

## Radiation-Driven Shock and Debris Propagation down a Partitioned Pipe\*

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## Abstract

Two experiments have been performed to measure the effects of pulsed radiation loads on the front of small tubular structures, using as an energy source the X-ray fluence produced by a Z-pinch at the Sandia National Laboratories Z Facility. The project had two major goals: to establish the feasibility of using the Z machine to study the phenomenology associated with debris generation and propagation down tubular structures with partitions; and to use the resultant experimental data to validate numerical hydrocodes (shock physics codes) so that we have confidence in their use in analyzing these types of situations. Two tubular aluminum structures (5 and 10 cm long and 1 cm inside diameter) were prepared, with aluminum partitions located at the front, halfway down the pipe, and at the rear. Interferometry (VISARs) provided multiple velocity histories for all of the partitions. In both experiments, the first barrier, which was exposed directly to the x-ray fluence, was launched into the pipe at a velocity of ~2 km/s, accelerating to give a mean velocity of approximately 2.6 km/s. Loss of plate integrity is inferred from the dispersed launch of the second partition at approx. 1 km/s. Wall shocks propagating at 4.5 km/s were inferred, although strain gage measurements did not succeed. Post-test metallography showed evidence of melting and partial vaporization of the plates, and turbulent mixing with material from the walls. Calculations qualitatively agree with the observed results, but slightly overpredict debris velocity, possibly due to overestimates of total energy fluence. An application for this work is the study of techniques for line-of-sight shock and debris mitigation on high-power pulse-power facilities such as Z and its follow-on machines.

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## I. Introduction

As more elaborate experiments are conceived to utilize the Z accelerator, NIF, and other pulsed-power facilities, the risk of experiment failure due to an impact of X-ray driven debris increases. At the same time, a study of such debris affords the opportunity to learn about X-ray coupling aspects of weapon effects phenomena. Centimeter-sized hohlrahms allow target structures of a size sufficient to accommodate a wide variety of diagnostics, while the hohlrahm temperatures achieved (150-250 eV) provide a useful spectrum of soft X-rays.

In the present study, we instrumented two tubular structures with multiple velocity interferometry systems (VISARs) and with strain gages to measure the response of these structures to the X-ray flux from the Z-pinch (Figure 1.1). This process included constructing fiber optic and cable connections to the experimental chamber to accommodate 10 new channels of VISAR and three strain gages per test.

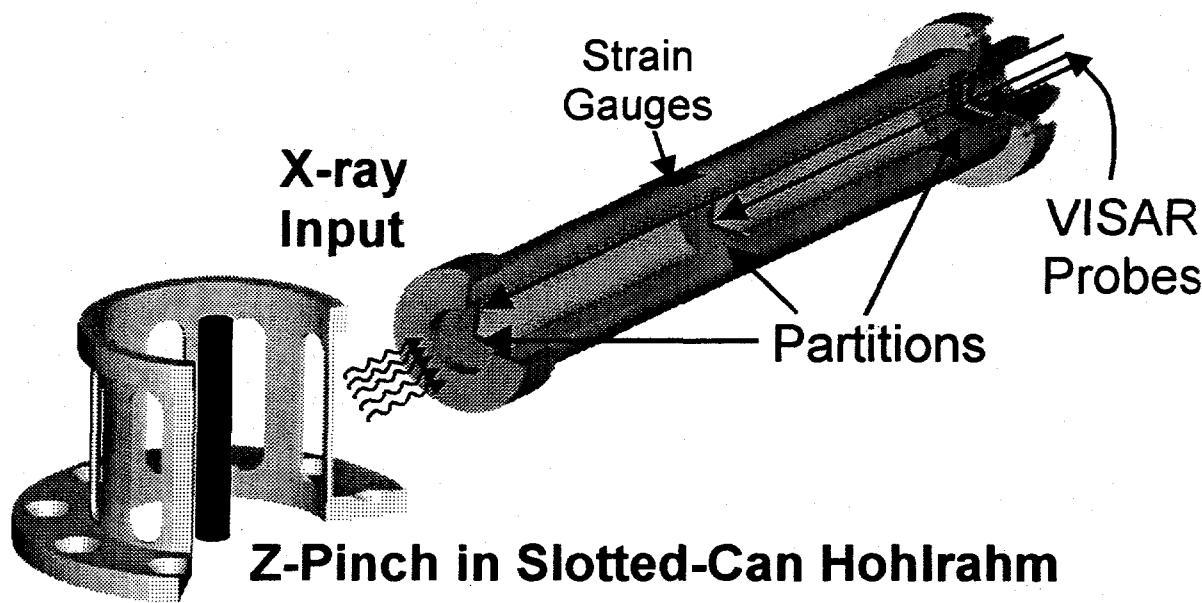


Figure 1.1. Basic configuration of tube/Z-pinch experiments

Both structures were recovered after their respective tests, and one was subjected to detailed metallographic, microprobe and SEM examination. The results of this examination, coupled with the time-resolved VISAR results, provide a picture of model response to the X-ray flux being a complicated process involving melting, vaporization, tube wall excoriating, and material diffusion into the walls – a stark contrast with a simple model of partitions traveling down the tube like flying plates.

## II. Experimental Configuration

A schematic drawing of the overall tube assembly is shown in Figure 2.1. The three partitions shown are machined by diamond-turning from 1100 alloy aluminum (essentially pure elemental aluminum), and are 1 mm thick except for the one most distant from the pinch, which is 3 mm thick. Diameters are 1 cm. The remainder of the tube structure is machined from 6061-T6 aluminum, an alloy whose dynamic response has been extensively studied over the years.

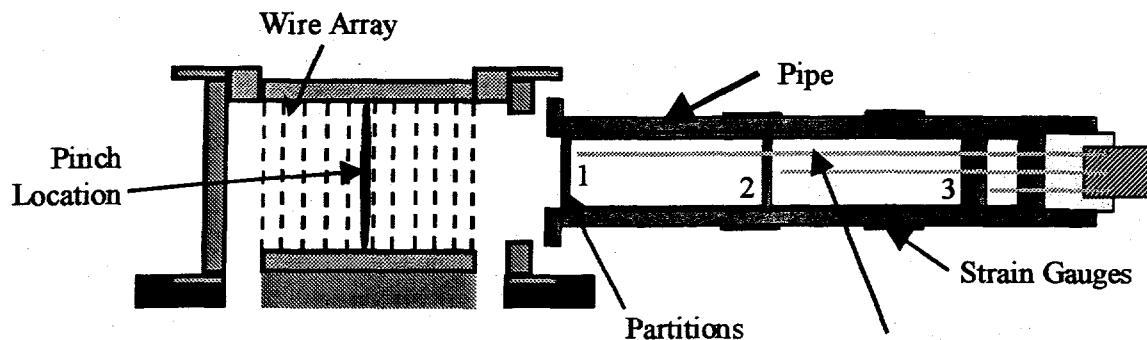
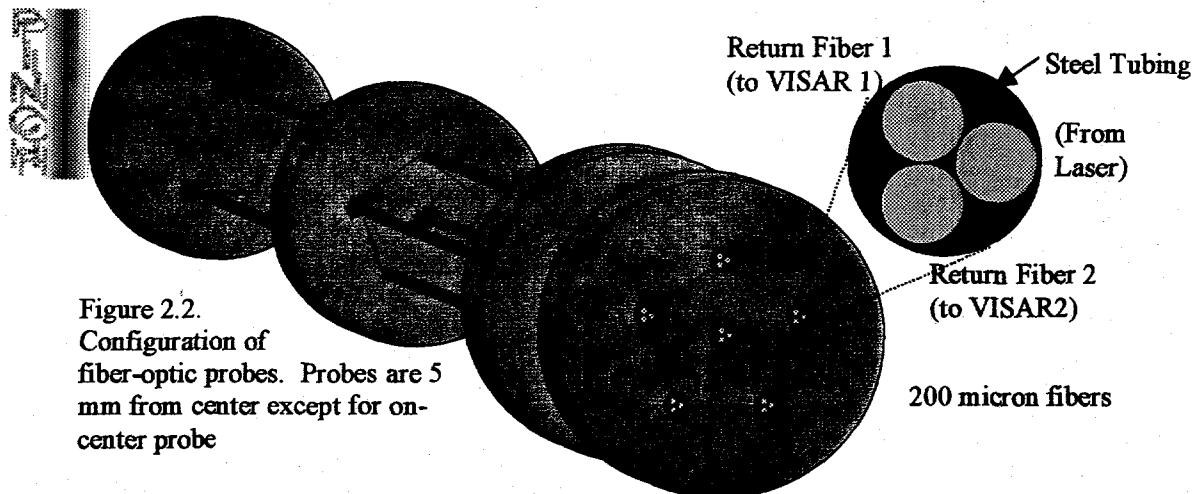


Figure 2.1. Schematic of tube experiment Long tube has partitions separated by 5 cm instead of 2.5 cm for short tube.

Lenseless fiber optic probes were introduced prior to emplacement of the partitions, using a jig to ensure that the ends were 0.5 mm from the final position of the partition. Each of these

probes was composed of 3 fiber-optics (one for light from the laser; the other two to transmit doppler-shifted light to the VISARS) in a bundle encased in a 1 mm diameter steel syringe tube. The 0.5 mm separation has been found to be a value allowing usable intensity return to the VISARS. Smaller spacings result in too little overlap between the area illuminated by the fiber from the laser and the areas contributing to the light returned to the VISARS. The configuration of holes for the fiber optics is shown in Figure 2.2. Because of the construction of these probes, the motion of only one of the partitions at the center could be monitored.



