

STABILIZATION OF SAWTOOTH OSCILLATION BY ISLAND HEATING

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ABSTRACT

Using the compressible resistive MHD equations in a finite aspect ratio cylinder, it is found that the $m = 1$ mode (the sawtooth oscillation) can saturate when the pressure inside the magnetic island is higher than that of the original core plasma. The saturation condition is of the form $\Delta s_p \geq 8 \epsilon_{q=1}^{-1} (1 - q_0)^2$. This saturation effect can be used to actively stabilize sawteeth by heating the island and/or by cooling the core plasma. This mechanism together with a stabilizing toroidal effect may also explain recent lower-hybrid-wave-driven tokamak experiments where the saturation of sawteeth has been observed.

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Sawtooth oscillation¹ in tokamaks degrades pressure confinement inside the safety factor $q = 1$ surface, and limits the central q_c to be close to unity. Suppression of sawteeth should give marked improvement in tokamak performance including better stability for $m \geq 2$ modes and better confinement times. However, the $m = 1$ mode which is responsible for the sawtooth crash has been found to be more difficult to stabilize than $m \geq 2$ modes.² Unlike $m \geq 2$ modes, which grow nonlinearly on a slow resistive time scale τ_η ,^{3,4} the nonlinear $m = 1$ mode (sawtooth crash) is driven by ideal free energy and grows on a much faster hybrid time scale $(\tau_\eta^{1/2} \tau_A^{1/2})$, where τ_A is the Alfvén time.⁴ The reason for this fast time scale is the fact that the island equilibrium for the $m = 1$ modes contains a singular current spike at the x-point as shown in Fig. 1.⁴ This should be contrasted with nonlinear $m \geq 2$ modes which go through a succession of regular equilibrium states.^{3,4}

Remembering that $m \geq 2$ modes are linearly stable to ideal modes, one may expect that if the $m = 1$ mode can be made stable to ideal linear modes, the nonlinear $m = 1$ mode may behave as nonlinear $m \geq 2$ modes, i.e., showing a slow nonlinear growth and saturation. This turns out to be the case as long as the linear stability is robust enough.⁵ Otherwise, the ideal driving free energy comes in nonlinearly even when linearly stable. From the equation for the ideal linear growth rate of the $m = 1$ mode,

$$\gamma = K \int_0^s \left\{ -2 \epsilon^2 r^2 \frac{\partial p}{\partial r} + \epsilon^2 r B_\theta^2 (3q + 1) (1 - q) \right\} dr, \quad (1)$$

where $r = s$ is the position of the $q = 1$ surface, one can see there are two ways to make the mode stable ($\gamma < 0$). One way is to have the q -profile rise inside the $q = 1$ surface as in reversed-field pinches. The other is to invert

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the pressure profile so that $P_{\text{center}} < P_{q=1}$. (Recently it was reported that when incompressible MHD codes were used, saturation of the $m = 1$ mode occurred.^{6,7} However, the incompressibility assumption generates an inverted pressure profile even when the initial pressure is zero in the calculation.⁸ This inverted pressure gives a saturation as discussed above. With the present compressible code with initial zero pressure, no saturation occurred.)

In this report, we generalize this stabilizing effect to include the magnetic island in nonlinear development. We find that pressure has the opposite effect on stability inside the island compared to the effect inside the initial core plasma, i.e., a peaked pressure gives stability while an inverted pressure gives instability. The total effect of pressure inside both the plasma core and the island can be approximated by ΔB_p where

$$\Delta B_p \equiv (P_I - P_c) / (B_{\theta, q=1}^2 / 2) .$$

Here P_I is the pressure at the center of the island and P_c is the pressure at the original magnetic axis. $\Delta B_p > 0$ gives stability. An example of a saturated $m = 1$ mode with $\Delta B_p = 0.25$ is shown in Fig. 2. Figure 2(a) and (b) show the pressure profile which is peaked inside the island. Figure 2(c) shows the flux ψ contours. Figure 2(d) shows the toroidal current density J_z profile along the midplane. Note that no current spike exists in the current profile, indicating a regular equilibrium state in contrast to the case shown in Fig. 1(b). The state had an initial q -profile of $q = q_0 [1 + (r/c)^2]$ with $q_0 = 0.95$, $r_{q=1} = 0.5$, and $\epsilon = 0.2$.

When we keep the pressure profile the same while reducing q_0 further, the state became unstable and went through a complete fast reconnection. From a series of such studies with different pressure profiles and $\epsilon_{q=1}$, we find the saturation condition between ΔB_p and q_0 as

$$\Delta s_p \geq 8 \epsilon_{q=1}^{-1} (\Delta q)^2, \quad (2)$$

where $\Delta q = 1 - q_0$ and $\epsilon_{q=1}$ is the inverse aspect ratio at the $q = 1$ surface.

