

Behavior of Titanium Sublimation and

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Sputter Ion Pumps in the  $10^{-11}$  Torr Range\*

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Abstract

In the proposed Intersecting Storage Accelerator, ISABELLE, 1200 pumping stations will be used to keep two 3 km long rings at a pressure of  $1 \times 10^{-11}$  Torr. It is clear that in such a large system, price and simplicity are very important. We have therefore undertaken a study on a well instrumented room temperature vacuum system with a surface area of  $6000 \text{ cm}^2$  and a volume of  $17 \text{ l}$ , pumped by a Ti-ball and an ion pump. Total pressure and residual gas composition were measured by a Helmer gauge and a quadrupole mass spectrometer. The final pressures of  $\sim 1 \times 10^{-11}$  Torr were reached with Ti films and a  $20 \text{ l s}^{-1}$  sputter-ion pump. The main residual gas components were hydrogen and methane. The ultimate pressure was determined primarily by the ability of Ti films to pump  $\text{H}_2$  and depend on the method of laying down the film and the surface temperature. Previous surface preparation seemed relatively unimportant. Two methods of pumping  $\text{CH}_4$  were investigated, namely, a) cracking the molecules on hot tungsten filament and b) conventional sputter-ion pumping. Sputter-ion pump was found to be more efficient and preferable.

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## I. Introduction

The Intersecting Proton Storage Accelerator Facility ISABELLE<sup>1</sup> will consist of two rings having a circumference of 3 km each. To insure proper operation of colliding beam experiments, the pressure in the vacuum chamber of the rings should be about  $1 \times 10^{-11}$  Torr (N<sub>2</sub> equivalent).<sup>2</sup> For the vacuum system we have selected an 8 cm diameter tube of aluminum alloy Al 6061 pumped every 5 m by a pumping station which contains a titanium sublimator and an ion pump. Extensive surface treatment and outgassing tests have been made on pipes of this Al alloy.<sup>4</sup> It has been found that a surface treatment consisting of chemical polishing and a glow discharge cleaning in argon and oxygen followed by  $\sim 200^{\circ}$  C bake-out resulted in a hydrogen outgassing rate of  $1 \times 10^{-13}$  Torr liter cm<sup>-2</sup> s<sup>-1</sup>. The content of other residual gases was negligible. It is clear that this low outgassing rate will produce a pressure rise of only  $\sim 2 \times 10^{-12}$  Torr above the pressure attained in the pumping station. Since more than 1200 of these units will be required, the main task becomes to design a simple inexpensive pumping station having a large pumping speed for hydrogen and operating routinely below  $3 \times 10^{-11}$  Torr hydrogen pressure.

Only a modest pumping speed is required for non-getterable gases (helium, methane and argon). A combination of a titanium sublimator and a small sputter ion pump satisfies the criteria of both economy and simplicity. A vacuum system to investigate these two methods of pumping was therefore constructed. Extensive data obtained in the  $10^{-11}$  Torr range confirmed that a small ion pump and a Ti-ball can routinely achieve the required pressures.

During the course of this work, which started as an engineering study of well understood phenomena,<sup>5-7</sup> it was realized that both titanium films and ion pumps behave differently at  $1 \times 10^{-11}$  Torr than at higher pressures. In fact, hydrogen pumping by Ti films was sufficiently different to warrant more funda-

mental experiments on Ti - H<sub>2</sub> systems at very low pressures which are now in progress. I will, however, limit my discussion to a description of how to achieve a nitrogen equivalent pressure of  $1 \times 10^{-11}$  Torr and what precautions have to be taken in the construction of such a system, in the selection of its components and in the interpretation of the results.

## II. Experimental Apparatus

The main factors which determined the achievement of  $1 \times 10^{-11}$  Torr in our experimental set-up were:

1. The ability of Ti films to pump hydrogen.
2. The ability of ion pumps to pump methane without introducing helium back into the system.

The apparatus in which this study was conducted is shown schematically in Fig. 1. It consists of a standard Varian 15 cm cross and a stainless steel cylinder of the same diameter containing a titanium sublimator. The surface area and the volume of the system are  $6000 \text{ cm}^2$  and  $17\ell$  respectively. The entire system can be covered with an oven and baked out up to  $360^\circ \text{ C}$ .