Strain gages were placed on the outside of the tube wall for both tests (see Fig. 2.1). The requirement for mounting points for associated circuits, as well as for gage protection from the x-ray flux, necessitated the use of a large housing for the tube experiment.

As a control, an aluminum disk similar to the front partition was placed adjacent to a second hohlrahm port and monitored by VISAR. This is labeled "X-ray input diagnostic" in Figure 2.3.

Fluence measurements were performed with diagnostics already in-place at Z for characterizing source terms. These did not affect the fluence delivered to the tube experiment or

the input diagnostic.

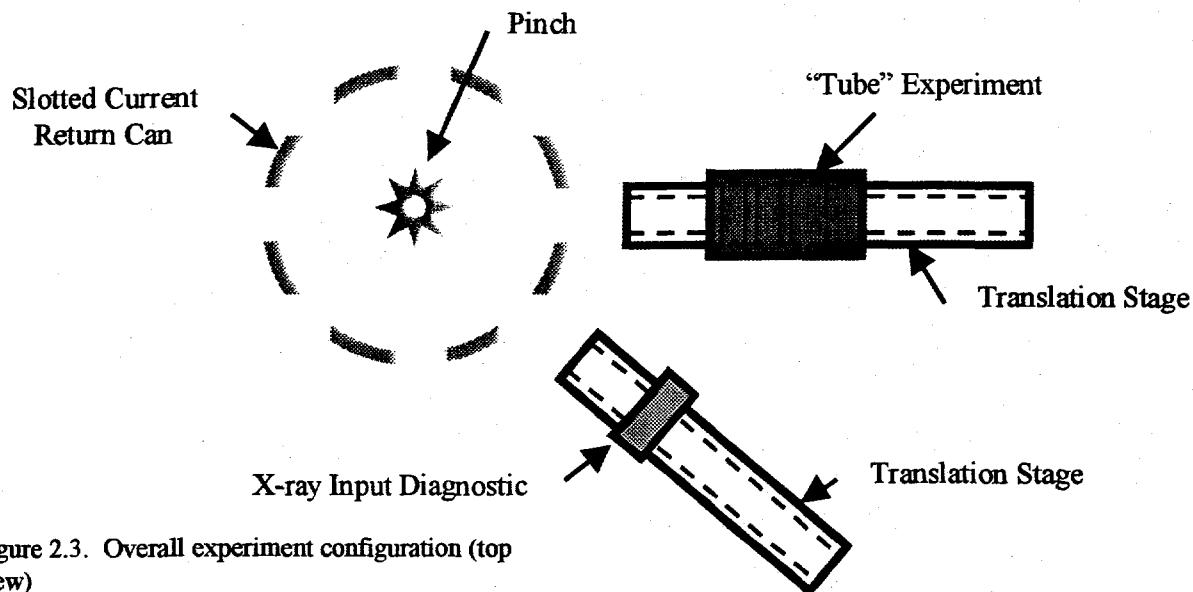


Figure 2.3. Overall experiment configuration (top view)

To effect the multibeam VISAR diagnostics required for this experiment, a 107 foot bundle of 40 fibers (200 micron multimode low OH FHP, Polymicro) and a 5 foot feedthru were manufactured. These connected the experiment in the evacuated center section of the Z facility with the screen room containing the VISAR and recording systems. They afforded the opportunity for flexibility in future tests.

Two multibeam Valyn International VISAR interferometers were used (one VLN-03 and one VLN-04 model) to monitor the motion of the partitions. Each of these interferometers has the capability of measuring velocity histories for up to 7 spots. In these experiments, both interferometers measured the velocity history of two points on the front partition (closest to the pinch; both at 0.25 cm radius from the axis of the tube), two points on the middle partition (one at the center, the other at 0.25 cm radius), and one on the rear partition (at 0.25 cm radius). Velocity-per-fringe sensitivities were chosen as 0.386 km/s (VLN-03) and 0.846 km/s (VLN-04). This afforded dual-delay-leg monitoring of all spots.

An additional pair of Valyn International ORB interferometers was used to monitor the motion of the X-ray input diagnostic, an aluminum disk similar to the front partition.

Data were recorded on LeCroy 7200 digitizers at 0.5 ns per point. Timing relative to pinch was established by assuming shock injection into the first partition at the moment of peak pinch. For the present experiment, timemarks were recorded on one digitizer and fringe records on others. Subsequent tests with timemarks injected onto all digitizers have shown that this gives 3 – 4 ns of jitter in the data (an amount small enough to not be a problem in the present experiment).

The overall assembly is shown in Figure 2.4. Again, note the relatively massive holding fixtures necessary to accommodate the supporting electronics for the strain gages. The tube was soft-mounted to the supporting structure using large RF gaskets (essentially steel mesh over a very soft elastomer ring) so that the motion of the tube was unconstrained by the mounting system.

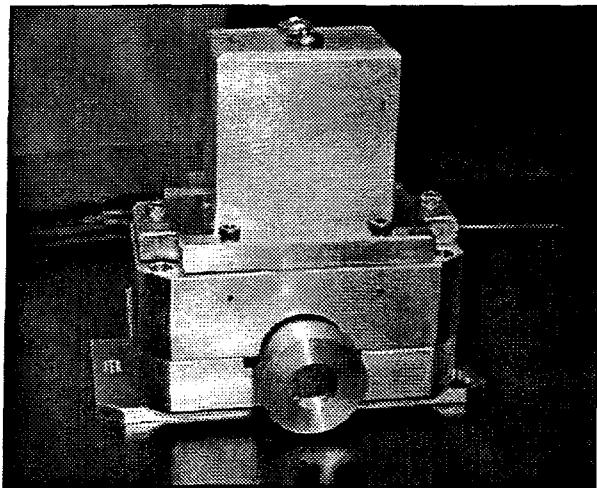


Figure 2.4. View of portion of long-tube assembly facing toward pinch. Front partition is the small circular area in the center of the base.

Figure 2.5 shows the assembly as mounted adjacent to the wire arrays, which generate the Z-pinch during the experiment.

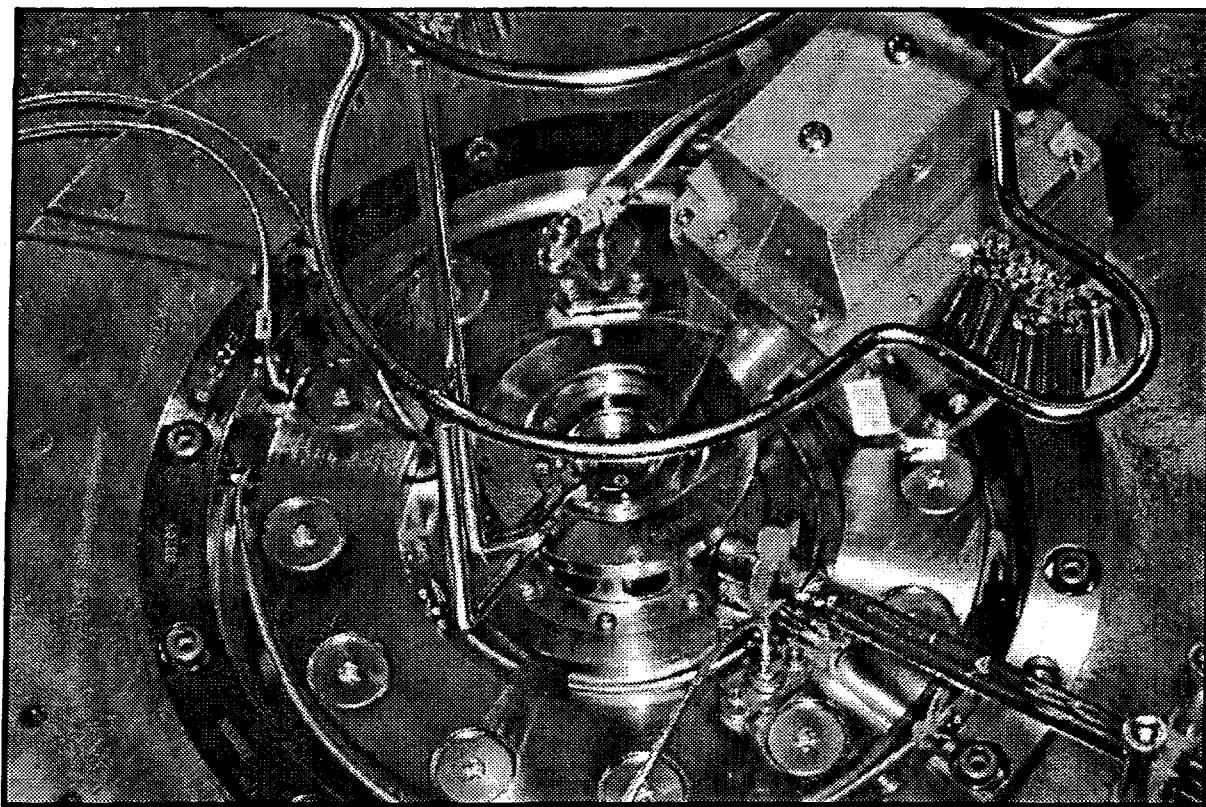


Figure 2.5. View of tube assembly mounted to stage of Z-pinch facility. Tube in mounting is at upper right (2:30). Wires to form pinch form a cone coming upward from the center of the large circular fixture. Small weights next to tube holder assembly maintain tension on wires. Probe at lower right (4:00) is the X-ray input diagnostic (an aluminum flyer plate similar to the front partition).

