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**COMPILATION OF DATA FROM EBR-II
NATURAL-CIRCULATION-TEST PROCEDURE EX-140,
SECTION IV, ADDENDUM 7C**

**J. L. Gillette, J. E. Sullivan, R. M. Singer,
J. V. Tokar, and E. M. Dean**

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ARGONNE NATIONAL LABORATORY
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ABSTRACT

The transition from forced to natural-circulation flow of primary coolant after loss of primary pumping power with concomitant reactor scram has been investigated in Experimental Breeder Reactor No. II. Before the loss-of-flow transient, the reactor was operated at 22.0 MWt (36.7% of the normal full-power value) and at 39.0% of normal full flow. All electrical power to the primary pumping system was terminated, causing the flow rate of the primary-system coolant to coast down. As the flow rate coasted down, the low-flow trip setting caused the reactor to scram. The transition from forced to natural-circulation flow was observed to be smooth, and the coolant temperatures throughout the reactor were observed to remain lower than the corresponding values at full-power operating conditions. Data were collected by the EBR-II data-acquisition system from the usual plant process instrumentation and instrumented subassembly XX08. The method used to correct the data for signal offsets is discussed. The corrected test data are presented graphically.

I. INTRODUCTION

Experimental verification of a smooth transition into natural-circulation flow after a protected loss of all plant pumping power is of extreme importance in demonstrating the safety of a liquid-metal fast breeder reactor (LMFBR). To this end, a number of natural-circulation tests¹⁻⁶ have been conducted in Experimental Breeder Reactor No. II (EBR-II) as part of the

experimentation with instrumented subassembly XX08.⁷

This test program can be broken down into two categories. The first consists of tests initiated from low reactor decay power levels (a maximum of 1.26% of the full operational power). Most of these tests¹⁻⁴ consisted of coastdowns from the flow level provided by the auxiliary electromagnetic (EM) primary pump (approximately 5.5% of normal full flow), which is in the reactor outlet pipe. These early tests, summarized in Ref. 8, were intended to provide information on the dependence of minimum natural-circulation flows and maximum coolant temperature on (1) the fission-product-decay power level and (2) the initial temperature distribution in the intermediate heat exchanger (IHX). This temperature distribution is determined by the ratio of primary-system to secondary-system flow rates through the IHX and affects natural-circulation flow by creating an initial buoyancy distribution in the primary-system coolant.

The remaining test in the low-decay-power test category is referred to as XX08 Test 10.⁵ This test was initiated with the auxiliary pump off and the primary-system mechanical pumps at high flow values. Four separate coastdowns were conducted as part of XX08 Test 10. The first three were initiated at approximately 100% of normal operating primary-system flow, but with different secondary-system flow rates through the IHX. That is, they had different initial temperature distributions in the IHX. The fourth coastdown of Test 10 was initiated at approximately 34% of the normal full operational flow. This value was selected because it was approximately the value at which the first of the second category of natural-circulation tests would be conducted. Thus Test 10 was designed to not only provide additional data on the effects of power level and initial temperature distribution, but also to provide a reference flow-coastdown curve for the second category of test.

The second natural-circulation-test category includes tests initiated with the reactor at some substantial fission power. This type of test would be more similar to an actual loss-of-pumping-power accident in an operating LMFBR. The first test in this category is referred to as XX08 Test 7A and is discussed in Ref. 6. The initial conditions for Test 7A were a reactor power level of 17.1 MWt (28.5% of the normal full-power value) and 32.1% of normal full operational flow. All temperatures reached during the test were below the normal full-power operating temperatures. Because Test 7A was

successfully completed, the next test was planned to be conducted at a higher initial power level and a higher flow rate. In this manner the conditions existing in an LMFBR under full operating conditions can be approached in a logical test sequence.

The second test in the second category is described in this report. EBR-II Test Procedure EX-140, Section IV, Addendum 7C (hereafter called XX08 Test 7C) was conducted on February 12, 1979. As with the first test in this category (7A), this test included operation of the reactor at reduced power and flow for a sufficient time to build up a near-equilibrium inventory of fission products. After termination of electrical power to the primary-system pumps, the flow within the primary system started to decay. The low-flow trip setting on the high-pressure-plenum flow to the reactor then scrammed the reactor. Eventually the flow in the primary system coasted down to a natural-circulation level, with buoyancy differences essentially provided by the fission-product-decay power within the reactor and the heat-removal capability of the secondary-sodium coolant in the IHX.

II. PLANT CONDITIONS

For Test 7C the reactor was loaded in the run-99D configuration shown in Fig. 1. The primary-tank sodium temperature had been reduced from the normal operating temperature of 700°F (371°C) to approximately 665°F (352°C) to provide a greater margin to the maximum allowable test temperatures. An approach to power was begun by establishing a flow rate equal to approximately 40% of the normal operating value and then increasing the reactor power. A final steady-state power of 22.0 MWt was eventually reached. This power represents 36.7% of the normal full power of 60.0 MWt. The reactor power was held at 22.0 MWt for approximately 3 h to establish a near-equilibrium state of the fission-product inventory throughout the reactor. During this time, the secondary-sodium and steam systems also reached near-equilibrium conditions.

After the reactor had been operating at the above conditions for the 3-h period, the electrical power to the auxiliary primary EM pump was removed, causing the primary-system flow rate to decrease slightly to 39.0%. The mixed mean reactor outlet coolant temperature increased to 840°F (449°C) at this time. The conditions in the secondary steam systems were not affected

C = Control rod
 D = Driver fuel
 K = Structural dummy
 P = $\frac{1}{2}$ driver fuel, $\frac{1}{2}$ SS
 PLUG = Instrumented-subassembly plug
 R = SS reflector
 S = Safety rod
 SSDR = Stainless steel drop rod
 X = Experimental subassembly

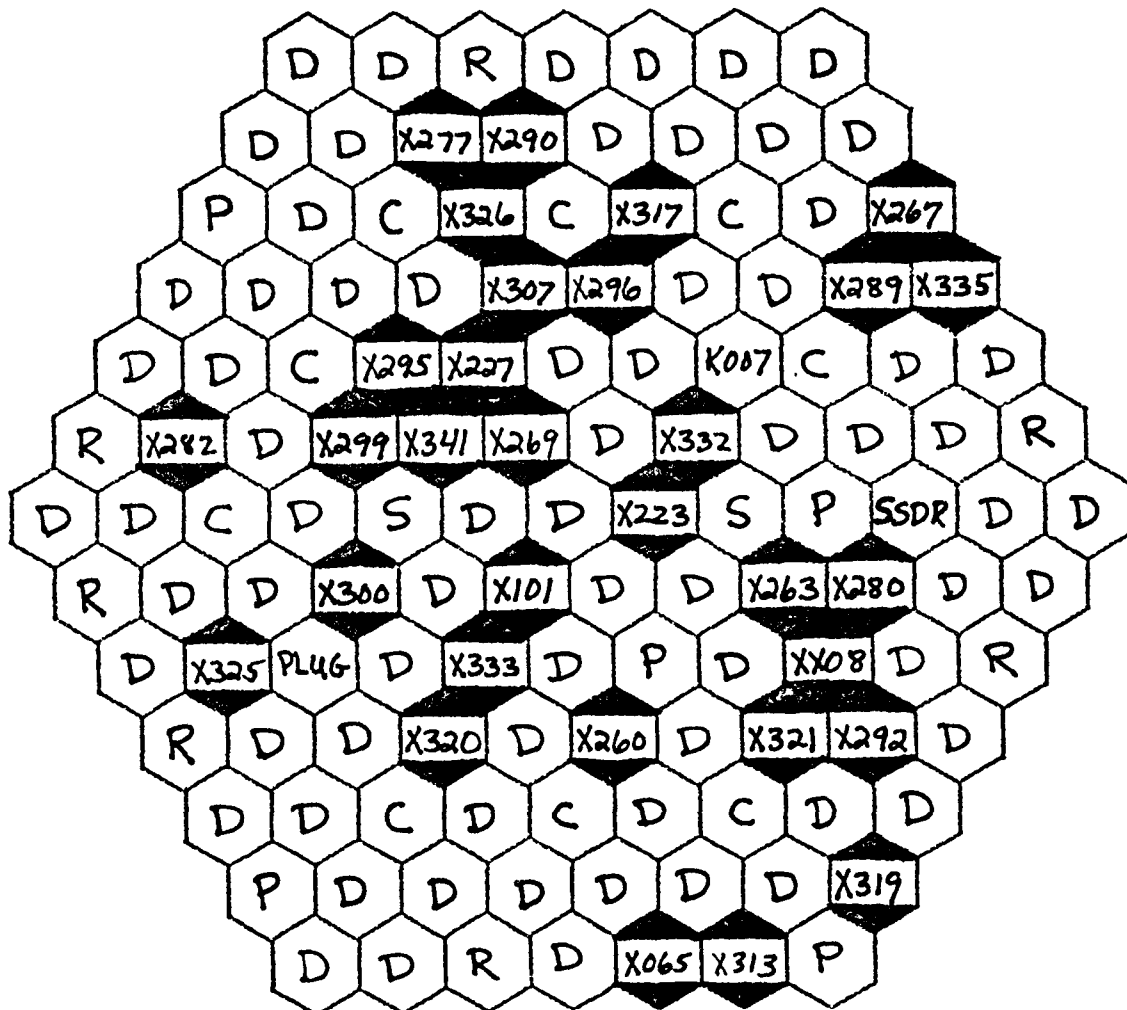


Fig. 1. Core Loading for Test 7C

by turning off the auxiliary pump. Table I lists several of the significant parameters during this part of the test.

Comparison of the data in Table I with the corresponding data for XX08 Test 7A⁶ shows that the initial conditions for Test 7C were, as desired, more representative of full-power operating conditions than those for the earlier test. For example, the reactor power level was increased from 17.1 to 22.0 MWt and the primary-system flow was increased from 32.1 to 39.0% of the

TABLE I. Reactor Conditions before Coastdown of Test 7C

Reactor power	22.0 ± 0.3 MWt
Primary-system flow	3226 gpm ^a (39.0% of normal full flow)
Primary pump No. 1 speed	319 rpm
Primary pump No. 2 speed	318 rpm
Reactor inlet coolant temperature	665°F (352°C)
Mixed mean reactor outlet coolant temperature	840°F (449°C)
Secondary-system flow	2246 gpm ^a (37.4% of full flow ^b)
IHX secondary-inlet temperature	577°F (303°C)
IHX secondary-outlet temperature	827°F (442°C)

^a1 gpm = $6.31 \times 10^{-5} \text{ m}^3/\text{s}$.

^bA typical value during full-power operation is ~86%.

normal full flow rate of 9000 gpm ($0.568 \text{ m}^3/\text{s}$). The reactor inlet coolant temperature was essentially the same in the two tests, but the mixed mean reactor outlet coolant temperature was higher in Test 7C. The data for the secondary system reflect the more severe conditions in the primary system for Test 7C.

III. TEST SEQUENCE

Approximately 17 minutes after the auxiliary pump had been turned off, and with the reactor under the conditions noted in Table I, the primary pumps were tripped by manually opening the 2400-V breakers and the clutch breakers on the motor-generator set. A delay of approximately 1 s occurred

between the opening of the breakers and the start of the flow coastdown. About 1 s after the coastdown was actually started (at 2.1 s after the breakers were opened), the reactor was scrammed by a low-flow trip on the flowmeter for high-pressure-plenum 2 (HPP2) of the reactor. The secondary-system flow was held constant at 37.4% during this time.

About 3 minutes after the primary-pump trip, it was noted that all temperatures in the primary system had reached their peak values and were slowly and steadily decreasing. To minimize the decrease in the primary-tank sodium temperature, the secondary-system pump was turned off and this system was allowed to coast down to its natural-circulation flow rate of approximately 2% of full flow. After several minutes of near-equilibrium conditions in the primary system, the auxiliary EM pump was turned on and the primary-system flow increased to approximately 5%. After an equilibrium state had been established for several minutes, the primary pumps were turned on to provide 100% of the normal full operational flow rate. From the data obtained at full flow, the instrumentation offsets and normalization factors were determined in the manner discussed in Sec. IV.

IV. INSTRUMENTATION AND DATA OFFSETS

The test data were collected at the rate of two samples per second by the EBR-II data-acquisition system (DAS). Data were obtained from the normal plant process instrumentation in the primary, secondary, and steam systems and from instrumented subassembly XX08. Included in the normal plant process instruments are thermocouples measuring the coolant temperature at the outlet of several subassemblies in the reactor. Figure 2 shows the location of the in-core subassembly outlet thermocouples (SOT's), and Table II notes the type of subassembly beneath each SOT during Test 7C. Also shown in Table II are the calculated powers⁹ and calculated flow rates for each of these subassemblies at the steady-state condition of 22.0 MWt total reactor power and 39.0% reactor flow. Instrumented subassembly XX08 is included in Table II, because coolant outlet thermocouples are part of its instrumentation package. The recorded flow rate for XX08 is the measured value.

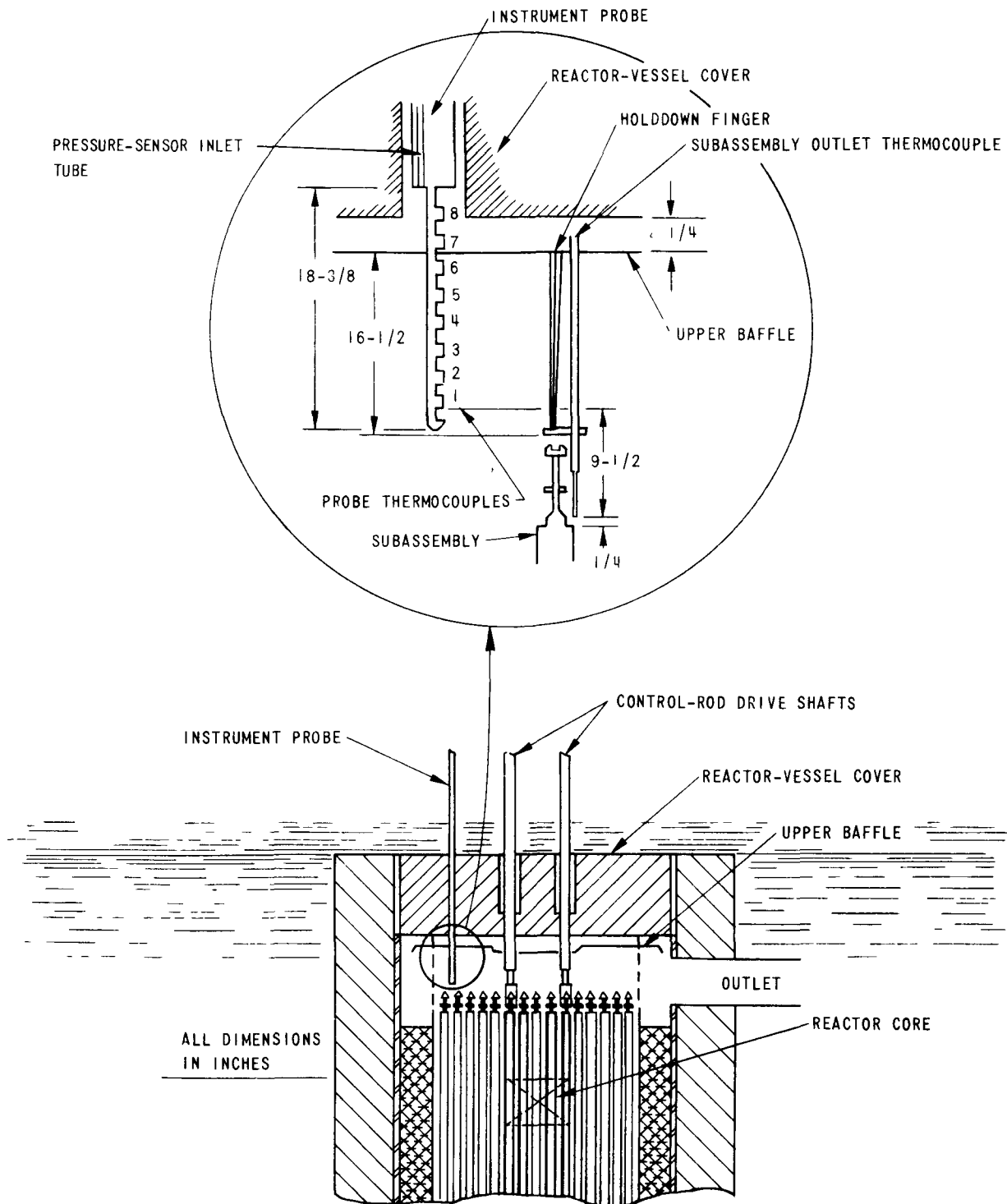


Fig. 2. Location of Subassembly Outlet Thermocouples and Orientation of Upper-plenum Instrument Probe in EBR-II.
Conversion factor: 1 in. = 25.4 mm.

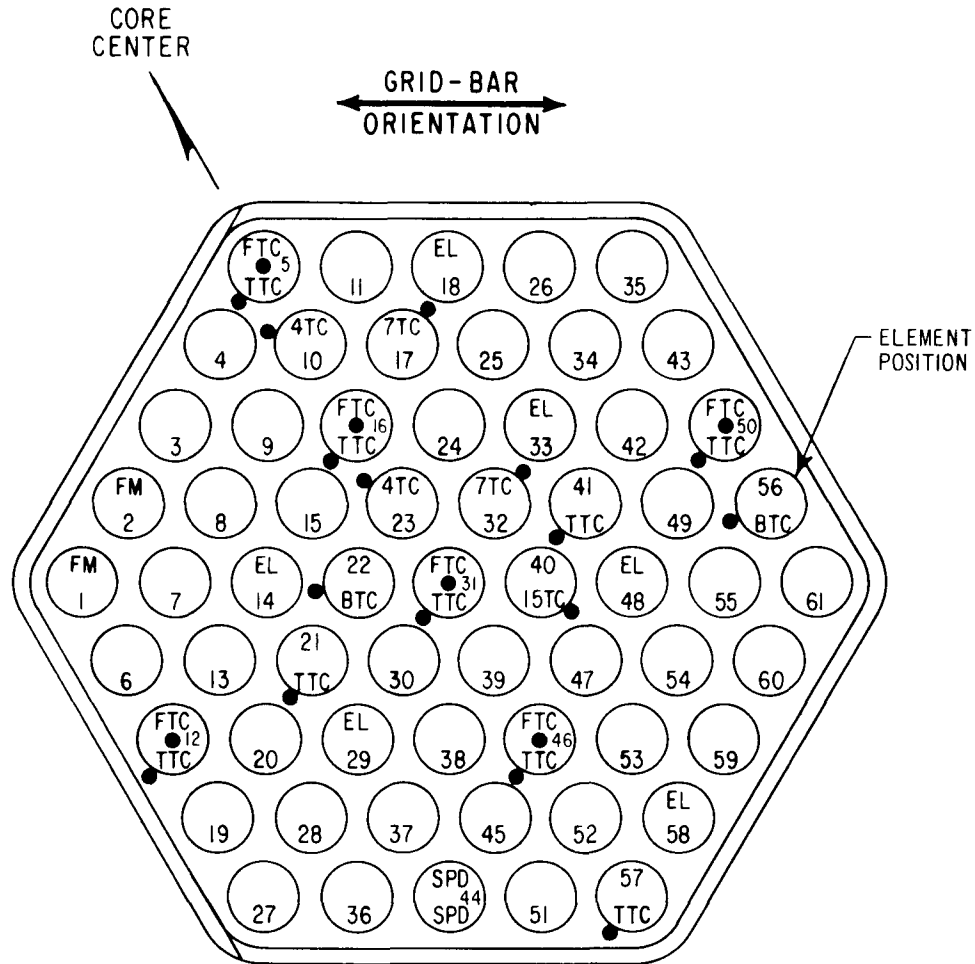
TABLE II. Locations and In-core Parameters of Subassemblies with SOT's during Test 7C

Location	Subassembly Type	Power, kWt	Flow, gpm ^a
1A1	Driver	275.9	51.84
2A1	Driver	275.0	50.69
2B1	X269A (structural experiment)	5.5	2.28
2C1	Driver	256.8	50.69
2E1	Driver	276.7	50.69
2F1	X101M (structural experiment)	6.6	4.89
3B1	X227A (37-pin oxide/bypass flow experiment)	121.1	19.98
3C1	Driver	270.9	43.69
3F1	X333 (19-pin oxide experiment)	90.3	8.69
4B1	Driver	259.8	33.63
4C3	Driver	251.0	33.63
4E1	Driver	256.0	33.63
4F1	X320 (structural experiment)	8.7	4.41
5A4	Driver	225.8	29.04
5C2	Driver	240.7	29.04
6C4	Driver	227.2	23.61
7A3	Driver	194.2	23.61
7D4	Driver	188.7	23.61
5D3	XX08	140.0	16.63

^aConversion factor: 1 gpm = $6.31 \times 10^{-5} \text{ m}^3/\text{s}$.

The coolant temperature in the reactor outlet plenum was measured by the "upper-plenum instrument probe." This probe is above the blanket subassembly in the 14D6 grid position and has thermocouples at eight different axial positions in the outlet plenum. The probe from which Test 7C data were obtained is essentially the same as that shown in Fig. 2.

The bulk of the in-core test data was obtained from instrumentation in instrumented subassembly XX08. This experiment is a uranium-metal-fueled subassembly equipped with two permanent-magnet flowmeters (providing three flow readings) at the core inlet and 24 thermocouples at different radial and axial locations within the subassembly. Figure 3 shows the pattern of



LEGEND	REQUIRED
FM FLOWMETER LEAD	2
SPD SELF-POWERED DETECTOR	2
BTC CORE BOTTOM COOLANT TC	2
4TC COOLANT TC 0.137m ABOVE CORE BOTTOM	2
7TC COOLANT TC 0.240m ABOVE CORE BOTTOM	2
TTC COOLANT TC TOP OF CORE	9
FTC FUEL CENTERLINE TC	6
15TC COOLANT TC 0.514m ABOVE CORE BOTTOM	1
EL EXTENDED-LENGTH (0.660m) MK II ELEMENTS	6

NOTES a) DOTS REPRESENT LATERAL POSITION OF TC JUNCTIONS IRRESPECTIVE OF AXIAL LOCATION

b) TWO OUTLET COOLANT TC's (NOT SHOWN) EXIST ABOVE THE FUEL ELEMENTS

c) NUMBERS INDICATE ELEMENT POSITION

Fig. 3. Location of Instrumentation Sensors in XX08

the XX08 instrumentation. Not shown in Fig. 3 are two thermocouples (OTC's) that measure the mixed mean outlet coolant temperature from XX08. The reader is referred to Ref. 7 for a more complete description of XX08.

As was noted previously, the final part of Test 7C consisted of operating the primary pumps at 100% flow. This action served two purposes. First, it provided full-flow readings for all primary-system flowmeters so that these readings could be used as normalization factors for subsequent data handling. Second, it provided nearly isothermal conditions so that offsets in the thermocouples in the primary system could be determined.

Several thermocouples measure the local temperature at various locations in the primary tank. In determining offsets we assumed that the average reading of these thermocouples under the nearly isothermal conditions noted above was, in fact, the true temperature of the sodium in the primary tank. All thermocouple readings were then corrected for offset by taking the difference between the isothermal (or average) value and the value actually recorded by the thermocouple. Where appropriate, the small temperature rise due to the low fission-product-decay power was added to the isothermal value before determining the offset.

As in all previous XX08 natural-circulation tests, the signal from the high-pressure-plenum (HPP2) flowmeter gave indications of negative (i.e., reverse) flow during various portions of the test. Because flow reversal in the high-pressure plenum was contrary to expected behavior and, more importantly, was totally inconsistent with other experimental data on flow and temperature, it was concluded that an offset existed in this flowmeter signal. Large differences between the measured flow rates for low-pressure-plenum 1 (LPP1) and the low-pressure-plenum 2 (LPP2) were also observed in this test. The two flow paths from the pumps to the low-pressure plenum were designed identically, and previous experience has shown the two measured flow rates to be nearly equal. Because of the large differences observed in this test, we concluded that these signals should also be corrected by an offset factor.

To quantify the offsets in these signals, a technique similar to that discussed in Refs. 1-5 was used. The basic premise of this technique is that at the flow rate supplied by the auxiliary pump, the percentage of full flow measured by the HPP2 flowmeter and by each of the two low-pressure-plenum flowmeters should be equal to that measured by the XX08 flowmeters.

For the HPP2 flowmeter, determining the offset in this manner is believed to be quite accurate, because the thermal and hydraulic characteristics of XX08 are similar to those of the average subassembly supplied with coolant from the high-pressure plenum. Some analytical predictions indicate, however, that because of the slightly greater power-to-flow ratio (and resultant buoyant driving force) in XX08 as compared to the average subassembly, the XX08 flow should be a higher percentage of the full-flow value. However, this difference is relatively slight, and no experimental data have verified it. Therefore, we concluded that we would achieve much greater accuracy by offsetting the HPP2 flowmeter rather than leaving the signal uncorrected.

Under conditions of fission-product-decay heat, a reflector or blanket subassembly will retain a greater fraction of its steady-state power than a fueled subassembly. Therefore, when forced flow is provided by the auxiliary pump, the temperature rises in these subassemblies are a larger fraction of the full-power temperature rises than those in fueled subassemblies. These larger temperature increases produce buoyant forces that are more comparable to the forced-flow driving forces than those developed in fueled subassemblies. Thus the net flow (forced plus convective) in blanket and reflector subassemblies will be a greater percentage of the full operational value than the net flow in fueled subassemblies.

As noted earlier, in determining the offsets in the low-pressure-plenum flowmeters, the signals were equated to the XX08-measured flow. It is likely, therefore, that the low-pressure-plenum flows reported in the appendix are slightly too low, especially at the auxiliary-pump flow level or lower. Nevertheless, we believe that these flows are much closer than the uncorrected values to those actually realized during the test, and therefore decided to use the corrective means discussed above.

In terms of an equation, the flowmeter offsets were determined by solving the following equality:

$$100 \times \frac{(\text{flow signal with auxiliary pump on}) + \text{offset}}{(\text{flow signal at full flow}) + \text{offset}} = \text{Percent of XX08 flow with auxiliary pump on.}$$

The offsets for the HPP2, LPP1, and LPP2 flowmeters determined from the above relationship were 0.075, 4.110, and -1.492%, respectively. These values were used in preparing the figures presented in the appendix.

Table III lists the correction factors for instruments in the primary system. The corrected data take the form of

$$\text{Corrected value} = (\text{DAS signal} + A)/B,$$

where A is the offset and B is a normalization factor. A value of B not equal to 1.0 is used to express the data in terms of percent of the full-flow value.

TABLE III. Correction Factors for Data from XX08 Test 7C

Parameter	Units	Correction Factors	
		A	B
XX08 lower flowmeter	%	0.0	0.4270
XX08 upper flowmeter--signal 1	%	0.0	0.3240
XX08 upper flowmeter--signal 2	%	0.0	0.3236
XX08 FTC-5	°F	2.1	1.0
XX08 FTC-12	°F	1.5	1.0
XX08 FTC-16	°F	1.6	1.0
XX08 FTC-31	°F	0.8	1.0
XX08 FTC-46	°F	1.2	1.0
XX08 FTC-50	°F	1.2	1.0
XX08 BTC-22	°F	1.3	1.0
XX08 BTC-56	°F	1.6	1.0
XX08 4TC-10	°F	1.8	1.0
XX08 4TC-23	°F	3.7	1.0
XX08 7TC-17	°F	3.2	1.0
XX08 7TC-32	°F	2.5	1.0
XX08 15TC-40	°F	1.6	1.0
XX08 TTC-5	°F	3.5	1.0
XX08 TTC-12	°F	1.0	1.0
XX08 TTC-16	°F	1.9	1.0
XX08 TTC-21	°F	2.3	1.0
XX08 TTC-31	°F	2.9	1.0

TABLE III (contd)

Parameter	Units	Correction Factors	
		A	B
XX08 TTC-41	°F	2.5	1.0
XX08 TTC-46	°F	0.1	1.0
XX08 TTC-50	°F	2.1	1.0
XX08 TTC-57	°F	0.5	1.0
XX08 OTC-1	°F	2.5	1.0
XX08 OTC-2	°F	-0.7	1.0
Primary-pump-1 speed	rpm	0.0	1.0
Primary-pump-2 speed	rpm	0.0	1.0
High-pressure-plenum-2 flow	%	0.075	1.0024
Low-pressure-plenum-1 flow	%	4.110	1.0524
Low-pressure-plenum-2 flow	%	-1.492	1.0215
Total primary flow (541 E)	%	0.0	0.9892
Bulk-sodium temp (501 X)	°F	-1.6	1.0
Bulk-sodium temp (501 AA)	°F	0.9	1.0
Bulk-sodium temp (501 V)	°F	-0.6	1.0
Bulk-sodium temp (501 W)	°F	0.4	1.0
Bulk-sodium temp (501 T)	°F	0.4	1.0
Bulk-sodium temp (501 D)	°F	1.3	1.0
Bulk-sodium temp (501 E)	°F	7.2	1.0
Bulk-sodium temp (501 Q)	°F	6.6	1.0
Bulk-sodium temp (501 F)	°F	9.4	1.0
Bulk-sodium temp (530)	°F	1.9	1.0
Primary-pump inlet temp	°F	4.0	1.0
Primary-pump-1 outlet temp (540 C)	°F	-7.5	1.0
Primary-pump-1 outlet temp (540 D)	°F	-8.1	1.0
Primary-pump-2 outlet temp (540 A)	°F	-6.8	1.0
Primary-pump-2 outlet temp (540 E)	°F	-6.1	1.0
Primary-pump-2 outlet temp (540 F)	°F	-5.6	1.0
Low-pressure-plenum sodium temp (540 AR)	°F	0.9	1.0
Low-pressure-plenum sodium temp (540 AS)	°F	2.1	1.0
Low-pressure-plenum sodium temp (540 AV)	°F	2.3	1.0
High-pressure-plenum sodium temp (540 AT)	°F	0.8	1.0

TABLE III (contd)

Parameter	Units	Correction Factors	
		A	B
Subassembly outlet temp, position 1A1	°F	1.8	1.0
Subassembly outlet temp, position 2A1	°F	7.7	1.0
Subassembly outlet temp, position 2B1	°F	3.2	1.0
Subassembly outlet temp, position 2C1	°F	0.4	1.0
Subassembly outlet temp, position 2E1	°F	2.4	1.0
Subassembly outlet temp, position 2F1	°F	5.3	1.0
Subassembly outlet temp, position 3B1	°F	2.2	1.0
Subassembly outlet temp, position 3C1	°F	-17.0	1.0
Subassembly outlet temp, position 3F1	°F	0.2	1.0
Subassembly outlet temp, position 4B1	°F	2.2	1.0
Subassembly outlet temp, position 4C3	°F	2.8	1.0
Subassembly outlet temp, position 4E1	°F	0.6	1.0
Subassembly outlet temp, position 4F1	°F	1.2	1.0
Subassembly outlet temp, position 5A4	°F	0.9	1.0
Subassembly outlet temp, position 5C2	°F	0.7	1.0
Subassembly outlet temp, position 6C4	°F	-0.5	1.0
Subassembly outlet temp, position 7D4	°F	3.0	1.0
Subassembly outlet temp, position 9E4	°F	2.9	1.0
Subassembly outlet temp, position 12E6	°F	0.0	1.0
Subassembly outlet temp, position 16E9	°F	-0.1	1.0
Upper-plenum-probe temp TC1	°F	2.2	1.0
Upper-plenum-probe temp TC2	°F	3.8	1.0
Upper-plenum-probe temp TC3	°F	1.6	1.0
Upper-plenum-probe temp TC4	°F	1.9	1.0
Upper-plenum-probe temp TC5	°F	2.2	1.0
Upper-plenum-probe temp TC6	°F	2.4	1.0
Upper-plenum-probe temp TC7	°F	2.3	1.0
Upper-plenum-probe temp TC8	°F	1.7	1.0
Upper-plenum-probe pressure 1	psi	0.0	1.0
Upper-plenum-probe pressure 2	psi	0.0	1.0
Reactor outlet temp (1534 CF)	°F	5.0	1.0
Reactor outlet temp (506 X)	°F	2.7	1.0

TABLE III (contd)

Parameter	Units	Correction Factors	
		A	B
IHX primary-inlet temp (507 BK)	°F	1.4	1.0
IHX primary-inlet temp (507 BQ)	°F	4.1	1.0
IHX primary-outlet temp (540 AB)	°F	-1.1	1.0
IHX primary-outlet temp (540 AC)	°F	-1.1	1.0
IHX primary-outlet temp (540 AD)	°F	-1.2	1.0
IHX primary-outlet temp (540 AE)	°F	-0.8	1.0
IHX primary-outlet temp (540 AM)	°F	-1.4	1.0
IHX primary-outlet temp (540 AN)	°F	-0.7	1.0
IHX primary-outlet temp (540 AP)	°F	-0.8	1.0
IHX primary-outlet temp (540 AQ)	°F	-0.7	1.0
IHX top orifice plate (507 CP)	°F	1.0	1.0
IHX bottom orifice plate (507 CC)	°F	2.1	1.0
IHX bottom orifice plate (507 BX)	°F	1.1	1.0
IHX bottom orifice plate (507 EF)	°F	0.9	1.0
IHX bottom orifice plate (507 EG)	°F	1.5	1.0
IHX bottom orifice plate (507 CA)	°F	1.0	1.0
IHX bottom orifice plate (507 CG)	°F	1.4	1.0

Conversion factors: °C = (°F - 32)/1.8; 1 psi = 6.89 kPa.

The "Neutron Power (Log Range B)" signal (pages A32 and A33 of the appendix) was normalized to yield the correct percent power during the initial steady-state portion of the test. Values of A = 0.0 and B = 0.749 were used for this purpose.

The secondary-sodium and steam signals are recorded without offset or normalization factor (i.e., A = 0.0 and B = 1.0).

V. TEST DATA

The data from XX08 Test 7C are presented in graphical form in the appendix. For each plot, time = 0 represents the time at which the primary pumps were tripped. For the primary-system data, the time period shown covers the interval from just before the auxiliary pump was turned off until the primary system was in an equilibrium natural-circulation state. The time intervals for the secondary- and steam-system data extend beyond that shown for the primary-system data so that any effects having longer time delays may be observed. Some primary-system data are shown twice, with the second plot, which has an expanded time scale, covering only the flow-coastdown interval. In this way, the coastdown characteristics can be observed in finer detail.

Included in the appendix are plots showing the average values of several combinations of parameters. In each case the heading on the plot states which instruments have been averaged.

The experimental data presented in this document will be compared with the analytical results in a subsequent report. However, some basic observations can be made from the data.

Curves for pump speed versus time are shown on pages A40-A41. From these curves, it is apparent that about 35 s elapsed from the interruption of the electrical power supply until primary pump No. 1 reached zero speed. For primary pump No. 2, however, 42 s were required. During this 7-s period when pump No. 2 was still running down and pump No. 1 was stopped, a measurably increased proportion of the total primary flow was supplied by pump No. 2. This is illustrated by the "hump" in the flow-coastdown transient measured by the HPP2 flowmeter and shown on pp. A36-A37. Unfortunately, the flowmeter in the high-pressure-plenum inlet pipe from pump No. 1 (i.e., HPP1) is no longer functional. As a result, no direct experimental observations can be made of the flow rate through this line. Calculations of this phenomenon, however, indicate that the flow in the line from pump No. 1 reversed during this 7-s period--i.e., some coolant pumped into the plenum by primary pump No. 2 bypassed the reactor core and went into the plenum-inlet pipe from primary pump No. 1. As additional evidence of this behavior, the in-core flow rate as measured by XX08 (pp. A2-A5) shows a smooth coastdown characteristic and a gradual transition from forced to

natural convective flow. The "hump" in the HPP2 flow did not cause a similar condition to appear in-core.

The thermal response of the primary coolant can be seen in the behavior of the XX08 top-of-core thermocouples (pp. A12-A21) and the subassembly outlet thermocouples (pp. A60-A79). For reference, the reactor inlet temperature was 665°F (352°C). Of particular interest are the responses of a thermocouple in an interior subchannel of the XX08 rod bundle (e.g., TTC-31, pp. A16-A17) and of a thermocouple next to the hex-can wall (e.g., TTC-57, pp. A20-A21). The initially hot interior subchannel and initially cool wall subchannel are observed to reach nearly the same peak temperature during the transient. This behavior, which has been repeatedly observed under low-flow conditions in EBR-II, is caused by intrasubassembly flow redistribution and transverse conduction and results in quite uniform transverse temperature gradients in subassemblies.

Pages A62-A63 and A68-A69 show the coolant temperatures at the outlet of two fueled subassemblies (2A1 and 4B1), one of which operated initially at a somewhat larger than average temperature rise, and the other at a smaller than average temperature rise. As was observed in a single subassembly, the transverse temperature differences between different subassemblies are seen to decrease during the natural-circulation transient. For these two fueled subassemblies, the initial at-power temperature rises differ by about 46%, but the temperature rises at the peak of the transient differ only by about 11%.

This significant flattening of the transverse reactor temperature profile is primarily due to buoyancy-induced flow redistribution and inter-subassembly heat transfer. The effects of intra- and intersubassembly heat transfer are discussed in detail in Ref. 10, where similar data from other natural-circulation tests in EBR-II are presented.

Comparison of the data in the appendix with the corresponding data in Ref. 6 shows the effects of the increased initial power and flow on the peak transient temperatures. The more severe initial conditions of Test 7C resulted in somewhat higher peak temperatures. However, the peak transient temperatures remained below the corresponding steady-state temperatures. These results, along with the attendant calculational results, provide solid evidence that the transition from forced to natural-circulation flow continues to be smooth even with more severe initial conditions. The next

series of XX08 natural-circulation tests will examine the dynamic effects of a primary-system flow coastdown and reactor scram followed sometime later by a flow coastdown in the secondary coolant system.

ACKNOWLEDGMENTS

We are very appreciative of the efforts of those people in the Operations and Analysis Department of the EBR-II Project who were instrumental in preparing for and conducting XX08 Test 7C. A special note of gratitude goes to William Booty for setting up the special data-acquisition-system program and to the operating crews for the expert and conscientious manner in which the test was conducted.

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2. J. L. Gillette et al., *Compilation of Data from EBR-II Natural-circulation-test Procedure EX-140, Section IV, Addendum 1E*, ANL/EBR-102 (September 1978).
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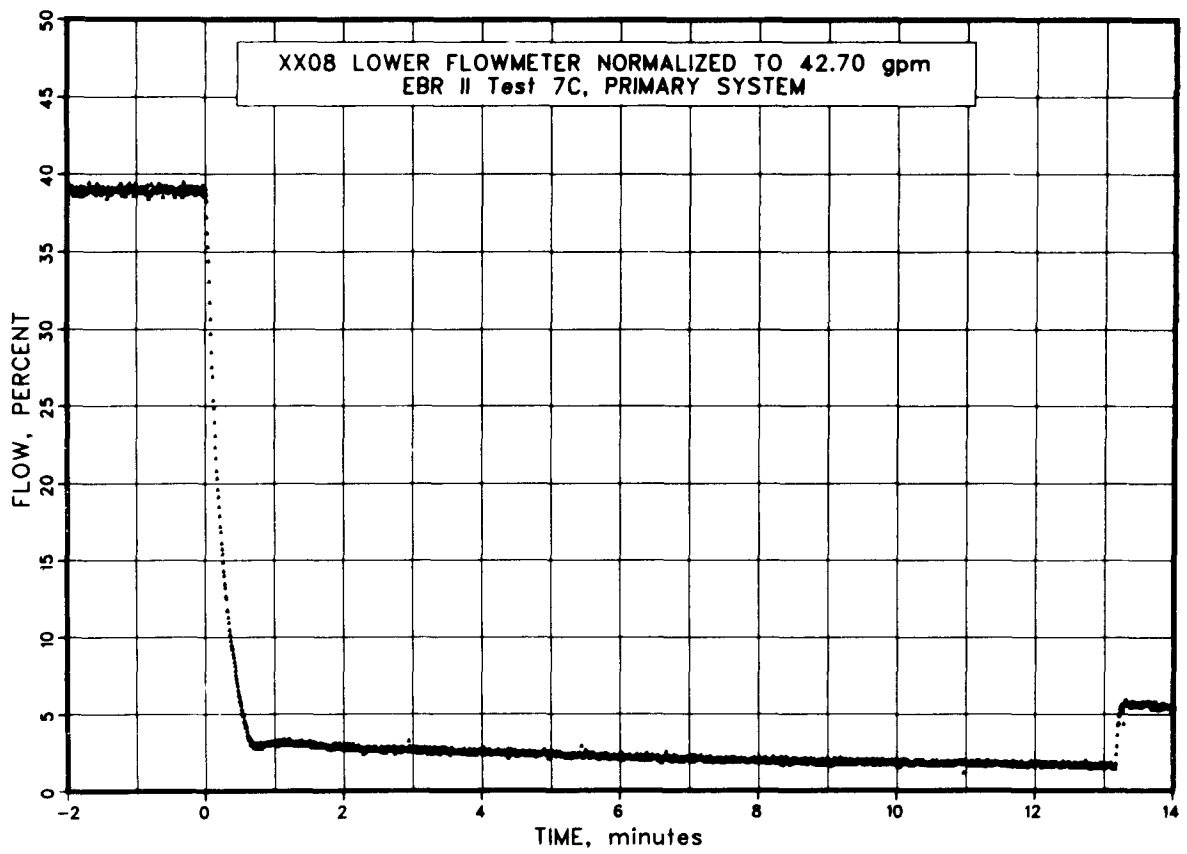
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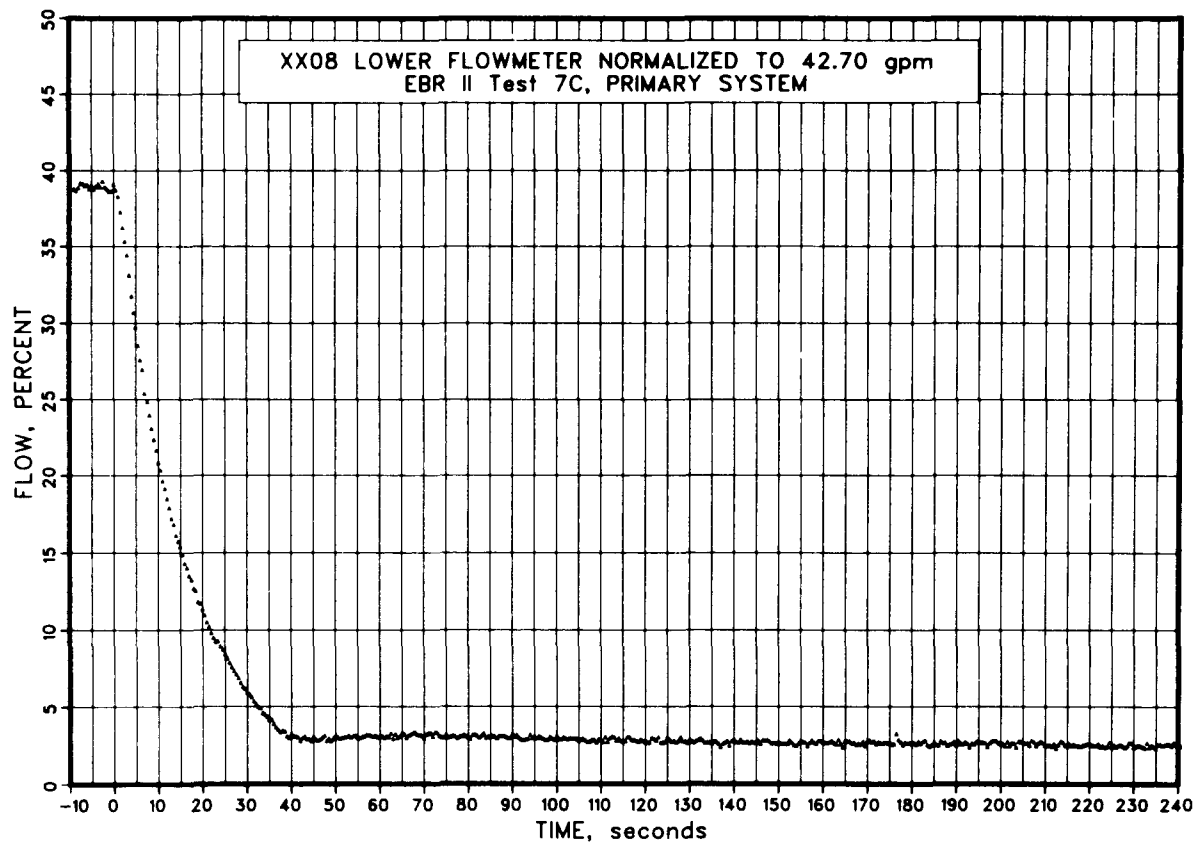
APPENDIX

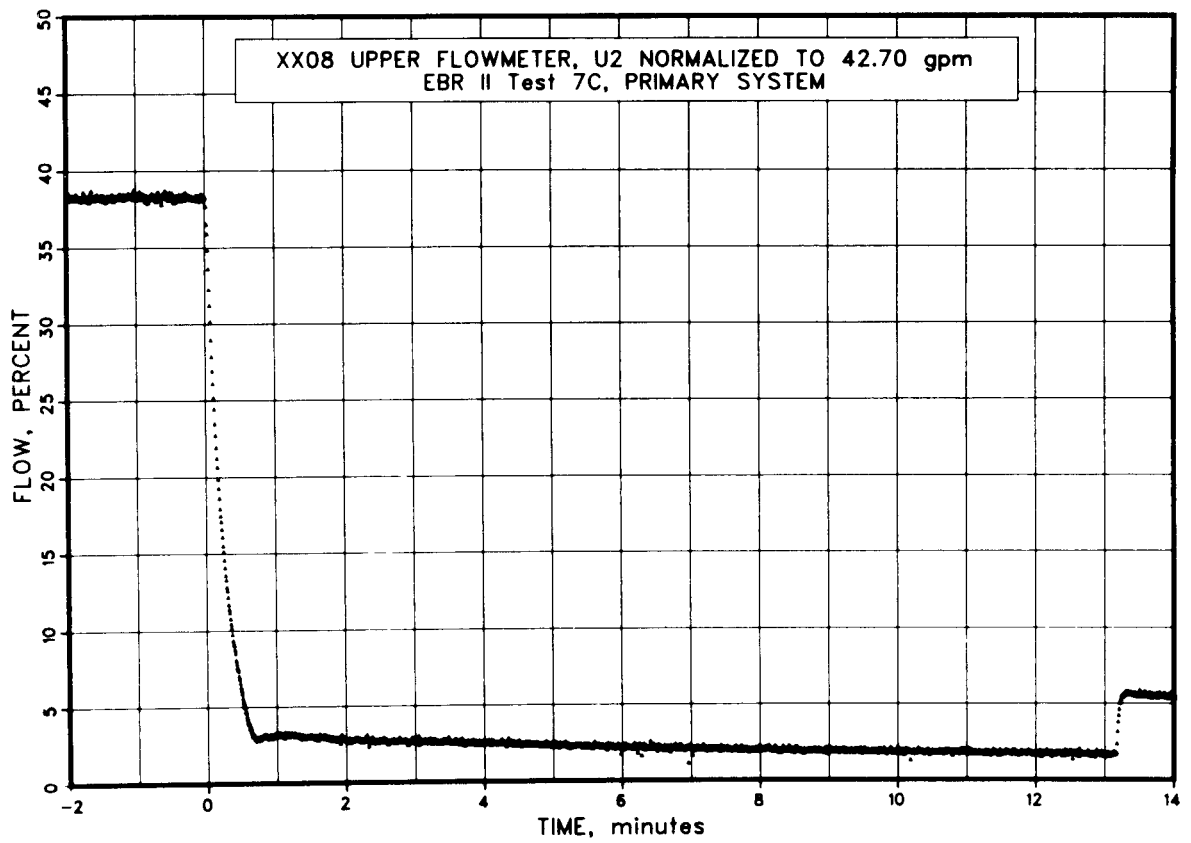
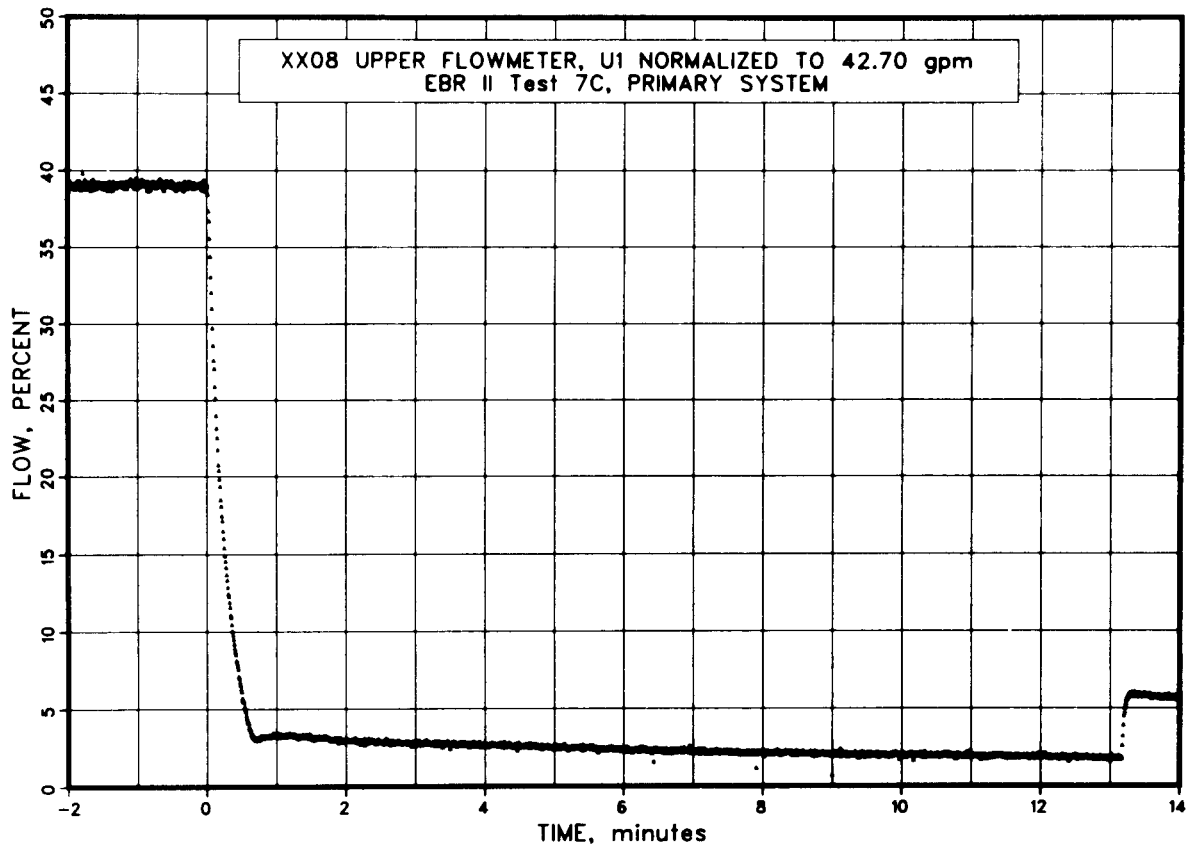
Plots of Data from Test 7C

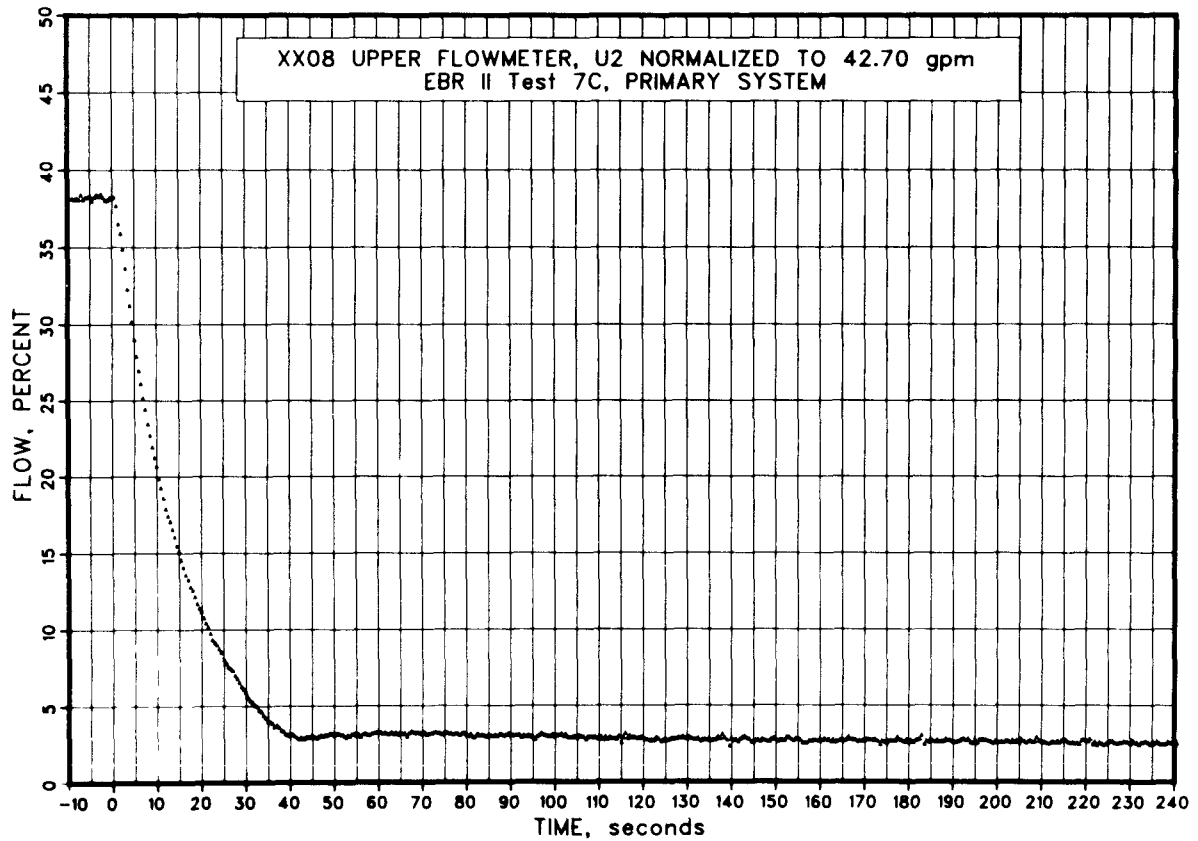
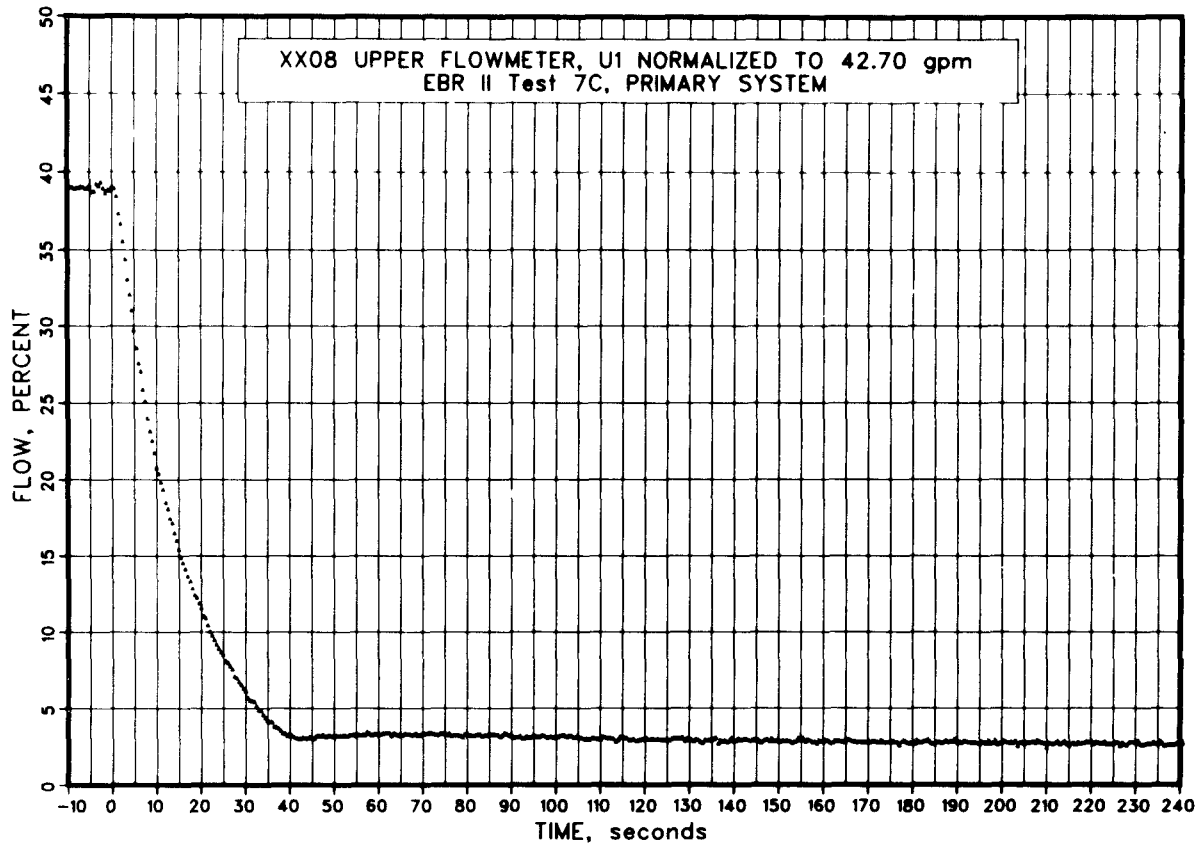
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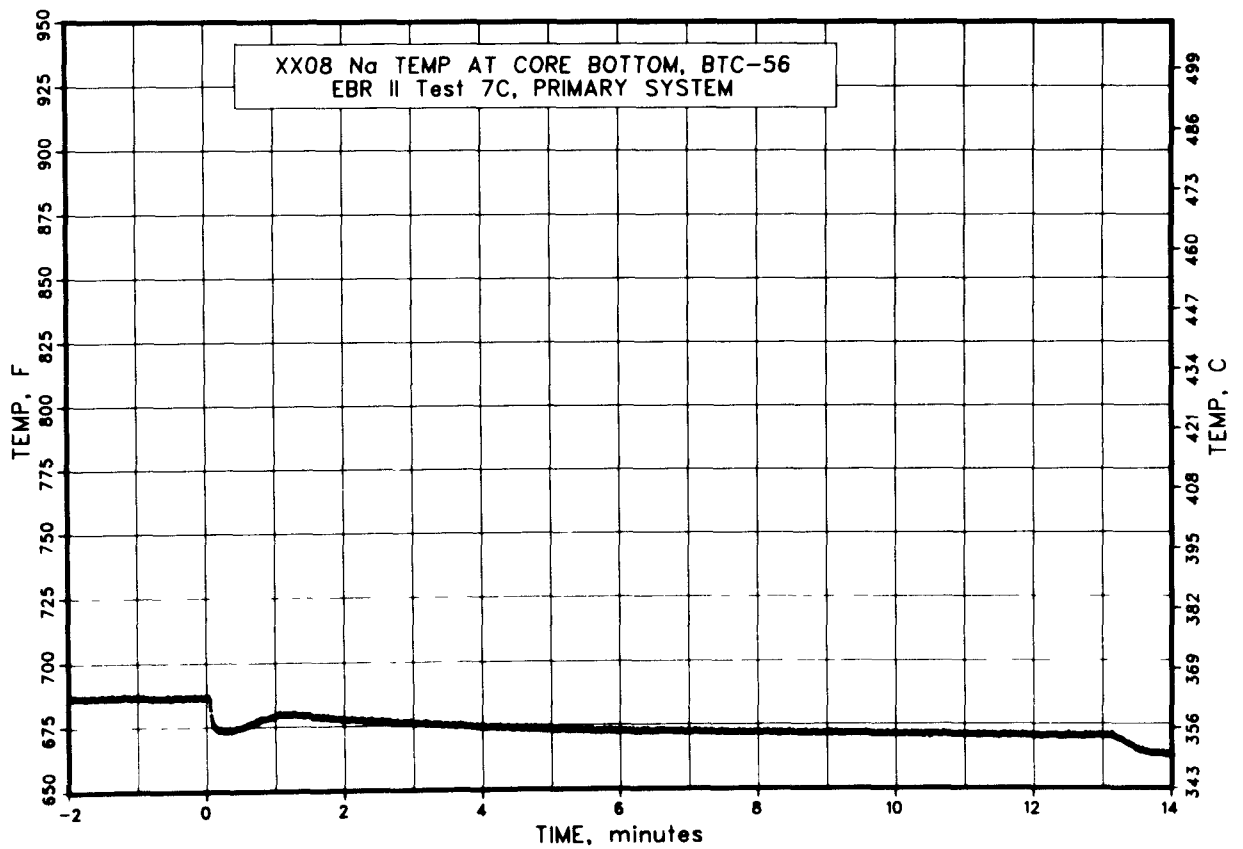
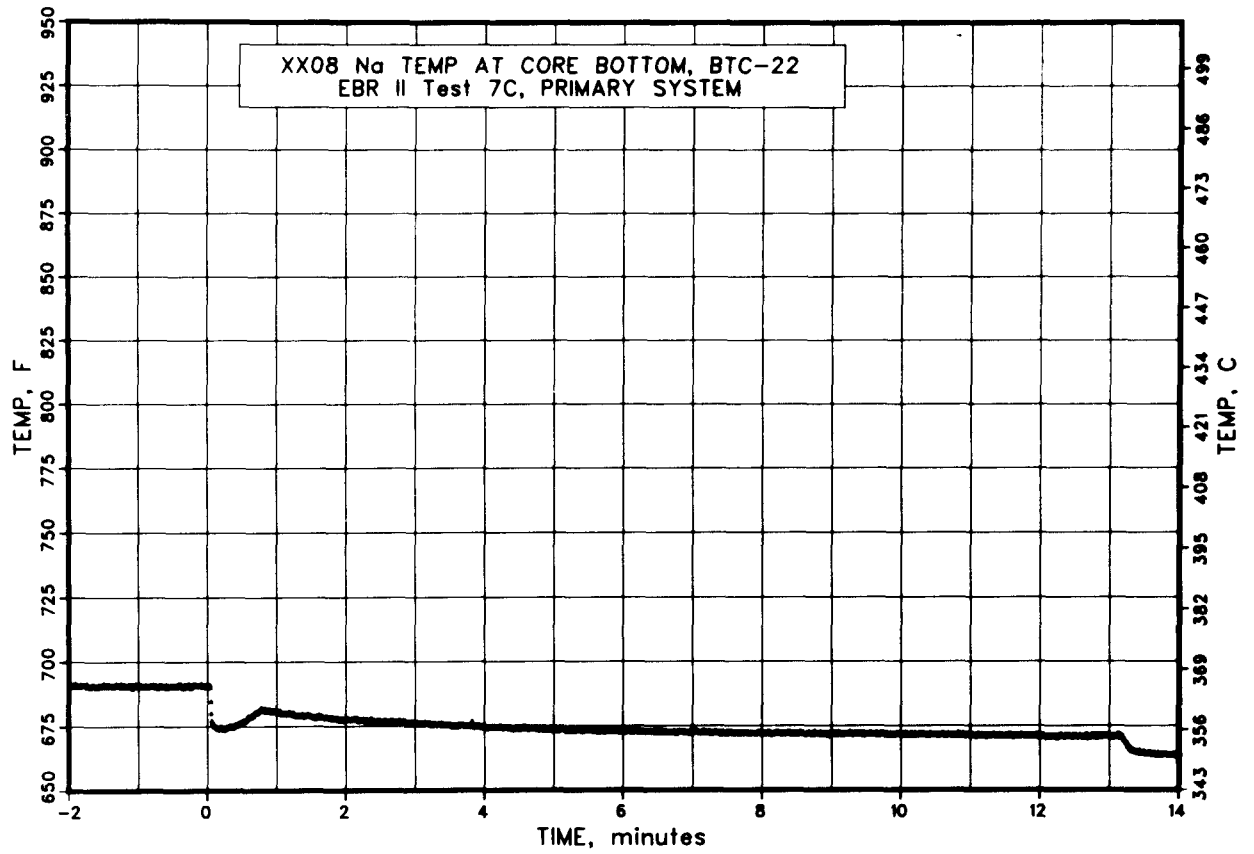
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Primary-system Data	A32-A107
Secondary-system Data	A108-A117
Steam-system Data	A118-A136

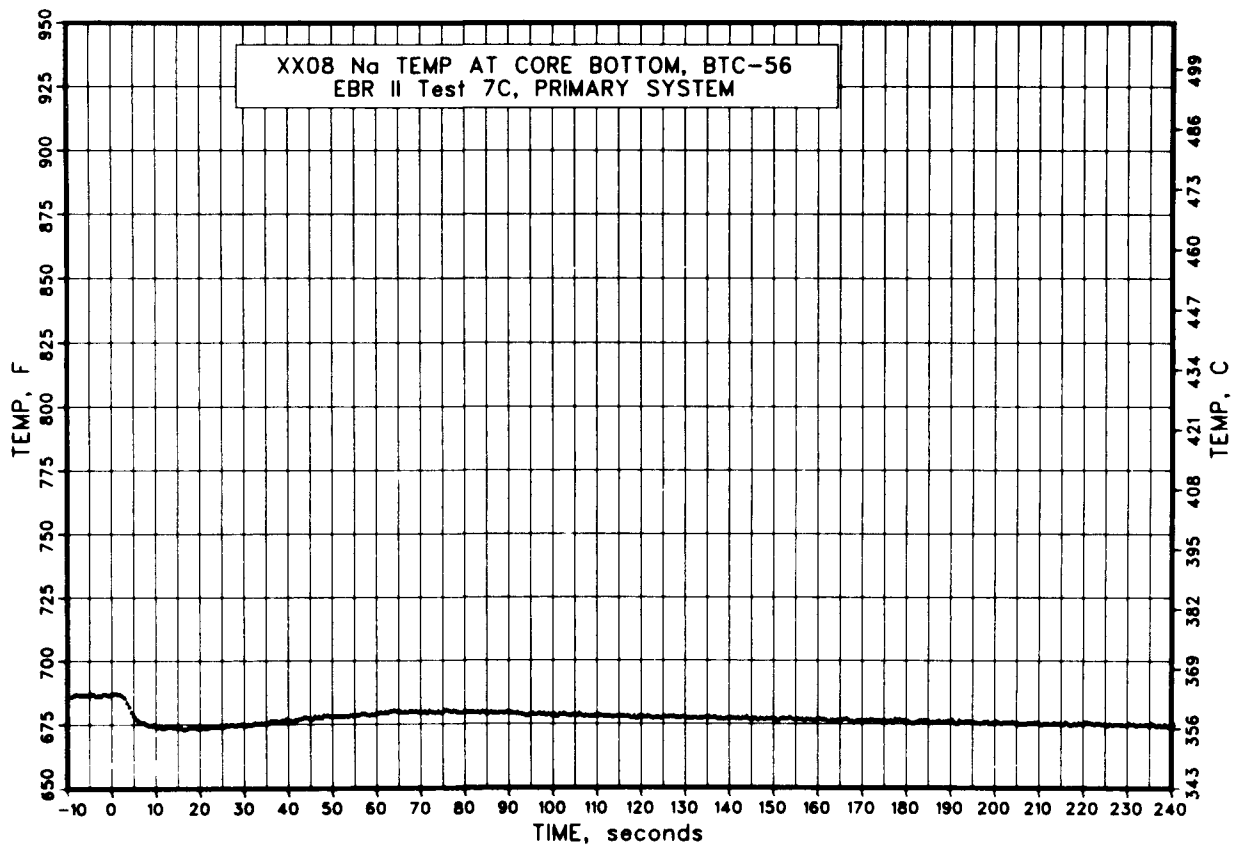
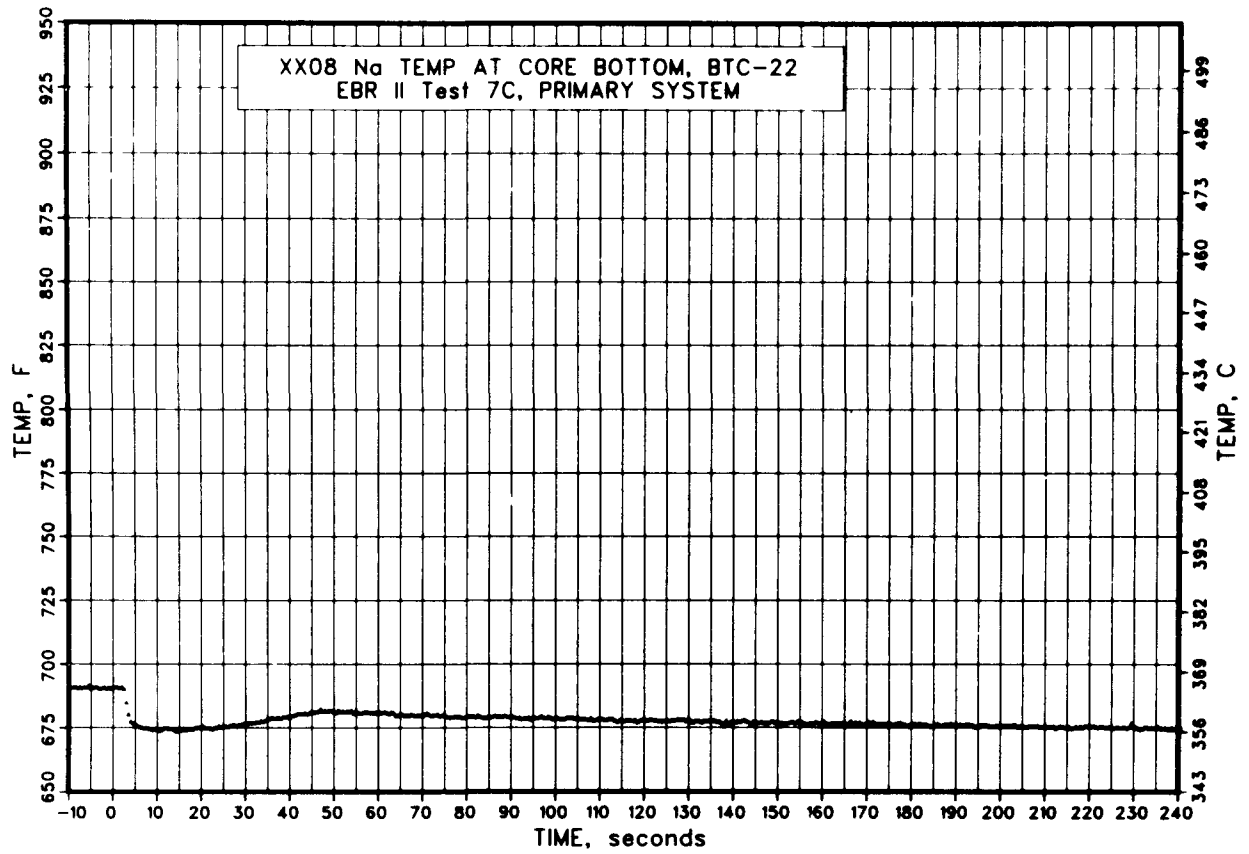


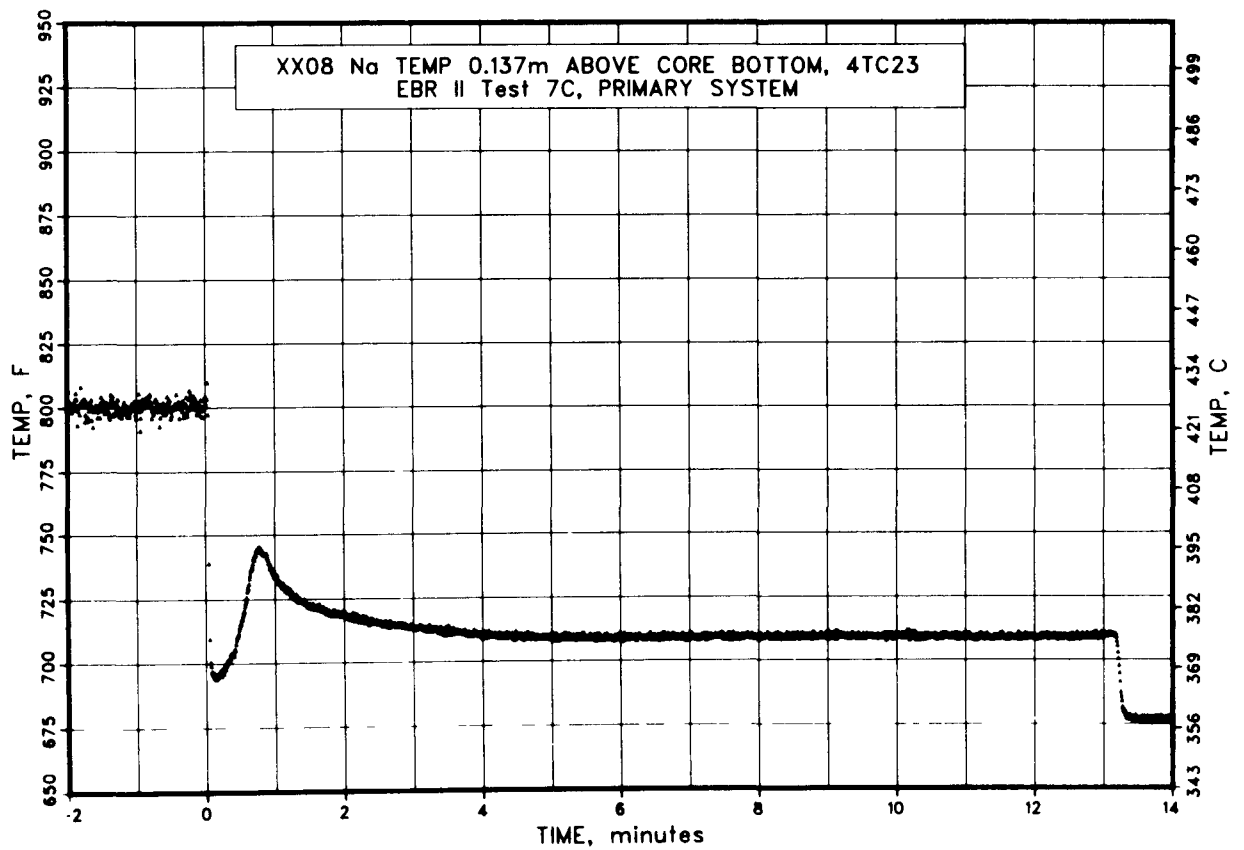
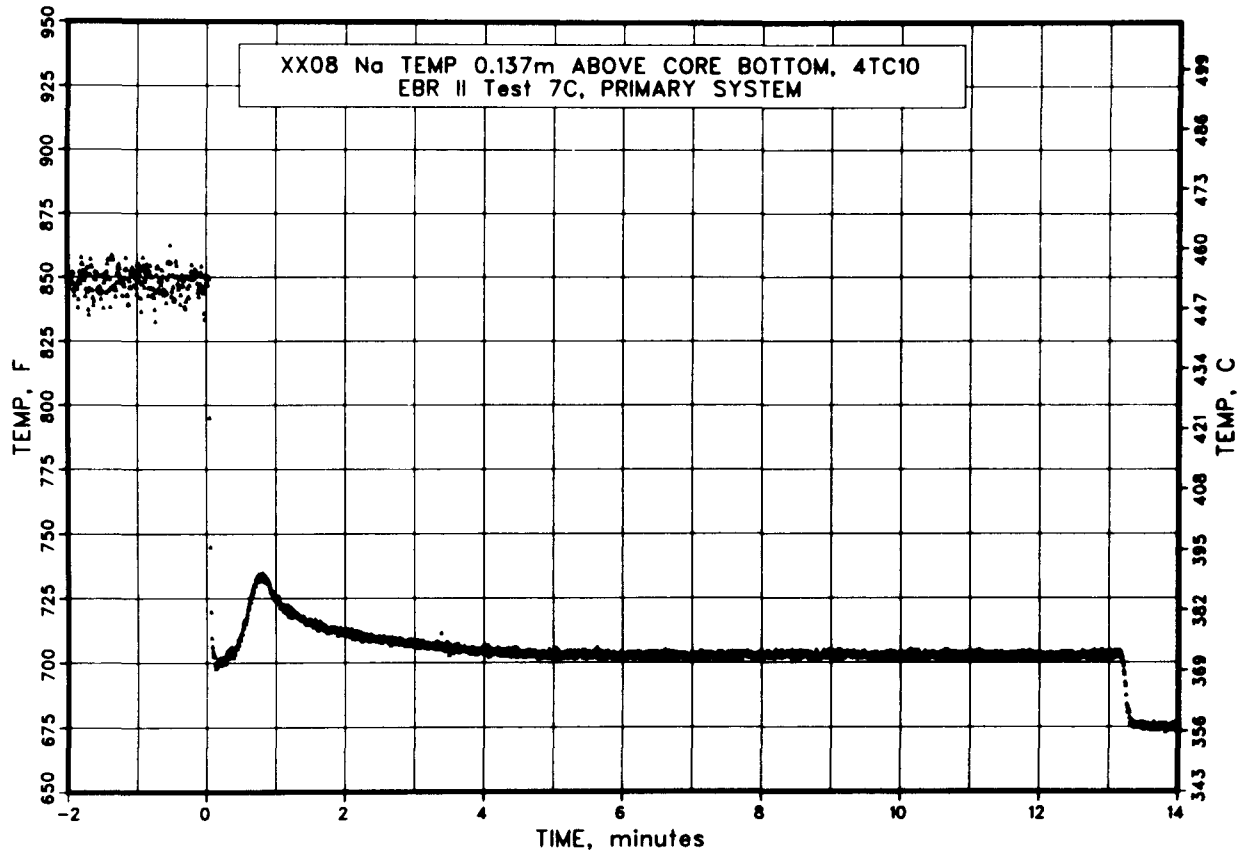


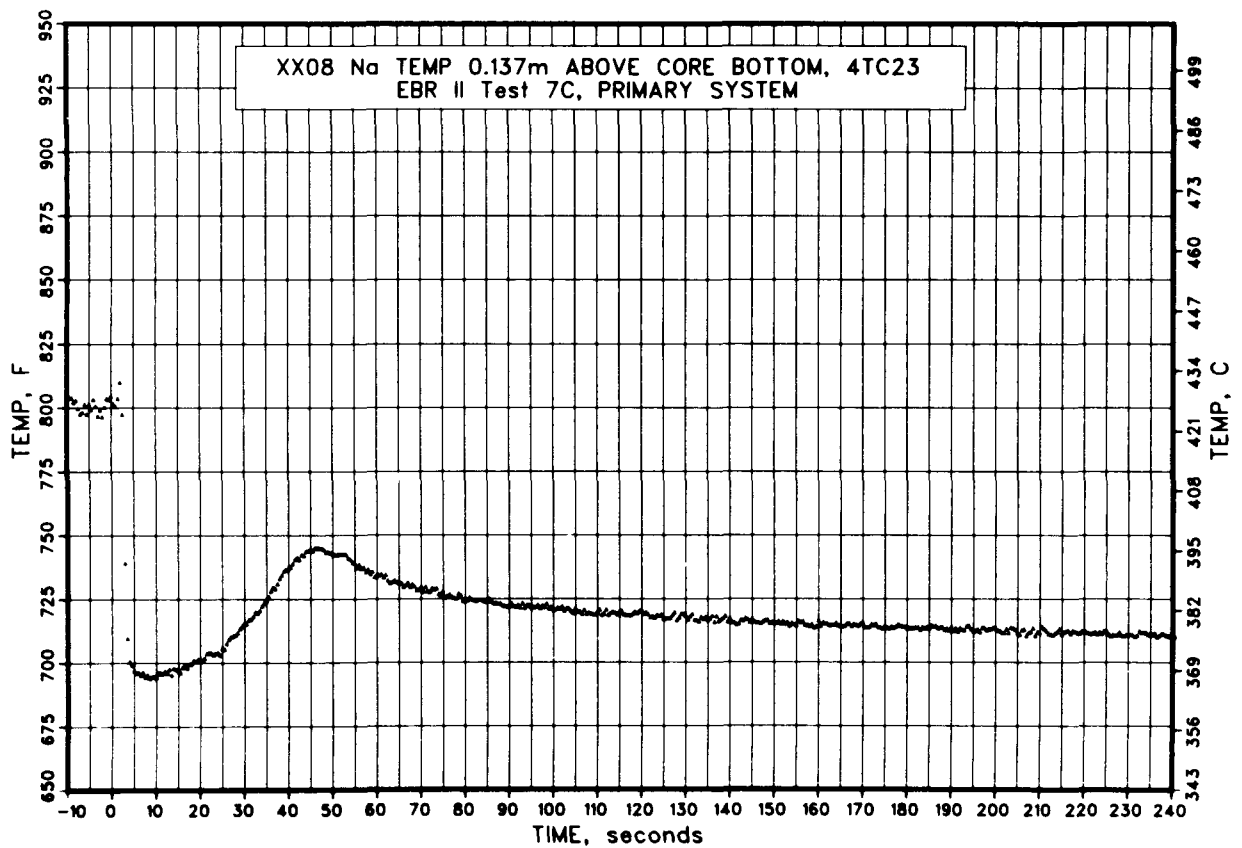
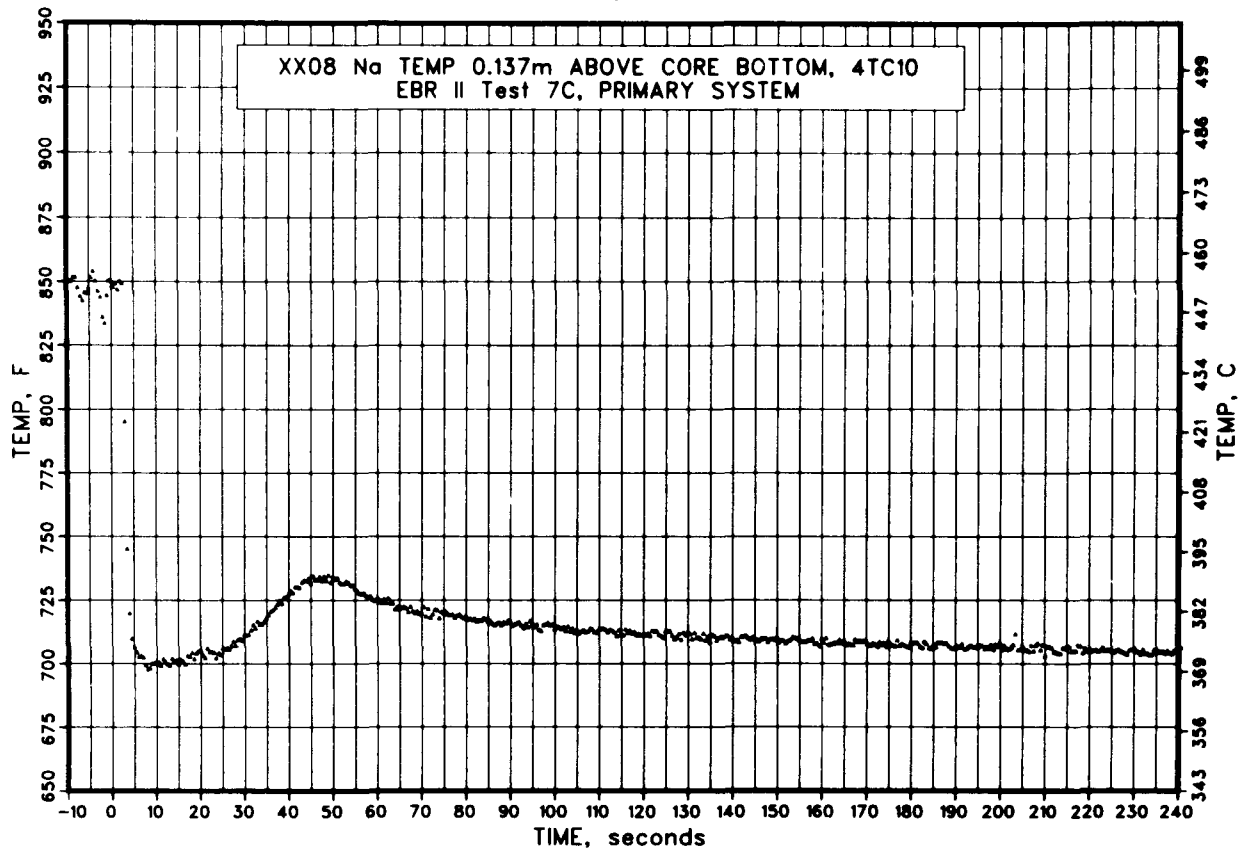




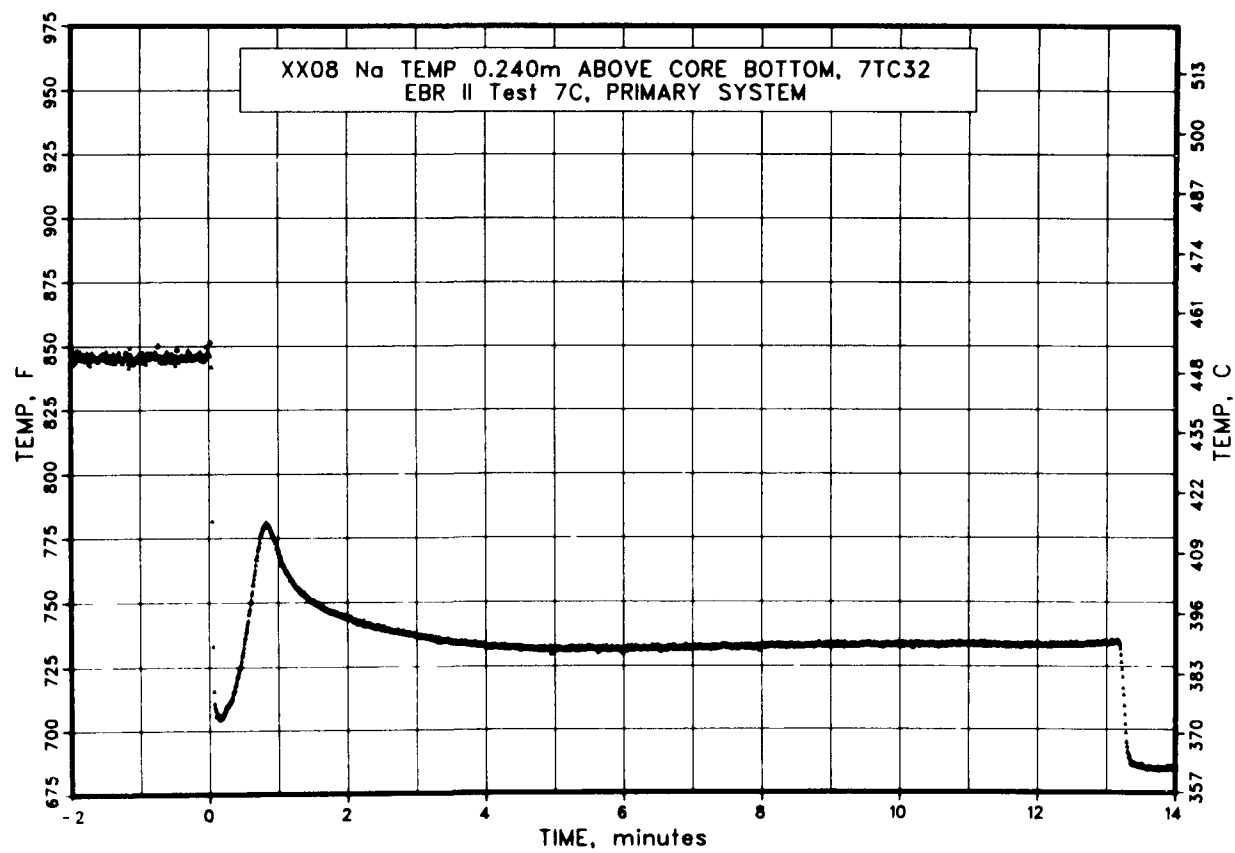
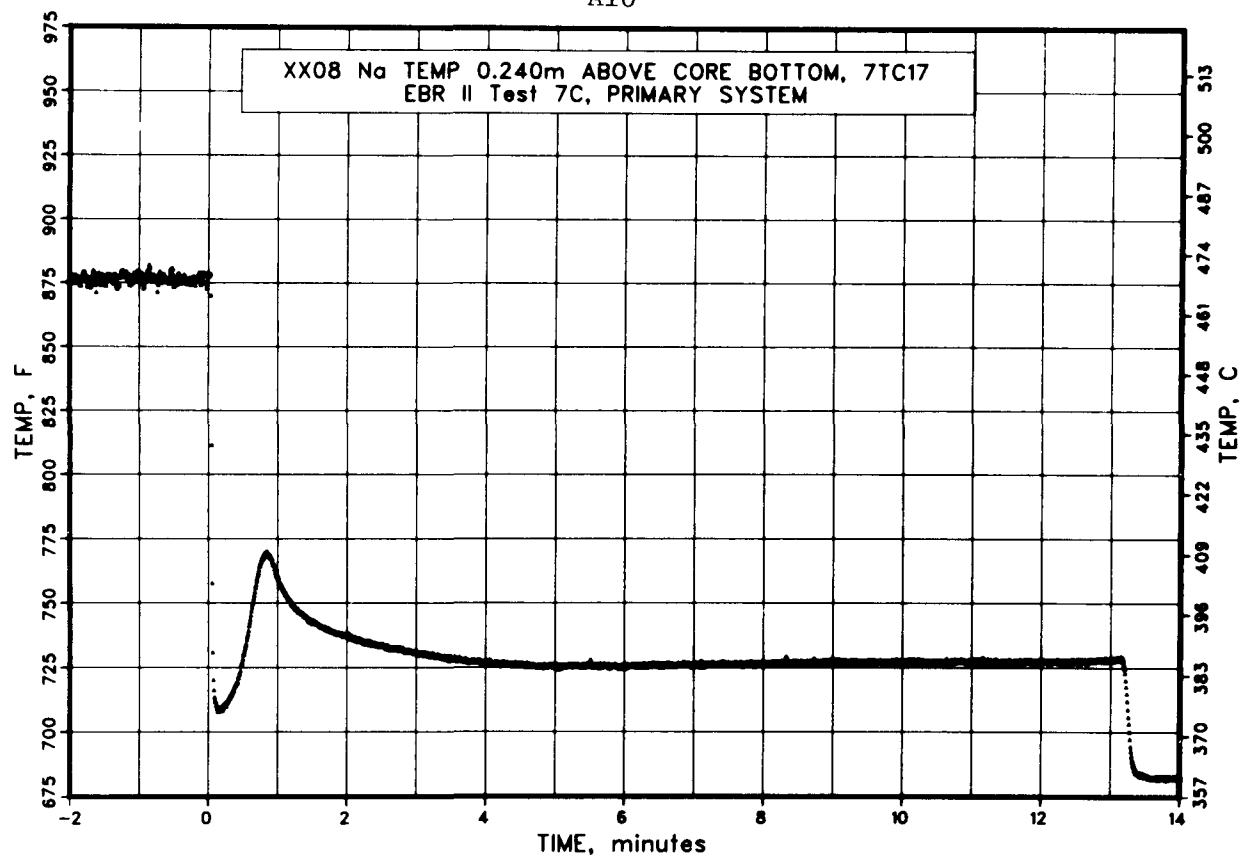




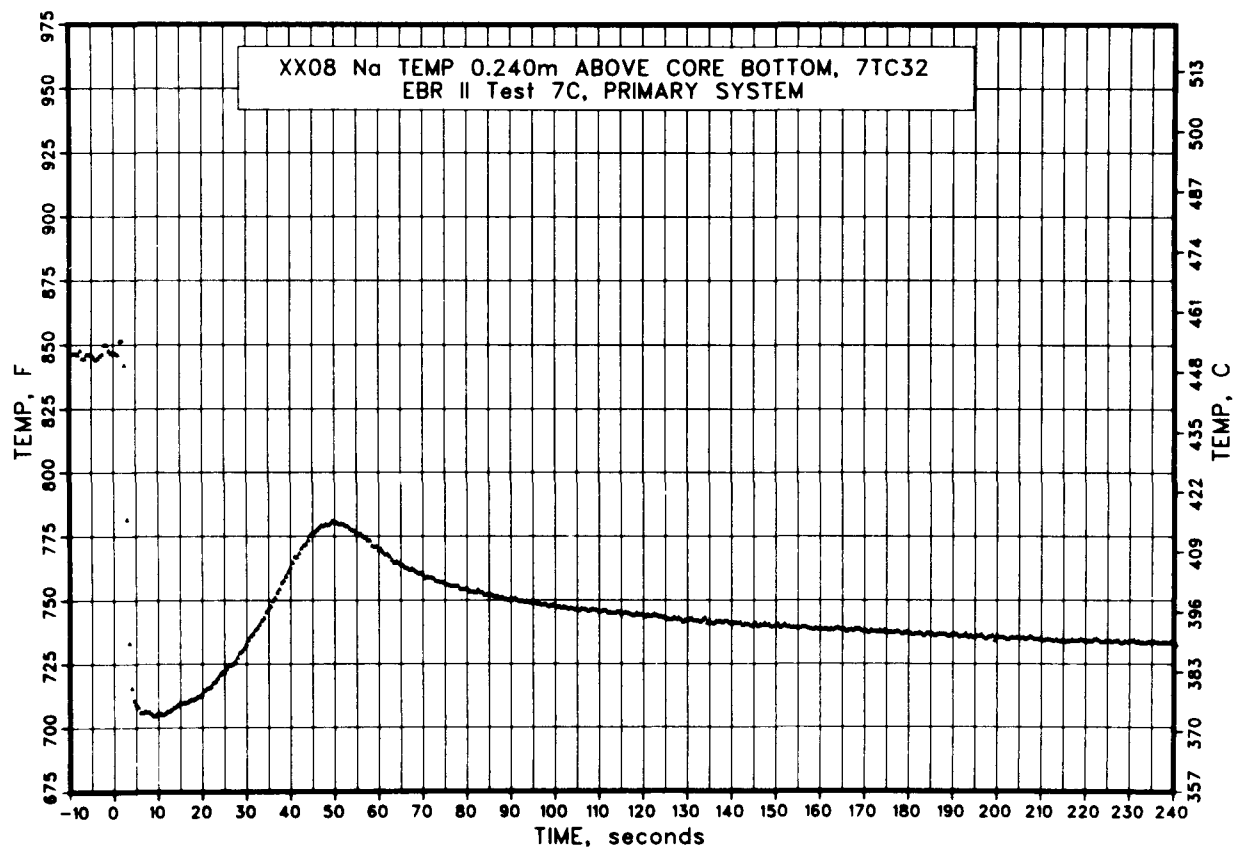
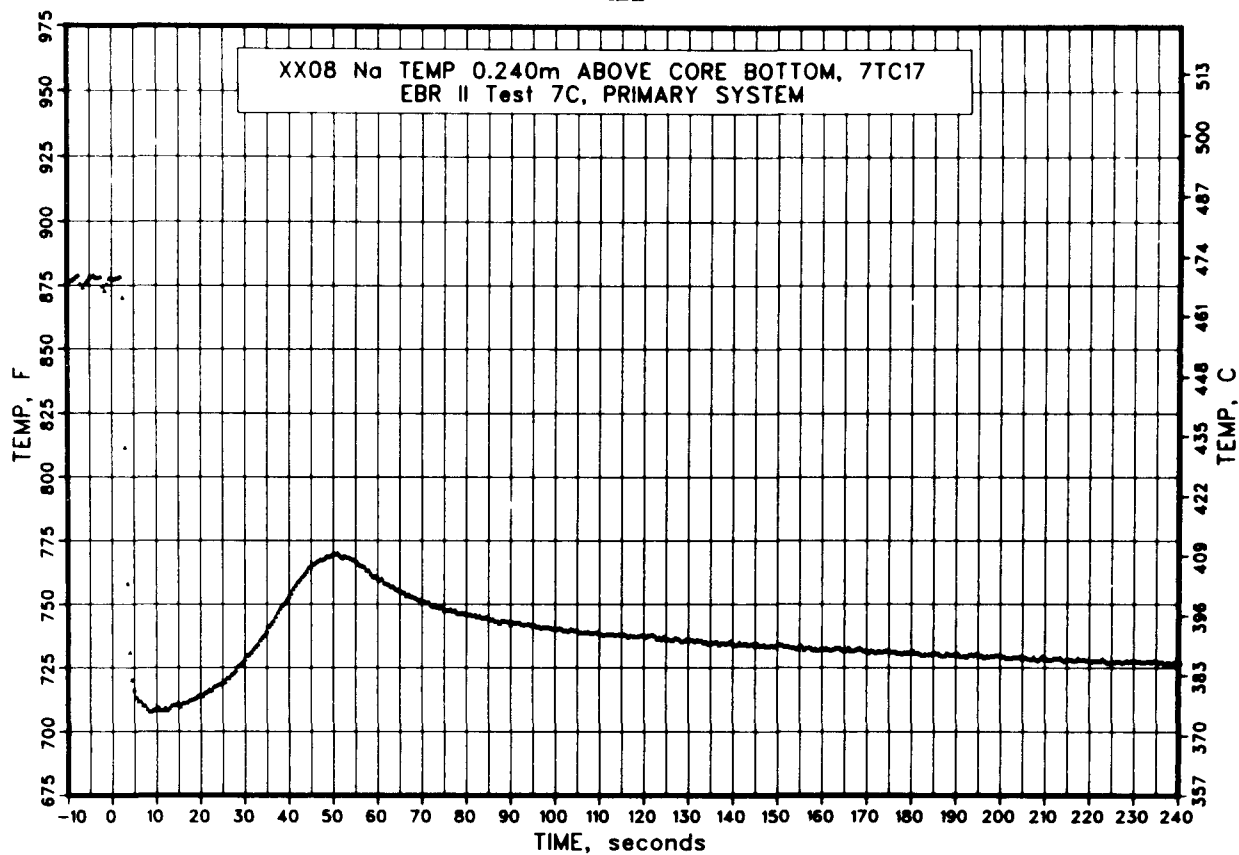


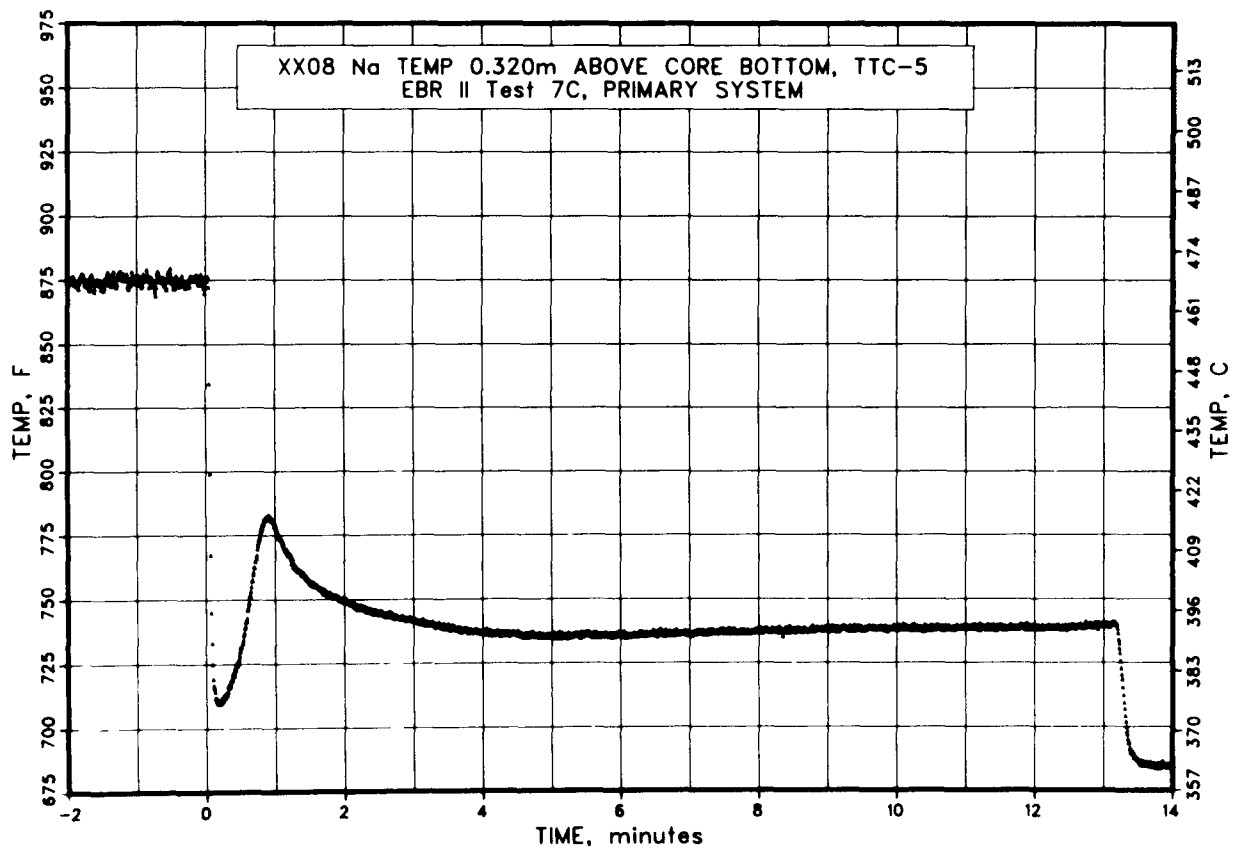
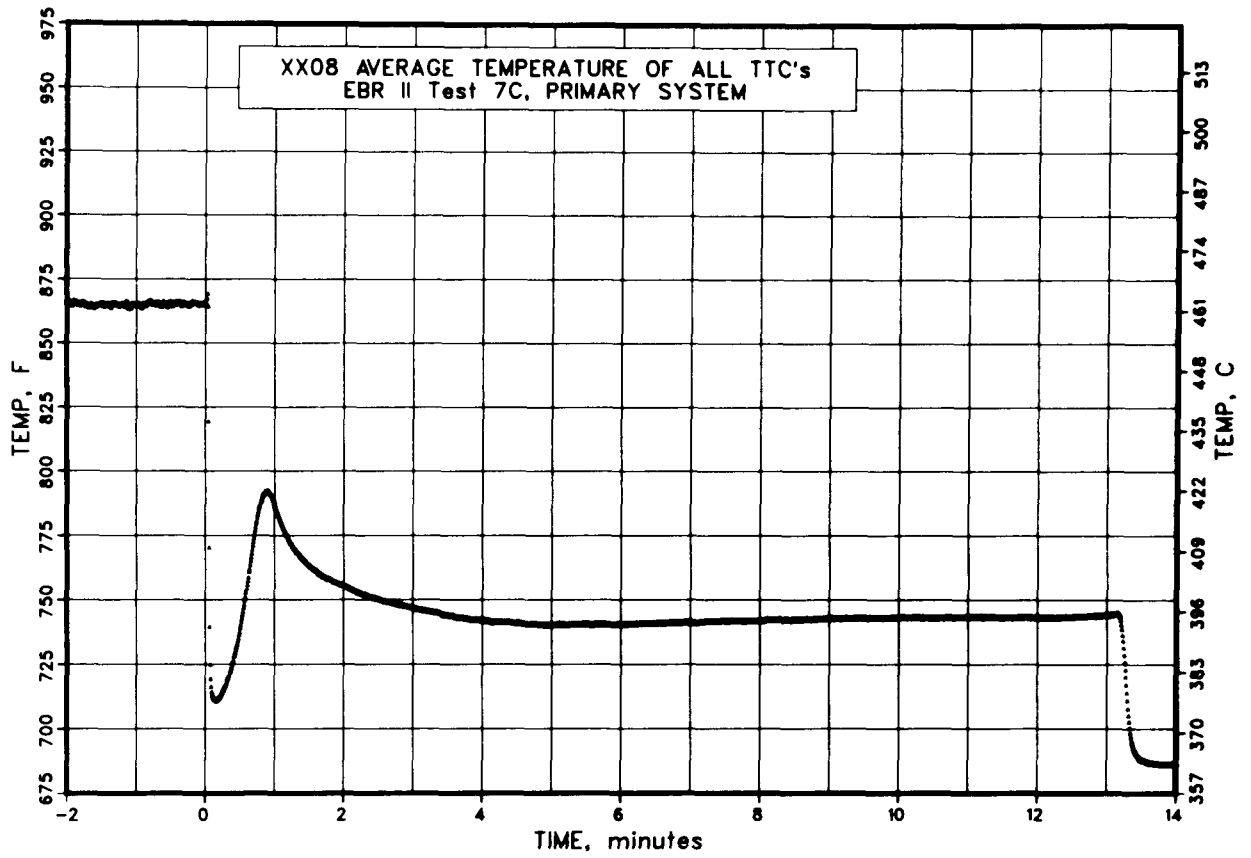