The total and partial pressures were measured by a Helmer gauge, G, and UTI quadrupole mass spectrometer, MS. It is essential that both measuring devices, but especially the mass spectrometer, be mounted directly inside the main vacuum volume. The mass spectrometer when connected to the cross through a N<sub>2</sub> conductance of  $30\ell \text{ s}^{-1}$  gave completely erroneous results. In order to reduce the heating of the walls of the apparatus and to extend the operation to  $1 \times 10^{-13}$  Torr, the Helmer gauge was operated with thoriated tungsten filament<sup>8</sup> which runs at a temperature  $< 1200 \text{ K}$  for the rated emission of 10 mA. Altogether three sputter ion pumps, S<sub>1</sub>, (Varian  $20\ell \text{ s}^{-1}$  and  $30\ell \text{ s}^{-1}$  triode pumps and Vecco  $30\ell \text{ s}^{-1}$  Mag-Ion pump) were tested during this experiment. They were connected either directly or through a 7 cm Varian all metal valve, V<sub>1</sub>, having N<sub>2</sub> conductance of  $\sim 32\ell \text{ s}^{-1}$ , to the cross (Fig. 1).

For every experimental run the system is first pumped out by a sorption pump and leak checked. This is followed by a  $150^{\circ}$  C bake to transfer most of the water and other easily removable gases into the sorption pump. After about 8 hours at this temperature,  $V_3$  in Fig. 1 is closed and  $V_4$  opened. The bake out continues into a  $100\ell\ s^{-1}$  ion pump,  $S_2$ , for a time at the temperature required by the various experimental schedules. During this bake out the Helmer gauge and the mass spectrometer are degassed and the Ti-ball is operated at standby power for 15 minutes. At the end of each bake out cycle,  $S_1$  is switched on. Thirty minutes later  $V_2$  is closed and the system is cooled down. In addition to the above cycle the Ti-ball was initially conditioned by being operated at its standby power for 50 hours while the system temperature was held at  $200^{\circ}$  C. During the cool down, the Helmer gauge and the mass spectrometer were again outgassed.

### III. Measurements

Total and partial pressures were measured as a function of three surface treatments.

1. Chemical cleaning in an acid solution of 33 percent hydrofluoric, 33 percent nitric, remainder distilled water for 10 minutes, followed by a thorough rinse in distilled water plus vacuum bake in a temperature range from 200 to  $350^{\circ}$  C.
2. 16 hour bake in oxygen-air at  $200^{\circ}$  C + vacuum bake at  $260^{\circ}$  C for 24 hours.
3. Glow discharge in  $2.5 \times 10^{-2}$  Torr oxygen, (flow rate  $5 \times 10^{-2}$  Torr  $\text{liters s}^{-1}$ , current density  $50\mu\text{A cm}^{-2}$ , total dose  $1.1 \times 10^{18}$  ions  $\text{cm}^{-2}$ ) +  $260^{\circ}$  C vacuum bake for 24 hours.

Furthermore, the methane pumping speed of 2 different gauges, three ion pumps and a hot tungsten filament were also investigated.

#### A. Total Pressure

The total pressures were measured in  $N_2$  equivalent on the Helmer gauge with the mass spectrometer switched off, because it was found that even with many outgassing cycles the mass spectrometer contributed 3 to 6 times more gas than the rest of the system. The Helmer gauge was compared by D. Edwards with the calibrated Varian nude BA gauge and the Balzer modulated BA gauge type IMR 105. All three gauges agreed with one another to within 17 percent. Hydrogen sensitivity was previously determined to be 2.8 (Ref. 9).

Equilibrium pressures were reached in about two days after bake out termination and the values read 50 hours after the bake out are tabulated in Table I. At this point the Ti-ball was turned on and 3 mg were deposited over an area  $\sim 2000\text{cm}^2$ . A few hours later, the Helmer gauge and the mass spectrometer were degassed and operated for about 8 hours, after which MS was switched off. With only the Helmer gauge on, the Ti-ball was flashed again to lay down 6 mg of titanium. Figure 2 shows a typical pressure behavior with time from the end of titanium sublimation. The pressures read 5 days after the second Ti flash are listed in Table I. In several cases the final pressures were reached in  $< 3$  days.

