

**Modifications of ORNL's Computer
Programs MSF-21 and VTE-21 for the
Evaluation and Rapid Optimization of
Multistage Flash and Vertical
Tube Evaporators**

P. Glueckstern
J. V. Wilson
S. A. Reed

OAK RIDGE NATIONAL LABORATORY

OPERATED BY UNION CARBIDE CORPORATION FOR THE ENERGY RESEARCH AND DEVELOPMENT ADMINISTRATION

MASTER

DISTRIBUTION OF THIS DOCUMENT IS UNLIMITED

27
1-14-76
25 up to NTIS

DISCLAIMER

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency Thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

DISCLAIMER

Portions of this document may be illegible in electronic image products. Images are produced from the best available original document.

Printed in the United States of America. Available from
National Technical Information Service
U.S. Department of Commerce
5285 Port Royal Road, Springfield, Virginia 22161
Price: Printed Copy \$5.50; Microfiche \$2.25

This report was prepared as an account of work sponsored by the United States Government. Neither the United States nor the Energy Research and Development Administration/United States Nuclear Regulatory Commission, nor any of their employees, nor any of their contractors, subcontractors, or their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness or usefulness of any information, apparatus, product or process disclosed, or represents that its use would not infringe privately owned rights.

OAK RIDGE NATIONAL LABORATORY

OPERATED BY
UNION CARBIDE CORPORATION
NUCLEAR DIVISION



POST OFFICE BOX X
OAK RIDGE, TENNESSEE 37830

June 15, 1976

Report No.: ORNL/TM-5230 Classification: Unclassified

Authors: Glueckstern, P., J. V. Wilson, S. A. Reed

Subject: Modifications of ORNL's Computer Programs MSF-21 and VTE-21
for the Evaluation and Rapid Optimization of Multistage
Flash and Vertical Tube Evaporators

Please correct the following errors in your copy(ies) of subject report.

Page 3, 5th line from bottom -- change HERC~~OV~~ to HREC~~OV~~.

Page 7, 14th line from bottom -- change with (LC~~ON~~) to width (LC~~ON~~).

Page 8, line 20 -- insert "The derivatives used in" before Newton's
method.

Page 8, line 21 -- change WEN~~OM~~ to WFN~~OM~~.

Page 61, second line with *** at right -- change X~~0~~(43)=8.D0 to
X~~0~~(43)=1.D0.

We apologize for your inconvenience.

A handwritten signature in dark ink, appearing to read "J. L. Langford". The signature is fluid and cursive, with a large, sweeping "L" and "f".

J. L. Langford
Laboratory Records Department
Information Division

Contract No. W-7405-eng-26

Reactor Division

MODIFICATIONS OF ORNL'S COMPUTER PROGRAMS MSF-21 AND VTE-21
FOR THE EVALUATION AND RAPID OPTIMIZATION OF MULTISTAGE
FLASH AND VERTICAL TUBE EVAPORATORS

P. Glueckstern
J. V. Wilson
S. A. Reed

JUNE 1976

NOTICE
This report was prepared as an account of work sponsored by the United States Government. Neither the United States nor the United States Energy Research and Development Administration, nor any of their employees, nor any of their contractors, subcontractors, or their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness or usefulness of any information, apparatus, product or process disclosed, or represents that its use would not infringe privately owned rights.

NOTICE: This document contains information of a preliminary nature and was prepared primarily for internal use at the Oak Ridge National Laboratory. It is subject to revision or correction and therefore does not represent a final report.

OAK RIDGE NATIONAL LABORATORY
Oak Ridge, Tennessee 37830
operated by
UNION CARBIDE CORPORATION
for the
ENERGY RESEARCH AND DEVELOPMENT ADMINISTRATION

DISTRIBUTION OF THIS DOCUMENT IS UNLIMITED

CONTENTS

	<u>Page</u>
ABSTRACT	v
1. INTRODUCTION	1
2. CONCEPTUAL DESIGN MODIFICATIONS	3
2.1 PLANT STRUCTURAL DESIGN	3
2.1.1 MSF Plants	3
2.1.2 VTE Plants	7
2.2 FEEDWATER PRETREATMENT SYSTEM	8
2.3 NONCONDENSABLE GAS REMOVAL SYSTEM	10
2.4 LISTING OF ADDITIONAL INPUT AND CALCULATED DESIGN VARIABLES	11
2.5 ADDITIONS TO GLOSSARY	12
3. COST UPDATING AND OTHER COSTING MODIFICATIONS	14
3.1 GENERAL	14
3.2 MODIFICATIONS AND UPDATING OF DIRECT CAPITAL COST COMPONENTS	14
3.3 MODIFICATIONS IN ESTIMATING INDIRECT CAPITAL COST COMPONENTS	21
3.4 MODIFICATIONS IN OPERATING COST COMPONENTS	22
3.5 MODIFICATIONS OF ANNUAL FIXED CHARGE RATE AND PLANT OPERATING FACTOR	23
APPENDICES	
A. Changes Made in Subroutine MAINM (MSF)	29
B. Changes Made in Subroutine MAINV (VTE)	31
C. Changes Made in Subroutine PLANTM (MSF)	33
D. Changes Made in Subroutine PLANTV (VTE)	39
E. Changes Made in Subroutine SIZEM (MSF)	45

F. Changes Made in Subroutine SIZEV (VTE)	51
G. Changes Made in Subroutine TECPAR	55
H. Changes Made in Subroutine OTHPAR	59
I. Changes Made in Subroutine PRICES	63
J. Changes Made in Subroutine COSTM (MSF)	71
K. Changes Made in Subroutine COSTV (VTE)	75
L. Changes Made in Subroutine FNANCE	79
M. Subroutine TITLER (New Subroutine)	81
N. Changes Made in Subroutine RITEM (MSF)	83
O. Changes Made in Subroutine RITEV (VTE)	91

ABSTRACT

Design and cost modifications were made to ORNL's Computer Programs MSF-21 and VTE-21 originally developed for the rapid calculation and design optimization of multistage flash (MSF) and multieffect vertical tube evaporator (VTE) desalination plants. The modifications include additional design options to make possible the evaluation of desalting plants based on current technology (the original programs were based on conceptual designs applying advanced and not yet proven technological developments and design features) and new materials and equipment costs updated to mid-1975.

1. INTRODUCTION

MSF-21 and VTE-21 are models of the multistage flash (MSF) and the vertical tube evaporator (VTE) processes developed at ORNL in the early 1970s for rapid calculation and design optimization of desalination plants. These programs were originally developed as subprograms of an overall system of programs termed ECON-21 consisting of six parts and documented under ORNL-TM-3535. MSF-21 is Part V and VTE-21 is Part VI of this set of documents.^{1,2}

MSF-21 and VTE-21 were not developed for the purpose of making detailed design computations and therefore apply various computational approximations for more rapid calculation and overall design optimization. Thus the design computations of MSF plants are based on the first and last stages of each section (recovery and reject) and a typical middle recovery section. As a result of this procedure the program runs rapidly but does not give stage by stage parameters.

The basic designs applied in these programs are ORNL's conceptual designs^{3,4} of advanced 250 Mgd MSF and VTE desalting plants, applying novel design features such as large train sizes of 62.5 Mgd, concrete evaporator shells, two-level brine flow (MSF), and very long tubing extending through half of all recovery section stages of the MSF plant.

Both programs comprise a number of subroutine which can be divided into four sections.

1. A main section (MAINM and MAINV for MSF and VTE respectively) where initialization is made, the structural units of the plant are defined, and all relevant other subroutines are called.
2. A design section comprising two subroutines, one for heat and mass balances (PLANTM and PLANTV for MSF and VTE respectively) and one for sizing of physical plant dimensions, equipment sizes, steam and electrical loads, and all other quantities which are necessary to compute the capital and product water costs (SIZEM and SIZEV for MSF and VTE respectively).

3. An economics section comprising three subroutines: (a) subroutine PRICES in which all unit equipment and materials costs for both the MSF and VTE are calculated, (b) subroutine FNANCE in which the overall economics parameters such as the fixed charge rate and the indirect capital cost component factors are calculated, and (c) a subroutine (COSTM and COSTV for MSF and VTE respectively) which finally calculates the capital and unit product water costs, based upon the values calculated in the two previous subroutines.
4. An output section, in which all output is printed.

The main purpose of the present modifications is twofold: to make possible the calculation and design optimization of desalting plants based on current technology and smaller sizes (rather than plants incorporating unproven design features) and to update the cost functions to the prices prevailing in mid-1975.

The design modifications made are mainly in the structural design and the design of the noncondensed gas removal (NCG) system and the feedwater pretreatment system. These modifications are described in Section 2, and the relevant changes in the Fortran statements of the programs are marked on the detailed listings given in Appendices A to H.

All costing modifications and updating are described in Section 3 and shown in the Fortran listing given in Appendices I to M. The changes made in the output subroutines are listed in Appendices N and O.

All notations used in this report are identical to those applied in the original programs documented in refs. 1 and 2. For ready understanding of the modifications described here, it is therefore necessary to read this report along with the original documents describing the programs MSF-21 and VTE-21.

2. CONCEPTUAL DESIGN MODIFICATIONS

2.1 PLANT STRUCTURAL DESIGN

2.1.1 MSF Plants

General — In MSF plants the evaporator shell and foundation cost is one of the two largest cost components, contributing about 30% of the total direct capital cost. This is, of course, a function of the plant dimensions which are determined by applying certain design criteria. In a long tube design, with a given tubing surface area (or performance ratio), the following factors affect the evaporator dimensions and total volume:

1. the maximum allowable mass flow per evaporator width ($\text{lb hr}^{-1} \text{ ft}^{-1}$),
2. tube velocity and tube diameter,
3. maximum length of tubing or number of water boxes, and
4. evaporator height determined by the freeboard between the tube bundle and the evaporator floor and the geometric shape of the tube bundle.

While the first two factors can be varied by applying appropriate input values in the MSF-21 code, the later two factors were fixed in accordance with the criteria applied in ORNL's 250 Mgd MSF conceptual design.

In order to make the computer program more applicable to current design practice as well as to plant sizes much smaller than the 250 Mgd conceptual design, additional design options have been added.

Tube Bundle Design and Height of Evaporator Shell

The height of the MSF shell of the recovery section (HERCØV) and the reject section (HREJCT) is calculated by the original MSF-21 program as the sum of built-in values for the height of the tube bundle above the evaporator floor and the calculated height of the tubesheet. The latter is calculated by adding 0.5 ft to the height of the tube bundle (HBNDLE).

HBNDLE was calculated by assuming an elliptical tube bundle having a width (WBUNDL) equal to the width of the product tray less 0.5 ft.

This procedure was modified to allow a design with a specified geometric shape of the tube bundle. The new procedure is as follows:

$$WBUNDL = (XT(126)*APTSE1)**.5 ,$$

where APTSE1 is the calculated tube bundle area and XT(126) an input value defining the ratio WBUNDL/HBNDLE. APTSE1 is calculated by:

$$APTSE1 = XT(127)*ARTUBE ,$$

where ARTUBE is the area required to place the tubes at a defined pitch and XT(127) an input value >1 for allowances of additional area for non-condensable gas removal openings or baffles.

As for the height of tube bundle above the evaporator floor, the built-in fixed value has been replaced by an input parameter XT(120) for the recovery section and XT(129) for the reject section.

For a design specifying a number of brine flow levels in the evaporator (LEV), the additional height for each additional flow level was specified by built-in values. These values were replaced by XT(121) and XT(125) for the recovery and reject section respectively.

MSF Evaporator Width — The outside width at the hot end (WHOT) and at the cold end (WCOLD) were originally calculated by adding built-in values for the thickness of the external and internal walls to the internal evaporator width, calculated according to the allowable brine flow per width of the brine tray. The built-in values which were adequate for only a concrete evaporator shell were replaced by the

following additional input parameters:

XT(122) = External wall thickness at the cold end of the evaporator, ft

XT(123) = Internal wall thickness, ft

XT(129) = Ratio of external wall thickness at the hot end to that at the cold end. This parameter is only applicable for a concrete evaporator shell.

Variation of Tube Length — This design variable affects the number of water boxes (and tube sheets) and, therefore, the total length of the evaporator, and consequently, the total pressure drop through the recovery stages (recycle brine) and the reject stages (makeup + reject flow). The maximum tube length is defined by a new input variable XT(200) and is applied to calculate the following:

- a. Number of tube bundles in recovery section (ENRSS). $ENRSS = ELE/XT(200) + 1$ (truncated to an integer), where ELE is the total length of the tubes in the recovery section.
- b. Total length (in ft) of recovery section (RECOLN). $RECOLN = ELE + (ENRSS-1)*9.667 + 20.0$.
- c. Required head of recycle pump. To the previous function calculating this value, the additional pressure drop $(ENRSS-1)*VHLR$ in the water boxes has been added; VHLR is the head loss per water box calculated by:
 $X\emptyset(204)*.0155*VE*VE$, where VE is the tube velocity and X $\emptyset$ (204) an input parameter defining the number of velocity head losses in each water box.

The same variations have been made also for the reject section. All of the relevant Fortran statements are included in subroutine SIZEM. A full listing of this subroutine, indicating the new statements by asterisks, is given in Appendix E.

Structural Units of the Plant — In the original MSF-21 code the main structural units are defined according to the following criteria:

1. Number of tube bundles (BNDLS): $BNDLS = FF/12.5 + .5$ (truncated to an integer), where FF is the desalting plant capacity in Mgd.
2. Number of modules (MODU): $MODU = 0.5*BNDLS$. This implies that each repetitive structural unit or module contains two tube bundles. Half-modules containing only one tube bundle are also allowed whenever the BNDLS is an odd number.
3. Number of trains (TRAINS). TRAINS is computed so that each train contains a maximum of 2-1/2 modules but must not be smaller than a certain minimum defined by an input value (XØ(43)). Each train has enclosing walls and a set of pumps, a brine heater, and a deaerator.
4. Number of buildings (BLDGS). A building is defined as a separate structure with its own external walls and contains two trains. (Whenever TRAINS is an odd number, one of the buildings contains only one train.)

In order to make the program more flexible and allow it to compute specified designs (such as, for example given, $BLDGS = TRAINS = MODU = BNDLS$), the following modifications were made in subroutine MAINM (Appendix A):

$$BNDLS = XØ(208)*XØ(43)$$

$$MODU = BNDLS/XØ(209)$$

$$TRAINS = XØ(43)$$

$$BLDGS = TRAINS/XØ(210)$$

By assigning appropriate values to the input parameters XØ(43), XØ(208), XØ(209) and XØ(210), a design having one bundle per module, one module per train, and one train per building can be specified. Half-modules and half-trains, however, cannot be specified. For a design of two trains per building and/or two modules per train, XØ(43) must be an even number. For a design of three trains per building and/or three modules

per train, $X\emptyset(43)$ must be a multiple of 3, and so on. Basically, the above modifications require that the user predefine the design layout of the main structural units, if a design other than that defined by $BNDLS = M\emptyset DU = TRAINS = BLDGS$ is desired.

2.1.2 VTE Plants

Structural Units of the Plant — VTE-21 defines the number of buildings, trains, and tube bundles similar to that defined in MSF-21. However, there is no definition of a module; but a train may contain, like a module in MSF-21, one or two tube bundles. The number of tube bundles is calculated as the nearest lower integer of $FF/62.5 + .5$.

In the modified VTE-21 program, BUNDLS, TRAINS and BLDGS are defined with the same set of input parameters as in MSF-21. The relevant Fortran statements in subroutine MAINV, shown in Appendix B, are marked by asterisks.

VTE-21 fits the VTE effects into a trapezoidal shell, in accordance with the proposed design layout defined in the 250 Mgd Conceptual Design.⁴ The total length of the plant is calculated by adding the final condenser shell with (LC $\emptyset$ N) to the calculated length of all VTE effects. The condenser tubes, calculated as a function of the heat load and the tubing parameters, are placed in the trapezoidal shell, containing the VTE effects, right after the last effect. If the width of the shell at the cold end is less than the calculated length of the condenser, the shell width at the cold end is enlarged accordingly. This layout, quite appropriate for large capacity trains, is not suitable for small capacity plants, or even for large plants composed of trains having 12.5 Mgd capacity. It was modified to contain a multiple-pass condenser having a length equal to the required width of the last VTE effect. This design will require a two-pass horizontal condenser for train sizes of 10 Mgd, or larger, and a three-pass horizontal or vertical condenser for train sizes smaller than 10 Mgd. The relevant new Fortran statements included in subroutine SIZEV are shown in Appendix F.

Preheater Design — The modifications concerning tube length, tube bundle design, and height of the preheater, identical to those made in the MSF-21 code, were also made in the MSF preheater section of the VTE-21 code. These modifications are included in subroutine SIZEV listed in Appendix F.

Change in Design Parameters — For parametric studies it is desirable to be able to specify the maximum brine concentration and the condenser temperature as part of the input data. VTE-21 was originally written to use heat rate and feed rate factors (QEFAC and FDFAC respectively) rather than the quantities above, so as to avoid certain iterative calculations. The program has now been modified so that the desired values of maximum brine concentration and of condenser temperature are the input parameters XT(151) and XT(152). Subroutine PLANTV has been modified so that FDFAC and QEFAC are changed iteratively until the desired values of condenser temperature and maximum concentration are obtained. This thwarts the original intent to make the program run rapidly. In both cases Newton's method is used, and satisfactory convergence is normally achieved in fewer than six iterations. The modifications are included in subroutine PLANTV listed in Appendix D. Newton's method came from differentiating the equations defining QNØM and QESP in the case of QEFAC; and WFX and WENØM in the case of FDFAC.

2.2 FEEDWATER PRETREATMENT SYSTEM

The computer programs MSF-21 and VTE-21 considered the consumption of the following chemicals:

- a. sulfuric acid (93% H_2SO_4)
- b. caustic (NaOH)
- c. antifoam
- d. chlorine

The equipment cost of the sulfuric acid system is calculated (in subroutine PRICES) as a function of the daily consumption, which in turn is calculated as a function of the plant capacity, concentration ratio and

total seawater salinity in subroutines SIZEM (MSF-21) and SIZEV (VTE-21). The equipment cost for the injection of the other chemicals is calculated as a function of the plant capacity, only.

The consumption of chemicals other than sulfuric acid is not calculated directly, but the annual cost for these chemicals is evaluated by using several input parameters, defining the specific cost per unit of water treated (see Section 3.4).

In the modified programs, the same systems are used for acid treated plant designs. The only exception is the addition of sodium sulfite for scavenging residual oxygen. It was assumed that this chemical will be injected by the antifoam injection pumps.

In order to make it possible to evaluate nonacid (polyphosphate or other additives) treated plants, the following modifications were made:

1. A selector switch NFEED has been incorporated. If NFEED = 1, acid treated plants are evaluated. If NFEED = 2, a threshold pretreatment system is evaluated.
2. An input parameter XO(207) defining the specific consumption of polyphosphates (or other additives) has been added.

For NFEED = 2, the daily consumption of polyphosphate is calculated by:

$$TNACDY = 12 \times 10^{-9} \times XO(207) \times (WP + WB) ,$$

where

TNACDY = daily consumption of polyphosphate or acid (if NFEED = 1),
tons/day

XO(207) = specific consumption of polyphosphate, ppm

WP = product water flow rate, lb/hr

WB = blowdown flow rate, lb/hr

The relevant Fortran statements in subroutine SIZEM and SIZEV are indicated in Appendices E and F respectively.

2.3 NONCONDENSABLE GAS (NCG) REMOVAL SYSTEM

The original computer programs determined the energy consumption of the deaerator steam-ejector system applied in the 250 Mgd conceptual designs with the aid of an empirical curve. This curve was fitted to express the mechanical power required to pump the off-gas from acid treated seawater, saturated with air, from the deaerator vacuum to atmospheric pressure. This calculated mechanical power was then added to the pumping power consumption of the desalting plant used to calculate the cost of electrical power consumption.

In the modified programs the equivalent electric power consumption was replaced by the actual motive steam consumption of a two-stage steam-jet air ejector operated by saturated steam at a pressure of 100 psig.

For a specified ejector operation at a given suction pressure, the ejector steam consumption was assumed to be proportional to the total NCG load, which is calculated as a function of the following three parameters:

- a. NCG concentration (ppm) in the makeup stream entering the deaerator,
- b. total makeup flow rate, and
- c. air inleakage into all vessels held under vacuum (deaerator and part of the evaporator stages or effects.)

The total makeup flow rate is calculated for each case as a function of the blowdown concentration ratio and, for the other two parameters, input values are applied.

Different input parameters were allocated for the acid and the threshold (i.e. polyphosphate or other additive) systems. For each of them, one variable defines the air inleakage (lb/hr) per evaporator train and a second variable defines the NCG concentration in the makeup water.

The plants applying threshold pretreatment obviously have a larger sea water makeup and a considerable larger amount of CO_2 will therefore be released in the evaporator.

The NCG load and the steam consumption is now calculated in subroutines SIZEM (MSF) and SIZEV (VTE) by the following equations:

for acid treated plant (NFEED = 1) —

$$XO(205) = XO(200)*TRAINS + XO(201)*(WP + WB) , \text{ and}$$

for threshold pretreatment (NFEED = 2) —

$$XO(205) = XO(202)*TRAINS*XO(203)*(WP + WB) ,$$

where

$XO(205)$ = total NCG load, lb/hr

$XO(200)$ = inleakage per train, lb/hr (in acid treated plants)

$XO(202)$ = same as $XO(200)$, but for threshold pretreatment

$XO(201)$ = NCG concentration in makeup of acid treated plants, ppm

$XO(203)$ = same as $XO(201)$, but for threshold pretreatment

WP = total product water flow rate, lb/hr

WB = total blowdown flow rate, lb/hr.

The total steam consumption is calculated by:

$$XO(206) = 9.6 \times 10^{-3} XO(205) \quad [10^6 \text{ Btu/hr}] .$$

2.4 LISTING OF ADDITIONAL INPUT AND CALCULATED DESIGN VARIABLES

$XO(200)$ = Air inleakage per evaporator train — acid treated plants,
lb/hr

$XO(201)$ = NCG concentration in makeup of acid treated plants, ppm

$XO(202)$ = Air inleakage per evaporator train — nonphosphate treated
plants, lb/hr

X0(203) = NCG concentration in makeup of phosphate treated plants, ppm
X0(204) = Number of velocity head losses per water box
X0(205) = Total calculated NCG load, lb/hr
X0(206) = Total calculated ejector steam consumption, 10^6 Btu/hr
X0(207) = Specific consumption of polyphosphates (or other additives),
ppm in makeup
X0(208) = Number of tube bundles per evaporator train
X0(209) = Number of tube bundles per evaporator module
X0(210) = Number of evaporator trains per building
XT(120) = Height of recovery stages tube bundles above the evaporator
floor, ft
XT(121) = Additional height of recovery stages for each additional brine
flow level (LEV > 1), ft
XT(122) = External wall thickness at the cold end of the evaporator, ft
XT(123) = Internal wall thickness, ft
XT(124) = Ratio of external wall thickness at the hot end to that at
the cold end (only applicable for concrete shells)
XT(125) = Additional height of reject stages for each additional brine
flow level (LEV > 1), ft
XT(126) = Ratio of tube bundle width to height
XT(127) = Ratio of total tube sheet area to area calculated to contain
tubes only
XT(200) = Maximum length of MSF tubing, ft

2.5 ADDITIONS TO GLOSSARY

A glossary of Fortran variables added to program MSF-21 or VTE-21 by the changes described above is given here.

APTSH = Tube sheet area of brine heater, ft^2

CØNPAS = Number of flow passes in final condenser

ENRJS = Number of applied tube lengths in reject stages

ENRSS = Number of applied tube lengths in recovery or preheater stages

ENRSSH = Number of applied tube lengths in hot section of recovery stages (concrete design only)

LPHE = Total length of preheater tubing, ft

NFEED = Selector switch defining pretreatment method

NFHS = ENRSS

NRJS = ENRJS

NRSS = ENRSS

NRSSH = ENRSSH

VHLR = Calculated head loss in recovery water box, psi

VHLRJ = Calculated head loss in reject water box, psi

VHLRS = Calculated head loss in preheater water box, psi

3. COST UPDATING AND OTHER COSTING MODIFICATIONS

3.1 GENERAL

All cost functions originally applied in the MSF-21 and VTE-21 computer programs were based on 1967 prices and, as already discussed, on the technology of large and advanced 250 Mgd conceptual designs. These functions were partially replaced by other cost functions and/or updated to mid-1975 prices by applying escalators based on commonly used cost indices. Indices published by the Bureau of Reclamation, *Chemical Engineering*, and the *Engineering News-Record* were applied for various equipment components detailed in the next subsection. For energy and operating materials costs, the computer programs have input variables so that any price levels can be applied. However, since some additional energy and materials consumptions were incorporated in the design modification, several new cost functions had to be added. All modified cost functions included in subroutines PRICES, COSTM and COSTV (Appendices I, J, and K) are marked by an asterisk, and all applied escalators are summarized in Table 1. All modified and new cost factors are also defined in a new subroutine (subroutine TITLER given in Appendix M).

3.2 MODIFICATIONS AND UPDATING OF DIRECT CAPITAL COST COMPONENTS

The following direct capital components are evaluated in the MSF-21 and VTE-21 computer programs:

- (1) Condensing Surface
- (2) Evaporator Shell and Foundation
- (3) Brine Heater
- (4) Final Condenser (VTE only)
- (5) Valves and Piping
- (6) Seawater Intake and Outfall
- (7) Pumps and Motors
- (8) Instrumentation
- (9) Electrical Equipment
- (10) Chemical Plant Equipment (Chemicals Injection Systems)

Table 1. Summary of escalators used for direct capital cost updating to mid-1975 prices

	XC multiplier	Escalator	Reference index or other basis
I. Unit costs common to MSF and VTE			
Steel shell, \$/ft ²	9	1.988	CE + 25%
Excavation, \$/ft ³	11	1.880	BuRec
Demisters, \$/ft ²	12	1.760	Quotations (40%) + ENR skilled labor (60%)
Weirs, \$/ft ²	13	3.180	CE + 100%
Pump motors, \$/hp	16	1.681	CE
Auxiliary pumps and drivers, \$/Mgd	17	1.912	CE
Submarine line, \$/gpm	20	1.850	BuRec
Valves, \$/gpm	23	1.912	CE
Plant piping and fittings, \$/Mgd	24	1.912	CE
Train piping and fittings, \$/Train	25	1.912	CE
Brine heater piping and fittings, \$/gpm	26	1.912	CE
Vent piping and fittings, \$/gpm	27	1.912	CE
Brine heater (BH) shell, \$/ft ²	40	1.988	CE + 25%
BH tube sheets, \$	215	1.590	CE (labor + materials)
BH tube sheet hole drilling, \$/hole	216	1.460	CE (erection + instal. labor)
BH tube sheet installation, \$/ft ²	217	2.000	ENR (skilled labor)
BH tubing installation, \$/ft	218	2.000	ENR (skilled labor)
BH tube rolling, \$/hole	219	1.460	CE (erection + instal. labor)
MSF tube sheets, \$/ft ²	3	1.590	CE (labor + materials)
Hole drilling, \$/hole	4	1.460	CE (erection + instal. labor)
Installing MSF tube sheets, \$/ft ²	5	2.000	ENR (skilled labor)
Installing MSF tubing, \$/ft	6	2.000	ENR (skilled labor)
Rolling MSF tubing, \$/tube	7	1.460	CE (erection + instal. labor)
II. Unit costs common to MSF only			
Pumps, \$/gpm	15	1.880	CE
Pump pits, \$/gpm	18	1.900	BuRec
III. Unit costs common to VTE only			
VE tube sheets, \$/ft ²	64	1.590	CE
VE hole drilling + rolling, \$/hole	65	1.460	CE
Installing VE tubes, \$/tube	66	2.000	ENR
VE bundle installation, \$/bundle	67	2.000	ENR
Installing preheater tubing, \$/ft	69	2.000	ENR
Horizontal tube sheets, \$/ft ²	70	1.590	CE
Hole drilling, \$/hole	71	1.460	CE
Installing horizontal tube sheets, \$/ft ²	72	2.000	ENR
Rolling horizontal tubes, \$/tube	73	1.460	CE
Pumps, \$/gpm	128	1.880	CE
Pump pits, \$/gpm	130	1.900	BuRec
Effect piping, \$/effect	132	1.912	CE

- (11) Noncondensable Gas (NCG) Removal Systems
- (12) Site Preparation, Including Buildings and Cranes.

The cost updating and/or modifications made for the above listed direct capital cost components were as follows:

1. Condensing Surface

The cost of this component was composed of tubing surface material cost, which is evaluated as a function of tubing size and material, tube bundle fabrication and installation costs based on cost functions for:

- (a) tube sheet material and fabrication,
- (b) hole drilling and tube rolling,
- (c) tube sheet installation, and
- (d) installation of tubing.

The cost functions for uninstalled tubing surface material were deleted; and, presently, the program applies input values expressing these surface costs in $\$/\text{ft}^2$ for every defined tubing surface.

For VTE an additional cost for tube nozzles has been added. The built-in cost is \$2 per nozzle. This cost can be varied by the XC cost multiplier XC(220).

The tube bundle fabrication and installation cost functions were updated to mid-1975 costs by applying the following escalators:

- (a) Tube sheet fabrication — *Chemical Engineering* (CE) Index for erection and installation labor.
- (b) Hole drilling and tube rolling — same as (a).
- (c) Tube sheet installation — *Engineering News-Record* (ENR) Index for skilled labor.
- (d) Tube installation — same as (c).

The basic difference between the CE and the ENR index computation method is that CE assumes gradual increase in productivity, and the resulting indices are therefore substantially lower than the ENR indices. Therefore, CE indices were applied only for work performed with the aid of machinery while ENR indices were applied for work where machinery is unlikely to be applied.

2. Evaporator Shell and Foundation

The following were included in calculating the capital cost of these items:

- (a) all steel parts of the evaporator shell including brine and product trays, and a phenolic coating of internal steel areas,
- (b) excavation proportional to the evaporator floor area,
- (c) demisters and miscellaneous small shell items,
- (d) brine flow weirs.

Each of the above components could be updated by applying escalators. For the steel work the CE index for buildings (materials and labor) was selected. The change from 1967 to mid-1975 of this index amounted to approximately 59%. This escalator would be suitable for the same design criteria applied in the original programs. However, as the phenolic coating was partially replaced by stainless steel (brine chambers) and copper-nickel (water boxes) linings, and the product trays were also assumed to be made of stainless steel, an additional cost increase factor had to be applied.

The effect of replacing only the phenolic coating was found to increase the cost of the steel work for a 12.5 Mgd size evaporator by about 15 to 20%. The escalator for the steel work was therefore increased by an additional 25%.

The cost escalator for the demisters was based on recently obtained quotations for stainless steel demisters and the ENR escalator for skilled labor.

The escalator for excavation was based on the index published by the Bureau of Reclamation.

The cost of the brine flow weirs was escalated according to the CE index for the steel work plus an additional 100% for replacing the phenolic coated steel by stainless steel.

3. Brine Heater

The brine heater cost was calculated by adding the cost of the shell and the cost of the installed heat transfer surface. The latter was estimated to be 143% of the tubing material cost. This estimate has been replaced by incorporating the cost functions applied for evaporator tube bundle fabrication and installation. The same escalators applied for the evaporator (condensing surface and shell cost) were also applied for the brine heater.

4. Final Condenser (VTE)

The appropriate shell cost and condensing surface cost applied for the evaporator were also used for the final condenser.

5. Valves and Piping

The CE index for pipe, valves, and fittings was applied for escalating the cost of this item.

6. Seawater Intake and Outfall

The Bureau of Reclamation's index for concrete pipelines was used to escalate this item.

7. Pumps and Motors

The CE indices for pumps and compressors and for electrical equipment and materials were used to escalate the cost of the pumps and the motors. The cost of pump pits was escalated by the Bureau of Reclamation's index for structures of pumping plants.

8. Instrumentation

The original programs applied the following cost function for the desalting plant unit instrumentation cost (UCI) in \$/gpd.

$$UCI(ff) = [2.29625 - 2.28269 \cdot \exp(-.0076527 \cdot FF)] / FF ,$$

where FF is the desalting plant capacity in Mgd.

Using this function and applying CE's index for process instrumentation, the cost for a 100-Mgd plant is calculated to be approximately $\$2.4 \times 10^6$, and for a 10-Mgd plant approximately \$285,000.

This function did not take into account the subdivision of the plant into several independently operating trains. Obviously, this, as well as the degree of automation incorporated, should be considered. For the time being, until a better cost function is obtained, UCI was replaced by:

$$UCI(FF, TRAINS) = 400,000 (FF/TRAINS/10)^{0.3174} \cdot TRAINS/FF .$$

For VTE plants an additional cost [set by the input variable XC(221)] proportional to the number of effects has been included.

9. Electrical Equipment

The original function was found to yield too low a cost for small units and was therefore replaced by a new function based on \$100/kW for a four-train plant with a total electrical power capacity of 40 MW. It has been assumed that 75% of this cost will be affected

by the number of trains. As with the original function, a scale factor of 0.8 has been applied. The resulting function is

$$\text{UCED}(\text{PMW}, \text{TRAINS}) = [7.5 \times 10^5 \times (\text{PW}/\text{TRAINS}/10)^{0.8} + 10^6 \times (\text{PMW}/40)^{0.8}] / \text{PMW} ,$$

where

UCEDK = the cost in \$/MW, and

PMW = electrical power capacity in MW .

The bases for this function were the escalated cost for the 250 Mgd VTE conceptual design⁴ and the escalated cost for the 2.5 Mgd Universal Design.⁵

10. Chemical Plant Equipment

The cost functions for acid and caustic dispensing systems, as well as all other treatment systems originally applied in the programs, were escalated by using the CE index for chemical plant costs. Some of these functions were rearranged to modify some reference values, but without changing the originally applied scale factors.

11. NCG Removal System

This system is composed of the deaerator, the decarbonator, and the steam-jet air ejectors. Since the design of this system has been basically modified (see Section 2.3), new cost functions had to be applied. The bases for the deaerator and decarbonator were the costs applied in the 2.5 Mgd Universal Design⁵ escalated to mid-1975 prices by applying the CE index for chemical plants.

The costs for the deaerator and decarbonator were correlated with the feedwater flow by applying a scale factor of 0.7.

The basis for the steam-jet air ejectors was Union Carbide cost data correlated to the NCG load.

12. Site Preparations, Buildings, and Cranes

The original programs correlated the costs of this component to \$/acre for site preparation and total plant capacity for buildings and cranes. The resulting figures obtained with these functions escalated with the ENR Building Cost Index seemed much too low in comparison with current estimates. These costs were therefore modified by using only the original site preparation cost function plus a general function for site development, including buildings, presented in the OSW Desalting Handbook for Planners.⁶ The assumption has been made that the cost for site development given by the Office of Saline Water (OSW) did not include an allowance for site preparation. Therefore the original site preparation function, suitably escalated, is used in conjunction with the OSW estimate to obtain the total site cost.

3.3 MODIFICATIONS IN ESTIMATING INDIRECT CAPITAL COST COMPONENTS

All indirect capital cost components are evaluated in Subroutine FNANCE (Appendix L). Originally the following components were evaluated:

- (1) overhead for design and supervision,
- (2) interest during construction,
- (3) owners cost for training and startup,
- (4) unusual construction cost, and
- (5) contingency.

In the modified subroutine FNANCE, the first three indirect capital cost components were not changed, but the "unusual construction costs" were assumed to be included in contingency. The current built-in factor for contingency is 25% but can be varied to any desired value by the input multiplication factor XC(62). A new factor expressing escalation during construction has been added to the original indirect cost component.

The calculation of the factor was based on similar assumptions to those made for estimating interest during construction. The built-in value for annual escalation rate is 8%. This rate can be changed by inserting any desired multiplication factor to the input variable XC(56).

3.4 MODIFICATIONS IN OPERATING COST COMPONENTS

The following components were included in the costing subroutines PRICES, COSTM, and COSTV:

- (1) process heat cost,
- (2) operation and maintenance labor cost,
- (3) cost of chemicals,
- (4) electrical power cost, and
- (5) cost of supplies and maintenance materials.

As already mentioned in Section 2.3, the energy consumption for the removal of noncondensable gases was expressed as equivalent electrical power consumption and was therefore included in the power cost. Currently, the heat consumption of steam-jet air ejectors is evaluated as a separate cost component as a function of the actual heat consumption, and the specified unit heat cost (appropriate to the thermodynamic parameters of the applied ejector steam) in the new input variable XC(210).

The modifications to the originally computed operating cost components included the following:

1. Process Heat Costs

Originally, these costs were evaluated by use of two allocated costs, one for nuclear and one for conventional plants. Currently, the unit heat costs are calculated as a function of the process steam temperature. This function was derived by using current costs for a 1000 MW(e) dual-purpose pressurized water reactor and fuel cycle costs based on WASH-1174, UC-2.

2. Operation and Maintenance Labor Cost

This component was modified based on the following assumptions:

- (a) A 100-Mgd plant will require a total O&M staff of 56 (38 operational and 18 maintenance).
- (b) The average man-year cost = \$16,000.
- (c) The total overhead for general and administration = 40%.
- (d) The scale factor for total O&M cost = 0.5.

3. Cost of Chemicals

The costs for consumption of chemicals were modified on the basis of the current unit costs and the specific consumptions listed in Table 2.

3.5 MODIFICATION OF ANNUAL FIXED CHARGE RATE AND PLANT OPERATING FACTOR

The cost functions used to evaluate the annual fixed charge rate are included in Subroutine FNANCE. The built-in values used in this function and the value of the plant operating factor were modified. The current built-in values are listed in Table 3.

Table 2. Summary of original and new input values used for the evaluation of operating costs

Operating cost component	XC multiplier	Built-in value	Remarks
I. Energy cost			
Nuclear process heat cost, $\$/10^6$ Btu	45	-	New function
Fossil plant process heat cost, $\$/10^6$ Btu	46	-	Function not available
Ejector heat cost, $\$/10^6$ Btu	210	0.70	For 100 psig nuclear steam
Nuclear electrical power cost, $\$/kWhr$	54	0.020	
Fossil plant electrical power cost, $\$/kWhr$	55	0.025	
II. Operation and maintenance labor	57	-	New function
III. Supplies and maintenance materials	58	0.007	Proportional to total capital cost
IV. Unit costs of chemicals			
Sulfuric acid (93% H_2SO_4), $\$/ton$	48	31.0	Consumption evaluated
Chlorine, $\$/lb$ seawater intake	50	2.64×10^{-7}	Based on 3 ppm and $\$176/ton$
Caustic + sodium sulfite, $\$/lb$ makeup water	51	8.5×10^{-7}	Based on 10 ppm caustic at $\$170/ton$ + 2 ppm sulfite at $\$305/ton$
Antifoam, $\$/lb$ makeup	52	7.05×10^{-7}	Based on 0.5 ppm at $\$1600/ton$
Polyphosphate (or equivalent), $\$/ton$	48	3000	Only for NFEED = 2

Table 3. Input variables for plant operating factor
and evaluation of annual fixed charge rate

	X0 value or XC multiplier	Built-in value
I. Plant operating factor, %	X0(38)	0.85
II. Fixed charge rate components:		
Interest rate	XC(60)	0.10
Taxes + insurances	XC(61)	0.01
Desalting plant life, years	X0(33)	30.0

REFERENCES

1. W. G. S. Fort, *Computer Codes for Office of Saline Water Program Analysis. Part V: MSF-21: A Fortran Code for the Rapid Calculation or Optimization of Multistage Flash (MSF) Desalination Plants*, ORNL-TM-3535 (February 1972).
2. W. G. S. Fort, J. V. Wilson, *Ibid.*, Part VI: *A Fortran Code for the Rapid Calculation or Optimization of Vertical Tube Evaporator (VTE) Desalination Plants*.
3. S. J. Senatore, J. A. Smith, *Study of 250-Mgd Multistage Flash Distillation Plant with Two Level Brine Flow, Part One; Part Two: Bechtel Corp., Preliminary Engineering Analysis and Capital Cost Estimate*, ORNL-4214 (Jan. 1969).
4. E. C. Hise, S. A. Thompson, *Conceptual Design Study of a 250-Million Gallons per Day Combined Vertical Tube - Flash Evaporator Desalination Plant*, ORNL 4260 (August 1968).
5. Burns and Roe, Inc., "Universal Design, Vol. I, Report on Design of a 2.5 Million Gallon Per Day Universal Desalting Plant," for Office of Saline Water, June 1969.
6. *Desalting Handbook for Planners*, U.S. Department of the Interior Office of Saline Water and the Bureau of Reclamation. 1st Ed. May 1972.

