results from the three holes that they tested south of the large gradient. Based on the stress measurements in the four holes, the tendency for strike-slip faulting is greatest in the southeastern hole, UE-25p#1, not in the northern Yucca Mountain area where G-2 is located, as Davies and Archambeau propose.

The available data (Stock et al. 1985 [DIRS 101027]; Stock and Healy (1988 [DIRS 101022]) do not support a residual stress effect from the Timber Mountain caldera, do not support a

modern stress field changing from strike-slip in northern Yucca Mountain to normal south of the hydraulic gradient, and do not support a southward decrease of the least principal stress. Although it is reasonable that the area of the large hydraulic gradient is less transmissive than the area to the south–southeast, a more reasonable explanation for this lower transmissivity is that durable differences of lithology, alteration history, and structural deformation have affected this region, rather than a transient state of stress. This mechanism is inconsistent with the existing data of Stock et al. (1985 [DIRS 101027]) and Stock and Healy (1988 [DIRS 101022]). In the Basin and Range Province, which includes the Yucca Mountain region, seismic and tectonic activity are in a waning phase with the focal point moving westward (BSC 2004 [DIRS 170017], Section 6.2.1.1). Therefore, any large changes to surface- and groundwater-flow directions, water level, water chemistry, and temperature due to the seismic activity are not credible. Therefore, the seismic effects on water table rise caused by seismic activity, or by migration of the large hydraulic gradient induced by seismic activity, are excluded from TSPA-LA on the basis of low probability.

Supporting Reports: Not applicable.

6.8.4   Hydrologic Response to Igneous Activity (1.2.10.02.0A)

FEP Description: Igneous activity includes magmatic intrusions which may alter groundwater flow pathways, and thermal effects which may heat up groundwater and rock. Igneous activity may change the groundwater flow directions, water level, water chemistry, and temperature. Eruptive and extrusive phases may change the topography, surface drainage patterns, and surface soil conditions. This may affect infiltration rates and locations.

Screening Decision: Excluded–Low Consequence.

Screening Argument: Intrusion of a basalt dike at or near the repository block could present a radical contrast in hydrological properties to the native rock. However, analogue studies show that alteration is quite limited, typically only found within a few meters of intrusions (Valentine et al. 1998 [DIRS 119132], p. 5-74). The effects of local-scale heterogeneity on unsaturated flow and transport at Yucca Mountain were investigated by Zhou et al. (2003 [DIRS 162133]). The conclusions reached in this study were that local heterogeneity in fracture permeability had a negligible effect on flow. Effects on transport were found to be more significant, but the uncertainty in transport behavior caused by local heterogeneity was less than that caused by uncertainty in matrix diffusion. Therefore, local variations in properties caused by dike intrusions would result in only minor changes to the flow patterns. Other aspects related to the effects of igneous intrusions, such as mineral alteration, are discussed in Sections 6.8.1 (FEP 1.2.04.02.0A) and 6.8.2 (FEP 1.2.06.00.0A). These aspects were also found to be limited in extent and duration.

Dikes are expected to range between about 0.5 m to 4.5 m in thickness, with an average of 1.5 m (BSC 2004 [DIRS 169980], Section 6.3.1). A simple conduction-only dike-cooling model indicates that a dike of 5.5 m thickness will cool to subboiling in less than 60 years, with boiling temperatures no more than 20 m from the dike (BSC 2004 [DIRS 170028], Figure D-1). Contact metamorphism caused by dikes appears to be confined to distances of less than 5 m from the dike (BSC 2004 [DIRS 169734], Section 4.2.3.5). With significant thermal perturbations limited

to less than 100 years and alteration limited to zones of a few meters around the dike, the thermal and chemical effects of basaltic magmatism on UZ processes is negligible. The effects on water level are discussed in Section 6.8.3 (FEP 1.2.10.01.0A).

Igneous activity could also affect the ground surface of the repository through eruptions of lava or ash. If lava were to dam one or more washes that drain the repository block, the dam would not produce a large surface-water impoundment relative to the repository emplacement area. Such lava dams would probably not be effective in any case, as the lava would consist of clinker or aa (aa is a lava flow with a surface typified by angular, jagged blocks). Another potential effect would be the deposition of an ash cover on the repository block. The median grain size of ash deposits investigated at the Lathrop Wells cone ranged from of 0.18 to 2.8 mm (BSC 2004 [DIRS 169980], Table C-7). This grain size is characteristic of a medium to coarse sand, which has a typical porosity range of 0.35 to 0.4 (Bear 1972 [DIRS 156269], pp. 40 and 46). Using these porosity and grain size ranges and the modified Kozeny-Carmen equation for permeability (Bear 1972 [DIRS 156269], p. 166):

$$k = \frac{d_m^2}{180} \frac{n^3}{(1-n)^2}$$
(Eq. 6-2)

where k is permeability, d_m is grain size, and n is porosity, the estimated permeability range of the ash deposit is 2×10^{-11} to 8×10^{-9} m^2. Bedrock permeability in the infiltration model ranges from 2×10^{-17} to 6×10^{-13} m^2 and soil permeability ranges from 6×10^{-13} to 4×10^{-12} m^2 (BSC 2004 [DIRS 170007], Appendix B). Therefore, an ash deposit is expected to be orders of magnitude more permeable than the underlying bedrock and soil. Rainfall will tend to infiltrate and run off along the ash-bedrock or ash-soil interface resulting in minimal effects of the ash on runoff or infiltration.

As an additional consideration, the mean probability for the occurrence of a volcanic intrusion at Yucca Mountain is 1.7×10^{-8} per year (BSC 2004 [DIRS 169989], Table 7-1). This results in a greatly reduced expected consequence from a probability-weighted perspective. This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.8.5 Seismic Activity Changes Porosity and Permeability of Rock (2.2.06.01.0A)

FEP Description: Seismic activity (fault displacement or vibratory ground motion) has a potential to change rock stresses and result in strains that affect flow properties in rock outside the excavation-disturbed zone. It could result in strains that alter the permeability in the rock matrix. These effects may decrease the transport times for potentially released radionuclides.

Screening Decision: Excluded–Low Consequence.

Screening Argument: This argument is directed towards the effects of seismic activity on the rock matrix. For effects of seismic activity on the rock fractures, see FEPs 2.2.06.02.0A and 2.2.06.02.0B. The effects of stress changes on flow in the UZ have been investigated in *Drift Scale THM Model* (BSC 2004 [DIRS 169864]). In this model, the effects of thermal stress are evaluated in terms of changes to rock fracture properties, but not rock matrix (BSC 2004 [DIRS 169864], Section 6.2). This modeling approach is based on the approximation that the effects of changes to the rock matrix porosity and permeability caused by changes in rock stress are negligible compared with changes to the fracture porosity and permeability. The basis for this approximation is that the matrix, being approximately 10 percent pore space and 90 percent solid, is stronger than the fractures, which are 100 percent pore space. The fractures are, therefore, more sensitive to mechanical strain; when a volume of fractured rock is subjected to a stress, most of the resulting strain occurs in the fractures. Furthermore, the fracture volume is only about 1 percent of the bulk volume. Therefore, when a small mechanical strain in the rock is mostly taken up by change in fracture volume, the change in fracture volume (and, therefore, fracture aperture) is relatively large, with a corresponding large change in fracture permeability. This should be true not only for thermal stress, but also for other sources of mechanical stress, such as seismic activity. Therefore, changes to the rock matrix characteristics due to seismic activity are excluded from TSPA-LA because they will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.8.6   Seismic Activity Changes Porosity and Permeability of Faults (2.2.06.02.0A)

FEP Description: Seismic activity (fault displacement or vibratory ground motion) has a potential to produce jointed-rock motion and change stress and strains that alter the permeability along faults. This could result in reactivation of preexisting faults or generation of new faults, which could significantly change the flow and transport paths, alter or short-circuit the flow paths and flow distributions close to the repository, and/or create new pathways through the repository. These effects may decrease the transport times for potentially released radionuclides.

Screening Decision: Excluded–Low Consequence.

Screening Argument: This FEP is similar in content to the one discussed in Section 6.8.7 (FEP 2.2.06.02.0B). Like fractures, faulting is a characteristic feature of Yucca Mountain geology. The present-day faults are addressed in the flow and transport models of the UZ (FEP 1.2.02.02.0A). Fault movements can affect the fracture properties through changes in rock stress. This aspect of the problem is discussed in Section 6.8.7 (FEP 2.2.06.02.0B). Fault movements can also change the properties of the faults themselves, and this aspect has been investigated with a sensitivity study reported in Appendix D.

Movements produced by a fault displacement will result in changes in the rock stress in the vicinity of the fault. The change in rock stress will decrease with distance from any given fault that does move. However, the magnitude of the changes in rock stress as a function of distance from the fault depends on the specific details of the fault displacement (e.g., magnitude of fault

motion, direction of fault movement, extent of the fault that participates in the movement) and the mechanical properties of the surrounding rock (e.g., fracture spacing, fracture stiffness, geomechanical properties of the rock matrix). Given some change in rock stress, the fractured rock mass will respond to the change in stress through deformation, or strain, in the rock. Note that this induced strain can affect the geometry of fractures in the rock. The effects of stress changes on flow in the UZ have been investigated in *Drift Scale THM Model* (BSC 2004 [DIRS 169864]). In this model, the effects of thermal stress are evaluated in terms of changes to rock fracture properties, but not rock matrix (BSC 2004 [DIRS 169864], Section 6.2); see FEP 2.2.06.01.0A. This modeling approach is used because the effects of changes to the rock matrix porosity and permeability caused by changes in rock stress are negligible compared with changes to the fracture porosity and permeability. It is reasonable to expect that this should be true for other sources of mechanical stress, such as seismic activity. In theory, the effects of a given fault displacement could be evaluated using process-level calculations for the effects of the induced stress and strain on fracture geometry. However, this direct approach was not further used to specifically evaluate seismic effects because of the large uncertainty in the specification of the seismic event and complexity of translating seismic motion along faults into imposed stresses. An alternative bounding approach was used to assess the potential effects of fault displacement on repository performance as described in Appendix D.

The approach used to investigate the effects of fault displacements was to evaluate the sensitivity of radionuclide transport in the UZ to changes in fracture apertures. (Appendix D, Section D3.2.6). This is investigated over a wide enough range to bound the potential changes in fracture aperture that could result from any fault displacement at Yucca Mountain with an annual exceedance probability greater than 10^{-8} (Section 5). The largest fault movement close to the repository is likely to be along the Solitario Canyon fault (Appendix D, Section D2.1.1). The general topic of seismic hazard at Yucca Mountain has been investigated in detail in *Probabilistic Seismic Hazard Analyses for Fault Displacement and Vibratory Ground Motion at Yucca Mountain, Nevada* (USGS 1998 [DIRS 100354]). For the Solitario Canyon fault, the hazard analysis shows fault displacement of approximately 10 m (USGS 1998 [DIRS 100354], Figure 8-3; DTN: MO0401MWDRPSHA.000 [DIRS 166962]) at an annual exceedance probability of 10^{-8} (Section 5). An approximately 10 m fault movement was used as the fault displacement for these analyses. The results of geomechanical models suggest that a factor of 10 change in aperture would bound the effects of tensile strain from such a fault movement (Appendix D, Section D3.2.6). Based on the cubic law for fracture permeability, a factor of 10 change in aperture leads to a factor of 1,000 change in permeability. Fracture permeabilities reduced by a factor of 1,000 were found to be inconsistent with infiltration rates. Therefore, reductions in aperture were limited to factors of 0.2, and in the case of a wetter climate, the lowest value that could be used was a factor of 0.5, leading to permeability reductions of 125 and 8, respectively.

The sensitivity study considered the effects of changes in fracture aperture on porosity, permeability, and capillary pressure (Appendix D, Section D3.2.7). Calculations were then performed for unsaturated flow and transport using the modified fracture properties (Appendix D, Section D3.3). A subset of these sensitivity calculations considered changes to these hydrological properties restricted to major faults (Solitario Canyon, Ghost Dance, Dune Wash, Bow Ridge, and Sundance faults) for present-day and glacial transition climates (Appendix D, Section D3.3.1, Figures D-7 and D-8). The results showed almost no change in

transport behavior between the repository and the water table for a range in fracture apertures affected by factors of 0.2 to 10 when only fault fractures are altered. This study concluded that radionuclide transport in the UZ is highly insensitive to the fault properties.

The results presented in Section D3.3 are supported by scientific notebook YMP-LBNL-GJM-GZ-1 (Zhang and Moridis 2004 [DIRS 171212], pp. 41-49). These results are also corroborated by an earlier study (CRWMS M&O (2000 [DIRS 151953], Section 6.2).

The analysis in Appendix D, as summarized the preceding paragraphs, considers the effects of altering the hydrologic properties of fractures in faults on transport. The effects on seepage have also been studied in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Sections 6.4.4.1.2 and 6.5.1.5). Dilation of fractures, resulting from seismic activity, increases the fracture aperture and permeability, allowing greater flow capacity to divert seepage around drifts; however, the increase in fracture aperture also reduces the capillary strength of the fractures, which acts to prevent water that percolates to the drift crown from seeping. These two effects counteract each other, resulting in effectively no increase in seepage. Therefore, changes to fault properties due to seismic activity are excluded because they will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.8.7   Seismic Activity Changes Porosity and Permeability of Fractures (2.2.06.02.0B)

FEP Description: Seismic activity (fault displacement or vibratory ground motion) has a potential to change stress and strains that alter the permeability along fractures. This could result in reactivation of pre-existing fractures or generation of new fractures, which could significantly change the flow and transport paths, alter or short-circuit the flow paths and flow distributions close to the repository, and/or create new pathways through the repository. These effects may decrease the transport times for potentially released radionuclides.

Screening Decision: Excluded–Low Consequence.

Screening Argument: Movements produced by a fault displacement will result in changes in the rock stress in the vicinity of the fault. The change in rock stress will decrease with distance from any given fault that does move. However, the magnitude of the changes in rock stress as a function of distance from the fault depends on the specific details of the fault displacement (e.g., magnitude of fault motion, direction of fault movement, extent of the fault that participates in the movement) and the mechanical properties of the surrounding rock (e.g., fracture spacing, fracture stiffness, geomechanical properties of the rock matrix). Given some change in rock stress, the fractured rock mass will respond to the change in stress through deformation, or strain, in the rock. This induced strain can affect the geometry of fractures in the rock.

The effects of stress changes on flow in the UZ have been investigated in *Drift Scale THM Model* (BSC 2004 [DIRS 169864]). In this model, the effects of thermal stress are evaluated in terms of changes to rock fracture properties, but not rock matrix (BSC 2004 [DIRS 169864], Section 6.2); see FEP 2.2.06.01.0A). This modeling approach is used because the effects of

changes to the rock matrix porosity and permeability caused by changes in rock stress are negligible compared with changes to the fracture porosity and permeability. It is reasonable to expect that this should be true for other sources of mechanical stress, such as seismic activity. In theory, the effects of a given fault displacement could be evaluated using process-level calculations for the effects of the induced stress and strain on fracture geometry. However, this direct approach was not further used to specifically evaluate seismic effects because of the large uncertainty in the specification of the seismic event and complexity of translating seismic motion along faults into imposed stresses. An alternative bounding approach was used to assess the potential effects of fault displacement on repository performance (Appendix D).

The sensitivity of radionuclide transport in the UZ to changes in fracture apertures was studied to investigate the effects of fault displacements (Appendix D, Section D3.2.6). This is investigated over a wide enough range to bound the potential changes in fracture aperture that could result from any fault displacement at Yucca Mountain, with an annual exceedance probability of greater than 10^{-8} (Section 5). The largest fault movement close to the repository is likely to be along the Solitario Canyon fault (Appendix D, Section D2.1.1). The general topic of seismic hazard at Yucca Mountain has been investigated in detail in *Probabilistic Seismic Hazard Analyses for Fault Displacement and Vibratory Ground Motion at Yucca Mountain, Nevada* (USGS 1998 [DIRS 100354]). For the Solitario Canyon fault, the hazard analysis shows fault displacement of 10 m (USGS 1998 [DIRS 100354], Figure 8-3) at an annual exceedance probability of 10^{-8} (Section 5). A 10-m fault movement was used as the fault displacement for these analyses. The results of geomechanical models suggest that a factor of 10 change in aperture would bound the effects of tensile strain from a 10-m fault movement (Appendix D). Based on the cubic law for fracture permeability, a factor of 10 change in aperture leads to a factor of 1,000 change in permeability. Fracture permeabilities reduced by a factor of 1,000 were found to be inconsistent with infiltration rates. Therefore, reductions in aperture were limited to factors of 0.2, and in the case of a wetter climate, the lowest value that could be used was a factor of 0.5, leading to permeability reductions of 125 and 8, respectively.

The sensitivity study considered the effects of changes in fracture aperture on porosity, permeability, and capillary pressure (Appendix D, Section D3.2.7). Calculations were then performed for unsaturated flow and transport using the modified fracture properties (Appendix D). Fracture permeabilities reduced by a factor of 1,000 were found to be inconsistent with infiltration rates under wetter climate conditions; therefore, rather than reducing infiltration rates, aperture reduction was limited to a factor of 2, leading to a permeability reduction of a factor of 8.

The combined effects of seismic and thermal stresses also have the potential to produce fracture changes. The general effects of thermal stresses on fracture permeability due to repository heating are evaluated in *Mountain-Scale Coupled Processes (TH/THC/THM)* (BSC 2004 [DIRS 169866], Section 6.5.12). This analysis indicates that in the zones near the repository and below the repository, the fracture permeability is either reduced or unaffected. However, radionuclide transport is slower when the fracture permeability is reduced (Appendix D). Therefore, no additional adverse effects result from the combination of seismic-induced and thermally induced stress changes.

In the context of the TSPA-SR three-dimensional UZ flow and transport model, sensitivity studies for UZ flow and transport presented in this analysis suggest that transport between the repository and the water table is only weakly coupled to changes in fracture aperture. Overall, insignificant changes in transport behavior are found for large changes in fracture aperture. Breakthrough at some points is found to be at most only about one order of magnitude earlier than the base case (under the present-day or the glacial transition climate), for an extremely conservative ten-fold increase in fracture aperture applied over the entire UZ domain. Effects of such magnitude on travel time are less significant than those caused by some of the other uncertainties. For example, infiltration uncertainties (BSC 2004 [DIRS 169861], Section 6.9) result in breakthrough curve uncertainties with more than 3 orders of magnitude variation. Therefore, changes to fracture properties due to seismic activity are excluded because they will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

The results presented in Section D3.3 are supported by scientific notebook YMP-LBNL-GJM-GZ-1, pp. 41-49 (Zhang and Moridis 2004 [DIRS 171212]). These results are also corroborated by an earlier study (CRWMS M&O (2000[DIRS 151953], Section 6.2).

Supporting Reports: Not applicable.

6.8.8 Seismic Activity Alters Perched Water Zones (2.2.06.03.0A)

FEP Description: Strain caused by stress changes from tectonic or seismic events could alter the rock permeabilities that allow formation and persistence of perched-water zones.

Screening Decision: Excluded–Low Consequence.

Screening Argument: Perched water zones below the elevation of the repository have been found in site characterization boreholes. The potential release of perched water (that might contain released radionuclides) as a result of stress changes and fracture openings driven by seismic activity was evaluated using a bounding scenario in which all perched water was suddenly released. Although this may only have a small effect on the ultimate cumulative releases of radionuclides to the SZ, it could focus the radionuclide releases in a relatively sharp "pulse" when the perched water is allowed to drain. This possibility was investigated by considering the volume of perched water in the fracture domain below the repository. The perched water in high-permeability fracture domains is the relevant feature because it is this volume that could potentially be quickly released to the saturated zone. Perched water in the matrix or low-permeability fractures would also ultimately desaturate, but this would be a much slower process and unlikely to cause any temporal pulses of radionuclide flux at the water table. The UZ flow model shows that the volume of perched water in the high-permeability fracture domain below the repository ranges from about 466 m^3 to 1,190 m^3 (Appendix A). This volume may be compared with the water flux entering the repository footprint (i.e., the average infiltration rate times the area of the repository footprint), which ranges from 2,000 m^3/yr to 192,000 m^3/yr (Appendix A). As shown in Appendix A, the perched-water volume is seen to represent about 0.006 to 0.2 years of water flux. Thus, the perched-water volume in high-permeability fractures is small compared to the water flux through the repository horizon

for one year. The sudden release of radionuclides that could be contained in this water volume would not cause a significant "pulse" in radionuclide mass flux at the water table. Therefore, the effects of changes in perched water due to seismic or tectonic effects are excluded from TSPA-LA because they will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. For comparison, note that water table rise caused by climate change in the nominal performance assessment calculations instantly releases radionuclides from a much larger quantity of water in the UZ – on the order of 10^8 m^3 of water (Section 6.2.5, FEP 1.3.07.02.0B). (This is an order of magnitude estimate based on the following data: Repository footprint $\approx 10^7$ m^2 (5×10^6 m^2) (BSC 2004 [DIRS 168370]); Water table rise $\approx$ 100 m (BSC 2004 [DIRS 170037], Section 6.4.5); Water content of rock $\approx$ 0.1 (range from 0.1 to 0.3 BSC 2004 [DIRS 170041], Table 6-6).   Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.8.9   Undetected Features in the UZ (2.2.12.00.0A)

FEP Description: Undetected features in the UZ portion of the geosphere can affect long-term performance of the disposal system. Undetected but important features may be present, and may have significant impacts.   These features include unknown active fracture zones, inhomogeneities, faults and features connecting different zones of rock, different geometries for fracture zones, and induced fractures due to the construction or presence of the repository.

Screening Decision: Excluded–Low Consequence.

Screening Argument: Two kinds of undetected features are of concern: (1) features which, on the basis of previous investigations, could be thought to be present, (2) features totally unexpected. Features that could be present include buried Plio-Pleistocene basaltic intrusions: such features may be the cause of unresolved anomalies in existing geophysical mapping and investigations of such anomalies are ongoing. As discussed in Section 6.8.4, FEP 1.2.10.02.0A, the effects of small intrusions, or more generally, any heterogeneous features approximating meter scale intrusions (or smaller) are expected to have a negligible effect on flow and transport behavior in the UZ. The scenario that a major, critical feature in the vicinity of Yucca Mountain, such as a large seismogenic fault zone, has been overlooked is not expected, given the extensive site characterization conducted at Yucca Mountain (DOE 2004 [DIRS 169734], p. 1-1).

Unexpected features encountered in waste emplacement drifts will be assessed in terms of potential standoffs for waste package emplacement. The design criterion for standoff between Type I faults and repository openings is 60 m (Doraswamy 2004 [DIRS 167101], Section 4.11.2). By way of corroboration and clarification, the following standoff requirements have been identified in *Underground Layout Configuration* (BSC 2003 [DIRS 165572], Sections 7.1.3 and 7.3.1):

> It is conservatively estimated that a 60-meter (197-foot) standoff from the trace of
> any Type I fault is adequate to reduce the impact of potential fault movement.
> This standoff considers potential fractured ground in proximity of the Type I fault

and uncertainty as to where the fault is located at depth. The use of a 60-meter (197-foot) standoff for a LA design is conservatively applied.

In the event that the standoff from repository openings to a Type I fault is waived following a site impact analysis, a standoff must be maintained between Type I faults and any waste package. A standoff must be maintained between splays associated with Type I faults and any waste package. Areas that contain Type I faults should be avoided, but if unavoidable, they must be allowed for in engineering design. It is conservatively estimated that a standoff from the edge of the Type I fault or fault zone by 15 meters (49 feet) is adequate to reduce the impact of potential fault movement. Using a 15-meter (49-foot) standoff to establish useable drift length for the LA design is conservatively applied.

Induced fractures may occur near waste emplacement drifts due to the disturbance of the rock stress field caused by the presence of the drift openings. Induced fractures are not unexpected features and are included by default in underground testing of drift seepage as discussed in Section 6.2.9 (FEP 2.2.01.01.0A)

The major effect of fault features and fracture zones on flow and transport patterns below the repository is to allow downward pathways for flow that has been diverted laterally (BSC 2004 [DIRS 169861], Sections 6.2.2.1 and 6.6.3). The effects of the fault properties have been found to be much less important in terms of radionuclide transport behavior (Appendix D). Lateral diversion beneath the repository is affected significantly by the presence of perched water bodies, which are postulated to exist as a result of permeability barriers (BSC 2004 [DIRS 169861], Sections 6.2.2.2 and 6.6.3). The effects of flow path diversion on transport may be evaluated based on the alternative perched water models presented in *UZ Flow Models and Submodels* (BSC 2001 [DIRS 158726], Section 6.2.2. Perched water models #1 and #2 are named the "flow-through" perched water model and "by-passing" perched water model, respectively (BSC 2001 [DIRS 158726], Section 6.2.2). For model #1, the minimum permeability barriers are introduced to produce the known perched water bodies. For model #2, all zeolitic units are modeled as unfractured and result in more extensive perched water. As the names imply, there is less lateral diversion in model #1 as compared with model #2 (BSC 2001 [DIRS 158726], Section 6.2.5). An extreme case is "no perched water" model #3, which does not introduce any permeability barrier, leading to minimal lateral flow. However, this model is not supported by the data because it does not predict perched water where such features are known to exist.

Comparisons for transport between the repository and the water table for the three perched water models were performed using sorbing and nonsorbing radionuclides (BSC 2001 [DIRS 158726], Section 6.7.2). The transport results for perched water models #1 and #2 have only minor differences (BSC 2001 [DIRS 158726], Figures 6-54 through 6-56). Although early breakthroughs are more substantial for model #3, transport times are about the same or longer after 1,000 years for both sorbing and nonsorbing radionuclides. Furthermore, the effect of a finite number of undetected fault features that could potentially act as pathways to the water table necessarily has less impact on flow pathways than model #3, as evidenced by the existence of large perched water bodies. Therefore, this FEP is excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible

environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.9 REPOSITORY-PERTURBED THMC

This group of FEPs is excluded from the TSPA-LA calculation. These FEPs concern the effects of changes to the thermal/hydrological/mechanical/chemical (THMC) environment as a result of repository excavations, heat, and materials, and the effects of these changes on hydrological, geochemical, and geomechanical processes.

Table 6-10 gives the FEP numbers and names categorized under Repository-Perturbed THMC.

Table 6-10. Excluded FEPs: Repository-Perturbed THMC

Section Number	FEP Number	FEP Name
6.9.1	2.1.09.12.0A	Rind (chemically altered zone) forms in the near-field
6.9.2	2.2.01.01.0B	Chemical effects of excavation and construction in the near-field
6.9.3	2.2.01.02.0A	Thermally-induced stress changes in the near-field
6.9.4	2.2.01.03.0A	Changes in fluid saturations in the excavation disturbed zone
6.9.5	2.2.01.04.0A	Radionuclide solubility in the excavation disturbed zone
6.9.6	2.2.01.05.0A	Radionuclide transport in the excavation disturbed zone
6.9.7	2.2.08.03.0B	Geochemical interactions and evolution in the UZ
6.9.8	2.2.08.07.0B	Radionuclide solubility limits in the UZ
6.9.9	2.2.10.01.0A	Repository-induced thermal effects on flow in the UZ
6.9.10	2.2.10.04.0A	Thermo-mechanical stresses alter characteristics of fractures near repository
6.9.11	2.2.10.04.0B	Thermo-mechanical stresses alter characteristics of faults near repository
6.9.12	2.2.10.05.0A	Thermo-mechanical stresses alter characteristics of rocks above and below the repository
6.9.13	2.2.10.06.0A	Thermo-chemical alteration in the UZ (solubility, speciation, phase changes, precipitation/dissolution)
6.9.14	2.2.10.07.0A	Thermo-chemical alteration of the Calico Hills unit
6.9.15	2.2.10.09.0A	Thermo-chemical alteration of the Topopah Spring basal vitrophyre
6.9.16	2.2.10.14.0A	Mineralogic dehydration reactions
6.9.17	2.2.08.05.0A	Diffusion in the UZ

DTN: MO0407SEPFEPLA.000 [DIRS 170760].

6.9.1 Rind (Chemically Altered Zone) Forms in the Near-Field (2.1.09.12.0A)

FEP Description: Thermal-chemical processes involving precipitation, condensation, and re-dissolution could alter the properties of the adjacent rock. These alterations may form a rind, or altered zone, in the rock, with hydrological, thermal, and mineralogical properties different from the initial conditions.

Screening Decision: Excluded–Low Consequence.

Screening Argument: The thermal-chemical interactions that will occur in the repository environment have been studied with respect to effects on the seepage water entering the waste emplacement drifts using the THC seepage model (BSC 2004 [DIRS 169856]). This model, which explicitly captures the effects of changes in temperature, pH, Eh, ionic strength (and other compositional variables), time dependency, precipitation or dissolution effects, and effects of resaturation, was used to examine near-field and drift seepage flow and chemistry (BSC 2004 [DIRS 169856], Section 6.2). Changes in fracture permeabilities were found to be on the order of the natural variation in these properties (BSC 2004 [DIRS 169856], Section 6.5.5.3; BSC 2004 [DIRS 170038], Table 6-5), with most of the substantial effects limited to regions above and to the side of the drift within about a drift diameter (BSC 2004 [DIRS 169856], Figures 6.5-39 and 6.5-40). The predicted mineral precipitation reduces permeability in the affected regions and leads to a reduction in flow around the drift. Likewise, any mineralogical changes are of very limited extent below the drift, resulting in negligible effects on radionuclide sorption (BSC 2004 [DIRS 169866], Section 6.4.3.3.3). THC effects on fracture characteristics have been evaluated with process models that explicitly account for fracture flow affected by THC parameter alterations (BSC 2004 [DIRS 169131], Section 6.4.4.2). It was demonstrated that the effects of these potential alterations on near-field and drift seepage flow can be neglected in the TSPA-LA, because the expected changes would lead to less seepage (BSC 2004 [DIRS 169131], Section 6.5.1.4). Consequently, neglect of this effect is likely to result in slightly conservative model predictions for both drift seepage and radionuclide transport phenomena. Therefore, this FEP is excluded because it will have no adverse affects on the radiological exposures to the RMEI, or radionuclide release to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Note that the THC effects (e.g., mineral precipitation) on fracture characteristics as they relate to near-field and drift seepage chemistry were also evaluated with the THC seepage model. A discussion is provided in FEP 2.2.03.02.0A.

Supporting Reports: Not applicable.

6.9.2   Chemical Effects of Excavation and Construction in the Near-Field (2.2.01.01.0B)

FEP Description: Excavation may result in chemical changes to the incoming groundwater and to the rock in the excavation disturbed zone.

Screening Decision: Excluded–Low Consequence.

Screening Argument: This FEP concerns the changes in the host rock environment immediately surrounding the waste emplacement drifts. Related FEP 1.1.02.00.0A (Chemical effects of excavation and construction in the EBS) is discussed in *Engineered Barrier System Features, Events, and Processes* (BSC 2004 [DIRS 169898, Section 6.2.1]). Changes are expected in the rock fracture properties from excavation disturbance, stress relief around the opening, and ground support. However, these changes will not affect water chemistry. Excavation will introduce water (for dust control), but this should not have any significant effect on water chemistry. This is based on the limited volumes of water that are typically lost during underground excavation (for example, for ESF construction the average was required to be less

than 7.4 m^3 per meter of tunnel length, with a projected tunnel width of 7.6 m, or approximately 1 m^3/m^2 of the projected horizontal area of an excavation (BSC 2002 [DIRS 160689], Section 13.2.16). Furthermore, any water that remains local to the emplacement drifts will be more strongly affected by ventilation and thermal dryout. Any construction water that penetrates the UZ deeply through fractures is not likely to have any significant interaction with released radionuclides. The ground support for the emplacement drifts can affect water flow patterns in the immediate vicinity of the drift and can affect the aqueous geochemistry in the drift environment and along flow pathways from the drift to the water table. However, detailed simulations were made using the predictive seepage model for performance assessment (BSC 2004 [DIRS 167652], Section 6.5) to study the effect of rock bolts in the drift crown on seepage into drifts. The effect of these features was found to have only a minor effect on seepage (less than 2 percent (BSC 2004 [DIRS 167652], Table 6-4)), owing to the small area for water to enter the rock-bolt boreholes from the surrounding formation (BSC 2004 [DIRS 169131], Section 6.4.2.5). From these results, the presence of rock bolts is not considered a relevant factor for seepage into drifts. Based on this finding, only a minor quantity of the total water intercepting a drift is likely to move through rock-bolt pathways. Other ground-support materials will not affect flow patterns in the rock, because these materials are entirely within the emplacement drift.

The principal ground support in the emplacement drifts is expected to be SS 316L rock bolts and steel sheets (BSC 2004 [DIRS 169058]). A model of the effects of steel ground support on aqueous chemistry was recently generated (BSC 2004 [DIRS 169860], Section 6.8). The model considered the interaction of "Bin 11" water with SS 316L ground support materials. Interaction with the abstracted "Bin 11" seepage water was chosen, because this is the most likely water to be present, occurring in almost 40 percent of the abstracted periods (BSC 2004 [DIRS 169860], Table 6.6-4). In addition, this Bin 11 water is seen to occur during the relevant period for the corrosion of 316L stainless steel, in the range of ~500 to 5,000 years for four of the five seepage water compositions shown in *Engineered Barrier System: Physical and Chemical Environment* (BSC 2004 [DIRS 169860], Tables 6.6-8 through 6.6-12). The effect of dissolving the abstracted SS316L steel species into Bin 11 water was found to be negligible. The Bin 11 water with and without the 5.52×10^{-5} moles of SS316L added was found to only have two differences in the water chemistries at the 6th significant figure for ionic strength and C total molality (BSC 2004 [DIRS 169860], Section 6.8.4.3). Use of "Bin 7" seepage water was selected as an uncertainty case and is described in *Engineered Barrier System: Physical and Chemical Environment* (BSC 2004 [DIRS 169860], Section 6.12.4.1). There is effectively no change in the aqueous water chemistry caused by abstracted stainless steel corrosion and corrosion product formation in this case, as with the basecase Bin 11 seepage water (BSC 2004 [DIRS 169860], Section 6.12.4.1.3).