It is apparent from Table I that with the exception of a  $200^\circ\text{C}$  bake and possibly the oxygen-air bake, all pressures are the same within our measuring tolerances for the surface treatments and the pumps investigated. Longer times (Fig. 2) and additional degassing of gauges produced negligible decreases in the final equilibrium pressures. The temperature of the surface on which titanium is deposited as well as its deposition rate seemed on the other hand to be critical in reaching these low pressures quoted. Raising the surface temperature to  $\sim 120^\circ\text{C}$  almost doubled the lowest equilibrium pressure achieved. Upon cooling a small area of the cross to 77 K, the pressure was reduced slightly

indicating still some  $\text{CH}_4$  present in the system.

Unfortunately below  $1.5 \times 10^{-11}$  Torr pressures, the Helmer gauge is often noisy which makes the exact measurements difficult. It is, therefore, not clear whether pressures below  $1 \times 10^{-11}$  Torr were reached in our system.

#### B. Partial Pressure

Quantitative determination of residual gases in the vacuum system under study was the most difficult task due to the considerable outgassing of the mass spectrometer and the low  $\text{CH}_4$  pumping speed of the ion pumps in the  $10^{-11}$  Torr range. Even with repeated degassing and filament conditioning the MS contribution to the residual pressure was several times the amount of the gas load from the wall of the system. The Helmer gauge on the other hand raised the partial pressures of  $\text{H}_2$  and  $\text{CH}_4$  by 4 and 2 percent respectively. Its contribution to other gases was immeasurable.

Before sublimation the pressure in the system was limited by the  $\text{H}_2$  pumping speed of the ion pump  $S_1$ . With bake out temperatures  $> 250^\circ \text{C}$  the main components of residual gas for most experimental runs fell within these limits

$\text{H}_2$	85 - 93 percent
$\text{CH}_4$	4 - 8 percent
CO	3 - 8 percent
$\text{CO}_2$	1 - 2 percent

After titanium sublimation sufficient pumping speed was provided for all gases by the titanium film except for  $\text{CH}_4$ . Noble gases were absent in our system with the exception of He in 2 runs which originated in the ion pump and was eventually almost eliminated.

It can be seen from Table I that the total pressures dropped below  $2 \times 10^{-11}$  Torr after sublimination. However, when the MS was switched on, the pressure (predominantly  $\text{CH}_4$ ) rose initially to  $1.5 \times 10^{-10}$  Torr (Fig. 3)

and was finally lowered after a few weeks of operation and extensive degassing to  $< 1 \times 10^{-10}$  Torr. It was suggested by J. P. Hobson that methane might originate in the filament. The filament was subsequently operated overnight (15 hours) at its maximum allowable temperature without affecting the  $\text{CH}_4$  content.

The principal factors which limited the achievement of low pressures in our vacuum system are best appreciated from Figs. 3 through 5. It should be pointed out here that total pressures are read on the Helmer gauge and are therefore given in  $\text{N}_2$  equivalent. To convert from partial pressure one must use the appropriate gauge sensitivity which is  $\sim 0.36$  for  $\text{H}_2$  and 1.5 for  $\text{CH}_4$ .<sup>10,11</sup> In cases where the total pressure is above  $5 \times 10^{-11}$  Torr, methane predominates and the pressure is limited by systems pumping speed for  $\text{CH}_4$ . Below  $3 \times 10^{-11}$  Torr the hydrogen pumping speed of titanium films determines the residual pressure. Not readily apparent from the spectra in Figs. 3 and 4 is the 1 amu mass peak (precursor of  $\text{H}_2$  peak), associated with and comprising about 10 percent of the methane peak.<sup>12</sup> When methane is eliminated, atomic hydrogen disappears as well (Fig. 5). Better representation of H peak can be obtained by expanding the x-axis but its amplitude remains the same as that of the precursor. Methane partial pressure was lowered in Figs. 4 and 5 by cooling a small area of the cross to 77 K. Mass peaks 12 and 28 in Fig. 5 originate in the ionizer.

