

Simulation Modeling of an Enhanced Low-Emission Swirl-Cascade Burner

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Dr. Ala Qubbaj, Mechanical Engineering Department

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**University of Texas pan American
1201 West University Drive
Edinburg, Texas 78539-2999**

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ABSTRACT

The research team was formed. The advanced CFDRC-CHEMKIN software package was installed on a SUN-SPARC dual processor workstation. The literature pertinent to the project was collected. The physical model was set and all parameters and variables were identified. Based on the physical model, the geometric modeling and grid generation processes were performed using the CFD-GEOM (Interactive Geometric Modeling and Grid Generation software). A total number of 11160 cells (248×45) were generated to numerically model the baseline, cascaded, swirling, and swirling-cascaded flames. With the cascade being added to the jet, the geometric complexity of the problem increased; which required multi-domain structured grid systems to be connected and matched on the boundaries.

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A. EXPERIMENTAL (PHYSICAL) MODEL

Figure 1(a) shows the actual physical model, which consists mainly of a combustion chamber made from steel, 63.5 cm x 63.5 cm cross-section and 139.7 cm height. The chamber is provided with air-cooled Pyrex windows of dimensions 38.1 cm x 114.3 cm on all four sidewalls. The top of the chamber is connected to the atmosphere through an exhaust duct (as seen in Fig. 1). The fuel and oxidant are introduced to the combustion chamber through separate streams in a non-premixed or diffusion combustion process. The fuel is introduced through a stainless steel burner, of internal diameter 3.2 mm, inserted in the centerline of the chamber, and the air is introduced through an annular inlet of diameter 0.2 m, surrounding the fuel burner as depicted in Figure 1. Swirl is imparted to the air stream at swirl number (SN) of 1. The swirl number represents the ratio between the angular and axial air velocities. The cascade consists of a set of four identical venturis, with circular arc profiles, to form a cascade. The dimensions of the venturis are given in table 1 and shown in Fig. 1. The simplified physical model used in the computations, assuming axisymmetric flow conditions, is provided in Fig. 2. The operating and boundary conditions are given in Table 1.

B. GEOMETRIC MODELING AND GRID GENERATION

The computational domain encompassed half of the flame jet assuming axisymmetric flow conditions (as seen in Fig. 2) and extended to 139.7 cm in the axial direction and 31.75 cm in the radial direction. The grid cells were generated with increasing spacing in the radial and axial directions; this provided an adequate resolution where gradients were large, i.e., near the centerline, and saved CPU time where gradients were small, near the edges (as seen in Fig.3)

The venturis were modeled as two-dimensional axisymmetric convergent nozzles around the jet. With the cascade being added to the jet, the geometric complexity of the problem increased; which required multi-domain structured grid systems to be connected and matched on the boundaries. The CFD-GEOM module (Interactive Geometric Modeling and Grid Generation Software) in the CFD-ACE+ package was used for geometric modeling and grid generation purposes.

C. RESULTS (pending)

The physical model was set, the geometric modeling and the grid generation processes were performed for the baseline, cascaded, air-swirling, and swirling-cascaded flames. Therefore, the numerical computations are about to start. The results are expected to be available soon.

D. CONCLUSION (pending)

As soon as the data become available, the conclusions will be made.

E. REFERENCES

Not available

Table 1: Operating and Boundary Conditions

Fuel	Natural Gas (95%+)
Burner diameter (d_b)	3.175 mm
Jet-exit Reynolds number	9000
Jet-exit/ Fuel axial velocity u_x	46.65 m/s
Venturi throat diameter (d)	0.0625 m
Venturi diameter ratio (D/d) [*]	1.25
Angular air velocities u_θ	3 m/s
Axial air velocity u_x	0.3 m/s
Swirl number (rw/U)	1.0
Near-burner axial location: x/d	4.63
Ambient temperature	295 K
Ambient pressure	100 kPa

