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NUMERICAL SOLUTION OF THE FOKKER-PLANCK EQUATIONS FOR A
MULTI-SPECIES PLASMA

John Killeen and Arthur A. Mirin

March 11, 1977

Lecture to be presented at the COLLEGE IN THEORETICAL AND
COMPUTATIONAL PLASMA PHYSICS

22 March 1977 - 9 April 1977 Tricase, Italy

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NUMERICAL SOLUTION OF THE FOKKER-PLANCK EQUATIONS FOR A MULTI-SPECIES PLASMA*

John Eilstein and Arthur A. Mirin
Lawrence Livermore Laboratory, Livermore, California 94550
and
Department of Applied Science, University
of California, Davis/Livermore, California 94550

ABSTRACT

Two numerical models used for studying collisional multi-species plasmas are described. The mathematical model is the Boltzmann kinetic equation with Fokker-Planck collision terms. A one-dimensional code and a two-dimensional code, used for the solution of the time-dependent Fokker-Planck equations for ion and electron distribution functions in velocity space, are described. The required equations and boundary conditions are derived and numerical techniques for their solution are given.

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*As part of the work performed under the Lawrence Livermore Laboratory contract with the University of California, Davis.

1. INTRODUCTION

In the simulation of magnetically confined plasmas where the ions are not Maxwellian and where a knowledge of the distribution functions is important, kinetic equations must be solved. The proposition that a stable mirror plasma will yield net thermonuclear power depends on the rate at which particles are lost out the ends of the mirror. At number densities and energies typical of mirror machines, the ion losses are due mostly to the scattering of charged particles into the vacuum by a directly space-averaged Coulomb collision. The kinetic equation describing this process is the Boltzmann equation with Fokker-Planck collision terms [1, 2].

The use of this equation is not restricted to mirror systems. The heating of plasmas by energetic neutral beams, the thermalization of α -particles in DT plasmas, the study of runaway electrons and ions in Tokamaks, and the performance of two-energy component fusion reactors are other examples where the solution of the Fokker-Planck equation is required [3].

The problem is to solve a nonlinear partial differential equation for the distribution function of each charged species in the plasma, as a function of seven independent variables (three spatial coordinates, three velocity coordinates, and time). Such an equation, even for a single species, exceeds the capability of any present computer to solve directly. Approximations are therefore required to treat the problem. Typical approximations that are made in present day codes are to neglect particle transport terms, to neglect the distribution function in the scattering function, to neglect space (and the direct effect of the magnetic field). These approximations reduce the number of

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independent variables in three-type velocity space (coordinates v , θ and ϕ), the speed and pitch angle, and the time. It is even worth mentioning there has been an evolution of numerical Pöcker-Flarek codes over the past fifteen years [2].

A multi-species code has been developed in order to study ion and electron mirror systems, including the effects of neutral gas drag. The principal assumptions of this code are that the "background potential" space distributions are isotropic and that the distribution functions can be represented by their l -pole angular eigenfunction. The resulting set of coupled equations for $f_{nl}(v)$ are then solved numerically using an implicit finite-difference scheme described in Section 3. An extensive parameter study [3] was conducted yielding values of the confinement parameter n_I and the figure of merit Q (the ratio of thermionization power to injected power) as a function of mirror ratio and injection energy.

In Section 4 we describe a highly versatile, two-dimensional multi-species code in which the ion kinetic equations are solved by finite-difference methods on a two-dimensional (v, θ) domain. The electron distribution function is still represented using the Legendre angular eigenfunction (isotropic in a full velocity space); hence, a one-dimensional electron kinetic equation is solved. In Ref. [3] we give a variety of applications of this code and describe diagnostics that have been added for the special problems. For mirror systems with beam injection, we find values of the confinement parameter n_I as much as 40% higher than those given by the one-dimensional Pöcker-Flarek code. We also consider two-component toroidal systems and calculate the energy multiplication factor for a number of different scenarios.

3. MULTI-SPECIES FOKKER-PLANCK EQUATIONS

The appropriate kinetic equations are Boltzmann equations with Fokker-Planck collision terms, often referred to simply as Fokker-Planck equations:

$$\frac{\partial f_a}{\partial t} + \frac{1}{m_a} \frac{\partial f_a}{\partial \mathbf{v}} \cdot \frac{\mathbf{F}}{c} = \frac{\partial f_a}{\partial \mathbf{v}} \cdot \frac{\partial f_a}{\partial \mathbf{v}} + \left(\frac{\partial f_a}{\partial t} \right)_c + \mathcal{L}_a + \mathcal{L}_a' \quad (1)$$

here f_a is the distribution function in 6-dimensional phase space for particles of type a , $\mathbf{F}$, $\mathcal{L}_a$ is the Lorentz term, $(\partial f_a / \partial t)_c$ is the collision term, and $\mathcal{L}_a$ contains loss terms.

