

CONF-780114--8

MASTER

ON THE DESIGN OF CPC PHOTOVOLTAIC SOLAR COLLECTORS

By

Robert M. Graven, Anthony J. Gorski, and William R. McIntire

MN ONLY

NOTICE

**PORTIONS OF THIS REPORT ARE ILLEGIBLE. It  
has been reproduced from the best available  
copy to permit the broadest possible avail-  
ability.**

—NOTICE—  
This report was prepared as an account of work sponsored by the United States Government. Neither the United States nor the United States Department of Energy, nor any of their employees, nor any of their contractors, subcontractors, or their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness or usefulness of any information, apparatus, product or process disclosed, or represents that its use would not infringe privately owned rights.

Prepared For

International Solar Energy Society

New Delhi, India

January 16-20, 1978



U of C-AUA-USDOE

*8B*  
DISTRIBUTION OF THIS DOCUMENT IS UNLIMITED

ARGONNE NATIONAL LABORATORY, ARGONNE, ILLINOIS

Operated under Contract W-31-109-Eng-38 for the  
U. S. DEPARTMENT OF ENERGY

## DISCLAIMER

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency Thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

## **DISCLAIMER**

**Portions of this document may be illegible in electronic image products. Images are produced from the best available original document.**

The facilities of Argonne National Laboratory are owned by the United States Government. Under the terms of a contract (W-31-109-Eng-38) between the U. S. Department of Energy, Argonne Universities Association and The University of Chicago, the University employs the staff and operates the Laboratory in accordance with policies and programs formulated, approved and reviewed by the Association.

#### MEMBERS OF ARGONNE UNIVERSITIES ASSOCIATION

The University of Arizona	Kansas State University	The Ohio State University
Carnegie-Mellon University	The University of Kansas	Ohio University
Case Western Reserve University	Loyola University	The Pennsylvania State University
The University of Chicago	Marquette University	Purdue University
University of Cincinnati	Michigan State University	Saint Louis University
Illinois Institute of Technology	The University of Michigan	Southern Illinois University
University of Illinois	University of Minnesota	The University of Texas at Austin
Indiana University	University of Missouri	Washington University
Iowa State University	Northwestern University	Wayne State University
The University of Iowa	University of Notre Dame	The University of Wisconsin

#### —NOTICE—

This report was prepared as an account of work sponsored by the United States Government. Neither the United States nor the United States Department of Energy, nor any of their employees, nor any of their contractors, subcontractors, or their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness or usefulness of any information, apparatus, product or process disclosed, or represents that its use would not infringe privately-owned rights. Mention of commercial products, their manufacturers, or their suppliers in this publication does not imply or connote approval or disapproval of the product by Argonne National Laboratory or the U. S. Department of Energy.

## BEGIN ON THE DESIGN OF CPC PHOTOVOLTAIC SOLAR COLLECTORS\*

Robert M. Graven, Anthony J. Gorski, and William R. McIntire  
Argonne National Laboratory  
Argonne, Illinois, U.S.A.

### ABSTRACT

Two new photovoltaic solar collectors have been designed, built and tested. A substantial improvement in performance has been achieved in that they produce more electrical power and use significantly less photovoltaic material per unit area than the present state-of-the-art flat panel arrays. A reflective style Compound Parabolic Concentrator (CPC) optical system was used for one collector, and a dielectric style (DCPC) optical system was used for the other collector to concentrate sunlight onto custom designed photovoltaic solar cells. For these two panels only periodic angular adjustments are required, which eliminates the need for two-axis tracking.

A modular design of individual sub-units containing an array of series and parallel circuits allows a user to select a variety of operating conditions. The dielectric CPC panel can provide a peak voltage selected from the range of 6V to 120V d.c., in steps of 6V, and a peak current from the range of 23A to 1.15A, in 1.15A increments, respectively. The modular design also allows rapid replacement and repair of individual sub-units. The mechanical assembly was designed to withstand a very heavy load of 250 Kg/m<sup>2</sup>.