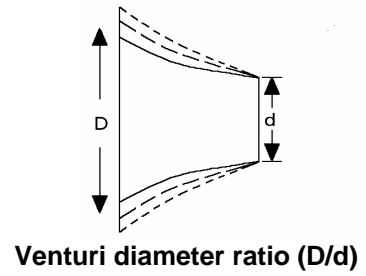
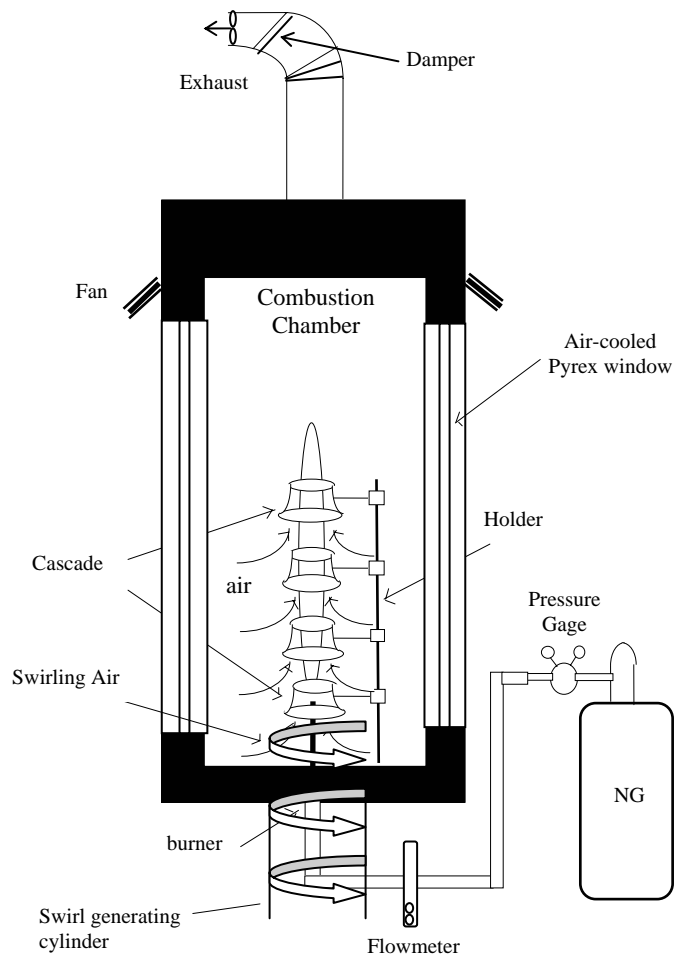


Figure1: Actual physical model

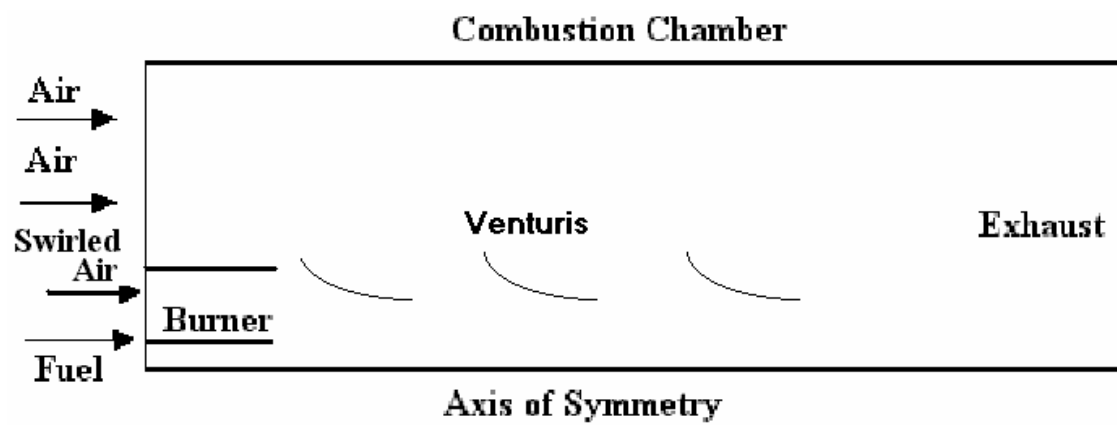


Figure2: Simplified Problem geometry

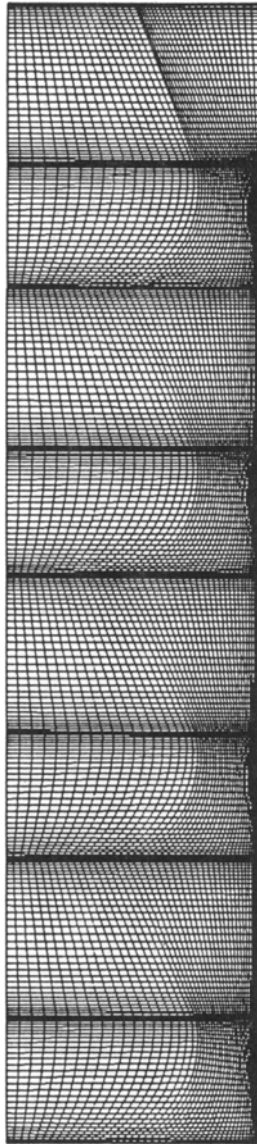


Figure 3: Non-uniform grid generated for flow computations