The Fokker-Planck collision term for an inverse-square force was derived by Rosenbluth, et al. [4] in the form

$$\left(\frac{\partial f_a}{\partial t} \right)_c = - \frac{1}{v} \frac{\partial f_a}{\partial v} \left(\frac{\partial f_a}{\partial v} \right) + \frac{1}{2} \frac{\partial^2}{\partial v^2} \left(\frac{\partial f_a}{\partial v} \right) \quad (2)$$

where $v_a = (\partial f_a / \partial v) / f_a$. In the present work we write the "Rosenbluth collision" [2]

$$E_a = - \frac{1}{v} \frac{\partial f_a}{\partial v} \ln \int f_b(\underline{v}') (\underline{v} - \underline{v}')^2 d\underline{v}' \quad (3)$$

$$E_a = - \frac{1}{v} \frac{\partial f_a}{\partial v} \ln \int f_b(\underline{v}') (\underline{v} - \underline{v}')^2 d\underline{v}' \quad (4)$$

The transformation of Eq. (2) to spherical polar coordinates (v, θ, ϕ) in velocity space has been given by Rosenbluth, et al. [4]. With our assumption of azimuthal symmetry, the resulting distribution functions are of the form $f_a(v, \mu, t)$, where $\mu = \cos \theta$ and $v = |\mathbf{v}|$. The equation for each species is

$$\begin{aligned}
\frac{1}{\Gamma_u} \frac{df_u}{dt} &= -\frac{1}{v^2} \frac{\partial}{\partial v} \left(f_u v^2 \frac{\partial h_u}{\partial v} \right) + \frac{1}{v^2} \frac{\partial}{\partial u} \left(f_u (1-u^2) \frac{\partial h_u}{\partial u} \right) + \frac{1}{2v^2} \frac{\partial^2}{\partial v^2} \left(f_u v^2 \frac{\partial^2 f_u}{\partial v^2} \right) \\
&\quad + \frac{1}{v^2} \frac{\partial^2}{\partial u^2} \left(f_u \frac{\partial^2 f_u}{\partial u^2} \right) - \frac{1}{v^2} (1-u^2) \frac{\partial^2 f_u}{\partial u^2} + \frac{1}{v} (1-u^2) \frac{\partial f_u}{\partial v} \\
&\quad + \frac{1}{v} u(1-u^2) \frac{\partial f_u}{\partial u} + \frac{1}{v} \frac{\partial}{\partial v} \left(f_u (1-u^2) \frac{\partial f_u}{\partial v} \right) + \frac{1}{v} \frac{\partial f_u}{\partial u} \\
&\quad + \frac{1}{2v^2} \frac{\partial}{\partial v} \left(f_u \frac{\partial}{\partial v} \right) + \frac{1}{v} (1-u^2) \frac{\partial^2 f_u}{\partial v^2} + \frac{\partial f_u}{\partial v} + \frac{\partial f_u}{\partial u} \\
&\quad + \frac{1}{v^2} \frac{\partial}{\partial v} \left(f_u \frac{\partial}{\partial v} \right) + \frac{1}{v^2} u(1-u^2) \frac{\partial^2 f_u}{\partial u^2} + \frac{\partial f_u}{\partial v} \\
&\quad + \frac{1}{v} (1-u^2) \frac{\partial^2 f_u}{\partial u \partial v} + \frac{\partial f_u}{\partial v}
\end{aligned}$$

The functions f_u and h_u , defined by eqs. (1) and (2), can be represented by expansions in Legendre polynomials. In certain special cases of physical purpose we let

$$f_u(t, u, v) = \sum_{l=0}^{\infty} \psi_l^u(v, t) P_l(u), \quad (3)$$

where

$$\psi_l^u(v, t) = \frac{v^{l+1}}{2^{l+1}} \int_{-1}^1 f_u(t, u, v) P_l(u) du. \quad (4)$$

The expansions for φ_a and h_a are

$$\varphi_a(v, \mu, t) = \sum_{j=0}^{\infty} \frac{1}{2^j} \frac{v^j}{Z_a} \ln A_a v^{A_a} \int_0^1 (v, t) P_j(\mu) \quad (8)$$

$$h_a(v, \mu, t) = \sum_{j=0}^{\infty} \frac{m_a + m_b}{m_b} \frac{1}{2^j} \frac{v^j}{Z_a} \ln A_a v^{A_a} \int_0^1 (v, t) P_j(\mu) \quad (9)$$

where

$$A_a^u = \frac{4L}{2\pi^2(1+L)} \int_0^1 \frac{(v')^{u+2}}{v'^{u+1}} \varphi_a^u(v', t) dv' + \int_0^1 \frac{v'}{(v')^{u+1}} \varphi_a^u(v', t) dv' \quad (10)$$

$$\begin{aligned} B_a^u &= \frac{4\pi}{2\pi^2(1+L)} \int_0^1 \frac{(v')^{u+2}}{v'^{u+1}} \varphi_a^u(v', t) dv' + \frac{1+1/2}{1+1/2} \frac{(v')^2}{v'} \varphi_a^u(v', t) dv' \\ &= \frac{v'}{(v')^{u+2}} \left(1 + \frac{1+1/2}{1+1/2} \frac{v^2}{(v')^2} \right) \varphi_a^u(v', t) dv' \end{aligned} \quad (11)$$

In the computations are taken a finite number of terms in the Legendre expansions of φ_a and h_a .

Loss Cone Limit, Antipolar Potential

Since examples studied are devoted to the problem of plasma confinement within systems of magnetic mirrors, we consider the mathematical description of such systems.

The loss cone angle is (Spitzer, [5])

$$\sin^2 \theta_{LC} = 1/B_m, \quad (12)$$

where $B_m = B_0/B_z$, B_0 is the magnetic field at the mirror, and B_z is the magnetic field at the interior point being considered. A particle

whose angle in velocity space is less than θ_{LC} , will be immediately lost from the mirror system. θ_{LC} is independent of velocity as well as particle mass and charge. Eq. (12) is derived under the assumption that no electrostatic potential exists, and θ_{LC} is the actual loss angle only under that condition.