The reflective CPC photovoltaic panel is 1.22m by 1.22m, requires thirty-six adjustments per year, and delivers 97 peak watts under 1 kW/m<sup>2</sup> of direct insolation. The dielectric CPC panel is also 1.22m by 1.22m, but only requires ten adjustments per year, and delivers 138 peak watts under 1 kW/m<sup>2</sup> of direct insolation. The net energy conversion efficiency over the entire dielectric CPC panel, including the frame, was 10.3%. The design considerations for these panels are summarized in this paper.

### INTRODUCTION

The design and development of solar collectors which produce both heat and electricity is influenced by many factors. Ordinarily, the cost, quoted in dollars per watt, is the dominant design consideration. Since the cost of producing photovoltaic cells is the major cost in collector manufacturing, it is obvious that the amount of photovoltaic material should be reduced. However, deciding when to stop attempting to reduce the amount of photovoltaic material is a complex function of the expected future costs of the material,

its packaging, and the efficiency of the cells operation. Each of these cost factors are, in turn dependent upon a wide variety of other conditions, usually quite unrelated to the physical or technical limitations of collector design.

One basic principle for the design of photovoltaic solar collectors should be to develop a durable, maintenance free product. The best design, from the user's viewpoint, is one that will last forever, and require no maintenance. Certainly, collectors which require two axis mechanical tracking equipment, must withstand extreme wind pressure, and maintain positioning to  $\pm 0.5$  degrees are poor candidates to meet these desired objectives. However, from a manufacturer's viewpoint, the repair and replacement activities can be rather profitable. This contradiction must be resolved in the users favor, if the implied and promised advantages of solar photovoltaic power are to be realized. In the spirit of attempting to develop a maintenance free collector, the use of the most durable materials and design is required.

### MECHANICAL DESIGN

The mechanical design of these collectors is based on the desire to produce a device that could withstand a very heavy static load of 250 Kg/m<sup>2</sup>. In addition, torsion, bending, vibration, and sheer forces were computed and a structural frame was assembled which would resist impacts and pressure from any direction. In particular, a metal border was provided surrounding the panels so that it could be rested on any corner or edge without damaging the panel. The self supporting frame has a variety of mounting holes to permit flexibility in attaching the collector to a base, and for adjustments of its tilt angle. Both collectors used essentially the same design for the support frame. In order to meet the time constraints for the construction of the panels, only standard aluminum channels, L's, and T's, were used; no attempt was made at reducing the weight of the frame and collector modules.

Acrylic (polymethyl-methacrylate) was used to form the dielectric CPC troughs, and for the covers of the reflective CPC modules. This material has shown resistance to damage from severe wind, rain, hail, ice, and snow storms as well as resistance to

\* This work was funded by The Division of Solar Energy of the U.S. Energy Research and Development Administration through the concentrator research program administered by the Sandia Laboratory.

degradation from ultraviolet radiation. An extended sandstorm would probably craze the surface, however, if a more resistant coating is applied, then damage from sandstorms may be reduced. Several coatings may be applied if the local conditions require anit-abrasive, anti-reflective, or anti-static treatment. Futhermore, acrylic is easily mass produced using injection molding techniques. Casting techniques, using an optically clear epoxy which is resistant to ultraviolet degradation, provide a manufacturing method and material for large panels which is also easily mass produced.

The mechanical structure is based on a modular design. The dielectric CPC panel consists of 20 modules arranged in a 4 by 5 array, and the reflective panel consists of 16 modules, arranged in a 4 by 4 array. The modular design was chosen to simplify the development of several prototype mini-panels, before a manufacturing commitment was made for a complete panel. It also allowed for the many presentations of the collector to a wide audience. In addition, the modular construction allowed several individuals to simultaneously assemble, and test easily handled units.

## ELECTRICAL DESIGN

Figure 1 illustrates the photovoltaic solar cells developed for these panels. The nominal dimensions of the cells were specified as 0.284 cm wide, 2.570 cm long, and 0.0305 cm thick. The minimum acceptable solar power conversion efficiency was 12%, at 28°C when illuminated at 1 W/cm<sup>2</sup> (equivalent to ten suns) with an AM1 (or equivalent) solar spectrum. The base layer is p-type and the diffused surface layer is n-type. Two cells are shown, one having grid fingers connected to the metalization pattern (shaded), and one without grid fingers. The performance of these two cells was not significantly different, due to the low concentration of sunlight.