Cementitious material (shotcrete) is planned for use as part of the ground support for the turnout intersections of the main access drifts and for the turnouts and intersections of the exhaust drifts with the emplacement drifts (BSC 2004 [DIRS 170058]). The incorporation of cementitious materials in the repository poses two concerns. The first is that the leaching of cementitious materials, particularly the shotcrete supporting the turnout intersections in the main access drifts and the intersections of the exhaust main drifts with the emplacement drifts, will affect repository performance by modifying the hydrologic properties of the surrounding rock and diverting the flow of water entering the drifts. The second concern is that an alkaline plume resulting from leaching of the cementitious material could enhance radionuclide transport to the

accessible environment, either through the complexation of radionuclides or through the presence of pseudocolloids.

No cementitious material will be used in the emplacement drifts (BSC 2004 [DIRS 169058]). In nonemplacement drifts, all cementitious material (concrete invert and shotcrete used in shafts) will be removed prior to closure except that necessary for ground support (BSC 2004 [DIRS 171676], Section 3.1.1.15.1). The only significant cementitious materials remaining in the repository will be shotcrete supports and grout for rock bolt placement in nonemplacement drifts and turnout intersections. These materials can result in changes in water composition, particularly alkalinity and sulfate concentration (Hardin 1998 [DIRS 100123], Section 6.3.4).

The scientific and technical basis for the impact of shotcrete support structures and rock-bolt grout on repository performance, in relation to potential modifications to the hydrology and the effect of cementitious leachates on radionuclide migration, is presented by Ziegler (2004 [DIRS 171694]). Several factors, including direct carbonation of the cement itself due to CO_2 gas diffusion and carbonation of any hyperalkaline plume that is generated as a result of cement-water interaction. Direct carbonation of the cement consumes portlandite and other high-pH phases, thus, rendering it benign. Diffusion of CO_2 gas into the hyperalkaline plume, if generated, reduces the pH and calcium concentration in solution through acidification and calcite precipitation. These processes will result in leachate from the cementitious materials and their reaction products being similar in water quality to ambient porewater (DTN: LB0408CMATUZFT.004 [DIRS 171706]). Therefore, the presence of cementitious materials will not significantly change the transport of radionuclides. Plumes of leachate from cementitious materials, where not completely neutralized by interaction with CO_2, may intersect radionuclide transport plumes from failed waste packages as they spread by diffusion and dispersion (DTN: LB0408CMATUZFT.003 [DIRS 171705]), but because the cementitious materials are only used in the turnouts (that is, at the ends) of emplacement drifts, and flow is mainly vertical in the UZ, such contact is somewhat limited, and as mentioned above, would not significantly affect radionuclide transport. Water is expected to move in a general vertical flow pattern through the waste emplacement horizon relative to the length scale of these drifts, with some flow diversion around the drifts resulting from the capillary barrier effect. This flow pattern is consistent with the drift-scale seepage model having no-flow lateral-boundary conditions (BSC 2004 [DIRS 167652], Section 6.3.1).

The low levels of lateral dispersion are apparent in the simulations of chloride plumes (BSC 2004 [DIRS 169866], Section 6.4.3.3.2, Figure 6.4-15) in which the plume variations between individual drifts and pillars between drifts are maintained from the repository to the water table. This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.9.3   Thermally Induced Stress Changes in the Near-Field (2.2.01.02.0A)

FEP Description: Changes in host rock properties may result from thermal effects or other factors related to emplacement of the waste. Properties that may be affected include rock strength, fracture spacing and block size, and hydrologic properties such as permeability and sorption.

Screening Decision: Excluded–Low Consequence.

Screening Argument: The results of the coupled drift-scale THM model presented in *Drift Scale THM Model* (BSC 2004 [DIRS 169864], Sections 6.5, 6.6, and 6.9) shows that the impact of time-dependent THM processes will last for well over 10,000 years, but these processes have a small or moderate impact on the drift scale TH behavior, including a negligible impact on the temperature evolution and small impact on the percolation flux. The model accounts for rock strength and fracture spacing. Rock strength is modeled as independent of temperature (BSC 2004 [DIRS 169864], Table 6.4.5-1). Similarly, fracture frequency (or spacing) is also modeled as independent of temperature (BSC 2004 [DIRS 169864], Table 4.1-3a). The THM model, including these parameterizations, were found to compare well with measured rock mechanical behavior in the drift-scale test (BSC 2004 [DIRS 169864], Section 7.4.2). These model results were obtained for a conservative estimate of input THM properties (thermal expansion coefficient and stress versus permeability function), which is sufficient for bounding the possible impact of the THM processes on permeability and percolation flux.

The THM simulations discussed in *Drift Scale THM Model* (BSC 2004 [DIRS 169864], Sections 6.5 through 6.7) suggest that temperature-induced stress decreases the vertical fracture permeability in the vicinity of waste emplacement drifts, especially in the Tptpmn unit (BSC 2004 [DIRS 169864], Figure 6.5.4-1). The vertical fracture permeability changes more than the horizontal fracture permeability because thermal expansion in the horizontal direction is constrained by surrounding rock, while expansion in the vertical direction is not constrained (that is, the ground surface can rise). However, these permeability changes do not result in significant changes in the flow fields (BSC 2004 [DIRS 169864], Sections 6.5.5 and 6.6.2). In particular, the seepage rates calculated for a permeability field including THM permeability changes were similar to, but slightly smaller than, those calculated for a permeability field representative of the initial postexcavation conditions. The simulation results from *Drift Scale THM Model* (BSC 2004 [DIRS 169864]) provide slightly conservative estimates of the expected seepage rates at long-term conditions with coupled THM property changes (BSC 2004 [DIRS 169131], Section 6.4.4.1). Therefore, the impact of THM property changes is neglected in the seepage abstraction.

Thermal effects on sorption are evaluated in Section 6.9.13 (FEP 2.2.10.06.0A). Thermal effects on fracturing, block size, rockfall, and drift degradation are included in the analysis of drift degradation (BSC 2004 [DIRS 166107], Sections 6.3 and 6.4)

The overall effect of THM coupled processes on drift-scale radionuclide transport may also be excluded, because the primary effect of THM processes leads to enhanced seepage diversion and reduced drift seepage, reduced water saturations beneath the drift and, therefore, greater partitioning of radionuclide releases to the rock matrix. This FEP is, therefore, excluded because

it will have no adverse affects on the radiological exposures to the RMEI, or radionuclide release to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.9.4 Changes in Fluid Saturations in the Excavation Disturbed Zone (2.2.01.03.0A)

FEP Description: Fluid flow in the region near the repository may be affected by the presence of the excavation, waste, and EBS. Some dry-out will occur during excavation and operations.

Screening Decision: Excluded–Low Consequence.

Screening Argument: Inclusion of preclosure dryout is not significant for thermal seepage (BSC 2004 [DIRS 170338], Section 6.2.1.3.3). The overall effect of ventilation dryout on drift-scale radionuclide transport may also be excluded, because thermal dryout and rewetting will erase nearly any effect of the ventilation dryout. Sensitivity studies in *FY 01 Supplemental Science and Performance Analyses, Volume 1: Scientific Bases and Analyses* (BSC 2001 [DIRS 155950], Section 5.3.2.4.4) indicate that inclusion of preclosure dryout gives rise to slightly higher temperatures during the heating period compared to a model that ignores the influence of preclosure dryout. Therefore, this FEP may be excluded based on low consequence. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Other aspects of this FEP are discussed elsewhere. For the effects of the excavation on fluid flow, see FEP 2.2.07.20.0A; for the effects of waste heat on fluid flow, see FEPs 2.2.10.10.0A and 2.2.10.12.0A; for the effects of the EBS (rock bolt holes) on fluid flow, see FEP 1.1.01.01.0B.

Supporting Reports: Not applicable.

6.9.5 Radionuclide Solubility in the Excavation Disturbed Zone (2.2.01.04.0A)

FEP Description: Radionuclide solubility limits in the excavation-disturbed zone may differ from those in the EBS.

Screening Decision: Excluded–Low Consequence.

Screening Argument: If solubility limits are lower in the EDZ than in the emplacement drifts, then some dissolved radionuclides will precipitate as water flows out of the drifts. In this case, exclusion of the FEP would not result in an underestimation of radionuclide transport. The magnitude of this conservative approximation may be qualitatively evaluated through a comparison of the different ranges of chemical environments estimated for the engineered barrier system as compared with the EDZ and UZ in general. The pH of waters inside the drift range from less than 5 to more than 10 (BSC 2004 [DIRS 169860], Figures 6.13-2 through 6.13-12). The evolution of water chemistry in the UZ, however, is not so broad. Near the drift the pH ranges from roughly 7 to 8.5 (BSC 2004 [DIRS 169856], Figures 6.5-12, 6.5-25, 6.5-58). Further out into the rock, the pH ranges from about 7 to 9 (BSC 2004 [DIRS 169866],

Figures 6.4-11, 6.4-13, 6.4-14, 6.4-17). Given the much larger range of pH inside the drift, equilibrium solution concentrations for radionuclides inside the drift could be significantly larger than equilibrium solution concentrations in the UZ. See also Section 6.9.6 (FEP 2.2.01.05.0A) for additional information on this subject. If solubility limits are higher in the EDZ than in the emplacement drifts, then radionuclides entering the EDZ will remain in solution and there will be no effect on radionuclide transport.

Solubility limits could also affect the formation of certain kinds of true colloids, such as polymeric forms of plutonium oxide (BSC 2004 [DIRS 170025], Section 6.3.1). However, these forms of colloids have not been observed to form in experiments on waste form degradation (BSC 2004 [DIRS 170025], Section 6.3.1). Furthermore, these colloids are expected to undergo formation of pseudocolloids in the near-field aquifer system (BSC 2004 [DIRS 170025], Section 6.3.1) and are, therefore, excluded.

Therefore, the effects of different solubility limits in the EDZ are excluded because they will have no adverse affects on the radiological exposures to the RMEI, or radionuclide release to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.9.6 Radionuclide Transport in the Excavation Disturbed Zone (2.2.01.05.0A)

FEP Description: Radionuclide transport through the excavation disturbed zone may differ from transport in the EBS and the undisturbed host rock. Transport processes such as dissolution and precipitation, sorption, and colloid filtration should be considered.

Screening Decision: Excluded–Low Consequence.

Screening Argument: This FEP refers to the effects of altered fracture properties in the disturbed zone immediately surrounding the waste emplacement drifts on radionuclide transport. The effects of changes in fracture aperture on radionuclide transport were investigated at the mountain scale (FEP 2.2.06.02.0B and Appendix D). The results of this analysis indicate that transport behavior is relatively insensitive to changes in fracture aperture by as much as a factor of 10. Drift-scale radionuclide transport analyses showed that the partitioning of radionuclides between fractures and matrix upon exiting the drift is also dependent upon the fracture water content (BSC 2004 [DIRS 170040], Sections 6.4 and 6.4.2). This parameter is treated as uncertain in the drift-scale transport model (BSC 2004 [DIRS 170040], Section 6.4.5). However, the uncertainty in fracture water content is dominated by the uncertainty in fracture residual saturation. The uncertainty for fracture residual saturation uses a broad range (0.001 to 0.1) based on experimental data for higher permeability capillary materials (BSC 2004 [DIRS 170040], Section 6.4.5). However, due to limited information regarding functional dependencies, this is not treated as a function of fracture aperture. Therefore, the neglect of the EDZ is not significant in terms of uncertainty for the residual saturation. Investigations on the effects of stress relief on fracture permeability in the EDZ have found that the vertical permeability beneath the drift is affected over a very narrow zone, on the order of 1 to 2 meters for changes in permeability more than a factor of 2 (BSC 2004 [DIRS 169864], Sections 6.5.1

and 6.6.1). Therefore, the limited extent of the EDZ compared with the overall transport path length in the UZ (approximately 300 m) also leads to the conclusion that the effects of the EDZ is negligible for colloid and radionuclide transport. Therefore, the effects of altered fracture properties in the EDZ are excluded because they will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

The effects of precipitation of aqueous radionuclides on transport in the EDZ also are excluded (FEP 2.2.01.04.0A). Excluding precipitation for radionuclides that undergo simple decay is conservative because this can only enhance the radionuclide mass flux at the accessible environment. For radionuclides that undergo chain decay, excluding precipitation will be conservative because the radionuclide source is not significantly depleted within the 10,000-year regulatory time period. In the latest total-system performance assessment, dose rates for all radionuclides are predicted to increase over tens of thousands of years (CRWMS M&O 2000 [DIRS 153246], Figures 4.1-5 and 4.1-7). This is a result of the spread of waste package failures over time (CRWMS M&O 2000 [DIRS 153246], Figure 4.1-9) and the slow release of radionuclides from the waste emplacement drifts. Therefore, during the 10,000-year period, the highest concentration for any radionuclide at the receptor is expected to occur under conditions giving the greatest transport rates. Reduced solubilities for neptunium, americium, plutonium, thorium, and uranium were investigated as a sensitivity in TSPA-SR (CRWMS M&O 2000 [DIRS 153246], Sections 3.5.5, 4.1.3, and Figures 4.1-19a and 4.1-20). The dose rates for radionuclides affected by the lower solubilities (including decay products such as ^{226}Ra) were found to be lower in the reduced-solubility case. This leads to the conclusion that suppressing precipitation of radionuclides in the TSPA-LA model results in higher calculated dose rates. Therefore, precipitation of radionuclides is excluded; this exclusion leads to underestimation of repository performance.

The principal effects of the near-field environment on transport are temperature and geochemical environment. Thermal effects on sorption are evaluated in Section 6.9.13 (FEP 2.2.10.06.0A), where increased temperatures are found to lead to increased sorption. Compositional variations found at the base of the drift in *Drift-Scale THC Seepage Model* (BSC 2004 [DIRS 169856], Figures 6.5-12 to 6.5-20) lie within the range of compositional variations expected in the unsaturated zone and accounted for in terms of radionuclide sorption (BSC 2004 [DIRS 164500], Section A4).

Supporting Reports: Not applicable.

6.9.7 Geochemical Interactions and Evolution in the UZ (2.2.08.03.0B)

FEP Description: Groundwater chemistry and other characteristics, including temperature, pH, Eh, ionic strength, and major ionic concentrations, may change through time, as a result of the evolution of the disposal system or from mixing with other waters. Geochemical interactions may lead to dissolution and precipitation of minerals along the groundwater flow path, affecting groundwater flow, rock properties, and sorption of radionuclides. Effects on hydrologic flow properties of the rock, radionuclide solubilities, sorption processes, and colloidal transport are

relevant. Kinetics of chemical reactions should be considered in the context of the time scale of concern.

Screening Decision: Excluded–Low Consequence.

Screening Argument: The thermal-chemical interactions that will occur in the repository environment have been studied with respect to effects on the seepage water entering the waste emplacement drifts using the THC seepage model (BSC 2004 [DIRS 169856]). This model, which explicitly captures the effects of changes in temperature, pH, Eh, ionic strength (and other compositional variables), time dependency, precipitation or dissolution effects, and effects of resaturation, was used to examine near-field and drift seepage flow and chemistry (BSC 2004 [DIRS 169856], Section 6.2). Changes in fracture permeabilities were found to be on the order of the natural variation in these properties (BSC 2004 [DIRS 169856], Section 6.5.5.3 and BSC 2004 [DIRS 170038], Table 6-5), with most of the substantial effects limited to regions above and to the side of the drift within about a drift diameter (BSC 2004 [DIRS 169856], Figures 6.5-39, 6.5-40). The predicted mineral precipitation reduces the permeability in the affected regions, and leads to a reduction in flow around the drift. These effects may be excluded because including such changes in fracture permeability would result in lower predicted doses in TSPA. Note that the effects of mineral precipitation on fracture permeability as it relates to near-field and drift seepage chemistry was also evaluated with the THC seepage model. A discussion is provided in Section 6.2.11, FEP 2.2.03.02A.

The geochemical model includes the major solid phases (minerals and glass) encountered in geological units at Yucca Mountain, together with a range of possible reaction product minerals, CO_2 gas, and the aqueous species necessary to include these solid phases and the porewater composition within the THC model (BSC 2004 [DIRS 169856], Table 6.2-2). Compositional changes were only calculated near the drift boundary for the drift-scale THC seepage model (BSC 2004 [DIRS 169856]). Results from these simulations show most compositional variations returning to unperturbed conditions in 10,000 years or less. Variations in pH (BSC 2004 [DIRS 169856], Figures 6.5-12 and 6.5-25), a key compositional variable for sorption of some radionuclides (BSC 2004 [DIRS 164500], Appendix A), roughly lie within the range of variability investigated for initial porewater compositions (BSC 2004 [DIRS 169856], Table 6.2-1). Bicarbonate is found to be depressed in concentration upon water resaturation at the drift wall, as expected based on the reduced pH values for the same time period.

Results were also investigated for the Tptpll (lower lithophysal unit) model considering a range of initial porewater compositions. In this model, five different initial porewater compositions were investigated (BSC 2004 [DIRS 169856], Table 6.2-1). Peak concentrations usually found at the time of rewetting in both models reflect mostly the small values of the first nonzero liquid-saturation output. In any case, elevated concentrations are predicted only for small liquid saturations that are not subject to significant fluid movement. The improved treatment of mineral precipitation at the boiling front used in the most recent THC model for the Tptpll also results in the prediction of lower, more realistic aqueous silica concentrations than in earlier models (BSC 2004 [DIRS 169856], Figure 6.5-16). This model also predicts upon rewetting, more rapid return to near-ambient conditions for aqueous Ca, Na, and Cl.

The findings indicate that at the drift wall, most of the significant compositional variations resulting from thermal-chemical processes are limited to low-saturation conditions over time periods that are short relative to the 10,000-year performance period. Similar magnitudes of variation in chloride and pH were found in the mountain-scale THC model results (BSC 2004 [DIRS 169866], Section 6.4.3.3.2). The magnitudes of the variations are found to be smaller at greater distances from the drift wall. As for the drift-scale study, variations in chloride are driven mainly by evaporation and are found to return to near-ambient values upon rewetting (BSC 2004 [DIRS 169866], Section 6.4.3.3.2). Variations in pH were found to lie roughly between 7 and 9, which is similar to the results for the drift-scale THC model (BSC 2004 [DIRS 169856], Figures 6.5-12, 6.5-25 and 6.5-58). The most persistent change in pH is a level of about 7 in the Calico Hills, down from values between 7.5 and 8 (BSC 2004 [DIRS 169866], Section 6.4.3.3.2, Figure 6.4-17), but this lies within the range of pH investigated for radionuclide sorption (BSC 2004 [DIRS 164500], Appendix A). Therefore, the effects of these changes are excluded because they will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.9.8 Radionuclide Solubility Limits in the UZ (2.2.08.07.0B)

FEP Description: Solubility limits for radionuclides may be different in unsaturated zone groundwater than in the water in the waste and EBS.

Screening Decision: Excluded–Low Consequence.

Screening Argument: In general the conditions that control the solubility of radionuclides will be different in the invert of the EBS and in the UZ, and may vary in the UZ with location and time. The conditions that control radionuclide solubility are identified in *Dissolved Concentration Limits of Radioactive Elements* (BSC 2004 [DIRS 169425]) and include pH, fugacity of CO_2, concentration of fluoride ion, and temperature. These variables are not all independent: at higher temperature, CO_2 gas is less soluble. This reduces the solubility of carbonate complexes, which at high pH are the species that contribute the most to actinide solubilities. The result is that actinides are less soluble at higher temperatures (BSC 2004 [DIRS 169425, Section 6.3.3.3, but note that only solubility limits at 25°C are used for TSPA). The drifts will be hotter than the UZ beneath the drifts at least for the first 8000 years (BSC 2004 [DIRS 169866], Figure 6.3.1-6). This suggests, therefore, that actinide solubility limits will be greater in the UZ than in the drift and will increase downward toward the water table. This will not necessarily be the case at every location or at every time. Therefore, both cases of solubility in the UZ are considered being greater and less than in the invert of the EBS.

If solubility limits are higher in the geosphere than in the emplacement drifts, then there is no effect on transport because all available radionuclides that were transported from the emplacement drift are already aqueous species.

If solubility limits are lower in the geosphere than in the emplacement drifts, then some dissolved radionuclides will precipitate there. This would reduce the amount of dissolved radionuclides available for transport in the geosphere. Subsequent cooling may increase the solubility, restoring the precipitated radionuclides to the aqueous phase; in this case precipitation would delay, but not prevent, transport of radionuclides. It is, therefore, conservative to neglect precipitation. The magnitude of this conservative approximation may be qualitatively evaluated through a comparison of the different ranges of chemical environments estimated for the engineered barrier system as compared with the UZ. The pH of waters inside the drift range from less than 5 to more than 10 (BSC 2004 [DIRS 169860], Figures 6.13-2 through 6.13-12). The evolution of water chemistry in the UZ, however, is not so broad. Near the drift the pH ranges from roughly 7 to 8.5 (BSC 2004 [DIRS 169856], Figures 6.5-12, 6.5-25, 6.5-58). Further out into the rock, the pH ranges from about 7 to 9 (BSC 2004 [DIRS 169866], Figures 6.4-11, 6.4-13, 6.4-14, 6.4-17). Given the much larger range of pH inside the drift, equilibrium solution concentrations for radionuclides inside the drift could be significantly larger than equilibrium solution concentrations in the UZ.

Solubility limits could also affect the formation of certain kinds of true colloids, such as polymeric forms of plutonium oxide (BSC 2004 [DIRS 170025], Section 6.3.1). However, these forms of colloids have not been observed to form in experiments on waste form degradation (BSC 2004 [DIRS 170025], Section 6.3.1). Furthermore, these colloids are expected to undergo formation of pseudocolloids in the near- or far-field aquifer system (BSC 2004 [DIRS 170025], Section 6.3.1) and are, therefore, excluded.

Analysis of coupled THC effects indicates that only small changes in hydrologic properties and mineralogy a result from these coupled processes (BSC 2004 [DIRS 169856], Section 6). Therefore, far-field changes are likewise expected to be small, including mineral precipitation or dissolution and alteration of minerals such as zeolites and clays. Therefore, coupled thermal-hydrologic-chemical effects on radionuclide transport properties and the effects of different solubility limits in the geosphere are excluded because they will have no adverse affects on the radiological exposures to the RMEI, or radionuclide release to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.9.9   Repository-Induced Thermal Effects on Flow in the UZ (2.2.10.01.0A)

FEP Description: Thermal effects in the geosphere could affect the long-term performance of the disposal system, including effects on groundwater flow (e.g., density-driven flow), mechanical properties, and chemical effects in the UZ.

Screening Decision: Excluded–Low Consequence.

Screening Argument: Thermal-hydrologic modeling at the mountain scale has been performed using two-dimensional cross-sectional and three-dimensional dual-permeability models (BSC 2004 [DIRS 169866], Section 6.1.2). During the early part of the heating period, important TH processes occur near the emplacement drifts. The mountain-scale models are used to capture

the TH behavior at later times, when the perturbation in temperature, and fracture and matrix liquid saturation, extends over a much larger space domain compared to the drift-scale effects. These mountain-scale TH processes include repository edge effects, large-scale enhanced water and gas flow, and potential alteration of perched-water bodies. Results from the modeling indicate that the induced flow from TH processes are much smaller than changes in flow resulting from climate change at 600 and 2,000 years (BSC 2004 [DIRS 169866], Figures 6.2-10a and b, 6.3.1-18), which are included in the flow and transport models (Section 6.2.4, FEP 1.3.01.00.0A). Percolation flux maps at the top of the CHn for the ambient and thermally perturbed case (at 500 years of heating) show very similar flow patterns with the exception of reduced flow through a central portion of the waste emplacement area under the thermally perturbed case (BSC 2004 [DIRS 169866], Figures 6.3.1-16a and b). For thermal effects on chemical processes, see FEPs 2.2.08.03.0B, 2.2.10.06.0A, 2.2.10.07.0A, and 2.2.10.09.0A. For thermal effects on mechanical processes, see FEPs 2.2.10.04.0A, 2.2.10.04.0B, and 2.2.10.05.0A.

Numerical simulations of flow at 100 years and 500 years after emplacement show reduced fracture saturation and diversion of percolating water around the dryout zone (BSC 2004 [DIRS 170338], Section 6.2.2.1). Because of the flow diversion, the dryout is more extensive and longer lasting beneath the drift; this is called the "drift shadow" effect. Note that there is no water flux inside the dryout region, because fracture saturation is zero. After resaturation in 1,000 to 2,000 years, saturations below the drift remain smaller than above, because of the "shadow zone" created by the diversion of flow around the drift (BSC 2004 [DIRS 170338], Section 6.2.2.1). In general, the TH dryout and associated coupled processes will lead to an environment where radionuclide transport in the vicinity of the drift is less likely (BSC 2004 [DIRS 170338], Section 6.2.2.1.1; BSC 2004 [DIRS 169856], Section 6.5.5.3).

The effects of repository heat and the associated dryout on shallow infiltration at the surface of Yucca Mountain were investigated in CRWMS M&O (1999 [DIRS 105031]). The primary issue for thermal effects at the ground surface is the change in temperature and its associated effect on vegetation. Based on the detailed analysis of soil temperature changes documented in CRWMS M&O (1999 [DIRS 103618]), the temperature rise will have a negligible effect on vegetation, and hence on surface infiltration.

This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Note that the effects of thermal-hydrologic processes on drift seepage and seepage water chemistry are addressed in FEPs 2.2.07.10.0A, 2.2.07.11.0A, 2.2.08.12.0A, 2.2.10.10.0A; and 2.2.10.12.0A.

Supporting Reports: Not applicable.

6.9.10 Thermo-Mechanical Stresses Alter Characteristics of Fractures near Repository (2.2.10.04.0A)

FEP Description: Heat from the waste causes thermal expansion of the surrounding rock, generating changes in the stress field that may change the properties (both hydrologic and mechanical) of fractures in the rock. Cooling following the peak thermal period will also change the stress field, further affecting fracture properties near the repository.

Screening Decision: Excluded–Low Consequence.

Screening Argument: The results of the coupled drift-scale thermal-hydrological-mechanical (THM) model presented in *Drift Scale THM Model* (BSC 2004 [DIRS 169864], Sections 6.5 and 6.6) show that the impact of time-dependent, THM processes will last for well over 10,000 years. These processes have a small or moderate impact on the drift scale TH behavior, including a negligible impact on the temperature evolution and small impact on the percolation flux (BSC 2004 [DIRS 169864], Section 6.9). These model results were obtained for a conservative estimate of input THM properties (thermal expansion coefficient and stress versus permeability function), which is sufficient for bounding the possible impact of the THM processes on permeability and percolation flux.

The THM simulations discussed in *Abstraction of Drift Seepage* (BSC 2004 [DIRS 169131], Section 6.4.4.1) suggest that temperature-induced stress changes give rise to changes in the vertical fracture permeability in the vicinity of waste emplacement drifts, particularly in the Tptpmn unit (BSC 2004 [DIRS 169131], Section 6.5.1.4). However, these permeability changes do not result in significant changes in the flow fields (BSC 2004 [DIRS 169864], Sections 6.5.5 and 6.6.2). In particular, the seepage rates calculated for a permeability field including THM permeability changes were similar to, but slightly smaller than, those calculated for a permeability field representative of the initial postexcavation conditions. The simulation results (BSC 2004 [DIRS 169864]) provide reasonably accurate (slightly conservative) estimates of the expected seepage rates at long-term conditions with coupled THM property changes (BSC 2004 [DIRS 169131], Section 6.4.4.1). Therefore, the impact of THM property changes is neglected in the seepage abstraction.

The overall effect of THM coupled processes on drift-scale radionuclide transport may also be excluded because the primary effect of THM processes leads to enhanced seepage diversion and reduced drift seepage, reduced water saturations beneath the drift, and therefore, greater partitioning of radionuclide releases to the rock matrix. Therefore, this FEP may be excluded based on low consequence because it has no adverse effects on the radiological exposures to the RMEI, or radionuclide release to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.9.11 Thermo-Mechanical Stresses Alter Characteristics of Faults near Repository (2.2.10.04.0B)

FEP Description: Heat from the waste causes thermal expansion of the surrounding rock, generating changes to the stress field that may change the properties (both hydrologic and mechanical) in and along faults. Cooling following the peak thermal period will also change the stress field, further affecting fault properties near the repository.

Screening Decision: Excluded–Low Consequence.

Screening Argument: The primary differences represented by faults, as compared with the general fractured rock mass, for flow, transport, drift seepage, and coupled processes, are the greater permeability and potential continuity of high-permeability pathways through the UZ. Thermal-mechanical effects on fault-fractures may be expected to be qualitatively similar to rock-mass fractures in the sense that THM processes will lead to reductions in vertical permeabilities, but increased horizontal permeability above the drift. Faults may be viewed as a specific type of heterogeneity in the fractured rock mass. From this viewpoint, *Drift Scale THM Model* (BSC 2004 [DIRS 169864], Section 6.10.5) indicates that the main effect of THM processes is on the mean permeability, and that it is appropriate to apply the mean permeability changes to a seepage analysis that considers either the homogenous or heterogeneous permeability field. This is the approach that is presented in FEP 2.2.10.04.0A. In that FEP, the effects of THM processes were found to result in slightly lower seepage rates than the unperturbed condition. Therefore, the screening arguments used in FEP 2.2.10.04.0A also apply here, and consequently this FEP may be excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.9.12 Thermo-Mechanical Stresses Alter Characteristics of Rocks above and below the Repository (2.2.10.05.0A)

FEP Description: Thermal-mechanical compression at the repository may produce tension fracturing in the Paintbrush non-welded tuff and other units above the repository. These fractures may alter unsaturated zone flow between the surface and the repository. Extreme fracturing may propagate to the surface, affecting infiltration. Thermal fracturing in rocks below the repository may affect flow and radionuclide transport to the saturated zone.

Screening Decision: Excluded–Low Consequence.

Screening Argument: The mountain-scale THM model (BSC 2004 [DIRS 169866], Section 6.5) assesses the magnitude and distribution of changes in hydrological properties and analyzes the impact of such changes on the mountain-scale vertical percolation flux through the repository horizon. The result shows that a maximum THM-induced change in hydrological properties occurs at around 1,000 years after emplacement, when the average temperature in the mountain is maximal. Near the repository level, thermal-elastic stresses tend to tighten vertical fractures to smaller apertures, leading to reduced permeability and increased capillary. At the

ground surface, in a zone extending about 100 m deep, compressive stresses are completely relieved from tension. In this zone, fractures will open elastically, and fracturing or shear-slip along preexisting fractures is possible.

Using a conservative estimate of input THM properties, changes in permeability by elastic closure or opening of preexisting fractures are within a factor of 0.3 to 5, whereas calculated changes in capillary pressure are within a factor of 0.7 to 1.2. In addition, a conservative three-order-of-magnitude increase in permeability and one-order-of-magnitude reduction in capillary strength were imposed for the zone of possible fracturing and shear slip near the ground surface. Despite these conservative estimates of potential changes in hydrological properties, the main conclusion from the results documented in *Mountain-Scale Coupled Processes (TH/THC/THM)* (BSC 2004 [DIRS 169866], Sections 6.5.10 to 6.5.14) is that THM-induced changes in the mountain-scale hydrological properties have no significant impact on the vertical percolation flux through the repository horizon. Again, these results were obtained for conservative estimates of the input THM properties, which is sufficient for bounding the possible impact of the THM processes on permeability and percolation flux on the mountain scale.

The effects of mechanical disturbance of fractures along radionuclide transport pathways are discussed in Section 6.8.7, FEP 2.2.06.02.0B. The conclusion reached in that section is that the effects of changes to fracture aperture or spacing on radionuclide transport are expected to be negligible over a wide range of permeability variation. In this case, the disturbance is caused by thermal-mechanical effects rather than by a seismic event. However, the conclusions reached in Section 6.8.7, FEP 2.2.06.02.0B are also applicable here because the analysis supporting the conclusions in Section 6.8.7, FEP 2.2.06.02.0B are based on a general sensitivity study of how fracture properties affect radionuclide transport. Furthermore, the general effects of thermal stresses on fracture permeability due to repository heating are evaluated in *Mountain-Scale Coupled Processes (TH/THC/THM)* (BSC 2004 [DIRS 169866], Section 6.5.12). This analysis indicates that in the zones near the repository and below the repository, the fracture permeability is either reduced or unaffected. Thus, it is conservative to not include thermal effects on fracture permeability because radionuclide transport is slower with reduced permeability (Appendix D, Section D3.3.1). Therefore, this FEP may be excluded based on low consequence because it has no adverse effects on the radiological exposures to the RMEI, or radionuclide release to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.9.13 Thermo-Chemical Alteration in the UZ (Solubility, Speciation, Phase Changes, Precipitation/Dissolution) (2.2.10.06.0A)

FEP Description: Thermal effects may affect radionuclide transport directly, by causing changes in radionuclide speciation and solubility in the UZ, or indirectly, by causing changes in the host rock mineralogy that affect the flow path. Relevant processes include volume effects associated with silica phase changes, precipitation and dissolution of fracture-filling minerals (including silica and calcite), and alteration of zeolites and other minerals to clays.

Screening Decision: Excluded–Low Consequence.