However, because of their greater mobility, the scattering rate of electrons will be greater than that of ions, and more electrons than ions will tend to leak out of the ends of the device. Hence, an multipolar potential will build up, being greatest at the center and decreasing towards the ends. The fact that this potential is established leads to a fundamental change in the loss characteristics for the two types of particles. The loss regions are then defined by a loss angle which is a function of speed and charge. If q_e is charge and ϕ is electrostatic potential, the loss angle is given by

$$\sin^2 \theta_{LC} = 1/R_R, \quad (13)$$

$$\text{where } R_R = \left(\frac{1 + \sum_n q_n^2 / \frac{1}{2} m_n v^2}{P_m} \right)^{-1} \quad (14)$$

μ_0 is the "effective" mirror ratio.

Equation (13) approaches Eq. (12) asymptotically as $v \rightarrow \infty$. For ions, the right hand side of Eq. (13) can exceed unity; no ion in such a velocity regime can be contained. Conversely, for electrons, this term can be less than zero; all electrons at such velocities will be electrostatically trapped. The loss region for ions is transformed from a cone

into a hyperboloid of one sheet. Its minimum radius occurs at $v = v_{\perp}$, and is equal to the minimum ion velocity possible for confinement. The electron loss region is transformed into a hyperboloid of two sheets.

3. SOLUTION OF THE ONE-DIMENSIONAL MULTI-SPECIES EQUATIONS

In this section we describe a numerical model which has proved very useful [7], in which we assume that the Rosenbluth potentials given by Eqs. (8) and (9) are isotropic

i.e.,

$$\frac{\partial \phi_a}{\partial \mu} = \frac{\partial h_a}{\partial \mu} = 0. \quad (15)$$

With this assumption Eq. (5) becomes

$$\begin{aligned} \frac{1}{r_a} \frac{dr_a}{dt} &= \frac{1}{v} \frac{\partial}{\partial v} \left(r_a v^2 \frac{\partial h_a}{\partial v} \right) + \frac{1}{2v^2} \frac{\partial^2}{\partial v^2} \left(r_a v^2 \frac{\partial \phi_a}{\partial v} \right) \\ &+ \frac{1}{2v^3} \frac{\partial \phi_a}{\partial v} \left[(1 - \mu^2) \frac{\partial^2 r_a}{\partial v^2} - 4\mu \frac{\partial r_a}{\partial v} - 2 r_a \right] \\ &- \frac{1}{v^2} \frac{\partial}{\partial v} \left(r_a \frac{\partial \phi_a}{\partial v} \right) + \frac{1}{v^3} \frac{\partial \phi_a}{\partial v} \left(\mu \frac{\partial r_a}{\partial v} + r_a \right). \end{aligned}$$

The above equation is separable, and if we let $r_a(v, \mu, t) = U_a(v, t) M_a(\mu)$, then

$$\begin{aligned} \frac{M_a}{r_a} \frac{dr_a}{dt} &= - \frac{M_a}{v^2} \frac{\partial}{\partial v} \left(U_a v^2 \frac{\partial h_a}{\partial v} \right) + \frac{M_a}{2v^2} \frac{\partial^2}{\partial v^2} \left(U_a v^2 \frac{\partial \phi_a}{\partial v} \right) - \frac{M_a}{v^3} \frac{\partial}{\partial v} \left(U_a \frac{\partial \phi_a}{\partial v} \right) \\ &+ \frac{U_a}{2v^3} \frac{\partial \phi_a}{\partial v} \left[(1 - \mu^2) \frac{\partial^2 M_a}{\partial v^2} - 4\mu \frac{\partial M_a}{\partial v} \right]. \end{aligned}$$

We obtain an eigenvalue problem for $M_\mu(u)$

$$(\Delta - \mu^2) \frac{d^2 M_\mu}{d\mu^2} - \frac{dM_\mu}{d\mu} + \Delta_\mu M_\mu = 0 \quad (16)$$

which is Legendre's equation on the domain $-\cos \theta_{LC}^0 \leq \mu \leq \cos \theta_{LC}^0$, where θ_{LC}^0 is the loss cone angle for a given ω . For each eigenvalue Δ_μ we have an equation of the form [10]. In the following we have replaced $U_\mu(v, t)$ by $r_\mu(v, t)$

$$\begin{aligned} \frac{1}{r_\mu} \frac{dr_\mu}{dt} = & \frac{1}{v^2} \frac{\partial}{\partial v} \left[v^3 \frac{\partial r_\mu}{\partial v} + \frac{\partial r_\mu}{\partial v} \right] + \frac{1}{2v^2} \frac{\partial}{\partial v} \left[v^3 r_\mu \frac{\partial^2 r_\mu}{\partial v^2} \right] \\ & - \frac{\Delta_\mu}{2v^2} \frac{\partial^2 r_\mu}{\partial v^2} r_\mu. \end{aligned} \quad (17)$$

The functions $h_\mu(v, t)$ and $g_\mu(v, t)$ are given by the equations

$$\begin{aligned} h_\mu(v, t) = & \sum_b \left(\frac{Z_b}{Z_\mu} \right)^2 \frac{m_a + m_b}{m_b} \ln A_{ab} \left[\int_0^v r_b(v', t) \frac{v'^2}{v} dv' \right. \\ & \left. + \int_v^\infty r_b(v', t) v' dv' \right] \end{aligned} \quad (18)$$

$$\begin{aligned} g_\mu(v, t) = & \sum_b \left(\frac{Z_b}{Z_\mu} \right)^2 \ln A_{ab} \left[\int_0^v r_b(v', t) v' \left(1 + \frac{1}{2} \frac{v'^2}{v^2} \right) v'^2 dv' \right. \\ & \left. + \int_v^\infty r_b(v', t) \left(1 + \frac{1}{2} \frac{v'^2}{v^2} \right) v'^3 dv' \right] \end{aligned} \quad (19)$$