APPENDICES

THIS PAGE
WAS INTENTIONALLY
LEFT BLANK

APPENDIX A

CHANGES MADE IN SUBROUTINE MAINM

	SUBROUTINE MAINM(FFF,IOPT,IOUT,CH20,CAPITL)	PR 15580
	IMPLICIT REAL*8(A-H,U-Z)	PR 15590
C		PR 15600
	DOUBLE PRECISION MODU	PR 15610
	DOUBLE PRECISION LEV,LF2	PR 15620
C		PR 15630
	COMMON/BLOC2/ P, Q, AH, AK, AN,PR	PR 15640
1	AR, FF, GE, GH, GR, HD,PR	PR 15650
2	PB, PE, QX(5), RP, SE, SH,PR	PR 15660
3	SR, TK, VE, VH, VR, WC,PR	PR 15670
4	AME, ATN, BPX(5), CCF, HIH, HLH,PR	PR 15680
5	HNH, HOH, OMX(5), PHE, PO3, RSE,PR	PR 15690
6	RSH, RSR, TC1, THF, TKX(5), TMC,PR	PR 15700
7	TME, TPE, UEX(5), UME, UMH, WPL,PR	PR 15710
8	BKTE, BKTH, BKTR, DTLS(5), ELEX(5), HLEX(5),PR	PR 15720
9	HUOX(5), MODU, ROE1, ROE2, APTSE, BDEPH,PR	PR 15730
+	CAPIL, HEADE, HEADH, HEADR, POBLD, PODEL,PR	PR 15740
A	POPRD, SUBEX(5), WCGLD, WMODC, WMODH, BHSHEL,PR	PR 15750
B	CSLTBH, CSLTBP, HOTLEN, HRECOV, HREJCT, RECOLN,PR	PR 15760
C	VAPSPC, WPRTRY, POREC	PR 15770
	COMMON/COMNAM/ AJ, CB, CO, CP, CR, PR	PR 15780
1	HB, PI, PO, Tb, TO, TP, PR	PR 15790
2	TS, WB, WF, WO, WP, WR, PR	PR 15800
3	AXJ, HBL, HPR, LEV, LF2, TCF, PR	PR 15810
4	ENBH, GPMB, GPMO, GPMH, GPMO, GPMO, PR	PR 15820
5	GPMR, HDEA, RPMB, RPMO, RPMO, RPMO, PR	PR 15830
6	RPMR, TSTH, WHOT, YEAR, ACRES, BHVOL, PR	PR 15840
7	BLOGS, BNDLS, HOLES, HPBLU, HPDEA, HPDEL, PR	PR 15850
8	HPPRD, HPREC, PLPRD, PLSEA, PODEA, ACNCEW, PR	PR 15860
9	ACNCFL, ACNCIW, ACNCPH, ACNCRF, ACNCTR, AEXCAV, PR	PR 15870
+	ASTLEW, ASTLFL, ASTLIW, ASTLPH, ASTLRF, ASTLTR, PR	PR 15880
A	AWEIRS, BHSURF, DINTAK, ENITSE, ENPIPE, ENSUPE, PR	PR 15890
B	ENSUPR, PIPELN, PLSZMG, REJLEN, STLEN, STLTMP, PR	PR 15900
C	TNACDY, TRAINS, TSAREA, VOLCNC, VOLSTL, WOCEAN	PR 15910
	COMMON/SHARE/ IFLIP,ISPOT	PR 15920
	COMMON/BLOC12/ XT	PR 15930
	COMMON/BLOC13/ XO	PR 15940
	COMMON/INDEX/IND(40)	PR 15950
	COMMON/TAPE/ LTAPE2	PR 15960
C		PR 15970
	DIMENSION X08(40),XL8(40),XH8(40)	PR 15980
	DIMENSION XT(300),XO(300)	PR 15990
	EXTERNAL PLANTM	PR 16000
C		PR 16010
	CALL ITIME(IZX,JZX)	PR 16020
	DATA PROC/'MSF'/	PR 16030
	IO = -2	PR 16040
	FF = FFF	PR 16050
	IFLIP = 1	PR 16060
	TSTH = XO(15)	PR 16070
	BDEPH = XO(18)	PR 16080
	BKTH = XO(19)	PR 16090
	BKTE = XO(20)	PR 16100
	BKTR = XO(21)	PR 16110
	RSH = XT(101)	PR 16120
	RSE = XT(102)	PR 16130
	RSR = XT(103)	PR 16140
	SH = XO(22)	PR 16150
	SE = XO(23)	PR 16160
	SR = XO(24)	PR 16170
	HD = XO(28)	PR 16180
	HB = XO(29)	PR 16190
	HBL = XO(30)	PR 16200
	WPL = XO(33)	PR 16210
	CSLTBP = XO(34)	PR 16220
	CSLTBH = XO(35)	PR 16230

```

CO = X0(36)
CP = X0(37)
LF2 = X0(38)
TS = X0(39)
TO = X0(40)
THF = X0(41)
YEAR = X0(79)
SILTMP = X0(83)
VCLSTL = 0.00
VOLCNC = 0.00
PIPELN = X0(87)
PLSZMG = FF
BNDLS = X0(208) * X0(43)
IF (X0(209) .GT. 2.00) STOP 209
MODU = BNDLS / X0(209)
TRAINS = X0(43)
BLDGS = TRAINS / X0(210)
NBRHTR = FF * .03200 / TRAINS + .5
ENBH = TRAINS * DFLOAT(NBRHTR)
ENBH = DMAX1(TRAINS, ENBH)
WP = FF * 1.06 * DEN(CP, 90.00) * .0055700
CALL VARSET(FF, PROC)
DO 110 I = 1, 12
  X08(I) = X0(I)
  XH8(I) = XT(2*I-1)
  XL8(I) = XT(2*I)
  IF (XL8(I) .GT. XH8(I)) XL8(I) = XH8(I)
  IF (X08(I) .LT. XL8(I)) X08(I) = XL8(I)
  IF (X08(I) .GT. XH8(I)) X08(I) = XH8(I)
110 CONTINUE
C
NCALLS = 0
IND(1) = 0
IF (IOPT .EQ. 0) GO TO 115
IF (IO .GT. 0) WRITE(6,5) FF
5  FORMAT(1H1, 'MSF', F8.2, ' MGD')
CALL SLIDE(12, X08, XH8, XL8, PLANTM, IO, 1, 7, 3, 1, NCALLS)
IF (IO .GT. 0) WRITE(6,6) FF
6  FORMAT(1H0, 'MSF', F8.2, ' MGD')
115 CONTINUE
IND(13) = 1
CALL PLANTM(X08, CH20)
NCALLS = NCALLS + 1
CAPITL = CAP11 * 1.0-6
KOUT = LTAPE2
CALL RITEM(IOPT, IOUT, KOUT)
WRITE(KOUT, 15) NCALLS, IND(1)
15  FORMAT(1H , 21HNUMBER OF PLANT CALLS , I5, 110)
CALL ITIME(IZXX, JZXX)
TCALC = DFLOAT(IZXX - IZX) * 1.0-2
WRITE(KOUT, 4) TCALC
4  FORMAT(1H , 18HTIME FOR THIS CASE, F8.2, 2X7HSECONDS)
RETURN
END

```

```

PR 16240
PR 16250
PR 16260
PR 16270
PR 16280
PR 16290
PR 16300
PR 16310
****
****
PR 16320
PR 16330
****
****
****
****
PR 16430
PR 16440
PR 16450
PR 16460
PR 16470
PR 16480
PR 16490
PR 16500
PR 16510
PR 16520
PR 16530
PR 16540
PR 16550
PR 16560
PR 16570
PR 16580
PR 16590
PR 16600
PR 16610
PR 16620
PR 16630
PR 16640
PR 16650
PR 16660
PR 16670
PR 16680
PR 16690
PR 16700
PR 16710
PR 16720
PR 16730
PR 16740
PR 16750
PR 16760
PR 16770
PR 16780
PR 16790

```

APPENDIX B

CHANGES MADE IN SUBROUTINE MAINV

```

SUBROUTINE MAINV(FF,IOPI,IOU,CH20,CAPITL)
IMPLICIT REAL*8(A-H,O-Z)

C
DOUBLE PRECISION NTRAIN
DOUBLE PRECISION KBH, KPH, KVE, LBH, MGD, NBH,
1 NPH, NVE, KCON, LMTD, LVEP, LMTDBH, LMTDCN
DOUBLE PRECISION INT, INSTRD, INSTRK, INSTRY, MAINTK, MAINTY
DOUBLE PRECISION LEV,LF2

C
COMMON/BLOCV2/ A(30), S, AE(30), QE, TC(30),
1 TE(30), TR, UE(30), UH(3), WM, WT(30),
2 ABH, APH, BPE(30), CIE(30), COE(30), DPE(30),
3 ELL, GBH, GPH, GPM, HOD, KBH,
4 KPH, KVE, LBH, MGD, NBH, NPH,
5 NVE(30), QPH, RBH, RPH, RVE, TOQ,
6 UBH, VBH, VPH, WPEX(30), BHLF, GCON,
7 HIBH, HIPH(3), HOBH, HOPH(3), KCON, LMTD(3),
8 LVEP, PHLF, QMSF(3), RCON, SUBF(3), TCON,
9 UCON, VCON, VLEN, VTLF, WOTH(3), ALFAE(30),
+ CGNLF, HICON, HOCON, HOTEL, PHHGT, POBLO,
A POPRO, POSEA, SURFF, VEHGT, WALVE, EFFSPC,
BELBNDL(30), HCOTCF, HCOTOD, HEADBH, HEADCN, HEADPH,
C LMTDBH, LMTDCN, PLNTLF, PODEAS, POFEED, SUMWPE,
D SUMWPH, TOTAVE, QESP,VEFEED(30), WBOOST, WDCOLD,
E NE, NTRN, IFEEED, IRECYC
COMMON/BLOCV3/ BHD, BHK, BHY, INT, PMO,
1 PMK, PMY, VPD, VPK, VPY, ACHR,
2 DEAD, DEAK, DEAY, ELEC, HEAT, SBOD,
3 SBCK, SBCY, CHEMK, CHEMY, HEATK, HEATY,
4 OPERK, OPERY, PLDIN, WAITD, WAITK, WAITY,
5 ANCGMP, CMCAPO, CMCAPK, CMCAPY, CNDSRD, CNDSRK,
6 CNDSTRY, ELECTD, ELECTK, ELECTY, INSTRD, INSTRK,
7 INSTRY, MAINTK, MAINTY, PHTUBD, PHTUBK, PHTUBY,
8 PLCAPD, PLCAPK, PLCAPY, POWERK, POWERY, RETUBK,
9 RETUBY, SHELLD, SHELLK, SHELLY, TOTALK, TOTALY,
+ TOTOPK, TOTOPY, TREPBH, TREPCH, TREPPH, TREPVE,
A VETLBD, VETUBK, VETUBY, CGPD
COMMON/COMNAM/ AJ, CB, CO, CP, CR,
1 HB, PI, PO, TB, TO, TP,
2 TS, WB, WF, WO, WP, WR,
3 AXJ, HBL, HPR, LEV, LF2, TCF,
4 ENBH, GPMB, GPMO, GPMH, GPMO, GPMO,
5 GPMR, HDEA, RPMB, RPMO, RPMH, RPMO,
6 RPMR, TSTH, WHOT, YEAR, ACRES, BHVOL,
7 BLDGS, BNDLS, HOLES, HPBLO, HPDEA, HPDEL,
8 HPRRO, HPREC, PLPRD, PLSEA, PODEA, ACNCEW,
9 ACNCFL, ACNCIW, ACNCPH, ACNCRF, ACNCTR, AEXCAV,
+ ASTLEW, ASTLFL, ASTLIW, ASTLPH, ASTLRF, ASTLTR,
A AWEIRS, BHSURF, DINTAK, ENITSE, ENPIPE, ENSUPE,
B ENSUPR, PIPELN, PLSZMG, REJLEN, STLLEN, STLTMP,
C TNACDY, TRAINS, TSAREA, VOLCNC, VOLSTL, MOCEAN
COMMON/SHARE/ IFLIP, ISPT
COMMON/BLOC12/ XT
COMMON/BLOC13/ XO
COMMON/INDEX/ IND(40)
COMMON/TAPE/ LTAPE2

C
DIMENSION XC7(40),XH7(40),XL7(40),XU(300),XT(300)
DIMENSION JB(13)
EXTERNAL PLANTV

C
CALL ITIME(IGNX,JT)
DATA PROC/'VTE'/
DATA JB/3,5,9,11,25,13,15,27,29,31,33,35,37/
DG 65 I=1,40
65 IND(I) = 1
IFLIP = 1
IO = -2

```

```

BNDLS=XO(208)*XO(43)
TRAINS=XO(43)
BLDGS=TRAINS/XO(210)
NTRAIN=TRAINS
NBRHTR = FF*.03200/NTRAIN+.5
ENBH = NTRAIN*DFLOAT(NBRHTR)
ENBH = DMAX1(NTRAIN,ENBH)
TRAINS = NTRAIN
LEV =1.00
PLSZMG = FF
TSTH = XO(15)
CP = XO(37)
PLNTLF = XO(33)
BHLF = XO(35)
CONLF = XO(34)
PHLF = XO(34)
HB = XO(29)
CC = XC(36)
LF2 = XO(38)
TC = XO(40)
TS = XO(39)
HBL = XC(30)
S = XO(23)
STLTMP = XO(83)
PIPELN = XO(87)
RBH = XT(101)
RPH = XT(102)
RCCA = XT(103)
KPH = XC(20)
KBH = XC(19)
KCGN = XO(21)
WALVE = XO(70)
RVE = XT(113)
KVE = XC(72)
SURFF = XO(74)
VTLF = XO(76)
YEAR = XO(79)
MGD = FF
WP =MGD*1.06*DEN(CP,90.00)*.0055700
CALL VARSET(FF,PROG)
DO 100 I=1,13
K=JB(I)
XO7(I) =XO(I)
XH7(I) =XT(K)
XL7(I) =XT(K+1)
IF(XL7(I) .GT. XH7(I)) XL7(I)=XH7(I)
IF(XO7(I) .LT. XL7(I)) XO7(I)=XL7(I)
IF(XO7(I) .GT. XH7(I)) XO7(I)=XH7(I)
100 CONTINUE
C
NCALLS = 0
IND(1) = C
IF(IOPT .EQ. 0) GO TO 105
IF(IO .GT. 0) WRITE(6,5) FF
5 FORMAT(1H1,'VTE',F8.2,' MGD')
CALL SLIDE(13,XO7,XH7,XL7,PLANTV,10,6,13,7,1,NCALLS)
IF(IO .GT. 0) WRITE(6,6) FF
6 FORMAT(1H0,'VTE',F8.2,' MGD')
105 CONTINUE
IND(13)=1
CALL PLANTV(XO7,CH20)
NCALLS = NCALLS +1
CAPITL = PLCIN * 1.0-6
KOUT = LTape2
CALL RITEV(IOPT,IOUT,KOUT)
WRITE(KOUT,15) NCALLS,IND(1)
15 FORMAT(1H ,21HNUMBER OF PLANT CALLS ,15,110)
CALL ITIME(IENDX,JT)
TCASE =DFLOAT(IENDX-IBGNX)*.01
WRITE(KCUT,10) TCASE
10 FORMAT(1H ,25HTIME TO COMPUTE THIS CASE,F7.2,8H SECONDS)
RETURN
END

```

```

****
****
****
****
PR 05580
PR 05590
PR 05600
PR 05610
PR 05620
PR 05630
PR 05640
PR 05650
PR 05660
PR 05670
PR 05680
PR 05690
PR 05700
PR 05710
PR 05720
PR 05730
PR 05740
PR 05750
PR 05760
PR 05770
PR 05780
PR 05790
PR 05800
PR 05810
PR 05820
PR 05830
PR 05840
PR 05850
PR 05860
PR 05870
PR 05880
PR 05890
PR 05900
PR 05910
PR 05920
PR 05930
PR 05940
PR 05950
PR 05960
PR 05970
PR 05980
PR 05990
PR 06000
PR 06010
PR 06020
PR 06030
PR 06040
PR 06050
PR 06060
PR 06070
PR 06080
PR 06090
PR 06100
PR 06110
PR 06120
PR 06130
PR 06140
PR 06150
PR 06160
PR 06170
PR 06180
PR 06190
PR 06200
PR 06210
PR 06220
PR 06230
PR 06240
PR 06250
PR 06260

```

APPENDIX C

CHANGES MADE IN SUBROUTINE PLANTM

```

SUBROUTINE PLANTM(X08,FFFFFF)
IMPLICIT REAL*8(A-H,O-Z)

DOUBLE PRECISION MODU
DOUBLE PRECISION LEV,LF2

COMMON/BLOC#1/   DIE,   DIH,   DIR,   DOE,   DOH,
1   DOR,   ELE,   ENE,   RLR,   RNR,   HDEL,
2   HREC,   APTSR,   ENITSR,

COMMON/BLOC#2/   P,   Q,   AH,   AK,   AN,
1   AR,   FF,   GE,   GH,   GR,   HD,
2   PB,   PE,   QX(5),   RP,   SE,   SH,
3   SR,   TK,   VE,   VH,   VR,   WC,
4   AME,   ATN,   BPX(5),   CCF,   HH,   HLH,
5   HNH,   HOH,   GMX(5),   PHE,   PO3,   RSE,
6   RSH,   RSR,   TCL,   THF,   TKX(5),   TMC,
7   TME,   TPE,   UEX(5),   UME,   UMH,   WPL,
8   BKTE,   BKTH,   BKTR,   DTLS(5),   ELEX(5),   HIEX(5),
9   HOEX(5),   MODU,   KOEL,   RUE2,   APTSE,   BDEPH,
+   CAPIL,   HEADE,   HEADH,   HEADR,   POBLD,   PODEL,
A   POPRD,   SUBEX(5),   WCOLD,   WMODC,   BHSHEL,
B   CSLTBH,   CSLTBP,   HOTLEN,   HRECOV,   HREJCT,   RECOLN,
C   VAPSPC,   WPRTRY,   POREC

COMMON/COMNAM/   AJ,   CB,   CO,   CP,   CR,
1   PB,   PI,   PO,   TB,   TO,   TP,
2   TS,   WB,   WF,   WO,   WP,   WR,
3   AXJ,   HBL,   HPR,   LEV,   LF2,   TCF,
4   ENBH,   GPMB,   GPMO,   GPMH,   GPMQ,   GPMF,
5   GPMR,   HDEA,   RPMB,   RPMO,   RPMH,   RPMF,
6   RPMR,   TSTH,   WHOT,   YEAR,   ACRES,   BHVOL,
7   BLDGS,   BNDLS,   HOLES,   HPBLD,   HPDEA,   HPDEL,
8   HPPRD,   HPREC,   PLPRD,   PLSEA,   PODEA,   ACNCEW,
9   ACNCFL,   ACNCIW,   ACNCPH,   ACNCRF,   ACNCTR,   AEXCAV,
+   ASTLEW,   ASTLFL,   ASTLIW,   ASTLPH,   ASTLRF,   ASTLTR,
A   AWEIRS,   BHSURF,   DINTAK,   ENITSE,   ENPIPE,   ENSUPE,
B   ENSUPR,   PIPELN,   PLSZMG,   REJLEN,   STLLEN,   STLTMP,
C   TNACDY,   TRAINS,   TSAREA,   VOLCNC,   VOLSTL,   WOCEAN

COMMON/SHARE/   IFLIP,   ISPTOT

COMMON/BLOC12/ XT
COMMON/BLOC13/ X0
COMMON/INDEX/IND(40)
COMMON/OVRLAY/ HOSAVE(15),CISAVE(15)
COMMON/IMPOSS/ IMPOSE,IMPOSR

DIMENSION CEX(5), DTX(5), TCX(5)
DIMENSION XT(300), X0(300)
DIMENSION X08(40)

EQUIVALENCE (AE,AME),(TE,TME),(UE,UME),(UH,UMH),
1 (TC,TMC)

SMOOTH(YCAL,YMIN,RANGER)=YMIN+(YCAL-YMIN)*
1 (.500+DATAN(RANGER*(YCAL-YMIN))/PI)

AK = X08(1)
VH = X08(2)
DOH = X08(3)
LEV = X08(4)
VR = X08(5)
DOR = X08(6)
AN = X08(7)
VE = X08(8)
DOE = X08(9)
RP = X08(10)

```

PR 16800
 PR 16810
 PR 16820
 PR 16830
 PR 16840
 PR 16850
 PR 16860
 PR 16870
 PR 16880
 PR 16890
 PR 16900
 PR 16910
 PR 16920
 PR 16930
 PR 16940
 PR 16950
 PR 16960
 PR 16970
 PR 16980
 PR 16990
 PR 17000
 PR 17010
 PR 17020
 PR 17030
 PR 17040
 PR 17050
 PR 17060
 PR 17070
 PR 17080
 PR 17090
 PR 17100
 PR 17110
 PR 17120
 PR 17130
 PR 17140
 PR 17150
 PR 17160
 PR 17170
 PR 17180
 PR 17190
 PR 17200
 PR 17210
 PR 17220
 PR 17230
 PR 17240
 PR 17250
 PR 17260
 PR 17270
 PR 17280
 PR 17290
 PR 17300
 PR 17310
 PR 17320
 PR 17330
 PR 17340
 PR 17350
 PR 17360
 PR 17370
 PR 17380
 PR 17390
 PR 17400
 PR 17410
 PR 17420
 PR 17430
 PR 17440

```

      TB = TO + XC8(11)
      CR = XC8(12)
      CALL DXX8(DIE,DIH,DIR,DUE,DOH,DOR)
C****
C      INITIAL ESTIMATES
C***
      IF(IFLIP.GT. 1)GO TO 105
      CLOS = 1.0-8
      CCF = 1.9*CC
      CEX(2) = 1.9*CO
      VAPSPC = DMAX1(WP/BNDLS*2.1640-6,2.00)
      WPTYMN=DMAX1(WP/(BNDLS*.5400*XU(85)),XT(128))
      WMODMN = XC(209)*(WPTYMN +VAPSPC)
      HOO = H(CO,TO)
      CSAV = XT(108)/VIS(2.*CG,150.00,.1400)
      DO 90 I=1,15
      HOSAVE(I) = 2.03*XT(109)
90    CISAVE(I) = CSAV
      TKES = TB+(THF-TB)/RP
      PEES = (THF-TKES)/(1.03-TKES)
      DO 100 I=1,5
      ELEX(I) = 4.0*(FLOAT(I)+1.0)
      BPX(1) = 1.000
100   CONTINUE
      GO TO 110
105   CONTINUE
      TKES = TK
      PEES = PE
C****
C      CHOOSE ENTRY POINT
C***
      IF((IND(10)+IND(11)+IND(12)+IND(13)).GT. 0) GO TO 110
      IF(IND(7).GT. 0) GO TO 130
      IF(IND(4).GT. 0) GO TO 135
      IF((IND(8)+IND(9)).GT. 0) GO TO 141
      IF(IND(1).GT. 0) GO TO 150
      IF((IND(5)+IND(6)).GT. 0) GO TO 152
      GO TO 170
110   CONTINUE
      HTBU = HOO+1.03/RP*(CR-1.00)/CR
      TBMAX = HINV(CP,HTBU)
      IF(TB.GT. (TBMAX-1.00))TB = TBMAX-DEXP(TBMAX-1.00-TB)
      HOB = H(CO,TB)
      CB = CR*CO
      HBB = H(CB,TB)
      CALL BPRAT(TB,CB,BPX(5))
      DTX(5) = DTDPT(TB)
      TP = TB-BPX(5)-(1.5+.001623*(TB-92.))*DTX(5)
C****
C      OVERALL TRAY HEAT AND MATERIAL BALANCE
C***
      HVBAR2 = HVBK(THF,TB)
      DHV2 = HVBAR2-HBB
      DC2 = CB-CP
115   CONTINUE
      HFF = H(CCF,THF)
      P=(HFF-HBB)/DHV2
      F = CCF+P*DC2-CB
      IF(DABS(F).LE. CLOS) GO TO 120
      CCF = CCF-F/(1.+DHDC(CCF,THF)*DC2/DHV2)
      GO TO 115
120   CONTINUE
C****
C      BRINE HEATER TUBE SIDE HEAT AND MATERIAL BALANCE
C***
      HTHF = HFF -1.03*P/RP
      TCF = HINV(CCF,HTHF)
C****
C      RECYCLE MIX HEAT AND MATERIAL BALANCE

```

```

PR 17450
PR 17460
PR 17470
PR 17480
PR 17490
PR 17500
PR 17510
PR 17520
PR 17530
PR 17540
PR 17550
****
****
PR 17580
PR 17590
PR 17600
PR 17610
PR 17620
PR 17630
PR 17640
PR 17650
PR 17660
PR 17670
PR 17680
PR 17690
PR 17700
PR 17710
PR 17720
PR 17730
PR 17740
PR 17750
PR 17760
PR 17770
PR 17780
PR 17790
PR 17800
PR 17810
PR 17820
PR 17830
PR 17840
PR 17850
PR 17860
PR 17870
PR 17880
PR 17890
PR 17900
PR 17910
PR 17920
PR 17930
PR 17940
PR 17950
PR 17960
PR 17970
PR 17980
PR 17990
PR 18000
PR 18010
PR 18020
PR 18030
PR 18040
PR 18050
PR 18060
PR 18070
PR 18080
PR 18090
PR 18100
PR 18110
PR 18120
PR 18130

```

```

C***      TC = TB
          PB = P*(CO-CP)/(CB-CO)
          HFTE = HBB + (P+PB)*(HOB-HBB)
          TE = MINV(CCF,HFTE)
          HTQ = HFF-HTHF-PB*HBB+(P+PB)*HOB
          Q = (HTQ-P*H(CP,TP))/(HGB-HOO)
          DENOO = DEN(CO,TC)
C****
C          RECOVERY SECTION HEAT AND MATERIAL BALANCE
C          COMPUTATION OF RECOVERY HEAT TRANSFER PARAMETERS
C***
          QTC = HFTE+HFF-HTHF
          DENFE = DEN(CCF,TCF)
          HVBAR1 = HVBE(TKES)
126 CONTINUE
          CEX(3) = (CCF - PEES*CP)/(1.-PEES)
          CALL BPRAT(TKES,CEX(3),BPX(3))
          DTX(3) = DTD(TKES)
          TPE = TKES-BPX(3)-(.5+.001623*(TKES-92.))*DTX(3)
          CE = CEX(3)
          HCETK = H(CE,TKES)
          A11 = HVBAR1-H(CP,TPE)
          A12 = -.8*PEES
          CCEK = DHDC(CE,TKES)*(CCF-CP)/(1.-PEES)
          A21 = HVBAR1-HCETK+CCEK
          A22 = 1.+A12
          DL1 = HFF-QTC-PEES*A11
          DL2 = HFF-PEES*HVBAR1-(1.-PEES)*HCETK
          TKX(3) = (TKES+(DL2*A11-DL1*A21))/(A11*A22-A12*A21)
          TK = TKX(3)
          HVBAR1 = HVBE(TK)
          PE = PEES + (HFF-PEES*HVBAR1-(1.-PEES)*H(CE,TK))/A21
          IF(DABS((TKX(3)-TKES)/TKX(3)) .LE. CLOS) GO TO 130
          PEES = PE
          TKES = TKX(3)
          GO TO 126
130 CONTINUE
          DTK = TK-100.
          ROE1 = (THF-TK)/AN
          ROC1 = (TCF-TE)/AN
          CEX(1) = (CCF-PE*CP/AN)/(1.-PE/AN)
          TKX(1) = THF-ROE1
          TKX(2) = .5*(THF-ROE1+TK)
          TCX(1) = TCF-ROC1
          TCX(2) = TE+(TKX(2)-TK)*(TCF-TE)/(THF-TK)
          TCX(3) = TE
          HVBRK2 = HVBE(TKX(2))
132 CONTINUE
          HEK2 = H(CEX(2),TKX(2))
          PK2 = (HFF-HEK2)/(HVBRK2-HEK2)
          F = CEX(2)*(1.-PK2)+CP*PK2-CCF
          IF(DABS(F) .LE. CLOS) GO TO 135
          FP = (1.-PK2)*(1.+(CEX(2)-CP)/(HVBRK2-HEK2)*DHDC(CEX(2),TKX(2)))
          CEX(2) = CEX(2)-F/FP
          GO TO 132
135 CONTINUE
          WMODCA = (WP/MODU*(1.-PE+PE/AN)/(P*XO(85))+VAPSPC*(LEV-1.))/LEV
          WMODC = SMOOTH(WMODCA,WMODMN,12.75D0)
          WPRTCA = WMODC/XO(209)-VAPSPC
          WPRTRY = SMOOTH(WPRTCA,WPTYMN,25.D0)
          WMODMI = XO(209)*(WPRTRY + .7857*VAPSPC)
          WMODCA = (WP/(P*MODU*XO(84))+.7857*VAPSPC*(LEV-1.))/LEV
          WMODH = SMOOTH(WMODCA,WMODMI,12.75D0)
          RXH = P*MODU*(LEV*(WMODH-.7857*VAPSPC)+.7857*VAPSPC)
          RXC = P*MODU*(LEV*(WMODC-VAPSPC)+VAPSPC)
          QX(1) = WP/RXH
          QX(2) = WP*(1.-PK2+PE/AN)/RXC
          QX(3) = WP*(1.-PE+PE/AN)/RXC
          QX(4) = WP*(1.-PE)/RXC

```

```

PR 18140
PR 18150
PR 18160
PR 18170
PR 18180
PR 18190
PR 18200
PR 18210
PR 18220
PR 18230
PR 18240
PR 18250
PR 18260
PR 18270
PR 18280
PR 18290
PR 18300
PR 18310
PR 18320
PR 18330
PR 18340
PR 18350
PR 18360
PR 18370
PR 18380
PR 18390
PR 18400
PR 18410
PR 18420
PR 18430
PR 18440
PR 18450
PR 18460
PR 18470
PR 18480
PR 18490
PR 18500
PR 18510
****
PR 18520
PR 18530
PR 18540
PR 18550
PR 18560
PR 18570
PR 18580
PR 18590
PR 18600
PR 18610
PR 18620
PR 18630
PR 18640
PR 18650
PR 18660
PR 18670
PR 18680
PR 18690
PR 18700
PR 18710
****
PR 18730
****
PR 18750
PR 18760
PR 18770
PR 18780
PR 18790
PR 18800
PR 18810
PR 18820

```

```

DO 140 I=1,2
CALL 8PRAT(TKX(I),CEX(I),BPX(I))
DTX(I) = DTC(DTKX(I))
140 CONTINUE
141 CONTINUE
GE = VE*DENFE
CONSLE = (DIE/12.)*2/4.*VE*3600.*DENFE/(DOE/12.)
IMPOSE = 0
DO 145 I=1,3
DHREC = H(CCF,TCX(I)+ROC1)-H(CCF,TCX(I))
TLX = TCX(I)+.5*ROC1
CALL UBAR(0.DO,TLX,CCF,CP,GE,DIE,DOE,SE,RSE,OMX(I),BKTE,UEX(I),
1 HIEX(I),HOEX(I))
CALL SUB(ROE1,TKX(I),QX(I),ELEX(I),BDEPH,SUBEX(I))
SMAX = TKX(I) - DTX(I) - BPX(I) - 1.0 - TCX(I) - ROC1
SUBEX(I) = DMIN1(SUBEX(I), SMAX)
ISPOT = I
LAPS = C
142 CONTINUE
SUBEES = SUBEX(I)
DTLS(I) = DTX(I)+BPX(I)+SUBEX(I)
TPEX = TKX(I) - DTLS(I)
TTD = TPEX-(TCX(I)+ROC1)
IF(TTD .LT. .0625D0) TTC = .0625D0*DEXP(TTD/.0625D0-1.D0)
OMX(I) = ROC1/DLOG(1.+ROC1/TTD)
IF(LAPS .NE. 0) GO TO 143
CALL UBAR1(TPEX,OMX(I),UEX(I),HIEX(I),HOEX(I))
143 CONTINUE
AEX = DHREC/(UEX(I)*OMX(I))
ELEX(I) = AEX*CONSLE
IF(TTD .LT. .0625D0) GO TO 144
CALL SUBM(ELEX(I),SUBEX(I))
CRIT = DABS(1.D0-SUBEES/SUBEX(I))
IF((LAPS .EQ. 0) .AND. (CRIT .LE. CLOSUR)) GO TO 145
LAPS = LAPS+1
IF((LAPS .GT. 2) .OR. (CRIT .LE. CLOSUR)) LAPS = 0
GO TO 142
144 IMPOSE = 1
145 CONTINUE
C****
C REJECT SECTION HEAT AND MATERIAL BALANCE
C COMPUTATION OF REJECT HEAT TRANSFER PARAMETERS
C***
150 CONTINUE
QX(5) = WP*(1.-P +(P-PE)/AK)/RXK
ROE2 = (TK-TB)/AK
ROC2 = (TC-TC)/AK
CEX(4) = ((1.-PE)*CE -(P-PE)*CP/AK)/(1.-PE-(P-PE)/AK)
CEX(5) = CB
TKX(4) = TK-ROE2
TKX(5) = TB
TCX(4) = TC -ROC2
TCX(5) = TO
CALL 8PRAT(TKX(4),CEX(4),BPX(4))
DTX(4) = DTC(DTKX(4))
152 CONTINUE
GR = VR*DENCO
CONSLR = (DIR/12.)*2/4.*VR*3600.*DENCO/(DOR/12.)
IMPCSR = 0
DO 160 I= 4,5
DHREJ = H(CO,TCX(I)+ROC2)-H(CO,TCX(I))
TLX = TCX(I)+.5*ROC2
CALL UBAR(0.DO,TLX,CO,CP,GR,DIR,DOR,SR,RSR,OMX(I),BKTR,UEX(I),
1 HIEX(I),HOEX(I))
CALL SUB(ROE2,TKX(I),QX(I),ELEX(I),BDEPH,SUBEX(I))
SMAX = TKX(I) - DTX(I) - BPX(I) - 1.0 - TCX(I) - ROC2
SUBEX(I) = DMIN1(SUBEX(I), SMAX)
ISPOT = I
LAPS = 0

```

PR 18830
PR 18840
PR 18850
PR 18860
PR 18870
PR 18880
PR 18890
PR 18900
PR 18910
PR 18920
PR 18930
PR 18940
PR 18950
PR 18960
PR 18963
PR 18967
PR 18970
PR 18980
PR 18990
PR 19000
PR 19010
PR 19020
PR 19030
PR 19040
PR 19050
PR 19060
PR 19070
PR 19080
PR 19090
PR 19100
PR 19110
PR 19120
PR 19130
PR 19140
PR 19150
PR 19160
PR 19170
PR 19180
PR 19190
PR 19200
PR 19210
PR 19220
PR 19230
PR 19240
PR 19250
PR 19260
PR 19270
PR 19280
PR 19290
PR 19300
PR 19310
PR 19320
PR 19330
PR 19340
PR 19350
PR 19360
PR 19370
PR 19380
PR 19390
PR 19400
PR 19410
PR 19420
PR 19430
PR 19440
PR 19450
PR 19453
PR 19456
PR 19460
PR 19470

158	CONTINUE	PR 19480
	SUBEES = SUBEX(I)	PR 19490
	DTLS(I) = DTX(I)+BPX(I)+SUBEX(I)	PR 19500
	TPEX = TKX(I) -DTLS(I)	PR 19510
	TTD = TPEX-(TCX(I)+ROC2)	PR 19520
	IF(TTD .LT. .062500) TTD = .062500*DEXP(TTD/.062500-1.00)	PR 19530
	OMX(I) = ROC2/DLOG(1.+ROC2/TTD)	PR 19540
	IF(LAPS .NE. 0) GO TO 159	PR 19550
	CALL UBAR1(TPEX,OMX(I),UEX(I),HIEX(I),HOEX(I))	PR 19560
159	CONTINUE	PR 19570
	ARX = DHREJ/(UEX(I)*OMX(I))	PR 19580
	ELEX(I) = ARX*CCNSLR	PR 19590
	IF(TTD .LT. .062500) GO TO 1591	PR 19600
	CALL SUBM(ELEX(I),SUBEX(I))	PR 19610
	CRIT = DABS(1.00-SUBEES/SUBEX(I))	PR 19620
	IF((LAPS .EQ. 0) .AND. (CRIT .LE. CLOSUR)) GO TO 160	PR 19630
	LAPS = LAPS+1	PR 19640
	IF((LAPS .GT. 2) .OR. (CRIT .LE. CLOSUR)) LAPS = 0	PR 19650
	GO TO 158	PR 19660
1591	IMPCSR = 1	PR 19670
160	CONTINUE	PR 19680
C****		PR 19690
C	BRINE HEATER HEAT AND MATERIAL BALANCE	PR 19700
C	COMPUTATION OF BRINE HEATER HEAT TRANSFER PARAMETERS	PR 19710
C***		PR 19720
170	CONTINUE	PR 19730
	GH = VH*DEN(CCF,THF)	PR 19740
	PHE =(THF-TCF)/DLOG((TS-TCF)/(TS-THF))	PR 19750
	TLH = .5*(THF+TCF)	PR 19760
	ISPCT = 6	PR 19770
	CALL UBAR(TS,TLH,CCF,0.00,GH,DIH,DOH,SH,RSH,PHE,BKTH,UH,H1H,H0H)	PR 19780
C****		PR 19790
C	SIZE PLANT	PR 19800
C***		PR 19810
	CALL SIZEP	PR 19820
C****		PR 19830
C****		PR 19840
C	COST PLANT	PR 19850
C***		PR 19860
	CALL COSTM	PR 19870
	FFFFFF = TC1	PR 19880
	IFLIP = IFLIP+1	PR 19890
	RETURN	PR 19900
	END	PR 19910

THIS PAGE
WAS INTENTIONALLY
LEFT BLANK

APPENDIX D

CHANGES MADE IN SUBROUTINE PLANTV

SUBROUTINE PLANTV(X07,GGG) PR 06270
 IMPLICIT REAL*8(A-H,O-Z) PR 06280
 C PR 06290
 DOUBLE PRECISION M, LAM, LAMDAE, IDVE, MAVG PR 06300
 DOUBLE PRECISION LPH, LVE, IDBH, IDPH, LCON, NCON, PR 06310
 1 NTPH, IDCON PR 06320
 DOUBLE PRECISION KBH, KPH, KVE, LBH, MGD, NBH, PR 06330
 1 NPH, NVE, KCON, LMTD, LVEP, LMTDBH, LMTDCN PR 06340
 DOUBLE PRECISION INT, INSTRD, INSTRK, INSTRY, MAINTK, MAINTY PR 06350
 DOUBLE PRECISION LEV,LF2 PR 06360
 C PR 06370
 COMMON/BLOCV1/ ANE, HVE, LPH, LVE, ACON, PR 06380
 1 GPMV, HPVE, HSEA, IDBH, IDPH, LCON, PR 06390
 2 NCON, NTPH, ODBH, ODPH, OQVE, POVE, PR 06400
 3 RPMV, HFEED, IDCON, ODCON, SUMWT, VETSA, PR 06410
 4 APTSCN, APTSEP, OVRHGT, TOTNVE, VEPMP, PR 06420
 COMMON/BLOCV2/ A(30), S, AE(30), QE, TC(30), PR 06430
 1 TE(30), TR, UE(30), UH(3), WM, WT(30), PR 06440
 2 ABH, APH, BPE(30), CIE(30), COE(30), DPE(30), PR 06450
 3 ELL, GBH, GPH, GPM, HOD, KBH, PR 06460
 4 KPH, KVE, LBH, MGD, NBH, NPH, PR 06470
 5 NVE(30), QPH, RBH, RPH, RVE, TOO, PR 06480
 6 UBH, VBH, VPH, WPEX(30), BHLF, GCON, PR 06490
 7 HIBH, HIPH(3), HOBH, HOPH(3), KCON, LMTD(3), PR 06500
 8 LVEP, PHLF, QMSF(3), RCON, SUBF(3), TCON, PR 06510
 9 UCON, VCON, VLEN, VTLF, WPTH(30), ALFAE(30), PR 06520
 + CONLF, HICON, HOCON, HOTE1, PHHGT, POBLO, PR 06530
 A POPRO, POSEA, SURFF, VEHGT, WALVE, EFFSPC, PR 06540
 BELBNDL(30), MCOTCF, HCGTQO, HEADBH, HEADCN, HEADPH, PR 06550
 C LMTDBH, LMTDCN, PLNTLF, PODEAS, POFEED, SUMWPE, PR 06560
 D SUMWPH, TOTAVE, QESP, VEFEEED(30), WBOOST, WDCOLD, PR 06570
 E NE, NTRN, IFEEED, IRECYC, PR 06580
 COMMON/BLOCV3/ BHD, BHK, BHY, INT, PMD, PR 06590
 1 PMK, PMY, VPD, VPK, VPY, ACHR, PR 06600
 2 DEAD, DEAK, DEAY, ELEC, HEAT, SBLO, PR 06610
 3 SBCK, SBCY, CHEMK, CHEMY, HEATK, HEATY, PR 06620
 4 OPERK, OPERY, PLDIN, WAITD, WAITK, WAITY, PR 06630
 5 ANCOMP, CMCAPD, CMCAPI, CMCAPI, CNDSD, CNDSD, PR 06640
 6 CNDSD, ELECTD, ELECTK, ELECTY, INSTRD, INSTRK, PR 06650
 7 INSTRY, MAINTK, MAINTY, PHTUBD, PHTUBK, PHTUBY, PR 06660
 8 PLCAPD, PLCAPK, PLCAPY, POWERK, POWERY, RETUBK, PR 06670
 9 RETUBY, SHELLD, SHELLK, SHELLY, TOTALK, TOTALY, PR 06680
 + TOTCPK, TOTOPY, TREPBH, TREPCH, TREPPE, PR 06690
 A VETUBD, VETUBK, VETUBY, CGPD, PR 06700
 COMMON/COMNAM/ AJ, CB, CO, CP, CR, PR 06710
 1 HB, PI, PO, TB, TP, PR 06720
 2 TS, WB, WF, WO, WP, WR, PR 06730
 3 AXJ, HBL, HPR, LEV, LF2, TCF, PR 06740
 4 ENBH, GPMB, GPMO, GPMH, GPMO, GPMO, PR 06750
 5 GPMR, HDEA, RPMB, RPMO, RPMH, RPMH, PR 06760
 6 RPMR, TSTH, WHOT, YEAR, ACRES, BHVOL, PR 06770
 7 BLDGS, BNDLS, HOLES, HPBLD, HPDEA, HPDEL, PR 06780
 8 HPRD, HPRE, PLPRD, PLSEA, PODEA, ACNCEW, PR 06790
 9 ACNCFL, ACNCIN, ACNCPI, ACNCRF, ACNCTR, AEXCAV, PR 06800
 + ASTLEW, ASTLFL, ASTLIW, ASTLRF, ASTLTR, PR 06810
 A AWEIRS, BHSURF, DINTAK, ENITSE, ENSUPE, PR 06820
 B ENSUPR, PIPELN, PLSZMG, REJLEN, STLEN, STLTP, PR 06830
 C TNACDY, TRAINS, TSAREA, VOLCNC, VOLSTL, WOCAN, PR 06840
 COMMON/SHARE/ IFLIP, ISPUT, PR 06850
 COMMON/BLOC12/ XT, PR 06860
 COMMON/BLOC13/ XO, PR 06870
 COMMON/INDEX/ IND(40), PR 06880
 COMMON/OVRIAY/ HNSAVE(15), CISAVE(15), PR 06890
 COMMON/IMPROVE/ IVERT, PR 06900
 COMMON/BLKFAC/ FDFAC, QEFAC, TRFAC, PR 06900

```

C      DIMENSION      M(30),      CAE(30),      GAM(3),      REFM(30),
1      THTX(4),      WPPHX(30),      WPROD(3),      WTRAX(30),
2      ABNDLV(30),      LAMDAE(30),      QBRINE(3),      RHOSTG(3),
3      TPRCDX(3),      BPEPH(3),      BPIE(30)
      DIMENSION X07(40)
      DIMENSION XC(300),XT(300)
C
      ABCISA(X3,X2,X1,Y3,Y2,Y1)= X3+((Y1*Y3-Y2*Y3)*(X3-X1)*(X2-X3))/
1      (Y1*Y2*(X1-X2)+Y1*Y3*(X3-X1)+Y2*Y3*(X2-X3))
C
      IERR=0
      DELTCF=10.
      VBH = X07(1)
      OCBH = X07(2)
      VCON = X07(3)
      ODCCN= X07(4)
      TRFAC= X07(5)
C
      VPH = X07(7)
      UDPH = X07(8)
      FDFAC = X07(9)
      ODVE = X07(10)
      LVE=X07(11)
      QEFAC = X07(12)
      ANE = X07(13)
      NPH=X07(6)*ANE
      CALL DXX8(IDPH,IDBH,IDCCN,ODPH,ODBH,ODCON)
      IF(IFLIP.GT. 1) GO TO 100
      TC(1)=TS
      CIE(1)=CO
      BPEB = 1.000
      DO 85 I=1,3
85  BPEPH(I) = 1.00
      CSAV = XT(108)/VIS(CO,150.00,.1400)
      DO 90 I=1,15
      HOSAVE(I) = 2.03*XT(109)
90  CSAVE(I) = CSAV
      ELREF = 3.+7.*DSQRT((MGD/TRAINS)/62.5)
      EFFSPC = 3.+75*ELREF
      DO 95 I=1,30
      BPE(I) = 1.000
      BPIE(I) = 1.00
95  A(I) = 7.00
      HOO = H(CO,TO)
      CLOSR = 1.C-8
      MAVG = XO(88)
      TEES = 100.00
      UE(1) = UVE(TS,KVE,WALVE,RVE,SLOPE)
      UV2 = UVE(1.5*(TS+TEES), KVE, WALVE, RVE, SLOPE)
      UENE = UVE(TEES, KVE, WALVE, RVE, SLOPE)
      UEBAX = (UE(1)+4.0*UV2+UENE)/6.0
      GO TO 105
100 IF(IND(13).GT. 0) GO TO 105
      IF(IND(12).GT.0.)GO TO 105
      IF((IND(10)+IND(11)).GT.0) GO TO 130
      IF(IND(9).GT. 0) GO TO 135
      IF((IND(6)+IND(7)+IND(8)).GT. 0) GU TO 180
      IF((IND(3)+IND(4)+IND(5)).GT. 0) GO TO 205
      GO TO 210
C****
C      VERTICAL TUBE SECTION
C****
105 NE = ANE +.5
      QNOM = (TS - (TG+10.0) - ANE*2.5)*UEBAX/ANE
      IVERT = 0
      M(NE) = XO(89)
      DO 110 I=1,NE
      AI = I
      REFM(I) = 1.+(AI-1.)/(ANE-1.)*(1.9072*(ANE-AI)-.061*(2*ANE-3*AI+2.))

