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**MUXS: A CODE TO GENERATE MULTIGROUP CROSS SECTIONS FOR SPUTTERING CALCULATIONS**

T. J. Hoffman, M. T. Robinson,<sup>\*</sup> and H. L. Dodds, Jr.<sup>\*\*</sup>

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**MASTER**

COMPUTER SCIENCES  
 at  
 Oak Ridge National Laboratory  
 Post Office Box X  
 Oak Ridge, TN 37830

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<sup>\*</sup> Solid State Division, Oak Ridge National Laboratory.

<sup>\*\*</sup> Department of Nuclear Engineering, University of Tennessee, Knoxville, TN.

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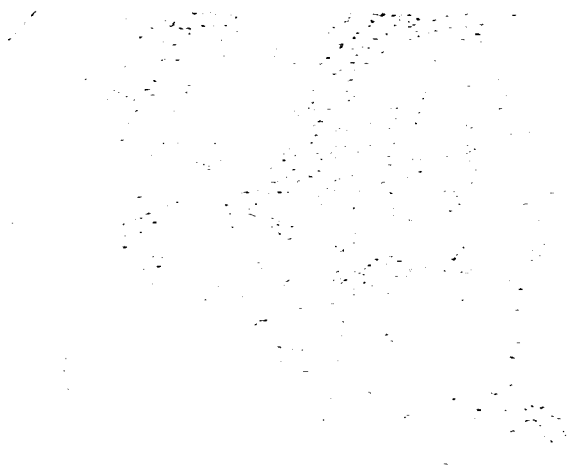
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## ABSTRACT

This report documents MUXS, a computer code to generate multigroup cross sections for charged particle transport problems. Cross sections generated by MUXS can be used in many multigroup transport codes, with minor modifications to these codes, to calculate sputtering yields, reflection coefficients, penetration distances, etc.

## I. INTRODUCTION

Over the past few years we have presented several papers<sup>1-5</sup> on the application of neutral-particle, multigroup methods to the analysis of charged particle transport problems. The purpose of this report is to document the computer code that was developed during that period to generate multigroup cross sections. For more detail on the problems that were studied, the approach taken to these problems, and the results of our calculations, the reader is referred to the references.

Charged particle transport differs considerably from that for neutral particles. Unlike the nuclear forces that determine the directional changes of neutrons, the Coulomb forces that affect the paths of charged particles are extremely long range. This phenomenon leads to essentially continuous interactions between an ion and its environment of electrons and nuclei. Treatment of the many small deflections of the ion using a Legendre expansion of the differential scattering cross section, as is done for multigroup neutral particle transport, is simply not feasible; too many terms in the series would be required. The approach we have taken, and that used by others as well, is to account for the energy lost by the ion when deflected through small angles with a continuous slowing down term. This approach ignores the directional change due to these interactions. All electronic interactions with the ion are included in this term. Interactions with the nuclei that result in a scattering angle that is less than a prescribed angle  $\theta_n$  are also treated as continuous interactions.

Scatterings through angles larger than  $\theta_n$  are termed "discrete interactions" and are included in the evaluation of the multigroup total and scattering cross sections.

Continuous interactions lead to a term in the Boltzmann equation that is not present in the transport of neutral particles. Therefore, in addition to the use of MUXS, one must modify the transport code in order to perform charged particle calculations. For this reason, the modifications we made to ANISN<sup>6</sup> for the analysis of sputtering problems are described in Appendix B of this report.

The codes MUXS and ANISN can be obtained from:

Radiation Shielding Information Center  
Oak Ridge National Laboratory  
Building 6025  
P. O. Box X  
Oak Ridge, TN 37830.

## II. MULTIGROUP PARAMETERS CALCULATED BY MUXS

As shown in Reference 1, the multigroup formulation of the sputtering problem can be written as follows:

$$\begin{aligned} \mu \frac{\partial \phi_G(x, \mu)}{\partial x} + \left( \Sigma_G^T - \Sigma_G^{CSD} \right) \phi_G(x, \mu) \\ = Q_G(x, \mu) + \Sigma_{G-1}^{CSD} \phi_{G-1}(x, \mu) \\ + \sum_{G'=1}^G \int_{-1}^1 \Sigma_{G' \rightarrow G}^S(\mu' \rightarrow \mu) \phi_{G'}(x, \mu') d\mu' \end{aligned} \quad (1)$$

for  $G = 1, 2, \dots, \text{NTOT}$ .

The first NI energy groups represent transport of the ions; the remaining NT=NTOT-NI are target atom energy groups.

The computer code MUXS generates the multigroup parameters  $\Sigma_G^T$ ,  $\Sigma_G^{CSD}$ , and the Legendre coefficients of  $\Sigma_{G' \rightarrow G}^S$ . The actual solution to Eq. 1 is obtained with a modified version of ANISN that is discussed in Appendix B.

In the development of the multigroup equation, the flux is assumed separable within each energy group, i.e.,

$$\phi(x, E, \mu) = \phi_G(x, \mu) W_G(E) \text{ for } E \in (E_g, E_{g-1}) \quad (2)$$

With this assumption, the following definitions for the multigroup cross sections are obtained:

$$\Sigma_G^T = \frac{N \int_{E_g}^{E_{g-1}} \sigma_t(E) W_G(E) dE}{\int_{E_g}^{E_{g-1}} W_G(E) dE}, \quad (3)$$

$$\Sigma_G^{CSD} = \frac{S(E_g) W_G(E_g)}{\int_{E_g}^{E_{g-1}} W_G(E) dE}, \quad (4)$$

and

$$\Sigma_{G \rightarrow H}^S(\mu) = \frac{N \int_{E_g}^{E_{g-1}} W_G(E) \sigma[E \rightarrow (E_h, E_{h-1}), \mu] dE}{\int_{E_g}^{E_{g-1}} W_G(E) dE}, \quad (5)$$

where

$N$  = target atom number density.

The functions  $\sigma_t(E)$ ,  $S(E)$ ,  $\sigma[E \rightarrow (E_h, E_{h-1}), \mu]$ , and  $W_G(E)$  and their evaluation by MUXS, are described in the following sections.

a. The Point-Energy Total Cross Section

The point-energy total cross section,  $\sigma_t(E)$  in Eq. 3, is obtained by integrating the differential cross section over all recoil particle energies that correspond to discrete interactions, i.e.,

$$\sigma_t(E) = \int_{T=\gamma_1 E}^{\gamma_2 E} d\sigma(E, T), \quad (6)$$

where

$d\sigma(E,T)$  = differential cross section for the elastic scattering of an incident particle of energy  $E$ , producing a recoiling target atom with energy  $T$ ,

$$\gamma_1 = \frac{\text{minimum recoil atom energy of a discrete interaction}}{\text{incident particle energy}},$$

$$= \frac{2m_1 m_2}{(m_1 + m_2)^2} \left\{ 1 + \frac{m_1}{m_2} \sin^2 \theta_n - \cos \theta_n \left[ 1 - \left( \frac{m_1}{m_2} \right)^2 \sin^2 \theta_n \right]^{1/2} \right\}, \quad (7)$$

$m_1$  = mass of the incident particle,

$m_2$  = mass of the recoil atom,

$\theta_n$  = minimum scattering angle for a discrete interaction,

and

$$\begin{aligned} \gamma_2 &= \frac{\text{maximum recoil atom energy}}{\text{incident particle energy}}, \\ &= \frac{4m_1 m_2}{(m_1 + m_2)^2}. \end{aligned} \quad (8)$$

Equations 7 and 8 are developed in reference 1.

#### b. The Stopping Cross Section

The stopping cross section,  $S(E)$  in Eq. 4, is the sum of the stopping cross section for electronic interactions and that for elastic

interactions in which the incident particle scatters through an angle less than  $\theta_n$ , i.e.,

$$S(E) = S_e(E) + N \int_{T=0}^{\gamma_1 E} T d\sigma(E, T). \quad (9)$$

The stopping cross section for electronic interactions is calculated with the following formula from Lindhard and Scharff.<sup>7</sup>

$$S_e(E) = kN \left( \frac{Z_1 Z_2 e^2}{a_{12}} \right)^{1/2} (\pi a_{12}^2) \left( \frac{4m_1}{m_1 + m_2} \right) \left( \frac{m_2}{m_1 + m_2} \right)^{1/2} E^{1/2}, \quad (10)$$

where

$$k = \frac{32}{3\pi} \left( \frac{m_e}{m_2} \right)^{1/2} \left( 1 + \frac{m_2}{m_1} \right)^{3/2} \frac{Z_1^{2/3} Z_2^{1/2}}{(Z_1^{2/3} + Z_2^{2/3})^{3/4}}, \quad (11)$$

$$a_{12} = \left( \frac{9\pi^2}{128} \right)^{1/3} a_0 \left[ Z_1^{2/3} + Z_2^{2/3} \right]^{-1/2} \quad (12)$$

$a_0 = 0.529 \text{ \AA}$ , the Bohr radius,

$m_e, e =$  mass in amu, charge of an electron,

$m_1, Z_1 =$  mass in amu, atomic number of the incident particle,

$m_2, Z_2 =$  mass in amu, atomic number of the recoil atom.

### c. Calculation of the Legendre Coefficients

In Eq. 5,  $\sigma[E \rightarrow E_h, E_{h-1}, \dots]$  represents the cross section for discrete interactions in which the incident particle of energy  $E$  scatters into

group H, i.e.,  $(E_h, E_{h-1})$ .  $\mu$  is the cosine of the scattering angle (laboratory). This cross section is expressed as a finite series of Legendre polynomials,  $P_\ell(\mu)$ , as follows:

$$\sigma[E \rightarrow (E_h, E_{h-1}), \mu] = \sum_{\ell=0}^{NCOEF-1} \sigma_{E \rightarrow IH}^{\ell} P_{\ell}(\mu), \quad (13)$$

where

$$\sigma_{E \rightarrow IH}^{\ell} = \frac{2\ell+1}{2} \int_{TMIN}^{TMAX} P_{\ell}(\mu) d\sigma(E, T) \quad (14)$$

For scatter from one ion group to another, this expression is

$$\sigma_{E \rightarrow IH}^{\ell} = \frac{2\ell+1}{2} \int_{\text{Max}(E-E_{h-1}, \gamma_1 E)}^{\text{Min}(E-E_h, \gamma_2 E)} P_{\ell}(\mu) d\sigma(E, T), \text{ for } IH \leq NI, \quad (15)$$

where

$$\mu = \left(1 - \frac{T}{E}\right)^{1/2} + \frac{1}{2} \left(1 - \frac{m_2}{m_1}\right) \left(\frac{T}{E}\right) \left(1 - \frac{T}{E}\right)^{-1/2} \quad (16)$$

The production of energetic target atoms as recoil atoms from ion scatterings is treated in a manner similar to the production of secondary gamma rays in neutron capture or inelastic scattering

reactions. However, unlike these neutron reactions, the recoil atom production is a highly anisotropic process. This anisotropy can be accounted for by treating these interactions in much the same manner one would treat the anisotropy of the emerging ion, i.e., with a Legendre expansion of the cosine of the angle between the incident particle direction and the emergent particle (recoil atom) direction. In the multigroup transport code, this process is treated as a "scatter" from an ion energy group into a target atom energy group. Therefore, transfer from an ion group into a target atom group is represented by the following Legendre coefficients:

$$\sigma_{E \rightarrow IH}^{\ell} = \frac{2\ell+1}{2} \int_{\text{Max}(E_{h-1}, \gamma_1 E)}^{\text{Min}(E_h, \gamma_2 E)} P_{\ell}(\eta) d\sigma(E, T), \text{ for } IH > NI, \quad (17)$$

where

$$\eta = (T/\gamma_2 E)^{\frac{1}{2}}. \quad (18)$$

Equations 16 and 18 are obtained from the conservation of energy and of momentum.

For interactions between a target atom with energy  $E$  and a stationary target atom, either or both can emerge in energy group  $IH$ .

Therefore, the following expression is used to evaluate the Legendre coefficients for target atom interactions:

$$\sigma_{E \rightarrow IH}^{\ell} = \frac{2\ell+1}{2} \int_{\text{Max}(E-E_{h-1}, \gamma_1 E)}^{\text{Min}(E-E_h, E)} P_{\ell}(\mu) d\sigma(E, T) + \frac{2\ell+1}{2} \int_{\text{Max}(E_{h-1}, \gamma_1 E)}^{\text{Min}(E_h, E)} P_{\ell}(\eta) d\sigma(E, T), \quad (19)$$

where

$$\mu = \left(1 - \frac{T}{E}\right)^{1/2}, \quad (20)$$

and

$$\eta = \left(\frac{T}{E}\right)^{1/2}. \quad (21)$$

#### d. Evaluation of the Weighting Function

Within each energy group, the energy-dependent particle flux is assumed to have the following functional form

$$\phi(E) = C_G E^{-XI_G} \text{ for } E_g < E < E_{g-1}. \quad (22)$$

In MUXS, the group flux,  $\phi_G$ , is assumed to be equal to  $\phi(E)$  at the center of the energy interval, i.e.,

$$\phi\left(\frac{E_g + E_{g-1}}{2}\right) = \frac{\phi_G}{E_{g-1} - E_g}. \quad (23)$$

It is also required that the energy dependent flux be continuous at the group boundary. This requirement is essential in order to conserve particles. Therefore, we require

$$C_G E_g^{-X I_G} = C_{G+1} E_g^{-X I_{G+1}}. \quad (24)$$

Equations 23 and 24 result in  $2^{*}NTOT-1$  equations for  $2^{*}NTOT$  unknowns. The additional condition used is that  $X I_1 = X I_2$ . These requirements result in the following equations for the  $X I_G$ 's:

$$X I_1 = \frac{\ln \left[ \frac{\phi_2}{\phi_1} \frac{(E_0 - E_1)}{(E_1 - E_2)} \right]}{\ln \left[ \frac{E_0 + E_1}{E_1 + E_2} \right]},$$

$$X I_G = \frac{X I_{G-1} \ln \left( \frac{E_{g-2} + E_{g-1}}{2E_{g-1}} \right) - \ln \left[ \frac{\phi_{G+1} (E_{g-2} - E_{g-1})}{\phi_G (E_{g-1} - E_g)} \right]}{\ln \left( \frac{E_{g-1} + E_g}{2E_{g-1}} \right)} \quad \text{for } G > 1. \quad (25)$$

Since the weighting function appears in both the numerator and denominator of the equations used by MUXS to evaluate the multigroup parameters, Eqs. 3-5, only  $X I_G$  is needed, i.e.,

$$W_G(E) \sim E^{-X I_G} \quad (26)$$

### III. CALCULATIONAL ALGORITHM IN MUXS

The generation of the multigroup cross sections consists of the following steps:

1. The point-energy total cross section,  $\sigma_t(E)$  of Eq. 3, and the  $P_0$  Legendre coefficient of the differential scattering cross section  $\sigma[E \rightarrow E_h, E_{h-1}]$  of Eq. 5, are calculated at energies corresponding to the abscissa of a Gauss-Legendre quadrature set. The stopping cross section,  $S(E)$  of Eq. 4, is evaluated at the group boundaries. These cross sections are obtained at energy  $E$  by calling the following subroutines.

- a. Subroutine TSIGMA. This routine sets up a table of the differential scattering cross section,  $DSIG(E,T)$ , as a function of  $T$ , the energy transferred to the recoiling target atom. The table is based on the approximation:

$$DSIG(T)/DSIG(TM) = (TM/T)^N,$$

where  $TM$  is the maximum possible transferred energy. The tables contain values of  $\ln(TM/T)$  and of  $N$ . The values of  $DSIG$  are retrieved by the function  $DSIG(T)$ .