The summations are taken over all the species of particles being considered, including type a. If we use Eqs. (13) and (19) to evaluate the coefficients of Eq. (17), then the equation for $f_a(v,t)$ becomes

$$\frac{\partial f_a}{\partial t} + \frac{1}{v} \frac{\partial}{\partial v} \left(v f_a \right) + \alpha_a \frac{\partial f_a}{\partial t} + \beta_a \frac{\partial f_a}{\partial v} = \gamma_a f_a \quad (20)$$

where

$$\begin{aligned} \alpha_a &= 4\pi \Gamma_a \int_0^1 \left(\frac{Z_b}{Z_a} \right)^2 \frac{m_a}{2v_b} \ln \Lambda_{ab} \int_0^v f_b(v',t) v'^2 dv' \\ \beta_a &= 4\pi \Gamma_a \int_0^1 \left(\frac{Z_b}{Z_a} \right)^2 \ln \Lambda_{ab} \left[\frac{1}{2v} \int_0^v f_b(v',t) v'^2 dv' + \frac{v^2}{3} \int_v^\infty f_b(v',t) v' dv' \right] \\ \gamma_a &= \frac{\Lambda_a}{2v} 4\pi \Gamma_a \int_0^1 \left(\frac{Z_b}{Z_a} \right)^2 \ln \Lambda_{ab} \left[\int_0^v f_b(v',t) v'^2 \left(1 - \frac{1}{3} \frac{v'^2}{v^2} \right) dv' \right. \\ &\quad \left. + \frac{2v}{3} \int_v^\infty f_b(v',t) v' dv' \right] \end{aligned}$$

The number density of particles of type a is

$$n_a(t) = 4\pi \int_0^\infty f_a(v,t) v^2 dv \quad (21)$$

The last term on the right of Eq. (20) is the particle loss term due to scattering into the loss cone. If $v_a = 0$ then $n_a(t)$ should remain constant in time when given the appropriate boundary conditions for the solution of Eq. (20)

$$(10) \quad \frac{d\mathbf{r}_n}{dt} = \int_{-\infty}^{\infty} \frac{v}{v_{\min} + v} \left(\frac{1}{v} \frac{d\mathbf{r}_n}{dt} + \mathbf{r}_n \frac{1}{v} \frac{dv}{dt} \right) f_n(v) dv = 0$$

is equivalent to

$$\left(\mathbf{r}_n f_n + \mathbf{r}_n \frac{d\mathbf{r}_n}{dv} \right) \Big|_{v=v_{\min}}^{v=v_{\max}} = 0 \quad (11)$$

for $t > 0$, where $v_{\min} \leq v \leq v_{\max}$ is the domain of Eq. (10). At $v = 0$, Eq. (11) is consistent with $d\mathbf{r}_n/dv = 0$, since $\lim_{v \rightarrow 0} (\mathbf{r}_n/v)(f_n/v) = 0$. In multiparticle problems with an arbitrary potential defined, the effective velocity domain will be the interval $(v_{\min}, v_{\max})$. In this case $v_{\min}$ will depend on the ion species and will equal zero for the electrons.

It is convenient to introduce dimensionless variables. Let $x = v/v_0$, where v_0 is a characteristic velocity, $\tau = t/\tau_0$ where τ_0 is a characteristic time, and let $F_n = (4\pi v_0^3/K_n) f_n$, where

$$n_n(0) = K_n \int_0^\infty F_n(x, 0) x^2 dx.$$

(The normalizing constants K_n are determined by the initial density and distribution for each species.) We generally take τ_0 to be defined by the electron equation, i.e., $\tau_0 = (2v_0^3/K_e)(m_e^2/\hbar c^4)$.

We define the functionals

$$H(F) = \int_x^\infty F(x, \tau) x dx \quad (12)$$

$$n(F) = \int_{-\infty}^{\infty} F(y, t) y^2 dy \quad (24)$$

$$F(F) = \int_{-\infty}^{\infty} F(y, t) y^2 dy \quad (25)$$

where $F(F)$ is the function $F(F)$ and $F(F)$ is the function $F(F)$.

$$\frac{\partial^2 F}{\partial t^2} + \frac{1}{x} \frac{\partial}{\partial x} \left[x \left(\frac{\partial F}{\partial x} + \frac{\partial F}{\partial y} \right) \right] + \frac{C}{x} F(F) = 0 \quad (26)$$

where

$$A_n = \frac{1}{x_0^2} \sum_{l=1}^{\infty} \left(\frac{x_l}{x_0} \right)^2 \frac{1}{x_l} \ln \frac{x_l}{x_0} n(F_l)$$

$$B_n = \frac{1}{x_0^2} \sum_{l=1}^{\infty} \left(\frac{x_l}{x_0} \right)^2 \frac{1}{x_l} \ln \frac{x_l}{x_0} \left[\frac{1}{x} E(F_l) + \frac{2x}{\delta} M(F_l) \right]$$

$$C_n = \frac{1}{x_0^2} \frac{1}{x} \sum_{l=1}^{\infty} \left(\frac{x_l}{x_0} \right)^2 \frac{1}{x_l} \ln \frac{x_l}{x_0} \left[\frac{1}{x} E(F_l) + \frac{2x}{\delta} M(F_l) \right]$$

To the right side of Eq. (26) we have added a source term $D_n(x, y)$ for each species.