### C. Methane Pumping Speed

It is obvious from the previous discussion that in titanium sublimation pumped systems, methane constitutes a major obstacle in maintaining the pressure in low  $10^{-11}$  Torr range. Compared with the  $\text{H}_2$  pumping speed, which can be increased by simply increasing the area of Ti film, the  $\text{CH}_4$  pumping speed will to a large extent determine the price of the ISABELLE pumping station. We have, therefore, investigated two methods of pumping  $\text{CH}_4$ , namely ion pumps and

methane cracking on hot tungsten filament. In addition the pumping speed of the Helmer and BAG were found to be  $\sim 0.06 \text{ l s}^{-1}$ .

The pumping speeds of sputter ion pumps were measured in the following way: The ion pump voltage was switched off to let the pressure increase. Then at some point  $P_0$ , the voltage was turned back on, while the output of the Helmer gauge was plotted versus time,  $t$ , on a strip chart recorder. From this plot the pumping speed,  $S$ , was calculated according to

$$P = P_0 e^{-(S/V)t},$$

where  $V$  is the volume of the vacuum system. The  $30 \text{ l s}^{-1}$  Mag-ion pump has the following pumping speeds,  $S$ , at the pressures listed below:

$$1 \times 10^{-10} \text{ Torr } S = 2 \text{ l s}^{-1}$$

$$8 \times 10^{-10} \text{ Torr } S = 1.8 \text{ l s}^{-1}$$

$$4 \times 10^{-10} \text{ Torr } S = 1.3 \text{ l s}^{-1}$$

The range of all three pumps in many measurements at  $4 \times 10^{-11}$  Torr was estimated to be between  $0.7$  and  $1.4 \text{ l s}^{-1}$ . At lower pressures pumping speeds could not be measured by this method, but it seems reasonable to assume that at  $1 \times 10^{-11}$  Torr  $S < 1 \text{ l s}^{-1}$  are to be expected. Taking into account the difficulties inherent in this method of measurement, we concluded that at  $4 \times 10^{-11}$  Torr all three pumps after conditioning had about the same pumping speeds namely  $(1.0 \pm 30\%) \text{ l s}^{-1}$ . Their striking pressures, i.e. the pressures at which the pumping started once the voltage was turned off and back on, varied from  $4 \times 10^{-11}$  to  $3 \times 10^{-10}$ . The pumps exhibited a number of other peculiarities<sup>13</sup> such as extinguishing the discharge in low  $10^{-11}$  Torr range and restarting again at higher pressure, gas liberation (mainly He and  $\text{CH}_4$ ) upon turn off, and excessive dark current. These problems were, however, largely eliminated by bake out and hi-potting.

It was pointed out to me by Dr. W. Lange<sup>14</sup> that methane can be removed by cracking the molecules on hot tungsten filament. Carbon is chemisorbed by

tungsten and hydrogen is pumped by Ti films. A 16 cm long filament, 0.25 mm in diameter, and a view port for pyrometric temperature measurements were incorporated into the apparatus in Fig. 1. Since the filament has to be operated between 2400 - 2500 K for efficient methane pumping,<sup>14</sup> the pressure in the system was always higher with the filament on. This was probably due to wall heating by radiated power, which was ~ 80 W. Even though methane pumping was observed, it was concluded that this method is not suitable for low pressure operation and was therefore abandoned.

#### IV. Conclusions

Based on the work presented, a few more general conclusions can be drawn:

1. Pressures of  $1 - 2 \times 10^{-11}$  Torr can be achieved routinely in a vacuum system pumped by Ti films and a  $20 \text{ l s}^{-1}$  ion pump.
2. In  $10^{-11}$  Torr range the only residual gases present were  $\text{H}_2$ , He, and  $\text{CH}_4$ . Below  $1 - 2 \times 10^{-11}$  the pressure was limited primarily by  $\text{H}_2$  and more work is being done on Ti -  $\text{H}_2$  system at these pressures.
3. Pumping speed of ion pumps drops drastically in  $10^{-11}$  Torr range, probably because only a few Penning cells are operating. Pumps used previously in unclean systems have to be vacuum fired before they are suitable for this operation. Better measurements are badly needed and will be carried out using a cryopump capable of operating in  $10^{-12}$  Torr range.