```

```

PR 06910
PR 06920
PR 06930
PR 06940
PR 06950
PR 06960
PR 06970
PR 06980
PR 06990
PR 07000
PR 07010
****
****
PR 07020
PR 07030
PR 07040
PR 07050
PR 07060
****
PR 07080
PR 07090
PR 07100
PR 07110
7120
PR 07130
PR 07140
****
PR 07150
PR 07160
PR 07170
PR 07180
PR 07190
PR 07200
PR 07210
PR 07220
PR 07230
PR 07240
PR 07250
PR 07260
PR 07270
PR 07280
PR 07290
PR 07300
PR 07310
PR 07320
PR 07330
PR 07340
PR 07350
PR 07352
PR 07354
PR 07356
PR 07358
PR 07360
PR 07370
PR 07380
****
PR 07400
PR 07410
PR 07420
PR 07430
PR 07440
PR 07450
PR 07460
PR 07470
PR 07480
PR 07490
PR 07500
PR 07510
PR 07520
PR 07530

```

```

1          )/(ANE-2.)
M(1) = 1.+(AI-1.)/(ANE-1.)*(6.+(MAVG-1.)*(ANE-AI)-(M(NE)-1.)
1          *(2.*ANE-3.*AI+2.))/(ANE-2.)
110 CONTINUE
115 QESP = QNOM*(.6+.4*QEFAC)
120 TE(1) = TS-A(1)
    UE(1) = UVE(TE(1),KVE,WALVE,RVE,SLOPE)
    F = QESP/UE(1)-A(1)
    IF(DABS(F) .LE. CLOSR) GO TO 125
    A(1) = DABS(A(1) + F/(1.+ QESP*SLOPE))
    GO TO 120
125 LAMDAE(1) = LAM(TE(1),PZVE,CO,BPIE(1))
    QESPX = QESP*ANE/MAVG
    TEX=TS-2.5*(ANE-1.)
    KNTR = 0
126 UV2 = UVE(.5*(TEES+TE(1)),KVE,WALVE,RVE,SLOP2)
    UE(NE) = UVE(TEES,KVE,WALVE,RVE,SLOPE)
    UEBAR = (UE(1)+4.*UV2+UE(NE))/6.
    F = TEES+QESPX/UEBAR-TEX
    IF(DABS(F) .LE. CLOSR) GO TO 127
    KNTR = KNTR+1
    IF(KNTR .GE. 20) GO TO 127
    FP = 1.+QESPX*(2.*SLOP2*UV2+UV2+SLOPE*UE(NE)*UE(NE))
    1      /(6.*UEBAR*UEBAR)
    TEES = DABS(TEES - F/FP)
    GO TO 126
127 CMX=XT(115)
    WFNOM=1.D-3*CMX*QESP*(ANE-1.)*(1.-5.D-4*(TE(1)-TEES))
    1      /(CMX*(1.-1.D-3*(TE(1)-TEES))-CO)
130 IDVE = CDVE -2.*WALVE
    GPM = XC(75) *IDVE/2.902 *DSQRT(LVE/10.)
    TERMN = 1./(PI*CDVE/12.*LVE*SURFF)
    TERMW = GPM *60./7.48
135 WFX = WFNOM*(1.+4*FDFAC)
    IF(IVERT .GT. 0) GO TO 105
136 CONTINUE
    IRECYC = 0
137 CONTINUE
    WTRAX(1) = WFX
    SUMWPE = 0.00
    SUMWPH = 0.00
    DO 165 I=1,NE
    WPEX(I) = QESP/LAMDAE(I)
    WPEX(I) = DMIN1(WPEX(I), WTRAX(I)*(.22-CIE(I))/(.22-CP))
    SUMWPE = SUMWPE +WPEX(I)
    VEFEED(I) = M(I)*TERMW*TERMN*DEN(CIE(I),TE(I))
    CAE(I) = (VEFEED(I)*CIE(I) -.5*WPEX(I)*CP)/(VEFEED(I)-.5*WPEX(I))
    COE(I) = (WTRAX(I)*CIE(I)-WPEX(I)*CP)/(WTRAX(I)-WPEX(I))
    CALL BPRAT(TE(I),CAE(I),BPE(I))
    IF(I .GE. NE) GO TO 165
    AI = I+1
    TC(I+1) = (TE(I)-BPE(I)-2.5667)/.991333
145 DPE(I) = 1.47779800+TC(I+1)*(.00377800-3.55560-5*TC(I+1))
    ALFAE(I) = DPE(I)+BPE(I)
    F = TC(I+1)+ALFAE(I)-TE(I)
    IF(DABS(F) .LE. CLOSR) GO TO 150
    TC(I+1) = TC(I+1)-F/(1.00377800-7.11120-5*TC(I+1))
    GO TO 145
150 QESPM = QESP/M(I+1)
1501 TE(I+1) = TC(I+1)-A(I+1)
    UE(I+1) = UVE(TE(I+1),KVE,WALVE,RVE,SLOPE)
    F = QESPM/UE(I+1)-A(I+1)
    IF(DABS(F) .LE. CLOSR) GO TO 151
    A(I+1) = DABS(A(I+1) + F/(1.+QESPM*SLOPE))
    GO TO 1501
151 TEX = TE(I+1)-(ANE-AI)*(TE(I)-TE(I+1))
C****
C      IS PLANT PHYSICALLY REASONABLE WITH GIVEN M-VALUES?

```

PR 07540
 PR 07550
 PR 07560
 PR 07570
 PR 07580
 PR 07590
 PR 07600
 PR 07610
 PR 07620
 PR 07630
 PR 07640
 PR 07650
 PR 07660
 PR 07670
 PR 07675
 PR 07680
 PR 07690
 PR 07700
 PR 07710
 PR 07720
 PR 07723
 PR 07726
 PR 07730
 PR 07740
 PR 07750
 PR 07760

 PR 07790
 PR 07800
 PR 07810
 PR 07820
 PR 07830
 PR 07840
 PR 07850
 PR 07860
 PR 07870
 PR 07880
 PR 07890
 PR 07900
 PR 07910
 PR 07920
 PR 07930
 PR 07940
 PR 07945
 PR 07950
 PR 07960
 PR 07970
 PR 07980
 PR 07990
 PR 08000
 PR 08010
 PR 08020
 PR 08030
 PR 08040
 PR 08050
 PR 08060
 PR 08070
 PR 08080
 PR 08090
 PR 08100
 PR 08110
 PR 08120
 PR 08130
 PR 08140
 PR 08150
 PR 08160
 PR 08170
 PR 08180

```

C****
IF(TEX .GE. (TO+20.)) GO TO 152
IVERT = 1
TEZ = (TO+20.+(ANE-AI)*TE(I))/(ANE-AI+1.)
TE(I+1) = DMIN1(TC(I+1)-1.,TEZ)
A(I+1) = TC(I+1)-TE(I+1)
UE(I+1) = UVE(TE(I+1),KVE,WALVE,RVE,SLOPE)
M(I+1) = QESP/(UE(I+1)*A(I+1))
152 WTRAXO = WTRAX(I)-WPEX(I)
CMAX=.1375-.000375*TE(I)
WPHMAX = WTRAXO*(CMAX-COE(I))/(CMAX-CP)
CIE(I+1) = WTRAXO*COE(I)/(WTRAXO-.15*WPEX(I))
HEII = F(COE(I),TE(I))
HVPH = HVBR(TE(I),TE(I+1))
AZ1 = (HVPH*COE(I)-HEII*CP)/(HVPH-HEII)
AZ2 = (COE(I)-CP)/(HVPH-HEII)
155 HEES = F(CIE(I+1),TE(I+1))
F = CIE(I+1)-AZ1-AZ2*HEES
IF(DABS(F) .LE. CLOS) GO TO 160
CIE(I+1) = CIE(I+1)-F/(1.+AZ2*DMDC(CIE(I+1),TE(I+1)))
CIE(I+1) = DABS(CIE(I+1))
GO TO 155
160 WPPHX(I) = WTRAXO*(HEII-HEES)/(HVPH-HEES)
WTRAX(I+1) = WTRAXO-WPPHX(I)
SUMWPH = SUMWPH+WPPHX(I)
C****
C IS CONC LOW ENOUGH TO PREVENT CA2SO4 SCALING W/O PRODUCT LOSS?
C****
IF(CIE(I+1) .LE. CMAX) GO TO 162
IRECYC = IRECYC+1
161 SUMWPH = SUMWPH-WPPHX(I)+WPHMAX
WPPHX(I) = WPHMAX
CIE(I+1) = CMAX
WTRAX(I+1) = WTRAXO-WPHMAX
162 CONTINUE
LAMDAE(I+1) = LAM(TE(I+1),PZVE,CIE(I+1),BPIE(I+1))
165 CONTINUE
C MODIFY FDFAC TO GET DESIRED CONCENTRATION RATIO
IF(DABS(XT(151)-COE(NE)).LT.0.001000) GO TO 166
FDFAC=FDFAC-(XT(151)-COE(NE))*CO*(1.+FDFAC)/(1.4*XT(151)*(XT(151)-C
10))
1820 FORMAT(' FDFAC=',F10.4,' COE(NE) =',F10.5)
GO TO 135
166 CONTINUE
WPX = SUMWPE +SUMWPH
WPXX= WPX-WPEX(NE)
ALFAE(NE) = BPE(NE)+DTDP(TE(NE))
TCON = TE(NE)-ALFAE(NE)
C MODIFY QEFAC TO GET DESIRED TCON
IF(DABS(TCCN-XT(152)).LE.0.0500) GO TO 170
QEFAC=QEFAC+(TCCN-XT(152))*(1.5+QEFAC)/(TS-TCON)
1720 FORMAT(' QEFAC=',F10.4,' TCON=',F10.2)
GO TO 115
170 CONTINUE
CALL BPRAT(TE(NE),COE(NE),BPEB)
TPPH = TE(NE)-BPEB -(.5+.001623*(TE(NE)-92.))*DTDP(TE(NE))
C****
C FIT VE EFFECTS INTO TRAPEZOIDAL SHELL AND FIND LENGTH OF VE PLANTPR
C****
AE(1) = WP/WPX
WF = WFX *AE(1)
DO 175 I=1,NE
AL(I) =AE(1)*M(I)
NVE(I)= AE(1)*TERMN
RHOREF = 14.634 *(1.-DEXP(-(TC(I)-59.6)/69.17))
ABNDLV(I) = (NVE(I)/TRAINS *(QDVE/3.)*(QDVE/3.))/RHOREF
175 CONTINUE
ELBNDL(1) = ELREF
ELBNDL(NE) = ELREF*M(NE)/REFM(NE)
WOTH(1) = ABNDLV(1)/ELBNDL(1)

```

```

PR 08190
PR 08200
PR 08210
PR 08220
PR 08230
PR 08240
PR 08250
PR 08260
PR 08270
****
PR 08300
PR 08310
PR 08320
PR 08330
PR 08340
PR 08350
PR 08360
PR 08370
PR 08380
PR 08390
PR 08395
PR 08400
PR 08410
PR 08420
PR 08430
PR 08440
PR 08450
PR 08460
PR 08470
PR 08480
PR 08490
PR 08500
PR 08510
PR 08520
PR 08530
PR 08540
PR 08550
****
****
****
****
****
PR 08560
PR 08570
PR 08580
PR 08590
****
****
****
****
****
PR 08600
PR 08610
PR 08620
PR 08630
PR 08640
PR 08650
PR 08660
PR 08670
PR 08680
PR 08690
PR 08700
PR 08710
PR 08720
PR 08730
PR 08740
PR 08750

```

```

      WOTH(NE)= ABNDLV(NE)/ELBNDL(NE)
      NEM2 = NE-2
      VXLEN = (ANE-1.)*(ELREF+EFFSPC)
176 VLEN = WOTH(1)+EFFSPC
      TNTHET = (WOTH(NE)-WOTH(1))/VXLEN
      DO 177 I=1,NEM2
      WOTH(I+1) = WOTH(I)+(ELBNDL(I)+EFFSPC)*TNTHET
      ELBNDL(I+1) = ABNDLV(I+1)/WOTH(I+1)
177 VLEN = VLEN+ELBNDL(I+1)+EFFSPC
      IF(DABS((VLEN-VXLEN)/VXLEN) .LE. CLOSUR) GO TO 178
      VXLEN = VLEN
      GO TO 176
178 VLEN = VLEN+EFFSPC+ELBNDL(NE)
      LPH = VLEN
      HOTE1 = H(CC,TE(1))
      HTOUT = (1.-WPXX/WFX)*H(CIE(NE),TE(NE)) +WPXX/WFX*H(CP,TPPH)
      QTRSP = HOTE1 - HTOUT
      NDEL = NE/2-2
      SUMRHO = (TE(1)-TE(NE))
      TCFSAV=TE(1)-DELTCF
      DO 179 J=1,3
      NJ = 2+(J-1)*NDEL
      CALL BPRAT(TE(NJ),CIE(NJ),BPEPH(J))
      DTPHX = DTDPI(TE(NJ))
      TPRODX(J) = TE(NJ)-BPEPH(J)-(.5+.001623*(TE(NJ)-92.))*DTPHX
      THTX(J) = TE(NJ)-BPEPH(J)-DTPHX
      WPROD(J) = 1.-WTRAX(NJ)/WFX
      QBRINE(J) = HOTE1-WTRAX(NJ)/WFX*H(CIE(NJ),TE(NJ))
      - WPROD(J)*H(CP,TPRODX(J))
179 CONTINUE
C****
C      PREHEATER
C****
180 DO 185 J=1,3
      RHOSTG(J) = (TE(1)-TE(NE))/NPH
185 QMSF(J) = (WF/TRAINS)/(WOTH(NJ)-(WOTH(NE)-WOTH(1))/NPH)
      TCF=DMIN1(TCFSAV,TE(1)-DELTCF)
      ELL = LPH/NPH
      GXX = (ELL*GDPH/12.)/(3600.*(IDPH/12.)*2/4.)
      CALL UBAR(-10.DO,TL,CO,CP,GPH,IDPH,UDPH,S,RPH,LMTD(I),KPH,UH(I),
      HIPH(I),HOPH(I))
      NITS = C
190 GPH = VPH*DEN(CO,TCF)
      ABYWF = GXX/GPH
      TCES =TCF
      HCOTCF = H(CO,TCF)
      HCCTGO = HCOTCF-QTRSP
      TOO = HINV(CO,HCCTGO)
      DO 195 I=1,3
      RHOSTG(I) = RHOSTG(I)*(TCF-TOO)/SUMRHO
      ROTRAY = (TE(1)-TE(NE))*RHOSTG(I)/(TCF-TOO)
      NJ = 2+(I-1)*NDEL
      CALL SUB(ROTRAY,TE(NJ),QMSF(I),ELL,XO(18),SUBF(I))
      HCTUBE = HCOTCF-QBRINE(I)
      TCTUBE = HINV(CO,HCTUBE)
      TSRFCE = THTX(I)-SUBF(I)
      THTUBE = TCTUBE +RHOSTG(I)
      TL = .5*(TCTUBE +THTUBE)
      TTD = TSRFCE -THTUBE
      IF(TTD .LT. 1.DO) TTD = DEXP(TTD-1.)
      LMTD(I) = RHOSTG(I)/DLOG(1.+RHOSTG(I)/TTD)
      ISPCT = I+6
      CALL UBARO(TSRFCE,TL,GPH,LMTD(I),UH(I),HIPH(I),HOPH(I))
      SPHT = (H(CO,THTUBE)-HCTUBE)/RHOSTG(I)
      GAM(I) = 1.-DEXP(-ABYWF*UH(I)/SPHT)
      RHOSTG(I) = (TSRFCE-TCTUBE)*GAM(I)
195 CONTINUE
      NITS = NITS+1
      IF(NITS .GT. 3) NITS=3
      SUMRHO = NPH*(RHOSTG(1)+4.*RHOSTG(2)+RHOSTG(3))/6.
      X1 = X2

```

PR 08760
 PR 08770
 PR 08780
 PR 08790
 PR 08800
 PR 08810
 PR 08820
 PR 08830
 PR 08840
 PR 08850
 PR 08860
 PR 08870
 PR 08880
 PR 08890
 PR 08900
 PR 08910
 PR 08920
 PR 08930
 PR 08940

 PR 08960
 PR 08970
 PR 08980
 PR 08990
 PR 09000
 PR 09010
 PR 09020
 PR 09025
 PR 09030
 PR 09040
 PR 09050
 PR 09060
 PR 09070
 PR 09080
 PR 09090
 PR 09100

 PR 09120
 PR 09130
 PR 09140
 PR 09150
 PR 09160
 PR 09170
 PR 09180
 PR 09190
 PR 09200
 PR 09210
 PR 09220
 PR 09230
 PR 09240
 PR 09250
 PR 09260
 PR 09270
 PR 09280
 PR 09310
 PR 09320
 PR 09330
 PR 09340
 PR 09350
 PR 09360
 PR 09370
 PR 09380
 PR 09390
 PR 09400
 PR 09410
 PR 09420
 PR 09430
 PR 09440
 PR 09450
 PR 09460
 PR 09470

```

X2 = X3
X3 = TCF
Y1 = Y2
Y2 = Y3
Y3 = SUMRHG-(TCF-TCO)
GO TO (196,197,198),NITS
196 GRADES = -NPH*(GAM(1)+4.*GAM(2)+GAM(3))/6.
DTCF = -Y3/GRADES
GO TO 199
197 DTCF = -Y3*(X3-X2)/(Y3-Y2)
IF(Y2*Y3 .LT. 0.00) GO TO 1991
GO TO 199
198 DTCF = ABCISA(X3,X2,X1,Y3,Y2,Y1)-X3
199 DTCF = DTCF/DABS(DTCF)*CMIN1(DABS(DTCF),5.00,.5*(TE(1)-TCES))
1991 TCF = TCES+DTCF
IF(DABS((TCF-TCES)/TCES) .LE. CLOS) GO TO 200
GO TO 190
200 IFEED = 0
TCFSAV = TCF
C****
C      IS REQUIRED FEED TEMPERATURE TOO LOW?
C****
IF(TOO .GT. TO) GO TO 202
IVERT = IVERT+1
DO 201 I=2,N
  AI = 1
201 M(I) = REFM(I)+.1*(AI-1.)/(ANE-1.)*DFLOAT(IVERT)
  IERR=IERR+1
  IF(IERR.LE.20) GO TO 130
  PRINT 2200
2200 FORMAT('OUNSATISFACTORY SOLUTION - TC <= TOO')
202 CONTINUE
C****
C      IS AVAILABLE FEED TEMPERATURE HIGH ENOUGH?
C****
IF((WFX*(HCCTOO-HOO)) .LE. QESP) GO TO 205
IFEED = 1
HCCTOO = HOO +QESP/WFX
TOO = HINV(CO,HCCTOO)
HCCTCF = HCCTOO +QTRSP
TCF = HINV(CO,HCCTCF)
C****
C      CONDENSER
C****
205 TR=TCO-XT(153)
GCON = VCON *DEN(CO,TR)
TL = .5*(TC+TR)
TTD = TCO-TR
LMTCCN = (TR-TC)/DLOG(1.+(TR-TO)/TTD)
ISPCT = 12
CALL UBAR(TCON,TL,CO,CP,GCON,IDCON,ODCON,XO(24),RCO,LMTDCN,KCON,
1      UCCN,HICON,HOCN)
C****
C      BRINE HEATER
C****
210 GBH = VBH*DEN(CC,TE(1))
TL = .5*(TCF+TE(1))
TTD = TS-TE(1)
LMTCBH = (TE(1)-TCF)/DLOG(1.+(TE(1)-TCF)/TTD)
ISPCT = 13
CALL UBAR(TS,TL,CO,0.00,GBH,IDBH,ODBH,XO(22),RBH,LMTDBH,KBH,UBH,
1      HIBH,HOBH)
C****
C      SIZE PLANT
CALL SIZEV
C
C****
C      COST PLANT
CALL COSTV
C
GGG = TOTALK
IFLIP = IFLIP+1
RETURN
END

```

```

PR 09480
PR 09490
PR 09500
PR 09510
PR 09520
PR 09530
PR 09540
PR 09550
PR 09560
PR 09570
PR 09580
PR 09590
PR 09600
PR 09610
PR 09620
PR 09630
PR 09640
PR 09650
PR 09660
PR 09670
PR 09680
PR 09690
PR 09700
PR 09710
PR 09720
PR 09730
PR 09740
****
****
****
****
PR 09760
PR 09770
PR 09780
PR 09790
PR 09800
PR 09810
PR 09820
PR 09830
PR 09840
PR 09850
PR 09860
PR 09870
PR 09880
****
PR 09900
PR 09910
PR 09920
PR 09930
PR 09940
PR 09950
PR 09960
PR 09970
PR 09980
PR 09990
PR 10000
PR 10010
PR 10020
PR 10030
PR 10040
PR 10050
PR 10060
PR 10070
PR 10080
PR 10090
PR 10100
PR 10110
PR 10120
PR 10130
PR 10140
PR 10150
PR 10160

```

APPENDIX E

CHANGES MADE IN SUBROUTINE SIZE

	SUBROUTINE SIZE	PR 19920
	IMPLICIT REAL*8(A-H,O-Z)	PR 19930
C		PR 19940
	DOUBLE PRECISION MODU	PR 19950
	REAL*8 LPHE	****
	DOUBLE PRECISION LEV,LF2	PR 19960
C		PR 19970
	COMMON/PINHAS/APTSH,ENRSS,ENRJS,LPHE,DUMDUM(16),NFEED,IIIIII(9)	****
	COMMON/BLOC1/ DIE, DIH, DIR, DUE, DOH,PR	19980
1	COR, ELE, ENE, RLR, RNR, HDEL,PR	19990
2	HREC, APTSR, ENITSR	PR 20000
	COMMON/BLOC2/ P, Q, AH, AK, AN,PR	20010
1	AR, FF, GE, GH, GR, HD,PR	20020
2	PB, PE, QX(5), RP, SE, SH,PR	20030
3	SR, TK, VE, VH, VR, WC,PR	20040
4	AME, ATN, BPX(5), CCF, HIH, HLH,PR	20050
5	FNH, HOH, OMx(5), PHE, PO3, RSE,PR	20060
6	RSH, KSR, TC1, THF, TKX(5), TMC,PR	20070
7	TME, TPE, UEX(5), UME, UMH, WPL,PR	20080
8	BKTE, BKTH, BKTR, DTLS(5), ELEX(5), HIEX(5),PR	20090
9	MOEX(5), MODU, ROE1, ROE2, APTSE, BDEPH,PR	20100
+	CAPIL, HEADE, HEADH, HEADR, POBLD, PODEL,PR	20110
A	POPRD, SUBEX(5), WCOLD, WMODC, WMODH, BHSHEL,PR	20120
B	CSLT8H, CSLT8P, HOTLEN, HRECOV, HREJCT, RECOLN,PR	20130
C	VAPSPC, WPRTRY, POREC	PR 20140
	COMMON/CCMNAM/ AJ, CB, CU, CP, CR, PR	20150
1	HB, PI, PO, TB, TO, TP, PR	20160
2	TS, WB, WF, WO, WP, WR, PR	20170
3	AXJ, HBL, HPR, LEV, LF2, TCF, PR	20180
4	ENBH, GPMB, GPMO, GPMH, GPMO, GPM, PR	20190
5	GPMR, HDEA, RPMB, RPMO, RPMH, RPMP, PR	20200
6	RPMP, TSTH, WHOT, YEAK, ACRES, BHVOL, PR	20210
7	BLOGS, BNDLS, HOLES, HPBLD, HPDEA, HPDEL, PR	20220
8	HPPRO, HPREC, PLPRD, PLSEA, PODEA, ACNCEW, PR	20230
9	ACNCFL, ACNCIW, ACNCPH, ACNCRF, ACNCTR, AEXCAV, PR	20240
+	ASTLEW, ASTLFL, ASTLIW, ASTLPH, ASTLRF, ASTLTR, PR	20250
A	AWEIRS, BHSURF, DINTAK, ENITSE, ENPIPE, ENSUPE, PR	20260
B	ENSUPR, PIPELN, PLSZMG, REJLEN, STLEN, STLTMP, PR	20270
C	TNACDY, TRAINS, TSARZA, VOLCNC, VOLSTL, WOCAN	PR 20280
	COMMON/BLOC12/ XT	PR 20290
	COMMON/BLOC13/ XO	PR 20300
	COMMON/SHARE/IFLIP,ISPOT	PR 20310
	COMMON/INDEX/ IND(40)	PR 20320
C		PR 20330
	DIMENSION XT(300),XO(300)	PR 20340
	DIMENSION XL(3),XMTX(3,3)	PR 20350
C		PR 20360
	IF(IFLIP.EQ.1) GO TO 90	PR 20370
	IF((IND(10)+IND(11)+IND(12)+IND(13)).GT.0) GO TO 90	PR 20380
	IF((IND(7)+IND(8)+IND(9)).GT.0) GO TO 96	PR 20390
	IF(IND(4).GT.0) GO TO 116	PR 20400
	IF((IND(1)+IND(5)+IND(6)).GT.0) GO TO 120	PR 20410
	GO TO 150	PR 20420
90	CONTINUE	PR 20430
	WF = WP/P	PR 20440
	WO = Q*WF	PR 20450
	WB = PB*WF	PR 20460
	WC = WO -WB -WP	PR 20470
	WR = WF -WB -WP	PR 20480
	WOCAN = WO+.2*(WB+WP)	PR 20490
	GO TO (91,92),NFEED	****
91	CONTINUE	****
	TNACDY = 15.68*FF*CO*CR/(CR-1.)	PR 20500
	GO TO 93	****
92	CONTINUE	****
	TNACDY=12.D-9*XO(207)*(WP+WB)	****

```

93 CONTINUE
  IF(IFLIP .GT. 1) GO TO 95
  DENOO = DEN(CO,TO)
  AMAX = PI * 18.**2/4.
  ANEED = WOCEAN/(DENOO *8.*3600.)
  NPIPE = ANEED/AMAX +1.
  ENPIPE =NPIPE
95 CONTINUE
  DINTAK = DSQRT((4.*WOCEAN)/(DENG0*ENPIPE*PI*2.88D4))
  HPR1 = XO(31) + XT(106)
  CALL HEADS(1.00,1.00,0.00,CP,TP,1.00,1.00,TRAINS,WP,HPR1,HEADP,
1      HPR,GPMP,RPMP,PUPRD,HPPRD)
  CALL HEADS(1.00,1.00,0.00,CB,TB,1.00,1.00,TRAINS,WB,HBL,HEAD8,HBL,
1      GPMB,RPMB,POBLD,HPBLD)
  CALL HEADS(1.00,1.00,0.00,CO,TB,1.00,1.00,TRAINS,WB+WP,XO(86),HDX,
1      HDEA,GPMD,RPMM,POUEA,HPDEA)
96 CONTINUE
  DO 100 I=1,3
  XL(I) = ELEX(I)
  DO 100 J=1,3
  XMTX(I,J) = TKX(I)**(J-1)
100 CONTINUE
  CALL DMATEQ(XMTX,XL,3,1,3)
  NAN =AN+.5
  ELE = TSTH/12.
  ELSTL = 0.000
  STLLEN =0.000
  STLSTG =0.000
  TTRAY = THF
  DO 110 I=1,NAN
  AI = I
  TTRAYX = TTRAY
  ELESV = ELE
  TTRAY = THF-AI*ROE1
  ELE = ELE +XL(1)+ TTRAY*(XL(2)+XL(3)*TTRAY) +TSTH/12.
  NRSS=ELE/XT(200)+1.
  ENRSS=NRSS
  IF(STLTMP .GE. THF) GO TO 105
  IF(DABS(.5*(TTRAYX+TTRAY)-STLTMP) .GT. .5*ROE1) GO TO 105
  ELSTL = ELESV +(ELE-ELESV)*(TTRAYX-STLTMP)/ROE1
  STLLEN = ELSTL +10.667
  IF(STLTMP .LT. 170.00) STLLEN = STLLEN + 9.667
  STLSTG = AI-1.+ .5*(1.+DCOS(PI*(STLTMP-TTRAY)/ROE1))
105 CONTINUE
  IF(DABS(.5*(TTRAYX+TTRAY)-170.00) .GT. .5*ROE1) GO TO 110
  ELEHOT = ELESV +(ELE-ELESV)*(TTRAYX-170.00)/ROE1
  NRSSH=ELEHOT/XT(200)+1.
  ENRSSH=NRSSH
  HOTLEN = ELEHOT +20.333
  1 +(ENRSSH-1.)*9.667
  HOTSTG = AI-1.+ .5*(1.+DCOS(PI*(170.00-TTRAY)/ROE1))
110 CONTINUE
  IF((STLTMP .GT. TKX(3)) .OR. (STLTMP .GE. THF)) GO TO 115
  ELSTL = ELE
  STLLEN = ELSTL + 29.667
  1 +(ENRSS-2.)*9.667
  STLSTG = AN
115 CONTINUE
  RECOLN = ELE + 29.667
  1 +(ENRSS-2.)*9.667
  GOLDN = RECOLN -HOTLEN
  ENE = WF/(GE *3600.*PI*(DIE/12.))**2/4.)
  AME = PI*(DOE/12.) *ELE *ENE
  ARTUBE = ENE/BNDS *.866*(1.3*DOE/12.))**2
  STXLEN = STLLEN
116 CONTINUE
  STLLEN = STXLEN
  WBTRYH =WMODH
  WBTRYC = WMODC

```

PR 20510

PR 20520

PR 20530

PR 20540

PR 20550

PR 20560

PR 20570

PR 20580

PR 20590

PR 20600

PR 20610

PR 20620

PR 20630

PR 20640

PR 20650

PR 20670

PR 20680

PR 20690

PR 20700

PR 20710

PR 20720

PR 20730

PR 20740

PR 20750

PR 20760

PR 20770

PR 20780

PR 20790

PR 20800

PR 20810

PR 20820

PR 20830

PR 20840

PR 20850

PR 20860

PR 20870

PR 20880

PR 20890

PR 20900

PR 20910

PR 20920

PR 20930

PR 20940

PR 20950

PR 20960

PR 20970

PR 20980

PR 20990

PR 21000

PR 21010

PR 21020

PR 21030

PR 21040

PR 21050

PR 21060

PR 21070

PR 21080

PR 21090

PR 21100

PR 21110

PR 21120

```

APTSEL=XT(127)*ARTUBE
WBUNDL=(XT(126)*APTSEL)**0.5
HBNDLE=WBUNDL/XT(126)
HTSHET=HBNDLE+0.500
WTSKET=WBUNDL+0.500
APTSE=WTSKET*HTSHET
XTEST=DMAX1(VAPSPC,2.00)
IF(WTSKET+XTEST.LE.WMODH) GO TO 1161
WTSKET=WMODH-XTEST
HTSHET=APTSE/WTSKET
1161 HRECOV=XT(120)+HTSHET+XT(121)*(LEV-1.00)
WPRTRY=WTSKET
WALLTH=XT(122)*(MODU-BLDGS)+XT(123)*2.00*BLDGS
WHOT=WMODH*MODU+XT(124)*WALLTH
WCOLD = WMODC*MODU+WALLTH
AROOFE = WHOT*HOTLEN + WCOLU*COLDLN
STLRF = STLEN*WHOT+DMAX1(0.00,STLEN-HOTLEN)*(WCOLD-WHOT)
CNCRF = AROOFE -STLRF
STLFL = STLRF
CNCFL = CNCRF
AWALLE = HRECOV*(RECOLN *2.*BLDGS +WCOLD)
STLWL = HRECOV*STLEN *2.*BLDGS
IF(STLWL .GT. 0.00) STLWL= STLWL +HRECOV*WHOT
IF(STLEN.GT.HOTLEN) STLWL=STLWL+HRECOV*(WCOLD-WHOT)
CNCWL = AWALLE -STLWL
ACWE = HRECOV*RECOLN*(TRAINS-BLDGS)
STLCW = HRECOV*STLEN*(TRAINS-BLDGS)
CNCW = ACWE -STLCW
ABTRYE = (ELEHOT*WBTTRYH +(ELE-ELEHOT)*WBTTRYC)*MODU*(LEV-1.)
STLBT = (ELSTL*WBTTRYH+DMAX1(0.00,ELSTL-ELEHOT)*(WBTTRYC-WBTTRYH))
1 *MODU*(LEV-1.)
CNCBT = ABTRYE -STLBT
APTRYE = ELE * WPRTRY *2.*MODU
STLPT = ELSTL * WPRTRY *2.*MODU
CNCPT = APTRYE -STLPT
STLVOL = HRECOV *STLFL
CNCVOL = HRECOV *CNCFL
ASTGWL = ((HOTSTG+1.)*WHOT+(AN-HOTSTG+1.)*WCOLD)*HRECOV
STLSW = 0.000
IF(STLSTG .GT. 0.00) STLSW =(STLSTG+1.)*WHOT*HRECOV
IF(STLSTG .GT. HOTSTG) STLSW =STLSW+((STLSTG-HOTSTG+1.)*(WCOLD-
WHOT) +WHOT)*HRECOV
1 CNCW = ASTGWL -STLSW
STLPH = STLFL +STLBT + STLPT +(STLWL+(STLCW+STLSW)*2.)*5./HRECOV
CNCPH = CNCFL + 5.*(CNCWL+2.*CNCW)/HRECOV
WEIRA = ((WMODH+(LEV-1.)*WBTTRYH)*(HOTSTG+1.)+(WMODC+(LEV-1.)*
WBTTRYC)*(AN-HOTSTG+1.))+WPRTRY*2.*(AN+1.)*MODU*1.
1 PWD = WCOLD*(1.-1./TRAINS) +(BLDGS-1.)*2.*HRECOV
NTRN = TRAINS +.1
PLSEA= 0.00
DO 117 K =1,NTRN
AIK = K-1
ZWD = PWD*(.5 -AIK/TRAINS)
117 PLSEA = PLSEA+DSQRT(ZWD**2 +250.00**2 +HD**2)
PLPRD =PWD +WCOLD/TRAINS +HRECOV
TV1= THF-ROE1-BPX(1)
CALL PSIA(TV1,PSTA1)
VHLR=155.0-4*XO(204)*VE*VE
CALL PSIA(TP,PSTA1)
HREC1 = HRECOV+HB +XT(105) +2.3*(PSTA1-PSTA1)
1 +(ENKSS+1.)*VHLR
CALL HEADS(DIE,GE,ELE,CCF,TME,TCF,TME,TRAINS,WF,HREC1,HEADE,HREC2,
1 GPMR,SPX,PWX,HPRX)
ENITSE = (AN-ENRSS)*BNDLS
ENSUPE = DMAX1(.500, (.15*ELE/DOE-AN)*BNDLS)
120 CUNINVE
STLEN = STXLEN
ATN = AN+AK
RLR = (ELEX(4)+ELEX(5))/2.*AK +(AK+1.)*TSTH/12.
RNN = WO/(GR*3600.*PI*(DIR/12.))**2/4.)