- b. Subroutine QUANC8. This routine integrates over T to determine the point cross sections using an adaptive quadrature. The adaptive quadrature ensures adequate accuracy in this precision-sensitive phase of the calculation.
2. The multigroup cross sections, SIG(G), are obtained from the point-energy cross sections, PSIG(E), using the following iterative procedure:
- a. An initial guess at the (infinite medium) group fluxes, PHIO(G), is made.
  - b. Using PHIO(G), the energy-dependent flux, Eq. 22, is obtained

$$PHE(E) = C(G) * E^{*+}(-XI(G)),$$

where C(G) and XI(G) are the group dependent parameters described in the previous section.

- c. The point cross sections are weighted by PHE(E) to obtain estimates of the multigroup cross sections, i.e.,

$$SIG(G) = \frac{\text{INTEGRAL OVER GROUP G OF PSIG(E)*PHE(E)}}{\text{INTEGRAL OVER GROUP G OF PHE(E)}}$$

The integral in the numerator is obtained using a Gauss-Legendre quadrature; the PSIG(E)'s were evaluated at the abscissas for this reason. The denominator is calculated analytically.

- d. With the estimated group cross sections, the infinite medium group fluxes,  $\Phi(G)$ , are calculated - see Reference 1.
- e. The fractional change in the group flux, i.e.,  $\Phi(G)$  versus  $\Phi_{IO}(G)$ , is calculated. If this change is greater than 1% for any group,  $\Phi_{IO}$  is set to  $\Phi$  and MUXS returns to step b.

Note that this iterative procedure does not require reevaluation of the point-energy cross sections, a major time-consumer in MUXS.

5. The higher order Legendre coefficients for the multigroup scattering matrix, Eq. 5, are calculated.

4. An ANISN-formatted, binary cross section file for the multigroup cross section set is created. This file is suitable for input to many multigroup transport codes, e.g., ANISN,<sup>6</sup> DOT,<sup>8</sup> MORSE.<sup>9</sup> Or, alternatively, this file can be converted into an AMPX<sup>10</sup> working library by the computer code LAVA.<sup>11</sup>

#### IV. INPUT DESCRIPTION FOR MUXS

The input data requirements for MUXS are as follows:

1. Identification record: The first 48 characters of this record are printed on the output record to identify the calculations and are also passed to ANISN for identification of the cross section set.

2. The NAMELIST input record &DATA contains the remaining information required.

- NI The number of ion groups.
- NT The number of target atom groups. The total number of groups (NI + NT) must not exceed 50. NT can be set to zero for problems that do not require the transport of the target atoms, e.g., ion range calculations.
- NCOEF The number of Legendre coefficients (must not exceed 20).
- UO The minimum energy in eV that a target atom must have to be considered as sputtered. The cohesive energy is an appropriate choice.
- DENSE The density of the target in atoms per cubic angstrom (or per barn-cm).
- TH The minimum laboratory scattering angle for discrete interactions in degrees.
- EI The initial kinetic energy of the incident ion in eV.
- NEWS Controls the level of output from the program as follows:
- NEWS=0 (The default value) causes printing of the input data, the converged fluxes, and the 1D multigroup cross sections.
- NEWS=1 Causes the printing (in addition to the above) of the fluxes at each iteration.

**NEWS=2** Causes the printing (in addition to both of the above) of the multigroup scattering matrix (Legendre coefficients).

**NEWS=3** Causes the printing (in addition to all of the above) of all of the interpolation tables generated by Subroutine **TSIGMA**.

The following three variables are arrays of two quantities. The first element refers to the incident ion. The second to the target atoms:

**AMU** The mass of the particle in atomic mass units.

**Z** The atomic number of the particle.

**BPAR** The screening length for interactions of the particle with the target atoms in angstroms. If these parameters are omitted or entered as zero, the program will supply values using the Firsov formula.<sup>12</sup>

#### V. MUXS SAMPLE PROBLEM

As an example of a MUXS problem, the following data was input (unit 5) to obtain multigroup cross sections for an 8 keV proton incident on a nickel target:

```
SPUTTERING CROSS SECTIONS FOR H INCIDENT ON NI - 20GPS
&DATA NI = 10, NT = 10, NCOEF = 20, UO = 4.458, TH = 2.5,
DENSE = 0.0913, EI = 8000, Z = 1.0, 29.0, AMU = 1.0, 58.71,
BPAR = 0.0, 0.075, NEWS = 0, &END
```

The printed output is shown in Fig. 1. The cross sections are stored by MUXS on unit 4. Calculation of sputtering yields with the cross sections produced in this MUXS sample problem is described in Appendix B.

SPUTTERING CROSS SECTIONS FOR H=>NI - 20GPa

10 ION GROUPS                      10 TARGET ATOM GROUPS                      20 LEGENDRE COEFFICIENTS

MINIMUM SCATTERING ANGLE (DEGREES) 2.5000000

TARGET BINDING ENERGY (E. V.) 4.4580000                      TARGET DENSITY (/ANGSTROMS \*\* 3) .91300000E-01

INITIAL INCIDENT ION KINETIC ENERGY (E. V.) 8000.0000

INCIDENT ION ATOMIC NUMBER 1.0000000                      ATOMIC MASS 1.0000000                      SCREENING LENGTH (ANGSTROMS) .13746768

TARGET ATOM ATOMIC NUMBER 28.000000                      ATOMIC MASS 58.710000                      SCREENING LENGTH (ANGSTROMS) .75000000E-01

FLUXES AFTER ITERATION 9

IG	FLUX	IG	FLUX	IG	FLUX	IG	FLUX	IG	FLUX
1	166.46	2	165.65	3	164.66	4	163.37	5	161.71
6	159.68	7	156.79	8	152.69	9	147.35	10	138.79
11	1.7759	12	4.4386	13	7.1491	14	9.3275	15	11.271
16	12.854	17	14.235	18	15.416	19	16.459	20	17.377

GROUP 1	SIGT	.44731371E-01	SIGSD	.58527676E-02	S	84.864471
GROUP 2	SIGT	.53468846E-01	SIGSD	.58514439E-02	S	76.395035
GROUP 3	SIGT	.65245509E-01	SIGSD	.58472604E-02	S	67.921173
GROUP 4	SICT	.81591964E-01	SIGSD	.58410652E-02	S	59.446594
GROUP 5	SIGT	.10502923	SIGSD	.58346502E-02	S	50.971115
GROUP 6	SICT	.13982838	SIGSD	.58285855E-02	S	42.494751
GROUP 7	SIGT	.1935272	SIGSD	.58034956E-02	S	34.020813
GROUP 8	SICT	.28095156	SIGSD	.57893470E-02	S	25.540710

Figure 1. Printed Output from MUXS Sample Problem

GROUP 9	SIGT .43571001	SIGSD .57744682E-02	S 17.061432
GROUP 10	SIGT .76317233	SIGSD .	S 8.5829124
GROUP 11	SIGT .81756902	SIGSD .30628532E-01	S 32.021469
GROUP 12	SIGT 1.0808506	SIGSD .62245183E-01	S 21.323410
GROUP 13	SIGT 1.2865772	SIGSD .98601043E-01	S 15.975158
GROUP 14	SIGT 1.4859104	SIGSD .15019125	S 12.779972
GROUP 15	SIGT 1.6666307	SIGSD .20868659	S 10.648841
GROUP 16	SIGT 1.8444185	SIGSD .28026819	S 9.1262932
GROUP 17	SIGT 2.0193663	SIGSD .36119848	S 7.9843016
GROUP 18	SIGT 2.1964455	SIGSD .45370114	S 7.0960989
GROUP 19	SIGT 2.3763485	SIGSD .55654293	S 6.3855524
GROUP 20	SIGT 2.5608454	SIGSD .67018253	S 5.8042583

Figure 1 (contd.)

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## Appendix A

## Listing of MUXS Program

C		MAIN0001
C		MAIN0002
C		MAIN0003
C		MAIN0004
C		MAIN0005
C		MAIN0006
C		MAIN0007
C		MAIN0008
C		MAIN0009
C		MAIN0010
C		MAIN0011
C		MAIN0012
C		MAIN0013
C		MAIN0014
C		MAIN0015
C		MAIN0016
C		MAIN0017
C		MAIN0018
C		MAIN0019
C		MAIN0020
C		MAIN0021
C		MAIN0022
C		MAIN0023
C		MAIN0024
C		MAIN0025
C		MAIN0026
C		MAIN0027
C		MAIN0028
C		MAIN0029
C		MAIN0030
C		MAIN0031
C		MAIN0032
C		MAIN0033
C		MAIN0034
C		MAIN0035
C		MAIN0036
C		MAIN0037
C		MAIN0038
C		MAIN0039
C		MAIN0040
C		MAIN0041
C		MAIN0042
C		MAIN0043
C		MAIN0044
C		MAIN0045
C		MAIN0046
C		MAIN0047
C		MAIN0048
C		MAIN0049
C		MAIN0050
C		MAIN0051
C		MAIN0052
C		MAIN0053
C		MAIN0054
C		MAIN0055

**'MUXS', A PROCEDURE FOR THE GENERATION OF  
MULTIGROUP CROSS SECTIONS FOR SPUTTERING CALCULATIONS  
USING THE MOLIERE APPROXIMATION TO THE THOMAS-FERMI POTENTIAL  
TO DESCRIBE THE SCATTERING OF PROJECTILES AND  
THE LSS ELECTRONIC STOPPING CROSS SECTION**

**REFERENCE:**

**T. J. HOFFMAN, M. T. ROBINSON, AND H. L. DODDS, JR.,  
MUXS: A CODE TO GENERATE MULTIGROUP CROSS SECTIONS FOR  
SPUTTERING CALCULATIONS, ORNL/CSD/TM-185, OAK RIDGE  
NATIONAL LABORATORY (1982).**

**INPUT DATA REQUIREMENTS (DATA SET REFERENCE NUMBER 5):**

- IDENTIFICATION RECORD: THE FIRST 48 BYTES OF THIS RECORD ARE  
PRINTED ON THE OUTPUT RECORD TO IDENTIFY THE CALCULATIONS AND  
ARE ALSO PASSED TO 'ANISN' FOR THE SAME PURPOSE.**
- THE 'NAMELIST' INPUT RECORD '&DATA' CONTAINS THE REMAINING  
INFORMATION REQUIRED:**

NI	THE NUMBER OF ION GROUPS	
NT	THE NUMBER OF TARGET ATOM GROUPS. THE TOTAL NUMBER OF GROUPS (NI + NT) MUST NOT EXCEED 50.	
NCOEF	THE NUMBER OF LEGENDRE COEFFICIENTS. MUST NOT EXCEED 20.	
UO	THE MINIMUM ENERGY THAT A TARGET ATOM MUST HAVE TO BE CONSIDERED AS SPUTTERED. THE COHESIVE ENERGY IS AN APPROPRIATE CHOICE. THE VALUE MUST BE IN E. V.	
DENSE	THE DENSITY OF THE TARGET IN ATOMS PER CUBIC ANGSTROM (OR PER BARN-CM).	
TH	THE MINIMUM LABORATORY SCATTERING ANGLE FOR DISCRETE ATOMIC INTERACTIONS.	
EI	THE INITIAL KINETIC ENERGY OF THE INCIDENT ION IN E. V.	
NEWS	CONTROLS THE LEVEL OF OUTPUT FROM THE PROGRAM, USING THE CODE:	
	NEWS = 0 (THE DEFAULT VALUE) CAUSES PRINTING OF THE INPUT DATA, THE CONVERGED FLUXES, AND THE 1D MULTIGROUP CROSS SECTIONS ONLY.	

## Appendix A (contd.)

C		MAIN0056
C	NEWS = 1 CAUSES THE PRINTING IN ADDITION OF THE FLUXES	MAIN0057
C	AT EACH ITERATION.	MAIN0058
C		MAIN0059
C	NEWS = 2 CAUSES THE PRINTING (IN ADDITION TO BOTH OF	MAIN0060
C	THE ABOVE) OF THE MULTIGROUP TRANSFER MATRIX	MAIN0061
C		MAIN0062
C	NEWS = 3 CAUSES THE PRINTING (IN ADDITION TO ALL OF THE	MAIN0063
C	ABOVE) OF ALL OF THE INTERPOLATION TABLES	MAIN0064
C	GENERATED BY 'TSIG'.	MAIN0065
C		MAIN0066
C	THE FOLLOWING THREE VARIABLES ARE ARRAYS OF TWO QUANTITIES. THE	MAIN0067
C	FIRST ELEMENT REFERS TO THE INCIDENT ION, THE SECOND TO THE TARGET	MAIN0068
C	ATOMS:	MAIN0069
C		MAIN0070
C	AMU THE MASS OF THE PARTICLE IN ATOMIC MASS UNITS.	MAIN0071
C		MAIN0072
C	Z THE ATOMIC NUMBER OF THE PARTICLE.	MAIN0073
C		MAIN0074
C	BPAR THE SCREENING LENGTH FOR INTERACTIONS OF THE PARTICLE	MAIN0075
C	WITH THE TARGET ATOMS, IN ANGSTROMS. IF THESE PARAMET-	MAIN0076
C	ERS ARE OMITTED OR ENTERED AS ZERO, THE PROGRAM WILL	MAIN0077
C	SUPPLY VALUES USING THE FIRSOV FORMULA.	MAIN0078
C		MAIN0079
C		MAIN0080
C	OUTPUT DATA SETS:	MAIN0081
C		MAIN0082
C	1. THE PRINTED OUTPUT IS DIRECTED TO THE STANDARD OUTPUT DATA	MAIN0083
C	SET ('FT06F001' IN IBM SYSTEMS).	MAIN0084
C		MAIN0085
C	2. DATA SET REFERENCE NUMBER 4 IS USED TO STORE THE 'ANISN'-	MAIN0086
C	ORIENTED MULTIGROUP CROSS SECTIONS IN UNFORMATTED FORM. IT	MAIN0087
C	IS ALSO USED FOR TEMPORARY STORAGE OF THE LEGENDRE COEFF-	MAIN0088
C	ICIENTS.	MAIN0089
C		MAIN0090
C		MAIN0091
C	DESCRIPTION OF THE COMMON BLOCKS. EXCEPT AS NOTED, ALL REAL	MAIN0092
C	VARIABLES ARE 'REAL*8'.	MAIN0093
C		MAIN0094
C	1. /PDAT/NI,NT,NCOEF,ION,DENSE,EI,UO,APQ(2),QGAM(2),RGAM(2),	MAIN0095
C	SGAM(2),GAMMA(2),TLOW(2),TLOG(2),APAR(2),BPAR(2),	MAIN0096
C	CPAR(2),ESTOP(2),NEWS,NTOT	MAIN0097
C		MAIN0098
C	ION USED TO INDICATE THE CURRENT PROJECTILE ( = 1 FOR THE	MAIN0099
C	INCIDENT ION, = 2 FOR THE TARGET ATOM).	MAIN0100
C		MAIN0101
C	APQ THESE FIVE ARRAYS CONTAIN VARIOUS FUNCTIONS OF THE	MAIN0102
C	QGAM MASSES OF THE TWO PARTICLES. EACH ARRAY CONTAINS TWO	MAIN0103
C	RGAM VALUES, ONE FOR EACH PARTICLE AS PROJECTILE.	MAIN0104
C	SGAM	MAIN0105
C	GAMMA	MAIN0106