Equation (26) is a system of coupled partial differential equations. For each particle species, n , we have an equation corresponding to A_n , the eigenvalue of Eq. (16). In principle we could consider several eigenvalues for each species, but in this paper we have used only the lowest eigenvalue corresponding to the first normal mode. Hence we have one equation for each species. In solving the system given by Eq. (26) we consider it as a vector equation of the form

$$\frac{d}{dt} \begin{pmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{pmatrix} = \begin{pmatrix} A_1 & A_2 & \dots & A_n \\ A_1 & A_2 & \dots & A_n \\ \vdots & \vdots & \ddots & \vdots \\ A_1 & A_2 & \dots & A_n \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{pmatrix} + \begin{pmatrix} b_1 \\ b_2 \\ \vdots \\ b_n \end{pmatrix} \quad (21)$$

where

$$A_i = \begin{pmatrix} a_{11} & a_{12} & \dots & a_{1n} \\ a_{21} & a_{22} & \dots & a_{2n} \\ \vdots & \vdots & \ddots & \vdots \\ a_{i1} & a_{i2} & \dots & a_{in} \\ \vdots & \vdots & \ddots & \vdots \\ a_{n1} & a_{n2} & \dots & a_{nn} \end{pmatrix}, \quad b_i = \begin{pmatrix} b_1 \\ b_2 \\ \vdots \\ b_n \end{pmatrix}$$

and A_i, b_i denote $n \times n$ and $n \times 1$ matrices, and $i = 1, \dots, n$, the source vector.

Let $x_i(t)$ and $u_i(t)$ denote the i -th component of x and u respectively.

$$\frac{dx_i}{dt} = \sum_{j=1}^n a_{ij} x_j + b_i, \quad i = 1, 2, \dots, n. \quad (22)$$

Let us discretize (22) with respect to t by the Euler method. Let Δt denote the time step with the i -th spatial coordinate.

We solve (22) by finite-difference method. On the domain

$0 \leq x_j \leq x_{j+1}$, $j = 1, \dots, n$, we have a finite-difference mesh denoted by x_j .

Let t_j denote the time $t = j \Delta t$, $j = 0, 1, \dots$. The j -spacing is variable and

we define $\Delta x_{j+1/2} = x_{j+1} - x_j$, $\Delta x_{j-1/2} = x_j - x_{j-1}$, $\Delta x_j = \frac{1}{2} (x_{j+1} - x_{j-1})$.

We apply (22) to the following explicit difference equation

$$\begin{aligned} \frac{p_{ij}^{n+1} - p_{ij}^n}{\Delta t} &= \sum_{j=1}^n \frac{a_{ij}^{n+1} x_j - a_{ij}^{n+1} x_{j-1}}{\Delta x_j} + \frac{b_i^{n+1}}{\Delta x_j} p_{ij}^{n+1} + p_{ij}^{n+1} \\ &= (1 - \rho) \sum_{j=1}^n \frac{a_{ij}^{n+1} x_j - a_{ij}^{n+1} x_{j-1}}{\Delta x_j} + \frac{b_i^{n+1}}{\Delta x_j} p_{ij}^n + p_{ij}^n \end{aligned} \quad (23)$$

$$F_j^n = \frac{p}{x_j} + \frac{1}{\Delta x_j} \left[\frac{A_{j+1/2}^{n+1/2}}{2} + \frac{P_{j+1/2}^{n+1/2}}{2\omega_{j+1/2}} \right]$$

$$F_{j+1}^n = F_{j+1}^{n-1} \left[\frac{(1-\rho)}{x_j} + \frac{1}{\Delta x_j} \left(\frac{A_{j+1/2}^n}{2} + \frac{P_{j+1/2}^n}{2\omega_{j+1/2}} \right) + F_{j+1/2}^{n-1} \right]$$

$$+ \frac{(1-\rho)}{x_j} \left[\frac{1}{\Delta x_j} \left(\frac{A_{j+1/2}^{n+1/2}}{2} + \frac{P_{j+1/2}^{n+1/2}}{2\omega_{j+1/2}} \right) + \frac{P_{j+1/2}^{n+1/2}}{2\omega_{j+1/2}} + F_{j+1/2}^{n+1/2} \right]$$

$$+ p^n \left[\frac{(1-\rho)}{x_j} + \frac{1}{\Delta x_j} \left(-\frac{A_{j+1/2}^n - 1/e}{2} + \frac{P_{j+1/2}^n - 1/e}{2\omega_{j+1/2}} \right) \right]$$

$$+ p_0^{n+1} + (1-\rho) p_0^n$$

In order to linearize the system (50) we extrapolate the q , p , γ defined above to the new time step, $n+1$, using their values at n and $n-1$. The method used to solve Eq. (50) is the standard tridiagonal method given by RICHMONT and MORTON [6].

At every time step we calculate the number density and average energy of each type of particle from the equations

$$n_p(\tau) = X_p I_2^p(\tau)$$

$$E_p(\tau) = \frac{3}{2} kT_p + \frac{1}{2} x_p v_0^2 I_4^p(\tau) / I_2^p(\tau)$$

where

$$I_2^p(\tau) = \int_0^\infty F_p(x, \tau) x^2 dx$$

$$I_4^p(\tau) = \int_0^\infty F_p(x, \tau) x^4 dx$$

It is convenient to solve the scattering ion term, $\hat{S}_{ij}^{(0)}$, and to add the contribution of the scattering electron term, Eq. (16), for a given v_{10} . For the calculation of the $\hat{S}_{ij}^{(0)}$ the equation corresponding to the first normal component of the Boltzmann equation is solved for the value

$$R_{ij} = (1 + R_{ij}^0)^{-1} \quad (31)$$

where $R_{ij}^0 = \hat{S}_{ij}^{(0)}/\hat{S}_{ij}^{(0)}$ is the ratio for particles of type i and depends on the scattering potential ϕ^0 .