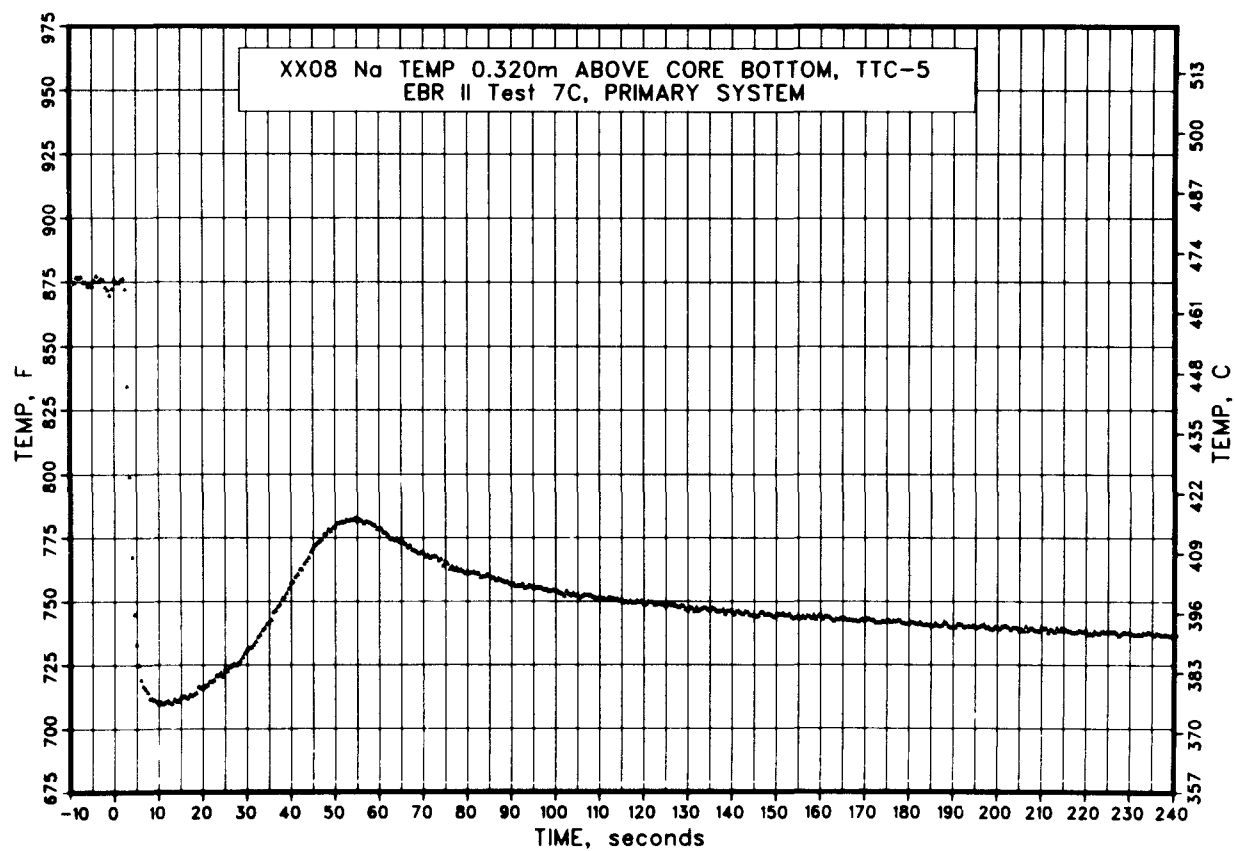
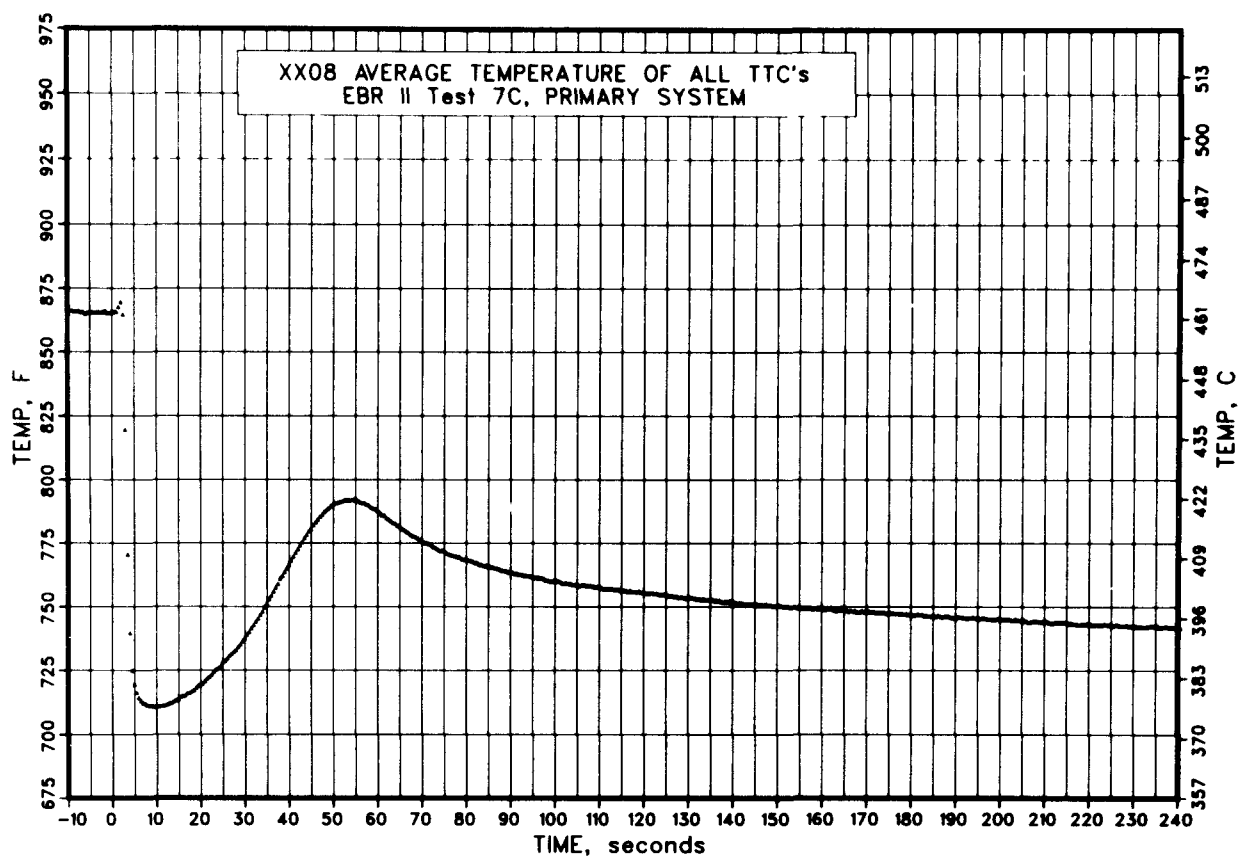
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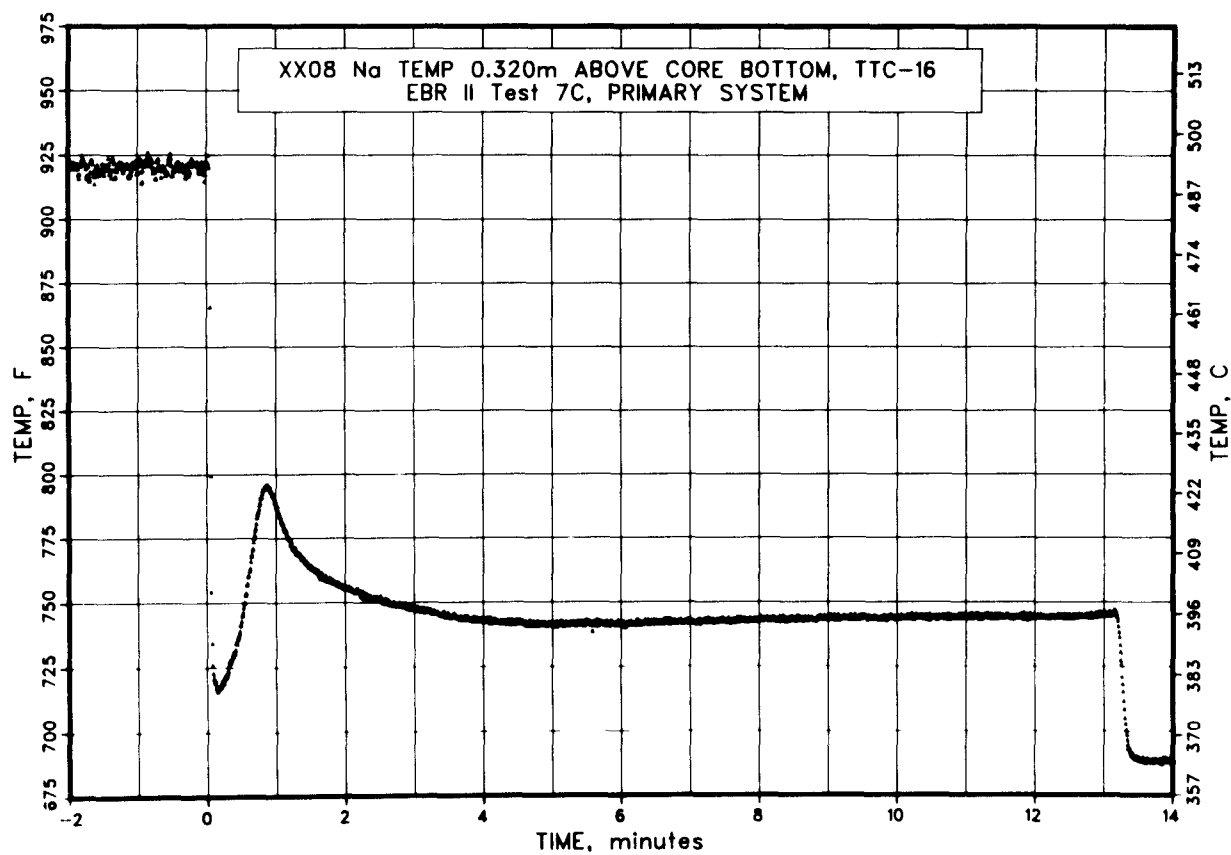
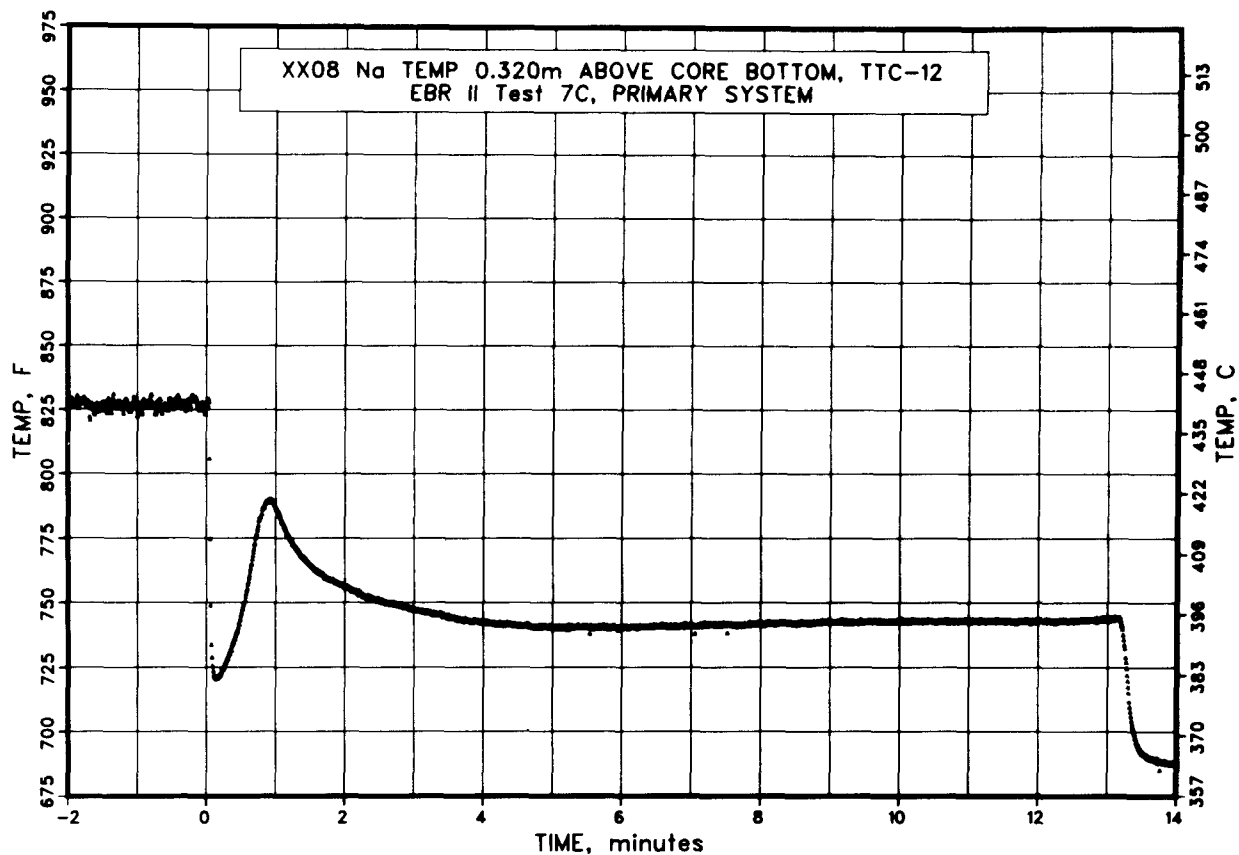


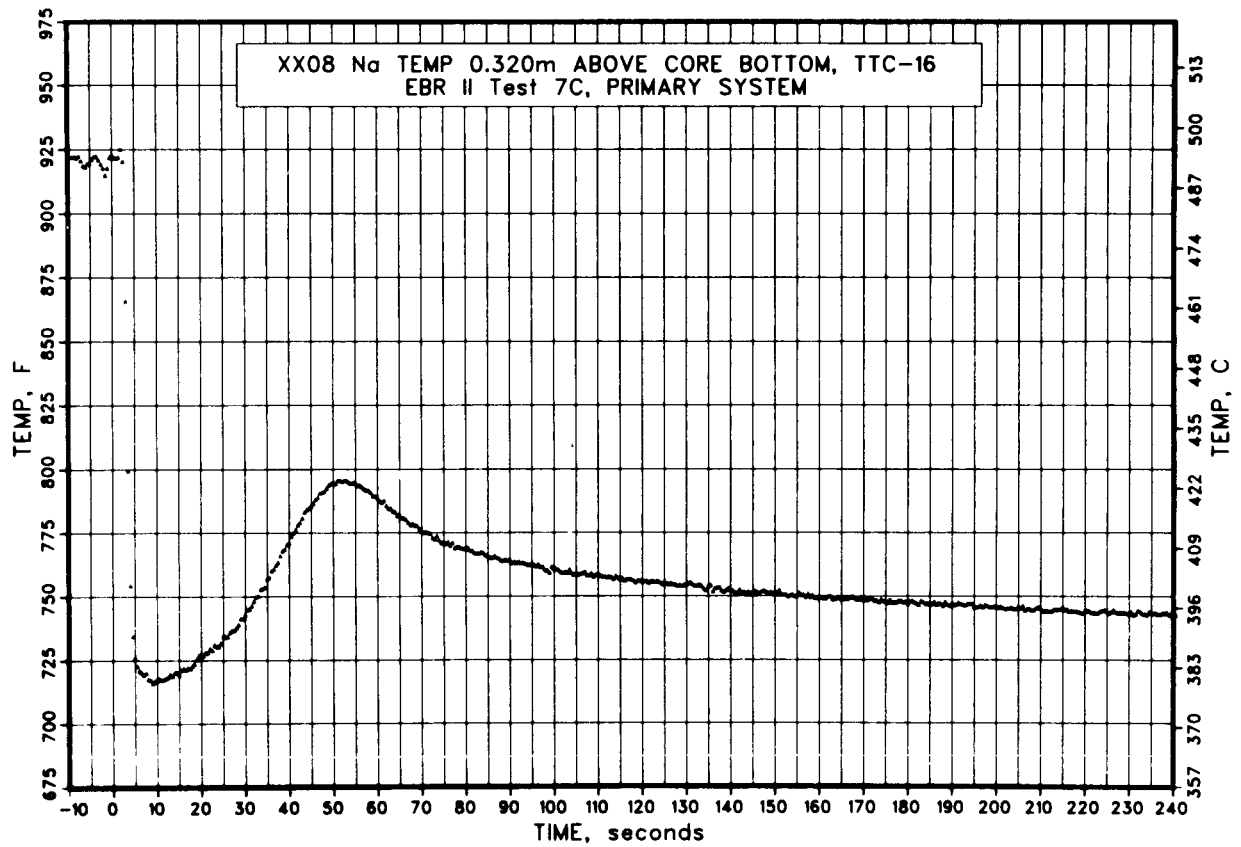
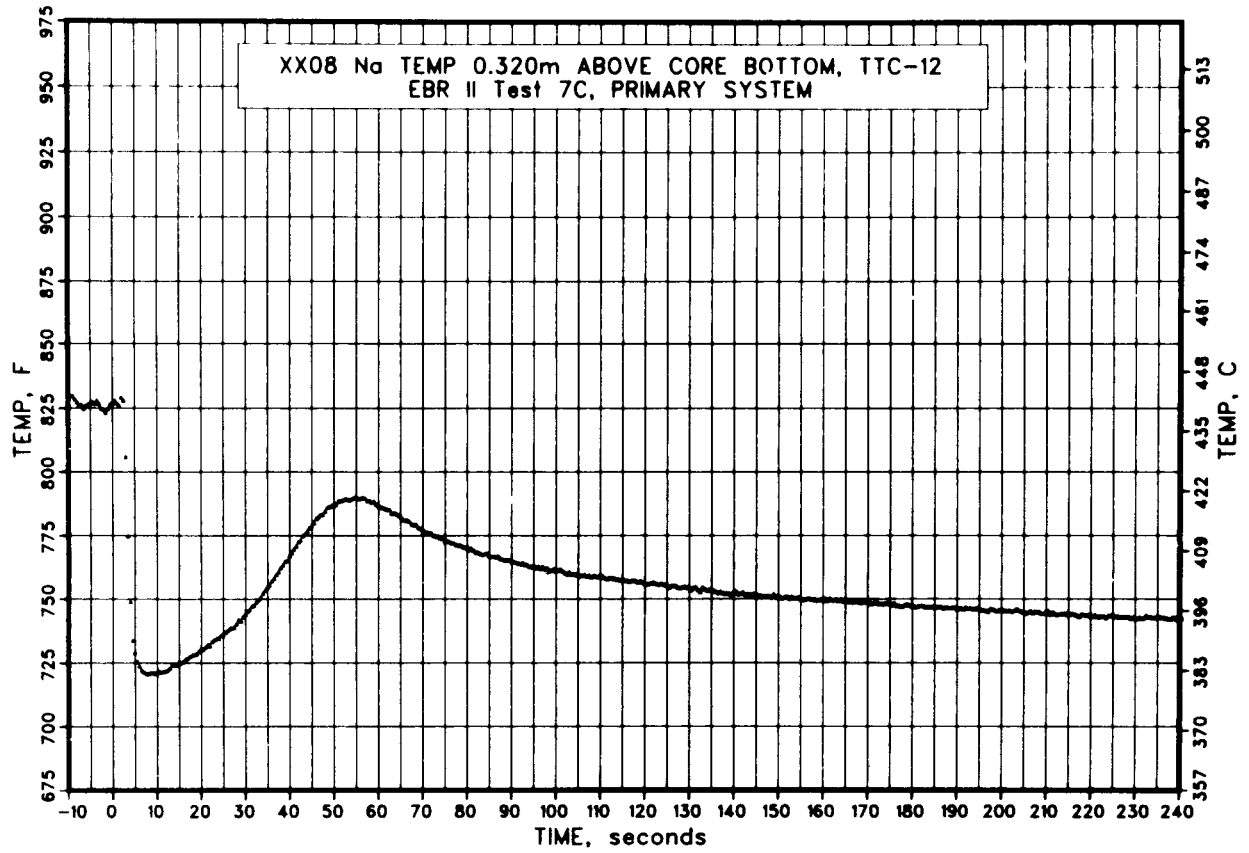
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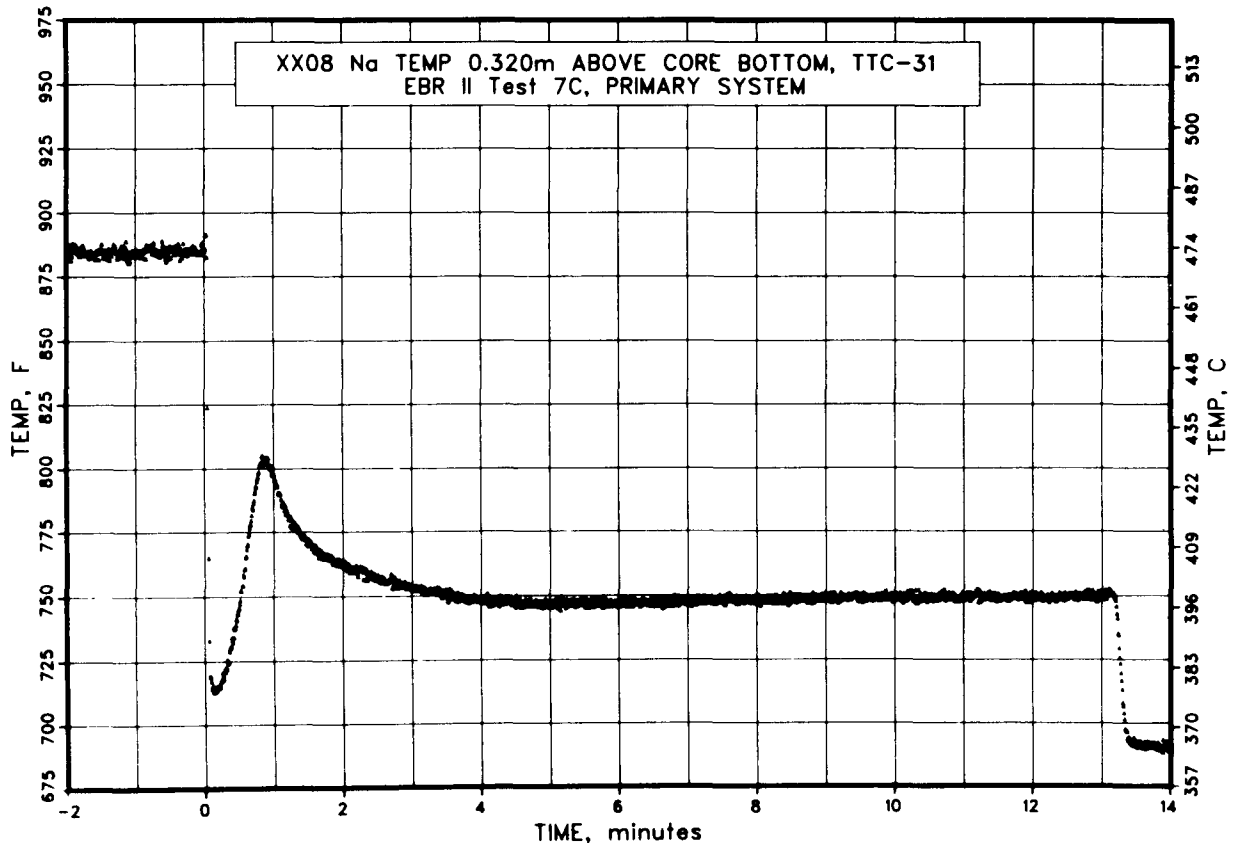
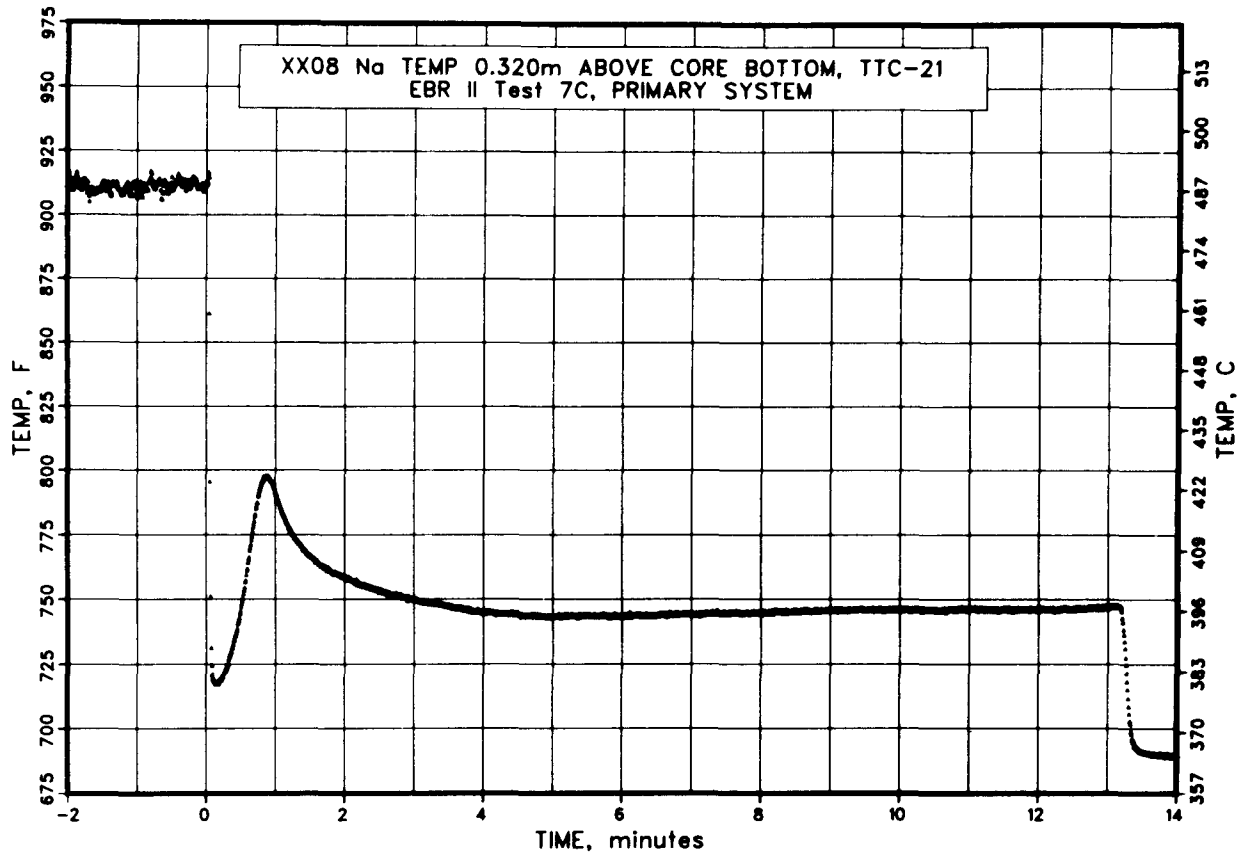


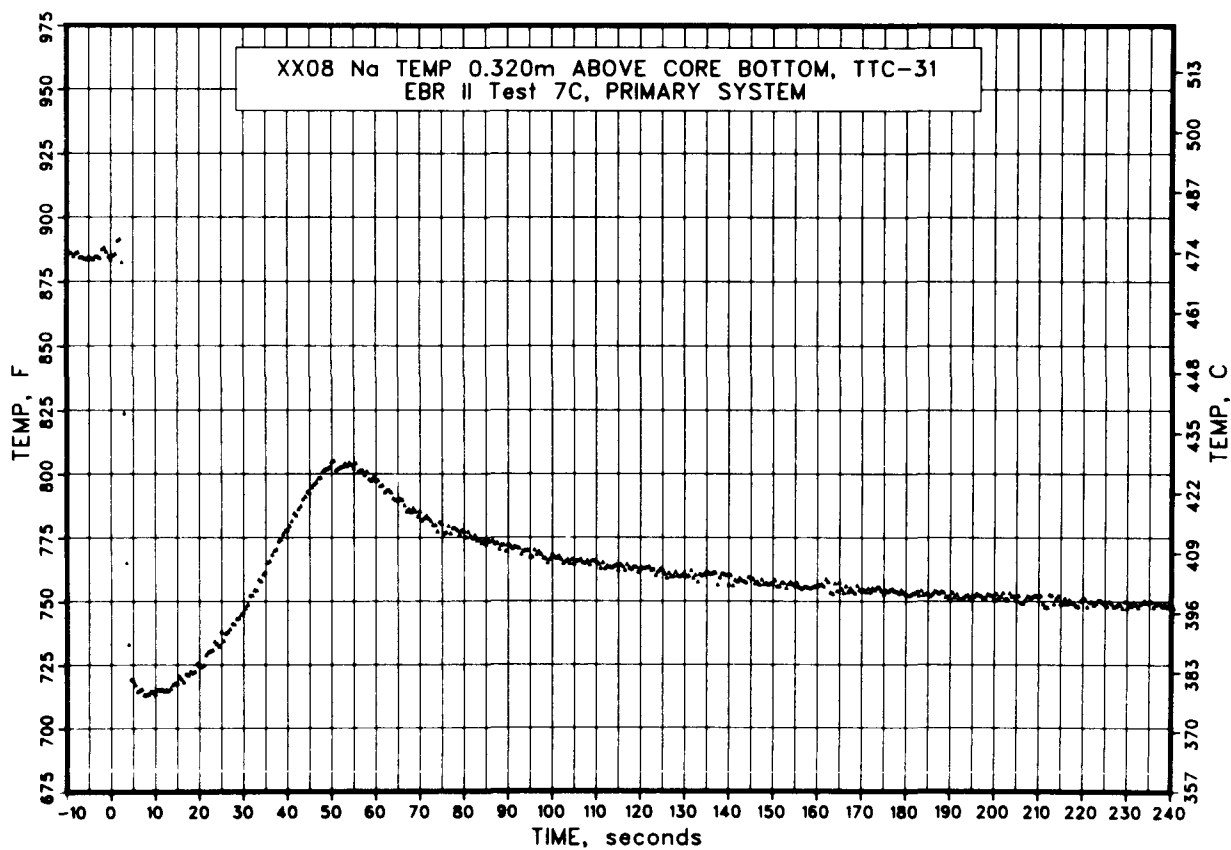
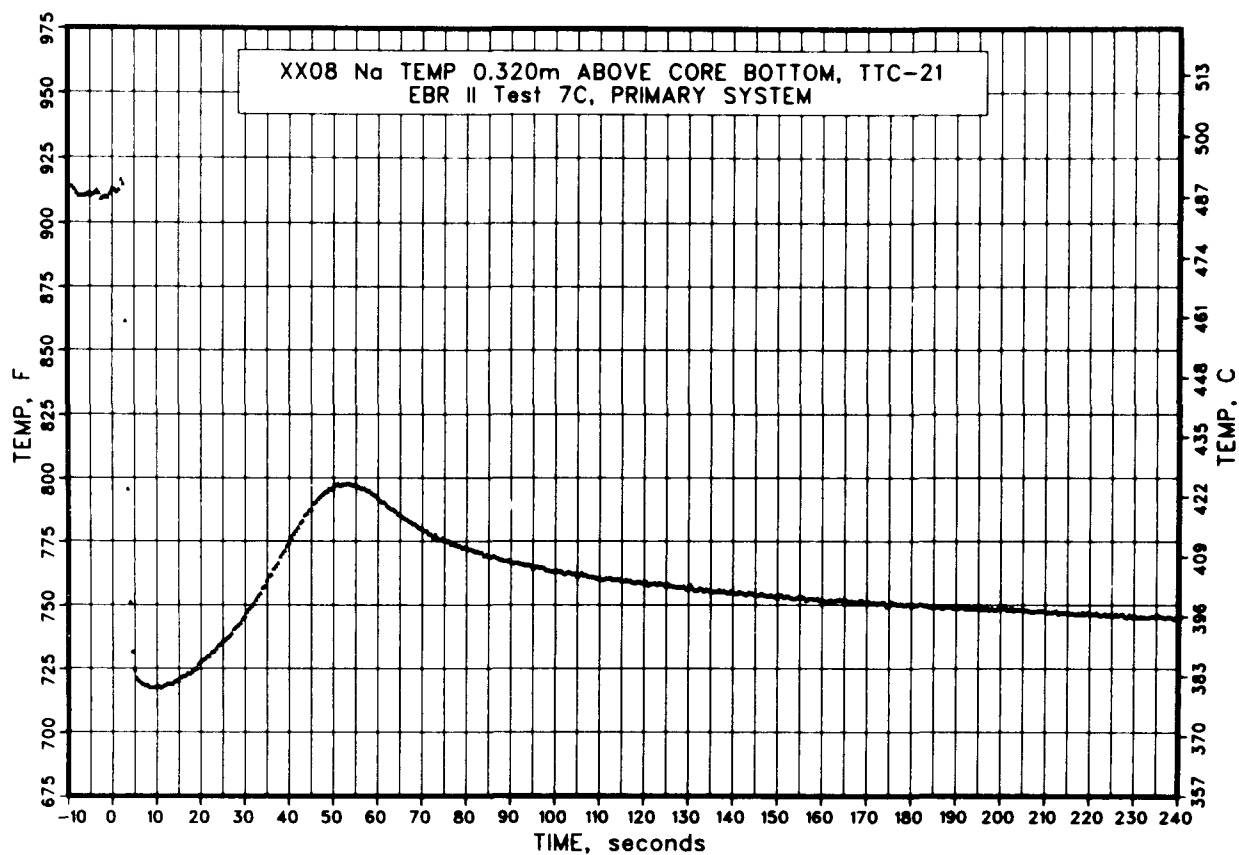


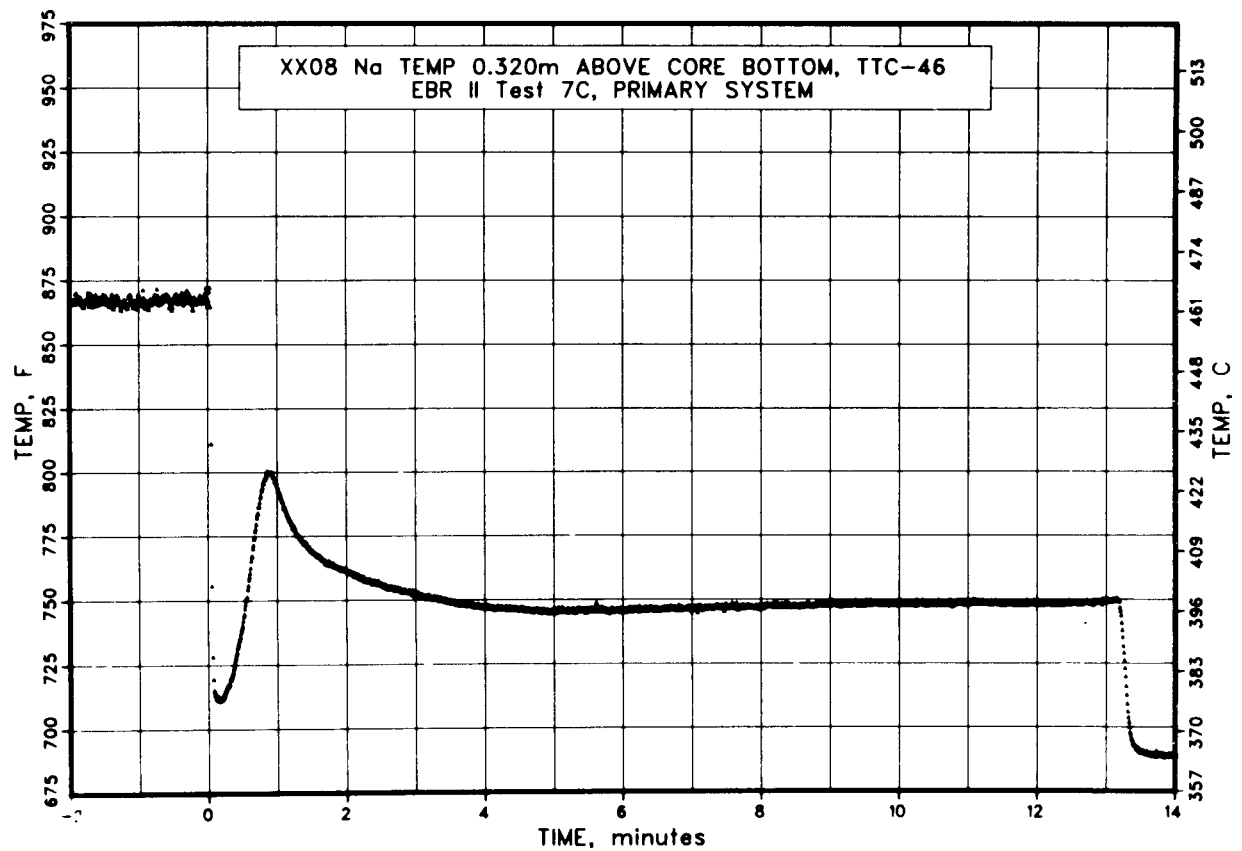
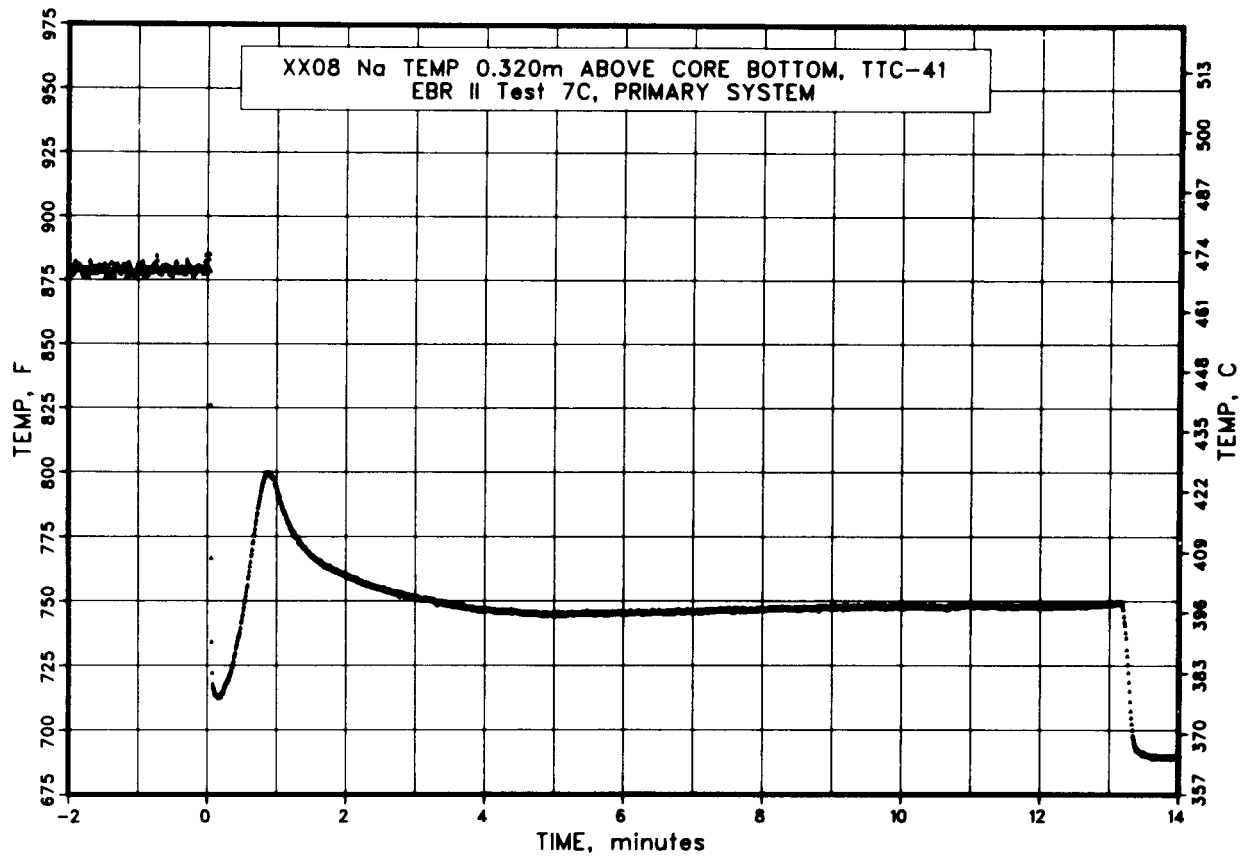


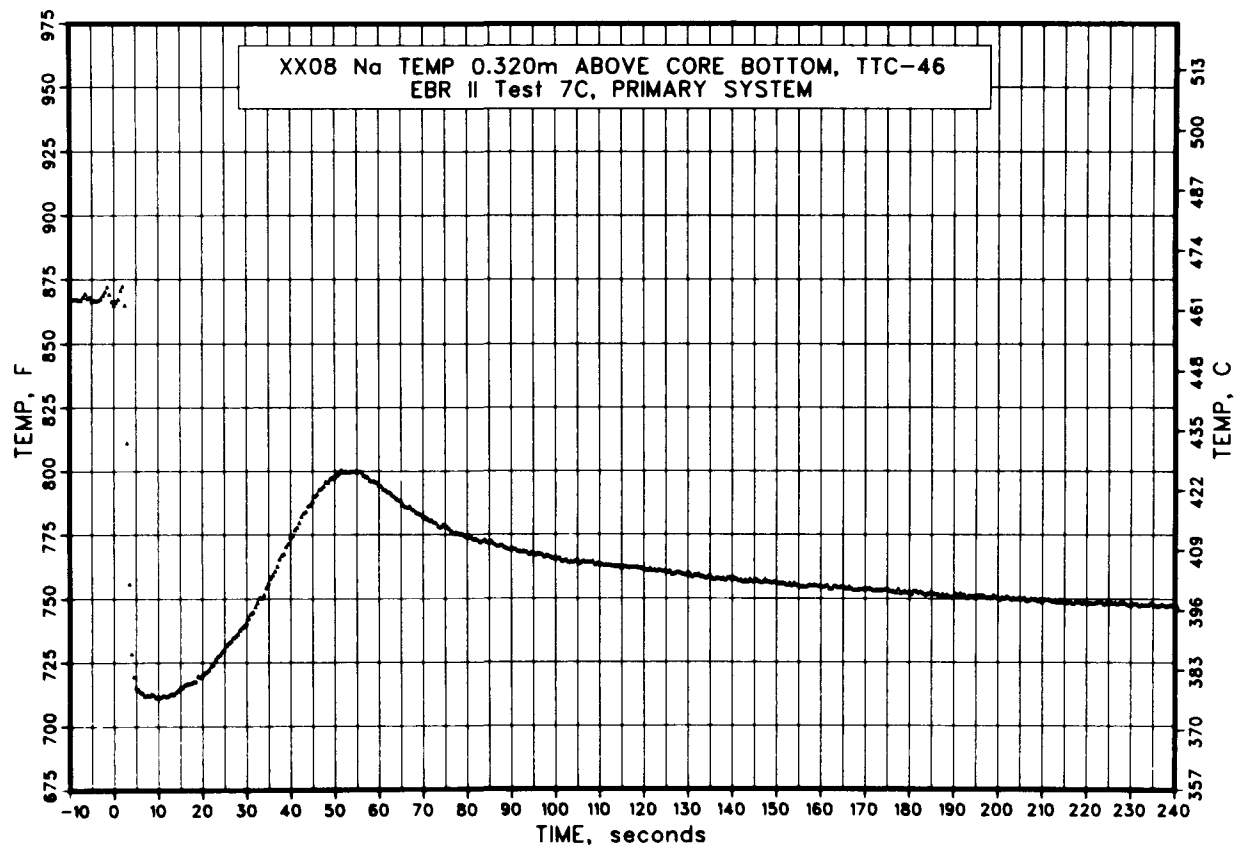
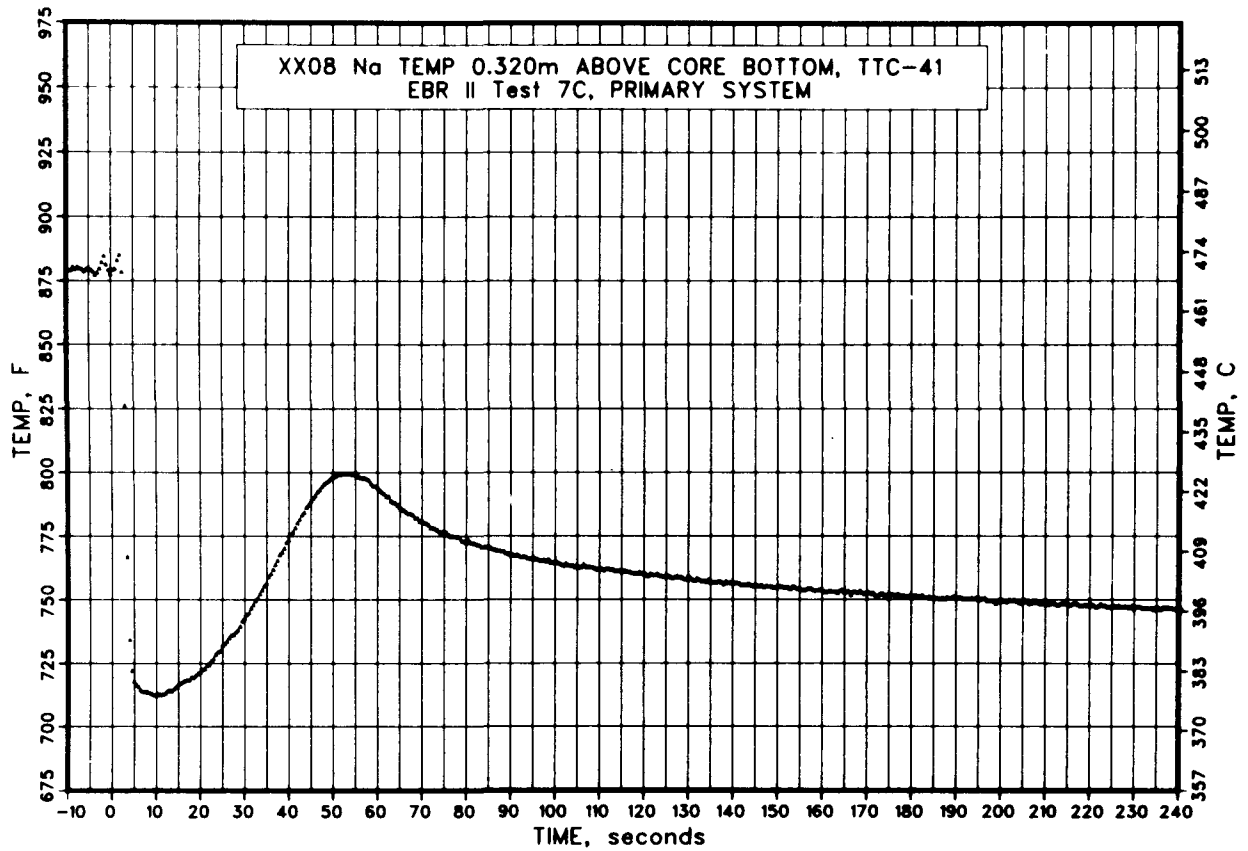


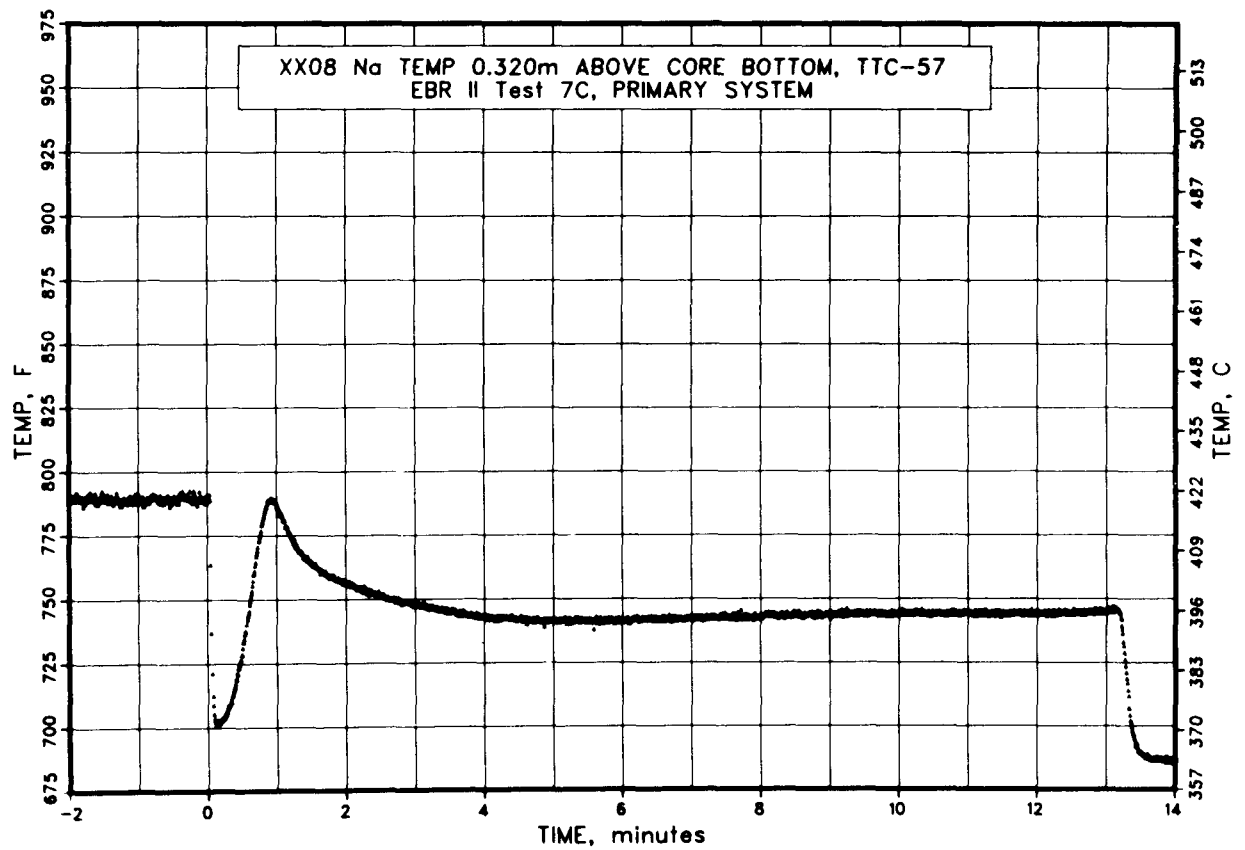
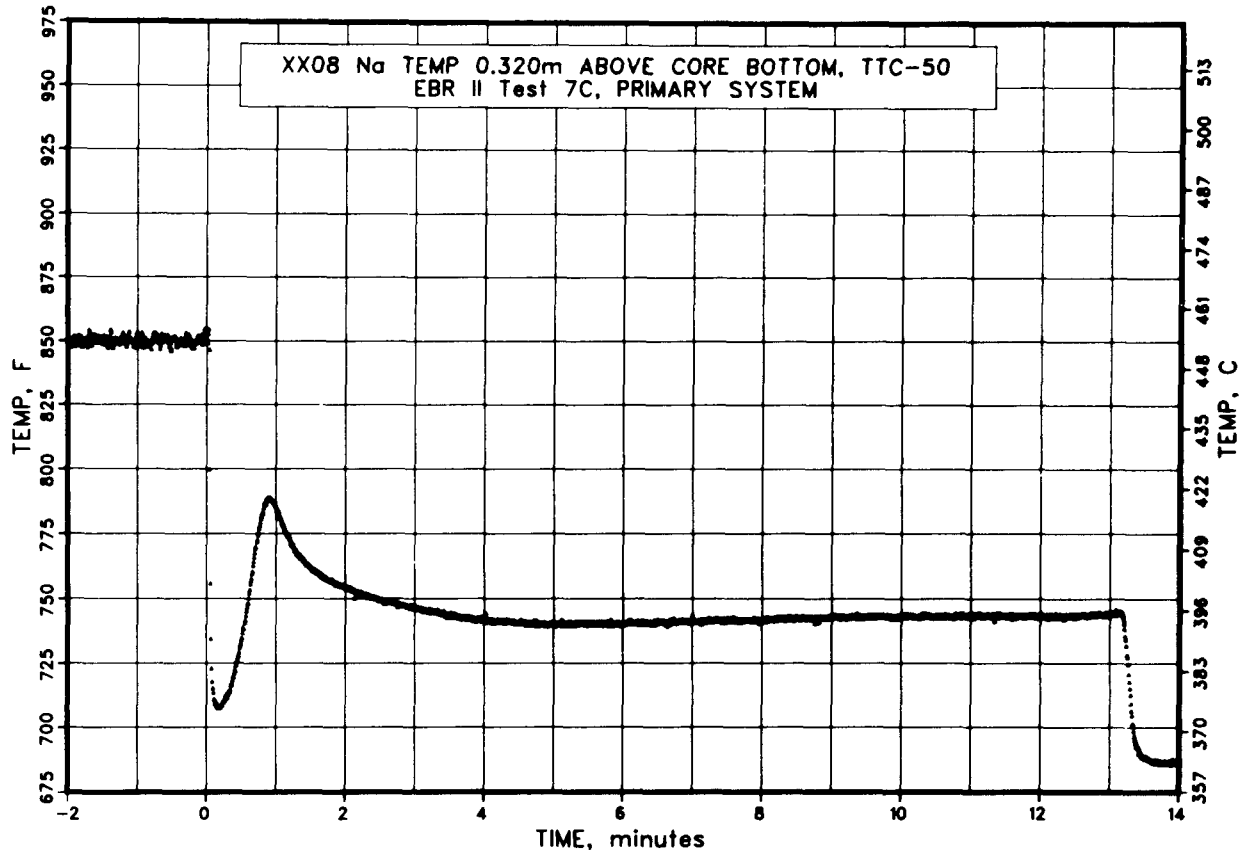


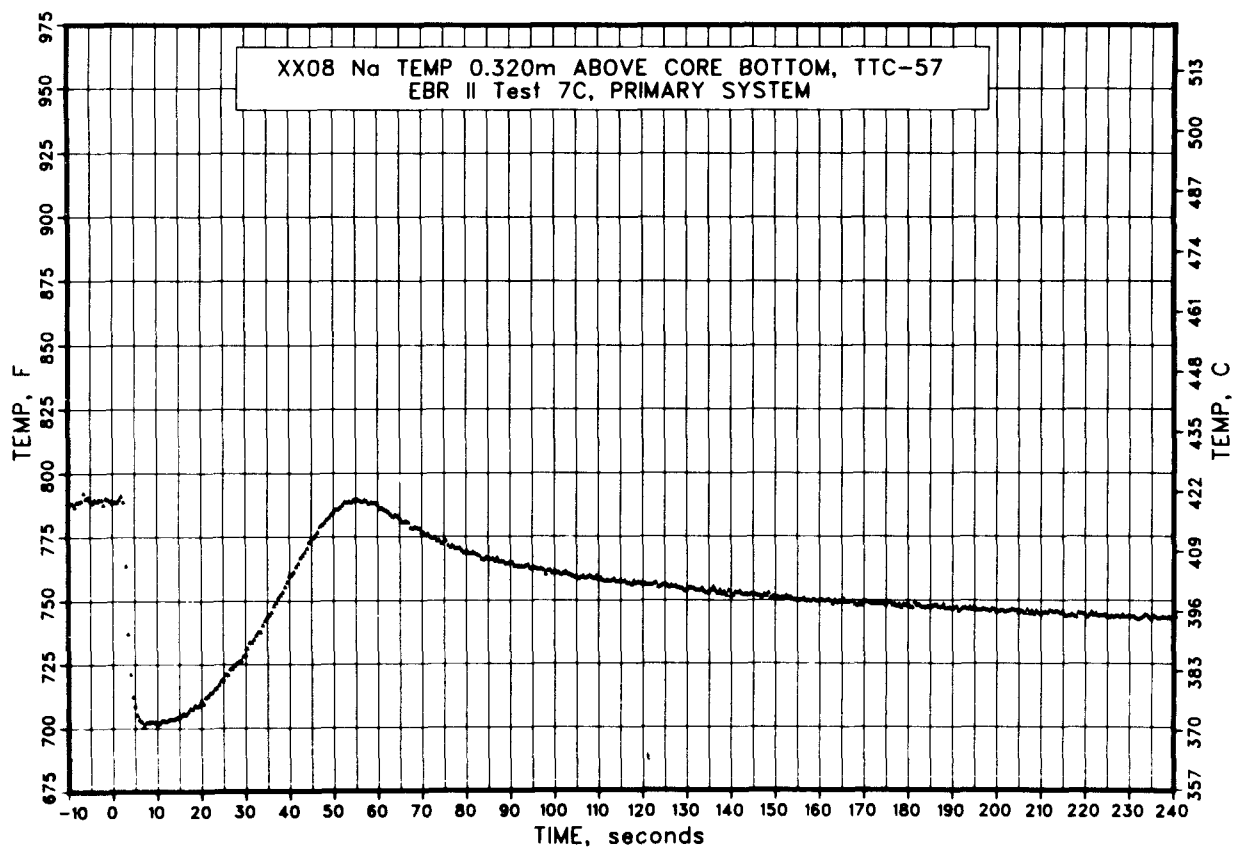
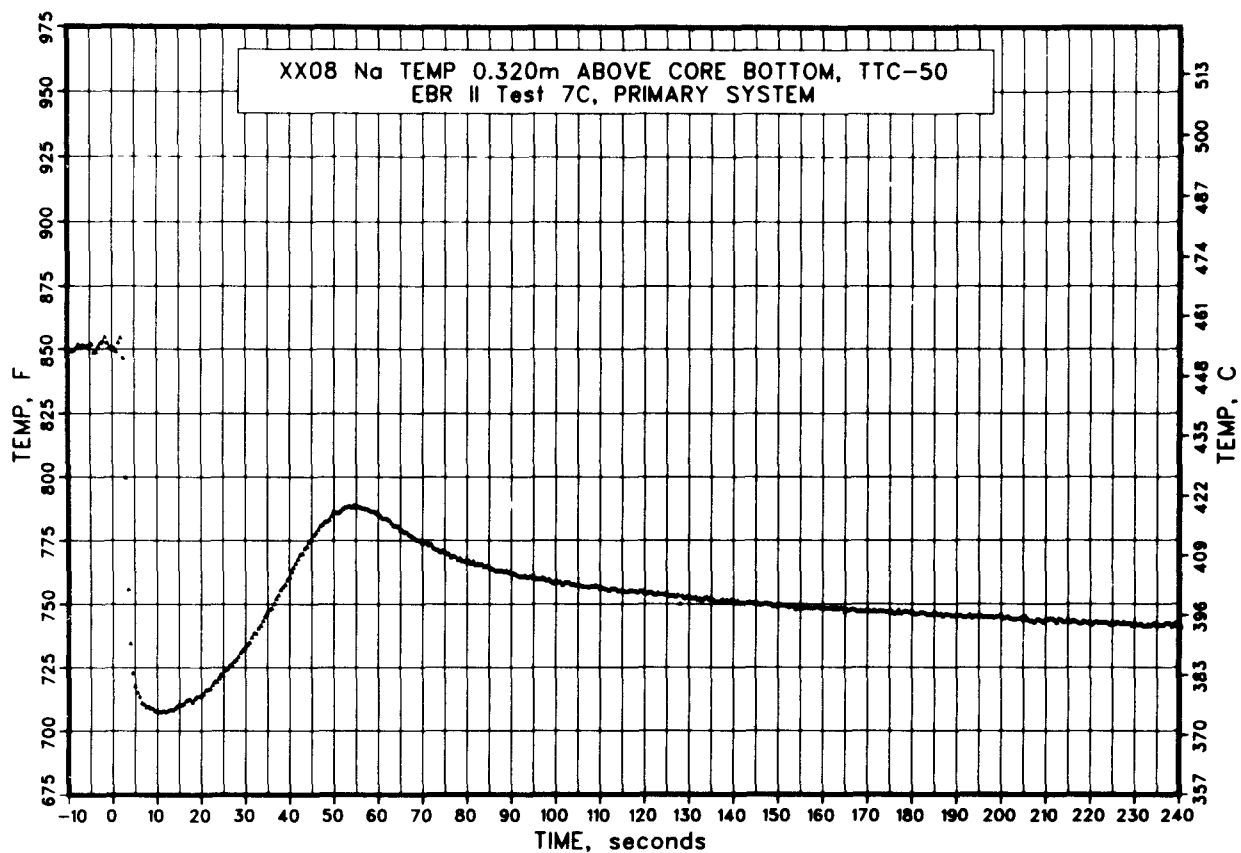


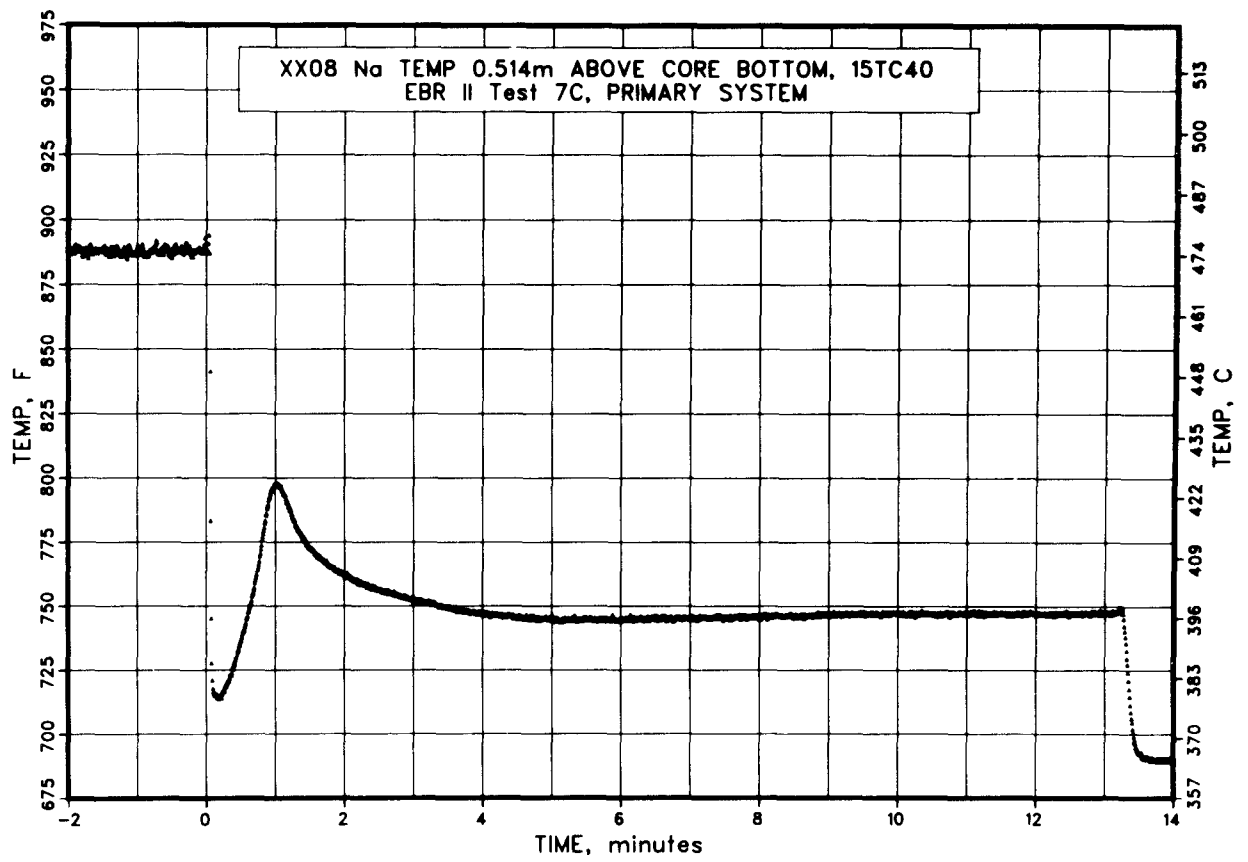


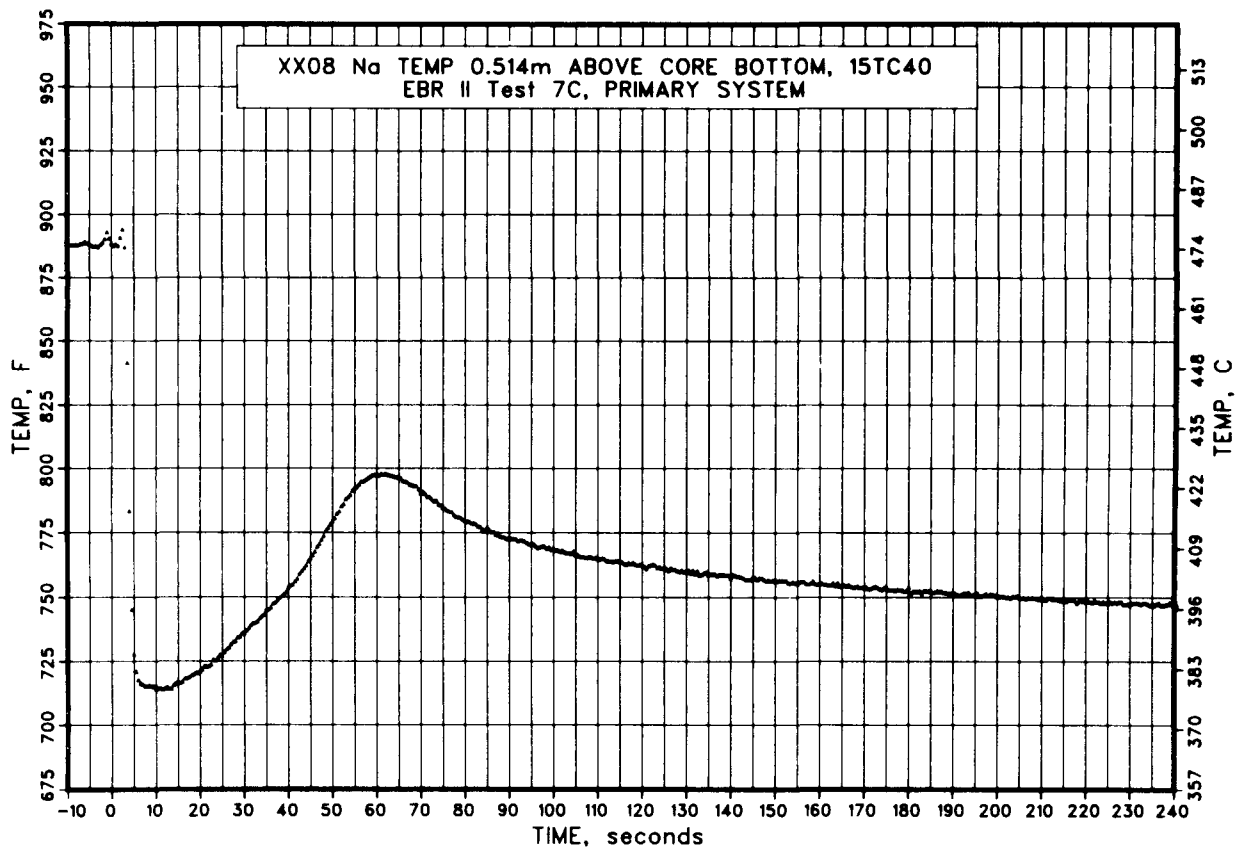


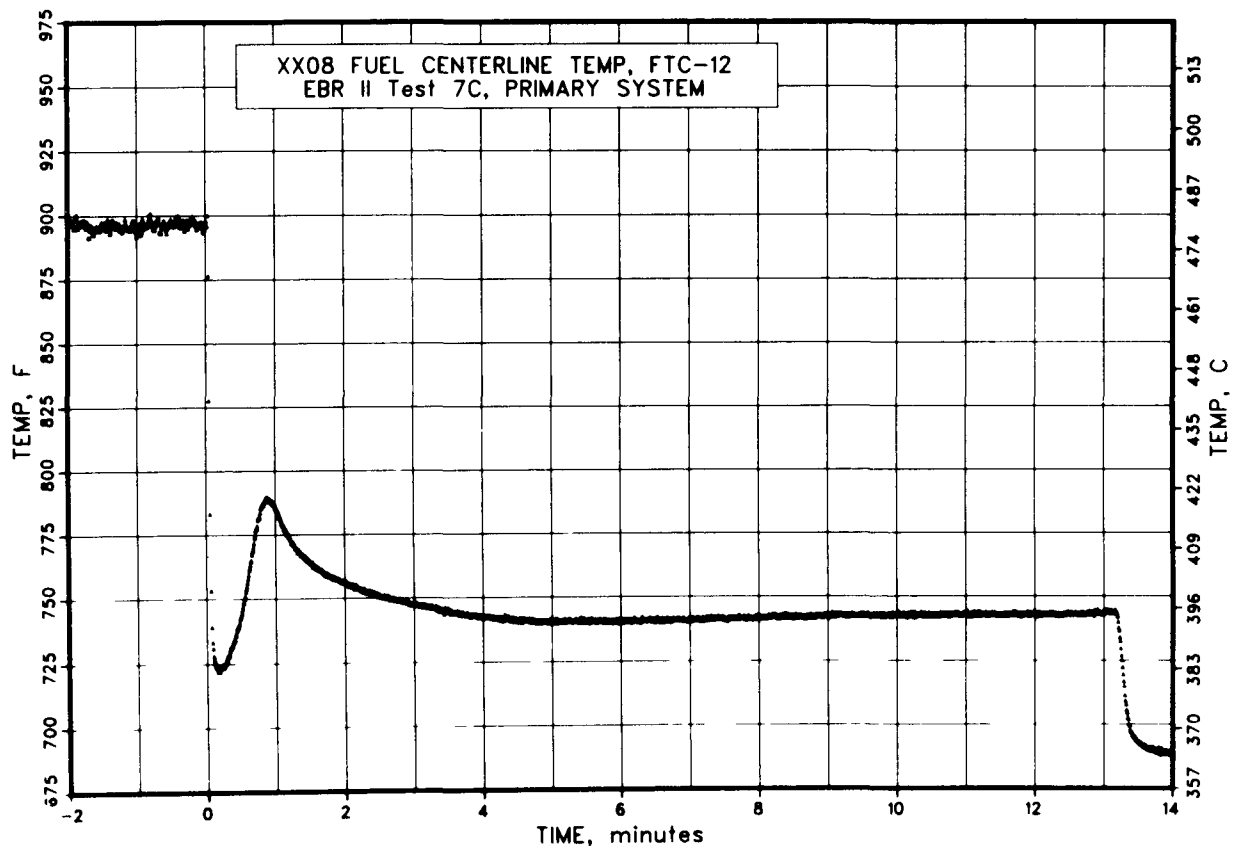
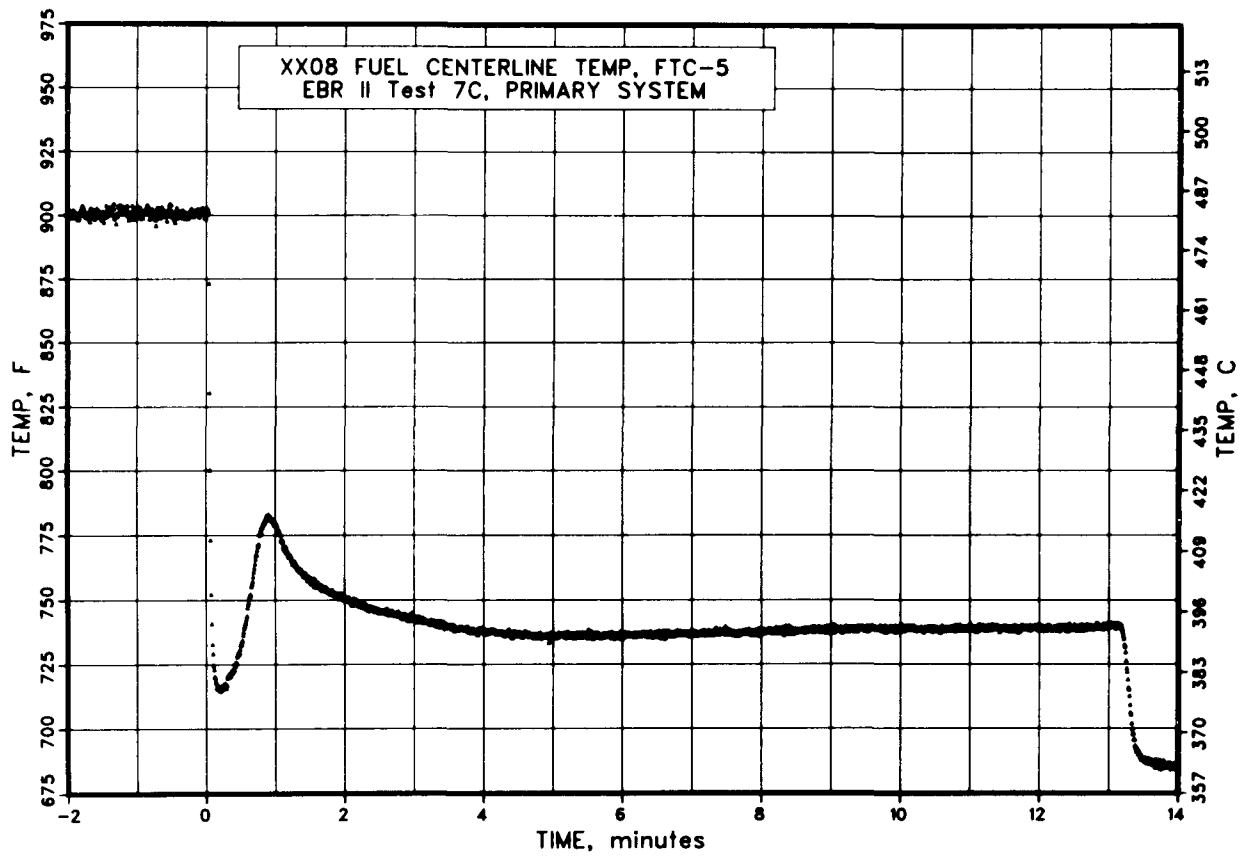


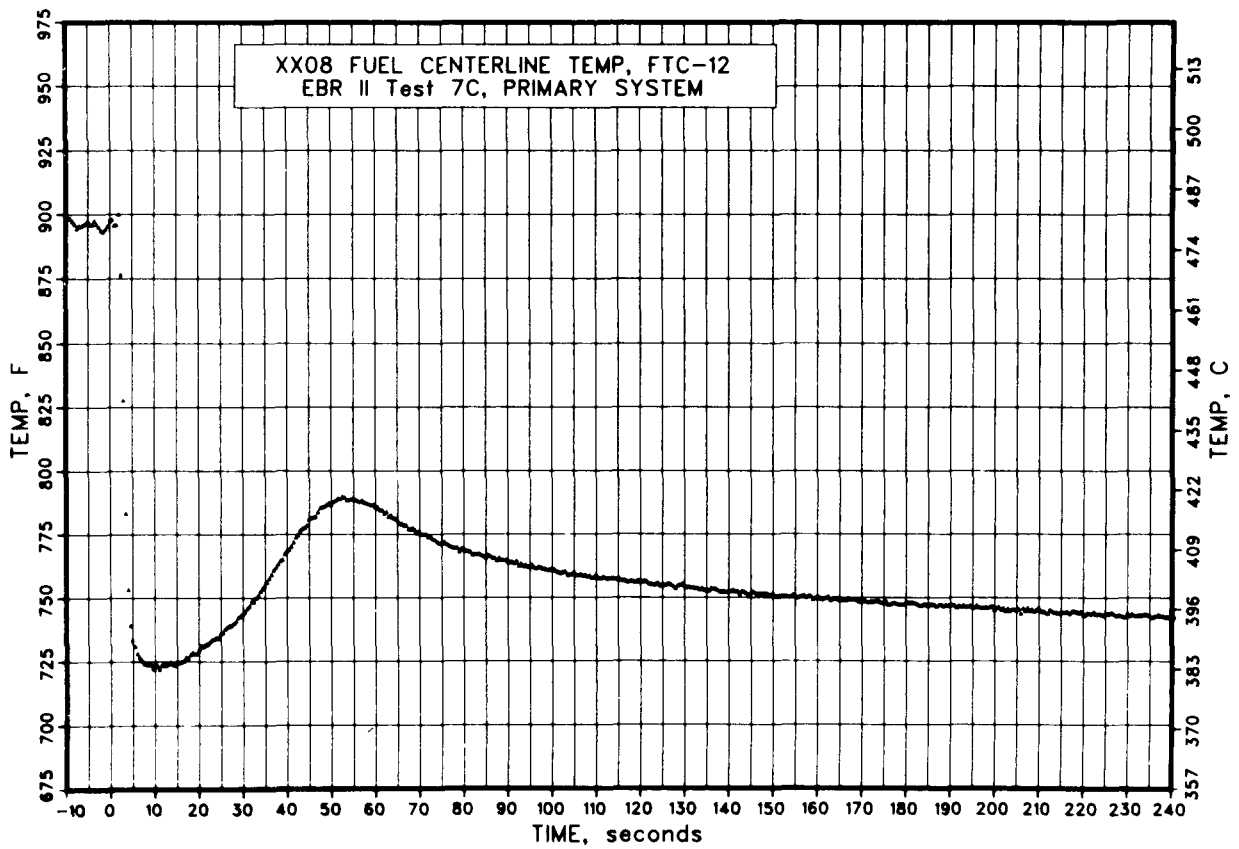
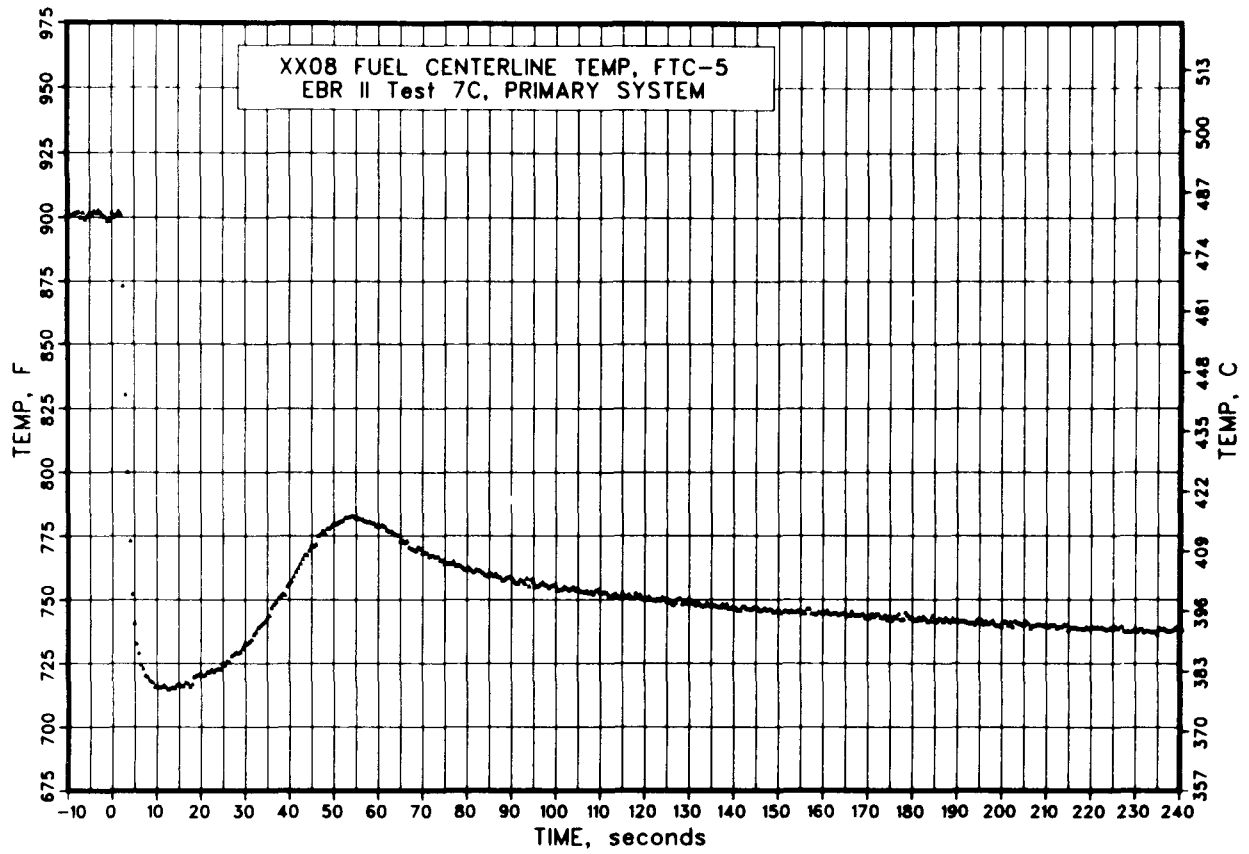


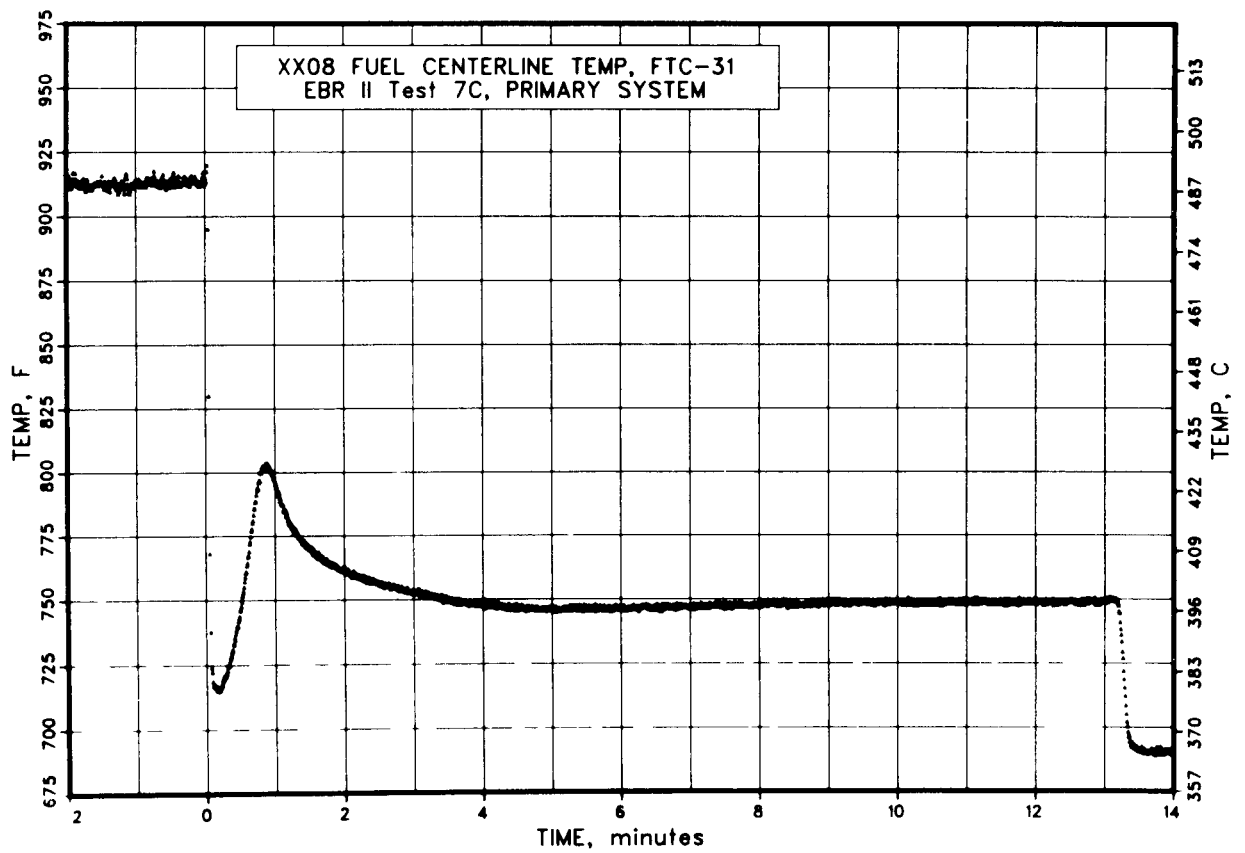
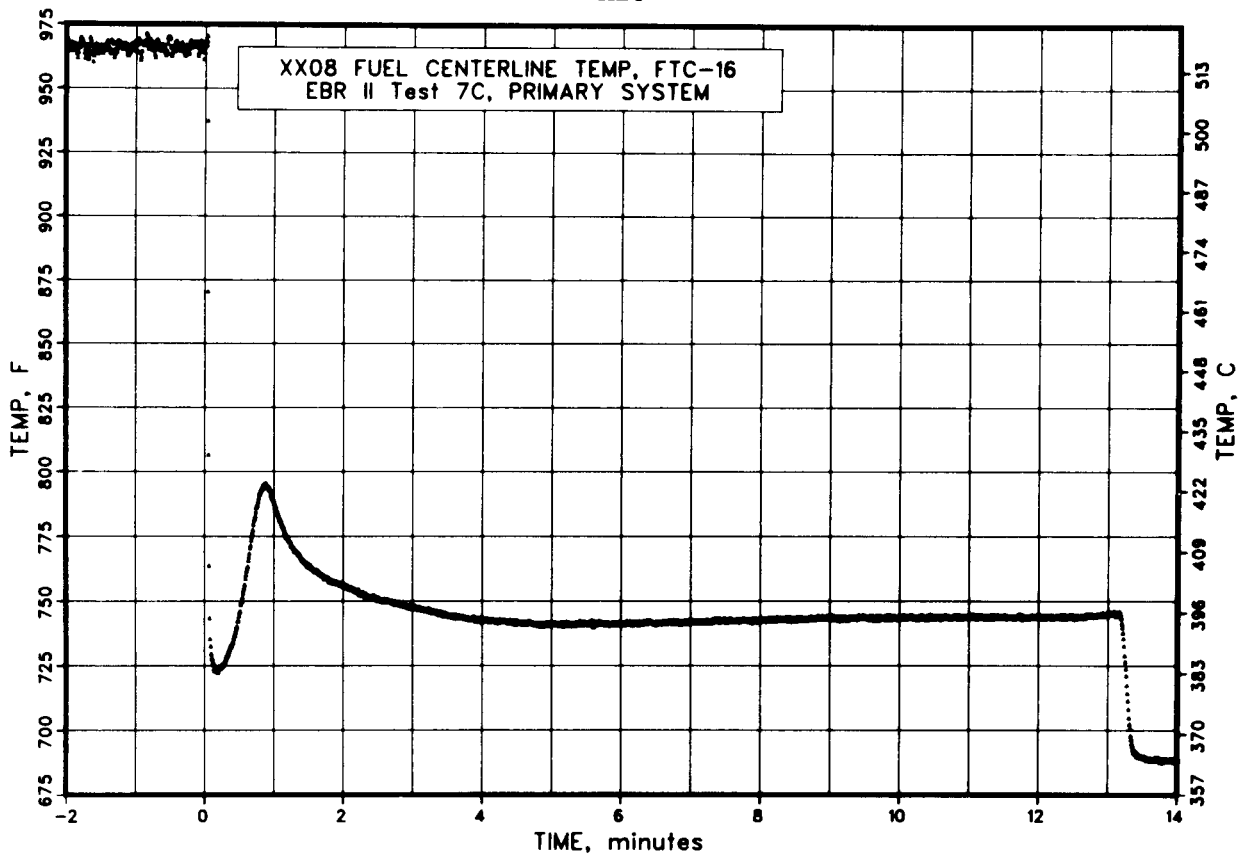


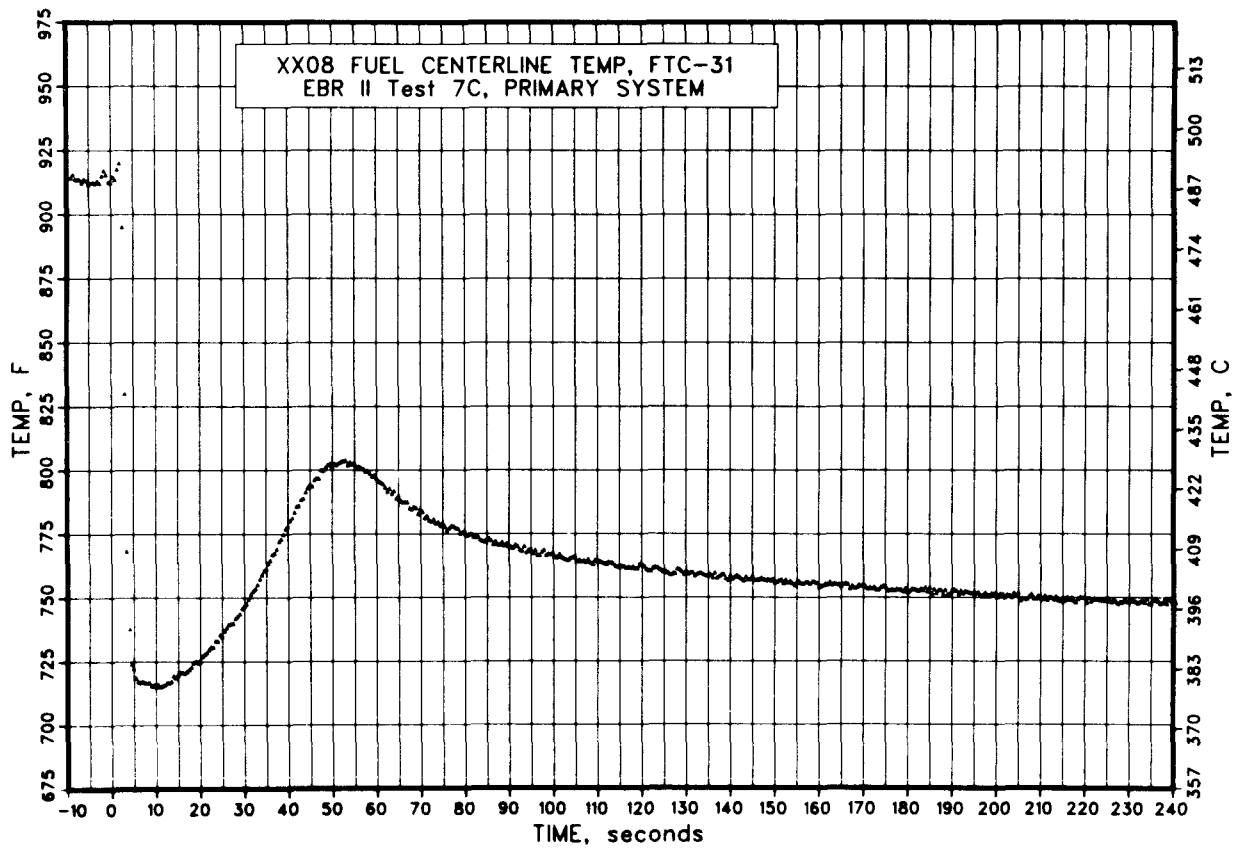
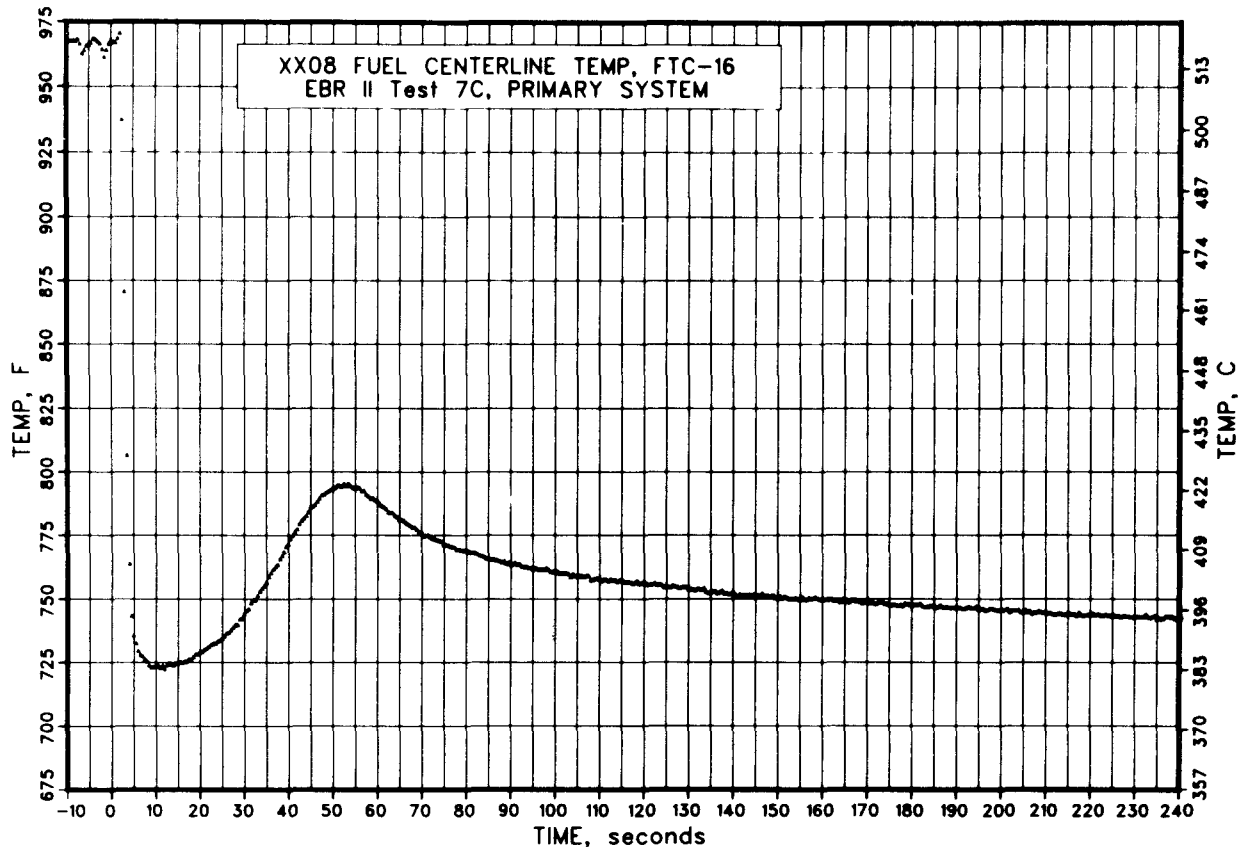


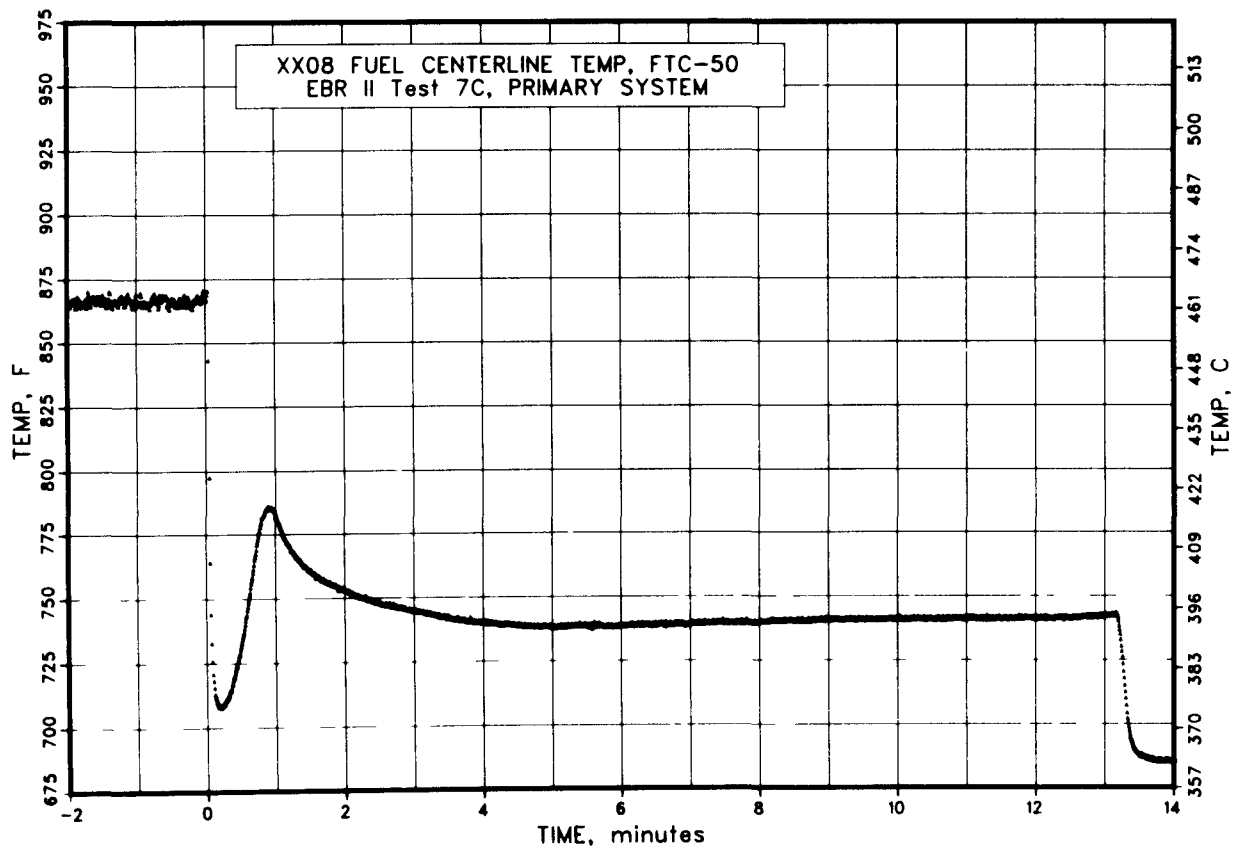
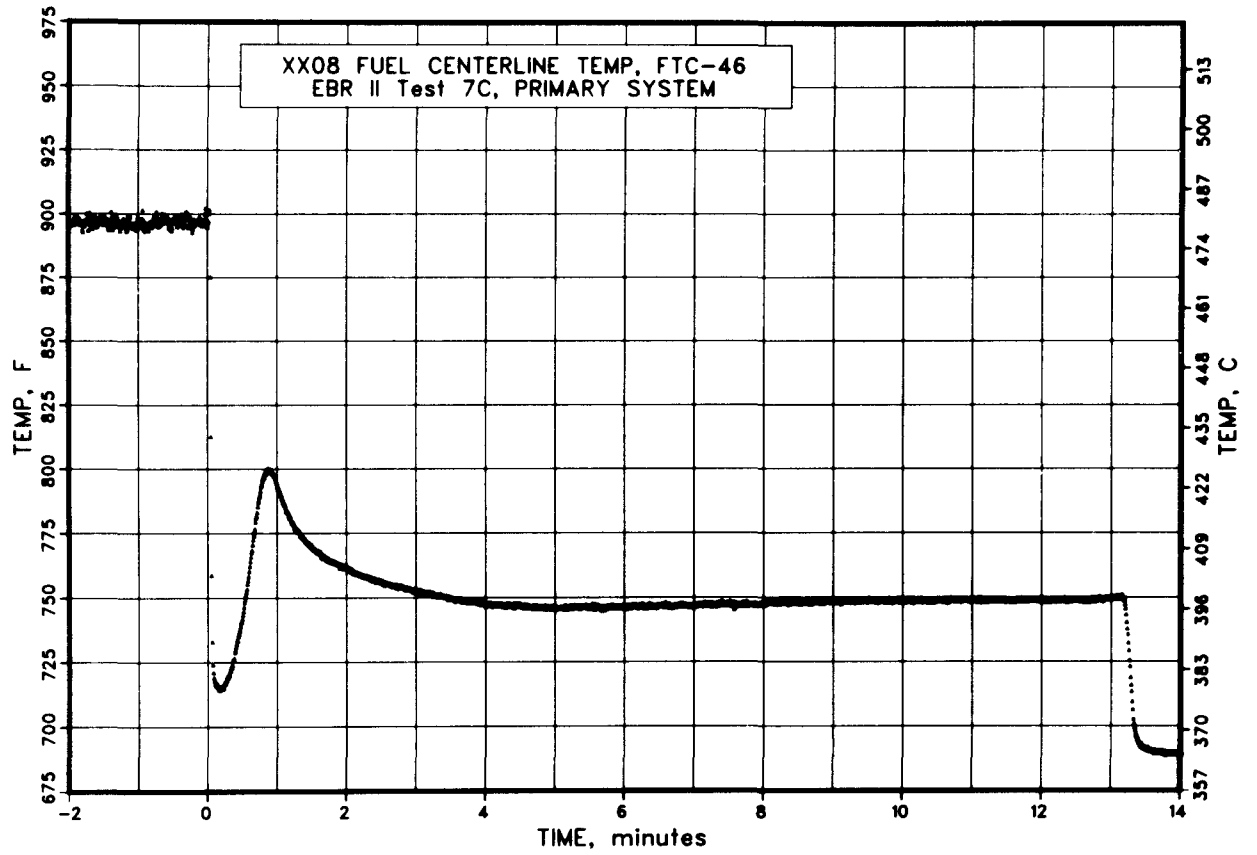


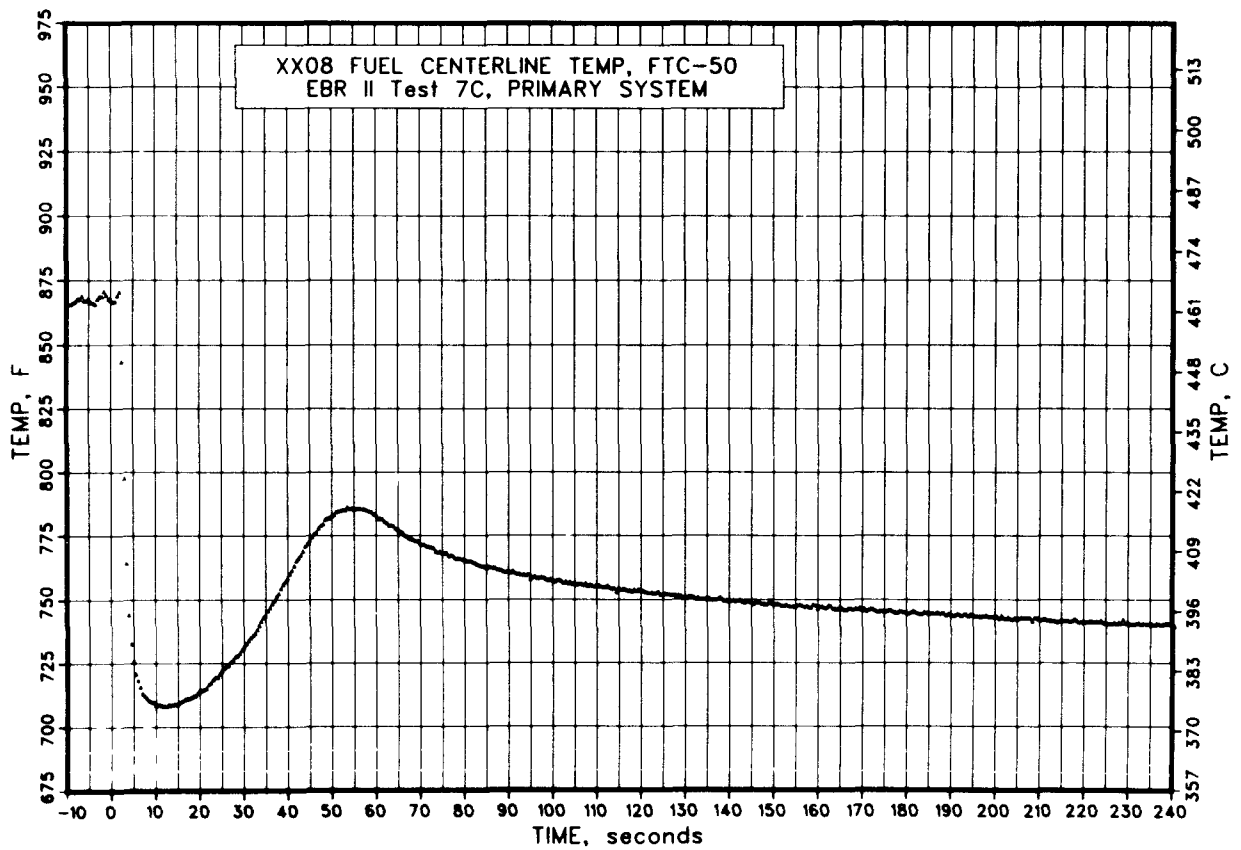
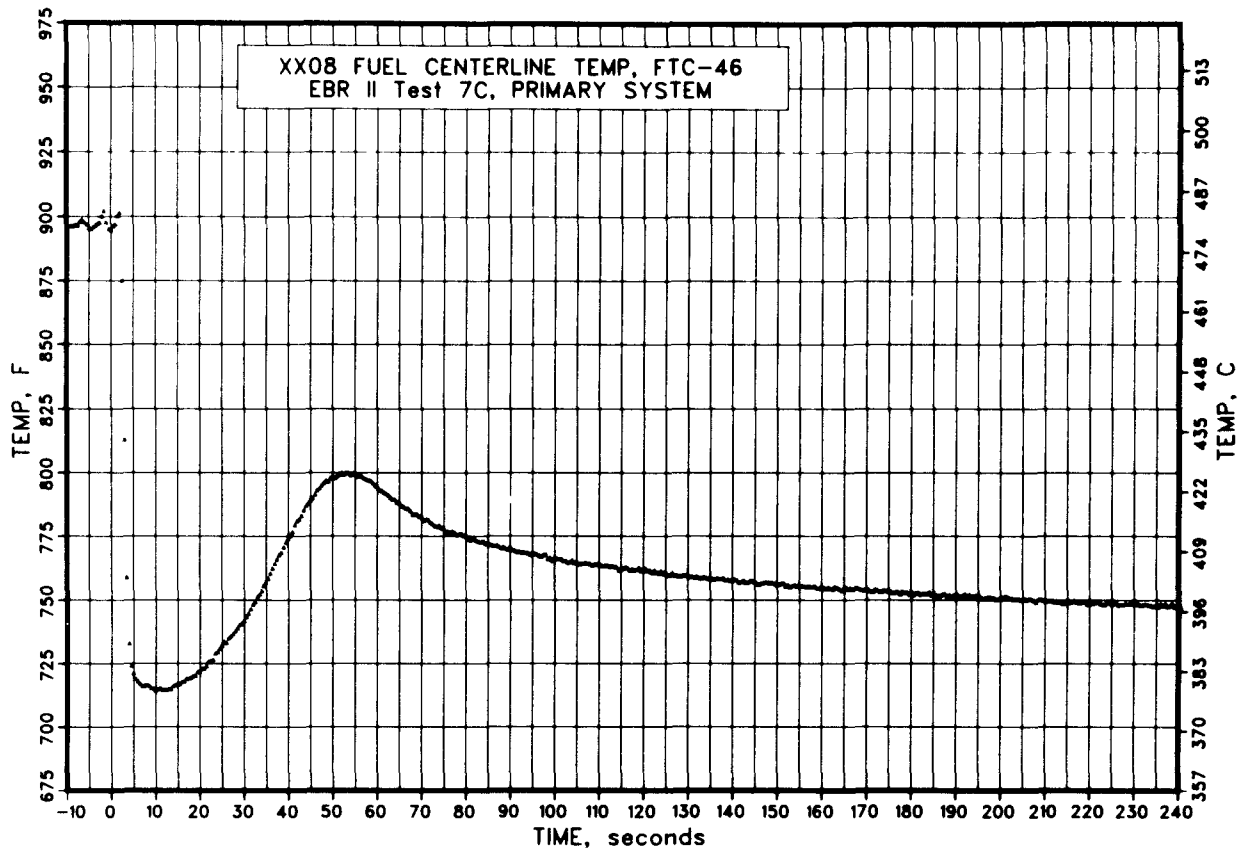


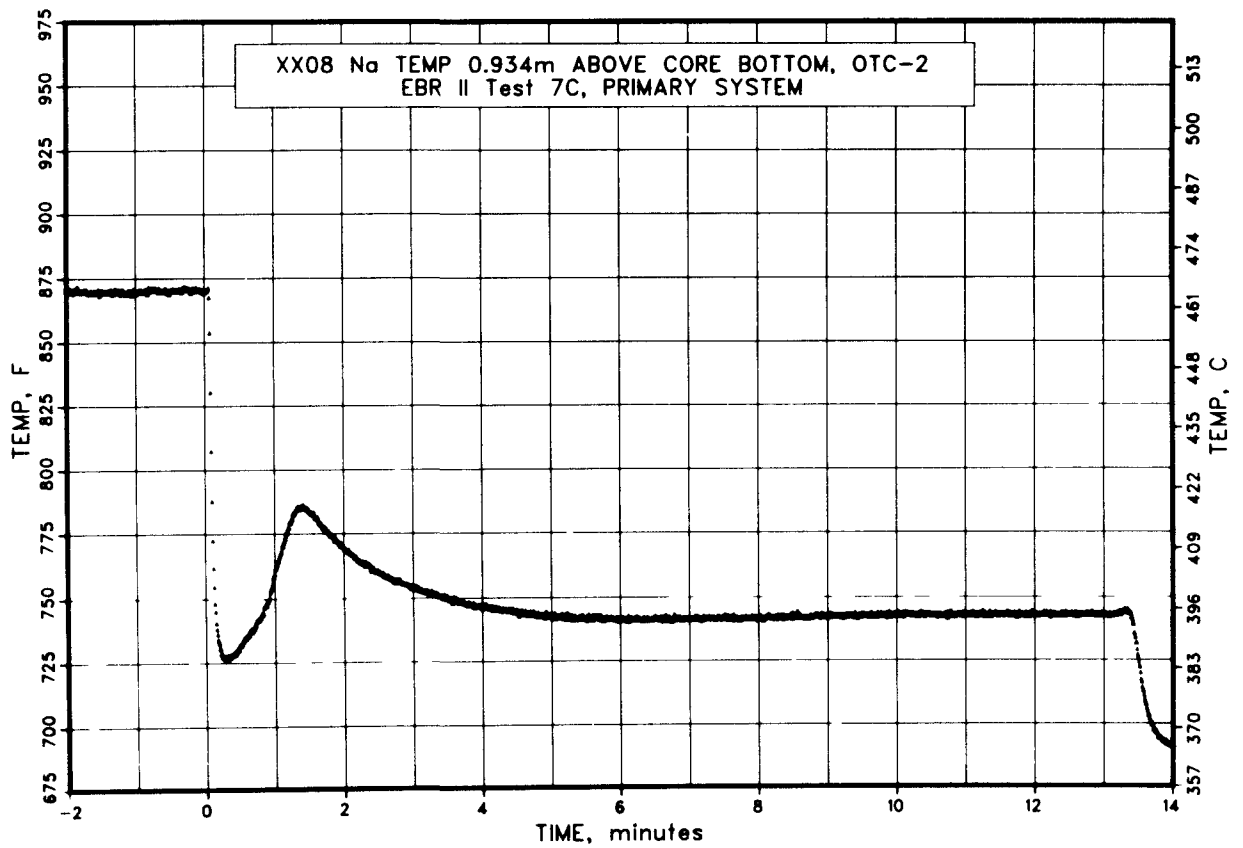
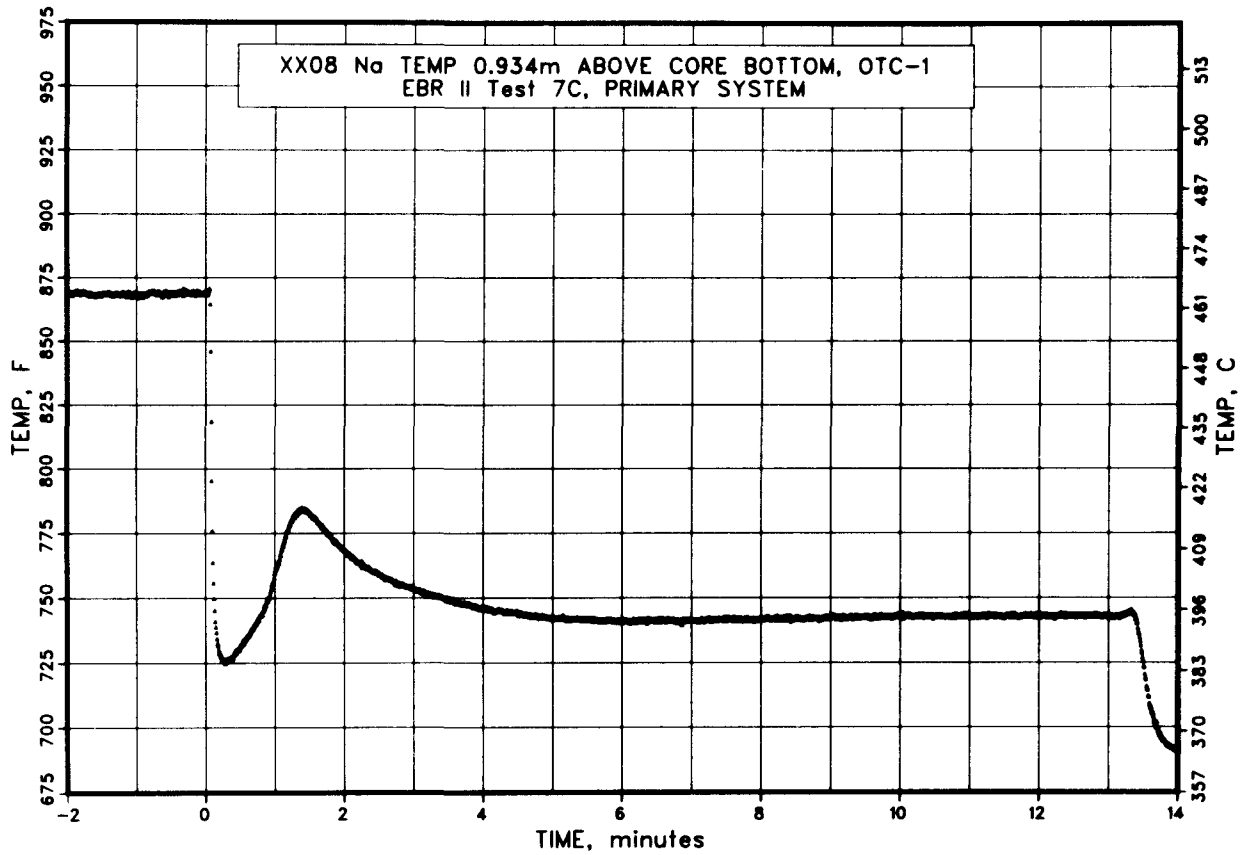