## Appendix A (contd.)

C			MAIN0107
C	TLOW	THESE TWO ARRAYS DESCRIBE THE MINIMUM VALUES OF THE	MAIN0108
C	TLOG	PROJECTILE KINETIC ENERGIES FOR WHICH DISCRETE INTER-	MAIN0109
C		ACTIONS ARE USED, ONE VALUE FOR EACH PROJECTILE.	MAIN0110
C			MAIN0111
C	APAR	MOLIERE POTENTIAL PARAMETERS, ONE VALUE FOR EACH	MAIN0112
C	CPAR	PROJECTILE.	MAIN0113
C			MAIN0114
C	ESTOP	THE PARAMETERS OF THE LSS INELASTIC ENERGY LOSS MODEL.	MAIN0115
C			MAIN0116
C	NTOT	NI + NT, THE TOTAL NUMBER OF ENERGY GROUPS.	MAIN0117
C			MAIN0118
C			MAIN0119
C	2. /WATE/U(4),W(4),AB(10),WT1(10),INP,MEHL		MAIN0120
C			MAIN0121
C	U, W	THE ABSCISSAS AND WEIGHTS FOR THE GAUSS-MEHLER QUADRAT-	MAIN0122
C		URE USED TO EVALUATE THE CLASSICAL SCATTERING INTEGRALS	MAIN0123
C		IN THE SUBROUTINE 'TSIGMA'.	MAIN0124
C			MAIN0125
C	AB, WT1	THE ABSCISSAS AND WEIGHTS FOR THE GAUSS-LEGENDRE QUAD-	MAIN0126
C		RATURE USED TO EVALUATE THE POINT-ENERGY LEGENDRE	MAIN0127
C		COEFFICIENTS IN THE SUBROUTINE 'LEGEND' AND FOR	MAIN0128
C		INTEGRATIONS OVER ENERGY IN THE SUBROUTINE 'CROSSX'.	MAIN0129
C			MAIN0130
C	INP	THE NUMBER OF POINTS IN THE GAUSS-LEGENDRE SET.	MAIN0131
C			MAIN0132
C	MEHL	THE NUMBER OF POINTS IN THE GAUSS-MEHLER SET.	MAIN0133
C			MAIN0134
C			MAIN0135
C	3. /SIGX/EBI(51),EBT(51),S(50),SIGT(50),SIGSD(50),SIGS(50,50,20)		MAIN0136
C			MAIN0137
C	EBI	ENERGY GROUP BOUNDARIES FOR THE ION GROUPS.	MAIN0138
C			MAIN0139
C	EBT	ENERGY GROUP BOUNDARIES FOR THE TARGET ATOM GROUPS.	MAIN0140
C			MAIN0141
C	S	STOPPING CROSS SECTION AT THE GROUP BOUNDARIES FOR THE	MAIN0142
C		CONTINUOUS INTERACTIONS (REAL*4).	MAIN0143
C			MAIN0144
C	SIGT	TOTAL GROUP CROSS SECTION FOR DISCRETE INTERACTIONS	MAIN0145
C		(REAL*4).	MAIN0146
C			MAIN0147
C	SIGSD	CONTINUOUS SLOWING DOWN GROUP CROSS SECTION (REAL*4).	MAIN0148
C			MAIN0149
C	SIGS	GROUP SCATTERING CROSS SECTION MATRIX FOR DISCRETE	MAIN0150
C		INTERACTIONS (REAL*4).	MAIN0151
C			MAIN0152
C			MAIN0153
C	4. /TABL/TMX,SIG0,KM,KQ,TE(200),SIG(200)		MAIN0154
C			MAIN0155
C	TMX	THE RECIPROCAL OF THE MAXIMUM POSSIBLE TRANSFERRED	MAIN0156
C		ENERGY, TM.	MAIN0157
C			MAIN0158

## Appendix A (contd.)

C	SIG0	THE DIFFERENTIAL CROSS SECTION FOR TRANSFERRING 'TM'.	MAIN0159
C			MAIN0160
C	KM	THE NUMBER OF ENTRIES IN THE INTERPOLATION TABLES.	MAIN0161
C			MAIN0162
C	KQ	KM - 1.	MAIN0163
C			MAIN0164
C	TE	LN( TM / T ) AT THE TABULAR POINTS, WHERE T IS THE	MAIN0165
C		TRANSFERRED ENERGY.	MAIN0166
C			MAIN0167
C	SIG	LN( SIGMA / SIG0 ) / LN( TM / T ), AT THE TABULAR	MAIN0168
C		POINTS, WHERE SIGMA IS THE DIFFERENTIAL CROSS SECTION	MAIN0169
C		FOR TRANSFERRING T.	MAIN0170
C			MAIN0171
C			MAIN0172
C	ERROR TERMINATIONS:		MAIN0173
C			MAIN0174
C	THE PROGRAM ALWAYS TERMINATES WITH 'STOP N', WHERE THE VALUE OF		MAIN0175
C	'N' IDENTIFIES THE TERMINAL CONDITION AS FOLLOWS:		MAIN0176
C			MAIN0177
C	N = 0	NORMAL TERMINATION AT THE END OF THE PROGRAM.	MAIN0178
C			MAIN0179
C	N = 8	STORAGE LIMITS FOR THE INTERPOLATION TABLES HAVE BEEN	MAIN0180
C		EXCEEDED IN 'TSIGMA'. INCREASE THE DIMENSIONS IN THE	MAIN0181
C		COMMON BLOCK 'TABL'.	MAIN0182
C			MAIN0183
C	N = 9	AN OVERFLOW HAS BEEN ENCOUNTERED IN 'DSIG/TDSIG'.	MAIN0184
C			MAIN0185
C	N = 10, 11, ..., 17	FAILURE OF CONVERGENCE OF THE INTEGRATION	MAIN0186
C		PROCEDURE 'QUANC8', CALLED AT SEVERAL POINTS IN	MAIN0187
C		'CROSSX'.	MAIN0188
C			MAIN0189
C	N = 18	FAILURE OF CONVERGENCE IN DETERMINING THE GAUSS -	MAIN0190
C		LEGENDRE PARAMETERS IN 'IMTQL2', CALLED FROM 'GAUSS',	MAIN0191
C		CALLED IN TURN FROM 'MAIN'.	MAIN0192
C			MAIN0193
C	VARIABLE SPECIFICATIONS:		MAIN0194
	IMPLICIT REAL*8 (A - H, O - Z)		MAIN0195
	INTEGER*4 NAME(12)		MAIN0196
	REAL*8 AMU(2),Z(2),GWS(10)		MAIN0197
	REAL*4 SIGT,SIGS,SIGSD,S,SPUN(2650)		MAIN0198
	COMMON/PDAT/NI,NT,NCOEF,ION,DENSE,EI,UO,APQ(2),QGAM(2),RGAM(2),		MAIN0199
	1 SGAM(2),GAMMA(2),TLOW(2),TLOG(2),APAR(2),BPAR(2),		MAIN0200
	2 CPAR(2),ESTOP(2),NEWS,NTOT		MAIN0201
	COMMON/SIGX/EBI(51),EBT(51),S(50),SIGT(50),SIGSD(50),		MAIN0202
	1 SIGS(50,50,20)		MAIN0203
	COMMON/WATE/U(4),W(4),AB(10),WT1(10),INP,MEHL		MAIN0204
C			MAIN0205
C	DEFINITION OF NAMELIST INPUT RECORD:		MAIN0206
	NAMELIST/DATA/NEWS,NI,NT,NCOEF,UO,DENSE,TH,EI,AMU,Z,BPAR		MAIN0207
C			MAIN0208
C	FORMAT FOR IDENTIFICATION RECORD:		MAIN0209
	10 FORMAT(12A4)		MAIN0210

## Appendix A (contd.)

C		MAIN0211
C	DEFAULT VALUES OF THE INPUT DATA:	MAIN0212
	NEWS = 0	MAIN0213
	BPAR(1) = 0D0	MAIN0214
	BPAR(2) = 0D0	MAIN0215
C		MAIN0216
C	READ THE CROSS SECTION TITLE:	MAIN0217
	READ(5, 10) NAME	MAIN0218
C		MAIN0219
C	READ 'NAMELIST' INPUT:	MAIN0220
	READ( 5, D:TA)	MAIN0221
C		MAIN0222
C	GENERATE QUADRATURE SETS	MAIN0223
	INP = 10	MAIN0224
	MEHL = 4	MAIN0225
	CALL MEHLER( MEHL, QA, U, W)	MAIN0226
	CALL GAUSS( INP, AB, WT1, GWS)	MAIN0227
	NTOT = NI + NT	MAIN0228
C		MAIN0229
C	CONSTRUCT MASS FACTORS:	MAIN0230
	QA = AMU(2) / AMU(1)	MAIN0231
	QB = 1D0 + QA	MAIN0232
	APQ(1) = QA / QB	MAIN0233
	QGAM(1) = 5D-1 * QB	MAIN0234
	RGAM(1) = 5D-1 * QGAM(1)	MAIN0235
	GAMMA(1) = APQ(1) / RGAM(1)	MAIN0236
	SGAM(1) = 1D0 / DSQRT( QA )	MAIN0237
	APQ(2) = 5D-1	MAIN0238
	RGAM(2) = 5D-1	MAIN0239
	GAMMA(2) = 1D0	MAIN0240
	QGAM(2) = 1D0	MAIN0241
	SGAM(2) = 1D0	MAIN0242
	TLOW(2) = DSIN( 1.7453292519943296D-2 * TH ) ** 2	MAIN0243
	QB = QA * QA - TLOW(2)	MAIN0244
	IF( QB .GT. 0D0 ) GO TO 20	MAIN0245
	QB = 0D0	MAIN0246
	GO TO 30	MAIN0247
	20 QB = DSQRT( QB * ( 1D0 - TLOW(2) ) )	MAIN0248
	30 TLOW(1) = ( QA + TLOW(2) - QB ) / ( QA + QA )	MAIN0249
	TLOG(1) = - DLOG( TLOW(1) )	MAIN0250
	TLOG(2) = - DLOG( TLOW(2) )	MAIN0251
	TLOW(1) = GAMMA(1) * TLOW(1)	MAIN0252
C		MAIN0253
C	EVALUATE THE MOLIERE POTENTIAL PARAMETERS:	MAIN0254
	IF( BPAR(1) .LE. 0D0 ) BPAR(1) = 0.468493440443D0 *	MAIN0255
	1 DEXP( - DLOG( DSQRT( Z(1) ) + DSQRT( Z(2) ) ) / 1.5D0 )	MAIN0256
	IF( BPAR(2) .LE. 0D0 ) BPAR(2) = 0.468493440443D0 *	MAIN0257
	1 DEXP( - ( 1.3862943611198906D0 + DLOG( Z(2) ) ) / 3D0 )	MAIN0258
	APAR(1) = 5.039645408D0 * Z(1) * Z(2)	MAIN0259
	APAR(2) = 5.039645408D0 * Z(2) * Z(2)	MAIN0260
	CPAR(1) = 0.35D0 * BPAR(1) / APAR(1)	MAIN0261
	CPAR(2) = 0.35D0 * BPAR(2) / APAR(2)	MAIN0262

## Appendix A (contd.)

C		MAIN0263
C	EVALUATE LSS INELASTIC STOPPING PARAMETERS:	MAIN0264
	QA = DEXP( DLOG( Z(1) ) / 3D0 )	MAIN0265
	QB = DEXP( DLOG( Z(2) ) / 3D0 )	MAIN0266
	QC = DEXP( 1.5D0 * DLOG( QA ** 2 + QB ** 2 ) )	MAIN0267
	ESTOP(1) = 1.2166547D0 * Z(1) * Z(2) * DSQRT( QA / AMU(1) ) / QC	MAIN0268
	ESTOP(2) = 0.43015246D0 * Z(2) * DSQRT( QB / AMU(2) )	MAIN0269
C		MAIN0270
C	REPORT THE INPUT PARAMETERS:	MAIN0271
	PRINT 100, NAME, NI, NT, NCOEF, TH, UO, DENSE, EI,	MAIN0272
	1 (Z(IH), AMU(IH), BPAR(IH), IH = 1, 2)	MAIN0273
C		MAIN0274
C	EVALUATE THE REQUIRED CROSS SECTIONS:	MAIN0275
	CALL CROSSX	MAIN0276
	DO 50 L = 1, NCOEF	MAIN0277
	LM1 = L - 1	MAIN0278
	IF( L .LE. 1 )	MAIN0279
	1 PRINT 110, (IG, SIGT(IG), SIGSD(IG), S(IG), IG = 1, NTOT)	MAIN0280
	IF( NEWS .LE. 2 ) GO TC 60	MAIN0281
C		MAIN0282
C	IF REQUESTED, PRINT MULTIGROUP TRANSFER MATRIX	MAIN0283
	DO 40 IG = 1, NTOT	MAIN0284
	IF( IG .EQ. 1 ) PRINT 120, LM1	MAIN0285
	40 PRINT 130, IG, NTOT, (SIGS(IH,IG,L), IH = 1, NTOT)	MAIN0286
	50 CONTINUE	MAIN0287
C		MAIN0288
C	CROSS SECTIONS ARE WRITTEN ON UNIT 4 (ANISN-FORMAT)	MAIN0289
	60 REWIND 4	MAIN0290
	IHM = NTOT + 3	MAIN0291
	NPUN = IHM * NTOT	MAIN0292
	DO 90 L = 1, NCOEF	MAIN0293
	DO 80 IG = 1, NTOT	MAIN0294
	IND = IHM * (IG-1) + 1	MAIN0295
	SPUN(IND) = 0.0	MAIN0296
	IND = IND + 1	MAIN0297
	SPUN(IND) = 0.0	MAIN0298
	IND = IND + 1	MAIN0299
	SPUN(IND) = 0.0	MAIN0300
	IF( L .EQ. 1 ) SPUN(IND) = SIGT(IG)	MAIN0301
	DO 70 IH = 1, NTOT	MAIN0302
	IND = IND + 1	MAIN0303
	SPUN(IND) = 0.0	MAIN0304
	IGR = IG - IH + 1	MAIN0305
	IF( IGR .GT. 0 ) SPUN(IND) = SIGS(IGR,IG,L)	MAIN0306
	70 CONTINUE	MAIN0307
	80 CONTINUE	MAIN0308
	IDENT = 0	MAIN0309
	WRITE(4) NTOT, IHM, IDENT, L, NAME	MAIN0310
	90 WRITE(4) (SPUN(IH), IH = 1, NPUN)	MAIN0311
C		MAIN0312
C	OUTPUT INDICATOR (TO ANISN) THAT LAST MATERIAL HAS BEEN READ	MAIN0313
	IDENT = 7	MAIN0314
	WRITE(4) NTOT, IHM, IDENT, L, NAME	MAIN0315

## Appendix A (contd.)

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C
C ADD ON SOME USEFUL INFORMATION FOR SPUTTERING CALCULATION
WRITE(4) (SIGSD(IH), IH = 1, NTOT)
NTP1 = NT + 1
WRITE(4) (EBT(IH), IH = 1, NTP1)
C
C NORMAL PROGRAM TERMINATION:
STOP 0
C
C OUTPUT FORMATS:
100 FORMAT('1',42X,12A4//25X,I3,' ION GROUPS',10X,I3,' TARGET ATOM GROMAINO326
1UPS',10X,I3,' LEGENDRE COEFFICIENTS'//41X,'MINIMUM SCATTERING ANGLMAINO327
2E (DEGREES)',G15.8//15X,'TARGET BINDING ENERGY (E. V.)',G15.8,10X,MAINO328
3'TARGET DENSITY (/ANGSTROMS ** 3)',G15.8//37X,'INITIAL INCIDENT IEMAINO329
4N KINETIC ENERGY (E. V.)',G15.8//' INCIDENT ION ATOMIC NUMBER',G15MAINO330
5.8,10X,'ATOMIC MASS',G15.8,10X,'SCREENING LENGTH (ANGSTROMS)',G15.MAINO331
68//' TARGET ATOM ATOMIC NUMBER',G15.8,10X,'ATOMIC MASS',G15.8,10XMAINO332
7,'SCREENING LENGTH (ANGSTROMS)',G15.8) MAINO333
110 FORMAT(//19X,'GROUP',I3,10X,'SIGT',G15.8,10X,'SIGSD',G15.8,10X,'S'MAINO334
1,G15.8) MAINO335
120 FORMAT(///' P',I2,' COEFFICIENT') MAINO336
130 FORMAT(/5X,'SIGS(IH ->',I3,')', IH = 1,',I3,')',/(10X,8G14.6)) MAINO337
END MAINO338
C
C SUBROUTINE CROSSX CRSX0001
C EVALUATES THE MULTIGROUP CROSS SECTIONS FROM WHICH 'ANISN' CAN CRSX0002
C PERFORM SPUTTERING AND OTHER ATOMIC TRANSPORT CALCULATIONS. CRSX0003
C
C SOME VARIABLE DEFINITIONS: CRSX0004
C
C PSIGT POINT ENERGY TOTAL CROSS SECTION FOR DISCRETE INTER- CRSX0005
C ACTIONS. CRSX0006
C
C PSIGS POINT ENERGY SCATTERING CROSS SECTION FOR DISCRETE CRSX0007
C INTERACTIONS. CRSX0008
C
C COEF POINT ENERGY LEGENDRE COEFFICIENTS. THESE COEFFICIENTS CRSX0009
C EVALUATED IN SUBROUTINE 'LEGEND' AND STORED ON DATA SET CRSX0010
C REFERENCE NUMBER 4. THEY ARE RECOVERED AND USED TO CRSX0011
C CALCULATE THE HIGHER ORDER MULTIGROUP LEGENDRE COEFF- CRSX0012
C CIENTS AFTER CONVERGENCE OF THE INFINITE MEDIUM FLUXES. CRSX0013
C
C PNORM USED TO RNORMALIZE THE HIGHER ORDER COEFFICIENTS TO CRSX0014
C THE P0 COEFFICIENT. CRSX0015
C
C TO OBTAIN THE MULTIGROUP CROSS SECTIONS, THE POINT CROSS SECTIONS CRSX0016
C ARE WEIGHTED BY: CRSX0017
C
C 
$$PHE(E) = C(G) * E ** (- XI(G) ),$$
 CRSX0018
C CRSX0019
C CRSX0020
C CRSX0021
C CRSX0022
C CRSX0023
C CRSX0024
C CRSX0025
C CRSX0026
C CRSX0027
C CRSX0028

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## Appendix A (contd.)