#### Acknowledgments

I would like to acknowledge many helpful discussions with Drs. J. P. Hobson and D. Edwards, Jr. I would also like to thank Mr. J. R. Aggus for his help in solving mechanical problems and Mr. Frank Timm for his able assistance throughout the experiments.

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TABLE I Comparison of Total Pressures in Torr N<sub>2</sub> Equivalent for Various Surface Treatments and Pumps.

Pump ls <sup>-1</sup>	Before Ti Sublimation		After Ti Sublimation	
	20	30	20	30
Treatment	Torr	Torr	Torr	Torr
1 + 200°C	9 x 10 <sup>-10</sup>		3 x 10 <sup>-11</sup>	
1 + 250°C	6 x 10 <sup>-10</sup>	5 x 10 <sup>-10</sup>	1.5 x 10 <sup>-11</sup>	2 x 10 <sup>-11</sup>
1 + 300°C	5 x 10 <sup>-10</sup>	5.5 x 10 <sup>-10</sup>	1.5 x 10 <sup>-11</sup>	1.5 x 10 <sup>-11</sup>
1 + 350°C		5 x 10 <sup>-10</sup>		< 1.5 x 10 <sup>-11</sup>
2		6.5 x 10 <sup>-10</sup>		2.5 x 10 <sup>-11</sup>
3	5.5 x 10 <sup>-10</sup>		< 1.5 x 10 <sup>-11</sup>	

Figure Captions

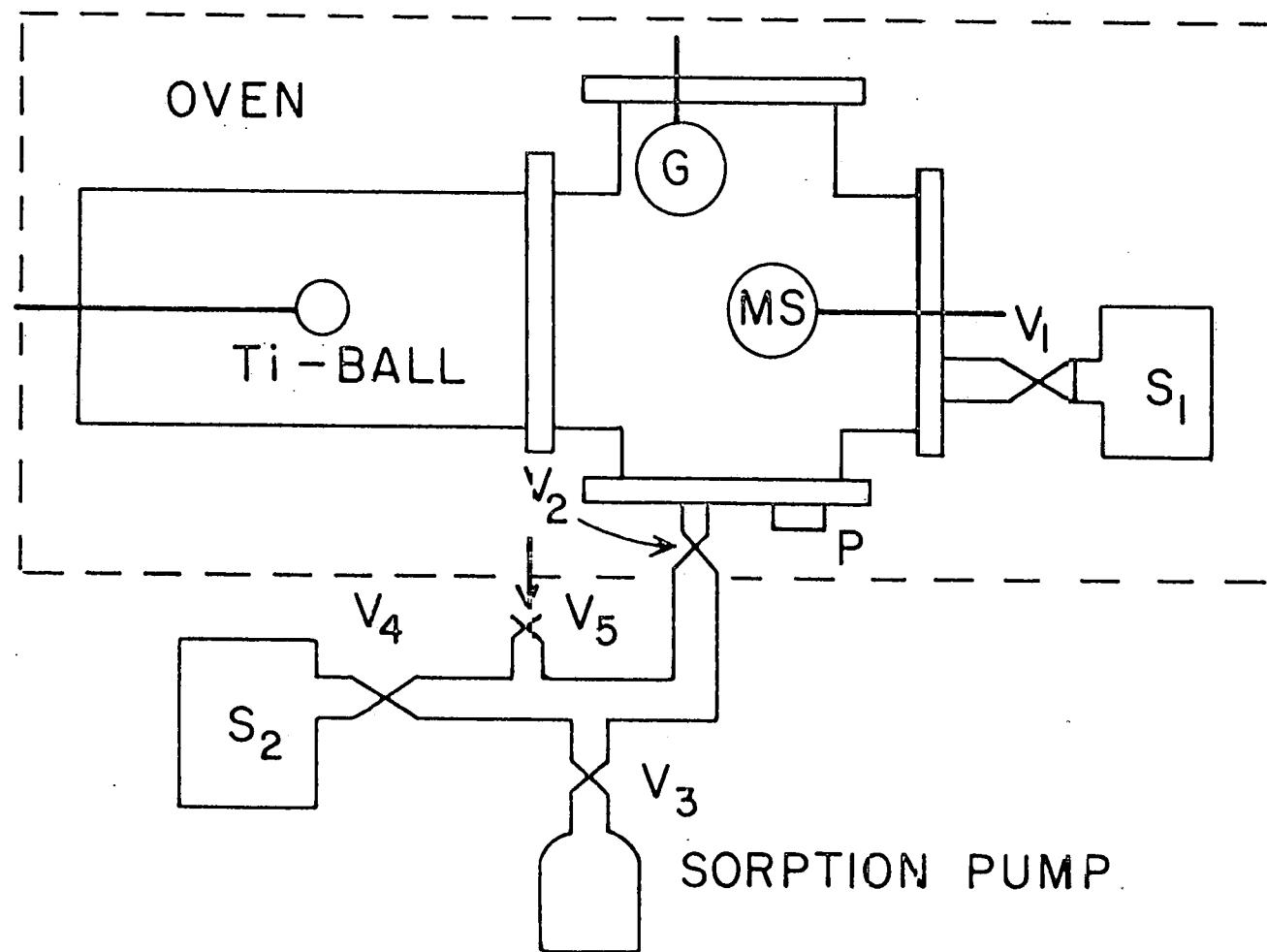
Fig. 1. Schematic diagram of the experimental vacuum system. G: Helmer gauge; MS: UTI Quadrupole mass spectrometer;  $S_1$ : Ion pump under test;  $V_1$ ,  $V_2$ ,  $V_3$ ,  $V_4$ : Varian 7 cm all metal valves;  $V_5$  variable bleed valve; P: Viewing port;  $S_2$ :  $100\text{ l.s}^{-1}$  pump. Neg. #7-80-76