The saturation condition, Eq. (2), can be used to actively stabilize sawteeth by heating the island and/or by cooling the original plasma core using pellet injection. In this scheme the condition (2) has to be satisfied continuously. This is possible because Δs_p only has to be increased as $\Delta q = 1 - q_0$ increases, which changes on a slow resistive time scale. The required Δs_p is in a practical range in high β tokamaks. For example, to stabilize down to $q_0 = 0.9$, $\Delta s_p = 0.8$ with $\epsilon_{q=1} = 0.1$ is required. This will give saturation until q_0 goes below 0.9.

The stabilization effect studied above can be also used to explain recent lower-hybrid-wave-driven tokamak experiments¹⁰ where saturation of sawteeth has been observed. Experimental ECE signals suggest that the island is heated effectively, and at an input power level where the saturation of sawteeth occurs, the island temperature reaches close to that of the peak temperature at the original axis. This will give $\Delta s_p = 0$ and hence no saturation from the condition (2). However, we have to take into account a toroidal stabilization effect which we neglected in our cylindrical model. If we assume that toroidal effects give saturation of the $m = 1$ mode up to $\Delta q = \delta$ in the absence of the island heating where δ is a small positive number, the island heating effect can be estimated to give saturation up to $\Delta q = \delta + (\epsilon_{q=1} \Delta s_{pI}/8)^{1/2} = \delta + 0.05$. Here $\Delta s_{pI} = 0.2$ and $\epsilon_{q=1} = 0.08$ is estimated from the experimental data. The sawtooth crash will be stabilized until $q_0 = 0.95 - \delta$ is reached. This time can be estimated as $\tau = \Delta q (T/\Delta T) (a_{q=1}^2 / \eta) \approx 100$ msec. Here the amplitude of the temperature oscillation $\Delta T/T = 0.2$ is used. This

can explain the saturation phenomena in PLT experiments. There is substantial uncertainty in the estimate of Δs_p . However, changing to $\Delta s_p = 0.05$ still gives a reasonable time scale of $\tau = 50$ msec.

The overall picture in this model is the following. As q_0 drops below one, the resistive mode is destabilized, but the ideal mode does not enter either linearly or nonlinearly until q_0 reaches $1 - \delta$. During this time, an island will form on a slow resistive time scale and will be heated by lower hybrid wave. q_0 drops further while the island heating keeps the stability condition (2) continuously satisfied until $q_0 = 0.95 - \delta$ is reached. One factor which may help the preferential heating of the island is the fact that the shear inside the island is usually lower than that of the main plasma core. This makes it harder to destroy good flux surfaces inside the island compared to the main plasma core. The toroidal effect we assumed here is far from certain. The curvature of the magnetic field, which determines the stability character of a given pressure profile, is quite different in a torus compared to a cylinder. In a complicated geometry of the nonlinear phase, how the toroidicity affects stability is not clearly known. This question will be studied using a three-dimensional code.

The above model does not completely explain the total elimination of the $m = 1$ mode found in the PLT lower hybrid wave experiments with even higher wave power. However, whether the $q = 1$ surface actually lies inside the plasma in this case is not clearly answered in the experiment. In our study, we have also neglected the fact that lower hybrid waves also drive plasma current such that the usual Ohm's law may have to be changed significantly and that a large portion of the plasma current is due to runaway electrons.

In the above study we have used the MH2D code which solves compressible helical MHD equations in the finite aspect ratio cylinder. The

compressibility is added into the incompressible 1MH2D code.^{4,10} (The reduced two-dimensional tokamak equations¹¹ which approximate a tokamak as an infinite aspect ratio cylinder are not applicable to the present case because these equations do not include compressibility and pressure effects.) The equations we use are described in the following.

In helical symmetry, all variables are functions of (r, ϕ) where the helical angle $\phi = \theta + \alpha z$ with helicity α and with the usual cylindrical coordinates (r, θ, z) . We use basis vectors $(\hat{r}, \hat{\phi}, \hat{e})$ where $\hat{r} = \nabla r$, $\hat{\phi} = \nabla \phi / |\nabla \phi|$, and $\hat{e} = \hat{r} \times \hat{\phi}$. Then, the magnetic field and the velocity can be represented as

$$\vec{B} = g \nabla \psi \times \hat{e} + B_e \hat{e} \quad ,$$

$$\vec{V} = g \nabla U \times \hat{e} + V_e \hat{e} + \nabla \chi \quad ,$$

where $g \equiv (1 + \alpha^2 r^2)^{-1/2}$.