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C WHERE C(G) AND XI(G) ARE GROUP DEPENDENT. XI IS OBTAINED FROM THE CR SX0029
C INFINITE MEDIUM GROUP FLUX, PHI(G). DEN(G) IS THE INTEGRAL OF CR SX0030
C PHE(E) OVER THE ENERGY GROUP. THE GROUP FLUX IS OBTAINED CR SX0031
C ITERATIVELY. PHIO(G) IS THE GROUP FLUX FROM THE PREVIOUS ITERATION. CR SX0032
C IT IS USED TO DETERMINE CONVERGENCE. CR SX0033
C CR SX0034
C VARIABLE SPECIFICATIONS: CR SX0035
  IMPLICIT REAL*8 (A - H, O - Z) CR SX0036
  EXTERNAL TDSIG,DSIG CR SX0037
  REAL*8 COEF(20),XI(50),PHI(50),DEN(50),PHIO(50),E(50,10), CR SX0038
  1 WTS(50,10),PSIGT(50,10),PSIGS(50,50,10),PNORM(50,50) CR SX0039
  REAL*4 SIGT,SIGS,SIGSD,S CR SX0040
  COMMON/PDAT/NI,NT,NCOEF,ION,DENSE,EI,UO,APQ(2),QGAM(2),RGAM(2), CR SX0041
  1 SGAM(2),GAMMA(2),TLOW(2),TLOG(2),APAR(2),BPAR(2), CR SX0042
  2 CPAR(2),ESTOP(2),NEWS,NTOT CR SX0043
  COMMON/SIGX/EBI(51),EBT(51),S(50),SIGT(50),SIGSD(50), CR SX0044
  1 SIGS(50,50,20) CR SX0045
  COMMON/WATE/U(4),W(4),AB(10),WT1(10),INP,MEHL CR SX0046
C CR SX0047
C GENERATE GROUP BOUNDARIES AND MAKE INITIAL FLUX GUESSES: CR SX0048
  NIP1 = NI + 1 CR SX0049
  NIP2 = NIP1 + 1 CR SX0050
  NTP1 = NT + 1 CR SX0051
  L = 1 CR SX0052
  IF( NT .EQ. 0 ) L = 2 CR SX0053
  EBI(1) = EI CR SX0054
  EBI(NIP1) = UO / GAMMA(L) CR SX0055
  A = ( DSQRT( EBI(1) ) - DSQRT( EBI(NIP1) ) ) / NI CR SX0056
  PHIO(1) = A CR SX0057
  DO 10 IG = 2, NI CR SX0058
  PHIO(IG) = A CR SX0059
  10 EBI(IG) = ( DSQRT( EBI(IG-1) ) - A ) ** 2 CR SX0060
  IF( NT .EQ. 0 ) GO TO 30 CR SX0061
  EBT(1) = EI * GAMMA(1) CR SX0062
  EBT(NTP1) = UO CR SX0063
  QQ = ( 1D0 / DSQRT( EBT(NTP1) ) - 1D0 / DSQRT( EBT(1) ) ) / NT CR SX0064
  PHIO(NIP1) = QQ CR SX0065
  DO 20 IG = 2, NT CR SX0066
  PHIO(NI+IG) = QQ CR SX0067
  20 EBT(IG) = ( 1D0 / ( QQ + 1D0 / DSQRT( EBT(IG-1) ) ) ) ** 2 ) CR SX0068
C CR SX0069
C DETERMINE POINT ENERGIES: CR SX0070
  30 DO 50 IG = 1, NI CR SX0071
  A = 0.5D0 * ( EBI(IG) - EBI(IG+1) ) CR SX0072
  QQ = 0.5D0 * ( EBI(IG) + EBI(IG+1) ) CR SX0073
  DO 40 NN = 1, INP CR SX0074
  40 E(IG,NN) = A * AB(NN) + QQ CR SX0075
  50 CONTINUE CR SX0076
  DO 70 IG = 1, NT CR SX0077
  A = 0.5D0 * ( EBT(IG) - EBT(IG+1) ) CR SX0078
  QQ = 0.5D0 * ( EBT(IG) + EBT(IG+1) ) CR SX0079
  DO 60 NN = 1, INP CR SX0080
  60 E(NI+IG,NN) = A * AB(NN) + QQ CR SX0081
  70 CONTINUE CR SX0082

```

## Appendix A (contd.)

```

C
C END OF INITIALIZATION.
C
C*****BEGIN ION POINT-ENERGY CROSS SECTION EVALUATION*****
C
C SET ION FLAG AND START LOOP OVER ALL ION GROUPS:
      ION = 1
      DO 110 IG = 1, NI
C
C CALCULATE STOPPING CROSS SECTION AT LOWER ENERGY GROUP BOUNDARIES:
      CALL T(SIGMA( EBI(IG+1) )
      TMIN = ODO
      TMAX = TLOW(1) * EBI(IG+1)
      CALL QUANC8( TDSIG, TMIN, TMAX, ODO, 1D-4, ELAS, ERREST,
      1
      NOFUN, FLAG)
      IF( FLAG .NE. ODO ) STOP 10
      S(IG) = ELAS + ESTOP(1) * DSQRT( EBI(IG+1) )
C
C EVALUATE TOTAL POINT ENERGY CROSS SECTION FOR DISCRETE INTERACTIONS:
      DO 100 NN = 1, INP
      CALL T(SIGMA( E(IG,NN) )
      TMIN = TLOW(1) * E(IG,NN)
      TMAX = GAMMA(1) * E(IG,NN)
      CALL QUANC8( D(SIG, TMIN, TMAX, ODO, 1D-5, TOT, ERREST,
      1
      NOFUN, FLAG)
      IF( FLAG .NE. ODO ) STOP 11
      PSIGT(IG,NN) = TOT
C
C CALCULATE POINT-ENERGY SCATTERING CROSS SECTION FOR INTERACTIONS IN
C WHICH THE INCIDENT ION EMERGES IN GROUP IH:
      DO 80 IH = IG, NI
      TMIN = DMAX1( E(IG,NN) - EBI(IH), TLOW(1) * E(IG,NN) )
      TMAX = DMIN1( E(IG,NN) - EBI(IH+1), GAMMA(1) * E(IG,NN) )
      SCAT = ODO
      IF( TMIN .GE. TMAX ) GO TO 80
      CALL QUANC8( DSIG, TMIN, TMAX, ODO, 1D-5, SCAT, ERREST,
      1
      NOFUN, FLAG)
      IF( FLAG .NE. ODO ) STOP 12
      CALL LEGEND( E(IG,NN), TMIN, TMAX, 0)
      80 PSIGS(IG,IH,NN) = SCAT
      IF( NT .EQ. C ) GO TO 100
C
C CALCULATE POINT-ENERGY SCATTERING CROSS SECTION FOR INTERACTIONS IN
C WHICH THE RECOIL TARGET ATOM EMERGES IN GROUP IF:
      DO 90 IF = 1, NT
      IHF = NI + IH
      TMIN = DMAX1( EBT(IH+1), TLOW(1) * E(IG,NN) )
      TMAX = DMIN1( EPT(IH), GAMMA(1) * E(IG,NN) )
      SCAT = ODO
      IF( TMIN .GE. TMAX ) GO TO 90

```

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CRSX0083
CRSX0084
CRSX0085
CRSX0086
CRSX0087
CRSX0088
CRSX0089
CRSX0090
CRSX0091
CRSX0092
CRSX0093
CRSX0094
CRSX0095
CRSX0096
CRSX0097
CRSX0098
CRSX0099
CRSX0100
CRSX0101
CRSX0102
CRSX0103
CRSX0104
CRSX0105
CRSX0106
CRSX0107
CRSX0108
CRSX0109
CRSX0110
CRSX0111
CRSX0112
CRSX0113
CRSX0114
CRSX0115
CRSX0116
CRSX0117
CRSX0118
CRSX0119
CRSX0120
CRSX0121
CRSX0122
CRSX0123
CRSX0124
CRSX0125
CRSX0126
CRSX0127
CRSX0128
CRSX0129
CRSX0130
CRSX0131
CRSX0132

```

## Appendix A (contd.)

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      CALL QUANC8( DSIG, TMIN, TMAX, ODO, 1D-5, SCAT, ERREST,
1          NCFUN, FLAG)
      IF( FLAG .NE. ODO ) STOP 13
      CALL LEGEND( E(IG,NN), TMIN, TMAX, 1)
90  PSIGS(IG,IHH,NN) = SCAT
100 CONTINUE
110 CONTINUE
      IF( NT .EQ. 0 ) GO TO 160
C
C  END OF ION POINT-ENERGY CROSS SECTION EVALUATION.
C
C *****BEGIN TARGET ATOM POINT-ENERGY CROSS SECTION EVALUATION*****
C
C  SET ION FLAG AND START LOOP OVER ALL TARGET ATOM GROUPS:
      ION = 2
      DO 150 IG = 1, NT
C
C  CALCULATE STOPPING CROSS SECTION AT LOWER ENERGY GROUP BOUNDARIES:
      IGG = NI + IG
      CALL TSIGMA( EET(IG+1) )
      TMIN = ODC
      TMAX = TLOW(2) * EET(IG+1)
      CALL QUANC8( DTSIG, TMIN, TMAX, ODO, 1E-4, ELAS, ERREST,
1          NOFUN, FLAG)
      IF( FLAG .NE. ODC ) STOP 14
      S(IGG) = ELAS + ESTOP(2) * DSQRT( EET(IG+1) )
C
C  EVALUATE TOTAL POINT-ENERGY CROSS SECTION FOR DISCRETE INTERACTIONS:
      DO 140 NN = 1, INP
      CALL TSIGMA( E(IGG,NN) )
      TMIN = TLOW(2) * E(IGG,NN)
      TMAX = E(IGG,NN)
      CALL QUANC8( DSIG, TMIN, TMAX, ODO, 1E-5, TOT, ERREST,
1          NCFUN, FLAG)
      IF( FLAG .NE. ODO ) STOP 15
      PSIGT(IGG,NN) = TOT
C
C  CALCULATE POINT-ENERGY SCATTERING CROSS SECTION FOR INTERACTIONS IN
C  WHICH THE INCIDENT TARGET ATOM EMERGES IN GROUP IH:
      DO 130 IH = IG, NT
      IHH = IH + NI
      TMIN = DMAX1( E(IGG,NN) - EET(IH), TLOW(2) * E(IGG,NN) )
      TMAX = DMIN1( E(IGG,NN) - EET(IH+1), E(IGG,NN) )
      SCAT = ODO
      IF( TMIN .GE. TMAX ) GO TO 120
      CALL QUANC8( DSIG, TMIN, TMAX, ODO, 1D-5, SCAT, ERREST,
1          NOFUN, FLAG)
      IF( FLAG .NE. ODC ) STOP 16
      CALL LEGEND( E(IGG,NN), TMIN, TMAX, 0)
120  PSJGS(IGG,IHH,NN) = SCAT
      PSIGS(IGG,IH,NN) = SCAT
C

```

## Appendix A (contd.)

```

C CALCULATE POINT-ENERGY SCATTERING CROSS SECTION FOR INTERACTIONS IN CRSX0185
C WHICH THE RECOIL TARGET ATOM EMERGES IN GROUP IF: CRSX0186
  TMIN = DMAX1( EBT(IH+1), TLOW(2) * E(IGG,NN) ) CRSX0187
  TMAX = DMIN1( EET(IH), E(IGG,NN) ) CRSX0188
  SCAT = ODC CRSX0189
  IF( TMIN .GE. TMAX ) GO TO 130 CRSX0190
  CALL GUANCB(DSIG, TMIN, TMAX, ODC, 1E-5, SCAT, ERPEST, CRSX0191
  1 MCFUN, FLAG) CRSX0192
  IF( FLAG .NE. ODC ) STOP 17 CRSX0193
  CALL LEGEND( E(IGG,NN), TMIN, TMAX, 1 ) CRSX0194
130 PSIGS(IGG,IHH,NN) = PSIGS(IGG,IHH,NN) + SCAT CRSX0195
140 CONTINUE CRSX0196
150 CONTINUE CRSX0197
C CRSX0198
C END OF TARGET ATOM POINT-ENERGY CROSS SECTION EVALUATION. CRSX0199
C CRSX0200
C*****START FLUX ITERATION AND MULTIGROUP (PO) CALCULATIONS*****CRSX0201
160 ITER = 0 CRSX0202
  DAMP = C.5DC CRSX0203
C CRSX0204
C EVALUATE XI, THE EXPONENT OF THE WEIGHTING FUNCTION: CRSX0205
170 XN = PHIO(2) * (EEI(1) - EBI(2)) / (PHIO(1) * (EEI(2) - EEI(3))) CRSX0206
  XD = ( EBI(1) + EBI(2) ) / ( EBI(2) + EBI(3) ) CRSX0207
  QQ = DLOG( XN ) / DLOG( XD ) CRSX0208
  IF( ITER .EQ. C ) XI(1) = QQ CRSX0209
  XI(1) = ( 1DC - DAMP ) * QQ + DAMP * XI(1) CRSX0210
  DO 180 IG = 2, NI CRSX0211
  XN = XI(IG-1) * CRSX0212
  1 DLOG( ( EBI(IG-1) + EBI(IG) ) / ( EBI(IG) + EBI(IG) ) ) CRSX0213
  2 - DLOG( PHIO(IG) * ( EEI(IG-1) - EBI(IG) ) / CRSX0214
  3 ( PHIO(IG-1) * ( EBI(IG) - EBI(IG+1) ) ) ) CRSX0215
  XD = DLOG( ( EBI(IG) + EEI(IG+1) ) / ( EEI(IG) + EBI(IG) ) ) CRSX0216
  QQ = XN / XD CRSX0217
  IF( ITER .EQ. 0 ) XI(IG) = QQ CRSX0218
180 XI(IG) = ( 1DC - DAMP ) * QQ + DAMP * XI(IG) CRSX0219
  IF( NT .EQ. 0 ) GO TO 200 CRSX0220
  XN = PHIO(NIP2) * ( EBT(1) - EBT(2) ) / CRSX0221
  1 ( PHIO(NIP1) * ( EET(2) - EET(3) ) ) ) CRSX0222
  XD = ( EBT(1) + EBT(2) ) / ( EBT(2) + EBT(3) ) CRSX0223
  QQ = DLOG( XN ) / DLOG( XD ) CRSX0224
  IF( ITER .EQ. C ) XI(NIP1) = QQ CRSX0225
  XI(NIP1) = ( 1DC - DAMP ) * QQ + DAMP * XI(NIP1) CRSX0226
  DO 190 IG = NIP2, NTOT CRSX0227
  IH = IG - NI CRSX0228
  XN = XI(IG-1) * CRSX0229
  1 DLOG( ( EET(IH-1) + EET(IH) ) / ( EET(IH) + EET(IH) ) ) ) CRSX0230
  2 - DLOG( PHIO(IG) * ( EBT(IH-1) - EBT(IH) ) / CRSX0231
  3 ( PHIO(IG-1) * ( EBT(IH) - EET(IH+1) ) ) ) CRSX0232
  XD = DLOG( ( EBT(IH) + EBT(IH+1) ) / ( EBT(IH) + EBT(IH) ) ) ) CRSX0233
  QQ = XN / XD CRSX0234
  IF( ITER .EQ. C ) XI(IG) = QQ CRSX0235
190 XI(IG) = ( 1DC - DAMP ) * QQ + DAMP * XI(IG) CRSX0236

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## Appendix A (contd.)