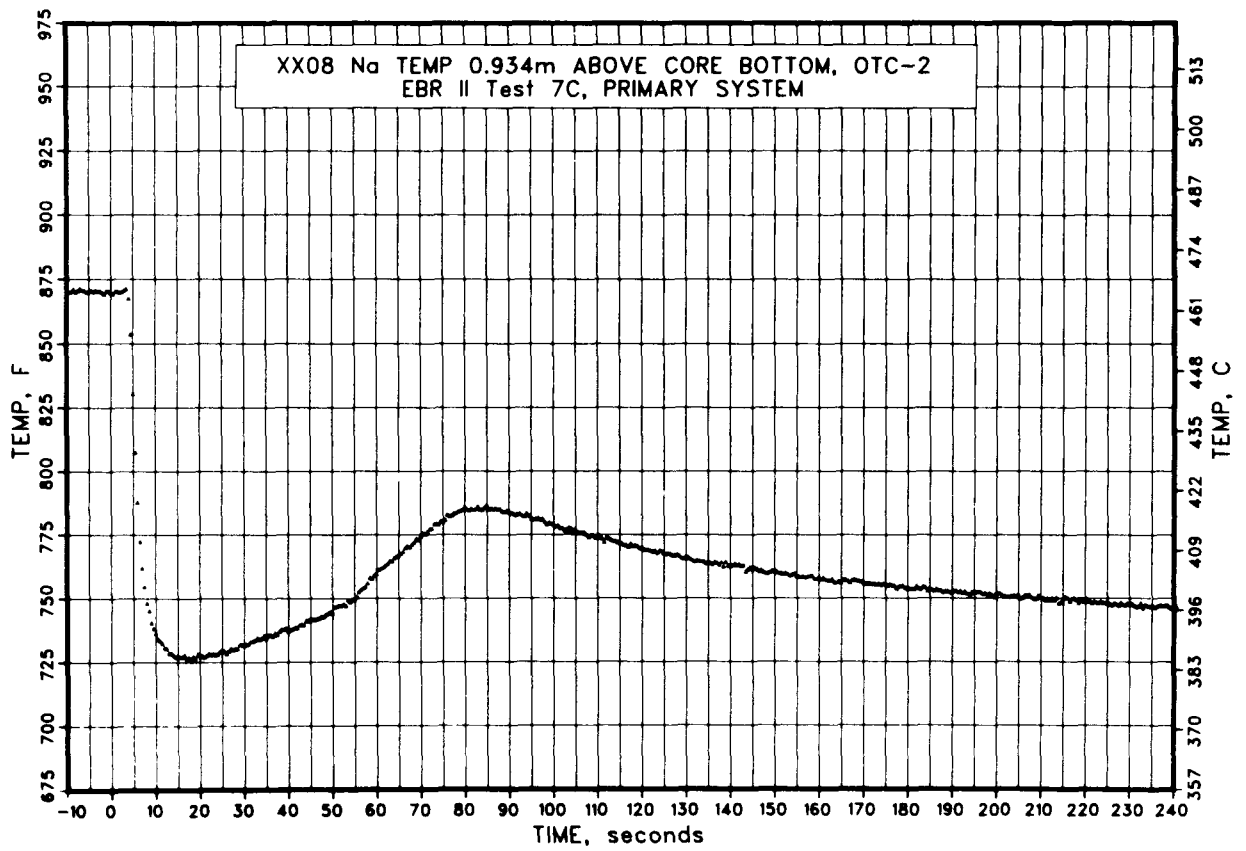
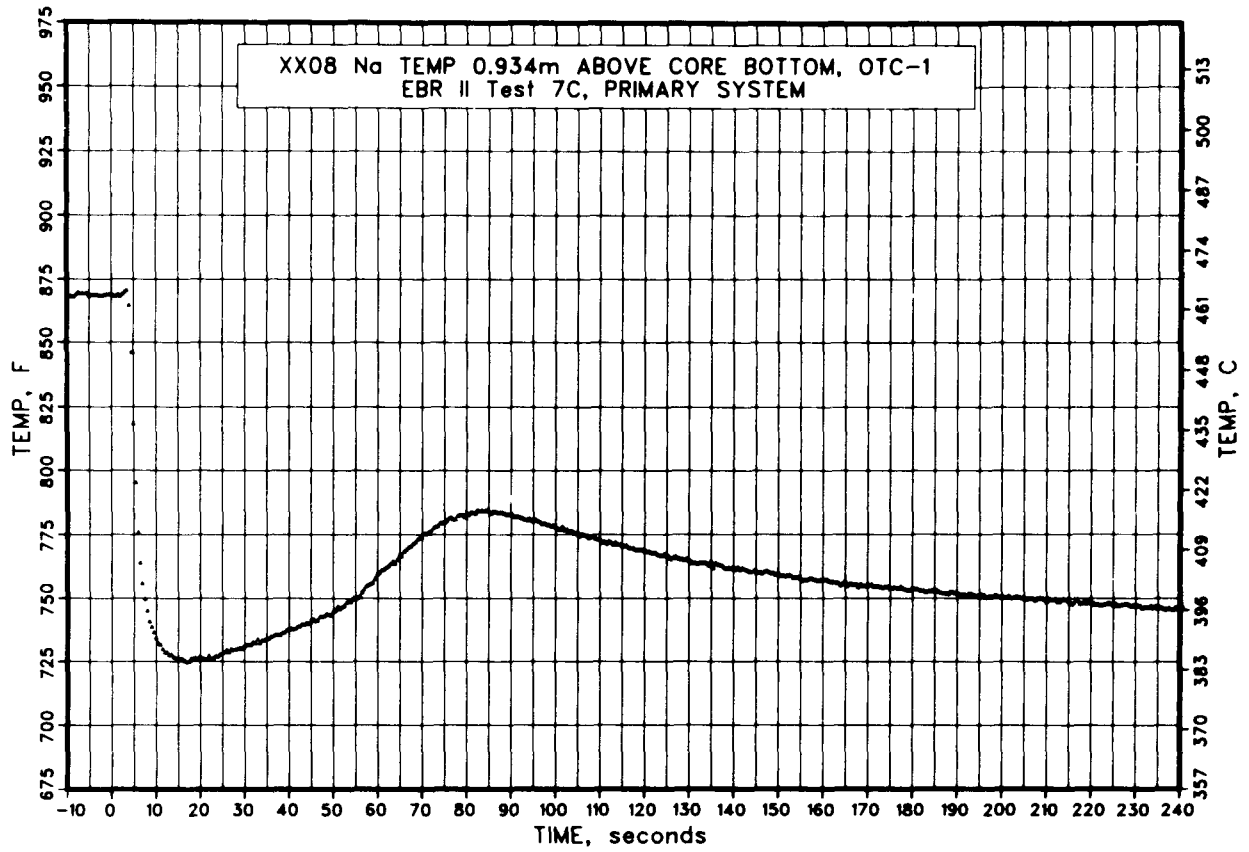


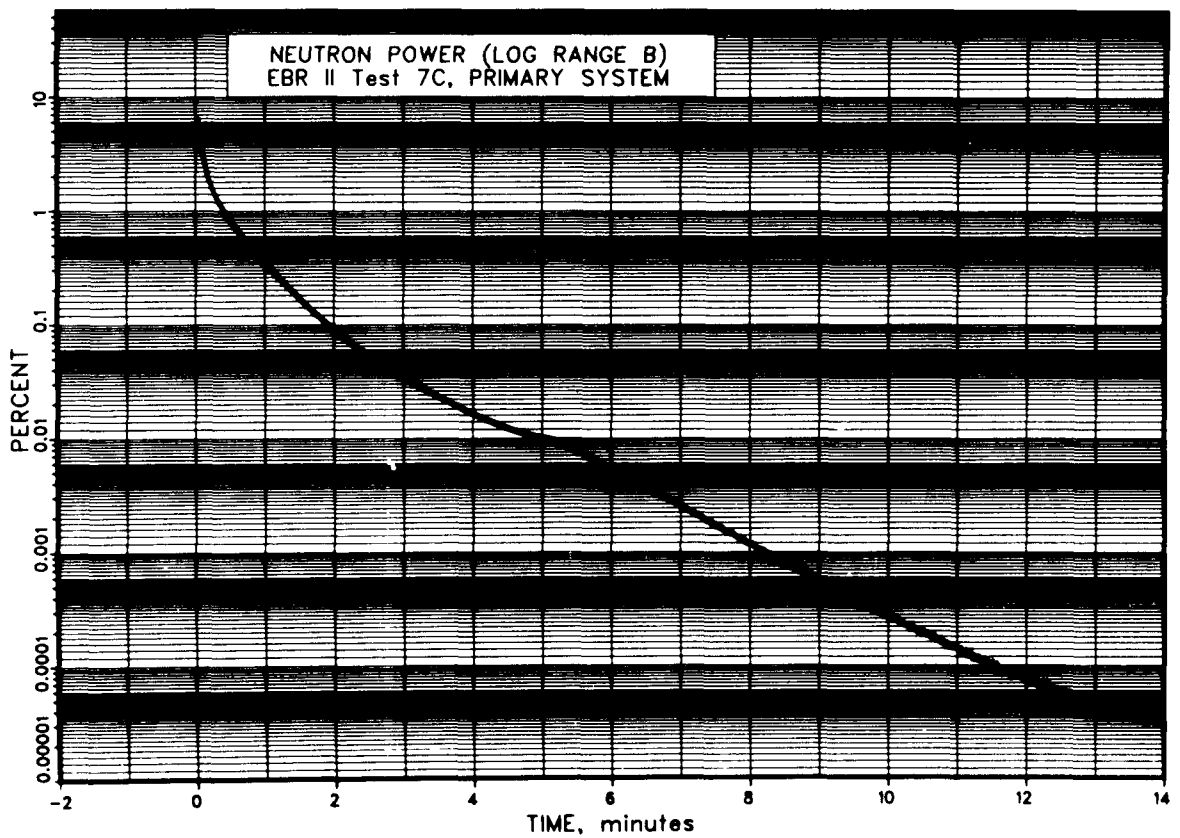
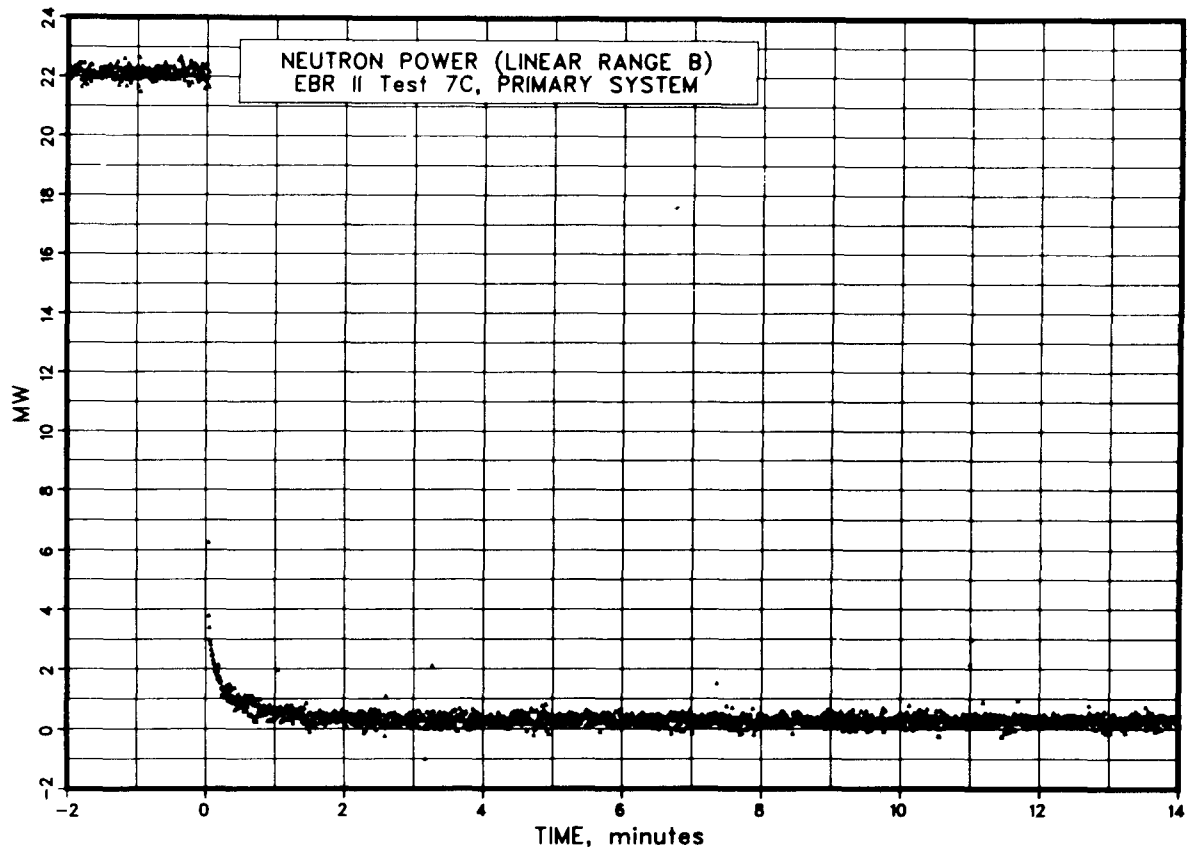


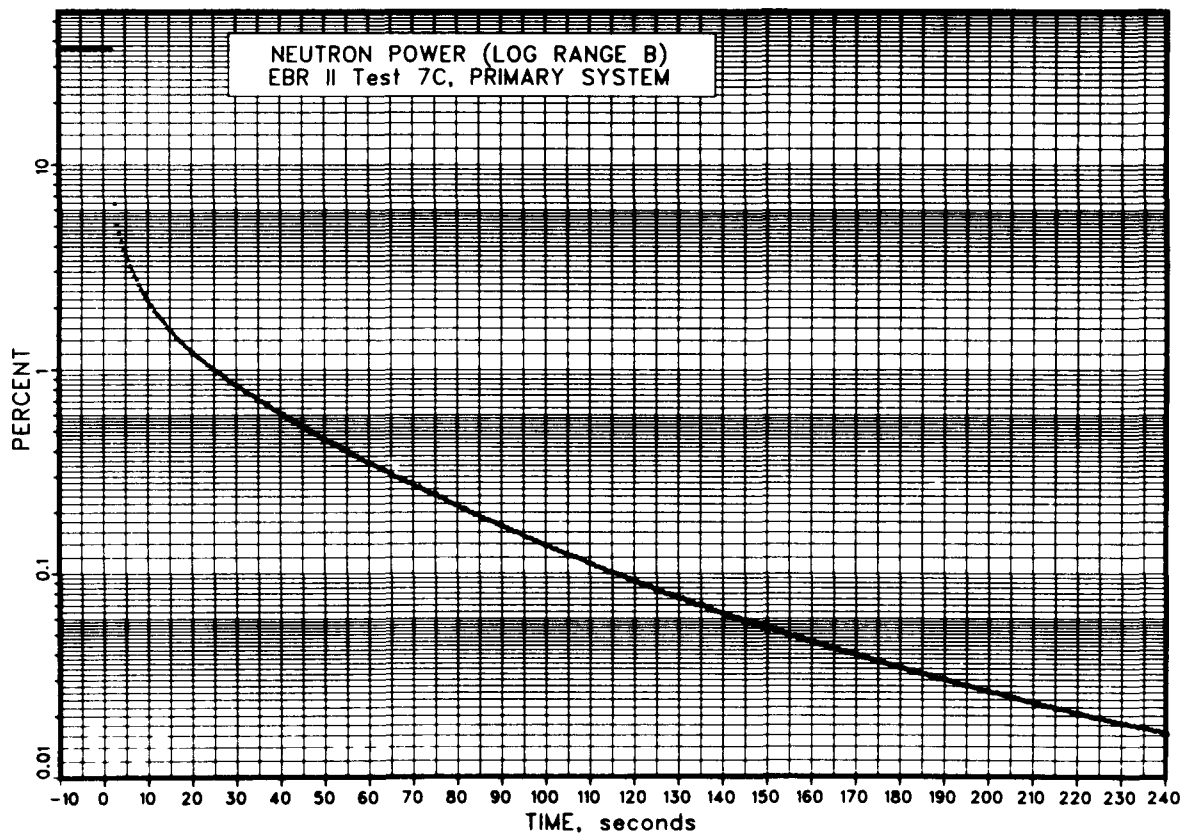
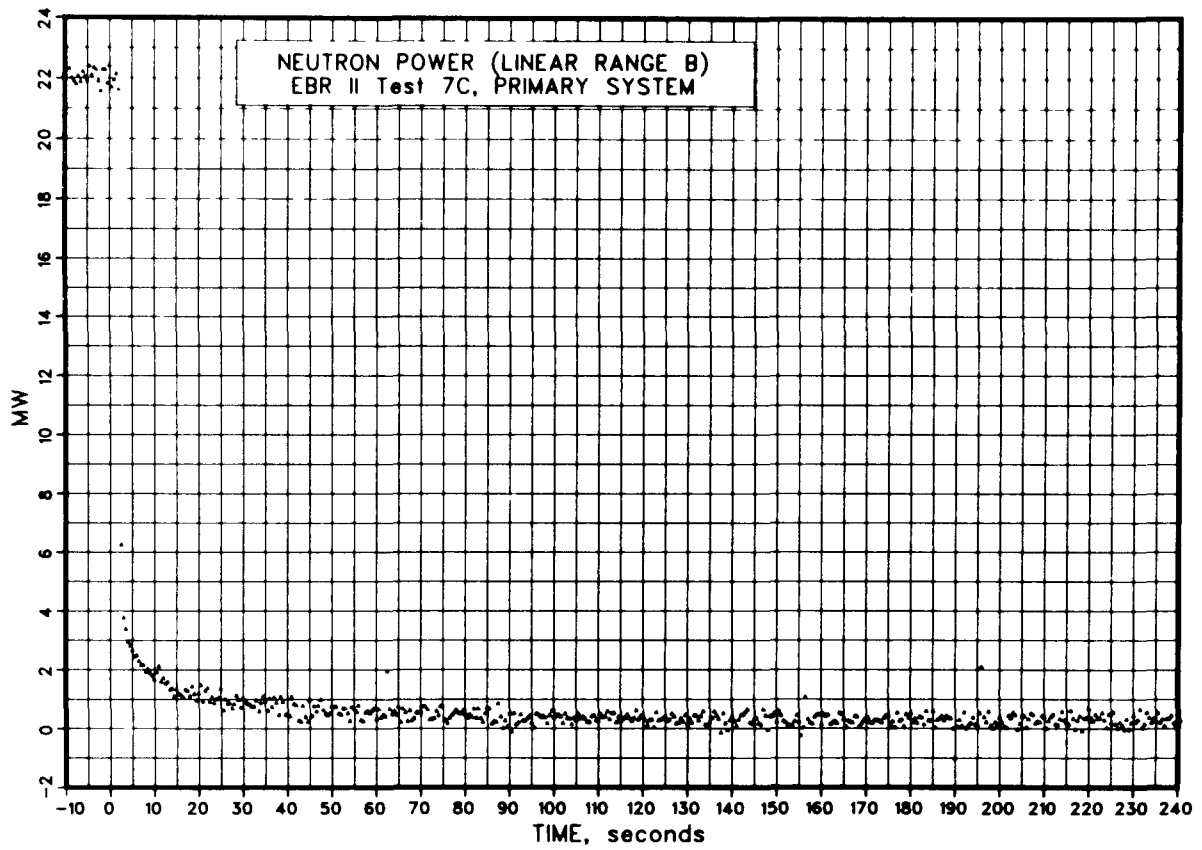


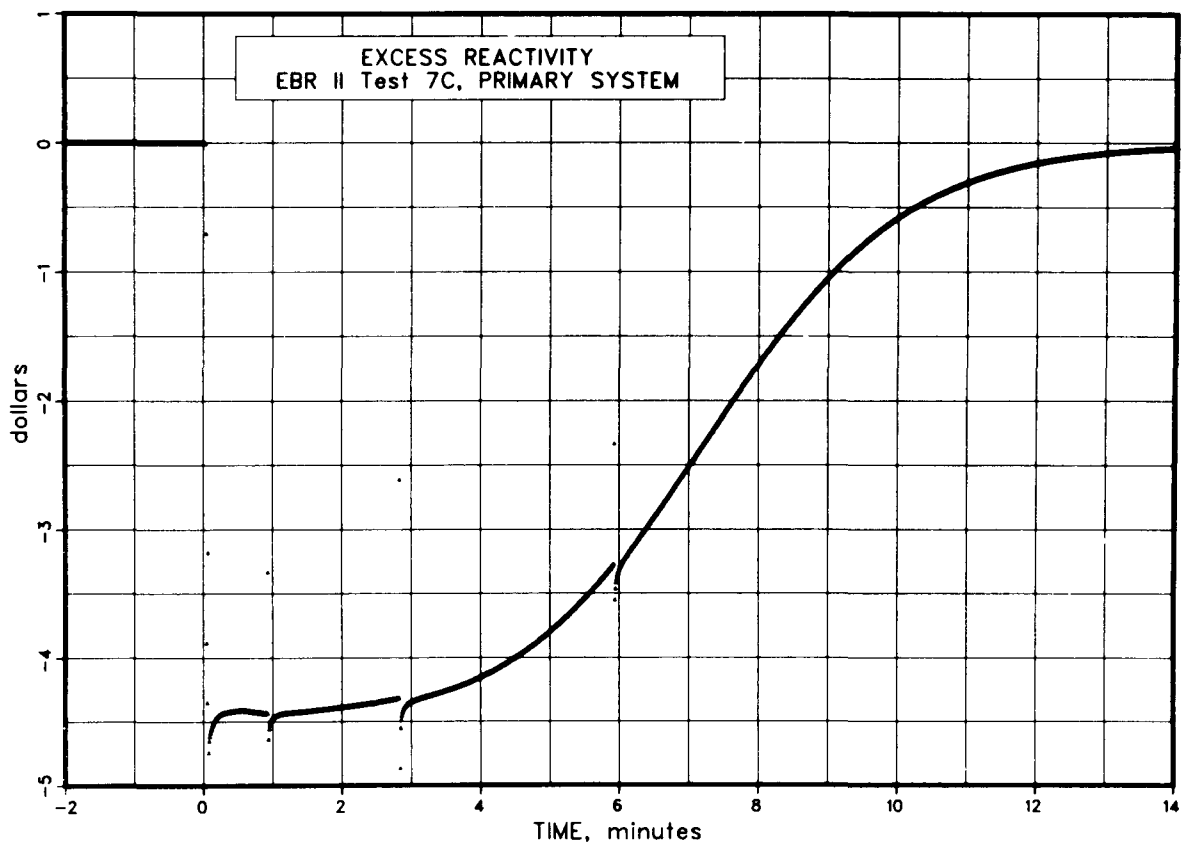


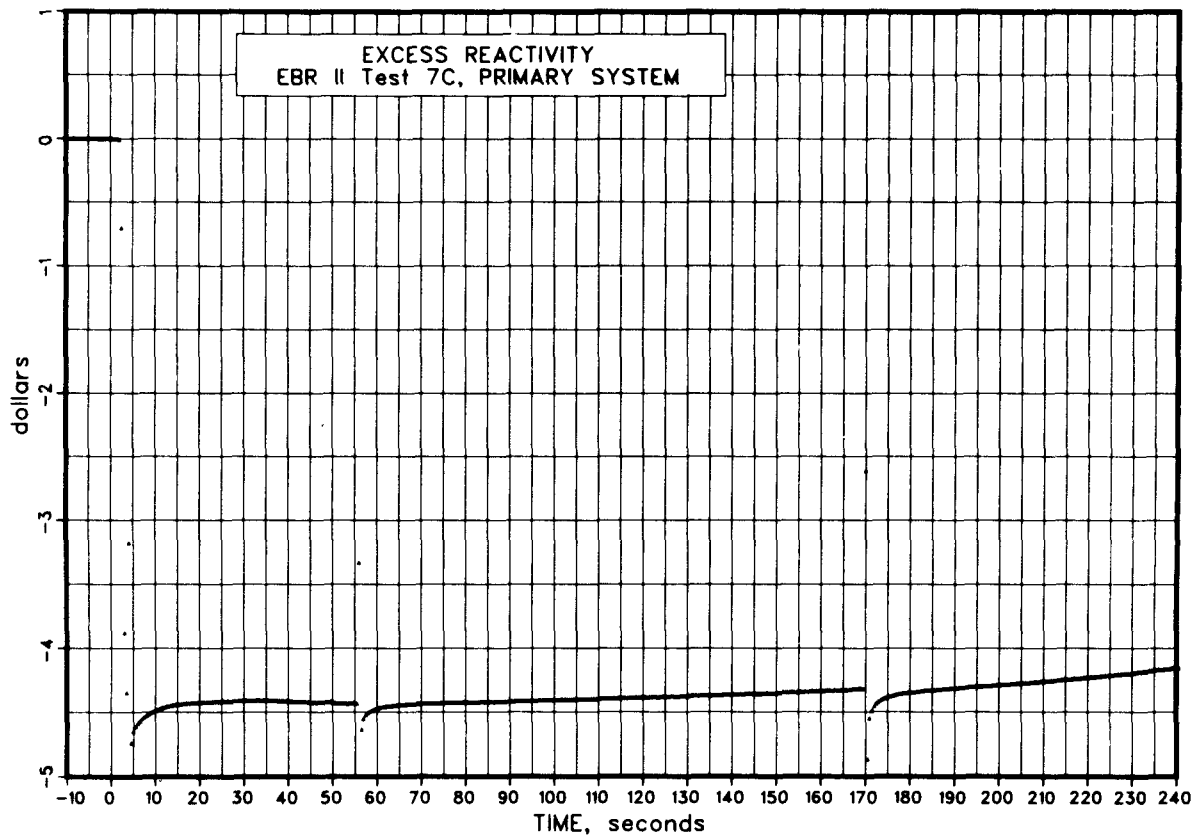


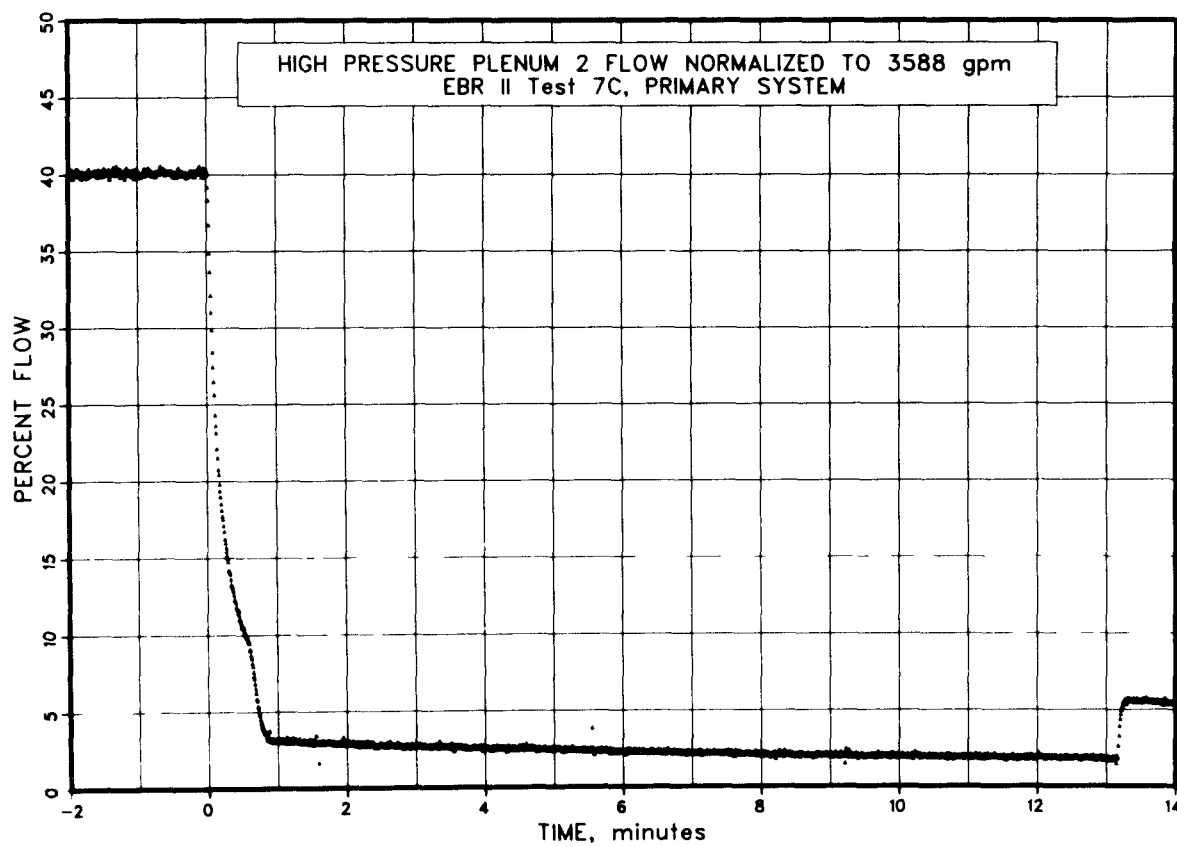
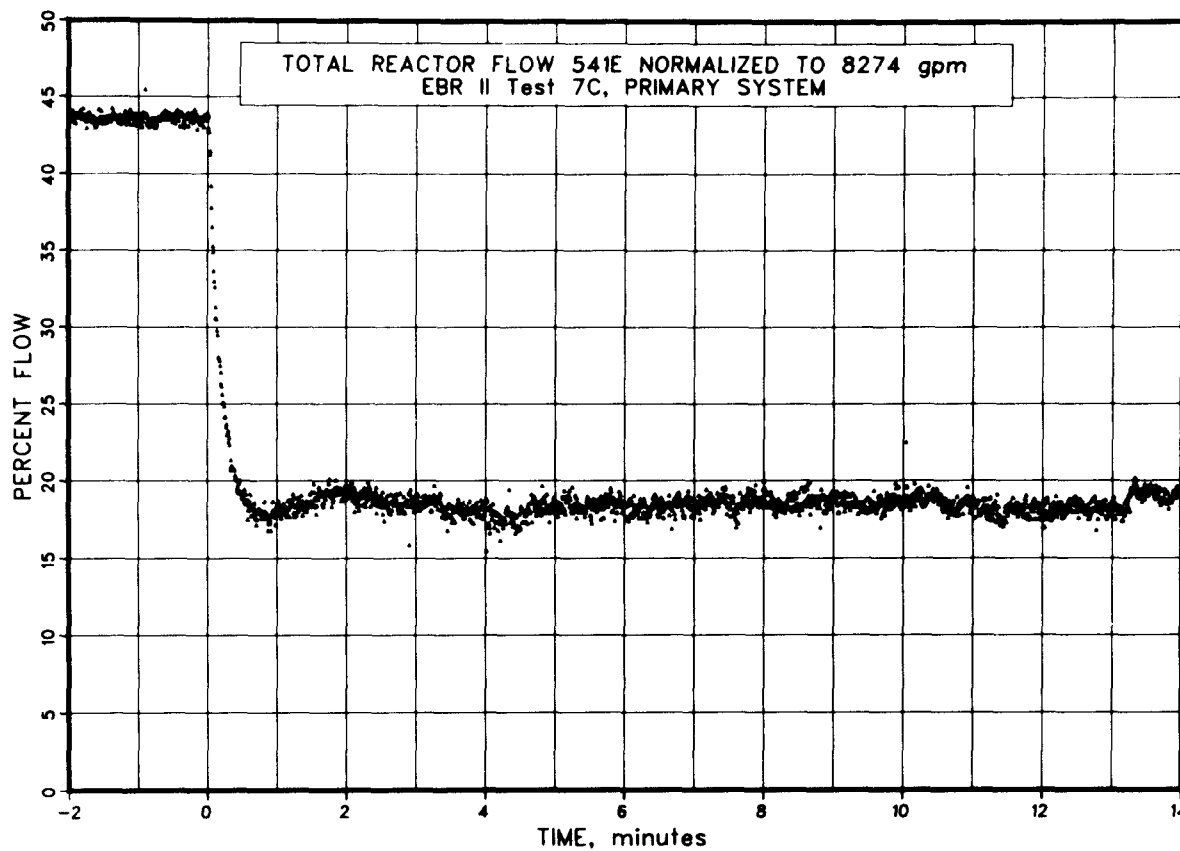


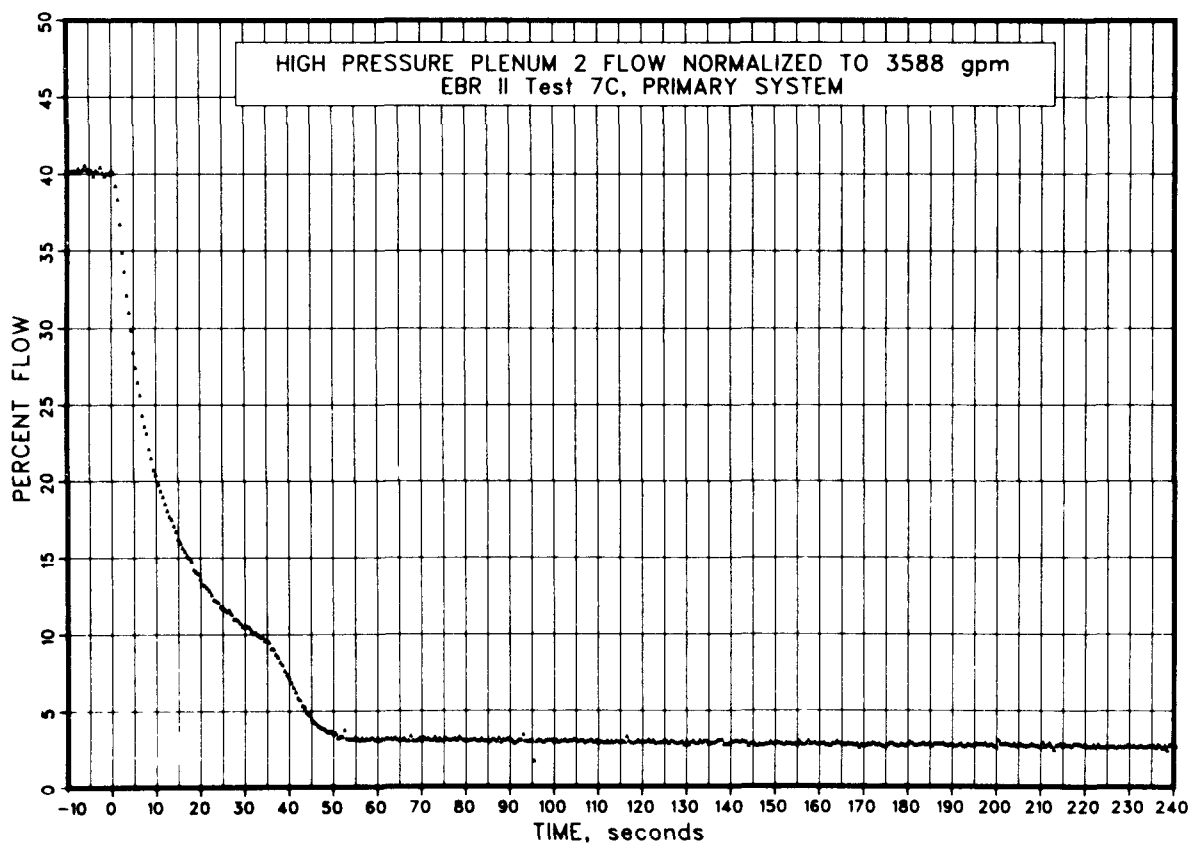
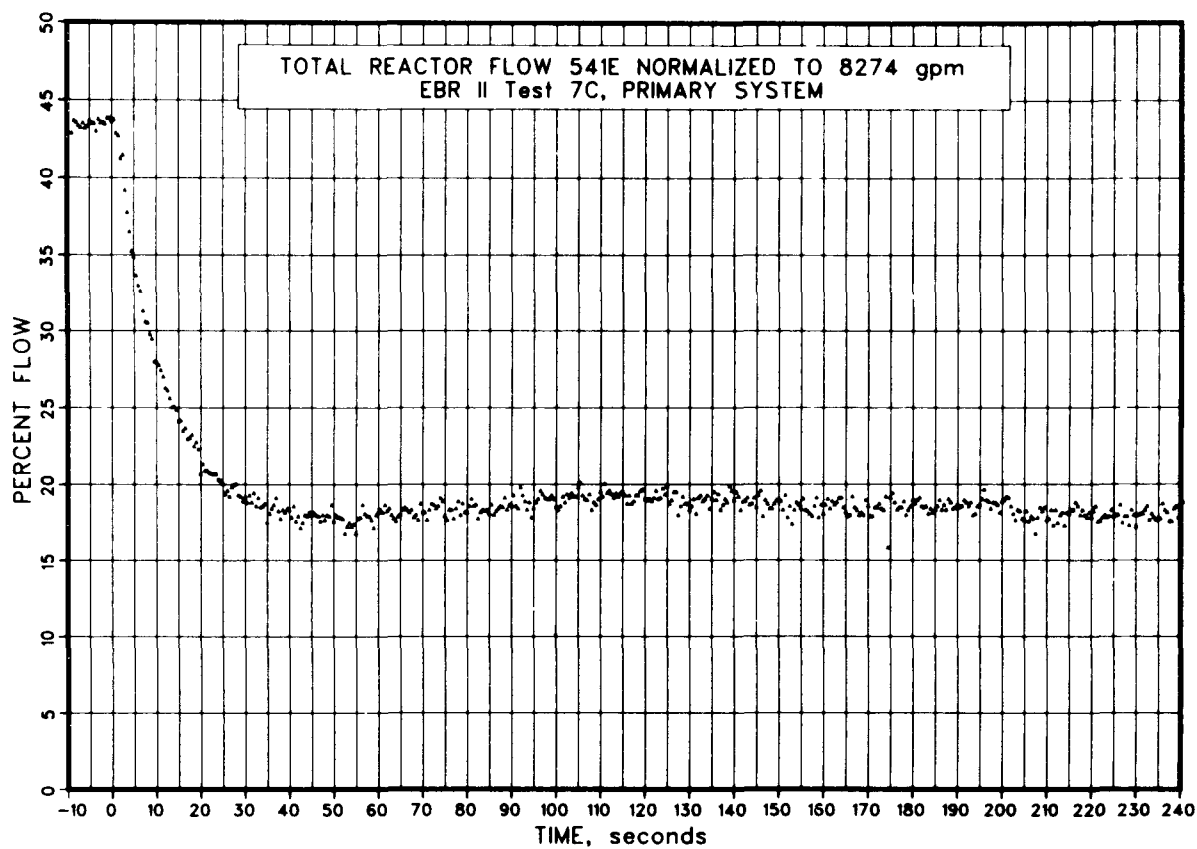


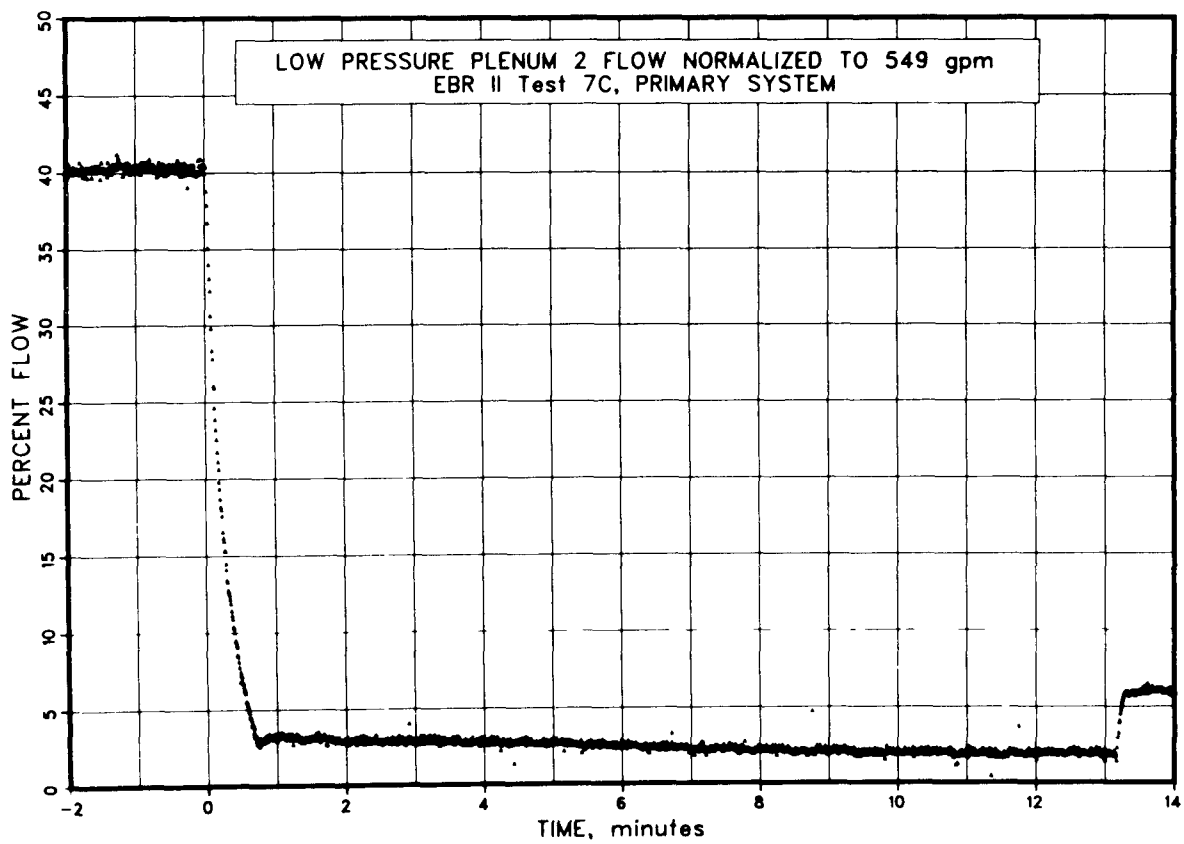
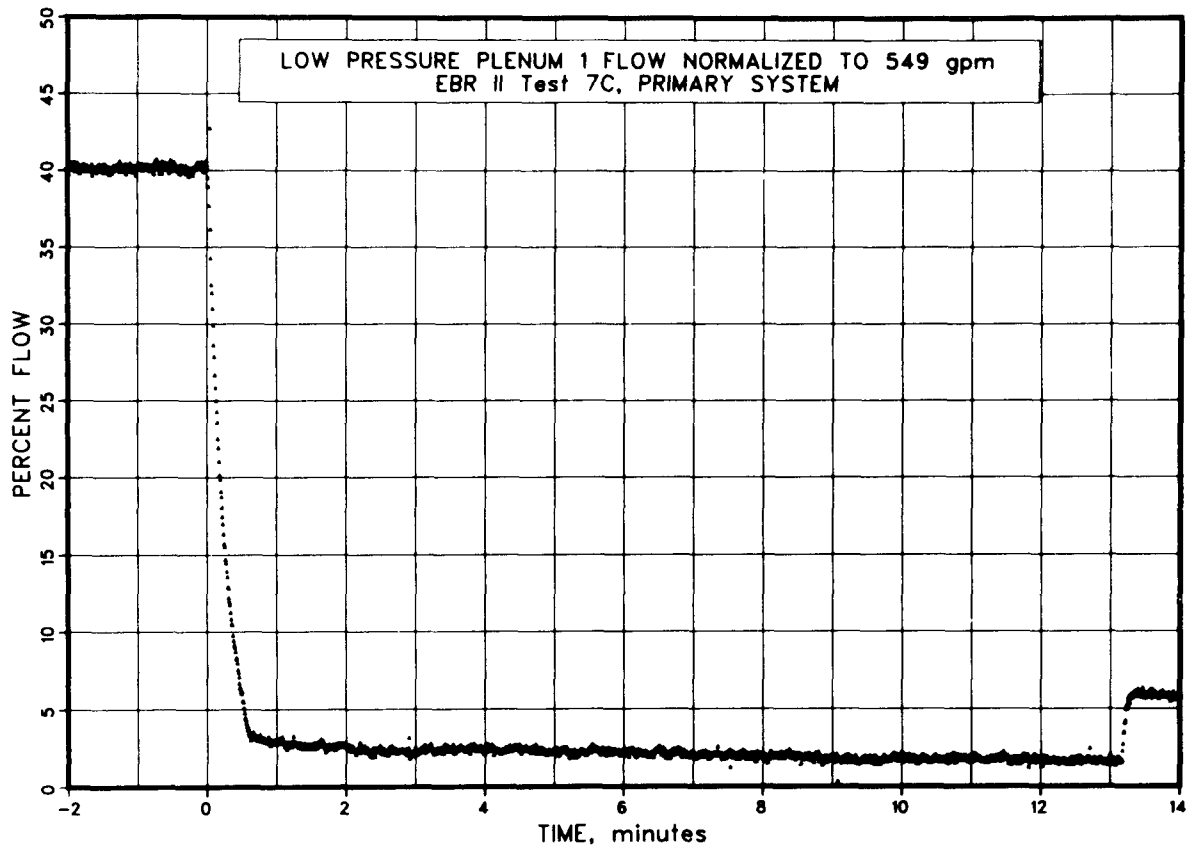


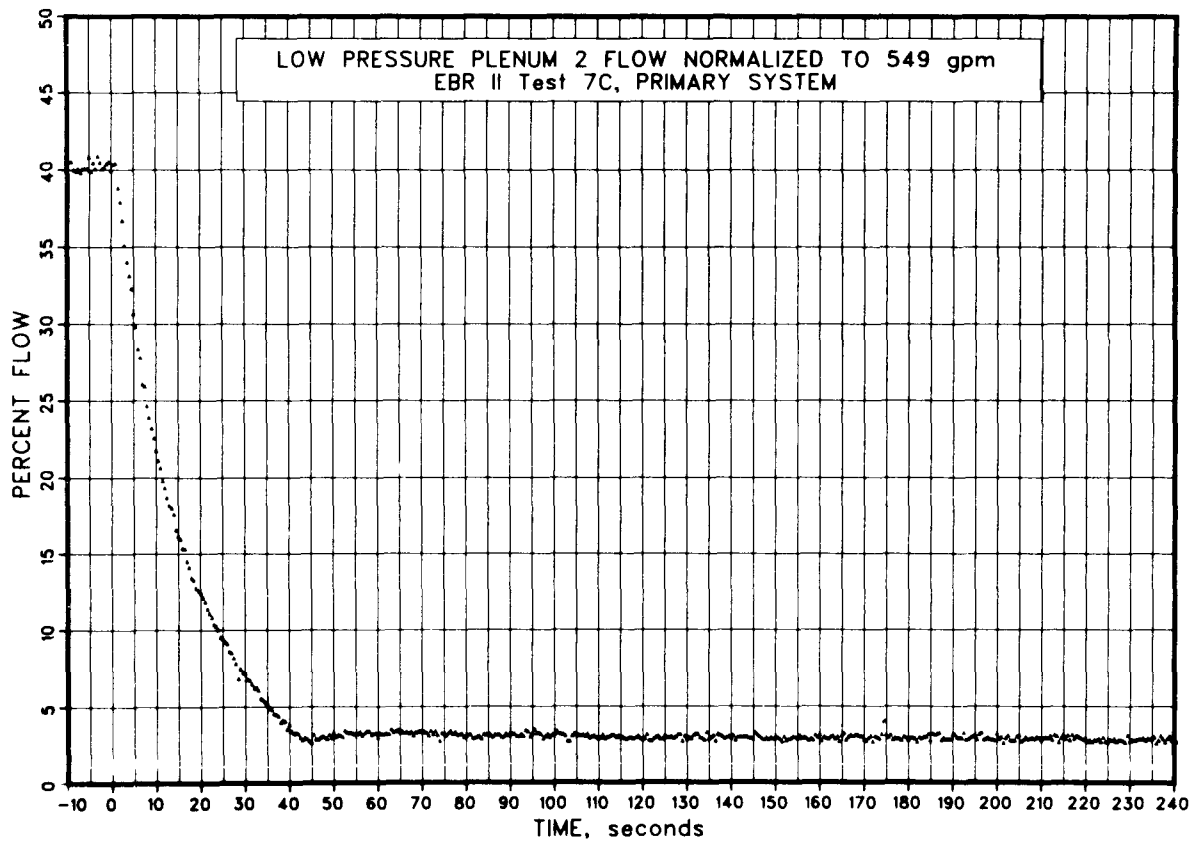
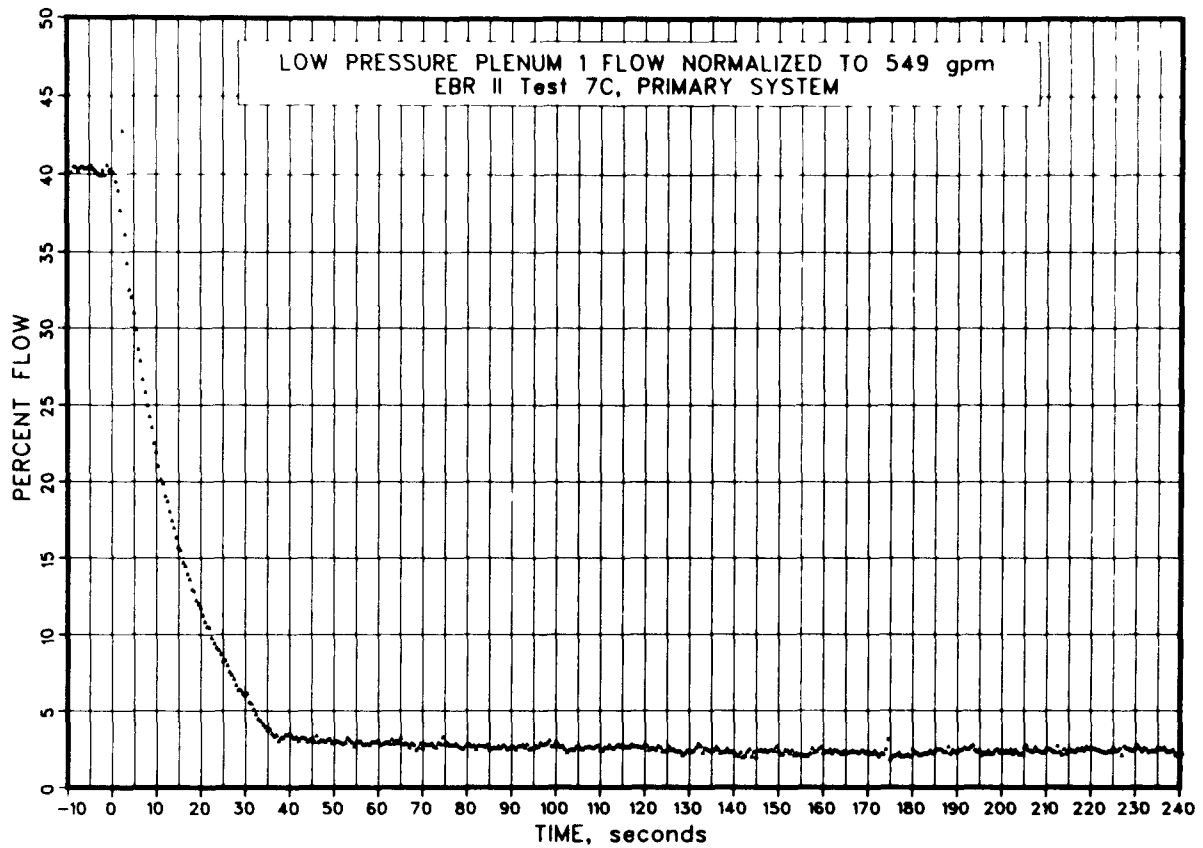




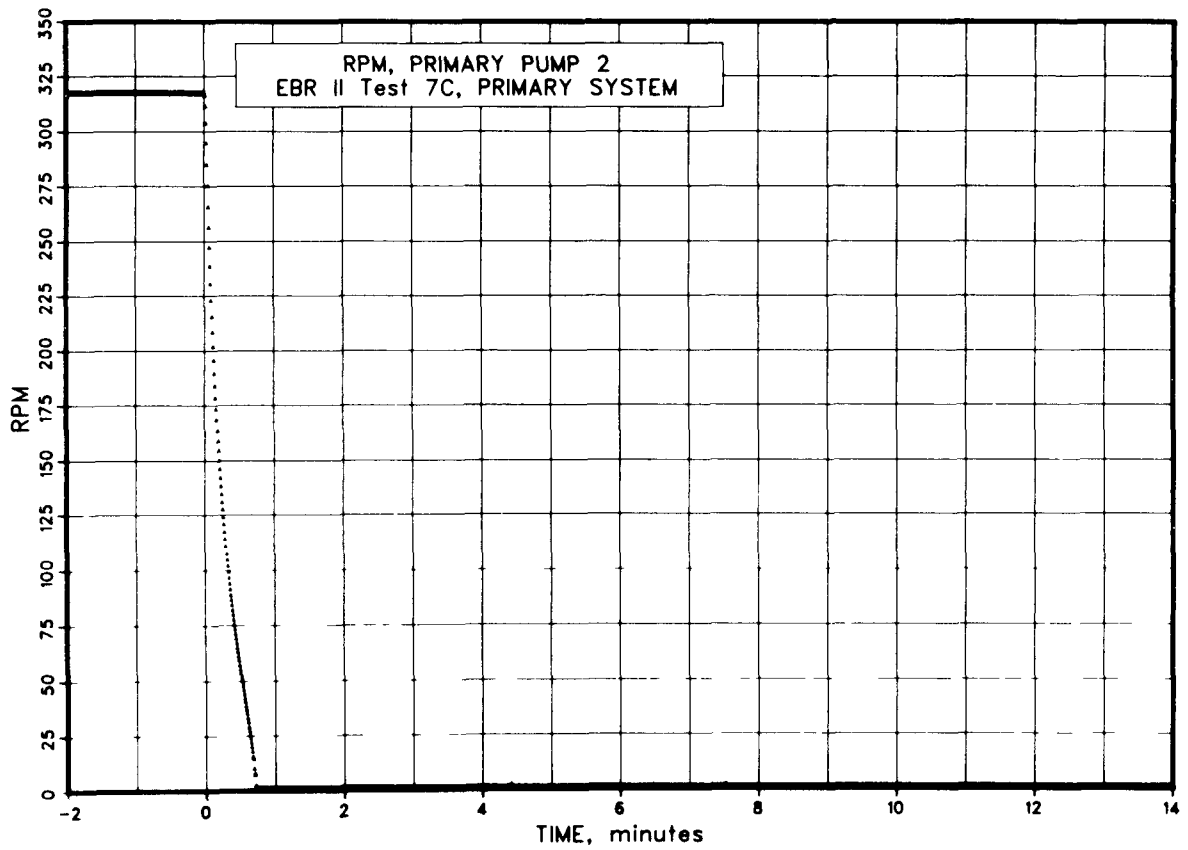
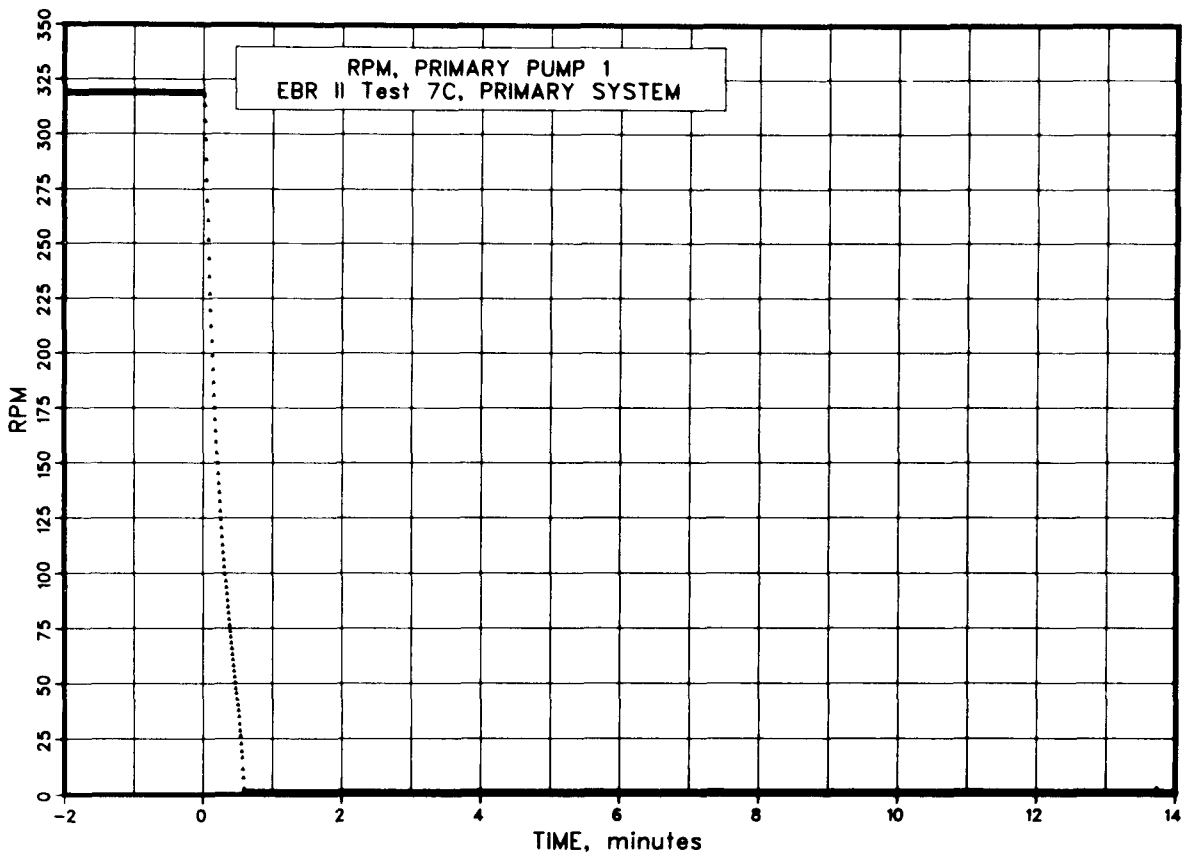


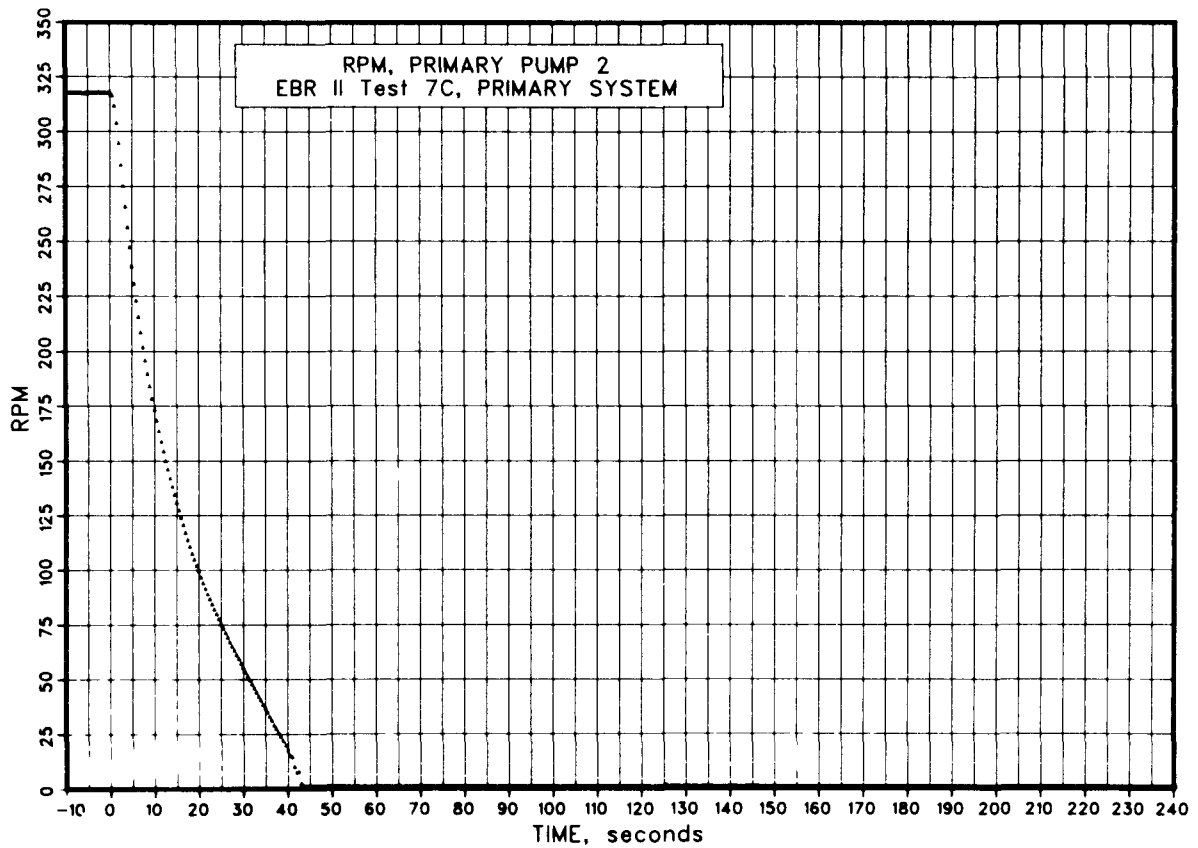
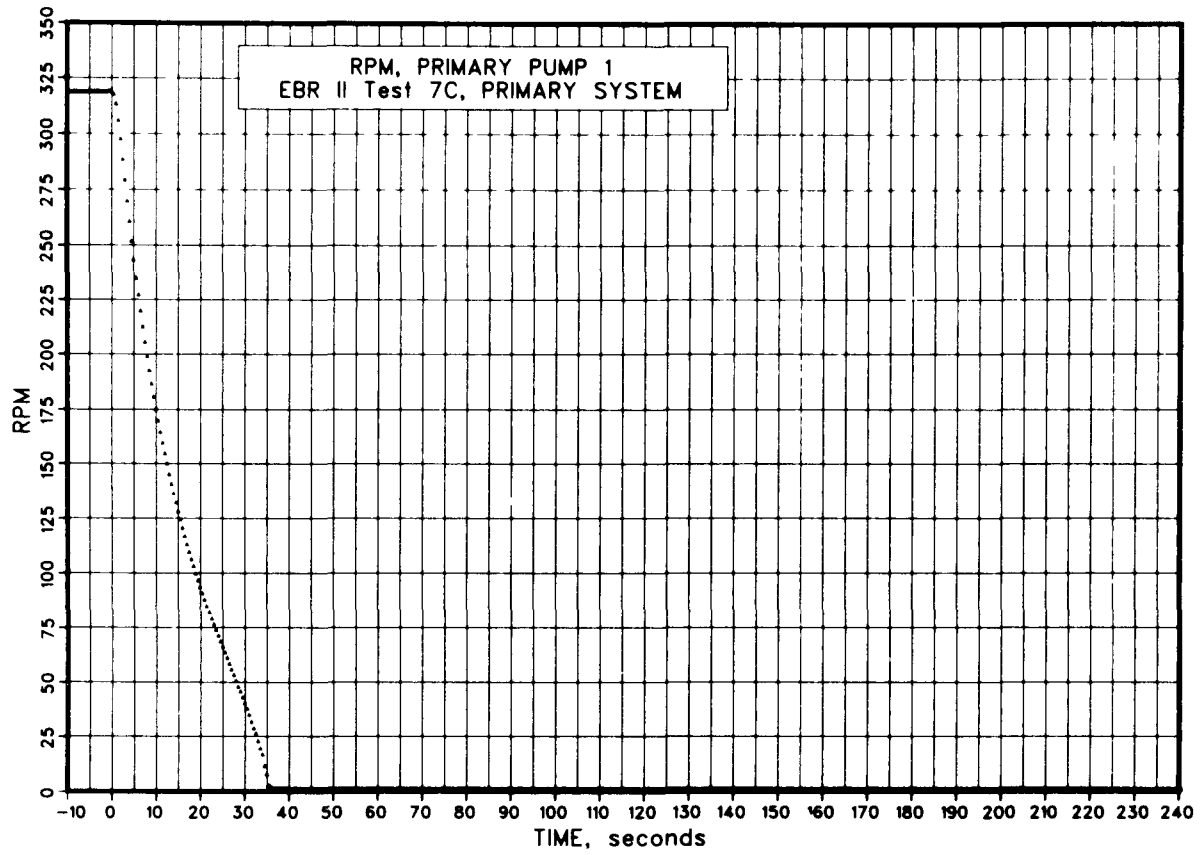


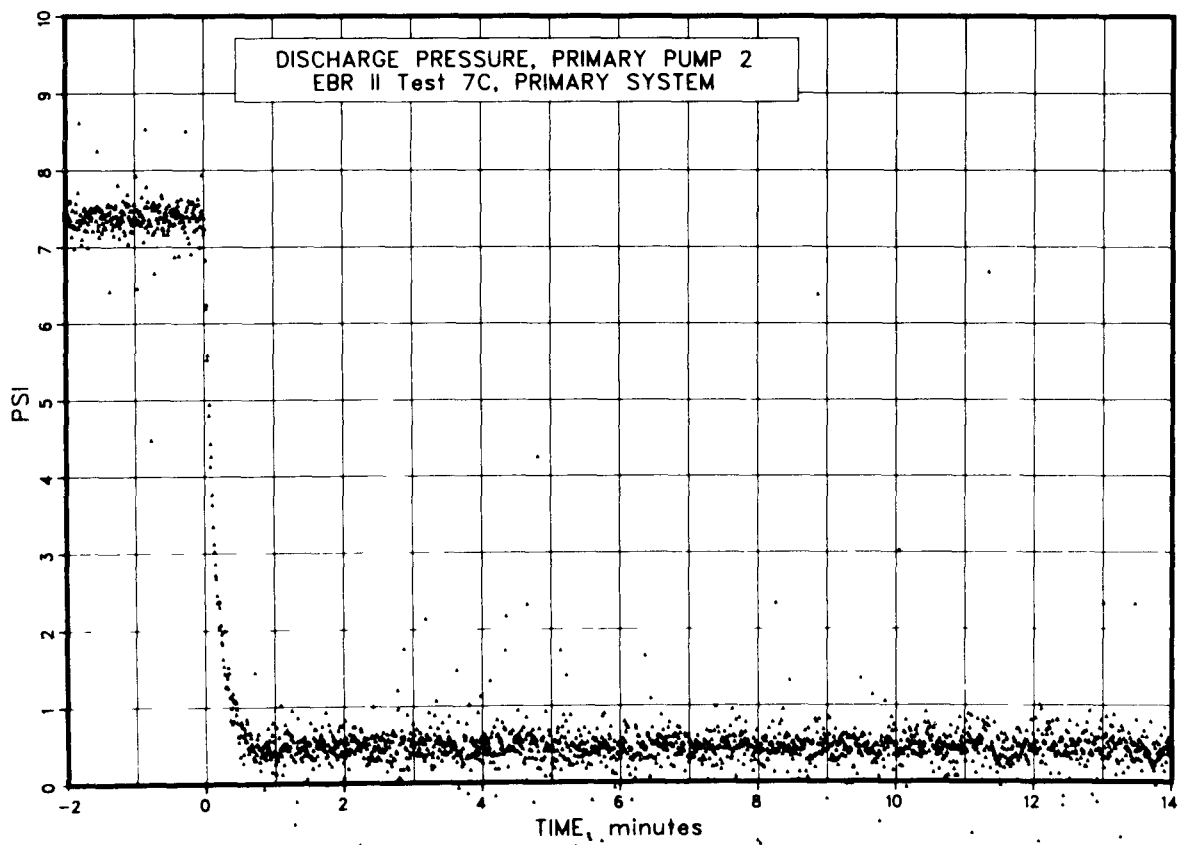
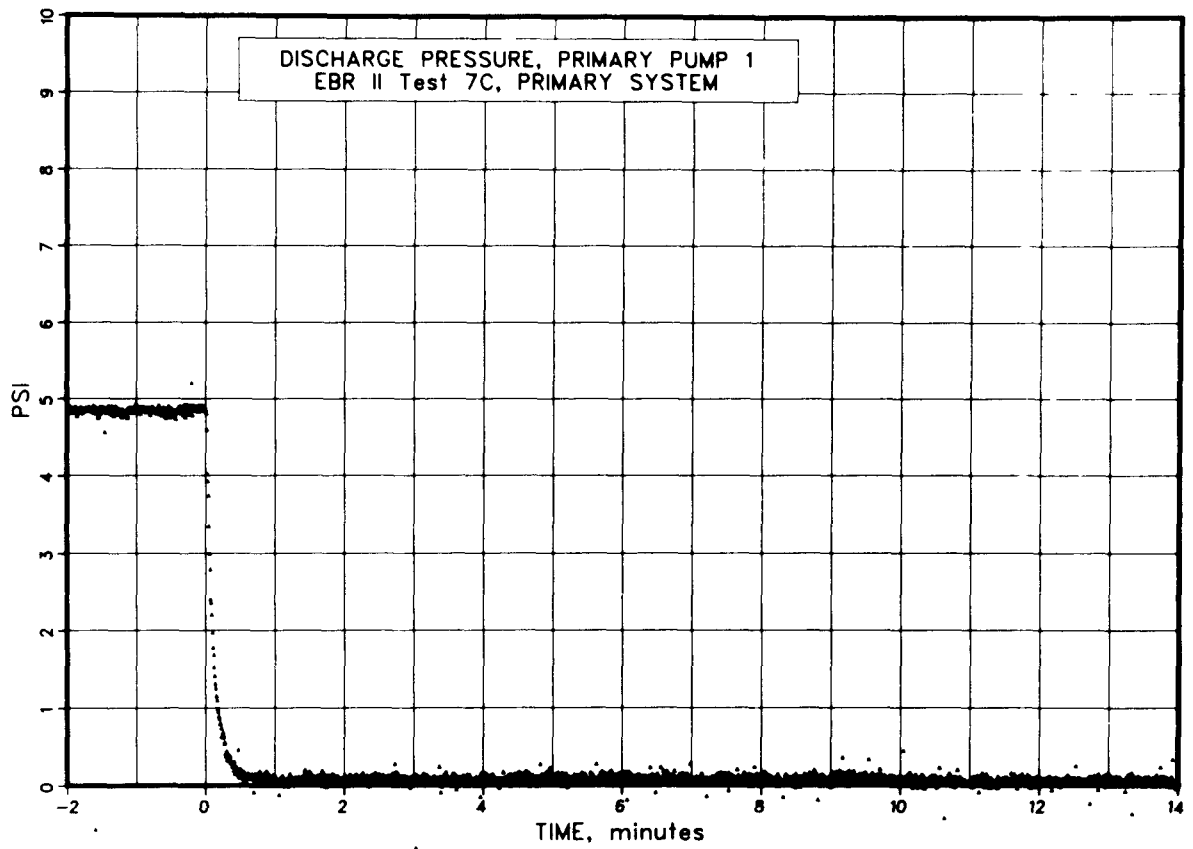


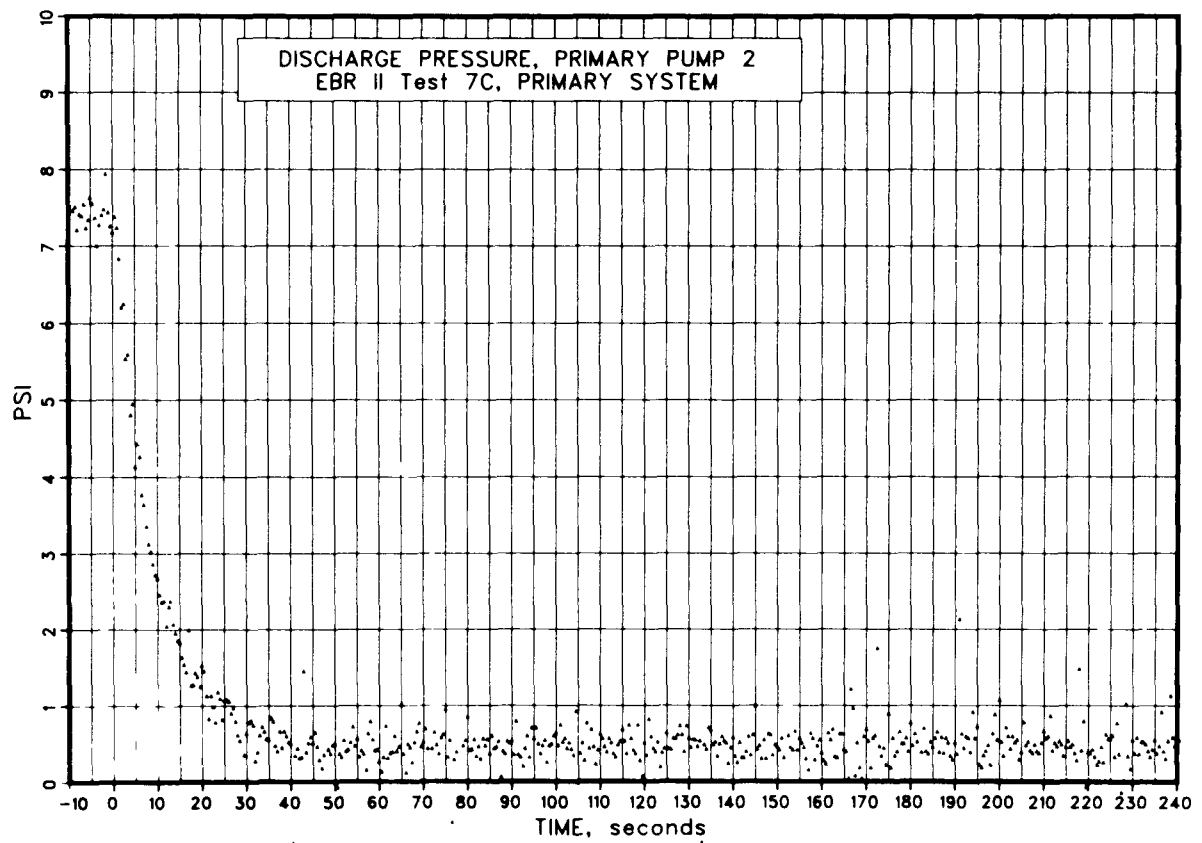
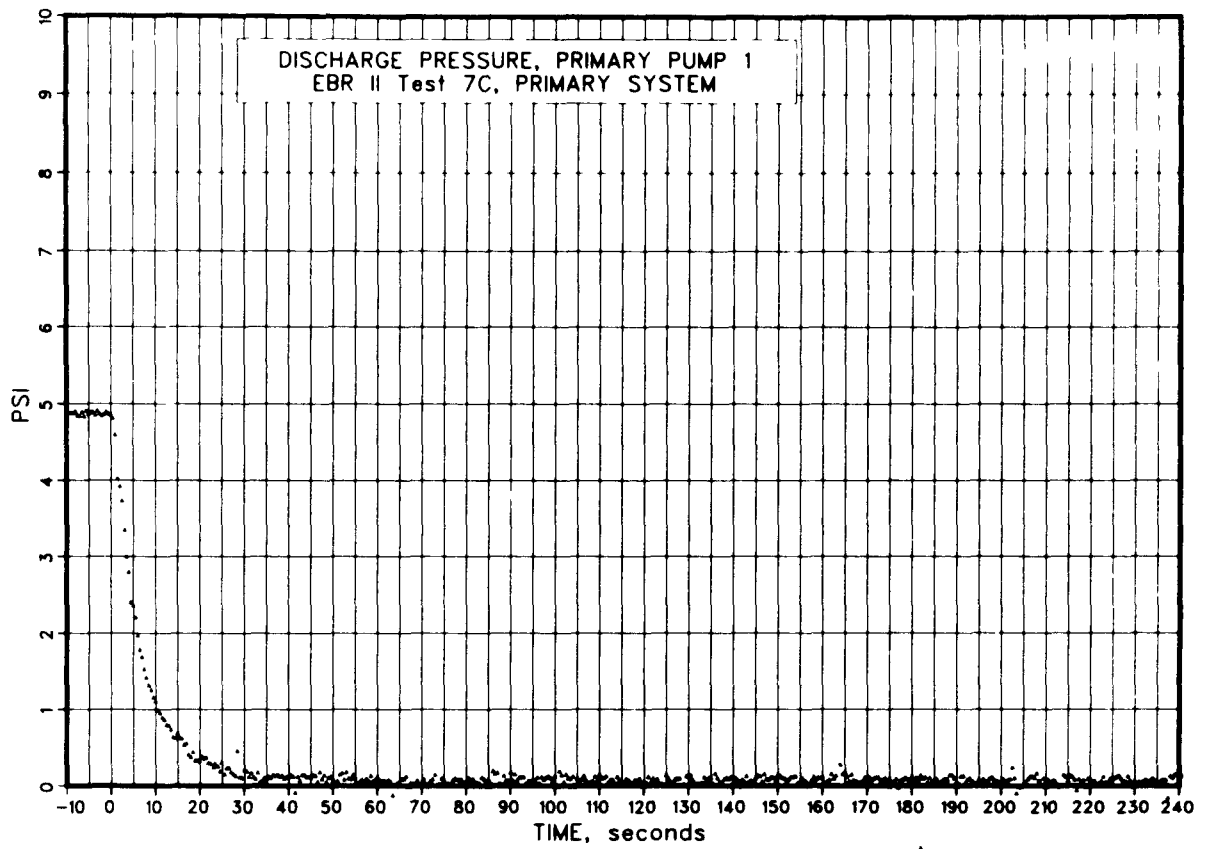


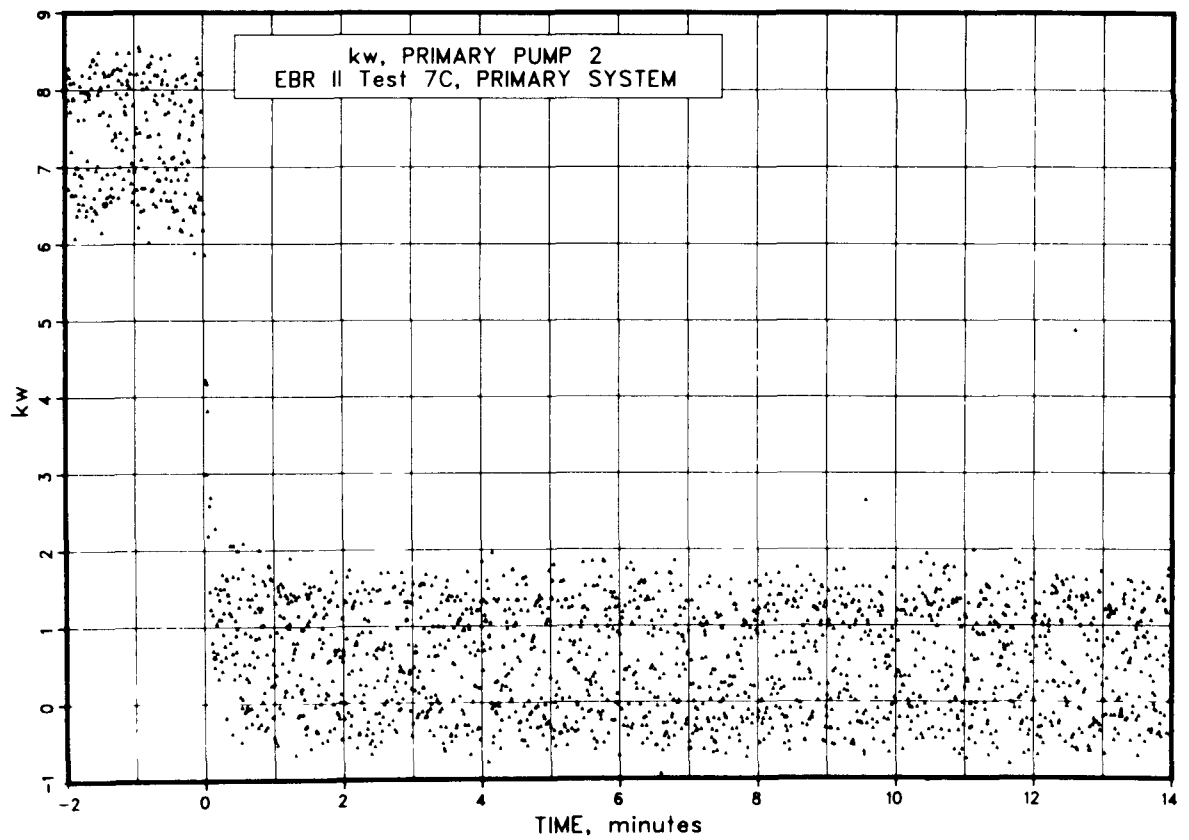
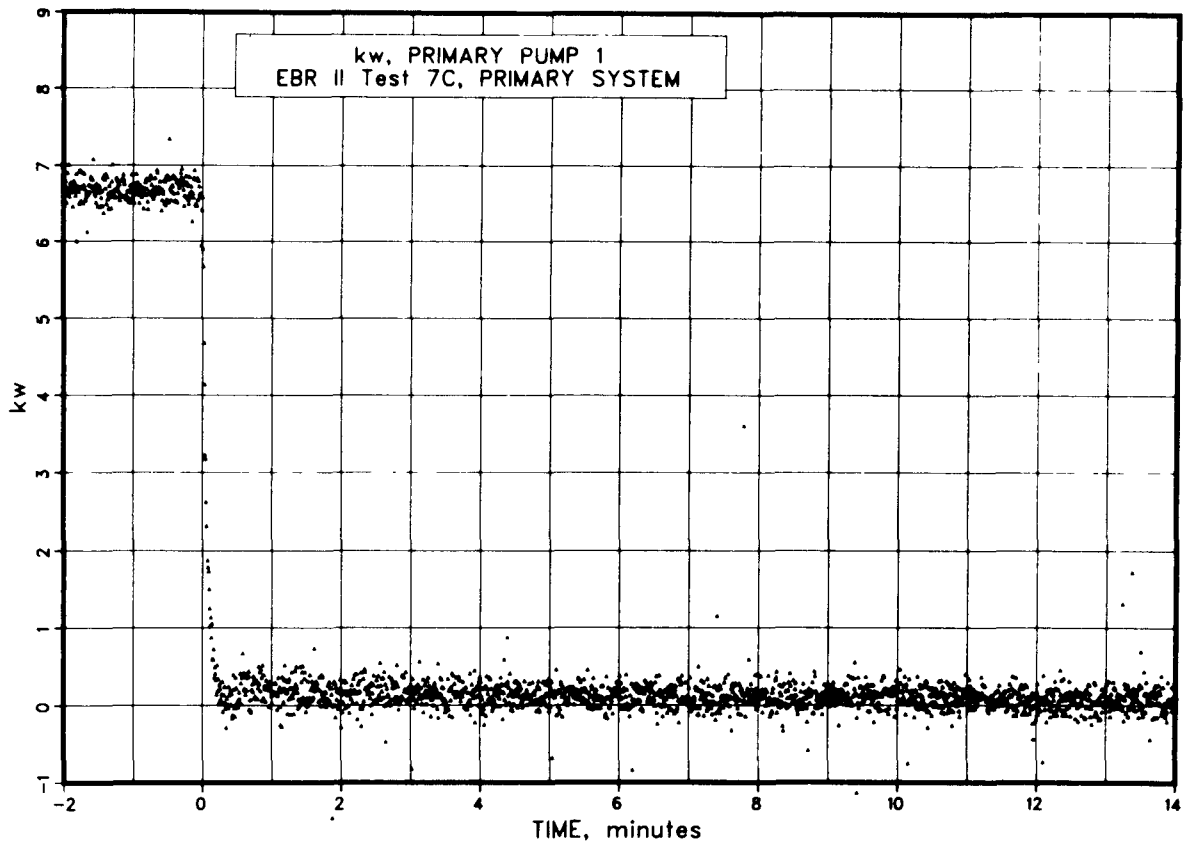
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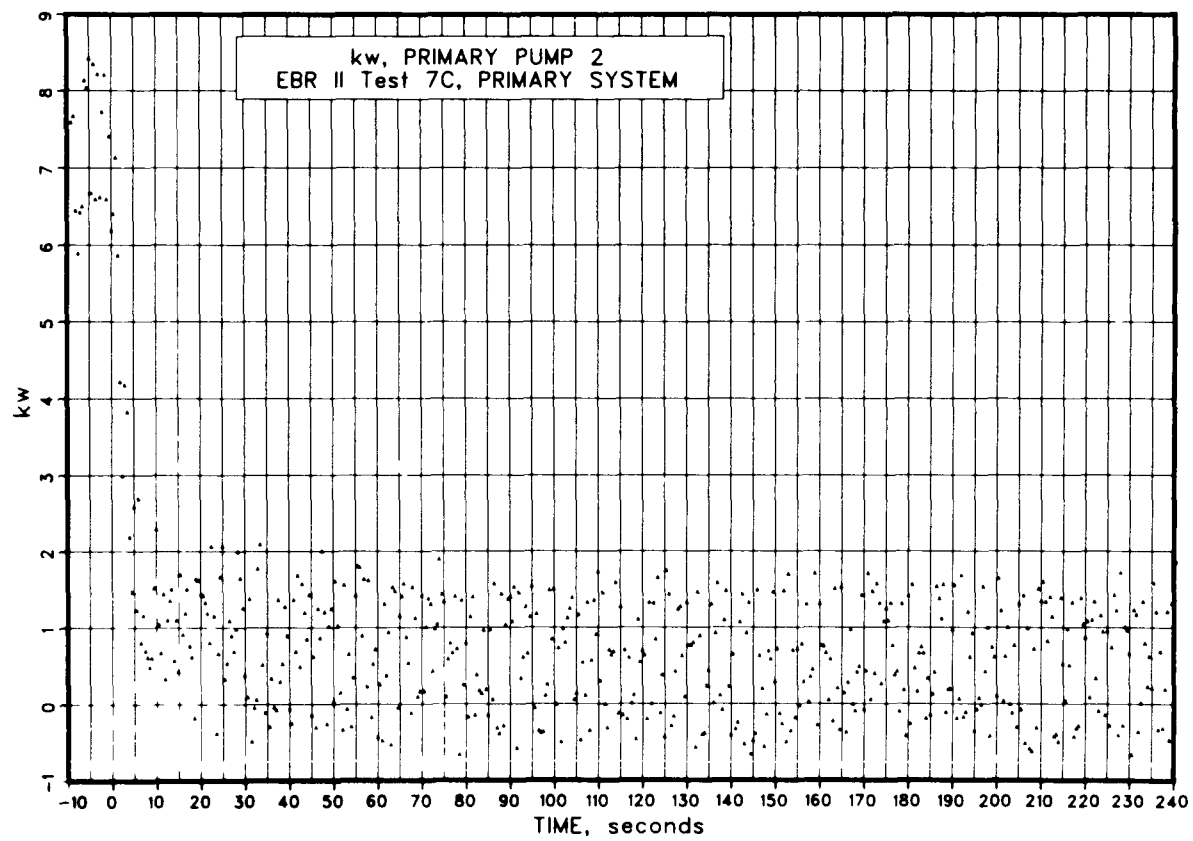
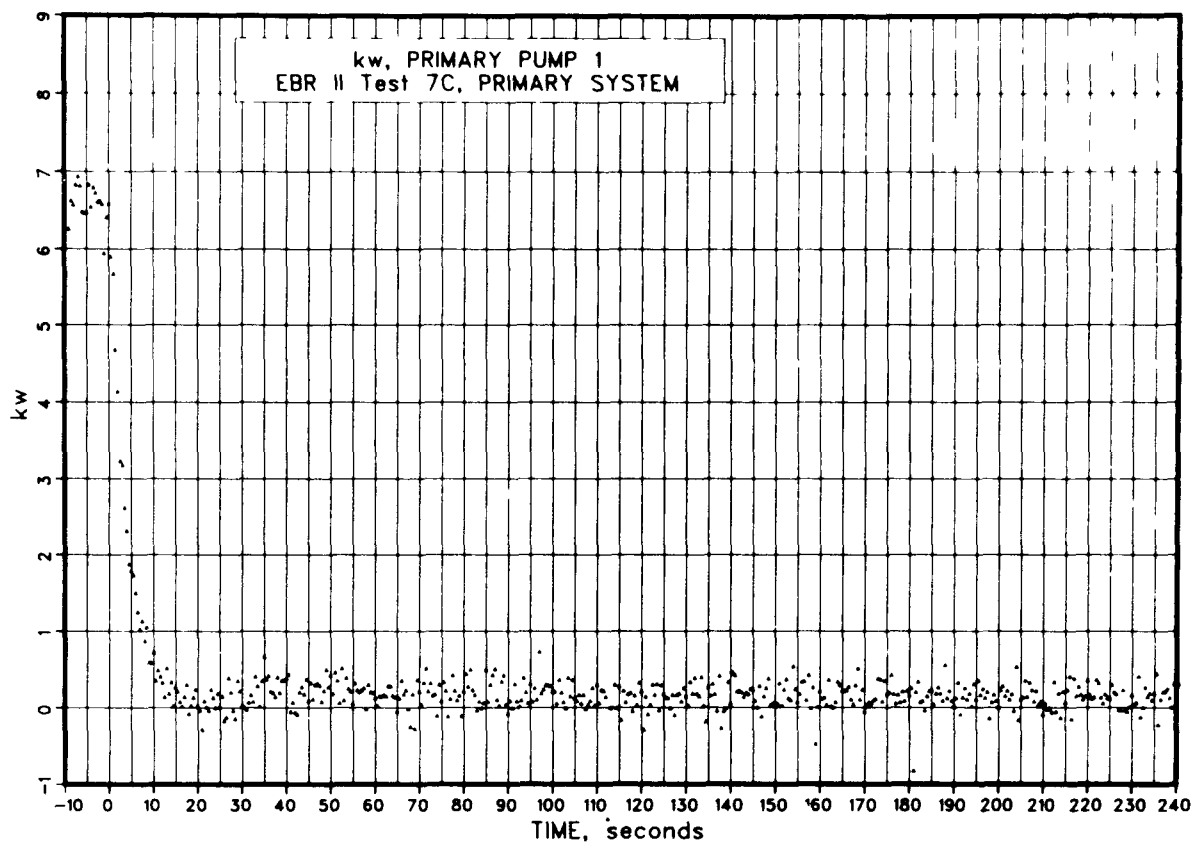




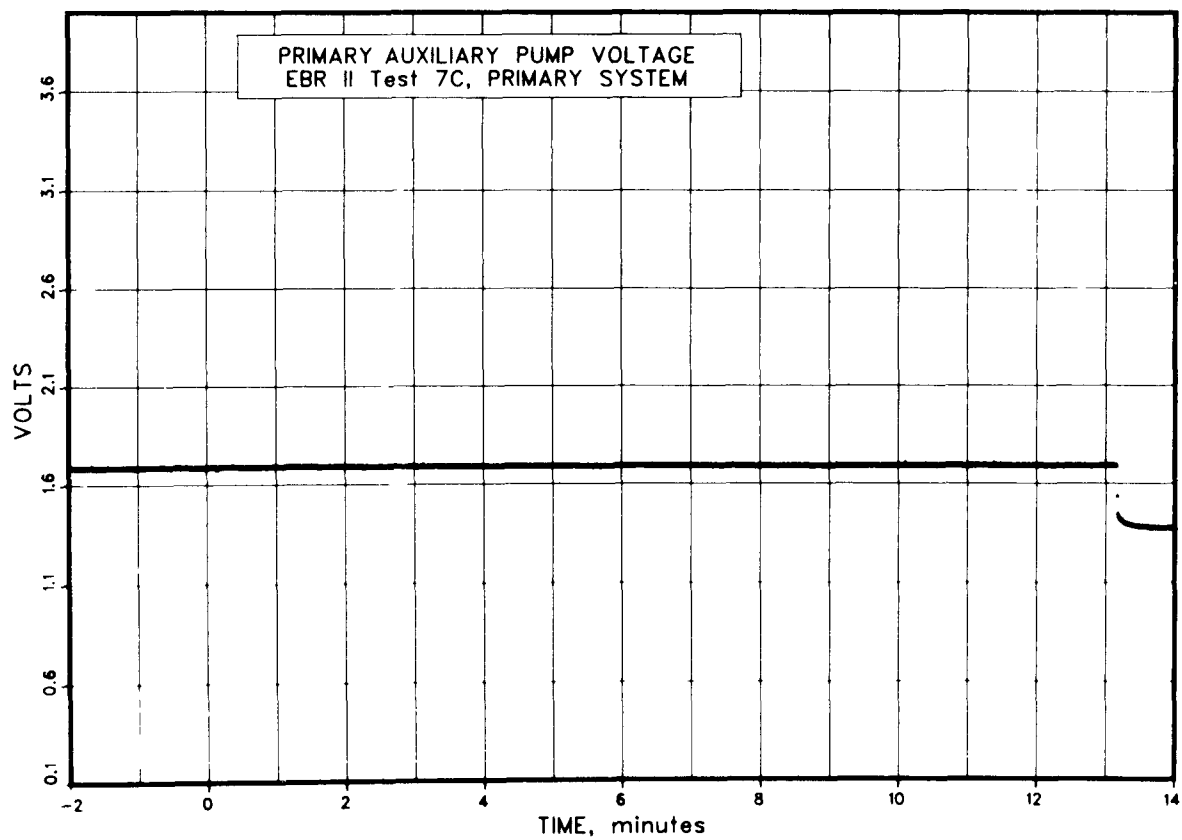
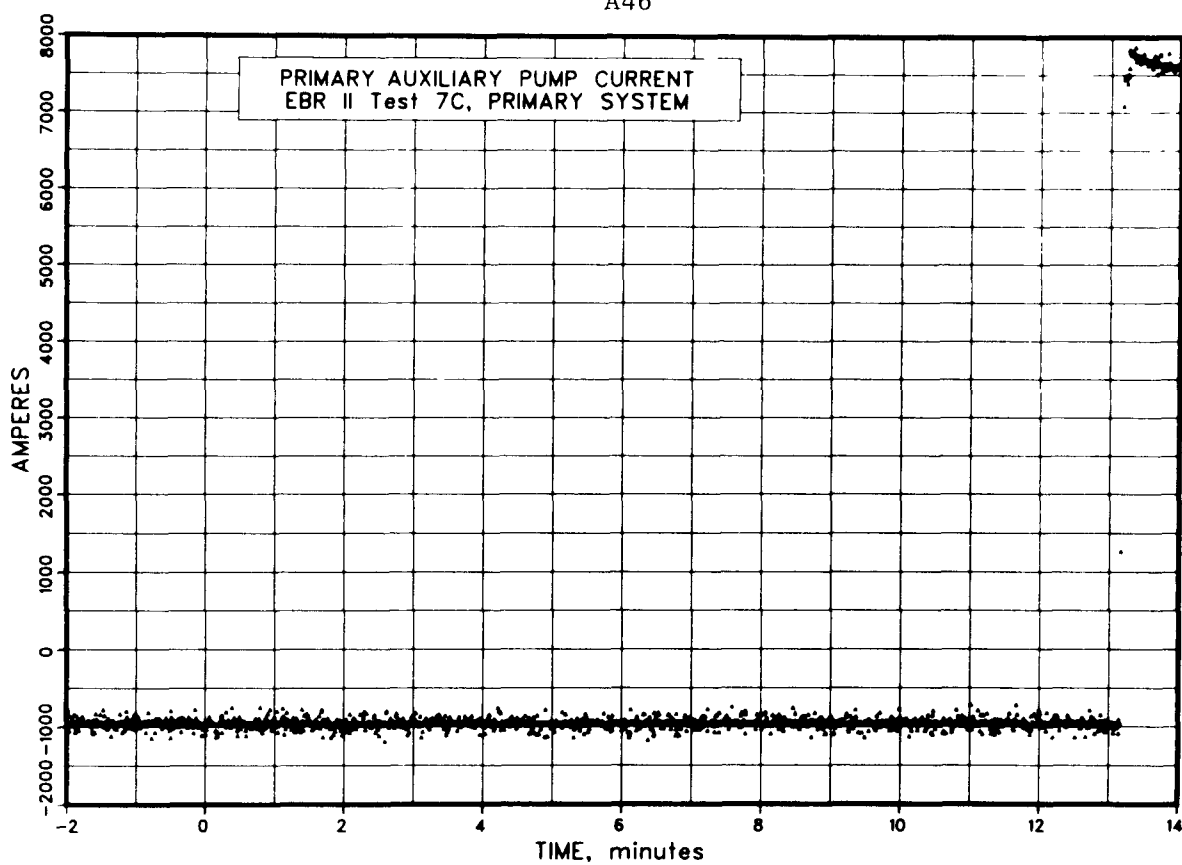




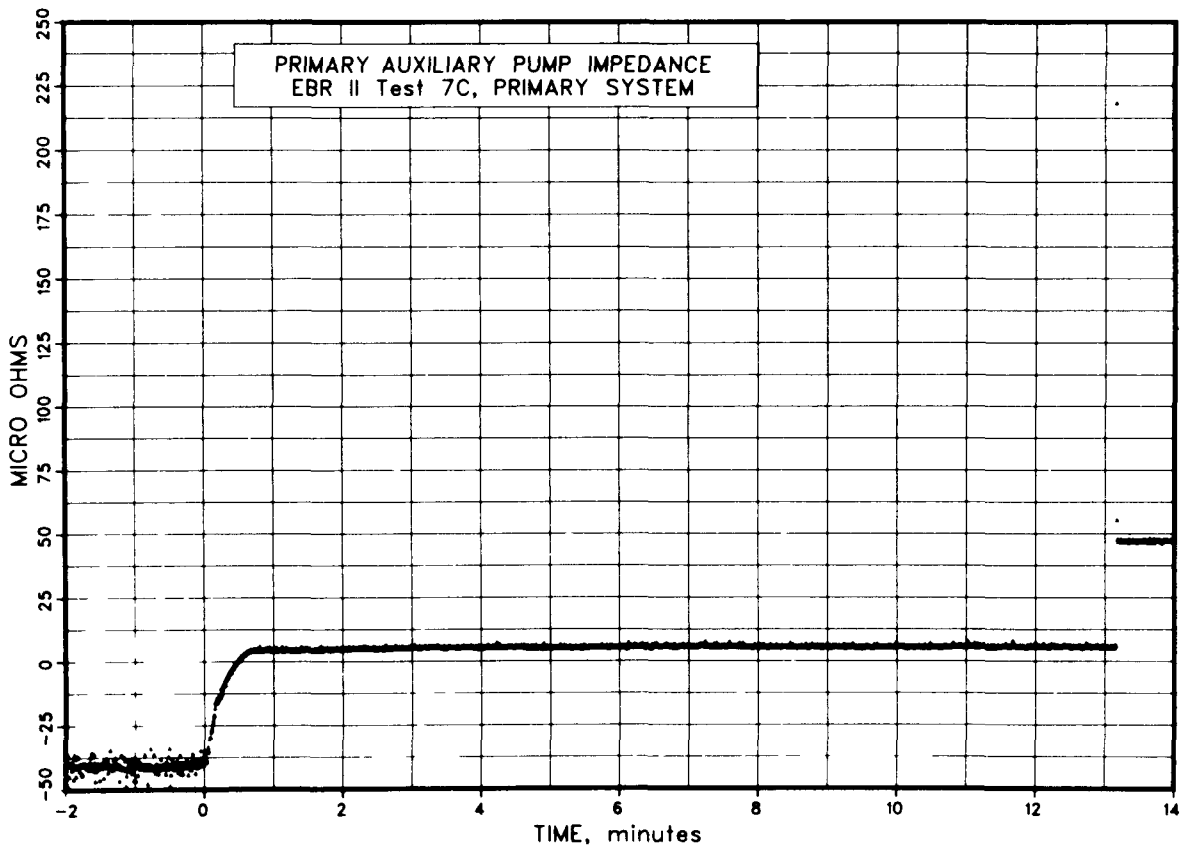
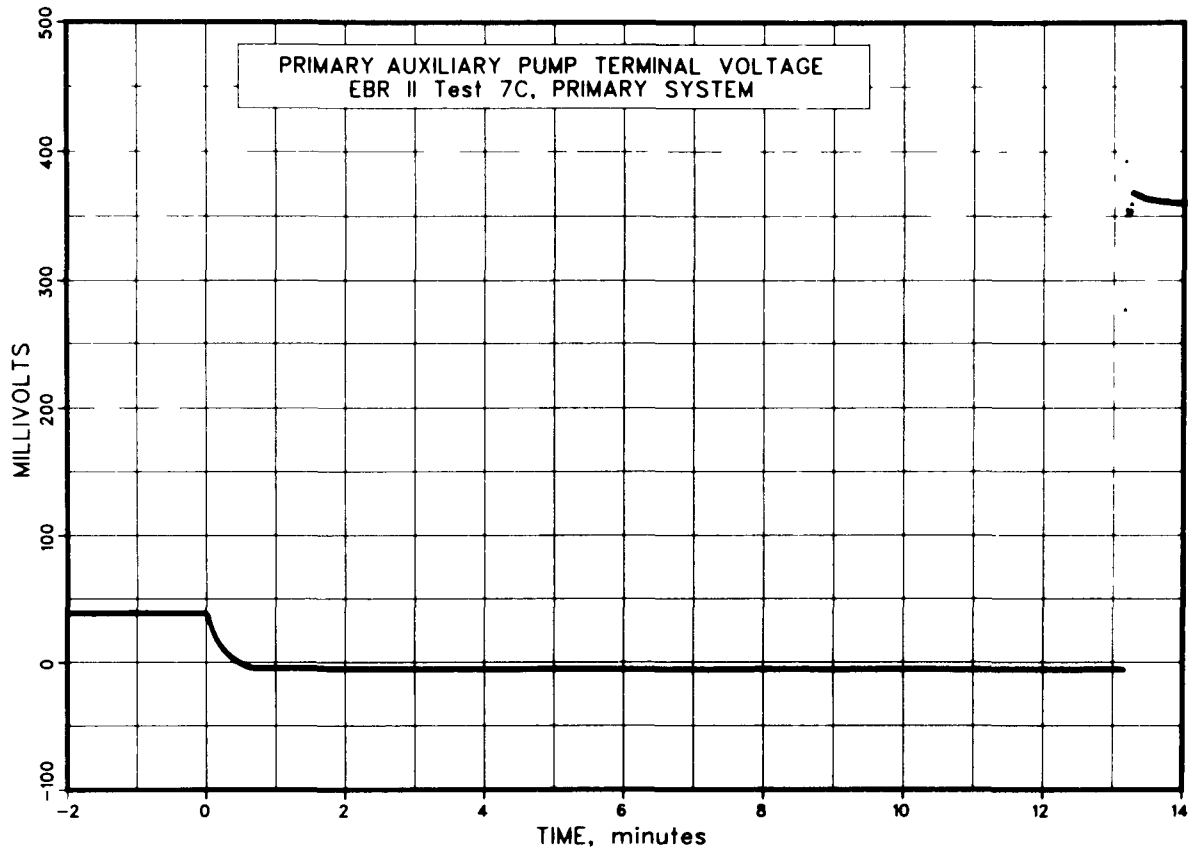