For ions we have

$$R_{ij} = R_{ij}^0 + \frac{\phi^0}{\frac{1}{2} m_{ij} v_{10}^2} \quad (32)$$

where $R_{ij} = \hat{S}_{ij}^{(0)}/\hat{S}_{ij}^{(0)}$, $\phi^0 = \frac{1}{2} m_{ij} v_{10}^2$.

For ions we have

$$R_{ij} = R_{ij}^0 + \frac{\phi_{ij}^0}{\frac{1}{2} m_{ij} v_{10}^2} \quad (33)$$

The procedure for determining ϕ^0 follows. Let

$$\begin{aligned} q^-(r) &= n_i(r) \\ q^+(r) &= \sum_j z_j n_j(r) \quad (i \neq e) \end{aligned}$$

(the sum taken over the ion species). At every time step q^- and q^+ are computed and the difference $(q^+ - q^-)/q^-$ is compared to a specified

is a sphere. If the radius of the sphere is r and the center is (x_0, y_0) , then the value of Δ_{ij} is given by the value of Δ_{ij} at the point closest to (x_0, y_0) . The general case of this is that Δ_{ij} is the value of Δ_{ij} at the point (x_0, y_0) if

$$\Delta_{ij} = \begin{cases} \Delta_{ij}(x_0, y_0) & \text{if } \sqrt{(x - x_0)^2 + (y - y_0)^2} \leq r \\ \Delta_{ij}(x, y) & \text{if } \sqrt{(x - x_0)^2 + (y - y_0)^2} > r \end{cases} \quad (5)$$

where $\Delta_{ij}(x_0, y_0) = \Delta_{ij}(x, y)$ is the value of Δ_{ij} at the value of (x, y) that satisfies $\Delta_{ij}(x, y) = \min_{(x, y) \in \mathbb{R}^2} \Delta_{ij}(x, y)$. We use the corresponding value of the function Δ_{ij} at the point (x_0, y_0) to obtain the value of Δ_{ij} at the point (x, y) if $\Delta_{ij}(x, y) = \min_{(x, y) \in \mathbb{R}^2} \Delta_{ij}(x, y)$.

$$\Delta_{ij} = \Delta_{ij}(x, y) + \frac{\Delta_{ij}(x_0, y_0) - \Delta_{ij}(x, y)}{\sqrt{(x - x_0)^2 + (y - y_0)^2}} \quad (6)$$

The separated approach can be generalized in the following way. Let $\mathcal{R}_i$ represent the set of i th points in the i th data set.

$$\Delta_{ij} = \min_{(x, y) \in \mathcal{R}_i} \left(\sum_{k=1}^n \frac{\Delta_{ij}^k(x, y)}{\Delta_{ij}^k(x_0, y_0)} \right) \quad (7)$$

where $\Delta_{ij}^k(x, y)$ are given by (4) with appropriate values of $\Delta_{ij}^k(x, y)$. Before computing Δ_{ij} we separate the points in $\mathcal{R}_i$ into n groups. Let $\mathcal{R}_i^k$ denote the k th group of points in $\mathcal{R}_i$. Let $\Delta_{ij}^k(x, y)$ denote the value of Δ_{ij} at the point (x, y) if $(x, y) \in \mathcal{R}_i^k$.

$$\frac{dH_k^H}{dt} = \sum_{j=1}^N \left(\frac{1}{\rho^j} \frac{\partial}{\partial v} \left(\rho_{jk}^H H_k^H \right) + \rho_{jk}^H \frac{\partial H_k^H}{\partial v} \right) - \frac{\gamma_{jk}^H}{\rho^j} \frac{dH_j^H}{dt} \quad (37)$$

for $k = 1, 2, \dots, K$.

A detailed description of this formulation appears in Killeen, et al. [3].

4. SOLUTION OF THE MULTI-SPECIES EQUATIONS IN A TWO-DIMENSIONAL VELOCITY SPACE

Equation (37) in (x,v) coordinates, written in conservative form, is

$$\frac{\partial}{\partial x} \left(\frac{H_k^H}{\rho^j} \right) + \frac{\partial}{\partial v} \left(\frac{H_k^H}{\rho^j} \right) + \frac{1}{v^2} \frac{\partial}{\partial v} \left(v^2 \frac{\partial H_k^H}{\partial v} \right) = 0 \quad (38)$$

and (39)

$$\frac{\partial}{\partial x} \left(\frac{H_k^H}{\rho^j} \right) + \frac{\partial}{\partial v} \left(\frac{H_k^H}{\rho^j} \right) + \frac{1}{v^2} \frac{\partial}{\partial v} \left(v^2 \frac{\partial H_k^H}{\partial v} \right) = 0 \quad (39)$$

$$\frac{\partial}{\partial x} \left(\frac{H_k^H}{\rho^j} \right) + \frac{\partial}{\partial v} \left(\frac{H_k^H}{\rho^j} \right) + \frac{1}{v^2} \frac{\partial}{\partial v} \left(v^2 \frac{\partial H_k^H}{\partial v} \right) = 0 \quad (40)$$

[illegible]

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[illegible]

[illegible]

$$F_{\lambda} = \frac{1}{\lambda} \frac{\partial F}{\partial \lambda} = \frac{1}{\lambda} \frac{\partial}{\partial \lambda} \left(\frac{1}{\lambda} \right) = -\frac{1}{\lambda^2}$$

The functions σ_n and τ_n are given by Eqs. (8) and (9).