Fig. 2. Total pressure versus time plot. Conditions: Second entry in Table I,  $20\text{ l s}^{-1}$  pump. Neg. #7-81-76

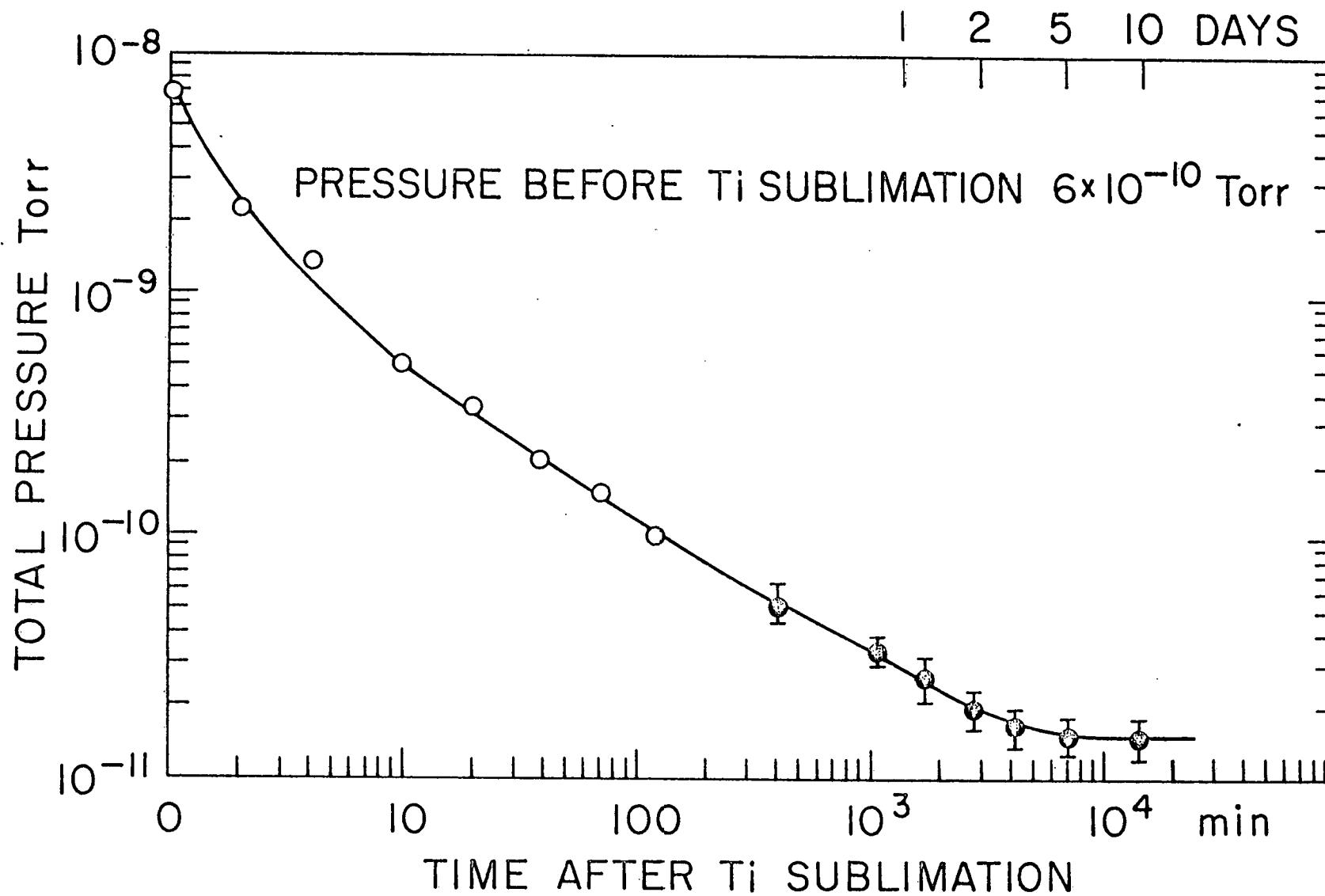
Fig. 3. Mass spectrum for 4th entry in table I. Partial pressures of  $\text{H}_2$  and  $\text{CH}_4$  are  $6.5 \times 10^{-11}$  Torr and  $7 \times 10^{-11}$  Torr. Total pressure before MS turn on  $2.5 \times 10^{-11}$  Torr. Neg. #7-83-76