```

```

****
****
****
****
****
****
****
****
****
****
PR 21210
PR 21220
PR 21230
PR 21240
PR 21250
PR 21260
PR 21270
PR 21280
PR 21290
****
PR 21300
PR 21310
PR 21320
PR 21330
PR 21340
PR 21350
PR 21360
PR 21370
PR 21380
PR 21390
PR 21400
PR 21410
PR 21420
PR 21430
PR 21440
PR 21450
PR 21460
PR 21470
PR 21480
PR 21490
PR 21500
PR 21510
PR 21520
PR 21530
PR 21540
PR 21550
PR 21560
PR 21570
PR 21580
PR 21590
PR 21600
PR 21610
PR 21620
****
PR 21630
PR 21640
****
PR 21650
PR 21660
PR 21670
PR 21680
PR 21690
PR 21700
PR 21710
PR 21720
PR 21730

```

```

AR = PI*(DOR/12.) *RLR *RNR
ARTUBR = RNR/BNCLS *.866*(1.3*DOR/12.)*2
HBNCLR = 4./PI*ARTUBR/WBUNCL
HTSHRT = HBNCLR *.5
APTSR = WTSHT * HTSHRT
HREJCT=XT(129)+HTSHRT+XT(125)*(LEV-1.00)
NRJS=RLR/XT(201)+1.
ENRJS=NRJS
REJLEN = RLR +(ENRJS+1.)*8.107
IF(TKX(3)-STLTMP)125,130,130
125 CONTINUE
STLLNR =0.00
ELSTLR =0.00
STLSTR =0.00
GO TO 145
130 CONTINUE
IF(TKX(5)-STLTMP) 135,140,140
135 CONTINUE
STLLNR = 7.667 +(TKX(3)-STLTMP)/(TKX(3)-TKX(5)) *RLR
ELSTLR = STLLNR -7.667
STLSTR = DFLOAT(IFIX(SNGL(ELSTLR/RLR *AK)))
GO TO 145
140 CONTINUE
STLLNR=REJLEN
ELSTLR = RLR
STLSTR = AK
145 CONTINUE
STLLEN = STXLEN+STLLNR
AROOFR = WCOLD*REJLEN
AWALLR = HREJCT*(REJLEN *2.*BLOGS +WCOLD)+ WCOLD*(HRECOV-HREJCT)
STLWLR = HREJCT*STLLNR *2.*BLOGS
IF(STLLNR .GT. 0.00) STLWLR =STLWLR + WCOLD*(HRECOV-HREJCT)
IF(STLLNR .EQ. REJLEN) STLWLR= AWALLR
CNCWLR= AWALLR -STLWLR
ACWR = HREJCT *REJLEN *(TRAINS-BLOGS)
STLCWR = HREJCT*STLLNR*(TRAINS-BLOGS)
ASTLCW = STLCW + STLCWR
CNCOWR = ACWR - STLCWR
ACNCCW = CNCOWR +CNCOWR
ABTRYR = RLR *WBTRYC*MODU *(LEV-1.)
STLBTR = ELSTLR*WBTRYC*MODU*(LEV-1.)
CNCBTR = ABTRYR -STLBTR
ASTLBT = STLBTR +STLBTR
ACNCBT = CNCBT +CNCBTR
APTRYR = RLR *WPTRY *2.*MODU
STLPTR = ELSTLR *WPTRY *2.*MODU
CNCPTR = APTRYR -STLPTR
ASTLPT = STLPT +STLPTR
ACNCPT = CNCPT +CNCPTR
STLVLR = HREJCT * WCOLD* STLLNR
CNCVLR = HREJCT * WCOLD *(REJLEN -STLLNR)
ASTGWR =(AK+1.)*HREJCT *WCOLD
STLSWR = STLSTR *HREJCT*WCOLD
IF(STLSTR .EQ. AK) STLSWR= STLSWR +HREJCT*WCOLD
CNCOWR = ASTGWR - STLSWR
ASTLSW = STLSW + STLSWR
ACNCOW = CNCOW + CNCOWR
STLPHR = WCOLD* STLLNR +STLBTR +STLPTR+(STLWLR+(STLCWR+STLSWR)*2.)
1 CNCOWR = AROOFR -WCOLD*STLLNR+(CNCWLR+2.*CNCOWR)*5./HREJCT
WEIRR = (WMODC +(LEV-1.)*WBTRYC +2.*WPTRY)*AK*MODU*1.
ASTLRF = STLRF + WCOLD*STLLNR
ACNCRF = CNCRF +AROOFR -WCOLD*STLLNR
ASTLFL = ASTLRF
ACNCFL = ACNCRF
ASTLEW = STLWL + STLWLR
ACNCEW = CNCWL +CNCWLR
ASTLIW = ASTLCW + ASTLSW
ACNCIW = ACNCCW + ACNCOW
VOLCNC = CNCVOL+CNCVLR

```

```

PR 21740
PR 21750
PR 21760
PR 21770
PR 21780
****
****
****
PR 21800
PR 21810
PR 21820
PR 21830
PR 21840
PR 21850
PR 21860
PR 21870
PR 21880
PR 21890
PR 21900
PR 21910
PR 21920
PR 21930
PR 21940
21950
PR 21960
PR 21970
PR 21980
PR 21990
PR 22000
PR 22010
PR 22020
PR 22030
PR 22040
PR 22050
PR 22060
PR 22070
PR 22080
PR 22090
PR 22100
PR 22110
PR 22120
PR 22130
PR 22140
PR 22150
PR 22160
PR 22170
PR 22180
PR 22190
PR 22200
PR 22210
PR 22220
PR 22230
PR 22240
PR 22250
PR 22260
PR 22270
PR 22280
PR 22290
PR 22300
PR 22310
PR 22320
+1.0-3PR 22330
+1.0-3PR 22340
PR 22350
PR 22360
+1.0-3PR 22370
+1.0-3PR 22380
+1.0-3PR 22390
+1.0-3PR 22400
+1.0-3PR 22410

```

[illegible]

THIS PAGE
WAS INTENTIONALLY
LEFT BLANK

APPENDIX F

CHANGES MADE IN SUBROUTINE SIZEV

```

SUBROUTINE SIZEV                                     PR 10720
IMPLICIT REAL*8(A-H,O-Z)                             PR 10730
REAL*8 LPHE                                           ****
REAL*8 NCOOL,LCOOL                                   ****

C
DOUBLE PRECISION NTRAIN                               PR 10740
DOUBLE PRECISION LPH, LVE, IDBH, IDPH, LCON, NCON,    PR 10750
1 NTPH, ICCON                                         PR 10760
DOUBLE PRECISION KBH, KPH, KVE, LBH, MGD, NBH,        PR 10770
1 NPH, NVE, KCON, LMTD, LVEP, LMTDBH, LMTDCN         PR 10780
DOUBLE PRECISION LEV,LF2                             PR 10790
PR 10800
C
COMMON/BLCCV1/ ANE, HVE, LPH, LVE, ACON,PR 10820
1 GPMV, HPVE, HSEA, IDBH, IDPH, LCON,PR 10830
2 NCON, NTPH, ODBH, ODPH, ODVE, POVE,PR 10840
3 RPMV, HFEED, IDCON, ODCON, SUMWT, VETSA,PR 10850
4 APTSCN, APTSEP, OVRHGT, TOTNVE, VEPMPS, PR 10860
COMMON/BLCCV2/ A(30), S, AE(30), QE, TC(30),PR 10870
1 TE(30), TR, UE(30), UH(3), WM, WT(30),PR 10880
2 ABH, APH, BPE(30), CIE(30), COE(30), OPE(30),PR 10890
3 ELL, GBH, GPH, GPM, HQO, KBH,PR 10900
4 KPH, KVE, LBH, MGD, NBH, NPH,PR 10910
5 NVE(30), QPH, RBH, RPH, RVE, TCC,PR 10920
6 UBH, VBH, VPH, MPEX(30), BHLF, GCON,PR 10930
7 HIBH, HIPH(3), HLBH, HUPH(3), KCON, LMTD(3),PR 10940
8 LVEP, PHLF, QMSF(3), KCON, SUBF(3), TCON,PR 10950
9 UCON, VCON, VLEN, VTLF, WOTH(30), ALFAE(30),PR 10960
+ CONLF, HICON, HQCON, HOTE1, PHHGT, POBLO,PR 10970
A POPRO, POSEA, SURFF, VEHGT, WALVE, EFFSPC,PR 10980
BELBNDL(30), HCOTCF, HCUTOD, HEADBH, HEADCN, HEADPH,PR 10990
C LMTDBH, LMTDCN, PLNTLF, PODEAS, POFEED, SUMMPE,PR 11000
D SUMWPH, TOTAVE, QESP,VEFEED(30), WBOOST, WOCOLD,PR 11010
E NE, NTRN, IFEEED, IRECYC, PR 11020
COMMON/COMNAM/ AJ, CB, CU, CP, CR, PR 11030
1 FB, PI, PG, TB, TO, TP, PR 11040
2 TS, WB, WF, WO, WP, WR, PR 11050
3 AXJ, HBL, HPR, LEV, LF2, TCF, PR 11060
4 ENBH, GPMB, GPMO, GPMH, GPMO, GPMP, PR 11070
5 GPMR, HDEA, RPMB, RPMO, RPMH, RPMP, PR 11080
6 RPMR, TSTH, WHGT, YEAR, ACRES, BHWOL, PR 11090
7 BLDGS, BNDLS, HOLES, HPBLD, HPDEA, HPDEL, PR 11100
8 HPPRD, HPREC, PLPRD, PLSEA, PODEA, ACNCEW, PR 11110
9 ACNCFL, ACNCIW, ACNCPH, ACNCRF, ACNCTR, AEXCAV, PR 11120
+ ASTLEW, ASTLFL, ASTLIW, ASTLPH, ASTLRF, ASTLTR, PR 11130
A AWEIRS, BHSURF, DINTAK, ENITSE, ENPIPE, ENSUPE, PR 11140
B ENSUPR, PIPELN, PLSZMG, REJLEN, STLEN, STLTMP, PR 11150
C TNACDY, TRAINS, TSAREA, VOLCNC, VOLSTL, WOCAN, PR 11160
COMMON/SHARE/ IFLIP,ISPOT, PR 11170
COMMON/PINHAS/APTSH,ENRSS,ENRJS,LPHE,DUMDUM(16),NFEED,IIIIII(9) ****
COMMON/BLCC12/ XT, PR 11180
COMMON/BLCC13/ XO, PR 11190
COMMON/INDEX/ IND(40), PR 11200
C
DIMENSION XO(300),XT(300) PR 11210
C
IF((IND(9)+IND(10)+IND(11)+IND(12)+IND(13)) .GT. 0) GO TO 90 PR 11240
IF((IND(6)+IND(7)+IND(8)) .GT. 0) GO TO 130 PR 11250
IF((IND(3)+IND(4)+IND(5)) .GT. 0) GO TO 140 PR 11260
GO TO 210 PR 11270
90 CONTINUE PR 11280
NTRAIN = TRAINS PR 11290
WHOT = ((WDTH(1)+1.)*(VLEN-ELBNDL(NE))-(WDTH(NE)+1.)*EFFSPC)/ PR 11300
(VLEN-ELBNDL(NE)-EFFSPC) PR 11310
WCCLD= WHOT + VLEN*(WDTH(NE)+1.-WHOT)/(VLEN-ELBNDL(NE)) PR 11320
VEHGT = LVE +EFFSPC +3.5 PR 11330

```

```

TANGEN = (WCCLD-WHOT)/VLEN
WALIVE = 0.00
VXLEN = 0.00
STLLEN = 0.00
STLIW = 0.00
DO 110 I=1,NE
VXLEN = EFFSPC + ELBNDL(I) + VXLEN
WALIVE = WALIVE + (WHOT+VXLEN*TANGEN)*VEHGT*NTRAIN
IF((I.EQ. 1).OR. (TC(I).LE. STLTMP)) GO TO 110
IF((TC(I).LE. STLTMP).AND. (TC(I-1).GT. STLTMP)) GO TO 100
GO TO 110
100 STLLEN = VXLEN - (EFFSPC+ELBNDL(I))*(STLTMP-TC(I))/(TC(I-1)-TC(I))
STLIW = WALIVE - ((WHOT+VXLEN*TANGEN)*VEHGT*NTRAIN)*(STLTMP-TC(I))
1
/((TC(I-1) - TC(I))
PR 11340
PR 11350
PR 11360
PR 11370
PR 11380
PR 11390
PR 11400
PR 11410
PR 11420
PR 11430
PR 11440
PR 11450
PR 11460
PR 11470
PR 11480
PR 11490
PR 11500
PR 11510
PR 11520
PR 11530
PR 11540
PR 11550
PR 11560
PR 11570
PR 11580
PR 11590
PR 11600
PR 11610
PR 11620
PR 11630
PR 11640
PR 11650
PR 11660
PR 11670
PR 11680
PR 11690
PR 11700
PR 11720
PR 11730
PR 11740
PR 11750
PR 11760
PR 11770
PR 11780
PR 11790
PR 11800
PR 11810
PR 11820
PR 11830
PR 11850
PR 11890
PR 11900
PR 11910
PR 11920
PR 11930

```

TANGEN = (WCCLD-WHOT)/VLEN
WALIVE = 0.00
VXLEN = 0.00
STLLEN = 0.00
STLIW = 0.00
DO 110 I=1,NE
VXLEN = EFFSPC + ELBNDL(I) + VXLEN
WALIVE = WALIVE + (WHOT+VXLEN*TANGEN)*VEHGT*NTRAIN
IF((I.EQ. 1).OR. (TC(I).LE. STLTMP)) GO TO 110
IF((TC(I).LE. STLTMP).AND. (TC(I-1).GT. STLTMP)) GO TO 100
GO TO 110
100 STLLEN = VXLEN - (EFFSPC+ELBNDL(I))*(STLTMP-TC(I))/(TC(I-1)-TC(I))
STLIW = WALIVE - ((WHOT+VXLEN*TANGEN)*VEHGT*NTRAIN)*(STLTMP-TC(I))
1
/((TC(I-1) - TC(I))
PR 11340
PR 11350
PR 11360
PR 11370
PR 11380
PR 11390
PR 11400
PR 11410
PR 11420
PR 11430
PR 11440
PR 11450
PR 11460
PR 11470
PR 11480
PR 11490
PR 11500
PR 11510
PR 11520
PR 11530
PR 11540
PR 11550
PR 11560
PR 11570
PR 11580
PR 11590
PR 11600
PR 11610
PR 11620
PR 11630
PR 11640
PR 11650
PR 11660
PR 11670
PR 11680
PR 11690
PR 11700
PR 11720
PR 11730
PR 11740
PR 11750
PR 11760
PR 11770
PR 11780
PR 11790
PR 11800
PR 11810
PR 11820
PR 11830
PR 11850
PR 11890
PR 11900
PR 11910
PR 11920
PR 11930

```

ENITSE=(NPH-ENRSS)*BNDLS
ENSUPE = DMAX1(.5DO, (.15*LPH/ODPH -NPH)*BNDLS)
HVE1 = OVRHGT +XO(211)
CALL HEADS(1.00,1.00,0.00,CVE,TVE,1.00,1.00,VEPMPS,SUMWT,HVE1,
1 HEADV,HVE,GPMV,RPMV,POVE,HPVE)
TV1 = TE(1) - (TE(1)-TB)/NPH -2.
CALL PSIA(TV1,PSTA1)
CALL PSIA(TOO,PSTAL)
VHLRS=155.0-4*XO(204)*VPH*VPH
HREC1 = HB +XT(105) +2.3*(PSTA1-PSTAL)
* +XY*VHLRS
XY=2.*ENRSS
CALL HEADS(IDPH,GPH,LPHE,CO,TOO,TCF,TOO,NTRAIN,WF,HREC1,HEADPH,
1 HREC2,GPMK,SPX,PWX,HPRX)
140 CONTINUE
STLLEN = STXLEN
HCOTR = H(CO,TR)
WO = QE/(HCOTR-HOO)
IF(MGD/NTRAIN.GE.10.00) GO TO 142
CONPAS=3.00
GO TO 143
142 CONPAS=2.00
143 CONTINUE
NCCN = WO/(PI*(IDCUN/12.))**2/4. *GCON *3600.)*CONPAS
ACON = QE/(UCON*LMTDCN)
LCON = ACUN/(NCCN*PI*ODCON/12.)
ABNDLC = NCON/NTRAIN *.866*(1.3*ODCON/12.))**2
DBNDLC = DSQRT(4.*ABNDLC/PI)
APTSCN = PI/4. *(DBNDLC +.5)**2
ENSUPR =DMAX1(.5DO, (.15*LCON/ODCON -1.)*NTRAIN)
EXCCN=0.00
ELLCN=C&NDLC*XT(130)+3.000
LVEP = VLEN +ELLCN
REJLEN = OVRHGT +ELLCN+EFFSPC
WDCOLD = WCOLD
WALSEP = DSQRT(LVEP**2 +(WDCOLD-WHOT)**2)
WALEVE = OVRHGT*((WHOT+WDCOLD)*NTRAIN +2.*BLDGS*(WALSEP+2.*EXCN))
ARCOFV = .5*(WDCOLD+WHOT)*NTRAIN*LVEP
WALINV = WALIVE +OVRHGT*WALSEP*(NTRAIN-BLDGS)+ARCOFV +APHIW
IF(TC(1) .LE. STLTMP) GO TO 150
IF((STLTMP .LT. TC(NE)) .AND. (STLTMP .GT. TCON)) GO TO 160
IF(STLTMP .LE. TCON) GO TO 170
ASTLRF = STLLEN *.5*(WHOT +STLLEN*TANGEN+WHOT) *NTRAIN
ASTLEW = OVRHGT *(WHOT*NTRAIN +2.*BLDGS*STLLEN/LVEP*WALSEP)
GO TO 180
150 ASTLRF = 1.0-3
ASTLEW = 1.0-3
GO TO 180
160 STLIW = WALIVE
VEROOF = .5*(WHOT +WCOLD)*VLEN
STLLEN = VLEN +ELLCN*(TC(NE)-STLTMP)/(TC(NE)-TCON)
ASTLRF = VEROOF*NTRAIN
ASTLEW = OVRHGT*(WHOT*NTRAIN +2.*BLDGS*(STLLEN/LVEP*WALSEP+EXCN))
GO TO 180
170 STLIW = WALIVE
STLLEN = LVEP
ASTLRF = ARCOFV
ASTLEW = WALEVE
180 CONTINUE
ASTLIW = STLIW +APHSTL +STLLEN/LVEP*OVRHGT*WALSEP*(NTRAIN-BLDGS)
1 +ASTLRF
ACNCRF = ARCOFV -ASTLRF +1.0-3
ACNCIW = WALINV -ASTLIW +1.0-3
ACNCEW = WALEVE -ASTLEW +1.0-3
ASTLFL = ASTLRF
ACNCFI = ACNCRF
VOLSTL = ASTLRF *OVRHGT
VOLCNC = ACNCRF *OVRHGT
ASTLTR = 1.0-3
ACNCTR = 1.0-3

```

```

****
PR 11950
****
PR 11970
PR 11980
PR 11990
PR 12000
PR 12010
****
PR 12020
****
****
PR 12030
PR 12040
PR 12050
PR 12060
PR 12070
PR 12080
****
****
****
****
****
PR 12100
PR 12110
PR 12120
PR 12130
PR 12140
PR 12150
****
****
PR 12190
PR 12200
****
PR 12220
PR 12230
****
PR 12250
PR 12260
PR 12270
PR 12280
PR 12290
PR 12300
PR 12310
PR 12320
PR 12330
PR 12340
PR 12350
PR 12360
PR 12370
****
PR 12390
PR 12400
PR 12410
PR 12420
PR 12430
PR 12440
PR 12450
PR 12460
PR 12470
PR 12480
PR 12490
PR 12500
PR 12510
PR 12520
PR 12530
PR 12540
PR 12550
PR 12560

```

```

AEXCAV = ASTLFL + ACNCFL
ASTLPH = 2.*ASTLFL + 5.*(2.*APHSTL/PHHGT + 2.*STLIW/VEHGT + STLLEN
1 /LVEP*WALSEP*(NTRAIN-BLDGS) + 2.*ASTLEW/OVRHGT)
ACNCPL = 2.*ACNCFL + 3.*(2.*(APHIW-APHSTL)/PHHGT + 2.*(MALIVE-STLIW)
1 /VEHGT)+5.*((LVEP-STLLEN)/LVEP*WALSEP*(NTRAIN-BLDGS)
2 + 2.*ACNCEW/OVRHGT)
ACRES = (WDCOLD*NTRAIN + 2.*OVRHGT*BLDGS)*(LVEP + 350.)/43.56D3
PMD = WDCOLD*(NTRAIN - 1.)+(BLDGS-1.)*2.*OVRHGT
NTRN = NTRAIN + .1
PLSEA = 0.00
DO 190 K=1,NTRN
AIK = K-1
ZWD = PMD*(.5-AIK/NTRAIN)
190 PLSEA = PLSEA + DSQRT(ZWD**2 + 250.00**2 + XO(28)**2)
PLPRD = PMD + WDCOLD
WM = WF*(HCOTR-HCOTO0)/(HCOTR-H00)
WM = DMAX(0.00,WM)
WBOUST = WF-WM + .2*WF
WOCEAN = WO + WM + .2*WF
HDEL1 = XO(28)+XT(104) + PHHGT + .5*VEHGT
CALL HEADS(IDCON,GCCN,LCON,CO,TO,TR,TO,NTRAIN,WOCEAN,HDEL1,HEADCN,
1 HSEA,GPMU,RPMU,PUSEA,HPUEL)
CALL HEADS(1.00,1.00,0.00,CO,TO,TO,TC,NTRAIN,WBOUST,XO(86),HDX,
1 HDEA,GPMO,RPMO,PODEA,HPDEA)
IF(IFLIP.GT. 1) GO TO 200
DENOO = DEN(CO,TO)
AMAX = PI * 18.**2/4.
ANEED = WOCEAN/(DENOO * 8.*3600.)
NPIPE = ANEED/AMAX + 1.
ENPIPE = NPIPE
200 DINTAK = DSQRT( 4.*WOCEAN/(DENOO*ENPIPE*PI * 2.88D4))
TSAREA = (ENITSE+ENSUPE + XY*BNCLS)*APTSEP + (ENSUPR+2.)*APTSCN
HOLES = NTPH/BNCLS*(ENITSE + ENSUPE + XY*BNCLS) + NCON/NTRAIN
1 *(ENSUPR+2.)
210 CONTINUE
ABH = WF*(HOTEL-HCOTCF)/(UBH*LMTDBH)
NBH = 576.* WF/(PI*IDBH**2 *GBH *3600.)
LBH = ABH/(NBH *PI *ODBH/12.)
ARTUBH = NBH/ENBH *.866*(1.3*ODBH/12.)*2
DITUBH = DSQRT( 4./PI *ARTUBH) +.5
APTSH = PI * DITUBH**2/4.
BHSURF = PI * DITUBH*(LBH + DITUBH)
BHVOL = APTSH *LBH
CALL HEADS(IDBH,GBH,LBH,CO,TO,TE(1),TCF,NTRAIN,WF,HREC2,HEADBH,
1 HFEED,GPMH,RPMH,POFEED,HPREC)
230 PO = POFEED + POPRO + POBLO + POVE + POSEA + PODEA
GO TO (660,670),NFEED
660 XO(200)=350.
XO(201)=30.0-6
XO(205)=XO(200)*TRAINS+XO(201)*(WP+WB)
GO TO 680
670 XO(202)=350.
XO(203)=100.0-6
XO(205)=XO(202)*TRAINS+XO(203)*(WP+WB)
680 XO(206)=XO(205)*9.60-3
RETURN
END

```

```

PR 12570
PR 12580
PR 12590
PR 12600
PR 12610
PR 12620
PR 12660
PR 12670
PR 12680
PR 12690
PR 12700
PR 12710
PR 12720
PR 12730
PR 12740
PR 12750
PR 12760
PR 12770
PR 12780
PR 12790
PR 12800
PR 12810
PR 12820
PR 12830
PR 12840
PR 12850
PR 12860
PR 12870
PR 12880
PR 12890
PR 12900
****
****
PR 12930
PR 12940
PR 12950
PR 12960
PR 12970
PR 12980
PR 12990
PR 13000
PR 13010
PR 13020
PR 13030
PR 13040
PR 13050
****
****
****
****
****
****
****
****
PR 13060
PR 13070

```

APPENDIX G
CHANGES MADE IN SUBROUTINE TECPAR

```

C      SUBROUTINE TECPAR
      SPECIAL FOR VTE ONLY
      IMPLICIT REAL*8 (A-H,O-Z)
      COMMON/BLOC12/XT(300)
      XT( 3)=10.00
      XT(4)=5.00
      XT( 5)=.7500
      XT( 6)=.7500
      XT( 9)=10.00
      XT(10)=5.500
      XT(11)=.7500
      XT(12)=.7500
      XT(13)=3.00
      XT(14)=1.00
      XT(15)=10.00
      XT(16)=5.00
      XT( 25)= 1.000
      XT( 26)= 0.000
      XT( 27)= .7500
      XT( 28)= .7500
      XT( 29)= 1.000
      XT( 30)= 0.000
      XT( 31)= 4.000
      XT( 32)= 2.000
      XT(33)=100.
      XT(34)=-20.
      XT( 35)= 1.000
      XT( 36)= 0.000
      XT( 37)= 20.00
      XT( 38)= 5.000
      XT(101)=.000500
      XT(102)=.000500
      XT(103)=.000700
      XT(104)=7.900
      XT(105)=16.700
      XT(106)=15.1500
      XT(107)=1.00
      XT(108)=1.00
      XT(109)=1.00
      XT(110)=1.00
      XT(111)=1.00
      XT(112)=1.00
      XT(113)=0.00
      XT(114)=1.00
      XT(115)=-.08400
      XT(120)=5.00
      XT(127)=1.500
      XT(130)=1.00
      XT(151)=-.0800
      XT(152)=95.00
      XT(153)=5.00
      XT(200)=70.00
      CALLT('UPPER LIMIT FOR VELOCITY IN PREHEATER TUBING (VTE)', 3)
      CALLT('LOWER LIMIT FOR VELOCITY IN PREHEATER TUBING (VTE)', 4)
      CALLT('UPPER LIMIT FOR CD OF PREHEATER TUBING (VTE)', 5)
      CALLT('LOWER LIMIT FOR CD OF PREHEATER TUBING (VTE)', 6)
      CALLT('UPPER LIMIT FOR VELOCITY IN CONDENSER TUBING (VTE)', 9)
      CALLT('LOWER LIMIT FOR VELOCITY IN CONDENSER TUBING (VTE)', 10)
      CALLT('UPPER LIMIT FOR CD OF CONDENSER TUBING (VTE)', 11)
      CALLT('LOWER LIMIT FOR CD OF CONDENSER TUBING (VTE)', 12)
      CALLT('UPPER LIMIT FOR PREHEATER STAGES/EFFECT (VTE)', 13)
      CALLT('LOWER LIMIT FOR PREHEATER STAGES/EFFECT (VTE)', 14)
      CALLT('UPPER LIMIT FOR VELOCITY IN PREHEATER TUBING (VTE)', 15)
      CALLT('LOWER LIMIT FOR VELOCITY IN PREHEATER TUBING (VTE)', 16)
      CALLT('UPPER LIMIT FOR X0(5) DEFINING COND. REJECT TEMP(VTE)', 25)
      CALLT('LOWER LIMIT FOR X0(5) DEFINING COND. REJECT TEMP(VTE)', 26)
      CALLT('UPPER LIMIT FOR CD OF PREHEATER TUBES (VTE)', 27)

```

```

CALLT('LOWER LIMIT FOR OD OF PREHEATER TUBES          (VTE)', 28)
CALLT('UPPER LIMIT FOR XO(9) DEFINING FEED FLOW RATE   (VTE)', 29)
CALLT('LOWER LIMIT FOR XO(9) DEFINING FEED FLOW RATE   (VTE)', 30)
CALLT('UPPER LIMIT FOR CD OF VERTICAL TUBES            (VTE)', 31)
CALLT('LOWER LIMIT FOR CD OF VERTICAL TUBES            (VTE)', 32)
CALLT('UPPER LIMIT FOR XO(11) DEFINING TE(NE)           (VTE)', 33)
CALLT('LOWER LIMIT FOR XO(11) DEFINING TE(NE)           (VTE)', 34)
CALLT('UPPER LIMIT FOR XO(12) DEFINING VE HEAT RATE     (VTE)', 35)
CALLT('LOWER LIMIT FOR XO(12) DEFINING VE HEAT RATE     (VTE)', 36)
CALLT('UPPER LIMIT FOR NUMBER OF VE EFFECTS             (VTE)', 37)
CALLT('LOWER LIMIT FOR NUMBER OF VE EFFECTS             (VTE)', 38)
CALLT(' FOULING FACTOR IN BRINE HEATER                  (VTE)', 101)
CALLT(' FOULING FACTOR IN PREHEATER                     (VTE)', 102)
CALLT(' FOULING FACTOR IN CONDENSER                     (VTE)', 103)
CALLT(' DUCTING HEAD LOSS IN SEAWATER SYSTEM, FEET      (VTE)', 104)
CALLT(' DUCTING HEAD LOSS IN PREHEATER SYSTEM, FEET     (VTE)', 105)
CALLT(' DUCTING HEAD LOSS IN PRODUCT SYSTEM, FEET      (VTE)', 106)
CALLT(' MULTIPLIER FOR FRICTION FACTOR                  (VTE)', 107)
CALLT(' MULTIPLIER FOR LIQUID FILM HEAT TRNSF COEFF     (VTE)', 108)
CALLT(' MULTIPLIER FOR CONDENSING HEAT TRNSF COEFF     (VTE)', 109)
CALLT(' MULTIPLIER FOR SUBMERGENCE SUPERHEAT            (VTE)', 110)
CALLT(' MULTIPLIER FOR DEMISTER AND BUNDLE SUPERHEAT    (VTE)', 111)
CALLT(' MULTIPLIER FOR WALL THICKNESS COEFF VE TUBES    (VTE)', 112)
CALLT(' FOULING FACTOR FOR VERTICAL EVAPORATOR TUBES    (VTE)', 113)
CALLT(' MULTIPLIER FOR FILM HEAT TRNSFR COEFF VE TUBES   (VTE)', 114)
CALLT(' CA2SO4 ANHYDRITE LIMITED CONCENTRATION          (VTE)', 115)
CALLT(' PREHEATER VERTICAL BELOW TUBES                  (VTE)', 120)
CALLT(' PREHEATER BUNDLE WIDTH/HEIGHT RATIO             (VTE)', 127)
CALLT(' LENGTH RATIO, CONDENSER TO LAST EFFECT          (VTE)', 130)
CALLT(' CONCENTRATION IN LAST EFFECT                     (VTE)', 151)
CALLT(' CONDENSING TEMPERATURE IN CONDENSER, F          (VTE)', 152)
CALLT(' CONDENSER TTD, F                                  (VTE)', 153)
CALLT(' MAXIMUM LENGTH OF TUBING, FT.                   (MSF,VTE)', 200)

```

RETURN

END

SUBROUTINE TECPAR

SPECIAL FOR MSF75

IMPLICIT REAL*8 (A-H,O-Z)

COMMON/BLOC12/XT(300)

```

CALLT('UPPER LIMIT FOR NUMBER OF REJECT STAGES        (MSF)', 1)
CALLT('LOWER LIMIT FOR NUMBER OF REJECT STAGES        (MSF)', 2)
CALLT('UPPER LIMIT FOR VELOCITY IN HEATER TUBING       (MSF)', 3)
CALLT('LOWER LIMIT FOR VELOCITY IN HEATER TUBING       (MSF)', 4)
CALLT('UPPER LIMIT FOR OD OF HEATER TUBING             (MSF)', 5)
CALLT('LOWER LIMIT FOR CD OF HEATER TUBING             (MSF)', 6)
CALLT('UPPER LIMIT FOR NUMBER OF PLANT LEVELS          (MSF)', 7)
CALLT('LOWER LIMIT FOR NUMBER OF PLANT LEVELS          (MSF)', 8)
CALLT('UPPER LIMIT FOR VELOCITY IN REJECT TUBING        (MSF)', 9)
CALLT('LOWER LIMIT FOR VELOCITY IN REJECT TUBING        (MSF)', 10)
CALLT('UPPER LIMIT FOR OD OF REJECT TUBING              (MSF)', 11)
CALLT('LOWER LIMIT FOR CD OF REJECT TUBING              (MSF)', 12)
CALLT('UPPER LIMIT FOR NUMBER OF RECOVERY STAGES        (MSF)', 13)
CALLT('LOWER LIMIT FOR NUMBER OF RECOVERY STAGES        (MSF)', 14)
CALLT('UPPER LIMIT FOR VELOCITY IN RECOVERY TUBING      (MSF)', 15)
CALLT('LOWER LIMIT FOR VELOCITY IN RECOVERY TUBING      (MSF)', 16)
CALLT('UPPER LIMIT FOR CD OF RECOVERY TUBING            (MSF)', 17)
CALLT('LOWER LIMIT FOR OD OF RECOVERY TUBING            (MSF)', 18)
CALLT('LOWER LIMIT FOR PERFORMANCE RATIO                (MSF)', 19)
CALLT('LOWER LIMIT FOR PERFORMANCE RATIO                (MSF)', 20)
CALLT('UPPER LIMIT FOR TEMP DIFF.(TBLOWDOWN-TOCEAN)    (MSF)', 21)
CALLT('LOWER LIMIT FOR TEMP DIFF.(TBLOWDOWN-TOCEAN)    (MSF)', 22)
CALLT('UPPER LIMIT FOR CONCENTRATION RATIO              (MSF)', 23)
CALLT('LOWER LIMIT FOR CONCENTRATION RATIO              (MSF)', 24)
CALLT(' FOULING FACTOR IN BRINE HEATER                   (MSF)', 101)
CALLT(' FOULING FACTOR IN RECOVERY                      (MSF)', 102)
CALLT(' FOULING FACTOR IN REJECT                          (MSF)', 103)
CALLT(' DUCTING HEAD LOSS IN SEAWATER SYSTEM, FEET        (MSF)', 104)
CALLT(' DUCTING HEAD LOSS IN RECYCLE                      (MSF)', 105)
CALLT(' DUCTING HEAD LOSS IN PRODUCT SYSTEM, FEET        (MSF)', 106)
CALLT(' MULTIPLIER FOR FRICTION FACTOR                   (MSF)', 107)

```

```

CALLT(' MULTIPLIER FOR LIQUID FILM HEAT TRNSF COEFF (MSF)',108)
CALLT(' MULTIPLIER FOR CONDENSING HEAT TRNSF COEFF (MSF)',109)
CALLT(' MULTIPLIER FOR SUBMERGENCE SUPERHEAT (MSF)',110)
CALLT(' MULTIPLIER FOR DEMISTER AND BUNDLE SUPERHEAT (MSF)',111)
CALLT('MAXIMUM LENGTH OF TUBING,FT (MSF)',200)
XT( 1)=10.00
XT( 2)=2.000
XT( 3)=10.00
XT(4)=5.00
XT( 5)=.7500
XT( 6)=.7500
XT( 7)=1.000
XT( 8)=1.000
XT( 9)=10.00
XT(10)=5.500
XT(11)=.7500
XT(12)=.7500
XT(13)=70.00
XT(14)=10.00
XT(15)=10.00
XT(16)=5.00
XT(17)=.7500
XT(18)=.7500
XT(19)=30.00
XT(20)=5.000
XT(21)=50.00
XT(22)=10.00
XT(23)=3.00
XT(24)=1.800
XT(101)=.000500
XT(102)=.000500
XT(103)=.000700
XT(104)=7.900
XT(105)=16.700
XT(106)=15.1500
XT(107)=1.00
XT(108)=1.00
XT(109)=1.00
XT(110)=1.00
XT(111)=1.00
XT(112)=1.00
XT(113)=1.00
XT(114)=1.00
XT(115)=1.00
XT(120)=7.200
XT(121)=5.00
XT(122)=.0500
XT(123)=.100
XT(124)=1.00
XT(125)=4.00
XT(126)=1.500
XT(127)=1.2500
XT(128)=3.00
XT(129)=4.00
RETURN
END

```

**THIS PAGE
WAS INTENTIONALLY
LEFT BLANK**

APPENDIX H

CHANGES MADE IN SUBROUTINE OTHPAR

```

SUBROUTINE OTHPAR                                PR 34080
IMPLICIT REAL*8(A-H,U-Z)                        PR 34090
COMMON/BLOC13/ XO                               PR 34100
DIMENSION XO(300)                               PR 34110
C                                                 PR 34120
C****                                           PR 34130
C THE FIRST FOURTEEN XO'S ARE RESERVED FOR VARIABLES OF OPTIMIZATIONPR 34140
C THESE XO'S ARE ASSIGNED VALUES IN SUBROUTINE VARSET,DEPENDING PR 34150
C UPON PROCESS AND PLANT SIZE - THESE FOURTEEN XO'S MAY BE PR 34160
C ASSIGNED VALUES BY INPUT ONLY BY SETTING THE XT'S CORRESPONDING PR 34170
C TO THE UPPER AND LOWER LIMITS OF THE VARIABLE TO THE VALUE WHICHPR 34180
C THE VARIABLE IN QUESTION IS TO ASSUME. PR 34190
C FOR A MULTI-STAGE FLASH PLANT,THESE XO'S REPRESENT THE FOLLOWING PR 34200
C VARIABLES- PR 34210
C PR 34220
C XO(1) = NUMBER OF HEAT REJECT STAGES PR 34230
C UPPER LIMIT, XT( 1) - LOWER LIMIT, XT( 2) XO( 1)PR 34240
C XO(2) = VELOCITY IN BRINE HEATER TUBING,FPS PR 34250
C UPPER LIMIT, XT( 3) - LOWER LIMIT, XT( 4) XO( 2)PR 34260
C XO(3) = OUTSIDE DIAMETER OF BRINE HEATER TUBING, INCHES PR 34270
C UPPER LIMIT, XT( 5) - LOWER LIMIT, XT( 6) XO( 3)PR 34280
C XO(4) = NUMBER OF PLANT LEVELS PR 34290
C UPPER LIMIT, XT( 7) - LOWER LIMIT, XT( 8) XO( 4)PR 34300
C XO(5) = VELOCITY IN HEAT REJECT TUBING,FPS PR 34310
C UPPER LIMIT, XT( 9) - LOWER LIMIT, XT(10) XO( 5)PR 34320
C XO(6) = OUTSIDE DIAMETER OF HEAT REJECT TUBING,INCHES PR 34330
C UPPER LIMIT, XT(11) - LOWER LIMIT, XT(12) XO( 6)PR 34340
C XO(7) = NUMBER OF HEAT RECOVERY STAGES PR 34350
C UPPER LIMIT, XT(13) - LOWER LIMIT, XT(14) XO( 7)PR 34360
C XO(8) = VELOCITY IN HEAT RECOVERY TUBING,FPS PR 34370
C UPPER LIMIT, XT(15) - LOWER LIMIT, XT(16) XO( 8)PR 34380
C XO(9) = OUTSIDE DIAMETER OF HEAT RECOVERY TUBING,INCHES PR 34390
C UPPER LIMIT, XT(17) - LOWER LIMIT, XT(18) XO( 9)PR 34400
C XO(10)= PERFORMANCE RATIO ,LB PRODUCT WATER PER THOUSAND BTU PR 34410
C UPPER LIMIT, XT(19) - LOWER LIMIT, XT(20) XO(10)PR 34420
C XO(11)= TEMPERATURE DIFFERENCE,(TBLWDOWN -TOCEAN) PR 34430
C UPPER LIMIT, XT(21) - LOWER LIMIT, XT(22) XO(11)PR 34440
C XO(12)= CONCENTRATION RATIO, BLOWDOWN TO FEED CONCENTRATIONS PR 34450
C UPPER LIMIT, XT(23) - LOWER LIMIT, XT(24) XO(12)PR 34460
C XO(13)= NOT USED PR 34470
C XO(14)= NOT USED PR 34480
C*** PR 34490
C FOR A VERTICAL TUBE EVAPORATOR PLANT, PR 34500
C PR 34510
C XO(1) = VELOCITY IN BRINE HEATER TUBING, FPS PR 34520
C UPPER LIMIT, XT(3) - LOWER LIMIT, XT(4) XO(1)PR 34530
C XO(2) = OUTSIDE DIAMETER OF BRINE HEATER TUBING, INCHES PR 34540
C UPPER LIMIT, XT(5) - LOWER LIMIT, XT(6) XO(2)PR 34550
C XO(3) = VELOCITY IN CONDENSER TUBING, FPS PR 34560
C UPPER LIMIT, XT(9) - LOWER LIMIT, XT(10) XO(3)PR 34570
C XO(4) = OUTSIDE DIAMETER OF CONDENSER TUBING, INCHES PR 34580
C UPPER LIMIT, XT(11) - LOWER LIMIT, XT(12) XO(4)PR 34590
C XO(5) = DEFINES CONDENSER REJECT TEMP BY TR =TFEED+X*(TCON-TFEED) PR 34600
C UPPER LIMIT, XT(25) - LOWER LIMIT, XT(26) XO(5)PR 34610
C XO(6) = NUMBER OF STAGES IN MSF PREHEATER PER EFFECT **** PR 34630
C UPPER LIMIT, XT(13) - LOWER LIMIT, XT(14) XO(6)PR 34640
C XO(7) = VELOCITY IN PREHEATER TUBING, FPS PR 34650
C UPPER LIMIT, XT(15) - LOWER LIMIT, XT(16) XO(7)PR 34660
C XO(8) = OUTSIDE DIAMETER OF PREHEATER TUBES, INCHES PR 34670
C UPPER LIMIT, XT(27) - LOWER LIMIT, XT(28) XO(8)PR 34680
C XO(9) = DEFINES FEED RATE BY WF =WFMIN +X*(WFMAX-WFMIN) PR 34690
C UPPER LIMIT, XT(29) - LOWER LIMIT, XT(30) XO(9)PR 34700
C XO(10)= OUTSIDE DIAMETER OF VERTICAL EVAPORATOR TUBES, INCHES PR 34710
C UPPER LIMIT, XT(31) - LOWER LIMIT, XT(32) XO(10)PR 34720
C XO(11)= LENGTH OF A VERTICLE EVAPORATOR TUBE, FEET PR 34730
C UPPER LIMIT, XT(33) - LOWER LIMIT, XT(34) XO(11)PR 34740
C XO(12)= DEFINES HEAT FLOW DOWN VERT. EVAP. BY Q = X*QNOMINAL PR 34750