Screening Argument: This FEP raises some issues already addressed in Section 6.9.7, FEP 2.2.08.03.0B and Section 6.9.8, FEP 2.2.08.07.0B. If solubility limits decrease in the geosphere so that they are lower than in the waste emplacement drifts, then some dissolved radionuclides will precipitate as water flows out of the drifts. This limits the dissolved radionuclides available for transport into the geosphere, which results in no adverse effect on performance. See also Section 6.9.6 (FEP 2.2.01.05.0A) for additional information on this subject. If solubility limits increase in the geosphere compared with the waste emplacement drift, there is no effect on transport because all available radionuclides from the source at the waste emplacement drift are already aqueous species. The effects of colloid formation are accounted for in the colloid source term (BSC 2004 [DIRS 170025], Section 6.5.2.3). Colloids are formed from the degradation of the high-level waste and spent nuclear fuel waste forms, EBS materials, and rock (BSC 2004 [DIRS 170025], Section 6.3.1). Radionuclides associated with colloids are modeled as either irreversibly or reversibly attached to colloids to encompass the broadest range of potential radionuclide-colloid interactions (BSC 2004 [DIRS 170041], Section 6.4.5). Elevated temperatures are expected to lead to fewer colloids due to the decrease in colloid stability. This is due to the greater energy of colloid motion at higher temperatures, which allows colloids to overcome the energy barrier associated with coagulation (BSC 2004 [DIRS 170025], Section 6.3.2.1). Boiling results in evaporation and this tends to increase the ionic strengths of colloid suspensions. This also leads to colloid instability due to compression of the electric double layer surrounding colloids (BSC 2004 [DIRS 170025], Section 6.3.2.1). Therefore, colloid entrainment as a result of boiling is not expected.

The effects of temperature on radionuclide sorption were evaluated in *Radionuclide Transport Models Under Ambient Conditions* (BSC 2004 [DIRS 164500], Appendix I). This evaluation focused on the radionuclides Cs, Sr, Ba (a proxy for Ra), Ce, Eu, U(VI), Np, Pu and Am (BSC 2004 [DIRS 164500], Section I1.4). The effects of temperature on sorption were found to be negligible for these radionuclides, except for Sr, Np, and U(VI). For these three radionuclides the effects of increased temperature leads to increased sorption (BSC 2004 [DIRS 164500], Section I5). Therefore, the effects of temperature on radionuclide transport can be excluded on the basis of low consequence because it has no adverse effects on performance.

The thermal-chemical interactions that will occur in the repository environment have been studied with respect to effects on the seepage water entering the waste emplacement drifts (BSC 2004 [DIRS 169856]). This model explicitly captures the effects of changes in temperature, pH, Eh, ionic strength (and other compositional variables), time dependency, precipitation or dissolution effects, and effects of resaturation (BSC 2004 [DIRS 169856], Section 6.2). Changes in fracture permeabilities were found to be on the order of the natural variation in these properties (BSC 2004 [DIRS 169856], Section 6.5.5.3 and BSC 2004 [DIRS 170038], Table 6-5), with most of the substantial effects limited to regions above and to the side of the drift within about a drift diameter (BSC 2004 [DIRS 169856], Figures 6.5-39 and 6.5-40). The predicted mineral precipitation decreases permeability in the affected regions, and leads to a reduction in flow around the drift. This is conservative for both drift seepage and radionuclide transport phenomena and this FEP is, therefore, excluded because it will have no adverse affects on the radiological exposures to the RMEI, or radionuclide release to the accessible environment.

The geochemical model includes the major solid phases (minerals and glass) encountered in geological units at Yucca Mountain, together with a range of possible reaction product minerals, CO_2 gas, and the aqueous species necessary to include these solid phases and the porewater composition within the THC model (BSC 2004 [DIRS 169856], Table 6.2-2). Compositional changes were only calculated at the drift boundary for the drift-scale THC seepage model (BSC 2004 [DIRS 169856]). Results from these simulations show most compositional variations returning to unperturbed conditions in 10,000 years or less. Variations in pH (BSC 2004 [DIRS 169856], Figures 6.5-12, 6.5-25, and 6.5-58), a key compositional variable for sorption of some radionuclides (BSC 2004 [DIRS 164500], Appendix A), roughly lie within the range of variability investigated for initial porewater compositions (BSC 2004 [DIRS 169856], Table 6.2-1). Bicarbonate is found to be depressed in concentration upon water resaturation at the drift wall, as expected based on the reduced pH values at the same time period.

Results were also investigated for the Tptpll (lower lithophysal unit) model considering a range of initial porewater compositions. In this model, five different initial porewater compositions were investigated (BSC 2004 [DIRS 169856], Table 6.2-1). Peak concentrations found at the time of rewetting in both models reflect mostly the small values of the first, nonzero, liquid-saturation output. In any case, elevated concentrations are predicted only for small liquid saturations that are not subject to significant fluid movement. The improved treatment of mineral precipitation at the boiling front used in the most recent THC model for the Tptpll also results in the prediction of lower, more realistic aqueous silica concentrations than in earlier models (BSC 2004 [DIRS 169856], Figure 6.5-16). This model also predicts, upon rewetting, more rapid return to near-ambient conditions for aqueous Ca, Na, and Cl.

The findings indicate that at the drift wall, most of the significant compositional variations resulting from thermal-chemical processes are limited to low-saturation conditions over time periods that are short relative to the 10,000-year performance period. Similar magnitudes of variation in chloride and pH were found in the mountain-scale THC model results (BSC 2004 [DIRS 169866], Section 6.4.3.3.2). The magnitudes of the variations are found to be smaller at greater distances from the drift wall. As for the drift-scale study, variations in chloride are driven mainly by evaporation and are found to return to near-ambient values upon rewetting (BSC 2004 [DIRS 169866], Section 6.4.3.3.2). Variations in pH were found to lie roughly between 7 and 9, which is similar to the results for the drift-scale THC model (BSC 2004 [DIRS 169856], Figures 6.5-12, 6.5-25, 6.5-58). The most persistent change in pH is a level of about 7 in the Calico Hills (BSC 2004 [DIRS 169866], Section 6.4.3.3.2, Figure 6.4-17), but this lies within the range of pH investigated for radionuclide sorption (BSC 2004 [DIRS 164500], Appendix A). Therefore, the effects of these changes are excluded because they will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable

6.9.14 Thermo-Chemical Alteration of the Calico Hills Unit (2.2.10.07.0A)

FEP Description: Fracture pathways in the Calico Hills may be altered by the thermal and chemical properties of the water flowing out of the repository.

Screening Decision: Excluded–Low Consequence.

Screening Argument: Model results show that significant glass alteration is found in the CHn at locations where temperatures by thermal heating exceed approximately 50°C (BSC 2004 [DIRS 169866], Section 6.4.3.3.3). Much of the reaction has taken place by 3,000 years, with the alteration rate decreasing strongly as temperatures decline in the rocks below the repository. The extent of glass alteration is limited to the strongly heated regions directly below the repository drifts, with little effects elsewhere. The dominant phases formed by volcanic glass reactions with aqueous fluids are zeolites, potassium feldspar, and albite (BSC 2004 [DIRS 169866], Section 6.4.3.3.3). Differences in radionuclide sorption between vitric and zeolitic rock are generally found to have either greater sorption on zeolitic rock (e.g., Am and U) or little difference in sorption (e.g., Np and Pu) (BSC 2004 [DIRS 164500], Appendix A). Therefore, the effects of mineral alteration from glass to zeolites on radionuclide sorption are expected to be either negligible or will have no adverse effect on repository performance.

The basal vitrophyre of the TSw and the underlying vitric units and glass-rich zeolitic units all contain abundant clinoptilolite, which (in the model simulations) breaks down at elevated temperatures (BSC 2004 [DIRS 169866], Section 6.4.3.3.3, Figure 6.4-24) to form predominantly stellerite (BSC 2004 [DIRS 169866], Section 6.4.3.3.3, Figure 6.4-21). Although stellerite is common in fractures in the devitrified tuffs in the TSw, it is not typical as an alteration product of glass in the vitric units. It is likely that the fixed composition of clinoptilolite used in the thermodynamic database limits its ability to form preferentially to stellerite under the changing calcium, sodium, and potassium concentrations in the aqueous fluid, thus, reducing its relative stability to stellerite, potassium feldspar, and albite at elevated temperatures. At near-ambient temperatures, clinoptilolite is stable in the simulation and actually precipitates preferentially in the glass-rich layers (BSC 2004 [DIRS 169866], Section 6.4.3.3.3, Figure 6.4-24). This trend is consistent with the observed mineral assemblage, although the 1 percent reacted in 7,000 years is probably greater than that actually formed in this short period of time (BSC 2004 [DIRS 169866], Section 6.4.3.3.3).

Changes in porosity and hence permeability are related to the net effects of volume changes taking place via mineral dissolution/precipitation. Mineral precipitation takes place through several different mechanisms and, therefore, the distribution in the changes in hydrological properties is related to the spatial distributions of the various processes. In the CHn there is a modest increase in porosity of about 1 percent, owing primarily to the reaction of clinoptilolite and glass to feldspars and stellerite (BSC 2004 [DIRS 169866], Section 6.4.3.3.4). As a consequence of the small fracture porosity changes, the fracture permeability does not show a significant reduction (BSC 2004 [DIRS 169866], Section 6.4.3.3.4, Figure 6.4-26). Permeability changes in the matrix of the CHn vitric and zeolitic units are minor because of the initially high porosity of these rocks (BSC 2004 [DIRS 169866], Section 6.4.3.3.4, Figures 6.4-25 and 6.4-26). Therefore, the porosity and permeability values in the matrix are essentially the same as the initial values. This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.9.15 Thermo-Chemical Alteration of the Topopah Spring Basal Vitrophyre (2.2.10.09.0A)

FEP Description: Heating the Topopah Spring basal vitrophyre with available water may cause alteration of the glasses to clays and zeolites. Possible effects include volume increases that plug fractures, changes in flow paths, creation of perched water zones, and an increase in the sorptive properties of the unit.

Screening Decision: Excluded–Low Consequence

Screening Argument: Model results show that, due to repository heating of the rock matrix, after 1000 years over 5 percent of the volcanic glass in the basal vitrophyre of the TSw has reacted and by 7000 years it has dissolved up to nearly 20 percent by volume (BSC 2004 [DIRS 169866], Section 6.4.3.3.3, Figure 6.4-20). The dominant phases formed by volcanic glass reactions with aqueous fluids are zeolites, potassium feldspar, and albite (BSC 2004 [DIRS 169866], Section 6.4.3.3.3). At locations beneath waste emplacement drifts, the principal precipitate is zeolite (stellerite) (BSC 2004 [DIRS 169866], Figures 6.4-20 through 6.4-24). Differences in radionuclide sorption between vitric and zeolitic rock are generally found to have either greater sorption on zeolitic rock (e.g., Am and U) or little difference in sorption (e.g., Np and Pu) (BSC 2004 [DIRS 164500], Appendix A). Therefore, the effects of mineral alteration from glass to zeolites on radionuclide sorption are expected either to be negligible or to have no adverse effects.

The basal vitrophyre of the TSw and the underlying vitric units and glass-rich zeolitic units all contain abundant clinoptilolite, which (in the model simulations) breaks down at elevated temperatures (BSC 2004 [DIRS 169866], Section 6.4.3.3.3, Figure 6.4-24) to form predominantly stellerite (BSC 2004 [DIRS 169866], Section 6.4.3.3.3, Figure 6.4-21). Although stellerite is common in fractures in the devitrified tuffs in the TSw, it is not typical as an alteration product of glass in the vitric units. It is likely that the fixed composition of clinoptilolite used in the thermodynamic database limits its ability to form preferentially to stellerite under the changing calcium, sodium, and potassium concentrations in the aqueous fluid, thus, reducing its relative stability to stellerite, potassium feldspar, and albite at elevated temperatures. At near-ambient temperatures, clinoptilolite is stable in the simulation and actually precipitates preferentially in the glass-rich layers (BSC 2004 [DIRS 169866], Section 6.4.3.3.3, Figure 6.4-24). This trend is consistent with the observed mineral assemblage, although the 1 percent reacted in 7,000 years is probably greater than that actually formed in this short period of time (BSC 2004 [DIRS 169866], Section 6.4.3.3.3).

Changes in porosity and hence permeability are related to the net effects of volume changes taking place via mineral dissolution/precipitation. Mineral precipitation takes place through several different mechanisms, and, therefore, the distribution in the changes in hydrological properties is related to the spatial distributions of the various processes. As in the CHn, there is a modest increase in porosity in the TSw basal vitrophyre owing primarily to the reaction of clinoptilolite and glass to feldspars and stellerite. As a consequence of the small fracture porosity changes, the fracture permeability does not show a significant reduction (BSC 2004 [DIRS 169866], Section 6.4.3.3.4, Figure 6.4-26). Permeability changes in the matrix are minor because of the initially high porosity of the vitric TSw vitrophyre rocks (BSC 2004

[DIRS 169866], Section 6.4.3.3.4, Figures 6.4-25 and 6.4-26). Therefore, the porosity and permeability values in the matrix are essentially the same as the initial values, and this FEP is excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.9.16 Mineralogic Dehydration Reactions (2.2.10.14.0A)

FEP Description: Mineralogic dehydration reactions release water affecting hydrologic conditions. Dehydration of zeolites below the repository may lead to large-scale volume changes affecting flow and/or drift stability.

Screening Decision: Excluded–Low Consequence.

Screening Argument: The predominant zone of zeolite-bearing minerals is at the base of the TSw (tsw39) and in the Calico Hills nonwelded unit (ch1, ch2, ch3, ch4, ch5, and ch6) (BSC 2004 [DIRS 169855], Section 5.2). Dehydration of zeolites below the repository could occur if temperatures in the zeolitic units exceed the estimated minimum alteration temperature of 85°C (Smyth 1982 [DIRS 119483], p. 201). Results of the two-dimensional mountain-scale TH calculations suggest that temperatures at the base of the TSw will remain below 77°C (BSC 2004 [DIRS 169866], Figure 6.2-6c). Note, however, that the highest temperatures occur in the southern portion of the repository (BSC 2004 [DIRS 169866], Figure 6.2-6c), where the percent of zeolitic alteration is low (BSC 2004 [DIRS 169855], Figures 6-6 through 6-8). Peak temperatures in the northern portion of the repository remain below 74°C. Furthermore, peak temperatures in the three-dimensional mountain-scale TH calculations predict a peak temperature of less than 75°C at the TSw-CHn interface (BSC 2004 [DIRS 169866], Section 6.3.1). Therefore, the temperature changes induced by the repository are not high enough to cause significant zeolite dehydration or volume changes in the zeolitic rock. This FEP is, therefore, excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Section 6.1.2 explains why low consequence for specific elements of the UZ system leads to low consequence for total system performance.

Supporting Reports: Not applicable.

6.9.17 Diffusion in the UZ (2.2.08.05.0A)

FEP Description: Molecular diffusion processes may affect radionuclide transport in the UZ. This includes osmotic processes in response to chemical gradients.

Screening Decision: Excluded–Low Consequence.

Screening Argument: When radionuclides are present in fractures or faults, they can be transported by advection, dispersion, and diffusion. Transport by advection and dispersion are included in FEP 2.2.07.15.0B, advection and dispersion in the UZ. Transport by diffusion is neglected because it is mathematically similar to dispersion (that is, flux is proportional to concentration gradient) and under all scenarios it is much smaller than transport by dispersion.

The mean value of the $\log_{10}$ of molecular diffusion coefficient is 4.69, giving a diffusion coefficient of 4.9×10^4 mm^2/yr (BSC 2004 [DIRS 170040], Table E-2). The corresponding value of dispersion coefficient is the product of the flow velocity and the dispersivity; the dispersivity has a fixed value of 10 m (BSC 2004 [DIRS 170041], Table 6-2). The smaller the flow velocity, the greater the ratio of diffusion coefficient to dispersion coefficient.

The flow velocity v depends upon the overall percolation flux q, the fraction of the flux which flows in fractures or faults (that is, not in the matrix) f, and the fracture porosity ϕ:

$$v = (qf)/\phi \qquad \text{(Eq. 6-3)}$$

Both q and f depend upon the flow field; that is, upon the climate (present, monsoon, or glacial transition) and whether the lower bound, mean, or upper bound infiltration is imposed as a boundary condition. Values of q and f are found in *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861], Tables 6.1-2 and 6.6-3, respectively). ϕ depends on the model layer, as shown in *Particle Tracking Model and Abstraction of Transport Processes* (BSC 2004 [DIRS 170041], Table 6-13). To minimize v and, therefore, maximize the importance of diffusion relative to dispersion, take q from the slowest flow field, and take f at the horizon where the greatest fraction of flow is through the matrix continuum. These are the lower bound for present-day climate, with f taken at the water table. This is the lower-bound present-day flow field (preq_1A) for which $q = 1.25$ mm/yr (BSC 2004 [DIRS 169861], Table 6.1-2), and $f = 0.43$ (BSC 2004 [DIRS 169861], Table 6.6-3). For model layers below the repository, the greatest ϕ, giving the slowest v, is 0.025 (layer tswf, BSC 2004 [DIRS 170041], Table 6-13). Substituting these values, minimum $v = 21.6$ mm/yr and minimum dispersion coefficient $= 2.16 \times 10^5$ mm^2/yr. This minimum is still 4.4 times larger than the diffusion coefficient. For the lower bound monsoon and glacial-transition flow fields, the ratios are 20 and 9.2 respectively, and the ratios are higher still for the mean and upper bound flow fields. These values all assume that the fractures are 100 percent saturated and, therefore, they represent lower bounds for velocity and dispersion coefficient. Therefore, under all flow scenarios diffusion in the UZ (other than matrix diffusion) is excluded because it will not significantly change radiological exposures to the RMEI or radiological releases to the accessible environment. Related FEPs 2.1.09.08.0A (Diffusion of dissolved radionuclides in EBS), and 2.1.09.24.0A (Diffusion of colloids in EBS) are treated in *Engineered Barrier System Features, Events, and Processes* (BSC 2004 [DIRS 169898], Sections 6.2.51 and 6.2.58).

Supporting Reports: Not applicable.

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7. CONCLUSIONS

This document presents the 93 FEPs associated with UZ flow and transport processes. The 41 FEPs identified in Section 6.2 are included in TSPA-LA. The remaining 52 FEPs are excluded from TSPA-LA, based on arguments presented in Sections 6.3 through 6.9. The FEPs analysis results are given in Table 7-1.

The conclusions from this document (FEP Screening Decision, TSPA Disposition for included FEPs, or Screening Argument for excluded FEPs) will be incorporated in the Yucca Mountain TSPA-LA FEP database. Because this is the only subsequent use for the conclusions of this report, there are no restrictions on this use. Any uncertainties or limitations are generally related to input documents and repository design and have been previously described in Section 1.3. The FEP database will contain all Yucca Mountain FEPs considered for TSPA-LA with FEP number, name, description, and relevant FEP analysis reports where the documentation of the screening of specific FEPs is summarized. The FEP database will also contain screening decisions (Include or Exclude), screening arguments, and TSPA dispositions quoted from this and all other FEP analysis reports.

All FEP information, including the unsaturated zone FEPs considered in this report, will be submitted to Technical Data Management System by the Yucca Mountain FEP database team as a final LA FEP list represented by a Data Tracking Number (DTN). Documentation of the FEP database is given in a separate AP-3.11Q report (BSC 2004 [DIRS 168706]. These final data will be qualified as technical product output from the AP-3.11Q report. The final LA FEP list DTN will supersede all previous FEP list DTNs.

The output DTN: LB0310FEPS0170.001 contains the sequence of calculations used to evaluate perched water as discussed in Appendix A. This DTN is intended only to provide information on the calculations carried out for this report. These data are not intended to be used as a source of input for other analyses.

The output DTN: LB0408U0170FEP.001 contains the input and output files used to evaluate transport with fracture apertures increased or decreased as a result of seismic activity, as discussed in Appendix D. A summary of that output DTN is presented in DTN: LB0408U0170FEP.002. These DTNs are intended only to provide information on the calculations carried out for this report. They are not intended to be used as a source of input for other analyses.

Table 7-1.   FEPs Analysis Results

FEP Number	FEP Name	Screening Decision	Screening Basis for Excluded FEPs	Section Number
1.1.01.01.0A	Open site investigation boreholes	Excluded	Low Consequence	6.3.1
1.1.01.01.0B	Influx through holes drilled in drift wall or crown	Excluded	Low Consequence	6.3.2
1.1.02.01.0A	Site flooding (during construction and operation)	Excluded	Low Consequence	6.3.3
1.1.02.02.0A	Preclosure ventilation	Included		6.2.1
1.1.04.01.0A	Incomplete closure	Excluded	Low Consequence and by Regulation	6.3.4
1.1.11.00.0A	Monitoring of the repository	Excluded	Low Consequence	6.3.5
1.2.02.01.0A	Fractures	Included		6.2.2
1.2.02.02.0A	Faults	Included		6.2.3
1.2.04.02.0A	Igneous activity changes rock properties	Excluded	Low Consequence	6.8.1
1.2.06.00.0A	Hydrothermal activity	Excluded	Low Consequence	6.8.2
1.2.07.01.0A	Erosion/denudation	Excluded	Low Consequence	6.5.1
1.2.07.02.0A	Deposition	Excluded	Low Consequence	6.5.2
1.2.09.02.0A	Large-scale dissolution	Excluded	Low Consequence	6.5.3
1.2.10.01.0A	Hydrologic response to seismic activity	Excluded	Low Consequence and Low Probability	6.8.3
1.2.10.02.0A	Hydrologic response to igneous activity	Excluded	Low Consequence	6.8.4
1.3.01.00.0A	Climate change	Included		6.2.4
1.3.04.00.0A	Periglacial effects	Excluded	Low Consequence and Low Probability	6.4.1
1.3.05.00.0A	Glacial and ice sheet effect	Excluded	Low Probability	6.4.2
1.3.07.01.0A	Water table decline	Excluded	Low Consequence	6.4.3
1.3.07.02.0B	Water table rise affects UZ	Included		6.2.5
1.4.01.00.0A	Human influences on climate	Excluded	By Regulation	6.6.1
1.4.01.01.0A	Climate modification increases recharge	Included		6.2.6
1.4.01.02.0A	Greenhouse gas effects	Excluded	By Regulation	6.6.2
1.4.01.03.0A	Acid rain	Excluded	By Regulation	6.6.3
1.4.01.04.0A	Ozone layer failure	Excluded	By Regulation	6.6.4
1.4.06.01.0A	Altered soil or surface water chemistry	Excluded	By Regulation	6.6.5
2.1.05.01.0A	Flow through seals (access ramps and ventilation shafts)	Excluded	Low Consequence	6.3.6
2.1.05.02.0A	Radionuclide transport through seals	Excluded	Low Consequence	6.3.7
2.1.05.03.0A	Degradation of seals	Excluded	Low Consequence	6.3.8
2.1.08.01.0A	Water influx at the repository	Included		6.2.7
2.1.08.02.0A	Enhanced influx at the repository	Included		6.2.8
2.1.09.12.0A	Rind (chemically altered zone) forms in the near-field	Excluded	Low Consequence	6.9.1
2.1.09.21.0C	Transport of particles larger than colloids in the UZ	Excluded	Low Consequence	6.4.4

Table 7-1. FEPs Analysis Results (Continued)

FEP Number	FEP Name	Screening Decision	Screening Basis for Excluded FEPs	Section Number
2.2.01.01.0A	Mechanical effects of excavation and construction in the near-field	Included		6.2.9
2.2.01.01.0B	Chemical effects of excavation and construction in the near-field	Excluded	Low Consequence	6.9.2
2.2.01.02.0A	Thermally-induced stress changes in the near-field	Excluded	Low Consequence	6.9.3
2.2.01.03.0A	Changes in fluid saturations in the excavation disturbed zone	Excluded	Low Consequence	6.9.4
2.2.01.04.0A	Radionuclide solubility in the excavation disturbed zone	Excluded	Low Consequence	6.9.5
2.2.01.05.0A	Radionuclide transport in the excavation disturbed zone	Excluded	Low Consequence	6.9.6
2.2.03.01.0A	Stratigraphy	Included		6.2.10
2.2.03.02.0A	Rock properties of host rock and other units	Included		6.2.11
2.2.06.01.0A	Seismic activity changes porosity and permeability of rock	Excluded	Low Consequence	6.8.5
2.2.06.02.0A	Seismic activity changes porosity and permeability of faults	Excluded	Low Consequence	6.8.6
2.2.06.02.0B	Seismic activity changes porosity and permeability of fractures	Excluded	Low Consequence	6.8.7
2.2.06.03.0A	Seismic activity alters perched water zones	Excluded	Low Consequence	6.8.8
2.2.06.04.0A	Effects of subsidence	Excluded	Low Consequence	6.5.4
2.2.07.01.0A	Locally saturated flow at bedrock/alluvium contact	Included		6.2.12
2.2.07.02.0A	Unsaturated groundwater flow in the geosphere	Included		6.2.13
2.2.07.03.0A	Capillary rise in the UZ	Included		6.2.14
2.2.07.04.0A	Focusing of unsaturated flow (fingers, weeps)	Included		6.2.15
2.2.07.05.0A	Flow in the UZ from episodic infiltration.	Excluded	Low Consequence	6.4.5
2.2.07.06.0A	Episodic/pulse release from repository	Excluded	Low Consequence	6.4.6
2.2.07.06.0B	Long-term release of radionuclides from the repository	Included		6.2.16
2.2.07.07.0A	Perched water develops	Included		6.2.17
2.2.07.08.0A	Fracture flow in the UZ	Included		6.2.18
2.2.07.09.0A	Matrix imbibition in the UZ	Included		6.2.19
2.2.07.10.0A	Condensation zone forms around drifts	Included		6.2.20
2.2.07.11.0A	Resaturation of geosphere dry-out zone	Included		6.2.21
2.2.07.15.0B	Advection and dispersion in the UZ	Included		6.2.22
2.2.07.18.0A	Film flow into the repository	Included		6.2.23
2.2.07.19.0A	Lateral flow from Solitario Canyon Fault enters drifts	Included		6.2.24
2.2.07.20.0A	Flow diversion around repository drifts	Included		6.2.25
2.2.08.01.0B	Chemical characteristics of groundwater in the UZ	Included		6.2.26
2.2.08.03.0B	Geochemical interactions and evolution in the UZ	Excluded	Low Consequence	6.9.7
2.2.08.04.0A	Re-dissolution of precipitates directs more corrosive fluids to waste packages	Included		6.2.27
2.2.08.05.0A	Diffusion in the UZ	Excluded	Low Consequence	6.9.17

Table 7-1. FEPs Analysis Results (Continued)

FEP Number	FEP Name	Screening Decision	Screening Basis for Excluded FEPs	Section Number
2.2.08.06.0B	Complexation in the UZ	Included		6.2.28
2.2.08.07.0B	Radionuclide solubility limits in the UZ	Excluded	Low Consequence	6.9.8
2.2.08.08.0B	Matrix diffusion in the UZ	Included		6.2.29
2.2.08.09.0B	Sorption in the UZ	Included		6.2.30
2.2.08.10.0B	Colloidal transport in the UZ	Included		6.2.31
2.2.08.12.0A	Chemistry of water flowing into the drift	Included		6.2.32
2.2.09.01.0B	Microbial activity in the UZ	Included		6.2.33
2.2.10.01.0A	Repository-induced thermal effects on flow in the UZ	Excluded	Low Consequence	6.9.9
2.2.10.03.0B	Natural geothermal effects on flow in the UZ	Included		6.2.34
2.2.10.04.0A	Thermo-mechanical stresses alter characteristics of fractures near repository	Excluded	Low Consequence	6.9.10
2.2.10.04.0B	Thermo-mechanical stresses alter characteristics of faults near repository	Excluded	Low Consequence	6.9.11
2.2.10.05.0A	Thermo-mechanical stresses alter characteristics of rocks above and below the repository	Excluded	Low Consequence	6.9.12
2.2.10.06.0A	Thermo-chemical alteration in the UZ (solubility, speciation, phase changes, precipitation/dissolution)	Excluded	Low Consequence	6.9.13
2.2.10.07.0A	Thermo-chemical alteration of the Calico Hills unit	Excluded	Low Consequence	6.9.14
2.2.10.09.0A	Thermo-chemical alteration of the Topopah Spring basal vitrophyre	Excluded	Low Consequence	6.9.15
2.2.10.10.0A	Two-phase buoyant flow/heat pipes	Included		6.2.35
2.2.10.11.0A	Natural air flow in the UZ	Excluded	Low Consequence	6.7.1
2.2.10.12.0A	Geosphere dry-out due to waste heat	Included		6.2.36
2.2.10.14.0A	Mineralogic dehydration reactions	Excluded	Low Consequence	6.9.16
2.2.11.02.0A	Gas effects in the UZ	Excluded	Low Consequence	6.7.2
2.2.11.03.0A	Gas transport in geosphere	Excluded	Low Consequence	6.7.3
2.2.12.00.0A	Undetected features in the UZ	Excluded	Low Consequence	6.8.9
2.3.01.00.0A	Topography and morphology	Included		6.2.37
2.3.11.01.0A	Precipitation	Included		6.2.38
2.3.11.02.0A	Surface runoff and flooding	Included		6.2.39
2.3.11.03.0A	Infiltration and recharge	Included		6.2.40
3.1.01.01.0A	Radioactive decay and ingrowth	Included		6.2.41

7.1 SATISFACTION OF YMRP ACCEPTANCE CRITERIA.

The satisfaction of acceptance criteria identified in Section 4.2 are summarized in Table 7-2.

Table 7-2.   Where YMRP Acceptance Criteria Have Been Addressed in This Report

YMRP Section	Acceptance Criterion	Subcriteria	How and Where addressed
Scenario Analysis and Event Probability: Scenario Analysis (from Section 2.2.1.2.1.3 of NUREG-1804 [DIRS 163274])	1. The Identification of a List of Features, Events, and Processes is Adequate	The Safety Analysis Report contains a complete list of features, events, and processes, related to the geologic setting or the degradation, deterioration, or alteration of engineered barriers (including those processes that would affect the performance of natural barriers), that have the potential to influence repository performance. The list is consistent with the site characterization data. Moreover, the comprehensive features, events, and processes list includes, but is not limited to, potentially disruptive events related to igneous activity (extrusive and intrusive); seismic shaking (high frequency–low magnitude, and rare large-magnitude events); tectonic evolution (slip on existing faults and formation of new faults); climatic change (change to pluvial conditions); and criticality.	See Section 6.1.1 of this report for a description and origin of the UZ FEP list and descriptions. The list of UZ FEPs is provided in Table 1-1. Included FEP descriptions and TSPA dispositions are provided in Section 6.2. See Section 6.1.1 of this report for a description and origin of the UZ FEP list and descriptions.
	2. Screening of the List of Features, Events, and Processes is Appropriate	(1) The U.S. Department of Energy has identified all features, events, and processes related to either the geologic setting or to the degradation, deterioration, or alteration of engineered barriers (including those processes that would affect the performance of natural barriers) that have been excluded;	See the method and approach discussion provided in Section 6.1.2. Excluded FEPs are identified in Sections 6.3 through 6.9
		(2) The U.S. Department of Energy has provided justification for those features, events, and processes that have been excluded. An acceptable justification for excluding features, events, and processes is that either the feature, event, and process is specifically excluded by regulation; probability of the feature, event, and process (generally an event) falls below the regulatory criterion; or omission of the feature, event, and process does not significantly change the magnitude and time of the resulting radiological exposures to the reasonably maximally exposed individual, or radionuclide releases to the accessible environment;	The justification for exclusion of each excluded FEP (by regulation, low probability, low consequence) is presented in Sections 6.3 through 6.9.
		(3) The U.S. Department of Energy has provided an adequate technical basis for each feature, event, and process, excluded from the performance assessment, to support the conclusion that either the feature, event, or process is specifically excluded by regulation; the probability of the feature, event, and process falls below the regulatory criterion; or omission of the feature, event, and process does not significantly change the magnitude and time of the resulting radiological exposures to the reasonably maximally exposed individual, or radionuclide releases to the accessible environment.	The technical basis for each excluded FEP is presented in Sections 6.3 through 6.9.

Table 7-2.   Where YMRP Acceptance Criteria Have Been Addressed in this Report (Continued)

YMRP Section	Acceptance Criterion	Subcriteria	How and Where addressed
Identification of Events with Probabilities Greater than 10^{-8} per Year Event Probability (from Section 2.2.1.2.2.3 of NUREG-1804 [DIRS 163274])	2. Probability Estimates for Future Events are Supported by Appropriate Technical Bases	(1) Probabilities for future natural events have considered past patterns of the natural events in the Yucca Mountain region, considering the likely future conditions and interactions of the natural and engineered repository system. These probability estimates have specifically included igneous events, faulting and seismic events, and criticality events.	FEPs are excluded on the basis of low probability in sections 6.4.2, and on the basis of low consequence and low probability in Sections 6.4.1 and 6.8.3. In Sections 6.4.1 and 6.4.2, the exclusion is based on future climate predictions, specifically that glacial conditions will not occur during the regulatory period. In Section 6.8.3, the exclusion is based on a lack of credible evidence for any mechanism to for a seismic event to cause the water table to rise to the elevation of the repository.
	3. Probability Model Support is Adequate	(1) Probability models are justified through comparison with output from detailed process level models and/or empirical observations (e.g., laboratory testing, field measurements, or natural analogs, including Yucca Mountain site data). Specifically: (a) For infrequent events, the U.S. Department of Energy justifies, to the extent appropriate, proposed probability models with data from reasonably analogous systems. Analog systems should contain significantly more events than the Yucca Mountain system, to provide reasonable evaluations of probability model performance; (b) The U.S. Department of Energy justifies, to the extent appropriate, the ability of probability models to produce results consistent with the timing and characteristics (e.g., location and magnitude) of successive past events in the Yucca Mountain system; and (c) The U.S. Department of Energy probability models for natural events use underlying geologic bases (e.g., tectonic models) that are consistent with other relevant features, events, and processes evaluated.	The prediction that glacial conditions will not occur at Yucca Mountain during the regulatory period is based upon a combination of a process model (Milankovich forcing) and the analogue climate stations that correspond to the data (oxygen isotope data and fossil data) from sites near Yucca mountain. Climate predictions are cited in the exclusion arguments in Section 6.4. The prediction that no seismic event will cause the water table to rise to the elevation of the repository (Section 6.8.3), is based on a lack of credible evidence for any mechanism to cause such a rise.