C		CRSX0237
C	CALCULATE DEN(G), THE INTEGRAL OF THE WEIGHT FUNCTION:	CRSX0238
	200 DO 210 IG = 1, NI	CRSX0239
	X11 = 1D0 - XI(IG)	CRSX0240
	210 DEN(IG) = ( EBI(IG) ** X11 - EBI(IG+1) ** X11 ) / X11	CRSX0241
	DC 220 IG = 1, NT	CRSX0242
	X11 = 1D0 - X1(IG+NI)	CRSX0243
	220 DEN(IG+NI) = ( EET(IG) ** X11 - EET(IG+1) ** X11 ) / X11	CRSX0244
C		CRSX0245
C	CALCULATE THE WEIGHTS FOR THE INTEGRATION OVER THE ENERGY GROUPS:	CRSX0246
	DO 240 IG = 1, NI	CRSX0247
	DO 230 NN = 1, INP	CRSX0248
	A = 0.5D0 * ( EBI(IG) - EBI(IG+1) )	CRSX0249
	230 WTS(IG,NN) = A * WT1(NN) * E(IG,NN) ** ( - XI(IG) ) / DEN(IG)	CRSX0250
	240 CONTINUE	CRSX0251
	DC 260 IG = 1, NT	CRSX0252
	DO 250 NN = 1, INP	CRSX0253
	A = 0.5D0 * ( EET(IG) - EET(IG+1) )	CRSX0254
	250 WTS(NI+IG,NN) = A * WT1(NN) * E(NI+IG,NN) ** ( - XI(NI+IG) )	CRSX0255
	1 / DEN(NI+IG)	CRSX0256
	260 CONTINUE	CRSX0257
C		CRSX0258
C	CALCULATE THE TOTAL MULTIGROUP CROSS SECTION:	CRSX0259
	DC 300 IG = 1, NTOT	CRSX0260
	SIGT(IG) = 0D0	CRSX0261
	DO 270 NN = 1, INP	CRSX0262
	270 SIGT(IG) = SIGT(IG) + DENSE * WTS(IG,NN) * SIGT(IG,NN)	CRSX0263
C		CRSX0264
C	CALCULATE THE CONTINUOUS SLOWING DOWN CROSS SECTION:	CRSX0265
	IF( IG .LT. NI ) SIGSD(IG) =	CRSX0266
	1 DENSE * S(IG) * EBI(IG+1) ** ( - XI(IG) ) / DEN(IG)	CRSX0267
	IF( IG .GT. NI ) SIGSD(IG) =	CRSX0268
	1 DENSE * S(IG) * EET(IG-NI+1) ** ( - XI(IG) ) / DEN(IG)	CRSX0269
C		CRSX0270
C	MODIFY THE TOTAL CROSS SECTION FOR 'ANISN':	CRSX0271
	SIGT(IG) = SIGT(IG) + SIGSD(IG)	CRSX0272
C		CRSX0273
C	CALCULATE THE MULTIGROUP SCATTERING MATRIX, PO COEFFICIENT:	CRSX0274
	DO 290 IH = IG, NTOT	CRSX0275
	SIGS(IG,IH,1) = 0D0	CRSX0276
	DO 280 NN = 1, INP	CRSX0277
	280 SIGS(IG,IH,1) = SIGS(IG,IH,1) +	CRSX0278
	1 DENSE * WTS(IG,NN) * PSIGS(IG,IH,NN)	CRSX0279
	290 CONTINUE	CRSX0280
	300 CONTINUE	CRSX0281
C		CRSX0282
C	PREVENT IONS FROM ENTERING THE TARGET ATOM GROUPS:	CRSX0283
	SIGSD(NI) = 0D0	CRSX0284
C		CRSX0285
C	UPDATE THE FLUXES USING THE NEW MULTIGROUP PARAMETERS:	CRSX0286
	PHI(1) = 1D0 / ( SIGT(1) - SIGS(1,1,1) )	CRSX0287
	DO 320 IG = 2, NTOT	CRSX0288
	SUM = SIGSD(IG-1) * PHI(IG-1)	CRSX0289
	IGM1 = IG - 1	CRSX0290
	DO 310 IH = 1, IGM1	CRSX0291

## Appendix A (contd.)

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310 SUM = SUM + SIGS(IH,IG,1) * PHI(IH)          CRSX0292
320 PHI(IG) = SUM / ( SIGT(IG) - SIGS(IG,IG,1) ) CRSX0293
ITER = ITER + 1                                  CRSX0294
C                                                 CRSX0295
C CHECK FOR CONVERGENCE OF THE FLUXES:          CRSX0296
  IFLG = 0                                       CRSX0297
  DO 330 IG = 1, NTOT                            CRSX0298
  IF( DABS( PHI(IG) - PHIO(IG) ) / PHIO(IG) .GT. 1D-2 ) IFLG = 1 CRSX0299
330 PHIO(IG) = PHI(IG)                          CRSX0300
C                                                 CRSX0301
C REPORT FLUXES, IF REQUESTED:                 CRSX0302
  IF( NEWS .LE. 0 .AND. IFLG .NE. 0 ) GO TO 170 CRSX0303
  PRINT 340, ITER, ( ( IG, PHI(IG) ), IG = 1, NTOT) CRSX0304
340 FORMAT(//5X,'FLUXES AFTER ITERATION',I4//8X,'IG',6X,'FLUX',13X,'IG' CRSX0305
1',6X,'FLUX',13X,'IG',6X,'FLUX',13X,'IG',6X,'FLUX',13X,'IG',6X,'FLUX',13X,'IG',6X,'FLUCRXC306
2X'/(I10,G15.5,I10,G15.5,I10,G15.5,I10,G15.5,I10,G15.5)) CRSX0307
  IF( IFLG .NE. 0 ) GO TO 170                   CRSX0308
C                                                 CRSX0309
C END OF FLUX ITERATION AND MULTIGROUP (PO) CALCULATIONS: CRSX0310
C                                                 CRSX0311
C*****CALCULATE HIGHER ORDER LEGENDRE COEFFICIENTS*****CRSX0312
C                                                 CRSX0313
C SAVE THE PO COEFFICIENT AND CLEAR THE CROSS SECTION MATRIX: CRSX0314
  DO 370 IG = 1, NTOT                            CRSX0315
  DO 360 IH = IG, NTOT                          CRSX0316
  PNORM(IG,IH) = SIGS(IG,IH,1)                 CRSX0317
  DO 350 L = 1, NCOEF                           CRSX0318
350 SIGS(IG,IH,L) = ODO                        CRSX0319
360 CONTINUE                                    CRSX0320
370 CONTINUE                                    CRSX0321
C                                                 CRSX0322
C RETRIEVE THE POINT-ENERGY COEFFICIENTS FROM DATA SET REFERENCE CRSX0323
C NUMB=4, WHERE THEY WERE SAVED BY 'LEGEND':   CRSX0324
  REWIND 4                                       CRSX0325
C                                                 CRSX0326
C ION CALCULATION:                             CRSX0327
  DO 430 IG = 1, NI                              CRSX0328
  DC 420 NN = 1, INP                            CRSX0329
  DO 390 IH = IG, NI                            CRSX0330
  IF( PSIGS(IG,IH,NN) .LE. ODO ) GO TO 390     CRSX0331
  READ(4) (COEF(L), L = 1, NCOEF)             CRSX0332
C                                                 CRSX0333
C INTEGRATE NUMERICALLY OVER THE ENERGY GROUP TO OBTAIN SIGS(IG,IH,L): CRSX0334
  DC 380 L = 1, NCOEF                          CRSX0335
380 SIGS(IG,IH,L) = SIGS(IG,IH,L) + DENSE * WTS(IG,NN) * COEF(L) CRSX0336
390 CONTINUE                                    CRSX0337
  DO 410 IH = 1, NT                             CRSX0338
  IHH = NI + IH                                CRSX0339
  IF( PSIGS(IG,IHH,NN) .LE. ODO ) GO TO 410   CRSX0340
  READ(4) (COEF(L), L = 1, NCOEF)             CRSX0341
  DO 400 L = 1, NCOEF                          CRSX0342

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## Appendix A (contd.)

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400 SIGS(IG,IHH,L) = SIGS(IC,IHH,L) + DENSE * WTS(IG,NN) * COEF(L)   CRSX0343
410 CONTINUE                                                         CRSX0344
420 CONTINUE                                                         CRSX0345
430 CONTINUE                                                         CRSX0346
C                                                                      CRSX0347
C TARGET ATOM CALCULATION:                                           CRSX0348
  DO 490 IG = 1, NT                                                  CRSX0349
    IGG = NI + IG                                                    CRSX0350
    DO 480 NH = 1, INP                                               CRSX0351
      DO 470 IH = IG, NT                                             CRSX0352
        IER = IH + NI                                               CRSX0353
        IF( PSIGS(IGG,IH,NN) .LE. ODO ) GO TO 450                  CRSX0354
        READ(4) (COEF(L), L = 1, NCOEF)                             CRSX0355
        DO 440 L = 1, NCOEF                                          CRSX0356
          440 SIGS(IGG,IHH,L) = SIGS(IGG,IHH,L) + DENSE * WTS(IGG,NN) * COEF(L) CRSX0357
        450 IF( PSIGS(IGG,IHH,NN) .LE. PSIGS(IGG,IH,NN) ) GO TO 470 CRSX0358
        READ(4) (COEF(L), L = 1, NCOEF)                             CRSX0359
        DO 460 L = 1, NCOEF                                          CRSX0360
          460 SIGS(IGG,IHH,L) = SIGS(IGG,IHH,L) + DENSE * WTS(IGG,NN) * COEF(L) CRSX0361
        470 CONTINUE                                                 CRSX0362
        480 CONTINUE                                                 CRSX0363
        490 CONTINUE                                                 CRSX0364
C                                                                      CRSX0365
C RENORMALIZE USING THE HIGHER PRECISION PO COEFFICIENT:           CRSX0366
  DO 520 IG = 1, NTOT                                               CRSX0367
    DO 510 IH = IG, NTOT                                            CRSX0368
      IF( PNORM(IG,IH) .EQ. CDO ) GO TO 510                          CRSX0369
      PNORM(IG,IH) = PNORM(IG,IH) / SIGS(IG,IH,1)                  CRSX0370
      DO 500 L = 1, NCOEF                                          CRSX0371
        SIGS(IG,IH,L) = SIGS(IG,IH,L) * PNORM(IG,IH)              CRSX0372
    500 CONTINUE                                                    CRSX0373
    510 CONTINUE                                                    CRSX0374
    520 CONTINUE                                                    CRSX0375
C                                                                      CRSX0376
C NORMAL TERMINATION OF THE PROCEDURE: RETURN TO CALLING PROGRAM.  CRSX0377
  RETURN                                                            CRSX0378
  END                                                                CRSX0379
C                                                                      T SIG0001
C SUBROUTINE TSIGMA(EP)                                             T SIG0002
C THIS PROCEDURE SETS UP A TABLE OF THE DIFFERENTIAL SCATTERING  T SIG0003
C SECTION, 'DSIG', AS A FUNCTION OF 'T', THE ENERGY TRANSFERRED  T SIG0004
C RECOILING TARGET ATOM. 'EP' IS THE ENERGY OF THE INCIDENT  T SIG0005
C PARTICLE.                                                         T SIG0006
C THE TABLE IS BASED ON THE APPROXIMATION:                         T SIG0007
C                                                                     T SIG0008
C   DSIG(T) / DSIG(TM) = (TM / T) ** N                             T SIG0009
C                                                                     T SIG0010
C WHERE 'TM' IS THE MAXIMUM POSSIBLE TRANSFERRED ENERGY. THE  T SIG0011
C TABLES CONTAIN VALUES OF LN( TM / T ) AND OF N. THE VALUES  T SIG0012
C OF 'DSIG' ARE RETRIEVED BY THE FUNCTION DSIG(T). THE TABLES  T SIG0013
C ARE PASSED IN THE COMMON BLOCK 'TABL'.                            T SIG0014

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## Appendix A (contd.)