### III. Numerical Simulation of Pipe Response

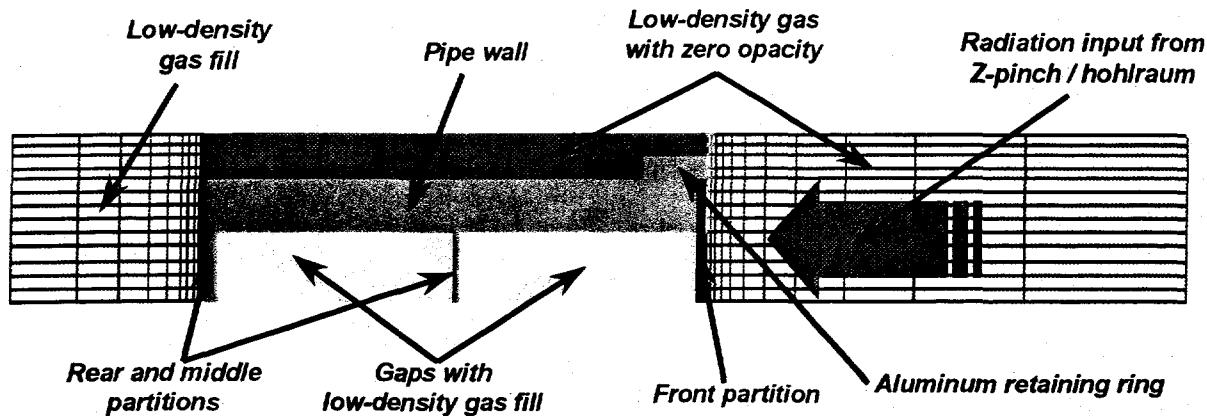
We performed a number of numerical simulations of the response of the partitioned pipe configuration, both pre-test and post-test. The calculations had three fundamental purposes. The first was to provide initial predictions of the pipe and partition responses to assist in the details of the experimental design. The second purpose was to help improve our understanding of the phenomenology involved in the dynamic response of the configuration in the pulsed radiation environment produced by the Z machine. Finally, post-shot calculations are providing validation

for our modeling capabilities so that we can use them for credible and reliable predictions under other but related conditions.

For these simulations, we are using the ALEGRA code (Summers, et al, 1997), which is a three-dimensional shock-physics computer program running in Lagrangian, Eulerian, and/or ALE coordinate systems. It can run on large massively parallel computers, and it has many physics options including radiation transport, MHD, hydrodynamics, material strength (including fracture), and conduction. In the present calculations we are using Eulerian coordinates, and are employing the hydrodynamics, material strength, and radiation transport options. Although we cannot provide a detailed description here, the latter uses the SP<sub>1</sub>/single-group approximation.

To model the partitioned pipe we used a non-uniform Eulerian mesh consisting of about 7,000 elements for the long pipe and nearly 4,000 elements for the short pipe. Two-dimensional cylindrical symmetry was used, and the pipe was surrounded by low-density gas with no opacity. The latter approach was employed to avoid using rigid boundary conditions on the pipe and to allow it to respond in a "breathing" mode if the dynamics of the problem so dictate. The axial zone sizes were large at both ends of the configuration, and were gradually reduced in dimension so that at either end of the pipe 0.2-mm resolution was provided. In the radial direction the resolution was uniform at 1 mm. This is not ideal, especially in terms of zonal aspect ratio, but it was the best balance between spatial resolution and computational running time. The numerical configuration is illustrated in Fig. 3.1; it is qualitatively similar for both the long and the short pipes.

Both the pipe and the partitions were made of standard aluminum, and in the calculations they were modeled with the nominal Sesame equations of state. Because it is virtually all vaporized by the radiation pulse, the front partition was assumed to behave hydrodynamically,



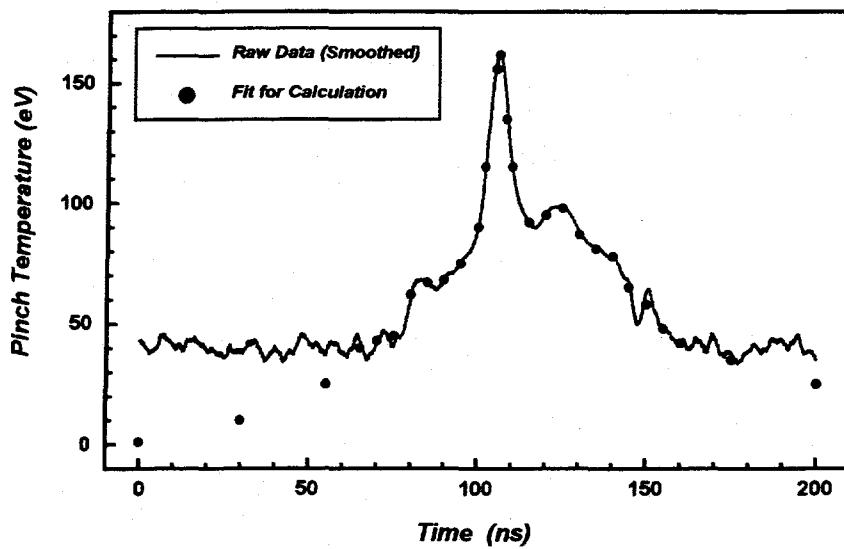
**Figure 3.1.** Configuration for numerical simulations. The sketch is not proportionally scaled, and applies to both long and short pipes. For the former the gaps between the partitions are 50 mm and the numerical mesh involves ~7,000 elements; the latter has gaps of 25 mm and employs ~3,800 elements. Only the upper half of the cylindrically symmetric configuration is shown.

where the other two barriers and the pipe wall were treated as elastic-plastic materials with a conventional 3-kilobar yield strength. The only other materials in the problem are the low-density gases surrounding the pipe and contained in the interior. Their density was kept low to be a reasonable simulation for the vacuum that existed in the actual experiments. In addition, their opacities were set to zero so they would not significantly perturb the radiation flow.

For all of the calculations the radiation input from the Z-pinch source was characterized as a time varying Planckian or black-body temperature history. For the calculations performed before the experiments, we assumed simply that the temperature was triangular in time with a base width of 40 ns, and a peak temperature of either 100 or 55 eV. The former represented the maximum level of loading that might be achieved in a Z-driven hohlraum situation. The lower temperature was our best estimate of the effective temperature anticipated at the sample location for the first experiment. The total energy fluences for these two cases differ by about a factor of

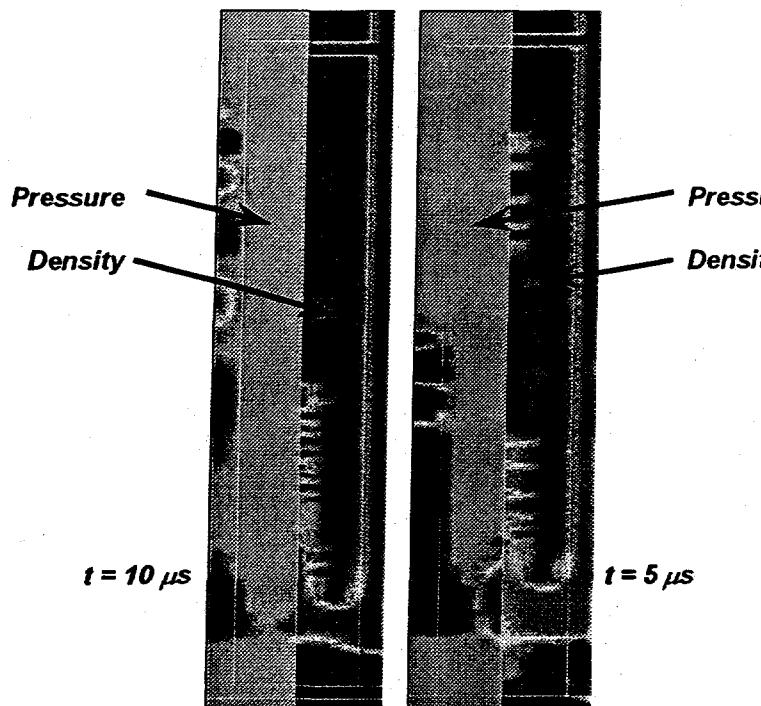
eleven. They also differ in terms of their radiation spectrum, but since the front partition is optically thick at the relevant wavelengths, this is probably not a major issue.

Diagnostics from the actual experiments yielded the actual temperature-time data shown in Fig. 3.2. Because the measurement threshold is in the region of 30 to 40 eV, the data show a baseline at this level. In the calculations we assumed that the temperature started at zero and increased to the measured value at a time of roughly 60 ns. The curve peaks at  $\sim 162$  eV and has a FWHM pulse width of  $\sim 40$  ns. Due to the geometric attenuation from the slotted-can hohlraum and the actual distance from the pinch at which the pipe was located, the total energy fluence incident on the front partition was about 3.3 percent of that represented by equivalent hohlraum boundary condition at the pinch temperature.



**Figure 3.2.** Measured temperature/time history from the Z pinch for the partitioned pipe experiments. The points represent the input used for the numerical simulations.