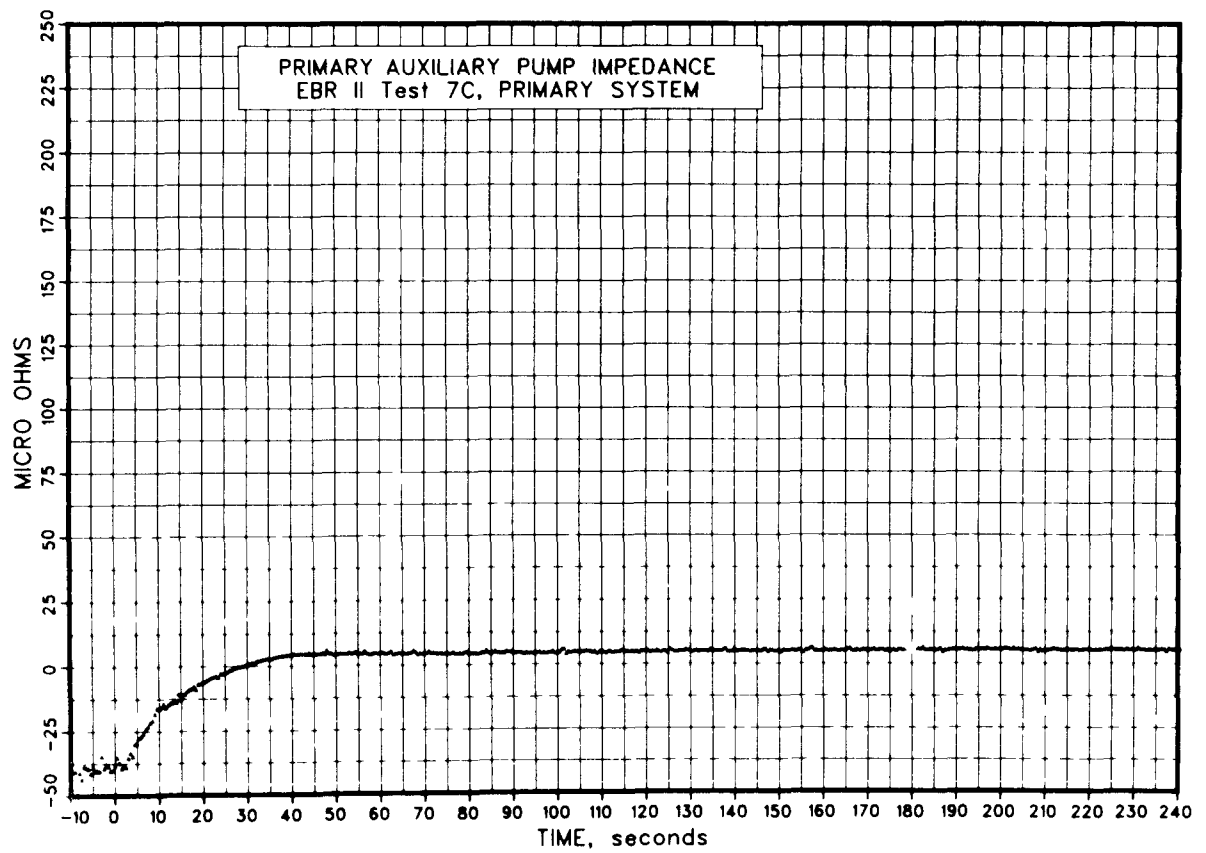
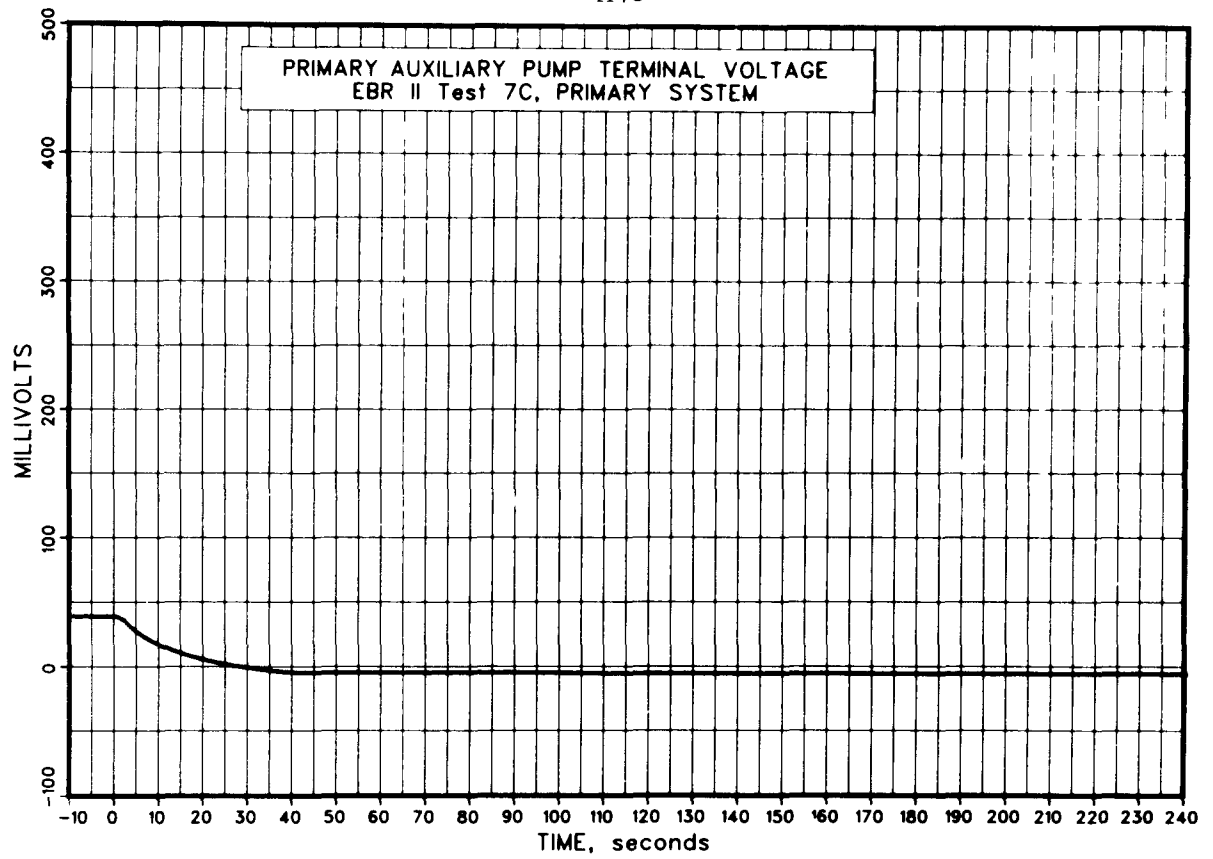


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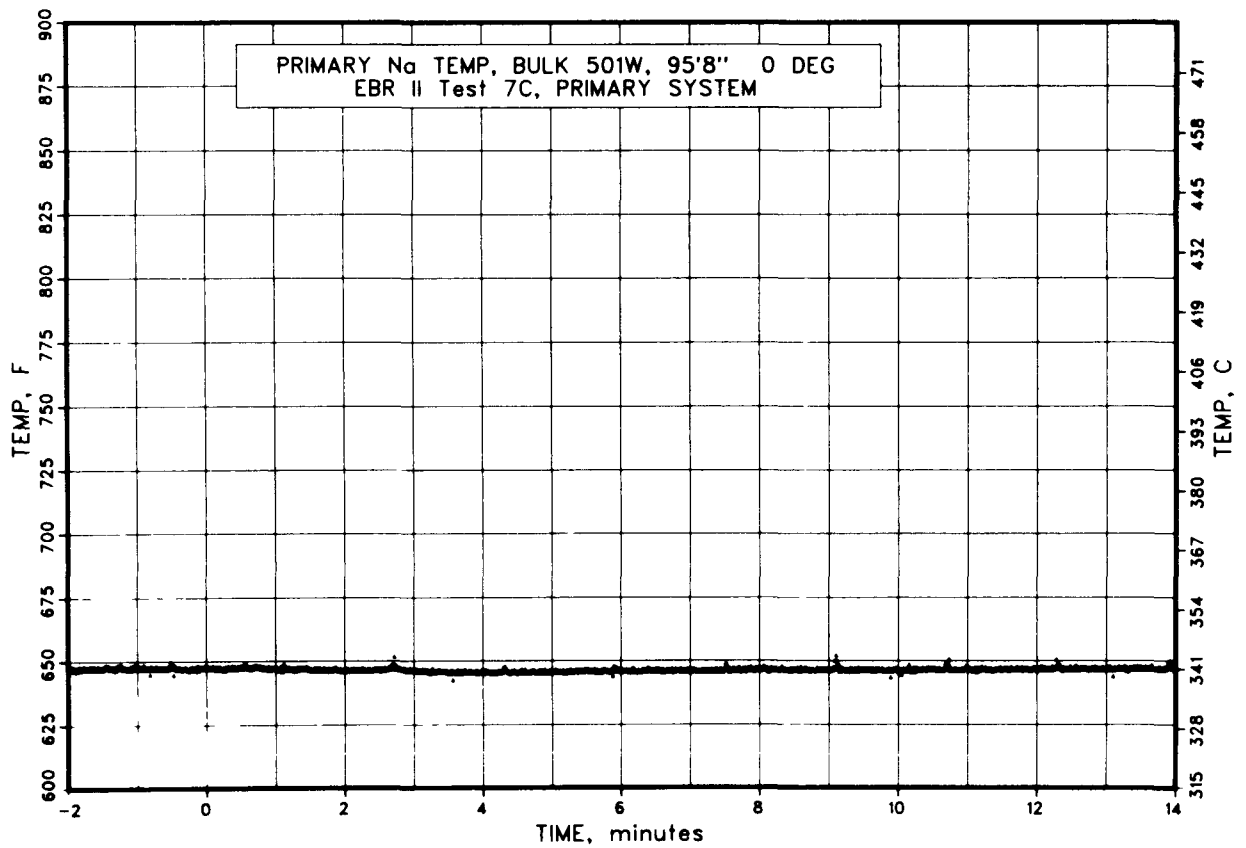
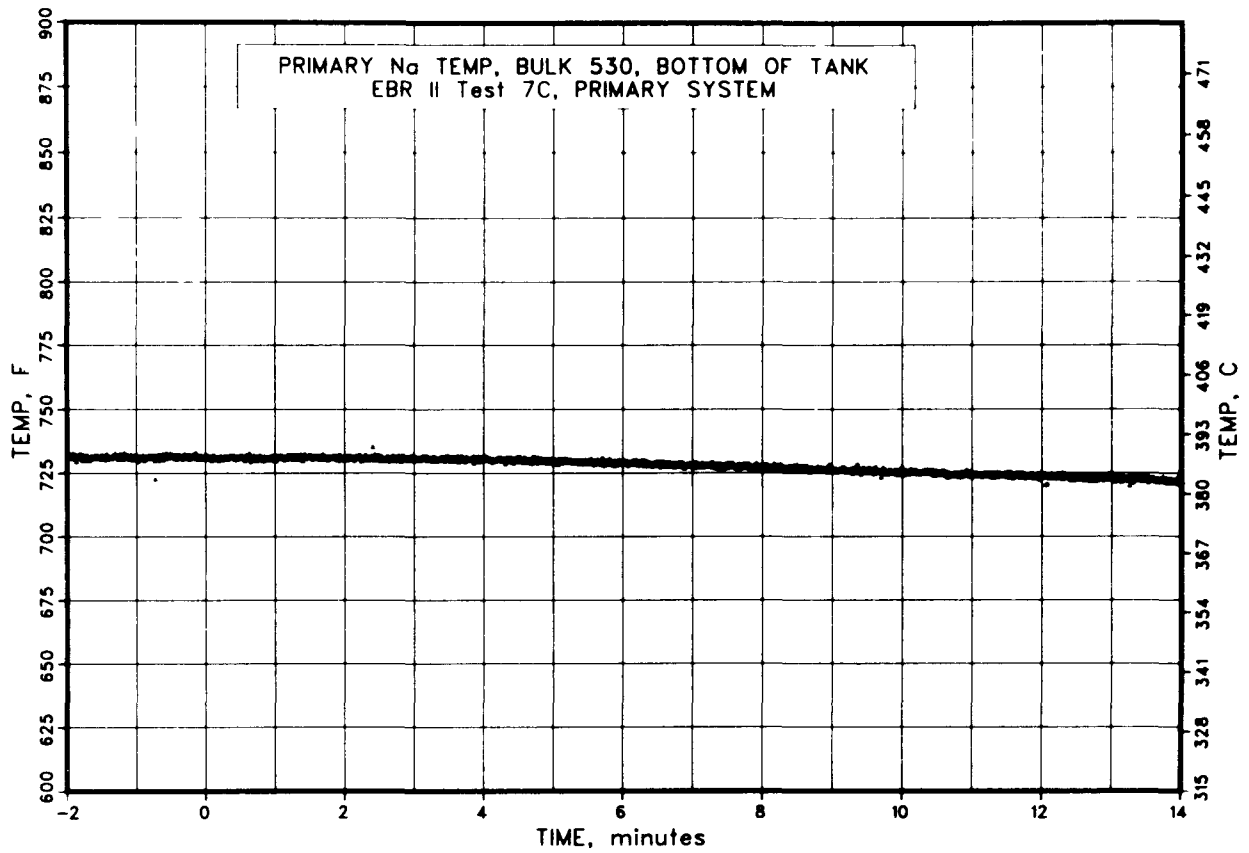


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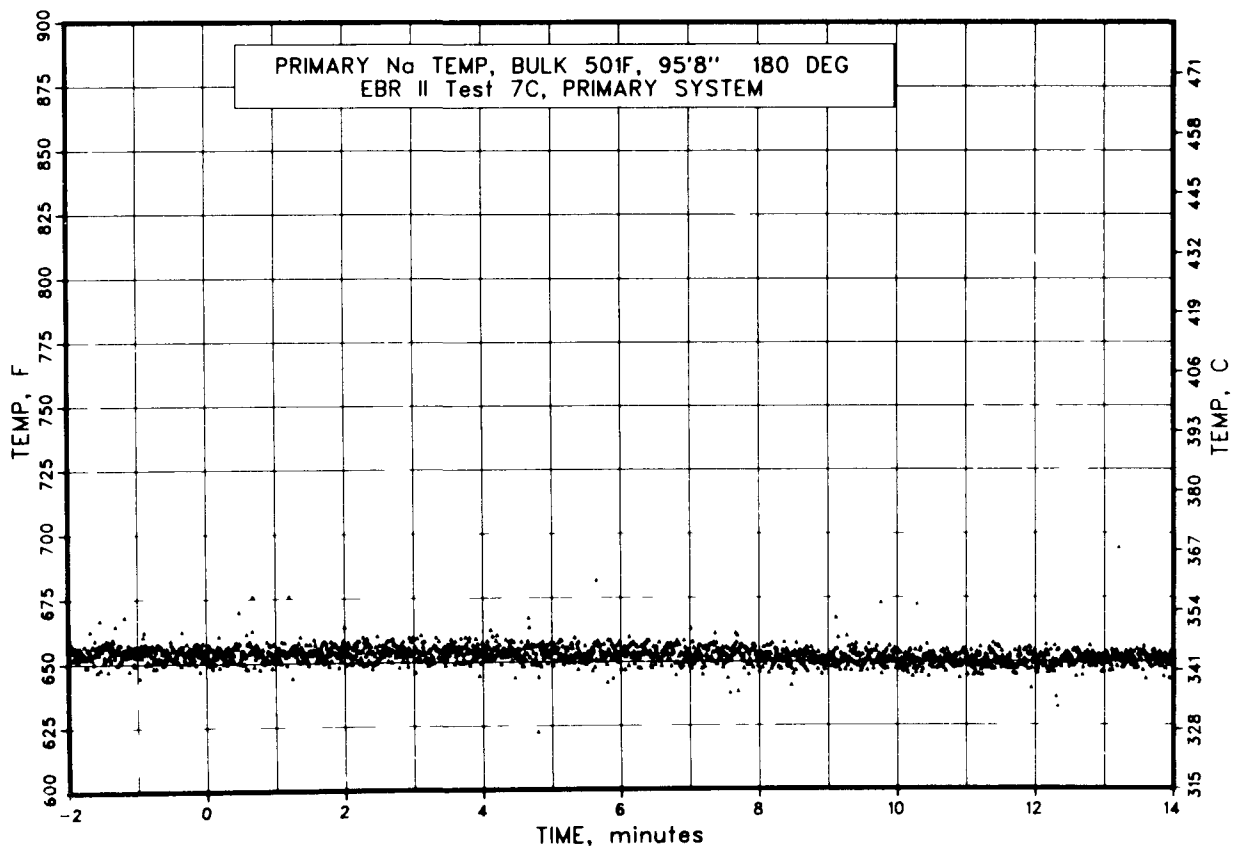
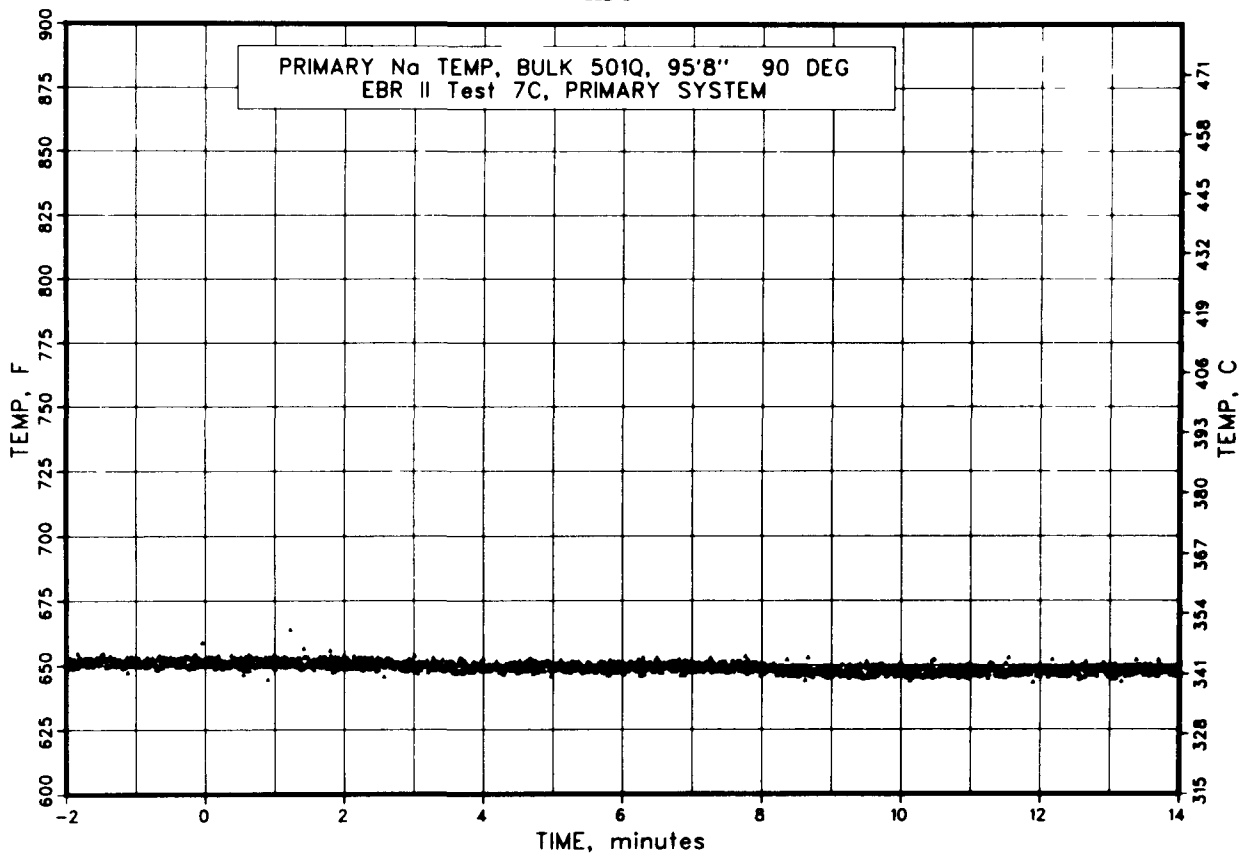




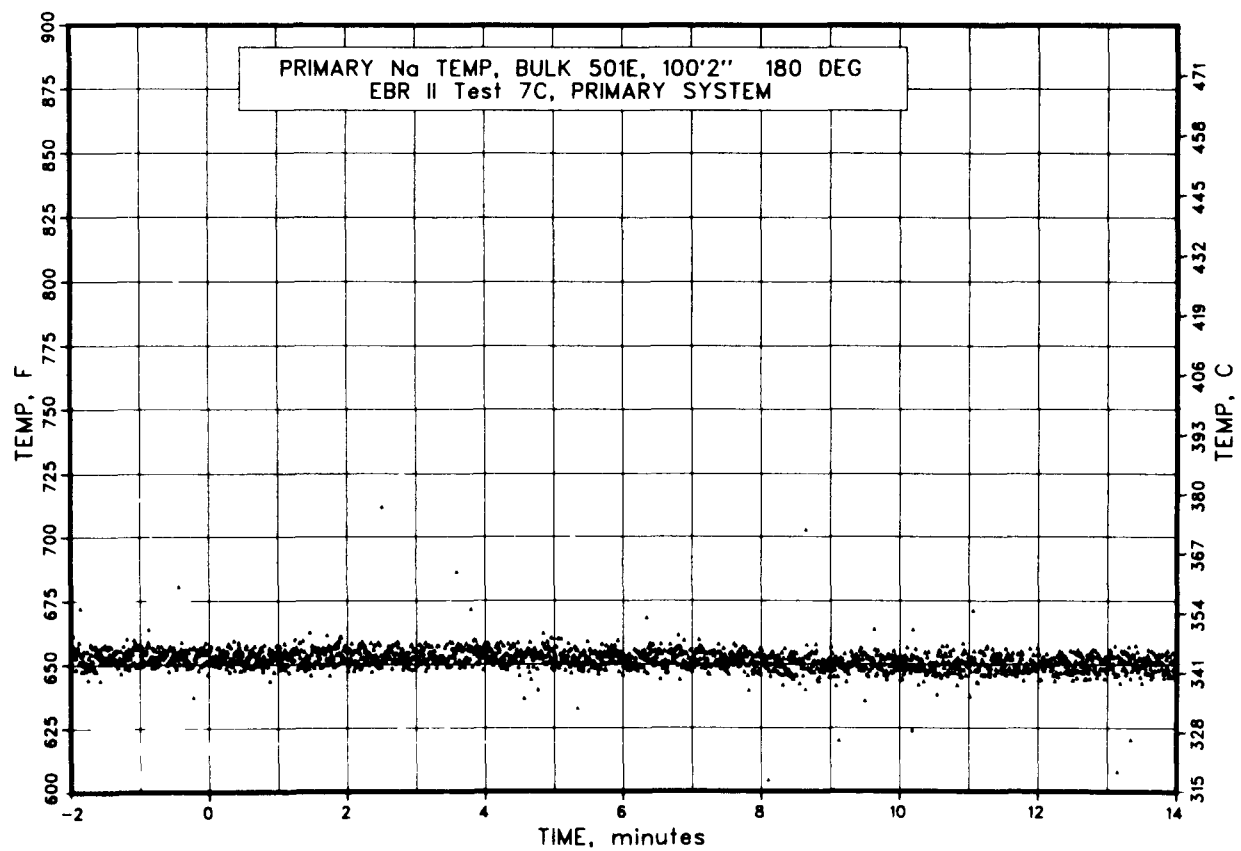
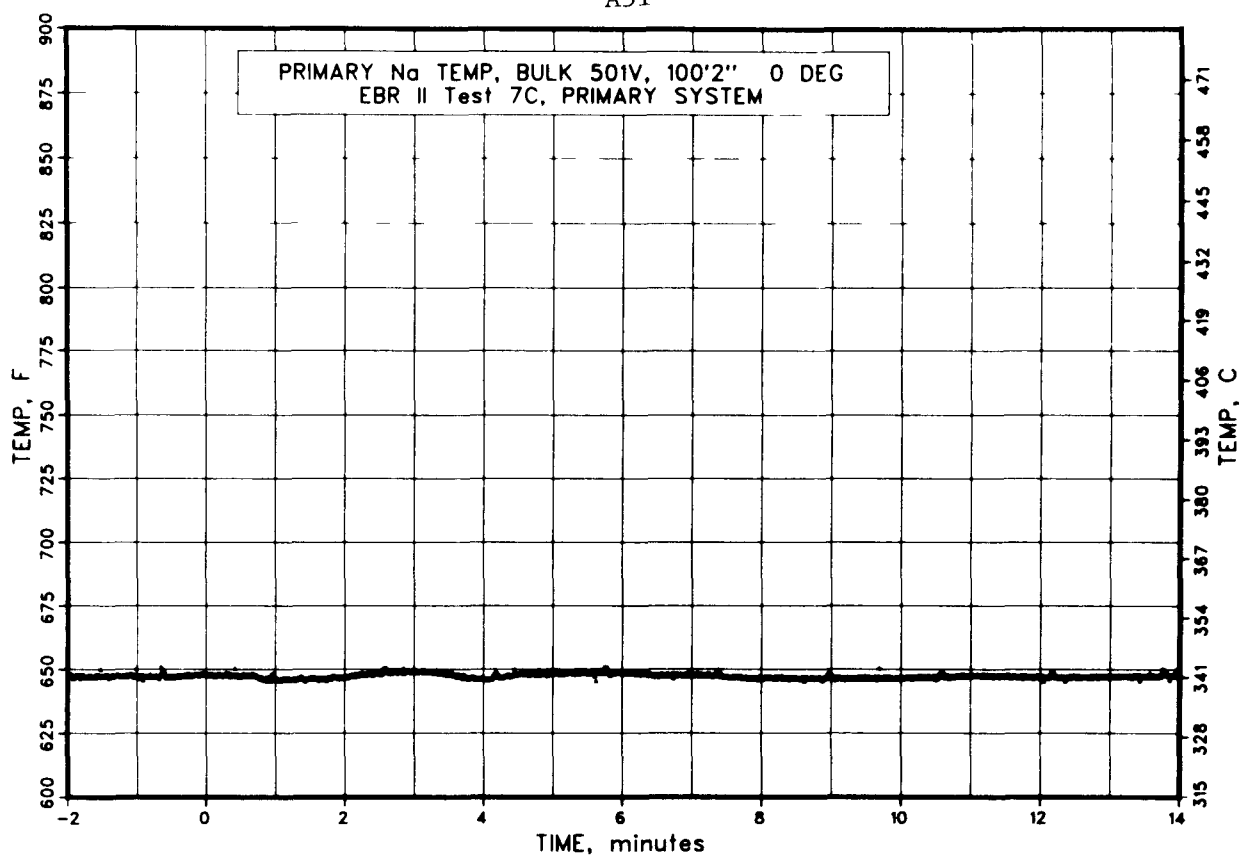
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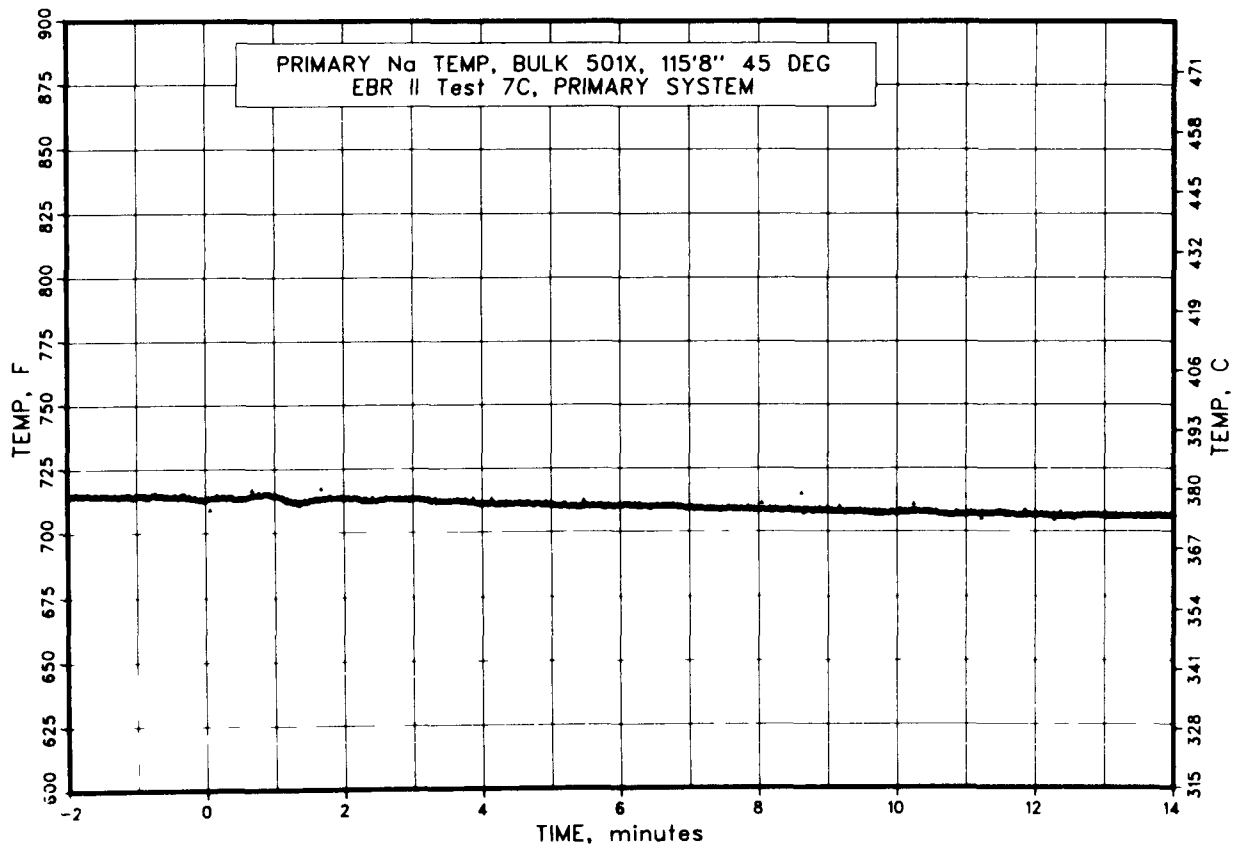
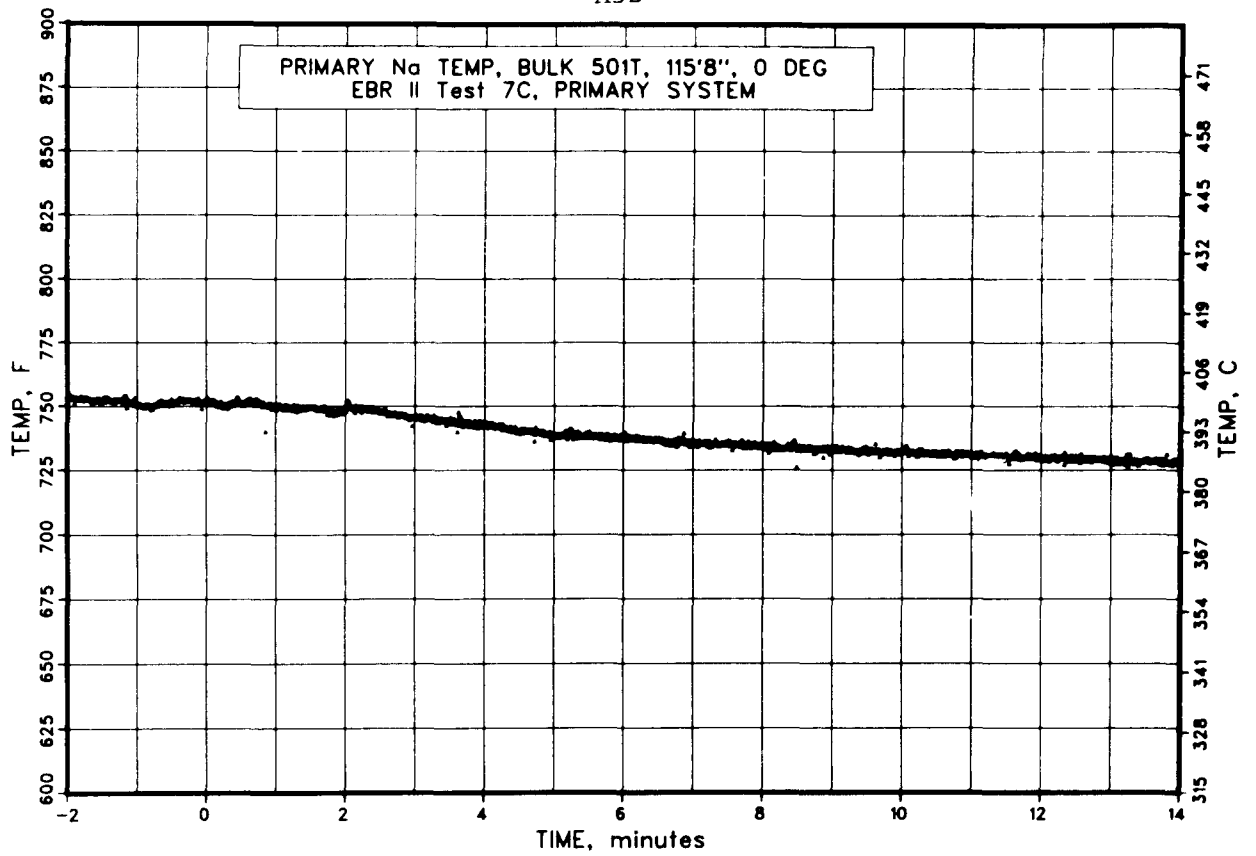
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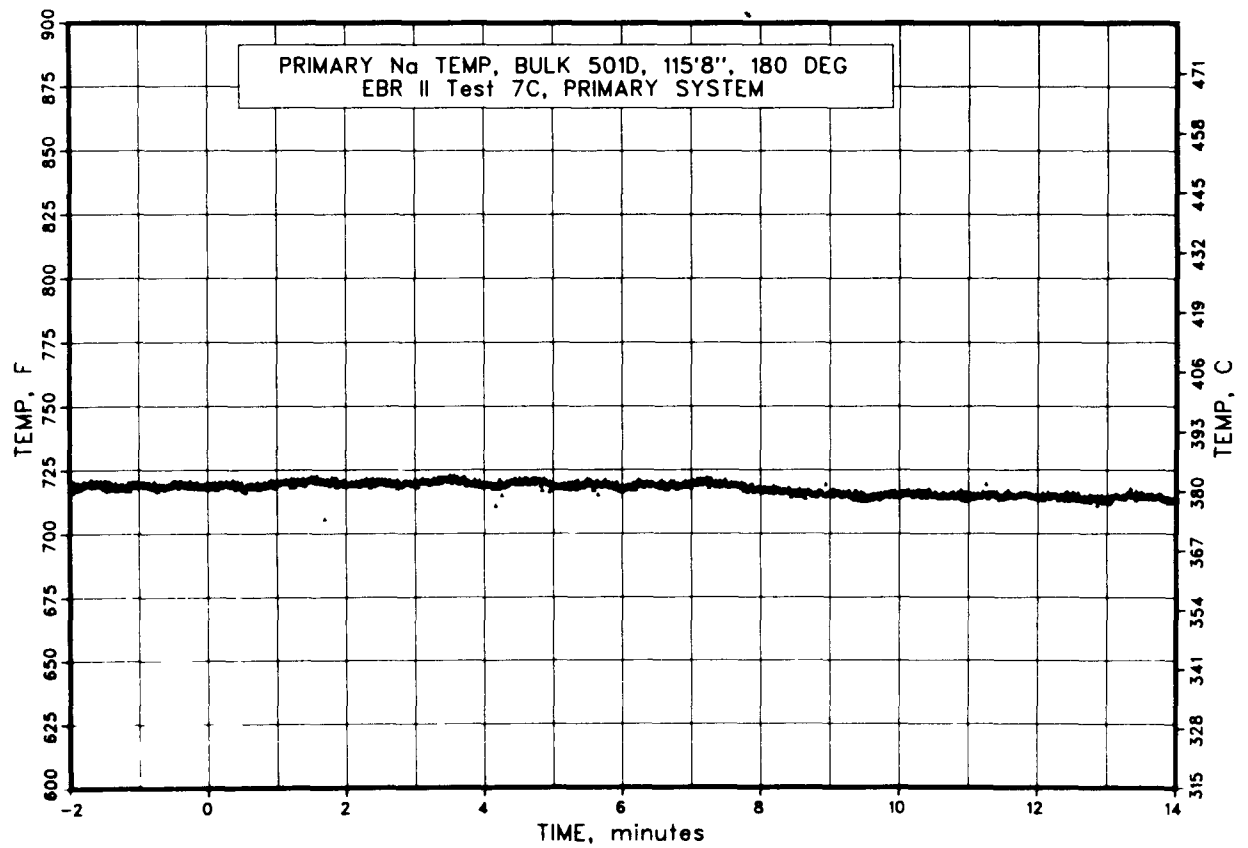
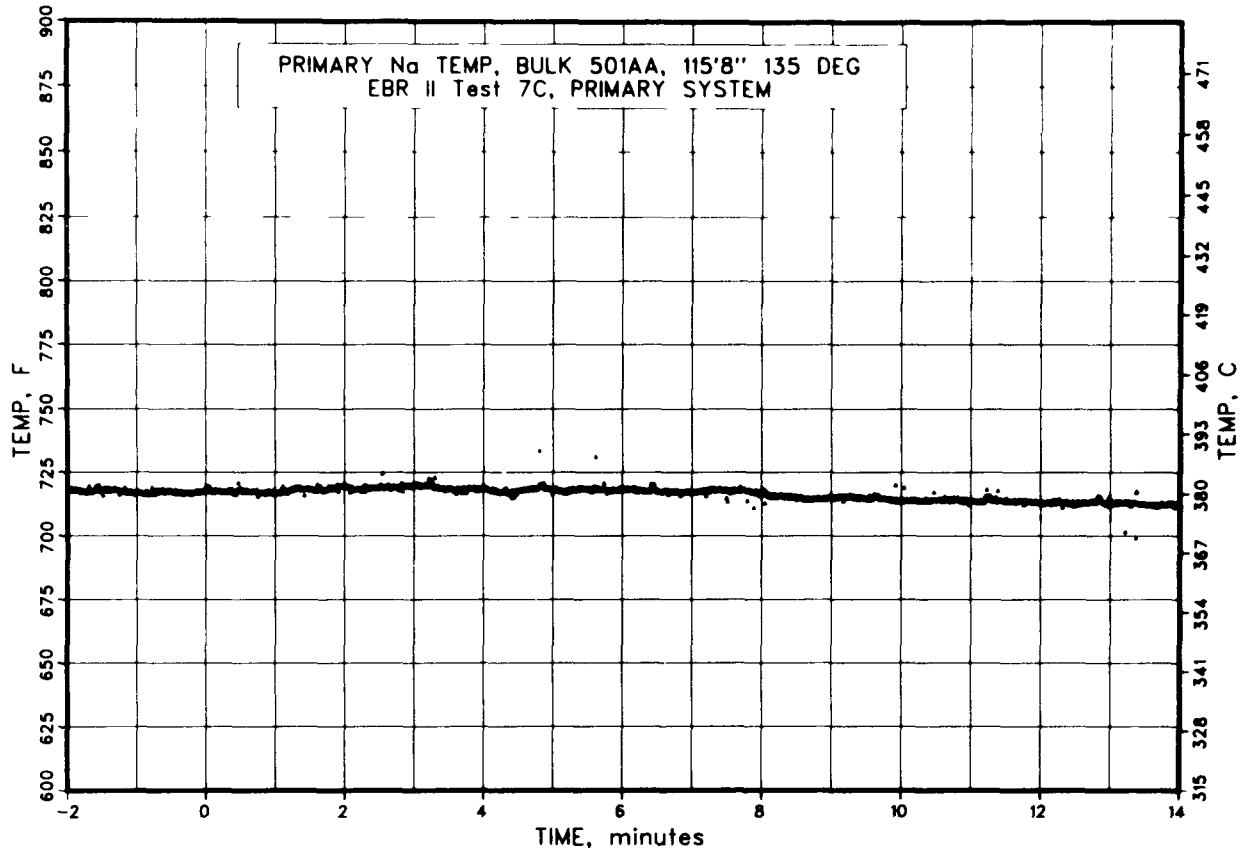


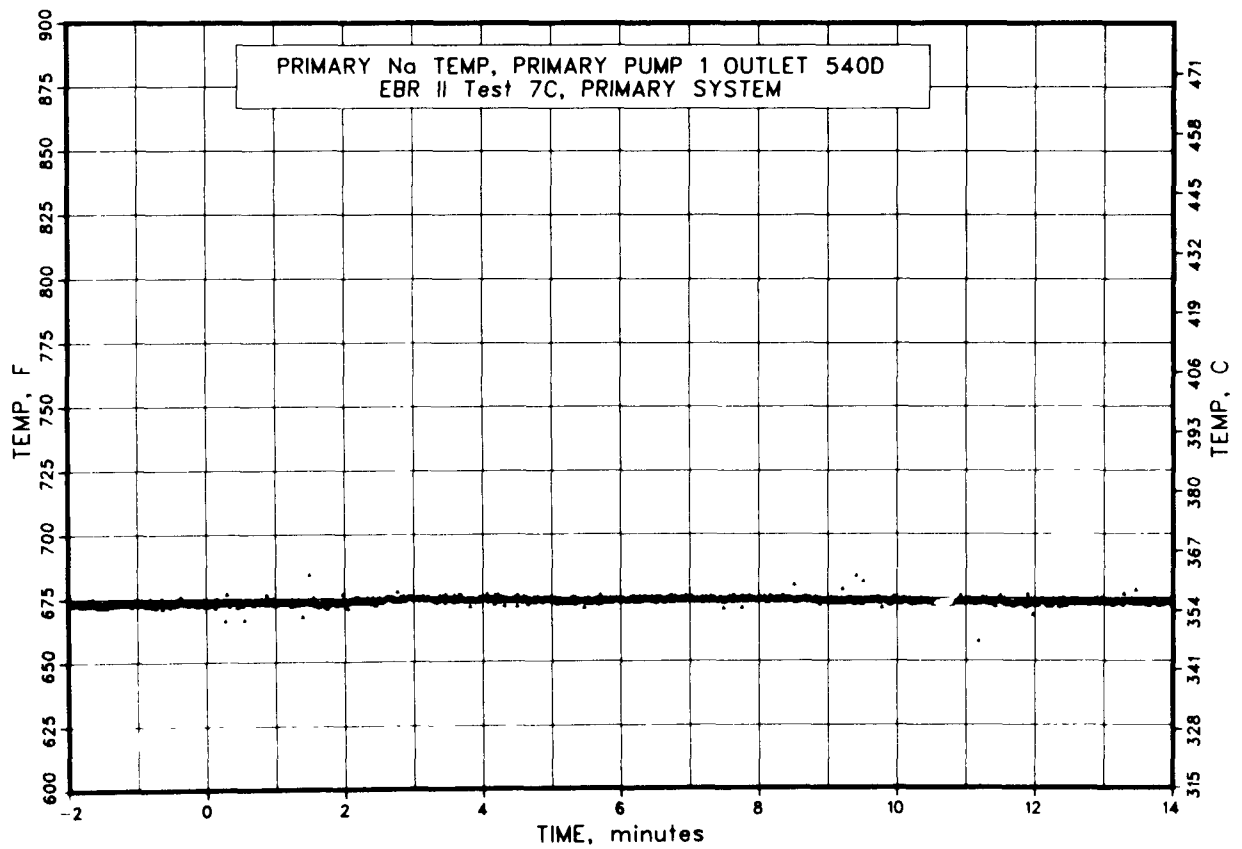
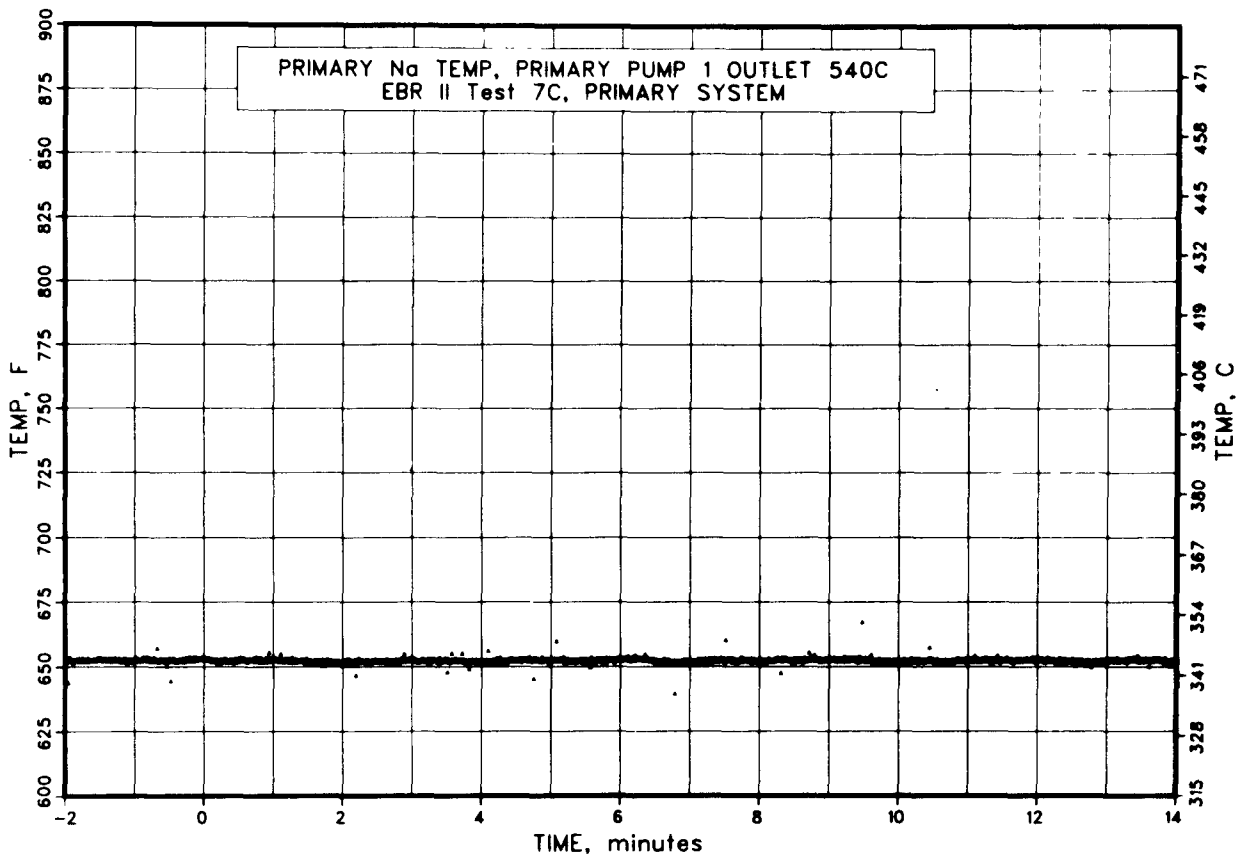
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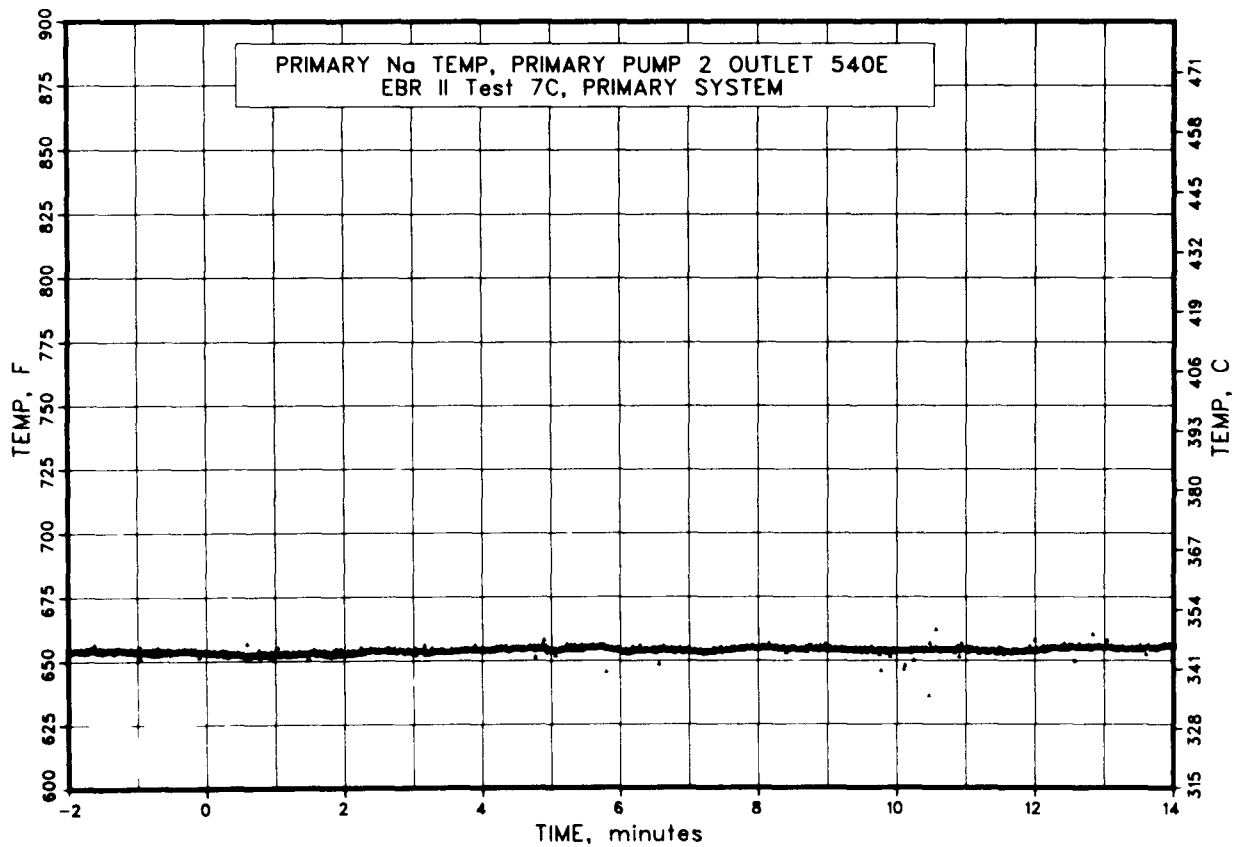
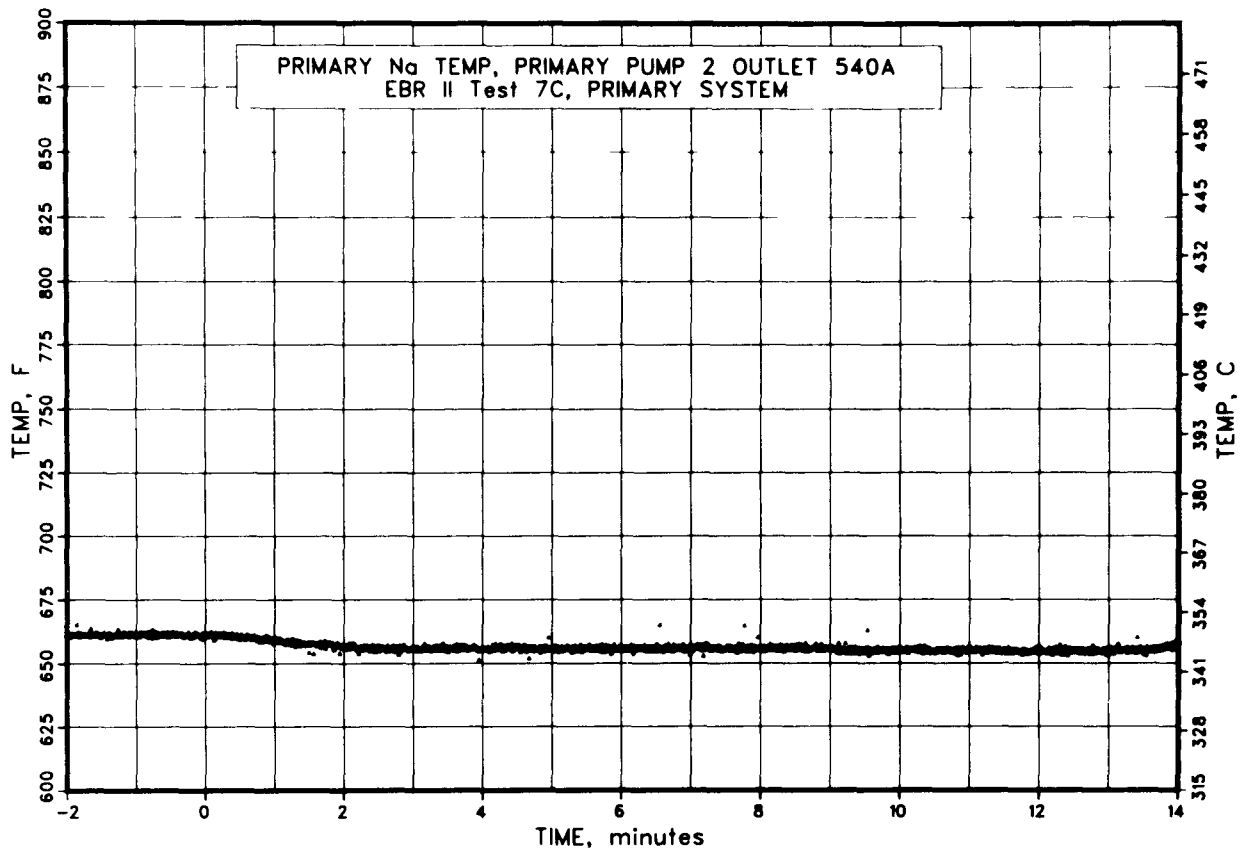


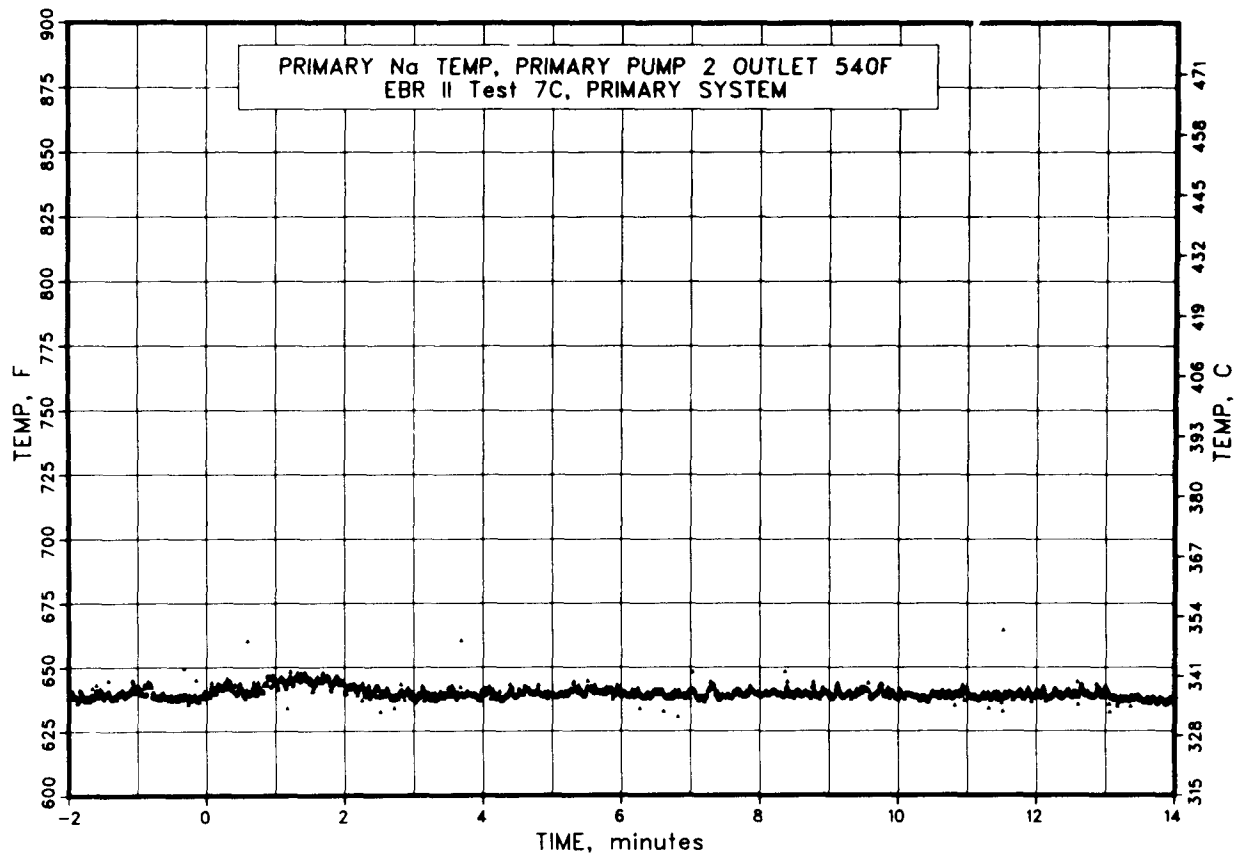
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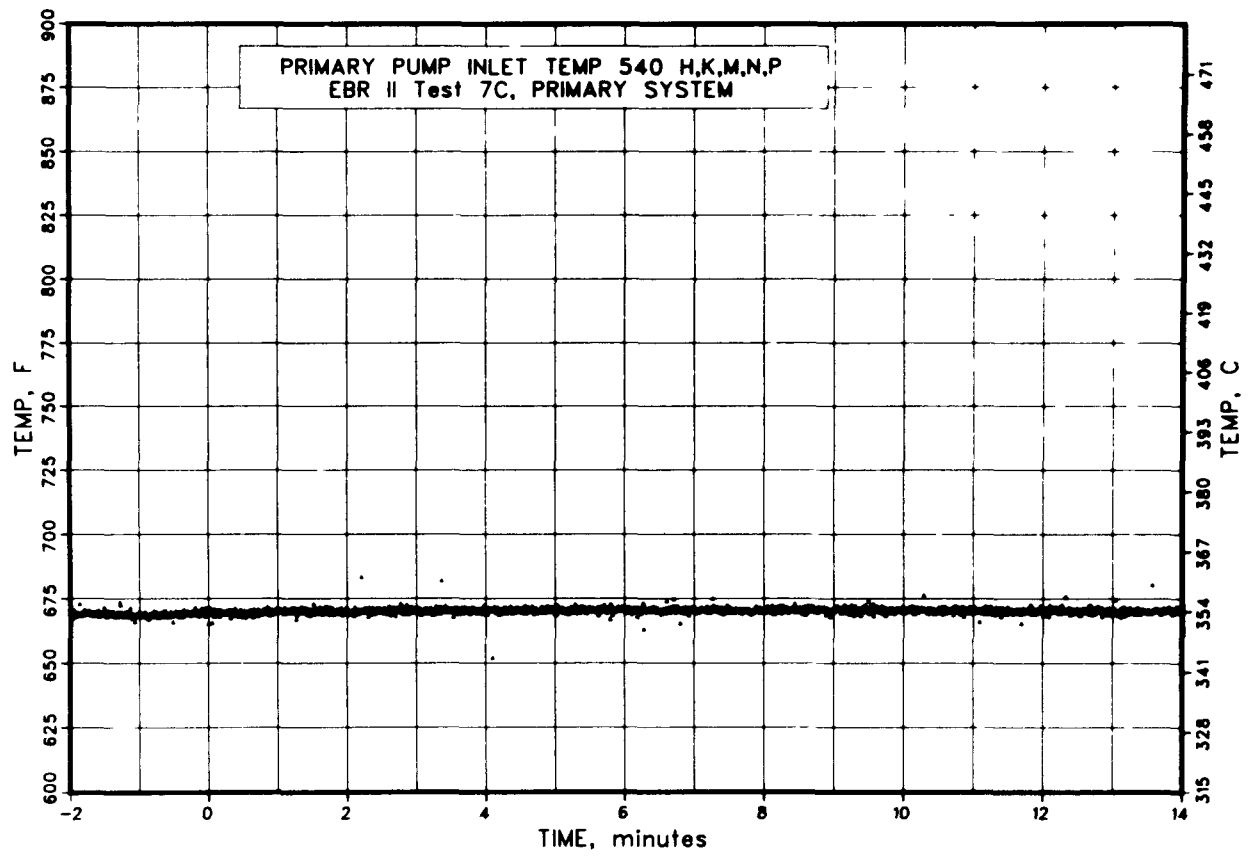


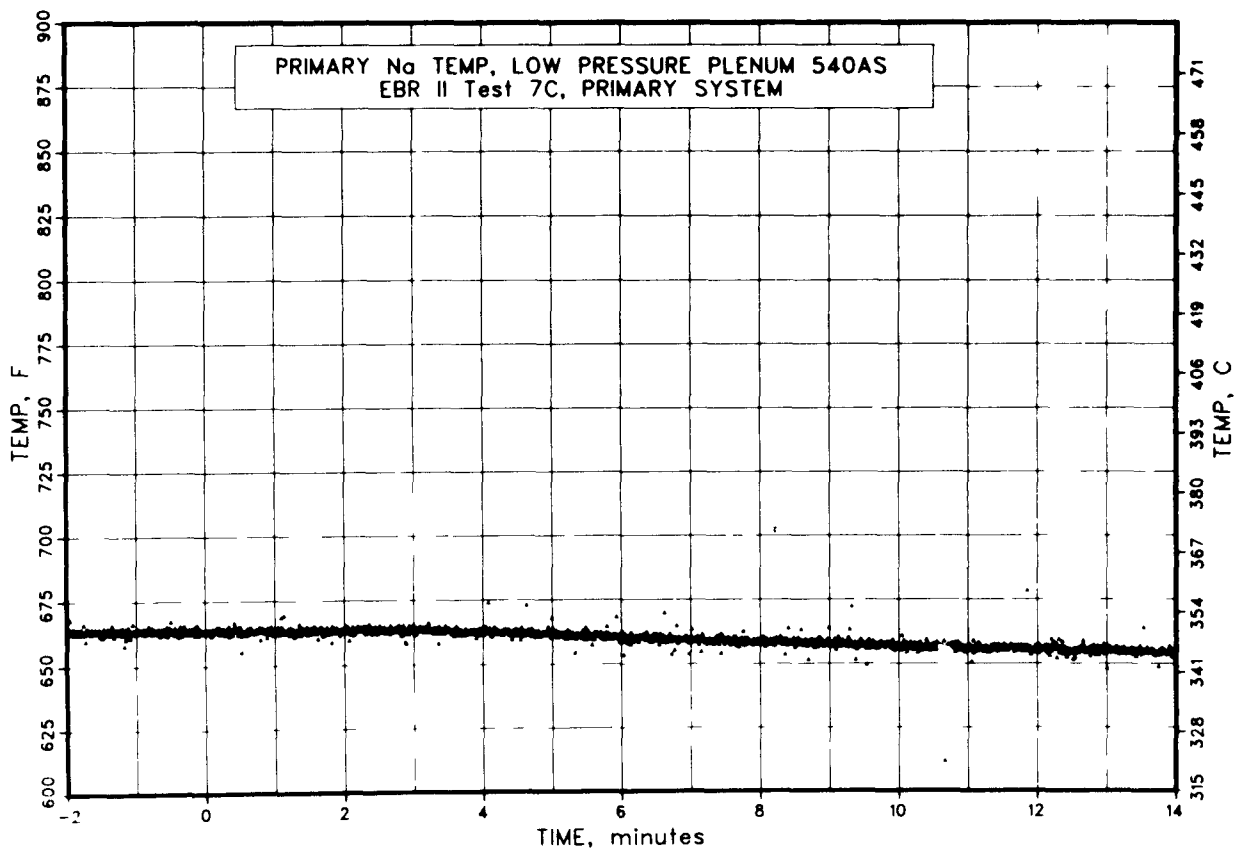
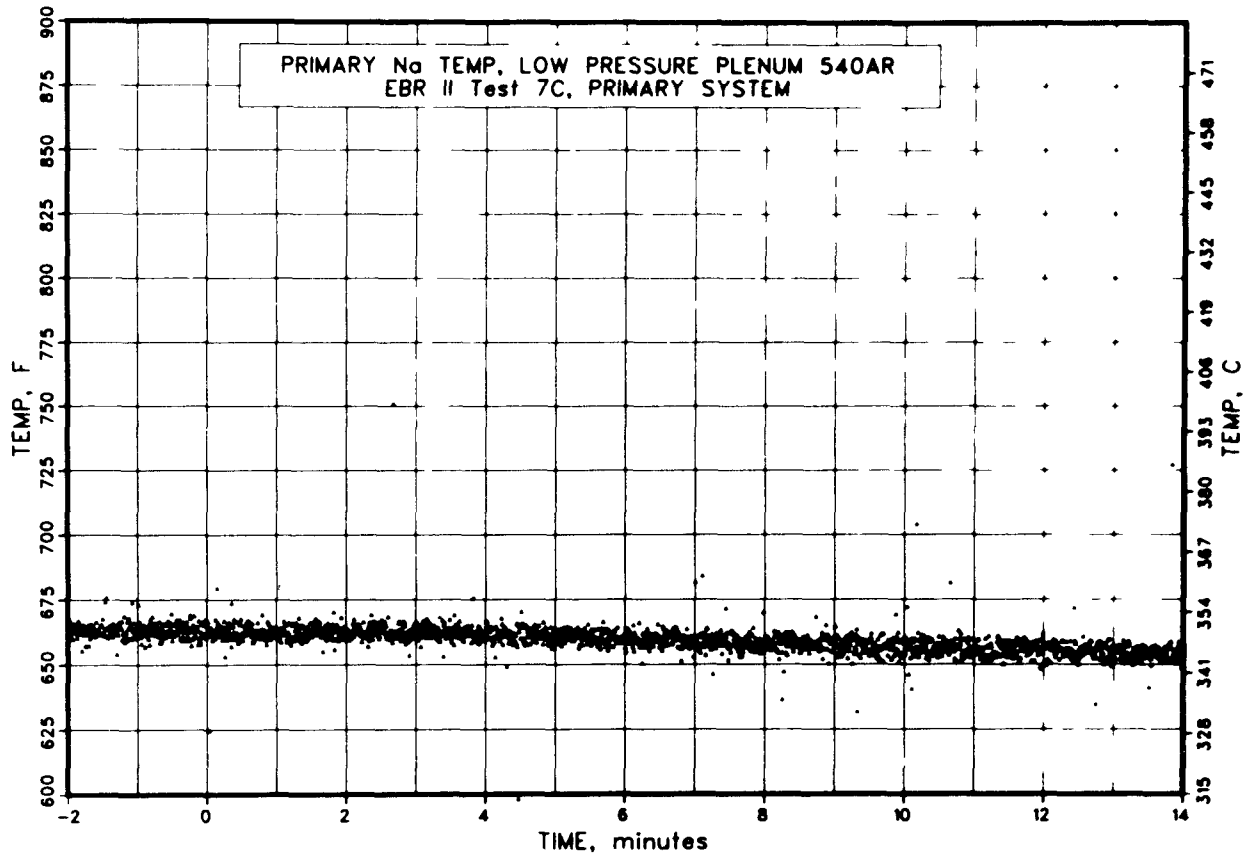


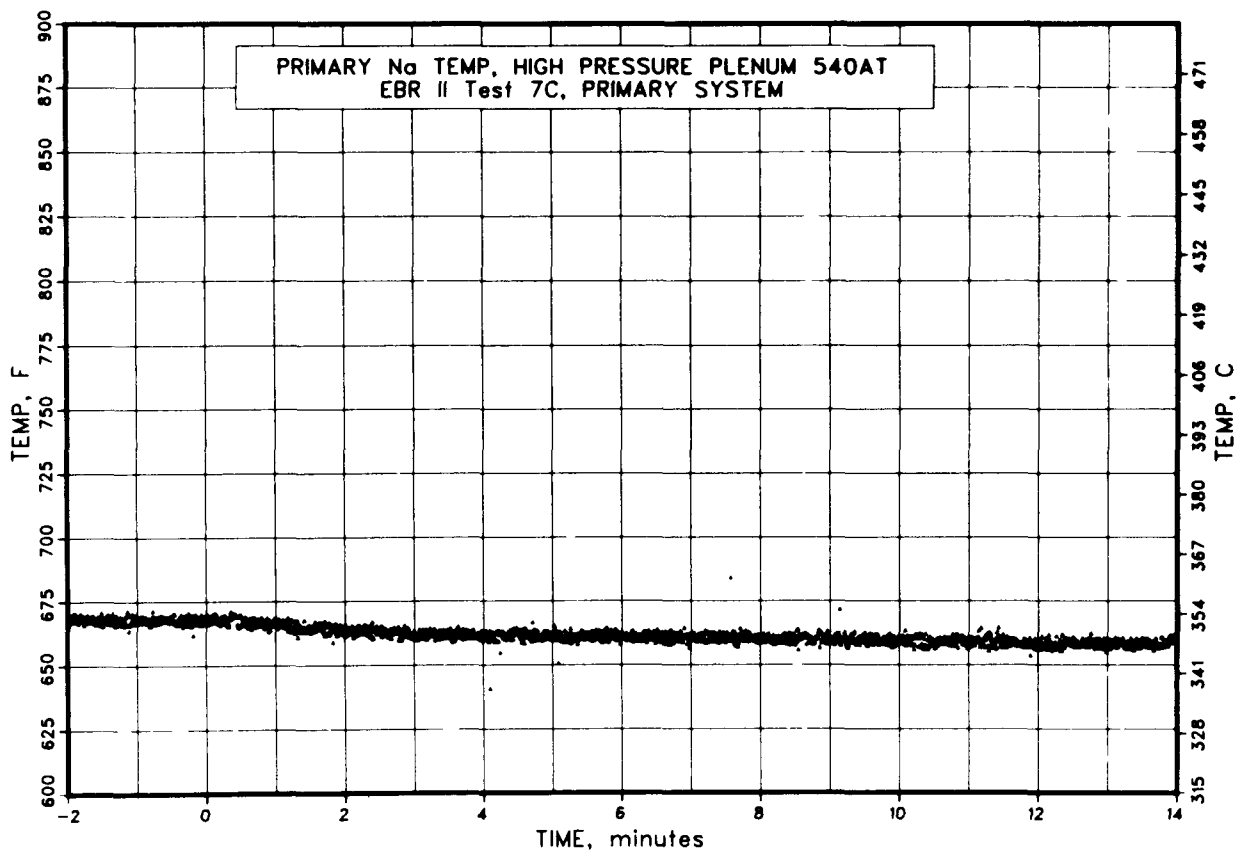
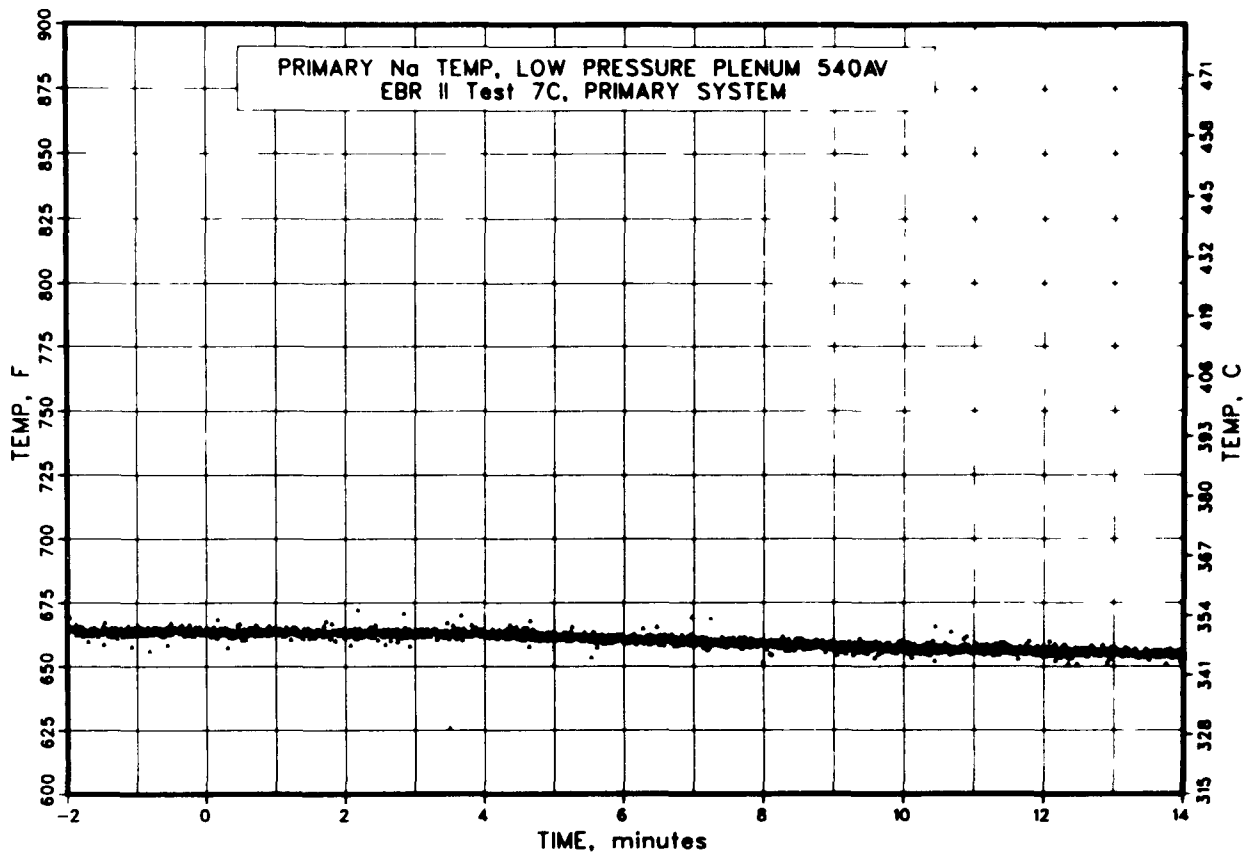


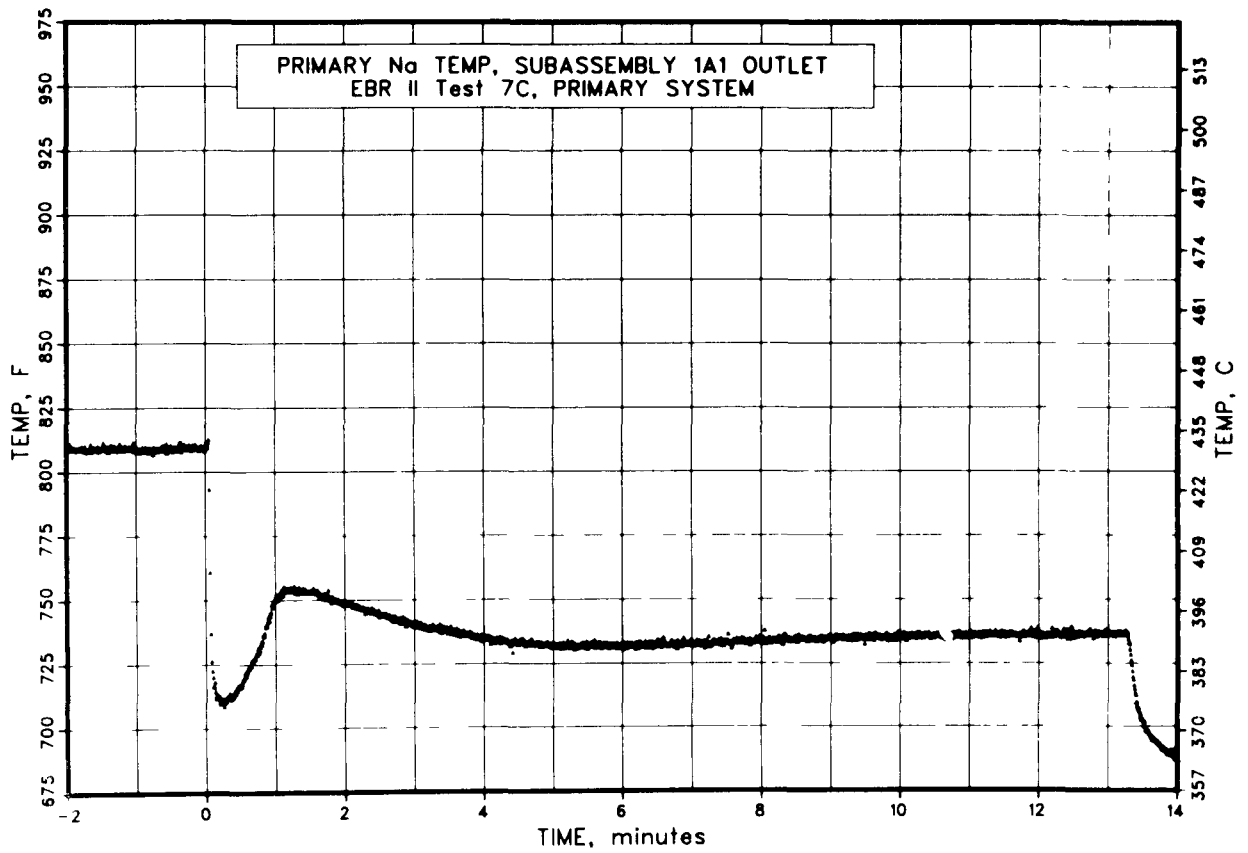
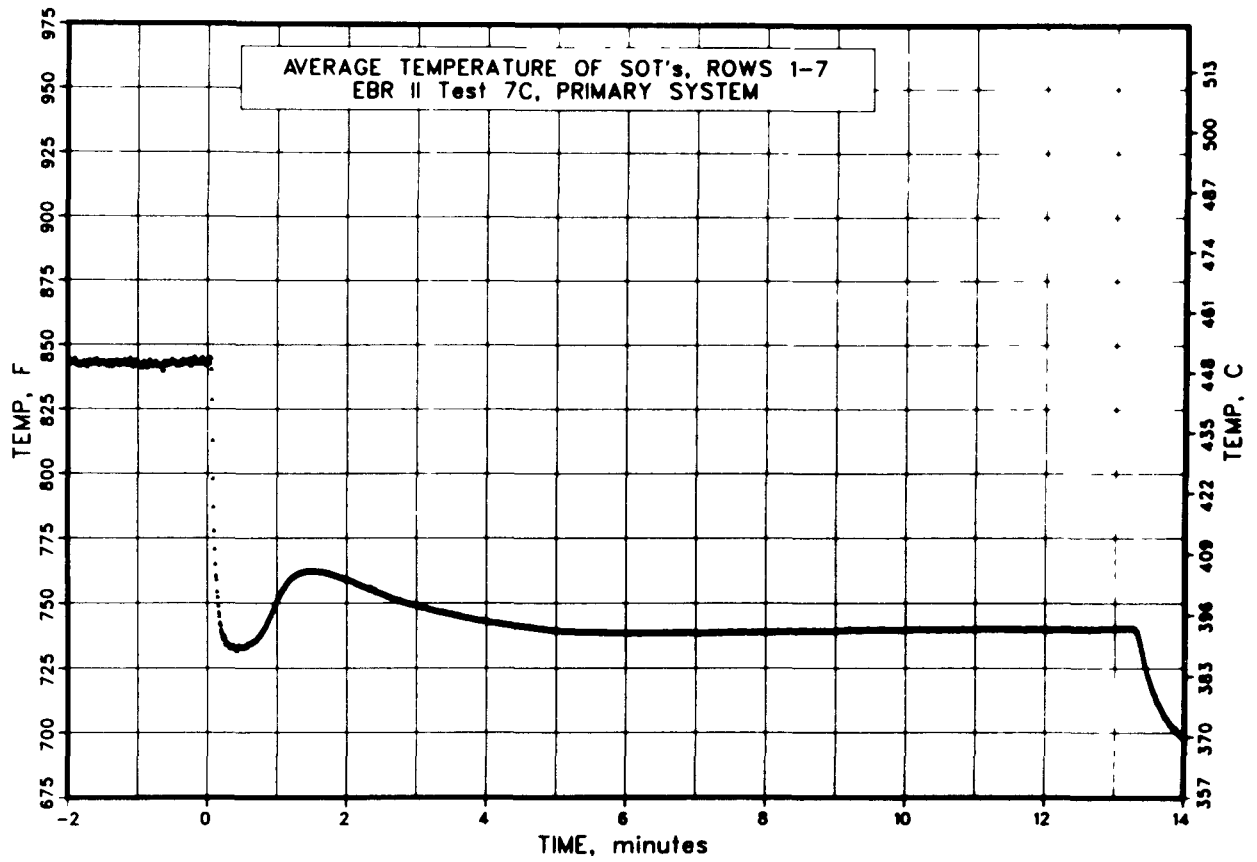


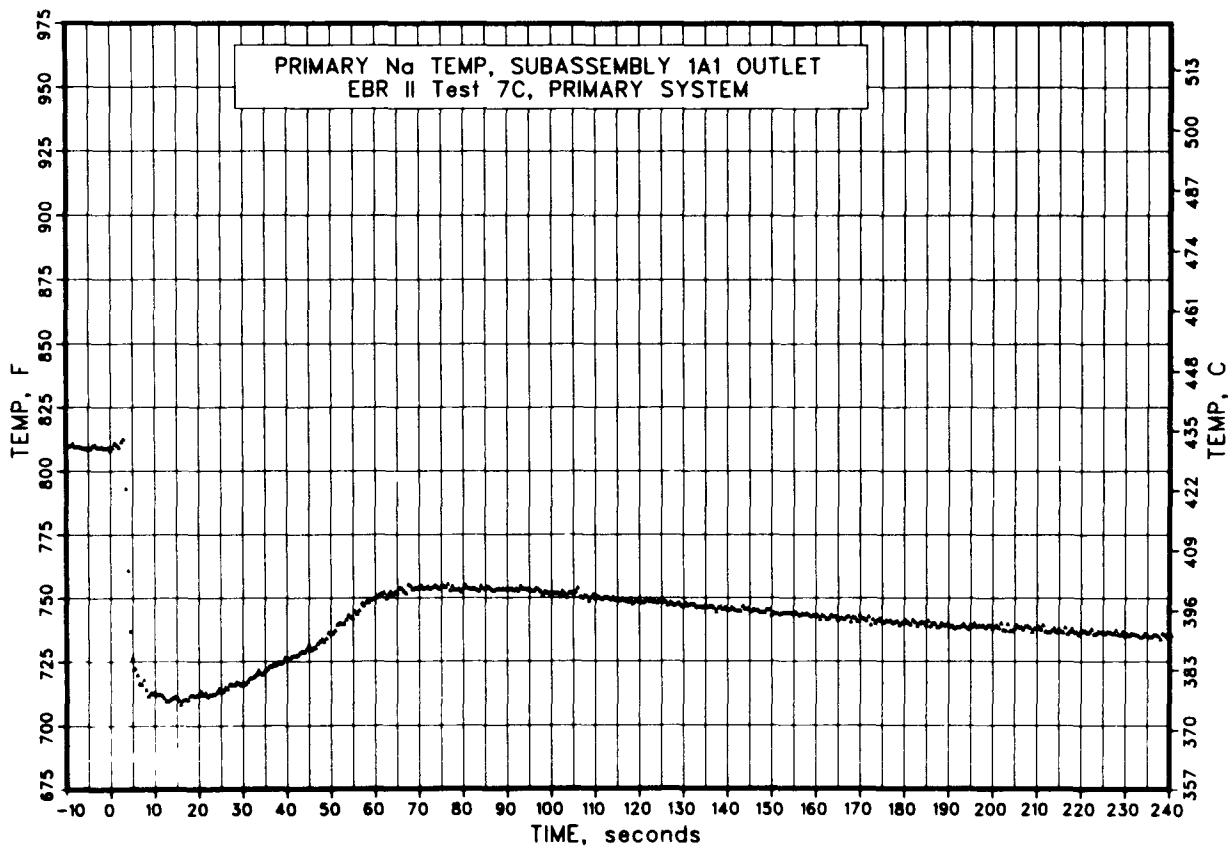
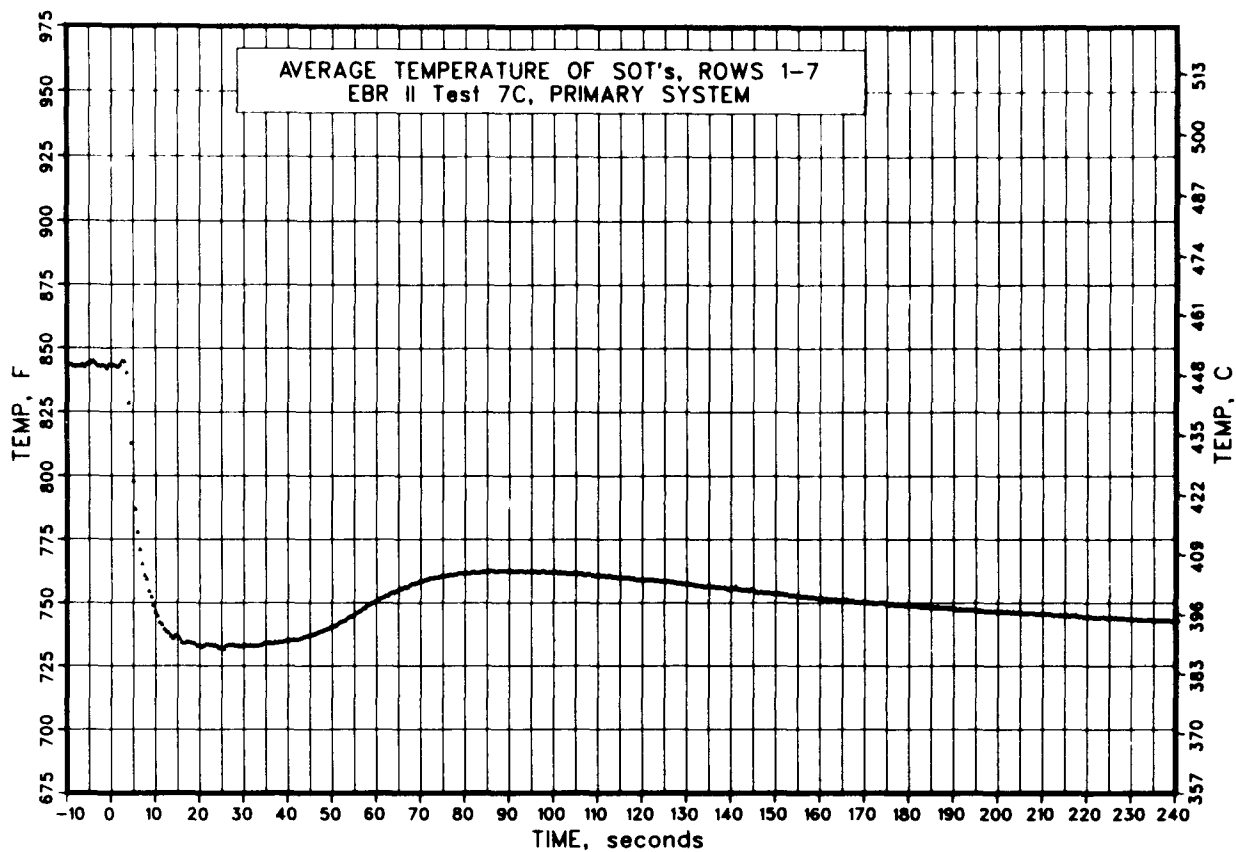


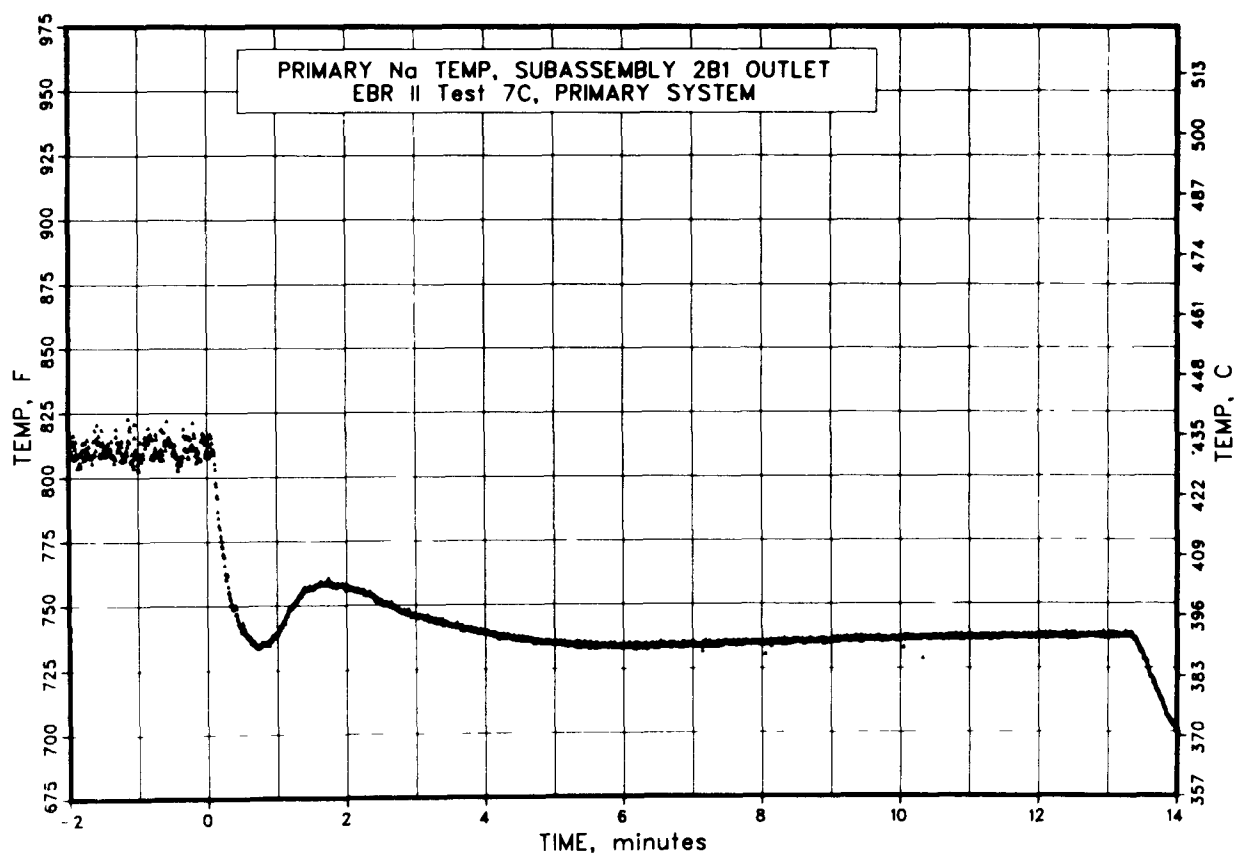
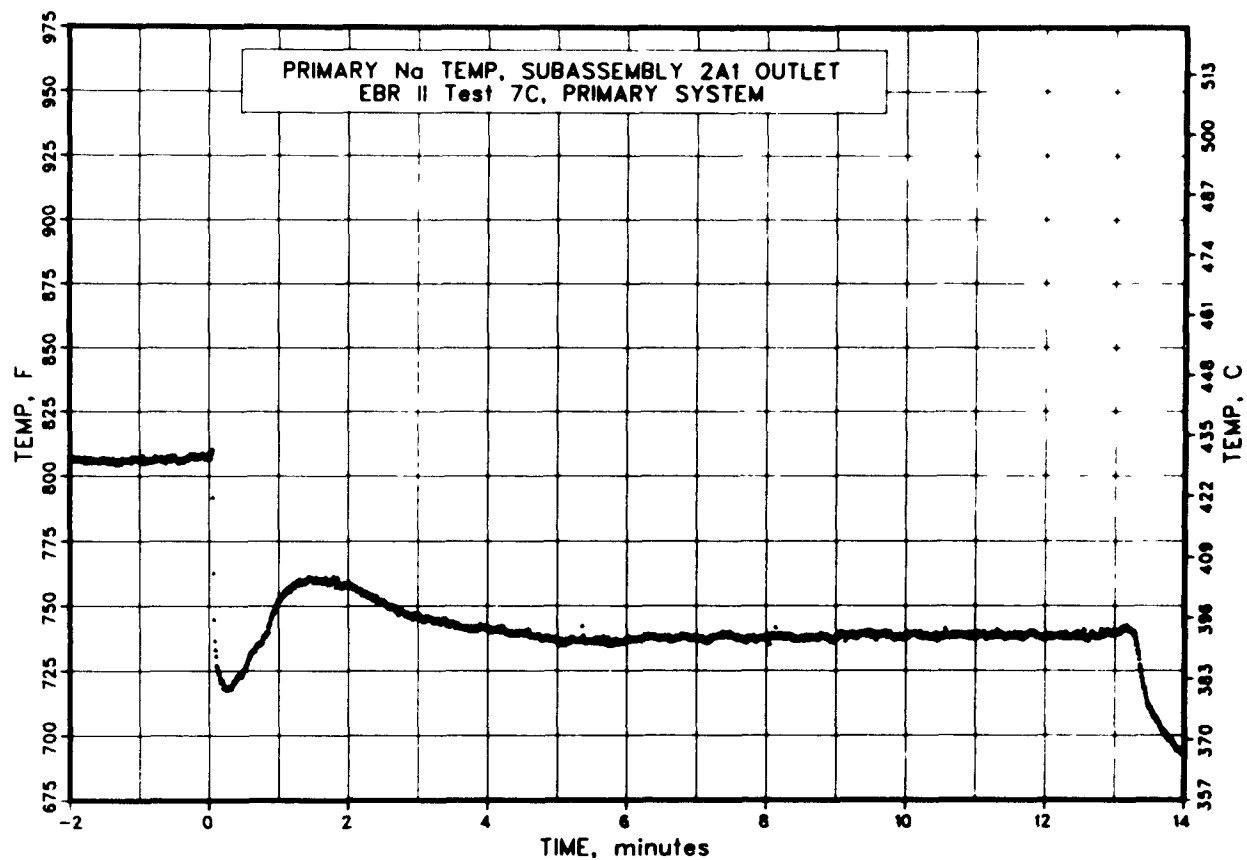


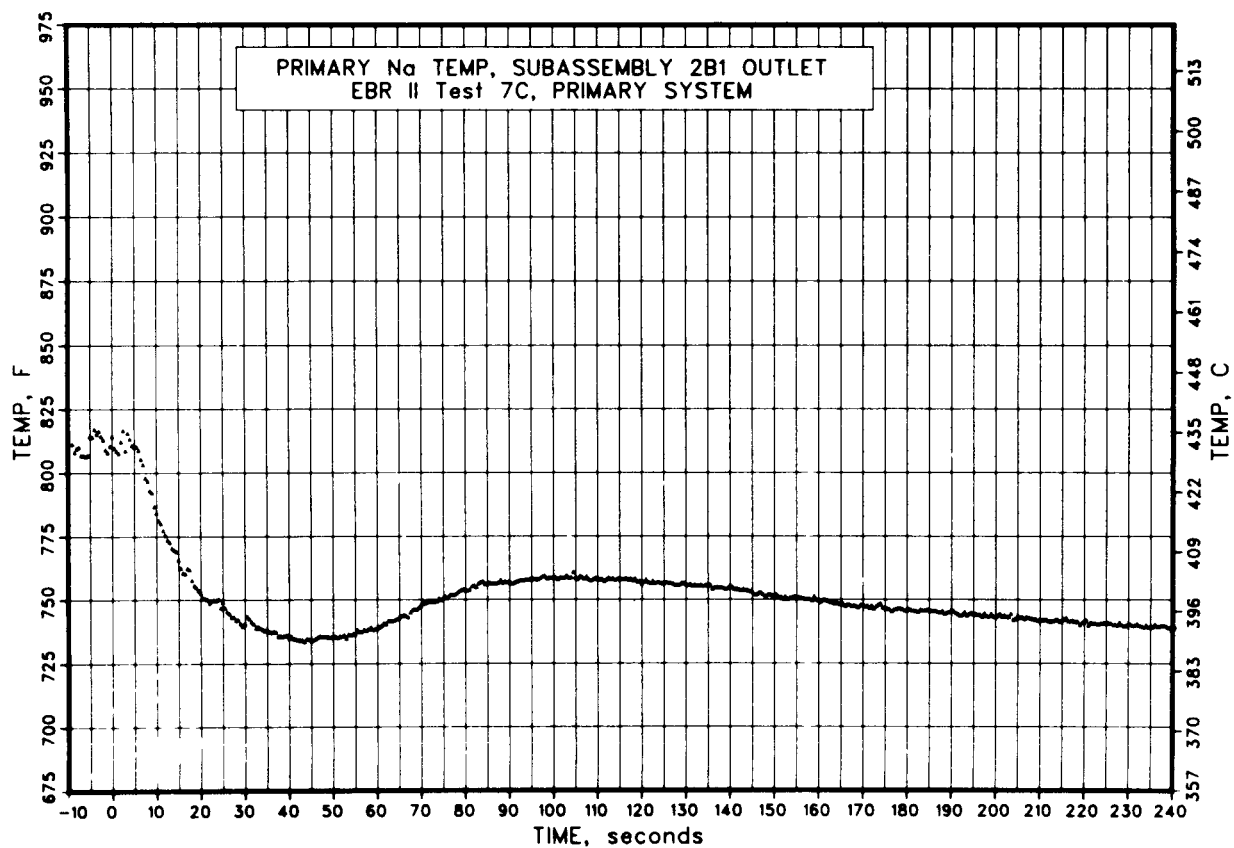
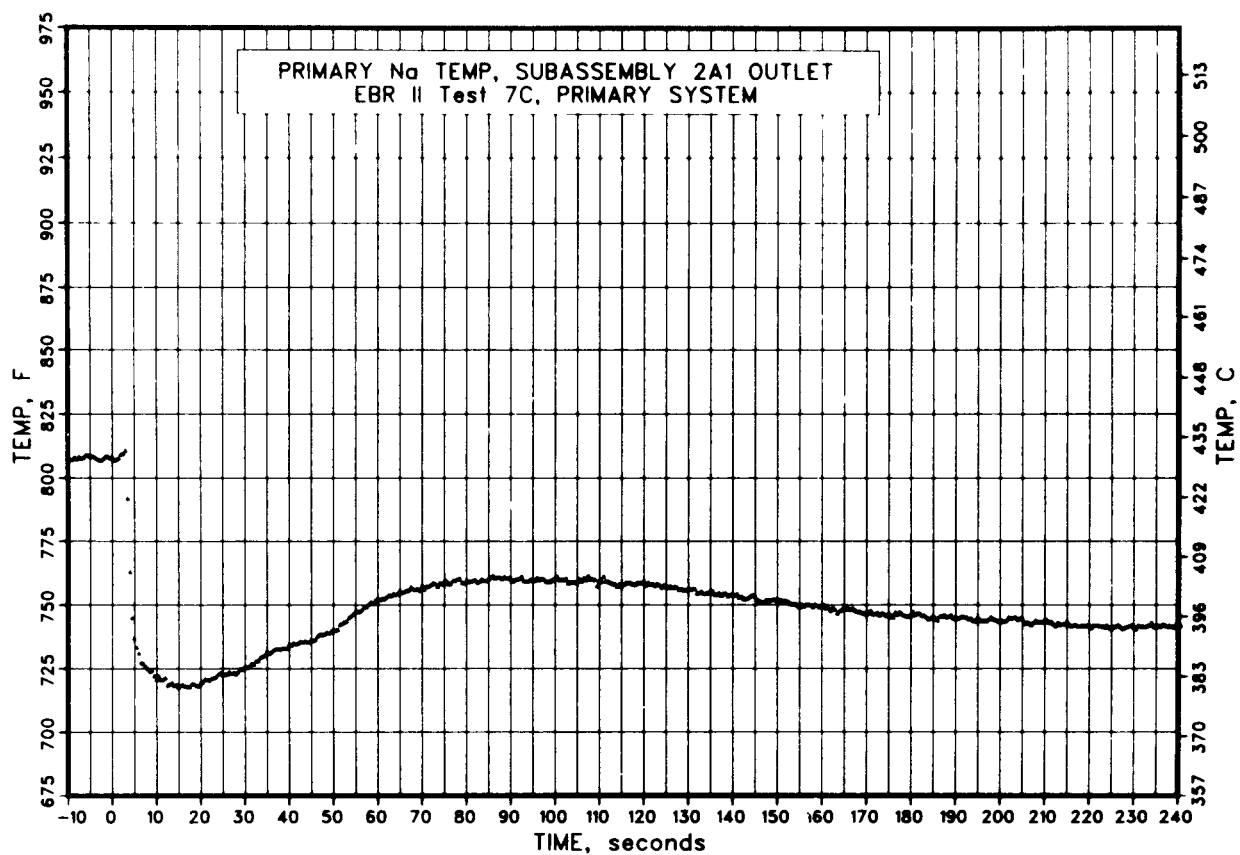


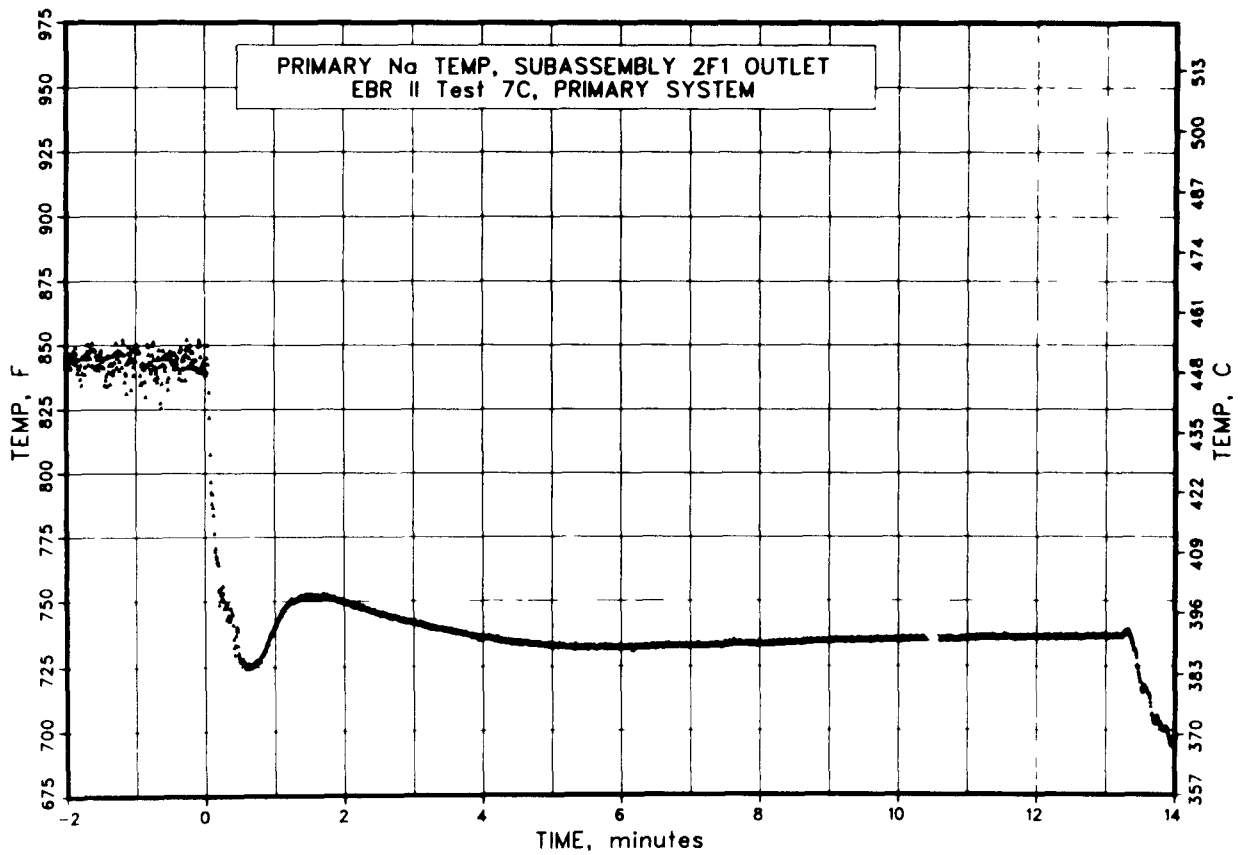
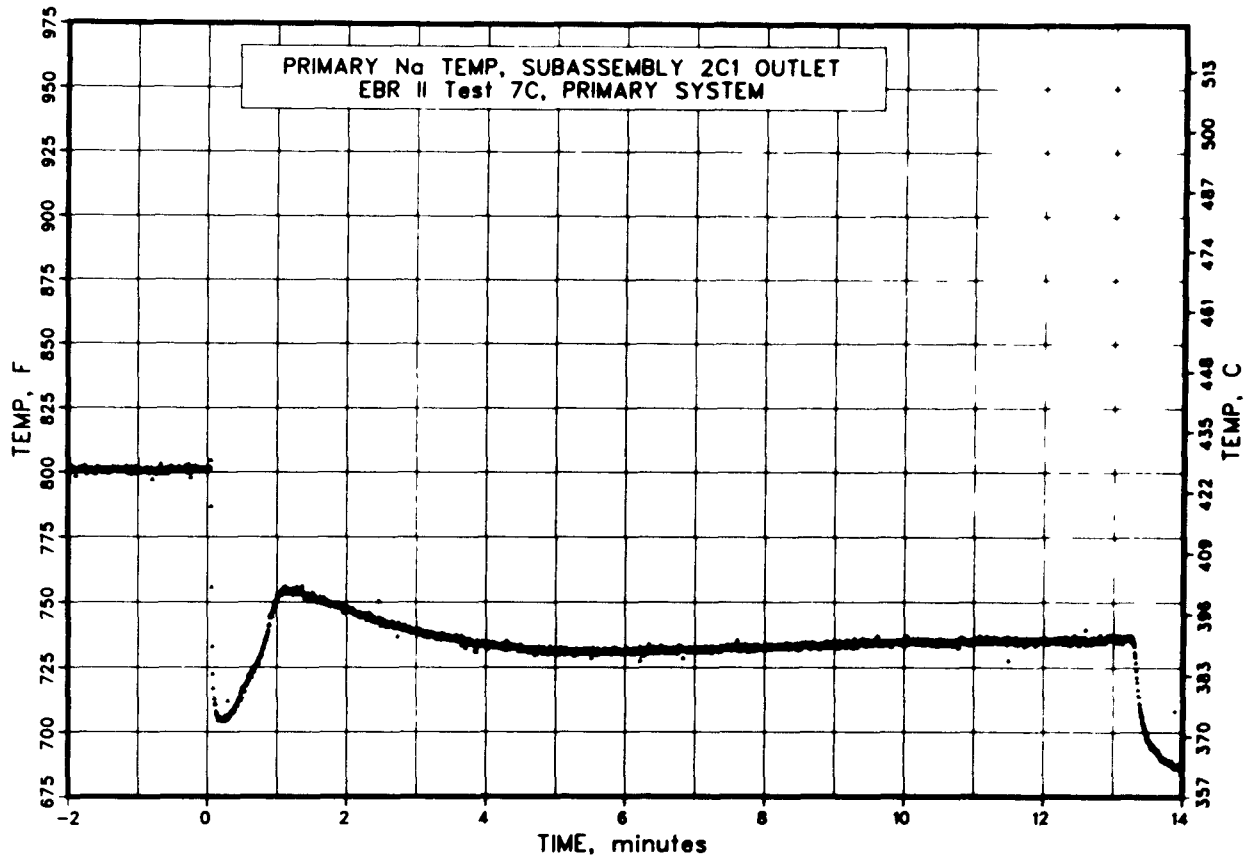