C		TSIG0015
C	VARIABLE SPECIFICATIONS:	TSIG0016
	IMPLICIT REAL*8 (A - H, O - Z)	TSIG0017
	REAL*8 DIM(2)	TSIG0018
	COMMON/PI AT/NI, NT, NCOEF, ION, DENSE, EI, UO, APQ(2), QGAM(2), RGAM(2),	TSIG0019
	1          SGAM(2), GAMMA(2), TLOW(2), TLOG(2), APAR(2), BPAR(2),	TSIG0020
	2          CPAR(2), ESTOP(2), NEWS, NTOT	TSIG0021
	COMMON/WATE/U(4), W(4), AB(10), WT1(10), INP, MEHL	TSIG0022
	COMMON/TABL/TMX, SIGO, KM, KQ, TE(200), SIG(200)	TSIG0023
	DATA C1, C2, C3/1.4421818D0, 6.19086846881D-2, -6.39879712938D-2/	TSIG0024
C		TSIG0025
	QX = APQ(ION) * EP	TSIG0026
	TMX = RGAM(ION) / QX	TSIG0027
C		TSIG0028
C	ESTIMATE THE SPACING IN THE IMPACT PARAMETER NEEDED TO CONSTRUCT	TSIG0029
C	TABLES WITH SUITABLE SPACINGS IN T AND SIGMA FOR INTERPOLATION.	TSIG0030
	XX = ( 0.43429448190325183D0 * DLOG( QX * CPAR(ION) ) ) + 6D0	TSIG0031
	DELS = BPAR(ION) * DEXP( 2.3025850929940457D0 *	TSIG0032
	1                          ( C1 + XX * ( C2 + C3 * XX ) ) )	TSIG0033
C		TSIG0034
C	EVALUATE CROSS SECTION IN HEAD-ON COLLISION:	TSIG0035
	L = 0	TSIG0036
	K = 0	TSIG0037
	SONE = 0D0	TSIG0038
	SAA = 1D-10	TSIG0039
	ASSIGN 120 TO MARK	TSIG0040
	GO TO 40	TSIG0041
C		TSIG0042
C	STEP TO THE NEXT IMPACT PARAMETER VALUE:	TSIG0043
	20 K = K + 1	TSIG0044
	IF( K .GT. 200 ) STOP 6	TSIG0045
	L = L + 1	TSIG0046
	IF( K .NE. 1 ) GO TO 30	TSIG0047
	SAA = 1D-5	TSIG0048
	GO TO 40	TSIG0049
	30 SAA = SONE + ( L - 1 ) * DELS	TSIG0050
C		TSIG0051
C	EVALUATION OF THE APSIS OF THE COLLISION, R.	TSIG0052
C	INITIAL ESTIMATE OF THE APSIS:	TSIG0053
	40 QA = CPAR(ION) * QX	TSIG0054
	QB = DLOG( QA )	TSIG0055
	QA = DEXP((6.20563D-3 * QB + 3.15458D-1) * QB - 4.54369D-1) + QA	TSIG0056
	R = EPAR(ION) / QA	TSIG0057
	IF( SAA .GT. R ) R = SAA	TSIG0058
C		TSIG0059
C	REFINE THE APSIS BY QUADRATIC EXTRAPOLATION:	TSIG0060
	50 CQ = R - POTENZ(R, DER) / QX	TSIG0061
	QA = DER(1) / QX	TSIG0062
	QB = CQ + CQ - QA	TSIG0063
	IF( QB .GT. 0D0 ) GO TO 70	TSIG0064
	60 R = R + SAA	TSIG0065
	GO TO 50	TSIG0066

## Appendix A (contd.)

```

70 QA = QO - QA - QA - DER(2) / (QX + QX)
   QC = R * QO - ( SAA * SAA )
   QA = QO / ( QB - QA * QO / ( QB * R ) )
   IF( QA .GT. R ) GC TO 60
   F = R - QA
   IF( DABS(QA) .GT. 1D-3 * R ) GO TO 50
C
C CONTINUE REFINEMENT BY FAST LINEAR EXTRAPOLATION:
80 QA = ( R * ( R - POTENZ(R,DER) / QX ) - ( SAA * SAA ) ) / QB
   R = R - QA
   IF( DABS(QA) .GT. 1D-8 * R ) GO TO 80
C
C THE BARYCENTRIC (CM) SYSTEM SCATTERING INTEGRALS:
   SUM = ODO
   DTHDS = GDO
   IF( R .LE. SAA ) GO TO 90
   GO TO 100
90 SA = POTENZ(SAA,DER) / (SAA * QX)
   SB = DSQRT( 1EO - SA )
   R = SAA / SB
100 QZ = R / QX
   PB = POTENZ(R,DER)
   PA = DER(1)
   PB = DER(1) / R
C
C GAUSS-MEHLER QUADRATURE OF THE SCATTERING INTEGRALS:
DO 110 J = 1, MEHL
   QA = R / U(J)
   QQ = SAA * U(J)
   QE = QZ * U(J)
   QC = POTENZ(QA,DER)
   QD = 1D-70 / QB
   IF( QD .GT. QC ) QC = ODO
   QB = QB * QC
   QQ = ( R + QQ ) * ( R - QQ ) - QB
   Q = W(J) / DSQRT( QQ )
   SUM = SUM + Q
110 DTHDS = DTHDS + Q * ( PB * U(J) * U(J) - DER(1) / QA ) / QQ
   PB = SAA * SUM
   RATIO = ( DSIN( 1.5707963267948966EO - PB ) ) ** 2
C
C CALCULATION OF THE DIFFERENTIAL CROSS SECTION:
   PA = 1EO / ( 1EO - 0.5DO * QZ * PA / (SAA * SAA) )
   DTHDS = DABS( QZ * DTHDS * R * PA + ( PA - 1EO ) * (SUM + SUM) )
   PA = 1D-10 * SUM
   IF( PB .LT. PA ) B = PA
   IF( RATIO .LT. 1D-10 ) PB = 1D-10
   DTHDS = 12.56637061439DO * TMX * SAA / ( DTHDS * DSIN( PB + PB ) )
   GO TO MARK, ( 120, 130, 140 )
120 SIGO = DTHDS
   ASSIGN 130 TO MARK
   GO TO 20

```

TSIG0067  
TSIG0068  
TSIG0069  
TSIG0070  
TSIG0071  
TSIG0072  
TSIG0073  
TSIG0074  
TSIG0075  
TSIG0076  
TSIG0077  
TSIG0078  
TSIG0079  
TSIG0080  
TSIG0081  
TSIG0082  
TSIG0083  
TSIG0084  
TSIG0085  
TSIG0086  
TSIG0087  
TSIG0088  
TSIG0089  
TSIG0090  
TSIG0091  
TSIG0092  
TSIG0093  
TSIG0094  
TSIG0095  
TSIG0096  
TSIG0097  
TSIG0098  
TSIG0099  
TSIG0100  
TSIG0101  
TSIG0102  
TSIG0103  
TSIG0104  
TSIG0105  
TSIG0106  
TSIG0107  
TSIG0108  
TSIG0109  
TSIG0110  
TSIG0111  
TSIG0112  
TSIG0113  
TSIG0114  
TSIG0115  
TSIG0116  
TSIG0117  
TSIG0118

## Appendix A (contd.)

130	TE(K) = - DLOG( RATIO )	TSIG0119
	SIG(K) = DLOG( DTHDS / SIGO ) / TE(K)	TSIG0120
	IF( L .LT. 4 ) GO TO 20	TSIG0121
	SFOUR = SAA	TSIG0122
	SAA = SONE + 1.5D0 * DELS	TSIG0123
	ASSIGN 140 TO MARK	TSIG0124
	GO TO 40	TSIG0125
C		TSIG0126
C	TEST THE CURRENT IMPACT PARAMETER SPACING:	TSIG0127
140	ASSIGN 130 TO MARK	TSIG0128
	QQ = - DLOG( RATIO )	TSIG0129
	PA = SIG(K-3) * (QQ - TE(K-2)) * (QQ - TE(K-1)) * (QQ - TE(K)) /	TSIG0130
1	((TE(K-3) - TE(K-2)) * (TE(K-3) - TE(K-1)) * (TE(K-3) - TE(K)))	TSIG0131
	PA = PA +	TSIG0132
1	SIG(K-2) * (QQ - TE(K-3)) * (QQ - TE(K-1)) * (QQ - TE(K)) /	TSIG0133
2	((TE(K-2) - TE(K-3)) * (TE(K-2) - TE(K-1)) * (TE(K-2) - TE(K)))	TSIG0134
	PA = PA +	TSIG0135
1	SIG(K-1) * (QQ - TE(K-3)) * (QQ - TE(K-2)) * (QQ - TE(K)) /	TSIG0136
2	((TE(K-1) - TE(K-3)) * (TE(K-1) - TE(K-2)) * (TE(K-1) - TE(K)))	TSIG0137
	PA = PA +	TSIG0138
1	SIG(K) * (QQ - TE(K-3)) * (QQ - TE(K-2)) * (QQ - TE(K-1)) /	TSIG0139
2	((TE(K) - TE(K-3)) * (TE(K) - TE(K-2)) * (TE(K) - TE(K-1)))	TSIG0140
	PA = DABS( SIGO * DEXP( PA * QQ ) / DTHDS - 1D0 )	TSIG0141
	IF( PA .GT. 1D-3 ) GO TO 150	TSIG0142
	IF( PA .GT. 1D-4 ) GO TO 160	TSIG0143
C		TSIG0144
C	INCREASE SPACING OF IMPACT PARAMETER:	TSIG0145
	DELS = 1.6D0 * DELS	TSIG0146
	L = 0	TSIG0147
	K = K - 4	TSIG0148
	GO TO 20	TSIG0149
C		TSIG0150
C	DECREASE IMPACT PARAMETER SPACING:	TSIG0151
150	DELS = 0.9D0 * DELS	TSIG0152
	L = 0	TSIG0153
	K = K - 4	TSIG0154
	GO TO 20	TSIG0155
C		TSIG0156
C	CONTINUE WITH CURRENT IMPACT PARAMETER SPACING:	TSIG0157
160	IF( TE(K) .GT. TLOG(ION) ) GO TO 170	TSIG0158
	SONE = SFOUR + DELS	TSIG0159
	L = 0	TSIG0160
	GO TO 20	TSIG0161
C		TSIG0162
C	PRINT TABLE IF REQUESTED AND RETURN TO CALLING PROCEDURE:	TSIG0163
170	KM = K	TSIG0164
	KQ = K - 1	TSIG0165
	IF( NEWS .GT. 2 ) PRINT 180, ION, EP, TLOG(ION), KM, TMY, SIGO,	TSIG0166
1	(J, TE(J), SIG(J), J = 1, KM)	TSIG0167
	RETURN	TSIG0168
C		TSIG0169



## Appendix A (contd.)

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70 IF( YF .GT. 174D0 ) STOP 9
   DSIG = SIGC * DEXP( YF )
   GO TO JTD, (80, 90)
80 TDSIG = TQ * DSIG
90 RETURN
   END
C
   FUNCTION PCTENZ( R, DER )
C VERSION A. THE MOLIERE APPROXIMATION TO THE THOMAS-FERMI INTER-
C ATOMIC POTENTIAL FUNCTION AND ITS DERIVATIVES. 'POTENZ = R * V(R)'.
C 'DER(1) = R**2 * DV(R)/DR'. 'DER(2) = R**3 * D(DV(R)/LR)/DR'.
   IMPLICIT REAL*8 (A - H, O - Z)
   REAL*8 DER(2), COEFF(9)
C
   COMMON/PDAT/NI, NT, NCOEF, ION, DENSE, PI, UO, APQ(2), QGAM(2), RGAM(2),
1      SGAM(2), GAMMA(2), TLCW(2), TLOG(2), APAR(2), BPAR(2),
2      CPAR(2), ESTOP(2), NEWS, NTOT
C
C VALUES OF NUMERICAL CONSTANTS. THE VALUES AFTER THE FIRST THREE ARE
C 11/7, 44/7, 176/7, 2/7, 40/7, 80G/7, RESPECTIVELY.
   DATA COEFF/177D0, 44.25D0, 8.85D0, 1.5714285714285714D0,
1      6.2857142857142857D0, 25.142857142857143D0,
2      0.28571428571428571D0, 5.7142857142857143D0,
3      114.28571428571429D0/
C
   FQ = 0.3D0 * R / BPAR(ION)
   IF( FQ .GT. COEFF(1) ) GO TO 20
   F1 = DEXP( - FQ )
   FEXP = F1
   GEXP = F1
   HEXP = F1
   IF( FQ .GT. COEFF(2) ) GO TO 10
   F1 = ( F1 * F1 ) ** 2
   FEXP = FEXP + COEFF(4) * F1
   GEXP = GEXP + COEFF(5) * F1
   HEXP = HEXP + COEFF(6) * F1
   IF( FQ .GT. COEFF(3) ) GO TO 10
   F1 = F1 * ( F1 * F1 ) ** 2
   FEXP = FEXP + COEFF(7) * F1
   GEXP = GEXP + COEFF(8) * F1
   HEXP = HEXP + COEFF(9) * F1
10 PCTENZ = APAR(ION) * FEXP
   GEXP = FEXP + FQ * GEXP
   DER(1) = - APAR(ION) * GEXP
   DER(2) = APAR(ION) * ( GEXP + GEXP + FQ * FQ * HEXP )
   RETURN
20 POTENZ = 0D0
   DER(1) = 0D0
   DER(2) = 0D0
   RETURN
   END
DSIG0049
DSIG0050
DSIG0051
DSIG0052
DSIG0053
DSIG0054
PTZA0001
PTZA0002
PTZA0003
PTZA0004
PTZA0005
PTZA0006
PTZA0007
PTZA0008
PTZA0009
PTZA0010
PTZA0011
PTZA0012
PTZA0013
PTZA0014
PTZA0015
PTZA0016
PTZA0017
PTZA0018
PTZA0019
PTZA0020
PTZA0021
PTZA0022
PTZA0023
PTZA0024
PTZA0025
PTZA0026
PTZA0027
PTZA0028
PTZA0029
PTZA0030
PTZA0031
PTZA0032
PTZA0033
PTZA0034
PTZA0035
PTZA0036
PTZA0037
PTZA0038
PTZA0039
PTZA0040
PTZA0041
PTZA0042
PTZA0043
PTZA0044
PTZA0045

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## Appendix A (contd.)

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C          SUBROUTINE LEGEND(E, TLO, THI, KOIL)
C          CALCULATES THE LEGENDRE COEFFICIENTS, COEF, FOR SCATTERINGS WITH AN
C          INCIDENT ENERGY OF E AND RECOIL ENERGIES IN (TLO, THI).
C          IF KOIL = 1, THE PROJECTILE IS THE RECOIL ATOM.
C          IF KOIL = 0, THE PROJECTILE IS THE INCIDENT PARTICLE.
C
C          IMPLICIT REAL*8 (A-H,O-Z)
C          DIMENSION P(20),COEF(20)
C          COMMON/PDAT/NT,NT,NCOEF,ION,DENSE,EI,UO,APQ(2),QGAM(2),RGAM(2),
C          1          SGAM(2),GAMMA(2),TLOW(2),TLOG(2),APAR(2),BPAR(2),
C          2          CFAR(2),ESTOP(2),NEWS,NTCT
C          COMMON/WATE/U(4),W(4),AB(10),WT1(1C),INP,MEHL
C
C          IF( KOIL .EQ. 1 ) GO TO 1C
C          ASSIGN 5C TO KOILX
C          GO TO 2C
C          1C ASSIGN 4C TO KOILX
C          2C A = 0.5D0 * ( THI - TLO )
C          B = 0.5D0 * ( THI + TLO )
C          QA = DSQRT( E )
C          DO 3C L = 1, NCOEF
C          3C COEF(L) = 0D0
C
C          INTEGRATE FROM TLO TO THI USING INP-POINT GAUSS-LEGENDRE QUADRATURE
C          DO 9C NN = 1, INP
C          T = A * AB(NN) + B
C          SIG = A * WT1(NN) * DSIG( T )
C          QB = DSQRT( E - T )
C
C          P(2) IS THE COSINE OF THE ANGLE BETWEEN THE INCIDENT PARTICLE AND
C          THE PROJECTILE UNDER CONSIDERATION.
C          P(1) = 1D0
C          P(2) = ( E - QGAM(ION) * T ) / ( QA * QB )
C          GO TO KOILX, ( 4C, 5C )
C          4C P(2) = SGAM(ION) * ( QA - QB * P(2) ) / DSQRT( T )
C          5C IF( NCOEF .LT. 3 ) GO TO 7C
C          XMU = P(2)
C
C          HIGHER ORDER POLYNOMIALS ARE FOUND WITH RECURRENCE RELATION.
C          DO 6C LL = 3, NCOEF
C          EL2 = LL - 2
C          6C P(LL) = ( (EL2 + EL2 + 1D0) * XMU * P(LL-1) - EL2 * P(LL-2) ) /
C          1          (EL2 + 1D0)
C          7C DO 8C LL = 1, NCOEF
C          EL = LL + LL - 1
C          8C COEF(LL) = COEF(LL) + EL * P(LL) * SIG
C          9C CONTINUE
C
C          TEMPORARILY STORE COEFFICIENTS ON UNIT 4
C          WRITE(4) (COEF(L), L = 1, NCOEF)
C          RETURN
C          END

```

```

LGND0001
LGND0002
LGND0003
LGND0004
LGND0005
LGND0006
LGND0007
LGND0008
LGND0009
LGND0010
LGND0011
LGND0012
LGND0013
LGND0014
LGND0015
LGND0016
LGND0017
LGND0018
LGND0019
LGND0020
LGND0021
LGND0022
LGND0023
LGND0024
LGND0025
LGND0026
LGND0027
LGND0028
LGND0029
LGND0030
LGND0031
LGND0032
LGND0033
LGND0034
LGND0035
LGND0036
LGND0037
LGND0038
LGND0039
LGND0040
LGND0041
LGND0042
LGND0043
LGND0044
LGND0045
LGND0046
LGND0047
LGND0048
LGND0049
LGND0050
LGND0051
LGND0052
LGND0053

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## Appendix A (contd.)