```

```

C          UPPER LIMIT, XT(35) - LOWER LIMIT, XT(36)          XO(12)PR 34750
C      XO(13)= NUMBER OF VERTICAL TUBE EFFECTS                PR 34760
C          UPPER LIMIT, XT(37) - LOWER LIMIT, XT(38)          XO(13)PR 34770
C      XO(14)= NOT USED                                         PR 34780
C****                                                         PR 34790
C                                                         PR 34800
C      CALLO('INTERMEDIATE TUBE SHEET THICKNESS, INCHES      (VTE,MSF)', 15)PR 34810
C          XO(15) = .7500                                       PR 34820
C                                                         PR 34830
C      CALLO('DEPTH OF FLASHING BRINE,MSF PLANT, FEET        (VTE,MSF)', 18)PR 34840
C          XO(18) = 1.2500                                       PR 34850
C                                                         PR 34860
C      CALLO('THERMAL CONDUCTIVITY OF BRINE HEATER TUBING (VTE,MSF)', 19)PR 34870
C          BTU/HR/FT/DEG F                                       PR 34880
C          XO(19) = 26.00                                         PR 34890
C                                                         PR 34900
C      CALLO('THERMAL COND.,RECOVRY(MSF),PRHTR(VTE) TUBING(VTE,MSF)', 20)PR 34910
C          BTU/HR/FT/DEG F                                       PR 34920
C          XO(20) = 26.00                                         PR 34930
C                                                         PR 34940
C      CALLO('THERMAL COND.,REJECT(MSF),CONDSR(VTE) TUBING(VTE,MSF)', 21)PR 34950
C          BTU/HR/FT/DEG F                                       PR 34960
C          XO(21) = 26.00                                         PR 34970
C                                                         PR 34980
C      CALLO('FLOODING FACTOR IN BRINE HEATER                 (VTE,MSF)', 22)PR 34990
C          XO(22) = 19.00                                         PR 35000
C                                                         PR 35010
C      CALLO('FLOODING FACTOR IN RECOVERY(MSF),PRHTR(VTE) (VTE,MSF)', 23)PR 35020
C          XO(23) = 19.00                                         PR 35030
C                                                         PR 35040
C      CALLO('FLOODING FACTOR IN REJECT(MSF),CONDSR(VTE) (VTE,MSF)', 24)PR 35050
C          XO(24) = 19.00                                         PR 35060
C                                                         PR 35070
C      CALLO('WALL THICKNESS OF BRINE HEATER TUBING, INCHES(VTE,MSF)', 25)PR 35080
C      XO(25)=.04900                                             ****
C                                                         PR 35100
C      CALLO('WALL THKNESS, RECOVERY(MSF),PRHTR(VTE) TUBING(VTE,MSF)', 26)PR 35110
C          INCHES                                                 PR 35120
C      XO(26)=.03500                                             ****
C                                                         PR 35140
C      CALLO('WALL THKNESS, REJECT(MSF),CONDSR(VTE) TUBING(VTE,MSF)', 27)PR 35150
C          INCHES                                                 PR 35160
C      XO(27)=.04900                                             ****
C                                                         PR 35180
C      CALLO('PUMPING HEAD,FEED SOURCE TO PLANT SITE,FEET      (ALL)', 28)PR 35190
C          XO(28) = 35.00                                         PR 35200
C                                                         PR 35210
C      CALLO('PUMPING HEAD,PLANT TO BRINE HEATER,FEET        (VTE,MSF)', 29)PR 35220
C          XO(29) = 25.00                                         PR 35230
C                                                         PR 35240
C      CALLO('BLOWDOWN PUMPING HEAD, FEET                     (ALL)', 30)PR 35250
C          XO(30) = 40.00                                         PR 35260
C                                                         PR 35270
C      CALLO('PRODUCT PUMPING HEAD, FEET                     (ALL)', 31)PR 35280
C          XO(31) = 92.00                                         PR 35290
C                                                         PR 35300
C      CALLO('PUMP AND MOTOR EFFICIENCY                       (ALL)', 32)PR 35310
C          XO(32) = .82700                                         PR 35320
C                                                         PR 35330
C      CALLO('DESALTING PLANT LIFE,YFARS                      (ALL)', 33)PR 35340
C          XO(33) = 30.00                                         PR 35350
C                                                         PR 35360
C      CALLO('TUBING(EXCEPT BRINE HTR AND VERT)LIFE,YEARS (VTE,MSF)', 34)PR 35370
C          XO(34) = 30.00                                         PR 35380
C                                                         PR 35390
C      CALLO('BRINE HEATER TUBING LIFE, YEARS                (VTE,MSF)', 35)PR 35400
C          XO(35) = 30.00                                         PR 35410
C                                                         PR 35420
C      CALLO('OCEAN SALT CONCENTRATION, WT. FRACTION          (VTE,MSF)', 36)PR 35430
C          XO(36) = .033600                                       PR 35440

```

C	CALLO('PRODUCT SALT CONCENTRATION, WT. FRACTION XO(37) = 25.0-6	(VTE,MSF)', 37)	PR 35450 PR 35460 PR 35470 PR 35480 PR 35490
C	CALLO('DESALTING PLANT LOAD FACTOR XO(38)=.8500	(ALL)', 38)	****
C	CALLO('STEAM TEMPERATURE, DEG F XO(39) = 258.00	(VTE,MSF)', 39)	PR 35510 PR 35520 PR 35530 PR 35540
C	CALLO('TEMPERATURE OF FEEDWATER, DEG F XO(40) = 65.00	(ALL)', 40)	PR 35550 PR 35560 PR 35570
C	CALLO('MAXIMUM BRINE TEMPERATURE, DEG F XO(41) = 250.00	(MSF)', 41)	PR 35580 PR 35590 PR 35600
C	CALLO('THE MINIMUM NUMBER OF TRAINS ALLOWED XO(43)=8.00	(ALL)', 43)	PR 35610 ****
C	CALLO('WALL THICKNESS, VERTICAL EVAPORATOR TUBING, IN. XO(70) = .04900	(VTE)', 70)	PR 35630 PR 35640 PR 35650 PR 35660
C	CALLO('THERMAL CONDUCTIVITY, VERTICAL EVAP. TUBES BTU/HR/FT/DEG F XO(72)=26.00	(VTE)', 72)	PR 35670 PR 35680 ****
C	CALLO('RATIO OF ACTUAL TO RUBBER BAND AREAS, VE TUBES XO(74) = 1.27300	(VTE)', 74)	PR 35700 PR 35710 PR 35720 PR 35730
C	CALLO('FEED RATE TO A 3 INCH OD, 10 FT LONG VE TUBE, GPM XO(75) = 2.000	(VTE)', 75)	PR 35740 PR 35750 PR 35760
C	CALLO('VERTICAL EVAPORATOR TUBE LIFE, YEARS XO(76) = 15.00	(VTE)', 76)	PR 35770 PR 35780 PR 35790
C	CALLO('YEAR PLANT CONSTRUCTION BEGINS XO(79)=1976.	(ALL)', 79)	PR 35800 ****
C	CALLO('MINIMUM PLANT SIZE(MGD) WITH ON-SITE ACID PLANT XO(80)=1000.00	(ALL)', 80)	PR 35820 PR 35830 ****
C	CALLO('MINIMUM PLANT SIZE(MGD) USING NUCLEAR HEAT+PWR XO(81) = 50.00	(ALL)', 81)	PR 35850 PR 35860 PR 35870 PR 35880
C	CALLO('MAXIMUM PLANT SIZE(MGD) WITH SUPPLIERS BURDEN XO(82) = 10.00	(ALL)', 82)	PR 35890 PR 35900 PR 35910
C	CALLO('MAXIMUM TEMPERATURE FOR CONCRETE SHELL XO(83)=0.00	(MSF,VTE)', 83)	PR 35920 ****
C	CALLO('MAX SPEC TRAY FLOW RATE AT HOT END OF RECOVERY XO(84) = 1.06	(MSF)', 84)	PR 35940 PR 35950 PR 35960 PR 35970
C	CALLO('MAX SPEC TRAY FLOW RATE AT COLD END OF RECOVERY XO(85) = .806	(MSF)', 85)	PR 35980 PR 35990 PR 36000
C	CALLO('DEAERATOR PUMPING HEAD, FEET XO(86) = 24.00	(MSF,VTE)', 86)	PR 36010 PR 36020 PR 36030
C	CALLO('TOTAL LENGTH OF INTAKE AND OUTFALL PIPING, FT XO(87) = 6000.00	(MSF,VTE)', 87)	PR 36040 PR 36050 PR 36060
C	CALLO('RATIO OF VE SURFACES, AVG OF ALL TO HOTTEST EFF. XO(88) = 1.151200	(VTE)', 88)	PR 36070 PR 36080 PR 36090
C	CALLO('RATIO OF VE SURFACES, COLDEST TO HOTTEST EFFECT XO(89) = 1.06100	(VTE)', 89)	PR 36100 PR 36110
C	CALLO('CONCENTRATION OF PRODUCT WATER, PPM XO(140) = 500.00	(ED)', 140)	PR 36810 PR 36820

CALLO('AIR LEAKAGE PER TRAIN, LB/HR (ACID)	(VTE,MSF)',200)	****
CALLO('PPM OF NCG FROM MAKE-UP FLOW IN EVAP.(ACID)	(VTE,MSF)',201)	****
CALLO('AIR LEAKAGE PER TRAIN, LB/HR (POLY)	(VTE,MSF)',202)	****
CALLO('PPM OF NCG FROM MAKE-UP FLOW IN EVAP.(POLY)	(VTE,MSF)',203)	****
CALLO('NO. OF VELOCITY HEADS LOST IN WATER BOXES	(VTE,MSF)',204)	****
XO(204)=2.00		****
CALLO('TOTAL NCG LOAD ON EJECTORS, LB/HR	(VTE,MSF)',205)	****
CALLO('HEAT REQUIRMENT FOR SJAE UNITS,MMBTU/HR	(VTE,MSF)',206)	****
CALLO('PPM POLYPHOSPHATE IN MAKE-UP STREAM	(VTE,MSF)',207)	****
XO(207)=3.00		****
CALLO('BUNDLES PER TRAIN	(ALL)',208)	****
XO(208)=1.00		****
CALLO('BUNDLES PER MODULE	(ALL)',209)	****
XO(209)=1.00		****
CALLO('TRAINS PER BUILDING	(ALL)',210)	****
XO(210)=1.00		****
CALLO('PRESSURE DROP IN VTE NOZZLES, FT.	(VTE)',211)	****
XO(211)=30.00		****
RETURN		PR 36830
END		PR 36840

APPENDIX I CHANGES MADE IN SUBROUTINE PRICES

	SUBROUTINE PRICES(PROC)		PR 54370
	IMPLICIT REAL*8(A-H,O-Z)		PR 54380
C			PR 54390
	DOUBLE PRECISION MSF		PR 54400
	DOUBLE PRECISION LPH, LVE, IDBH, IDPH, LCON, NCON,		PR 54410
	1 NTPH, IDCON		PR 54420
	REAL*8 LPHE		****
	REAL*8 KBH,KPH,KVE,LBH,MGD,NBH,NPH,NVE,KCON		****
	DOUBLE PRECISION MODU		PR 54430
	DOUBLE PRECISION LEV,LF2		PR 54440
C			PR 54450
	COMMON/PINHAS/APTSH,ENRSS,ENRJS,LPHE,DUMDUM(16),NFEED,IIIIII(9)		
	COMMON/BLOC13/ XO(300)		
	COMMON/BLOC1/ DIE, DIH, DIR, DOE, DOH, PR 54460		
1	DOR, ELE, ENE, RLR, RNR, HDEL, PR 54470		
2	HREC, APTSR, ENITSR, AN, PR 54480		
	COMMON/BLOC2/ P, Q, AH, AK, AN, PR 54490		
1	AR, FF, GE, GH, GR, HD, PR 54500		
2	PB, PE, QX(5), RP, SE, SH, PR 54510		
3	SR, TK, VE, VH, VR, WC, PR 54520		
4	AME, ATN, BPX(5), CCF, HIH, HLH, PR 54530		
5	MNH, HOH, OMX(5), PHE, POJ, RSE, PR 54540		
6	RSH, RSR, TCL, THF, TKX(5), TMC, PR 54550		
7	TME, TPE, UEX(5), UME, UMH, WPL, PR 54560		
8	BKTE, BKTH, BKTR, DTLS(5), ELEX(5), HIEX(5), PR 54570		
9	HOEX(5), MODU, ROEL, ROE2, APTSE, BDEPH, PR 54580		
+	CAPIL, HEAOE, HEADH, HEADR, POBLO, PODEL, PR 54590		
A	POPRD, SUBEX(5), WCOLD, WMUDC, WMODH, BHSHEL, PR 54600		
B	CSLTBH, CSLTBP, HOTLEN, HRECOV, HREJCT, RECOLN, PR 54610		
C	VAPSPC, WPRTRY, POREC, PR 54620		
	COMMON/BLOCV1/ ANE, HVE, LPH, LVE, ACON, PR 54630		
1	GPMV, HPVE, HSEA, IDBH, IDPH, LCON, PR 54640		
2	NCON, NTPH, ODBH, ODPH, ODVE, POVE, PR 54650		
3	RPMV, HFEED, IDCON, UDCON, SUMMT, VETSA, PR 54660		
4	APTSCN, APTSEP, OVRHGT, TOTNVE, VEPHPS, PR 54670		
	COMMON/BLOCV2/ A(30), S, AE(30), QE, TC(30), ****		
1	TE(30), TR, UE(30), UH(3), WM, WT(30), ****		
2	ABH, APH, BPE(30), CIE(30), COE(30), DPE(30), ****		
3	ELL, GBH, GPH, GPM, HOO, KBH, ****		
4	KPH, KVE, LBH, MGD, NBH, NPH, ****		
5	NVE(30), QPH, RBH, RPH, RVE, TOQ, ****		
6	UBH, VBH, VPH, WPEX(30), BHLF, GCON, ****		
7	HIBH, HIPH(3), HOBH, HOPH(3), KCON, LMTD(3), ****		
8	LVEP, PHLF, QMSF(3), RCON, SUBF(3), TCON, ****		
9	UCON, VCON, VLEN, VTLF, WIDTH(30), ALFAE(30), ****		
+	CONLF, HICON, HGCUN, HOTE1, PMHGT, POBLO, ****		
A	POPRD, POSEA, SURFF, VEHGT, WALVE, EFFSPC, ****		
	BELBNDL(30), HCOTCF, HCOTOO, HEADBH, HEADCN, HEADPH, ****		
C	LMTDBH, LMTDCN, PLNTLF, PODEAS, POFEED, SUMWPE, ****		
D	SUMWPH, TOTAVE, QESP, VEFEE(30), WBOOST, WDCOLD, ****		
E	NE, NTRN, IFEE, IRECYC, ****		
	COMMON/CONNAM/ AJ, CB, CU, CP, CR, PR 54680		
1	HB, PI, PO, TB, TO, TP, PR 54690		
2	TS, WB, WF, WO, WP, MR, PR 54700		
3	AXJ, HBL, HPR, LEV, LF2, TCF, PR 54710		
4	ENBH, GPMB, GPMO, GPMH, GPMO, GPMH, PR 54720		
5	GPMR, HDEA, RPMB, RPMO, RPMH, RPMP, PR 54730		
6	RPMR, TSTH, WHOT, YEAR, ACRES, BHVOL, PR 54740		
7	BLDGS, BNDLS, HOLES, HPBLD, HPDEA, HPDEL, PR 54750		
8	HPPRD, HPREC, PLPRD, PLSEA, PODEA, ACNCEW, PR 54760		
9	ACNCFL, ACNCIW, ACNCPH, ACNCRF, ACNCTR, AEXCAV, PR 54770		
+	ASTLEW, ASTLIW, ASTLPH, ASTLRF, ASTLTR, PR 54780		
A	AWEIRS, BHSURF, DINTAK, ENITSE, ENPIPE, ENSUPE, PR 54790		
B	ENSUPR, PIPELN, PLSZMG, KEJLEN, STLEN, STLTMP, PR 54800		
C	TNACDY, TRAINS, TSAREA, VOLCNC, VOLSTL, WOCEAN, PR 54810		
	COMMON/BLOC14/ XC		PR 54820

```

COMMON/SHARE/ IFLIP,ISPOT
C
DIMENSION XC(500)
DATA MSF,VTE,ED/'MSF','VTE','ED'/
C
UFHEAC(TS)= 1.
UNHEAC(TS)=(-78.5331+.644544*TS-.000608477*TS*TS)*0.01
C
UNIT COSTS ARE FOR THIRD QUARTER OF 1975
C
NOTE REORDERING OF CARDS HERE
C
*****
C
UNIT COSTS FOR THIRD QUARTER 1967
C
*****
C**** UNIT COSTS OF HORIZONTAL TUBE BUNDLE FABRICATION
C** UNIT COST OF TUBE SHEETS, $/SHEET - TUBE SHEETS ARE STEEL
C WITH 1/8 INCH CU-NI CLADDING
UCSHET(TKNS,AREA) = 9.929*TKNS*AREA
C** UNIT COST OF HOLE DRILLING AND TUBE ROLLING, $/HOLE
UCDRIL(TSTH,DIA) = .0449 + .1538*(TSTH*DIA)**2
C** UNIT COST OF TUBE SHEET INSTALLATION, $/TUBE SHEET
UCTSIN(TSTH,AREA,RFSNO,SHTNO)= 2.676*TSTH*AREA*
1 (RFSNO/SHTNO)**.1
C** UNIT COST OF INSTALLING TUBING, $/LINEAR FT.
UCTUIN(REFEET,FEET) = .07277*(REFEET/FEET)**.1
C
*****
C
C**** UNIT COSTS OF STEEL SHELL
C UNIT COST OF ROOF, $/SQ FT
USTLRF(AREA) = 13.53*(54601./AREA)**.1
C UNIT COST OF FLOOR AND FOUNDATION, $/SQ FT
USTLFL(AREA) = 5.373*(54601./AREA)**.1 + 11.27*(54601./AREA)**.03
C UNIT COST OF EXTERIOR WALLS, $/SQ FT
USTLEW(AREA) = 18.36*(21120./AREA)**.1
C UNIT COST OF INTERIOR WALLS, $/SQ FT
USTLIW(AREA) = 12.22*(154160./AREA)**.1
C UNIT COST OF INTERIOR FRAMING, $/CU FT SHELL VOLUME
USTLIF(VOLUME) = 1.238*(1.416206/VOLUME)**.1
C UNIT COST OF TRAYS, $/SQ FT
USTLTR(AREA) = 26.16*(67684./AREA)**.1
C UNIT COST OF PHENOLIC COATING, $/SQ FT
USTLPH(AREA) = 1.338*(180200./AREA)**.03
C
C**** UNIT COSTS OF CONCRETE SHELL
C UNIT COST OF ROOF, $/SQ FT
UCNCRF(AREA) = 11.11*(185497./AREA)**.03 + 5.17*(185497./AREA)**.1
C UNIT COST OF FLOOR AND FOUNDATION, $/SQ FT
UCNCFL(AREA) = 12.54*(185497./AREA)**.03 + 5.29*(185497./AREA)**.1
C UNIT COST OF EXTERIOR WALLS, $/SQ FT
UCNCEW(AREA) = 14.22*(48291./AREA)**.03 + 13.26*(48291./AREA)**.1
C UNIT COST OF INTERIOR WALLS, $/SQ FT
UCNCIW(AREA) = 6.96*(376165./AREA)**.03
C UNIT COST OF INTERIOR FRAMING, $/CU FT SHELL VOLUME
UCNCIF(VOL) = .261*(5.39306/VOL)**.03 + .109*(5.39306/VOL)**.1
C UNIT COST OF TRAYS, $/SQ FT
UCNCTR(AREA) = 8.28*(224140./AREA)**.03
C UNIT COST OF PHENOLIC COATING ON STEEL, $/SQ FT
UCNCPH(AREA) = 1.577*(2.05/AREA)**.03
C
C** UNIT COST OF EXCAVATION, $/SQ FT FLOOR AREA
UEXCAY(AREA) = .5461*(240100./AREA)**.03
C** UNIT COST OF DEMISTERS AND MISC SMALL SHELL ITEMS, $/MGD
UMISCI(PLCAP) = 10200.*(250./PLCAP)**.03
C** UNIT COST OF WEIRS, $/SQ FT WEIR AREA
UWEIRS(AREA) = 59.36*(19860./AREA)**.03
C
*****

```

```

PR 54830
PR 54840
PR 54850
PR 54860
PR 54870
****
****
****
****
PR 54960
PR 54970
****
PR 55010
PR 55020
PR 55030
PR 55040
PR 55050
PR 55060
PR 55070
PR 55080
PR 55090
PR 55100
PR 55110
PR 55120
PR 55130
PR 55140
PR 55150
PR 55160
PR 55170
PR 55180
PR 55190
PR 55200
PR 55210
PR 55220
PR 55230
PR 55240
PR 55250
PR 55260
PR 55270
PR 55280
PR 55290
PR 55300
PR 55310
PR 55320
PR 55330
PR 55340
PR 55350
PR 55360
PR 55370
PR 55380
PR 55390
PR 55400
PR 55410
PR 55420
PR 55430
PR 55440
PR 55450
PR 55460
PR 55470
PR 55480
PR 55490
PR 55500
PR 55510
PR 55520
PR 55530
PR 55540
PR 55550
PR 55560
PR 55570
PR 55580

```

C			PR 55590
C****	UNIT COST OF PUMPS , \$/GPM -PUMPS HAVE NI-RESIST CASINGS AND		PR 55600
C	316 SS IMPELLERS AND SHAFTS.		PR 55610
	UCPUMP(GPM,HEAD) = 23.762*(1.-.8696*DEXP(-.004426*HEAD))		PR 55620
1	/GPM**.15		PR 55630
C			PR 55640
C			PR 55650
C****	UNIT COST OF MOTORS ,\$/HP -MOTORS OF 500 OR MORE HORSEPOWER		PR 55660
C	ARE SYNCHRONOUS -SMALLER MOTORS ARE INDUCTION		PR 55670
	UCMOTR(HP,RPM) = 28.309*(1.+56.8D3 *RPM**(-.972)/HP**.736)		PR 55680
1	*(1.-.954*DEXP(-.004*HP))		PR 55690
C			PR 55700
C****	UNIT COST OF AUXILIARY PUMPS AND DRIVES,\$/MGD PLANT CAPACITY		PR 55710
	UCPAUP(PLCAP) =140.*(250./PLCAP)**.2		PR 55720
C			PR 55730
C****	UNIT COST OF PITS FOR RECYCLE,MAKE-UP,PRODUCT AND BLOWDOWN		PR 55740
C	PUMPS, \$/GPM PUMP CAPACITY		PR 55750
	UCPPIT(GPMP) = 1.17*(2.259D6/GPMP)**.2		PR 55760
C			PR 55770
C	*****		PR 55780
C			PR 55790
C****	UNIT COSTS OF SUBMARINE LINE INTAKE AND OUTFALL SYSTEM		PR 55800
	UCINSL(GO,DIA,TRAINS,PIPENO,PIPELN)=		PR 55810
C**	UNIT COST OF SCREENS, \$/GPM SEAWATER INTAKE		PR 55820
1	1.511D0		PR 55830
C**	UNIT COST OF INTAKE CAPS, \$/GPM		PR 55840
2	+ 2696.D0/GO *PIPENO * DIA**1.9		PR 55850
C**	UNIT COST CF DRAFT TUBES, \$/GPM		PR 55860
3	+ 94.12 *(TRAINS/GO)**.35		PR 55870
C**	UNIT COST OF MATERIAL, \$/GPM		PR 55880
4	+4.08*PIPELN*DIA**1.9*PIPENO**.97/GO		PR 55890
C**	UNIT COST OF LABOR ,\$/GPM		PR 55900
5	+20.85*PIPELN *DIA**1.1*PIPENO**.8/GO		PR 55910
C			PR 55920
C	*****		PR 55930
C			PR 55940
C****	UNIT COST OF HYDRAULICALLY OPERATED BUTTERFLY VALVES ,\$/GPM		PR 55950
	UCVALV(GPM) =(248.6+.008588*GPM**1.2)/GPM		PR 55960
C			PR 55970
C****	UNIT COST OF PLANT (SEAWATER,REJECT,AND INTERTRAIN) PIPING AND		PR 55980
C	FITTINGS, \$/GPM SEAWATER FLOW FOR DISTILLATION PLANTS.		PR 55990
	UCPLPF(PLSEA,GPMO,GPMP,PLPRD,TRAINS) =		PR 56000
C**	UNIT COST OF SEAWATER INTAKE PIPING ,\$/GPM SEAWATER FLOW		PR 56010
1	.0481*PLSEA*(GPMO/TRAINS)**.5/GPMO		PR 56020
C**	UNIT COST OF SEAWATER INTAKE FITTINGS,\$/GPM SEAWATER FLOW		PR 56030
2	+1.488*(GPMO/TRAINS)**.8 *TRAINS/GPMO		PR 56040
C**	UNIT COST OF PLANT REJECT PIPING ,\$/GPM SEAWATER FLOW		PR 56050
3	+0.0481*PLSEA*((GPMO-GPMP)/TRAINS)**.5/GPMO		PR 56060
C**	UNIT COST OF PLANT REJECT FITTINGS,\$/GPM SEAWATER FLOW		PR 56070
4	+1.326*((GPMO-GPMP)/TRAINS)**.8 *TRAINS/GPMO		PR 56080
C**	UNIT COST OF INTERTRAIN PIPING ,\$/GPM SEAWATER FLOW		PR 56090
5	+0.0481*GPMP**.5/GPMO*PLPRD		PR 56100
C**	UNIT COST OF INTERTRAIN FITTINGS, \$/GPM SEAWATER FLOW		PR 56110
6	+0.4302*GPMP**.8*TRAINS/GPMO		PR 56120
C			PR 56130
C****	UNIT COSTS OF INTRA-TRAIN PIPING AND FITTINGS FOR MSF PLANT,		PR 56140
C	\$/TRAIN		PR 56150
	UCTRPF(PLCAP,TRAINS,PLEVEL,REJLEN) =		PR 56160
C**	UNIT COST OF TRAIN PIPING, \$/TRAIN		PR 56170
1	3.28D4*(PLCAP/TRAINS)**.5*(.95+.05*(PLEVEL-1.))		PR 56180
2	*(.95+.05*REJLEN/90.33)		PR 56190
C**	UNIT COST OF TRAIN FITTINGS, \$/TRAIN		PR 56200
3	+12.1D3*(PLCAP/TRAINS)**.8		PR 56210
C			PR 56220
C****	UNIT COSTS OF BRINE HEATER PIPING AND FITTINGS,\$/GPM BH FLOW		PR 56230
	UCBHPF(ENBH,GPMH,PLEVEL)=		PR 56240
C**	UNIT COST OF BRINE HEATER PIPING,\$/GPM BH FLOW		PR 56250
1	88.00*ENBH*(GPMH/ENBH)**.5*(.9+.1*(PLEVEL-1.))/GPMH		PR 56260
C**	UNIT COST OF BRINE HEATER FITTINGS,\$/GPM BRINE HEATER FLOW		PR 56270
2	+1.455*ENBH*(GPMH/ENBH)**.8*(.9+.1*(PLEVEL-1.))/GPMH		PR 56280

```

C
C**** UNIT COST OF VENT AND DRAIN PIPING, $/GPM MAKE-UP FLOW
      UCVNTD(GPMU,PLCAP) = 2.205*(3.472D5/GPMU)**.03
      1 +2984.*(PLCAP/250.)**.2/GPMU
C
C *****
C NOTE REORDERING OF CARDS HERE
C
C**** UNIT COST OF BRINE HEATER SHELL AND INSTALLATION, $/SQ FT
      SHELL SURFACE
      UCBHSH(SURF,VOL,RFSURF,RFVOL) = 136.85*(RFSURF/SURF)**.1
      1 +34.87*VOL/SURF*(VOL/RFVOL)**.1
C
C *****
C UNIT COSTS FOR THIRD QUARTER 1975
C NOTE RE-ORDERING OF CARDS HERE
C
C *****
C
C** UNIT COST OF ACID DISPENSING AND CAUSTIC TREATMENT SYSTEMS,
      $/TON OF H2SO4 PER DAY.
C UCACCT(TNACDY,TRAINS)=8.04*(TNACDY/TRAINS/13.15)**.3*TRAINS/TNACDY
C** UNIT COST OF CHLORINATION EQUIPMENT, $/GPM SEAWATER INTAKE
      UCCHLO(GPMO) = 1.108*(2.205/GPMO)**.3
C ANTIFOAM + SULFITE OR POLYPHOSPHATE, $/GPM
C UCAFSS(GPMU,TRAINS)=20.03*(GPMU/TRAINS/1735.0)**.3*TRAINS/GPMU
C** UNIT COST OF PRODUCT WATER TREATMENT, CHEMICAL BLDG., AND
      MISC AIR AND HYDRAULIC SYSTEMS, $/MGD PLANT CAPACITY
C UCPAUX(PLCAP) = 12840.*(100.00/PLCAP)**.3
C
C *****
C
C**** UNIT COST OF INSTRUMENTATION
      UCI(FF,TRAINS)=400.03*(FF/TRAINS/10.0)**.3174*TRAINS/FF
C
C *****
C
C**** UNIT COST OF ELECTRICAL DISTRIBUTION EQUIPMENT, $/MW
      UCEDK(PMW,TRAINS)=(750.03*(PMW/TRAINS/10.0)**.8*TRAINS+
      1 1000.03*(PMW/40.0)**.8)/PMW
C
C *****
C
C**** UNIT COST OF DECARBONATOR AND STEAM EJECTORS AND DEAERATOR
      DEAERATOR, $/GPM
      UCDEA(FLOW,TRAINS)=100.03*(FLOW/TRAINS/4.203)**.7*TRAINS/FLOW
C DECARBONATOR, $/GPM
      UCDCR(FLOW,TRAINS)=46.03*(FLOW/TRAINS/4.203)**.7*TRAINS/FLOW
C STEAM EJECTORS, $/LB/HR NCG
      UCSJAE(GL,TRAINS)=(78.03*(GL/TRAINS/500.0)**.453
      1 +6.03*(GL/TRAINS/500.0)**.83+40.03)*TRAINS/GL
C
C *****
C
C**** UNIT COST OF SITE PREPARATION, $/ACRE
      UCSITS(ACRES)=75.03*(11.4/ACRES)**.03
C
C**** UNIT COST OF BUILDINGS AND CRANES, $/MGD PLANT CAPACITY
      UCBLCR(PLCAP)=30.03*(100./PLCAP)**.35
C
C *****
C
C**** UNIT COST OF OPERATING AND MAINTENANCE LABOR, $/YR PER MGD
      UCOPAN(PLCAP)=12.503*(100./PLCAP)**.5
C
C
C** COST FACTORS WHICH APPLY TO ALL PROCESSES
C

```

```

PR 56290
PR 56300
PR 56310
PR 56320
PR 56330
PR 56340
****
PR 56720
PR 56730
PR 56740
PR 56750
PR 56760
PR 56770
PR 56780
****
****
PR 56350
PR 56390
PR 56400
****
PR 56420
PR 56430
****
****
PR 56470
PR 56480
****
PR 56500
PR 56510
PR 56520
PR 56530
****
PR 56550
PR 56560
PR 56570
PR 56580
****
****
PR 56630
PR 56640
PR 56650
****
****
****
****
****
****
PR 56700
PR 56710
PR 56790
PR 56800
****
PR 56820
PR 56830
****
PR 56850
PR 56860
PR 56870
PR 56880
****
PR 56900
PR 56910
PR 56920
PR 56930
PR 56940
PR 57000

```

```

      GO TO (95,96),NFEED
95  XC(48)=31.00
      GO TO 97
96  XC(48)=3000.00
97  CONTINUE
      XC(49)=25.00
C
      XC(50)=2.64E-7
C
      XC(54)=.0200
C
      XC(55)=.02500
C
      XC(56)=.0800
C
      XC(58)=.00700
C
      XC(60)=.100
C
      XC(61) = .0100
C
      XC(62) = .2500
C
      IF(IFLIP .EQ. 0) GO TO 100
      IF((PROC .NE. MSF) .AND. (PROC .NE. VTE)) GO TO 400
100 CONTINUE
C**
C****  CGST FACTORS WHICH APPLY TO BOTH MSF AND VTE PROCESSES
C**
      IF(VOLSTL .LT. 5.00) GO TO 110
      XC(9) =(USTLRF(ASTLRF)*ASTLRF +USTLFL(ASTLFL)*ASTLFL
1      +USTLEW(ASTLEW)*ASTLEW +USTLIW(ASTLIW)*ASTLIW
2      +USTLIF(VOLSTL)*VOLSTL +USTLTR(ASTLTR)*ASTLTR
3      +USTLPH(ASTLPH)*ASTLPH)/VOLSTL
110 CONTINUE
C
      IF(VOLCNC .LT. 5.00) GO TO 120
      XC(10) =(UCNCRF(ACNCRF)*ACNCRF +UCNCFL(ACNCFL)*ACNCFL
1      +UCNCEW(ACNCEW)*ACNCEW +UCNCIW(ACNCIW)*ACNCIW
2      +UCNCIF(VOLCNC)*VOLCNC +UCNCTR(ACNCTR)*ACNCTR
3      +UCNCPH(ACNCPH)*ACNCPH)/VOLCNC
120 CONTINUE
C
      XC(11) = UEXCAV(AEXCAV)
C
      XC(12) = UMISCI(PLSZMG)
C
      XC(13) = UWEIRS(AWEIRS)
C
      XC(17) = UCPAUP(PLSZMG)
C
      XC(20)=UCINSL(GPMO,DINTAK,TRAINS,ENPIPE,PIPELN)
C
      XC(24) = UCPLPF(PLSEA,GPMO,GPMP,PLPRD,TRAINS)
C
      XC(25) = UCTRPF(PLSZMG,TRAINS,LEV,REJLEN)
C
      XC(26) = UC8HPF(ENBH,GPMH,LEV)
C
      XC(27) = UCVNTD(GPMB+GPMP,PLSZMG)
C
      GO TO (121,122),NFEED
121 CONTINUE
      XC(30) =(UCADCT(TNACDY,TRAINS)*TNACDY+UCAFSS(GPMB+GPMP,TRAINS)*
1(GPMB+GPMP)
1      +UCCHLG(GPMO)*GPMO)/PLSZMG +UCPAUX(PLSZMG)
      GO TO 123
122 XC(30)=(UCAFSS(GPMB+GPMP,TRAINS)*(GPMB+GPMP)
1      +UCCHLG(GPMO)*GPMO)/PLSZMG +UCPAUX(PLSZMG)

```

```

****
****
****
****
****
PR 57950
****
PR 58010
****
PR 57030
****
PR 57060
****
PR 57090
****
PR 58130
****
PR 57120
PR 57140
PR 57150
****
PR 57180
PR 57190
PR 57200
PR 57210
PR 57220
PR 57230
PR 57240
PR 57260
PR 57270
PR 57280
PR 57290
PR 57300
PR 57310
PR 57320
PR 57340
PR 57350
PR 57360
PR 57370
PR 57380
PR 57390
PR 57400
PR 57420
PR 57430
PR 57450
PR 57460
PR 57480
PR 57490
PR 57510
PR 57520
PR 57540
PR 57550
PR 57570
PR 57580
PR 57600
PR 57610
PR 57630
PR 57640
PR 57660
PR 57670
****
****
****
****
****
****
****
****

```

```

123 CONTINUE
C      XC(32) = UCI(PLSZMG,TRAINS)
C      GO TO (130,140),NFEE0
130 XC(36)=UCDEA(GPMB+GPMP,TRAINS)+UCDCR(GPMB+GPMP,TRAINS)
    GO TO 150
140 XC(36)=UCDEA(GPMB+GPMP,TRAINS)
150 XC(200)=UCSJAE(X0(205),TRAINS)
C      XC(4J) = UCBHSH(BMSURF,BHVOL,1935.D0,6526.3D0)
C      XC(42)= UCSITS(ACRES)
C      XC(43) = UCBLCR(PLSZMG)
C      XC(45)=UNHEAC(1S)
C      XC(46)= UFHEAC(1S)
C      XC(51) = 8.5D-7
C      XC(52) = 7.05D-7
C      XC(57) = UCCPAN(PLSZMG)
C      XC(210)=.70D0
C      IF(IFLIP.EQ. 0) GO TO 200
C      IF(PROC.NE. MSF) GO TO 300
200 CONTINUE
C**
C****  COST FACTORS WHICH APPLY TO MSF PROCESS ONLY
C**
C      XC(1) = 1.849D0
C      XC(2) = 2.552
C      XC(3) = (UCSHET(TSTH,APTSE)*ENITSE +UCSHET(.5*TSTH,APTSE)*ENSUPE
1          +UCSHET(3.0833*TSTH,APTSE)*2.*BNCLS*ENKSS
2          +UCSHET(TSTH,APTSR)*ENITSR +UCSHET(.5*TSTH,APTSR)*ENSUPR
3          +UCSHET(3.0833*TSTH,APTSR)*2.*ENRJS*BNCLS)/TSAREA
C      XC(4) = ((UCDRIL(TSTH,DOE)*ENITSE +UCDRIL(.5*TSTH,DOE)*ENSUPE
1          +UCDRIL(3.0833*TSTH,DOE)*2.*ENRJS*BNCLS)*ENE/BNCLS
2          + (UCDRIL(TSTH,DOR)*ENITSR +UCDRIL(.5*TSTH,DOR)*ENSUPR
3          +UCDRIL(3.0833*TSTH,DOR)*2.*ENRJS*BNCLS)*RNR/BNCLS)/HOLES
C      TX=2.*ENRJS
C      TY=2.*ENRJS
C      XC(5) = (UCTSIN(TSTH,APTSE,940.D0,ENITSE)*ENITSE
1          +UCTSIN(.5*TSTH,APTSE,937.D0,ENSUPE)*ENSUPE
2          +UCTSIN(3.0833*TSTH,APTSE,80.0D0,TX*BNCLS)*TX*BNCLS
3          +UCTSIN(TSTH,APTSR,20.D0,ENITSR)*ENITSR
4          +UCTSIN(.5*TSTH,APTSR,256.D0,ENSUPR)*ENSUPR
5          +UCTSIN(3.0833*TSTH,APTSR,40.D0,TY*BNCLS)*TY*BNCLS)/TSAREA
C      XC(6) = (UCTUIN(116.86D6,ELE*ENE)*ELE*ENE
1          +UCTUIN(7.536D6,RLR*RNR) *RLR*RNR)/(ELE*ENE+RLR*RNR)
C      XC(7) = (UCDRIL(3.0833*TSTH,DOE)*TX*ENE
1          +UCDRIL(3.0833*TSTH,DOR)*TY*RNR)/(ENE+RNR)
C      XC(15)=(UCPUMP(GPMD/TRAINS,HDEL)*GPMD
1          +UCPUMP(GPMR/TRAINS,HREC)*GPMR
2          +UCPUMP(GPMP/TRAINS,HPR) *GPMP
3          +UCPUMP(GPMB/TRAINS,HBL) *GPMB
4          +UCPUMP(GPMD/TRAINS,HDEA)*GPMD)/
5          (GPMD+GPMR+GPMP+GPMB+GPMD)

```

```

****
PR 57710
PR 57730
PR 57740
****
****
****
****
****
PR 57770
PR 57790
PR 57800
PR 57820
PR 57830
PR 57850
PR 57860
PR 57880
PR 57890
****
PR 57920
PR 57980
****
PR 58040
****
PR 58070
PR 58090
****
PR 58100
PR 58140
PR 58150
PR 58160
PR 58170
PR 58180
PR 58190
****
PR 58220
****
PR 58250
PR 58270
****
PR 58290
****
PR 58310
PR 58330
****
PR 58350
****
PR 58370
****
****
PR 58390
PR 58400
****
PR 58420
PR 58430
****
PR 58450
PR 58470
PR 58480
PR 58490
PR 58510
PR 58520
PR 58530
PR 58550
PR 58560
PR 58570
PR 58580
PR 58590
PR 58600