8.   REFERENCES AND INPUTS

8.1   DOCUMENTS CITED

The following is a list of the references cited in this document. Column 2 represents the unique six digit numerical identifier (the Document Input Reference System number), which is placed in the text following the reference callout (e.g., BSC 2002 [DIRS 160819]). The purpose of these numbers is to assist in locating a specific reference. Within the reference list, multiple sources by the same author (e.g., BSC 2002) are sorted alphabetically by title.

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8.2   CODES, STANDARDS, REGULATIONS, AND PROCEDURES

10 CFR 63. Energy: Disposal of High-Level Radioactive Wastes in a Geologic Repository at Yucca Mountain, Nevada. Readily available.

156605

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8.3   SOURCE DATA, LISTED BY DATA TRACKING NUMBER

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LA0311AM831341.001. Correlation Matrix for Sampling of Sorption Coefficient Probability Distributions. Submittal date: 11/06/2003.   167015

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LA0407AM831341.004. Batch Sorption Coefficient Data for Neptunium on Yucca Mountain Tuffs in Representative Water Compositions. Submittal date: 07/12/2004. 170622

LA0407AM831341.005. Batch Sorption Coefficient Data for Plutonium on Yucca Mountain Tuffs in Representative Water Compositions. Submittal date: 07/12/2004. 170625

LA0407AM831341.006. Batch Sorption Coefficient Data for Uranium on Yucca Mountain Tuffs in Representative Water Compositions. Submittal date: 07/12/2004. 170628

LA0408AM831341.001. Unsaturated Zone Distribution Coefficients (Kds) for U, Np, Pu, Am, Pa, Cs, Sr, Ra, and Th. Submittal date: 08/24/2004. 171584

LA9908JC831321.001. Mineralogic Model "MM3.0" Version 3.0. Submittal date: 08/16/1999. 113495

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LB02091DSSCP3I.002. 1-D Site Scale Calibrated Properties: Data Summary. Submittal date: 09/18/2002. 161433

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LB0302DSCPTHCS.002. Drift-Scale Coupled Processes (THC Seepage) Model: Data Summary. Submittal date: 02/11/2003.　　161976

LB0302PTNTSW9I.001. PTN/TSW Interface Percolation Flux Maps for 9 Infiltration Scenarios. Submittal date: 02/28/2003.　　162277

LB0302SCMREV02.002. Seepage-Related Model Parameters K and 1/A: Data Summary. Submittal date: 02/28/2003.　　162273

LB03033DUZTRAN.001. TC and NP Distributions/Transport in UZ Flow-Fields. Submittal date: 03/28/2003.　　170372

LB0304SMDCREV2.002. Seepage Modeling for Performance Assessment, Including Drift Collapse: Summary Plot Files and Tables. Submittal date: 04/11/2003.　　163687

LB0305PTNTSW9I.001. PTN/TSW Interface Percolation Flux Maps for 9 Alternative Infiltration Scenarios. Submittal date: 05/12/2003.　　163690

LB0305TSPA18FF.001. Eighteen 3-D Site Scale UZ Flow Fields Converted from TOUGH2 to T2FEHM Format. Submittal date: 05/09/2003.　　165625

LB0306DRSCLTHM.001. Drift Scale THM Model Predictions: Simulations. Submittal date: 06/26/2003.　　169733

LB0307DSTTHCR2.002. Drift-Scale Coupled Processes (DST Seepage) Model: Data Summary. Submittal date: 07/24/2003.　　165541

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LB0308DRSCLTHM.001. Drift Scale THM Model Predictions for Poor Quality Rock in Tptpll: Simulations. Submittal date: 08/29/2003.　　171567

LB0311ABSTHCR2.001. Drift Scale Coupled Process Abstraction Model (for Intact-Drift Case). Submittal date: 11/07/2003.　　166714

LB0311ABSTHCR2.003. THC Simulations Considering Drift Degradation: Summary/Abstraction Data Files. Submittal date: 11/07/2003. 166713

LB0312TSPA06FF.001. Six Flow Fields with Raised Water Tables. Submittal date: 12/23/2003. 166671

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LB990801233129.003. TSPA Grid Flow Simulations for AMR U0050, "UZ Flow Models and Submodels" (Flow Field #3). Submittal date: 11/29/1999. 122757

LB990801233129.009. TSPA Grid Flow Simulations for AMR U0050, "UZ Flow Models and Submodels" (Flow Field #9). Submittal date: 11/29/1999. 118717

LB9908T1233129.001. Transport Simulations for the Low, Mean, and Upper Infiltration Scenarios of the Present-Day, Monsoon, and Glacial Transition Climates for AMR U0050, "UZ Flow Models and Submodels." Submittal date: 03/11/2000. 147115

LL000122051021.116. Summary of Analyses of Glass Dissolution Filtrates. Submittal date: 01/27/2000. 142973

LL020711323125.001. Pre-Test Calculations for Grout Carbonation Experiments. Submittal date: 08/13/2002. 172026

LL030211423125.005. Cementitious Grout-Seepage Water Interaction. Submittal date: 02/02/2004. 172020

LL030211523125.006. EQ3/6 Modeling of Grout-Reacted Liquid Carbonation Experiments. Submittal date: 07/01/2003.

172021

MO0004QGFMPICK.000. Lithostratigraphic Contacts from MO9811MWDGFM03.000 to be Qualified Under the Data Qualification Plan, TDP-NBS-GS-000001. Submittal date: 04/04/2000.

152554

MO0004YMP98132.004. Flood Inundation Areas in the Vicinity of Yucca Mountain. Submittal date: 03/31/2000.

149806

MO0010CPORGLOG.003. Calculated Porosity Values at Depth Derived from Qualified Geophysical Log Data from Modern Boreholes. Submittal date: 10/16/2000.

155959

MO0011YMP00114.000. Potential Repository Site. Submittal date: 11/21/2000.

171565

MO0012MWDGFM02.002. Geologic Framework Model (GFM2000). Submittal date: 12/18/2000.

153777

MO0401MWDRPSHA.000. Results of the Yucca Mountain Probabilistic Seismic Hazard Analysis (PSHA). Submittal date: 01/21/2004.

166962

MO0407SEPFEPLA.000. LA FEP List. Submittal date: 07/20/2004.

170760

MO9906GPS98410.000. Yucca Mountain Project (YMP) Borehole Locations. Submittal date: 06/23/1999.

109059

MO9912GSC99492.000. Surveyed USW SD-6 As-Built Location. Submittal date: 12/21/1999.

165922

SN0306T0504103.005. Revised Groundwater Colloid Mass Concentration Parameters for TSPA (Total System Performance Assessment). Submittal date: 06/30/2003.

164132

SN0306T0504103.006. Revised Sorption Partition Coefficients (Kd Values) for Selected Radionuclides Modeled in the TSPA (Total System Performance Assessment). Submittal date: 06/30/2003.

164131

SN0308T0503100.008. Revised Frequency Distributions for Net Infiltrations and Weighting Factors Applied to Lower, Mean, and Upper Climates. Submittal date: 08/28/2003.

165640

SN0310T0505503.004. Initial Radionuclide Inventories for TSPA-LA. Submittal date: 10/27/2003.

168761

SNF40060298001.001. Unsaturated Zone Lithostratigraphic Contacts in Borehole USW SD-6. Submittal date: 10/15/1998.

107372

TM000000SD12RS.012. USW SD-12 Composite Borehole Log (0.0'-1435.3') and Weight Logs (1,438.8-2,151.7'). Submittal date: 09/08/1995. 105627

TMUSWNRG7A0096.002. Geophysical Logs for Borehole USW NRG-7/7A. Submittal date: 11/27/1996. 166424

8.4   OUTPUT DATA, LISTED BY DATA TRACKING NUMBER

LB0310FEPS0170.001.   Computations of Perched Water Volume in Repository Footprint and Flux through Repository. Submittal date: 10/31/2003.

LB0408U0170FEP.001. T2R3D transport calculations for flow fields with fracture apertures increased or decreased due to seismic activity. Submittal date: 09/01/2004.

LB0408U0170FEP.002.   Summary of transport calculations for flow fields with fracture apertures increased or decreased due to seismic activity.   Submittal date: 09/01/2004.

8.5   SOFTWARE CODES

BSC 2001. *Software Code: PHREEQC.* V2.3. PC, LINUX, Windows 95/98/NT, Redhat 6.2. 10068-2.3-00. 155323

LANL (Los Alamos National Laboratory) 2003. *Software Code: FEHM.* V2.21. SUN, SunOS 5.8; PC, Windows 2000 and Linux 7.1. 10086-2.21-00. 165741

LBNL (Lawrence Berkeley National Laboratory) 1999. *Software Code: T2R3D.* V1.4. FORTRAN 77, SUN, DEC/ALPHA. 10006-1.4-00. 146654

LBNL 2000. *Software Code: TOUGH2.* V1.4. Sun Workstation and DEC/ALPHA. 10007-1.4-01. 146496

LBNL 2002. *Software Code: TOUGHREACT.* V3.0. DEC ALPHA/OSF1 V5.1, DEC ALPHA/OSF1 V5.0, Sun UltraSparc/Sun OS 5.5.1, PC/Linux Redhat 7.2. 10396-3.0-00. 161256

LBNL 2003. *Software Code: WTRISE.* V2.0. PC/WINDOWS 2000/98; DEC ALPHA/OSF1 V5.1. 10537-2.0-00. 163453

LLNL (Lawrence Livermore National Laboratory) 1999. *Software Code: NUFT V3.0s.* V3.0s. 10088-3.0s-00. 127906

SNL (Sandia National Laboratories) 2001. *Software Code: Infil.* VA_2.a1. DEC Alpha, VMS AXP V7.2-1. 10253-A_2.a1-00. 147608

USGS (U.S. Geological Survey) 2001. *Software Code: INFIL.* V2.0. PC, Windows NT 4.0. 10307-2.0-00. 139422

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APPENDIX A

PERCHED WATER VOLUME

A1. COMPUTING PERCHED WATER VOLUME IN REPOSITORY FOOTPRINT AND FLUX THROUGH REPOSITORY

Perched water volumes and flux through the repository are evaluated here to support arguments concerning the potential effects of boreholes on drainage of perched water as discussed in Section 6.3.1 and seismic effects on perched water in Section 6.8.8. Perched water volumes and flux through the repository are extracted from the UZ flow model output data set contained in DTN: LB03023DSSCP9I.001 [DIRS 163044]. The files used are: the *.out* files contained within the zipped files *glaq_lA.tar.gz*, *glaq_mA.tar.gz*, *glaq_uA.tar.gz*, *monq_lA.tar.gz*, *monq_mA.tar.gz*, *monq_uA.tar.gz*, *preq_lA.tar.gz*, *preq_mA.tar.gz*, and *preq_uA.tar.gz*. (Here *glaq, monq,* and *preq* refer to the glacial-transition, monsoon, and present climate states, and *lA, uA,* and *mA* refer to flow fields with boundary conditions imposed by the lower, upper and mean infiltration maps.)

To assess the flux through the proposed repository horizon, the flux represented in the first 241,914 connections in the flux output are searched for flux through repository cells. The first 237,338 connections in the TOUGH2 output file are the vertical connections for the interior cells (not including the boundary cells), as can be seen in the mesh file. However, the additional 4,576 (horizontal) connections do not involve any of the 469 repository cells and, therefore, do not contribute to the calculations of vertical flux through the proposed repository.

The cells are first checked against the list of 469 repository cells. The first 62,000 connections are copied as text from the flow field output file (a text file created in Microsoft Word) to Microsoft Excel. The text in the Excel file is converted to column data using the "Text to Columns" function. The spreadsheet is then sorted in ascending order on Column 1. This sorts the fracture and matrix cells and also sorts the header information, which is deleted. The matrix cells are cut and pasted onto the second worksheet in the file. Columns F, G, H, and I are redundant and deleted. The 469 repository cell names are pasted into Column L. The following formulas are used to check which site-scale-model cells in Columns A and B are in the repository:

Frn = MATCH(Arn,L$1:L$469,0)

Grn = MATCH(Brn,L$1:L$469,0)

(Here *Frn* means any cell in column F of the worksheet, with *rn* representing the same row number on both sides of the equation, and similarly for other letter-designated columns). The list of gridblock names is needed for extracting the vertical flux through the repository zone from the file *total_rep_q.dat*. There are a total of 469 blocks within the repository zone; their names are listed in the file *REPO_Z*. Both these files are found in the attached compact disc for *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861], Appendix C) titled, *C.2/files in table C.2.5-1/*.

These are used for both the fracture and matrix worksheets. These expressions return the index number of Column L if the cell names match and return the error message #N/A if the cell names do not match. Similar manipulations are used for the flux output from TOUGH2, connections 62001–124000, 124001–186000, and 186001–241914. (Data from each of the nine flow fields is

divided into three segments to fit within the row-number limit of Microsoft Excel.) Once the cell identifications have been made for the glacial transition upper case, the same results for Columns F and G are copied onto the files generated for the other infiltration and climate scenarios. The manipulations are carried out for each of the nine flow fields. These files are saved as:

gt upper flux 1-62000.xls
gt upper flux 62001-124000.xls
gt upper flux 124001-186000.xls
gt upper flux 186001-241914.xls

gt mean flux 1-62000.xls
gt mean flux 62001-124000.xls
gt mean flux 124001-186000.xls
gt mean flux 186001-241914.xls

gt lower flux 1-62000.xls
gt lower flux 62001-124000.xls
gt lower flux 124001-186000.xls
gt lower flux 186001-241914.xls

ms upper flux 1-62000.xls
ms upper flux 62001-124000.xls
ms upper flux 124001-186000.xls
ms upper flux 186001-241914.xls

ms mean flux 1-62000.xls
ms mean flux 62001-124000.xls
ms mean flux 124001-186000.xls
ms mean flux 186001-241914.xls

ms lower flux 1-62000.xls
ms lower flux 62001-124000.xls
ms lower flux 124001-186000.xls
ms lower flux 186001-241914.xls

pd upper flux 1-62000.xls
pd upper flux 62001-124000.xls
pd upper flux 124001-186000.xls
pd upper flux 186001-241914.xls

pd mean flux 1-62000.xls
pd mean flux 62001-124000.xls
pd mean flux 124001-186000.xls
pd mean flux 186001-241914.xls

pd lower flux 1-62000.xls
pd lower flux 62001-124000.xls
pd lower flux 124001-186000.xls
pd lower flux 186001-241914.xls

For each case (1-62000, 620001-124000, 124001-186000, and 186001-241914), Columns A through G for the repository cells are copied and pasted into a summary file for the given climate scenario. The same operations are performed for the fractures and matrix on separate worksheets in the summary file. The data are then sorted by Columns G and F, respectively, in ascending order. Each cell has two vertical fluxes representing inflow and outflow. The second set of values ordered through Column G are cut and pasted into Columns I through O. Columns B, G, H, and M are not needed and deleted. "Duplicate" cells are identified in 24 instances due to the cells having the same name except for the case of one of the letters (that is, upper case vs. lower case), which are not distinguished by the MATCH command. The "duplicate" cells are identified manually in Column L by marking them with a "1." The other cells are marked with a "0" in Column L. The summary files with marked duplicates are stored in the following files (for each of the nine flow fields):

Repository cells with vertical flux and marked duplicates gt upper.xls
Repository cells with vertical flux and marked duplicates gt mean.xls
Repository cells with vertical flux and marked duplicates gt lower.xls
Repository cells with vertical flux and marked duplicates ms upper.xls
Repository cells with vertical flux and marked duplicates ms mean.xls
Repository cells with vertical flux and marked duplicates ms lower.xls
Repository cells with vertical flux and marked duplicates pd upper.xls
Repository cells with vertical flux and marked duplicates pd mean.xls
Repository cells with vertical flux and marked duplicates pd lower.xls

The worksheet is then sorted on Column L in descending order and the 24 "duplicates" are deleted. Column L is deleted, and Column A is copied into Column M. The larger of the two vertical fluxes is found through the following formula:

O_{rn} = IF(C_{rn}>I_{rn},C_{rn},I_{rn})

The total flux for each continuum is summed in Cell O470, and then the fracture and matrix flux are summed on the fracture worksheet in Cell O471. The total flux in kg/s is converted to kg/yr in Cell O473, using the following formula on the fracture worksheet:

O472 = O471*3600*24*365.25

This flux is converted to m^3/yr by dividing by the density (997 kg/m^3) in Cell O473 on the fracture worksheet. These results are saved in the following files:

Repository cells with vertical flux - gt upper.xls
Repository cells with vertical flux - gt mean.xls
Repository cells with vertical flux - gt lower.xls

Repository cells with vertical flux - ms upper.xls

Repository cells with vertical flux - ms mean.xls
Repository cells with vertical flux - ms lower.xls

Repository cells with vertical flux - pd upper.xls
Repository cells with vertical flux - pd mean.xls
Repository cells with vertical flux - pd lower.xls

Perched water volumes are extracted from the summary files described in Section A2. These summary files contain the capillary pressure, saturation, and volume information needed to determine perched water volumes. Only perched water within the fractures of the repository footprint is considered. For each climate–infiltration scenario, the segments are 61000–122000, 122001–184000, and 184001–245506. The segment 1–61000 is not needed because it doesn't contain any repository elements. For each case, Columns A through AN are sorted on Column T in descending order. This brings all of the repository footprint cells to the top of the list. The cells not in the footprint are deleted. The data in Columns A through AN are then sorted on the fracture capillary pressure in Column E in descending order. Cells with fracture capillary pressure less than 0 are deleted. The matrix data and layer properties are also deleted. The fracture bulk volume is given in Column L and fracture porosity in Column R.

The product of the bulk volume times the porosity gives the volume of water in the fracture cells (because the cell is saturated). This is computed as follows (here capital letters refer to columns and rn refers to any row number):

$$Vrn = Lrn*Rrn$$

The data are sorted in descending order, based on the permeability in Column S. The total fracture volume is computed as follows:

$$AC1 = SUM(V:V)$$

The total fracture volume in high-permeability fractures (permeability greater than 10^{-15} m^2) is found by first assigning the volumes of high-permeability fractures as follows:

$$Wrn = IF(Srn>10^-15,Vrn,0)$$

Then the volumes are summed:

$$AC2 = SUM(W:W)$$

These calculations are given in the following files:

gt upper perched 61001-122000.xls
gt upper perched 122001-184000.xls
gt upper perched 184001-245506.xls

gt mean perched 61001-122000.xls
gt mean perched 122001-184000.xls
gt mean perched 184001-245506.xls

gt lower perched 61001-122000.xls
gt lower perched 122001-184000.xls
gt lower perched 184001-245506.xls

ms upper perched 61001-122000.xls
ms upper perched 122001-184000.xls
ms upper perched 184001-245506.xls

ms mean perched 61001-122000.xls
ms mean perched 122001-184000.xls
ms mean perched 184001-245506.xls

pd lower perched 61001-122000.xls
pd lower perched 122001-184000.xls
pd lower perched 184001-245506.xls

pd upper perched 61001-122000.xls
pd upper perched 122001-184000.xls
pd upper perched 184001-245506.xls

pd mean perched 61001-122000.xls
pd mean perched 122001-184000.xls
pd mean perched 184001-245506.xls

pd lower perched 61001-122000.xls
pd lower perched 122001-184000.xls
pd lower perched 184001-245506.xls

The results of these extractions are summarized in Table A-1. Flux years are the total perched water volume in high permeability fractures divided by the total flow through the repository. This represents the amount of time needed through the percolation flux to generate the same volume of water as in the high-permeability fractures of the perched water zones.

Table A-1. Extraction Results

Scenario	Total Volume of Perched Water in High-Permeability Fractures (m^3)	Total Flow through Repository Footprint (m^3/yr)	Flux Years
Present day, Lower Infiltration	4.66E+02	2.00E+03	2.33E-01
Present day, Mean Infiltration	4.66E+02	2.07E+04	2.25E-02
Present day, Upper Infiltration	6.50E+02	6.03E+04	1.08E-02
Monsoon, Lower Infiltration	6.50E+02	2.31E+04	2.81E-02
Monsoon, Mean Infiltration	6.50E+02	6.18E+04	1.05E-02
Monsoon, Upper Infiltration	6.50E+02	1.58E+05	4.12E-03
Glacial transition, Lower Infiltration	6.50E+02	1.04E+04	6.25E-02
Glacial transition, Mean Infiltration	6.50E+02	9.75E+04	6.67E-03
Glacial transition, Upper Infiltration	1.19E+03	1.92E+05	6.22E-03

Output DTN: LB0310FEPS0170.001.

A2. EXTRACTING OUTPUT FROM UZ FLOW MODEL FOR SATURATION AND RELATIVE PERMEABILITY

Each of nine flow fields contains data for saturation and relative permeability. The flow field output is given in DTN: LB03023DSSCP9I.001 [DIRS 163044]. For each flow field, the output for cells 1–61000, 61001–122000, 122001–184000, and 184001–245506 were copied as text from text files downloaded from the DTN and pasted into Microsoft Excel as text. The text was then converted to Columns (A through H) in the spreadsheet using the Excel function "text to columns." The spreadsheet was sorted by cell name in ascending order, and the header information was deleted. Columns A through G of the mesh files for the same range of cells were copied into Columns J through P and Column H (with the repository footprint designation) was copied into Column T. The assignment of the footprint designation is discussed in Section A3. All of the matrix elements were cut from the bottom of the file and pasted into Columns V through AN such that the fracture cells in Column A match the matrix cells in Column V.

Data for the porosity and permeability by rock type was extracted from a file in DTN: LB03023DSSCP9I.001 [DIRS 163044] (e.g., *glaq_uA.dat*). This information was copied into Columns AP through AR, with the rock type designation in Column AP, the porosity of the rock type in Column AQ, and the permeability of the rock type in Column AR. The porosity and permeability for the fractures and matrix were then assigned to each grid.

First, the rock type of the fractures in Column K and the rock type of the matrix in Column AF were compared with the rock types in Column AP:

$Qrn = MATCH(Krn,AP1:AP98,0)$ for the fractures

$ALrn = MATCH(AFrn,AP1:AP98,0)$ for the rock matrix

The MATCH function returns the array index of the first value in Column AP that matches the value in Columns K or AF. This index is then used to extract the porosity and permeability as follows:

$Rrn = INDEX(AQ\$1:AQ\$98,\$Qrn)$ for fracture porosity
$Srn = INDEX(AR\$1:AR\$98,\$Qrn)$ for fracture permeability
$AMrn = INDEX(AQ\$1:AQ\$98,\$ALrn)$ for matrix porosity
$ANrn = INDEX(AR\$1:AR\$98,\$ALrn)$ for matrix permeability

The resulting output files are:

gt upper 1-61000.xls
gt upper 61001-122000.xls
gt upper 122001-184000.xls
gt upper 184001-245506.xls

gt mean 1-61000.xls
gt mean 61001-122000.xls
gt mean 122001-184000.xls
gt mean 184001-245506.xls

gt lower 1-61000.xls
gt lower 61001-122000.xls
gt lower 122001-184000.xls
gt lower 184001-245506.xls

ms upper 1-61000.xls
ms upper 61001-122000.xls
ms upper 122001-184000.xls
ms upper 184001-245506.xls

ms mean 1-61000.xls
ms mean 61001-122000.xls
ms mean 122001-184000.xls
ms mean 184001-245506.xls

ms lower 1-61000.xls
ms lower 61001-122000.xls
ms lower 122001-184000.xls
ms lower 184001-245506.xls

pd upper 1-61000.xls
pd upper 61001-122000.xls
pd upper 122001-184000.xls
pd upper 184001-245506.xls

pd mean 1-61000.xls
pd mean 61001-122000.xls
pd mean 122001-184000.xls
pd mean 184001-245506.xls

pd lower 1-61000.xls
pd lower 61001-122000.xls
pd lower 122001-184000.xls
pd lower 184001-245506.xls

A3.   EXTRACTION OF REPOSITORY FOOTPRINT FROM MESH FILE

Extract from the file *mesh_2kb.dkm* (from DTN: LB03023DSSCP9I.001 [DIRS 163044]) under the ELEM label the mesh in three, 64000-row groups and one 53,506-row group.   This comprises the entire listing of cells for the three-dimensional UZ site-scale flow model.   Store these in files called the following:

1-64000 1st file.xls
64001-128000 1st file.xls
128001-192000 1st file.xls
192001-245506 1st file.xls

The structure of the grid leads to many cells having the same x-y coordinates. The ELEM file is also structured such that these cells are listed in adjacent rows. The "raw" cell information is trimmed to contain only the cell name and the x and y coordinates (Columns E and F in the "1st files"). These are given in Columns A, B, and C. Columns D and E contain a repeat of the contents of B and C. In Column F, the following formula is applied:

$$Frn = IF(Drn=Drn-1,IF(Ern=Ern-1,Frn-1+1,1))$$

where Drn = the element of Column D in the same row as in Column F. The exception is in row 1, where F1=1. This generates a count of the number of consecutive rows with the same x-y coordinates. A "reverse count" is done in Column G by initiating the count from the last row using the following formula:

$$Grn = IF(Drn+1=Drn,IF(Ern+1=Ern,1+Grn+1,1),1)$$

Column F is used to identify the first (top) grid with the given x-y coordinate using the following formula in Column H:

$$Hrn = IF(Frn=1,1,0)$$

Column I is used to identify the total number of consecutive rows having the same x–y coordinate using the following formula:

$$Irn = IF(Hrn=1,Grn,0)$$

The results of these calculations are stored in the following files:

1-64001 sorting for independent x-y 2nd file.xls
64001-128000 sorting for independent x-y 2nd file.xls
128001-192000 sorting for independent x-y 2nd file.xls
192001-245506 sorting for independent x-y 2nd file.xls

The results are sorted by Column H, which contains 1 or 0 depending on whether or not the cell is at the top of a column of cells or not. Only cells with a 1 in Column H are retained. 531 independent columns are identified. Note that the values in Column I give the number of cells in the column having the same x–y values. Repository cells are identified in file *rep.xls* in Output-DTN: LB0310FEPS0170.001. Plots confirm that these cells lie within the proposed repository footprint. The list of repository cells in the UZ grid and the cell coordinates are given in *repository cells.xls*.

The drift end-point coordinates in meters (Nevada State Plane coordinates) for the repository design are given in *Repository Design, Repository/PA IED Subsurface Facilities* (BSC 2003 [DIRS 161727]).

Plots shown in Figures A-1 and A-2 show the correspondence between the UZ grid coordinates for the repository cells and the design coordinates for the endpoints of the waste emplacement drifts.
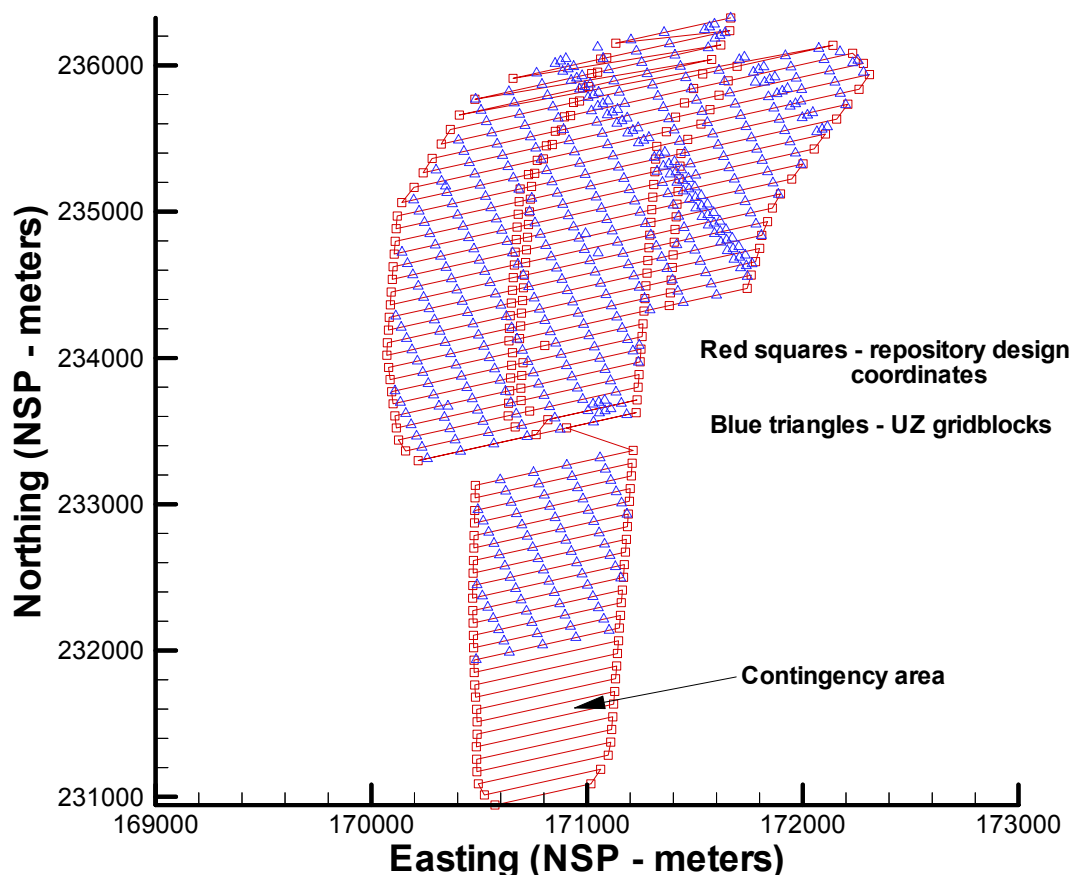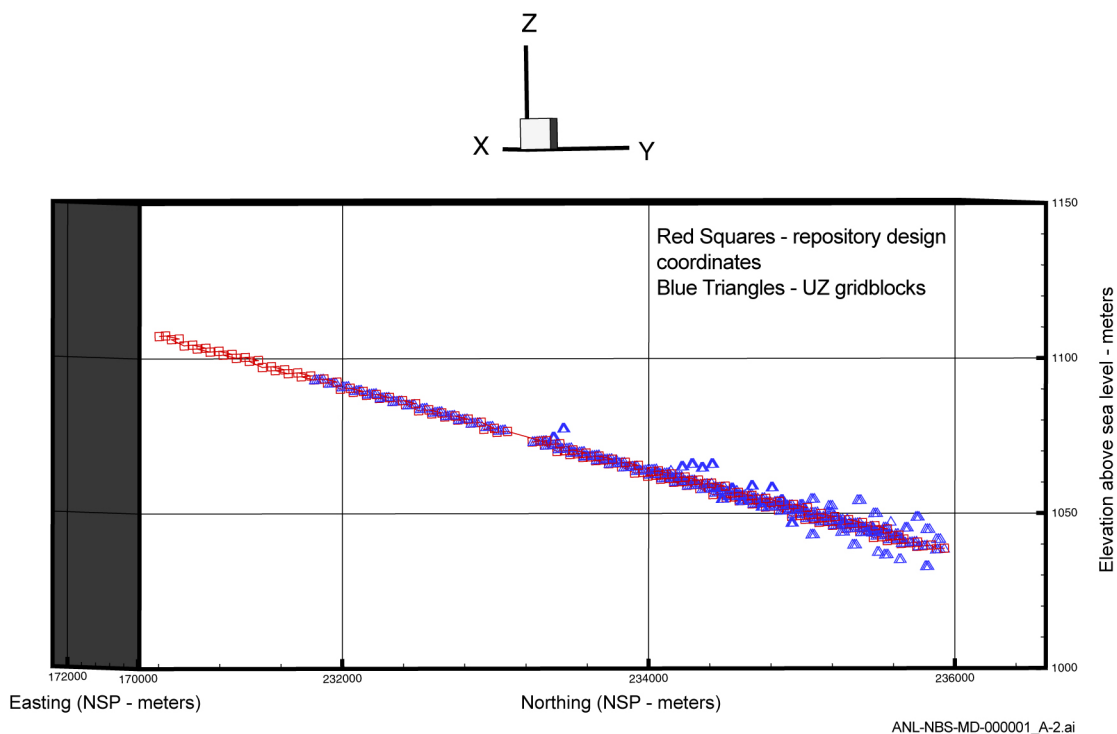
DTNs: LB0310FEPS0170.001 [output]; LB03023DSSCP9I.001 [DIRS 163044].