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C      THIS ROUTINE COMPUTES THE ABCISSAS T(J) AND WEIGHTS W(J) FOR GAUS0006
C      AN N-POINT GAUSS-LEGENDRE QUADRATURE. THESE ARE USED WHEN GAUS0007
C      ONE WISHES TO APPROXIMATE THE INTEGRAL FROM -1 TO +1 OF F(X) GAUS0008
C      GAUS0009
C      N GAUS0010
C      BY      SUM W F(T) GAUS0011
C      J=1 J   J   GAUS0012
C      B      REAL SCRATCH ARRAY OF LENGTH N GAUS0013
C      GAUS0014
C      OUTPUT PARAMETERS (BOTH DOUBLE PRECISION ARRAYS OF LENGTH N) GAUS0015
C      GAUS0016
C      T      WILL CONTAIN THE DESIRED NODES. GAUS0017
C      W      WILL CONTAIN THE DESIRED WEIGHTS W(J). GAUS0018
C      GAUS0019
C      GAUS0020
C      ACCURACY GAUS0021
C      GAUS0022
C      THE ROUTINE WAS TESTED UP TO N = 512. COMPARISON WITH GAUS0023
C      TABLES IN REF. 3 SHOWED 12 OR MORE SIGNIFICANT DIGITS GAUS0024
C      OF ACCURACY. GAUS0025
C      GAUS0026
C      METHOD GAUS0027
C      GAUS0028
C      THE COEFFICIENTS OF THE THREE-TERM RECURRENCE RELATION GAUS0029
C      FOR THE CORRESPONDING SET OF ORTHOGONAL POLYNOMIALS ARE GAUS0030
C      USED TO FORM A SYMMETRIC TRIDIAGONAL MATRIX, WHOSE GAUS0031
C      EIGENVALUES (DETERMINED BY THE IMPLICIT QL-METHOD WITH GAUS0032
C      SHIFTS) ARE JUST THE DESIRED NODES. THE FIRST COMPONENTS OF GAUS0033
C      THE ORTHONORMALIZED EIGENVECTORS, WHEN PROPERLY SCALED, GAUS0034
C      YIELD THE WEIGHTS. THIS TECHNIQUE IS MUCH FASTER THAN USING A GAUS0035
C      ROOT-FINDER TO LOCATE THE ZEROS OF THE ORTHOGONAL POLYNOMIAL. GAUS0036
C      FOR FURTHER DETAILS, SEE REF. 1. GAUS0037
C      GAUS0038
C      GAUS0039
C      REFERENCES GAUS0040
C      GAUS0041
C      1. GOLUB, G. H., AND WELSCH, J. H., "CALCULATION OF GAUSSIAN GAUS0042
C      QUADRATURE RULES," MATHEMATICS OF COMPUTATION 23 (APRIL, GAUS0043
C      1969), PP. 221-230. GAUS0044
C      GAUS0045
C      2. GOLUB, G. H., "SOME MODIFIED MATRIX EIGENVALUE PROBLEMS," GAUS0046
C      SIAM REVIEW 15 (APRIL, 1973), PP. 318-334 (SECTION 7). GAUS0047
C      GAUS0048
C      3. STROUD AND SECREST, GAUSSIAN QUADRATURE FORMULAS, PRENTICE-GAUS0049
C      HALL, ENGLEWOOD CLIFFS, N.J., 1966. GAUS0050
C      GAUS0051
C      IMPLICIT REAL*8 (A - H, O - Z) GAUS0052
C      REAL*8 T(N),W(N),B(N) GAUS0053
C      NM1 = N - 1 GAUS0054
C      W(1) = 1D0 GAUS0055
C      DO 10 I = 1, NM1 GAUS0056
C      T(I) = 0D0 GAUS0057
C      W(I+1) = 0D0 GAUS0058
C      ABI = I GAUS0059

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## Appendix A (contd.)

10	B(I) = ABI / DSQRT( 4DO * ABI * ABI - 1DO)	GAUS0060
	T(N) = ODO	GAUS0061
	CALL IMTQL2( N, T, B, W, IERR )	GAUS0062
	IF( IERR .NE. 0 ) STOP 18	GAUS0063
	DO 20 I = 1, N	GAUS0064
20	W(I) = 2DO * W(I) * W(I)	GAUS0065
	RETURN	GAUS0066
	END	GAUS0067
C		IMTQ0001
	SUBROUTINE IMTQL2( N, D, E, Z, IERR)	IMTQ0002
C		IMTQ0003
C	THIS SUBROUTINE IS A TRANSLATION OF THE ALGOL PROCEDURE IMTQL2,	IMTQ0004
C	NUM. MATH. 12, 377-383(1968) BY MARTIN AND WILKINSON,	IMTQ0005
C	AS MODIFIED IN NUM. MATH. 15, 450(1970) BY DUBRULLE.	IMTQ0006
C	HANDBOOK FOR AUTO. COMP., VOL.II-LINEAR ALGEBRA, 241-248(1971).	IMTQ0007
C	THIS IS A MODIFIED VERSION OF THE 'EISPACK' ROUTINE IMTQL2.	IMTQ0008
C		IMTQ0009
C	THIS SUBROUTINE FINDS THE EIGENVALUES AND FIRST COMPONENTS OF THE	IMTQ0010
C	EIGENVECTORS OF A SYMMETRIC TRIDIAGONAL MATRIX BY THE IMPLICIT QL	IMTQ0011
C	METHOD.	IMTQ0012
C		IMTQ0013
C	ON INPUT:	IMTQ0014
C		IMTQ0015
C	N IS THE ORDER OF THE MATRIX;	IMTQ0016
C		IMTQ0017
C	D CONTAINS THE DIAGONAL ELEMENTS OF THE INPUT MATRIX;	IMTQ0018
C		IMTQ0019
C	E CONTAINS THE SUBDIAGONAL ELEMENTS OF THE INPUT MATRIX	IMTQ0020
C	IN ITS FIRST N-1 POSITIONS. E(N) IS ARBITRARY;	IMTQ0021
C		IMTQ0022
C	Z CONTAINS THE FIRST ROW OF THE IDENTITY MATRIX.	IMTQ0023
C		IMTQ0024
C	ON OUTPUT:	IMTQ0025
C		IMTQ0026
C	D CONTAINS THE EIGENVALUES IN ASCENDING ORDER. IF AN	IMTQ0027
C	ERROR EXIT IS MADE, THE EIGENVALUES ARE CORRECT BUT	IMTQ0028
C	UNORDERED FOR INDICES 1, 2, ..., IERR-1;	IMTQ0029
C		IMTQ0030
C	E HAS BEEN DESTROYED;	IMTQ0031
C		IMTQ0032
C	Z CONTAINS THE FIRST COMPONENTS OF THE ORTHONORMAL EIGENVECTORS	IMTQ0033
C	OF THE SYMMETRIC TRIDIAGONAL MATRIX. IF AN ERROR EXIT IS	IMTQ0034
C	MADE, Z CONTAINS THE EIGENVECTORS ASSOCIATED WITH THE STORED	IMTQ0035
C	EIGENVALUES;	IMTQ0036
C		IMTQ0037
C	IERR IS SET TO	IMTQ0038
C	ZERO FOR NORMAL RETURN,	IMTQ0039
C	J IF THE J-TH EIGENVALUE HAS NOT BEEN	IMTQ0040
C	DETERMINED AFTER 30 ITERATIONS.	IMTQ0041
C		IMTQ0042

## Appendix A (contd.)

C	INTEGER I, J, K, L, M, N, II, MML, IERR	IMTQ0043
	REAL*8 D(N), F(N), Z(N), B, C, F, G, F, P, S, MACHEP	IMTQ0044
	REAL*8 DSQRT, DABS, DSIGN	IMTQ0045
C		IMTQ0046
C	:::::::::::: MACHEP IS A MACHINE DEPENDENT PARAMETER SPECIFYING	IMTQ0047
C	THE RELATIVE PRECISION OF FLOATING POINT ARITHMETIC.	IMTQ0048
C	MACHEP = 16D0 ** (-13) FOR LONG FORM ARITHMETIC	IMTQ0049
C	ON S360 ::::::::::	IMTQ0050
C	DATA MACHEP/Z3410000000000000/	IMTQ0051
C		IMTQ0052
	IERR = 0	IMTQ0053
	IF (M .EQ. 1) GO TO 1001	IMTQ0054
C		IMTQ0055
	E(N) = 0D0	IMTQ0056
	DC 240 L = 1, N	IMTQ0057
	J = 0	IMTQ0058
C	:::::::::::: LOOK FOR SMALL SUB-DIAGONAL ELEMENT ::::::::::	IMTQ0059
105	DO 110 M = L, N	IMTQ0060
	IF (M .EQ. N) GO TO 120	IMTQ0061
	IF (DABS(E(M)) .LE. MACHEP * (DABS(D(M)) + DABS(D(M+1))))	IMTQ0062
X	GO TO 120	IMTQ0063
110	CONTINUE	IMTQ0064
C		IMTQ0065
120	P = D(L)	IMTQ0066
	IF (M .EQ. L) GO TO 240	IMTQ0067
	IF (J .EQ. 30) GO TO 1000	IMTQ0068
	J = J + 1	IMTQ0069
C	:::::::::::: FORM SHIFT ::::::::::	IMTQ0070
	G = (D(L+1) - P) / (2D0 * E(L))	IMTQ0071
	R = DSQRT(G*G+1D0)	IMTQ0072
	G = D(M) - P + E(L) / (C + DSIGN(R, G))	IMTQ0073
	S = 1D0	IMTQ0074
	C = 1D0	IMTQ0075
	P = 0D0	IMTQ0076
	MML = M - L	IMTQ0077
C		IMTQ0078
C	:::::::::::: FOR I=M-1 STEP -1 UNTIL L DC -- ::::::::::	IMTQ0079
	DO 200 II = 1, MML	IMTQ0080
	I = M - II	IMTQ0081
	F = S * E(I)	IMTQ0082
	B = C * E(I)	IMTQ0083
	IF (DABS(F) .LT. DABS(G)) GO TO 150	IMTQ0084
	C = G / F	IMTQ0085
	R = DSQRT(C*C+1D0)	IMTQ0086
	E(I+1) = F * R	IMTQ0087
	S = 1D0 / R	IMTQ0088
	C = C * S	IMTQ0089
	GO TO 160	IMTQ0090
150	S = F / G	IMTQ0091
	R = DSQRT(S*S+1D0)	IMTQ0092
	E(I+1) = G * R	IMTQ0093
	C = 1D0 / R	IMTQ0094
	S = S * C	IMTQ0095
		IMTQ0096

## Appendix A (contd.)

160	G = D(I+1) - P	IMTQ0097
	R = (D(I) - G) * S + 2D0 * C * B	IMTQ0098
	P = S * R	IMTQ0099
	D(I+1) = G + P	IMTQ0100
	G = C * R - B	IMTQ0101
C	:::::::::: FORM FIRST COMPONENT OF VECTOR ::::::::::	IMTQ0102
	F = Z(I+1)	IMTQ0103
	Z(I+1) = S * Z(I) + C * F	IMTQ0104
200	Z(I) = C * Z(I) - S * F	IMTQ0105
C		IMTQ0106
	D(L) = D(L) - P	IMTQ0107
	E(L) = G	IMTQ0108
	E(M) = 0D0	IMTQ0109
	GO TO 105	IMTQ0110
240	CONTINUE	IMTQ0111
C		IMTQ0112
C	:::::::::: ORDER EIGENVALUES AND EIGENVECTORS ::::::::::	IMTQ0113
	DO 300 II = 2, N	IMTQ0114
	I = II - 1	IMTQ0115
	K = I	IMTQ0116
	P = D(I)	IMTQ0117
C		IMTQ0118
	DO 260 J = II, N	IMTQ0119
	IF (D(J) .GE. P) GO TO 260	IMTQ0120
	K = J	IMTQ0121
	P = D(J)	IMTQ0122
260	CONTINUE	IMTQ0123
C		IMTQ0124
	IF (K .EQ. I) GO TO 300	IMTQ0125
	D(K) = D(I)	IMTQ0126
	D(I) = P	IMTQ0127
	P = Z(I)	IMTQ0128
	Z(I) = Z(K)	IMTQ0129
	Z(K) = P	IMTQ0130
300	CONTINUE	IMTQ0131
C		IMTQ0132
	GO TO 1001	IMTQ0133
C	:::::::::: SET ERROR -- NO CONVERGENCE TO AN	IMTQ0134
C	EIGENVALUE AFTER 30 ITERATIONS ::::::::::	IMTQ0135
1000	IERR = L	IMTQ0136
1001	RETURN	IMTQ0137
C	:::::::::: LAST CARD OF IMTQL2 ::::::::::	IMTQ0138
	END	IMTQ0139
C		QNC80001
	SUBROUTINE QUANC8( FUN, A, B, ABSERR, RELERR, RESULT, ERREST,	QNC80002
	1, NOFUN, FLAG)	QNC80003
C	ESTIMATE THE INTEGRAL OF FUN(X) FROM A TO B TO A USER PROVIDED	QNC80004
C	TOLERANCE: AN AUTOMATIC ADAPTIVE ROUTINE BASED ON THE 8-PANEL	QNC80005
C	NEWTON-COTES RULE.	QNC80006
C		QNC80007

## Appendix A (contd.)

C	INPUT :	QNC80008
C		QNC80009
C	FUN THE NAME OF THE INTEGRAND FUNCTION SUBPROGRAM FUN(X).	QNC80010
C	FUNCTION NAME SHOULD APPEAR IN AN EXTERNAL STATEMENT IN	QNC80011
C	CALLING PROGRAM	QNC80012
C		QNC80013
C	A THE LOWER LIMIT OF INTEGRATION.	QNC80014
C		QNC80015
C	B THE UPPER LIMIT OF INTEGRATION.(B MAY BE LESS THAN A.)	QNC80016
C		QNC80017
C	RELERR A RELATIVE ERROR TOLERANCE. (SHOULD BE NON-NEGATIVE)	QNC80018
C		QNC80019
C	ABSERR AN ABSOLUTE ERROR TOLERANCE. (SHOULD BE NON-NEGATIVE)	QNC80020
C		QNC80021
C	OUTPUT:	QNC80022
C		QNC80023
C	RESULT AN APPROXIMATION TO THE INTEGRAL HOPEFULLY SATISFYING THE	QNC80024
C	LEAST STRINGENT OF THE TWO ERROR TOLERANCES.	QNC80025
C		QNC80026
C	ERREST AN ESTIMATE OF THE MAGNITUDE OF THE ACTUAL ERROR.	QNC80027
C		QNC80028
C	NOPUN THE NUMBER OF FUNCTION VALUES USED IN CALCULATION OF RESULT.	QNC80029
C		QNC80030
C	FLAG A RELIABILITY INDICATOR. IF FLAG IS ZERO, THEN RESULT	QNC80031
C	PROBABLY SATISFIES THE ERROR TOLERANCE. IF FLAG IS	QNC80032
C	XXX.YYY , THEN XXX = THE NUMBER OF INTERVALS WHICH HAVE	QNC80033
C	NOT CONVERGED AND 0.YYY = THE FRACTION OF THE INTERVAL	QNC80034
C	LEFT TO DO WHEN THE LIMIT ON NOPUN WAS APPROACHED.	QNC80035
C		QNC80036
C	REFERENCE:	QNC80037
C		QNC80038
C	G. E. FORSYTHE, M. A. MALCOLM, AND C. B. MOLER, COMPUTER	QNC80039
C	METHODS FOR MATHEMATICAL COMPUTATIONS (PRENTICE-HALL, ENGLEWOOD	QNC80040
C	CLIFFS, N. J., 1977), PP. 84-105.	QNC80041
C		QNC80042
C	DOUBLE PRECISION FUN, A, B, ABSERR, RELERR, RESULT, ERREST, FLAG	QNC80043
C	INTEGER NOPUN	QNC80044
C	DOUBLE PRECISION W0,W1,W2,W3,W4,AREA,X0,F0,STONE,STEP,COR11,TEMP	QNC80045
C	DOUBLE PRECISION QPREV,QNOW,QDIFF,QLEFT,ESTERR,TOLERR	QNC80046
C	DOUBLE PRECISION QRIGHT(31),F(16),X(16),FSAVE(8,30),XSAVE(8,30)	QNC80047
C	DOUBLE PRECISION DABS,DMAX1	QNC80048
C	INTEGER LEVMIN,LEVMAX,LEVOUT,NOMAX,NOFIN,LEV,NIM,I,J	QNC80049
C		QNC80050
C	*** STAGE 1 *** GENERAL INITIALIZATION	QNC80051
C	SET CONSTANTS.	QNC80052
C		QNC80053
C	LEVMIN = 1	QNC80054
C	LEVMAX = 30	QNC80055
C	LEVOUT = 6	QNC80056
C	NOMAX = 5000	QNC80057
C	NOFIN = NOMAX - 8*(LEVMAX-LEVOUT+2**((LEVOUT+1)))	QNC80058
C		QNC80059