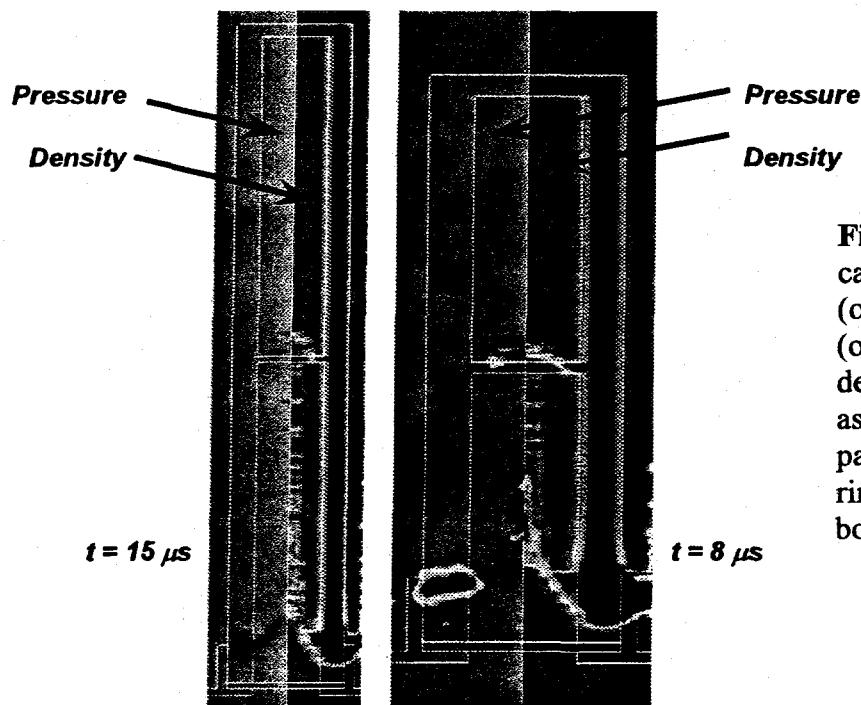
Pre-shot calculations used the simplified radiation inputs to clarify the expected responses of the pipe. We used only the long-pipe geometry, but looked at both the 100 and 55 eV sources. Figure 3.3 shows selected plots from the two runs. Both illustrate the region from the front partition to the middle one, on the left showing the results for a peak source temperature of 55 eV, and on the right for a peak of 100 eV. Consequently the total energy fluence is roughly



**Figure 3.3.**  
 Representative images from pre-shot calculations. The radiation input was a 40-ns-wide triangular pulse peaking at 55 eV (on the left) and 100 eV (on the right). The radiation is incident from the bottom, and the total energy fluence is  $\sim 11$  times greater for the higher temperature calculation on the right.

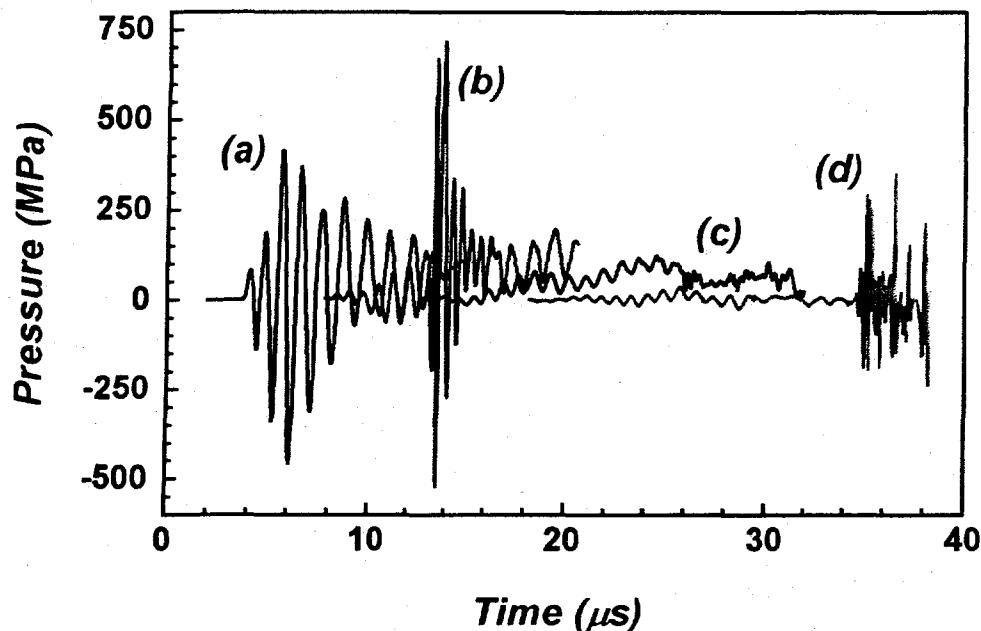
11 times greater for the 100-eV problem (the ratio of the fourth power of the peak temperatures). The left half of each image shows the pressure, where the right half indicates the material density. In the higher fluence case ( $T_{\max} = 100$  eV), we see that the debris from the fully vaporized front partition precedes the pressure waves in the pipe wall, and by the time of the plot (5  $\mu$ s) is nearly to the middle partition. In contrast, the lower fluence associated with other calculation (at  $T_{\max} = 55$  eV) still vaporizes the front partition, but the resulting debris velocity is, as indicated on the left-hand image (at 10  $\mu$ s), only about one-fourth as great. In this case the pressure waves in the pipe wall precede the debris by nearly a factor of two in time. It is this latter situation that most closely matches the anticipated experimental conditions. These two calculations clearly illustrate two different response regimes, and their dependence on total energy fluence.

Based on the experimental measurements we repeated the calculations, both for the long pipe and for the short pipe. Results are shown in Figure 3.4. In both cases we used the radiation input shown in Fig. 3.2. As above we show both the pressure and the density for, on the left, the long pipe, and on the right, the short pipe. The entire pipes are shown, including front, middle, and rear partitions. We have picked times that show the debris just after penetrating the middle partitions. For the long pipe this is at  $15 \mu\text{s}$ , and for the short pipe it is at  $8 \mu\text{s}$ . These times are as expected since the pipe lengths differ by a factor of two. Both calculations exhibit characteristics similar to the lower temperature and fluence pre-shot problems; that is the pressure waves in the pipe walls precede the debris by about a factor of two in time.



**Figure 3.4.** Post-shot calculations for long pipe (on the left) and short pipe (on the right). The detailed geometry associated with the front partition and its retaining ring can be seen at the bottom of the images.

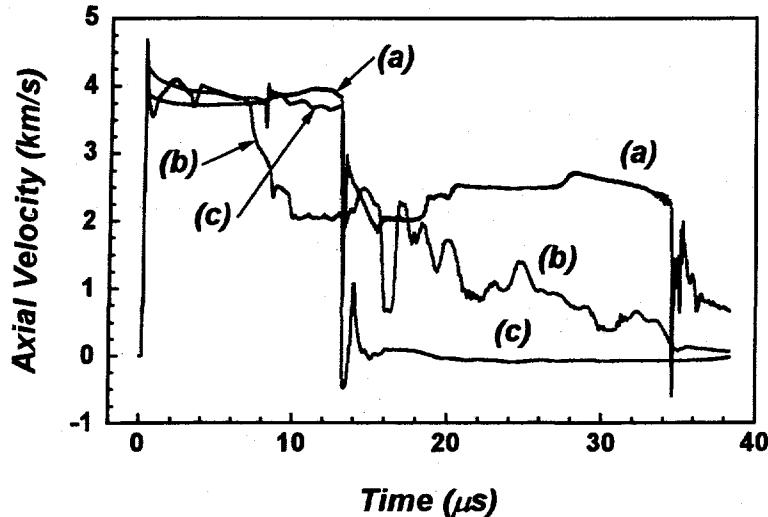
To provide more quantitative output we plot pressure and velocity histories for Lagrangian tracer particles embedded in the pipe wall and in the three partitions, using the long-pipe calculation. Figure 3.5 shows pressure traces for four points spaced along the length of the pipe wall. The locations are, respectively, midway between the first and second partition,



**Figure 3.5.** Calculated pressure histories for points along the wall of the long-pipe configuration. All points are for halfway through the wall thickness. Curve (a) is for the axial location midway between the front and middle partitions; (b) is adjacent to the middle partition; (c) is at the midpoint between the middle and rear partitions; and (d) is opposite the rear partition.

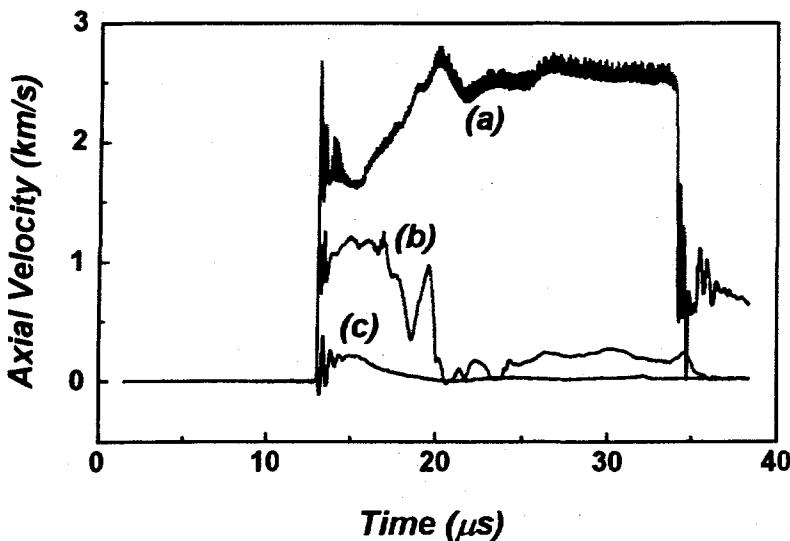
opposite the middle barrier, halfway between the middle and rear partitions, and finally, opposite the rear partition. All these points were at the midpoint in the wall thickness. The ringing in all the traces appears to be characteristic of the loading on the front barrier. The point halfway between the first two partitions exhibits a peak pressure of almost 5 kb, while between the second and third, the wall pressure is only a little over 1 kb. The traces opposite the barriers are interesting because they clearly indicate the debris impacts at 13 and 35  $\mu$ s, respectively. Both of these traces also show the initial pressure waves moving up the pipe wall, starting at times roughly half of those associated with the debris.