Figure A-1. Coordinates of UZ Grid Repository Gridblocks Compared with Repository Design Drift
        Endpoint Coordinates (Plan View)

The remaining results described here are for processing the cells 64001 to 128000. The same procedure is applied to the other cell groupings (128001 to 192000 and 192001 to 245506), but the specific number of cells involved changes. The x-y coordinates for the UZ grid in the repository are compared against the x–y coordinates of the grid columns identified for "top" cells. Repository easting coordinates are put in row 1 in Columns K through IK and repository northing coordinates are put in row 2, Columns K through IK. This accounts for 235 repository x–y coordinates. The remaining 234 coordinates are put in rows 534 and 535 following the last identified "top" cell, Columns K through IJ. Then, the x–y coordinate for the grid columns in Columns B and C, rows 3 through 533, are compared with the repository x–y coordinates using the following formula:

clrn = IF(ABS(cl$1-$Brn)<10,1,0)*IF(ABS(cl$2-$Crn)<10,1,0)

DTN: LB0310FEPS0170.001 [OUTPUT]; DTN: LB03023DSSCP9I.001 [DIRS 163044].

Figure A-2. Coordinates of UZ Grid Repository Gridblocks Compared with Repository Design Drift Endpoint Coordinates (Elevation)

Here, cl$1 designates a value from row 1 with a variable column letter (cl). This is notation analogous to the use of rn for a variable row number. This formula identifies if the grid column and the repository cell lie within 10 m of each other in both the northing and easting directions. If so, a value of 1 is returned and the column lies within the repository footprint. If not, a value of 0 is returned and the cell lies outside the repository footprint. For the repository cells coordinates in rows 534 and 535, an analogous formula is used:

cl(rn+533) = IF(ABS(cl$534-$Brn)<10,1,0)*IF(ABS(cl$535-$Crn)<10,1,0)

Column J is used to sum the values across the spreadsheet columns to find if a UZ grid column lies within the footprint:

Jrn = SUM(Krn:IKrn)

For rn = 3 to 533

and

Jrn = SUM(Krn:IJrn)

For rn = 536 to 1066.

These files are saved as:

1-64000 comparison with repository x-y 3rd file.xls
64001-128000 comparison with repository x-y 3rd file.xls
128001-192000 comparison with repository x-y 3rd file.xls
192001-245506 comparison with repository x-y 3rd file.xls

Because of the large number of "top" cells in the first 64,000 cells, the x–y 3rd file is split into two parts, Part 1 one for the first 235 repository cell comparison and Part 2 for the second 234 repository cell comparison. Note that no cells were found within the footprint for cells 1–64,000. Therefore, further processing for this group is not needed. The results in Column J from rows 536 to 1,066 are combined with the results for Column J from rows 3 to 533, such that if a "1" is returned from either list, the value of Column J is "1" and "0" otherwise. The data from these files are then sorted by Column J to reduce the to spreadsheet entries to the footprint columns in the UZ grid. Then Column A contains the node name for the top of each footprint column in the UZ grid, Columns B and C contain the x–y coordinates and Column D contains the number of elements in each UZ grid column. This results in 352 columns in the repository footprint. The top cell names and the number of elements in each grid are transposed into rows 3 and 4, respectively from Columns F through IS (248 cells) and in rows 251 and 252, Columns F through DE (104 cells). These spreadsheets are saved as:

64001-128000 repository footprint top cells 4th file.xls
128001-192000 repository footprint top cells 4th file.xls
192001-245506 repository footprint top cells 4th file.xls

The files containing the ELEM information are then reopened (see "1st files" discussed above). Rows 1 and 2, Columns F through IS are copied to rows 1 and 2 of the corresponding 1st file in Columns I through IV from the 4th files. The repository footprint top cells for each column are compared with the cells in Column A of the spreadsheet using the formula:

clrn = IF(cl\$1=\$Arn,cl\$2,0)

Thus, if the cell name from the ELEM information in Column A equals the top cell of a grid column inside the footprint, the value of the number of cells in that grid column returned. If not, a value of 0 is returned. Once all columns have been checked, the values for each row are summed using the following formula:

=SUM(Irn:IVrn)

for rows 3 through the last element in each spreadsheet.

The results are stored in:

64001-128000 construct footprint tag for cells part 1 5th file.xls
128001-192000 construct footprint tag for cells part 1 5th file.xls
192001-245506 construct footprint tag for cells part 1 5th file.xls

The same search operation is conducted on the "1ˢᵗ file" using the repository top cell names and # of elements from rows 251 and 252, Columns F through DE of the "4ᵗʰ file." The results are stored in:

64001-128000 construct footprint tag for cells part 2 5th file.xls
128001-192000 construct footprint tag for cells part 2 5th file.xls
192001-245506 construct footprint tag for cells part 2 5th file.xls

The "1ˢᵗ file" is again reopened and the results from Columns H in part 1 and part 2 of the 5ᵗʰ files are copied into Columns H and I respectively for the 1ˢᵗ file. The combination of columns H and I give the total number of cells in each column of the footprint and are computed in Column J using the formula:

$$Jrn = Hrn + Irn$$

The cells are identified in Column K as to whether or not the corresponding cell lies in the footprint through the following formula:

$$Krn = IF(K(rn-1)>1, K(rn-1)-1, 2*J2)$$

This formula initiates a count at the top cell if the previous cell in Column K is 0 or 1 and if J in the given row is greater than 0. The count is initiated as $2*Jrn$ because there are fracture and matrix cells in each column. Then each cell is given a designation as being in the repository footprint in Column L using the following formula:

$$Lrn = IF(Krn>0, "RF", 0)$$

The results are saved in the following files:

1-64000 cells with footprint tag 6th file.xls
64001-128000 cells with footprint tag 6th file.xls
128001-192000 cells with footprint tag 6th file.xls
192001-245506 cells with footprint tag 6th file.xls

The file is then consolidated to Columns A through G and Columns H through K are deleted leaving Column G containing either a 0 (outside footprint) or and "RF" denoting inside the footprint. These are saved as:

1-64000 cells with footprint tag summary 7th file.xls
64001-128000 cells with footprint tag summary 7th file.xls
128001-192000 cells with footprint tag summary 7th file.xls
192001-245506 cells with footprint tag summary 7th file.xls

Note that files for steps 4, 5, and 6 for the cells 1–64,000 were not created because there are no repository footprint cells in these first 64,000 cells.

For subsequent uses, these four sets of files were broken down into the following:

1-61000 cells with footprint tag.xls
61001-122000 cells with footprint tag.xls
122001-184000 cells with footprint tag.xls
184001-245506 cells with footprint tag.xls

In addition, these groupings were ordered (in ascending order) by the cell names in Column A, which segregates the fracture and matrix cells.
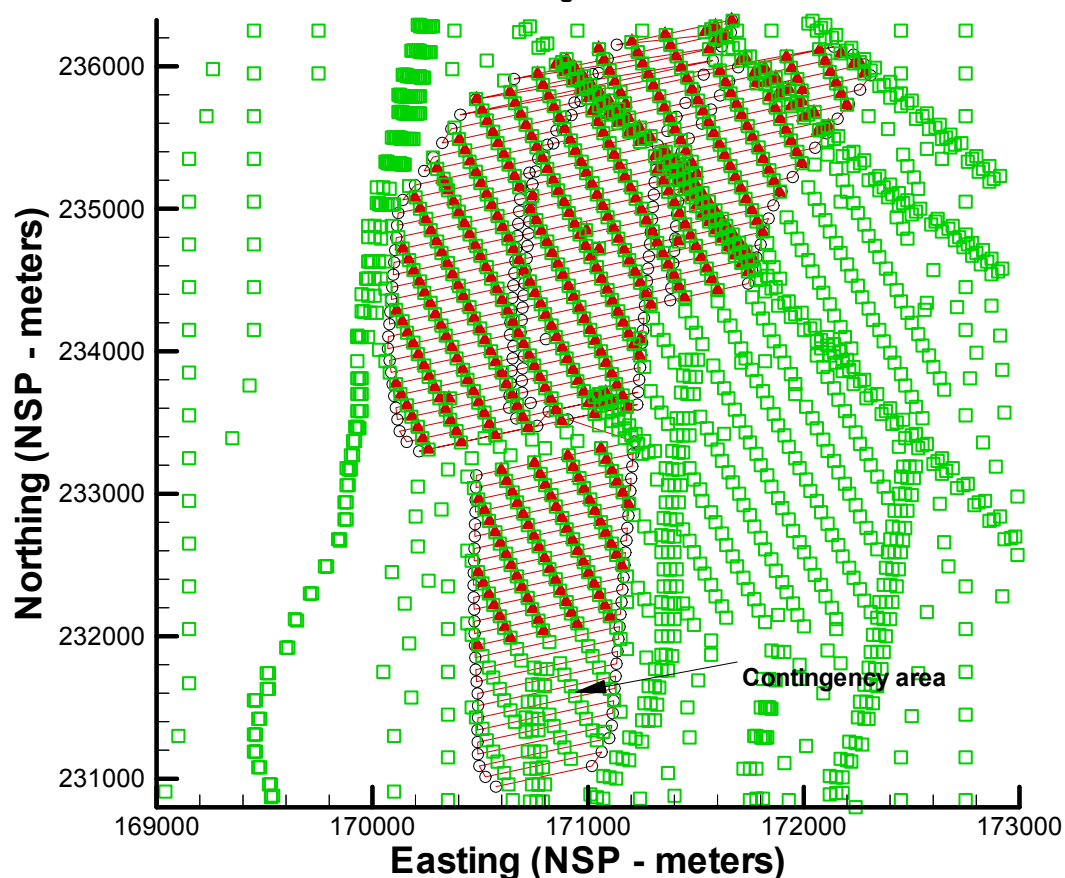
File information including all file names, file dates and times, and file sizes are documented in DTN: LB03023DSSCP9I.001 [DIRS 163044] and output DTN: LB0310FEPS0170.001.

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APPENDIX B

PTn LOCATIONS RELATIVE TO WASTE EMPLACEMENT

Figure B-1 shows the PTn coverage over the UZ flow model and waste emplacement areas. The PTn is present over all waste emplacement locations. The coordinates for the PTn are given in the mesh_3dn.dkm file of DTN: LB03023DSSCP9I.001 [DIRS 163044]. The repository coordinates are in file rep.xls in Output-DTN: LB0310FEPS0170.001.

Source: DTN: LB03023DSSCP9I.001 [DIRS 163044] LB0310FEPS0170.001 [output].

NOTE: Green squares – UZ model grid locations with PTn cover; Red triangles – UZ model repository grid locations; Black circles – waste emplacement drift endpoints.

Figure B-1. PTn Coverage over the UZ Flow Model and Waste Emplacement Areas

File information including all file names, file dates and times, and file sizes are documented in DTN: LB03023DSSCP9I.001 [DIRS 163044] and output DTN: LB0310FEPS0170.001.

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APPENDIX C

QUALIFICATION OF UNQUALIFIED DATA

Some data used as direct input (Tables 4-1 and 4-2) were acquired during earlier studies sponsored by the DOE Nevada Nuclear Waste Storage Investigation, before the establishment of a 10 CFR 60, Subpart G-compliant quality assurance program. These data have been qualified in Sections C1 through C3 and C5 through C11, in accordance with AP-SIII.2Q, *Qualification of Unqualified Data*.

Other data used as direct input were obtained from outside sources. These data are demonstrated in Sections C4 to be suitable for use within this report in accordance with AP-SIII.9Q, *Scientific Analyses*.

Other data used as direct input were obtained from the product output of a superseded or cancelled document. These data are demonstrated in Sections C12 through C15 to be suitable for use within this report in accordance with AP-SIII.9Q. See Section D3.1 for justification for the use of DTNs developed for the TSPA model for Site Recommendation.

All other direct input data are qualified.

C1. STRESS FIELD AT YUCCA MOUNTAIN

References:

Stock, J.M. and Healy, J.H. 1988. "Stress Field at Yucca Mountain, Nevada." Chapter 6 of *Geologic and Hydrologic Investigations of a Potential Nuclear Waste Disposal Site at Yucca Mountain, Southern Nevada*. Carr, M.D. and Yount, J.C., eds. Bulletin 1790. Denver, Colorado: U.S. Geological Survey. TIC: 203085 [DIRS 101022].

Stock, J.M.; Healy, J.H.; Hickman, S.H.; and Zoback, M.D. 1985. "Hydraulic Fracturing Stress Measurements at Yucca Mountain, Nevada, and Relationship to the Regional Stress Field." *Journal of Geophysical Research, 90*, (B10), 8691-8706. Washington, D.C.: American Geophysical Union. TIC: 219009 [DIRS 101027].

Description of Use:

Stock and Healy (1988 [DIRS 101022]) measured in-situ stresses in four boreholes (USW G-1, USW G-2, USW G-3, and UE25p1) and found that in all four boreholes $S_v > S_H > S_h$, where subscripts v, H, and h represent the vertical, greatest horizontal, and least horizontal stress, respectively. This corresponds to a normal faulting regime. The direction of least horizontal stress was N 60° W to N 65° W. Stock et al. (1985 [DIRS 101027]) report the same data. The data are used in Section 6.8.3 to show that USW G-2, north of the repository, is in the same normal-faulting regime as the other boreholes.

Extent and Quality of Corroborating Data: These data are qualified by comparison with DTN: SNF37100195002.001, which reports the mean of five hydraulic fracturing in situ stress measurements in a 30 m borehole drilled from the thermal test facility alcove in the ESF. The values reported there also show $S_v > S_H > S_h$, with S_h acting in N 75° W (±14°).

Because DTN: SNF37100195002.001 is qualified and the values agree with those reported in Stock and Healy (1988 [DIRS 101022]) and Stock et al. (1985 [DIRS 101027]), the data of Stock and Healy (1988 [DIRS 101022]) and Stock et al. (1985 [DIRS 101027]) are qualified by corroboration.

Qualifications of Personnel or Organizations Generating the Data: Joann M. Stock is Professor of Geology and Geophysics at California Institute of Technology. Her research interests involve a wide range of tectonic problems, including global and regional plate tectonic questions, including Tectonic Evolution of the Gulf of California and Stress Field variations around the Los Angeles region. She holds B.S., M.S., and Ph.D. from Massachusetts Institute of Technology.

C2. WATER TABLE EXCURSIONS INDUCED BY SEISMIC EVENTS

Reference: Carrigan, C.R.; King, G.C.P.; Barr, G.E.; and Bixler, N.E. 1991. "Potential for Water Table Excursions Induced by Seismic Events at Yucca Mountain, Nevada." *Geology, 19*, (12), 1157-1160. Boulder, Colorado: Geological Society of America. TIC: 242407 [DIRS 100967].

Description of Use: Numerical simulations by Carrigan et al. (1991 [DIRS 100967]) of tectonohydrological coupling involving earthquakes typical of the Basin and Range province (~ 1 m slip) produced 2 to 3 m excursions of a water table 500 m below ground surface. Extrapolation to an event of about 4 m slip would result in a transient rise of 17 m near the fault (Carrigan et al. 1991 [DIRS 100967], p. 1,159). These data are used in Section 6.8.3 as typical examples to exclude FEP 1.2.10.01.0A, Hydrologic response to seismic activity.

Extent to which the Data Demonstrate the Properties of Interest: Changes in water level due to seismic activity are identified in the FEP description as being possibly of consequence. Numerical simulations by Carrigan et al. (1991 [DIRS 100967]) of tectonohydrological coupling involving earthquakes typical of the Basin and Range province (~ 1 m slip) produced 2 to 3 m excursions of a water table 500 m below ground surface. Extrapolation to an event of about 4 m slip would result in a transient rise of 17 m near the fault (Carrigan et al. 1991 [DIRS 100967], p. 1,159). Carrigan et al. (1991 [DIRS 100967]) modeled a 100 m wide fracture zone centered on a vertical fault, with vertical permeability increased by a factor of 10^3. Water level excursions in the fracture zone were twice as great as in the adjacent block. For a fault-fracture zone with 1 m slip, transient excursions of about 12 m can occur.

Extent and Quality of Corroborating Data: These simulated water-table rises are qualified by corroboration with observations cited by Carrigan et al. (1991 [DIRS 100967]). The Dixie Valley – Fairview Peak, Nevada, earthquake, magnitude ~7, produced water table excursions of 1 to 3 m, as well as long-term changes in the regional hydrology (Raney 1988 [DIRS 147173], p. 44). The 1983 Borah Peak, Idaho earthquake, magnitude ~7.3, caused increases of about 4 m, with water levels returning to normal within 2 weeks to 2 months (Dudley 1990 [DIRS 147175]). These data serve to qualify the simulation results.

An independent model by Bredehoeft (1992 [DIRS 101122]) calculated a 1-m water table rise due to a magnitude 6 earthquake; this is consistent with the data cited above and the results of Carrigan et al. (1991 [DIRS 100967]).

C3.   EXTENT OF CONTACT METAMORPHISM RESULTING FROM AN IGNEOUS EVENT

Reference: Valentine, G.A.; WoldeGabriel, G.; Rosenberg, N.D.; Carter Krogh, K.E.; Crowe, B.M.; Stauffer, P.; Auer, L.H.; Gable, C.W.; Goff, F.; Warren, R.; and Perry, F.V. 1998. "Physical Processes of Magmatism and Effects on the Potential Repository: Synthesis of Technical Work Through Fiscal Year 1995." Chapter 5 of *Volcanism Studies: Final Report for the Yucca Mountain Project*. Perry, F.V.; Crowe, B.M.; Valentine, G.A.; and Bowker, L.M., eds. LA-13478. Los Alamos, New Mexico: Los Alamos National Laboratory. TIC: 247225 [DIRS 119132].

Description of Use: Data cited are used in Section 6.8.1 and 6.8.4 to exclude FEPs 1.2.04.02.0A, Igneous activity changes rock properties and 1.2.10.02.0A, Hydrologic response to igneous activity. The data show that contact metamorphism from intrusive dikes is generally confined to distances of a few meters around the dike. This area is too small to have a significant effect on the overall hydrologic properties of the UZ.

Extent to which the Data Demonstrate the Properties of Interest: The data show that the hydrologic effect of igneous intrusion effect is limited in extent.

Extent and Quality of Corroborating Data: WoldeGabriel et al. (1999 [DIRS 110071]) studied the effects of a basaltic intrusion at Grants Ridge, New Mexico, on the country rock, consisting of silicic tuffs and volcaniclastic sediments. The field and laboratory data suggest that the physical changes due to the thermal effects of the intruded plug were confined to within 10 m of the plug. The reason for this localized effect is that the rock was unsaturated at the time of the intrusion.   Lack of water prevented fluid-driven convective heat transfer, hydrothermal circulation, and extensive alteration of the country rock. These observations corroborate the data of Valentine et al. (1998 [DIRS 119132], p. 5-74) and confirm that the effects of igneous intrusion are into unsaturated tuff are localized.

Qualifications of Personnel or Organizations Generating the Data: Greg A. Valentine leads the Hydrology, Geochemistry, and Geology Group at Los Alamos National Laboratory. He is technical lead for igneous consequences at the Yucca Mountain Project. His fields of research include numerical simulation of flow in porous media, explosive volcanic eruptions and magma chamber dynamics. His field studies are related to volcanic hazards assessment, large-volume pyroclastic eruptions, fossil hydrothermal systems, intrusion mechanisms and dynamics. Dr. Valentine received his Ph.D.   in Geological Sciences (1988) from the University of California, Santa Barbara and a B.S. in Geological Engineering and Geology (1984) from the New Mexico Institute of Mining and Technology.

C4.   LIMITED ENTRAINMENT OF CLAY PARTICLES

Reference: Vanoni, V.A., ed. 1977. "Sediment Transportation Mechanics." *Sedimentation Engineering*. Pages 17-315. New York, New York: American Society of Civil Engineers. Figure 2-51. TIC: 255225 [DIRS 164901].

Description of Use: This Figure shows experimental data on clay erosion caused by entrainment of particles in flowing water. The data show that entrainment of particles ceased after 5 days, for a variety of experimental conditions. These data are used in Section 6.4.4 to exclude FEP 2.1.09.21.0C Transport of particles larger than colloids in the UZ.

Reliability of Source of the Data: This book was prepared by the Task Committee for the Preparation of the Manual on Sedimentation of the Sedimentation Committee of the Hydraulics Division of the American Society of Civil Engineers. As such, it represents the standard engineering practice under the auspices of the principal professional association concerned with sediment transport. Professor Vito Vanoni (1904-1999) was on the faculty at California Institute of Technology and was a recognized expert in the field of sediment transport and engineering.

C5.   EFFECT OF RADIOACTIVE WASTE HEAT ON SOIL TEMPERATURE

Reference: CRWMS M&O 1999. *Impact of Radioactive Waste Heat on Soil Temperatures*. BA0000000-01717-5700-00030 REV 0. Las Vegas, Nevada: CRWMS M&O. ACC: MOL.19990309.0403 [DIRS 103618].

Description of Use: This is a 1-D simulation of soil temperature for a repository heat load of 900 mW/m^2. It is used in Section 6.9.9 to demonstrate that the soil will not become so hot as to change the vegetation cover. A change in the vegetation cover would change the hydrologic properties; the results of this simulation show that no such change would occur. This conclusion provides the basis to exclude FEP 2.2.10.01.0A, Repository-induced thermal effects on flow in the UZ.

Extent to which the Data Demonstrate the Properties of Interest: The simulated temperatures show temperature at various depths in the soil. At 2 m depth, CRWMS M&O (1999 [DIRS 103618], Figure 30) shows a maximum temperature increase of 0.8 °C above ambient. This increase would be superimposed on the annual temperature cycle.

Extent and Quality of Corroborating Data: Three-dimensional coupled TH simulations have been done.   The temperature profiles shown in *Mountain-Scale Coupled Processes (TH/THC/THM)* (BSC 2004 [DIRS 169866], Figure 6.3.1-6) for Column h47, at 170743.5 m E and 235090.3 m N (near the center of the repository) can be taken as representative.   The maximum temperature gradient shown in that figure is 0.33 °C/m. At 2 m depth, this is 0.66 °C increase over ambient, which agrees with *Impact of Radioactive Waste Heat on Soil Temperatures* (CRWMS M&O 1999 [DIRS 103618] Figure 30). A slightly cooler temperature would be expected in this case because the three-dimensional model allows some heat loss in lateral directions, and also because this model includes preclosure ventilation. Both data sets confirm that the soil temperature increase will not be great enough to affect the hydrology through loss of vegetation.

C6. EFFECTS OF CEMENTITIOUS MATERIAL ON GROUNDWATER QUALITY

Reference: DTNs: LB0408CMATUZFT.003 [DIRS 171705]; LB0408CMATUZFT.004 [DIRS 171706]

Description of Use: These data show that leachate from the cementitious materials and their reaction products will be similar in water quality to ambient pore water; therefore, the presence of cementitious materials will not significantly change the transport of radionuclides. They are used in Section 6.9.2 to support the exclusion of FEP 2.2.01.01.0B, Chemical effects of excavation and construction in the near-field.

Extent to which the Data Demonstrate the Properties of Interest: The property of interest is the chemistry of leachate of cementitious materials. This is shown to be similar to the native groundwater.

Qualifications of Personnel or Organizations Generating the Data: John Apps holds the B.Sc. in Mining Geology with First Class Honors from Imperial College of Science and Technology, London, and A.M. and Ph.D. in Geology from Harvard University. In the past has served on Waste Management as a member of the Panel on Savannah River Plant Wastes, and the Engineering Review Group of Office of Nuclear Waste Isolation.

Technical Assessment: Qualification of DTN: LB0408CMATUZFT.003 [DIRS 171705]; LB0408CMATUZFT.004 [DIRS 171706] is based upon the qualified status of their source DTNs, the qualified status of the software used to develop the data, and the following argument that the input data and software were used correctly.

1.   DTN: LB0408CMATUZFT.002 [DIRS 172022] presents results of calculations based on the Papadakis (2000 [DIRS 172019]) model of the rates of carbonation of the cementitious materials.   This effect is important because it causes subsequent infiltration water to contact calcite rather than the reactive cementitious materials that can generate high pH values and high calcium concentrations. A water reacting with calcite results in concentrations typical of ambient pore water (circumneutral pH and moderate cation concentrations).

2.   DTN: LB0408CMATUZFT.003 [DIRS 171705] presents calculations of the horizontal spreading of the plume as a result of hydrodynamic dispersion and molecular diffusion. These calculations show that horizontal spreading is minimal.

3.   DTN: LB0408CMATUZFT.004 [DIRS 171706] presents the results of EQ3/6 7.2b calculations on the equilibrium phase assemblage expected after hydrothermal (elevated temperature, in the presence of water) reaction with the cementitious materials. These phase assemblages are presented as a function of the calcium and silica contents of the cement. This is important, since reaction will have the effect of generating new assemblages that produce lower pH values when leached with water than would be obtained by reaction with a portlandite-based cement.

4.   Already-qualified experimental data (DTNs: LL030211423125.005 [DIRS 172020] and LL030211523125.006 [DIRS 172021]) are used to support the argument that CO_2

gas present in the drift environment will react with any hyperalkaline plume that is generated, reducing both the solution pH and the calcium concentration to values close to ambient pore water values.

DTN: LB0408CMATUZFT.002 [DIRS 172022], which presents the results of calculations carried out with the Papadakis (2000 [DIRS 172019]) model. This model provides rates of carbonation of Portland cement as a result of the diffusion of CO_2 gas through the pores of the cement, where it reacts with the phases there to form calcite. The model assumes rates are limited by the rate of diffusion of CO_2 through the pores—no limitation based on the intrinsic rate of reaction with CO_2 is considered. In addition, the process requires that an aqueous film wetting the cementitious grain be present, since the aqueous phase is the medium in which the reaction occurs. It is possible that the Papadakis (2000 [DIRS 172019]) equation will not hold up at very low relative humidities, since in this case the aqueous film wetting the cement grains may be only partly present. Otherwise, the Papadakis (2000 [DIRS 172019]) model is a straightforward implementation of the analytical solution for gas diffusion, which then provides the rate at which the carbonation front (conversion to calcite) occurs. It is implemented here with the software Excel, which is exempt from software qualification requirements. Similar calculations were used to plan carbonation tests over a 1-DTN DTN: LL020711323125.001 [DIRS 172026])—the calculations presented here use the same Papadakis model, but are extended to time scales of 50 years (Ziegler 2004 [DIRS 171694], Table D-5), with data presented in DTN: LB0408CMATUZFT.002 [DIRS 172022]). A range of input values of Portlandite cement, silica fume, and water content in the cement recipe are considered—these control the porosity of the resulting cement, which controls the rate of CO_2 gas diffusion through the pores. Also considered in Ziegler (2004 [DIRS 171694], Table D-5) are ranges in the relative humidity, which is the other control besides the porosity on the rate of CO_2 diffusion through the pores of the cement. These input parameters cover the range of likely conditions and materials to be used in the drift environment. Since the Papadakis (2000 [DIRS 172019]) model is based on a well known analytical solution to the diffusion equation and it has been calibrated independently for different cement "recipes" (the relative proportions of water, Portland cement, and silica fume), the data produced from the model can be accepted as qualified.

DTN: LB0408CMATUZFT.003 [DIRS 171705] presents calculations on the horizontal spreading of an aqueous plume as result of both hydrodynamic dispersion and molecular diffusion. The input values for these calculations are based on independently qualified data. These qualified input data are clearly identified. The calculation itself is a straightforward one based on analytical solutions to the diffusion-dispersion equation in which Fick's Law (diffusion and dispersion is proportional to the concentration gradient) is used. The calculations were carried out with the commercial software Microsoft Excel, thus, removing the need to qualify the software.

DTN: LB0408CMATUZFT.004 [DIRS 171706] presents calculations using the qualified code EQ3/6 version 7.2b (database DATA.0) of the equilibrium phase assemblage as a function of differing calcium and silica contents of the cement. These calculations demonstrate that elevated temperatures, as are expected in the drift environment, will convert the primary assemblage of portlandite $(CaOH)_2$) and silica fume to other phases. These other phases, when reacted with water, will show a lower pH than would a water reacted with portlandite (Ziegler 2004 [DIRS 171694], Table D-12). This calculation assumes equilibrium conditions will prevail and

that kinetic considerations are not important. While this is not universally a reasonable assumption, it is applicable here because of the elevated temperatures, which accelerate reaction rates.

DTNs: LL030211423125.005 [DIRS 172020] and LL030211523125.006 [DIRS 172021] represent data that are already qualified. These data support the argument that CO_2 gas present in the atmosphere will diffuse into any hyperalkaline fluid that is formed and neutralize it over time. The neutralization involves lowering of the pH (CO_2 is a weak acid that counteracts the high hydroxyl in the cement-reacted water) and reduction of the calcium concentration as a result of the precipitation of calcite. Both of these effects were demonstrated clearly in the experiments described in these two DTNs.

The input data are either already qualified or have been determined by this technical assessment to be suitable for use in this application. The software used to develop DTNs LB0408CMATUZFT.003 [DIRS 171705] and LB0408CMATUZFT.004 [DIRS 171706] is either exempt from qualification requirements or has been qualified. The results of the calculations are reasonable and in agreement with chemical principles. Therefore DTNs LB0408CMATUZFT.003 [DIRS 171705] and LB0408CMATUZFT.004 [DIRS 171706] are qualified for the purpose of simulating the chemistry of leachates of cementitious materials.

C7. CHEMICAL EVIDENCE FOR LONG-TERM TEMPERATURE STABILITY AT YUCCA MOUNTAIN

Reference: Wilson, N.S.F.; Cline, J.S.; and Amelin, Y.V. 2003. "Origin, Timing, and Temperature of Secondary Calcite–Silica Mineral Formation at Yucca Mountain, Nevada." *Geochimica et Cosmochimica Acta, 67*, (6), 1145-1176. New York, New York: Pergamon. TIC: 254369 [DIRS 163589].

Description of Use: Studies of secondary minerals at Yucca Mountain using petrography, fluid-inclusion microthermometry, and U–Pb dating indicate that temperatures have remained close to the current ambient values over the past 2 to 5 million years (Wilson et al. 2003 [DIRS 163589], Section 8). These data are used in Section 6.8.2 to exclude FEP 1.2.06.00.0A, Hydrothermal activity .

Extent to which the Data Demonstrate the Properties of Interest: The property of interest is the long-term stability of the temperature regime at Yucca Mountain, as demonstrated by the relation between the temperatures (inferred from the composition of fluid inclusions) and the age of the inclusions, inferred from the U–Pb isotope dating.

Extent and Quality of Corroborating Data: These data are corroborated by an independent study by Bish and Aronson 1993 [DIRS 100006]. They correlated temperatures of formation of illite-smectite and ages from K/Ar dating to conclude that no significant hydrothermal alteration has since 10.7 Ma. These are independent data supporting the conclusion of Wilson et al. 2003 [DIRS 163589]. Additional corroborating data are presented by Whelan et al. (2002 [DIRS 160442])

Reliability of Data Source: Wilson, N.S.F.; Cline, J.S.; and Amelin, Y.V (2003) published their experimental results in the journal Geochimica et Cosmochimica Acta. Published for over

100 years, the Geochimica et Cosmochimica Acta is a professional scientific research journal for geochemistry and cosmochemistry. It is sponsored by The Geochemical Society and The Meteoritical Society and is published by Elsevier Science Ltd. Contributions to the journal are evaluated for scientific merit by thorough professional review. Peer review is an essential and integral aspect of *Geochimica et Cosmochimica Acta*. The fundamental role of the reviewer is to advise the Associate Editor and the Executive Editor on the virtues, or lack thereof, of a manuscript submitted for publication. Normally the journal requires three "external" reviews. The Associate Editor writes a report summarizing reviewer opinion, presenting his/her overall evaluation based on his/her own reading of the manuscript and the advice of the reviewers.

C8. DEHYDRATION TEMPERATURE OF ZEOLITIC MINERALS

Reference: Smyth, J.R. 1982. "Zeolite Stability Constraints on Radioactive Waste Isolation in Zeolite-Bearing Volcanic Rocks." *Journal of Geology, 90*, (2), 195-201. Chicago, Illinois: University of Chicago Press. TIC: 221104 [DIRS 119483].

Description of Use: Smyth (1982 [DIRS 119483], p. 201) reviewed literature on the thermal stability of clinoptilolite, heulandite, mordenite, and analcime and concluded that dehydration of zeolites below the repository could occur if temperatures in the zeolitic units exceed the estimated minimum alteration temperature of 85°C (Smyth 1982 [DIRS 119483], p. 201). These data are used in Section 6.9.16 to exclude FEP 2.2.10.14.0A, Mineralogic dehydration reactions, on the basis of low consequence.

Extent to which the Data Demonstrate the Properties of Interest: The property of interest is the dehydration temperature of zeolitic minerals in the CHn; if the temperature exceeds the dehydration temperature, the permeability of the CHn would increase, and water would be released below the repository. TH Simulations show that the temperatures in the zeolitic formation do not reach the dehydration temperature.

Extent and Quality of Corroborating Data: These data are corroborated by an independent study by Carey and Bish 1996 ([DIRS 105200], Figure 10). Thermogravimetric analysis was used to monitor dehydration reactions of clinoptilolite. From the data, dehydration curves were presented showing less than 5 percent water loss was calculated for 85°C. This amount of water loss is small enough to confirm the findings of Smyth 1982 [DIRS 119483].

C9. POTENTIAL DOSE FROM GAS-PHASE RELEASE OF CARBON-14

Reference: DOE (U.S. Department of Energy) 2002. *Final Environmental Impact Statement for a Geologic Repository for the Disposal of Spent Nuclear Fuel and High-Level Radioactive Waste at Yucca Mountain, Nye County, Nevada*. DOE/EIS-0250. Washington, D.C.: U.S. Department of Energy, Office of Civilian Radioactive Waste Management. ACC: MOL.20020524.0314 through MOL.20020524.0320 [DIRS 155970].

Description of Use: An analysis of the potential dose from gas-phase release of carbon-14 shows that the maximum dose was found to be 1.8×10^{-10} mrem per year (DOE 2002 [DIRS 155970], Section I.7). This is based upon a calculation that, of all the ^{14}C in a waste

package, 2 percent is in the gas phase. This dose estimate is used in Section 6.7.3 to exclude FEP 2.2.11.03.0A, Gas transport in geosphere, on the basis that it is much smaller than then dose from aqueous transport.