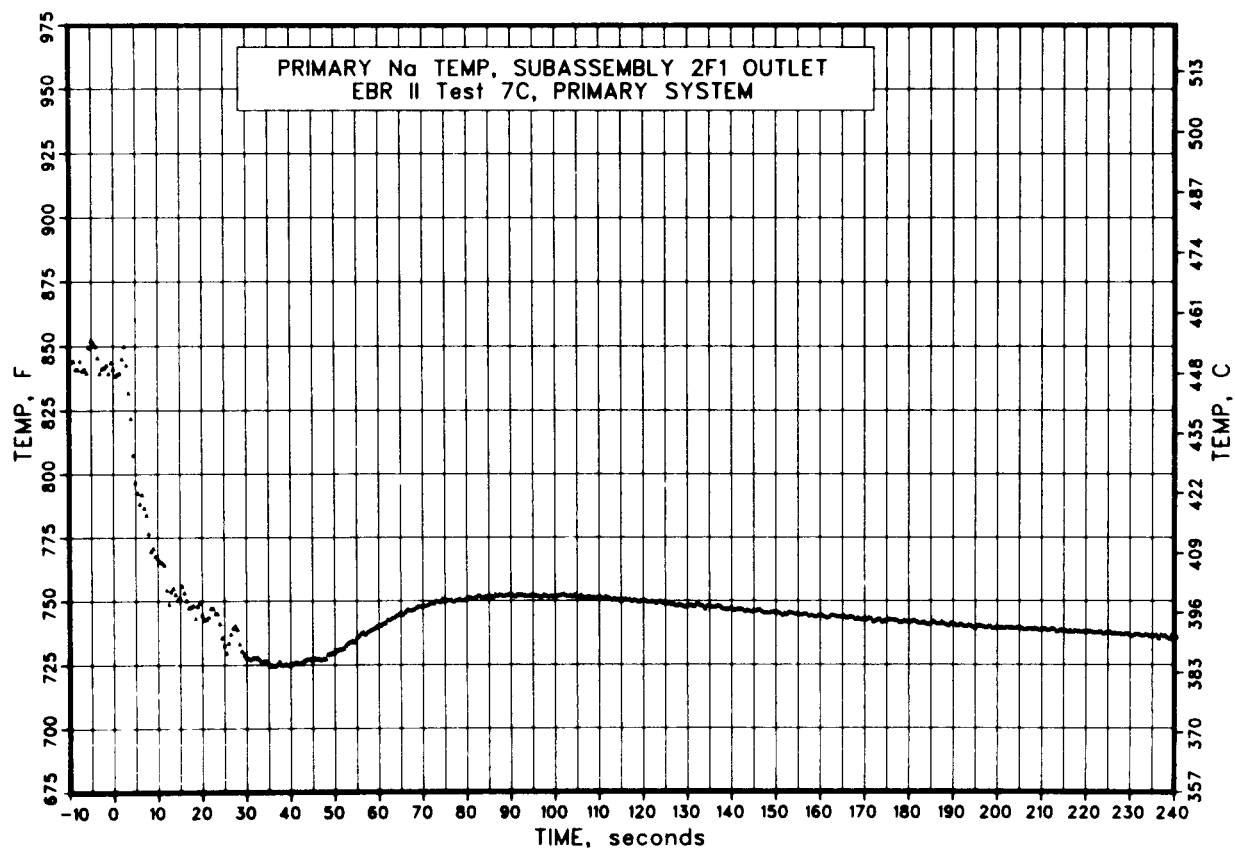
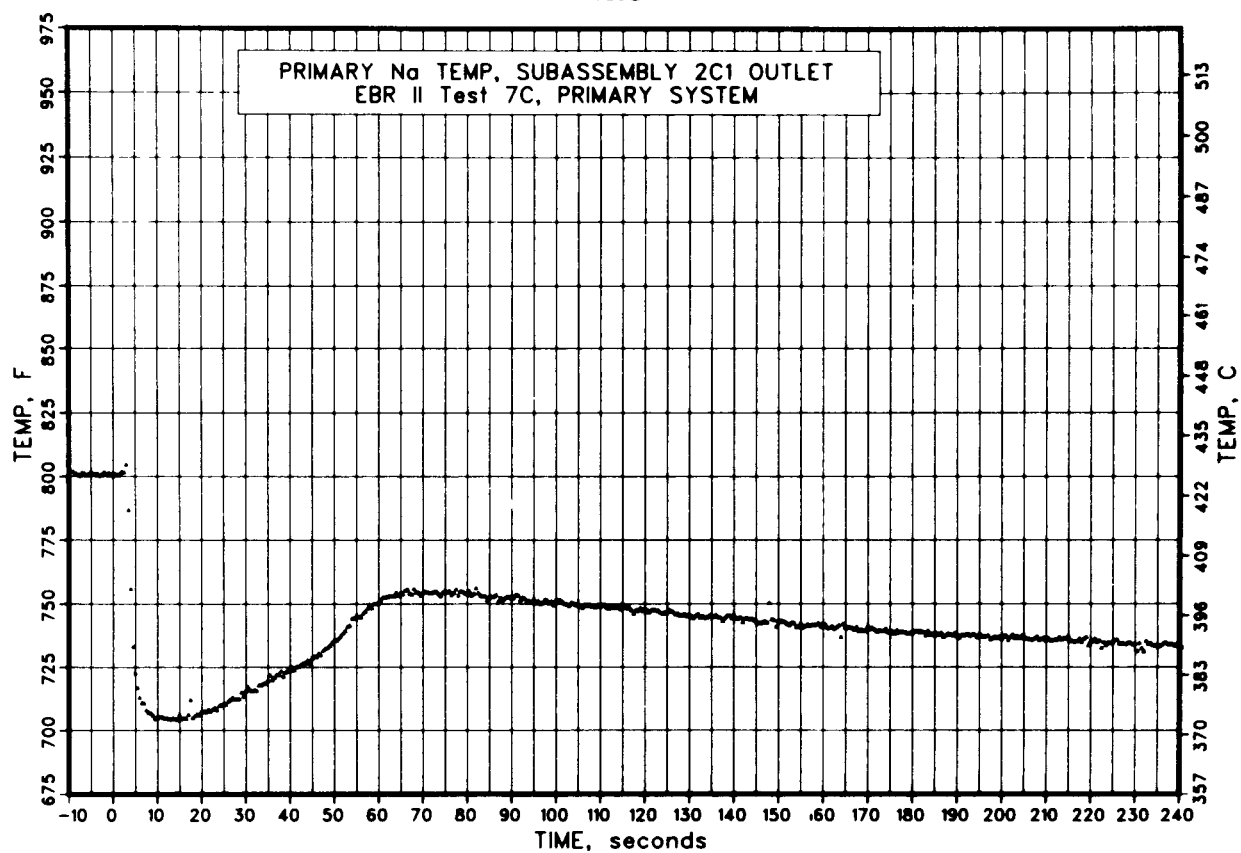


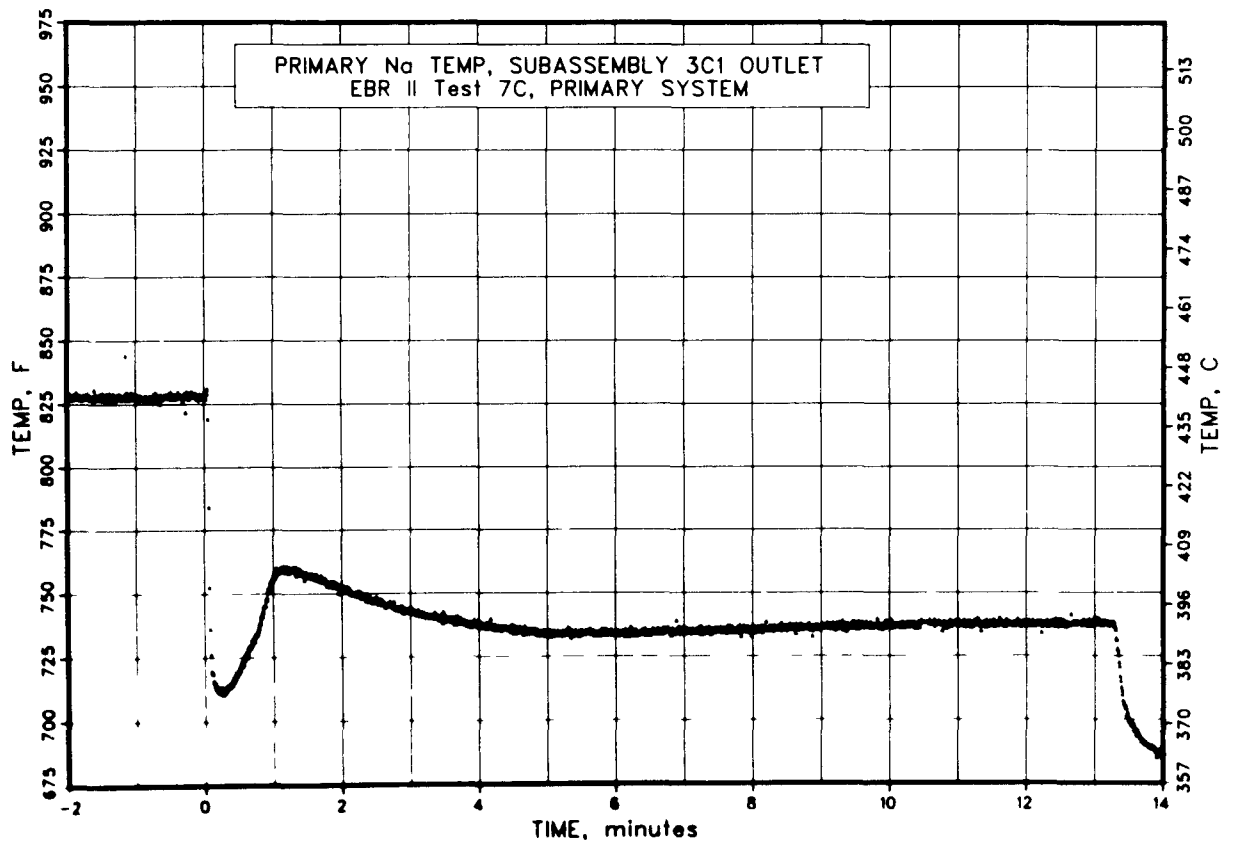
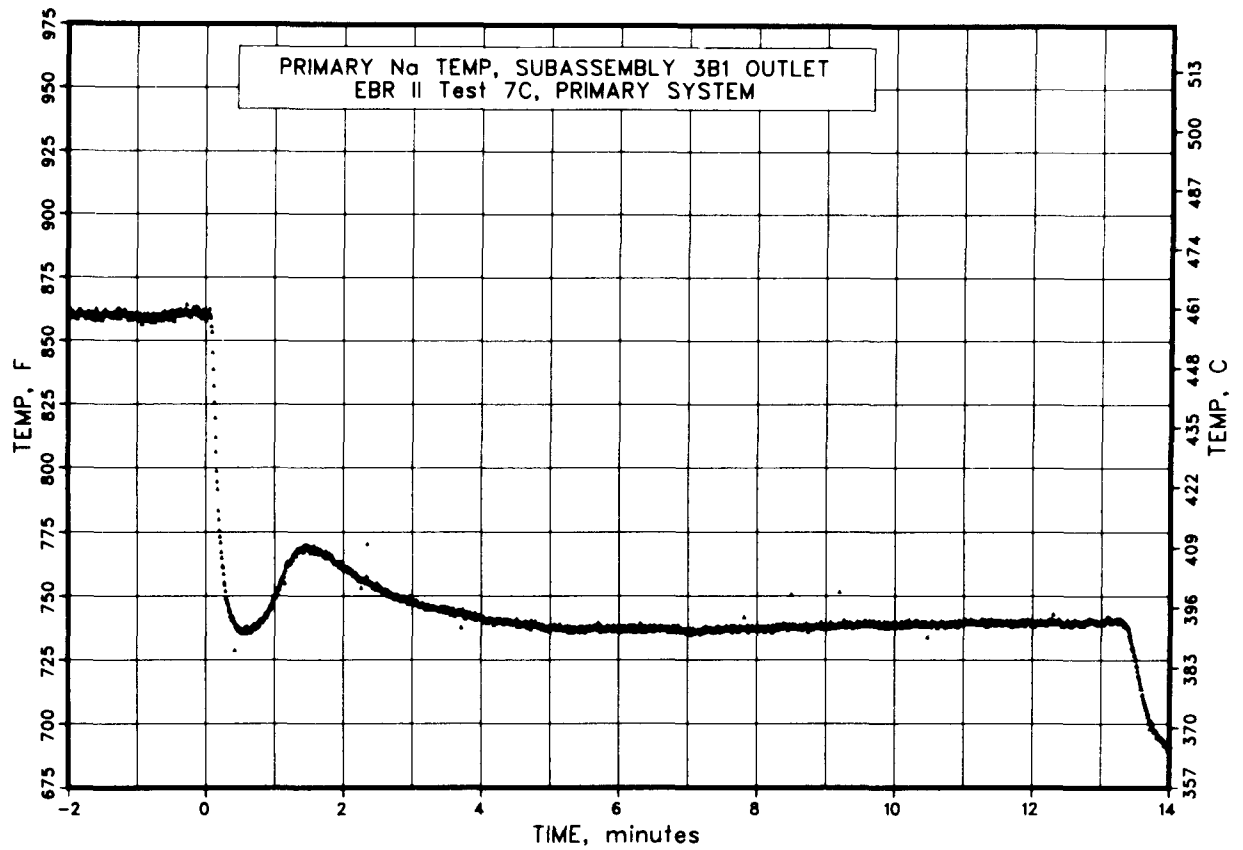


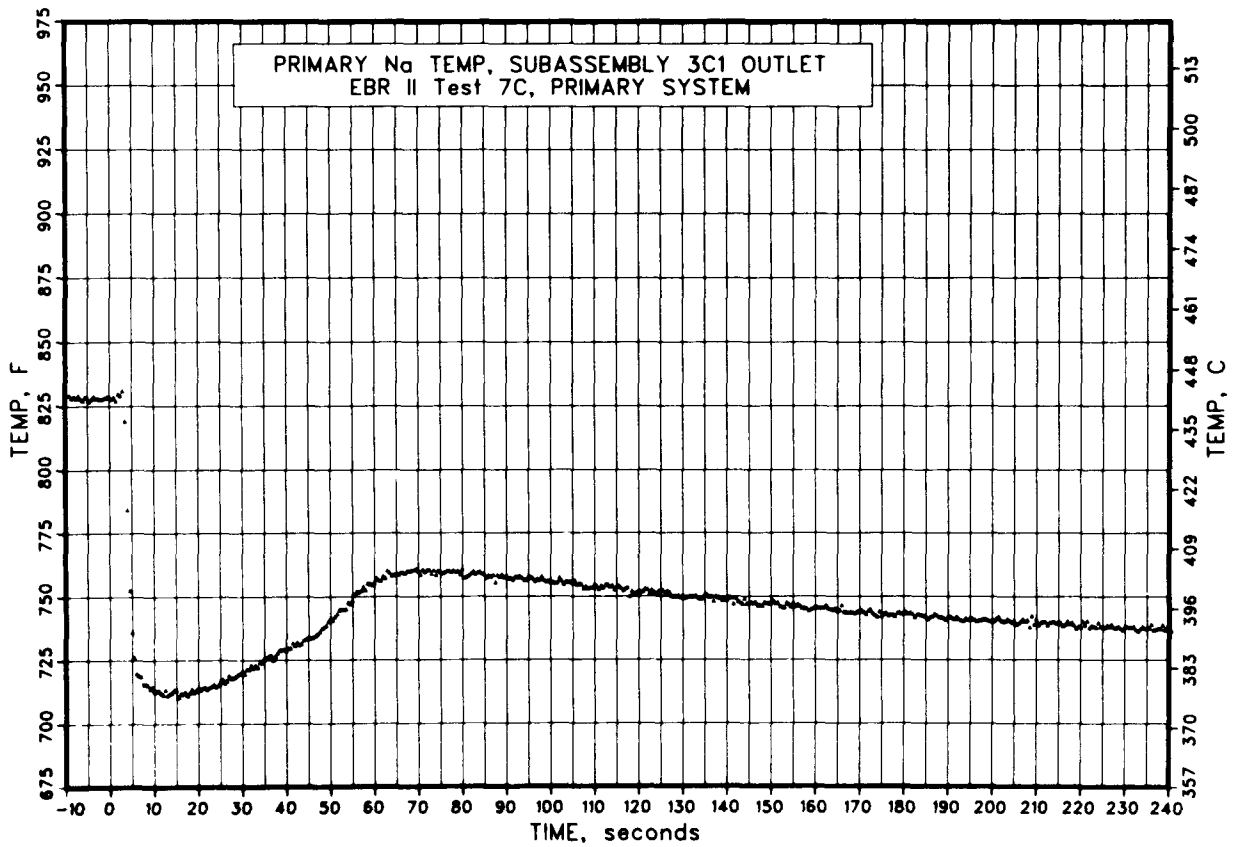
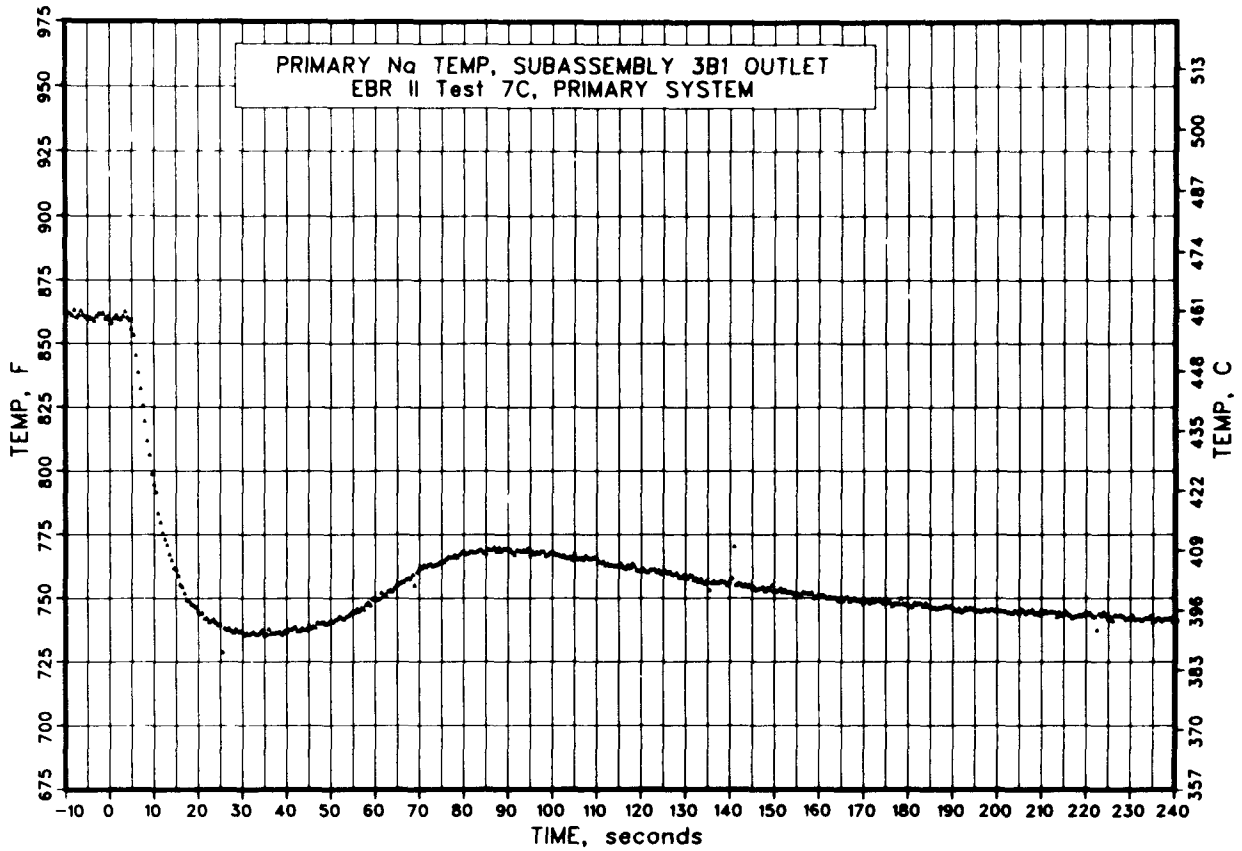


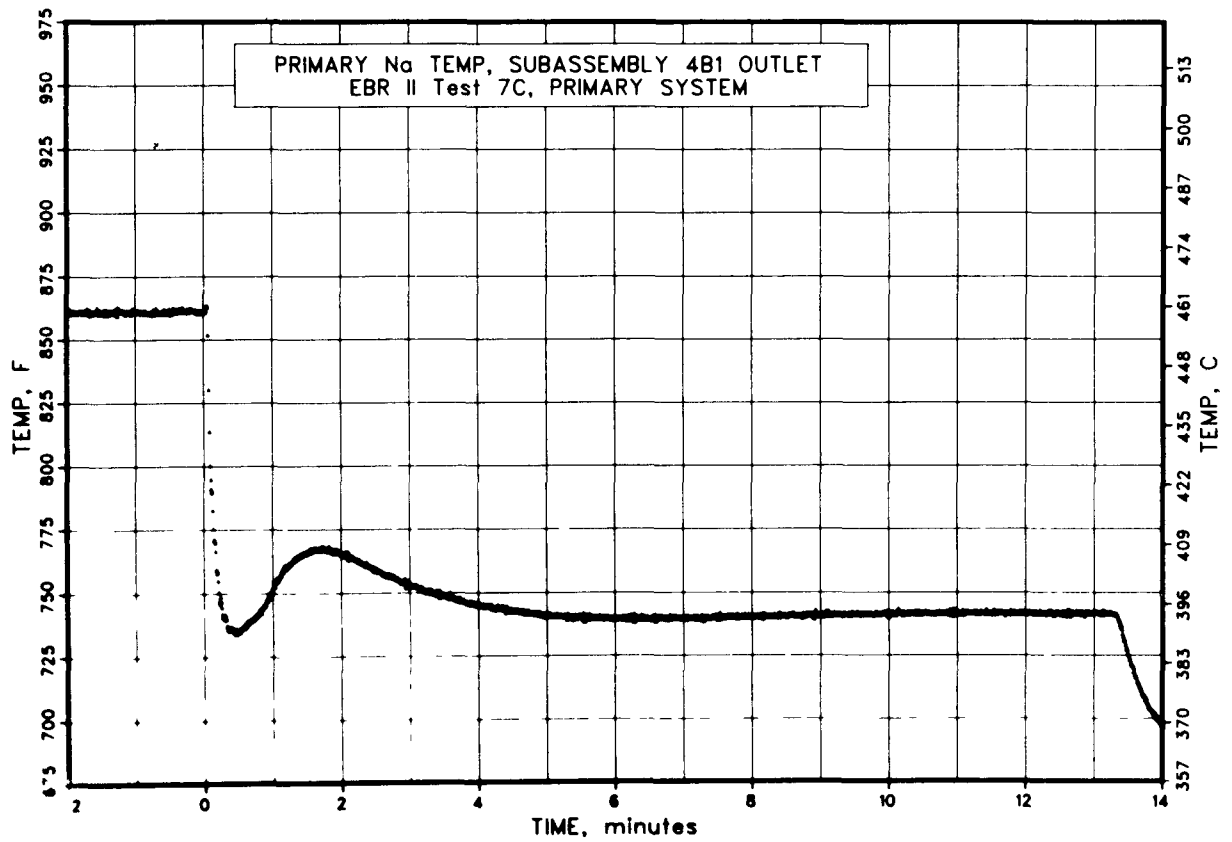
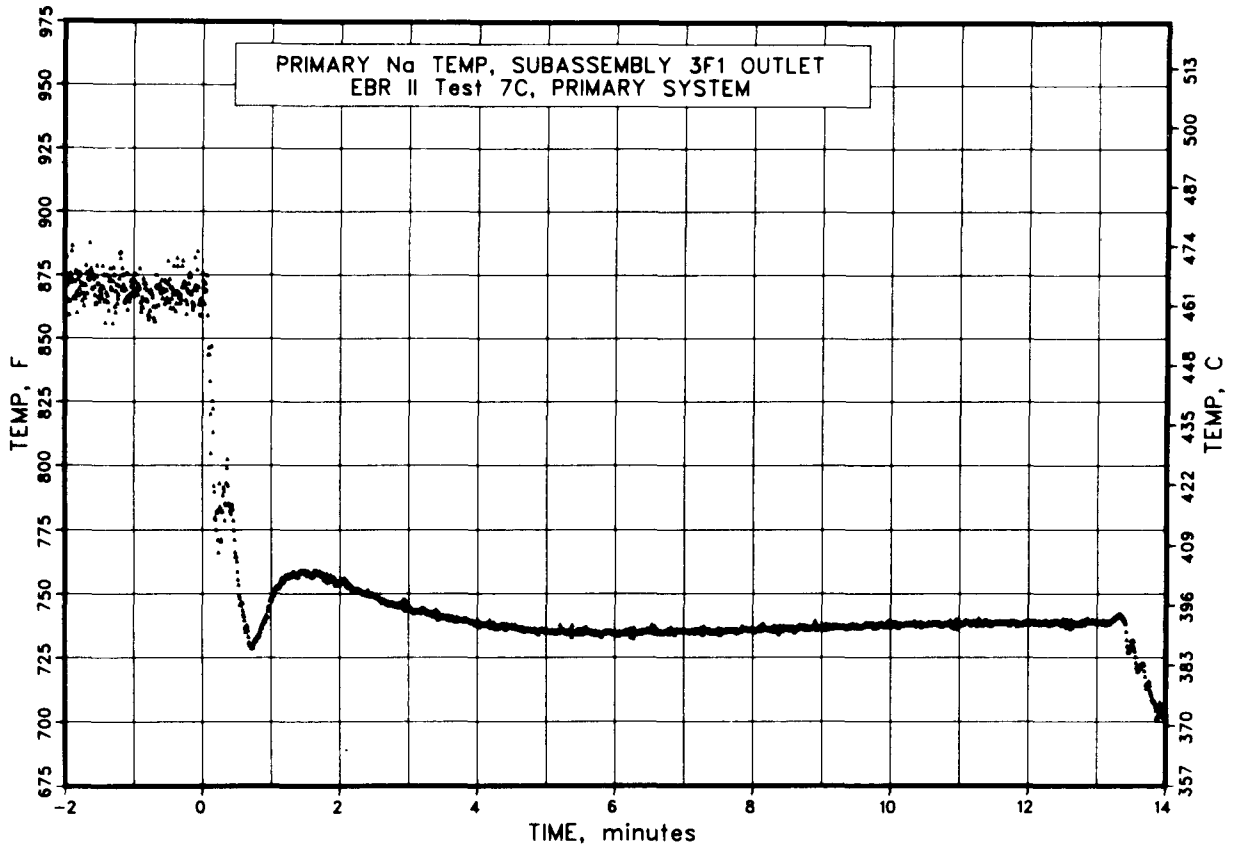


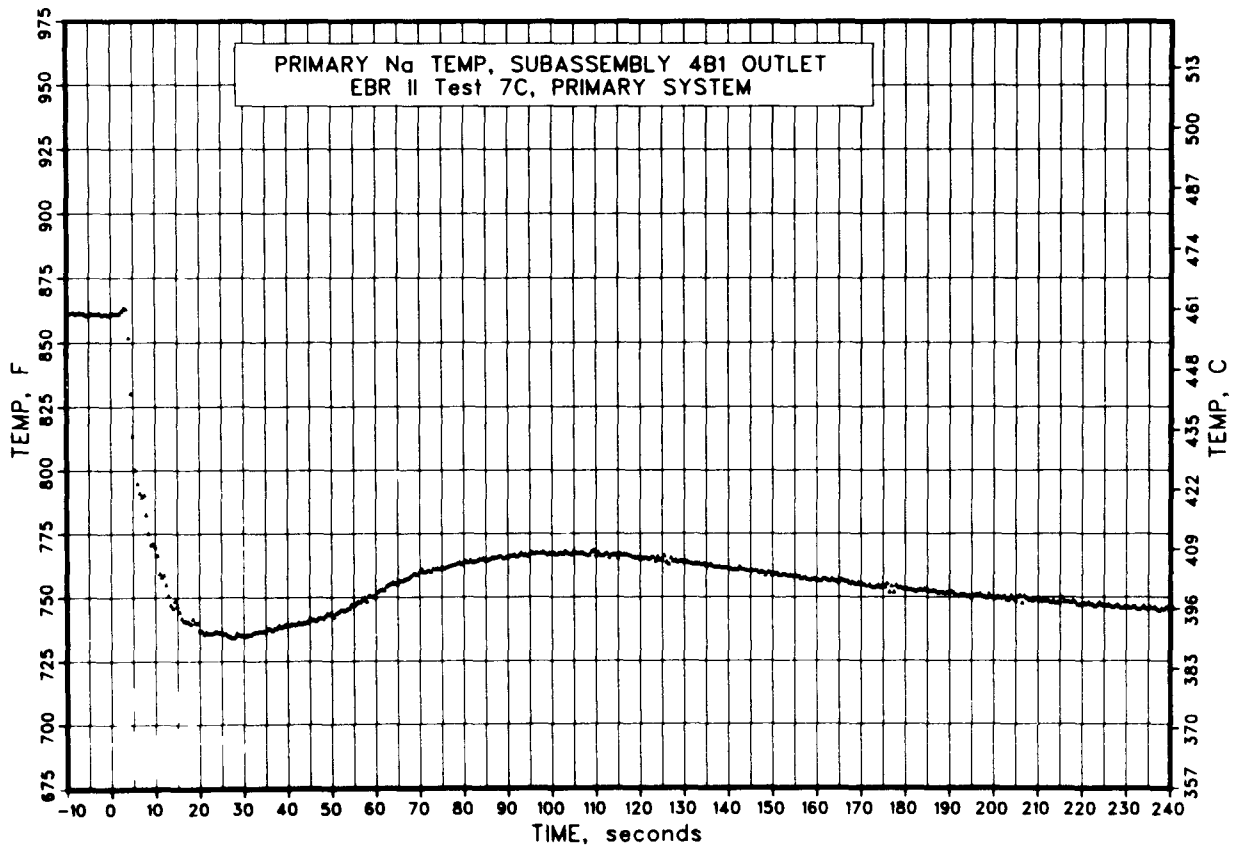
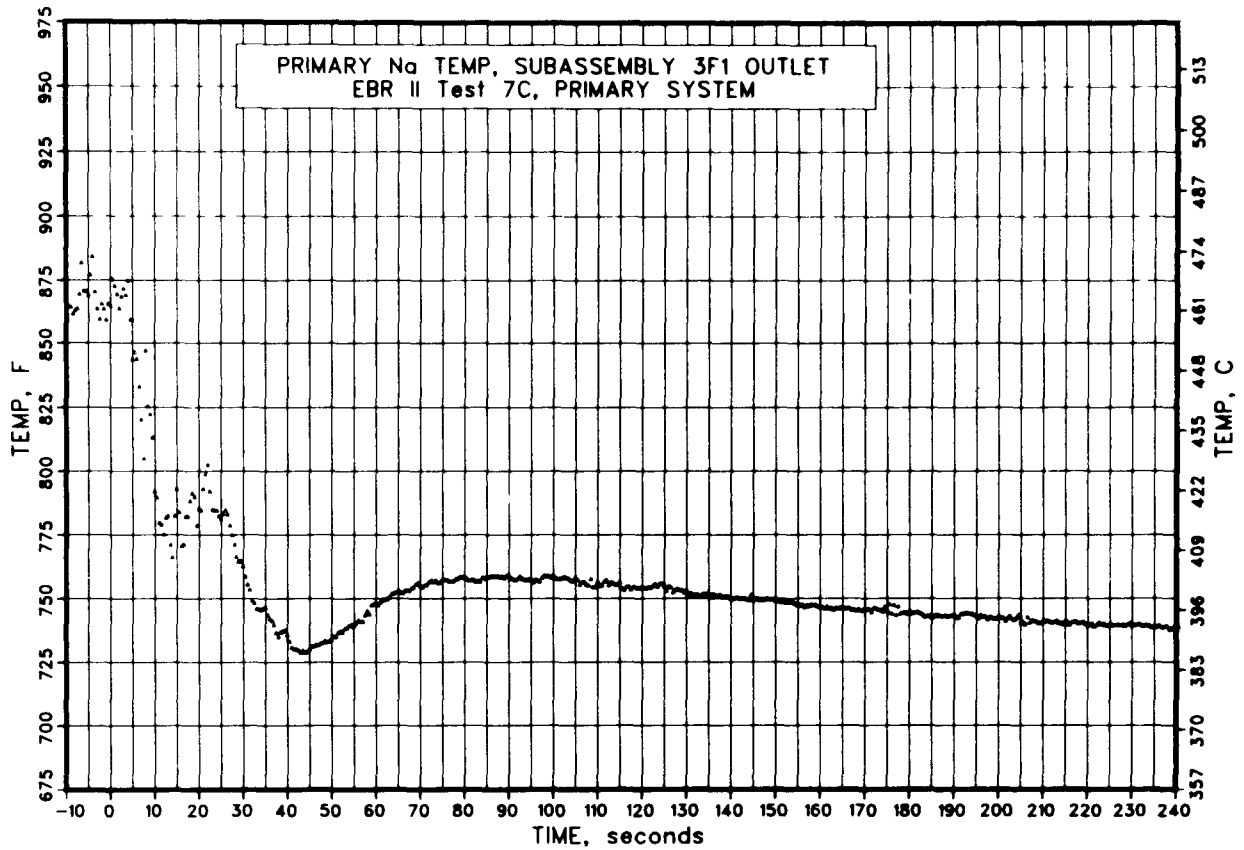


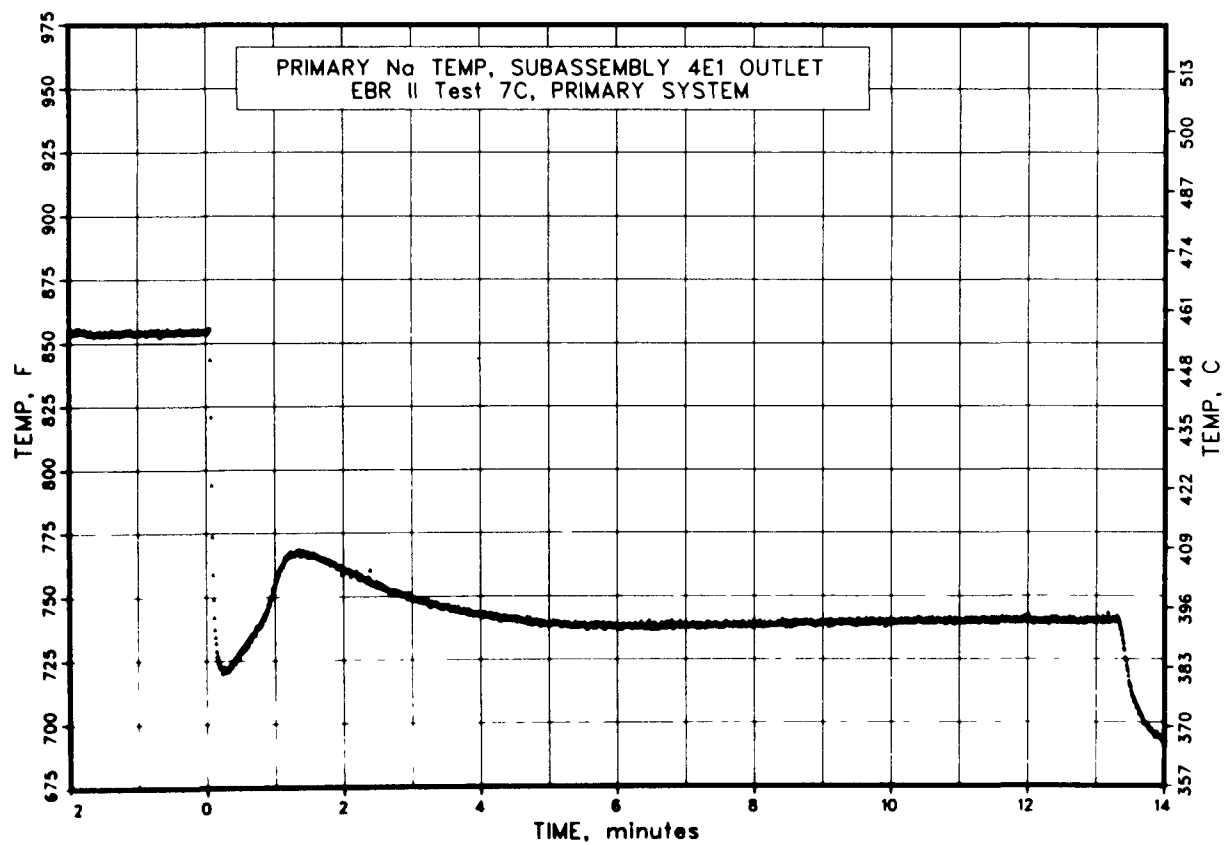
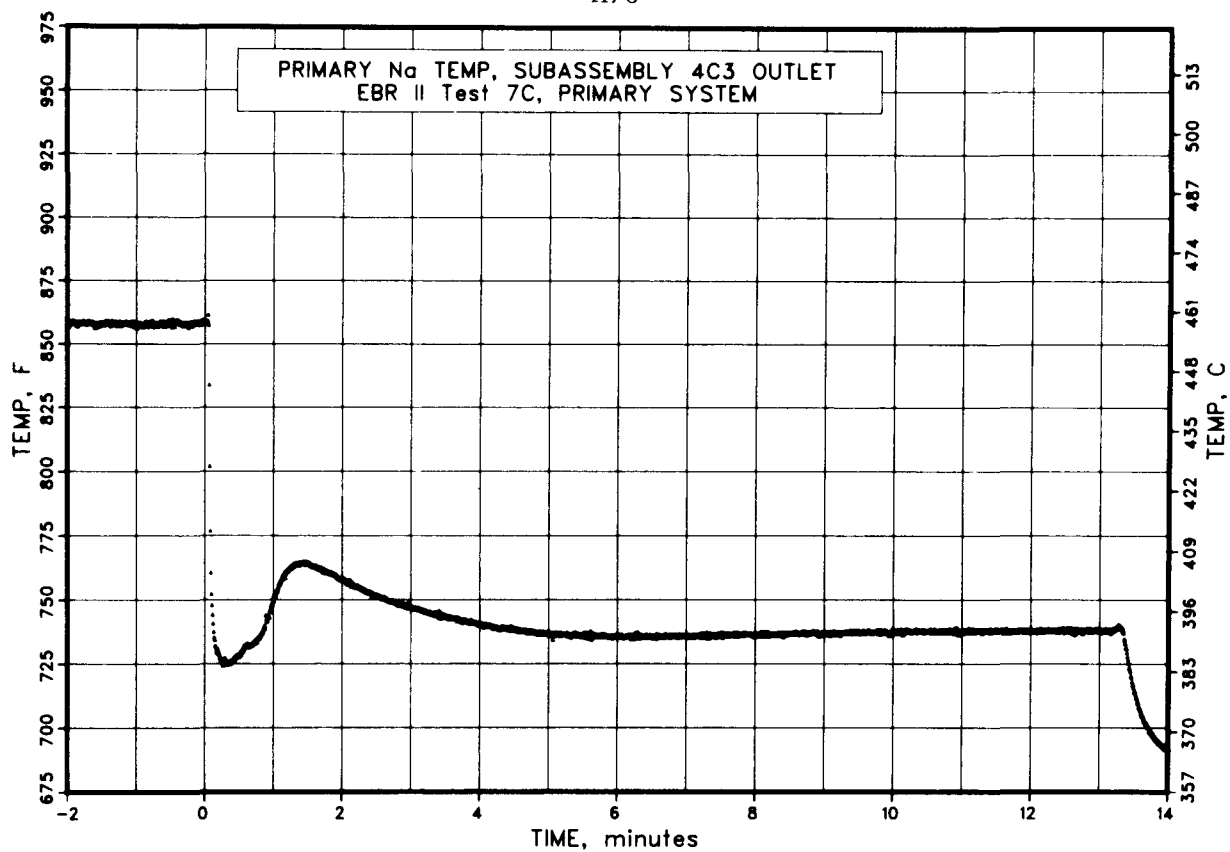


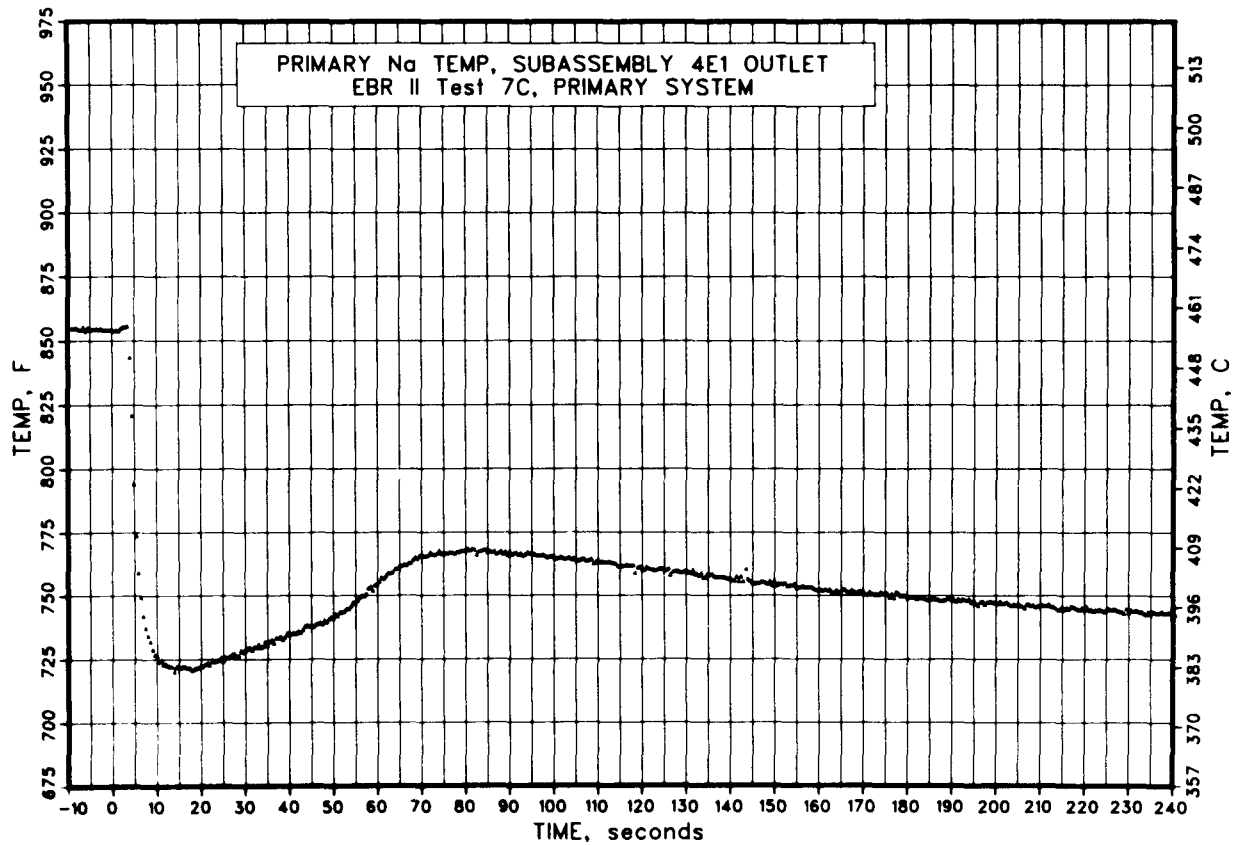
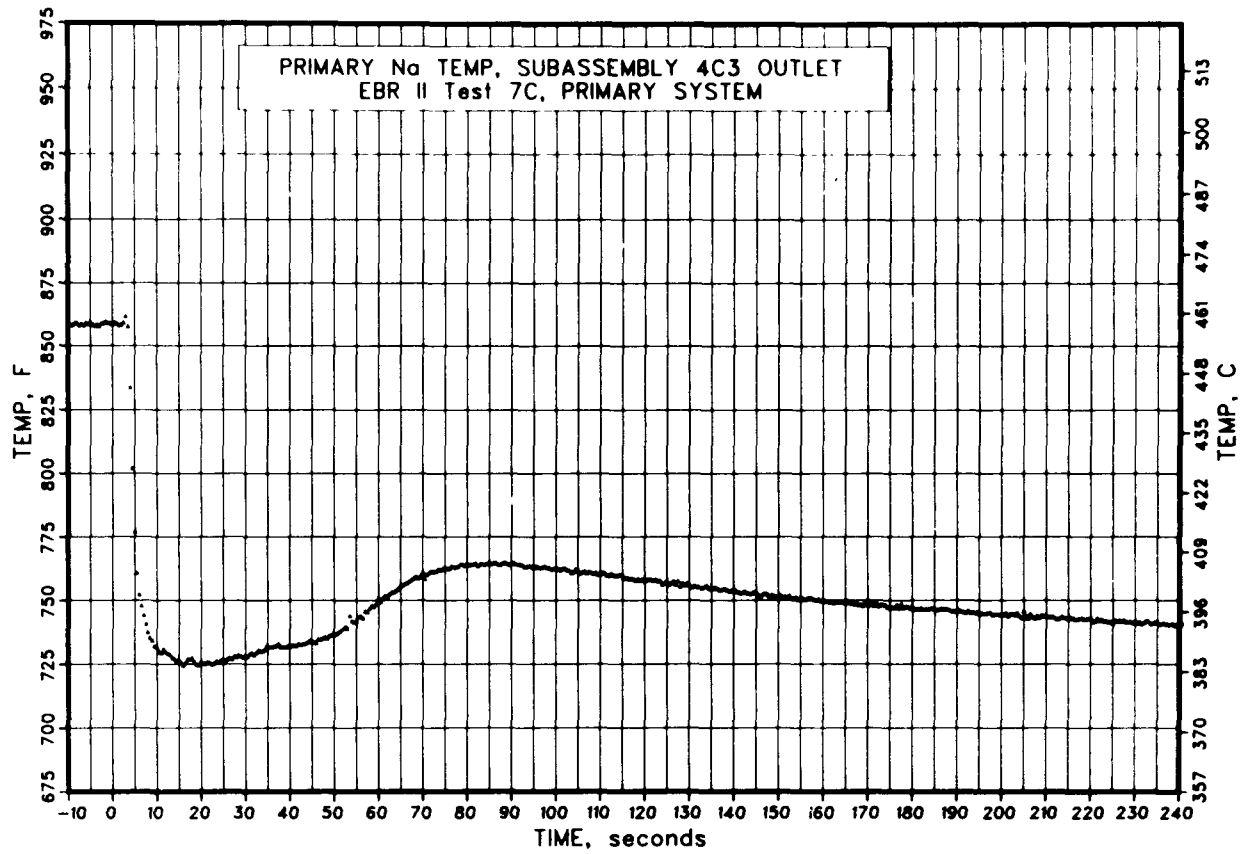


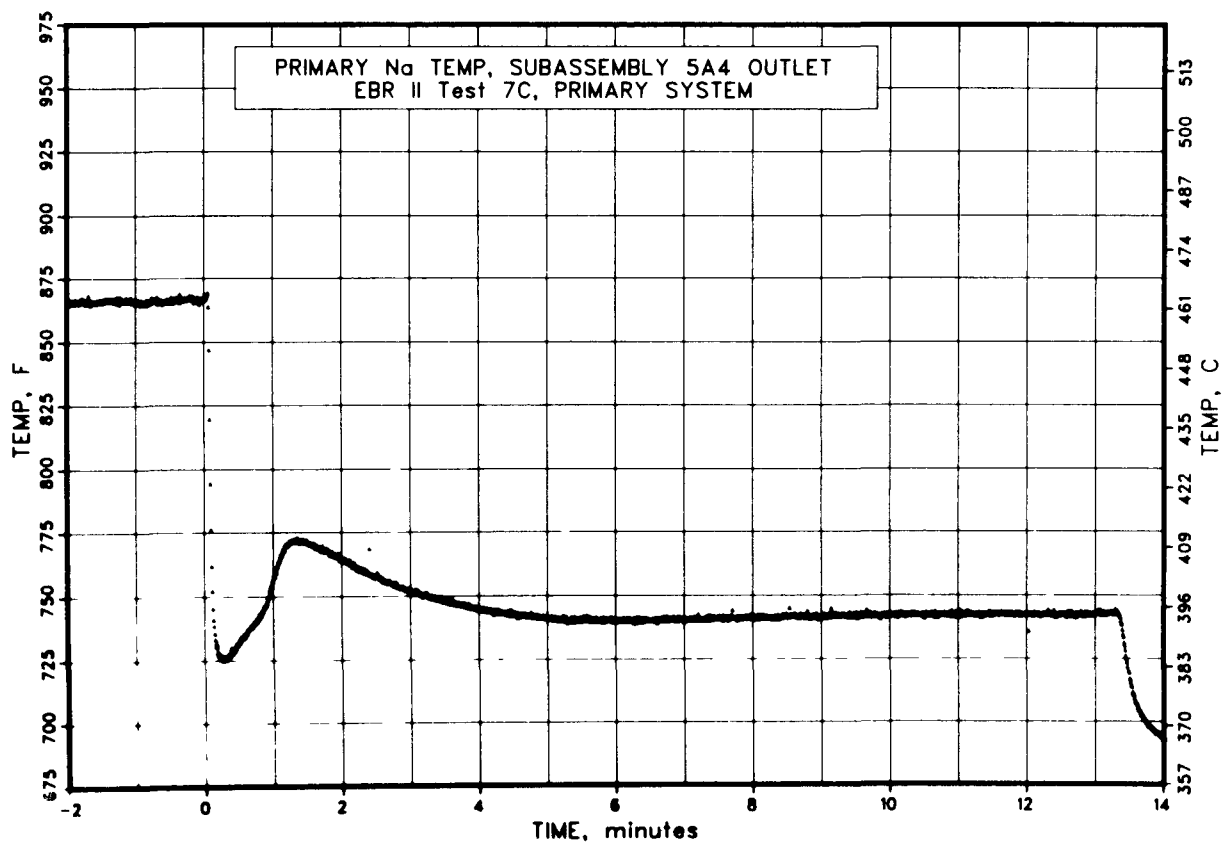
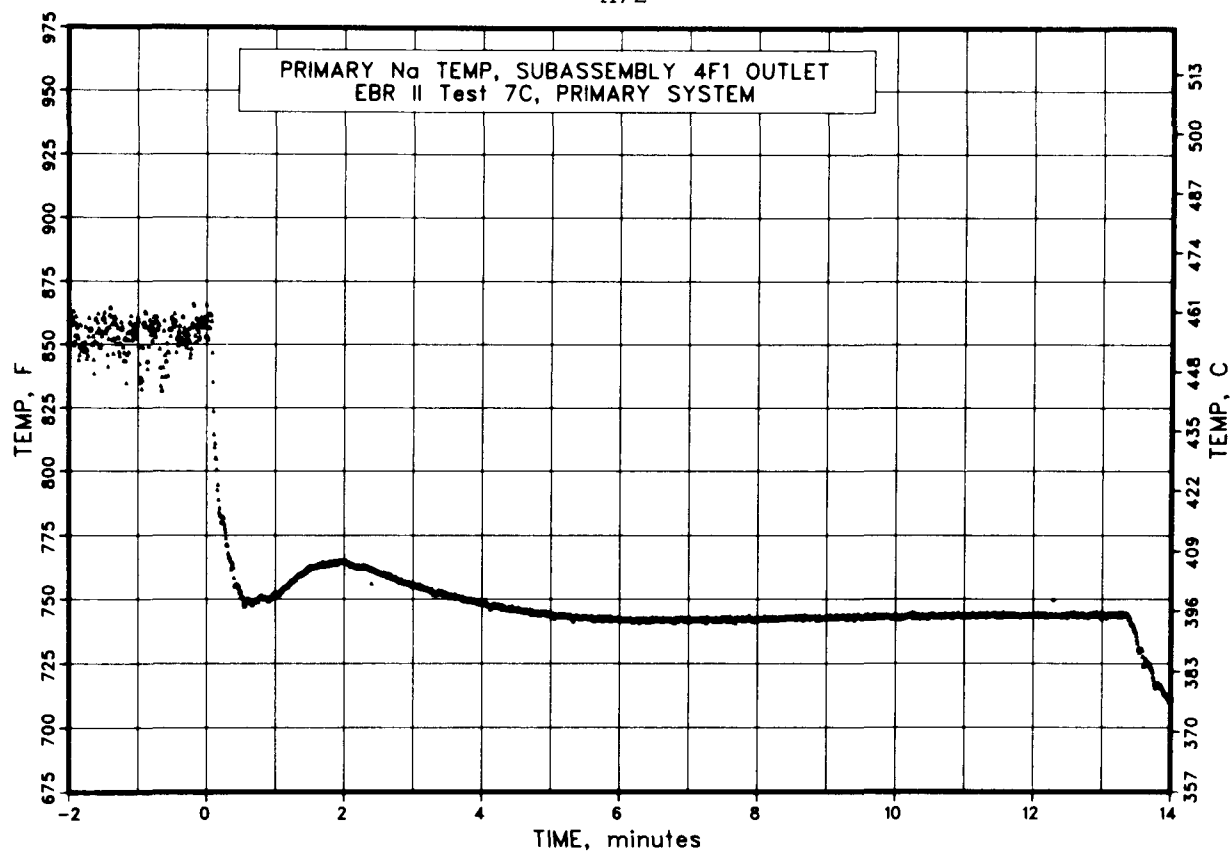


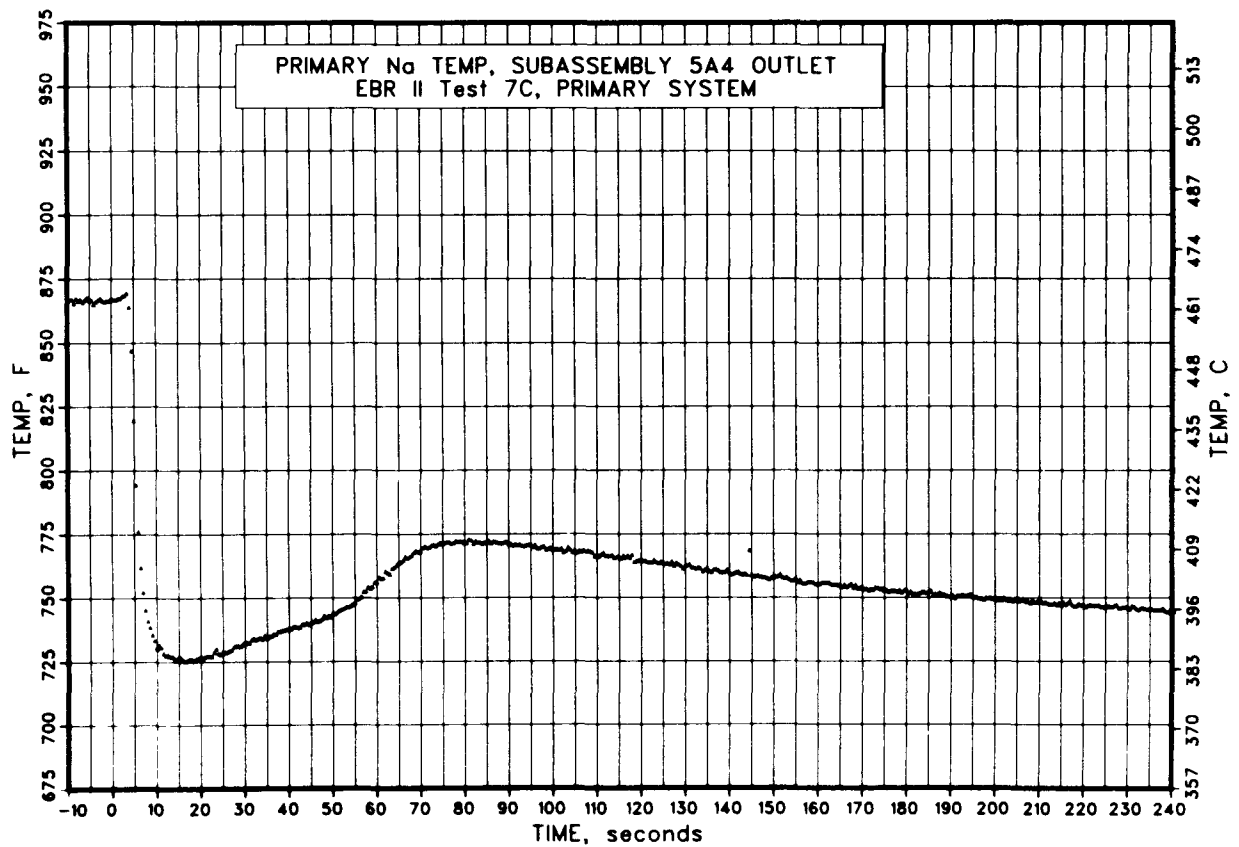
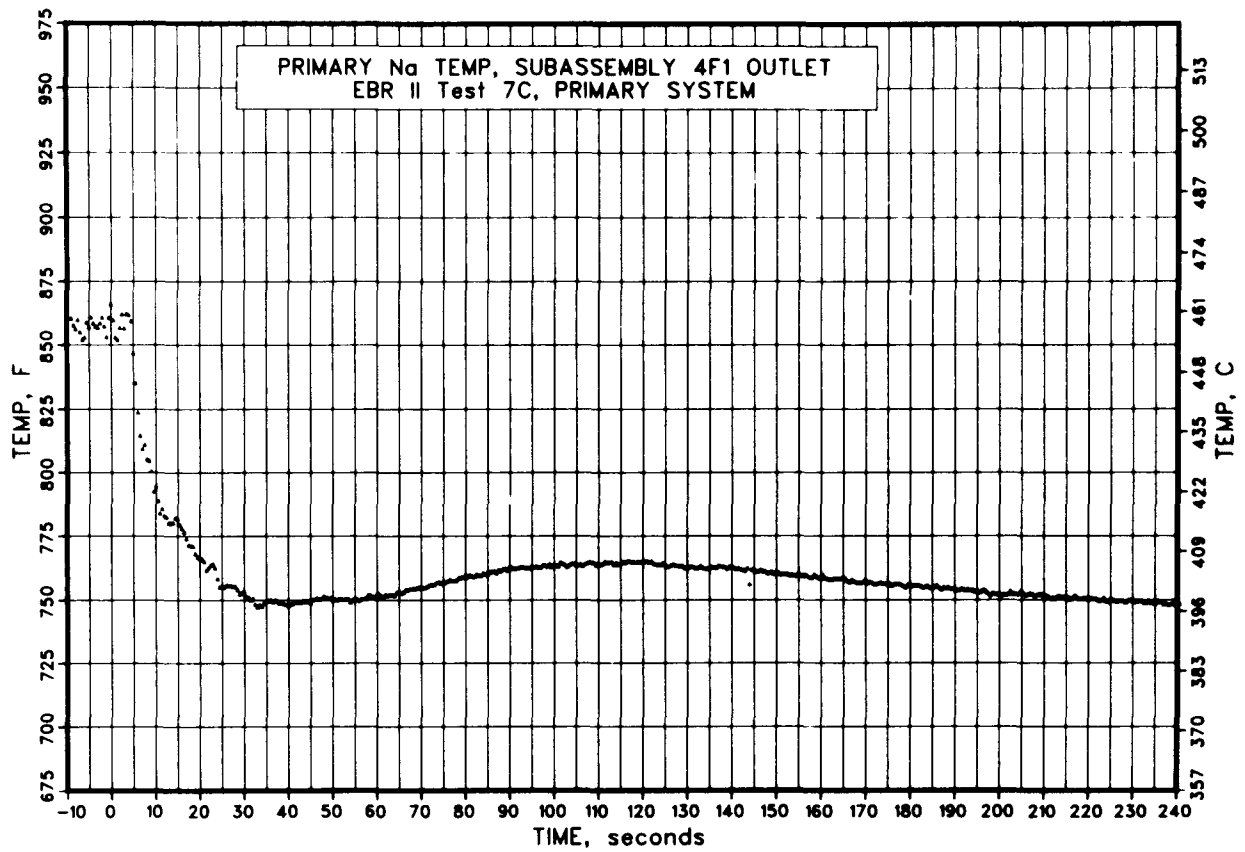


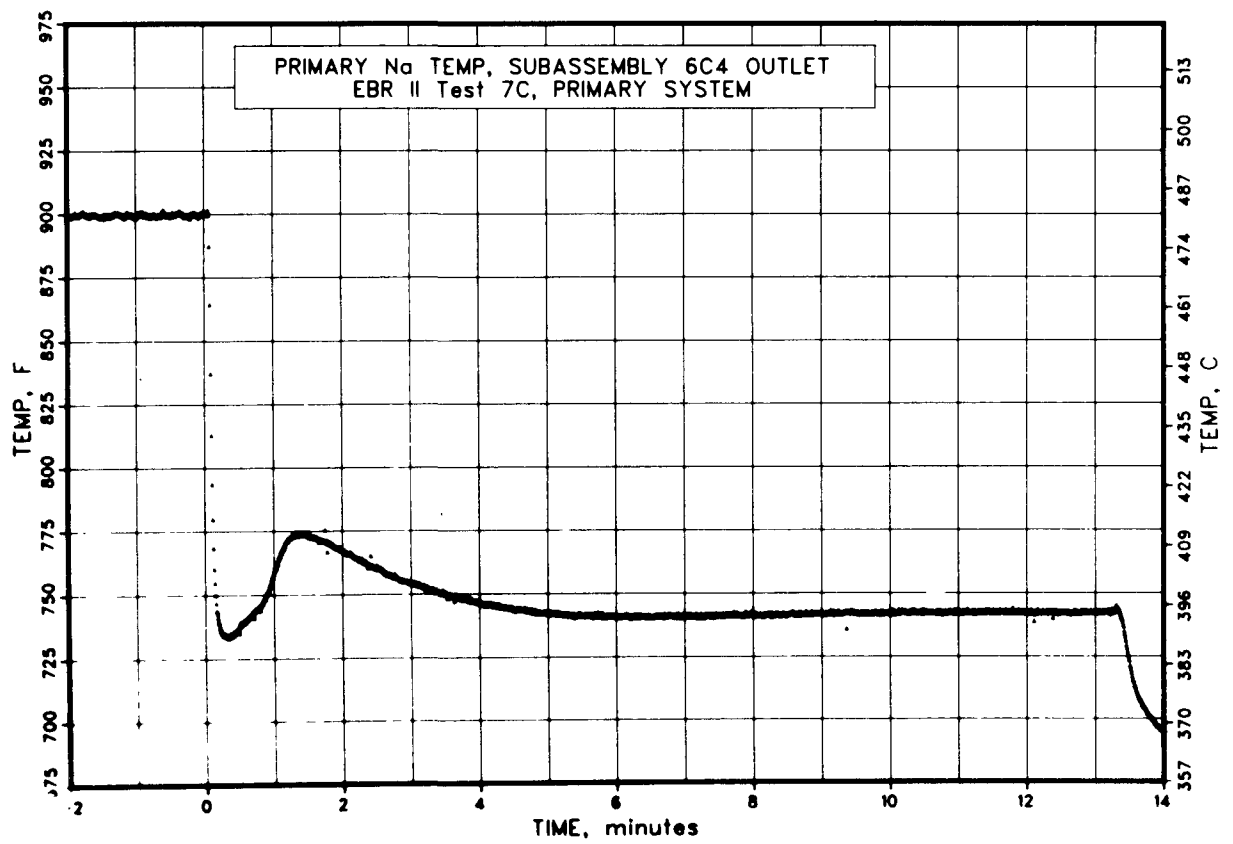
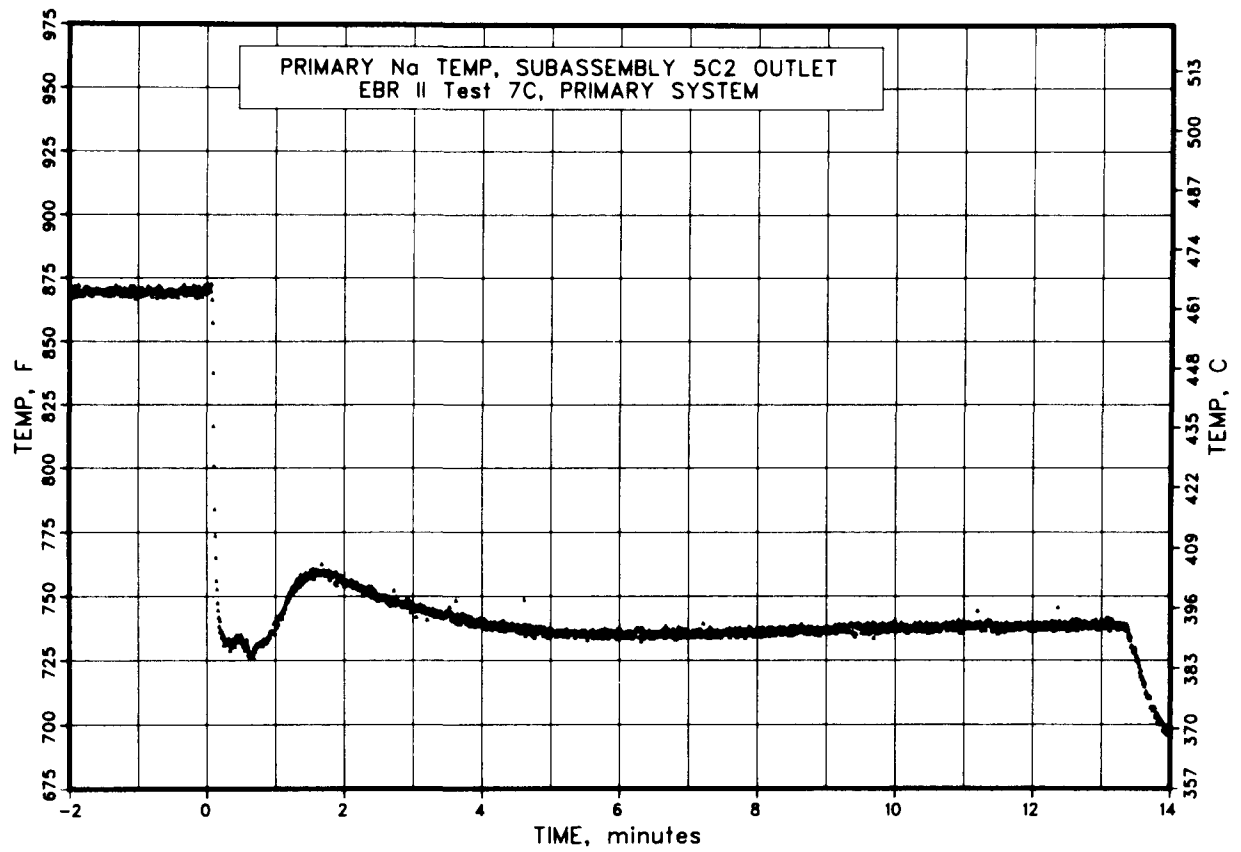


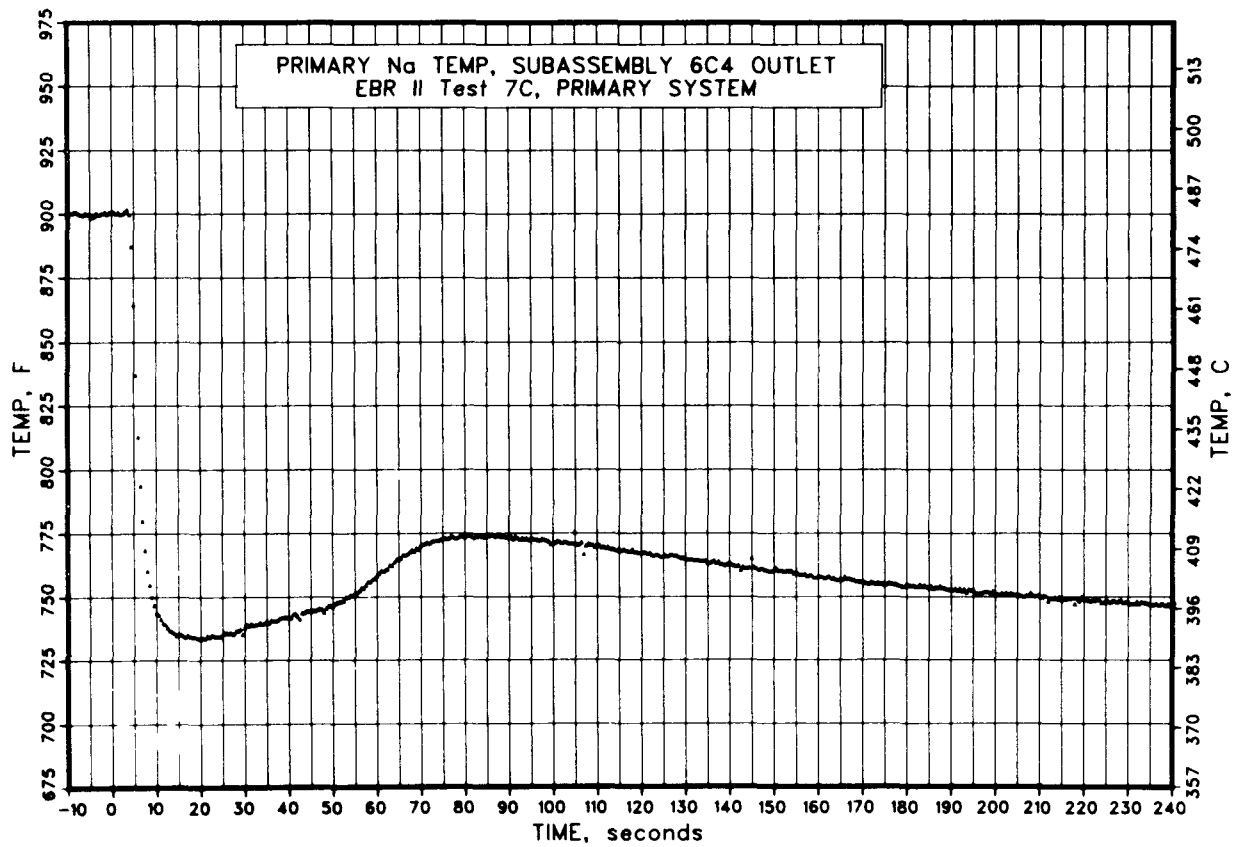
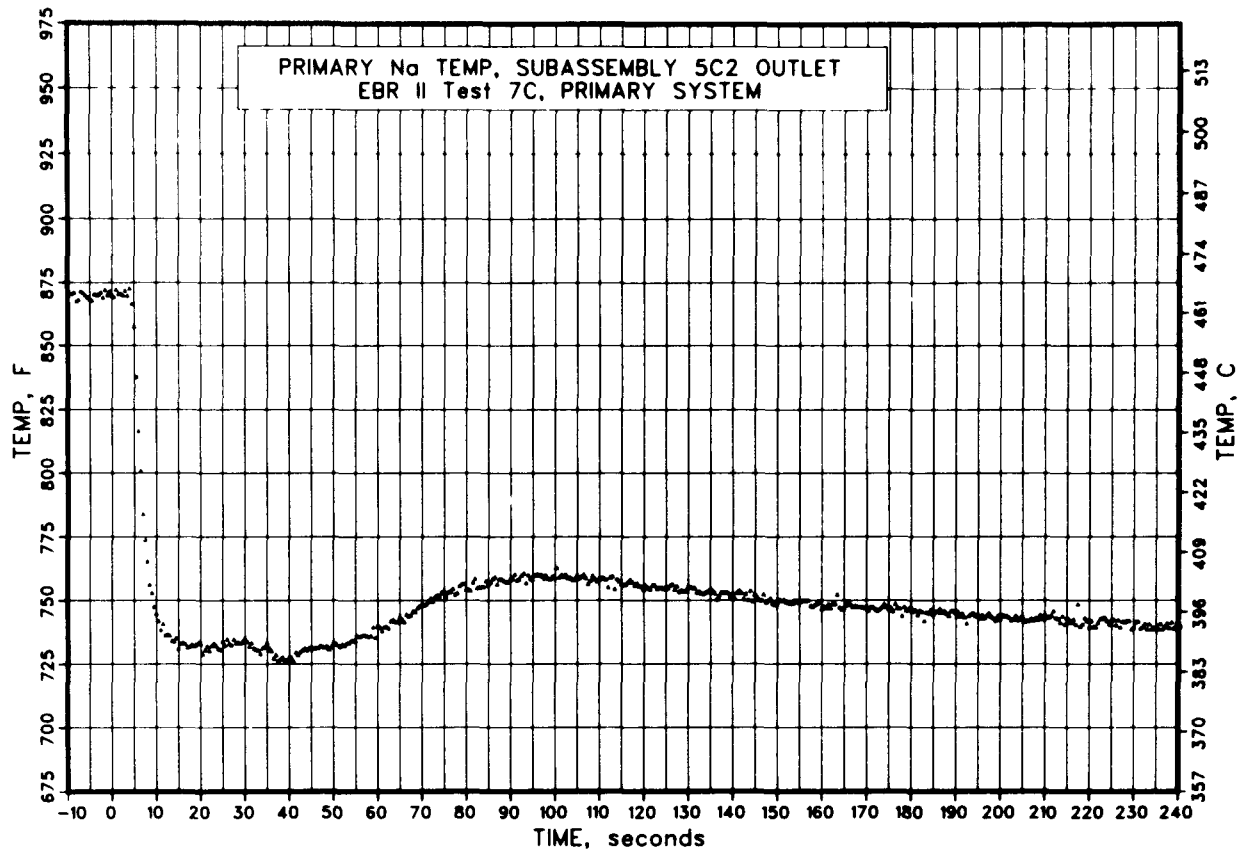


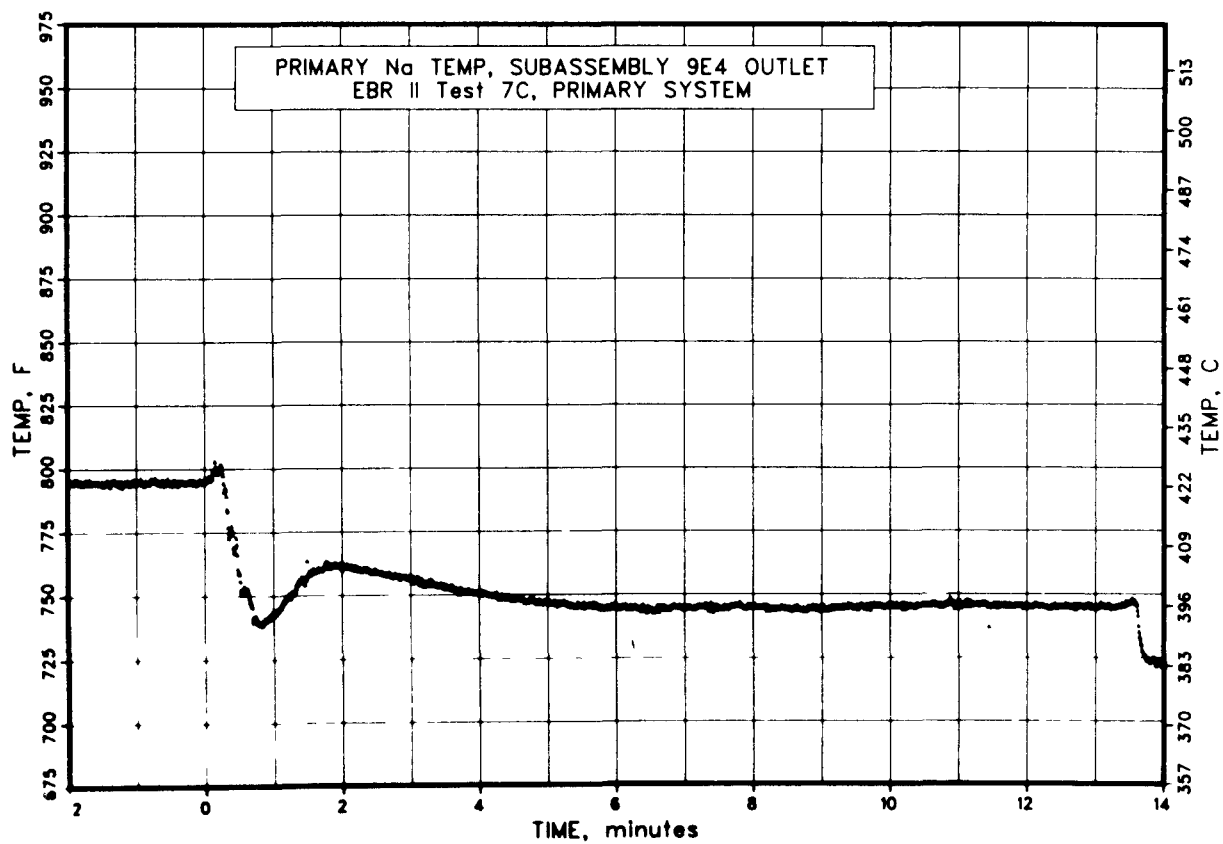
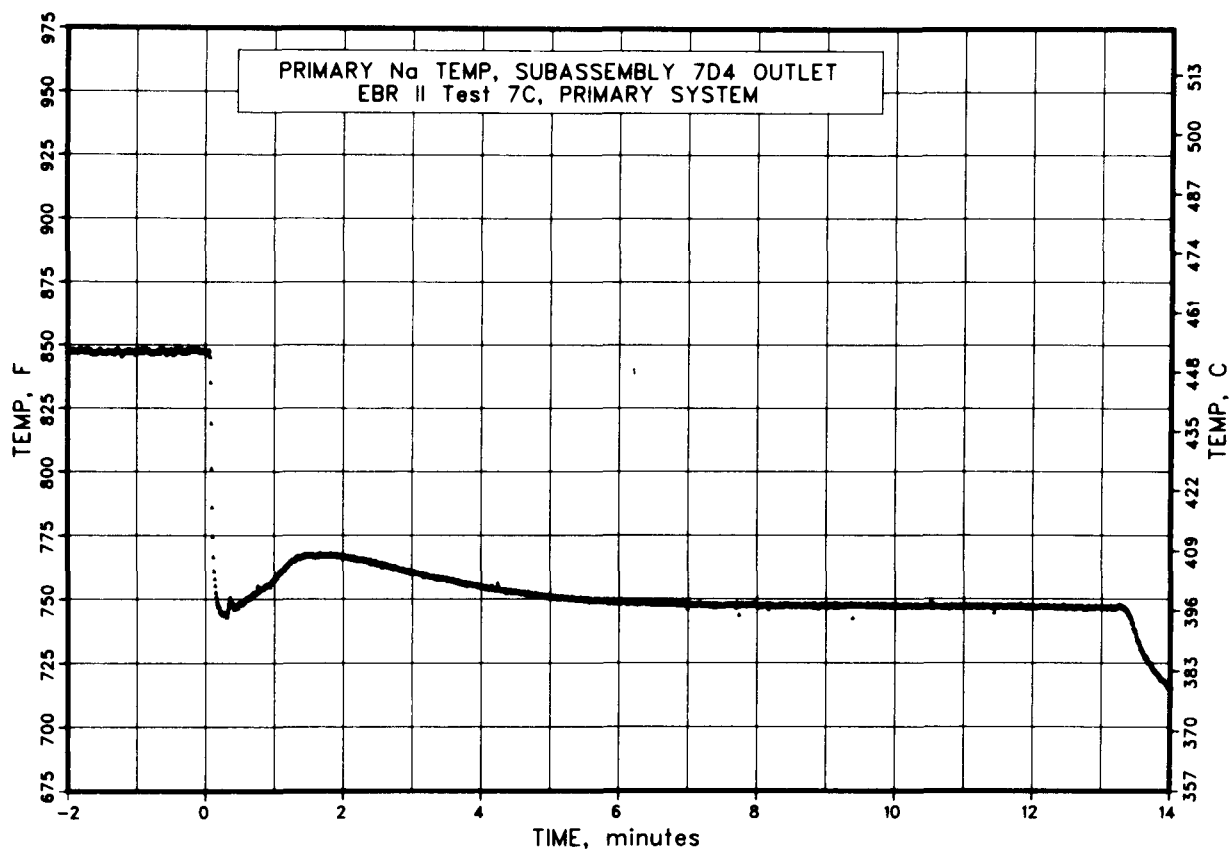


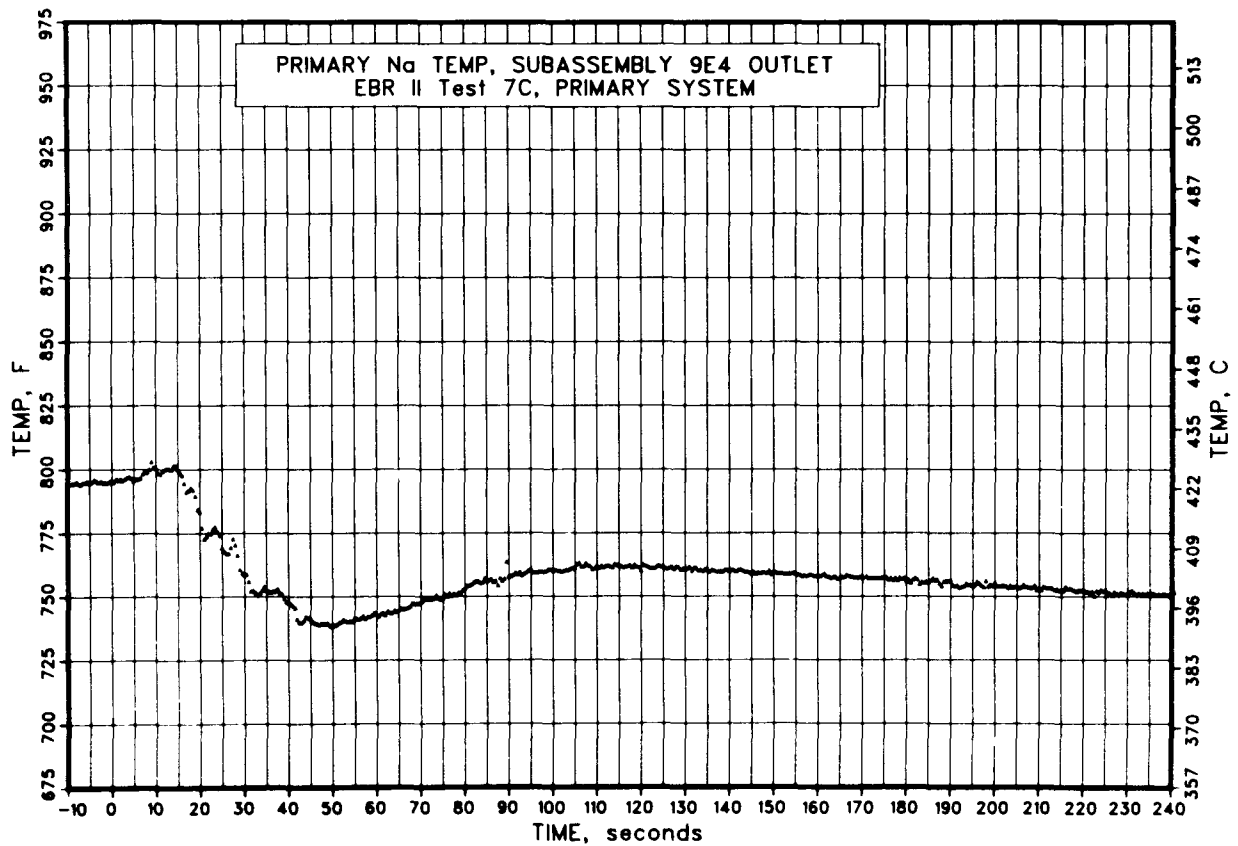
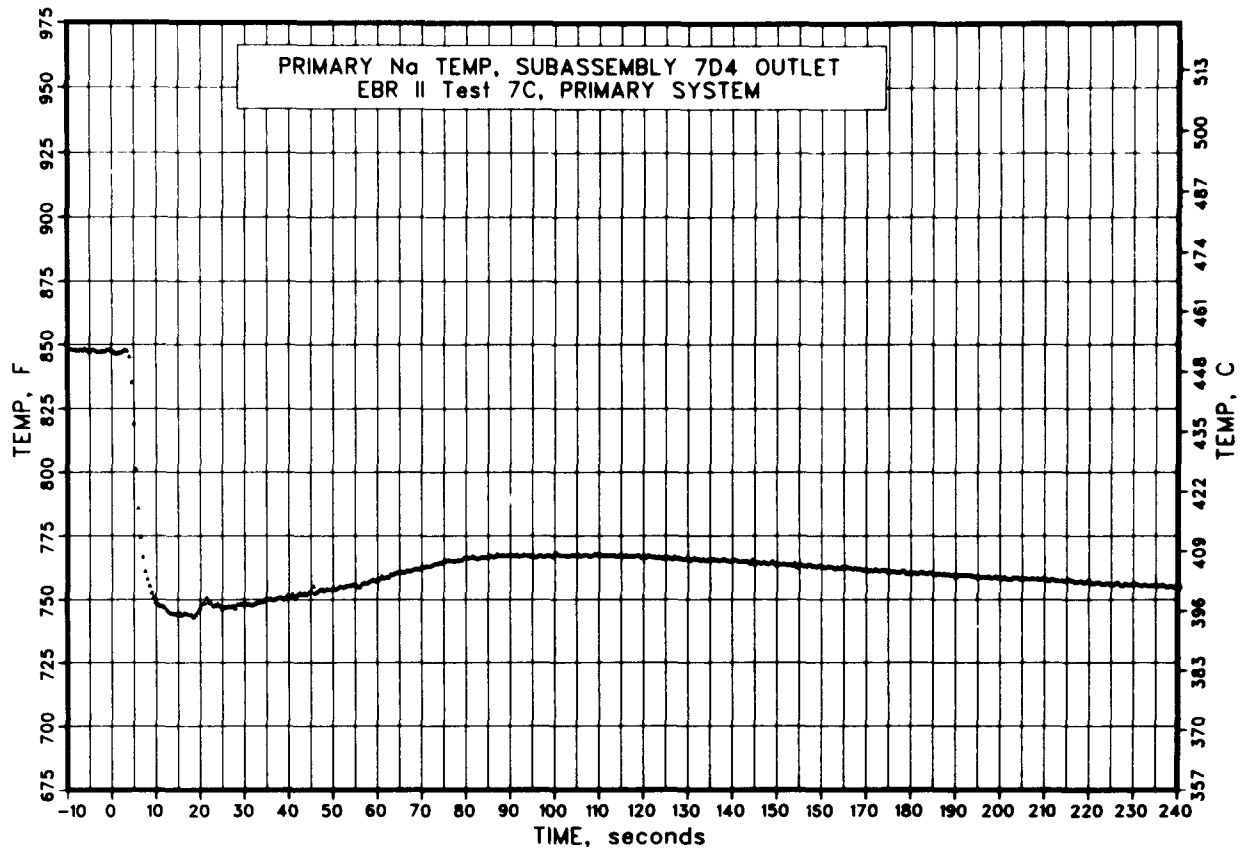


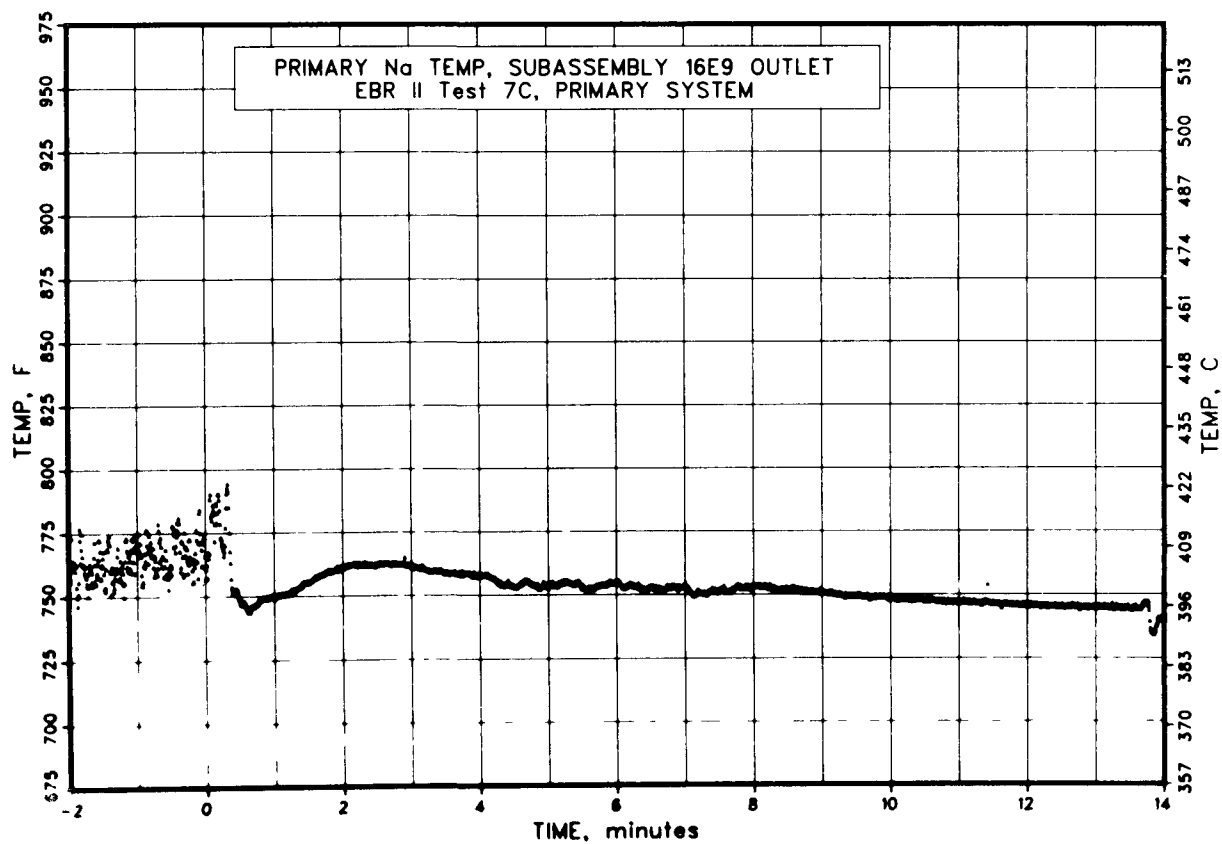
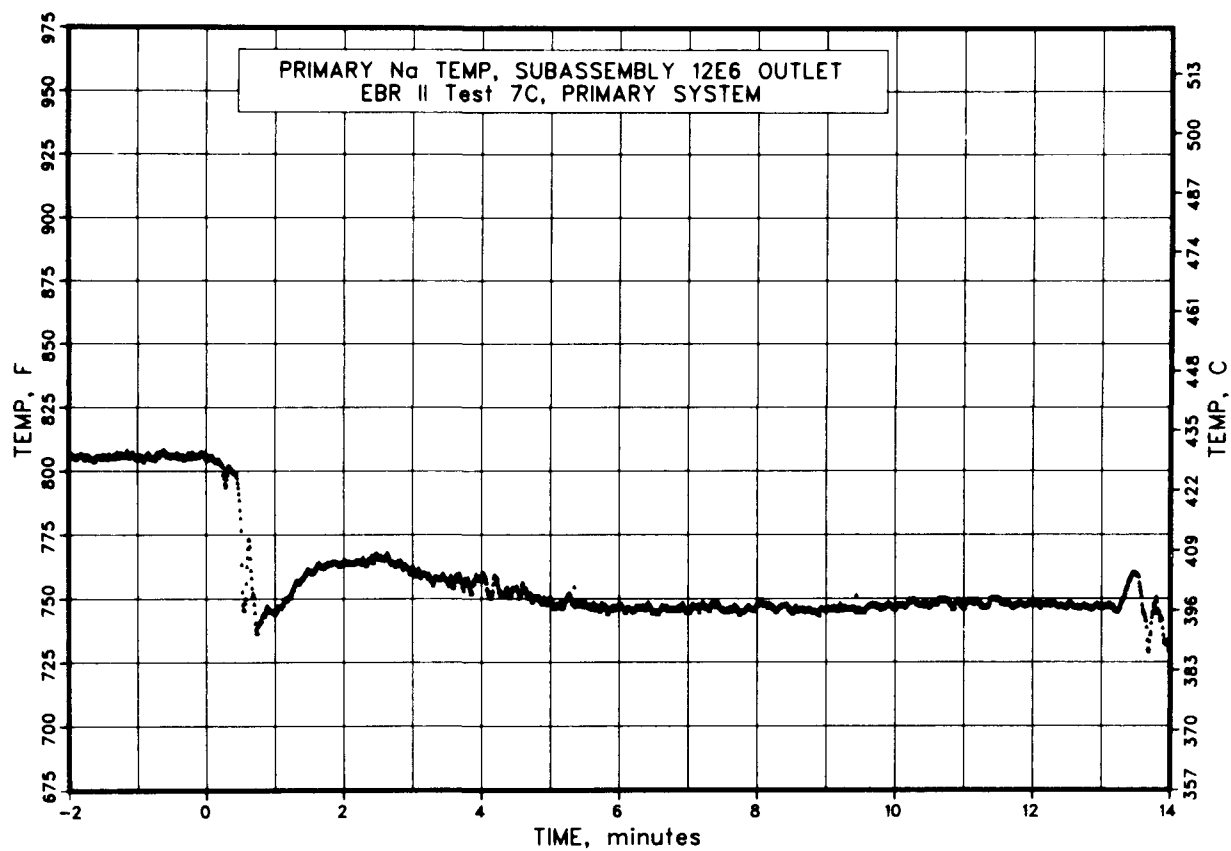


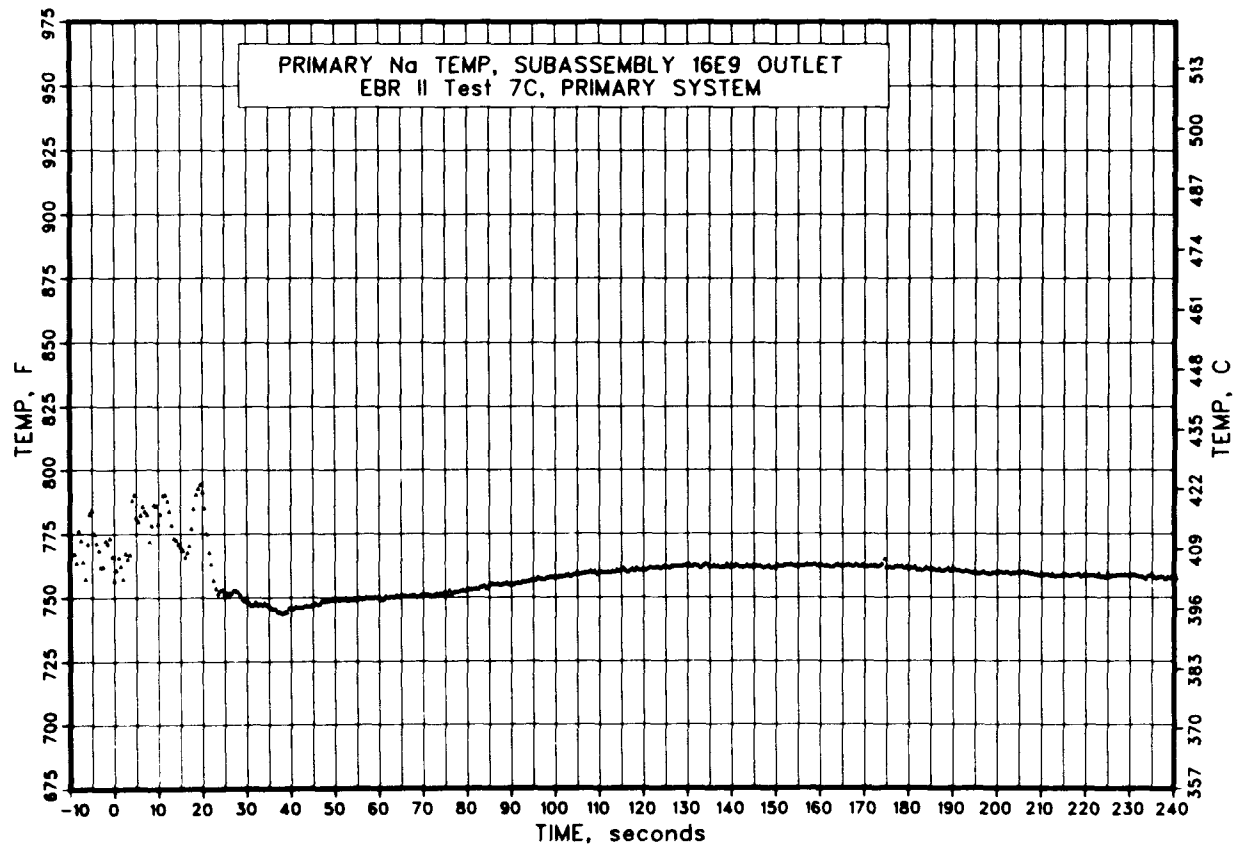
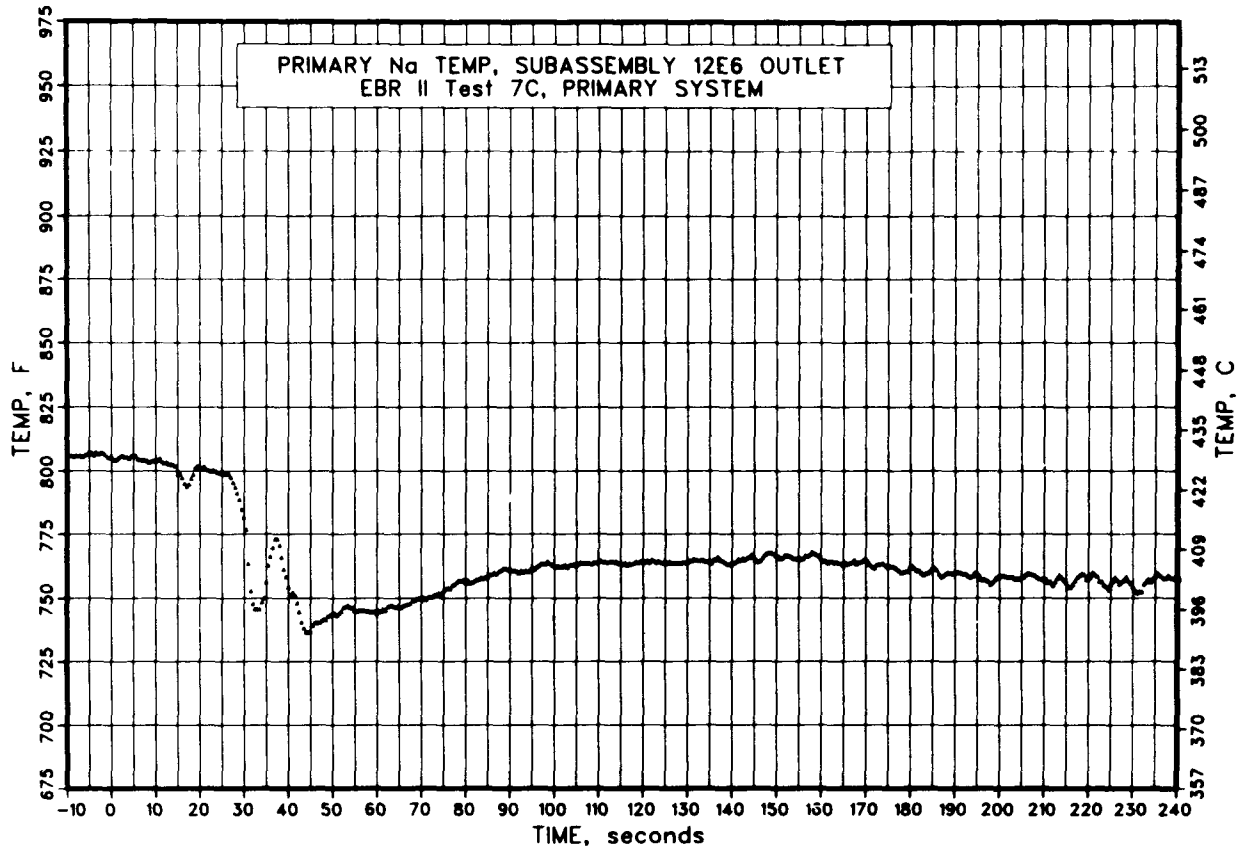


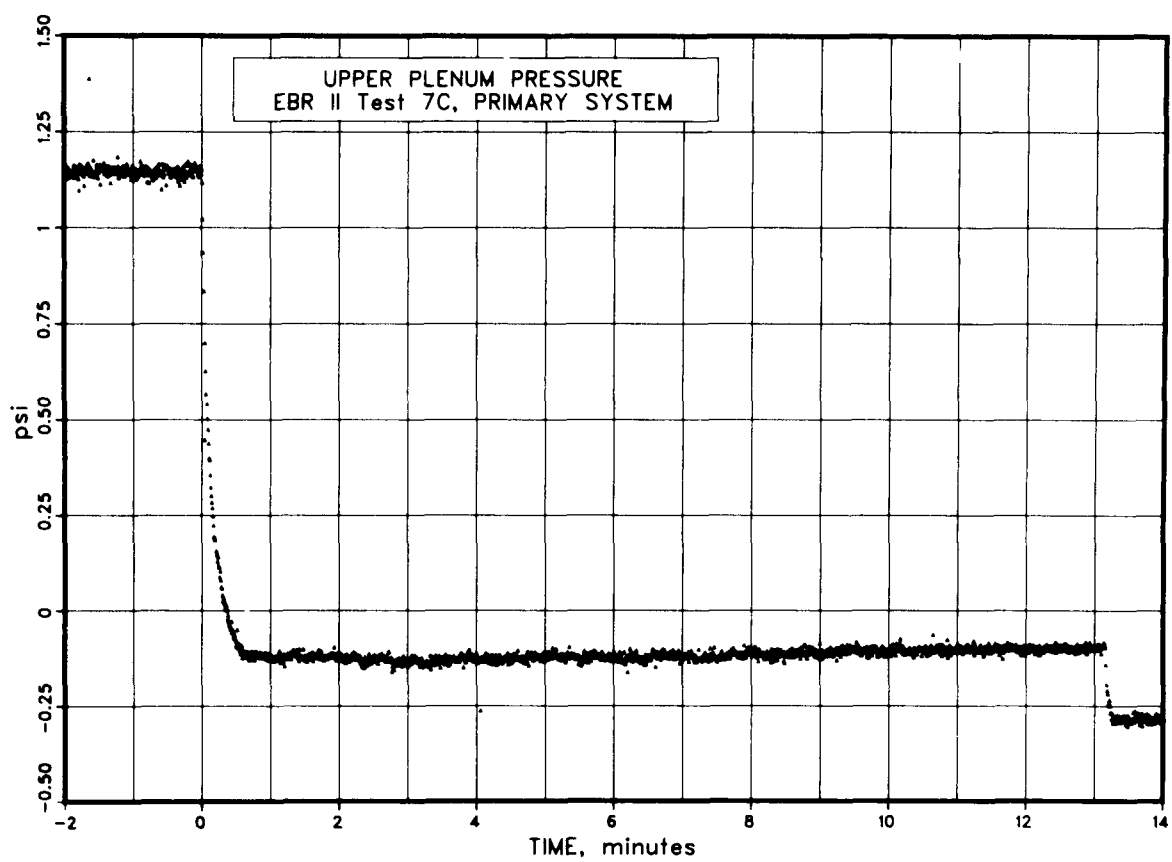


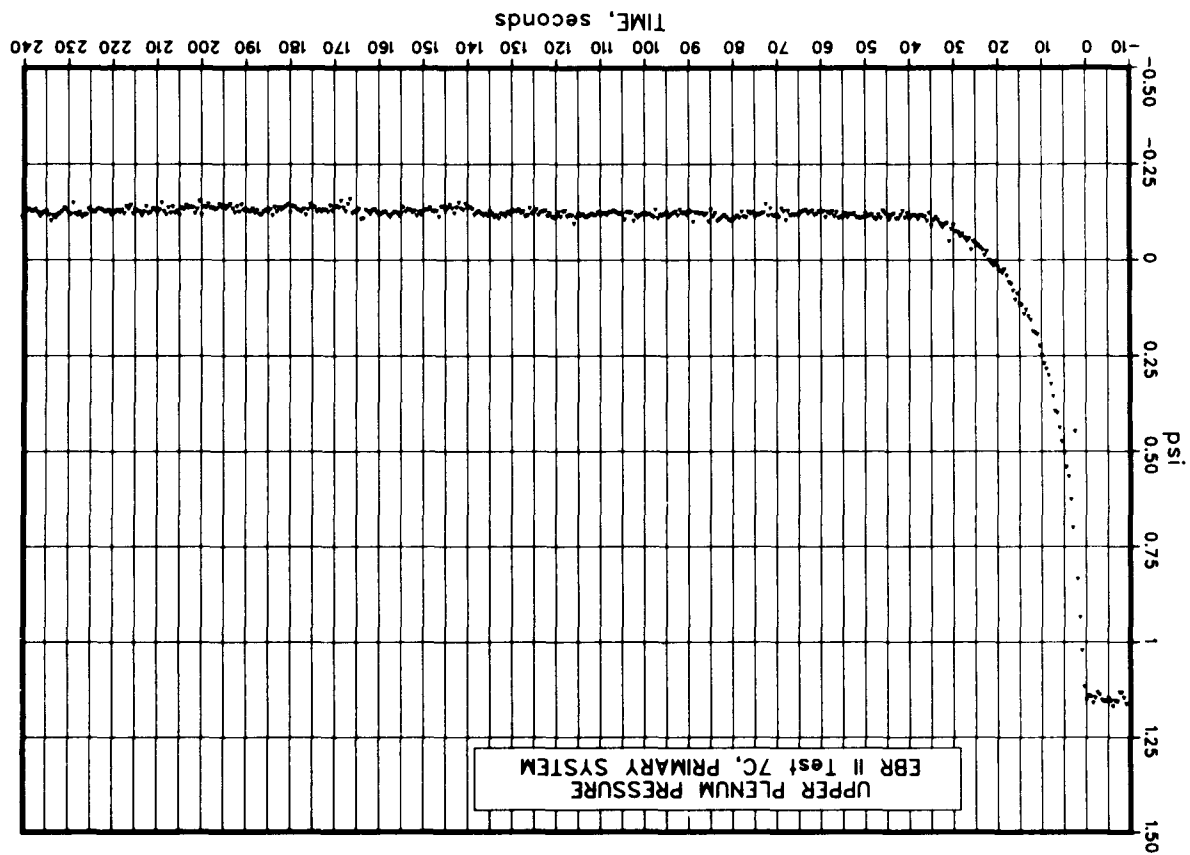




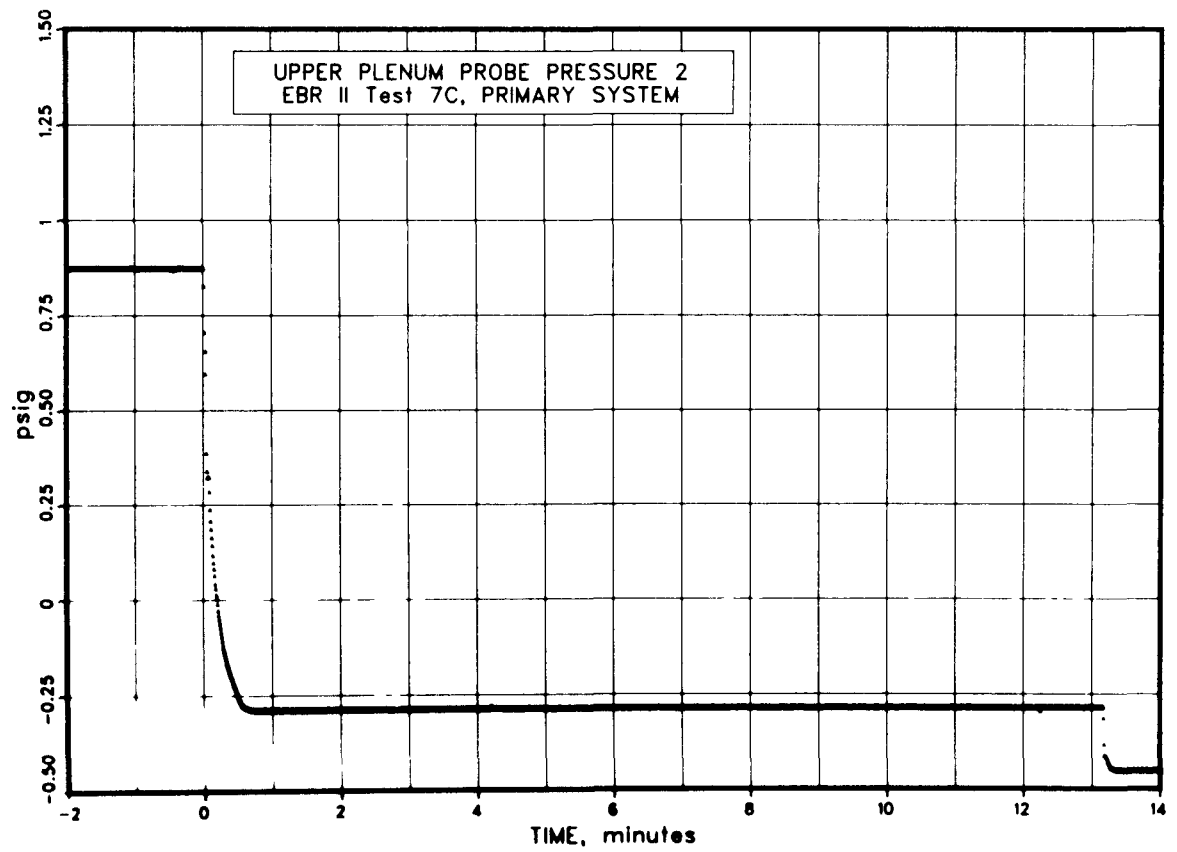
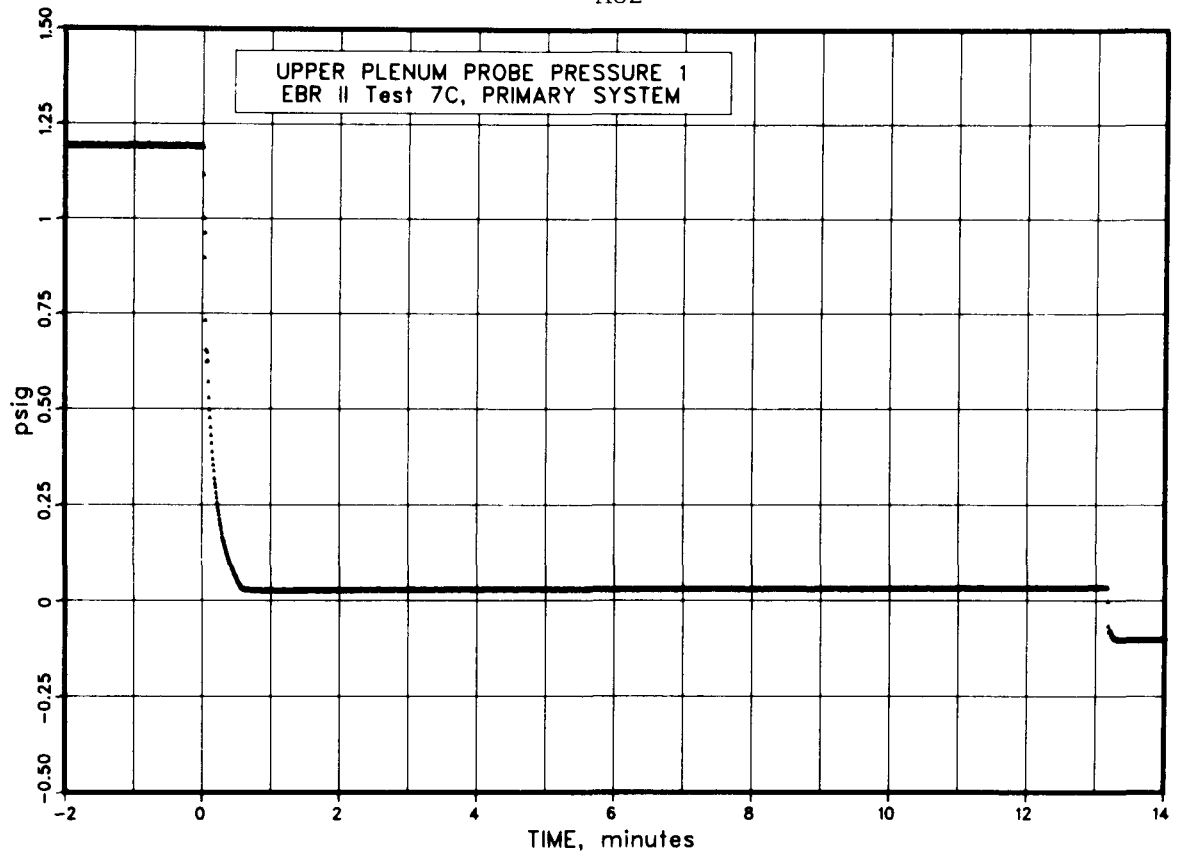