Next we plot, in Fig. 3.6, the velocity histories for the rear of the front partition. At early times these traces show uniformity across the diameter, and peak at  $\sim 4$  km/s. The on-axis trace drops to  $\sim 2.5$  km/s after penetrating the middle partition at about 13  $\mu$ s, and drops further, to  $\sim 1$  km/s or less, on impact with the rear barrier. The off-axis velocities show that after the initial



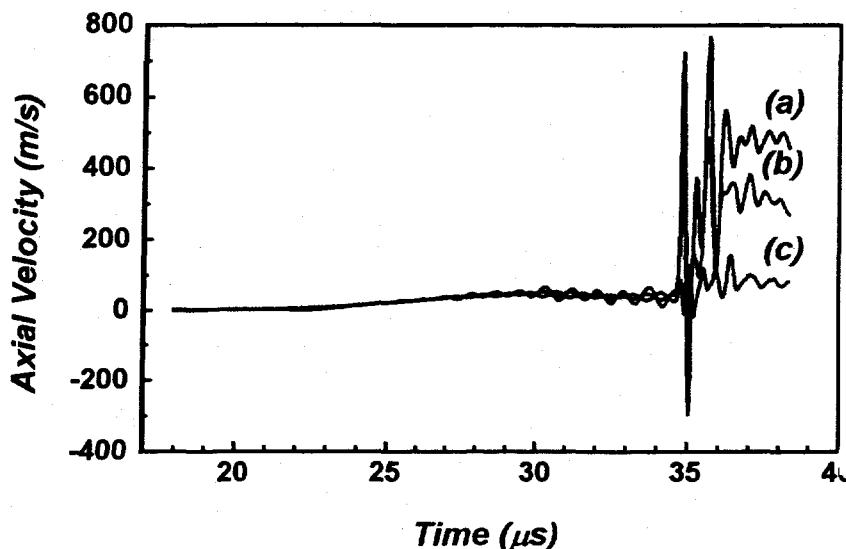
**Figure 3.6.** Calculated axial velocity histories for the rear of the front partition of the long pipe. Curve (a) is for the axis; (b) is for a radius of 0.15 cm; and (c) is for a radius of 0.30 cm.

interactions associated with the front partition, the debris motion becomes strongly peaked toward the axis, especially at later times. Similarly, the rear-surface velocities for the middle partition are plotted in Fig. 3.7. The most obvious feature is the velocity increase at 13  $\mu$ s from



**Figure 3.7.** Calculated axial velocity histories for the rear of the middle partition of the long-pipe configuration. Curve (a) is for the axial location; (b) is for a radius of 0.15 cm; and (c) is for a radius of 0.3 cm.

the impact of the front-barrier debris. In an analogous fashion the velocities drop when the middle-barrier debris hits the rear partition at 34  $\mu$ s. It is even more evident here that the debris velocities are strongly peaked toward the pipe axis. Finally, the velocities for the rear partition, as plotted in Fig. 3.8, show the effects of both the stress waves in the pipe wall and the debris. The small motions from the wall signals are evident between 20 and 25  $\mu$ s, well before the debris arrives, at  $\sim$ 34  $\mu$ s. The calculated rear-surface velocities of this partition are relatively low, with a maximum value a little over 0.7 km/s, but they are still strongly peaked toward the axis.



**Figure 3.8.**  
Calculated axial velocity histories for back of the long-tube rear partition. Curve (a) is for the on-axis position; (b) is for a radius of 0.15 cm; and (c) is for a 0.3-cm radius.

These calculations give particle velocities significantly higher than our measured VISAR records, but they are certainly qualitatively similar. Our best guess for the source of the discrepancy is that the total energy fluence incident on the target was probably less than we used in the calculations. It should be noted that the attenuated radiation input at the sample location was determined solely on geometric arguments. We hope that future diagnostics will give more direct results for the on-target radiation parameters, especially when complicated source configurations, like the slotted-can hohlraum, are employed.

#### IV. Results from Time-Resolved Diagnostics

##### *Long Tube*

Good-quality VISAR records were obtained for all channels except for one spot on the front partition; the records were unusably noisy for both VISARs for that spot. The results are shown in aggregate in Figure 4.1, and partition-by partition in Figure 4.2.

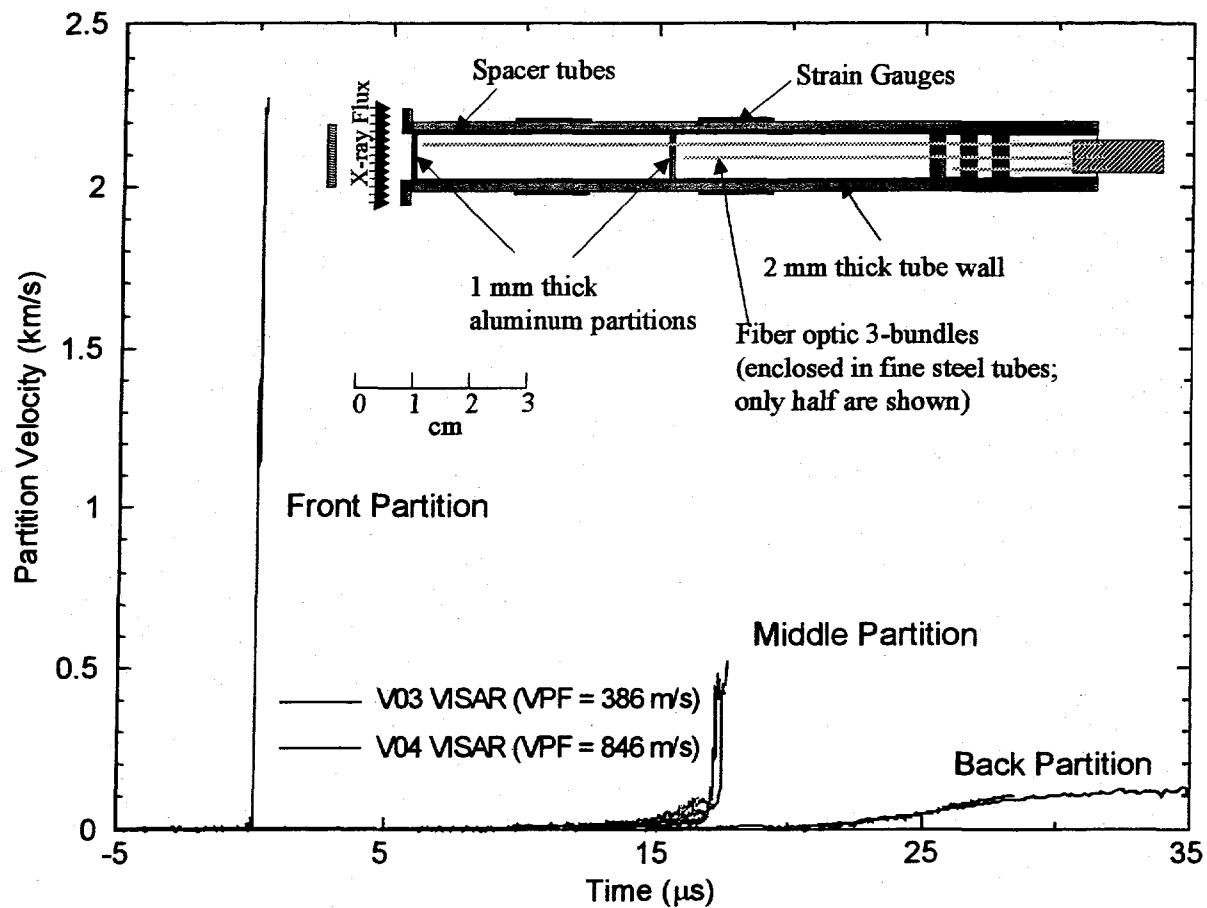


Figure 4.1. Aggregate of long-tube VISAR velocity histories

The front partition accelerates to a velocity of about 2.2 km/s; the middle, to 0.5 km/s, and the back, to about 120 m/s. Arrival times are presented in Table 4.1, and calculated partition velocities, in Table 4.2.