Extent to which the Data Demonstrate the Properties of Interest: The property of interest is the amount of ^{14}C that can be rapidly released as gas from each package. The total ^{14}C inventory per package of Commercial Spent Nuclear Fuel is 1.37 g (DTN: SN0310T0505503.004 [DIRS 168761]), the same value as used in DOE 2002 [DIRS 155970], Section I.7, with 2 percent distribution to the gas phase.

Extent and Quality of Corroborating Data: For TSPA 1991, two percent was taken as the fraction of ^{14}C in the waste package that is in the gaseous form and therefore available for release as soon as the waste container has failed (Barnard et al. 1992 [DIRS 100309], Section 5.2. Oversby (1987 [DIRS 103446], p. 93) reported rapid release of 0.3 percent of the inventory from oxidation testing of a fuel assembly, with subsequent releases being orders of magnitude lower. These data support gas-phase rapid release of not more than 2 percent of the ^{14}C inventory.

C10. EROSION RATE AT YUCCA MOUNTAIN

References: YMP (Yucca Mountain Site Characterization Project) 1993. Evaluation of the Potentially Adverse Condition "Evidence of Extreme Erosion During the Quaternary Period" at Yucca Mountain, Nevada. Topical Report YMP/92-41-TPR. Las Vegas, Nevada: Yucca Mountain Site Characterization Office. Section 3.4. ACC: NNA.19930316.0208 [DIRS 100520].

DOE (U.S. Department of Energy) 1988. Site Characterization Plan Yucca Mountain Site, Nevada Research and Development Area, Nevada. DOE/RW-0199. Nine volumes. Washington, D.C.: U.S. Department of Energy, Office of Civilian Radioactive Waste Management. Section 1.1.3.3.2. ACC: HQO.19881201.0002 [DIRS 100282].

YMP (Yucca Mountain Site Characterization Project) 1995. Technical Basis Report for Surface Characteristics, Preclosure Hydrology, and Erosion. YMP/TBR-001, Rev. 0. Las Vegas, Nevada: Yucca Mountain Site Characterization Office. ACC: MOL.19951201.0049 [DIRS 102215].

Description of Use: These three sources are used to demonstrate that, although erosion processes will be ongoing at Yucca Mountain during the next 10,000 years, the rate of erosion (including mass wasting – e.g., landslides) is too slow to significantly change the hydrologic regime or to expose the repository at the surface.

The data are used in Section 6.5.1 to exclude FEP 1.2.07.01.0A, Erosion/Denudation, and in Section 6.5.2 to exclude FEP 1.2.07.02.0A, Deposition.

Prior Use of the Data: *Site Characterization Plan Yucca Mountain Site, Nevada Research and Development Area, Nevada* (DOE 1988 [DIRS 100282]) is cited in the Yucca Mountain Site Description (BSC 2004 [DIRS 169734]) as indirect input. The text of *Site Characterization Plan Yucca Mountain Site, Nevada Research and Development Area, Nevada* (DOE 1988

[DIRS 100282], Section 3.4) is quoted verbatim in *Technical Basis Report for Surface Characteristics, Preclosure Hydrology, and Erosion* (YMP 1995 [DIRS 102215], Section 4.1.2).

Extent to which the Data Demonstrate the Properties of Interest: The property of interest is the age of colluvial boulder deposits, as determined by the cation ratio of rock varnish (ratio of minor elements that systematically decrease with increasing exposure age).

Technical Adequacy of Equipment and Procedures used to Collect and Analyze the Data: The rock-varnish-cation-ratio method is well established (Harrington and Whitney 1987 [DIRS 106095]; Whitney and Harrington 1993 [DIRS 107303]).

Prior Peer or Other Professional Reviews of the Data and their Results: Most important, the data used to derive the erosion and canyon downcutting rates and cited in Section 6.5.1 of this report were reviewed by a technical assessment team (CRWMS M&O 1992 [DIRS 171834]; YMP 1993 [DIRS 100520], Appendix A). The technical assessment team reviewed the scientific notebooks and unanimously concluded that the age determinations were the best being done at that time in the scientific community (Hawley et al. 1989 [DIRS 170911]).

C11. EFFECT OF LOCAL HETEROGENEITY

Reference: Zhou, Q.; Liu, H-H.; Bodvarsson, G.S.; and Oldenburg, C.M. 2003. "Flow and Transport in Unsaturated Fractured Rock: Effects of Multiscale Heterogeneity of Hydrogeologic Properties." *Journal of Contaminant Hydrology, 60,* [1-2], 1-30. New York, New York: Elsevier. TIC: 253978 [DIRS 162133]**.**

Description of Use: These data are used along with the data of Valentine et al. (1998 [DIRS 119132], p. 5-74) to show that the hydrologic effect of an igneous intrusion would be insignificant because it would be limited in extent. The data of Valentine et al. (1998 [DIRS 119132], p. 5-74) show that igneous activity would change the hydrologic properties of host rock over a limited area (within 10 m of an intrusion). The data of Zhou et al. (2003 [DIRS 162133]) show that a heterogeneity of fracture permeability at this scale would have a negligible effect on flow. This conclusion is used in Section 6.8.4. to exclude FEP 1.2.10.02.0A, Hydrologic response to igneous activity .

Extent to which the Data Demonstrate the Properties of Interest: The property of interest is the effect of local heterogeneity on flow. Zhou et al. (2003 [DIRS 162133]) used a two-dimensional mesh, with layer heights the same as in the UZ model, and used the same calibrated layer-scale values for the fracture and matrix hydrologic properties. Case A used uniform fracture permeability; in case B the fracture permeability was varied stochastically. The breakthrough curves for nonsorbing tracers were not significantly different in these two cases.

Technical Adequacy of Equipment and Procedures Used to Collect and Analyze the Data: The software used for simulations was TOUGH2 V. 1.4 and T2R3D V. 1.4. This software has been qualified for the Yucca Mountain project (although for this use the software was not obtained from Software Configuration Management)

Qualifications of Personnel or Organizations Generating the Data: Quanlin Zhou has B. Eng. and M. Eng degrees in Hydrology and Water Resources from Hohai University, Nanjing,

P. R. China, and Ph.D. in Groundwater Hydrology from Technion-Israel Institute of Technology, Haifa, Israel. While at Technion he was awarded the Miriam and Aaron Gutwirth Prize (1999) and the Irmay Prize (1998).

Lawrence Berkeley National Laboratory has been responsible for simulations of UZ flow since the inception of the Yucca Mountain Project.

C12. FLOW AND TRANSPORT SIMULATIONS WITH ALTERNATIVE PERCHED-WATER MODELS

Reference: BSC 2001. *UZ Flow Models and Submodels.* MDL-NBS-HS-000006 REV 00 ICN 01. Las Vegas, Nevada: Bechtel SAIC Company. ACC: MOL.20020417.0382. [DIRS 158726].

Use of the Data: Simulations of transport of sorbing and nonsorbing radionuclides under various perched water regimes are presented in *UZ Flow Models and Submodels* (BSC 2001 [DIRS 158726], Section 6.7.2). The perched water models represent the effects of undetected features that might be present in the UZ. Simulation results are used in Section 6.8.9 to show that breakthrough curves are only slightly different under the various models; this supports the argument for exclusion of FEP 2.2.12.00.0A, Undetected features in the UZ .

Reason for Supersession: The report (BSC 2001 [DIRS 158726]) was revised to comply with AP-SIII.10Q and to generate flow fields with revised input data and a revised grid. In this revision, the alternative perched-water models were not included, only the primary model, which is used for TSPA-LA.

Reliability of Input Source: The source is a model report that was produced under the then-current revision of AP-SIII.10Q. The input data (rock properties, mesh, and infiltration map) were qualified and have since been superseded, but they are qualitatively similar to the corresponding data that are now qualified. This is shown by the fact that both BSC 2001 [DIRS 158726] and the current controlled version, BSC 2004 [DIRS 169861], produce flow fields that contain perched water bodies. The software used in *UZ Flow Models and Submodels* (BSC 2001 [DIRS 158726]), T2R3D V. 1.4 (LBNL 1999 [DIRS 146654]), and TOUGH2 V. 1.4 (LBNL 2000 [DIRS 146496]), is still on the SCM baseline.

Qualifications of Personnel or Organizations Generating the Input: Lawrence Berkeley National Laboratory has been responsible for simulations of UZ flow since the inception of the Yucca Mountain Project. The same personnel and organization are responsible for the present controlled version of the model report and for the flow fields used in TSPA. Yu-Shu Wu has a Ph.D. in Mineral Engineering from the University of California Berkeley and is group leader at Lawrence Berkeley National Laboratory. Now (2004) he is associate editor of *Water Resources Research.*

Corroborating Input: These data (flow fields and transport simulations for various perched water models) are output from the UZ Flow model documented in BSC 2001 [DIRS 158726]. The model was validated (BSC 2001 [DIRS 158726], Section 6.8.3) by comparison with data, including perched water data.

C13. EFFECT OF PRECLOSURE DRYOUT ON POSTCLOSURE TEMPERATURE

Reference: BSC (Bechtel SAIC Company) 2001. *FY 01 Supplemental Science and Performance Analyses, Volume 1: Scientific Bases and Analyses.* TDR-MGR-MD-000007 REV 00 ICN 01. Las Vegas, Nevada: Bechtel SAIC Company. ACC: MOL.20010801.0404; MOL.20010712.0062; MOL.20010815.0001., Section 5.3.2.4.4 [DIRS 155950].

Use of the Data: The sensitivity studies in *FY 01 Supplemental Science and Performance Analyses, Volume 1: Scientific Bases and Analyses* (BSC 2001 [DIRS 155950], Section 5.3.2.4.4) indicate that inclusion of preclosure dryout gives rise to slightly higher temperatures during the heating period compared to a model that ignores the influence of preclosure dryout. These data are used in Section 6.9.4 to exclude the effects of dryout occurring during excavation and operation.

Reason for Cancellation: These data are based on the design for TSPA-SR. TSPA-SR has been superseded because changes in models, input data, and design require that the TSPA be recalculated for LA. However, the basic repository design and the treatment of precipitation in TSPA have not changed.

Reliability of Input Source: The calculations presented in *FY 01 Supplemental Science and Performance Analyses, Volume 1: Scientific Bases and Analyses* (BSC 2001 [DIRS 155950], Section 5.3.2.4.4) are adequate for the intended use regarding this FEP because these were performed using a qualified thermal-hydrologic model (NUFT V3.0 [DIRS 127906]); see BSC 2001 [DIRS 155950], Table 1-2, Sections 5.3.2.4.1 and 5.3.2.4.4) for a similar design thermal load (BSC 2001 [DIRS 155950], Table 2-1; BSC 2004 [DIRS 169866], Section 4.1.5).

Qualifications of Personnel or Organizations Generating the Input: Lawrence Livermore National Laboratory developed the NUFT model. The same personnel and organization are responsible for the present controlled version of the model report that is used in TSPA.

C14. DOSE RATES INCREASING OVER TIME

Reference: CRWMS M&O 2000. *Total System Performance Assessment for the Site Recommendation.* TDR-WIS-PA-000001 REV 00 ICN 01. Las Vegas, Nevada: CRWMS M&O. ACC: MOL.20001220.0045 [DIRS 153246], Sections 3.5.5 and 4.1.3; Figures 4.1-5, 4.1-7, 4.1-9, 4.1-19a, and 4.1-20

Use of the Data: In the latest total-system performance assessment, dose rates for all radionuclides are predicted to increase over tens of thousands of years (CRWMS M&O 2000 [DIRS 153246], Figures 4.1-5 and 4.1-7). This is a result of the spread of waste package failures over time (CRWMS M&O 2000 [DIRS 153246], Figures 4.1-9) and the slow release of radionuclides from the waste emplacement drifts. Therefore, during the 10,000-year period, the highest concentration for any radionuclide at the receptor is expected to occur under conditions giving the greatest transport rates. Reduced solubilities for neptunium americium, plutonium, thorium, and uranium were investigated as a sensitivity in TSPA-SR (CRWMS M&O 2000 [DIRS 153246], Sections 3.5.5, 4.1.3, and Figures 4.1-19a and 4.1-20). The dose rates for radionuclides affected by the lower solubilities (including decay products such as ^{226}Ra) were

found to be lower in the reduced-solubility case. These data are used in Section 6.9.6 to support the argument that precipitation of radionuclides has no adverse affect on repository performance, and to support exclusion of FEP 2.2.01.05.0A, Radionuclide transport in the excavation disturbed zone.

Reason for Cancellation: TSPA-SR has been canceled because changes models, input data, and design require that the TSPA be recalculated for LA. However, the basic repository design and the treatment of precipitation in TSPA have not changed.

Reliability of Input Source: The total-system performance assessment for Site Recommendation (CRWMS M&O 2000 [DIRS 153246], Sections 3.5.5 and 4.1.3) was performed using qualified software for a repository design, engineered system design, and, waste inventory that is similar to that used for license application. Therefore, the qualitative trends cited for total system performance should be sufficiently representative for its intended use regarding this FEP.

C15. ENDPOINT COORDINATES OF REPOSITORY DRIFTS

Reference: BSC (Bechtel SAIC Company) 2003. Repository Design, Repository/PA IED Subsurface Facilities. 800-IED-EBS0-00402-000-00B. Las Vegas, Nevada: Bechtel SAIC Company. ACC: MOL.20030109.0146. [DIRS 161727].

Use of the Data: These data define the areal extent and elevation of the repository (Figures A-1 and A-2). They are used in Section A1 to calculate the volume of perched water in the repository and to compare it to the flux through the repository (Table A-1). This comparison is used in Section 6.8.8 to exclude FEP 2.2.06.03.0A, Seismic activity alters perched water zones.

The data are also used in Appendix B to determine that the PTn hydrogeologic unit overlies the entire repository (Figure B-1). This fact is used in Section 6.4.5 to exclude FEP 2.2.07.05.0A, Flow in the UZ from episodic infiltration.

Reason for Supersession: To accommodate rail haulage, the length of drift turnout was increased. This required two more emplacement drifts to accommodate the same total drift length. The drift-to-drift spacing was not changed.

Justification for Use: The differences between the superseded design (BSC 2003 [DIRS 161727]) and the superseding design (BSC 2004 [DIRS 164519]) is not significant for the purposes of these calculations. Comparison of the map in Figures A-1 and B-1 with the map in *D&E/PA/C IED Subsurface Facilities* (BSC 2004 [DIRS 164519]) shows that the footprint of the repository is unchanged. Also, the repository is still located in the Tptpmn and Tptpll hydrogeologic units. Therefore, it is still completely overlain by the PTn and the volume of perched water is the same as calculated in Table A-1.

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APPENDIX D

**ANALYSIS OF SENSITIVITY OF TRANSPORT TO CHANGES
IN FRACTURE APERTURE**

D1.   INTRODUCTION

This appendix documents a recalculation of a portion of the complete sensitivity analysis documented in *Fault Displacement Effects on Transport in the Unsaturated Zone* (CRWMS M&O 2000 [DIRS 151953]). The reason for the recalculation is that the original analysis was conducted using software for transport calculations on a platform not approved for use in the software baseline. This analysis is repeated here for the most important three-dimensional site scale model results using a qualified software for transport on an approved platform.

The technical purpose of this appendix is to evaluate the potential for changes to the hydrogeologic system caused by fault displacement to affect radionuclide transport in the UZ at Yucca Mountain. The repository is bounded on the west by the Solitario Canyon fault and on the east by the Bow Ridge fault. The northern boundary of this structural block is bounded by the Drill Hole Wash fault. There are also three intrablock faults: the Ghost Dance, Sundance, and Dune Wash faults. For the purposes of this analysis, the focus is on two possible effects of fault displacement along the bounding faults: (1) uniform change in fracture properties throughout the UZ flow model domain and (2) change in fracture properties within the faults only. These two hypothetical end-member cases model the bounding cases of mechanical strain being either uniformly distributed throughout the strata bounded by the faults or localized to the individual fault zones. In the physical system, the strain would be spatially distributed in some manner that lies between these end-member cases. This evaluation used the bounding case estimates to determine whether FEPs 2.2.06.02.0A (Seismic activity changes porosity and permeability of faults) and 2.2.06.02.0B (Seismic activity changes porosity and permeability of fractures) can be excluded.

These two end-member cases were evaluated by simulating the flow and transport in the UZ for a pulse input tracer at the repository location. For a specific cross-section, computer simulations were performed assuming (1) a change in fracture properties throughout the UZ models (which assumes all fracture apertures are uniformly altered), and (2) a change in fracture properties in the fault zones only. Simulations were performed for the present-day climate and a wetter, glacial-transition climate case. Tracer breakthrough curves computed at the water table were used to examine the potential impact induced on transport in the UZ.

The effects of fault displacement on UZ transport encompasses four FEPS:

        1.2.02.02.0A Faults
        1.2.10.01.0A Hydrologic response to seismic activity
        2.2.06.02.0A Seismic activity changes to porosity and permeability of faults
        2.2.06.02.0B Seismic activity changes to porosity and permeability of fractures.

D2.   SENSITIVITY ANALYSES

As stated in Section D1, the purpose of this report is to describe the potential for fault displacement events during the postclosure period that affect performance through changes in radionuclide transport in the UZ at Yucca Mountain. In particular, the effects of fault displacement on repository performance will be addressed in terms of changes in the simulated breakthrough at the water table of a pulse input of tracer at the repository.

The approach for the analysis of fault displacement effects on transport in the UZ is divided into two distinct components: a review of site description information which provides a basis for defining bounding conditions and for understanding the physical significance of the results (Section D2); and a modeling component to provide quantitative analysis of the sensitivity of the UZ flow system to changes in hydrologic parameters (Section D3).

D2.1   SITE DESCRIPTION INFORMATION

The spatial and temporal patterns of faulting and fracturing of the volcanic bedrock are the fundamental elements of the structural geology of the repository for high-level radioactive wastes at Yucca Mountain. To document and discuss these patterns, a comprehensive program of geologic mapping and fractured rock mass studies has been conducted as an integral part of the site characterization. Of particular importance to this analysis are geologic observations related to displacement in fault zones and observations of the characteristics of the faults zones made during the excavation of the ESF and in the enhanced characterization of the repository block (ECRB) Cross Drift. The observations are briefly described in Section D2.1.1. These observations provide a basis for determining the reasonableness and appropriateness of the range of inputs used in the modeling analysis in Section D3 and for interpreting the level of conservatism represented by the models.

However, the primary controlling factor for amount of flux through the UZ is the amount of precipitation available to infiltrate and percolate through the UZ. This variable is highly dependent on climate conditions. To address this variable, present day average and glacial-transition climate conditions (CRWMS M&O 1998 [DIRS 100356], Section 2.4.1.1) were used as bounding conditions. The differences in these climate states are briefly explained in Section D2.1.2.

D2.1.1   Geologic Setting

The Yucca Mountain area is cut by steeply dipping, north-south-striking normal faults which separate the Tertiary volcanics into blocks one to four kilometers wide (Scott 1990 [DIRS 106751]). The repository lies in the central block of the central Yucca Mountain structural domain. The central block is bounded on the west by the Solitario Canyon fault, on the east by the Bow Ridge fault, and on the north by the northwest-striking Drill Hole Wash fault. The southern boundary is marked by a transition to structural styles that accompany greater magnitudes of extension and continue south. Intrablock faults include the Ghost Dance, Sundance, and the Dune Wash faults.

The repository area is bounded by the Solitario Canyon fault to the west and the Ghost Dance fault to the east. Both faults dip steeply toward the west, and displacement, amount of

brecciation, and number of associated splays vary considerably along their trace (Scott and Bonk 1984 [DIRS 104181]; Day et al. 1998 [DIRS 101557]).

Surface geologic mapping (Scott and Bonk 1984 [DIRS 104181]; Day et al. 1998 [DIRS 101557]), underground mapping of the ESF, geophysical surveys, and borehole studies show that the Yucca Crest subblock is little deformed, and cut only by widely spaced intrablock faults (Ghost Dance and Dune Wash). Within structural blocks, small amounts of strain are accommodated along intrablock faults. In many cases, intrablock faults appear to represent local structural adjustments in response to displacements on the block-bounding faults. Many of the intrablock faults within this part of Yucca Mountain are short, discontinuous, have minor cumulative displacement (1 to 10 m), and represent the localization of slip along pervasive preexisting weaknesses in the rock mass (Potter et al. 1996 [DIRS 106582], 1996 [DIRS 106583]). In some cases, intrablock faults are expressions of hanging wall or footwall deformation that affect the block within a few hundred meters of the block-bounding faults. The eastern and southern edges of the central block, however, are cut by numerous faults associated with block margin deformation (Solitario Canyon and Bow Ridge faults).

D2.1.1.1   Fracture Attributes

The fracture network acts as a significant preexisting weakness in the rock mass that can accommodate extensional strain through distributed slip along many reactivated joints. Evidence for reactivation of joints includes the presence of thin breccia zones along cooling joints and observable slip lineations along joint surfaces (Sweetkind et al. 1996 [DIRS 106957]). Cooling joints originally formed as tensional openings, having only face separation, not shear. However, thin selvages of tectonic breccia are often present along the trace of cooling joints, indicating later slip. Subsequent analyses performed here (see Section D3.2) will consider the dilation or compression of any hydraulically connected fractures at Yucca Mountain, regardless of whether the fractures originated as tensional openings during cooling of the rock or from past seismic activity and regardless of distance from the fault.

There are a number of primary controls on fracture characteristics within the Paintbrush Group that are related to stratigraphy, upon which any later tectonic signature (such as fault displacement) is superimposed. Fracture characteristics in the pyroclastic flows at Yucca Mountain are primarily controlled by variations in the degree of welding (CRWMS M&O 1998 [DIRS 100126], Section 3.6). The intensity of fracturing increases with degree of welding within the welded pyroclastic flows because of the presence of cooling joints, and because increasing brittleness of the rock favors an increase in the number of tectonic joints. Lithophysal development, alteration, and pumice content are secondary controls important in specific stratigraphic intervals. These lithostratigraphic controls affect fracture spacing, type, number of sets, continuity of individual fractures within each lithostratigraphic zone, and they also affect the fracture connectivity of the network as a whole (Sweetkind and Williams-Stroud 1996 [DIRS 100182], pp. 60 to 66; Sweetkind et al. 1997 [DIRS 100183], pp. 62 to 67).

Each lithostratigraphic zone at Yucca Mountain has characteristic fracture attributes, including predominant orientations, spacing, trace length, and joint type (Sweetkind et al. 1997 [DIRS 100183], p. 76); each is unique in its ability to deform by distributed slip. The result is

stratigraphic control of structural geometry—what may be a discrete break in one lithostratigraphic unit may be a broad zone of distributed deformation in another.

An analysis of fracture apertures is available from the ECRB Cross Drift Study (DTN: GS990408314224.001 [DIRS 108396] and GS990408314224.002 [DIRS 105625]). The largest aperture recorded was 520 mm. Approximately 64 percent of the observed fractures exhibited zero aperture. Of the over 1800 fractures measured, only 40 apertures were measured as greater than 20 mm, or about 2 to 3 percent. The remaining apertures were less than 20 mm.

The relationship of fractures smaller than 1 m in length to faults was evaluated by visual examination of every fault in the ESF (Sweetkind et al. 1997 [DIRS 100183], p. 68) that could be correlated with a fault mapped at the surface (Day et al. 1998 [DIRS 101557]). Four principal conclusions were reached, based on observations in the ESF (Sweetkind et al. 1997 [DIRS 100183], pp. 68, 71).

The first conclusion is that the width of the zone of influence on fracture frequency in the immediate vicinity of a fault is, in general, quite narrow, ranging from less than 1 m to about 7 m from the fault.

The second conclusion regarding the relationship between faults and fracture attributes is that the width of the zone of influence in the immediate vicinity of a fault correlates, in a general way, with the amount of cumulative fault offset. Therefore, faults with the largest potential future displacement are the most likely to influence the repository block. Intrablock faults with very small amounts of cumulative offset (1 to 5 m) have zones of influence that are 1 to 2 m in width. Block-margin faults with tens of meters of cumulative offset (faults at ESF Stations 11+20 and 70+58) have zones of influence that range up to 6 to 7 m wide. The limited available data from block-bounding faults are not definitive regarding the nature of attendant fracturing.

The third conclusion is that the width of the zone of influence around a fault does not appear to be related to depth, at least within the ESF. The width of the zones of influence is similar for small faults observed along the North Ramp, where overburden is 50 to 60 m thick, as it is for small faults observed elsewhere in the ESF, where overburden thickness is two to three times greater. However, upward-splaying faults can result in apparent broad zones of influence at the surface because of the overlap of fractured zones surrounding individual fault splays.

The fourth conclusion is that the amount of deformation associated with faults appears, in part, to be dependent upon which lithologic unit is involved in the faulting. In the ESF, overall variability in the frequency of fractures 1 m long or longer is primarily a function of lithology, not proximity to faults (Sweetkind et al. 1997 [DIRS 100183], p. 68). Fracture intensity correlates to lithologic differences, lowest in lithophysal units and nonwelded to partially-welded tuffs, and highest in densely welded, nonlithophysal rock. Faults within nonwelded to partly welded portions of the crystal-poor vitric zone of the Tiva Canyon Tuff are generally sharp, discrete breaks with minimal fault gouge or secondary shear surfaces. Individual pumice clasts along some faults can be traced to the fault surface without visible sign of breakage, and wall rocks show little evidence of deformation. In comparison to brittle, welded rocks, nonwelded units apparently can accommodate a greater amount of extensional strain before failing by fracture.

D2.1.1.2   Fault Attributes

In the following descriptions, fault length refers to the maximum length of a given fault or fault zone as reported or shown on maps in published references (e.g., Piety 1996 [DIRS 106540]). Unless otherwise indicated, the following descriptions for regional faults, including temporal and behavioral data, are from Piety (1996 [DIRS 106540]), and the field reconnaissance work is from Anderson et al. (1995 [DIRS 101422]). Piety's report (1996 [DIRS 106540]) is an excellent synthesis of most of the data available for characterizing regional faults, and contains an extensive list of published references.

The Solitario Canyon Fault Zone: The Solitario Canyon Fault Zone is the most laterally continuous fault and displays the most total offset of any structure in the immediate vicinity of Yucca Mountain. Day et al. (1998 [DIRS 101557], p. 6) consider the Solitario Canyon Fault Zone to be one in a series of major north-south trending, block-bounding faults. The fault has been extensively investigated by trenching at the surface in Solitario Canyon (Ramelli et al. 1996 [DIRS 101106]).   The Solitario Canyon fault has normal down-to-the-west displacement of about 260 m near the repository block and is the most significant of the faults involved in this analysis.

The main trace of this fault extends southward from Yucca Wash for about 18 km. It is located about 1 km from the western boundary of the repository site (Simonds et al. 1995 [DIRS 101929]). Total bedrock displacement varies from 61 m down-to-the-east at the northern end, to more than 500 m down-to-the-west at the southern end (Scott and Bonk 1984 [DIRS 104181]). Average dip of the fault plane is 72°W. Slickensides indicate a component of left-lateral slip.

Map patterns demonstrate that tectonic mixing of various Paintbrush Group lithologies has occurred within the most intensely deformed parts of block-bounding fault systems. This is most apparent in the Solitario Canyon fault system (Scott and Bonk 1984 [DIRS 104181]; Day et al. 1998 [DIRS 101557]). In this system, which is up to 400 m wide, there are domains in which lenses from stratigraphically diverse parts of the Tiva Canyon Tuff are juxtaposed; similar zones in which slices of Topopah Spring Tuff are mixed; and several areas where lenses from more than one Paintbrush Group formation are tectonically mixed (Day et al. 1998 [DIRS 101557]). Individual fault strands within these tectonically-mixed zones are highly brecciated, and in some cases, the fault-bounded lenses have a high degree of internal brecciation.

The SCFZ was not crossed during the ESF excavation. In the ECRB Cross Drift, the SCFZ was expected to be composed of two major normal fault strands; the first (eastern strand) was projected as the "main splay" with a predicted total offset of about 230 m. The second (western strand) was projected with a predicted cumulative offset of about 165 m (USGS 1998 [DIRS 100354]). Between these two larger strands, several smaller faults were expected to be associated with the SCFZ faulting. The tunnel boring for the ECRB Cross Drift was stopped between the two strands based on programmatic considerations, and the western strand was not intersected.

The as-built geologic cross-section for the ECRB Cross Drift (DTN: GS990408314224.006 [DIRS 108409]) shows that the eastern strand was encountered at Station 25+85 (that is, 2,585 m from the start of the survey line) and has approximately 260 m of cumulative normal offset. Shears and small faults increase in intensity prior to (east of) of Station 25+00. The Solitario Canyon Fault Zone influences rock in the footwall of the fault to about Station 25+00 (or approximately 85 m from the fault proper) in the form of increased shear intensity. Spacing of faults and shears decreases, while continuity and amount of cumulative offset increases with proximity to the eastern strand of the Solitario Canyon Fault Zone. At Station 25+30, a small fault oriented 200/83 is intercepted by the tunnel. Although the cumulative offset along the fault is approximately 1 m or less, the rock is intensely fractured after (west of) Station 25+40. The rock from Station 25+80 to 25+82 (between 3 and 5 m from the fault) is a clast-supported breccia. The rock is shattered to the point of not having recognizable structure. From Station 25+82 to 25+85, the rock is a clast-supported breccia. The main plane of displacement along the eastern strand of the Solitario Canyon Fault Zone is at Station 25+85, (left wall, springline). The fault plane is defined by an 8 to 12 cm thick zone of fault gouge composed of about 85 percent clay and about 15 percent fine to medium sand. The gouge is firm and was slightly damp at the time of excavation in October 1998, but dry by February 1999. On the west (hanging wall) side of the fault plane described above, there is a zone of matrix-supported breccia that extends along the left wall from Station 25+85.5 to 25+89.90. The farthest western zone along the eastern strand of the Solitario Canyon Fault Zone is composed of a clast-supported breccia extending along the left wall from Station 25+89.9 to 25+99.15 (or a distance of approximately 14 m west of the fault). This zone is bounded on the west side by a thin, discontinuous, matrix-supported breccia about 10- to 20-cm thick.

Ghost Dance Fault Zone–The Ghost Dance fault is in the central part of the repository block. It is mapped for approximately 3 km as a zone of numerous splays that not only parallel the main north-trending trace of the zone, but locally branch away from the main trace. In general, it is a north-striking normal fault zone, dipping steeply west (75° to 85°) with down-to-the-west displacement. The Ghost Dance fault bifurcates; one branch connects with the Abandoned Wash fault to the southwest (Scott and Bonk 1984 [DIRS 104181]; Day et al. 1996 [DIRS 124302]), and a second branch trends southeast, but does not appear to connect with the Dune Wash fault (Day et al. 1996 [DIRS 124302]) subdivided the fault into three sections on the basis of cumulative offset and brecciation.

Along the northern segment, north of Split Wash, the fault is a relatively narrow zone (2 to 4 m wide) with as much as 6 m of down-to-the-west total displacement.

The central segment of the Ghost Dance fault zone has greater down-to-the-west displacement than the northern segment, and extends from Split Wash to Broken Limb Ridge. On Antler Ridge, there is 13 to 20 m of cumulative displacement across several splays of the Ghost Dance that are distributed over a map width of approximately 100 to 150 m (Day et al. 1998 [DIRS 101557], p. 9). Individual splays are characterized by 1 to 2 m-wide breccia zones.

To the south on Whale Back Ridge, the fault zone is about 55 m wide and has about 30 m cumulative down-to-the-west offset. There, the zone is bounded by two north-striking faults. The eastern fault is the main trace of the Ghost Dance. Locally, the immediate hanging wall of the principal splay of the Ghost Dance fault is highly fractured. On the south-facing slope of

Broken Limb Ridge, the cumulative offset is less than 6 m, and intense fracturing in the hanging wall extends about 15 m to the west.

The amounts of displacement and brecciation along the southwestern projection of the Ghost Dance fault across Highway Ridge are considerably less than those preserved along the central segment. Cumulative offset on the fault increases to the southwest from Ghost Dance Wash, becoming about 17 m down-to-the-west in Abandoned Wash on the eastern splay of the Abandoned Wash fault (Day et al. 1998 [DIRS 101557], p. 10).

In the Ghost Dance Wash area (near the southern bend in the ESF), displacement on the fault is less than 3 m both on the surface and in the ESF, and deformation is also confined to a relatively narrow zone (2 m) of intense fracturing and brecciation.

The geotechnical baseline report (CRWMS M&O 1998 [DIRS 109848], p. 4-15) stated that the Ghost Dance fault might be encountered in the ECRB Cross Drift, but the fault should have minimal cumulative offset. The geologic cross section from the baseline report accurately predicted the fault in the vicinity of Station 4+80. A shear (that is, less than 0.1m displacement) was encountered at Station 4+99 (left wall, springline) which has been identified as the northern distal end of the Ghost Dance fault. This feature is the only north-trending, conspicuous discontinuity in this portion of the tunnel. The feature consists primarily of a 1 to 10-cm thick zone of silty/sandy gouge with clasts. The gouge thickens slightly in the crown to 10 cm, but is only 2 to 4-cm thick elsewhere. The gouge is surrounded by a zone of intensely fractured and crushed rock. On the right wall, this fractured zone is approximately 0.4 m thick on the east side of the feature, and 0.6 m thick on the west side of the feature (DTN: GS990408314224.003 [DIRS 108404]) .