Fig. 4. Mass spectrum for 4th entry in Table I. Partial pressures of  $\text{H}_2$  and  $\text{CH}_4$  are  $4.5 \times 10^{-11}$  Torr and  $1.5 \times 10^{-11}$  Torr. Total pressure before MS turn on  $1.5 \times 10^{-11}$  Torr. Neg. #7-84-76

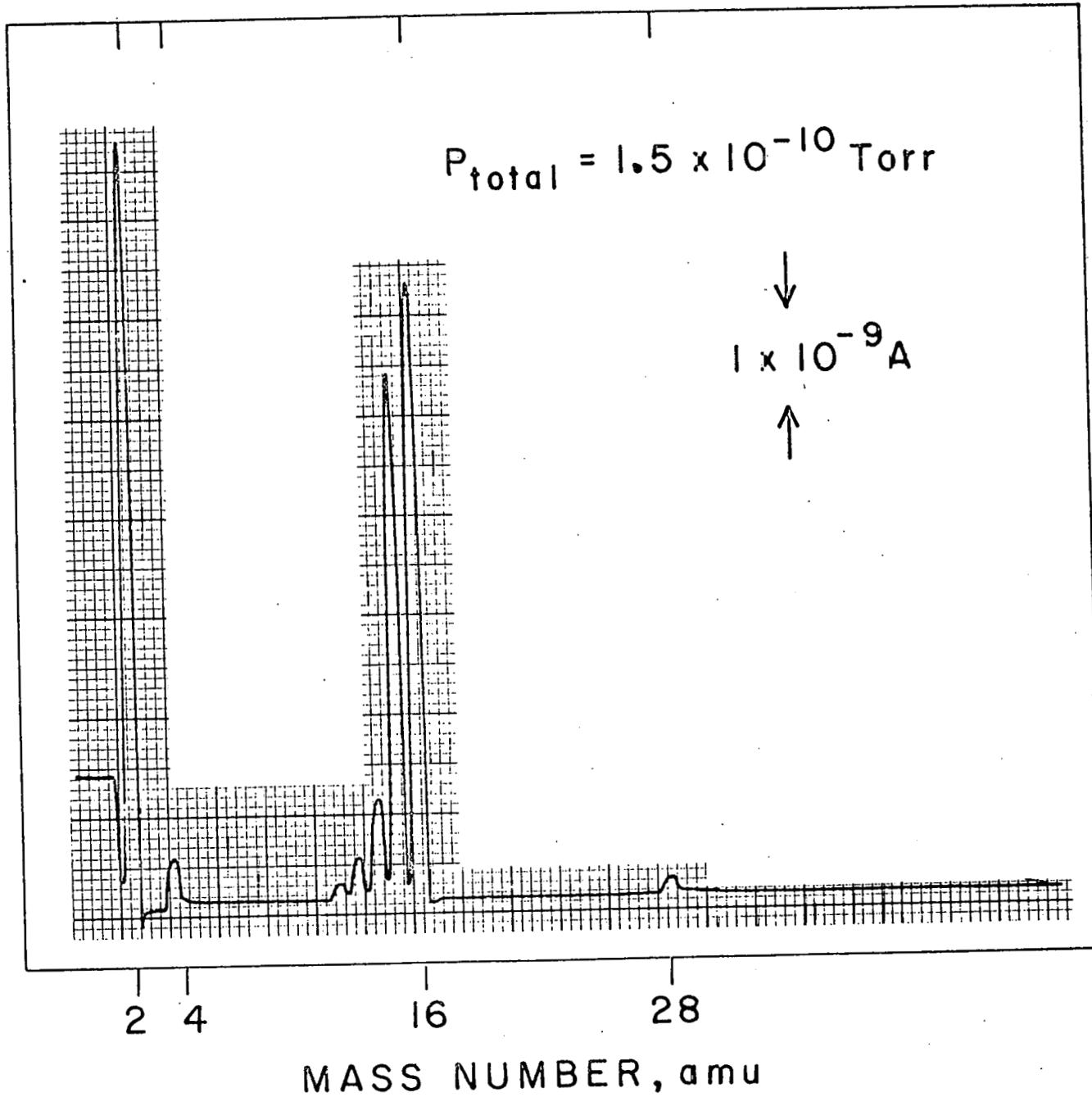
Fig. 5. Mass spectrum for 4th entry in Table I.  $\text{H}_2$  partial pressure is  $3.3 \times 10^{-11}$  Torr. Total pressure before MS turn on  $< 1.5 \times 10^{-11}$  Torr. Neg. #7-82-76



VACUUM SYSTEM



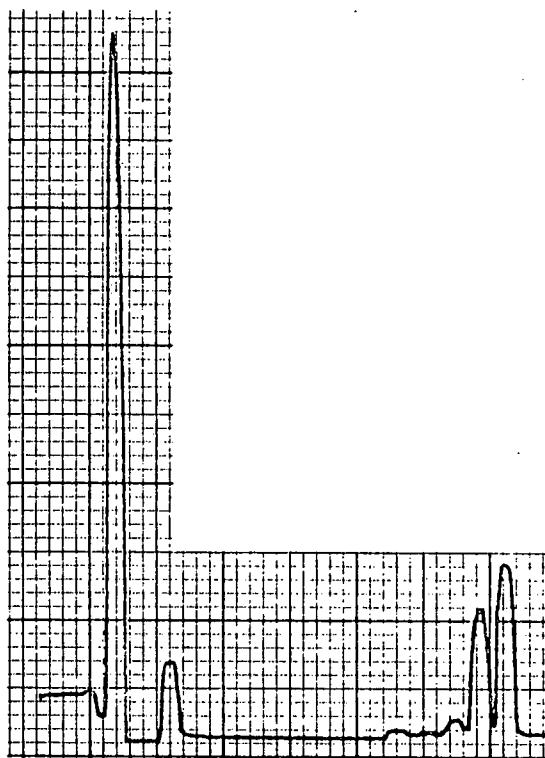
PARTIAL PRESSURE



PARTIAL PRESSURE

$$P_{\text{total}} = 4 \times 10^{-11} \text{ Torr}$$

$$1 \times 10^{-9} \text{ A}$$



2 4

16

40

MASS NUMBER, amu

PARTIAL PRESSURE