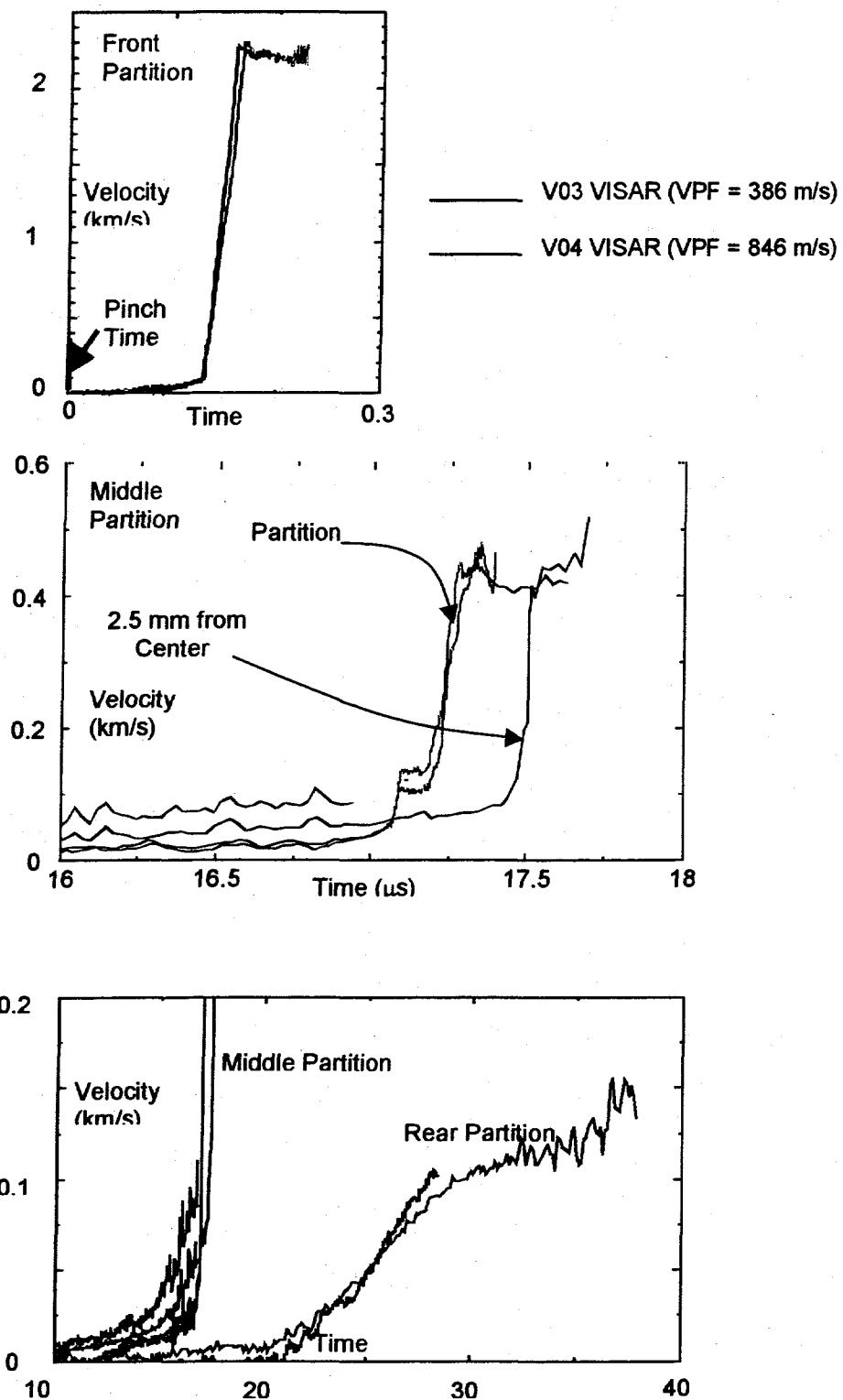


Figure 4.2. Detail plots of VISAR velocity histories for long-tube experiment. (Top) Front partition. (Middle) Middle partition. (Bottom) Middle and rear partitions. All times are relative to peak pinch. Velocities in km/s.

Table 4.1. Observed Arrivals – Short and Long Tubes (time in  $\mu$ s after peak pinch)

Partition ↓	Long Tube Experiment		Short Tube Experiment	
	Toe	Main Arrival	Toe	Main Arrival
Front	0.06	0.15	0.07	0.15
Middle	9.33 edge – 12.38 center	17.50 edge – 17.09 center	8.2	9.64 edge- 9.54 center
Rear	21.16	~25?	12.55	~20?

Table 4.2. Precursor and Plate Velocities (calculated from observed arrival times). All velocities are in km/s.

Interval ↓	Long Tube Experiment		Short Tube Experiment	
	Precursor	Plate	Precursor	Plate
Front - Middle	5.39	2.95 center 2.88 edge	3.07	2.66 center 2.63 edge
Middle - Back	4.23	6.3?	5.75	1.58

### ***Short Tube***

Good-quality VISAR records were obtained for all channels except for two channels on the middle partition. The VLVN-04 Data 2 record for the half-radius spot was lost when a digitizer plugin failed to trigger. As well, the VLVN-03 trace for the center spot was quite noisy, but usable. The results are shown in aggregate in Figure 4.3, and partition-by partition in Figure 4.4.

The front partition accelerates to a velocity of about 1.75 km/s; the middle, to 1 km/s, and the back, to about 100 m/s. Arrival times are presented in Table 4.1, and calculated partition velocities, in Table 4.2.

### ***Strain Gages***

The gages were overwhelmed by electrical noise, and so no usable data were recovered.

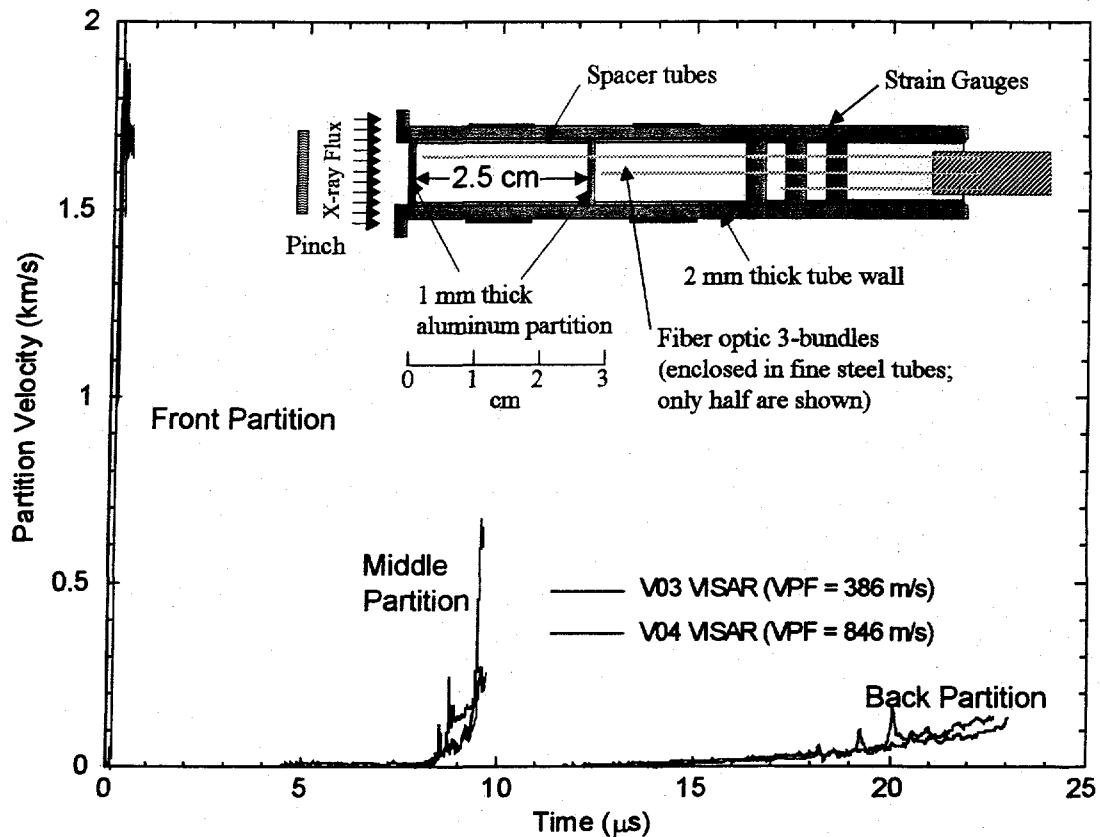


Figure 4.3. Aggregate of Short Tube VISAR velocity histories

### Discussion

In both experiments, the front partition was abruptly accelerated to  $\sim 2$  km/s. Loss of signal after a short period (less than 300 ns) is consistent with (1) a loss of reflectivity of the partition due to shock breakout, and (2) an expected impact of the surface on the fiber ends at about 250 ns after the start of surface motion. An apparent decrease in surface velocity of this partition is probably an artifact, caused by the change in direction required of light traversing the path from the sending fiber to the surface, and into a receiving fiber.