Dune Wash Fault–This south- and southeast-trending fault is mapped along the eastern side of the repository site for a distance of 3 km. It is mapped in exposures of bedrock as a west-dipping normal fault with down-to-the-west displacement. Toward the northern end of the fault, Tertiary volcanic rocks are displaced a total of 50 to 100 m (Day et al. 1996 [DIRS 124302], 1998 [DIRS 100027]; Scott and Bonk 1984 [DIRS 104181]). However, no evidence of Quaternary movement has been found in surficial deposits that bury the fault toward the south, and no per-event displacement data are available.

The Dune Wash fault is exposed in the ESF near Station 67+88, where the cumulative offset is 65 m (Sweetkind et al. 1997 [DIRS 100183], Table 21), and the zone of increased fracture frequency in the vicinity of the fault is 6 to 7 m wide. This fault was not encountered in the Cross Drift.

Sundance Fault–The Sundance fault is located in the north-central portion of the repository block.

A detailed investigation of the Sundance fault has been conducted by Potter et al. (1999 [DIRS 107259]). The maximum width of the Sundance fault zone is about 75 m, and the cumulative down-to-the-northeast vertical displacement across the fault zone does not exceed 11 m. The faults in this zone are almost exclusively characterized by down-to-the-northeast displacement (Potter et al. 1999 [DIRS 107259], pp. 5 to 6). Even though some horizontal

slickensides have been observed, significant strike-slip displacement along the Sundance fault zone is not evident. Potter et al. (1999 [DIRS 107259], p. 9) concluded that the Sundance fault zone has a significantly smaller along-strike extent than had been suggested by previous workers.

Individual faults in the Sundance fault zone and elsewhere at Yucca Mountain are vertically and laterally discontinuous; one or more mechanisms of strain accommodation must operate in the Tiva Canyon Tuff to accommodate displacements in the rock volume between the discontinuous discrete fault segments. Two probable mechanisms are: distributed brittle deformation associated with diffuse breccia bodies, and minor cumulative offsets along numerous preexisting cooling joints (Potter et al. 1999 [DIRS 107259], pp. 13 to 14).

The ESF passes beneath the southeastern end of the Sundance fault zone, as mapped by Potter et al. (1999 [DIRS 107259]), where displacement is minimal on the south flank of Live Yucca Ridge. In the ESF, the fault is identified within a broad zone of discontinuous minor northwest-striking faults and joints in the middle nonlithophysal zone of the Topopah Spring Tuff. The exposure in the ESF is similar in character to the fault zone mapped at the surface near its southeastern termination on the south-facing slope of Live Yucca Ridge (Potter et al. 1999 [DIRS 107259], p. 8; Day et al. 1998 [DIRS 101557]).

The Geotechnical Baseline Report (USGS 1998 [DIRS 100354]) predicted the Sundance fault to be near Station 10+70 to 11+00. The Sundance fault was encountered along the left wall at Station 11+35.40 to 11+36.70 (DTN: GS990408314224.003 [DIRS 108404]). The fault intercepts the right wall at Station 11+35 to 11+36.2, approximately 35 m southwest of the location predicted. The amount of displacement is thought to be on the order of several meters, but is indeterminate. The margins of the fault zone were unaltered except in the immediate area of the fault, which exhibits some iron oxide stainings along the right wall. All portions of the Sundance fault were dry at the time of excavation.

The fault zone is composed of three distinct zones along the left wall. Zone 1 is adjacent to the footwall plane, and is a matrix-supported, uncemented breccia. Zone 1 is approximately 20 cm thick on the left wall, thinning to 4 cm on the right wall. Zone 2 along the exposure of the Sundance fault is approximately 0.7 m thick and is a matrix-supported breccia. Zone 3 varies in thickness from 0.3 m on the left wall, to zero on the right wall. Despite the very sharp and distinct plane of the fault at the footwall, distinct slickensides are not evident. Faint, low-angle slickensides can be interpreted on the left wall, and undulations in the fault plane with low-angle plunges occur at the boundary between Zones 1 and 2. The footwall rock is intact, even within 10 cm of the fault plane. The hanging wall is slightly more fractured, with an intensely fractured zone about 1 m thick.

Bow Ridge Fault–This fault is a prominent north-striking, west-dipping, normal-oblique (sinistral) slip fault. It is about 10 km long and lies along the east side of the repository area. The fault is buried beneath alluvium and colluvium for most of its extent along the western margin of Midway Valley. The best topographic expression of the fault occurs where a 760-m-long section follows the base of the west side of Exile Hill (Simonds et al. 1995 [DIRS 101929]; Menges and Whitney (1996 [DIRS 106343], p. 2-3); Menges et al. 1997 [DIRS 105139]). Tertiary volcanics are displaced at least 125 m down-to-the-west at this locality. The fault dips 65°E to 75°E.

Trenches on the surface and the ESF expose a complex fault zone in highly-fractured Tertiary volcanic bedrock and colluvial deposits that have been subjected to multiple Quaternary faulting events. At least two and possibly three surface-rupture events are evident in late to middle Pleistocene colluvial deposits at trench 14D (Menges and Whitney 1996 [DIRS 106343]; Menges et al. 1997 [DIRS 105139]). A minimum age of 48 ± 20 thousand years is established for the most recent surface-rupture event. Displacements range from 14 to 44 cm for individual faulting events, and cumulative displacement is from 30 to 70 cm for all events younger than 500 thousand years. Average recurrence intervals vary from 70 to 215 thousand years. Recurrence intervals for individual events vary more widely from 40 to 350 thousand years. Average slip rates are 0.002 to 0.007 mm/yr (Menges and Whitney 1996 [DIRS 106343]; Menges et al. 1997 [DIRS 105139]).

The Bow Ridge fault has very little attendant fracturing despite the 100 m cumulative offset and its exposure near the surface (approximately 35 m of overburden). Lack of deformation around the fault zone probably results from the presence of nonwelded pre-Rainier Mesa Tuff in the hanging wall of the fault.

D2.1.1.3 Significance of Geologic Setting to the Analysis

The descriptions in Sections D2.1.1.1 and D2.1.1.2 suggest that an analysis of fault displacement effects needs to be considered from two perspectives: the impact on fractures throughout the repository as a whole, and the effect on fractures in the immediate vicinity of the faults only. Furthermore, the range of fault characteristics that was described supports the idea that movement on the Solitario Canyon fault may be considered the bounding scenario.

As stated in Section D2.1.1.1, the fracture network at Yucca Mountain acts as a significant preexisting weakness in the rock mass that can accommodate extensional strain through distributed slip along many reactivated joints. Evidence for reactivation of joints includes the presence of thin breccia zones along cooling joints and observable slip lineations along joint surfaces (Sweetkind, Potter, and Verbeek 1996 [DIRS 106957]). There are a number of primary controls on fracture characteristics within the Paintbrush Group that are related to stratigraphy, upon which any later tectonic signature (such as fault displacement) is superimposed. The existence of distributed slip suggests that changes in strain (such as would be associated with a significant fault displacement) are likely to be propagated throughout the repository area. Also, some fault zones (such as the Ghost Dance and Solitario Canyon) may be on the order of 100 to 400 m wide. Although strain is expected to diminish with distance from the fault, these observations suggest that the effect of strain distributed in the fractures throughout the repository should be considered.

The presence of gouge and brecciated zones only in limited proximity to the fault planes, however, suggests that much of the strain will be mechanically dissipated within or near the fault plane itself. For instance, as described in Section D2.1.1.2, in the Solitario Canyon fault zone in the ECRB Cross Drift, the total displacement is approximately 260 m, but the gouge and brecciated zones are limited to less than 20 m. Similarly, the Dune Wash fault as exposed in the ESF exhibits a cumulative offset of 65 m (Sweetkind et al. 1997 [DIRS 100183], Table 21), but the zone of increased fracture frequency in the vicinity of the fault is only 6 to 7 m wide. A third example is the observation of the Sundance fault in the ECRB Cross Drift; with an assumed,

though indeterminate displacement of several meters, the footwall rock is intact, even within the 10 cm of the fault plane. The hanging wall is slightly more fractured, with an intensely fractured zone about 1 m thick. Consequently, an analysis of fault displacement should also consider a case where the effects of strain are limited to the immediate vicinity of the fault zone (Section D3.3.2).

D2.1.2   Fault Displacement Hazards

Fault displacement hazards at Yucca Mountain have been investigated in detail in the report "Probabilistic Seismic Hazard Analyses for Fault Displacement and Vibratory Ground Motion at Yucca Mountain, Nevada" (USGS 1998 [DIRS 100354]). Several original approaches to characterizing the fault displacement potential were developed by the seismic source expert teams. The approaches were based primarily on empirical observations of the pattern of faulting at the site during past earthquakes (determined from data collected during fault studies at Yucca Mountain). Empirical data were fit by statistical models to allow use by the experts. The results of this analysis were curves representing probabilistic predictions of fault displacements.

Nine locations within the preclosure controlled area were identified to demonstrate the fault displacement methodology. The term "preclosure controlled area" is defined in DOE's Interim Guidance (Dyer 1999 [DIRS 105655]). These locations were chosen to represent the range of potential faulting conditions. Two of the nine sites each had four identified faulting conditions. Some of these locations lie on faults that may experience both principal faulting and distributed faulting. The other points are sites only of potential distributed faulting.

With the exception of the block-bounding Bow Ridge and Solitario Canyon faults (sites 1 and 2, respectively), the mean displacements are 0.1 cm or less at a 10^{-5} annual exceedance probability, and on the order of 1 m or less at 10^{-8} annual exceedance probability (USGS 1998 [DIRS 100354], Figures 8-4 through 8-14). For the Ghost Dance fault, the range of displacements per event is 0.6 m to about 1.5 m at 10^{-8} mean annual exceedance probability (USGS 1998 [DIRS 100354], Figure 8-5). Thus, sites not located on a block-bounding fault, such as sites on the intrablock faults, other small faults, shear fractures, and intact rock, are estimated to have displacements significantly less than 0.1 cm for mean annual exceedance probabilities of 10^{-5}.

For Solitario Canyon fault and Bow Ridge fault (USGS 1998 [DIRS 100354], Figures 8-2 and 8-3), the mean displacements are 7.8 and 32 cm, respectively, for these two faults at a 10^{-5} annual exceedance probability. At lower annual exceedance probabilities, the fault displacement hazard results are driven by the upper tails of uncertainty distributions and are close to 5 m.

For purposes of determining the appropriateness of the chosen bounding conditions based on the Probabilistic Seismic Hazard Assessment, per-event displacements can be used as a comparison. As described in Section D2.1.1 above, the largest estimate of per event displacement for the faults intersected by the two-dimensional cross section used for the analysis is 1.4 m along the Solitario Canyon fault. A displacement of 1.2 m corresponds to the 15th percentile curve at a 10^{-8} annual exceedance probability (USGS 1998 [DIRS 100354], Figure 8-3). As described in Section D3.2.6, strains associated with a displacement of 10 m are used as bounding conditions. Given that the assumed bounding condition is about a factor of 10 greater than measured

displacement and the probabilistic displacement event suggested by the 15th percentile curve, the values used in this analysis are judged to be extremely conservative.

D2.1.3 Climate Data

The primary controlling factor for flow through the UZ is the amount of infiltration through the system. This variable is highly dependent on precipitation and climate conditions. To address this constraint, present-day average and long-term average conditions were used as bounding conditions.

Present day climate conditions represent relatively dry, interglacial conditions, while the glacial transition conditions represent typical conditions at Yucca Mountain between the wet and dry extremes based on available paleoclimate data (CRWMS M&O 1998 [DIRS 100356], Section 2.4.1.1). Because these two sets of conditions represent relatively stable (that is, long-term conditions) rather than extreme conditions (that is, short-duration climatic states such as superpluvial periods), they were chosen as representative conditions for this analysis.

D3. EFFECTS OF FAULT DISPLACEMENTS ON UZ FLOW AND TRANSPORT

As discussed in Section D2, fault displacements are expected to occur along existing faults in the vicinity of Yucca Mountain. The movement produced by a fault displacement will result in changes in the rock stress in the vicinity of the fault. Obviously, the change in rock stress will decrease with distance from any given fault that does move. However, the magnitude of the changes in rock stress as a function of distance from the fault depends on the specific details of the fault displacement (e.g., magnitude of fault motion, direction of fault movement, extent of the fault that participates in the movement) and the mechanical properties of the surrounding rock (e.g., fracture spacing, fracture stiffness, geomechanical properties of the rock matrix). Given some change in rock stress, the fractured rock mass will respond to the change in stress through deformation, or strain, in the rock. Of particular importance is the fact that this induced strain can affect the geometry of fractures in the rock. The effects of changes in properties of the rock matrix (as opposed to the fractures) are assumed to have a negligible effect on UZ flow and transport. Several fracture properties (permeability, capillary pressure, porosity) are a function of fracture aperture, which can be changed significantly by small strains if these strains are allocated entirely to the fracture apertures. The sensitivity of fracture aperture to mechanical strain is due to the small porosity of the fracture continuum. The matrix, on the other hand, has much greater porosity than the fractures in general, and its properties are not expected to be as sensitive to mechanical strain. This approximation is reasonable given the fact that fracture porosity is much less than matrix porosity at Yucca Mountain.

In theory, the effects of a given fault displacement could be evaluated using process-level calculations for the effects of the induced stress and strain on fracture geometry. Then the effects of this change in fracture geometry on the fluid-flow properties of the fracture network could be evaluated. However, this method was not used in this analysis due to the large uncertainty and complexity of the problem.

Some of the effects of previous fault displacements at Yucca Mountain can be examined directly. Previous fault displacements have resulted in observable changes to the structure of the

surrounding rock (Section D2.1.1). However, geologic observations are not adequate to assess the effects of some of the changes caused by fault displacements that could be important to UZ flow and transport. In particular, the effects of previous fault displacements on the present-day fracture apertures at Yucca Mountain are difficult to determine by observation. For example, it is difficult to determine by geologic observation that a given fracture with an effective hydraulic aperture of, approximately 200 μm, may have had an effective hydraulic aperture of 150 μm at some point in the past before to a fault displacement event. In fact, it is difficult to determine the effective hydraulic apertures of the present-day fractures at Yucca Mountain by direct observation (Sonnenthal et al. 1997 [DIRS 101296], Section 7.5.4). Fracture apertures at Yucca Mountain are determined through pneumatic flow tests (giving the fracture permeability) and a theoretical model relating fracture frequency (determined by observation of fractures), fracture permeability, and fracture aperture (Sonnenthal et al. 1997 [DIRS 101296], Section 7.5.4).

D3.1   USE OF SR MODEL

In this work, steady state flow fields with fracture apertures undisturbed or changed (to represent the effects of seismic activity) were first calculated, and then used to run transport simulations. A steady state flow field had previously been calculated for the SR model (CRWMS M&O 2000 [DIRS 151953], Section 6.2.1), and this result provided a flow field that could be used as an initial guess to determine the steady state flow fields for these calculations. For this reason these calculations were done using the SR model. The SR and LA models are similar enough that use of the SR model instead of the LA model is appropriate for the purpose of determining the sensitivity of transport to fracture aperture. The SR and LA flow and transport models are based on the same dual-permeability/active fracture conceptual model and numerical implementation. The main differences in the model set-up are the nonlocal connections introduced for the PTn/TSw interface between fractures and rock matrix. However, these lie above the repository and should have negligible effect on flow and transport below the repository. The most significant differences between the models is the shift in repository footprint to the north for the LA case compared with the SR design and some limited changes in parameterization based on new calibrations for the LA case.

Transport results for present-day and glacial-transition climate scenarios are compared in Figures D-1 and D-2. The transport results are for a uniform, instantaneous release of tracer mass from all repository locations at time zero. The tracer is nonsorbing, but can diffuse into the matrix. The present-day scenarios are shown in Figures D-1a and D-1b, which present the fractional cumulative breakthrough curves and normalized mass arrival rate curves, respectively. (For a unit tracer released at the repository at time zero, the fractional breakthrough curve represents the tracer cumulative arrival at the water table as a function of time. The normalized mass arrival rate is the time-derivative of the breakthrough curve.) These curves show that differences between SR and LA are small in comparison with the uncertainty represented by the lower, mean, and upper infiltration scenarios for this climate. The glacial-transition scenarios are shown in Figures D-2a and D-2b, which present the fractional cumulative breakthrough curves and normalized mass arrival rate curves, respectively. Although differences between the SR and LA cases are more pronounced for the glacial-transition case, these differences are still small in comparison with the uncertainty for this climate. Furthermore, the goal of the present analysis is to compare the relative effects of changes in fracture aperture on UZ transport behavior, and given that the conceptual and numerical models are for the SR and LA models are nearly the

same, the SR model should be suitable for assessing transport sensitivity to seismic-induced changes in fracture properties.
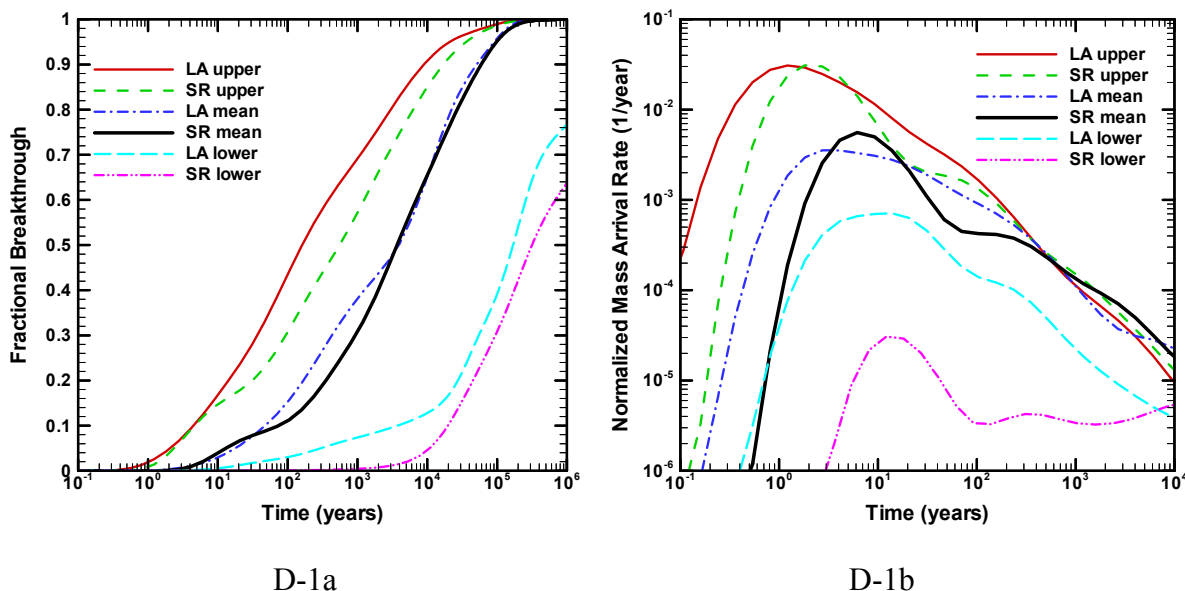
D-1a

D-1b

DTNs: LB03033DUZTRAN.001 [DIRS 170372] LA transport breakthrough curves.
         LB9908T1233129.001 [DIRS 147115] SR transport breakthrough curves.

Figure D-1.   Comparison of SR And LA Transport Results for an Instantaneous Release of (Nonsorbing) Tracer Mass at the Repository Horizon at Time Zero under Present-Day Climate. a) Cumulative Fractional Breakthrough, b) Normalized Mass Arrival Rate
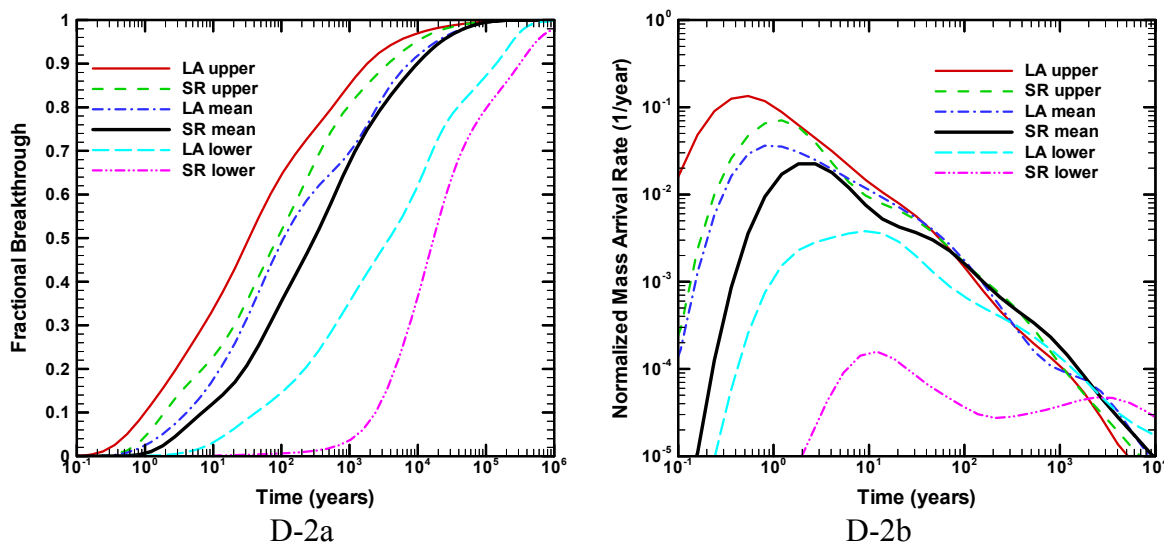
D-2a

D-2b

DTNs: LB03033DUZTRAN.001 [DIRS 170372] LA transport breakthrough curves.
         LB9908T1233129.001 [DIRS 147115] SR transport breakthrough curves.

Figure D-2.   Comparison of SR and LA Transport Results for an Instantaneous Release of (Nonsorbing) Tracer Mass at the Repository Horizon at Time Zero under Glacial-Transition Climate. a) Cumulative Fractional Breakthrough, b) Normalized Mass Arrival Rate

D3.2   ANALYSIS APPROACH

In the absence of definitive, predictive process modeling or definitive geologic observational evidence, a bounding approach is used to assess the potential effects of fault displacement on repository performance. The problem is bounded if large enough changes in fracture aperture are evaluated. Here, "large enough changes" are defined to be changes that can be justified as larger than any expected changes resulting from any fault displacements (near Yucca Mountain) that have an annual exceedance probability greater than 10^{-8} (Section 5, Assumption 5.1). Given an assumed change in aperture, it is possible to estimate the change in fracture hydraulic properties using theoretical models that relate the changes in fracture properties to the changes in fracture aperture (Section D3.2.7). The effects of the modified fracture properties on transport behavior between the repository and the water table can be evaluated using the UZ site-scale flow and transport models. Changes in transport are identified through the use of breakthrough curves for a simulated nonsorbing tracer. Transport of a nonsorbing tracer is used because this is expected to be more sensitive to changes in fracture aperture, because the effects of fracture aperture dominate fracture/matrix interaction for such a tracer (given fixed matrix properties).

If the identified changes in transport are small, then it can be concluded that the effects of fault displacement on potential radionuclide transport are negligible and can be excluded from further consideration in TSPA.

For such a method to be valid, the assumed changes in fracture aperture must be shown to represent a bounding change in fracture aperture for the effects of any fault displacement near Yucca Mountain. The justification that the assumed changes in fracture aperture bound the range of expected changes is given in Section D3.2.6.

The spatial distribution of changes to fracture aperture within the modeling domain is treated using two end-member scenarios:

1. All fracture apertures are altered uniformly throughout the UZ model domain (both fault zones and fractured rock).

2. Only fracture apertures in the faults zones are altered.

Isolating the effects of fault displacement to the fault zones provides the most reasonable expected case, which emphasizes the effects of property contrasts between the fault zones and the fractured rock. A large change in fracture properties over the entire UZ domain (fault zones and fractured rock) is an extreme bound for the possible effects of fault displacement. These cases bound the expected extremes for the spatial distribution of changes to fracture properties as a result of fault displacement.

Sensitivity calculations are performed for both the present-day (dry) climate and the long-term, glacial-transition (wetter) climate. The average infiltration rates used in the TSPA-SR UZ flow model for the present-day mean climate is about 4.6 mm/year and for the glacial-transition mean climate is about 18 mm/year (BSC 2001 [DIRS 158726], Table 6-3). The water table elevation remains unchanged in this analysis as a result of fault displacement or climate change. Maintaining a fixed water table provides a reference point for comparisons of the effects of fault

displacements on radionuclide transport. This is reasonable as a basis for comparison of the effects of fault displacement.

Fault displacements may result in changes to perched water. However, the effects of these changes in perched water on potential radionuclide transport are assumed to be negligible. The sensitivity of radionuclide transport to different perched water models has been shown to be small (CRWMS M&O 2000 [DIRS 134732]). Furthermore, the potential release of the perched water (and associated radionuclides) due to some disruptive event is expected to have a negligible effect on radionuclide releases at the water table (Section 6.8.8). Therefore, any additional changes in perched water, except for those changes caused by changes in fracture properties, are not expected to have significant consequences.

Thermal-hydrologic processes due to waste heat from the repository will affect UZ flow and transport. However, the effects of thermal-hydrologic processes are expected to be negligible with respect to this sensitivity study on the effects of fault displacements on mountain-scale UZ transport (Section 6.8.9).

D3.2.1 Dual-Permeability Concept

The conceptual model for unsaturated flow and transport used in this analysis is called the dual-permeability model. In the version of the dual permeability model used in this analysis, there are two continua representing the fracture and matrix that overlap in the macroscopic flow continuum. At every macroscopic "point" there are separate hydrologic conditions, properties, and other factors, for the fracture continuum and for the matrix continuum. Therefore, at every macroscopic "point" there is also a defined flux of water (flow rate of water per unit area) in the fracture continuum and in the matrix continuum. Practically speaking, the macroscopic point (or length scale) is defined by the grid discretization. At the microscopic (or sub-grid) scale, the fractures and matrix are spatially distinct, with length scales that define the microscopic geometric arrangement of the fracture and matrix continua. Given this microscopic geometry of the continua and the properties and conditions defined in each continuum, a flux of fluid at each macroscopic point between the fracture and matrix continua is also defined. In other words, there is also an exchange of flow between the fracture and matrix continua as well as flow through each continuum at each macroscopic point.

Although the dual-permeability model has been described above in terms of a flow model, an analogous description can also be made for the transport model. That is, transport takes place at each macroscopic point in both the fracture and matrix continua (each continuum having its own transport properties and conditions), and there is, likewise, a transport exchange between the fracture and matrix continua.

The dual-permeability model for flow and transport can be used in three, two, or one dimension. For example, a one-dimensional problem would have flow and transport in one linear direction only. This is easiest to understand for a problem in which flow occurs along one axis, say the z-axis. Assume that the rock properties and conditions at the boundaries of the model are independent of the remaining two spatial coordinates, x and y. Then the only spatial variations that could possibly occur in the problem are in the z direction. The spatial evolution of the problem can be completely described in terms of z. The x and y dimensions only enter the

problem in a trivial sense to scale the total quantity of flow and transport that take place in the real three-dimensional domain. This simple scaling can be done after analyzing the spatial (and temporal) variations in the problem. Numerically, the one-dimensional dual-permeability model is configured using a stack of paired grid cells as shown in the one-dimensional connection diagram give in Figure D-3. One stack represents the fracture continuum and one stack represents the matrix continuum. The dual-permeability connection diagram can be extended to two dimensions as shown in Figure D-4. In three dimensions, the conceptual nature of the dual-permeability model (with overlapping continua) becomes more apparent in so far as a connection diagram is concerned. In this case, there is no "extra" dimension for the fracture/matrix node pairing, so the fracture/matrix node pairs must overlap spatially in a three-dimensional connection diagram.

D3.2.2   Active Fracture Concept

The dual-permeability model used in these calculations employs the active fracture concept. The active-fracture-dual-permeability model (Liu et al. 1998 [DIRS 105729]; BSC 2004 [DIRS 170035]) takes into account that only a portion of the fracture network (conceptualized as a continuum in the dual-permeability model) is actively involved in conducting water, while other fractures are bypassed. It conjectures that only a portion of the fracture network is hydraulically active and only this active portion is in hydraulic contact with the rock matrix. As a result of such conceptualization, capillary pressure and relative permeability for the entire fracture network are treated as equal to those for the active portion, and the geometric fracture-matrix interface area is scaled down to define an active fracture-matrix interface area for use in fracture-matrix interaction. Therefore, the mechanism of the active fracture model hinges upon how the active fracture network is defined. In the UZ flow model used here, the fraction of active fractures is defined as an exponential function of the effective water saturation for the entire fracture network, with the exponent being treated as a fitting parameter. Subsequently, the capillary pressure and the relative permeability functions for the entire fracture network are defined by using the effective water saturation of active fractures. In addition, the active fracture-matrix interface area is defined as the geometric fracture-matrix interface area multiplied by a power function of the effective water saturation of the active fractures.
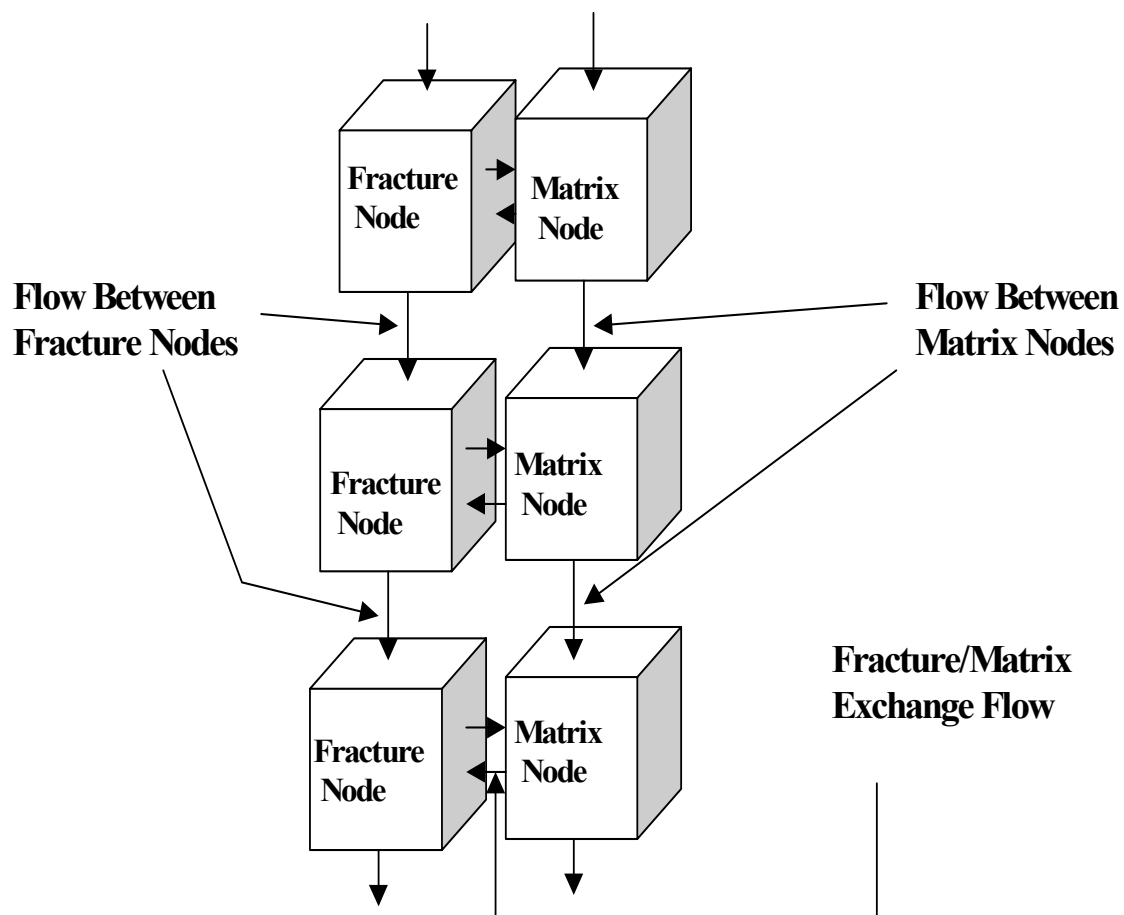
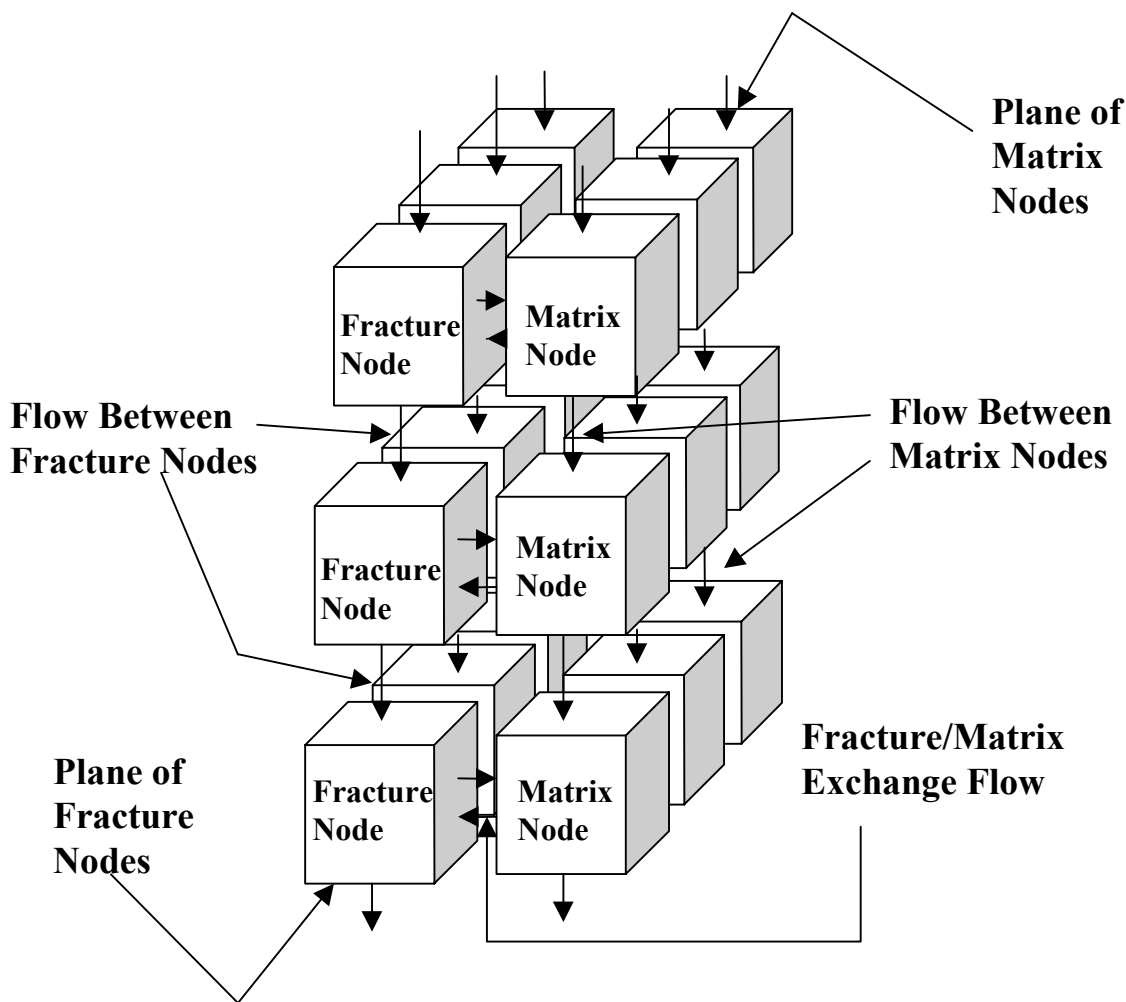Figure D-3. Conceptual Connection Diagram for a One-Dimensional Dual-Permeability Model

Figure D-4. Conceptual Connection Diagram for a Two-Dimensional Dual-Permeability Model

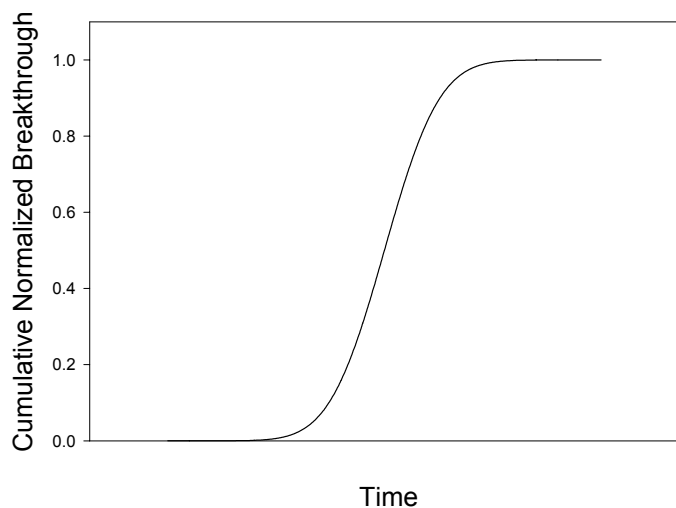## D3.2.3   Site-Scale Models for UZ Flow and Transport

The site-scale model for UZ flow uses the software TOUGH2 V1.4 (LBNL 2000 [DIRS 146496]). TOUGH2 is a multipurpose numerical model that, among other problems, can solve fluid flow problems in geologic materials (Pruess 1991 [DIRS 100413]). The standard differential conservation equations describing flow are cast in an integrated form for the numerical solution methods used in TOUGH2. The solution to these conservation equations is obtained by discretization of problem in space and time. In this analysis, TOUGH2 is used to solve the equations for unsaturated flow in a fractured rock domain representative of Yucca Mountain. Unsaturated flow is defined to be the flow of water only in a geologic material with pore spaces partially filled with water and partially filled with air. In an unsaturated flow model (as opposed to a two-phase flow model), the air is assumed to be at static equilibrium. As discussed in Section D3.2.1, fractured rock is represented using an active-fracture-dual-permeability conceptual model.