```

```

C      XC(16) =(UCMOTR(HPDEL,RPMD)*HPDEL +UCMOTR(HPREC,RPMR)*HPREC      PR 58610
1      +UCMOTR(HPPRD,RPMP)*HPPRD +UCMOTR(HPBLD,RPMB)*HPBLD      PR 58630
2      +UCMOTR(HPDEA,RPMM)*HPDEA)/(HPDEL+HPREC+HPPRD+HPBLD+HPDEA) PR 58640
C      XC(18) =UCPPIT(GPMR+GPMP+GPMB+GPMD)      PR 58650
C      GPM1 = DMAX1(1.00,GPMO-GPMD)      PR 58660
C      XC(23) =(UCVALV(GPMO/TRAINS)*GPMO +UCVALV(GPMD/TRAINS)*GPMD      PR 58680
1      +2.*UCVALV(GPMR/TRAINS)*GPMR +UCVALV(GPM1/TRAINS)*GPM1      PR 58690
2      +2.*UCVALV(GPMB/TRAINS)*GPMB      PR 58710
3      +3.*UCVALV(GPMP/TRAINS)*GPMP +2.*UCVALV(GPMH/ENBH)*GPMH      PR 58720
4      /(2.*(GPMO+GPMR+GPMB+GPMH) +3.*GPMP)      PR 58730
C      XC(34) = 1.0-3*UCEDK(PO,TRAINS)      PR 58740
C      XC(38)= 2.552      PR 58750
C      HLH = AH/(HMH*PI*DOH/12.)      PR 58760
C      ENSUPH=.15*HLH*ENBH/DOH      PR 58770
C      XC(215)=UCSHET(3.0833*TSTH,APTSH)*2.*ENBH+      PR 58790
1      UCSHET(0.5*TSTH,APTSH)*ENSUPH      PR 58800
C      XC(216)=(UCDRIL(3.0833*TSTH,DOH)*2.+      PR 58830
1      UCDRIL(0.5*TSTH,DOH )*ENSUPH/ENBH)*HMH      PR 58840
C      XC(217)=UCTSIN(3.0833*TSTH,APTSH,100.00,2.*ENBH)*2.*ENBH+      PR 58850
1      UCTSIN(0.5*TSTH,APTSH,1000.00,ENSUPH)*ENSUPH      PR 58860
C      XC(218)=UCTUIN(100.06,HMH*HLH)*HMH*HLH      PR 58870
C      XC(219)=UCDRIL(3.0833*TSTH,DOH )*HMH*2.      PR 58880
C      XC(39)=(XC(215)+XC(216)+XC(217)+XC(218)+XC(219))/AH      PR 58890
C      RETURN      PR 58900
300 CONTINUE      PR 58910
C**      COST FACTORS WHICH APPLY TO VTE PROCESS ONLY      PR 58920
C****      PR 58930
C**      XC(63) = 3.77600      PR 58940
C      XC(64) = UCSHET(1.00,1.00)      PR 58950
C      XC(65) = UCDRIL(1.00,ODVE)      PR 58960
C      XC(66) = UCTUIN(2.61406,TOTNVE*LVE)      PR 58970
C      XC(67) = 2.*UCTSIN(1.00,VETSA/(2.*ANE*TRAINS),60.00,2.*ANE*TRAINS) PR 58980
C      XC(68) = 1.89900      PR 58990
C      XC(69) = (UCTUIN(116.8606,LPH*NTPH)*LPH*NTPH      PR 59000
1      +UCTUIN(7.53606,LCON*NCON)*LCON*NCON)/      PR 59010
2      (LPH*NTPH + LCON*NCON)      PR 59020
C      TX=2.*ENRSS      PR 59030
C      XC(70) =(UCSHET(TSTH,APTSEP)*ENITSE +UCSHET(.5*TSTH,APTSEP)*ENSUPEPR 59170
1      +UCSHET(3.0833*TSTH,APTSEP)*TX*BNCLS      PR 59180
2      +UCSHET(.5*TSTH,APTSCN)*ENSUPR      PR 59190
3      +UCSHET(3.0833*TSTH,APTSCN)*2.*TRAINS)/TSAREA      PR 59200
C      XC(71) =(UCDRIL(TSTH,ODPH)*ENITSE +UCDRIL(.5*TSTH,ODPH)*ENSUPEPR 59210
1      +UCDRIL(3.0833*TSTH,ODPH)*TX*BNCLS)*NTPH/BNCLS      PR 59220
2      +(UCDRIL(.5*TSTH,ODCON)*ENSUPR      PR 59230
3      +UCDRIL(3.0833*TSTH,ODCON)*2.*TRAINS)*NCON/TRAINS )/HOLES      PR 59240
C      XC(72) = (UCTSIN(TSTH,APTSEP,940.00,ENITSE)*ENITSE      PR 59250
1      +UCTSIN(.5*TSTH,APTSEP,937.00,ENSUPE)*ENSUPE      PR 59260
2      +UCTSIN(3.0833*TSTH,APTSEP,40.00,TX*BNCLS)*TX*BNCLS      PR 59270
3      +UCTSIN(.5*TSTH,APTSCN,256.00,ENSUPR)*ENSUPR      PR 59280
4      +UCTSIN(3.0833*TSTH,APTSCN,40.00,2.*TRAINS)*2.*TRAINS)      PR 59290
5      /TSARFA      PR 59300
C      XC(73) = (UCDRIL(3.0833*TSTH,ODPH)*NTPH      PR 59310
1      +UCDRIL(3.0833*TSTH,ODCON)*NCON)/(NTPH +NCON)      PR 59320

```

400 RETURN
END

APPENDIX J

CHANGES MADE IN SUBROUTINE COSTM

	SUBROUTINE COSTM	PR 22740
	IMPLICIT REAL*8(A-H,O-Z)	PR 22750
C		PR 22760
	DOUBLE PRECISION MODU	PR 22770
	DOUBLE PRECISION LEV,LF2	PR 22780
C		PR 22790
	COMMON/BLOCM1/ DIE, DIH, DIR, DOE, DOH, PR 22800	
1	DOR, ELE, ENE, RLR, RNR, HDEL, PR 22810	
2	HREC, APTSR, ENITSR, PR 22820	
	COMMON/BLOCM2/ P, Q, AH, AK, AN, PR 22830	
1	AK, FF, GE, GH, GR, HD, PR 22840	
2	PB, PE, QX(5), RP, SE, SH, PR 22850	
3	SK, TK, VE, VH, VR, WC, PR 22860	
4	AME, ATN, BPX(5), CCF, HIH, HLH, PR 22870	
5	HNH, HOH, OMX(5), PHE, PO3, RSE, PR 22880	
6	RSH, RSR, TC1, THF, TKX(5), TMC, PR 22890	
7	TME, TPE, UEX(5), UME, UMH, WPL, PR 22900	
8	BKTE, BKTH, BKTR, DTLS(5), ELEX(5), HLEX(5), PR 22910	
9	HOEX(5), MODU, RGE1, ROE2, APTSE, BDEPH, PR 22920	
+	CAPI1, HEADE, HEADH, HEADR, POBLD, PODEL, PR 22930	
A	POPRD, SUBEX(5), WCOLD, WMODC, WMODH, BHSHEL, PR 22940	
B	CSLTBH, CSLTBP, HOTLEN, HRECOV, HREJCT, RECOLN, PR 22950	
C	VAPSPC, WPRTRY, POREC, PR 22960	
	COMMON/BLOCM3/ EA, ES, CC1, CC2, EAL, PR 22970	
1	EA2, EEC, HC1, HC2, OC1, OC2, PR 22980	
2	PMC, TC2, VPC, BHC1, BHC2, CIBC, PR 22990	
3	DEA1, DEA2, EEC1, EEC2, PMC1, PR 23000	
4	SITE, SMAP, VPC1, VPC2, WAIT, AMSC1, PR 23010	
5	AMSC2, CAPI2, CAPI3, CAPI4, CIBC1, CIBC2, PR 23020	
6	SITE1, SITE2, WAIT1, WAIT2, CHMPTC, CHMPT1, PR 23030	
7	CHMPT2, CINSTC, CINST1, CINST2, DEACST, POCST1, PR 23040	
8	POCST2, RATEIN, RETUB1, RETUB2, SMAPPH, PR 23050	
9	CD, BHC, ES1, ES2, PR 23060	
	COMMON/COMNAM/ AJ, CB, CO, CP, CR, PR 23070	
1	HB, PI, PO, TB, TP, PR 23080	
2	TS, WB, WF, WO, WP, WR, PR 23090	
3	AXJ, HBL, HPR, LEV, LF2, TCF, PR 23100	
4	ENBH, GPMB, GPMO, GPMH, GPMO, GPMP, PR 23110	
5	GPMR, HDEA, RPMO, RPMH, RPMH, RPMP, PR 23120	
6	RPMR, TSTH, WHOT, YEAR, ACRES, BHVOL, PR 23130	
7	BLOGS, BNDLS, HOLES, HPBLD, HPDEA, HPDEL, PR 23140	
8	HPPRD, HPREC, PLPRD, PLSEA, PODEA, ACNCEW, PR 23150	
9	ACNCFL, ACNCIW, ACNCPH, ACNCRF, ACNCTR, AEXCAV, PR 23160	
+	ASTLEW, ASTLFL, ASTLIW, ASTLPH, ASTLRF, ASTLTR, PR 23170	
A	AWEIRS, BHSURF, DINTAK, ENITSE, ENPIPE, ENSUPE, PR 23180	
B	ENSUPR, PIPELN, PLSZMG, REJLEN, STLLN, STLTMP, PR 23190	
C	TNACDY, TRAINS, TSAREA, VOLCNC, VOLSTL, WOCEAN, PR 23200	
	COMMON/BLOCK6/ FC, PR 23210	
	COMMON/BLOC13/ XO, PR 23220	
	COMMON/BLOC14/ XC, PR 23230	
	COMMON/SHARE/ IFLIP, ISPT, PR 23240	
C		PR 23250
	DIMENSION XC(300), PR 23260	
	DIMENSION XC(500), FC(500), PR 23270	
C		PR 23280
	EQUIVALENCE (AE,AME), PR 23290	
	EQUIVALENCE (SMAP,SSMAP),(AJ,ASJ),(RATEIN,RTEIN), PR 23300	
	DATA PROC/'MSF'/, PR 23310	
C		PR 23320
	CALL PRICES(PROC), PR 23330	
	DO 100 J=1,300, PR 23340	
	XC(J) = XC(J) * FC(J), PR 23350	
100	CONTINUE, PR 23360	
C		PR 23370
	IF(IFLIP.GT. 1) GO TO 120, PR 23380	

```

C**      SMALL PLANT COST FACTORS
FEA = .89273800*(FF/10.)**(-.1332870-1)
FES = .10244201*(FF/10.)**(-.27393900)
FPMC = .11269301*(FF/10.)**(-.2687310-1)
FVPC = .14114301*(FF/10.)**(-.10426300)
FCHMPT = .60358600*(FF/10.)**(-.30953000)
FINSTC = .94309900*(FF/10.)**(-.71686200)
FEEC = .97491500*(FF/10.)**(-.1059920-1)
FDEA = .17580101*(FF/10.)**(-.36116300)
FBHC = .95267200*(FF/10.)**(-.23526300)
C**      TUBING REPLACEMENT FACTORS
CALL TUBREP(WPL,CSLTBP,XC(60),SMAPPP)
CALL TUBREP(WPL,CSLTBH,XC(60),SMAPPH)
120 CONTINUE
C****
C      CALCULATE COST OF COMPONENTS, $ - DIRECT
C**
      TSHETS = XC(3) * TSAREA + XC(4) * HOLES + XC(5) * TSAREA
      TUBING = XC(1) * AME + XC(2) * AR + XC(6) * (ELE * ENE + RLR * RNR)
      + XC(7) * (ENE + RNR)
1      EA = TSHETS + TUBING
      ES = XC(9) * VOLSTL + XC(10) * VOLCNC + XC(11) * (ASTLFL + ACNCFL)
      + XC(12) * FF + XC(13) * AWEIRS
      PUMPS = XC(15) * (GPMO + GPMR + GPMP + GPMB + GPMH)
      PMOTR = XC(16) * (HPDEL + HPREC + HPPRD + HPBLD + HPDEA) * TRAINS
      PTAUX = XC(17) * FF + XC(18) * (GPMR + GPMP + GPMB + GPMH)
      PMC = PUMPS + PMOTR + PTAUX
      WAIT = XC(20) * GPMO
      VALVES = XC(23) * (2. * (GPMO + GPMR + GPMB + GPMH) + 3. * GPMP)
      PLNTPF = XC(24) * GPMO
      TRANPF = XC(25) * TRAINS
      BHTRPF = XC(26) * GPMH
      VPC = VALVES + PLNTPF + TRANPF + BHTRPF + XC(27) * (GPMB + GPMP)
      CHMPTC = XC(30) * FF
      IF(FF .GT. X0(80)) CHMPTC = CHMPTC + XC(29) * TNACDY
      CINSTC = XC(32) * FF
      EEC = XC(34) * PU * 1.03
      DEACST = XC(36) * (GPMB + GPMP) + XC(200) * X0(205)
      BHTUB = (XC(38) + XC(39)) * AH
      BHSHEL = XC(40) * BHSURF * ENBH
      BHC = BHTUB + BHSHEL
      SITE = (XC(31) + XC(42)) * ACRES
      CIBC = XC(43) * FF
      IF(FF .GT. X0(82)) GO TO 130
C      CORRECT CAPITAL COSTS TO SMALL PLANT RANGE
      EA = EA * FEA
      ES = ES * FES
      PMC = PMC * FPMC
      VPC = VPC * FVPC
      CHMPTC = CHMPTC * FCHMPT
      CINSTC = CINSTC * FINSTC
      EEC = EEC * FEEC
      DEACST = DEACST * FDEA
      BHC = BHC * FBHC
130 CONTINUE
C
C      DIRECT CAPITAL COST, MILLIONS OF $
CD = 1.0 - 6 * (EA + ES + PMC + WAIT + VPC + CHMPTC + CINSTC
      + EEC + DEACST + BHC + SITE + CIBC)
C****
C      CALCULATE HIGHER COST FACTOR
C**
      AXJ = 1.00
      CALL FNANCE(CD,ASJ,SSMAP,PSAJ,RTEIN,AJBR,WPL,YEAR)
      IF(FF .GT. X0(82)) GO TO 200
C      ADD SUPPLIERS BURDEN FOR SMALL PLANTS
      AXJ = ASJ / (AJBR * 1.06995)
      EA = EA * AXJ
      ES = ES * AXJ
      PMC = PMC * AXJ

```

PR 23390
 PR 23400
 PR 23410
 PR 23420
 PR 23430
 PR 23440
 PR 23450
 PR 23460
 PR 23470
 PR 23480
 PR 23490
 PR 23500
 PR 23510
 PR 23520
 PR 23530
 PR 23540
 PR 23550
 PR 23560
 PR 23570
 PR 23580
 PR 23590
 PR 23600
 PR 23610
 PR 23620
 PR 23630
 PR 23640
 PR 23650
 PR 23660
 PR 23670
 PR 23680
 PR 23690
 PR 23700
 PR 23710
 PR 23720
 PR 23730
 PR 23740
 PR 23750

 PR 23770
 PR 23780
 PR 23790
 PR 23800
 PR 23810
 PR 23820
 PR 23830
 PR 23840
 PR 23850
 PR 23860
 PR 23870
 PR 23880
 PR 23890
 PR 23900
 PR 23910
 PR 23920
 PR 23930
 PR 23940
 PR 23950
 PR 23960
 PR 23970
 PR 23980
 PR 23990
 PR 24000
 PR 24010
 PR 24020
 PR 24030
 PR 24040
 PR 24050
 PR 24060
 PR 24070
 PR 24080

WAIT = WAIT*AXJ	PR 24090
VPC = VPC*AXJ	PR 24100
CHMPTC = CHMPTC*AXJ	PR 24110
CINSTC = CINSTC*AXJ	PR 24120
EEC = EEC*AXJ	PR 24130
DEACST = DEACST*AXJ	PR 24140
BHC = BHC*AXJ	PR 24150
SITE = SITE*AXJ	PR 24160
CIBC = CIBC*AXJ	PR 24170
CD=1.D-6*(EA+ES+PMC+WAIT+VPC+CHMPTC+CINSTC	PR 24180
1 +EEC+DEACST+BHC+SITE+CIBC)	PR 24190
ASJ = AJBR	PR 24200
PSAJ = SSMAP*ASJ	PR 24210
200 CONTINUE	PR 24220
C	PR 24230
C DIRECT + INDIRECT CAPITAL, \$	PR 24240
CAP11 = CD *1.0D6 * ASJ	PR 24250
C SPECIFIC INVESTMENT, \$/GPD	PR 24260
CAP12 = CAP11/(FF*1D6)	PR 24270
C****	PR 24280
C CALCULATE COST OF COMPONENTS, \$/YEAR	PR 24290
C**	PR 24300
EA2 = EA*PSAJ	PR 24310
ES2 = ES * PSAJ	PR 24320
PMC2 = PMC * PSAJ	PR 24330
WAIT2 = WAIT*PSAJ	PR 24340
VPC2 = VPC * PSAJ	PR 24350
CHMPT2 = CHMPTC * PSAJ	PR 24360
CINST2 = CINSTC * PSAJ	PR 24370
EEC2 = EEC * PSAJ	PR 24380
DEA2 = DEACST * PSAJ	PR 24390
BHC2 = BHC * PSAJ	PR 24400
SITE2 = SITE * PSAJ	PR 24410
CIBC2 = CIBC * PSAJ	PR 24420
RETUB2 = EA*SMAPPP + BHTUB*SMAPPH	PR 24430
C****	PR 24440
C CALCULATE COST OF COMPONENTS, CENTS/KGAL	PR 24450
C**	PR 24460
CFG = .365*LF2 *FF *1D4	PR 24470
C	PR 24480
EA1 = EA2/CFG	PR 24490
ES1 = ES2/CFG	PR 24500
PMC1 = PMC2/CFG	PR 24510
WAIT1 = WAIT2/CFG	PR 24520
VPC1 = VPC2/CFG	PR 24530
CHMPT1 = CHMPT2/CFG	PR 24540
CINST1 = CINST2/CFG	PR 24550
EEC1 = EEC2/CFG	PR 24560
DEA1 = DEA2/CFG	PR 24570
BHC1 = BHC2/CFG	PR 24580
SITE1 = SITE2/CFG	PR 24590
CIBC1 = CIBC2/CFG	PR 24600
RETUB1 = RETUB2/CFG	PR 24610
C	PR 24620
C COST OF CAPITAL ITEMS, CENTS/KGAL	PR 24630
CAP13 = EA1+ES1+PMC1+WAIT1+VPC1+CHMPT1+CINST1+EEC1+DEA1+BHC1+SITE1	PR 24640
1 +CIBC1	PR 24650
C COST OF CAPITAL ITEMS, \$/YEAR	PR 24660
CAP14 = CAP13*CFG	PR 24670
C****	PR 24680
C CALCULATE OPERATING COSTS	PR 24690
C**	PR 24700
C OPERATING COSTS, \$/YEAR	PR 24710
HC2 = 8.76*LF2*WP/RP*XC(45)	PR 24720
IF(FF .LT. X0(81)) HC2 = HC2*XC(46)/XC(45)	PR 24730
ACID = 365.*LF2*TNACDY*XC(49)	PR 24740
IF(FF .LE. X0(80)) ACID = ACID*XC(48)/XC(49)	PR 24750
CLORIN = 8760.*WOCEAN*LF2*XC(50)	PR 24760
CAUSTC = 8760.*(WB+WP)*LF2*XC(51)	PR 24770
DEFGM = 8760.*(WB+WP)*LF2*XC(52)	PR 24780

CC2 = ACID + CLORIN + CAUSTIC + DEFOM	PR 24790
POCST2=8760.*LF2*PO*XC(54)*1000.	****
IF(FF .LT. XD(81)) POCST2 = POCST2*XC(55)/XC(54)	PR 24810
OC2 = XC(57)*FF	PR 24820
AMSC2 = XC(58) * CAPI1	PR 24830
C	PR 24840
C OPERATING COSTS, CENTS/KGAL	PR 24850
HC1 = HC2/CFG	PR 24860
CC1 = CC2/CFG	PR 24870
POCST1 = POCST2/CFG	PR 24880
UC1 = UC2/CFG	PR 24890
CC1=CC1+WB/WP	****
C ALLOWS 1 CENT/KGAL FOR REMOVING COPPER IONS FORM BRINE	****
CC2=CC1*CFG	****
AMSC1 = AMSC2/CFG	PR 24900
C	PR 24910
C COST OF PRODUCT WATER, CENTS/KGAL	PR 24920
XC(211)=8760.*LF2*XC(206)*XC(210)	****
XC(212)=XC(211)/CFG	****
TC1 = CAPI3 +AMSC1+POCST1+HC1+OC1+CC1+REFUB1	PR 24930
1 +XC(212)	****
C COST OF PRODUCT WATER, \$/YEAR	PR 24940
TC2 = TC1 * CFG	PR 24950
C****	PR 24960
RETURN	PR 24970
END	PR 24980

APPENDIX K

CHANGES MADE IN SUBROUTINE COSTV

```

SUBROUTINE COSTV
C*****
C      COST VARIABLES ARE OF THE FORM, 'NAME*', WHERE
C      * = Y FOR COST $/YEAR,
C      * = K FOR COST, CENTS/KGAL,
C      * = D FOR COST $ - DIRECT
C*****
C*****
C      IMPLICIT REAL*8(A-H,O-Z)
C
C      DOUBLE PRECISION LPH, LVE, IDBH, IDPH, LCON, NCON,
C      1 NTPH, IDCON
C      DOUBLE PRECISION KBH, KPH, KVE, LBH, MGD, NBH,
C      1 NPH, NVE, KCON, LMTD, LVEP, LMTDBH, LMTDCN
C      DOUBLE PRECISION INT, INSTRD, INSTRK, INSTRY, MAINTK, MAINTY
C      DOUBLE PRECISION LEV, LF2
C
C      COMMON/BLOCKV1/ ANE, HVE, LPH, LVE, ACON,
C      1 GPMV, HPVE, HSEA, IDBH, IDPH, LCON,
C      2 NCON, NTPH, IDBH, IDPH, ODPH, ODPH,
C      3 RPMV, HFEED, IDCON, ODPH, SUMWT, VETSA,
C      4 APTSCN, APTSEP, QVRHGT, TOTNVE, VEPHPS,
C      COMMON/BLOCKV2/ A(30), S, AE(30), QE, TC(30),
C      1 TE(30), TR, UE(30), UH(3), WM, WT(30),
C      2 ABH, APH, BPE(30), CIE(30), COE(30), DPE(30),
C      3 ELL, GBH, GPH, GPM, HQO, KBH,
C      4 KPH, KVE, LBH, MGD, NBH, NPH,
C      5 NVE(30), QPH, RBH, RPH, RVE, TOQ,
C      6 UBH, VBH, VPH, WPEX(30), BHLF, GCON,
C      7 HIBH, HIPH(3), HOBH, HOPH(3), KCON, LMTD(3),
C      8 LVEP, PHLF, QMSF(3), RCON, SUBF(3), TCON,
C      9 UCON, VCON, VLEN, VTLF, WOTH(30), ALFAE(30),
C      + CONLF, HICON, HCCON, HOTE1, PHHGT, POBLU,
C      A POPRO, POSEA, SURFF, VEHGT, WALVE, EFFSPC,
C      BELBNDL(30), HCOTCF, HCOTQO, HEADBH, HEADCN, HEADPH,
C      C LMTDBH, LMTDCN, PLNTLF, PODEAS, POFEED, SUMWPE,
C      D SUMMPH, TOTAVE, QESP, VEFEED(30), WBOOST, WDCOLD,
C      E NE, NTRN, IFEED, IRECYC, PR 13450
C      COMMON/BLOCKV3/ BHD, BHK, BHY, INT, PMD,
C      1 PMK, PMY, VPD, VPK, VPY, ACHR,
C      2 DEAD, DEAK, DEAY, ELEC, HEAT, SBOD,
C      3 SBCK, SBCY, CHENK, CHENY, HEATK, HEATY,
C      4 GPERK, OPERY, PLDIN, WAITD, WAITK, WAITY,
C      5 ANCCMP, CMCAPD, CMCAPK, CMCAPY, CNDSRD, CNDSRK,
C      6 CNDSTRY, ELECTD, ELECTK, ELECTY, INSTRD, INSTRK,
C      7 INSTRY, MAINTK, MAINTY, PHTUBD, PHTUBK, PHTUBY,
C      8 PLCAPD, PLCAPK, PLCAPY, POWERK, POWERY, RETUBK,
C      9 RETUBY, SHELLD, SHELLK, SHELLY, TOTALK, TOTALY,
C      + TOTOPK, TOTOPY, TREPBH, TREPCH, TREPPH, TREPVE,
C      A VETUBD, VETUBK, VETUBY, CGPD, PR 13570
C      COMMON/CONNAM/ AJ, CB, CO, CP, CR,
C      1 HB, PI, PO, TB, TO, TP,
C      2 TS, WB, WF, WO, WP, WR,
C      3 AXJ, HBL, HPR, LEV, LF2, TCF,
C      4 ENBH, GPMB, GPMH, GPMO, GPMY, GPMZ,
C      5 GPMR, HDEA, RPMB, RPMH, RPMY, RPMZ,
C      6 RPMR, TSTH, WHOT, YEAR, ACRES, BHVOL,
C      7 BLDGS, BNDLS, HOLES, HPBLD, HPDEA, HPDEL,
C      8 HPRPD, HPREC, PLPRD, PLSEA, PODEA, ACNCEW,
C      9 ACNCFL, ACNCIW, ACNCPH, ACNCRF, ACNCTR, AEXCAV,
C      + ASTLEW, ASTLFL, ASTLIW, ASTLPH, ASTLRF, ASTLTR,
C      A AWEIRS, BHSURF, DINTAK, ENITSE, ENPIPE, ENSUPE,
C      8 ENSUPR, PIPELN, PLSZMG, REJLEN, STLEN, STLIMP,
C      C TNACDY, TRAINS, TSAREA, VULCNC, VOLSTL, WDCOAN,
C      COMMON/BLOCK6/ FC

```



```

SHELLD = SHELLD*FES
PMD = PMD*FPMC
VPD = VPD*FVPC
CMCAPD = CMCAPD*FCHMPT
DEAD = DEAD*FDEA
CNDSRD = CNDSRD*FEA
BHD = BHD*FBHC
INSTRD = INSTRD*FINSTC
ELECTD = ELECTD*FEEC
108 CONTINUE
C
C***** DIRECT CAPITAL COST OF PLANT
PLCAPD = VETUBD +PHTUBD +SHELLD +PMD +WAITD +VPD +CMCAPD +DEAD
1 +CNDSRD +BHD +INSTRD +ELECTD +SBCD
DC = PLCAPD*1.D-6
C*****
C*****
C CALCULATE AJ, HIGHER COST FACTOR
AXJ = 1.C
CALL FNANCE(DC,AJ,ACHR,ANCOMP,INT,AJBR,PLNTLF,YEAR)
IF(MGD.GT. XO(82)) GO TO 110
C** ADD SUPPLIERS BURDEN FOR SMALL PLANTS
AXJ = AJ/(AJBR*1.06995)
VETUBD = VETUBD*AXJ
PHTUBD = PHTUBD*AXJ
SHELLD = SHELLD*AXJ
PMC = PMD*AXJ
WAITD = WAITD*AXJ
VPD = VPD*AXJ
CMCAPD = CMCAPD*AXJ
DEAD = DEAD*AXJ
CNDSRD = CNDSRD*AXJ
BHD = BHD*AXJ
INSTRD = INSTRD*AXJ
ELECTD = ELECTD*AXJ
SBCD = SBCD*AXJ
PLCAPD = VETUBD +PHTUBD +SHELLD +PMD +WAITD +VPD +CMCAPD +DEAD
1 +CNDSRD +BHD +INSTRD +ELECTD +SBCD
DC = PLCAPD*1.D-6
AJ = AJBR
ANCOMP = AJ*ACHR
110 CONTINUE
C*****
C***** PLANT COST, DIRECTS + INDIRECTS
PLDIN=AJ*PLCAPD
C*****
C CALCULATE COST OF COMPONENTS, $/YEAR
VETUBY=ANCOMP*VETUBD
PHTUBY=ANCOMP*PHTUBD
SHELLY=ANCOMP*SHELLD
PMY =ANCOMP*PMD
WAITY =ANCOMP*WAITD
VPY =ANCOMP*VPD
CMCAPY=ANCOMP*CMCAPD
INSTRY=ANCOMP*INSTRD
ELECTY=ANCOMP*ELECTD
DEAY =ANCOMP*DEAD
CNDSKY=ANCOMP*CNDSRD
BHY =ANCOMP*BHD
SBCY =ANCOMP*SBCD
PLCAPY=ANCOMP*PLCAPD
RETUBY = TREPVE*VETUBD +TREPPI*PHTUBD +TREPPI*CNDSRD
1 +(XC(133)+XC(126))*ABH*TREPBH
C*****
C*****
C COST OF COMPONENTS, CENTS/KGAL
CKGAL = 1.05/(PLF*MGD*365.D6)
PHTUBK=CKGAL*PHTUBY
VETUBK=CKGAL*VETUBY
SHELLK=CKGAL*SHELLY

```

```

PR 14410
PR 14420
PR 14430
PR 14440
PR 14450
PR 14460
PR 14470
PR 14480
PR 14490
PR 14500
PR 14510
PR 14520
PR 14530
PR 14540
PR 14550
PR 14560
PR 14570
PR 14580
PR 14590
PR 14600
PR 14610
PR 14620
PR 14630
PR 14640
PR 14650
PR 14660
PR 14670
PR 14680
PR 14690
PR 14700
PR 14710
PR 14720
PR 14730
PR 14740
PR 14750
PR 14760
PR 14770
PR 14780
PR 14790
PR 14800
PR 14810
PR 14820
PR 14830
PR 14840
PR 14850
PR 14860
PR 14870
PR 14880
PR 14890
PR 14900
PR 14910
PR 14920
PR 14930
PR 14940
PR 14950
PR 14960
PR 14970
PR 14980
PR 14990
PR 15000
PR 15010
PR 15020
PR 15030
PR 15040
PR 15050
PR 15060
PR 15070
PR 15080
PR 15090
PR 15100

```

```

PMK      =CKGAL*PMY
WAITK    =CKGAL*WAITY
VPK      =CKGAL*VPY
CMCAPK   =CKGAL*CMCAPY
INSTRK   =CKGAL*INSTRY
ELECTK   =CKGAL*ELECTY
DEAK     =CKGAL*DEAY
CNDSRK   =CKGAL*CNDSRY
BHK      =CKGAL*BHY
SBCK     =CKGAL*SBCY
PLCAPK   =CKGAL*PLCAPY
RETUBK   =CKGAL*RETUBY
C*****
CGPD= PLDIN/(MGD*1.06)
C*****
C*****
C          CALCULATE OPERATING COSTS
C*****
HEAT = XC(45)
IF(MGD .LT. XO(81)) HEAT = XC(46)
HEATY=HEAT*(QE+QPH)*PLF*8760.00-6
ACID = 365.*PLF *TNACDY* XC(49)
IF(MGD .LE. XO(80)) ACID =ACID*XC(48)/XC(49)
CLORIN = 8760.* WOCEN*PLF * XC(50)
CAUSTC = 8760.*(WB+WP)*PLF * XC(51)
DEFOM  = 8760.*(WB+WP)*PLF * XC(52)
CHEMY  = ACID+ CLORIN+ CAUSTC+ DEFOM
ELEC   = XC(54)
IF(MGD .LT. XO(81)) ELEC = XC(55)
POWERY = 8.7606*ELEC*PO
OPERY  = XC(57) *MGD
MAINTY = XC(58) * PLDIN
HEATK  =CKGAL*HEATY
CHEMK  =CKGAL*CHEMY
POWERK =CKGAL*POWERY
OPERK  =CKGAL*OPERY
MAINTK =CKGAL*MAINTY
C*****
C          TOTAL OPERATING CUST
TOTOPY=HEATY+CHEMY+POWERY+OPERY+MAINTY
IUTOPK=CKGAL*TOTOPY
C*****
C          TOTAL
XC(211)=8760.*LF2*XC(206)*XC(210)
TOTALY=PLCAPY+RETUBY+TOTOPY
1 +XC(211)
XC(212)=XC(211)*CKGAL
TOTALK=PLCAPK+RETUBK+TOTOPK
1 +XC(212)
RETURN
END

```

```

PR 15110
PR 15120
PR 15130
PR 15140
PR 15150
PR 15160
PR 15170
PR 15180
PR 15190
PR 15200
PR 15210
PR 15220
PR 15230
PR 15240
PR 15250
PR 15260
PR 15270
PR 15280
PR 15290
PR 15300
PR 15310
PR 15320
PR 15330
PR 15340
PR 15350
PR 15360
PR 15370
PR 15380
PR 15390
PR 15400
PR 15410
PR 15420
PR 15430
PR 15440
PR 15450
PR 15460
PR 15470
PR 15480
PR 15490
PR 15500
PR 15510
PR 15520
PR 15530
****
PR 15540
****
****
PR 15550
****
PR 15560
PR 15570

```

APPENDIX L

CHANGES MADE IN SUBROUTINE FNANCE

	SUBROUTINE FNANCE(CD,ASJ,SSMAP,PSAJ,RTEIN,AJBR,WPL,YEAR)	PR 36940
	IMPLICIT REAL*8(A-H,O-Z)	
	DIMENSION XC(500)	PR 36960
	COMMON/BLOC14/ XC	PR 36970
C		PR 36980
C	OVERHEAD FOR DESIGN AND JOB SUPERVISION	PR 37010
C	AJSD = 'OAK RIDGE'	PR 37020
C	ABSD = 'BURNS AND ROE'	PR 37030
	AJSD = 1.05+.17582*DEXP(-2.089D-2*CD)	PR 37040
	ABSD = .4977*(AJSD-1.)+1.	PR 37050
	AJSDCT = AJSD	****
C	CONSTRUCTION TIME IN MONTHS	PR 37070
	TIME = 54.1*(1.-(.006*CD+1.1)**(-2.632))	PR 37080
C	INTEREST RATE	PR 37090
	RTEIN = XC(60)	PR 37100
C	INTEREST DURING CONSTRUCTION	PR 37110
	AJIC = 1.+.0399*TIME*RTEIN	PR 37120
C	ESCALATION DURING CONSTRUCTION	****
	AJESC=1.+.0434*TIME*XC(56)	****
C	UNUSUAL CONSTRUCTION EXPENSE AND CONTINGENCY	PR 37150
	AJFOR = 1.00+XC(62)	PR 37160
C	CWNERS CGST (TRAINING AND STARTUP)	PR 37170
	AJCWN = 1.019	PR 37180
C		PR 37190
C	HIGHER CGST FACTOR	PR 37200
C	ASJ = 'OAK RIDGE'	PR 37210
C	AJBR = 'BURNS AND ROE'	PR 37220
	ASJ = AJSDCT*AJIC*AJESC*AJFOR*AJOWN	PR 37230
	AJBR = ABSD*AJIC*AJESC	PR 37240
C		PR 37250
C	ANNUAL CHARGE FACTOR ON TOTAL CAPITAL	PR 37260
	SSMAP = XC(61)+RTEIN/(1.-1./(1.+RTEIN)**WPL)	PR 37270
C		PR 37280
C	ANNUAL CHARGE FACTOR ON DIRECT CAPITAL	PR 37290
	PSAJ = SSMAP *ASJ	PR 37300
C		PR 37310
	RETURN	PR 37320
	END	PR 37330

THIS PAGE
WAS INTENTIONALLY
LEFT BLANK

APPENDIX M

CHANGES MADE IN SUBROUTINE TITLER

SUBROUTINE TITLER			
CALLC('UNIT COST OF RECOVERY TUBING, \$/SQ.FT.	(MSF)',	1)PR	58200
CALLC('UNIT COST OF REJECT TUBING, \$/SQ FT	(MSF)',	2)PR	58230
CALLC('UNIT COST OF TUBE SHEETS, \$/SQ FT	(MSF)',	3)PR	58260
CALLC('UNIT COST OF HOLE DRILLING, \$/HOLE	(MSF)',	4)PR	58320
CALLC('UNIT COST OF INSTALLING TUBE SHEETS, \$/SQ FT	(MSF)',	5)PR	58380
CALLC('UNIT COST OF INSTALLING TUBING, \$/LINEAR FOOT	(MSF)',	6)PR	58460
CALLC('UNIT COST OF ROLLING TUBING, \$/TUBE	(MSF)',	7)PR	58500
CALLC('UNIT COST OF STEEL SHELL, \$/CUBIC FOOT	(MSF,VTE)',	9)PR	57250
CALLC('UNIT COST OF CONCRETE SHELL, \$/CUBIC FOOT	(MSF,VTE)',	10)PR	57330
CALLC('UNIT COST OF EXCAVATION FOR SHELL, \$/SQ FT	(MSF,VTE)',	11)PR	57410
CALLC('UNIT COST OF DEMISTERS +MISC EQUIP, \$/MGD	(MSF,VTE)',	12)PR	57440
CALLC('UNIT COST OF WEIRS, \$/SQ FT	(MSF,VTE)',	13)PR	57470
CALLC('UNIT COST OF PUMPS, \$/GPM	(MSF)',	15)PR	58540
CALLC('UNIT COST OF PUMP MOTORS, \$/HP	(MSF)',	16)PR	58620
CALLC('UNIT COST OF AUXILIARY PUMPS +DRIVES, \$/MGD	(MSF,VTE)',	17)PR	57500
CALLC('UNIT COST OF PUMP PITS, \$/GPM PIT FLOW	(MSF)',	18)PR	58670
CALLC('UNIT COST OF SUBMARINE LINE INTAKE, \$/GPM	(MSF,VTE)',	20)PR	57530
CALLC('UNIT COST OF VALVES, \$/GPM VALVE FLOW	(MSF)',	23)PR	58700
CALLC('UNIT COST OF PLANT PIPING AND FITTINGS, \$/GPM	(MSF,VTE)',	24)PR	57560
CALLC('UNIT COST OF TRAIN PIPING +FITTINGS, \$/TRAIN	(MSF,VTE)',	25)PR	57590
CALLC('UNIT COST OF BRINE HTR PIPING+FITTINGS, \$/GPM	(MSF,VTE)',	26)PR	57620
CALLC('UNIT COST OF VENT AND DRAIN PIPING, \$/GPM MU	(MSF,VTE)',	27)PR	57650
CALLC('UNIT COST OF CHEM,AIR, HYDRAULIC EQUIP, \$/MGD	(MSF,VTE)',	30)PR	57680
CALLC('UNIT COST OF INSTRUMENTATION, \$/MGD PRODUCT	(VTE,MSF)',	32)PR	57720
CALLC('UNIT COST OF ELECTRICAL DISTRIBUTION EQUIP., \$/KW	(MSF)',	34)PR	58780
CALLC('UNIT COST OF BRINE HEATER TUBING, \$/SQ FT	(MSF)',	38)PR	58810
CALLC('UNIT COST OF BH BUNDLE FABRICATION, \$/FT2 BH AREA	(MSF)',	39)PR	58840
CALLC('UNIT COST OF BRINE HEATER SHELL, \$/FT2 SHELL	(MSF,VTE)',	40)PR	57780
CALLC('UNIT COST OF SITE PREPARATION, \$/ACRE	(MSF,VTE)',	42)PR	57810
CALLC('UNIT COST OF BLDGS AND CRANES, \$/MGD	(MSF,VTE)',	43)PR	57840
CALLC('UNIT COST OF STEAM HEAT, NUCLEAR, \$/MMBTU	(VTE,MSF)',	45)PR	57870
CALLC('UNIT COST OF STEAM HEAT, FOSSIL, \$/MMBTU	(VTE,MSF)',	46)PR	57900
CALLC('UNIT COST OF 93PC H2SO4, OR PHOSPHATE, \$/TON	(ALL)',	48)PR	57930
CALLC('UNIT COST OF CHLORINE TREATMENT, \$/LB WATER	(ALL)',	50)PR	57990
CALLC('UNIT COST OF CAUSTIC TREATMENT, \$/LB WATER	(VTE,MSF)',	51)PR	58020
CALLC('UNIT COST OF DEFOAM + SULFITE TREAT., \$/LB	(VTE,MSF)',	52)PR	58050
CALLC('UNIT COST OF ELECTRICITY, NUCLEAR, \$/KWH	(ALL)',	54)PR	57010
CALLC('UNIT COST OF ELECTRICITY, FOSSIL, \$/KWH	(ALL)',	55)PR	57040
CALLC('ANNUAL ESCALATION RATE, FRACTION	(ALL)',	56)PR	57070
CALLC('UNIT COST OF O AND M LABOR, \$/YEAR PER MGD	(MSF,VTE)',	57)PR	58080
CALLC('UNIT COST OF MAINT.+SUPPLIES, \$/YR/\$ CAPITAL	(ALL)',	58)PR	58110
CALLC('INTEREST RATE	(ALL)',	60)PR	57100
CALLC('UNIT COST OF TAXES, INSURANCE, ETC, \$/YR/\$ CAPITAL	(ALL)',	61)PR	57130
CALLC('FRACTION OF CAPITAL FOR UNUSUAL CONST. EXPENSE	(ALL)',	62)PR	57160
CALLC('UNIT COST OF VERTICAL TUBE SURFACE, \$/SQ FT	(VTE)',	63)PR	58930
CALLC('UNIT COST OF VE TUBE SHEETS, \$/SQ FT	(VTE)',	64)PR	58960
CALLC('UNIT COST OF VE HOLE DRILLING AND ROLLING, \$/HOLE	(VTE)',	65)PR	58990
CALLC('UNIT COST OF INSTALLING VE TUBES, \$/FOOT	(VTE)',	66)PR	59020
CALLC('UNIT COST OF VE BUNDLE INSTALLATION, \$/BUNDLE	(VTE)',	67)PR	59050
CALLC('UNIT COST OF PREHEATER TUBING, \$/SQ FT	(VTE)',	68)PR	59080
CALLC('UNIT COST OF INSTALLING HORIZONTAL TUBING, \$/FT	(VTE)',	69)PR	59110
CALLC('UNIT COST OF HORIZONTAL TUBE SHEETS, \$/SQ FT	(VTE)',	70)PR	59160
CALLC('UNIT COST OF HOLE DRILLING, HORIZ. TUBES, \$/HOLE	(VTE)',	71)PR	59220
CALLC('UNIT COST OF INSTALLING HORIZ. TUBE SHEETS, \$/FT2	(VTE)',	72)PR	59280
CALLC('UNIT COST OF ROLLING HORIZONTAL TUBES, \$/TUBE	(VTE)',	73)PR	59360
CALLC('UNIT COST OF CONDENSER TUBING, \$/SQ FT	(VTE)',	74)PR	59400
CALLC('UNIT COST OF BRINE HEATER TUBING, \$/SQ FT	(VTE)',	126)PR	59430
CALLC('UNIT COST OF ELECTRICAL DISTRIBUTION EQPT, \$/KW	(VTE)',	127)PR	59460
CALLC('UNIT COST OF PUMPS, \$/GPM	(VTE)',	128)PR	59500
CALLC('UNIT COST OF PUMP MOTORS, \$/HP	(VTE)',	129)PR	59590
CALLC('UNIT COST OF PUMP PITS, \$/GPM	(VTE)',	130)PR	59670
CALLC('UNIT COST OF VALVES, \$/GPM	(VTE)',	131)PR	59700
CALLC('UNIT COST OF EFFECT PIPING, \$/EFFECT	(VTE)',	132)PR	59820
CALLC('UNIT COST OF BH BUNDLE FABRICATION, \$/FT2 BH AREA	(VTE)',	133)PR	59850
CALLC('COST OF SJAE SYSTEM, \$	(VTE,MSF)',	200)	