The same solar cell assembly was used for both the dielectric and the reflective CPC panels. Kovar was used as the heat sink material, in order to match the coefficient of expansion for the silicon. The Kovar heat sinks were plated with silver and solder, and served as the rear electrical contact for the diodes. The heat sinks were soldered to circuit sheets for the reflective panel, and to small buss bars for the dielectric panel. Each cell was tested and binned, before they were assembled into arrays. Each array was again tested, before the optical components were attached. Nine cells were wired in parallel to form one row of a dielectric CPC module, and ten cells were wired in parallel to form one row of a reflective CPC module. Having nine or ten cells in parallel provides a substantial improvement in reliability over the usual designs which ordinarily have one string of diodes in a simple series arrangement, where if one diode opens, the entire panel is worthless. Twelve rows were wired in series to complete a module which would be capable of charging a 6V battery.

The modular design permitted various combinations of modules to provide a selection of voltage and cur-

rent combinations. One disadvantage of the modular approach is that full use of the illuminated surface of the panel is not achieved. For a commercial panel this disadvantage should be minimized, but for the experimental prototypes we developed it was not an important consideration.

Several solar cell and heat sink assemblies were designed that could be readily manufactured using automatic assembly equipment. Many variations are available in the cell-sink assembly for semiconductor wafers, ribbons, tubes, sticks, slices and chips. The cost of manufacture, assembly, and testing determines the configuration of concentrator, cell, and heat exchanger. If the cost of high efficiency solar cells continues to decline, then the design must reflect the rising relative cost of other materials, inventory costs, shipping, repair, and marketing limitations. The CPC shape allows many variations in the concentration, and hence the amount of photovoltaic material needed to produce electricity.

## THERMAL DESIGN

The thermal design is the basis for all solar collectors. The design objective is usually the highest possible collection efficiency consistent with a useable quality (temperature) of heat. For flat plate photovoltaic collectors the thermal aspects are often considered to be of secondary importance, however for concentrating collectors the heat is available at higher temperatures and hence will have more uses.

The present collectors are designed to maintain the solar cells at a minimum temperature in order to eliminate the need for any active cooling equipment. An extended surface heat sink was selected to provide less than 6°C temperature rise between the cells and a 60°C ambient, under a 1 Kw/m<sup>2</sup> insolation.

The dielectric CPC panel receives a total of 1,254 W (or 4,270 Btu/hr.) of which approximately 10% is converted to electricity, about 20% is rejected from the front surface, and about 70% is available at the rear surface for heating. If the air flow across the rear heat exchanger is controlled, then various temperatures may be obtained. A primary goal should be to develop a collector that will provide electricity and heat for a residence in the amounts, and at the time, each is needed.

## PERFORMANCE

Figure 2 gives the characteristic current, voltage curve for an average dielectric CPC module. The module is 27.4 cm by 22.9 cm, has an open circuit voltage of 7.76 volts, a short circuit current of 1.21 amps, and a peak power of 7.01 watts.

Figure 3 presents a comparison of the power obtained from an array of photovoltaic cells without a concentrator, and with the dielectric CPC

attached to the solar cells, both curves are for 1  $\text{Kw}/\text{m}^2$  of direct insolation.

Figure 4 illustrates the performance of the dielectric CPC panel having 20 modules. One row of four modules were wired in parallel, and five rows were wired in series, to obtain this particular curve.

Figure 5 gives the characteristic current, voltage curve for the reflective CPC panel. This panel was composed of 16 reflective CPC modules, and had a power conversion efficiency of 9.64% over its active area.

Figure 6 provides a comparison of the output power for the reflective CPC modules, with and without the concentrators.

#### ACKNOWLEDGEMENTS

The administrative assistance of M. Kyle, W. Schertz, and S. Zwerdling, the technical advice of A. Rabl, K. Reed, and R. Winston, the construction, assembly, and testing by P. Albrecht, R. Rush, and A. Wantruba, the cost calculations by R. Cole, and the patience and understanding of D. Knox are all gratefully acknowledged.