Transport simulations in this appendix are based on transport studies of conservative tracers using the T2R3D V1.4 code (LBNL 1999 [DIRS 146654]). The dual-permeability modeling

approach with the three-dimensional TSPA-SR grid, as discussed in Section D3.1, is used in the transport simulations. T2R3D is an integrated finite-difference transport model that is intended to solve mass transport problems in geologic materials. The fracture-continuum permeability and van Genuchten α values for these simulations were obtained from DTN: LB990801233129.009 [DIRS 118717] and LB990801233129.003 [DIRS 122757], and the grid was obtained from LB990801233129.001 [DIRS 122753].

D3.2.4   Breakthrough Curves

Breakthrough curves are used in this analysis to describe the behavior of radionuclide transport in the unsaturated zone. A breakthrough curve is generated by releasing particles uniformly over the fracture nodes of all the grid cells within the repository. Particles are only released to the fracture nodes because fractures are expected to be the main transport pathway at the repository horizon. Particles are released over some period (short relative to the transport time of the problem), approximating an "instantaneous" release of the particles. For this analysis, the particles are released uniformly over a period of 1 year. The breakthrough curve shows the total mass that has arrived at the water table (over the entire model domain) relative to the total mass released as a function of time, as shown in Figure D-5.


NOTE: Time axis is arbitrary.

Figure D-5. Schematic Diagram of a Breakthrough Curve

D3.2.5   Problem Domain

The TSPA-SR site-scale UZ flow and transport model is shown in plan view in Figure D-6 (BSC 2001 [DIRS 158726], Figure 6-2). An east-west vertical cross-section and a one-dimensional column are extracted from this three-dimensional model for some subdimensional calculations.
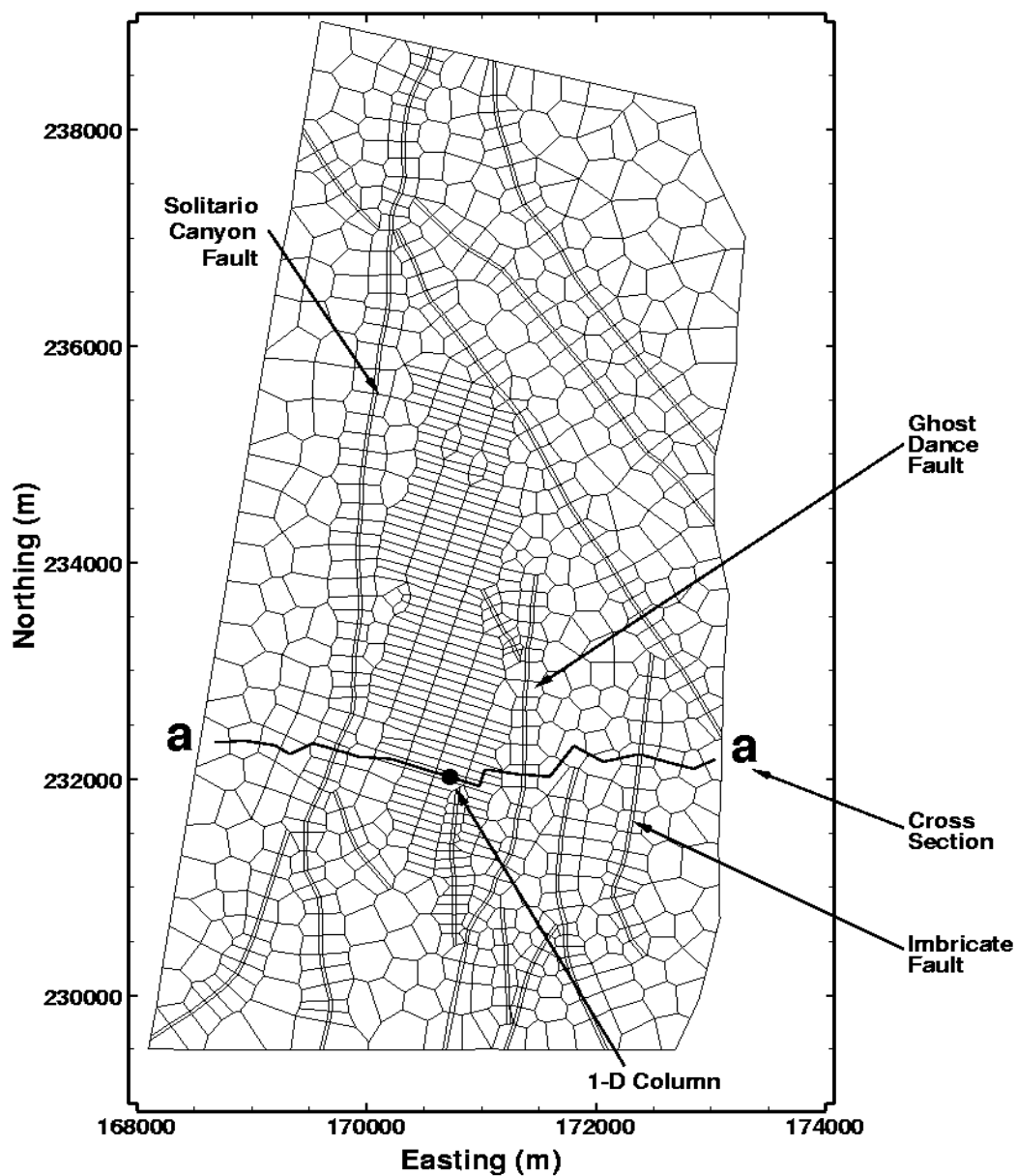
NOTE: The location of the one-dimensional column is shown by a '•' symbol and the two-dimensional cross section by line 'a-a' (added to this figure from BSC 2001 [DIRS 158726], Figure 6-2.

Figure D-6. Plan View of the Locations of the Two-Dimensional Cross Section and the Nearby Faults within the TSPA-SR UZ Grid.

D3.2.6 Bounds on the Change in Fracture Aperture

The approach used to investigate the effects of fault displacements is to evaluate the sensitivity of radionuclide transport in the UZ to changes in fracture apertures. This is investigated over a wide enough range to bound the potential changes in fracture aperture that could result from any fault displacement at Yucca Mountain with an annual exceeding probability of greater than 10^{-8}. The largest fault movement close to the repository is likely to be along Solitario Canyon fault. The general topic of seismic hazard at Yucca Mountain has been investigated in detail in the report "Probabilistic Seismic Hazard Analyses for Fault Displacement and Vibratory Ground Motion at Yucca Mountain, Nevada" (USGS 1998 [DIRS 100354]). For Solitario Canyon fault, the hazard analysis shows fault displacement 5 m (USGS 1998 [DIRS 100354], Figure 8-3) at an annual exceedance probability of 10^{-8}. The conservative fault displacement for bounding analyses is taken as 10 m.

Geomechanical models used to investigate the amount of strain induced by fault movements in the rock at Yucca Mountain show that changes in strain extend several kilometers from a fault movement (Gauthier et al. 1995 [DIRS 103258]; National Research Council 1992 [DIRS 105162], Appendix D). Using a three-dimensional elastic boundary element model of Yucca Mountain, Gauthier et al. (1995 [DIRS 103258]) investigated the effects of a right-lateral, strike-slip fault displacement on a fault dipping 60° E. The fault movement was 1 m along a 30 km section of the fault. The results show strains of 10 microns per meter (10 micro-strain, or 10 μs) up to 8 km from the fault. Geomechanics calculations were also performed in the National Research Council (1992 [DIRS 105162], Appendix D) report. This calculation was for a normal displacement along a fault dipping 60° E to the vertical. The simulated fault movement was 1 meter along 30 km section from the surface to a depth of 10 km. The results of this calculation show 50 μs two kilometers from the fault plane and 10 μs about 6 km from the fault plane. If these models were used for a 10 m fault movement instead of 1 m, the strains would be amplified proportionally because of the linearity of the elastic model. Therefore, for a bounding fault movement of 10 meters along Solitario Canyon fault, an elastic model would predict strains up to 500 μs two kilometers from the fault and 100 μs six kilometers from the fault. If the conservative approach is taken that all the strain accumulates in the fractures, then an estimate of the change in aperture can be made. First, assume a lower bound aperture of 100 μm in the present-day system (Sonnenthal et al. 1997 [DIRS 101296], Table 7.12) and a fracture spacing of approximately 1 m (Sonnenthal et al. 1997 [DIRS 101296], Table 7.7). Then a tensile strain of 500 μs would result in a new fracture aperture of about 600 μm. For a compressive strain of 500 μs, then the fractures would essentially be closed and the rock matrix would necessarily be compressed.

Changes in fracture properties are related to dilation or compression of existing fractures rather than the generation of new fractures. This approximation relies on the fact that the rock at Yucca Mountain is highly fractured and that fractured rock is mechanically weaker along existing fractures than intact rock. This assumption is supported by the results of the Probabilistic Seismic Hazard Analysis, which show that the probability for fault displacement to occur along existing fractures is more likely than for intact rock (USGS 1998 [DIRS 100354], Section 8.2.1). Therefore, strain due to fault displacement is likely to occur along existing fractures rather than initiate new fractures.

These results suggest that a factor of 10 change in aperture would bound the effects of tensile strain. In fact, because the average aperture at Yucca Mountain is approximately 200 μm (Sonnenthal et al. 1997 [DIRS 101296], Table 7.12), a factor of 10 change would result in fractures with an average aperture of 2,000 μm, or 2 mm. With regard to the reduction in aperture under compressive strain, other limitations constrain the change in fracture aperture. Attempts were made to use a factor of 10 reduction in aperture; however, convergence problems were encountered with the flow model. This is likely the result of insufficient bulk permeability in the system to accommodate the imposed infiltration flow conditions. Therefore, reductions in aperture were limited to factors of 0.2.

D3.2.7 Affected Parameters

Given a change in aperture, theoretical models are available to quantitatively model the associated changes in fracture permeability, fracture capillary pressure, and fracture porosity. Fracture aperture enters flow and transport modeling in different ways. Aperture affects the permeability and capillary pressure used for steady-state unsaturated flow calculations. For radionuclide transport calculations, the fracture aperture affects the fracture porosity. Fracture aperture also affects matrix diffusion for radionuclide transport, but for these simulations the matrix diffusion coefficient was set to zero. The fracture apertures used in these different parameters are not necessarily the same because the theoretical models strictly apply to idealized "parallel plate" fractures. Therefore, the aperture for permeability, capillary pressure, and porosity are generally different values. However, it is assumed that an increase or decrease in aperture will affect these physical characteristics in proportion to the functional dependence on aperture in the theoretical models.

The relationship for permeability, known as the cubic law, (Freeze and Cherry 1979 [DIRS 101173], Section 2.12; Sonnenthal et al., 1997 [DIRS 101296], Section 7.5.4) is the following:

$$k = \overline{f}\, \frac{b^3}{12} \qquad\qquad \text{(Eq. D-1)}$$

where $\overline{f}$ is the average fracture spatial frequency, k is the permeability, and b is the fracture aperture. As can be seen, the permeability is proportional to the cube of the fracture aperture.

The relationship between capillary pressure and saturation is derived from van Genuchten (1980 [DIRS 100610]), noting that $S_e = \Theta$ in van Genuchten's notation:

$$P_c = \frac{2\tau \cos\theta}{b\rho g}\left[S_e^{-1/m} - 1\right]^{(1-m)} \qquad\qquad \text{(Eq. D-2)}$$

where P_c is the capillary pressure (expressed as elevation above the water table by inclusion of ρ and g terms), τ is the surface tension of an air/water interface, θ is the contact angle between the air/water interface and the mineral surface, ρ is the density of water, g is the acceleration of gravity, S_e is the effective water saturation (normalized for the residual and maximum

saturations), and *m* is a parameter describing the variation in capillary pressure with water saturation.

The collection of terms, $\dfrac{b\rho g}{2\tau\cos\theta}$, is known as the van Genuchten α parameter. The van Genuchten α parameter scales the overall capillary pressure in the system. The parameter *m* accounts for the distribution of fracture apertures that the air–water interface encounters as a function of water saturation. The van Genuchten α parameter is directly proportional to fracture aperture.

The relationship for porosity, ϕ_f, is the following:

$$\phi_f = \overline{f}b \tag{Eq. D-3}$$

The porosity is also found to be proportional to the fracture aperture.

Now, let *b* be changed to *b** ; then correspondingly *k*, α, and ϕ_f, are changed to *k**, α*, and ϕ_f^*. These variables can be used to express the following relationships:

$$k^* = (b^*/b)^3 k \tag{Eq. D-4}$$

$$\alpha^* = (b^*/b)\alpha \tag{Eq. D-5}$$

$$\phi_f^* = (b^*/b)\phi_f \tag{Eq. D-6}$$

The factor of change in fracture aperture (*b*/b*) is then used to directly assign the new values of permeability, capillary pressure (*α*), and porosity.

In addition, the volumes for fracture and matrix elements should also be varied. Assume V_f and V_m as the original fracture and matrix element volumes, then the fracture and matrix element volumes varied due to fracture aperture change can be calculated as

$$V_f^* = V_f(\phi_f^*/\phi_f) \tag{Eq. D-7}$$

$$V_m^* = V_m(1-\phi_f^*)/(1-\phi_f) \tag{Eq. D-8}$$

Such variation in fracture and matrix element volumes only changes the partition of the bulk grid-cell volume (into either V_f and V_m or V_f^* and V_m^*) which itself remains as a constant.

D3.2.8   Calculation Procedures

Each calculation involves two major computer programs: TOUGH2 version 1.4 (Pruess 1987 [DIRS 100684], 1991) and T2R3D version 1.4 (LBNL 1999 [DIRS 146654]). TOUGH2 with its EOS9 module (for single-phase unsaturated flow) is used for computing unsaturated flow fields. Through transient simulations, steady-state flow fields are obtained and used in subsequent transport simulations. T2R3D performs transport calculations using the flow field calculated by TOUGH2.

The matrix and fracture parameter values both for the hydrogeologic units and the faults are taken from the TSPA-SR base-case UZ flow model (BSC 2001 [DIRS 158726]) and treated as the base case for this study. Sensitivity cases are conducted using fracture apertures modified as discussed in Sections D3.2, D3.2.6 and D3.2.7. Flow and transport modeling calculations are performed for present-day and glacial-transition climates. The UZ flow results from the base-case UZ flow calculation are processed to obtain the initial condition for calculations involving cases affected by fault displacement.

The input and output files for the calculations presented in Section D3.3 (output from this report) are available from the technical database under DTN: LB0408U0170FEP.002 [output].

UZ flow properties affected by fracture aperture were varied for the sensitivity study reported in this analysis. For the UZ transport calculations, diffusivity was given a nominal value of 3.2×10^{-11} m^2/s, with a tortuosity of 0.7, for an effective diffusivity of 2.24×10^{-11} m^2/s, as discussed in *UZ Flow Models and Submodels* (BSC 2004 [DIRS 169861], Sections 6.5.2 and 6.7.1). Only nonsorbing transport is investigated here. Dispersion has been shown to have little effect on transport results in the UZ over a wide range of dispersivities investigated (CRWMS M&O 1998 [DIRS 100364], Section 7.6.1.2.6), therefore, a dispersivity of zero was assigned.

D3.3 Results

The next two subsections describe the effects of fracture aperture changes on flow in the UZ and on mass releases at the water table. Results for cases in which the fracture apertures are varied are compared with the corresponding base cases. The first subsection, D3.3.1, considers a three-dimensional model when fracture apertures are only changed in the fault zones, not in the fractured rock. The second subsection, D3.3.2, describes the results for transport in a three-dimensional model with fracture apertures changed both in the fault zones and in the fractured rock. These three-dimensional calculations are performed for present-day and the glacial-transition climates. Mass transport calculations correspond to the instantaneous release of tracer mass at the repository at time zero.

D3.3.1 Fracture Apertures Altered in Fault Zones Only; Three-Dimensional Calculations for Present-Day and Glacial-Transition Climates

In this set of calculations, only the fracture apertures for the fault zones are changed by given factors. This is a reasonable case, although some effects on fracture properties may extend beyond the fault zone. The flow and transport calculations results shown in this section were performed as described in Section D3.2.8.

As shown in Figures D-7 and D-8 respectively for the present-day climate and the glacial-transition climate, the breakthroughs for the altered cases remain essentially unchanged from the base case. This indicates that if only the fault fracture apertures are affected by factors of 0.2 to 10, there would be virtually no impact to UZ flow and transport.
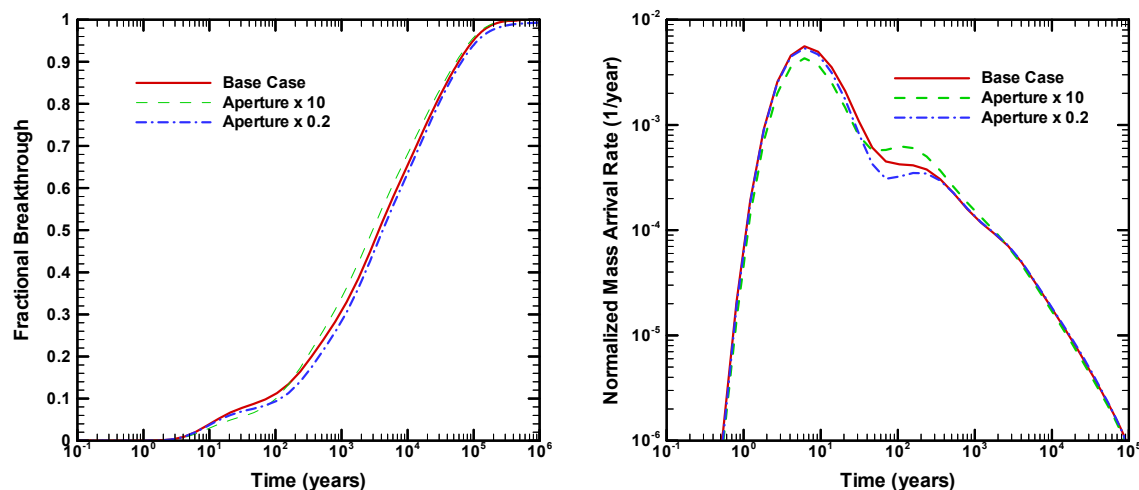
Output DTN: LB0408U0170FEP.002.

Figure D-7. Breakthrough Curves under Present-day Infiltration when Fracture Property Changes are Limited to the Fault Fractures.
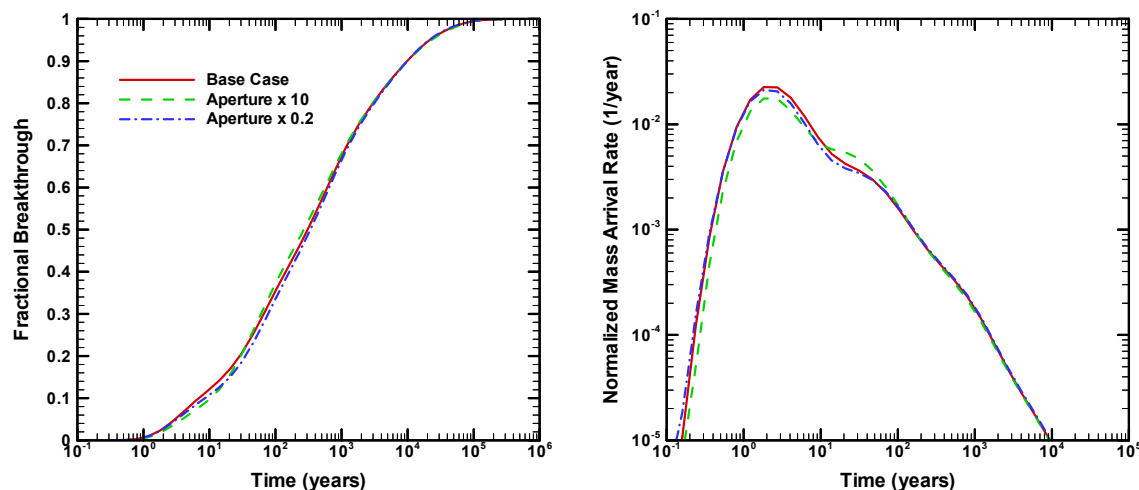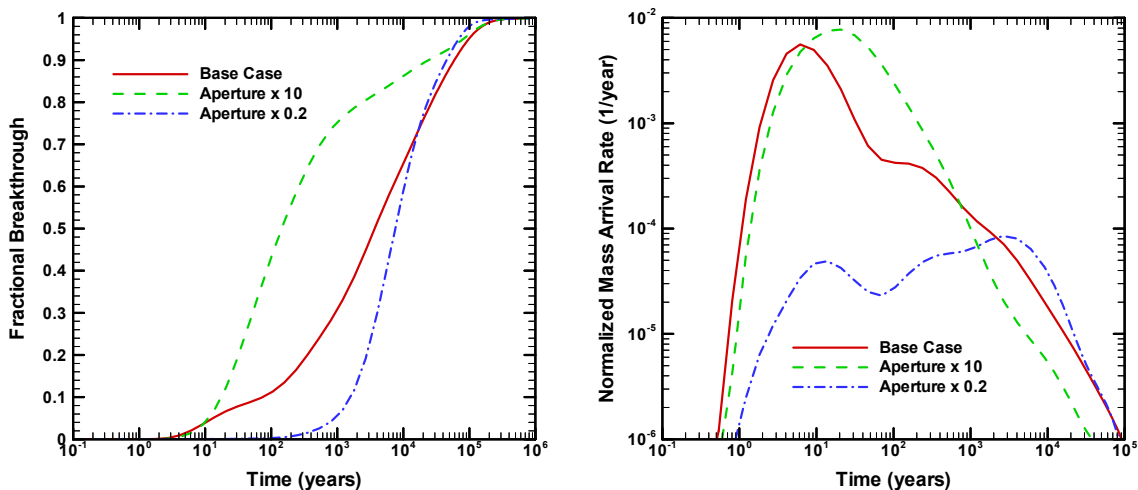

Output DTN: LB0408U0170FEP.002.

Figure D-8. Breakthrough Curves under Glacial-Transition Infiltration when Fracture Property Changes are Limited to the Fault Fractures.

D3.3.2 Fracture Apertures Altered Uniformly Across the Repository Block; Three-dimensional Calculations for Present-Day and Glacial-Transition Climates

The three-dimensional flow and transport calculations described in this section were performed as described in Section D3.2.8. The breakthrough curves for the present-day and the glacial-transition climates are shown in Figures D-9 and D-10, respectively. The results exhibit much greater influence as compared with the case in which fracture property changes are confined to the fault zones. For the factor-of-10 case, travel time (for 0.5 fractional breakthrough) is found to decrease by about a factor of 25 for the present-day case and a factor of 11 for the glacial-

transition climate. On the other hand, the normalized mass arrival rates are likely to be more significant for dose due because the rate of radionuclide mass arrival at the accessible environment is what controls dose rates. Comparisons between peak mass arrival rates for present-day and glacial-transition show that the effects of fault displacement are about a factor of 1.4 and 1.3, respectively. Furthermore, the peak doses occur slightly later for the ×10 aperture case. For the ×0.2 aperture case, the breakthrough curves are significantly delayed relative to the base case and the peak mass arrival rate is reduced by substantially more than one order of magnitude.

Output. DTN: LB0408U0170FEP.002.

Figure D-9. Breakthrough Curves under Present-Day Infiltration with Change in Fracture Properties Throughout the Entire Model Domain.
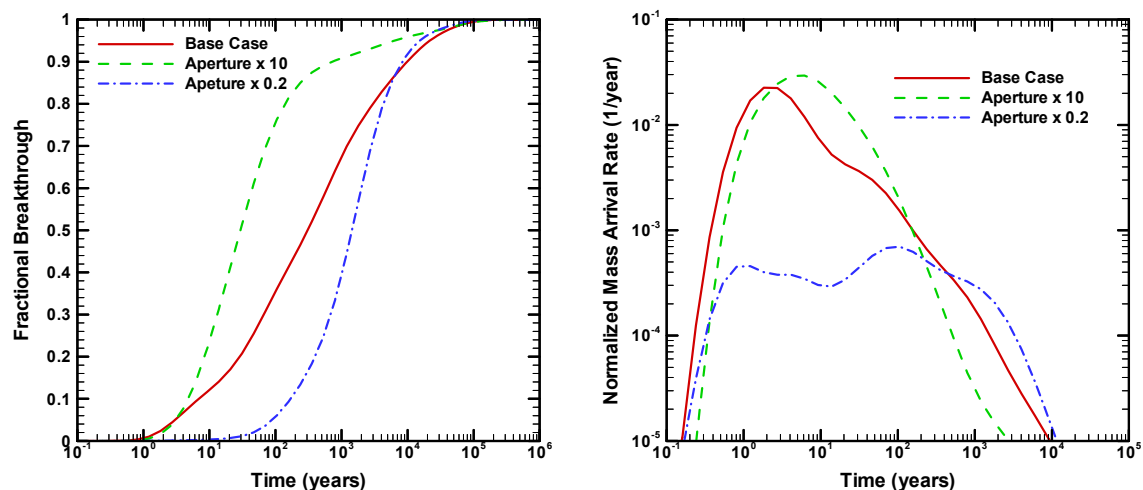
Output DTN: LB0408U0170FEP.002.

Figure D-10.   Breakthrough Curves under Glacial-Transition Infiltration with Change in Fracture Properties Throughout the Entire Model Domain.

D3.4   Discussion

The effect of changing fracture apertures on mass transport reflects the trend observed in the effect on flow; increased aperture leads to greater transport in fractures and shorter travel time to the water table. This leads to a consistent trend for simulated tracer breakthrough profiles at the water table. If the fracture apertures are decreased (increased), the travel times of the majority of the particles are increased (decreased), causing delayed (earlier) breakthrough. In particular, when fracture apertures are increased, the travel times of some particles are decreased due to enhanced transport in the fractures.

Capillary and gravity forces in the fractures of the dual-permeability model tend to work against fracture-matrix inter-flow and keep water flowing in the fractures. Note that fracture-matrix inter-flow is driven by the matrix-fracture capillary pressure difference. Assuming the inter-flow is from the fractures to the matrix, larger fracture apertures tend to promote fracture-to-matrix flow due to decreased fracture capillary pressure and increased matrix capillary pressure (that is, increased matrix-fracture capillary pressure differential). On the other hand, as fracture aperture is increased, gravity exerts more effect to keep flow within the fractures. The decreased capillary pressure in the fractures is roughly inversely proportional to the fracture aperture. In addition, due to the use of upstream weighting of the relative permeability in the numerical scheme of TOUGH2, the fracture relative permeability is used with the matrix absolute permeability to estimate the effective permeability of the fracture/matrix interface for fracture to matrix flow. The fracture relative permeability is the effective permeability for the fracture system at the given flow rate divided by the absolute permeability of the fracture system (i.e. a saturated fracture system). Thus, when the fracture apertures are increased, the fracture relative permeability (for about the same amount of fracture flow) decreases roughly in proportion to the cube of the aperture ratio. This is due to the fact that the effective permeability is roughly set by the amount of flow and the saturated permeability is proportional to the cube of the fracture aperture (Equation D-1). Therefore, the fracture/matrix interface effective permeability is also reduced by this ratio. This reduction of the fracture/matrix interface effective permeability leads toward greater flow and transport in the fractures when fracture apertures are increased. The above mechanism for enhanced fracture transport when fracture aperture is increased can be further promoted by the use of active-fracture-dual permeability model. The active-fracture-dual-permeability model, among other things, scales the fracture-matrix interface areas using a function of water saturation in the fractures, and thus can further reduce fracture-to-matrix transport because fracture-matrix interface areas are reduced as a result of the generally reduced water saturation in the fractures.

D4.   CONCLUSIONS

This study attempts to address the potential effects of fault displacement on transport in the UZ using sensitivity analysis that is conducted by perturbing fracture parameters. The degree of such perturbations are conservatively based on phenomenological assessment of the geological information of the site.

The SR UZ flow and transport models have been found to be substantially the same as the LA UZ flow and transport models. Differences in cumulative fractional breakthrough and mass arrival rates for the SR and LA models are found to be less than uncertainties in these models. Thus, use of the SR model for this sensitivity study is adequate for its intended purpose.

In the context of the TSPA-SR three-dimensional UZ flow and transport model, sensitivity studies for UZ flow and transport presented in this analysis suggest that transport between the repository and the water table is only weakly coupled to changes in fracture aperture. Overall, insignificant changes in transport behavior are found for large changes in fracture aperture. Changes in fracture aperture confined to the fault zones show virtually no effect on transport behavior. Breakthrough is found to be at most about 25 times earlier than the base case (under the present-day or the glacial-transition climate), for an extremely conservative ten-fold increase in fracture aperture applied over the entire UZ domain. Nevertheless, changes in the peak mass arrival rate at the water table are much smaller, factors of 1.4 and 1.3 for present-day and glacial-transition climates, respectively. Effects of such magnitude on travel time and mass arrival rates are no more significant than those caused by uncertainties in infiltration (CRWMS M&O 2000 [DIRS 134732]). Given that the more realistic case where fracture changes are confined to the fault zones and the relatively limited changes found for the extremely conservative change in properties over the entire domain, the effects of fault displacement on UZ transport is expected to be negligible. Therefore, models for TSPA-LA may exclude the effects of fault displacement on UZ transport.