CALLC('UNIT COST OF EJECTOR STEAM,\$/MMBT	(MSF,VTE)',210)PR 58105
CALLC('UNIT COST OF EJECTOR STEAM, \$/MMBTU	(VTE,MSF)',210)
CALLC('ANNUAL COST OF EJECTOR STEAM, \$/YR	(VTE,MSF)',211)
CALLC('COST OF EJECTOR STEAM PER 1000 GAL, \$	(VTE,MSF)',212)
CALLC('COST OF BRINE HEATER TUBE SHEETS, \$	(MSF,VTE)',215)
CALLC('COST OF BRINE HEATER SHEETS HOLE DRILLING	(MSF,VTE)',216)
CALLC('COST OF BRINE HEATER SHEET INSTALLATION	(MSF,VTE)',217)
CALLC('COST OF BRINE HEATER TUBING INSTALLATION	(MSF,VTE)',218)
CALLC('COST OF BRINE HEATER TUBE ROLLING	(MSF,VTE)',219)
CALLC('UNIT COST OF NOZZLES	(VTE)',220)
CALLC('COST OF INSTRUMENTATION FOR ONE EFFECT	(VTE)',220)
RETURN	
END	

APPENDIX N

CHANGES MADE IN SUBROUTINE RITEM

```

SUBROUTINE RITEM(IOPT,IOUT,L)
  IMPLICIT REAL*8(A-H,O-Z)
C
DOUBLE PRECISION LAM,MSFID,LAMSTM
DOUBLE PRECISION MODU
REAL*8 LPHE
DOUBLE PRECISION LEV,LF2
C
COMMON/PINHAS/APTSH,ENRSS,ENRJS,LPHE,DUMDUM(16),NFEED,IIIIII(9)
COMMON/BLOC1/  DIE,      DIH,      DIR,      DUE,      DOH,
1  DOR,      ELE,      ENE,      RLR,      RNR,      HDEL,
2  HREC,      APTSR,    ENITSR
COMMON/BLOC2/  P,      Q,      AH,      AK,      AN,
1  AR,      FF,      GE,      GH,      GR,      HO,
2  PH,      PE,      QX(5),  RP,      SE,      SH,
3  SR,      TK,      VE,      VH,      VR,      WC,
4  AME,      ATN,      BPX(5), CCF,      HIH,      HLH,
5  HNH,      HOH,      OMX(5), PHE,      POJ,      RSE,
6  RSH,      RSR,      TCL,      THF,      TKX(5),  TMC,
7  TME,      TPE,      UEX(5),  UME,      UMH,      WPL,
8  BKTE,      BKTH,      BKTR,    DTLS(5),  ELEX(5),  HIEX(5),
9  HOEX(5),    MODU,      ROEL,      RUE2,      APTSE,      BDEPH,
+  CAPI1,      HEADE,      HEADH,      HEADR,      POBLD,      PODEL,
A  POPRD,      SUBEX(5),  WCOLD,      WMODC,      WMODH,      BHSHEL,
B  CSLTBH,      CSLTBP,  HOTLEN,      HRECOV,      HREJCT,      RECOLN,
C  VAPSPC,      WPRTRY,  POREC
COMMON/BLOC3/  EA,      ES,      CC1,      CC2,      EA1,
1  EA2,      EEC,      HC1,      HC2,      OC1,      OC2,
2  PMC,      TC2,      VPC,      BHC1,      BHC2,      CIBC,
3  DEAI,      DEAI,      EEC1,      EEC2,      PMC1,      PMC2,
4  SITE,      SMAP,      VPC1,      VPC2,      WAIT,      AMSC1,
5  AMSC2,      CAPI2,      CAPI3,      CAPI4,      CIBC1,      CIBC2,
6  SITE1,      SITE2,      WAIT1,      WAIT2,      CHMPTC,      CHMPT1,
7  CHMPT2,      CINSTC,  CINST1,  CINST2,      DEACST,      POCST1,
8  POCST2,      RATEIN,  RETUB1,  RETUB2,      SMAPPH,      SMAPPP,
9  CD,      BHC,      ES1,      ES2
COMMON/COMNAM/ AJ,      CB,      CU,      CP,      CR,
1  HB,      PI,      PO,      TB,      TO,      TP,
2  TS,      WB,      WF,      WO,      WP,      WR,
3  AXJ,      HBL,      HPR,      LEV,      LF2,      TCF,
4  ENBH,      GPMR,      GPMQ,      GPMH,      GPMO,      GPMP,
5  GPMR,      HDEA,      RPMR,      RPMQ,      RPMH,      RPMP,
6  RPMR,      TSTH,      WHUT,      YEAR,      ACRES,      BHVOL,
7  BLDGS,      BNDLS,      HULES,      HPBLD,      HPDEA,      HPDEL,
8  HPPRD,      HPREC,      PLPRD,      PLSEA,      PODEA,      ACNCEW,
9  ACNCFL,      ACNCIW,  ACNCPH,  ACNCRF,  ACNCTR,  AEXCAV,
+  ASTLEW,      ASTLFL,  ASTLIW,  ASTLPH,  ASTLRF,  ASTLTR,
A  AWEIRS,      BHSURF,  DINTAK,  ENITSE,  ENPIPE,  ENSUPE,
B  ENSUPR,      PIPELN,  PLSZMG,  REJLEN,  STLEN,   STLIMP,
C  TNACDY,      TRAINS,  TSAREA,  VOLCNC,  VOLSTL,  WOCEAN
COMMON/BLOC12/ XT
COMMON/BLOC13/ XO
COMMON/BLOC14/ XC
COMMON/NAME/ ANAME(10), AMONTH, IDAY, IYEAR
COMMON/DECKID/ MSFID(10), VTEID(10), EDID(10)
COMMON/IMPOSS/ IMPOSE,IMPOSR
C
DIMENSION XT(300),XO(300)
DIMENSION XC(500)
C
EQUIVALENCE (AE,AME) , (TC,TNC) , (TE,TNE) , (UE,UME) ,
I  (UH,UMH)
C****
C  SOME QUANTITIES FOR OUTPUT
C****

```

```

SITEC = SITE + CIBC
SITEC1= SITE1+ CIBC1
SITEC2= SITE2+ CIBC2
TOC2 = HC2 +CC2 + POCST2 +OC2 +AMSC2+XC(211)
TOC1 = HC1 +CC1 + POCST1 +OC1 +AMSC1 +XC(212)
EFF = XO(32)
LAMSTM = LAM(TS,PSTM,0.00,0.00)
WS = 1.03/RP*WP/LAMSTM
CDMM = CD*1.06
CPPPM = CP*1.006
WSMM = WS *1.0-6
WPM = WP *1.0-6
WBM = WB *1.0-6
WOM = WO *1.0-6
WCMM = (WC-WP-WB)* 1.0-6
WRMM = WR *1.0-6
WFM = WF *1.0-6
ENRK = 1.0-3 *DFLOAT(IFIX(SNGL(RNR)))
ENK = 1.0-3 *DFLOAT(IFIX(SNGL(ENE)))
ENHK = 1.0-3 *DFLOAT(IFIX(SNGL(HNH)))
ARKK = 1.0-3*AR
AEKK = 1.0-3*AE
AHKK = 1.0-3*AH
WOCMM = 1.0-6*WOCEAN
VOMTOT = (VCLSTL+VOLCNC)*1.0-6
HIE = (HIE(1)+ 4.*HIE(2) +HIE(3))/6.
HOE = (HOE(1)+ 4.*HOE(2) +HOE(3))/6.
UE = (UE(1) + 4.*UE(2) +UE(3) )/6.
SUBE=(SUBEX(1)+4.*SUBEX(2)+SUBEX(3))/6.
DTLSE =(DTLS(1)+4.*DTLS(2)+DTLS(3))/6.
OM1 = (OMX(1) +4.*OMX(2) +OMX(3))/6.
HIR = .5*(HIE(4) +HIE(5))
HOR = .5*(HOE(4) +HOE(5))
UR = .5*(UE(4) +UE(5))
SUBR =.5*(SUBEX(4)+SUBEX(5))
DTLSR=.5*(DTLS(4)+DTLS(5))
OM2 =.5*(OMX(4)+OMX(5))
UNARAE = EA/(AME+AR)
UNPUMP = XC(15)
UNDRVE = XC(16)
USHELV = ES/VOMTOT*1.0-6
UFC = XC(55)*100.00
IF(FF .GE. XO(81)) UFC = XC(54)*100.00
EXSTM = XC(46)*100.00
IF(FF .GE. XO(81)) EXSTM = XC(45)*100.00
EACHG = XC(1)
RACHG = XC(2)
HACHG = XC(38)
WPE = WF*PE
WPR = WP-WPE
TOTLEN = RECOLN+REJLEN
WALLE = XC(26)
STFEJ=XC(210)*100.00
EJC2=XC(211)
EJC1=XC(212)
WALLR = XC(27)
WALLH = XC(25)
ESTGL = (ELEX(1)+4.*ELEX(2)+ELEX(3))/6.
RSTGL = .5*(ELEX(4)+ELEX(5))
QEL = (QX(1)+4.*QX(2)+QX(3))/6.
QRL = .5*(QX(4) +QX(5))
BPKE = (BPX(1) +4.*BPX(2) +BPX(3))/6.
BPRR = .5*(BPX(4)+BPX(5))
POTCT = PO +PO3
PSAJ = AJ *SMAP
UNELCT = XC(34)
UNARHI = XC(38)+XC(39)
UNSHLS = XC(9)
UNSHLC = XC(10)

```

```

PR 66220
PR 66230
PR 66240
****
****
PR 66270
PR 66280
PR 66290
PR 66300
PR 66310
PR 66320
PR 66330
PR 66340
PR 66350
PR 66360
PR 66370
PR 66380
PR 66390
PR 66400
PR 66410
PR 66420
PR 66430
PR 66440
PR 66450
PR 66460
PR 66470
PR 66480
PR 66490
PR 66500
PR 66510
PR 66520
PR 66530
PR 66540
PR 66550
PR 66560
PR 66570
PR 66580
PR 66590
PR 66600
PR 66610
PR 66620
PR 66630
PR 66640
PR 66650
PR 66660
PR 66670
PR 66680
PR 66690
PR 66700
PR 66710
PR 66720
PR 66730
****
****
PR 66740
PR 66750
PR 66760
PR 66770
PR 66780
PR 66790
PR 66800
PR 66810
PR 66820
PR 66830
PR 66840
PR 66850
PR 66860
PR 66870
PR 66880

```

```

NPAGE = 1
WRITE(L,1) NPAGE
WRITE(L,115) MSFID
WRITE(L,202) AMONTH
202 FORMAT(1H ,A8,I3,',',',',I5)
CCC = CAPI1 *1.0-6
WRITE(L,2) (ANAME(KK),KK=1,10),FF,TC1,CCC
2 FORMAT(//////////1H ,10A8//1H ,'
INT CAPACITY - MGD',F29.3/1H0,'UNIT COST OF DESALTED WATER - CENTS
2PER KILOGALLON',F19.3/1H0,'CAPITAL COST OF PLANT(DIRECT+INDIRECT)-
3 MILLIONS CF DOLLARS',F10.3)
IF(IOPT .EQ. 0) WRITE(L,200)
IF(IOPT .NE. 0) WRITE(L,201)
200 FORMAT(1H0,/1H0,'THE PLANT HAS NOT BEEN OPTIMIZED')
201 FORMAT(1H0,/1H0,'THE PLANT HAS BEEN OPTIMIZED')
IF(IMPOSE .GT. 0) WRITE(L,203)
IF(IMPOSR .GT. 0) WRITE(L,204)
203 FORMAT(1H0,' THE INPUT DATA SPECIFY PHYSICALLY IMPOSSIBLE CONDITIO
INS IN THE RECOVERY SECTION'/8X' OUTPUT VALUES ARE MEANINGLESS')
204 FORMAT(1H0,' THE INPUT DATA SPECIFY PHYSICALLY IMPOSSIBLE CONDITIO
INS IN THE REJECT SECTION'/8X' OUTPUT VALUES ARE MEANINGLESS')
C
IF(IOUT .EQ. 0) GO TO 1000
C
NPAGE = 2
WRITE(L,1) NPAGE
WRITE(L,115) MSFID
WRITE(L,202) AMONTH
1 FORMAT(1H1,46HRECYCLE MULTISTAGE FLASH PLANT - ROUTINE MSF21,7X,
15HPAGE ,I1)
WRITE(L,3) (ANAME(KK),KK=1,10)
3 FORMAT(1H0,10A8)
WRITE(L,4)
4 FORMAT(1H0,31X,17HCOST SUMMARY PAGE )
WRITE(L,5)
5 FORMAT(1H0,18HCAPITAL COMPONENTS ,8X,9HCOST-$/YR,7X,11HCOST-C/KPR
1GAL,5X,12HCOST-$DIRECT )
WRITE(L,6)
6 FORMAT(1H ,18H----- 8X,9H-----,7X,11H-----
1---,5X,12H----- )
WRITE(L,7) EA2,EA1,EA
7 FORMAT(1H0,20HCONDENSING SURFACE ,F15.2,F16.4,F19.2)
WRITE(L,8) ES2,ES1,ES
8 FORMAT(1H ,20HSHLL AND FOUNDATION ,F15.2,F16.4,F19.2)
WRITE(L,9) PMC2,PMC1,PMC
9 FORMAT(1H ,20HPUMPS AND MOTORS ,F15.2,F16.4,F19.2)
WRITE(L,10) WAIT2,WAIT1,WAIT
10 FORMAT(1H ,20HSEA-WATER INTAKE ,F15.2,F16.4,F19.2)
WRITE(L,11) VPC2,VPC1,VPC
11 FORMAT(1H ,20HVALVES AND PIPING ,F15.2,F16.4,F19.2)
WRITE(L,12) CHMPT2,CHMPT1,CHMPTC
12 FORMAT(1H ,20HCHEMICAL CAPITAL ,F15.2,F16.4,F19.2)
WRITE(L,13) CINST2,CINST1,CINSTC
13 FORMAT(1H ,20HINSTRUMENTS ,F15.2,F16.4,F19.2)
WRITE(L,14) EEC2,EEC1,EEC
14 FORMAT(1H ,20HELECTRICAL ,F15.2,F16.4,F19.2)
WRITE(L,15) DEA2,DEA1,DEACST
15 FORMAT(1H ,20HNCG REMOVAL SYSTEM ,F15.2,F16.4,F19.2)
WRITE(L,16) BHC2,BHC1,BHC
16 FORMAT(1H ,20HBRINE HEATER ,F15.2,F16.4,F19.2)
WRITE(L,17) SITEC2,SITEC1,SITEC
17 FORMAT(1H ,20HSITE, 8LDGS, CRANES ,F15.2,F16.4,F19.2)
WRITE(L,18) CAPI4,CAPI3,CDMM
18 FORMAT(1H0,20H TOTAL CAPITAL ,F15.2,F16.4,F19.2)
WRITE(L,19)
19 FORMAT(1H0,20HTOTAL INVESTMENT, )
WRITE(L,20) CAPI1
20 FORMAT(1H ,20H $DIR+IND ,31X,F19.2)
WRITE(L,21)
21 FORMAT(1H ,20HSPECIFIC INVESTMENT, )

```

WRITE(L,22) CAPI2		PR 67590
22 FORMAT(1H ,20H	\$/GPD ,31X,F16.5)	PR 67600
WRITE(L,23) RETUB2, RETUB1		PR 67610
23 FORMAT(1H0,20H RETUBING	,F15.2,F16.4)	PR 67620
WRITE(L,24)		PR 67630
24 FORMAT(1H0,20HOPERATING COMPONENTS	)	PR 67640
WRITE(L,25)		PR 67650
25 FORMAT(1H ,20H-----	)	PR 67660
WRITE(L,26) HC2, HC1		PR 67670
26 FORMAT(1H0,20HPROCESS HEAT	,F15.2,F16.4)	****
WRITE(6,271) EJC2,EJC1		****
271 FORMAT(1H0,20HSTEAM TO EJECTORS	,F15.2,F16.4)	****
WRITE(L,27) CC2,CC1		PR 67690
27 FORMAT(1H ,20HCHEMICALS	,F15.2,F16.4)	PR 67700
WRITE(L,28) POCST2,POCST1		PR 67710
28 FORMAT(1H ,20HPOWER	,F15.2,F16.4)	PR 67720
WRITE(L,29) OC2, OC1		PR 67730
29 FORMAT(1H ,20HOPERATING	,F15.2,F16.4)	PR 67740
WRITE(L,30) AMSC2, AMSC1		PR 67750
30 FORMAT(1H ,20HMAINT. + SUPPLIES	,F15.2,F16.4)	PR 67760
WRITE(L,31) TOC2, TOC1		PR 67770
31 FORMAT(1H0,20H TOTAL OPERATING	,F15.2,F16.4)	PR 67780
WRITE(L,32) TC2, TC1		PR 67790
32 FORMAT(1H0,20HTOTAL(CAP+RETUB+OP)	,F15.2,F16.4)	PR 67800
WRITE(L,33)		PR 67810
33 FORMAT(1H0,20HCOST FACTORS	)	PR 67820
WRITE(L,34) UFC		PR 67830
34 FORMAT(1H0,20HCOST OF POWER,C/KWHR , F15.6)		PR 67840
WRITE(L,35) EXSTM		PR 67850
35 FORMAT(1H ,20HCOST OF HEAT,C/MMBTU , F15.6)		PR 67860
WRITE(L,831) STFEJ		****
831 FORMAT(21H EJECT. STEAM,C/MMBTU ,F15.6)		****
WRITE(L,36) SMAP		PR 67870
36 FORMAT(1H ,20HANNUAL CHARGE RATE , F15.6)		PR 67880
WRITE(L,37) RATEIN		PR 67890
37 FORMAT(1H ,20HINTEREST RATE , F15.6)		PR 67900
WRITE(L,38) AJ		PR 67910
38 FORMAT(1H ,20HHIGHER COST FACTOR , F15.6)		PR 67920
WRITE(L,39) EFF		PR 67930
39 FORMAT(1H ,20HPUMP AND MOTOR EFF. , F15.6)		PR 67940
WRITE(L,40) LF2		PR 67950
40 FORMAT(1H ,20HPLANT LOAD FACTOR , F15.6)		PR 67960
WRITE(L,41) WPL		PR 67970
41 FORMAT(1H ,20HPLANT LIFE,YEARS , F15.6)		PR 67980
WRITE(L,42)		PR 67990
42 FORMAT(1H0,28X,6HREJECT,10X,8HRECOVERY,7X,12HBRINE HEATER)		PR 68000
WRITE(L,43) CSLTBP, CSLTBP, CSLTBH		PR 68010
43 FORMAT(1H0,20HTUBE LIFE,YEARS ,F14.3,2F17.3)		PR 68020
WRITE(L,44) RACHG,EACHG,HACHG		PR 68030
44 FORMAT(1H ,20HAREA COST,\$/SQ.FT. ,F14.3,2F17.3)		PR 68040
WRITE(L,441) UNARAE		PR 68050
441 FORMAT(1H ,43HINSTALLED EVAPORATOR SURFACE COST,\$/SQ.FT. ,F8.3)		PR 68060
C		PR 68070
NPAGE = 3		PR 68080
WRITE(L,1) NPAGE		PR 68090
WRITE(L,115) MSFID		PR 68100
WRITE(L,202) AMONTH		PR 68110
WRITE(L,3) (ANAME(KK),KK=1,10)		PR 68120
WRITE(L,45)		PR 68130
45 FORMAT(1H0,27H I SUMMARY OF PLANT DATA)		PR 68140
WRITE(L,46)		PR 68150
46 FORMAT(1H0,14H GENERAL)		PR 68160
WRITE(L,47) FF		PR 68170
47 FORMAT(1H ,35H PLANT CAPACITY, MGD ,F16.4)		PR 68180
WRITE(L,471) RP		PR 68190
471 FORMAT(1H ,35H PERFORMANCE RATIO ,F16.4)		PR 68200
WRITE(L,48) CU		PR 68210
48 FORMAT(1H ,35H SEA WATER CONCENTRATION ,F16.4)		PR 68220
WRITE(L,49) CPPPM		PR 68230
49 FORMAT(1H ,35H PRODUCT CONCENTRATION, PPM ,F16.4)		PR 68240

WRITE(L,50) CR			PR 68250
50 FORMAT(1H ,35H	CONCENTRATION RATIO	,F16.4)	PR 68260
WRITE(L,51) AK			PR 68270
51 FORMAT(1H ,35H	NO OF REJECT STAGES	,F16.4)	PR 68280
WRITE(L,52) AN			PR 68290
52 FORMAT(1H ,35H	NO OF RECOVERY STAGES	,F16.4)	PR 68300
53 FORMAT(1H ,35H	PERFORMANCE RATIO	,F16.4)	PR 68310
WRITE(L,531) YEAR			PR 68320
531 FORMAT(1H ,35H	YEAR CONSTRUCTION STARTED	,F16.4)	PR 68330
WRITE(L,54)			PR 68340
54 FORMAT(1H0,26H	TEMPERATURES - DEG F)		PR 68350
WRITE(L,55) TS			PR 68360
55 FORMAT(1H ,35H	STEAM	,F16.4)	PR 68370
WRITE(L,56) THF			PR 68380
56 FORMAT(1H ,35H	MAXIMUM BRINE	,F16.4)	PR 68390
WRITE(L,57) TB			PR 68400
57 FORMAT(1H ,35H	BLOWDOWN	,F16.4)	PR 68410
WRITE(L,58) TP			PR 68420
58 FORMAT(1H ,35H	PRODUCT	,F16.4)	PR 68430
WRITE(L,59) TO			PR 68440
59 FORMAT(1H ,35H	OCEAN	,F16.4)	PR 68450
WRITE(L,60)			PR 68460
60 FORMAT(1H0,34H	FLOW RATES, MILLIONS OF LB/HR)		PR 68470
WRITE(L,61) WSMM			PR 68480
61 FORMAT(1H ,35H	STEAM	,F16.4)	PR 68490
WRITE(L,62) WPMM			PR 68500
62 FORMAT(1H ,35H	PRODUCT	,F16.4)	PR 68510
WRITE(L,63) WBMM			PR 68520
63 FORMAT(1H ,35H	BLOWDOWN	,F16.4)	PR 68530
WRITE(L,64) WOCMM			PR 68540
64 FORMAT(1H ,35H	SEA INTAKE	,F16.4)	PR 68550
WRITE(L,65) WCPM			PR 68560
65 FORMAT(1H ,35H	HEAT REJECT	,F16.4)	PR 68570
WRITE(L,66) WRMM			PR 68580
66 FORMAT(1H ,35H	RECYCLE	,F16.4)	PR 68590
WRITE(L,67) WFMM			PR 68600
67 FORMAT(1H ,35H	RECCV. TUBING, BRINE HTR.	,F16.4)	PR 68610
WRITE(L,68) WOMM			PR 68620
68 FORMAT(1H ,35H	REJECT TUBING	,F16.4)	PR 68630
WRITE(L,69)			PR 68640
69 FORMAT(1H0,34H II	DESCRIPTION OF PHYSICAL PLANT)		PR 68650
WRITE(L,691) BLDGS			PR 68660
691 FORMAT(1H0,35H	NO OF BUILDINGS	,F16.4)	PR 68670
WRITE(L,70) TRAINS			PR 68680
70 FORMAT(1H ,35H	NO OF TRAINS	,F16.4)	PR 68690
WRITE(L,71) MODU			PR 68700
71 FORMAT(1H ,35H	NO OF MODULES	,F16.4)	PR 68710
WRITE(L,711) LEV			PR 68720
711 FORMAT(1H ,35H	NO OF LEVELS	,F16.4)	PR 68730
WRITE(L,72) HRECOV			PR 68740
72 FORMAT(1H ,35H	RECOVERY HEIGHT, FT	,F16.4)	PR 68750
WRITE(L,721) STLEN			PR 68760
721 FORMAT(1H ,35H	LENGTH OF STEEL SECTION, FT	,F16.4)	PR 68770
WRITE(L,722) HGTLEN			PR 68780
722 FORMAT(1H ,35H	HI-FLOW LENGTH, FT	,F16.4)	PR 68790
WRITE(L,73) RECCLN			PR 68800
73 FORMAT(1H ,35H	RECOVERY LENGTH, FT	,F16.4)	PR 68810
WRITE(L,731) WHOT			PR 68820
731 FORMAT(1H ,35H	HI-FLOW WIDTH, FT	,F16.4)	PR 68830
WRITE(L,74) WCOLD			PR 68840
74 FORMAT(1H ,35H	LO-FLOW WIDTH, FT	,F16.4)	PR 68850
WRITE(L,741) HREJCT			PR 68860
741 FORMAT(1H ,35H	REJECT HEIGHT, FT	,F16.4)	PR 68870
WRITE(L,75) REJLEN			PR 68880
75 FORMAT(1H ,35H	REJECT LENGTH, FT	,F16.4)	PR 68890
WRITE(L,76)			PR 68900
76 FORMAT(1H ,35H	TOTAL PLANT VOLUME,	)	PR 68910
WRITE(L,77) VOMTOT			PR 68920
77 FORMAT(1H ,35H	MILLIONS OF CUBIC FEET	,F16.4)	PR 68930

C	NPAGE = 4		PR 68940
	WRITE(L,1) NPAGE		PR 68950
	WRITE(L,115) MSFID		PR 68960
	WRITE(L,202) AMONTH		PR 68970
	WRITE(L,3) (ANAME(KK),KK=1,10)		PR 68980
	WRITE(L,78)		PR 68990
	78 FORMAT(1H0,22HIII TUBING PARAMETERS)		PR 69000
	WRITE(L,79)		PR 69010
	79 FORMAT(1H0,40X,6HREJECT,8X,8HRECOVERY,4X,12HBRINE HEATER)		PR 69020
	WRITE(L,80) DOR ,DOE, DOH		PR 69030
	80 FORMAT(1H ,32H OUTSIDE DIAMETER, IN. ,3F15.5)		PR 69040
	WRITE(L,90) XO(27), XO(26), XO(25)		PR 69050
	90 FORMAT(1H ,32H WALL THICKNESS, IN. ,3F15.5)		PR 69060
	WRITE(L,91) XO(21), XO(20), XO(19)		PR 69070
	91 FORMAT(1H ,32H K,BTU/HR FT2 F ,3F15.5)		PR 69080
	WRITE(L,92) XT(103),XT(102),XT(101)		PR 69090
	92 FORMAT(1H ,32H FOULING RESISTANCE ,3F15.5)		PR 69100
	WRITE(L,93) XO(24), XO(23), XO(22)		PR 69110
	93 FORMAT(1H ,32H FLOODING FACTOR ,3F15.5)		PR 69120
	WRITE(L,94) ENRK ,ENRK ,ENHK		PR 69130
	94 FORMAT(1H ,32H NO OF TUBES (THOUSANDS) ,3F15.5)		PR 69140
	WRITE(L,95) RLR, ELE, HLH		PR 69150
	95 FORMAT(1H ,32H TUBE LENGTH, FT ,3F15.5)		PR 69160
	WRITE(L,96) ARKK, AEKK, AHKK		PR 69170
	96 FORMAT(1H ,32H AREA,THOUSANDS OF SQ FT ,3F15.5)		PR 69180
	WRITE(L,97) VR, VE, VH		PR 69190
	97 FORMAT(1H0,32H VELOCITY, FPS ,3F15.5)		PR 69200
	WRITE(L,98) HEADR, HEADE, HEADH		PR 69210
	98 FORMAT(1H ,32H FRICTIONAL HEAD, FT ,3F15.5)		PR 69220
	WRITE(L,99) UR, UE, UH		PR 69230
	99 FORMAT(1H0,32H OVERALL U, B/HR-FT2-F ,3F15.5)		PR 69240
	WRITE(L,100) HIR, HIE, HIH		PR 69250
	100 FORMAT(1H ,32H H INSIDE , B/HR-FT2-F ,3F15.5)		PR 69260
	WRITE(L,101) HOR, HOE, HOH		PR 69270
	101 FORMAT(1H ,32H H OUTSIDE, B/HR-FT2-F ,3F15.5)		PR 69280
	WRITE(L,102) OM2, OM1, PHE		PR 69290
	102 FORMAT(1H ,32H AVG LMTD, DEG F ,3F15.5)		PR 69300
	WRITE(L,103) TO, TE, TCF		PR 69310
	103 FORMAT(1H0,32H TEMPERATURE IN, DEG F ,3F15.5)		PR 69320
	WRITE(L,104) TB ,TCF, THF		PR 69330
	104 FORMAT(1H ,32H TEMPERATURE OUT, DEG F ,3F15.5)		PR 69340
	WRITE(L,105)		PR 69350
	105 FORMAT(1H0,23H IV PUMPING PARAMETERS)		PR 69360
	WRITE(L,106)		PR 69370
	106 FORMAT(1H0, 38X,8HFLOW-GPM,8X,7HHEAD-FT, 8X,8HPOWER-MW)		PR 69380
	WRITE(L,107) GPMD,HDEL,PODEL		PR 69390
	107 FORMAT(1H ,32H SEA-WATER DELIVERY ,3F15.5)		PR 69400
	WRITE(L,108) GPMR,HREC,POREC		PR 69410
	108 FORMAT(1H ,32H RECYCLE ,3F15.5)		PR 69420
	WRITE(L,109) GPMB,HBL,PUBLD		PR 69430
	109 FORMAT(1H ,32H BLOWDOWN ,3F15.5)		PR 69440
	WRITE(L,110) GPMP,HPR,PCPRD		PR 69450
	110 FORMAT(1H ,32H PRODUCT ,3F15.5)		PR 69460
	WRITE(L,111) GPMD,HDEA,PODEA		PR 69470
	111 FORMAT(1H ,32H DEAERATOR ,3F15.5)		PR 69480
	WRITE(L,1111) PO		PR 69490
	1111 FORMAT(1H0,32H TOTAL (ELECTRICAL) ,30X,F15.5)		PR 69500
C	1000 CONTINUE		PR 69510
	NPAGE = 5		PR 69560
	WRITE(L,113) NPAGE		PR 69570
	113 FORMAT(1H1,46HRECYCLE MULTISTAGE FLASH PLANT - ROUTINE MSF21,7X,		PR 69580
	131HCONDENSED SUMMARY OF PLANT DATA,25X,5HPAGE ,11)		PR 69590
	WRITE(L,115) MSFID		PR 69600
115	FORMAT(1H ,10A8)		PR 69610
	WRITE(L,202) AMONTH		PR 69620
	WRITE(L,3) (ANAME(KK),KK=1,10)		PR 69630
	WRITE(L,800G) FF ,RP ,P ,PE ,Q ,CR ,		PR 69650
			PR 69660

1	WRITE(L,8005)	CC	,CP	,CCF	,CB	,LF2	,YEAR	PR	69670
1		TS	,THF	,TCF	,TK	,TPE	,TB		PR 69680
1	WRITE(L,8010)	TE	,TP	,TO			,STLTMP		PR 69690
1		WS	,WF	,WR	,WPE	,WPR	,WP		PR 69700
1		WB	,WU	,WC	,WOCEAN				PR 69710
1	WRITE(L,8015)	AN	,ESTGL	,RECOLN	,HRECOV	,VOLSTL	,STLLEN		PR 69720
1		AK	,RSTGL	,REJLEN	,HREJCT	,VOLCNC	,HOTLEN		PR 69730
1	WRITE(L,8020)	WHOT	,WCOLD	,ATN	,ENBH	,BLDGS	,TRAINS		PR 69740
1		TOTLEN	,VCMTOT		,ACRES	,MODU	,LEV		PR 69750
1	WRITE(L,8025)	DCE	,WALLE	,ELE	,ENE	,AE	,VE		PR 69760
1		DOR	,WALLR	,RLR	,RNR	,AR	,VR		PR 69770
2		DOH	,WALLH	,HLH	,HNN	,AH	,VH		PR 69780
1	WRITE(L,8030)	UE	,HIE	,HOE	,BKTE	,RSE	,OM1		PR 69790
1		UR	,HIR	,HOR	,BKTR	,RSR	,OM2		PR 69800
2		UH	,HIH	,HOH	,BKTH	,RSH	,PHE		PR 69810
1	WRITE(L,8035)	QEL	,SUBE	,DTLSE	,BPKE	,ROE1	,BDEPH		PR 69820
1		QRL	,SUBR	,DTLSR	,BPRR	,ROE2			PR 69830
1	WRITE(L,8040)	HREC	,HDEL	,HDEA	,HPR	,HBL			PR 69840
1		RPMR	,RPMO	,RPMH	,RPM	,RPMB			PR 69850
2		HPREC	,HPDEL	,HPDEA	,HPPRD	,HPBLD			PR 69860
3		POREC	,PODEL	,PODEA	,POPRD	,POBLD	,PO		PR 69870
4		HEADE	,HEADR	,HEADH		,PO3	,POTOT		PR 69880
1	WRITE(L,8045)	AJ	,AXJ	,RATEIN	,SMAP	,PSAJ	,EXSTM		PR 69890
1		WPL	,CSLTBP	,CSLTBH	,SMAPPP	,SMAPPH	,UFC		PR 69900
1	WRITE(L,8050)	EACHG	,HACHG	,RACHG	,UNPUMP	,UNDRVE	,UNELCT		PR 69910
1		UNARAE	,UNARHI	,XC(56)	,UNSHLS	,UNSHLC	,USHELV		PR 69920
1	WRITE(L,8055)	EA	,ES	,PMC	,WAIT	,VPC	,CHMPTC		PR 69930
1		CINSTC	,EEC	,DEACST	,BHC	,SITE	,CIBC		PR 69940
1	WRITE(L,8060)	EA1	,ES1	,PMC1	,WAIT1	,VPC1	,CHMPT1		PR 69950
1		CINST1	,EEC1	,DEA1	,BHC1	,SITE1	,CIBC1		PR 69960
2		RETUB1	,HC1	,CC1	,POCST1	,OC1	,AMSC1		PR 69970
1	WRITE(L,8065)	EA2	,ES2	,PMC2	,WAIT2	,VPC2	,CHMPT2		PR 69980
1		CINST2	,EEC2	,DEA2	,BHC2	,SITE2	,CIBC2		PR 69990
2		RETUB2	,HC2	,CC2	,POCST2	,OC2	,AMSC2		PR 70000
1	WRITE(L,8070)	COMM	,CAPI1	,CAPI2					PR 70010
1				,CAPI4	,RETUB2	,TOC2	,TC2		PR 70020
2				,CAPI3	,RETUB1	,IOC1	,IC1		PR 70030
8000	FORMAT(1H0,'FF	RP	P	PE	Q	CR	,6D14.6/		PR 70040
1		CP	CCF	CB	LF2	YEAR	,6D14.6/		PR 70050
8005	FORMAT(1H0,'TS	THF	TCF	TK	TPE	TB	,6D14.6/		PR 70060
1		TE	TP	TO		STLTMP	,3D14.6,28XPR		PR 70070
2									PR 70080
8010	FORMAT(1H0,'WS	WF	WR	WPE	WPR	WP	,6D14.6/		PR 70090
1		WU	WC	WOCEAN			,4D14.6/		PR 70100
8015	FORMAT(1H0,'AN	ESTGL	RECOLN	HRECOV	VOLSTL	STLLEN	,6D14.6/		PR 70110
1		AK	RSTGL	REJLEN	HREJCT	VOLCNC	HOTLEN		PR 70120
8020	FORMAT(1H0,'WHOT	WCOLD	ATN	ENBH	BLDGS	TRAINS	,6D14.6/		PR 70130
1		TOTLEN	VOMTGT	ACRES	MODU	LEV	,2D14.6,14XPR		PR 70140
2									PR 70150
8025	FORMAT(1H0,'DUE	WALLE	ELE	ENE	AE	VE	,6D14.6/		PR 70160
1		DOR	WALLR	RLR	RNR	AR	VR		PR 70170
2		DOH	WALLH	HLH	HNN	AH	VH		PR 70180
8030	FORMAT(1H0,'UE	HIE	HOE	BKTE	RSE	OM1	,6D14.6/		PR 70190
1		UR	HIR	HOR	BKTR	RSR	OM2		PR 70200
2		UH	HIH	HOH	BKTH	RSH	PHE		PR 70210
8035	FORMAT(1H0,'QEL	SUBE	DTLSE	BPKE	ROE1	BDEPH	,6D14.6/		PR 70220
1		QRL	SUBR	DTLSR	BPRR	ROE2	,5D14.6/		PR 70230
8040	FORMAT(1H0,'HREC	HDEL	HDEA	HPR	HBL		,5D14.6/		PR 70240
1		RPMR	RPMO	RPMH	RPM	RPMB	,5D14.6/		PR 70250
2		HPREC	HPDEL	HPDEA	HPPRD	HPBLD	,5D14.6/		PR 70260
3		POREC	PODEL	PODEA	POPRD	POBLD	PO		PR 70270
4		HEADE	HEADR	HEADH		PO3	POTOT		PR 70280
5							,3D14.6,14XPR		PR 70290
8045	FORMAT(1H0,'AJ	AXJ	RATEIN	SMAP	PSAJ	HEAT	,6D14.6/		PR 70300
1		WPL	CSLTBP	CSLTBH	SMAPPP	SMAPPH	ELEC		PR 70310
8050	FORMAT(1H0,'EACHG	HACHG	RACHG	UNPUMP	UNDRVE	UNELCT	,6D14.6/		PR 70320
1		UNARAF	UNARHI	AERTE	UNSHLS	UNSHLC	USHELV		PR 70340
8055	FORMAT(1H0,'EA	ES	PMC	WAIT	VPL	CHMPTC	,6D14.6/		PR 70350
1		CINSTC	EEC	DEACST	BHC	SITE	CIBC		PR 70360
8060	FORMAT(1H0,'EA1	ES1	PMC1	WAIT1	VPC1	CHMPT1	,6D14.6/		PR 70370

```

      1      * CINST1 EEC1  DEA1  BHC1  SITE1  CIBC1  *,6D14.6/  PR 70380
      2      * RETUB1 HC1   CC1   POCST1 OC1   AMSC1  *,6D14.6)  PR 70390
8065 FORMAT(1H0,'EA2  ES2  PMC2  WAIT2  VPC2  CHMPT2 *,6D14.6/  PR 70400
      1      * CINST2 EEC2  DEA2  BHC2  SITE2  CIBC2  *,6D14.6/  PR 70410
      2      * RETUB2 HC2   CC2   POCST2 OC2   AMSC2  *,6D14.6)  PR 70420
8070 FORMAT(1H0,'COMM  CAPI1 CAPI2  *,3D14.6/  PR 70430
      1      *      CAPI4  RETUB2 TOC2  TC2   *,28X,  PR 70440
      2 4D14.6/  PR 70450
      3      *      CAPI3  RETUB1 TOC1  TC1   *,28X,  PR 70460
      4 4D14.6)  PR 70470
      RETURN  PR 70480
      END     PR 70490