#### REFERENCES

R. Cole, A. Gorski, R. Graven, W. McIntire, W. Schertz, R. Winston, and S. Zwerdling, "Application of Compound Parabolic Concentrators to Solar Photovoltaic Conversion", Argonne National Laboratory report ANL-77-42, February 1977.

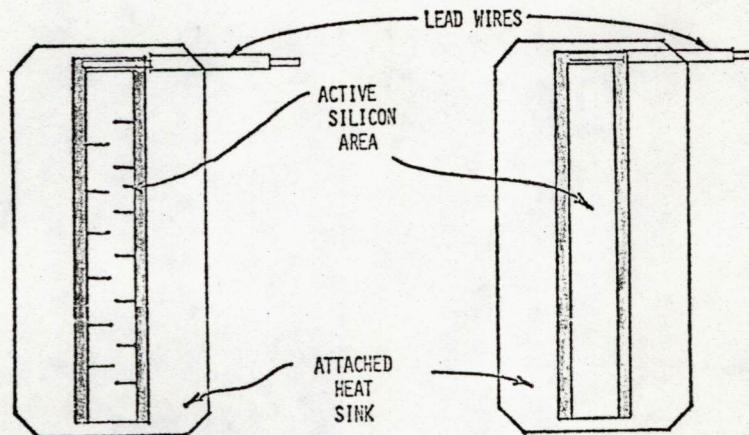


FIGURE 1. PHOTOVOLTAIC SOLAR CELLS

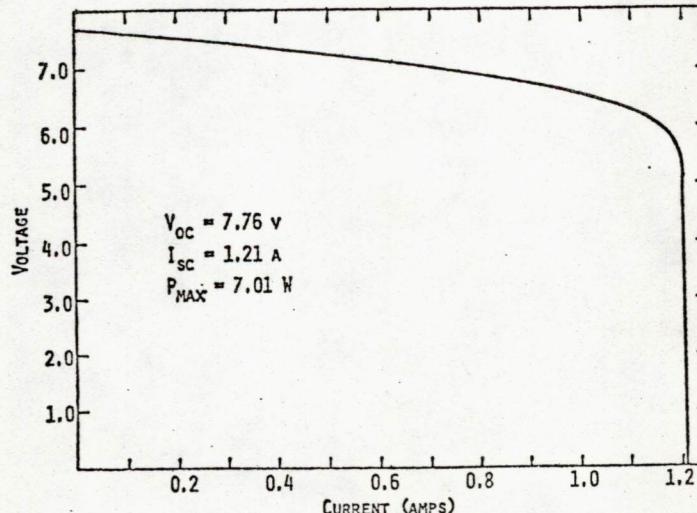


FIGURE 2. AVERAGE DCPC MODULE PERFORMANCE  
(SCALED TO 1  $\text{Kw}/\text{m}^2$  DIRECT)