The helical compressible MHD equations with a scalar resistivity η are (in rationalized emu units)

$$\frac{d\psi}{dt} = - \frac{\eta J_e}{g} \quad ,$$

$$\left(\frac{d}{dt}\right)(\Delta^{\dagger} U) = -\vec{B} \cdot \nabla (g \vec{j}_e) + g W_e \nabla^2 \chi + \alpha^2 g^2 \left[\frac{\partial (V_e^2 - B_e^2)}{\partial \phi} \right] - 2\alpha \vec{V} \cdot \nabla (g^3 V_e) \quad ,$$

$$\left(\frac{d}{dt}\right)(g B_e) = \vec{B} \cdot \nabla (g V_e) - g B_e \nabla^2 \chi + 2\alpha g^4 \vec{V} \cdot \nabla \psi + \left\{ \nabla \cdot \left[g^2 \eta \nabla \left(\frac{B_e}{g} \right) \right] + \eta (2\alpha g^3) J_e \right\} \quad ,$$

$$\left(\frac{d}{dt}\right)\left(\frac{V_e}{g}\right) = \vec{B} \cdot \nabla \left(\frac{B_e}{g}\right) \quad , \quad (3)$$

$$\frac{\partial v^2 \chi}{\partial t} + \frac{1}{2} v^2 (g^2 \nabla u \cdot \nabla u + v_e^2 + 2 \nabla \chi \times g \nabla u \cdot \hat{e} + \nabla \chi \cdot \nabla \chi)$$

$$+ \nabla \chi \times g \nabla \left(\frac{w_e}{g} \right) \cdot \hat{e}$$

$$= - \nabla \cdot (g w_e \nabla u - g v_e \nabla \left(\frac{v_e}{g} \right))$$

$$+ \nabla \cdot (g J_e \nabla \psi - g B_e \nabla \left(\frac{B}{g} \right)) - v^2 p \quad ,$$

$$\frac{dp}{dt} = - \gamma p \nabla^2 \chi + \nabla \cdot [\kappa \cdot \nabla p] + S_p \quad .$$

Here,

$$\nabla f = \left(\frac{\partial f}{\partial r} \right) \nabla r + \left(\frac{\partial f}{\partial \phi} \right) \nabla \phi = \left(\frac{\partial f}{\partial r} \right) \hat{r} + \left(\frac{1}{r g} \right) \left(\frac{\partial f}{\partial \phi} \right) \hat{\phi} \quad ,$$

$$\Delta^\dagger f \equiv \nabla \cdot (g^2 \nabla f) = \left(\frac{1}{r} \right) \left[\left(\frac{\partial}{\partial r} \right) \left(\frac{r g^2 \partial f}{\partial r} \right) \right] + \left(\frac{1}{r^2} \right) \left(\frac{\partial^2 f}{\partial \phi^2} \right) \quad ,$$

$$J_e = -(\Delta^\dagger \psi / g + 2 \alpha g^2 B_e), \quad w_e = -(\Delta^\dagger U / g + 2 \alpha g^2 v_e), \quad \vec{\nabla} \cdot \nabla f = (\nabla f \times g \nabla U) \cdot \hat{e} + \nabla \chi \cdot \nabla f \quad ,$$

$$\vec{B} \cdot \nabla f = (\nabla f \times g \nabla \psi) \cdot \hat{e} \quad ,$$

and

$$d/dt = \partial/\partial t + V \cdot \nabla.$$

In the above equations, we assumed an appropriate density source S_p in the density equation (i.e., $\partial \rho / \partial t = - \text{div} (\rho \vec{V}) + S_p$) such that $\rho = 1$ always. Such

a density source will somewhat change the time scales of local phenomena, but not the overall physics. This approximation significantly reduces the complexity of the equations and also greatly enhances the numerical accuracy of the calculation. The heat conduction term is not solved by a direct method because the large κ_{\parallel} ($\kappa_{\parallel} \gg \kappa_{\perp}$) causes a large numerical error. Instead this term is solved using the artificial parallel velocity method described in Ref. 12. This gives the $B \cdot \nabla p = 0$ condition in an efficient way. By setting $\chi \equiv 0$ in the above equations, the incompressible helical MHD equations^{4,10} can be obtained.

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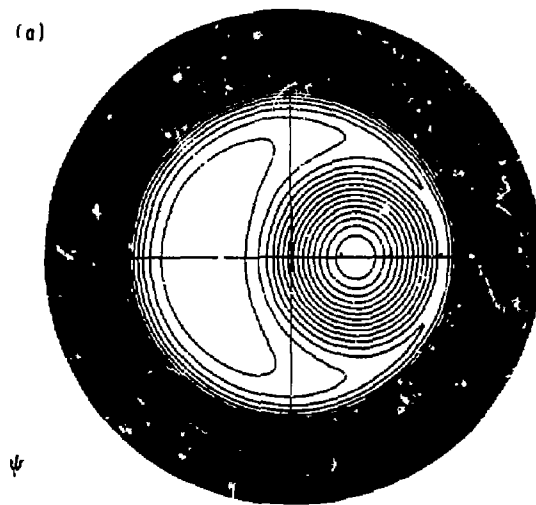
FIGURE CAPTIONS

Fig. 1 Plasma profiles during a fast reconnection, (a) helical flux contours, and (b) toroidal current profile along the midplane. At the x-point, $J_z \rightarrow \infty$ as $\eta \rightarrow 0$.