On the middle partition, the primary arrival appears to impact the center 10 – 40 ns earlier than the edge (short and long tubes, respectively). Modeling of the experiment using ALEGRA (previous section) predicts this as well, and suggests that the front partition does not

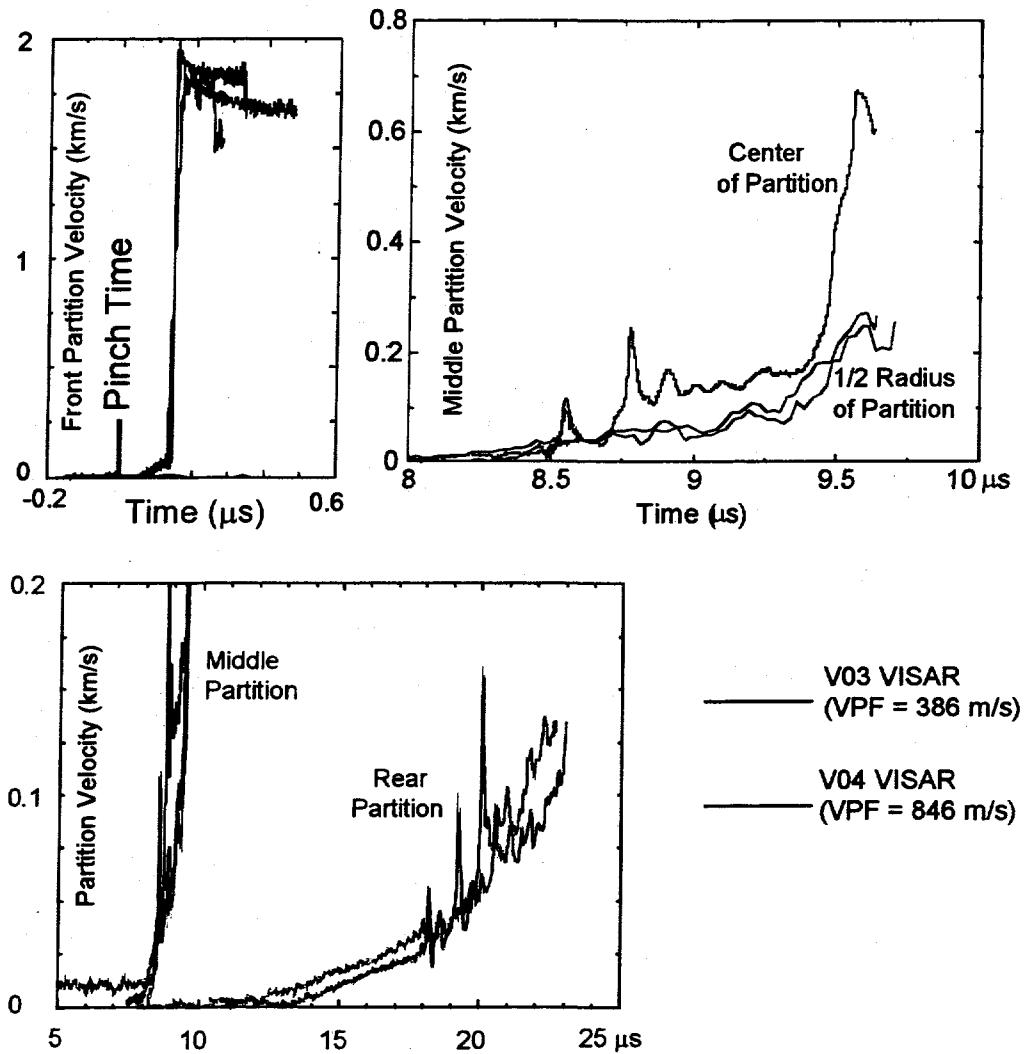


Figure 4.4. Detail plots of VISAR velocity histories for short-tube experiment. (Top Left) Front partition. (Top right) Middle partition. (Bottom) Middle and rear partitions. All times are relative to peak pinch.

travel as a disk, but as a debris pattern strongly focussed on the axis of the tube. The mean velocity of the main impacting mass along the first half of the tube length (2.9 km/s for the long tube and 2.4 km/s for the short tube) is slightly greater than the values suggested by VISAR measurements of the initial launch of the front partition (2.2 km/s for the long tube and 1.8 km/s

for the short tube).

It is difficult to identify a clean arrival for the back partition in either experiment. This is consistent with the arrival of a dispersed cloud of debris, melt, and/or vapor, and strongly suggests that the middle plate loses integrity in the course of the experiment, as also suggested by numerical simulations.

The toes of the waveforms carry additional information. For the long-tube experiment, they suggest a signal propagating along the walls of the pipe at ~5.4 km/s. This is consistent with the velocity of a low-amplitude shock propagating in aluminum. Results for the short tube experiment show more scatter.

## V. Results from Post-Event Analysis

### *Visual Examination / Metallography*

Both tubes were recovered after the respective experiments. The long tube remains integral. The short tube was sliced lengthwise by diamond saw and examined. Figure 5.1 shows photographs of one of the two halves.

It is clear that a combination of violent processes has occurred. Specific observations are:

- 1) No recognizable macroscopic fragments remain from the front and middle partitions. The edge portions of the rear partition are recognizable, although the central half is destroyed.
- 2) Some of the original steel tubing used to support the VISAR fibers is still present, although it is discolored as if by heat.
- 3) There is an abundance of bubbles in this metal, occasionally to the point of a spongy texture.
- 4) There are numerous translucent whitish spots on the remaining lengths of steel tubing.
- 5) There is an excoriated appearance to portions of the steel tubes and the walls.

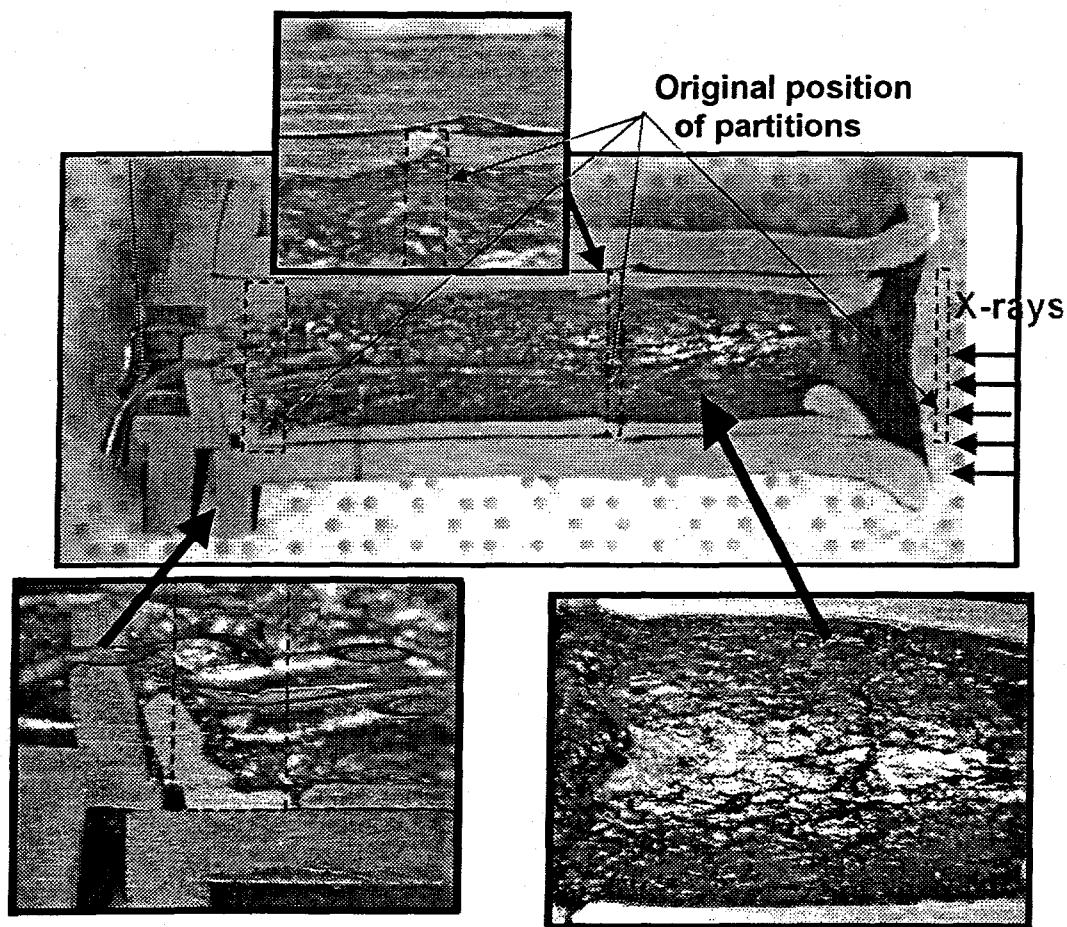


Figure 5.1. Post-test photographs of half of the short tube. Original positions of aluminum partitions are shown by dashed rectangles (displaced downward for clarity).

- 6) The material at the distal end of the tube is preferentially distributed toward the walls.
- 7) Additional material deposited on the inside of the tube assembly throughout the 30% distal from the pinch shows vesicles consistent with partial vaporization.
- 8) The metal on the inside of the pipe is definitely cooled from a melt. This is indicated by the texture.
- 9) The front of the main tube has been flared, and the front of the separator tubing inside the main tube has been folded back.

10) General structural deformation reflects large stresses transmitted through the tube. The liner is slightly separated from the outer wall of the pipe. The distal end of the tube has been noticeably strained.

Several interpretations may be advanced based on these observations:

- 1) The metal on the inside of the pipe is definitely cooled from a melt. This is indicated by the texture.
- 2) The front and middle partitions were pervasively melted, and at least the front of the front partition was vaporized.
- 3) Enough aluminum vapor was generated to form the majority of the bubbles.
- 4) Note that the barriers were nearly pure Al, while the tube structure was 6061-T6.
- 5) The whitish spots on the steel tubing may be oxidized aluminum [if an atmosphere was present], or may be artifacts of the process of bisecting the recovered structure.
- 6) The debris/vapor/liquid flow excoriated the outsides of the steel tubes and the inner wall of the pipe.