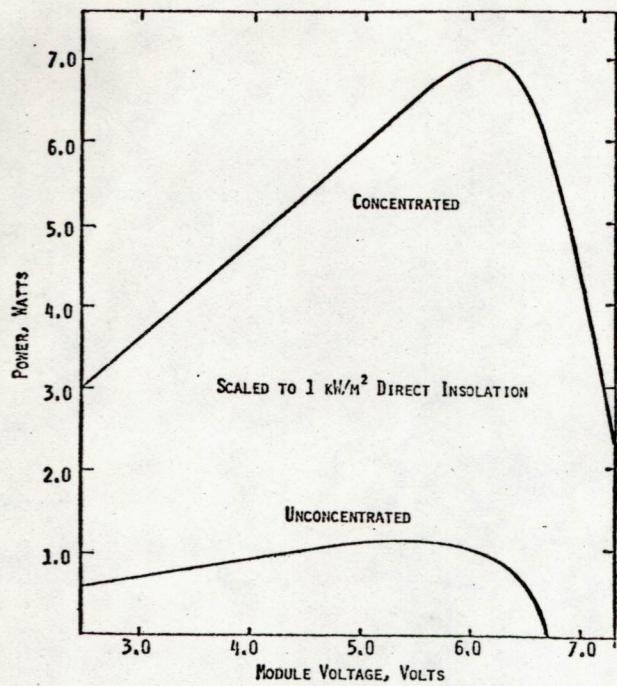


FIGURE 3. AVERAGE DCPC MODULE POWER CURVES

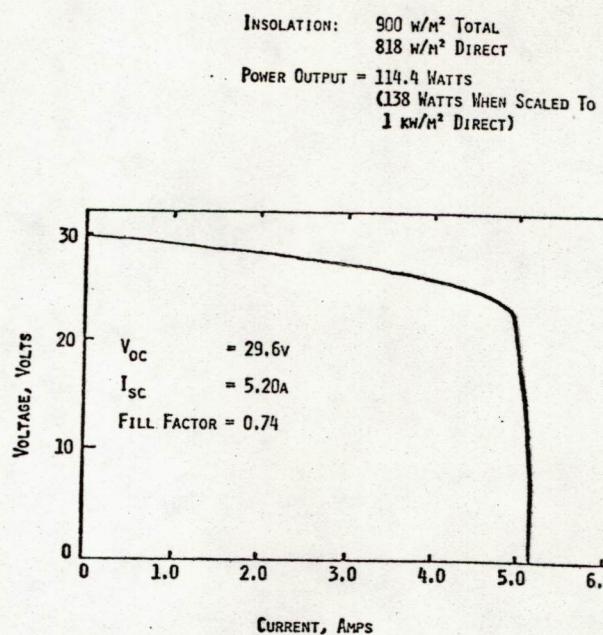


FIGURE 4. PERFORMANCE CURVE FOR DCPC PANEL

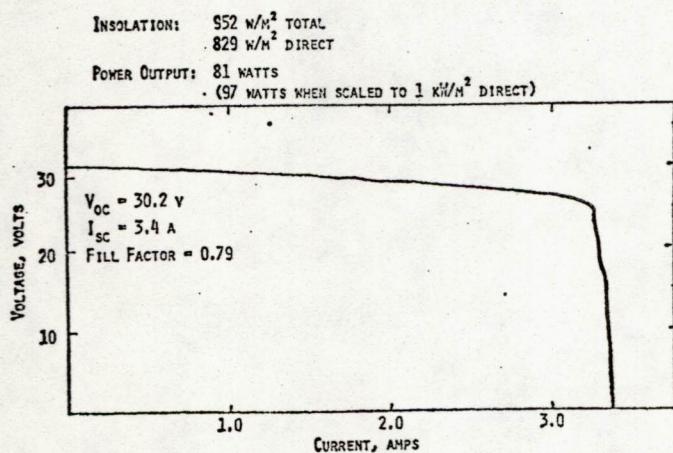


FIGURE 5. PERFORMANCE OF CPC PANEL

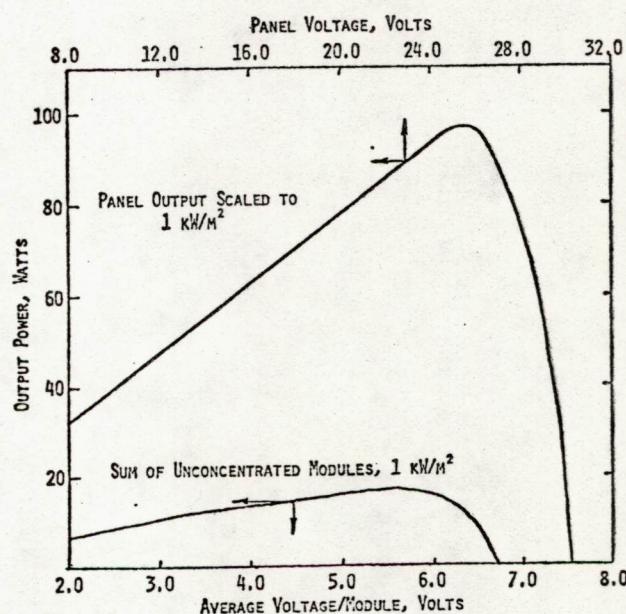


FIGURE 6. CPC PANEL OUTPUT POWER