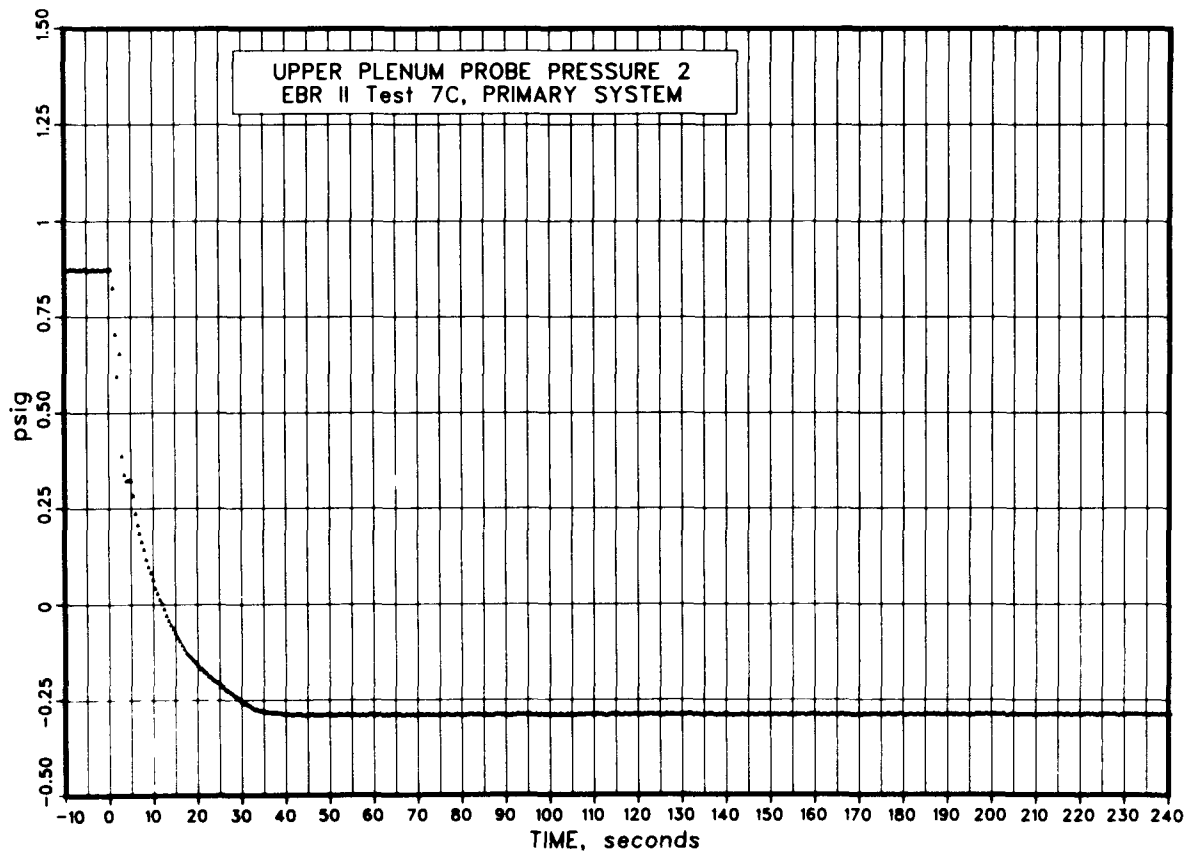
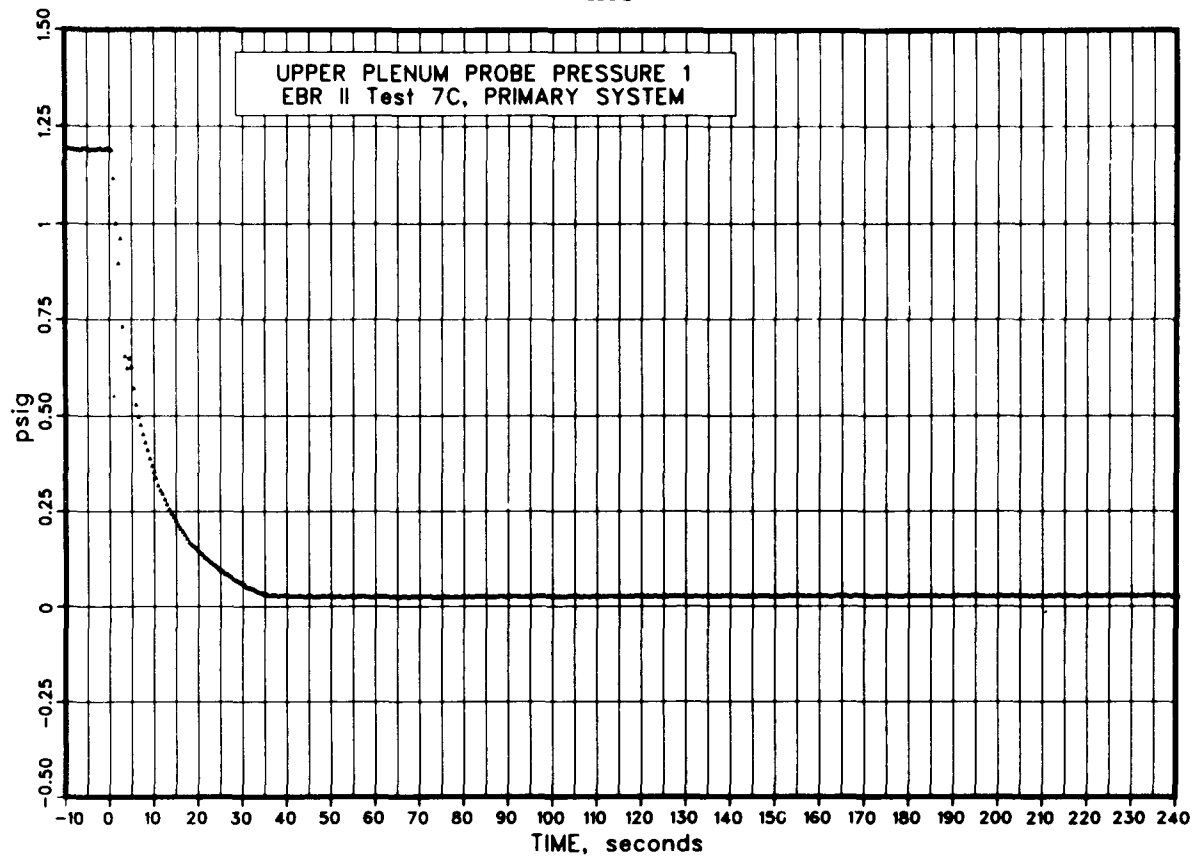


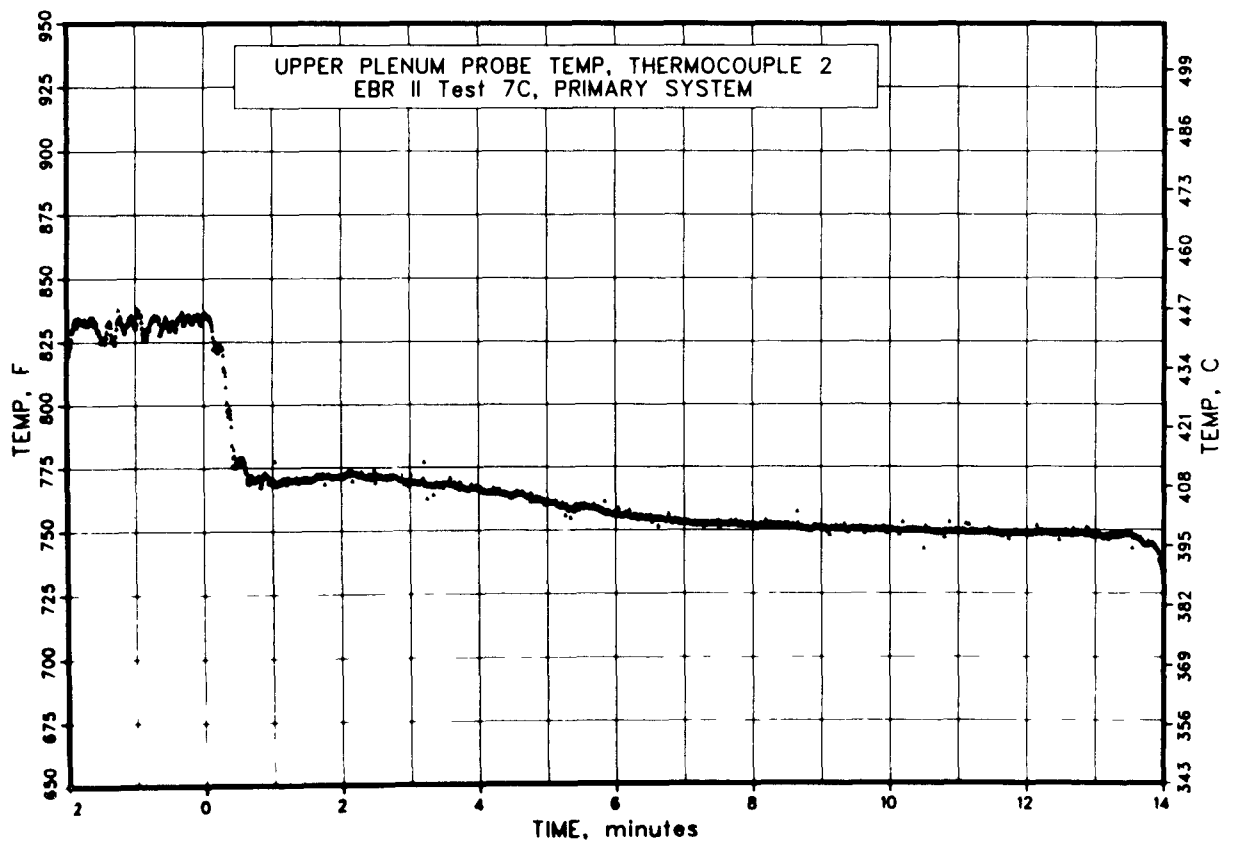
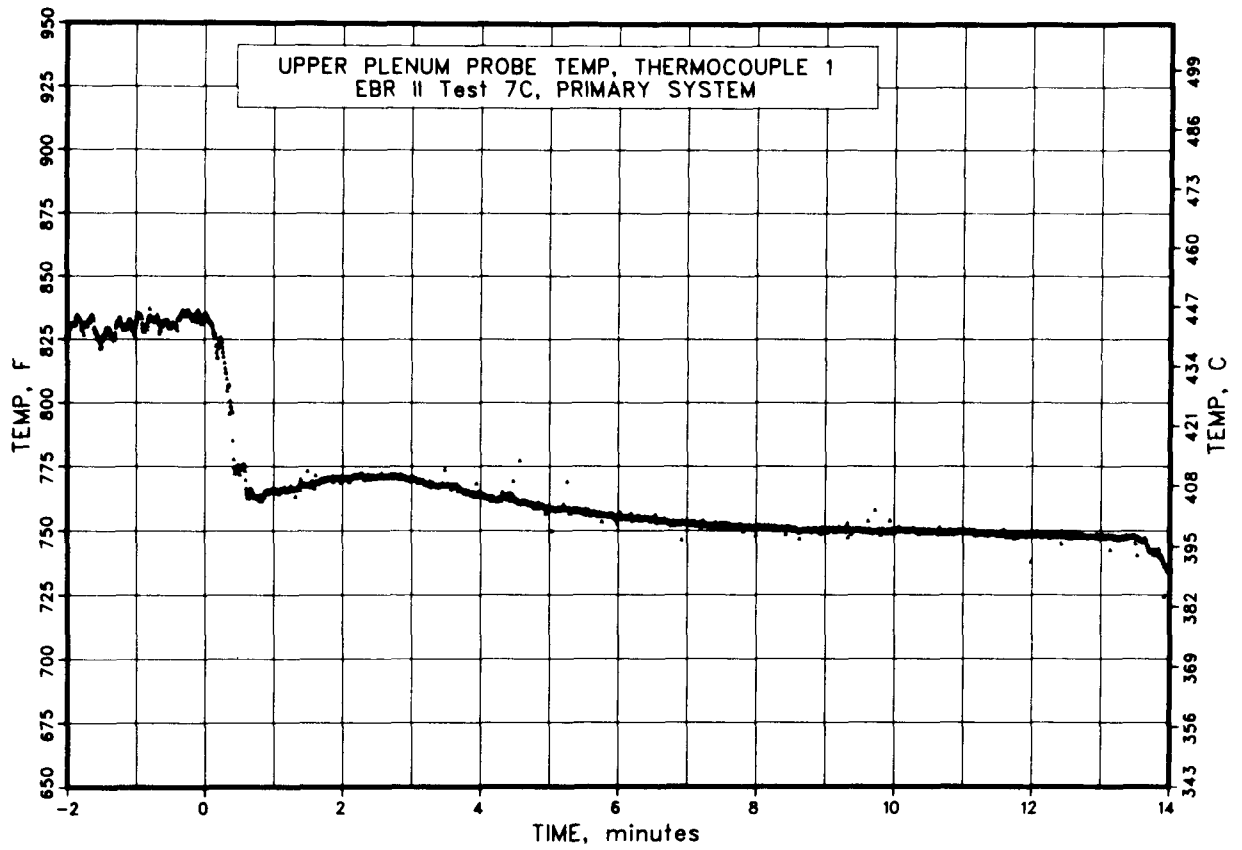


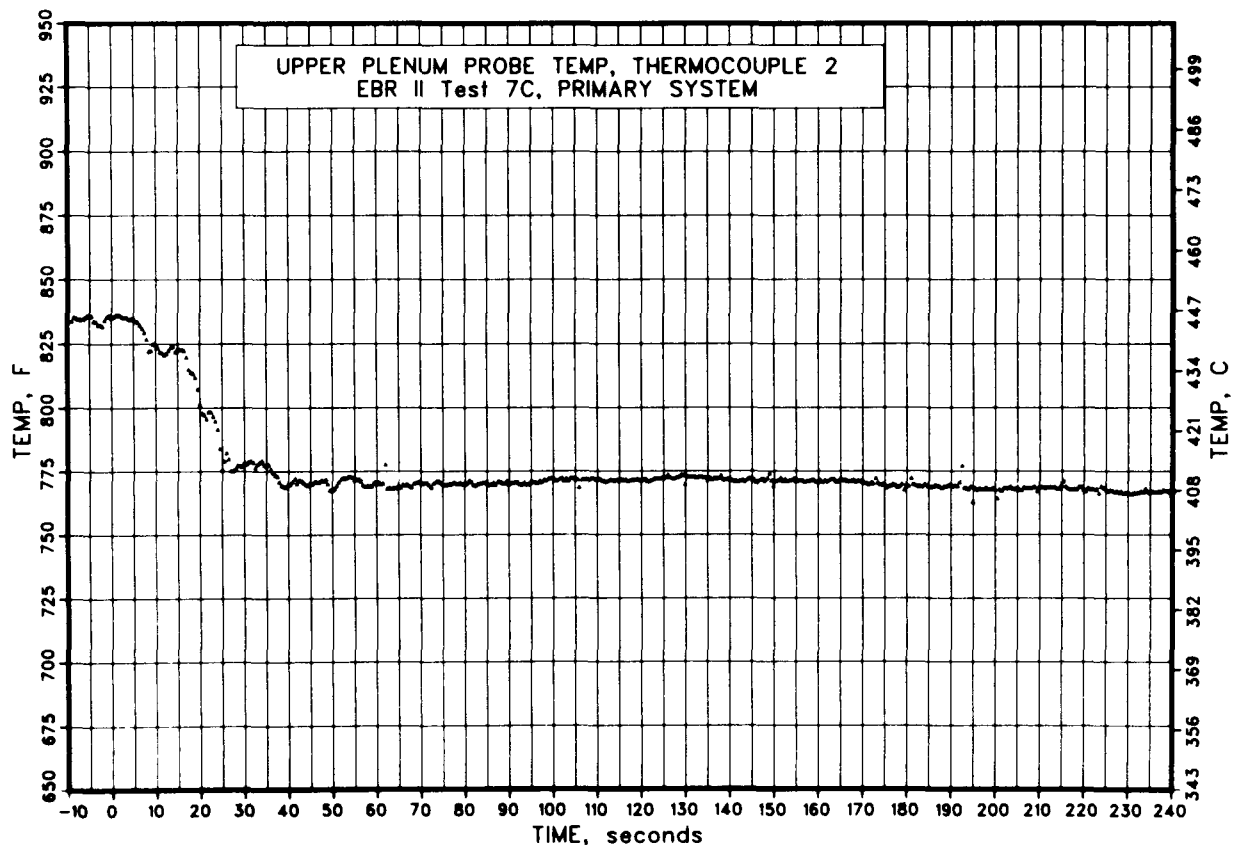
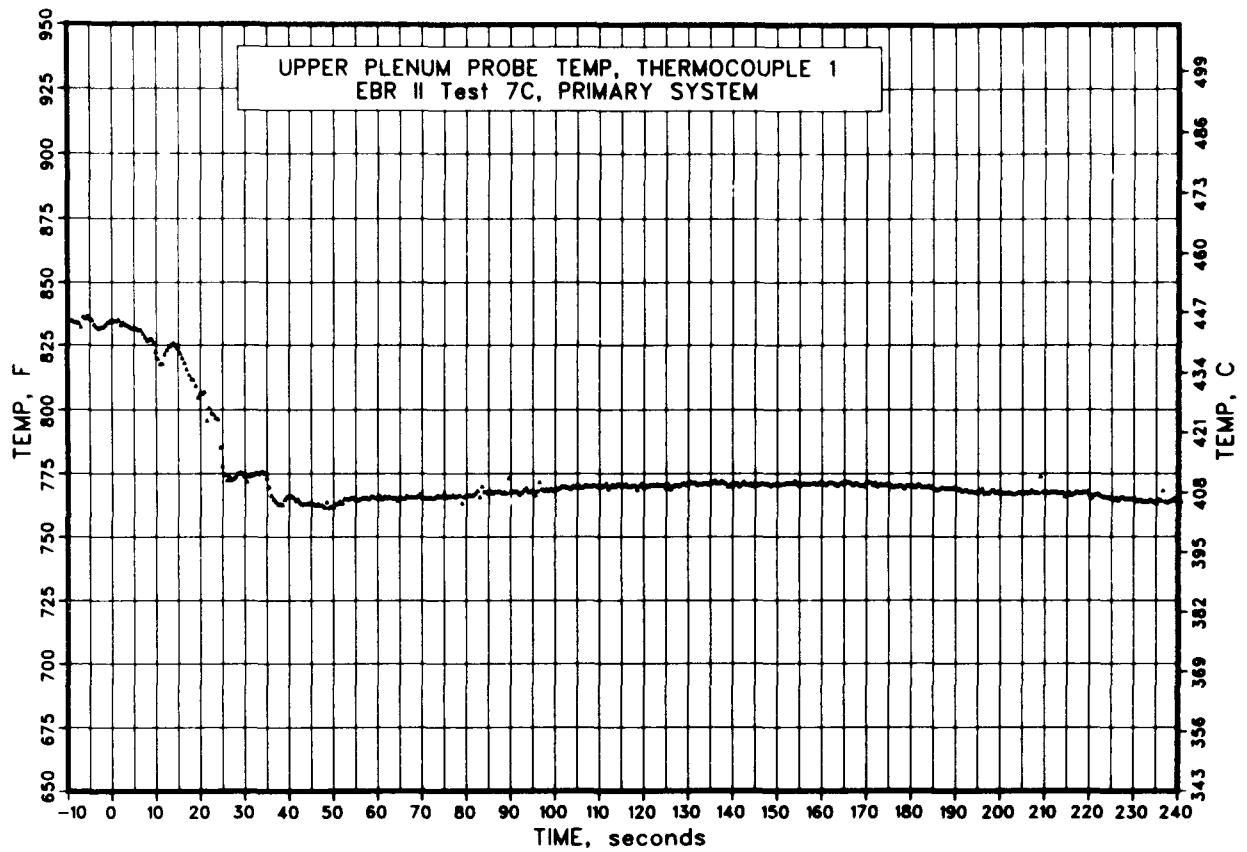


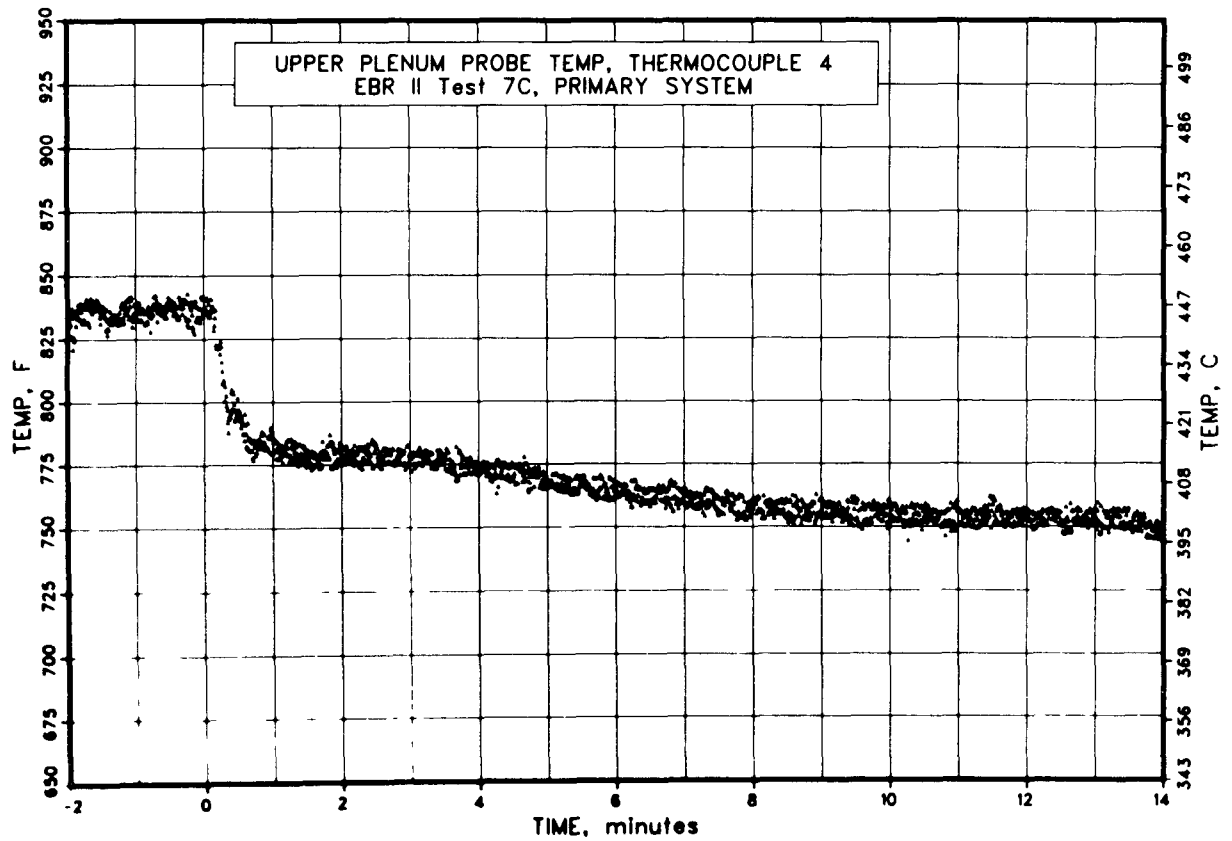
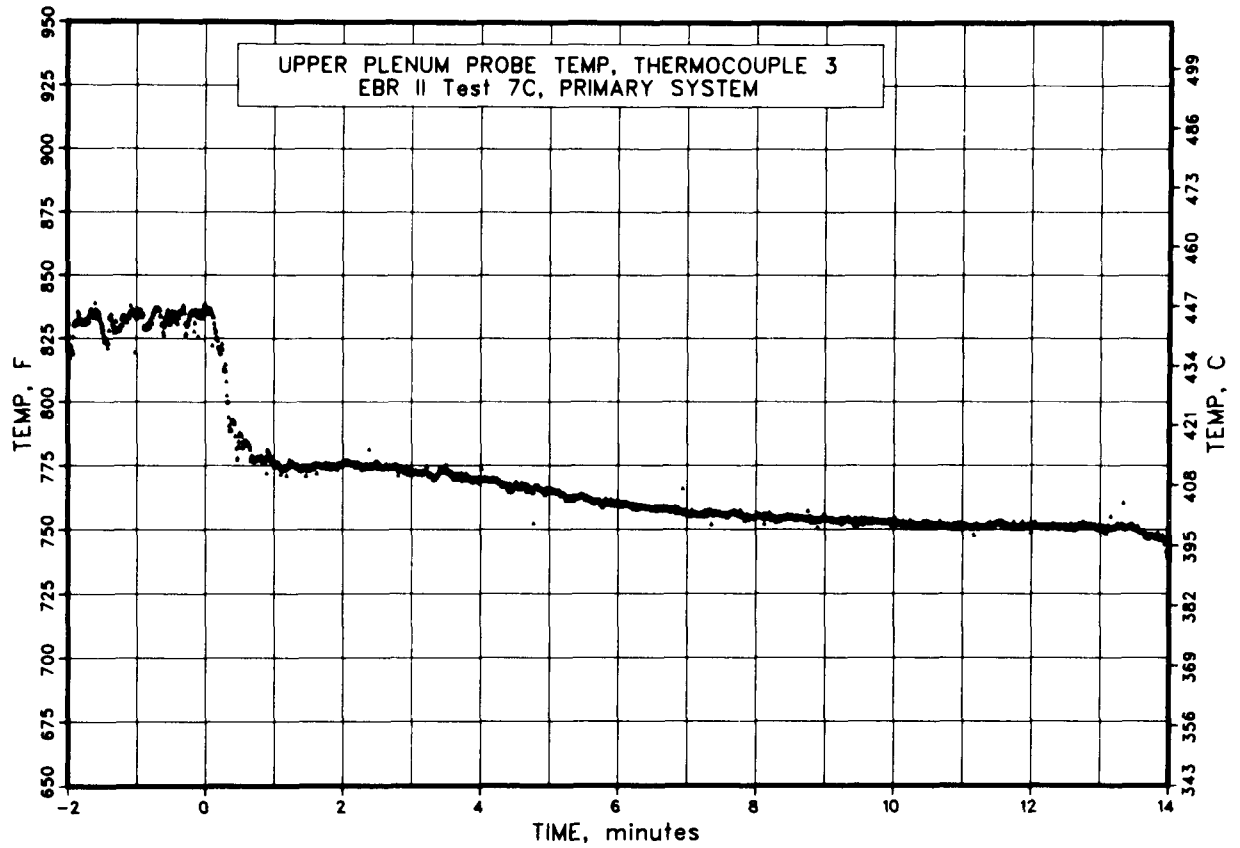
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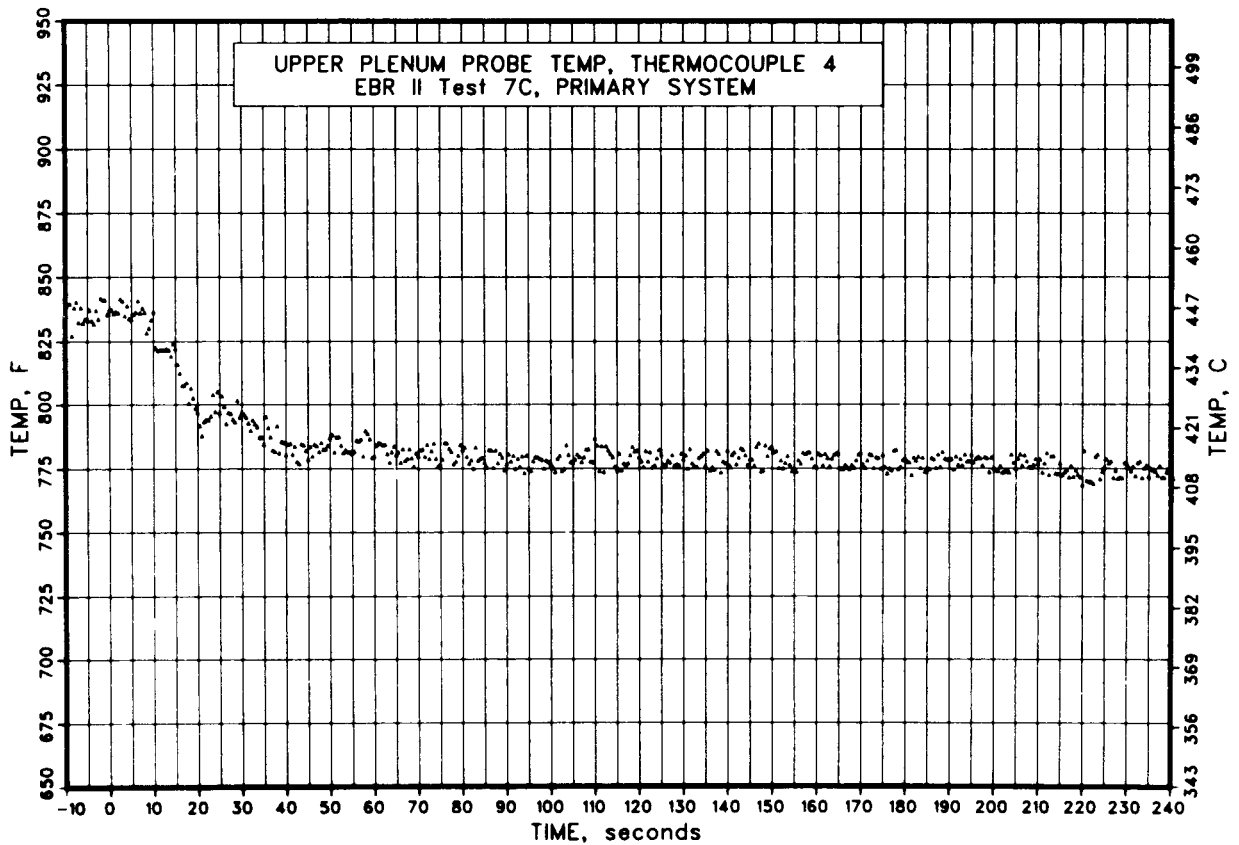
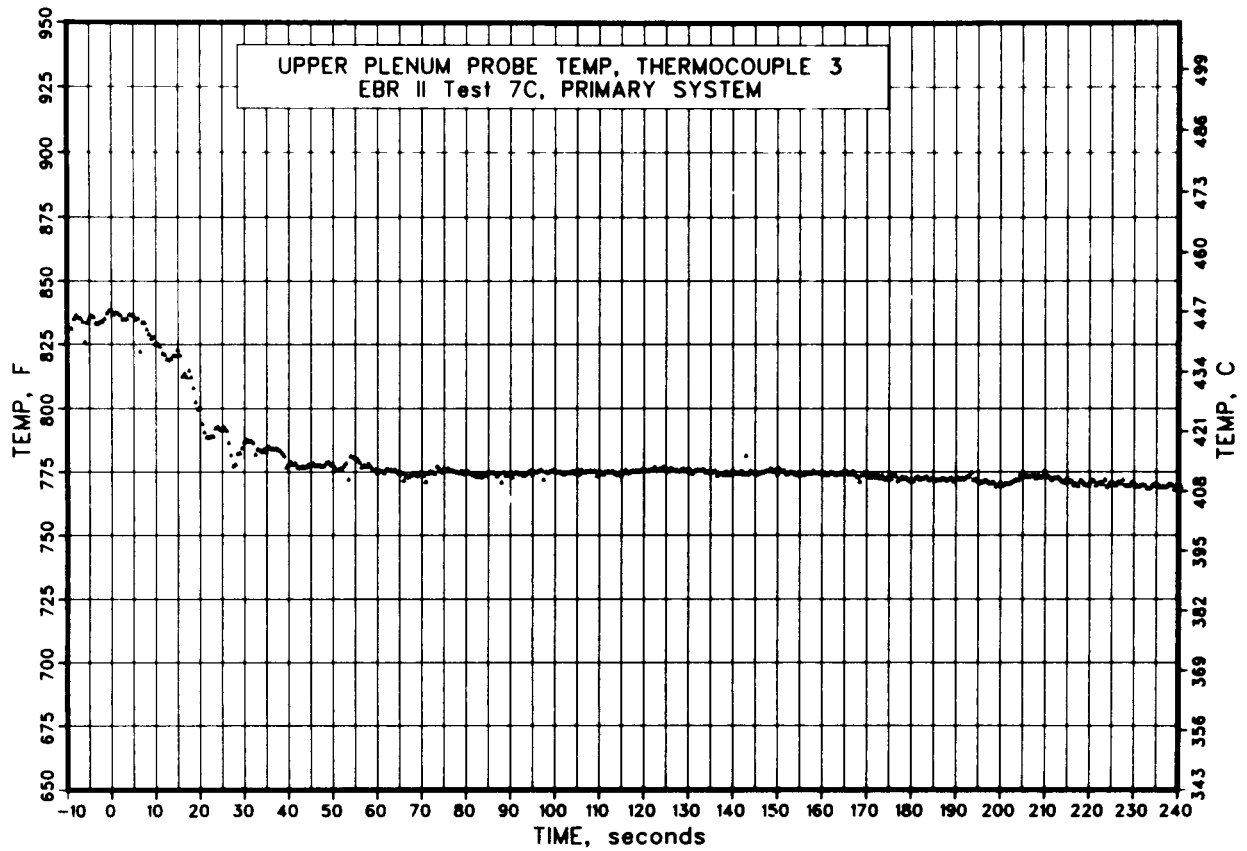


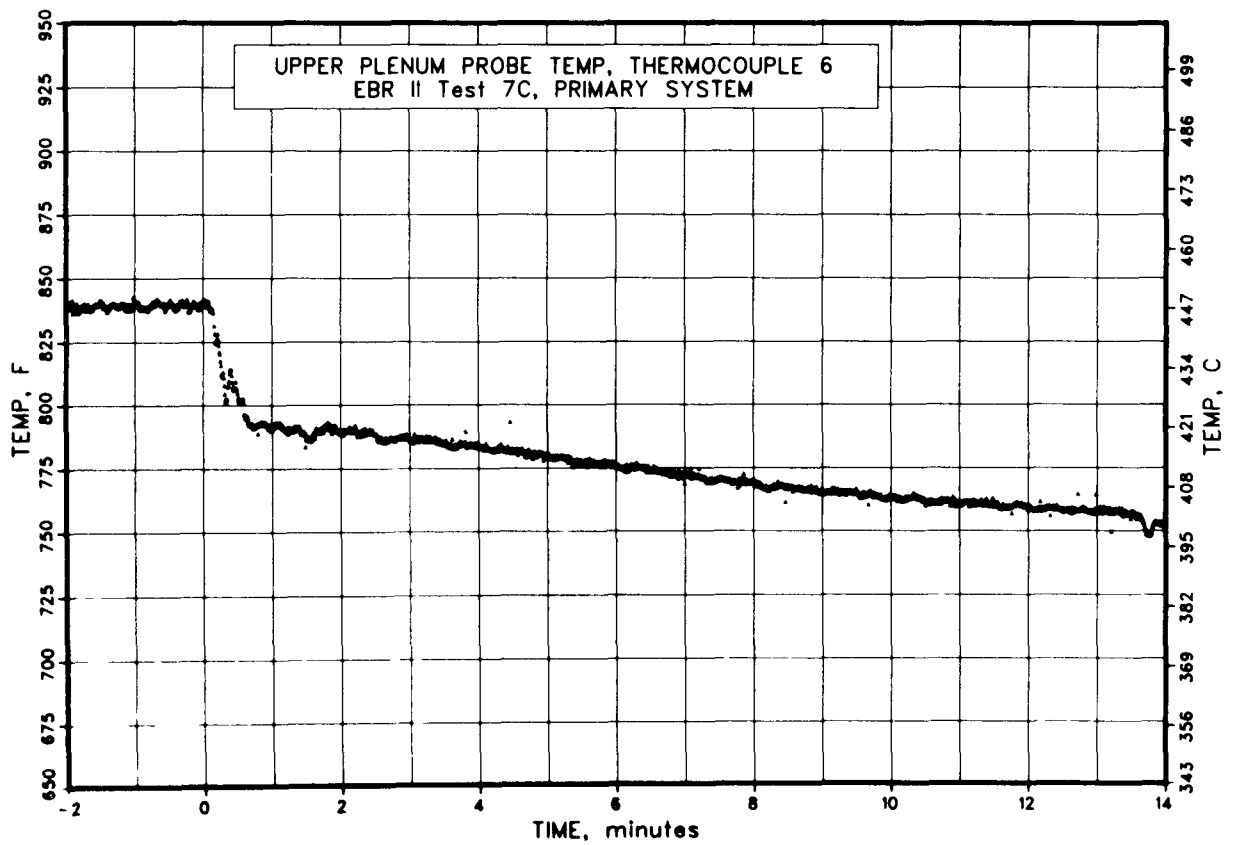
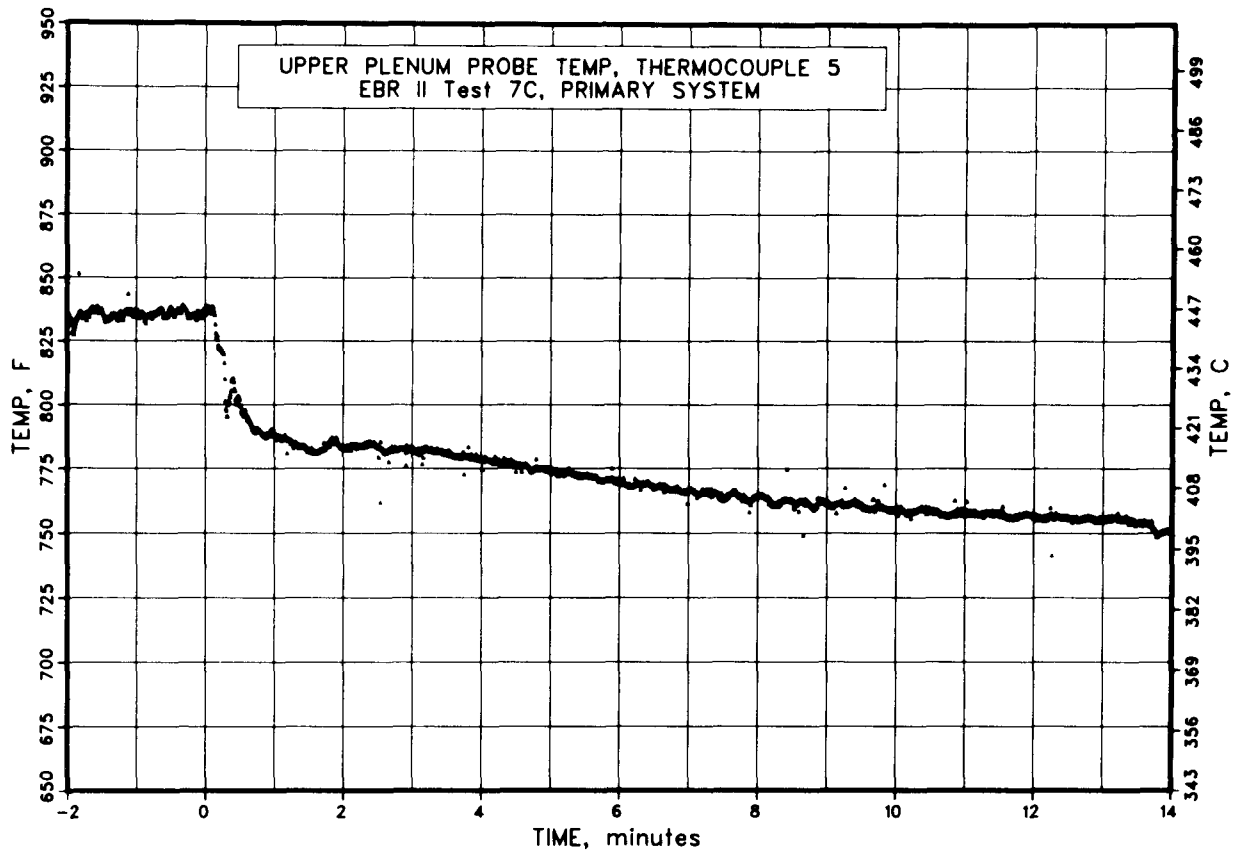


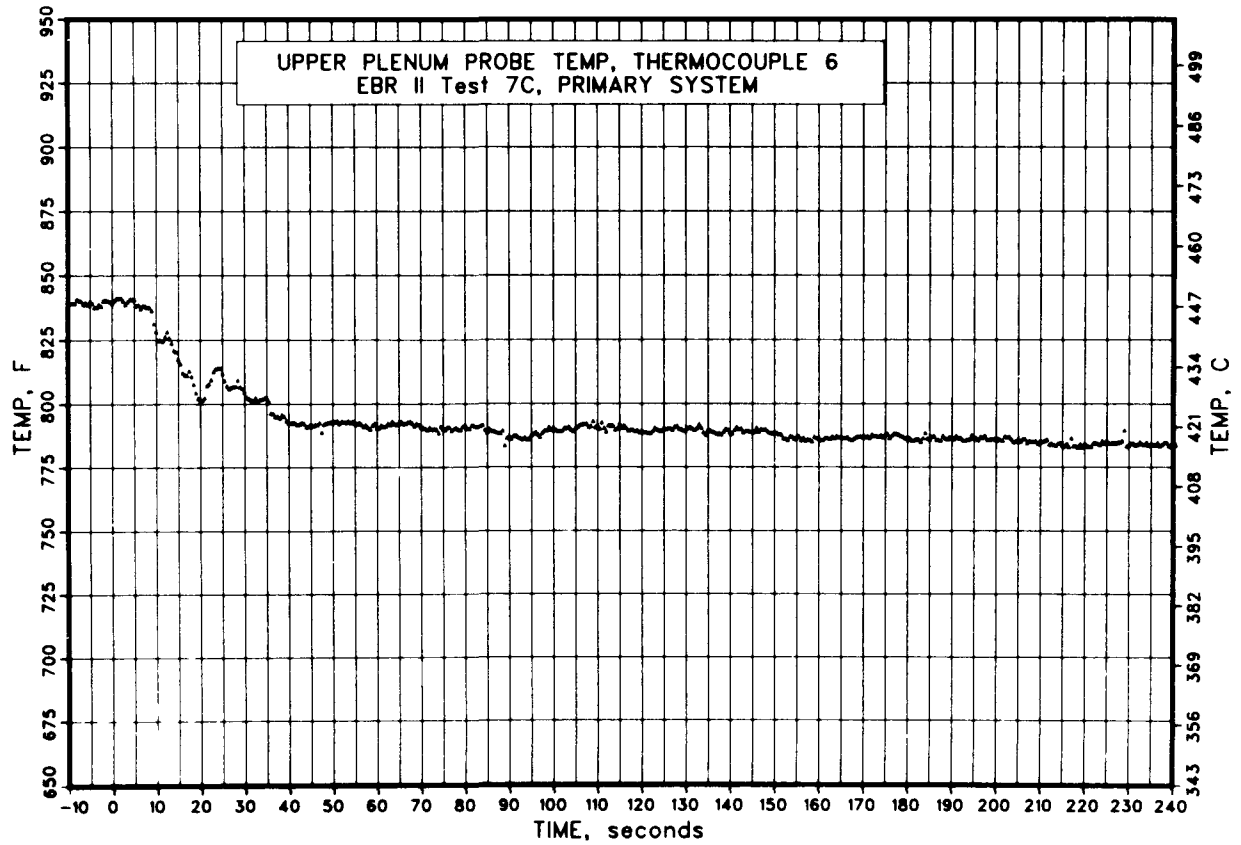
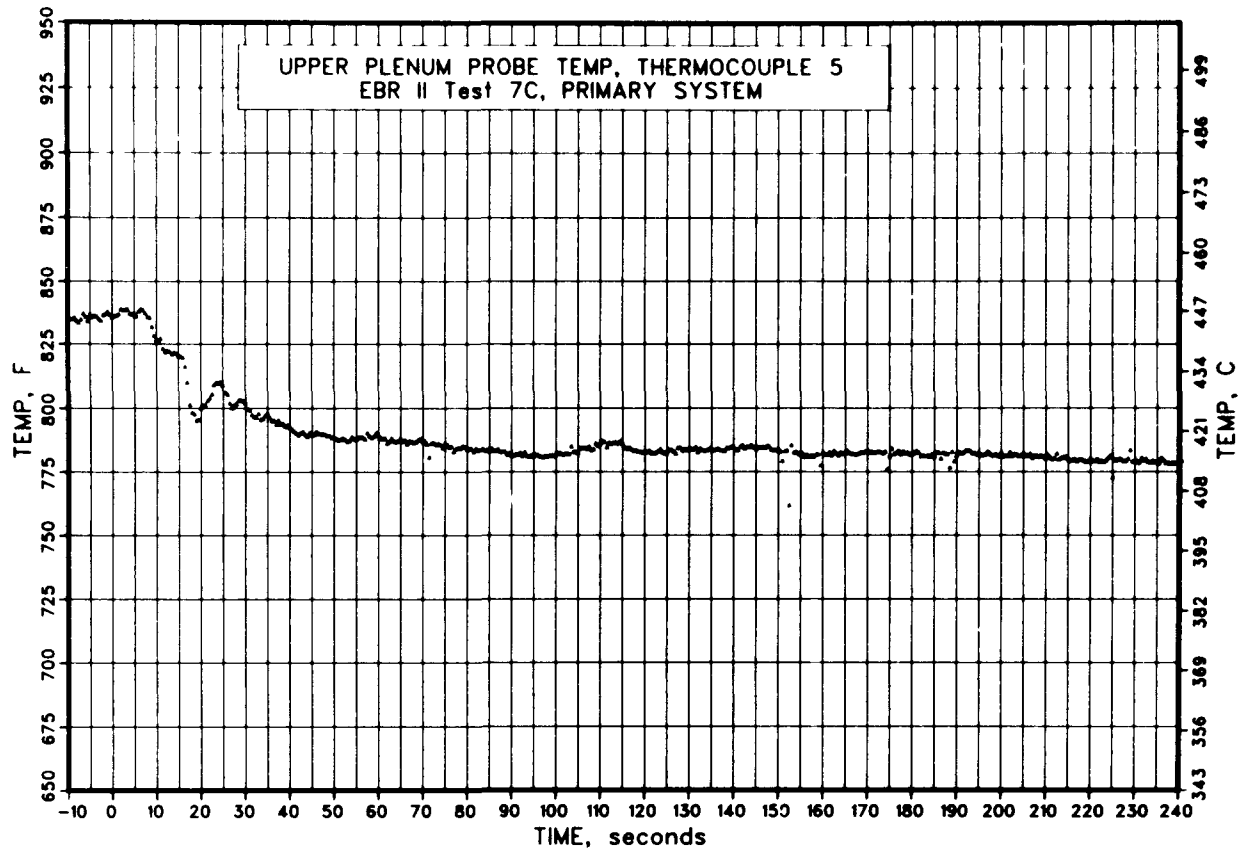


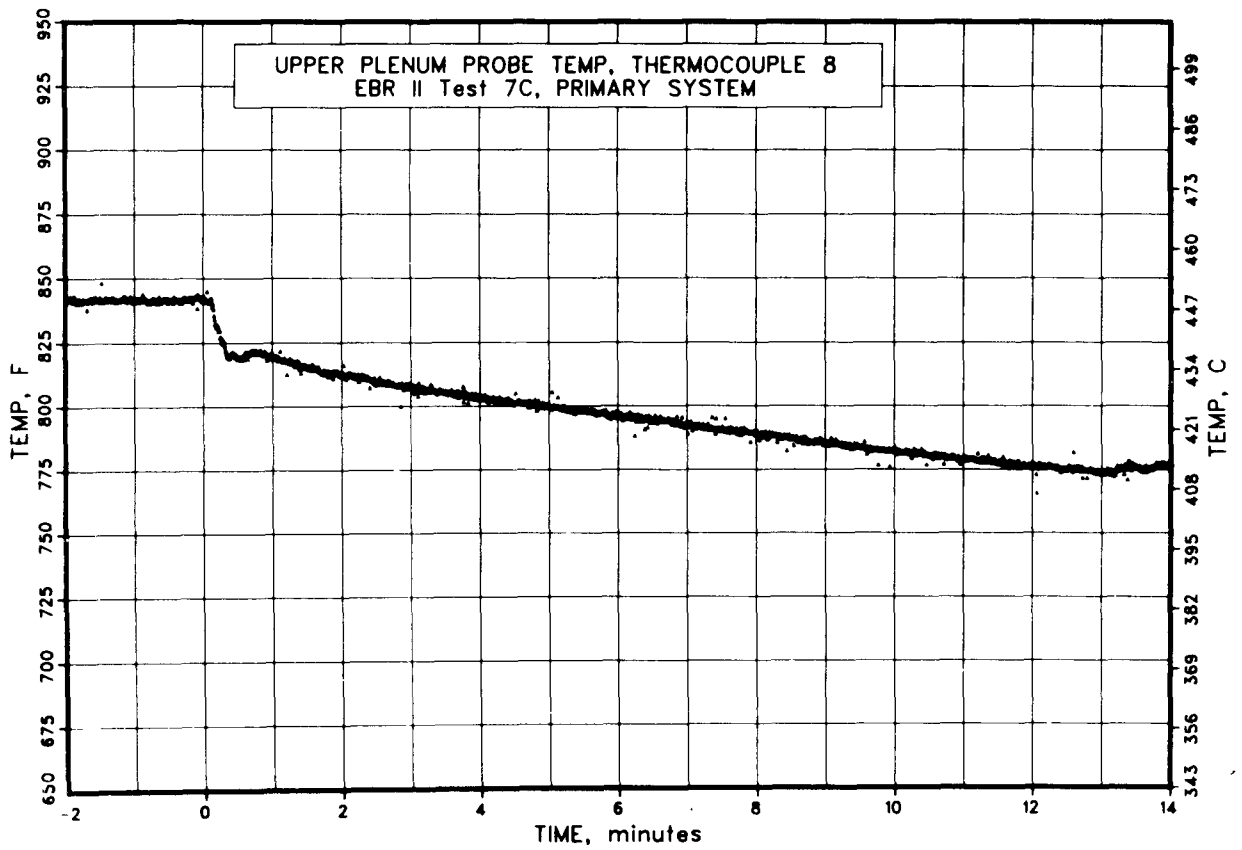
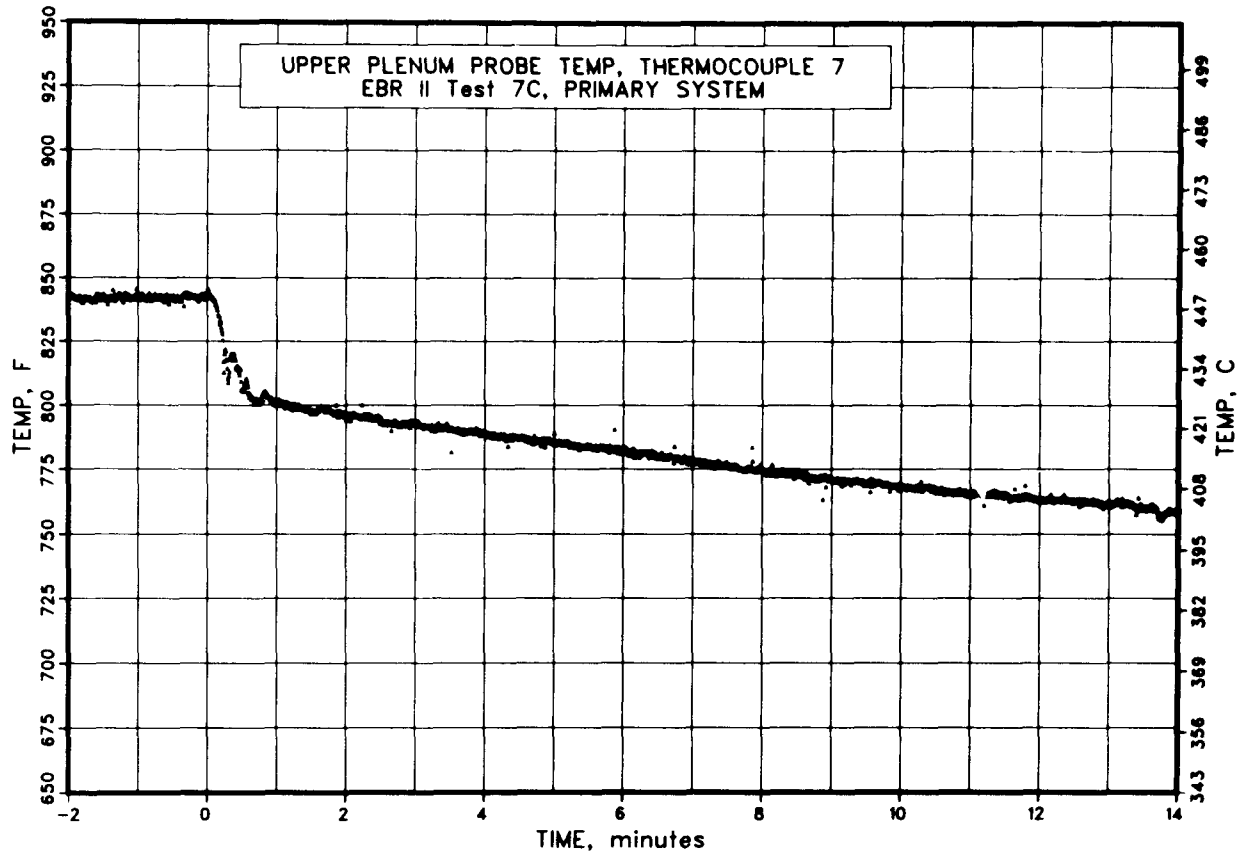


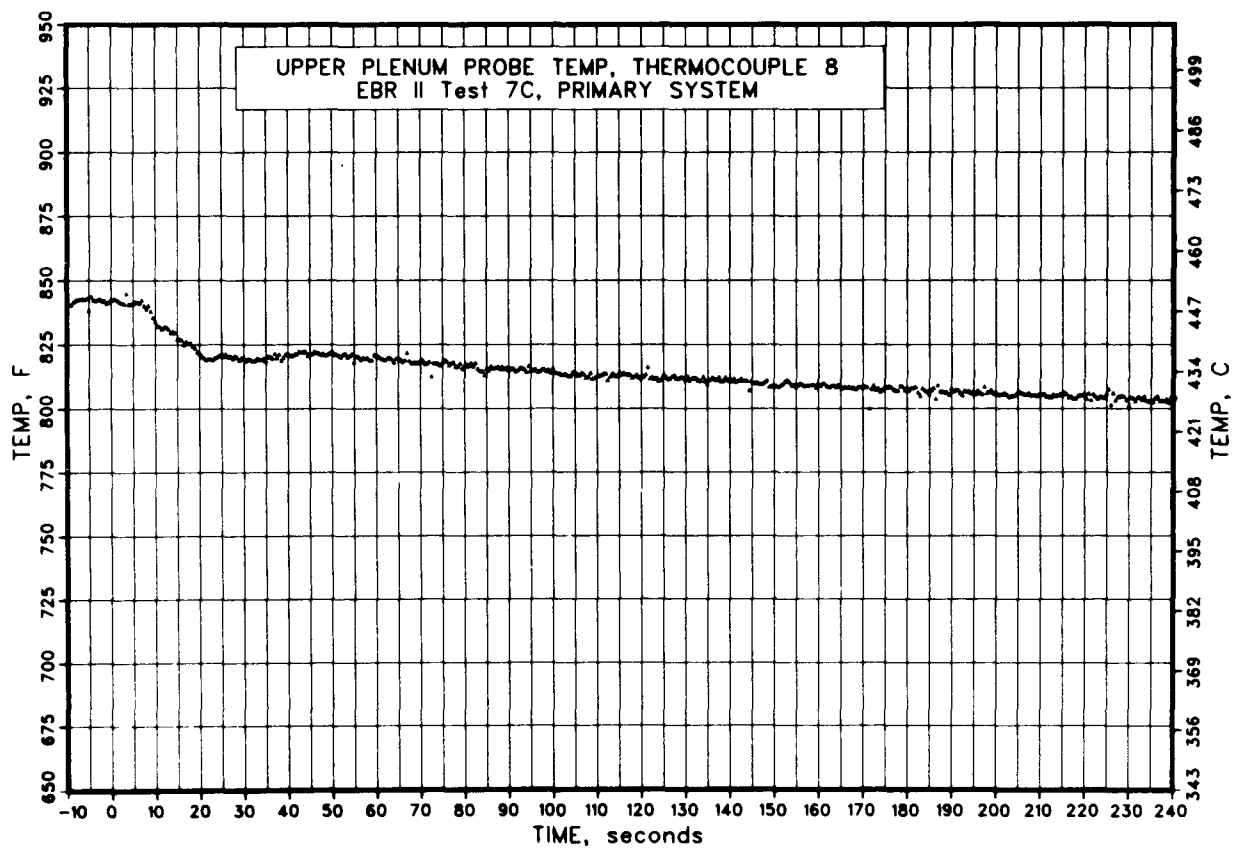
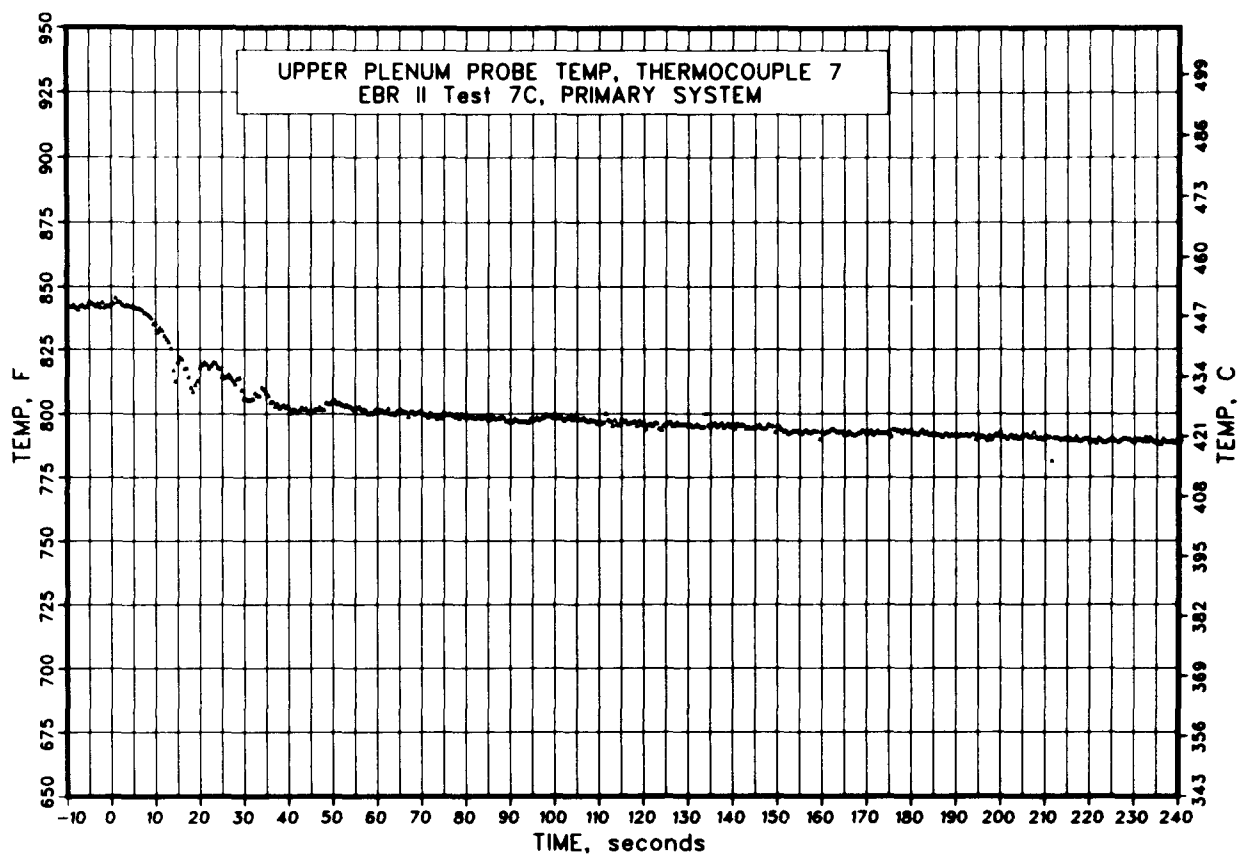


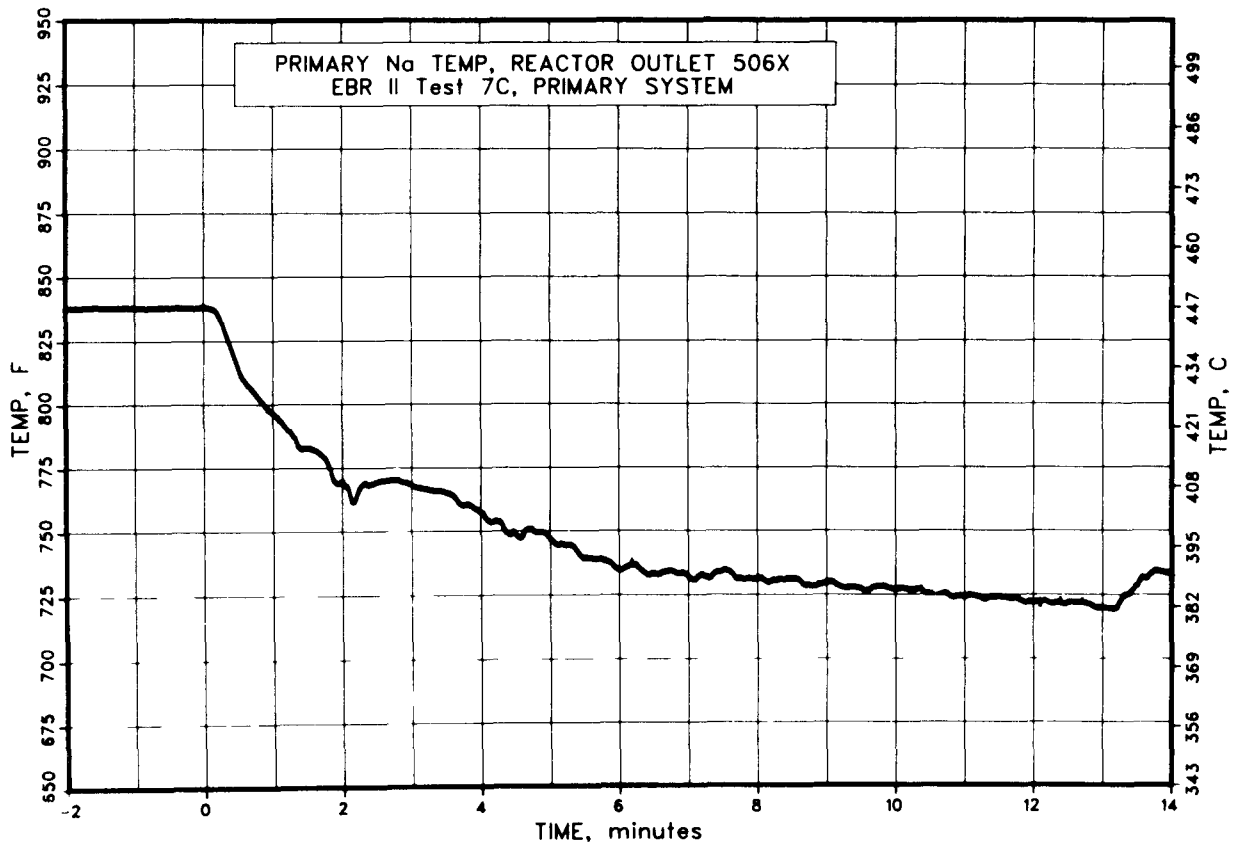
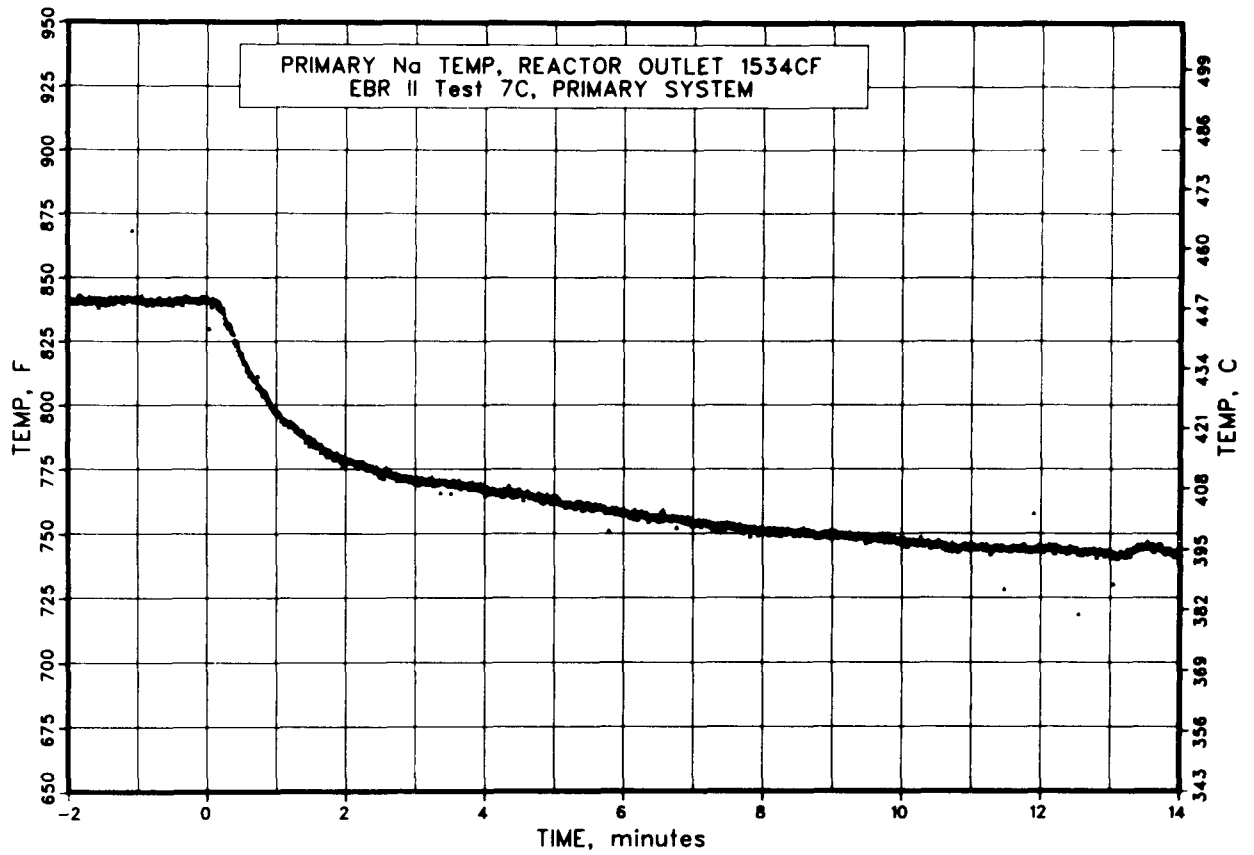


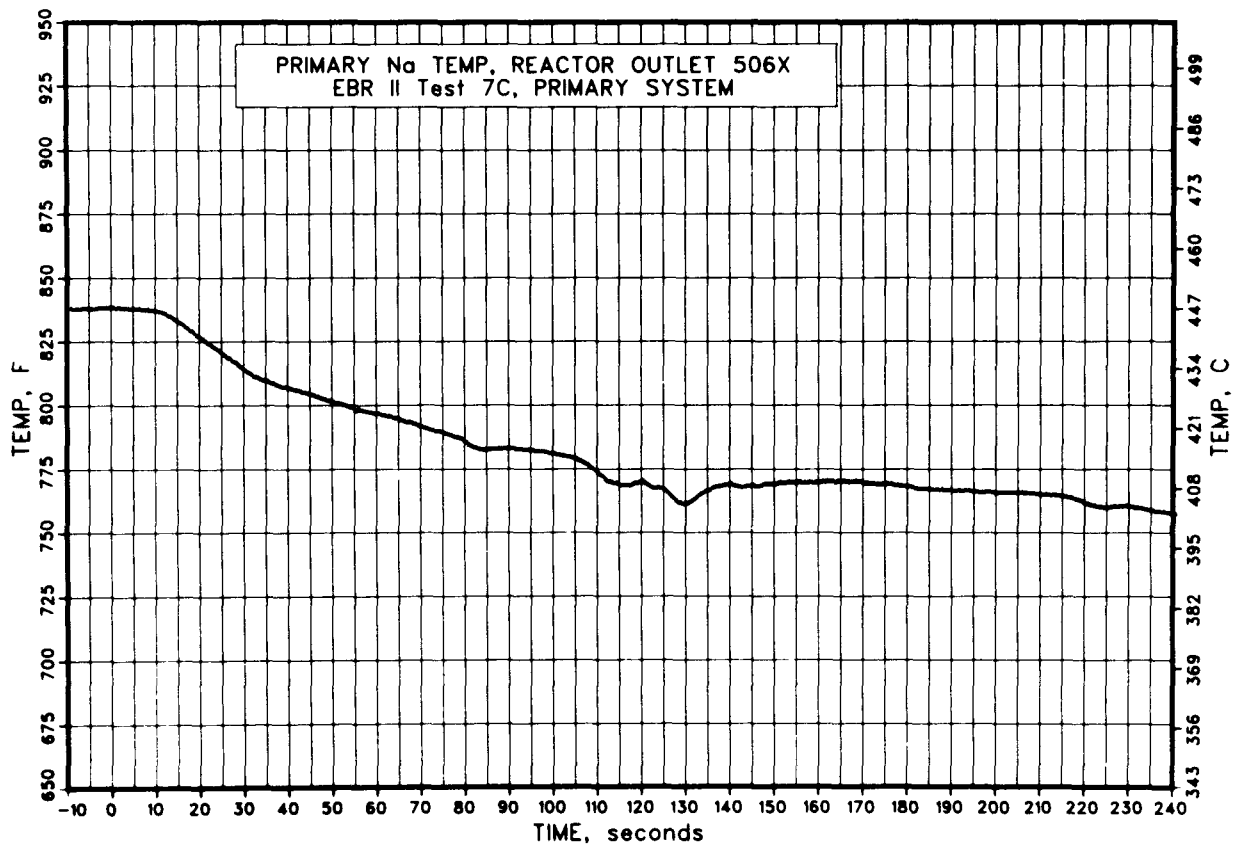
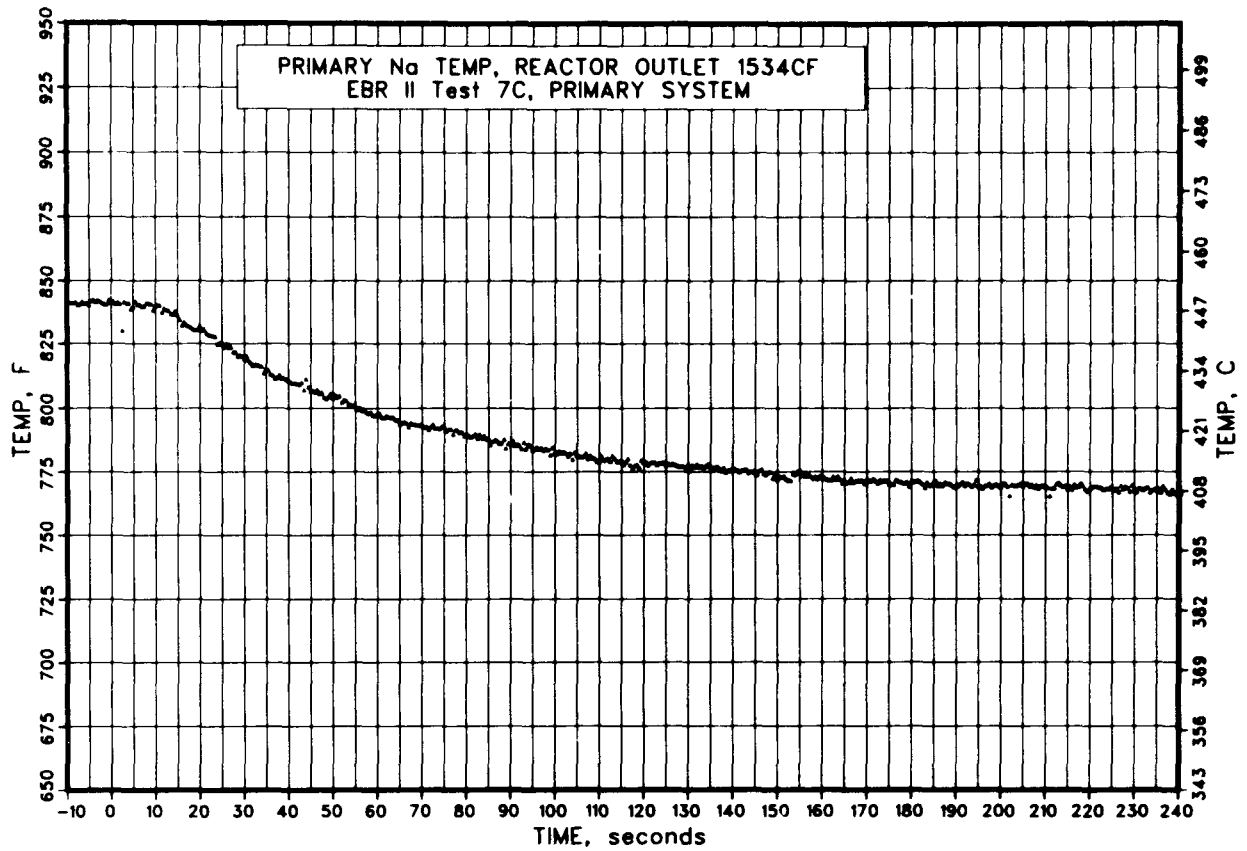


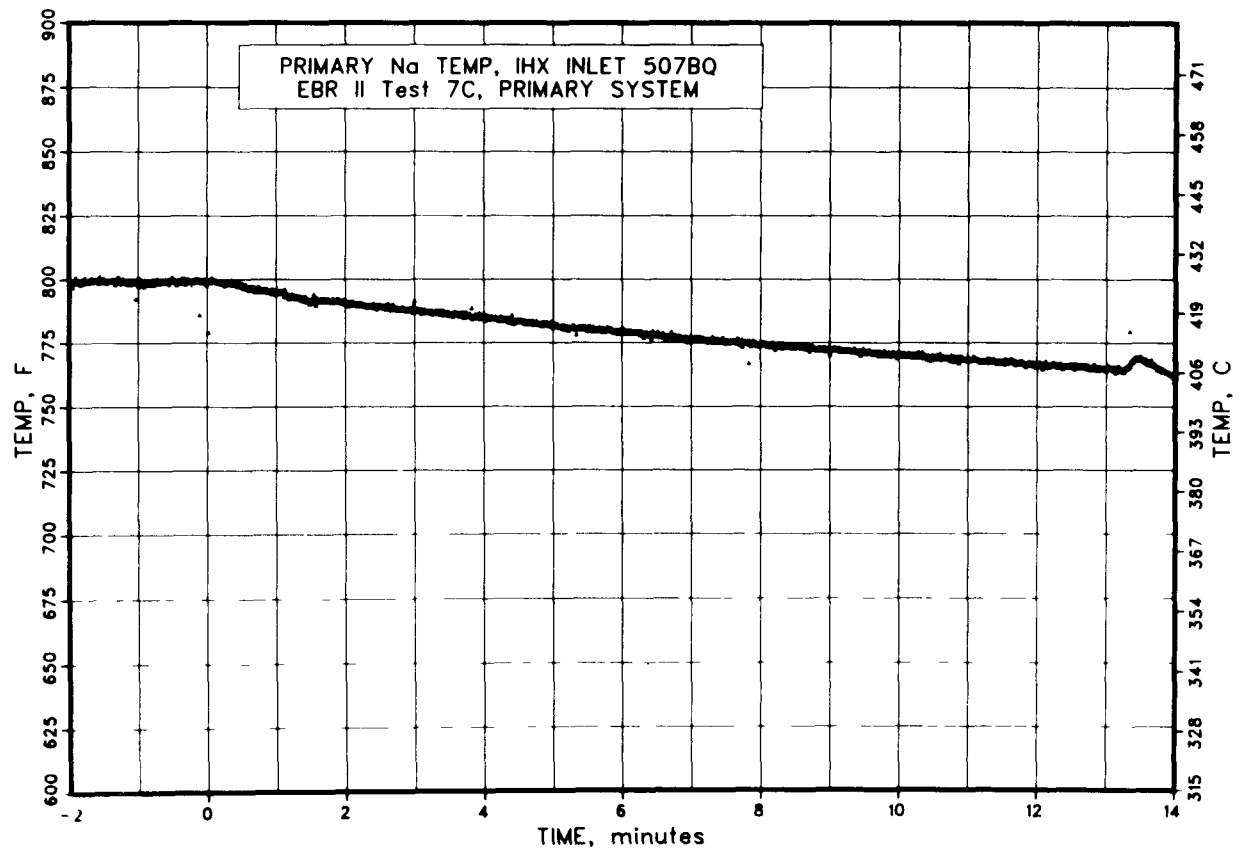
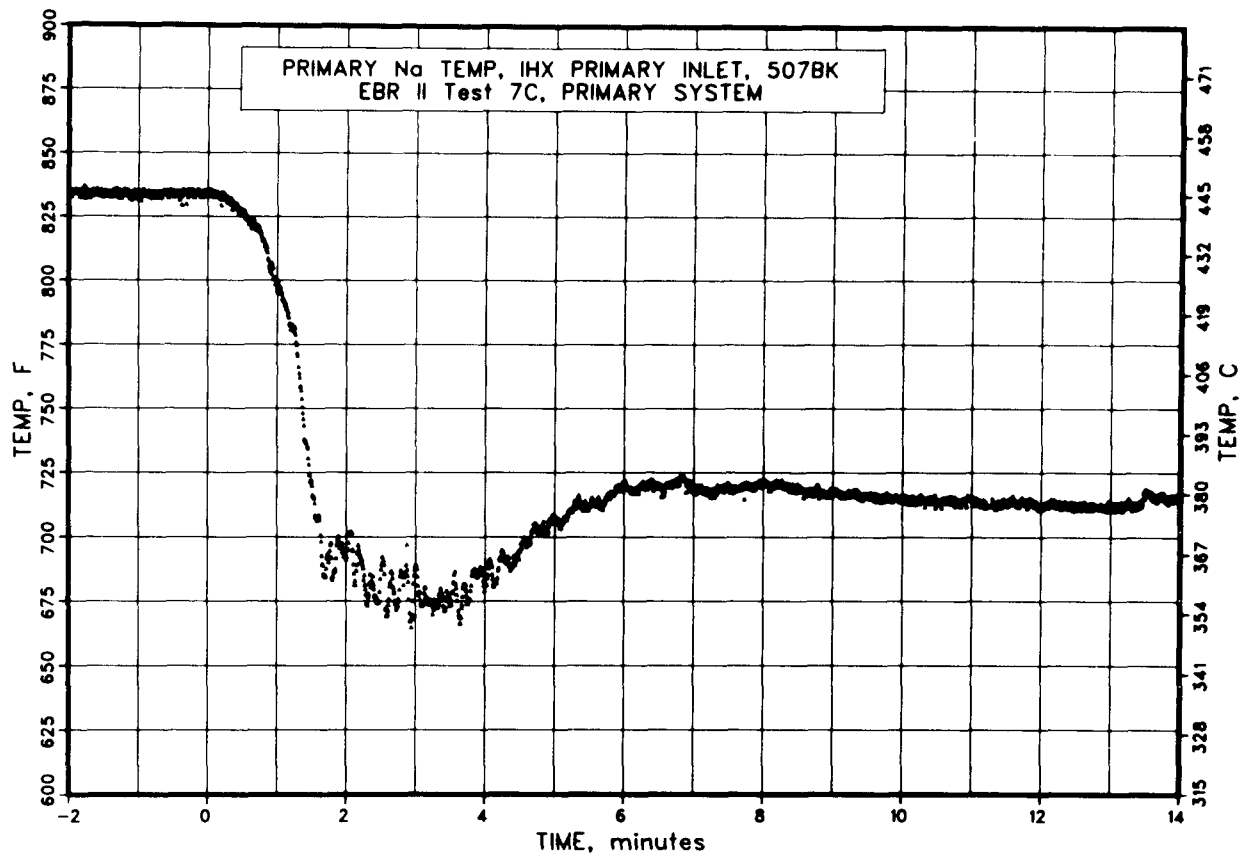


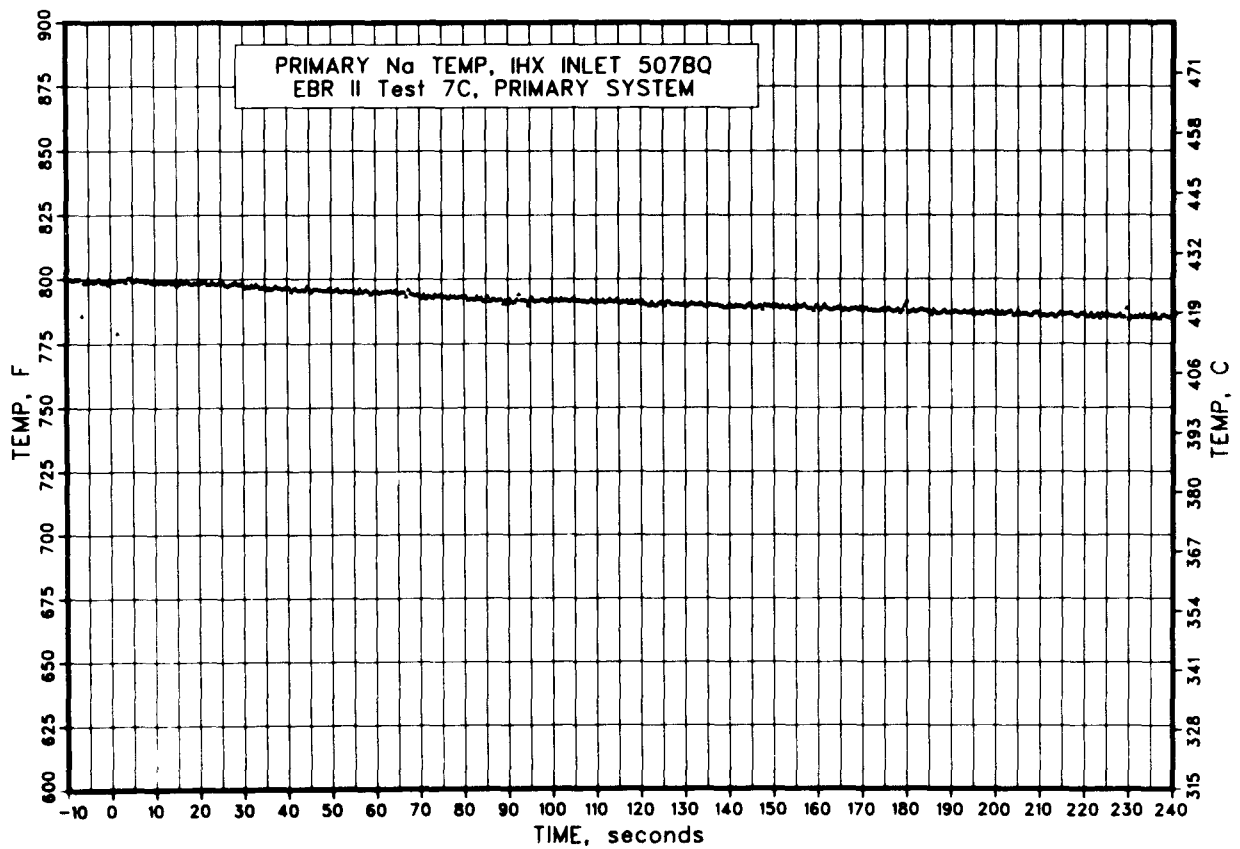
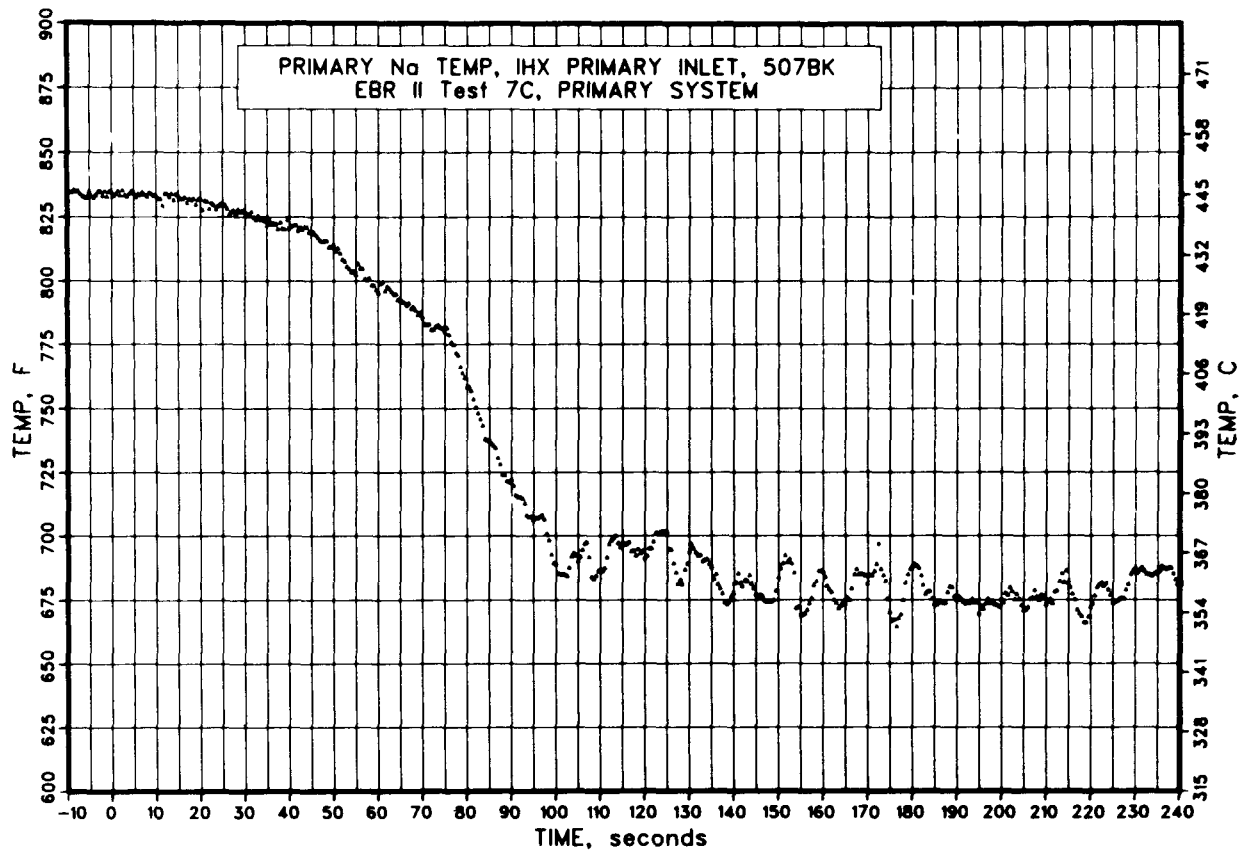


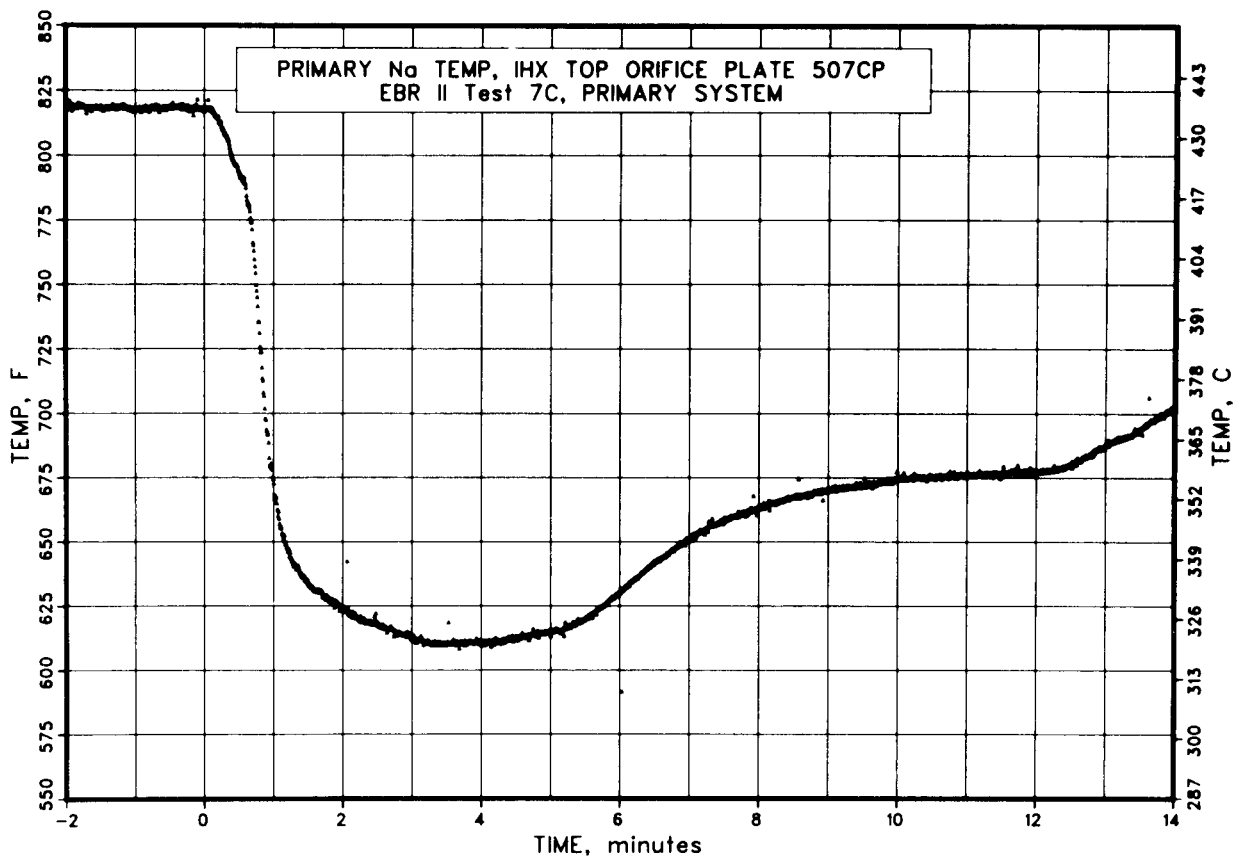


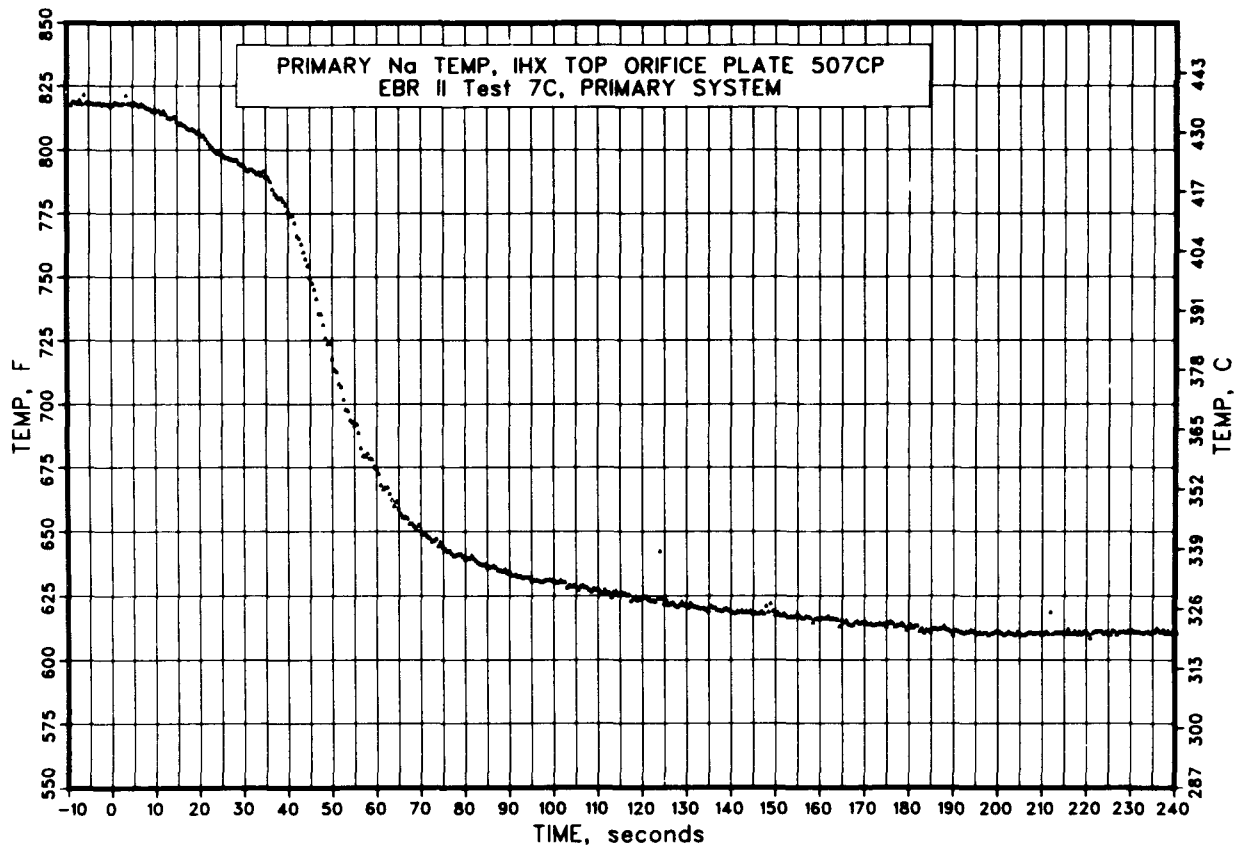


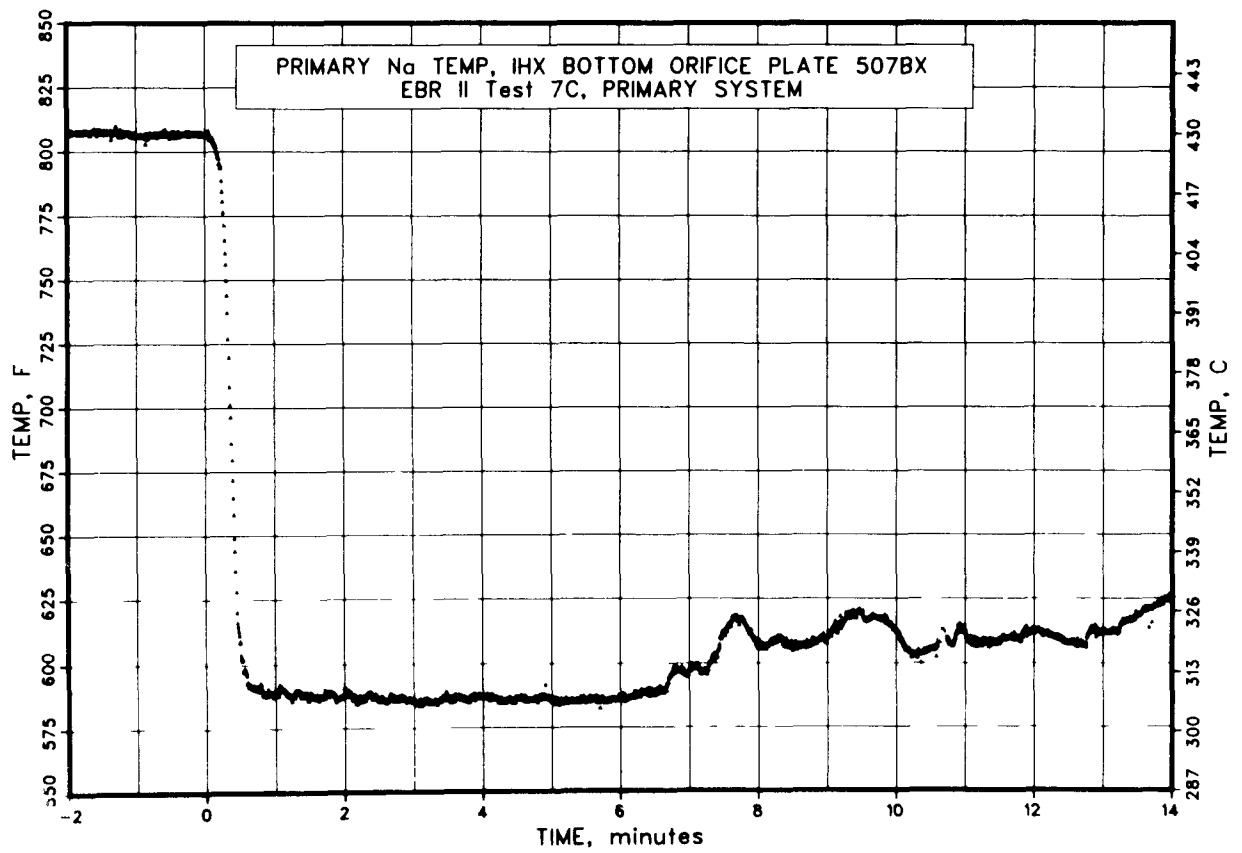
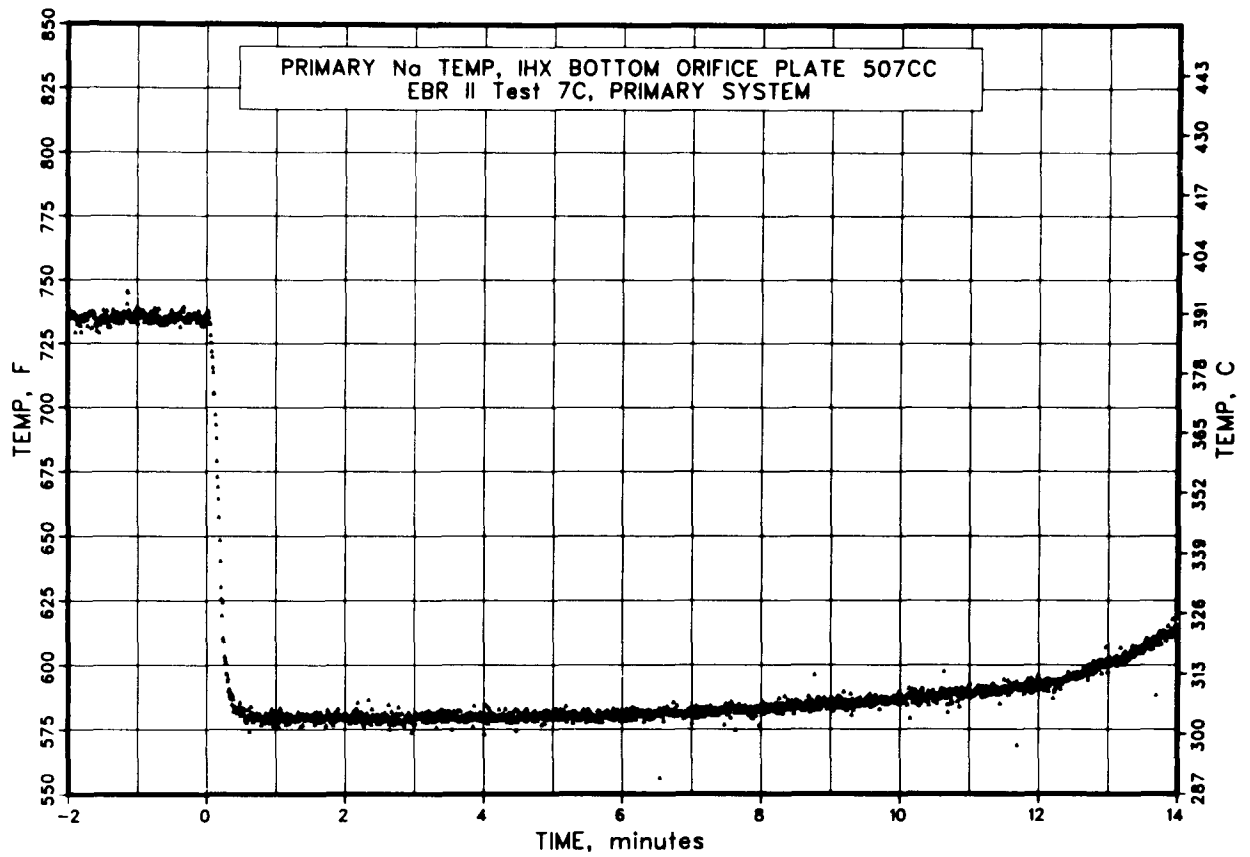


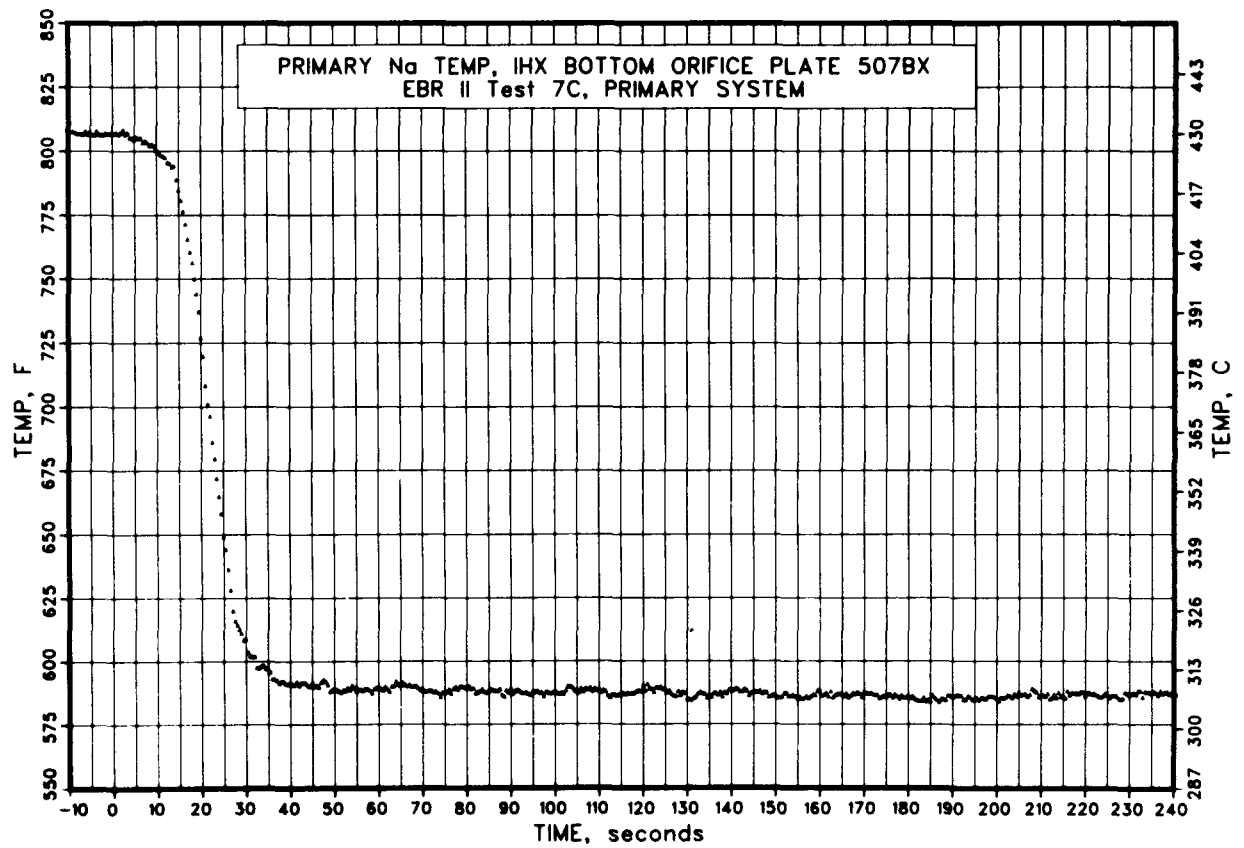
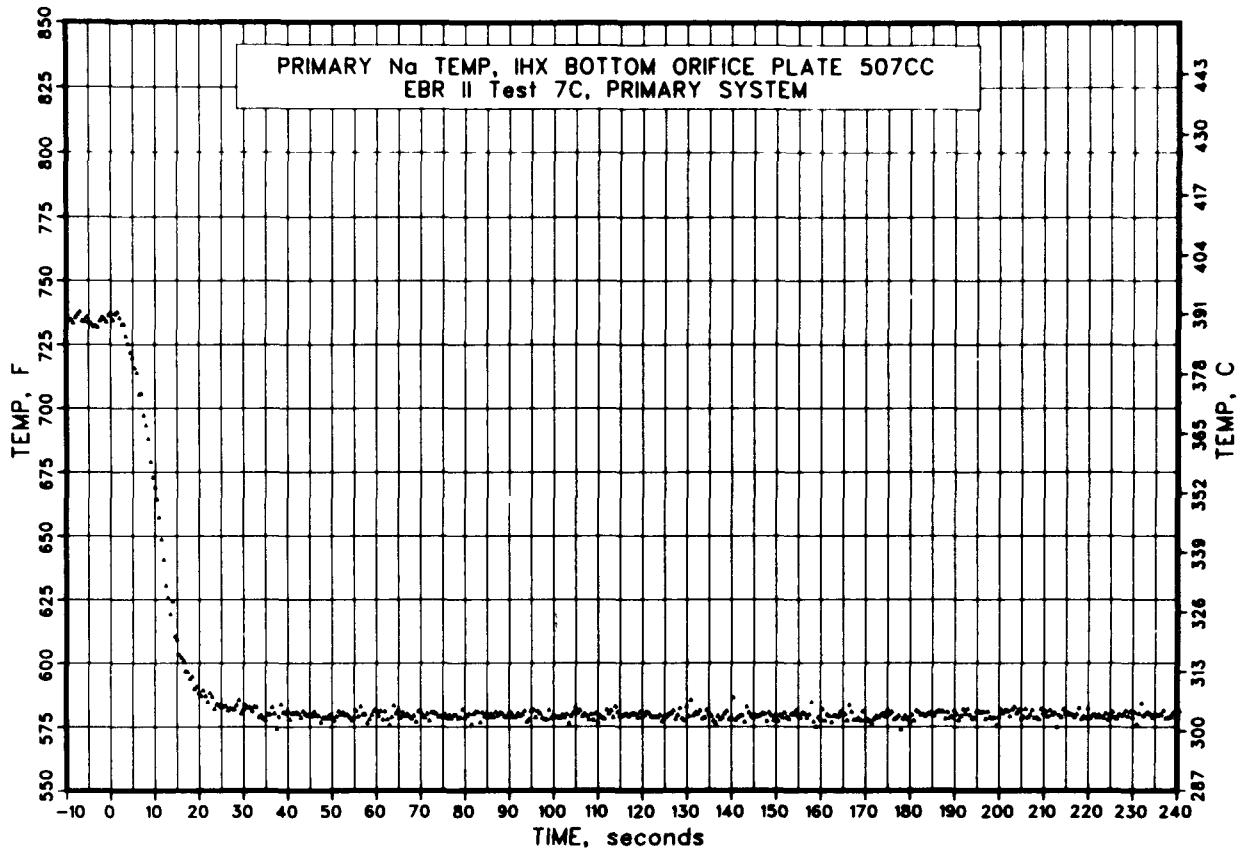