Fig. 2 A saturated state with $\Delta\beta_p = 0.25$. (a) and (b) show the pressure profile which is peaked inside the island. (c) is the helical flux contours and (d) the toroidal current profile along the midplane. Note that no current spike exists in the current profile.

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(a)



ψ

(b)

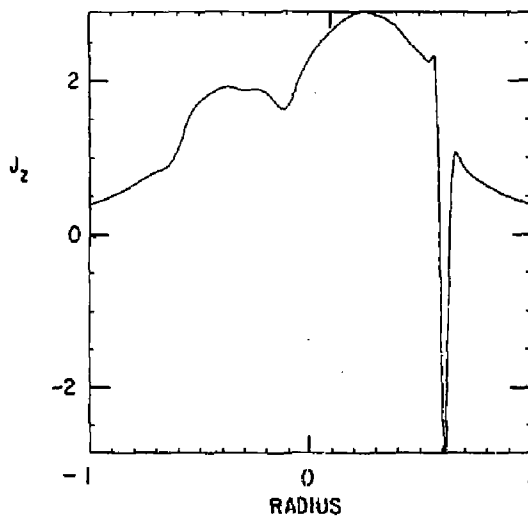


Fig. 1

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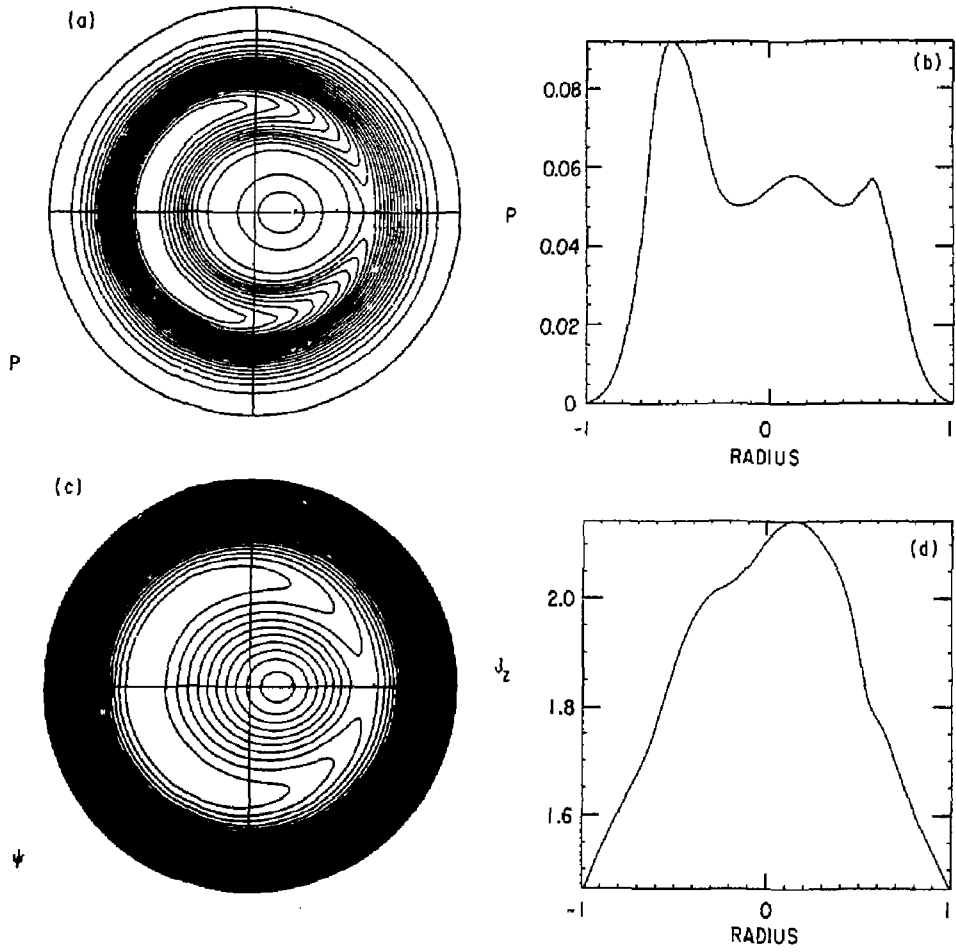


Fig. 2

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