Equation (10) is integrated using the method of splitting, or fractional, integrals, or first solution.

$$\frac{\partial \mathcal{L}}{\partial \mathbf{h}} = \frac{\partial \mathcal{L}}{\partial \mathbf{h}^T} \mathbf{h} = \frac{\partial \mathcal{L}}{\partial \mathbf{h}^T} \frac{\partial \mathbf{h}}{\partial \mathbf{h}^T} = \frac{\partial \mathcal{L}}{\partial \mathbf{h}^T} \mathbf{I} = \frac{\partial \mathcal{L}}{\partial \mathbf{h}^T} \quad (10)$$

using an explicit difference algorithm (1), has the advantage

$$\frac{1}{r_n} \frac{\partial p}{\partial r} = \frac{1}{v^2 \sin \theta} \frac{\partial H}{\partial \theta} \quad (48)$$

in an explicit manner.

Equation (47) is differentiated as follows:

$$\begin{aligned} \frac{p_{i,j}^{n+1} - p_{i,j}^n}{\Delta v_{i,j}} &= \frac{A_{i,j-1}^n (p_{i,j-1}^{n+1} - p_{i,j-1}^n) - A_{i,j+1}^n (p_{i,j+1}^{n+1} - p_{i,j+1}^n)}{\Delta v_{i,j}} \\ &+ \frac{1}{v_{i,j}^2 \Delta v_{i,j}} \frac{p_{i,j+1/2}^n (p_{i,j+1}^{n+1} - p_{i,j+1}^n) - p_{i,j-1/2}^n (p_{i,j-1}^{n+1} - p_{i,j-1}^n)}{\Delta v_{i,j/2}} \\ &+ \frac{1}{\Delta v_{i,j} \Delta \theta_j} \frac{p_{i,j-1}^n (p_{i,j-1/2}^{n+1} - p_{i,j-1/2}^n) - p_{i,j+1}^n (p_{i,j+1/2}^{n+1} - p_{i,j+1/2}^n)}{\Delta \theta_j} \\ &= \frac{p_{i,j-1}^n (p_{i,j-1/2}^{n+1} - p_{i,j-1/2}^n) - p_{i,j+1}^n (p_{i,j+1/2}^{n+1} - p_{i,j+1/2}^n)}{\Delta \theta_j^2} \end{aligned} \quad (49)$$

Here, $p_{i,j}^n = p(v_{i,j}, \theta_j, t_n)$.

By rearranging terms, Eq. (49) may be put into the tri-diagonal form:

$$-p_{i,j-1}^{n+1} + \beta_{i,j}^n p_{i,j}^{n+1} - p_{i,j+1}^{n+1} = \delta_{i,j}^n \quad (50)$$

We see that the terms of mixed second derivative type may not be written fully implicitly if we wish to maintain a tri-diagonal form. Equation (48) is integrated in a similar manner, with the roles of v and θ reversed.

The direct two-dimensional approach for determining the ion velocity-space distribution in a π -confined plasma can be used to analyze many different physical situations which cannot be studied with the one-dimensional, liquid-ion, multi-mode approach described in Section 3. In particular, transient plasmas, which rapidly are altered in either experiments or astrophysical situations, and which do not satisfy the equilibrium condition of a liquid-ion multi-mode ion distribution. Furthermore, the trajectory of a self-consistent neutral beam given a set of initial conditions that are sharply peaked in velocity space, so that many modes are excited and the required data adequate representation.

The two-dimensional approach is more complicated than the one-dimensional approach, and the numerical calculations are more involved. However, the two-dimensional approach is more general and can be used to study a wider range of physical situations. The two-dimensional approach is more computationally intensive than the one-dimensional approach, but it is more flexible and can be used to study a wider range of physical situations. The two-dimensional approach is more computationally intensive than the one-dimensional approach, but it is more flexible and can be used to study a wider range of physical situations.

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which serves as the figure of merit for a pulsed TWT system [14].

Several features of the Fokker-Planck model are especially appropriate for representing physically significant effects in a TWT. The random motion of the electrons produces noise, and the collisionless interaction of all species, including self-interaction, is properly accounted for regardless of the form of the distribution function. Electron particles and impurity ions are treated on an equal footing with the electrons and ions, and since there is no inherent restriction on the number of species, which can be treated in the code. Many other advantages are of great importance for implementing neutral beam heating in the toroidal plasma, and the two-dimensional nature of our velocity space (v_x, v_y) is especially useful for simulations of the plasma heating by neutral beams and the plasma cooling during decay.

The equilibrium distribution, f_0 , for the electrons of the plasma, is assumed to be

$$\frac{2\pi}{v} f_0 = \text{constant} \times \exp\left(-\frac{mv^2}{2kT_e}\right) \quad (52)$$

$$f_0 = 0 \quad \text{for } |v| > v_{\text{thermal}} \quad (53)$$

where $v_{\text{thermal}} = (2kT_e/m)^{1/2}$ is the thermal velocity. For a time-dependent magnetic field, $B(t)$, the equilibrium distribution, f_0 , changes to time, t , and these equations are solved numerically.

$$\frac{d}{dt} \left(\frac{1}{v} \right) = -\frac{1}{v} \frac{dv}{dt} = -\frac{1}{v} \frac{1}{B} \frac{dB}{dt} \quad (54)$$

$$\frac{d}{dt} \left(\frac{1}{v} \right) = -\frac{1}{v} \frac{dv}{dt} = -\frac{1}{v} \frac{1}{B} \frac{dB}{dt} \quad (55)$$