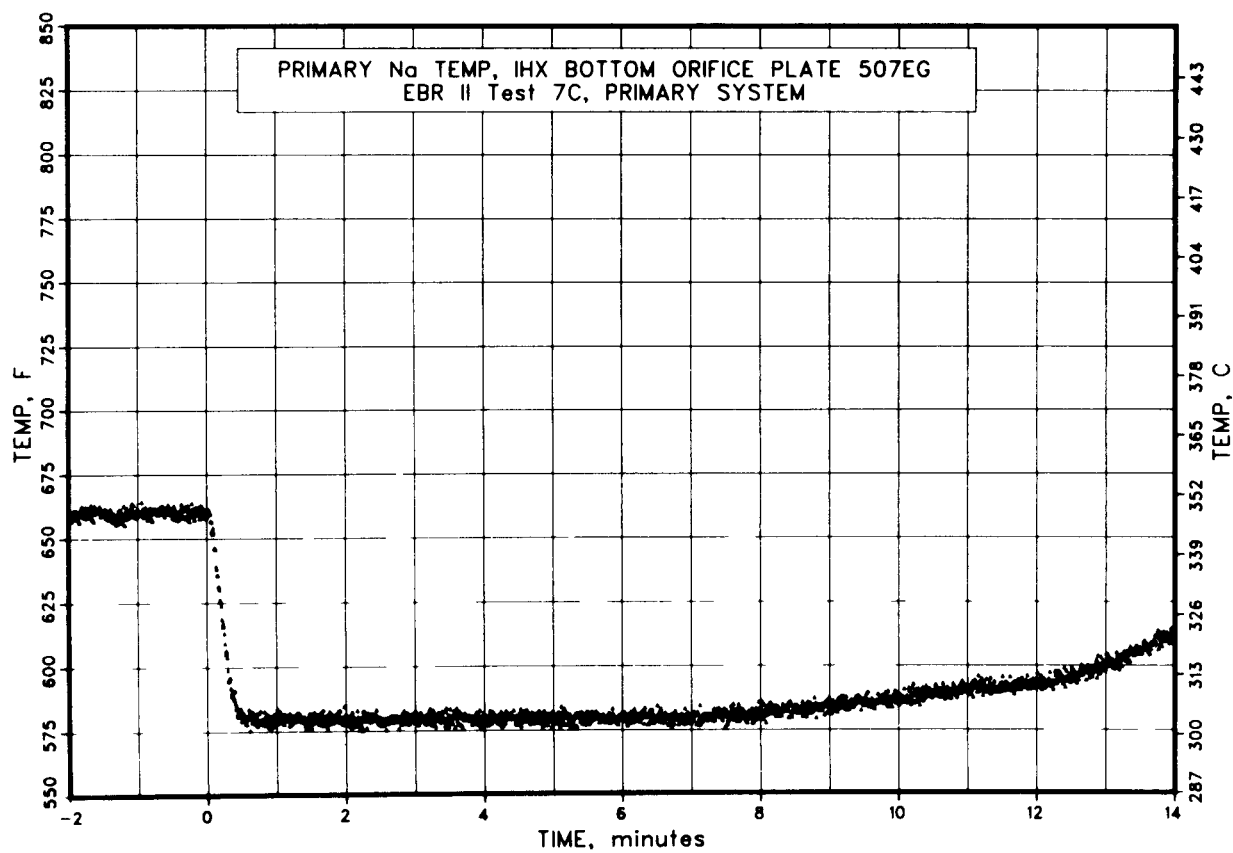
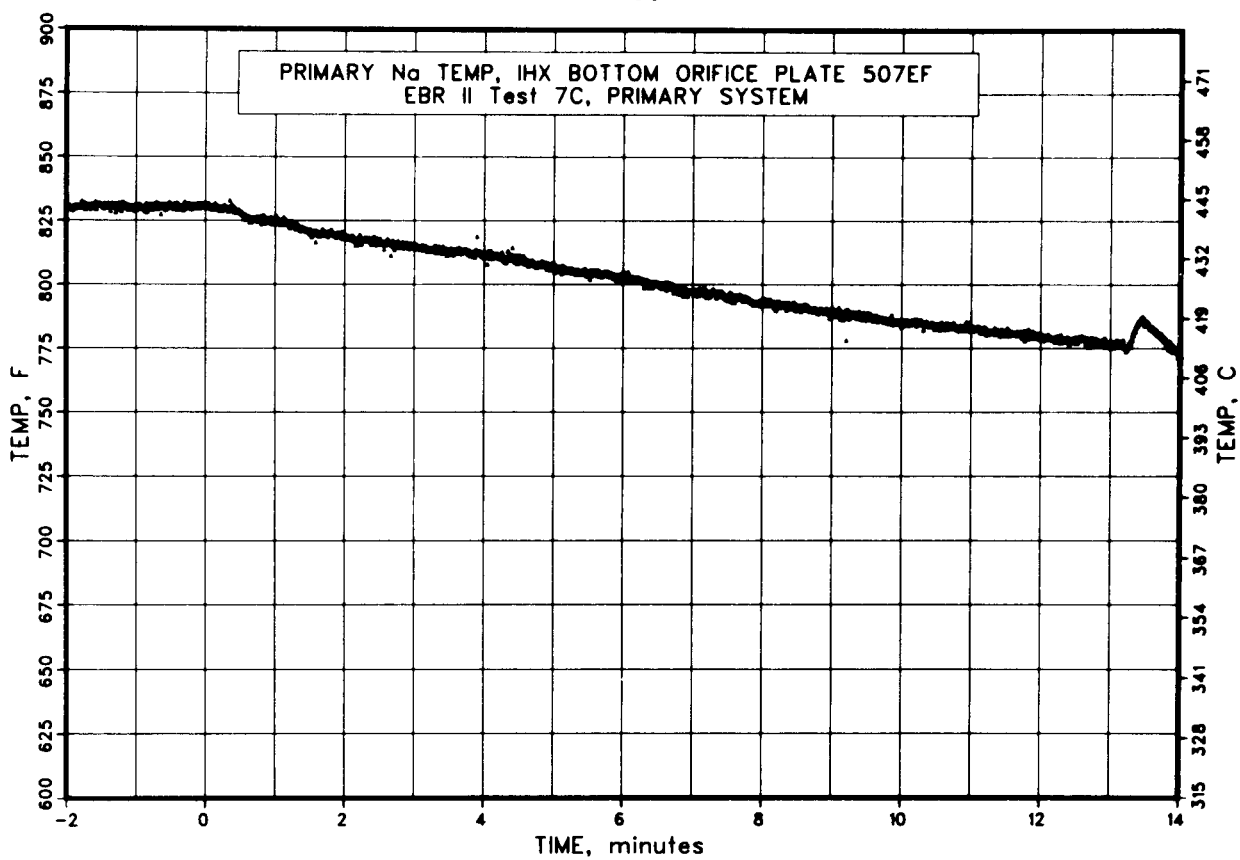




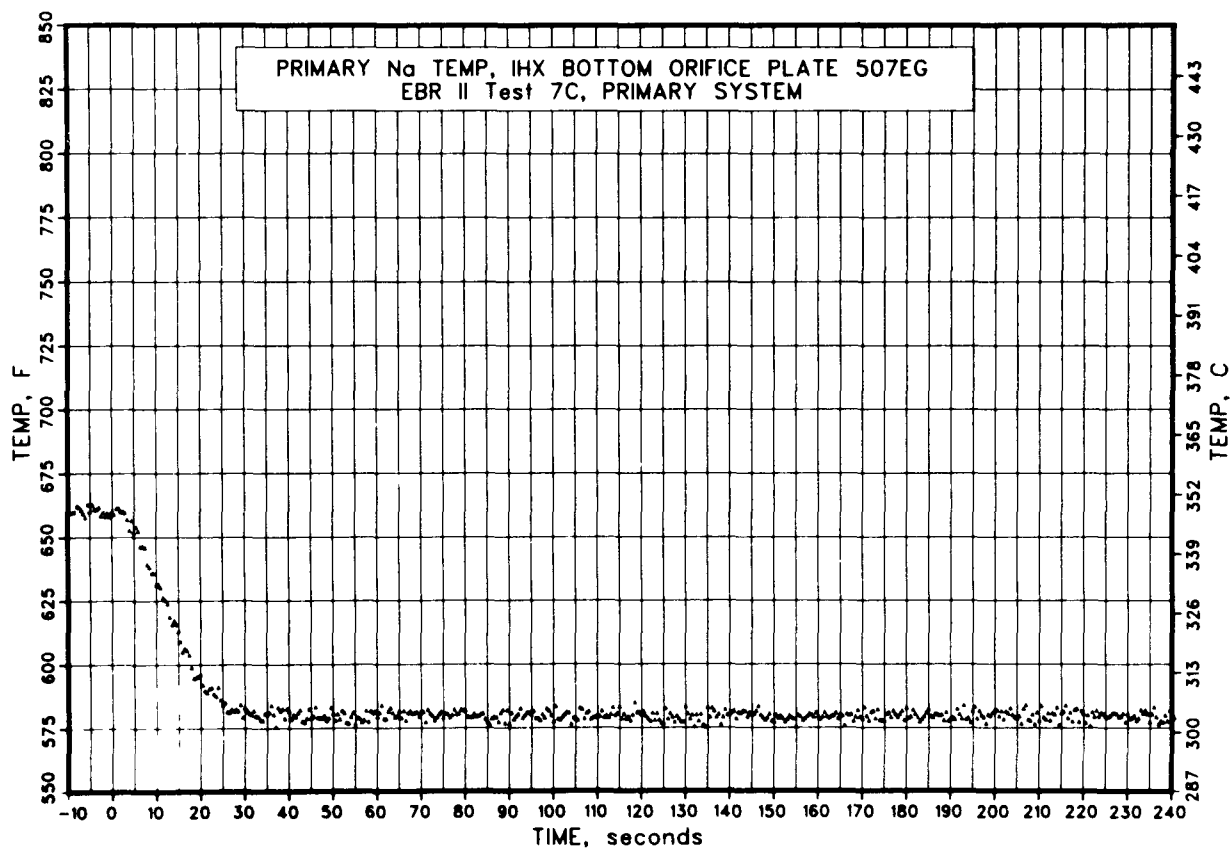
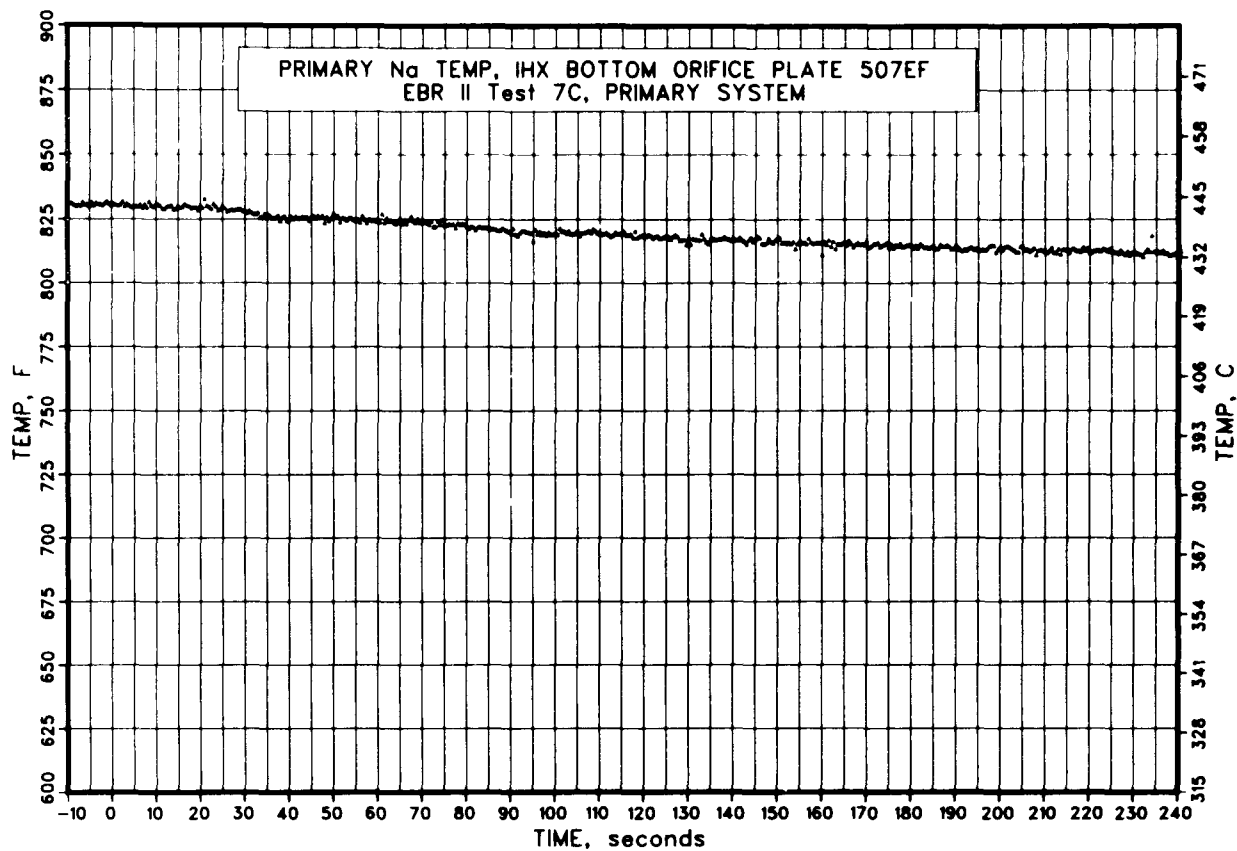




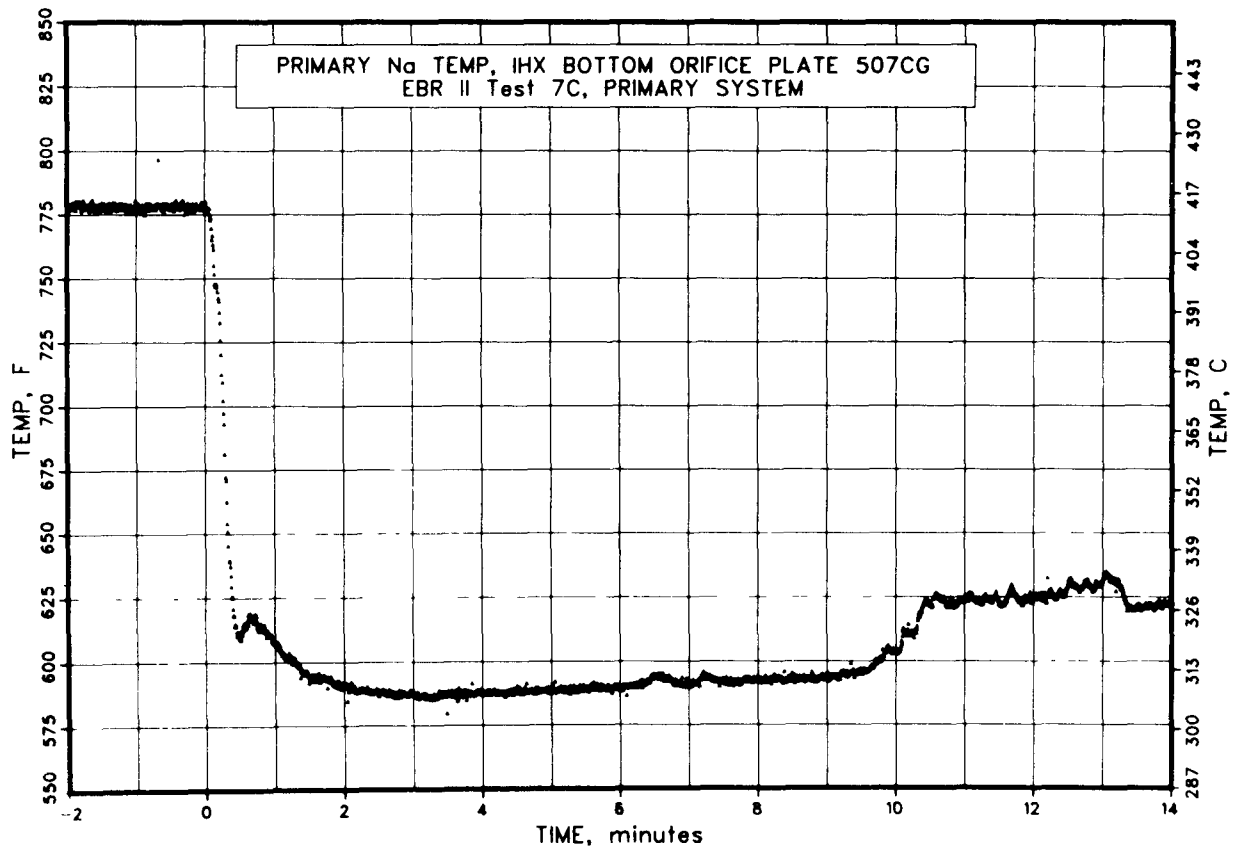
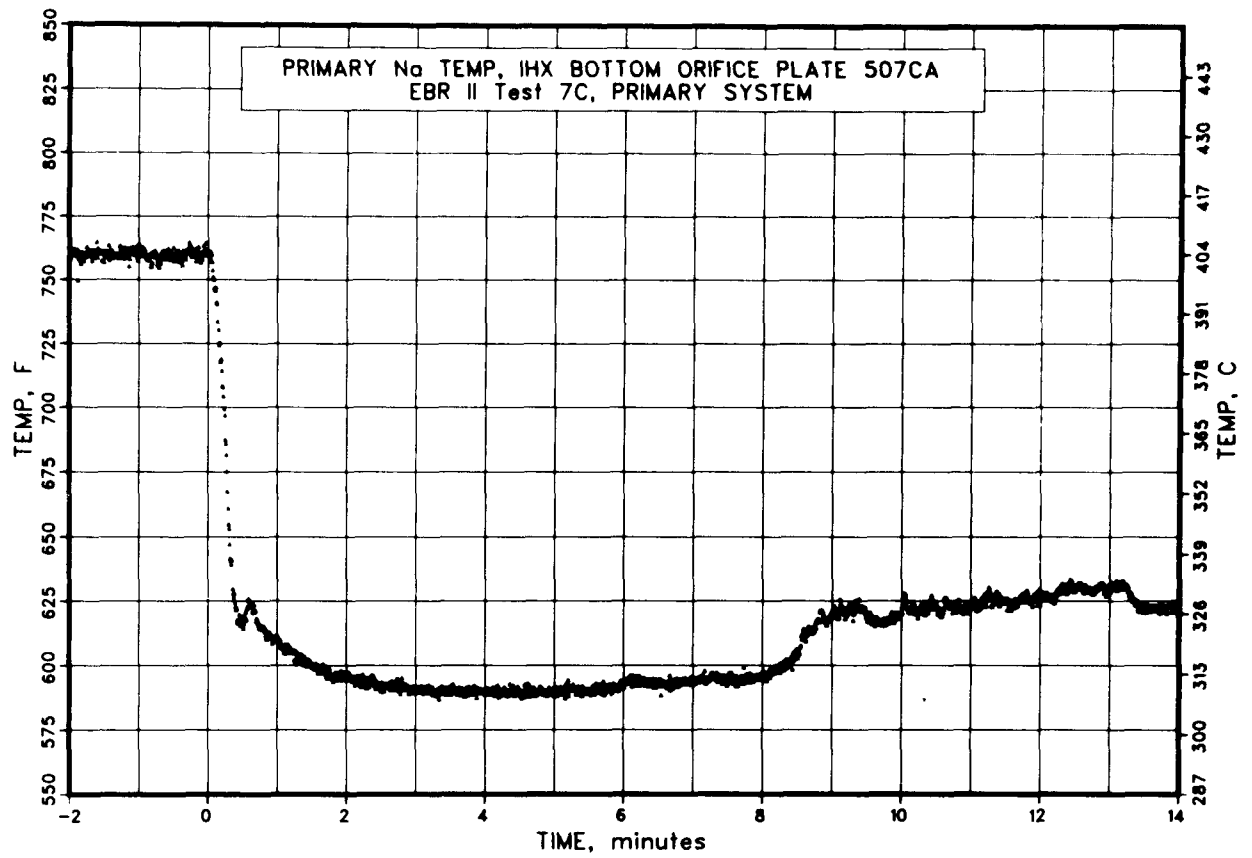
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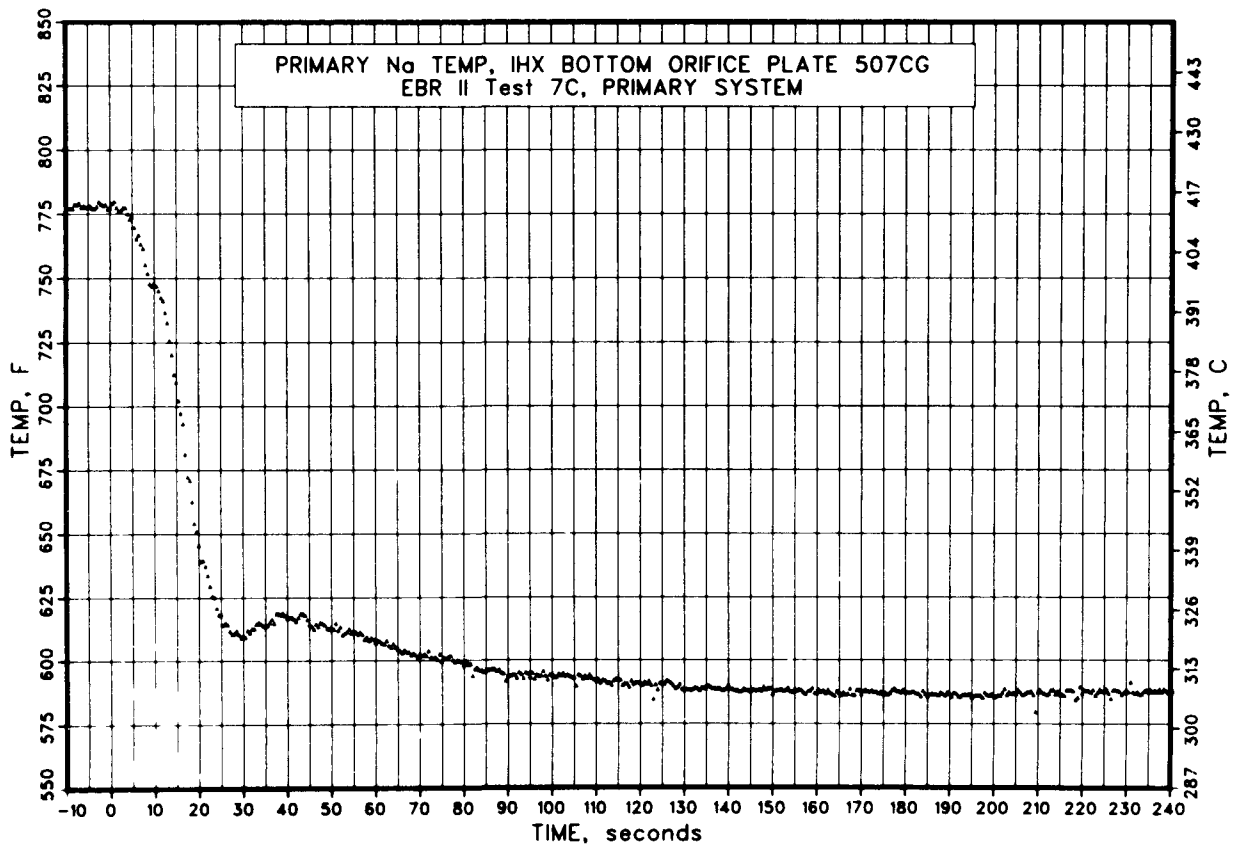
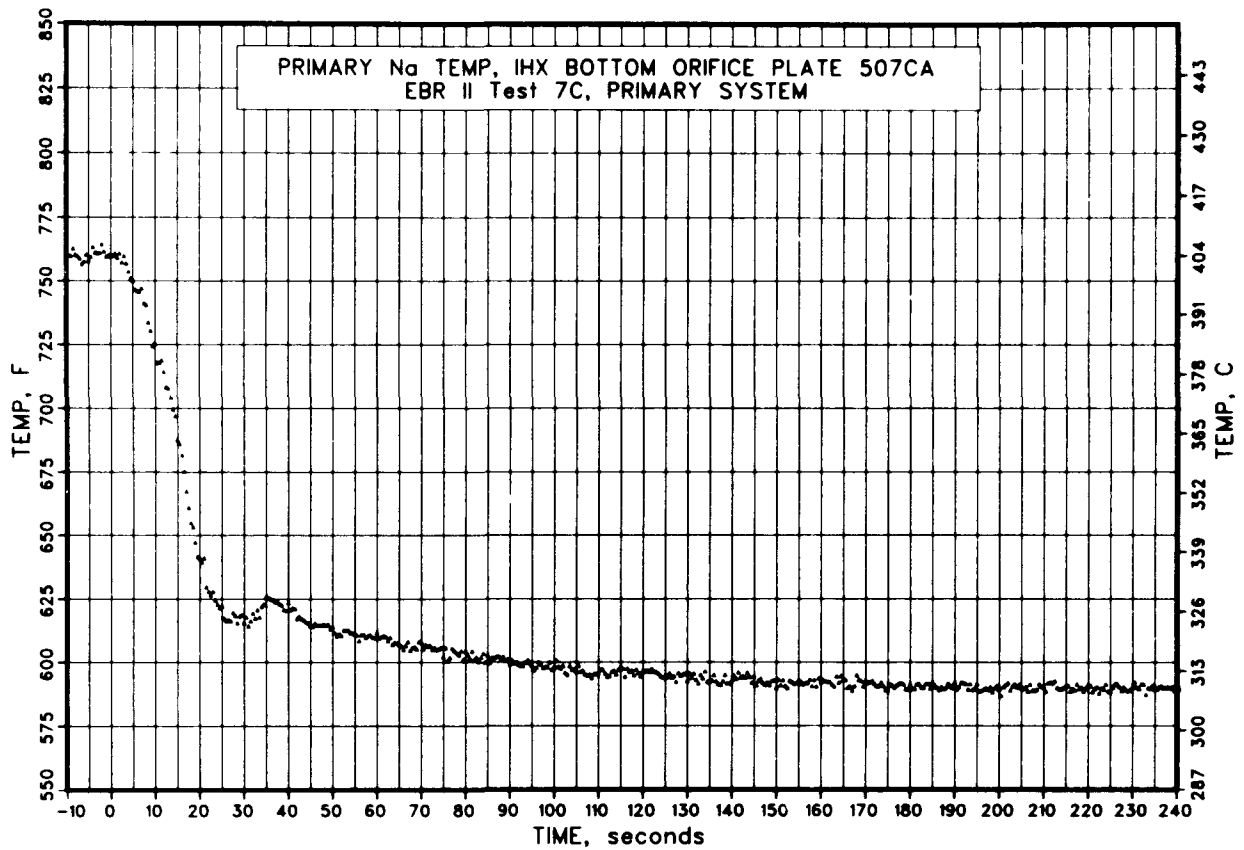


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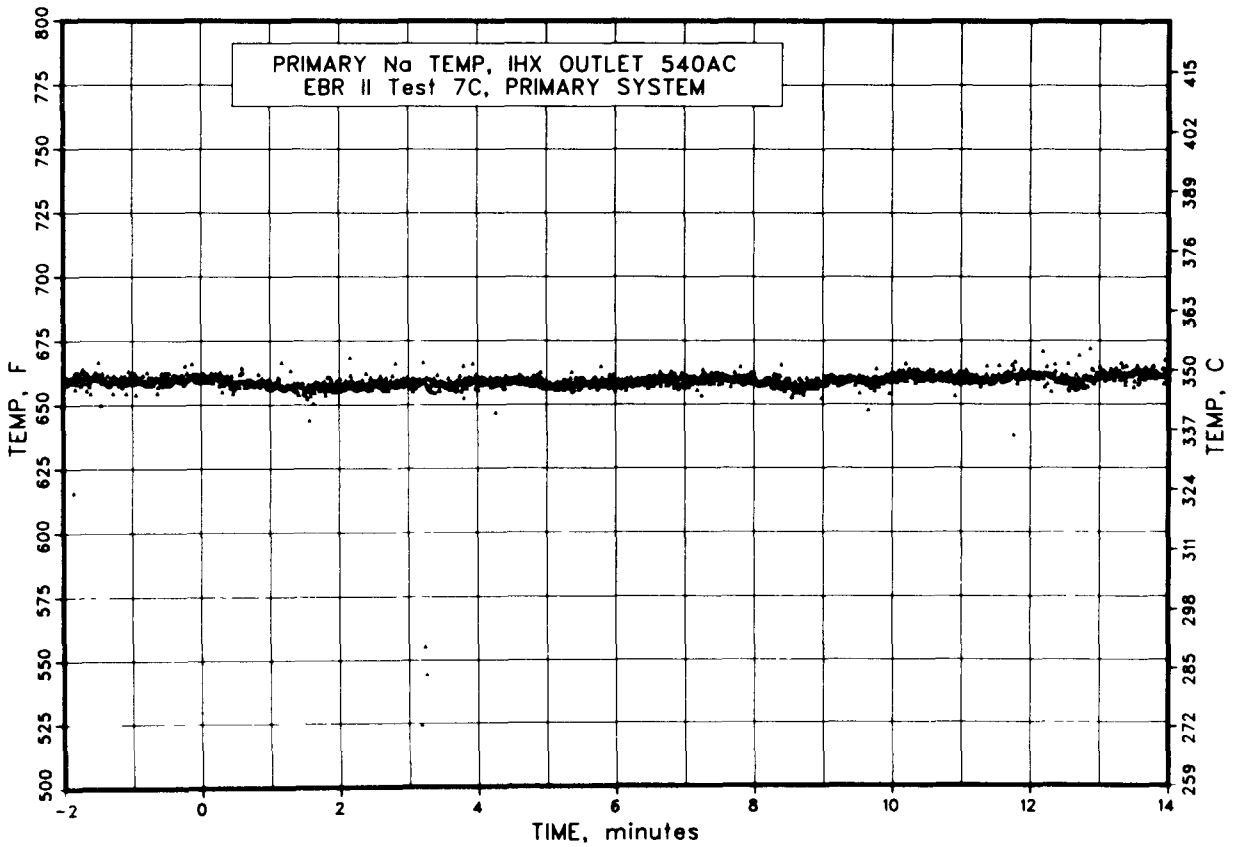
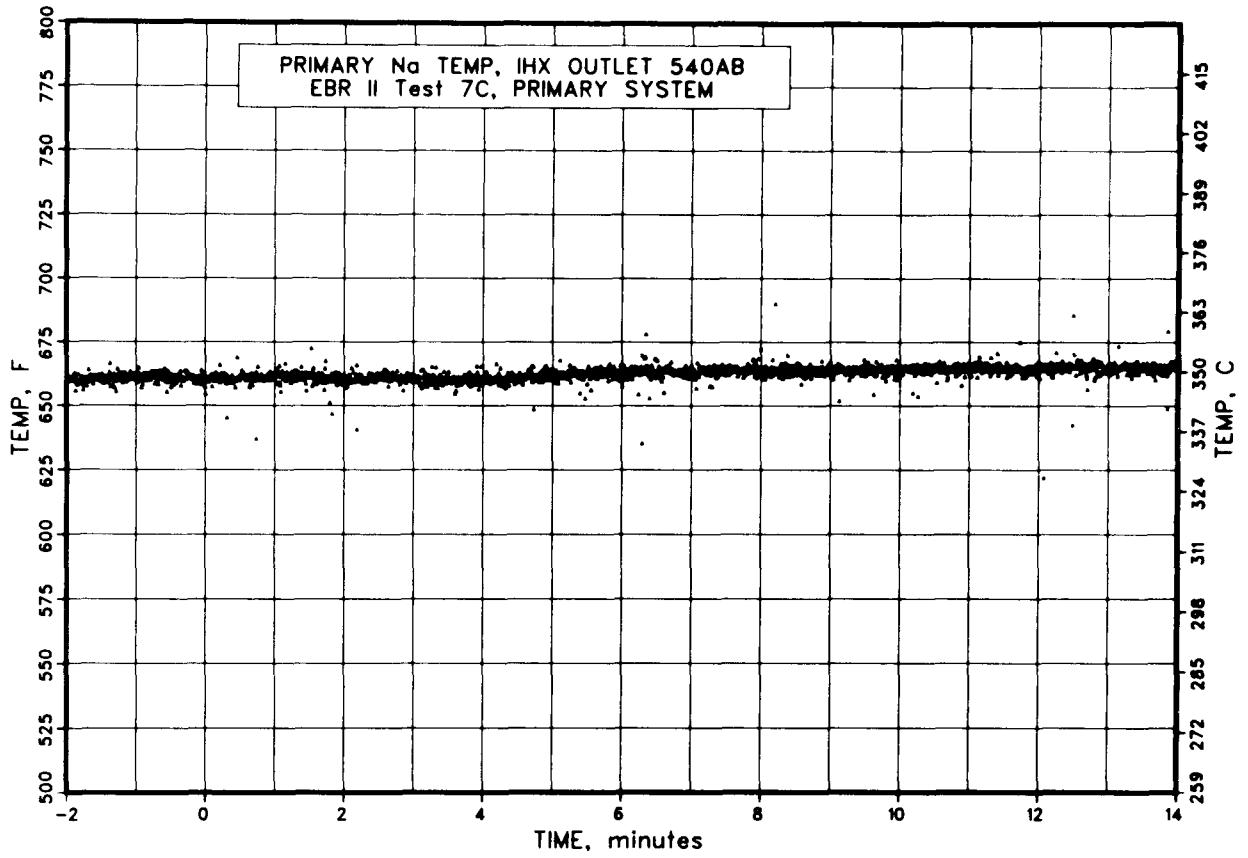


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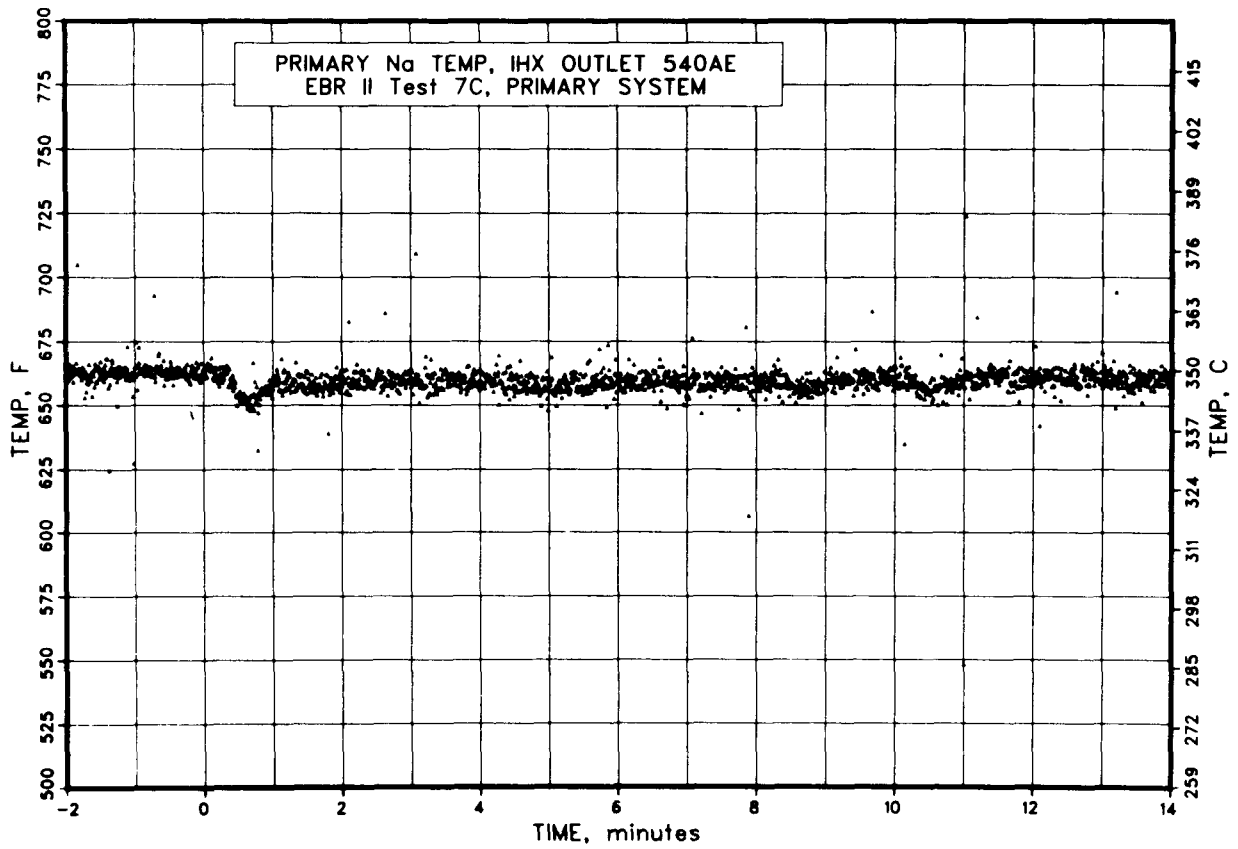
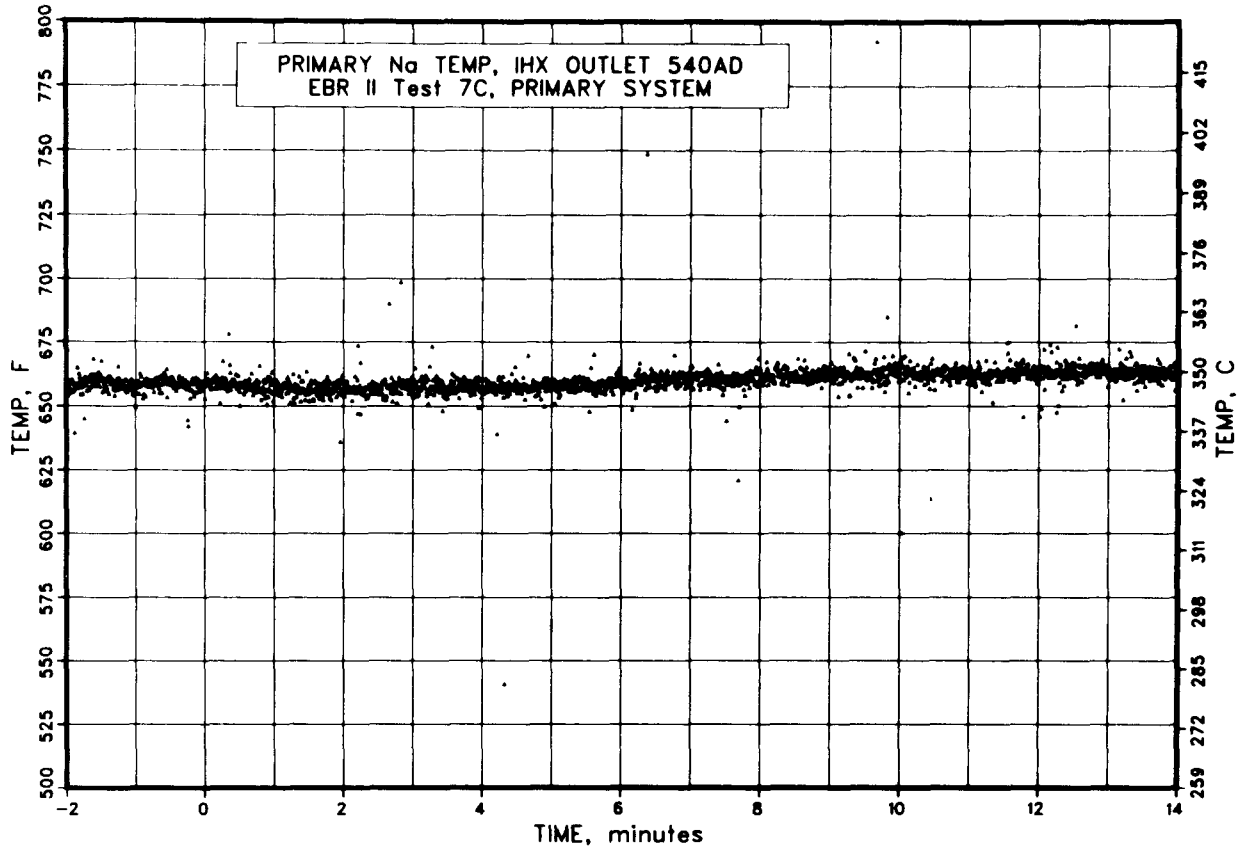


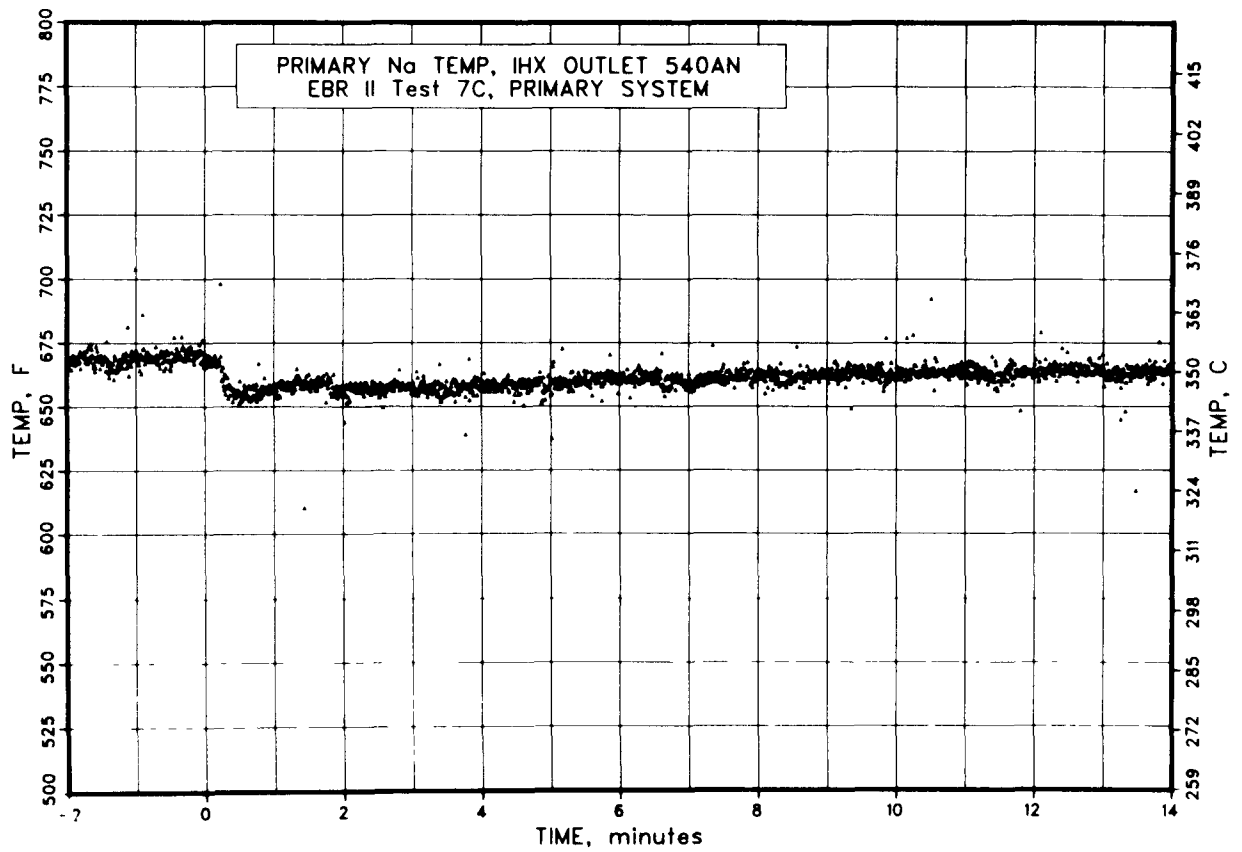
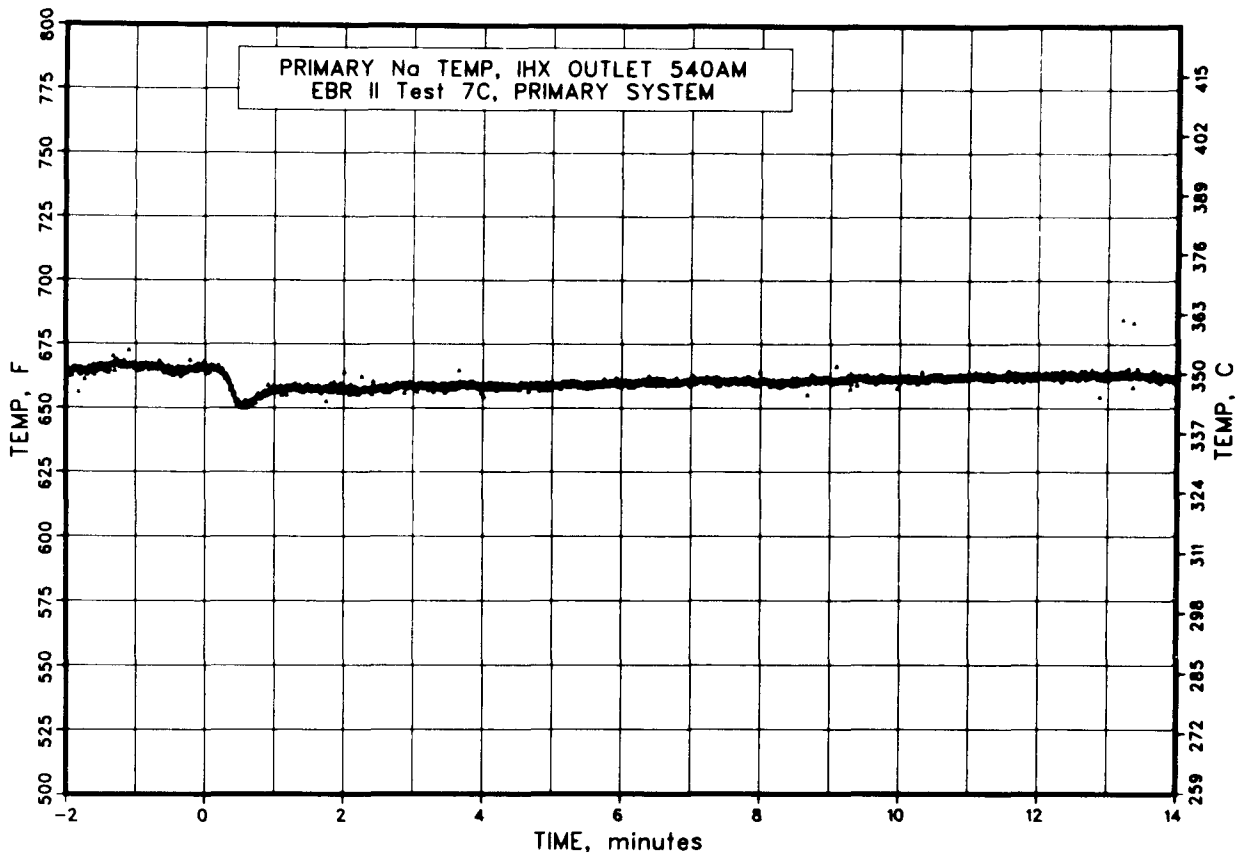


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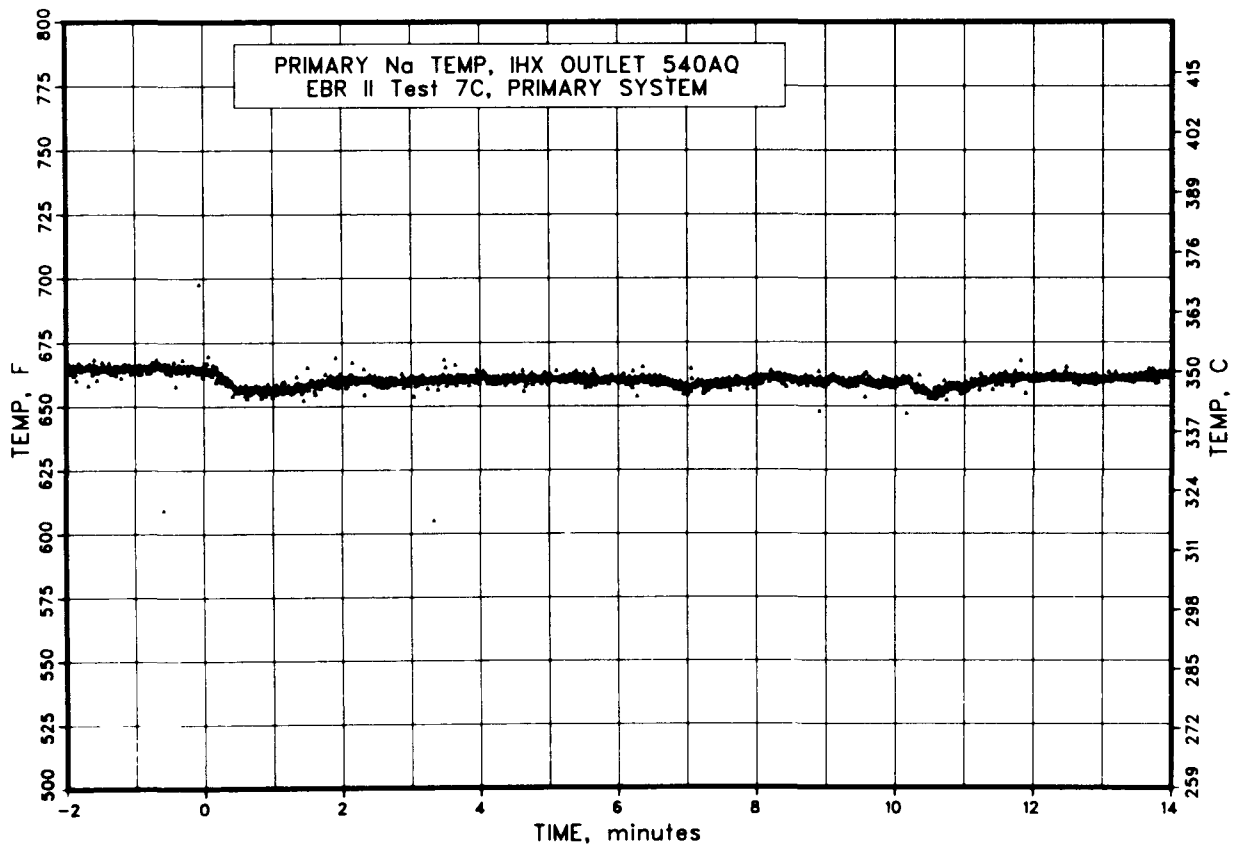
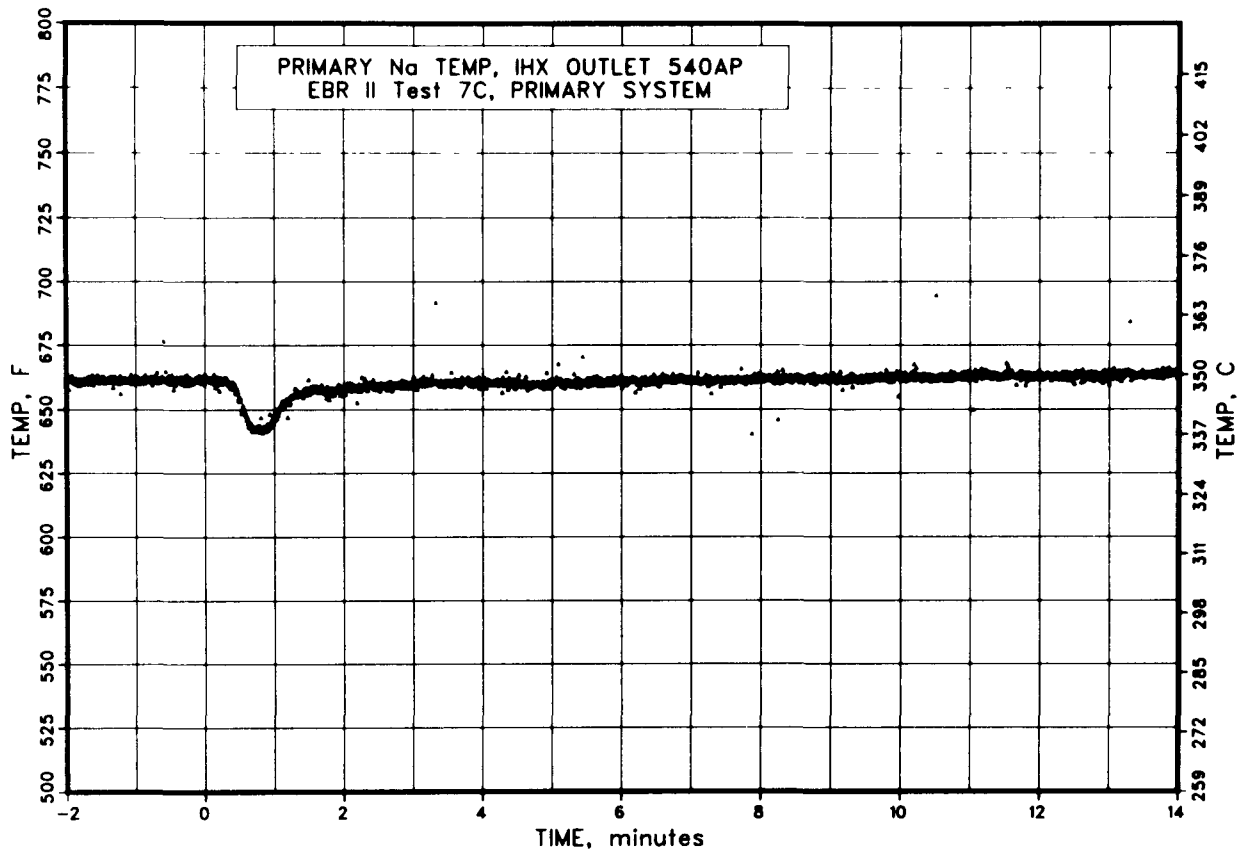


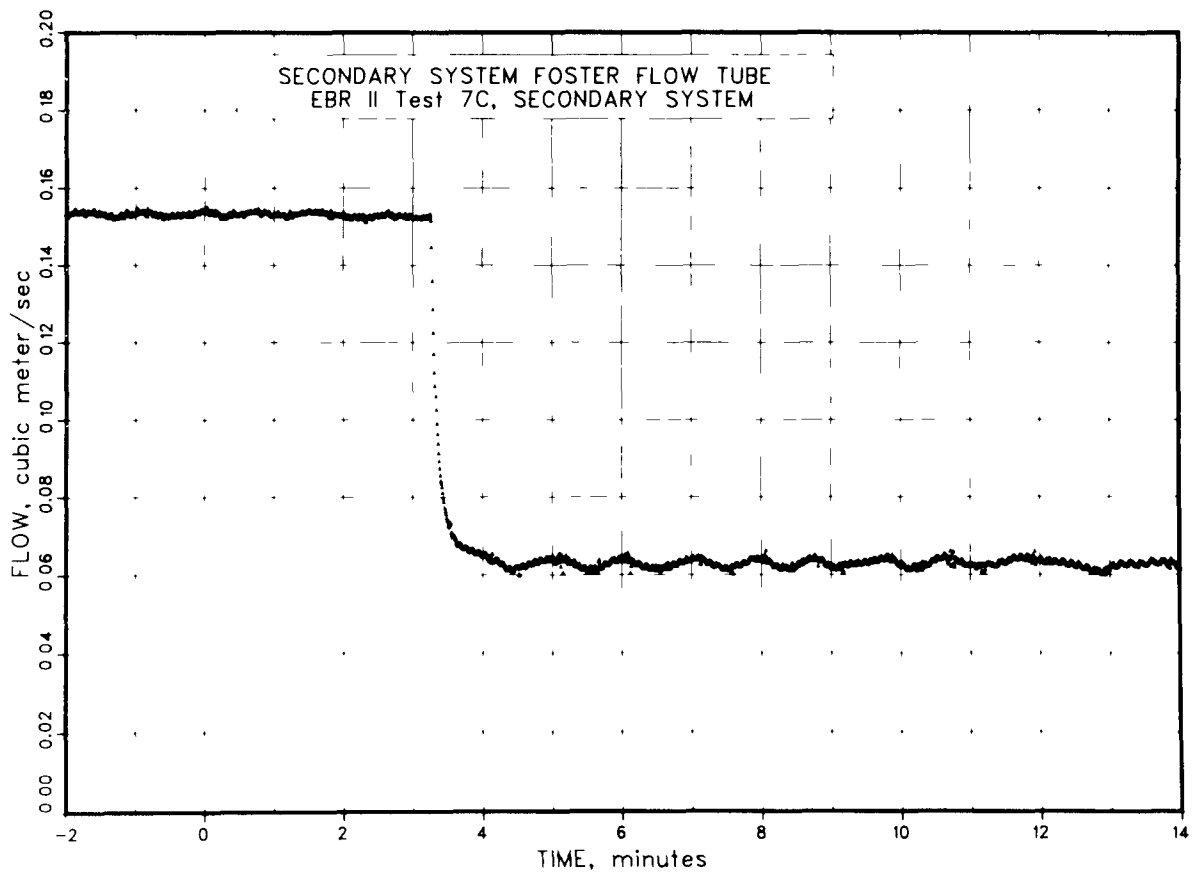
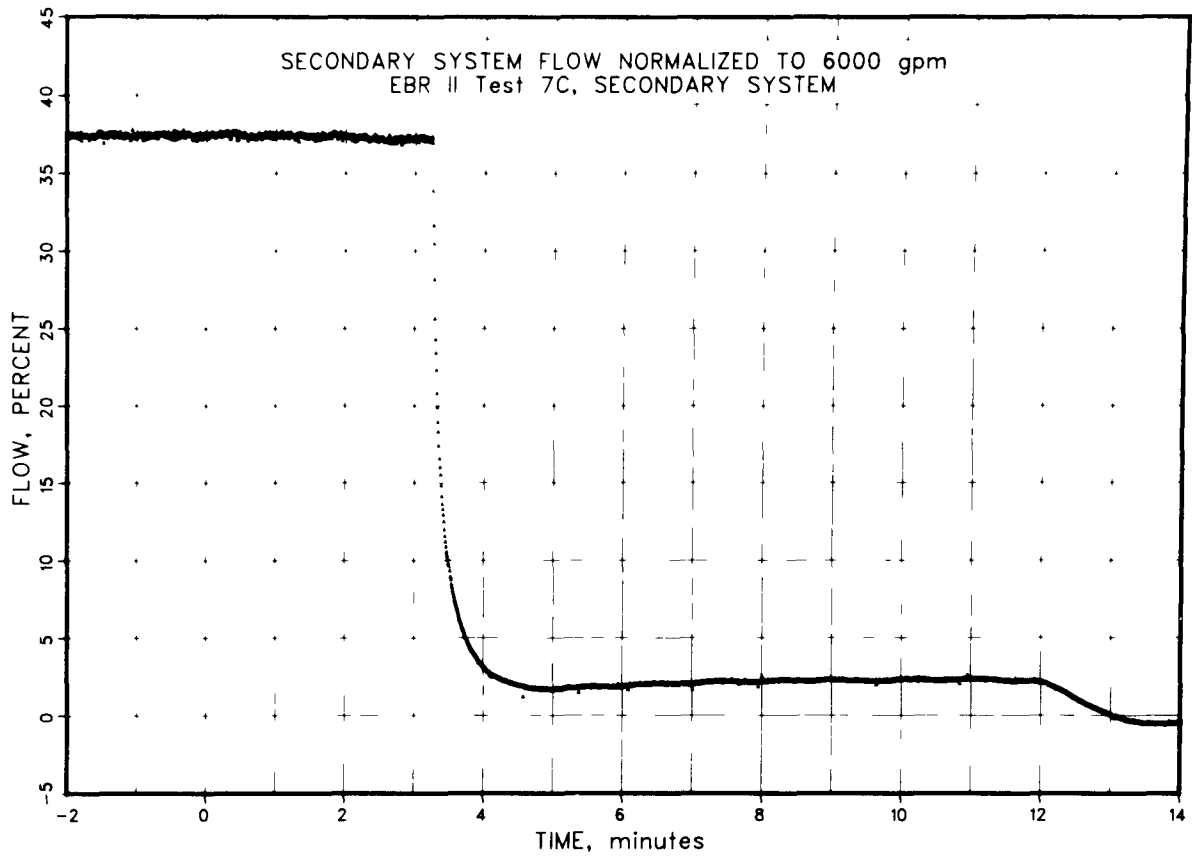
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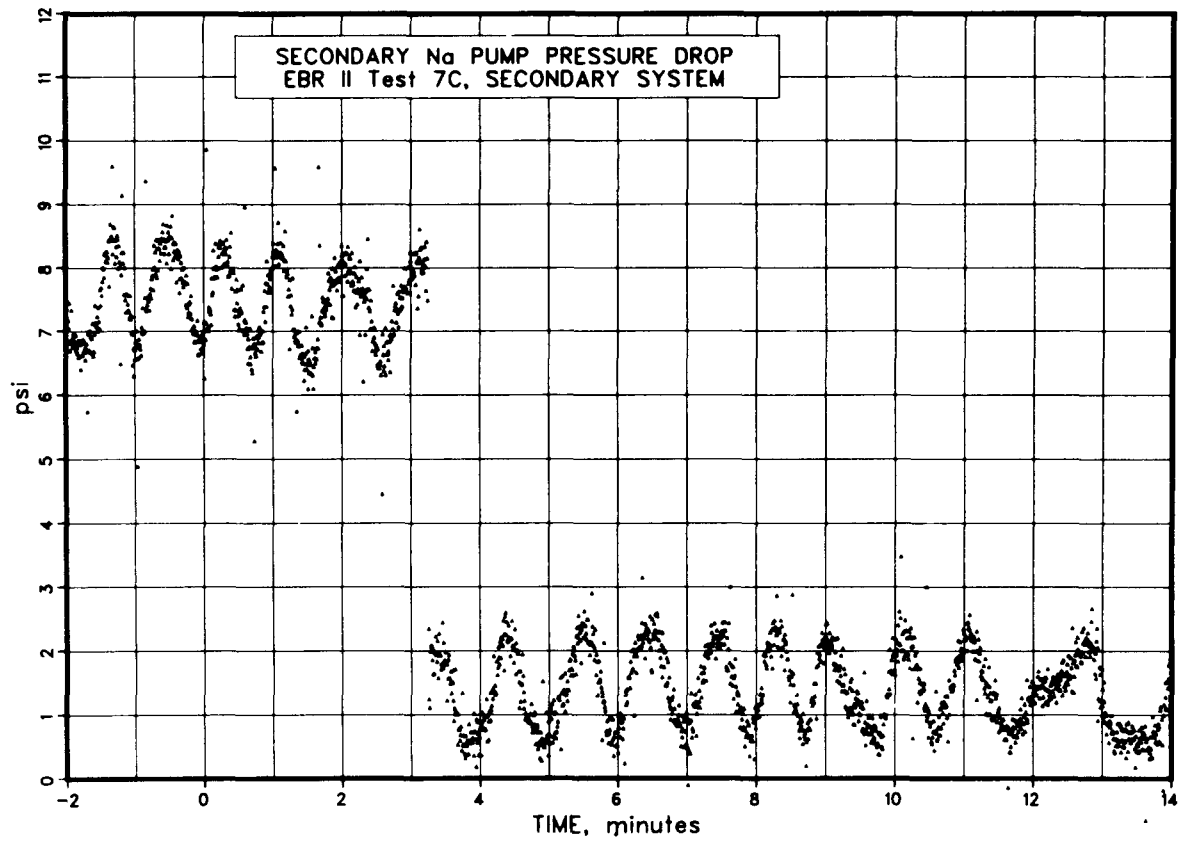




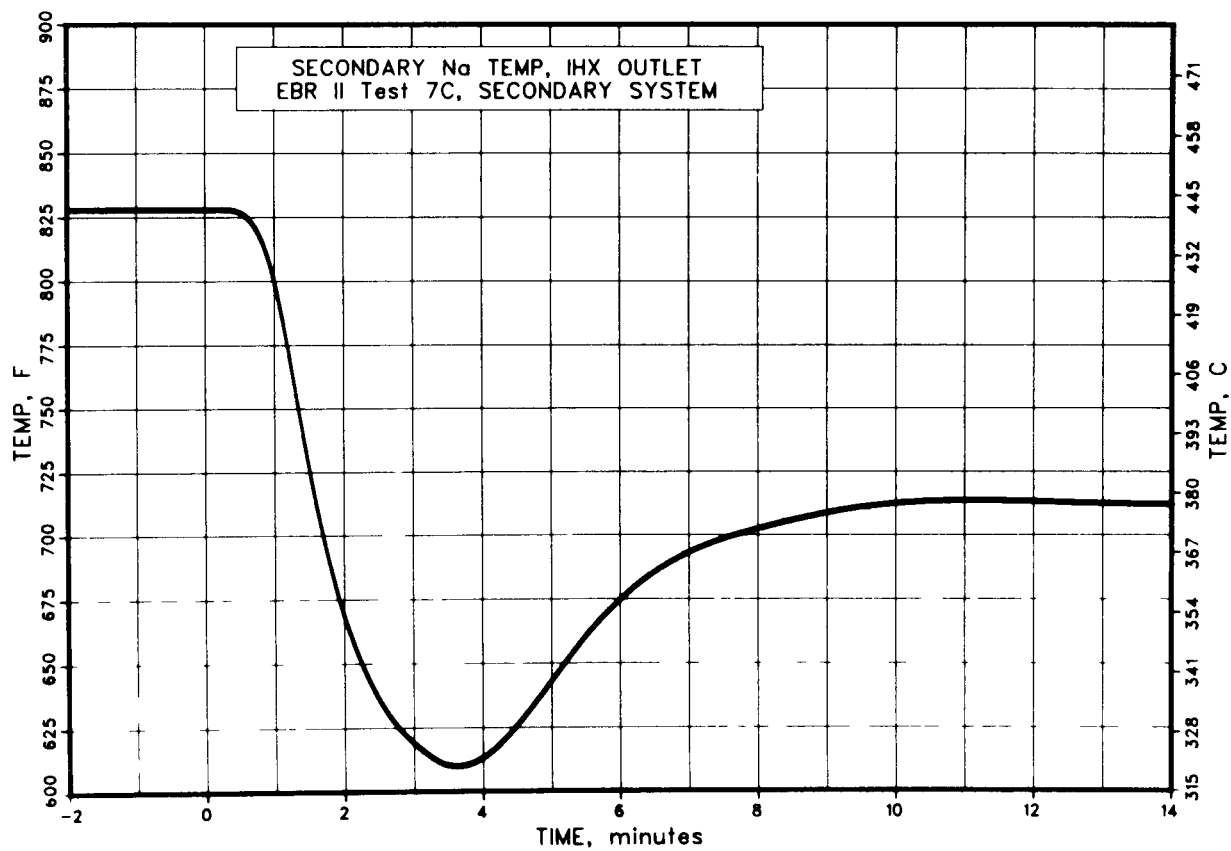
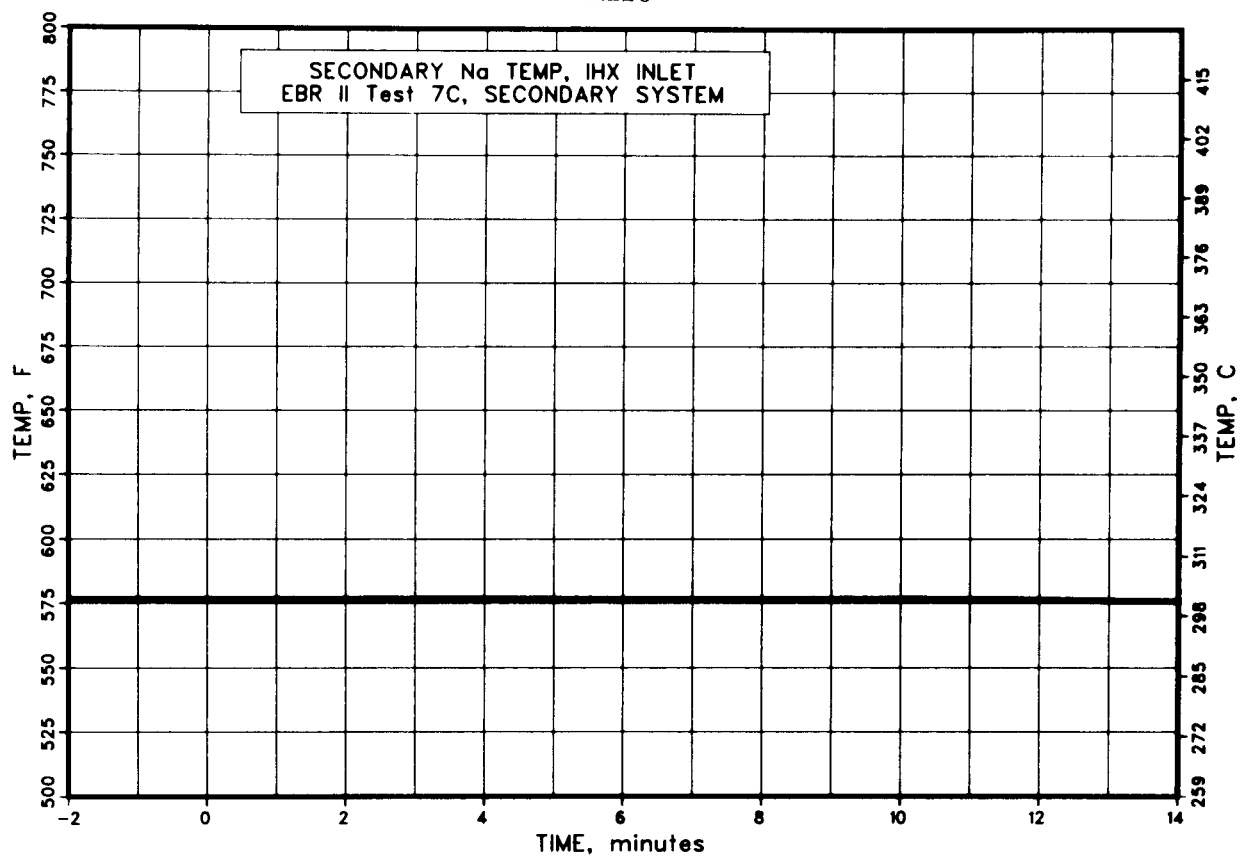
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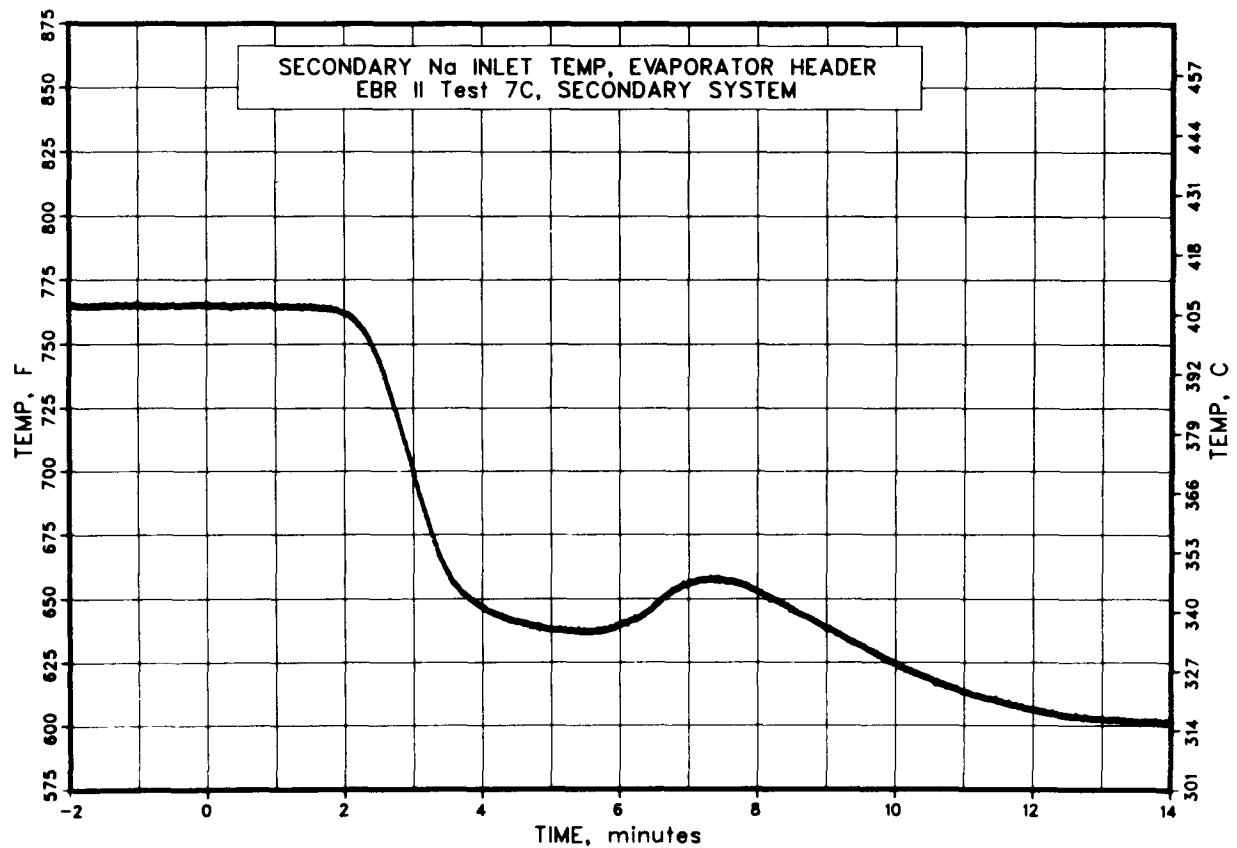
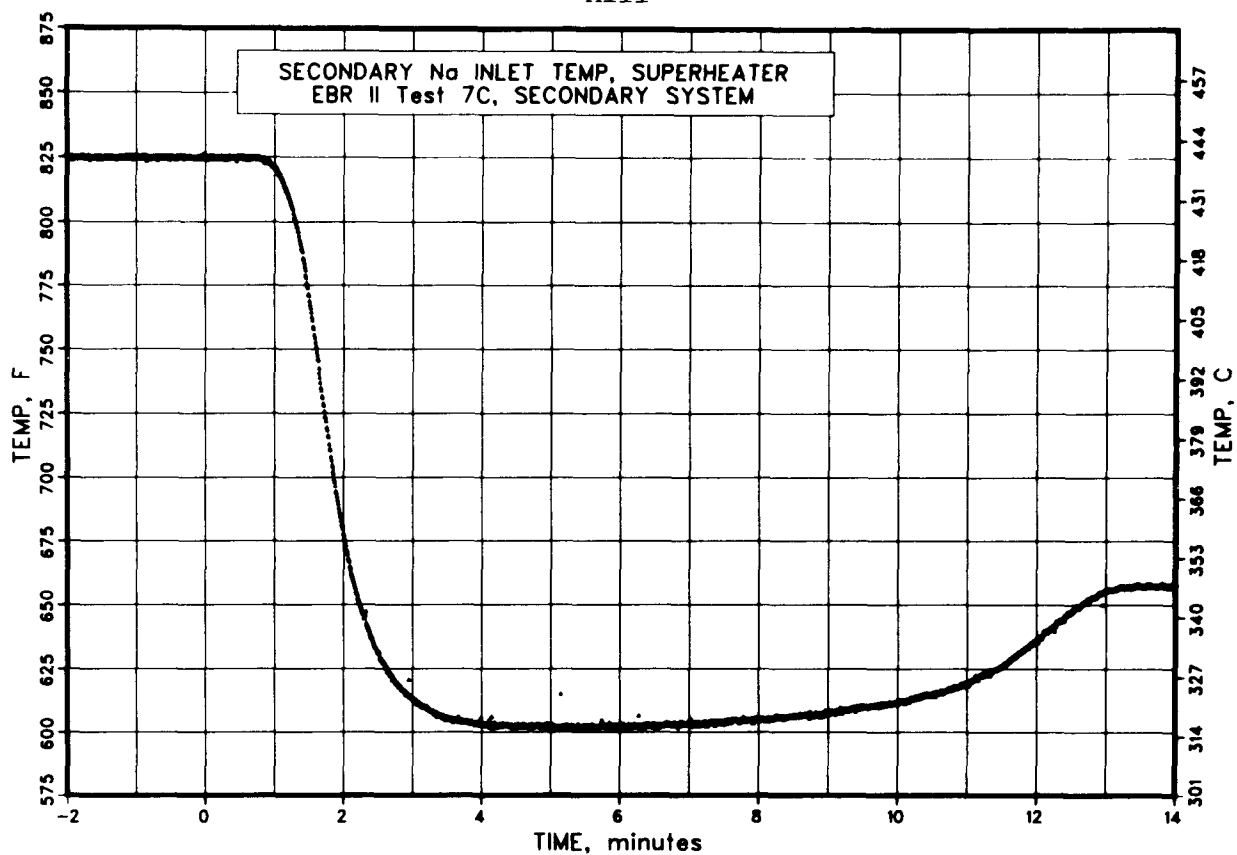




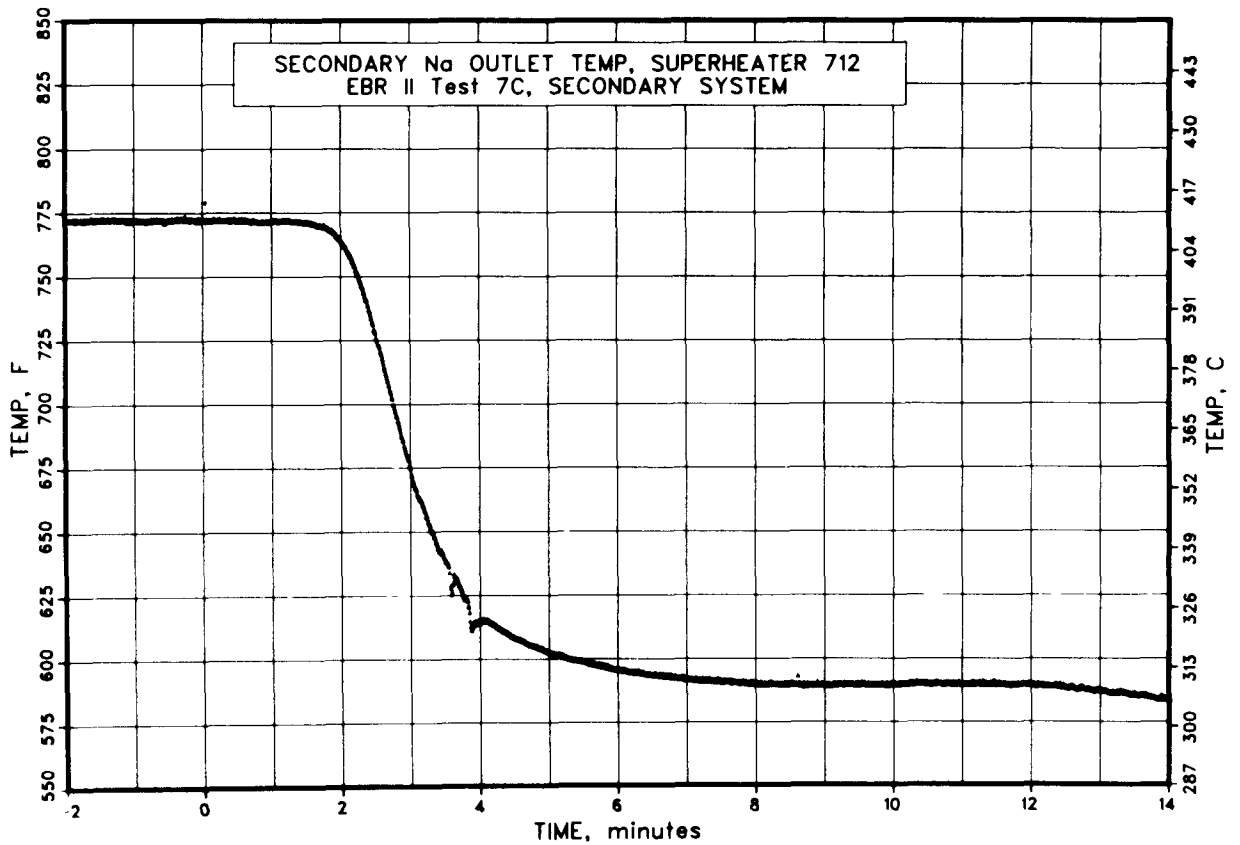
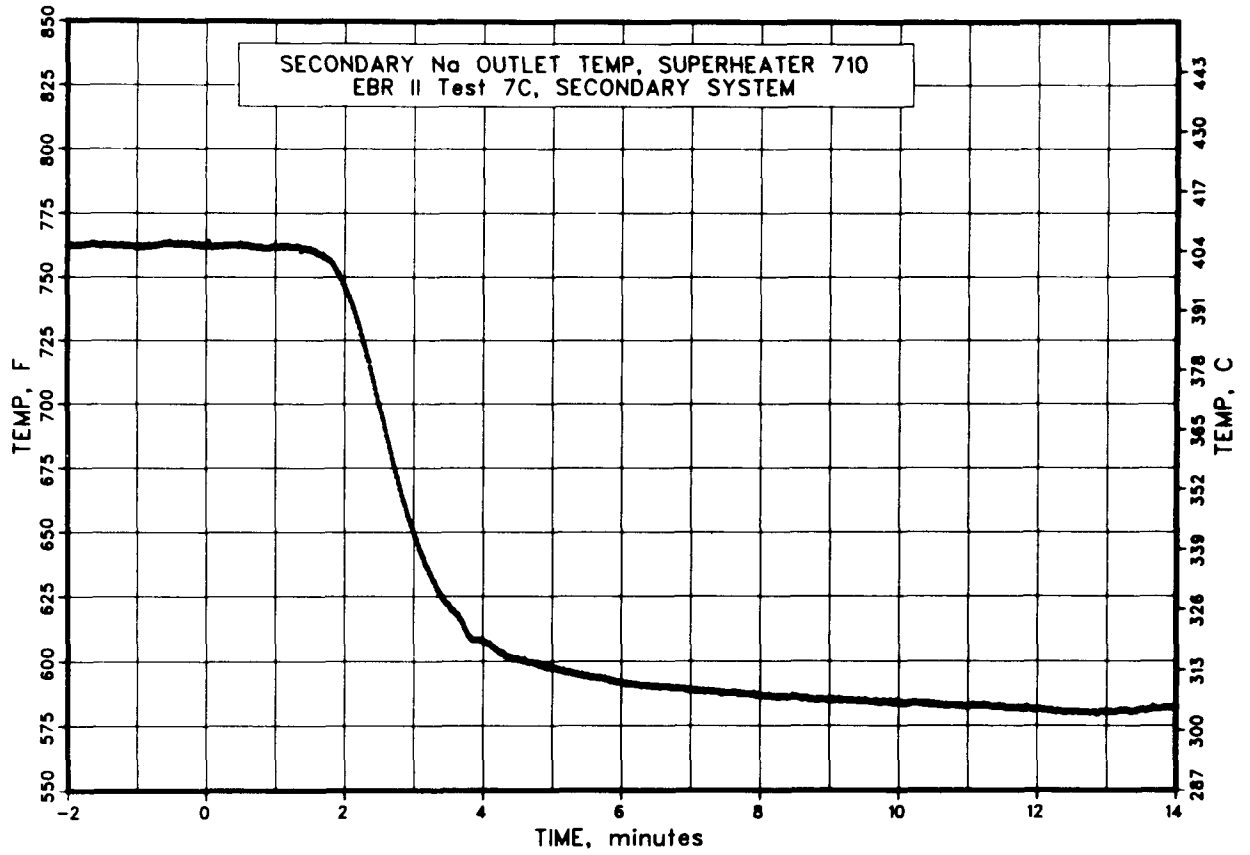
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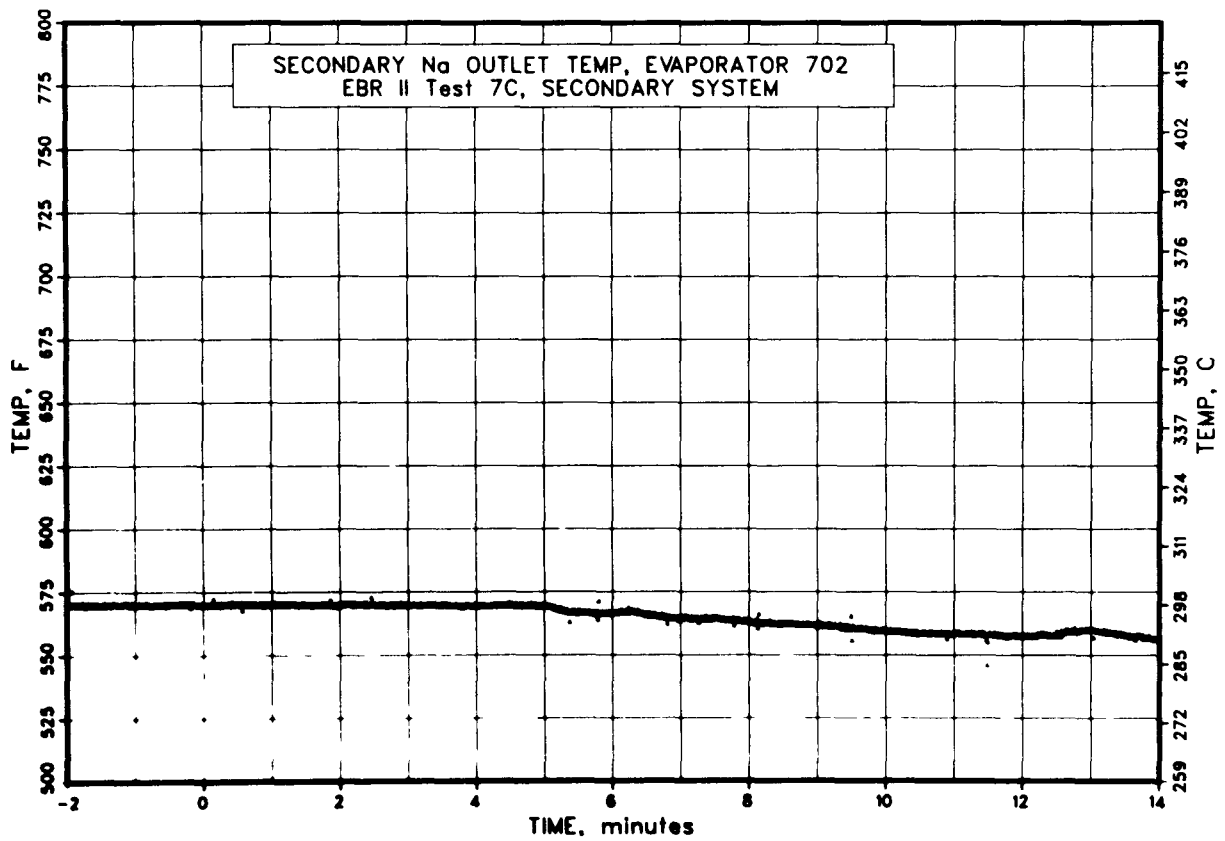
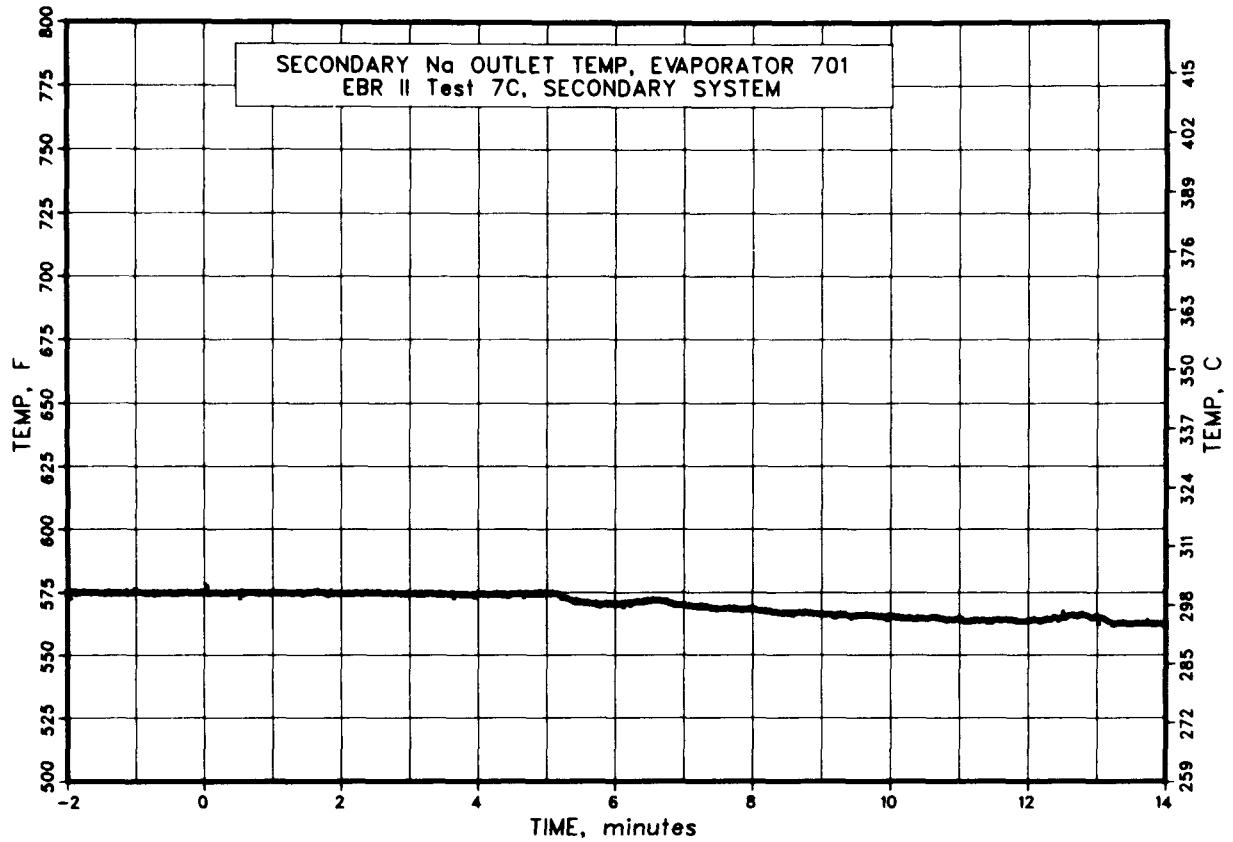
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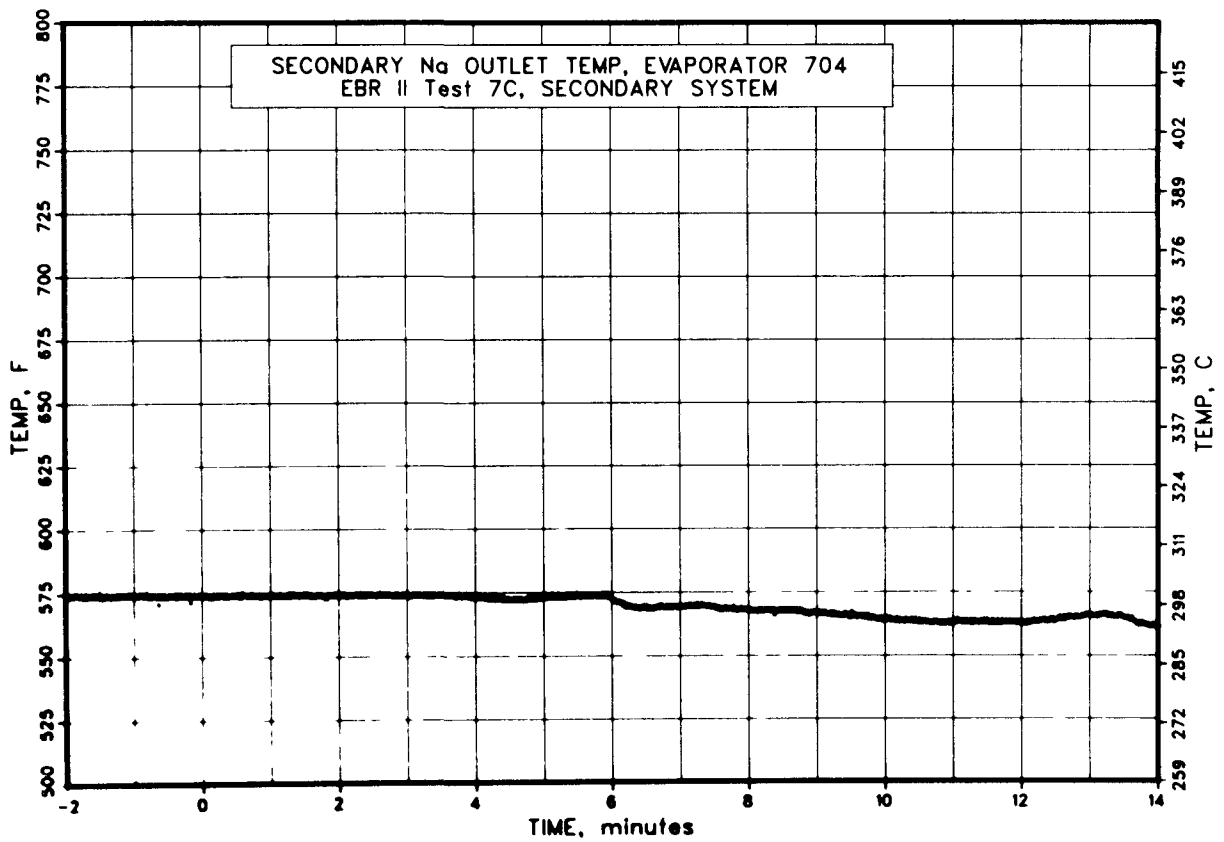
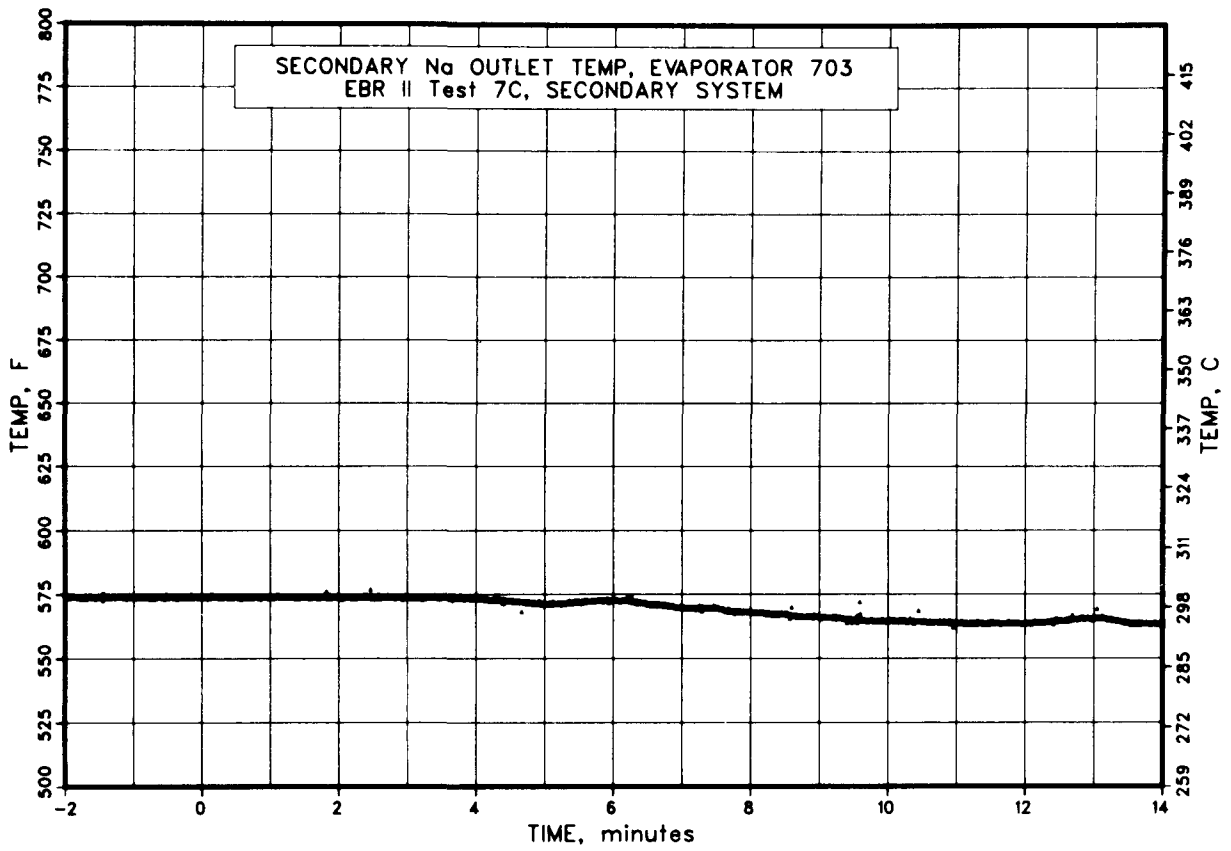
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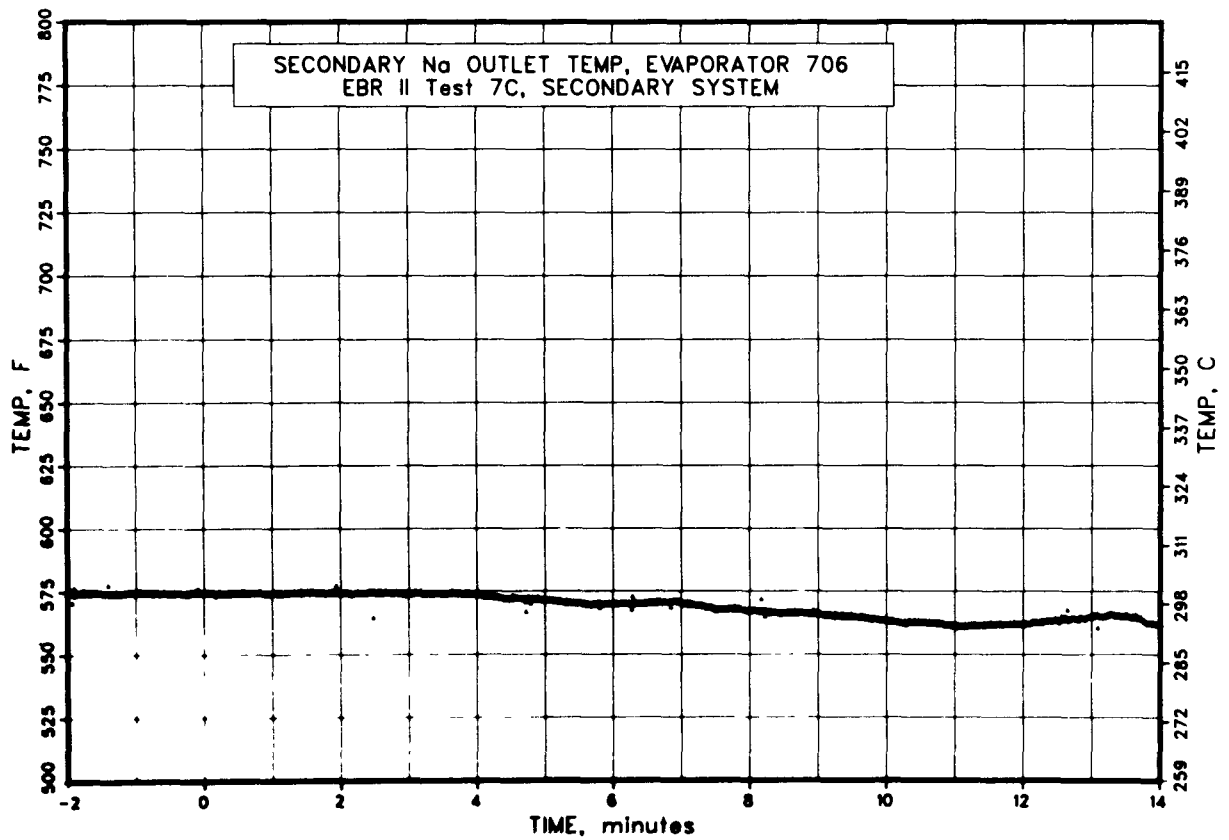
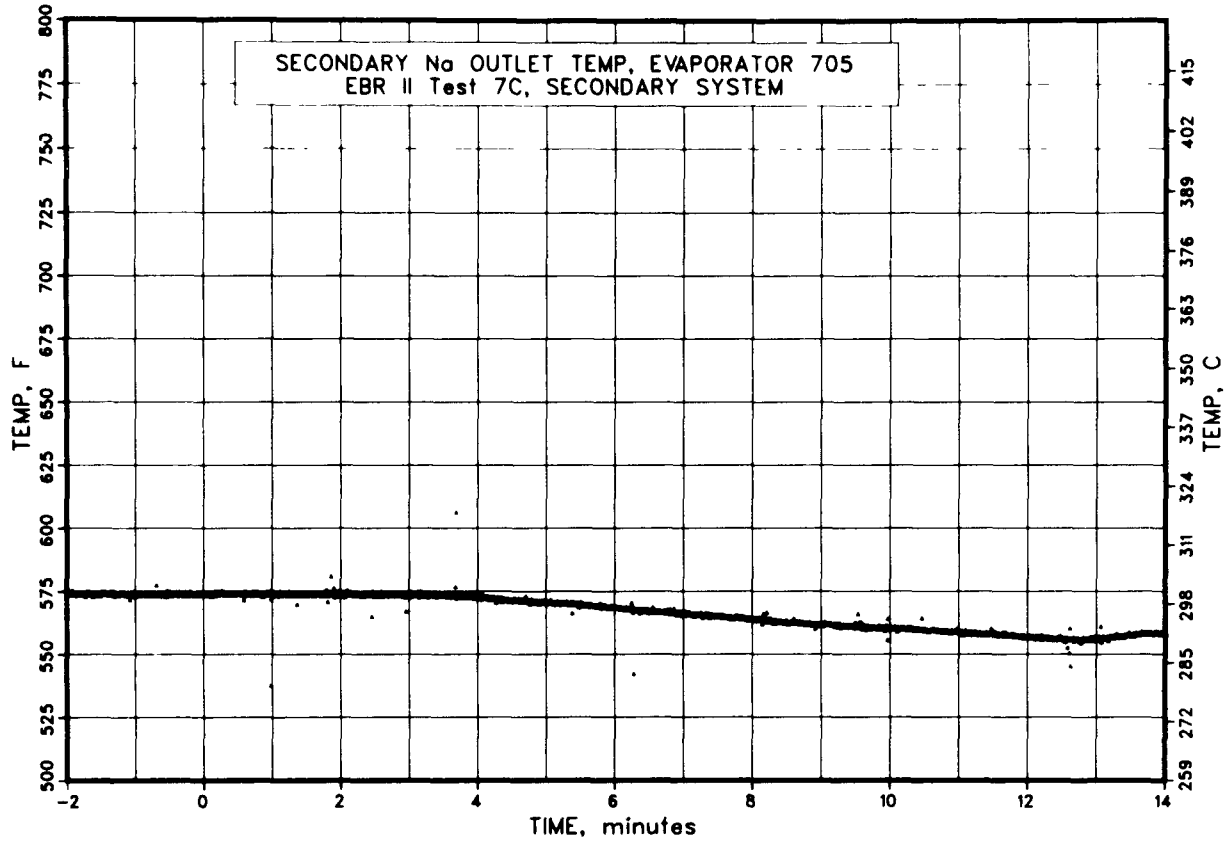
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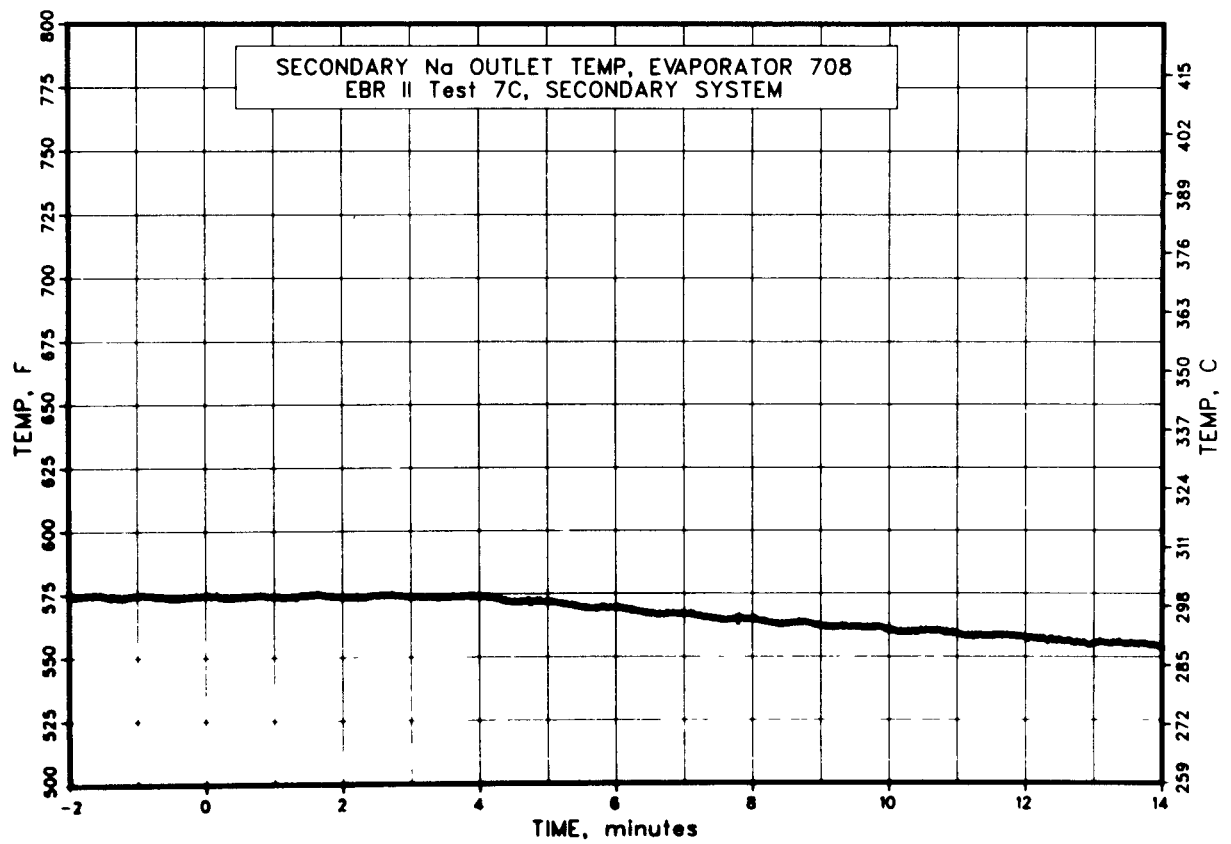
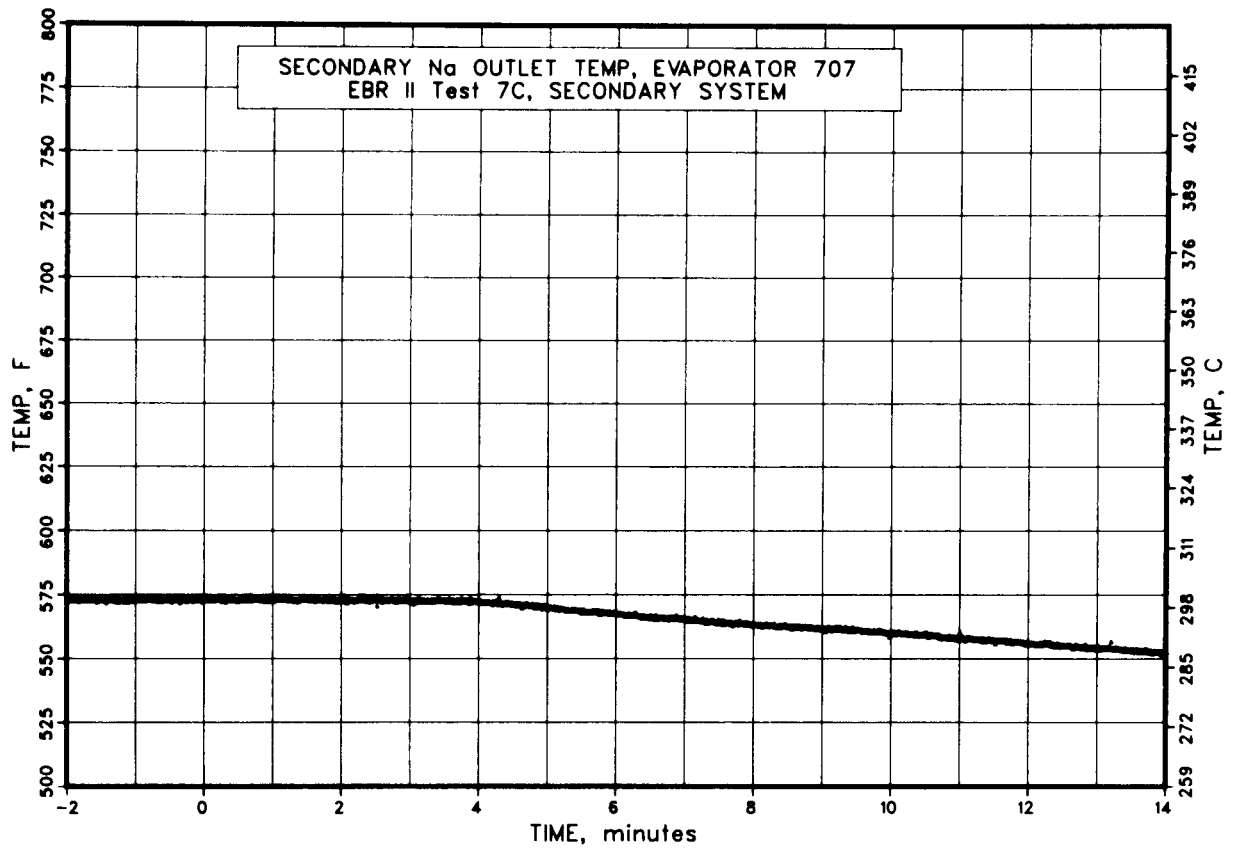