#### ***Microprobe/SEM Analysis***

The other half of the short tube was analyzed by scanning electron microscopy and microprobe for further information about tube/partition behavior during the experiment. Representative results are shown in Figure 5.2. "BSE" is backscattered electron imaging (utilizing low-energy electrons); this generally produced better contrast than did scanning electron microscope settings. Although numerous elemental images were taken (selecting x-ray energies characteristic of elements of interest to produce elemental maps), results from these will be summarized in text form in the present report.

Comments about specific sites follow (see letters on Fig. 5.2 images for locations):

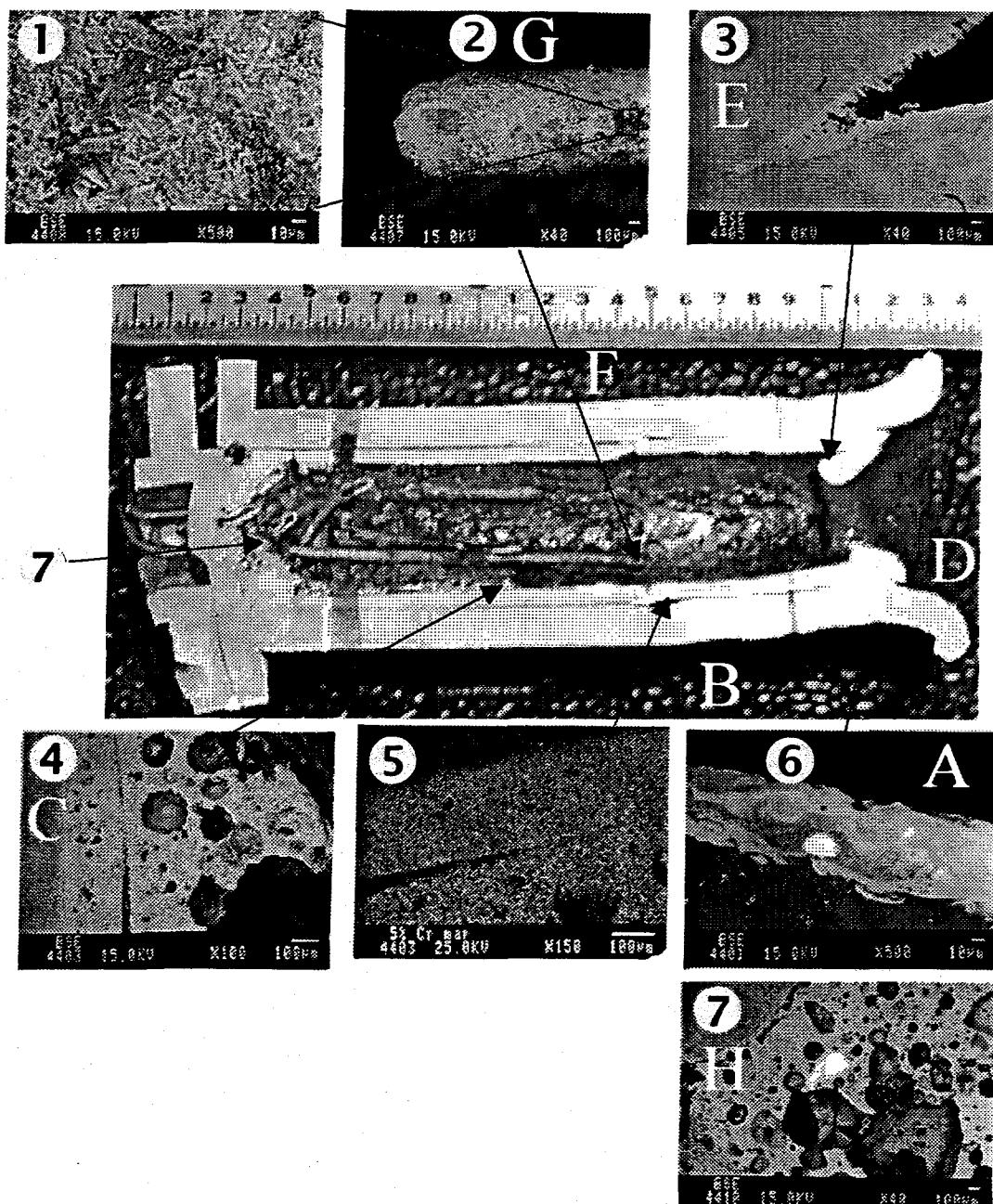


Figure 5.2. Representative microprobe (plate 3) and SEM (BSE) results from short tube experiment. Ruler on reference photo is in inches. Scale bars at lower right corners of (1) and (6) are 10 microns; others are 100 microns. Letters are to reference locations discussed in text.

A) (Outside of tube on front flare) Aluminum structure has "skin" 30 – 50 microns thick of turbulent mixed aluminum and stainless steel. Sample composition was 48% Al, 23% Fe, balance a mixture approximately that of stainless steel.

B) (Outside of tube about 25% of the way back) 2 layers of melt solidified. The basal layer is steel-rich; the outer is aluminum-rich. Turbulence of (A) is not observed.

C) (Inside tube, near base) Three distinct layers are observed above the aluminum substrate. The outer layer is coarsely vesicular, ranging to 600 – 700 microns in thickness (more locally), with exsolved intermetallic crystals of iron aluminides (with some Cr and Ni). These are likely to be Cr and Ni-bearing  $FeAl_3$ . The next, also iron-rich, appears to be a chill zone ~150 microns thick. Delamination is observed between these two layers. The deepest layer is ~35 - 40 microns thick, and appears to be a zone of diffusion of iron into the aluminum substrate.

D) (Outside of fold point on spacer tube; proximal to pinch) Note that some copper is present here, possibly from copper tape used to secure near-pinches wiring.

E) (Inside of fold on spacer tube; opposite side from (D).) Layered "coxcomb" texture.

F) (Outside of tube about 30% of the way back; opposite side from (B).) Weight percentages 20% Ni, 10 – 11% Cu, balance Al

G) (Eroded tip region of steel tubing from fiber optics) The white patches observed optically are alumina, and are several microns thick.

H) The region inside the tube at the distal end from the pinch contains an appreciable volume of

what appears to be an coarsely vessicular aluminum matrix saturated with ferrous metals.

These observations suggest the following inferences:

- 1) The outside of the tube, which shows thin layers of cryptocrystalline, turbulently mixed metal compositions, cooled rapidly after the initial flux of X-ray energy.
- 2) The middle of the structure, which contains a more homogenized elemental mixture with a porphyritic texture (isolated crystals in a cryptocrystalline matrix), remained hotter longer than the outside.
- 3) Aluminum was oxidized within the structure at the steel tubes to produce aluminum oxide. The source of oxygen, or the reduced material, is a mystery inasmuch as the test was conducted under vacuum. It seems unlikely that the aluminum oxide was introduced during the later cutting process. The possibility must be considered that air remained in the tube.

One of the potentially greatest benefits of the microprobe in this analysis, mapping the final locations of the partitions, could not be readily achieved because of the similarity between the 1100 Al composition of the partitions (pure Al) and the 6061-T6 composition of the tubes. The composition of 6061-T6 aluminum is shown in Table 5.1. In future tests it may be worth considering making partitions and pipe (or other vessel) of different elements to better allow such mapping.

Table 5.1. Composition of 6061-T6 Aluminum (from Matweb)

Component	Wt%	Component	Wt%	Component	Wt%
Si	0.4 – 0.8	Fe	Max. 0.7	Cu	0.15 – 0.4
Mn	Max. 0.15	Mg	0.8 – 1.2	Cr	0.04 – 0.35
Zn	Max. 0.25	Ti	Max. 0.15	Al	98

## VI. Conclusions

In these two experiments, several diagnostics have been used to observe debris flow in a tube subject to a strong cold x-ray fluence from a Z-pinch peaking at approximately 160 eV. Both velocity interferometry and post-test (metallurgical and microprobe) analysis suggest a violent flow pattern including loss of plate integrity and preferential rapid propagation along the center channel. The post-shot analysis also suggests the extensive melting and partial vaporization of the front and middle partitions occurred. This is dramatically different from the behavior expected for normal aluminum plate impacts at similar mean velocities (~2 – 2.5 km/s), where melting would not be expected.

It is extremely difficult to deploy strain gages in the Z environment due to the electromagnetic interference present during the experiment ( $10^{13} - 10^{14}$  amps adjacent to the gages, as well as large currents in many parts of the hibay)

In future experiments, it may be worthwhile to fabricate partitions and tubes (or other elements) from different elements so that microprobe mapping of final part distributions may be more easily done.

These experiments successfully combined the unique x-ray production aspects of the Z-facility with a much larger number of shock compression diagnostics than previously used in this environment. A worthwhile extension of this work will be to include the penetrating x-ray imagery expected from the Backlighter diagnostic in future experiments. This will provide real-time imagery of debris flow in pipes such as described here.

Numerical simulations qualitatively match the dynamic response of the configurations, but appear to overpredict the debris velocities. We feel that an overestimate of the total energy fluence on the sample is probably the source of the discrepancy. We anticipate that diagnostics will be improved on future experiments of this type.

### References

Matweb: Available on the World Wide Web at <http://www.matweb.com>; see under Material Type, 6000-series aluminum alloys. Essentially similar information available from Metals Handbook Vol.2 - Properties and Selection: Nonferrous Alloys and Special-Purpose Materials, ASM International 10th Ed. 1990.

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