Since B is essentially just the toroidal field strength, it varies inversely with R , yielding

$$\frac{\dot{B}}{B} = - \frac{\dot{R}}{R} \quad (56)$$

and thus results the form of the $\nabla \cdot \mathbf{E}$ term becomes

$$\frac{\partial \mathbf{E}}{\partial t} + \frac{\dot{B}}{B} \left[\mathbf{r} - 1 + \frac{1}{R} \sin^2 \theta \right] \cdot \frac{\partial \mathbf{r}}{\partial t} + \frac{\dot{B}}{B} \sin^2 \theta \left(\frac{\partial \mathbf{r}}{\partial t} \cdot \frac{\partial \mathbf{r}}{\partial t} \right) \cdot \mathbf{r} + 1. \quad (57)$$

where $(\partial \mathbf{r} / \partial t)_{\theta} = 1$, given by Eq. (52). For isotropic electrons we have

$$\frac{\partial \mathbf{E}}{\partial t} \cdot \mathbf{r} = \frac{1}{R} \nabla \cdot \frac{\partial \mathbf{E}}{\partial t} \frac{\mathbf{r}}{R} = \left(\frac{\partial \mathbf{E}}{\partial t} \right)_{\theta} \cdot \mathbf{r} + \mathbf{E} \cdot \mathbf{r} \quad (58)$$

The source term J_{α} in Eq. (1) is of the form

$$J_{\alpha}(v, \theta, t) = \sum_{\ell} J_{\alpha}^{\ell}(t) \cdot J_{\alpha}^{\ell}(v, \theta) \delta_{\ell}^{\alpha, \ell}(t) \quad (59)$$

where the shape function $J_{\alpha}^{\ell}(v, \theta)$ is a Gaussian in v and $\cos \theta$ respectively, $\delta_{\ell}^{\alpha, \ell}(t)$ is either 0 or 1, and $J_{\alpha}^{\ell}(t)$ is a current.

The last term J_{α} may contain several loss processes. Losses due to charge exchange with the beam are expressed as

$$J_{\alpha}^{\ell} = - \sum_{\ell', \ell''} L_{\alpha \ell'}^{\ell} \cdot L_{\ell'}^{\ell''}(t) \cdot J_{\ell'}^{\ell''}(v, \theta, t) \quad (60)$$

where the quantities $L_{\alpha \ell'}^{\ell}$ are constant parameters. The presence of the vector $\delta_{\ell'}^{\alpha, \ell''}(t)$ allows the whole charge exchange process to be implemented in a simple way; that is, a given charge exchange term along with its corresponding source term appears in the same temporal function $\delta_{\ell'}^{\alpha, \ell''}(t)$.

The effects of finite particle and energy confinement times in a Tokamak are incorporated by adding a contribution to L_A of the form

$$L_A^T = - \frac{f_A(v, \theta, t)}{\tau_p} + \frac{1}{v^2} \frac{\partial}{\partial v} \left[\frac{1}{\tau_e} - \frac{1}{\tau_p} \frac{v^3 f_A(v, \theta, t)}{2} \right] \quad (61)$$

where τ_p and τ_e are particle and energy confinement times, respectively. If we ignore all other terms in Eq. (1) and compute moments, we find

$$\frac{\partial n_A}{\partial t} = - \frac{n_A}{\tau_p} \quad (62)$$

$$\frac{\partial (n_A \bar{\epsilon}_A)}{\partial t} = - \frac{n_A \bar{\epsilon}_A}{\tau_e} \quad (63)$$

In problems where one wants to observe the relaxation of a distribution in the absence of a loss cone, or where one assumes that ions in a loss cone domain are not lost instantly, full velocity space boundary conditions are applied, namely:

$$(a) \quad f(v=0, \theta) \text{ is independent of } \theta \quad (64)$$

$$(b) \quad \frac{\partial f}{\partial v}(v=0, 0 \leq \theta < 2\pi) = 0 \quad (65)$$

$$(c) \quad \frac{\partial f}{\partial \theta}(y, 0=0) = \frac{\partial f}{\partial \theta}(y, \theta=2\pi) = 0 \quad (66)$$

The first condition is a result of continuity at $v=0$. The second and third conditions are a result of the requirement that the distribution be azimuthally symmetric.

5. REFERENCES

1. J. Killeen and K. D. Mark, The Solution of the Fokker-Planck Equation for a Mirror-Confined Plasma, in Methods in Computational Physics (Academic Press, New York, 1968), Vol. 7, pp. 421-489.
2. A. H. Futch, Jr., J. F. Holdren, J. Killeen, and A. A. Mirin, Plasma Phys. 14, 211 (1972).
3. J. Killeen, A. A. Mirin, and M. E. Reink, The Solution of the Kinetic Equations for a Multi-Species Plasma, in Methods in Computational Physics (Academic Press, New York, 1974), Vol. 12, Chapter VI.
4. M. N. Rosenbluth, W. M. MacDonald, and D. L. Jassby, Phys. Rev. 107, 1 (1957).
5. L. Spitzer, Physics of Fully Ionized Gases, 2nd ed. (Wiley Interscience, New York, 1962).
6. R. D. Richtmyer and K. W. Morton, Difference Methods for Initial-Value Problems (Interscience-John Wiley, New York, 1967).
7. J. M. Dawson, H. P. Furth, and F. H. Tenney, Phys. Rev. Lett. 26, 1156 (1971).
8. H. P. Furth and D. L. Jassby, Phys. Rev. Lett. 32, 1176 (1974).

NOTES

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