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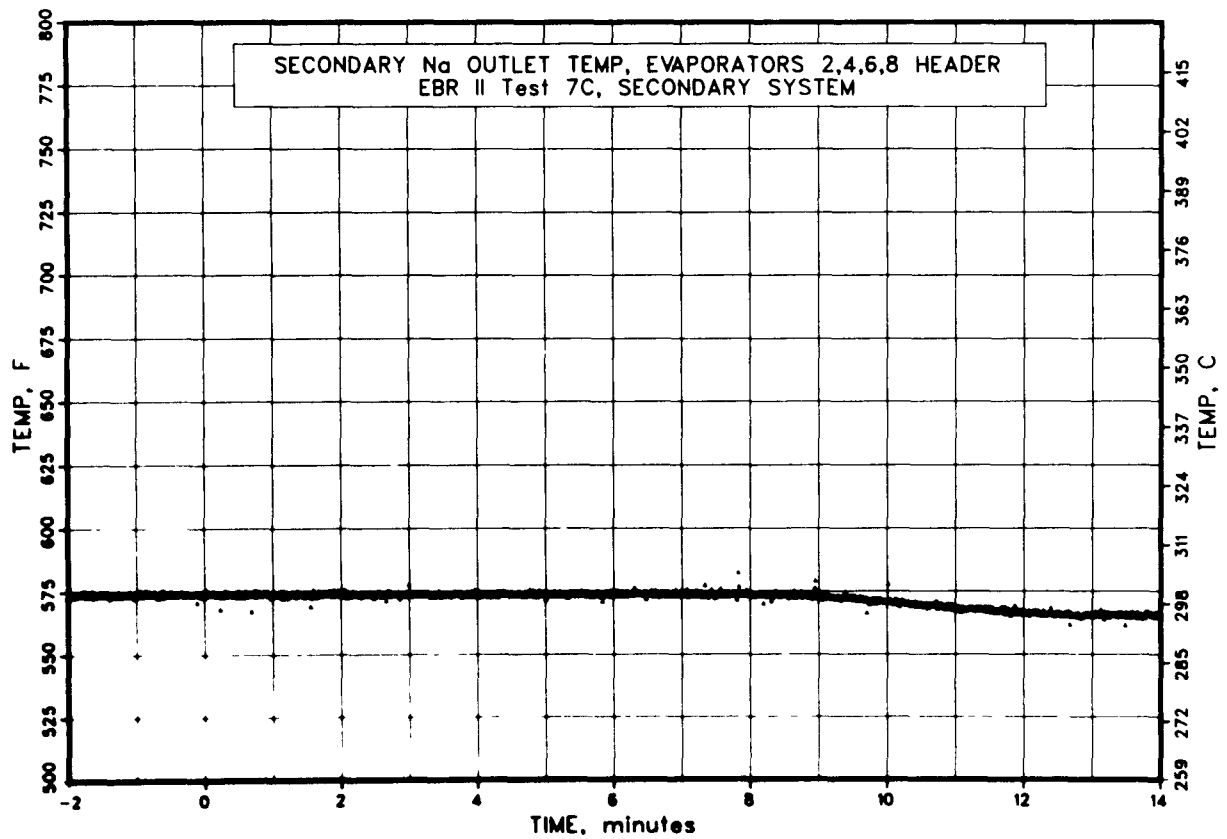
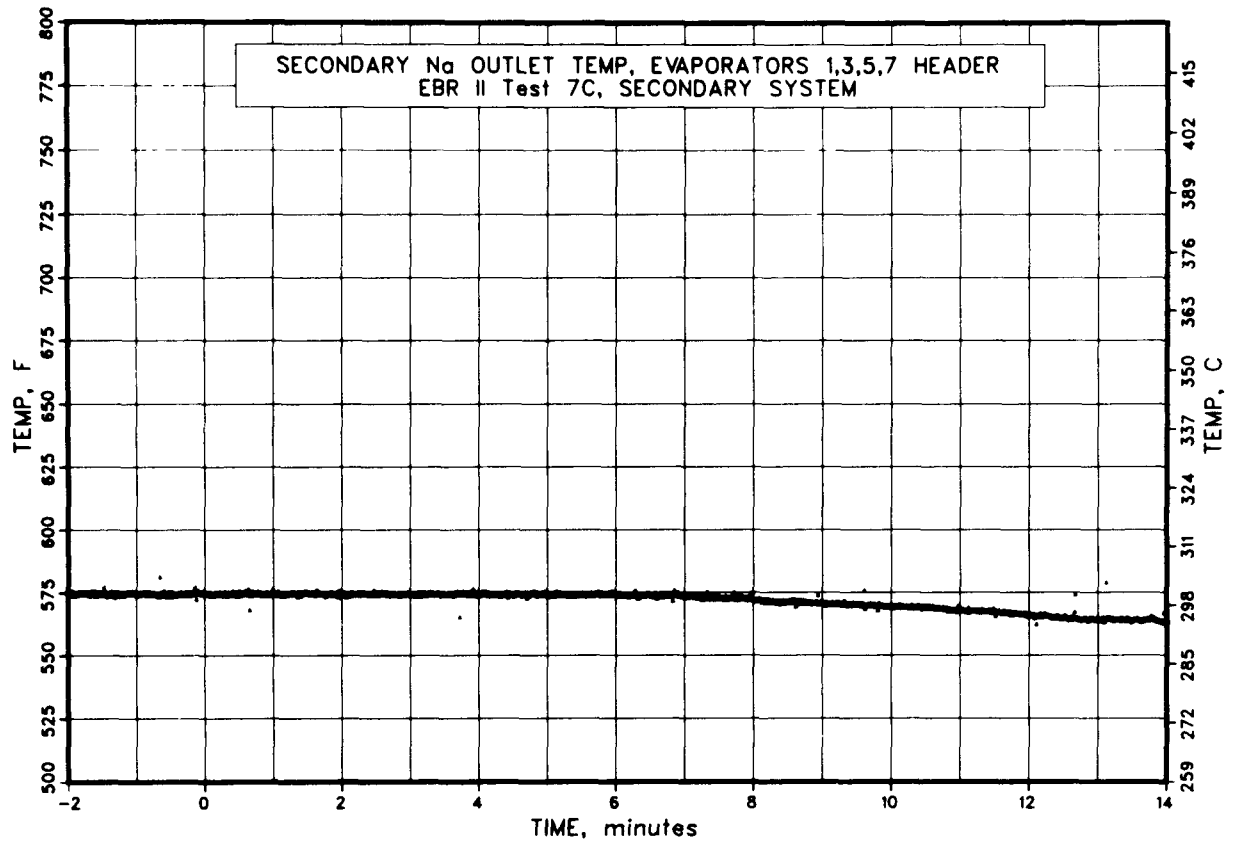


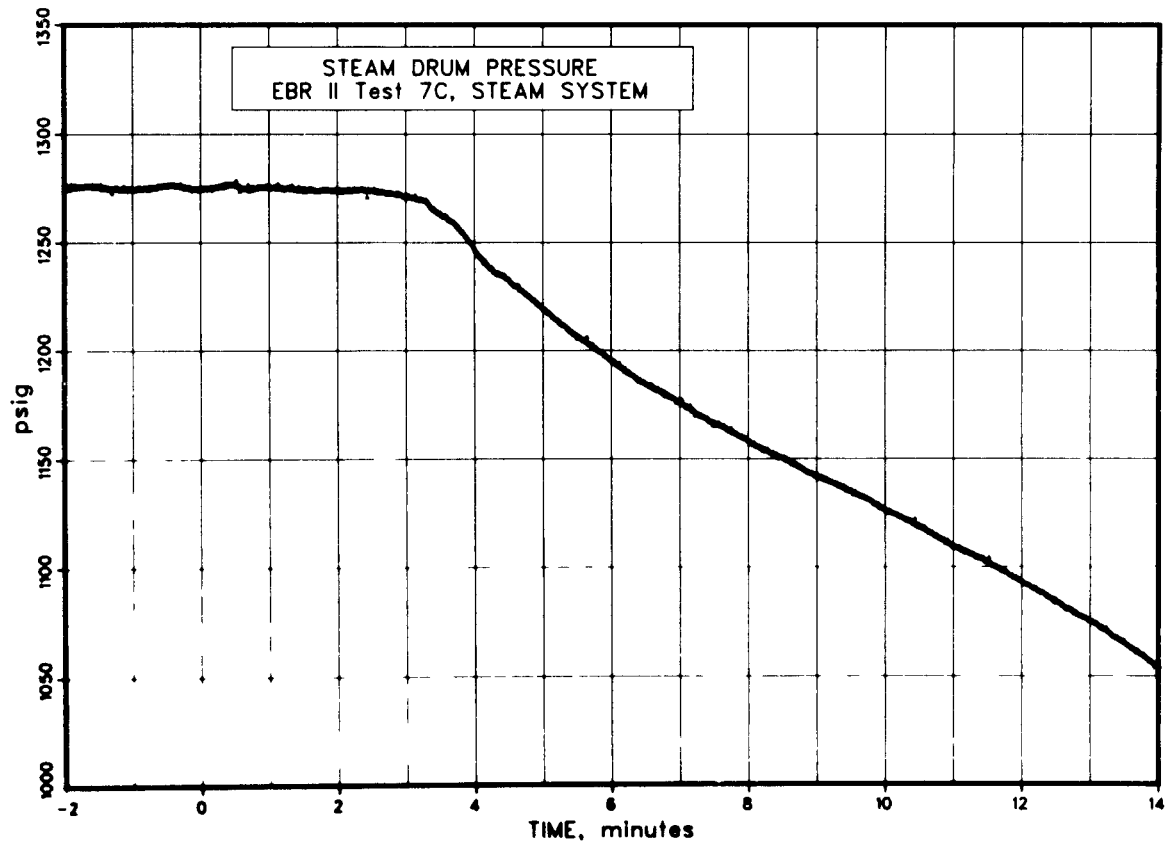
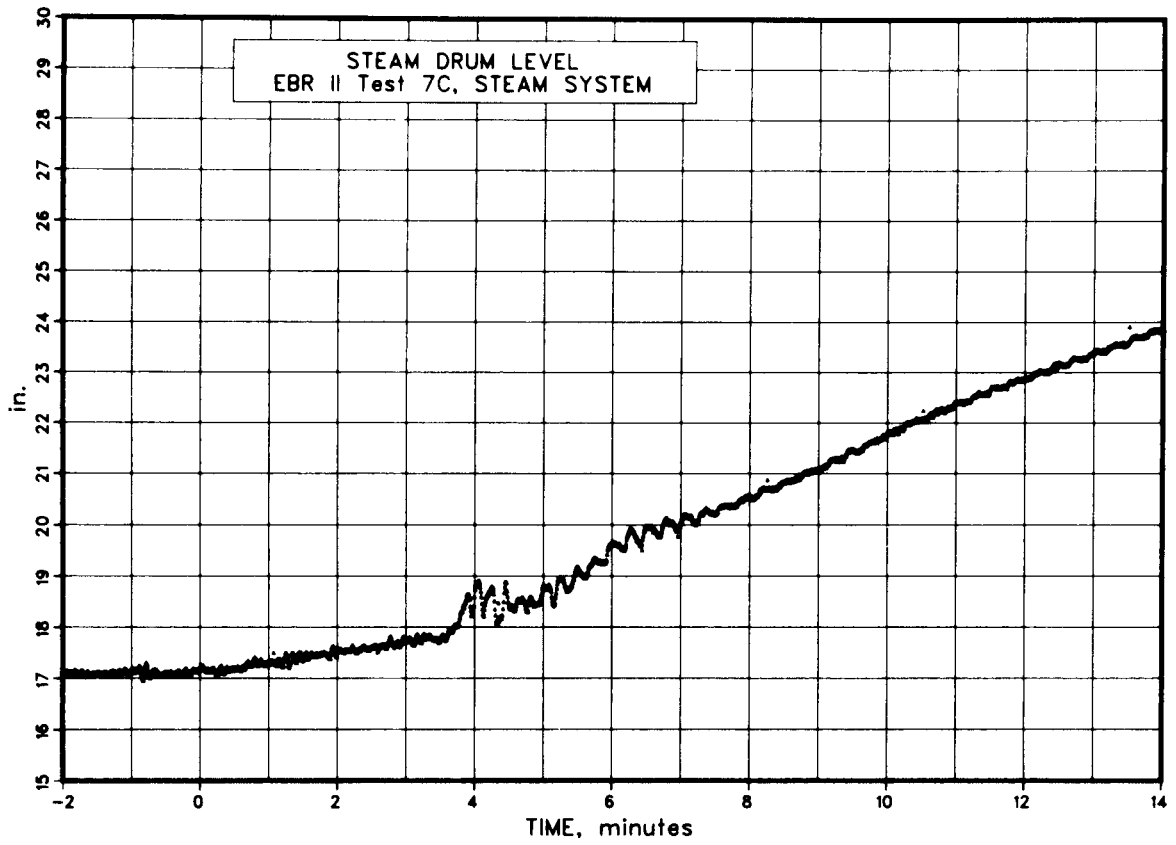
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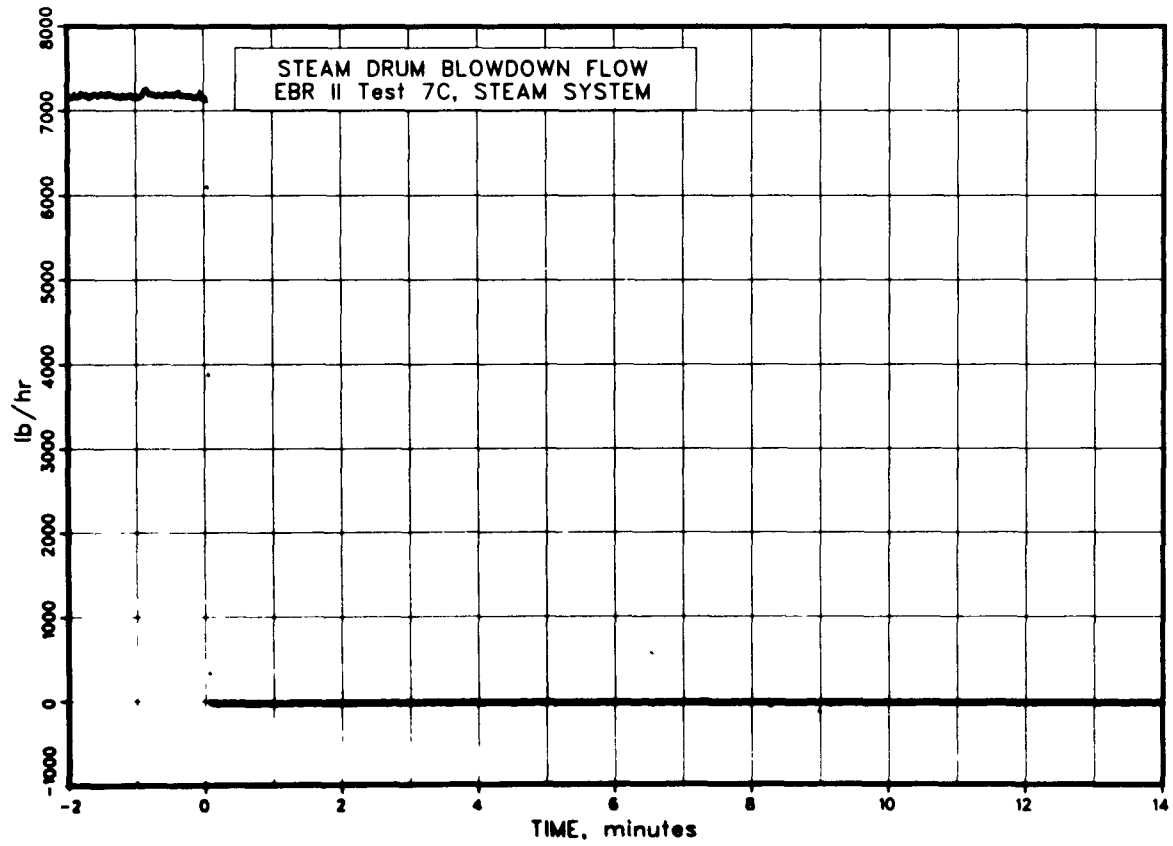
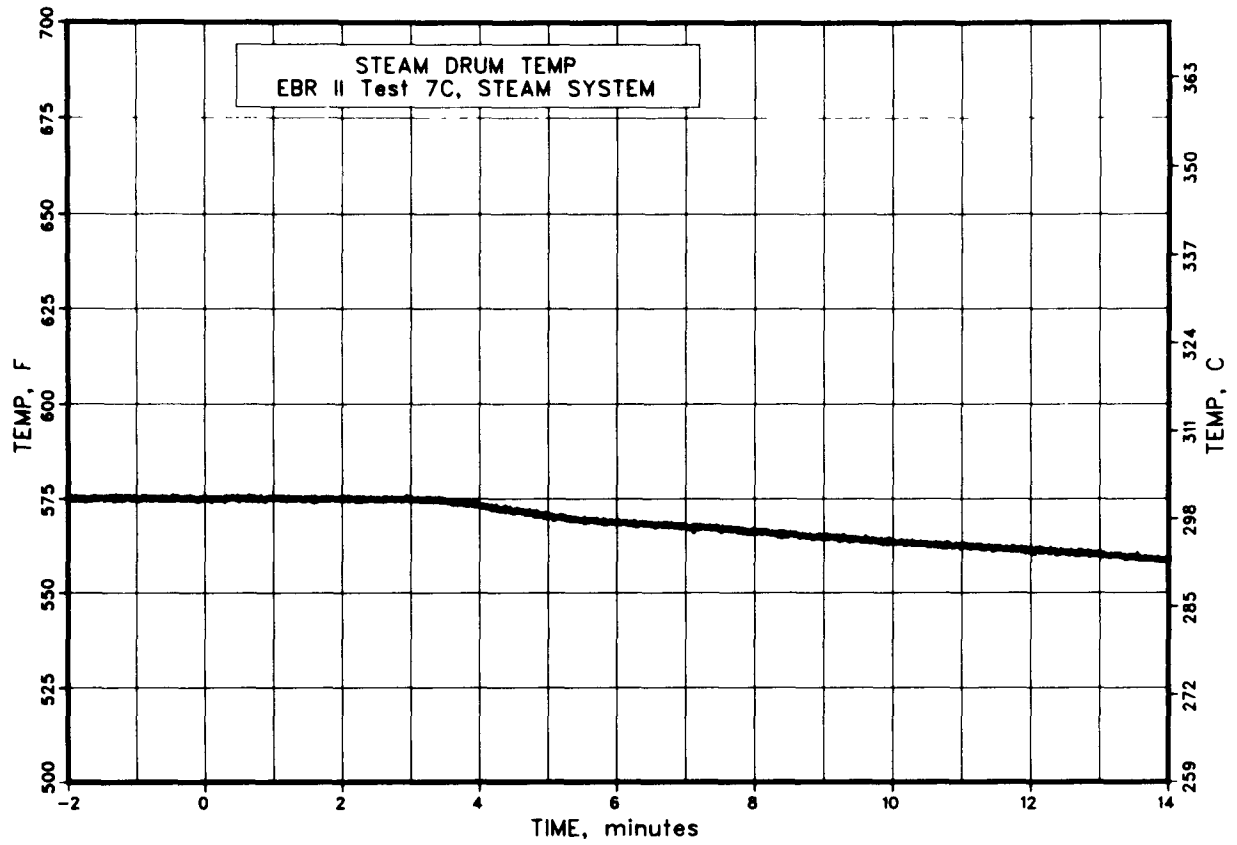


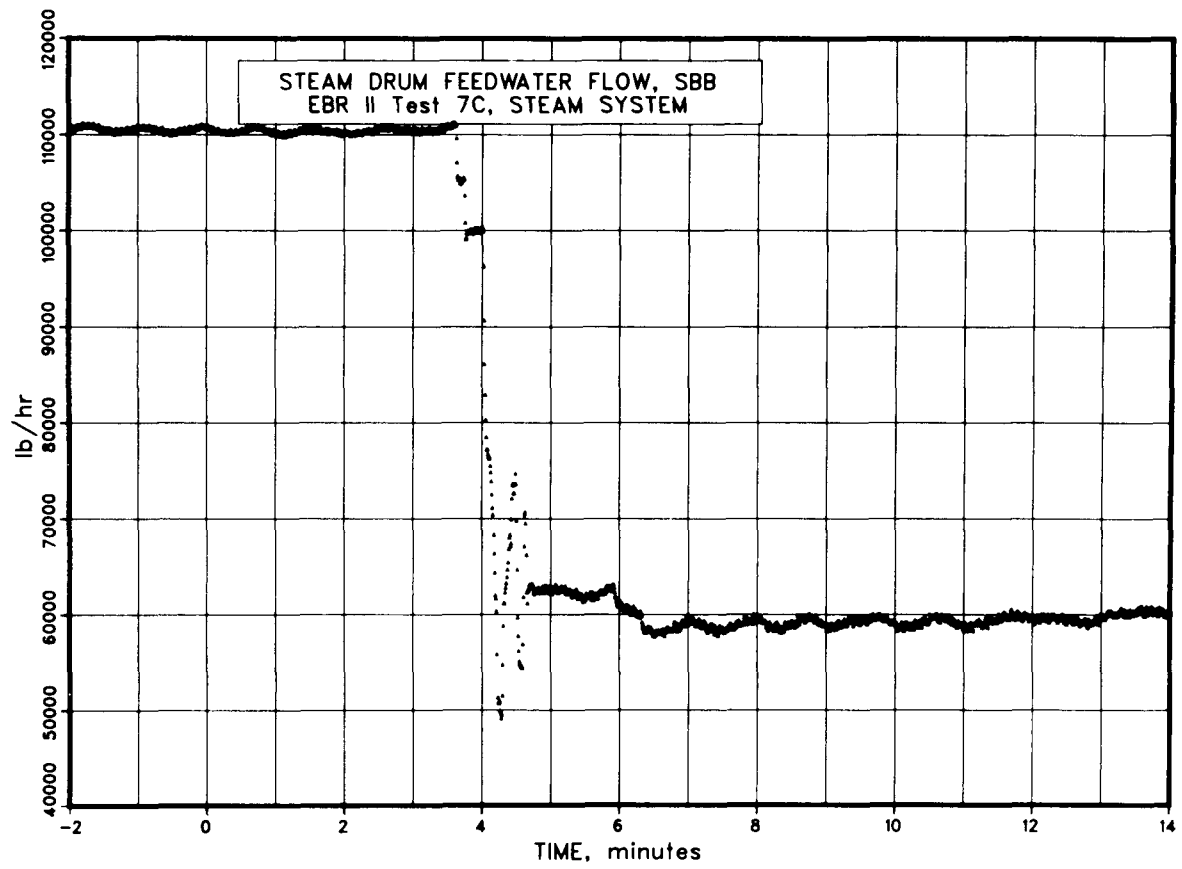
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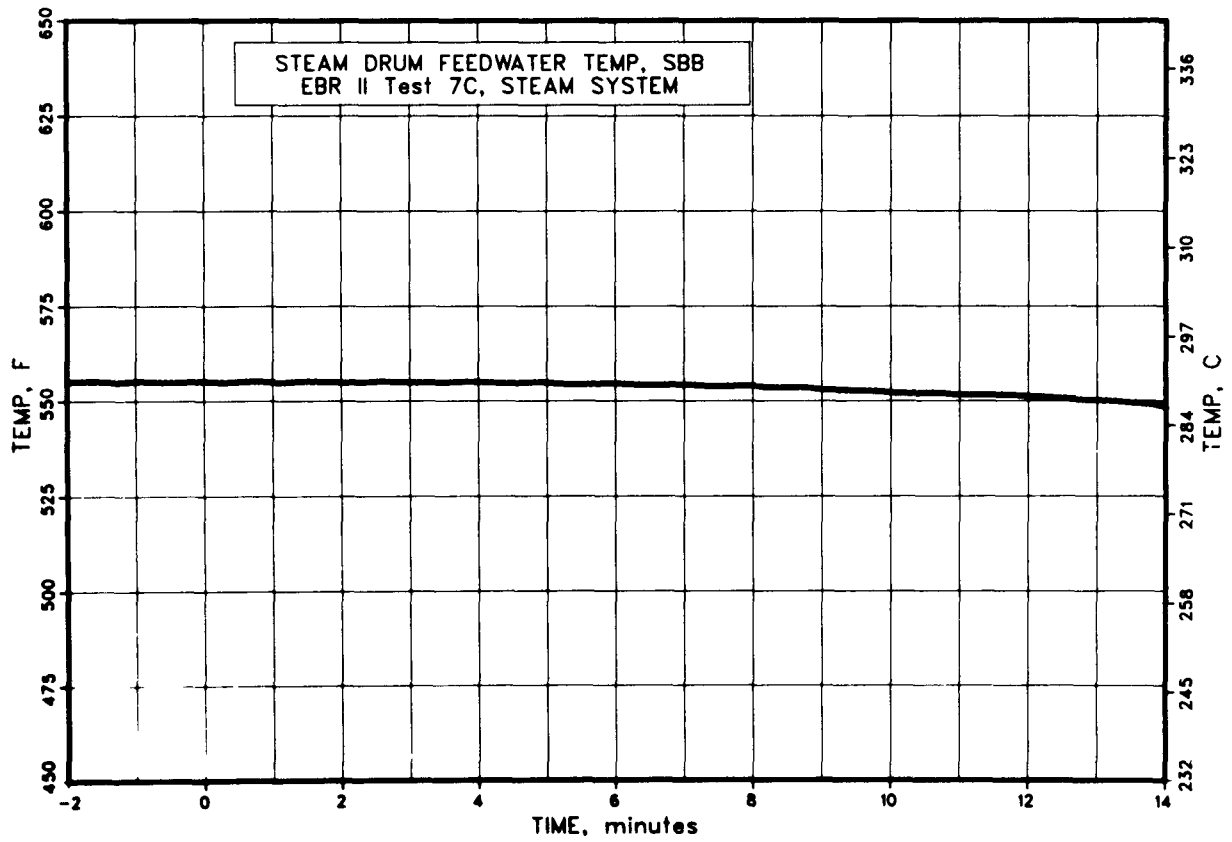
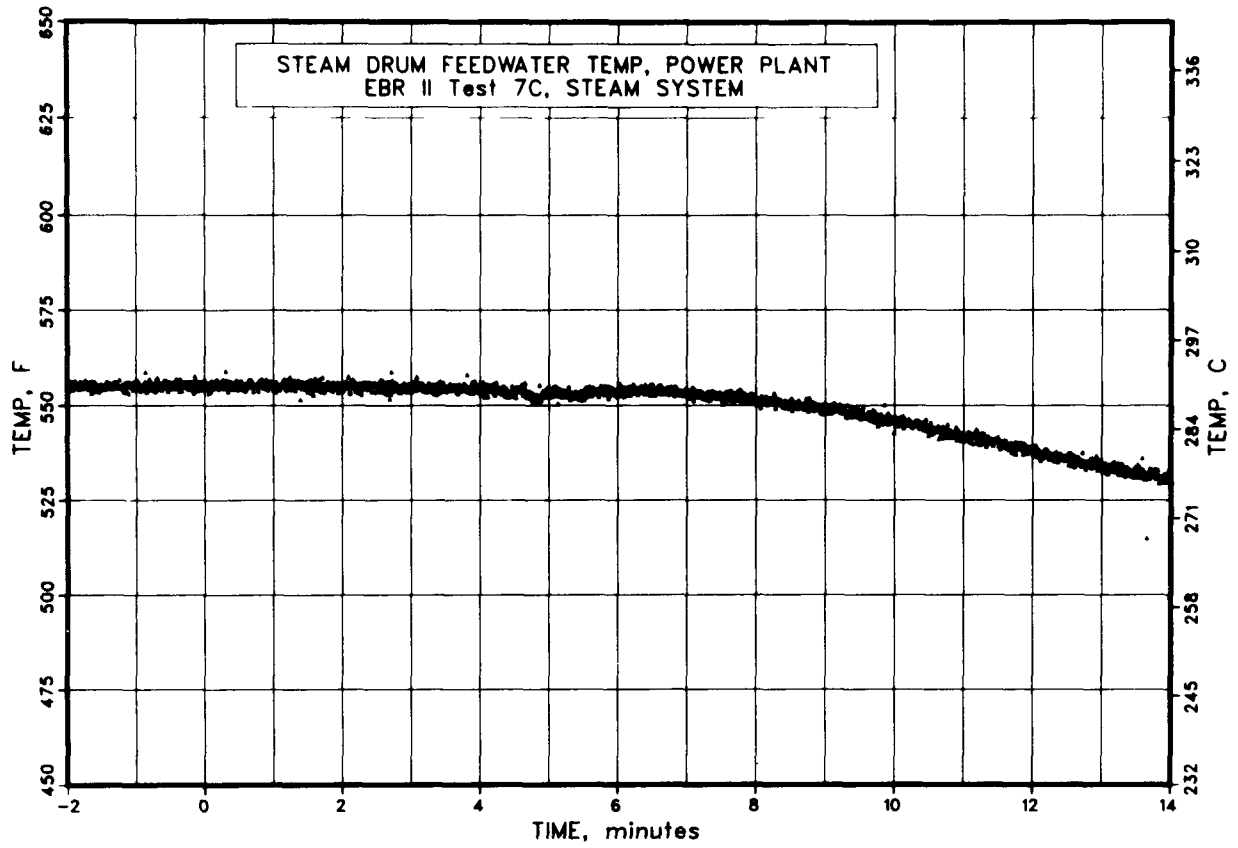


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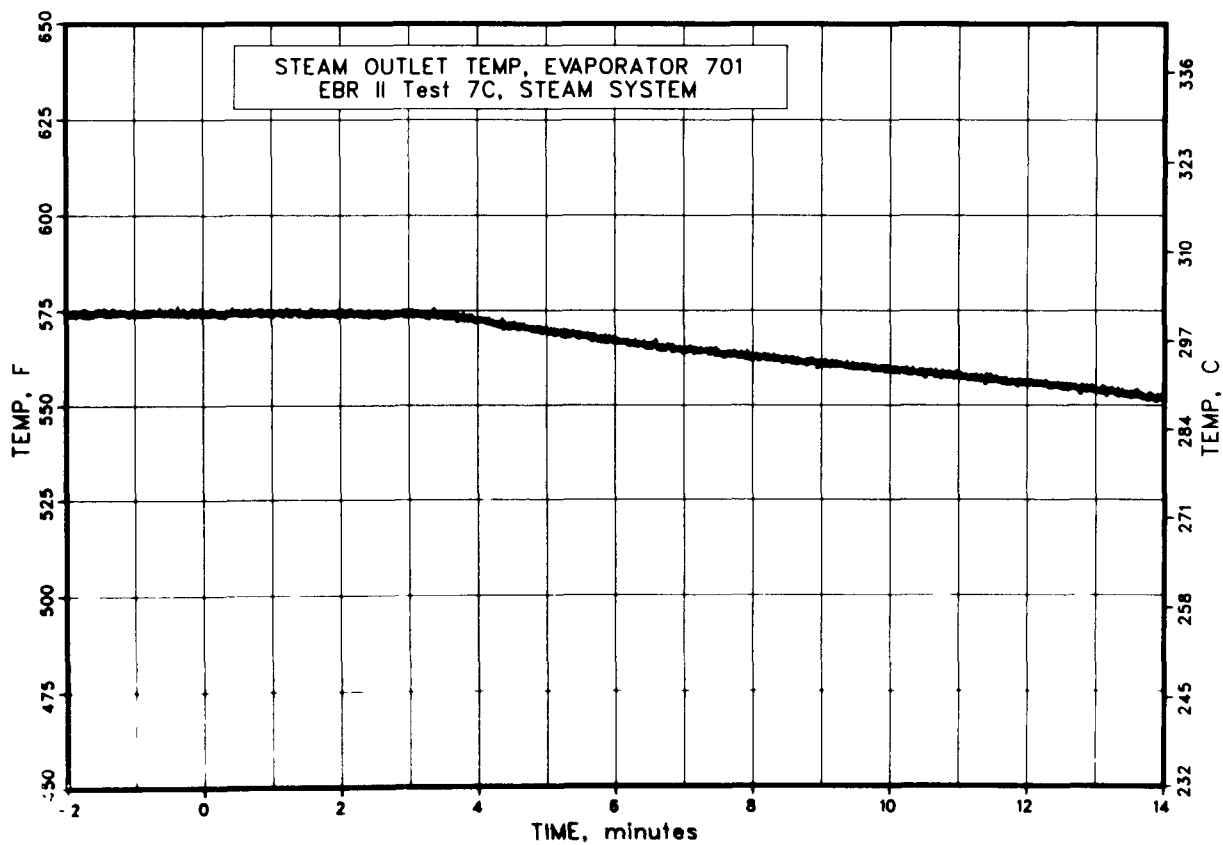
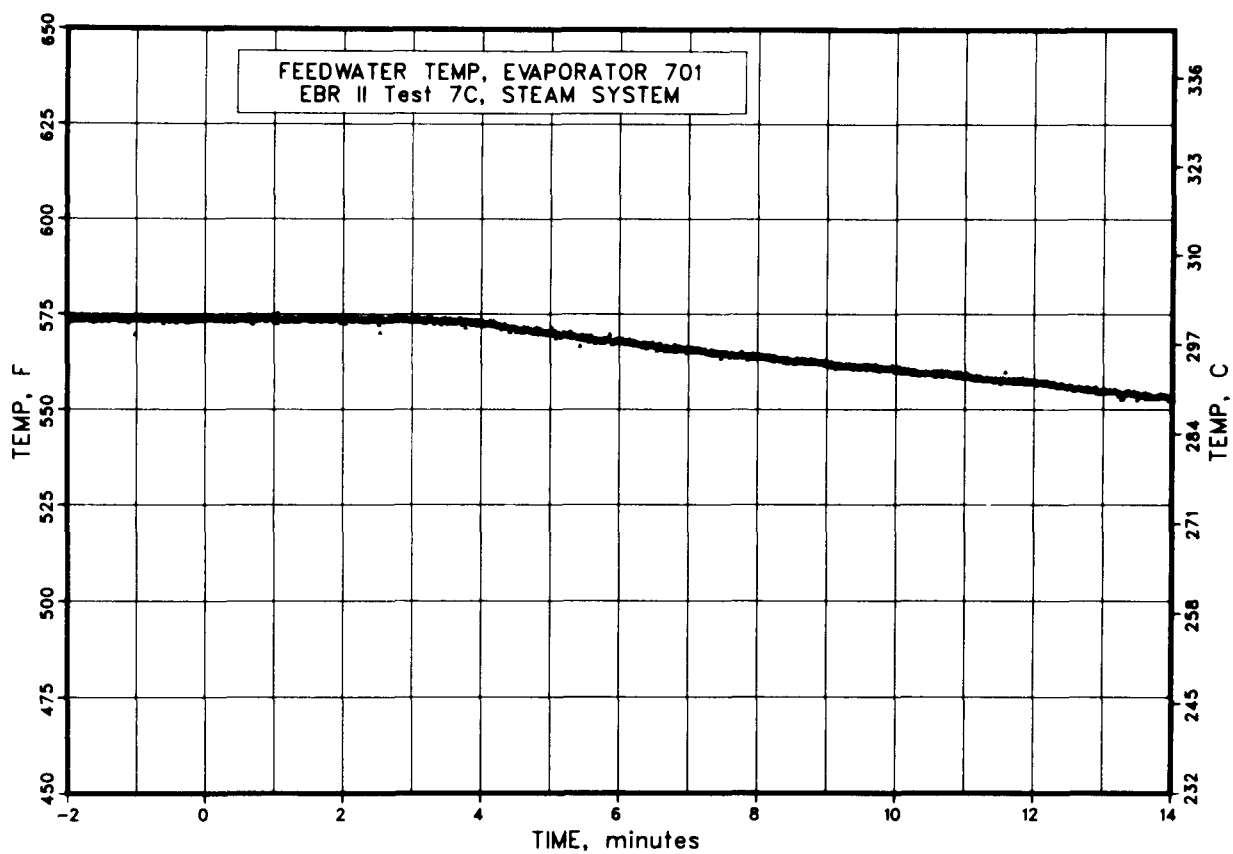




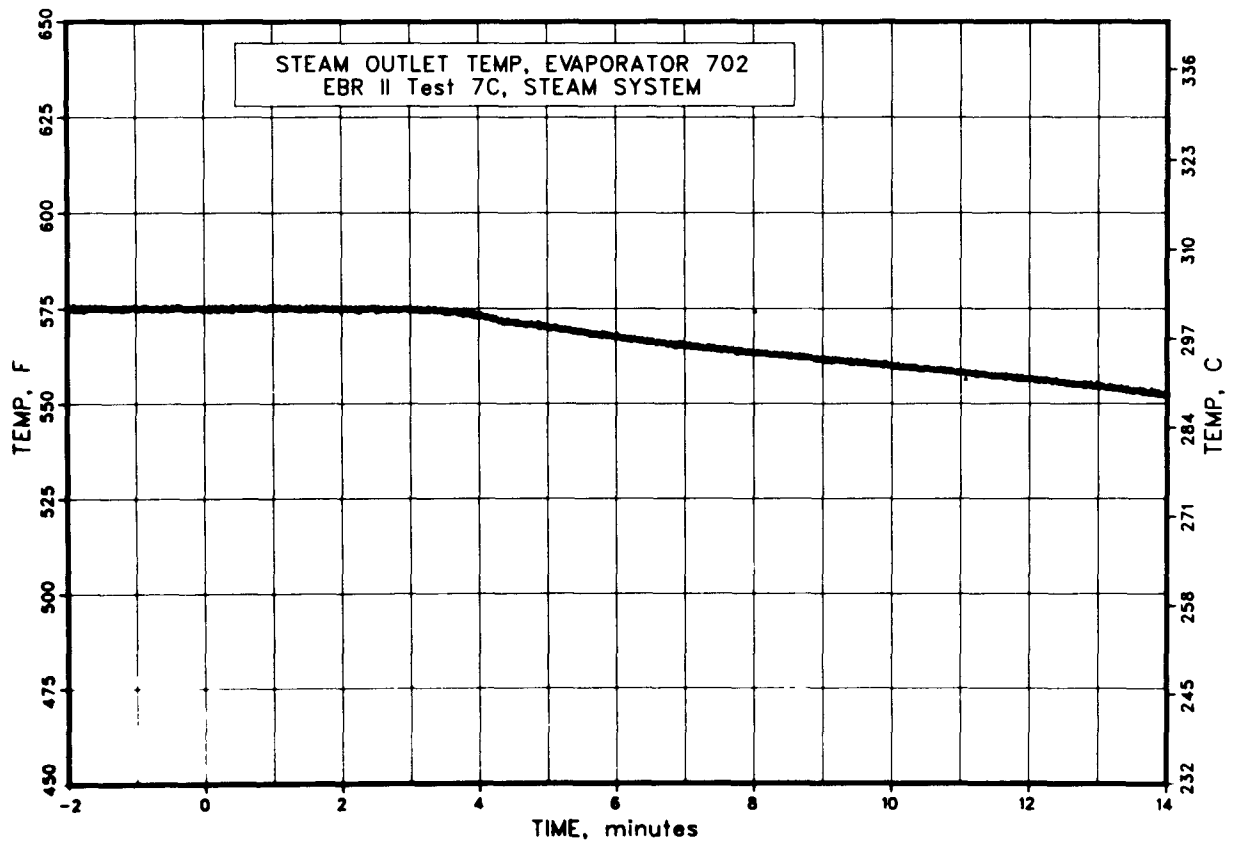
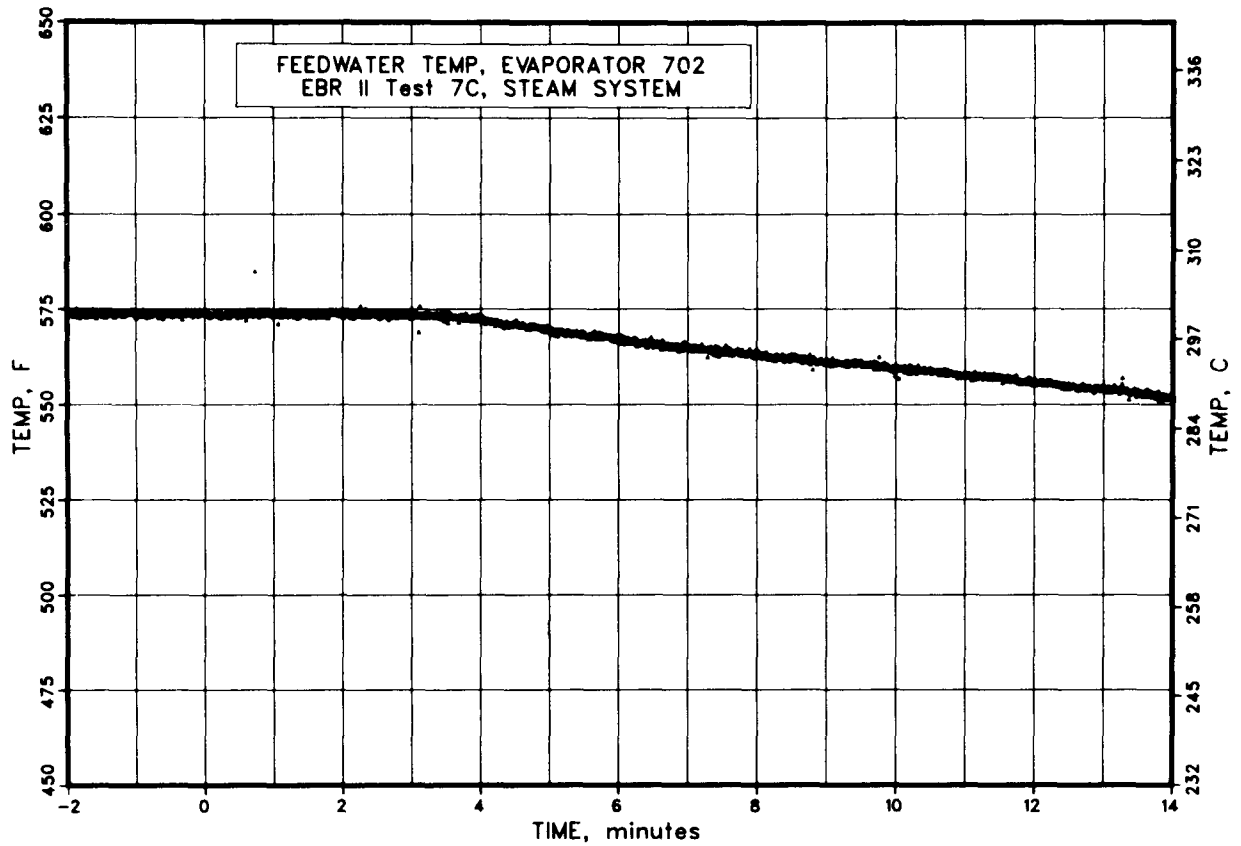
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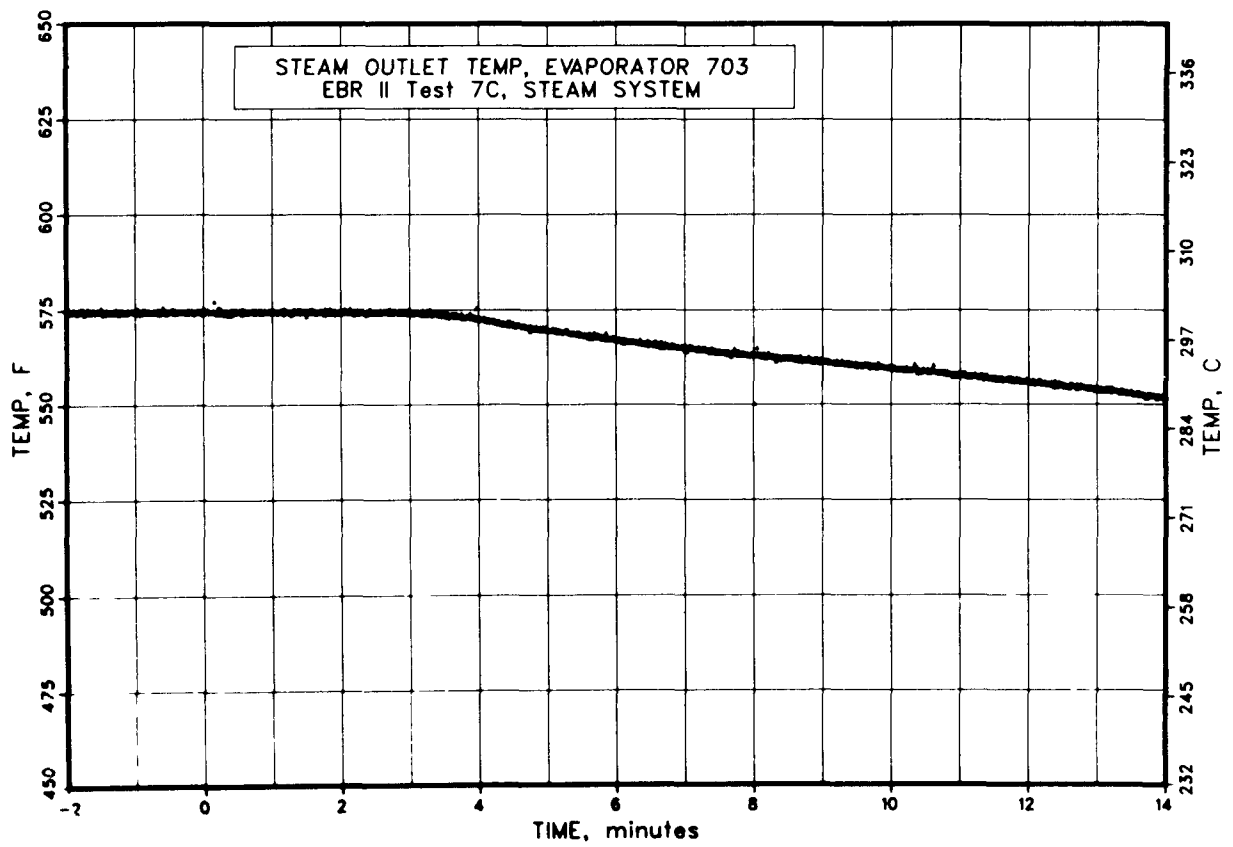
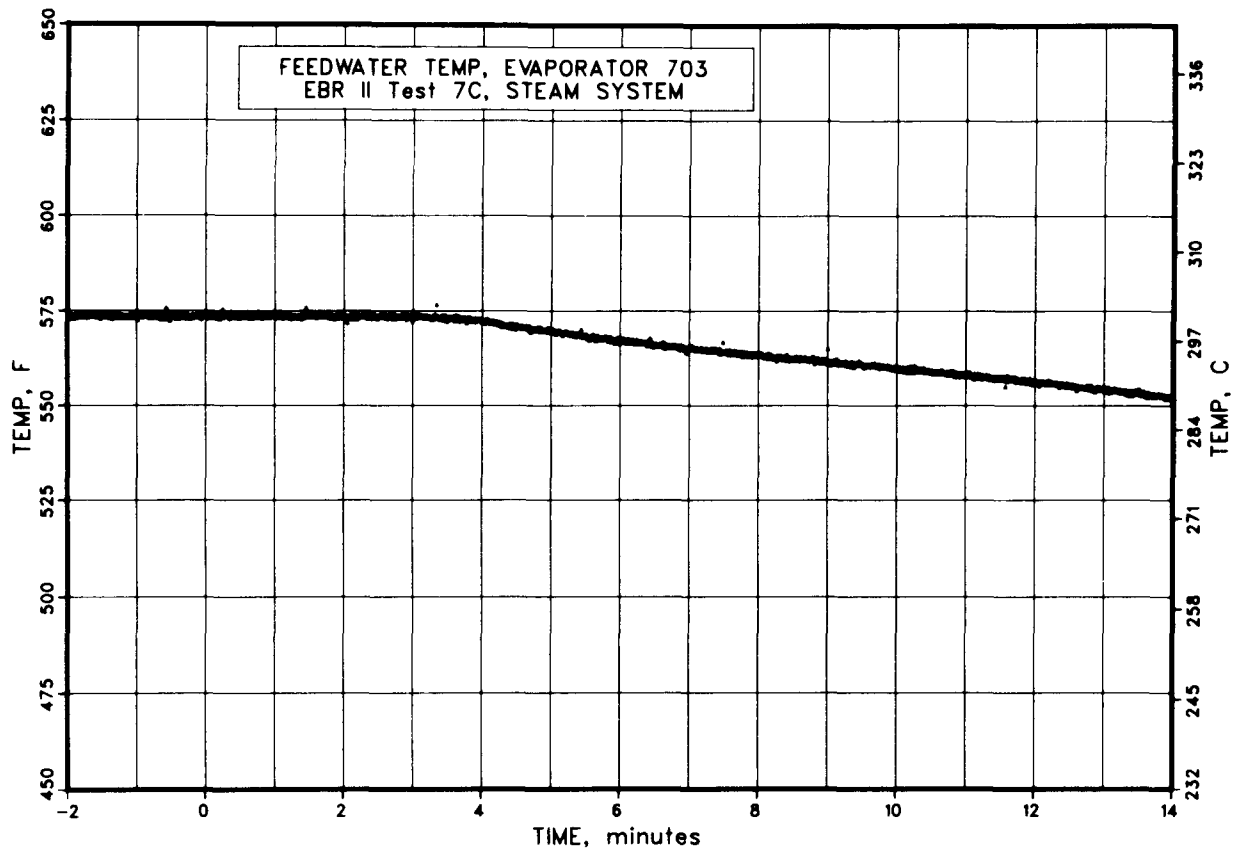
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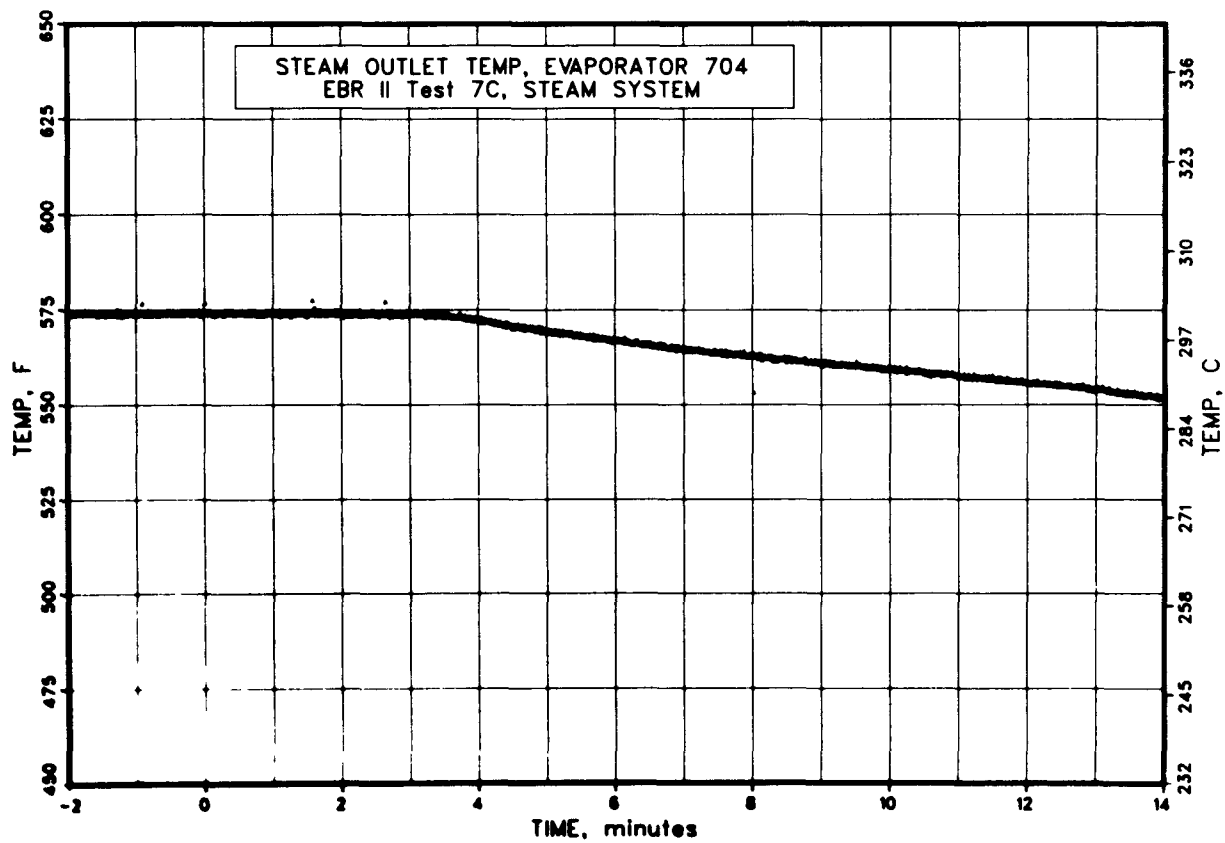
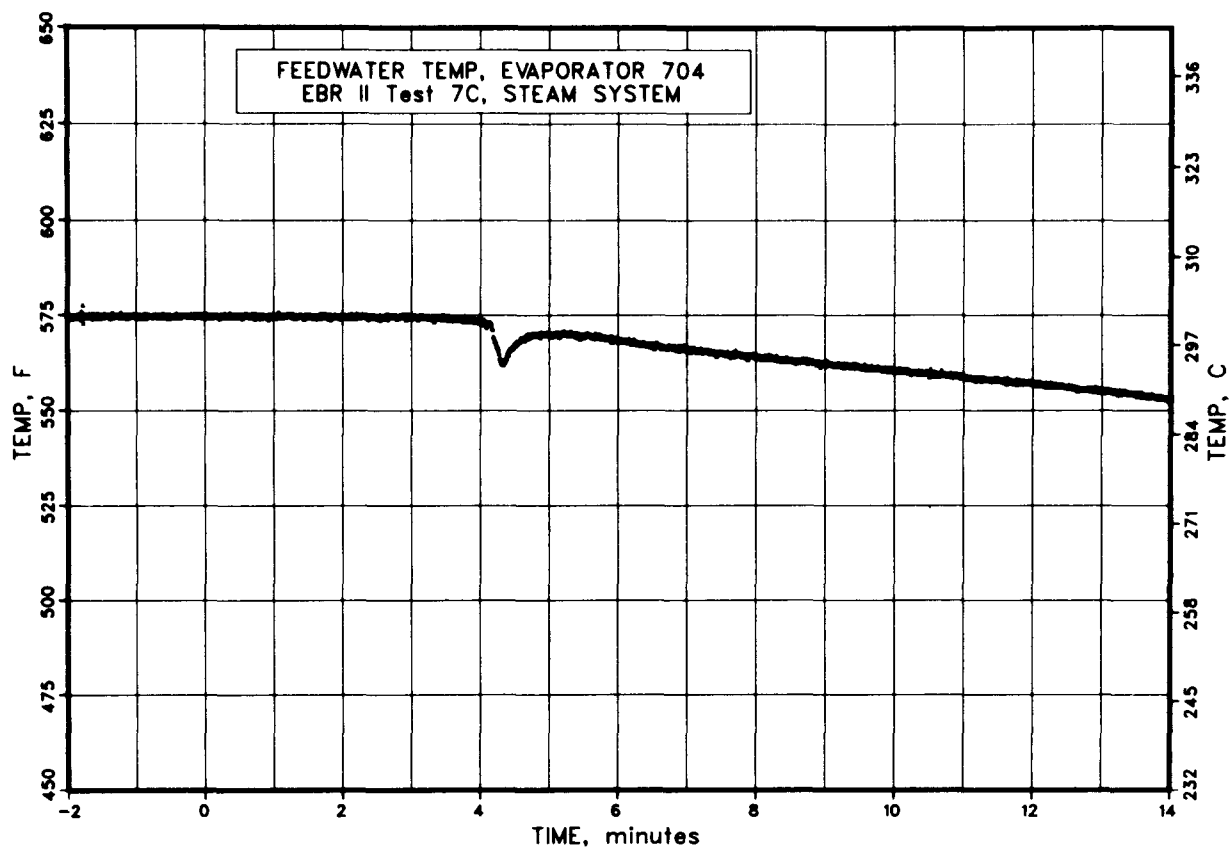


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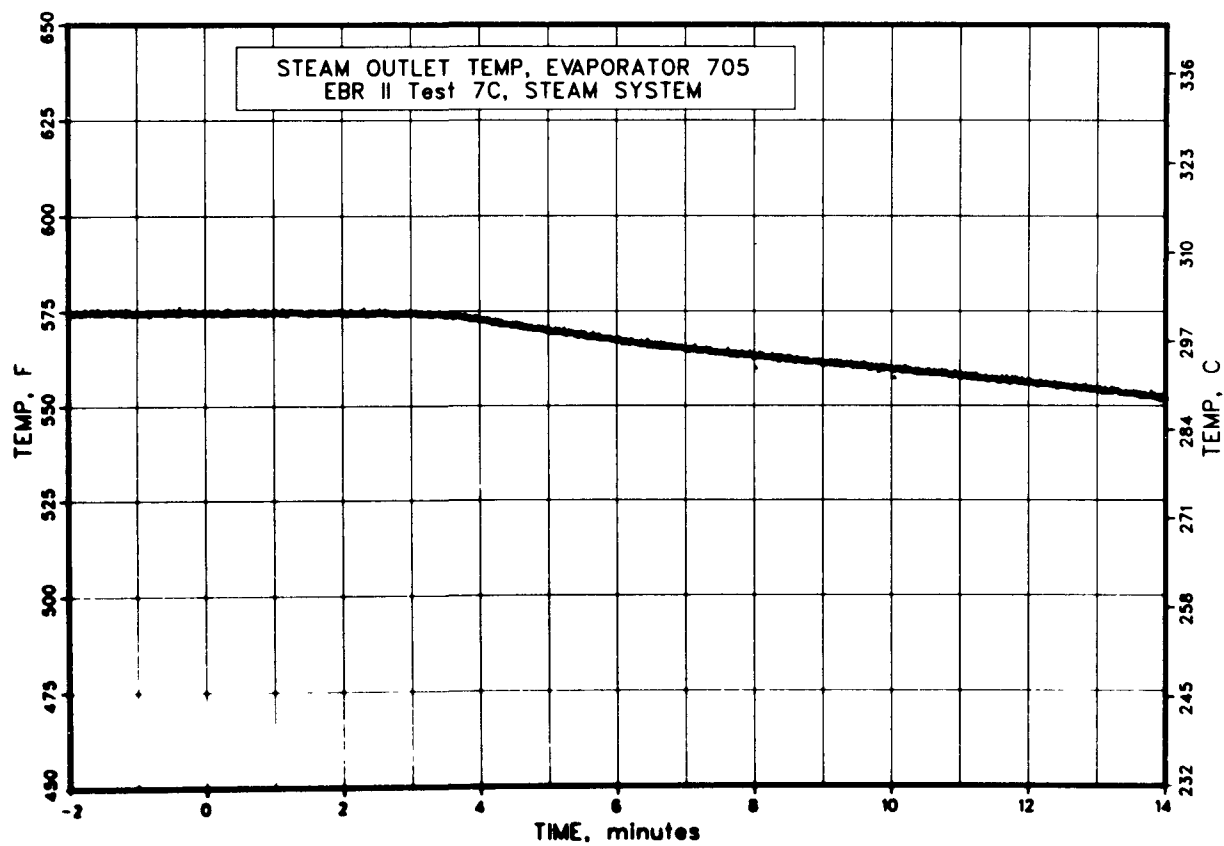
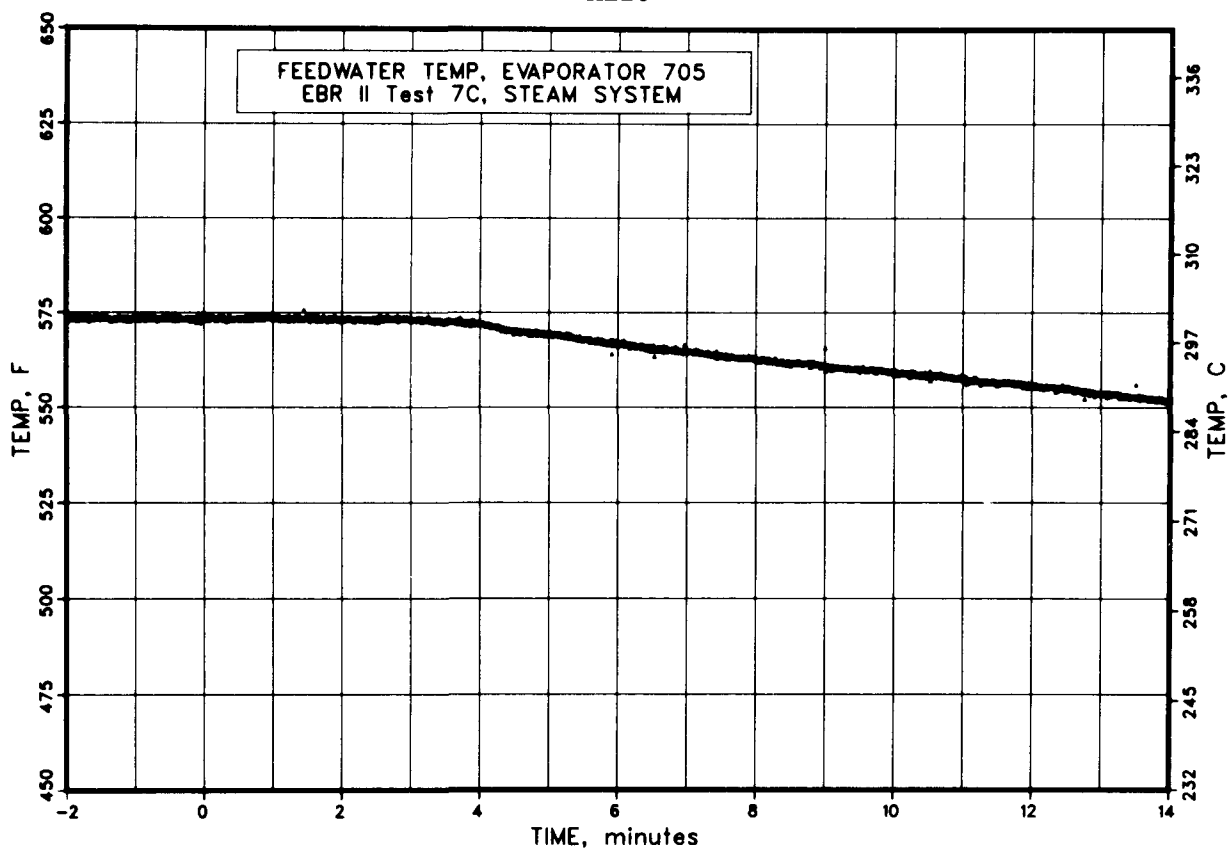


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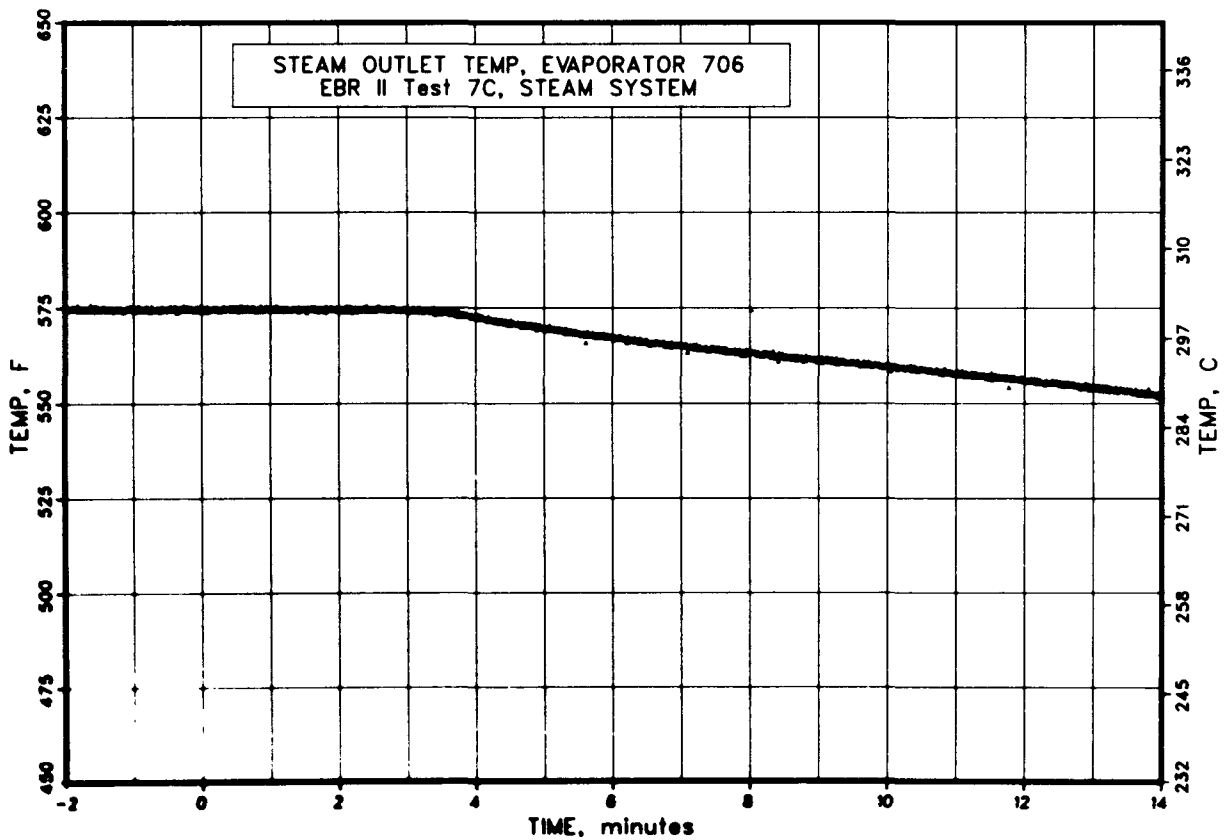
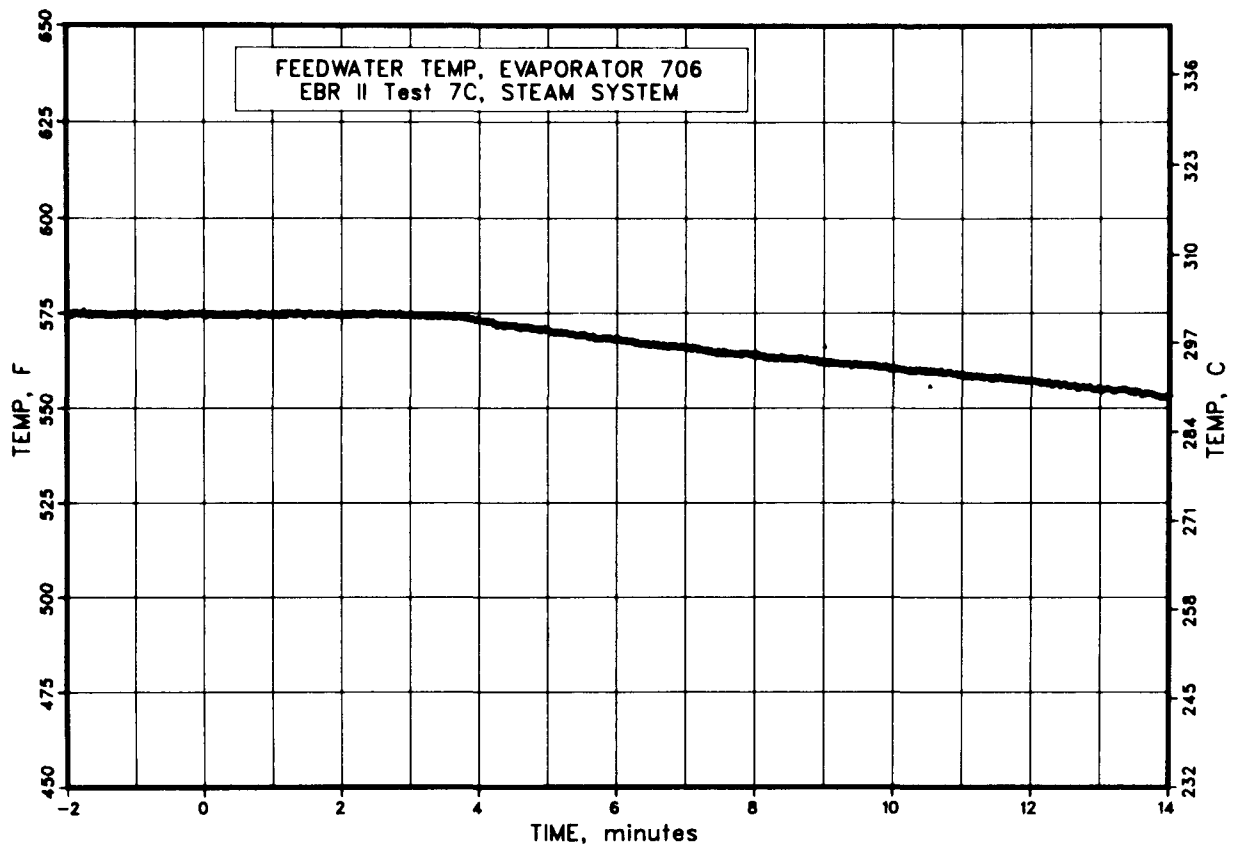




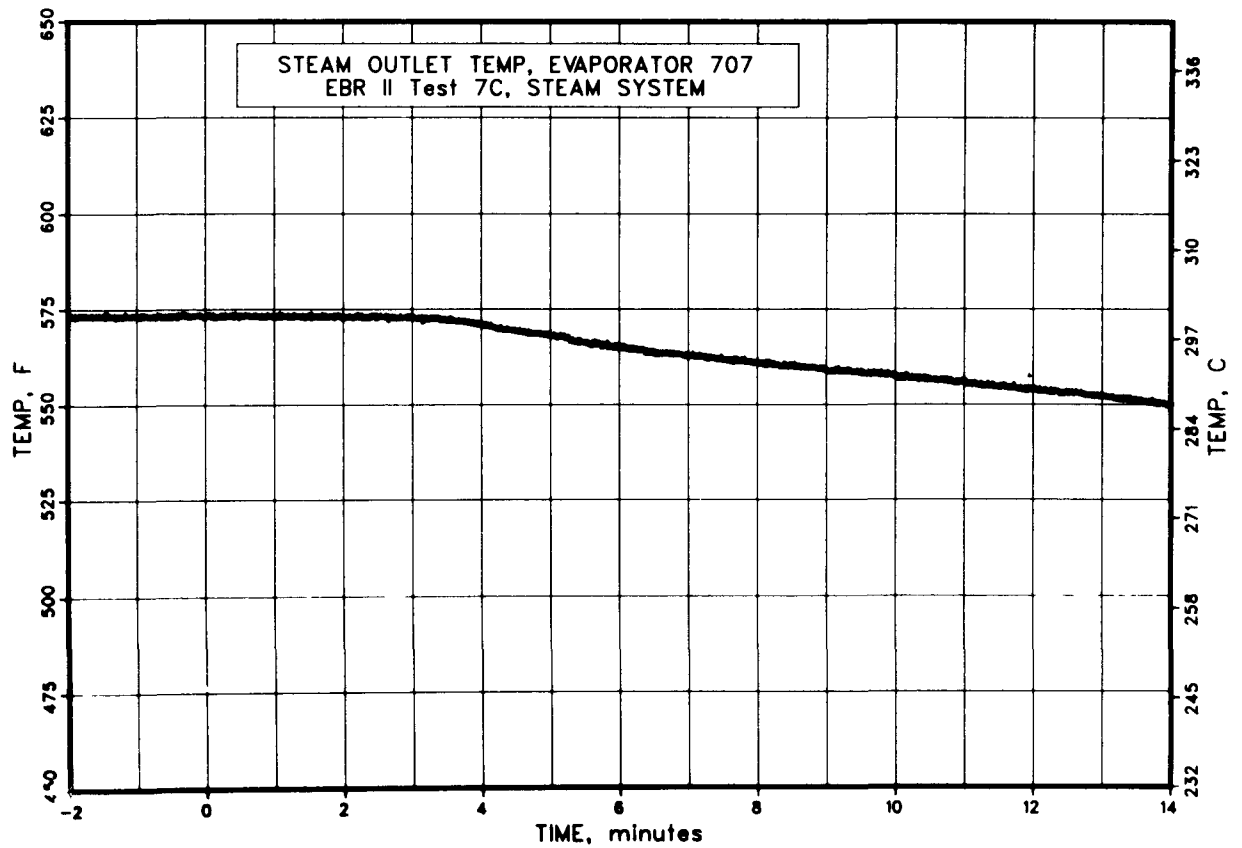
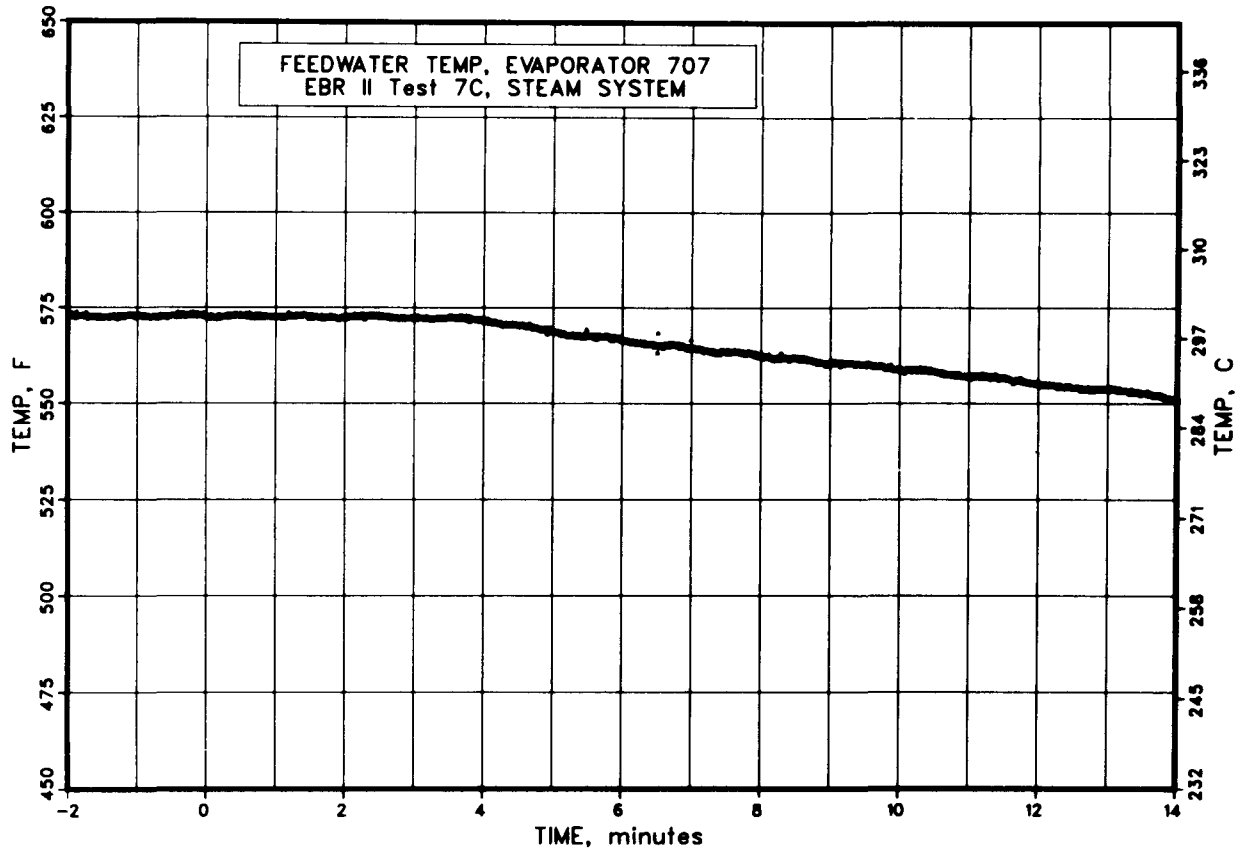
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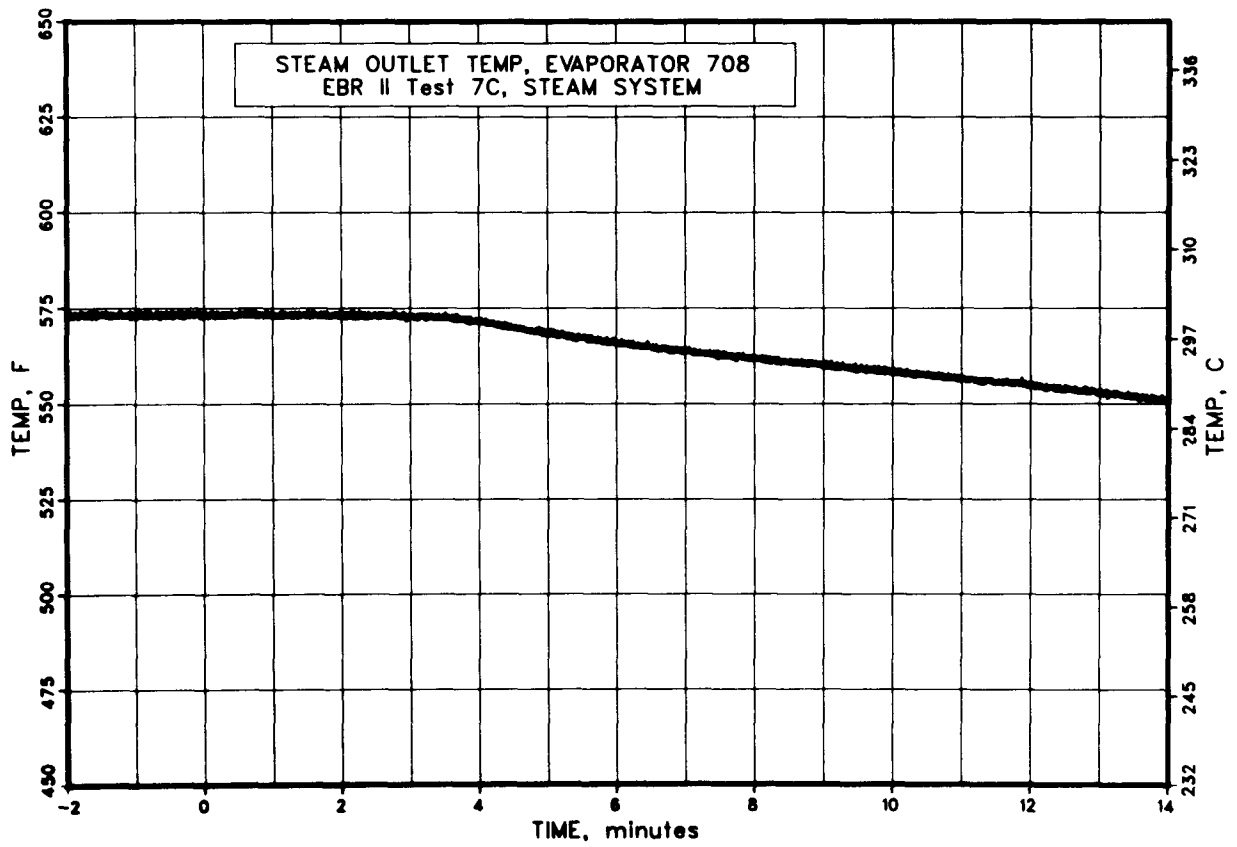
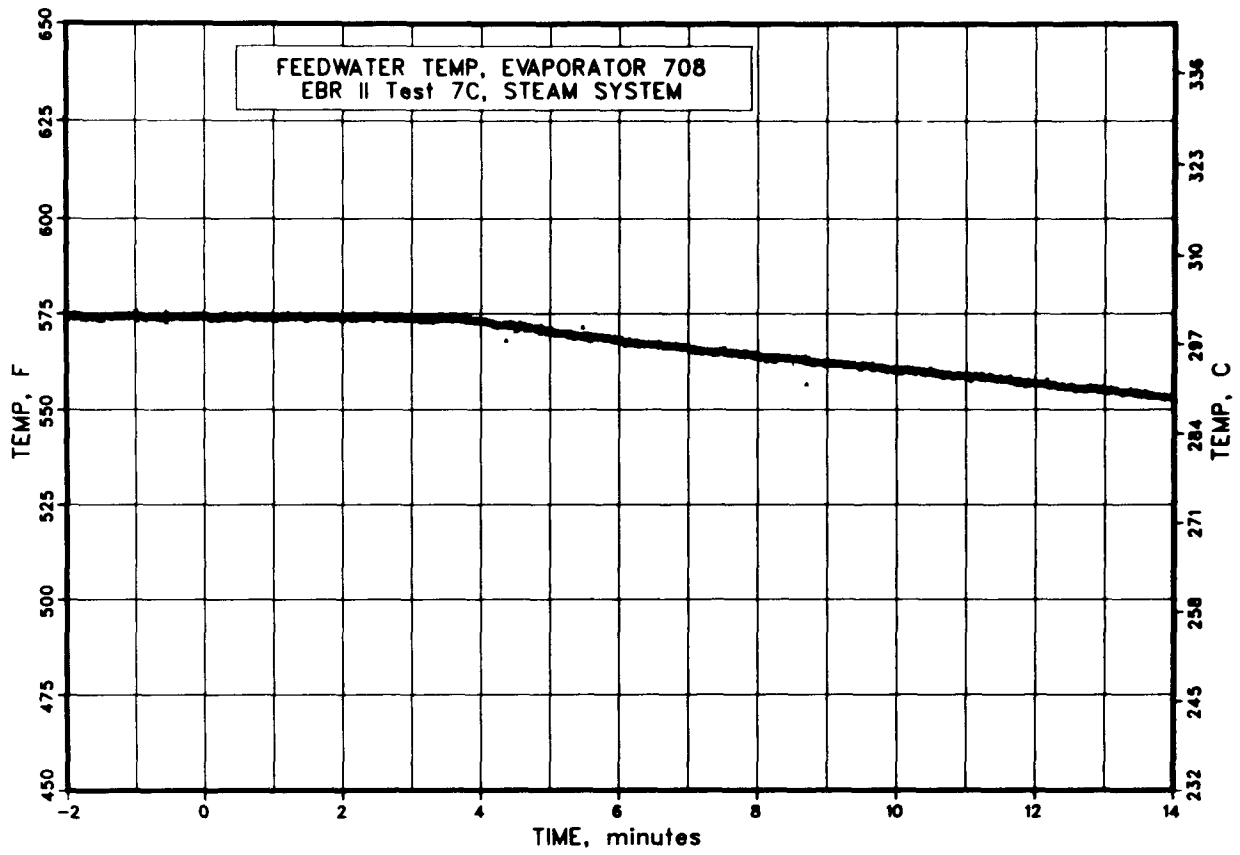
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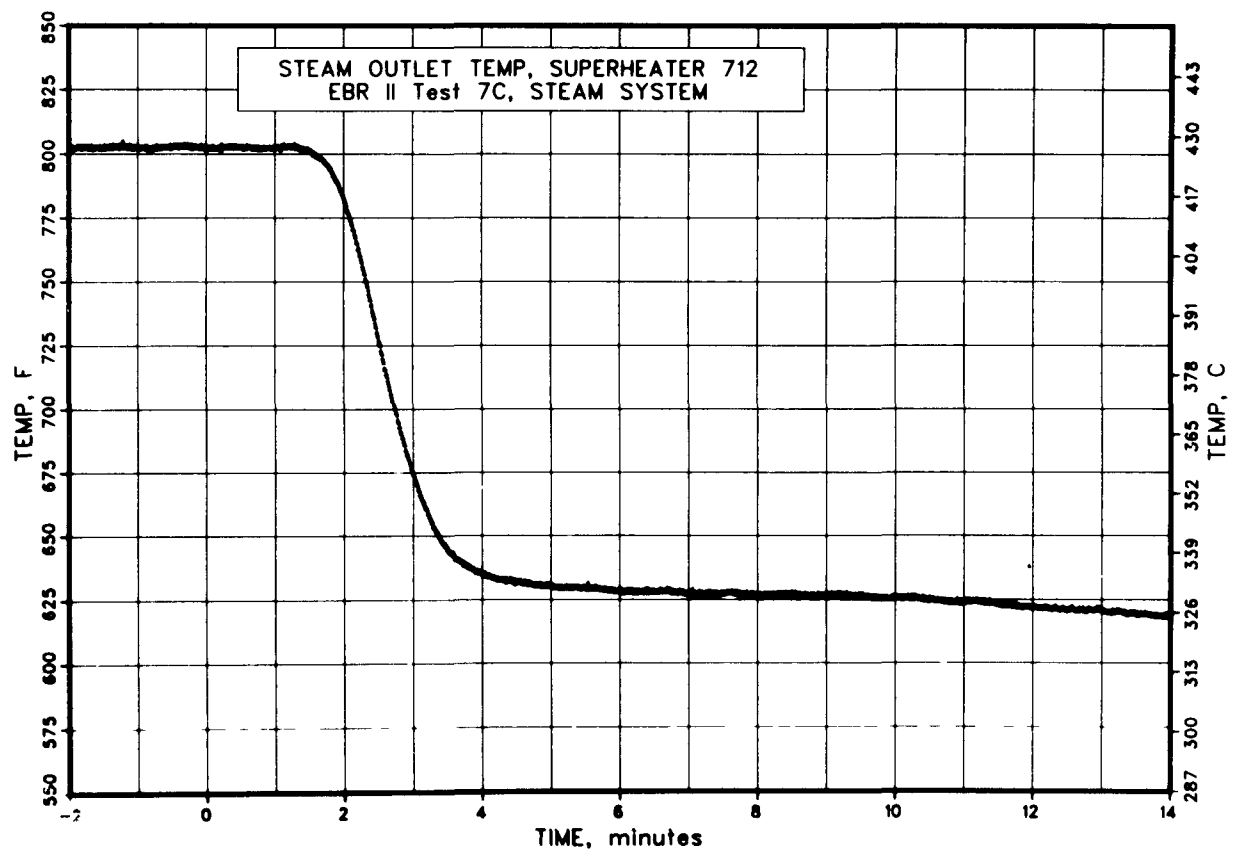
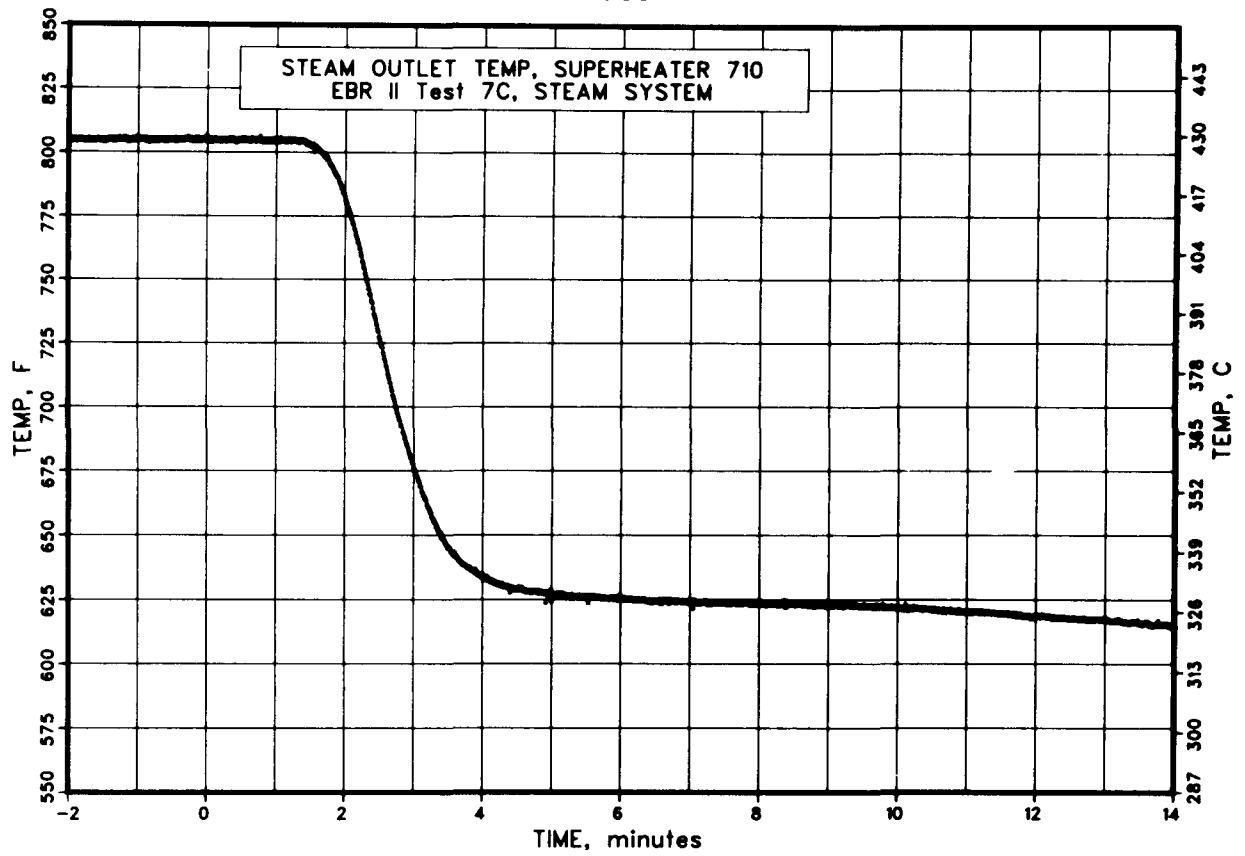


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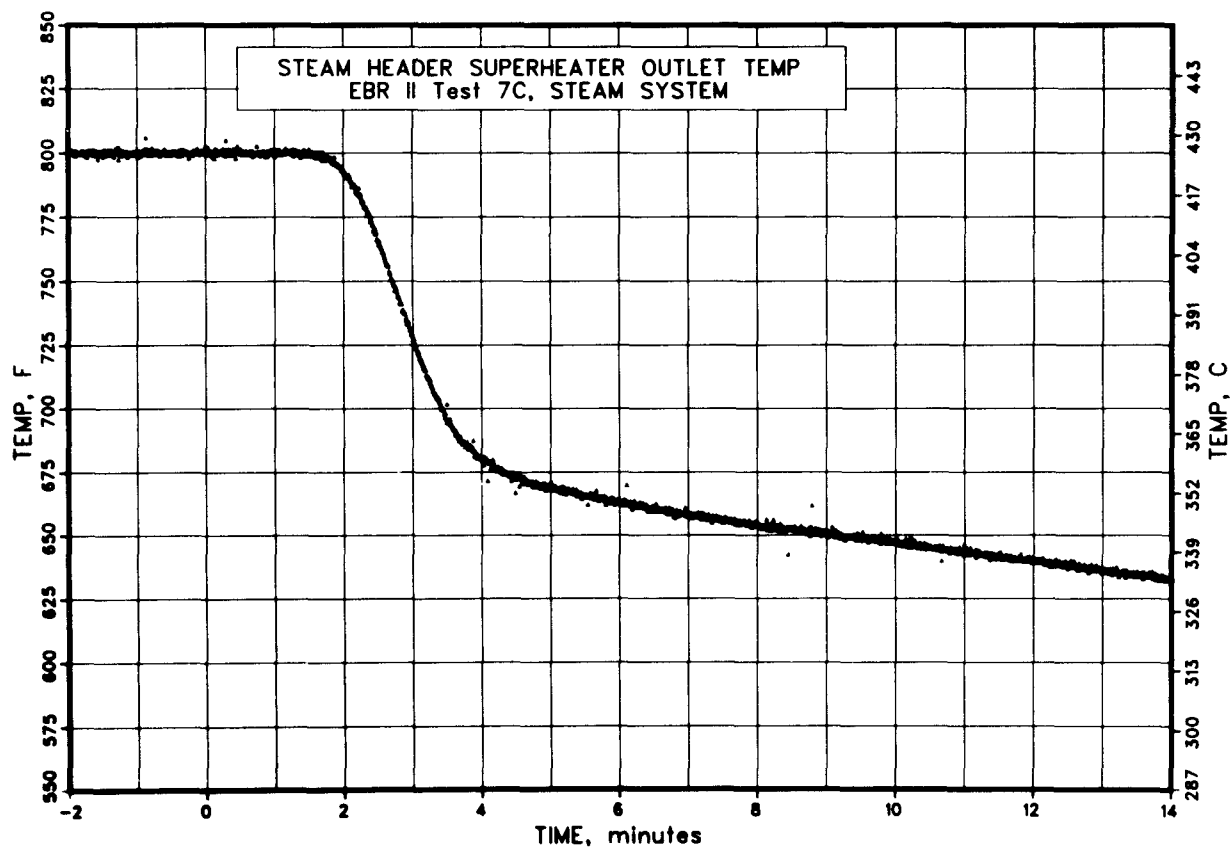
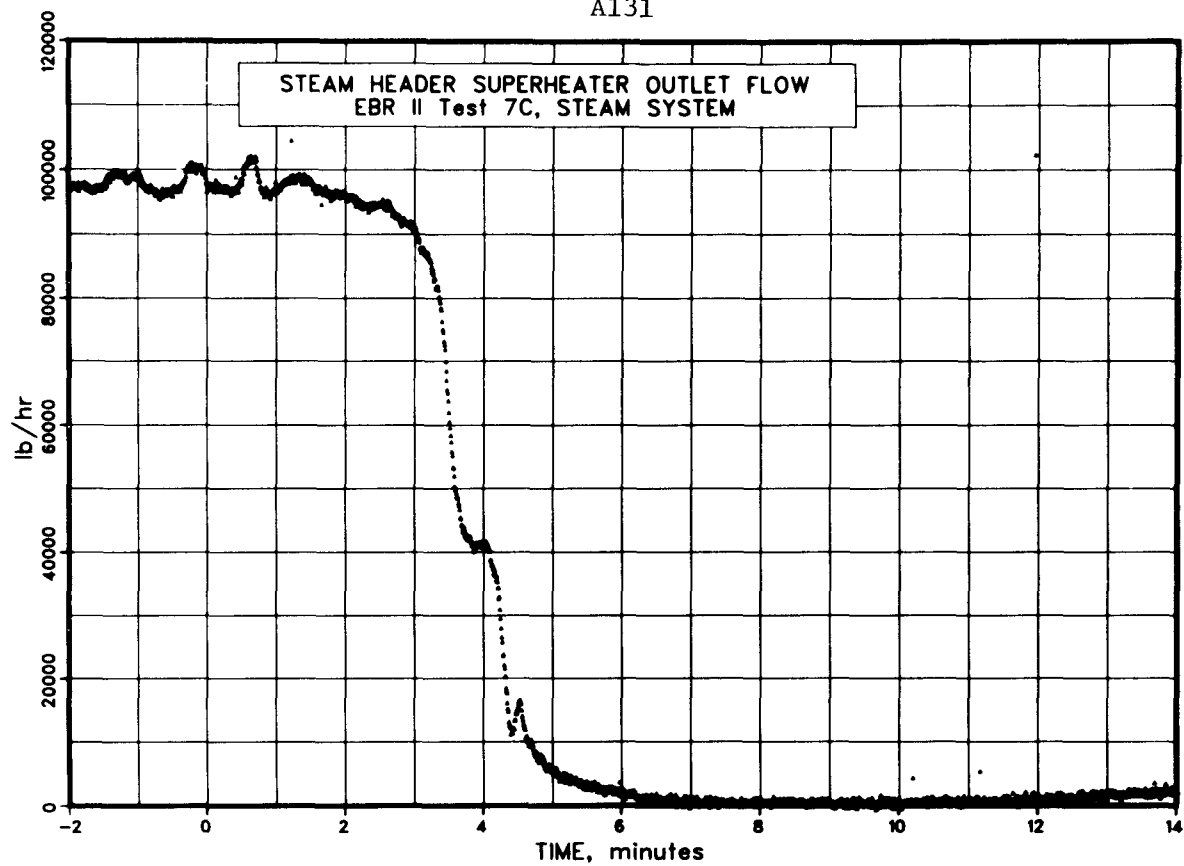


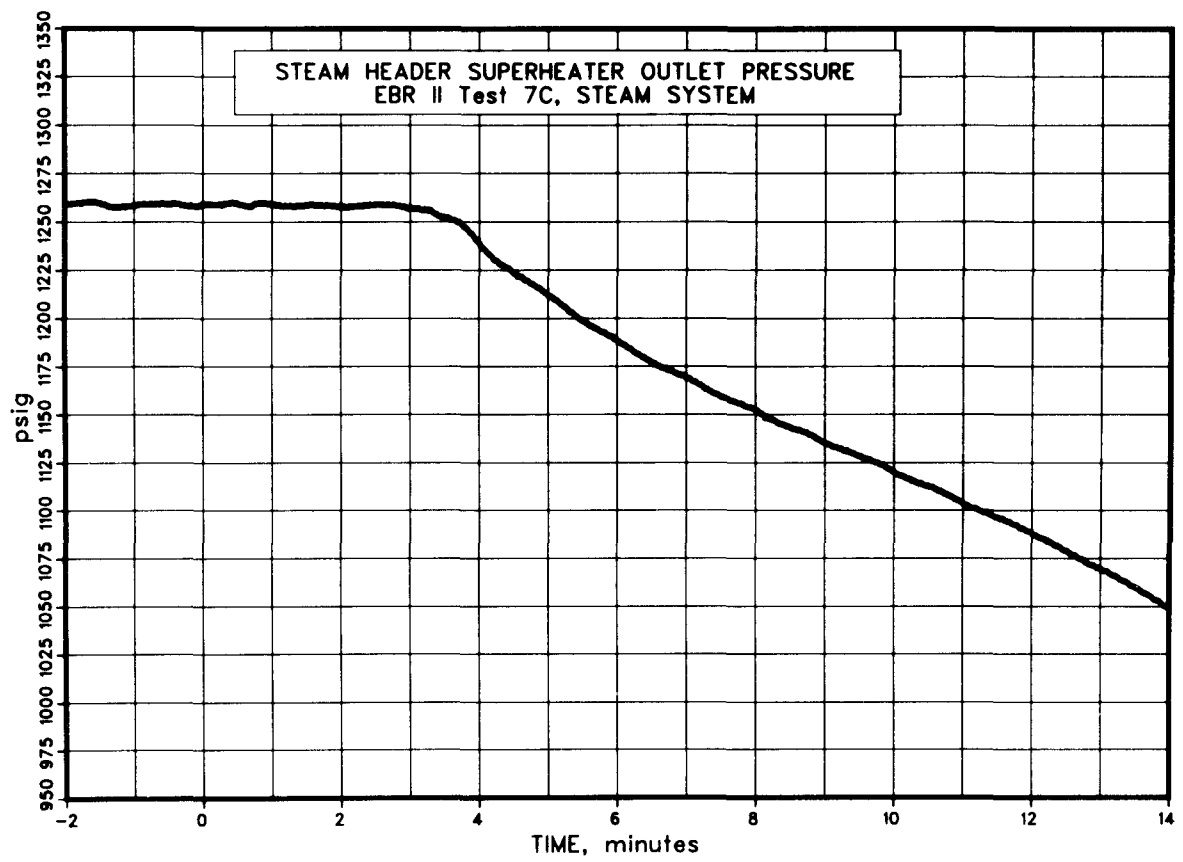
A129



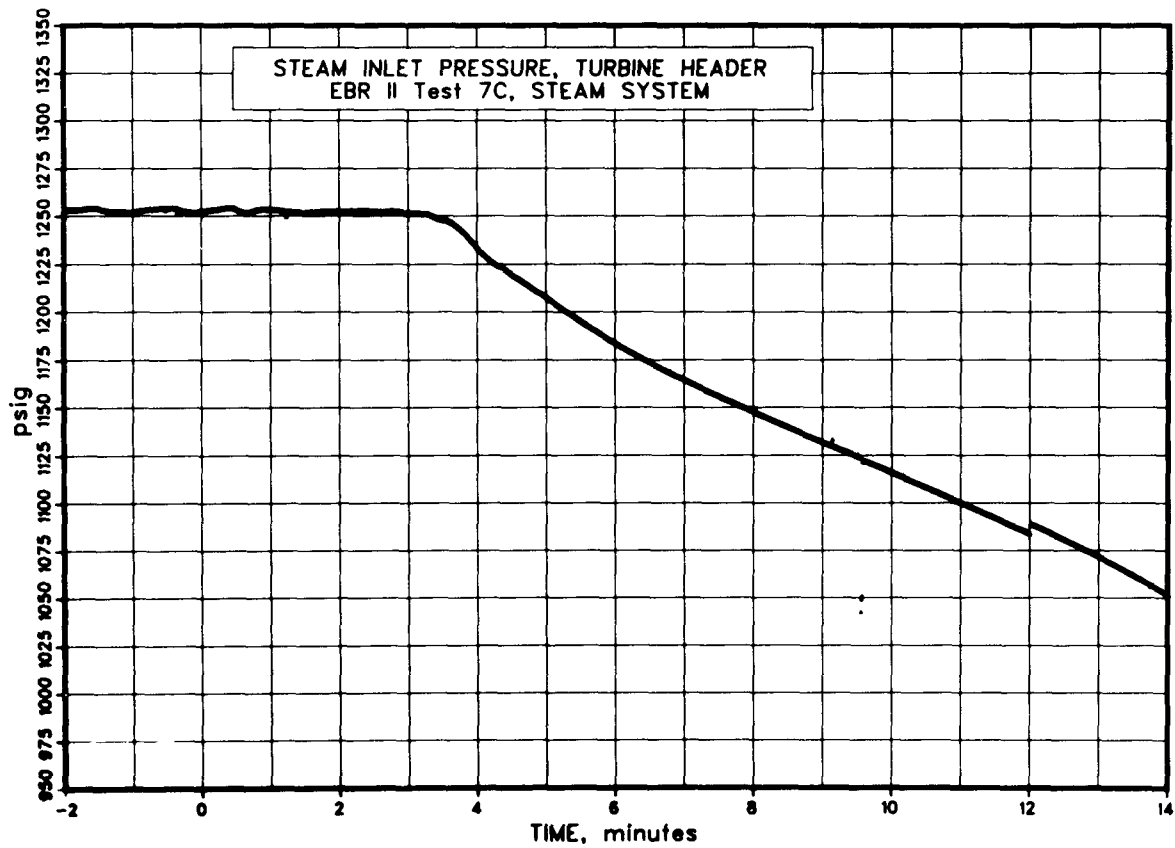
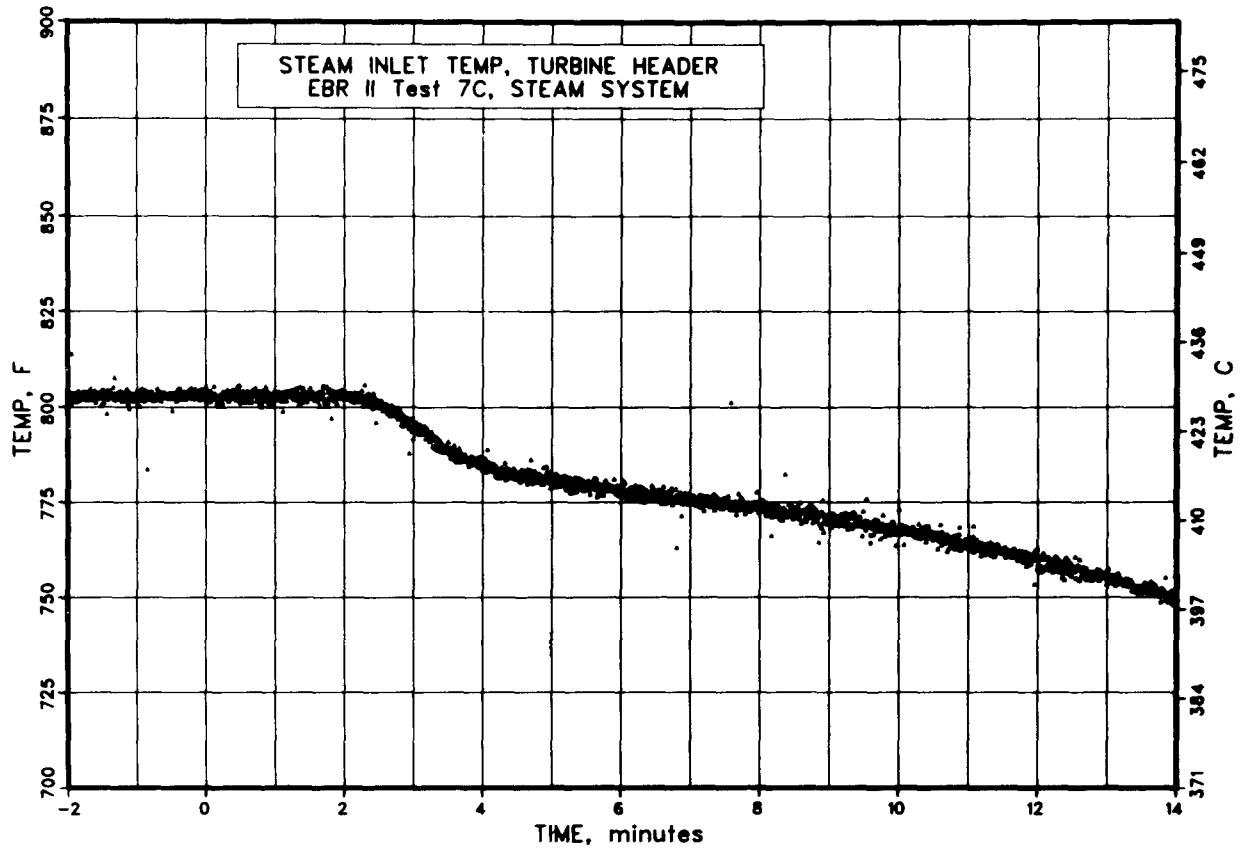


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A133



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