```

APPENDIX C

CHANGES MADE IN SUBROUTINE RITEV

```

SUBROUTINE RITEV(IOPT,ICUT,L)
IMPLICIT REAL*8(A-H,O-Z)
C
REAL*8 LPHE
DOUBLE PRECISION LAM,LAMDAS,MAVG
DOUBLE PRECISION LPH, LVE, IDBH, IDPH, LCON, NCON,
1 NTPH, IDCCN
DOUBLE PRECISION KBH, KPH, KVE, LBH, MGD, NBH,
1 NPH, NVE, KCON, LMTD, LVEP, LMTDBH, LMTDCN
DOUBLE PRECISION INT, INSTRD, INSTRK, INSTRY, MAINTK, MAINTY
DOUBLE PRECISION LEV, LF2, MSFID
C
COMMON/BLOCV1/ ANE, HVE, LPH, LVE, ACON, PR 60930
1 GPMV, HPVE, HSEA, IDBH, IDPH, LCON, PR 60940
2 NCON, NTPH, QDBH, ODPH, OOVE, POVE, PR 60950
3 RPMV, HFEED, IDCCN, ODCON, SUMWT, VETSA, PR 60960
4 APTSCN, APTSEP, CVRHGT, TOTNVE, VEPMS, PR 60970
COMMON/PINHAS/APTSH,ENRSS,ENRJS,LPHE,DUMDUM(16),NFEED,IIIIII(9)
COMMON/BLOCV2/ A(30), S, AE(30), QE, TC(30), PR 60980
1 TE(30), TR, UE(30), UM(3), WM, WT(30), PR 60990
2 ABH, APH, BPE(30), CIE(30), COE(30), DPE(30), PR 61000
3 ELL, GBH, GPH, GPM, HQD, KBH, PR 61010
4 KPH, KVE, LBH, MGD, NBH, NPH, PR 61020
5 NVE(30), QPH, RBH, RPH, RVE, TOU, PR 61030
6 UBH, VBH, VPH, WPEX(30), BHLF, GCON, PR 61040
7 HIBH, HIPH(3), HOBH, HOPH(3), KCON, LMTD(3), PR 61050
8 LVEP, PHLF, QMSF(3), RCON, SUBF(3), TCON, PR 61060
9 UCON, VCON, VLEN, VILF, WOTH(30), ALFAE(30), PR 61070
+ CONLF, HICON, HOCON, HOTE1, PHMGT, POBLO, PR 61080
A POPRG, POSEA, SURFF, VEHGT, WALVE, EFFSPC, PR 61090
BELBNDL(30), HCOTCF, HCOTUD, HEADBH, HEADCN, HEADPH, PR 61100
C LMTDBH, LMTDCN, PLNTLF, PUDEAS, POFEED, SUMWPE, PR 61110
D SUMWPH, TOTAVE, QESP,VEFEED(30), WBOOST, WDCOLD, PR 61120
E NE, NTRN, IFEED, IRECYC, PR 61130
COMMON/BLOCV3/ BHD, BHK, BHY, INT, PMD, PR 61140
1 PMK, PMY, VPD, VPK, VPY, ACHR, PR 61150
2 DEAD, DEAK, DEAY, ELEC, HEAT, SBOD, PR 61160
3 SBCK, SBCY, CHEMK, CHEMY, HEATK, HEATY, PR 61170
4 GPERK, OPERY, PLDIN, WAITD, WAITK, WAITY, PR 61180
5 ANCCMP, CMCAPD, CMCAPI, CMCAPI, CNDSRD, CNDSRK, PR 61190
6 CNDSRY, ELECTD, ELECTK, ELECTY, INSTRD, INSTRK, PR 61200
7 INSTRY, MAINTK, MAINTY, PHTUBD, PHTUBK, PHTUBY, PR 61210
8 PLCAPD, PLCAPK, PLCAPY, POWERK, POWERY, RETUBK, PR 61220
9 RETUBY, SHELLD, SHELLK, SHELLY, TOTALK, TOTALY, PR 61230
+ TOTOPK, TOTOPY, TREPBN, TREPBN, TREPPE, PR 61240
A VETUBD, VETUBK, VETUBY, CGPD, PR 61250
COMMON/COMNAM/ AJ, CB, CO, CP, CR, PR 61260
1 HB, PI, PO, TB, TO, TP, PR 61270
2 TS, WB, WF, WD, WP, WR, PR 61280
3 AXJ, HBL, HPR, LEV, LF2, TCF, PR 61290
4 ENBH, GPMB, GPMO, GPMH, GPMO, GPMP, PR 61300
5 GPMR, HDEA, RPMB, RPMO, RPMH, RPMP, PR 61310
6 RPMR, TSTH, WHOT, YEAR, ACRES, BHVOL, PR 61320
7 BLOGS, BNDLS, HOLES, HPBLD, HPDEA, HPDEL, PR 61330
8 HPPRD, HPREC, PLPRD, PLSEA, PODEA, ACNCEW, PR 61340
9 ACNCFL, ACNCIW, ACNCPH, ACNCRF, ACNCTR, AEXCAV, PR 61350
+ ASTLEW, ASTLFL, ASTLIW, ASTLPH, ASTLRF, ASTLTR, PR 61360
A AWEIRS, BHSURF, DINTAK, ENITSE, ENPIPE, ENSUPE, PR 61370
B ENSUPR, PIPELN, PLSZMG, REJLEN, STLEN, STLTMP, PR 61380
C TNACDY, TRAINS, TSAREA, VOLCNC, VOLSTL, WOCCEAN, PR 61390
COMMON/BLOC13/ XO(300)
COMMON/BLOC14/ XC(500)
COMMON/NAME/ ANAME(10), AMONTH, IDAY, IYEAR
COMMON/DECKID/ MSFID(10),VTEID(10),EDID(10)
COMMON/IMPOVE/ IVERT

```

```

COMMON/BLKFAC/ FDFAC, QEFAC, TRFAC
C
C DIMENSION WPEI(30)
C
EFF = XC(32)
WALCON = XO(27)
WALPH = XO(26)
WALBH = XC(25)
WPE = SUMWPE *AE(1)
WPPH = SUMWPH *AE(1)
PRP = 1.03 *WP/(QE+QPH)
PRVE = 1.03*WPE/QE
PRPH = 1.03*WPPH/QPH
LAMCAS = LAM(TS,PS,0.00,0.00)
WSE = QE/LAMDAS
WSPH = QPH/LAMDAS
WS = WSE +WSPH
TM = TE(1)
DELTC = TCON -TR
WR = DMAX1(0.00,WO-WF+WM)
VEYNI = AEXCAV *VEHGT
PHVCL = AEXCAV *PHHGT
AVGUPH = (UH(1)+4.*UH(2)+UH(3))/6.
AVH1PH = (H1PH(1)+4.*H1PH(2)+H1PH(3))/6.
AVHCPH = (HCPH(1)+4.*HCPH(2)+HCPH(3))/6.
AVLTPH = (LMTD(1)+4.*LMTD(2)+LMTD(3))/6.
AVGSUB = (SUBF(1)+4.*SUBF(2)+SUBF(3))/6.
AVQMSF = (QMSF(1)+4.*QMSF(2)+QMSF(3))/6.
CAPF = LF2
CFVEI = VETUBD/TOTAVE
CFPHI = PHTUBD/APH
CFBFI = XC(133)+XC(126)
CFCONI = CNDSRD/ACON
CRVE = CIE(NE)/CO
EFFL = VLEN/ANE
WVEMAX = WULULD
WVEMIN = WHGT
TOTVOL = VOLCNC +VOLSTL
QTR = WF*(HCOTCF-HCOTOC)
ROA = (TCF-TUU)/NPH
CFSHEL = SHELLD/TOTVOL
CFVE = XC(63)
CFPH = XC(68)
CFCCN = XC(74)
CFBH = XC(126)
CFPUMP = XC(128)
POTCT = PQ +POCEAS
AVDPE = 0.000
DPE(NE)=0.00
AVBPE = 0.000
AVGUE=0.000
AVDTVE = 0.000
MAVG = 0.00
DO ICO I=1,NE
AVGUE=AVGUE+UE(I)
WPEI(I) = WPEX(I)*AE(1)
AVDTVE = AVDTVE+A(I)
AVDPE = AVDPE+DPE(I)
AVBPE = AVBPE+BPE(I)
MAVG = MAVG+AE(I)/AE(1)
100 CONTINUE
AVGUE=AVGUE/ANE.
AVDTVE = AVDTVE/ANE
AVDPE = AVDPE/(ANE-1.00)
AVBPE = AVBPE/ANE
MAVG = MAVG/ANE
ELEC = 100.00*ELEC
HEAT = 100.00*HEAT
C
WRITE(L,200)

```

```

PR 61560
PR 61570
PR 61580
PR 61590
PR 61600
PR 61610
PR 61620
PR 61630
PR 61640
PR 61650
PR 61660
PR 61670
PR 61680
PR 61690
PR 61700
PR 61710
PR 61720
PR 61730
PR 61740
PR 61750
PR 61760
PR 61770
PR 61780
PR 61790
PR 61800
PR 61810
PR 61820
PR 61830
PR 61840
PR 61850
PR 61860
PR 61870
PR 61880
PR 61890
PR 61900
PR 61910
PR 61920
PR 61930
PR 61940
PR 61950
PR 61960
PR 61970
PR 61980
PR 61990
PR 62000
PR 62010
PR 62020
****
PR 62030
PR 62040
PR 62050
PR 62060
PR 62070
PR 62080
PR 62090
PR 62100
PR 62110
PR 62120
PR 62130
PR 62140
PR 62150
PR 62160
PR 62170
PR 62180
PR 62190
PR 62200
PR 62210
PR 62220
PR 62230

```

```

WRITE(L,115) VTEID                                PR 62240
115 FORMAT(1H ,10A8)                                PR 62250
WRITE(L,202)AMGNTH                                PR 62260
202 FORMAT(1H ,A8)                                PR 62270
CCC = PLDIN*1.0-6                                PR 62280
WRITE(L,2) (ANAME(KK),KK=1,10),MGD,TOTALK,CCC      PR 62290
2 FORMAT(//////////1H ,10A8////1H ,"            PLAPR 62300
INT CAPACITY - MGD',F29.3/1H0,'UNIT COST OF DESALTED WATER - CENTS PR 62310
2PER KILOGALLON',F19.3/1H0,'CAPITAL COST OF PLANT(DIRECT+INDIRECT)-PR 62320
3 MILLIONS OF DOLLARS',F10.3)                    PR 62330
IF(IQPT .EQ. 0) WRITE(L,4)                        PR 62340
IF(IQPT .NE. 0) WRITE(L,5)                        PR 62350
4 FORMAT(1H0,/1H0,'THE PLANT HAS NOT BEEN OPTIMIZED') PR 62360
5 FORMAT(1H0,/1H0,'THE PLANT HAS BEEN OPTIMIZED') PR 62370
IF(IFEED .GT. 0) WRITE(L,6)                        PR 62380
6 FORMAT(1H0,'THE DESIGN CONSTRAINTS HAVE REQUIRED AN INEFFICIENT USPR 62390
1E OF CONDENSING SURFACE IN THE PREHEATER')        PR 62400
IF(IRECYC .GT. 0) WRITE(L,7)                      PR 62410
7 FORMAT(1H0,'THE CA2SO4 SOLUBILITY CONSTRAINT HAS REDUCED THE PRODU PR 62420
1CT FROM THE PREHEATER')                          PR 62430
IF(IVERT .GT. 0) WRITE(L,8)                        PR 62440
8 FORMAT(1H0,'THE INPUT DATA HAVE REQUIRED THAT THE STANDARD M-VALUEPR 62450
1S BE REVISED TO KEEP THE PLANT PHYSICALLY REASONABLE') PR 62460
IF(IQOUT .EQ. 0) GO TO 1C00                        PR 62470
C                                                    PR 62480
WRITE(L,200)                                       PR 62490
200 FORMAT(1H1,'VERTICAL TUBE EVAPORATOR PLANT - ROUTINE VTE21') PR 62500
WRITE(L,115) VTEID                                PR 62510
WRITE(L,202)AMONTH                                PR 62260
C                                                    PR 62530
I. SUMMARY OF PLANT DATA
C                                                    PR 62540
GENERAL
C                                                    PR 62550
WRITE(L,8005) MGD ,PRP ,
1 CO ,PRVE , PR 62560
2 CP ,PRPH , PR 62570
4 CR , PR 62580
5 NE , PR 62590
6 NPH, YEAR PR 62600
C TEMPERATURES - DEG.F PR 62610
WRITE(L,8010) TS ,WS , PR 62620
1 TM ,WSE , PR 62630
2 TE(NE),WSPH , PR 62640
3 TB ,WP , PR 62650
4 TP ,WPE , PR 62660
5 T00 ,WPPH , PR 62670
6 TC ,WB , PR 62680
7 WOCEAN, PR 62690
8 DELTC ,WR , PR 62700
9 VPH PR 62710
C II. DESCRIPTION OF PHYSICAL PLANT PR 62720
C PLANT DIMENSIONS, FT. PR 62730
WRITE(L,8015) LVEP ,OVRHGT , PR 62740
1 LPH ,VEHGT , PR 62750
2 WVEMIN ,PHHGT , PR 62760
3 WVEMAX ,VEVOL , PR 62770
4 NTRN ,PHVOL , PR 62780
5 STLEN ,STLTMP PR 62790
C TUBING DESCRIPTION PR 62800
WRITE(L,8020) ODVE ,ODPH ,ODCON , PR 62810
1 VALVE ,WALPH ,WALCON, PR 62820
2 KVE ,KPH ,KCON , PR 62830
3 RVE ,RPH ,RCON , PR 62840
4 XO(23),XO(24), PR 62850
5 TCTNVE,NTPH ,NCON , PR 62860
6 LVE ,LPHE ,LCON , PR 62870
7 TOTAVE,APH ,ACON , PR 62880
8 AVGUE ,AVGUPH,UCON PR 62890
C III. HEAD REQUIREMENTS AND PUMPING REQUIREMENTS PR 62900
WRITE(L,8030) HSEA ,POSEA , PR 62910
1 HFEED ,PGFEED , PR 62920
2 HPR ,PGPRO , PR 62930

```

3	MBL	,POBLU	,	PR 62940
4	HVE	,PCVE	,	PR 62950
5	HDEA	,PODEA	,	PR 62960
6		PC		PR 62970
	WRITE(L,660)			PR 63000
	WRITE(L,115) VTEID			PR 63010
C	IV. SUBSIDIARY SECTIONS			PR 63020
	WRITE(L,8035) LMTDBH,LMTDCN,			PR 63030
1	HIBH	,HICON	,	PR 63040
2	HOBH	,HOCN	,	PR 63050
3	UBH	,UCCN	,	PR 63060
4	QPH	,QE	,	PR 63070
5	RBH	,RCN	,	PR 63080
6	ABH	,ACN	,	PR 63090
A	NBH	,NCN	,	PR 63100
7	LBH	,LCN	,	PR 63110
A	TCF	,TO	,	PR 63120
8	TM	,TR	,	PR 63130
9	WF	,WO		PR 63140
	WRITE(L,200)			PR 63150
	WRITE(L,115) VTEID			PR 63160
	WRITE(L,202) AMONTH			PR 62260
	WRITE(L,3) (ANAME(KK),KK=1,10)			PR 63180
3	FLHMAT(1HO,10A8)			PR 63190
	WRITE(L,650)			PR 63200
	WRITE(L,655) (I,UE(I),WT(I),CIE(I),IE(I),TC(I),WPEI(I),			PR 63210
1	AE(I),NVE(I),A(I),ALFAE(I),I=1,NE)			PR 63220
	WRITE(L,665) TCON			PR 63230
650	FORMAT(1HC,53X,14HVE EFFECT DATA/			PR 63240
1	1HO,6HEFFECT,4X,4HUBAR,10X,2HWT,9X,3HCIE,7X,2HTE,			PR 63250
2	7X,2HTC,9X,3HWPE,8X,10HAREA (FT2),4X,			PR 63260
3	10HNUM. TUBES,4X,7HDELTA-T,4X,5HALPHA/)			PR 63270
655	FORMAT(1H ,14,2X,F10.2,E14.4,F10.5,2F9.2,3E14.4,F9.2,F11.4)			PR 63280
660	FORMAT('1')			PR 63290
665	FORMAT(50X,F9.2)			PR 63300
8005	FORMAT(3HC 1 2X 21HSUMMARY OF PLANT DATA/1HO 3X 7HGENERAL 48X			PR 63310
	118HPERFORMANCE RATIOS/ 8X 20HPLANT CAPACITY, MGD 10X F10.2, 16X			PR 63320
	27HOVERALL 19X F10.4/ 8X 23HSEA WATER CONCENTRATION 7X F10.5,16X			PR 63330
	33HVE 23X F10.4/ 8X 23HPRODUCT CONCENTRATION 7X F10.6, 16X			PR 63340
	412HPHTR(ACTUAL) 14X F10.4/			PR 63350
5	8X, 19HCONCENTRATION RATIO ,11X, F10.4/			PR 63360
6	8X 17HNUMBER OF EFFECTS 13X 110 /8X 25HNO STAGES IN PREHEAT			PR 63370
7	TER 5X,F10.0/8X 25HYEAR CONSTRUCTION STARTED 5X,F10.0)			PR 63380
8010	FORMAT(1HC 3X 20HTEMPERATURES - DEG F 37X 13HFLOWS, LBS/HR /8X			PR 63390
1	5HSTEAM 25X F10.3, 16X 11HTGTAL STEAM 10X E15.6/8X 13HMAXIMUM BRPR			PR 63400
2	INE 17X F10.3, 16X 8HVE STEAM 13X E15.6/8X 12HFINAL EFFECT 18X			PR 63410
3	F10.3, 16X 10HPHTR STEAM 11X E15.6/8X 8HBLOWDOWN 22X F10.3,16X			PR 63420
4	13HTGTAL PRODUCT 8X E15.6/			PR 63430
5	8X 7HPRODUCT 23X F10.3, 16X 10HVE PRODUCT 11X E15.6 /			PR 63440
6	8X 14HDEAERATED FEED 16X F10.3, 16X 12HPHTR PRODUCT 9X E15.6 /			PR 63450
7	8X 5HOCEAN 25X F10.3, 16X 8HBLOWDOWN 13X E15.6 /			PR 63460
7	64X 16HSEA INTAKE 5X E15.6/			PR 63470
8	8X 18HCONDENSER APPROACH 12X F10.3 , 16X 16HCONDENSER REJECT 5X			PR 63480
9	E15.6 / 64X 18HTUBE VELOCITY, FPS F18.3)			PR 63490
8015	FORMAT(33H011 DESCRIPTION OF PHYSICAL PLANT /1HO 3X 20HPLANT DIMENPR			PR 63500
	1SICNS, FT /8X 20HOVERALL PLANT LENGTH 10X F10.3, 16X 14HOVERALL HEPR			PR 63510
	21GHT 7X F15.3/8X 18HVE AND PHTR LENGTH 12X F10.3, 16X 9HVE HEIGHT			PR 63520
	312X F15.3/8X 15HMIN TRAIN WIDTH 15X F10.3, 16X 11HPHTR HEIGHT 10X			PR 63530
	4F15.3/8X 15HMAX TRAIN WIDTH 15X F10.3, 16X 20HVE SHELL VOLUME, FT3			PR 63540
	5D16.6/8X 12HNO OF TRAINS 18X 110, 16X 22HPHTR SHELL VOLUME, FT3			PR 63550
	6D14.6/8X 21HLENGTH OF STEEL SHELL 9X F10.3, 16X 25HTEMP AT SIL-CNCPR			PR 63560
	7 INTERFACE F11.3)			PR 63570
8020	FORMAT(1HO 3X 18HTUBING DESCRIPTION/ 43X 2HVE 21X 9HPREHEATER			PR 63580
	116X 9HCONDENSER / 8X 19HOUTSIDE DIA, INCHES F21.3,2F26.3/8X			PR 63590
	222HWALL THICKNESS, INCHES,F18.3,2F26.3/ 8X 14HK,8TU/HR FT2 F			PR 63600
	33F26.3/ 8X 18HFLOULING RESISTANCE F22.5,2F26.5/8X 15HFLOODING FACTOPR			PR 63610
	4R 9X 16X 2F26.3/ 8X 11HNO OF TUBES 3X,3F26.0 / 8X 15HTUBE LPR			PR 63620
	LENGTH FT			PR 63630
5	9X F16.3, 2F26.3/ 8X 17HSURFACE AREA, FT2 E23.8,2E26.8/PR			PR 63640
6	8X 18HAVG OVERALL UBAR F22.3, 2F26.3)			PR 63650

```

8030 FORMAT(26H0III HEAD REQUIREMENTS, FT 33X 30HPUMPING POWER REQUIREMPR 63660
IENTS, MW//8X 18HSEA WATER DELIVERY 12X F10.3, 16X 12HINTAKE PUMPSPR 63670
215XF10.4/ 8X 14HPREHEATER FEED16X F10.3, 16X 15HPHTR FEED PUMPS12XPR 63680
3F10.4/8X 16HPRODUCT DELIVERY14X F10.3, 16X 13HPRODUCT PUMPS 14X PR 63690
4F10.4/8X 18HBLWDOWN DISCHARGE12X F10.3, 16X 15HBLWDOWN PUMPS 12XPR 63700
6F10.4/8X 16HVERTICAL EFFECTS 14X F10.3, 16X 12HEFFECT PUMPS 15X PR 63710
7F10.4/8X 17HBOOSTER-DEAERATOR 13X F10.3, 16X 13HBOOSTER PUMPS 14X PR 63720
8F10.4/64X 18HTOTAL (ELECTRICAL) 9X F10.4) PR 63730
8035 FORMAT(24HC IV SUBSIDIARY SECTIONS / 35X 12HBRINE HEATER 10X PR 63750
1 9HCCONDENSER / 1H0 7X 7HMDT, F 17X 2F16.3/ PR 63760
2 8X 20HH INSIDE, B/HR FT2 F 4X2F16.2/PR 63770
3 8X 21HH OUTSIDE, B/HR FT2 F 3X 2F16.2PR 63780
4/ 8X 21HVERALL U, B/HR-FT2-F 3X PR 63790
52F16.3/ 8X 17HHEAT RATE, BTU/HR 7XPR 63800
62E16.6/ 8X 18HFOULING RESISTANPR 63810
7CE 6X 2F16.5/ 8X 17HSURFACE APR 63820
8KEA, FT2 7X 2E16.6/ 8X 11HNO OF TPR 63830
9UBES 13X2F16.0/ 8X 15HTUBE LENGTH,PR 63840
A FT,9X,2F16.3/ PR 63850
B8X,20HTEMP-COOLANT IN, F ,4X,2F16.3/ PR 63860
C8X,20HTEMP-COOLANT EXIT, F,4X,2F16.3/ PR 63870
D8X,9HTUBE FLOW,15X,2E16.6) PR 63880
C***** OUTPUT COST CALCULATIONS PR 63890
WRITE(L,200) PR 63900
WRITE(L,115) VTEID PR 63910
WRITE(L,202)AMONTH PR 62260
WRITE(L,3) (ANAME(KK),KK=1,10) PR 63930
WRITE(L,605) PR 63940
WRITE(L,610) VETUBY,VETUBK,VETUBD,PHTUBY,PHTUBK,PHTUBD, PR 63950
1 SHELLY,SHELLK,SHELLD,PMY ,PMK ,PMD , PR 63960
2 WAITY ,WAITK ,WAITD ,VPY ,VPK ,VPD , PR 63970
3 CMCAPY ,CMCAPK,CMCAPD,INSTRY,INSTRK,INSTRD, PR 63980
4 ELECTY,ELECTK,ELECTD,DEAY ,DEAK ,DEAD , PR 63990
5 CNDSTRY,CNDSRK,CNDSRD,BHY ,BHK ,BHD , PR 64000
6 SBCY ,SBCK ,SBCD , PR 64010
WRITE(L,615) PLCAPY,PLCAPK,PLCAPD,PLDIN ,CGPD , PR 64020
1 RETUBY,RETUBK PR 64030
STFEJ=XC(210)*100.D0 *****
LJC2=XC(211) *****
EJC1=XC(212) *****
WRITE(L,620) HEATY ,HEATK ,EJC2,EJC1,CHEMY,CHEMK , PR 64040
1 POWERY,POWERK,OPERY ,UPERK , PR 64050
2 MAINTY,MAINTK PR 64060
WRITE(L,625) TOTOPY,TOTOPK,TOTALY,TOTALK PR 64070
WRITE(L,630) ELEC ,HEAT,STFEJ ,ACHR ,INT ,AJ , *****
1 EFF ,CAPF ,PLNTLF PR 64090
WRITE(L,635) VTLE ,PHLF ,BHLF ,CONLF , PR 64100
1 TREPVE,TREPPE,TREPUH,TREPCN, PR 64110
2 CFVEI ,CFPHI ,CFBHI ,CFCONI PR 64120
605 FORMAT(1H0,57X,17HCOST SUMMARY PAGE / PR 64130
1 1H0,15X,10HCOMPONENTS,19X,9HCOST-$/YR, PR 64140
2 7X,11HCOST-C/KGAL,7X,13HCOST-$ DIRECT/ PR 64150
3 1H ,15X,10H-----,19X,9H-----, PR 64160
4 7X,11H-----,7X,13H-----) PR 64170
610 FORMAT(1HC,4X,21HEFFECT TUBES + SHEETS ,13X,F15.2,F16.4,F21.2/ PR 64180
1 1H ,4X,21HPHTR TUBES + SHEETS ,13X,F15.2,F16.4,F21.2/ PR 64190
2 1H ,4X,21HVE + PHTR SHELL ,13X,F15.2,F16.4,F21.2/ PR 64200
3 1H ,4X,21HPUMPS AND MOTORS ,13X,F15.2,F16.4,F21.2/ PR 64210
4 1H ,4X,21HSEA-WATER INTAKE ,13X,F15.2,F16.4,F21.2/ PR 64220
5 1H ,4X,21HVALVES AND PIPING ,13X,F15.2,F16.4,F21.2/ PR 64230
6 1H ,4X,21HCHEMICAL CAPITAL ,13X,F15.2,F16.4,F21.2/ PR 64240
7 1H ,4X,21HINSTRUMENTS ,13X,F15.2,F16.4,F21.2/ PR 64250
8 1H ,4X,21HELECTRICAL ,13X,F15.2,F16.4,F21.2/ PR 64260
9 1H ,4X,21HNCG REMOVAL SYSTEM ,13X,F15.2,F16.4,F21.2/ PR 64270
A 1H ,4X,21HCONDENSER ,13X,F15.2,F16.4,F21.2/ PR 64280
B 1H ,4X,21HBRINE HEATER ,13X,F15.2,F16.4,F21.2/ PR 64290
C 1H ,4X,21HSITE, BLDGS., CRANES ,13X,F15.2,F16.4,F21.2/ PR 64300
D 1H ,93X,13HCOST-$DIR+IND,7X,5H$/GPD,/ PR 64310
E 1H ,93X,25H-----) PR 64320

```

```

615 FORMAT(1H ,8X,13HTOTAL CAPITAL,17X,F15.2,F16.4,F21.2,F15.2,F12.4/ PR 64330
1      1H0,8X,13HRETUBING ,17X,F15.2,F16.4) PR 64340
620 FORMAT(1H0,4X,19HPROCESS HEAT ,15X,F15.2,F16.4/ PR 64350
*      1H ,4X,19HSTEAM TO EJECTORS ,15X,F15.2,F16.4/ *****
1      1H ,4X,19HCHEMICAL ,15X,F15.2,F16.4/ PR 64360
2      1H ,4X,19HPOWER ,15X,F15.2,F16.4/ PR 64370
3      1H ,4X,19HOPERATING ,15X,F15.2,F16.4/ PR 64380
4      1H ,4X,19HMAINT. + SUPPLIES ,15X,F15.2,F16.4) PR 64390
625 FORMAT(1H0,8X,15HTOTAL OPERATING,15X,F15.2,F16.4/ PR 64400
1      1H0,33HTOTAL(CAPITAL+RETUBING+OPERATING),5X,F15.2,F16.4) PR 64410
630 FORMAT(13HOCOST FACTORS/ PR 64420
1      35HOCOST OF ELECTRICITY, C/KWHR ,F16.6/ PR 64430
2      35H COST OF PROCESS HEAT, C/MBTU ,F16.6/ *****
*      35H COST OF EJECTOR STEAM, C/MBTU ,F16.6/ *****
3      35H ANNUAL CHARGE RATE ,F16.6/ PR 64450
4      35H INTEREST RATE ,F16.6/ PR 64460
5      35H HIGHER COST FACTOR ,F16.6/ PR 64470
6      35H PUMP AND MOTOR EFFICIENCY ,F16.6/ PR 64480
7      35H PLANT LOAD FACTOR ,F16.6/ PR 64490
8      35H PLANT LIFE, YEARS ,F16.6) PR 64500
635 FORMAT(1H0,27X,16H VERTICAL EVAP. ,16H PREHEATER , PR 64510
1      16H BRINE HEATER ,16H CONDENSER / PR 64520
2      21HCTUBE LIFE, YEARS ,5X,4F16.8/ PR 64530
3      21H RETUBING CHARGE RATE,5X,4F16.8/ PR 64540
4      21H AREA COST, $/SQ.FT. ,5X,4F16.8/3X 11H(INSTALLED) ) PR 64550
C PR 64560
1000 CONTINUE PR 64570
C PR 64580
WRITE(L,7000) PR 64590
WRITE(L,115) VTEID PR 64600
WRITE(L,202)AMCNTH PR 64620
WRITE(L,3) (ANAME(KK),KK=1,10) PR 64620
WRITE(L,7005) MGD ,PRP ,PRVE ,PRPH ,CRVE ,CR , PR 64630
1      CO ,CP ,CB ,CIE(NE),MAVG ,CAPF , PR 64640
WRITE(L,7010) TS ,TM ,TCF ,TE(NE) ,TCON ,STLTMP , PR 64650
1      TO ,TOO ,TB ,TP ,TR ,STLLEN , PR 64660
WRITE(L,7015) WP ,WPE ,WPPH ,WOCEAN ,WF , PR 64670
1      WC ,WR ,WM ,WSE ,WSPH ,WS , PR 64680
WRITE(L,7020) ANE ,EFFL ,LVEP ,VEHGT ,VEVOL ,TRAINS , PR 64690
1      NPH ,ELL ,LPH ,PHHGT ,PHVOL ,BLOGS , PR 64700
2      WVEMAX ,WVEMIN ,ACRES ,QVRHGT ,TOTVOL ,FNBH , PR 64710
WRITE(L,7025) QDBH ,WALBH ,LBH ,NBH ,ABH ,VBH , PR 64720
1      OCPH ,WALPH ,LPH ,NTPH ,APH ,VPH , PR 64730
2      ODCON ,WALCON ,LCON ,NCON ,ACON ,VCON , PR 64740
3      ODVE ,WALVE ,LVE ,TOTNVE ,TOTAVE ,GPM , PR 64750
WRITE(L,7030) UBH ,HIBH ,HOBH ,KBH ,RBH ,LMTDBH , PR 64760
1      AVGUPH ,AVHIPH ,AVHOPH ,KPH ,RPH ,AVLTPH , PR 64770
2      UCON ,HICON ,HOCON ,KCON ,RCON ,LMTDCN , PR 64780
3      AVGUE , , KVE ,RVE ,AVDTVE , PR 64790
WRITE(L,7035) QE , ,AVDPE ,AVDPE , PR 64800
1      QPH ,QTR ,AVQMSF ,AVGSUB ,ROA , PR 64810
WRITE(L,7040) HSEA ,HFEED ,HPR ,HBL ,HVE ,HDEA , PR 64820
1      RPMO ,RPMR ,RPMP ,RPMB ,RPMV ,RPM , PR 64830
2      POSEA ,POFEED ,POPRO ,POBLO ,POVE ,PODEA , PR 64840
3      HEADPH ,HEADBH ,HEADCN ,EFF ,POUEAS ,PO , PR 64850
WRITE(L,7045) AJ ,AXJ ,INT ,ACHR ,ANCOMP ,FDFAC , *****
1      VTLF ,PHLF ,BHLF ,CONLF ,PLNTLF ,QEFAC , *****
2      TREPVE ,TREPPH ,TREPBH ,TREPCH ,XC(56) ,TRFAC , *****
WRITE(L,7050) CFVE ,CFPH ,CFBH ,CFCON ,CFSHEL ,HEAT , PR 64890
1      CFVEI ,CFPHI ,CFBHI ,CFCONI ,CFPUMP ,ELEC , PR 64900
WRITE(L,7055) VETUBD ,PHTUBD ,SHELLD ,PMO ,WAITD , PR 64910
1      VPD ,CMCAPD ,DEAD ,CNUSRD ,BHD ,PLCAPD , PR 64920
2      INSTRD ,ELECTD ,SBCD , , ,PLDIN , PR 64930
WRITE(L,7060) VETUBY ,PHTUBY ,SHELLY ,PMY ,WAITY , PR 64940
1      VPY ,CMCAPY ,DEAY ,CNDSRY ,BHY ,RETUBY , PR 64950
2      INSTRY ,ELECTY ,SBCY , , ,PLCAPY , PR 64960
3      HEATY ,CHEMY ,POWERY ,OPERY ,MAINTY ,TOTOPY , PR 64970
4      TCTALY , , , , , PR 64980
WRITE(L,7065) VETUBK ,PHTUBK ,SHELLK ,PMK ,WAITK , PR 64990

```

```

1          VPK      ,CMCAPK ,DEAK      ,CNDSRK ,BHK      ,RETUBK ,      PR 65000
2          INSTRK ,ELECTK ,SBCK      ,PLCAPK ,      PR 65010
3          HEATK  ,CHEMK  ,POWERK ,OPERK  ,MAINTK ,TOTOPK ,      PR 65020
4          YEAR   ,CGPD   ,TOTALK      PR 65030
C          PR 65040
C OUTPUT FORMATS FOR CONDENSED SUMMARY PAGE      PR 65050
C          PR 65060
7000 FORMAT(1H1,'VERTICAL TUBE EVAPORATOR PLANT - ROUTINE VTE21',7X,      PR 65070
1          ' CONDENSED SUMMARY OF PLANT DATA')      PR 65080
7005 FORMAT(1HC,'MGO      PRP      PRVE      PRPH      CRVE      CR      ',6D14.6/      PR 65090
1          ' CO      CP      CB      CIE(NE) MAVG      CAPF      ',6D14.6/      PR 65100
7010 FORMAT(1HC,'TS      TM      TCF      TE(NE) TCON      STLTMP      ',6D14.6/      PR 65110
1          ' TO      TOO      TB      TP      TR      STLTEN      ',6D14.6/      PR 65120
7015 FORMAT(1HC,'WP      WPE      WPPH      WOCEAN      WF      ',3D14.6,14XPR 65130
A2D14.6/      PR 65140
1          ' WO      WR      WM      WSE      WSPH      WS      ',6D14.6/      PR 65150
7020 FORMAT(1HC,'ANE      EFFL      LVEP      VEHGT      VEVOL      TRAINS      ',6D14.6/      PR 65160
1          ' NPH      ELL      LPH      PHHGT      PHVOL      BLDGS      ',6D14.6/      PR 65170
2          ' WVEMAX      WVEMIN      ACRES      OVRHGT      TOTVOL      ENBH      ',6D14.6/      PR 65180
7025 FORMAT(1HC,'OQBH      WALBH      LBH      NBH      ABH      VBH      ',6D14.6/      PR 65190
1          ' ODPH      WALPH      LPH      NTPH      APH      VPH      ',6D14.6/      PR 65200
2          ' ODCN      WALCON      LCON      NCON      ACON      VCON      ',6D14.6/      PR 65210
3          ' OOVE      WALVE      LVE      TOTNVE      TOTAVE      GPM      ',6D14.6/      PR 65220
7030 FORMAT(1HC,'UBH      HIBH      HOBH      KBH      RBH      LMTDBH      ',6D14.6/      PR 65230
1          ' AVGUPH      AVHIPH      AVHOPH      KPH      RPH      AVLTPH      ',6D14.6/      PR 65240
2          ' UCON      HICON      HOCON      KCON      RCON      LMTDCN      ',6D14.6/      PR 65250
3          ' AVGUE      KVE      RVE      AVDTVE      ',D14.6,28XPR 65260
4          3D14.6)      PR 65270
7035 FORMAT(1HC,'QE      AVDPE      AVBPE      ',D14.6,14X,PR 65280
12D14.6/      PR 65290
2          ' QPH      QTR      AVQMSF      AVGSUB      ROA      ',2D14.6,14XPR 65300
33D14.6)      PR 65310
7040 FORMAT(1HC,'HSEA      HFEED      HPR      HBL      HVE      HDEA      ',6D14.6/      PR 65320
1          ' RPMG      RPMR      RPMF      RPMb      RPMV      RPMH      ',6D14.6/      PR 65330
2          ' POSEA      POFEED      POPRO      POBLO      POVE      PODEA      ',6D14.6/      PR 65340
3          ' HEADPH      HEADBH      HEADCN      EFF      PODEAS      PO      ',6D14.6/      PR 65350
7045 FORMAT(1HC,'AJ      AXJ      INT      ACHR      ANCONP      FDFAC      ',6D14.6/      ****
1          ' VTLF      PHLF      BHLF      CONLF      PLNTLF      QEFAC      ',6D14.6/      ****
2          ' TREPVE      TREPPH      TREPbH      TREPCN      AERTE      TRFAC      ',6D14.6/      ****
7050 FORMAT(1HC,'CFVE      CFPH      CFBH      CFCON      CFSHEL      HEAT      ',6D14.6/      PR 65390
1          ' CFVEI      CFPHI      CFBHI      CFCONI      CFPUMP      ELEC      ',6D14.6/      PR 65400
7055 FORMAT(1HC,'VETUBD      PHTUBD      SHELLD      PMD      WAITD      ',5D14.6/      PR 65410
1          ' VPD      CMCAPO      DEAD      CNDSRD      BHD      PLCAPO      ',6D14.6/      PR 65420
2          ' INSTRD      ELECTD      SBOD      PLDIN      ',3D14.6,      PR 65430
A28X,D14.6)      PR 65440
7060 FORMAT(1HC,'VETUBY      PHTUBY      SHELLY      PMY      WAITY      ',5D14.6/      PR 65450
1          ' VPY      CMCAPY      DEAY      CNDSRY      BHY      RETUBY      ',6D14.6/      PR 65460
2          ' INSTRY      ELECTY      SBCY      PLCAPY      ',3D14.6,      PR 65470
A28X,D14.6/      PR 65480
3          ' HEATY      CHEMY      POWERY      OPERY      MAINTY      TOTOPY      ',6D14.6/      PR 65490
4          ' TOTALY      ',70X,D14.6)PR 65500
7065 FORMAT(1HC,'VETUBK      PHTUBK      SHELLK      PMK      WAITK      ',5D14.6/      PR 65510
1          ' VPK      CMCAPK      DEAK      CNDSRK      BHK      RETUBK      ',6D14.6/      PR 65520
2          ' INSTRK      ELECTK      SBCK      PLCAPK      ',3D14.6,      PR 65530
A28X,D14.6/      PR 65540
3          ' HEATK      CHEMK      POWERK      OPERK      MAINTK      TOTOPK      ',6D14.6/      PR 65550
4          ' YEAR      CGPD      TOTALK      ',42X,3D14.6)PR 65560
RETURN      PR 65570
END      PR 65580

```

THIS PAGE
WAS INTENTIONALLY
LEFT BLANK

Internal Distribution

- | | |
|-------------------------|--------------------------------------|
| 1. T. D. Anderson | 15-39. S. A. Reed |
| 2. S. J. Ball | 40. M. W. Rosenthal |
| 3. D. F. Cope | 41. M. R. Sheldon |
| 4. W. B. Cottrell | 42. M. J. Skinner |
| 5. F. L. Culler | 43. I. Spiewak |
| 6. G. G. Fee | 44. J. J. Taylor |
| 7. M. J. Goglia | 45. D. B. Trauger |
| 8. R. F. Hibbs | 46. W. J. Wilcox |
| 9. R. E. MacPherson | 47-51. J. V. Wilson |
| 10. W. J. McCarthy, Jr. | 52-53. Central Research Library |
| 11. J. W. Michel | 54. Document Reference Section |
| 12. J. S. Johnson | 55-57. Laboratory Records Department |
| 13. J. E. Jones | 58. Laboratory Records, RC |
| 14. H. Postma | |

External Distribution

- 59-63. Pinhas Glueckstern, Desalting Dept., Mekoroth Water Co.,
9 Lincoln Street, Tel Aviv, Israel.
- 64-68. W. F. Savage, Advanced Concepts Evaluation Branch, U.S. Energy
Research and Development Administration, Washington, D.C. 20545
- 69-70. Director, Division of Nuclear Research and Applications, ERDA,
Washington, D. C. 20545
71. Director, Reactor Division, ERDA, ORO
72. Research and Technical Support Division, ERDA, ORO
- 73-99. Technical Information Center, ERDA