## Appendix A (contd.)

C	TROUBLE WHEN NOFUN REACHES NOFIN	QNC80060
C		QNC80061
	W0 = 3956D0 / 14175D0	QNC80062
	W1 = 23552D0 / 14175D0	QNC80063
	W2 = -3712D0 / 14175D0	QNC80064
	W3 = 41984D0 / 14175D0	QNC80065
	W4 = -13160D0 / 14175D0	QNC80066
C		QNC80067
C	INITIALIZE RUNNING SUMS TO ZERO.	QNC80068
C		QNC80069
	FLAG = 0D0	QNC80070
	RESULT = 0D0	QNC80071
	COR11 = 0D0	QNC80072
	ERREST = 0D0	QNC80073
	AREA = 0D0	QNC80074
	NOFUN = 0	QNC80075
	IF (A .EQ. P) RETURN	QNC80076
C		QNC80077
C	*** STAGE 2 *** INITIALIZATION FOR FIRST INTERVAL	QNC80078
C		QNC80079
	LEV = 0	QNC80080
	NIM = 1	QNC80081
	XC = A	QNC80082
	X(16) = B	QNC80083
	QPREV = 0D0	QNC80084
	FO = FUN(X0)	QNC80085
	STONE = 0.0625D0 * (B - A)	QNC80086
	X(8) = 0.5D0 * (X0 + X(16))	QNC80087
	X(4) = 0.5D0 * (X0 + X(8))	QNC80088
	X(12) = 0.5D0 * (X(8) + X(16))	QNC80089
	X(2) = 0.5D0 * (X0 + X(4))	QNC80090
	X(6) = 0.5D0 * (X(4) + X(8))	QNC80091
	X(10) = 0.5D0 * (X(8) + X(12))	QNC80092
	X(14) = 0.5D0 * (X(12) + X(16))	QNC80093
	DO 25 J = 2, 16, 2	QNC80094
	F(J) = FUN(X(J))	QNC80095
	25 CONTINUE	QNC80096
	NOFUN = 9	QNC80097
C		QNC80098
C	*** STAGE 3 *** CENTRAL CALCULATION	QNC80099
C	REQUIRES QPREV, X0, X2, X4, ..., X16, F0, F2, F4, ..., F16.	QNC80100
C	CALCULATES X1, X3, ..., X15, F1, F3, ..., F15, QLEFT, QRIGHT, QNOW, QDIFF, AREA.	QNC80101
	30 X(1) = 0.5D0 * (X0 + X(2))	QNC80102
	F(1) = FUN(X(1))	QNC80103
	DO 35 J = 3, 15, 2	QNC80104
	X(J) = 0.5D0 * (X(J-1) + X(J+1))	QNC80105
	F(J) = FUN(X(J))	QNC80106
	35 CONTINUE	QNC80107
	NOFUN = NOFUN + 2	QNC80108
	STEP = 0.0625D0 * (X(16) - X0)	QNC80109
	QLEFT = (W0*(F0 + F(8)) + W1*(F(1)+F(7)) + W2*(F(2)+F(6))	QNC80110
	1 + W3*(F(3)+F(5)) + W4*(F(4)) * STEP	QNC80111

## Appendix A (contd.)

```

      QRIGHT(LEV+1) = (W0*(F(8)+F(16))+W1*(F(9)+F(15))+W2*(F(10)+F(14)) QNC80112
1      + W3*(F(11)+F(13)) + W4*F(12)) * STEP QNC80113
      QNOW = QLEFT + QRIGHT(LEV+1) QNC80114
      QDIFF = QNOW - QPREV QNC80115
      AREA = AREA + QDIFF QNC80116
C QNC80117
C *** STAGE 4 *** INTERVAL CONVERGENCE TEST QNC80118
      ESTERR = DABS(QDIFF) / 1023D0 QNC80119
      TOLERR = DMAX1(ABSERR,RELERR*DABS(AREA)) * (STEP/STONE) QNC80120
      IF (LEV .LT. LEVMIN) GO TO 50 QNC80121
      IF (LEV .GE. LEVMAX) GO TO 62 QNC80122
      IF (NOFUN .GT. NOFIN) GO TO 60 QNC80123
      IF (ESTERR .LE. TOLERR) GO TO 70 QNC80124
C QNC80125
C *** STAGE 5 *** NO CONVERGENCE QNC80126
C LOCATE NEXT INTERVAL. QNC80127
50 NIM = NIM + NIM QNC80128
      LEV = LEV + 1 QNC80129
C QNC80130
C STORE RIGHT HAND ELEMENTS FOR FUTURE USE. QNC80131
      DO 52 I = 1, 8 QNC80132
          FSAVE(I,LEV) = F(I+8) QNC80133
          XSAVE(I,LEV) = X(I+8) QNC80134
52 CONTINUE QNC80135
C QNC80136
C ASSEMBLE LEFT HAND ELEMENTS FOR IMMEDIATE USE. QNC80137
      QPREV = QLEFT QNC80138
      DO 55 I = 1, 8 QNC80139
          J = - I QNC80140
          F(J+J+18) = F(J+9) QNC80141
          X(J+J+18) = X(J+9) QNC80142
55 CONTINUE QNC80143
      GO TO 30 QNC80144
C QNC80145
C *** STAGE 6 *** TROUBLE SECTION QNC80146
C NUMBER OF FUNCTION VALUES IS ABOUT TO EXCEED LIMIT. QNC80147
60 NOFIN = NOFIN + NOFIN QNC80148
      LEVMAX = LEVOUT QNC80149
      FLAG = FLAG + (B - XC) / (B - A) QNC80150
      GO TO 70 QNC80151
C QNC80152
C CURRENT LEVEL IS LEVMAX. QNC80153
62 FLAG = FLAG + 1D0 QNC80154
C QNC80155
C *** STAGE 7 *** INTERVAL CONVERGED QNC80156
C ADD CONTRIBUTIONS INTO RUNNING SUMS. QNC80157
70 RESULT = RESULT + QNOW QNC80158
      ERREST = ERREST + ESTERR QNC80159
      COR11 = COR11 + QDIFF / 1023D0 QNC80160
C QNC80161
C LOCATE NEXT INTERVAL. QNC80162
C QNC80163

```

## Appendix A (contd.)

72 IF (NIM .EQ. 2*(NIM/2)) GO TO 75	QNC80164
NIM = NIM / 2	QNC80165
LEV = LEV - 1	QNC80166
GO TO 72	QNC80167
75 NIM = NIM + 1	QNC80168
IF (LEV .LE. 0) GO TO 80	QNC80169
C	QNC80170
C ASSEMBLE ELEMENTS REQUIRED FOR THE NEXT INTERVAL.	QNC80171
QPREV = GRICHT(LEV)	QNC80172
X0 = X(16)	QNC80173
F0 = F(16)	QNC80174
DO 78 I = 1, 8	QNC80175
F(I+I) = FSAVE(I,LEV)	QNC80175
X(I+I) = XSAVE(I,LEV)	QNC80177
78 CONTINUE	QNC80178
GO TO 30	QNC80179
C	QNC80180
C *** STAGE 8 *** FINALIZE AND RETURN	QNC80181
80 RESULT = RESULT + COR11	QNC80182
C	QNC80183
C MAKE SURE ERREST NOT LESS THAN ROUNDOFF LEVEL.	QNC80184
IF (ERREST .EQ. CDO) RETURN	QNC80185
82 TEMP = DAES(RESULT) + EPREST	QNC80186
IF (TEMP .NE. DABS(RESULT)) RETURN	QNC80187
ERREST = ERREST + EPREST	QNC80188
GO TO 82	QNC80189
END	QNC80190

50

## Appendix B

## ANISN Sputtering Calculations Using MUXS Data

Three changes were made to the standard version of ANISN in order to perform sputtering calculations with the cross sections generated by MUXS:

1. From Eq. 1,  $\Sigma_{G-1}^{CSD} \phi_{G-1}(x, \mu)$  must be added to the total source term for group G if  $G > 1$ . We have made this change to ANISN in Subroutine S833. Two arrays are used: E3SAV1(I,M) and E3SAV2(I,M) where I is an index for the spatial mesh interval and M is an index for the angular quadrature interval. E3SAV1 saves  $\Sigma_G^{CSD} \phi_G(x, \mu)$  for the current energy group being processed by S833. E3SAV2 is the value of  $\Sigma_{G-1}^{CSD} \phi_{G-1}(x, \mu)$  obtained from the previous call to S833. E3SAV2 is added to the total source term, XNRI, if the group being processed is not group 1.
2. An angle dependent response function for the leakage is needed to prevent leakage by target atoms with energy less than  $U_0/\mu^2$ , where  $U_0$  is the surface binding energy and  $\mu$  is the cosine of the angle between the surface normal and the target atom direction. This is essentially a post-editing procedure and would require no modification to ANISN if a spherically symmetric surface binding energy were assumed.<sup>13</sup> We have made this change to Subroutine SUMMARY of ANISN. The current at the right surface of the slab, XND, is multiplied by this response function, R, to obtain the right leakage for the summary

tables, i.e., RCT. The ion source is assumed to have been input on the right surface of the slab by the user. With this change, the calculated sputtering yield will be printed as a function of the energy group in the summary tables under the heading "RT LEAKAGE."

3. We have also modified Subroutine S833 to input  $\Sigma_G^{CSD}$ , SIGSD, and the target atom energy group structure, EBT, from the cross section file produced by MUXS. With this change, all card input to ANISN is the same as that for the standard version.

The modified ANISN routines, S833 and SUMMARY, along with the required data and JCL for a problem with an 8 kev proton incident on a nickel target, are shown in Figure B1. The statements that were added are indented and commented.

This problem was run with the cross sections obtained from MUXS using the input described in Section V. The calculated sputtering yield is 0.00818 Ni atom/incident proton. This result is in excellent agreement with the experimental value (.00822 Ni atom/incident proton) obtained by Roth, Bohdansky, and Ottenberger.<sup>14</sup>

```

//TJHANSF JCB (21541,16), '6025 T J HOFFMAN', TIME=6
//STP3 EXEC FORTHCLG, PARM.FORT='XREF', PARM.LKED='MAP,LET,LIST',
// GOSIZE=950K
C MAIN ROUTINE - ALLOT SPACE ( LIM1 AND DUMY )
COMMON/BULKBU/D(1),LIM1,DUMY(170000)
LIM1=170000
CALL CLEAR(3,LIM1)
CALL CONTRL
STOP
END
SUBROUTINE S833(XN,XNN,ST,SR,CS,MA,J5,AA,SAT,SA,CH,XNA,XNR,PNC,DSNANSN2192
1 ,W,XNI,NO,R,DA,DB,DC,DS,V,XNF,P,WD,CT,SG,XND,I1, M1,I2,IM1,MRANSN2193
1,ART,ALFT) ANSN2194
C *** ITER *IMPOSSIBLE TO *TRANSLATE, *EXPLAIN OR *REMEMBER ANSN219
C SPUTTERING CHANGE - SETUP ARRAYS, COMMON/SPUT/
REAL*8 EBT,UO
DIMENSION E3SAV1(201,33),E3SAV2(201,33)
COMMON/SPUT/SIGSD(50),EET(51),UO,NI
DIMENSION XN(1) ,XNN(1),ST(1),SR(1),CS(1),MA(1),J5(1),AA(1), ANSN2196
1 SAT(1) ,SA(1) ,CH(1) ,XNA(1) ,XNR(1),PNC(1) ,DSN(1), ANSN21
2 W(1),XNI(1), NO(1),B(1) ,DA(1) ,DE(1) ,DC(1) ,DS(1) , ANSN2198
3 V(1),XNE(1),FA(1) ,WD(1),CT(1),SG(1),XND(1) ,MR(1) ANSN2199
4 ,ART(1),ALFT(1) ANSN2200
COMMON /BULKBU/ ANSN2201
$ D(1),LIM1,LXKI,LFD,LXN,LR,LVE,LW,LDSN,IMA,LMZ,LMB,IMC,LXMD, ANSN2202
1LMTT,LCRX,LFIX,LFLT,LQ,LPA,LJ5,LRM,LDF,LJ3,LJ4,LIGT,LART,LALFT, ANSN2203
2LFGP,LFGG,IEND,LV,IAA,LWD,LMR,LPRC,LXJ,ICH,LCA,LCF,LCT,LCS,LTAB, ANSN2204
3LXND,LSA,LSAT,LRAV,LRA,LXNN,LXNF,LXNP,LXNA,LSR,LST,LQG,LFG,LSG, ANSN2205
4LXKE,LXNI,LXNC,LT3,LT5,LDA,LDB,IDC,LDS,LB,IGMP,IGMM,IIGG,IFRR,IMJTANSN2206
5,IHG,IMP,MP,NDS,NUS,SDG,SCG,AG,XNLGG,XNLG,SNG,ALA,ASR,EAM,EPG,EO, ANSN2207
6F1,E2,E3,E4,E5,E6,E7,E8,E9,E10,E11,E12,E13,E14,E15,E16,E17,E18,E19 ANSN2208
7,E20,ESC,ESP,FVP,EVPP,FTP,IC,ICVT,IGP,IG,IHP,IIC,IIG,IP,I2P,I01, ANSN2209
8I02,I03,I04,I05,I06,I07,I08,I09,I0G,IT,LC,MG,PI,ML,PM,NFK,YITR, ANSN2210
9XLAP,XLAPP,XLAP,XLA,XKIO,XNII,ZZ1,ZZ2,ZZ3,XNB,XKEP,XKIP,IH,J,K,I, ANSN2211
AM,J,N,NN,ISV, ANSN2212
EID,I7H,ISCT,ISN,IGF,IBL,IBR,I2M,IM,IFVT,IGM,IPT,IHS,IHM,MS,MCR,MTPANSN2213
C,MT,IDFM,IPVT,IQM,I2M,IPP,IIM,ID1,ID2,ID3,ID4,I2M,IDAT1,IDAT2,IFG, ANSN2214
FIFLU,IFN,IPRT,IXTR, ANSN2215
EEV,EVM,FPS,BF,DY,DZ,DFM1,XNF,PV,PYF,XLAL,YLAF,EQL,XNPM, ANSN2216
FT(12),NIN,NOU,NT1,NT2,NT3,NT4,NT5,NT6,NT7 ANSN2217
C SPUTTERING CHANGE - INPUT DATA
DATA ICALL/C/
IF(ICALL.EQ.0) GO TO 200
210 READ(4) N1,N2,IDENT
IF(IDENT.EQ.7) GO TO 220
READ(4) DUM!
GO TO 210
220 READ(4) (SIGSD(IGG),IGG=1,IGM)
DO 230 IGG=1,IGM
IF(SIGSD(IGG).EQ.C.) GO TO 240
230 CONTINUE
NI=IGM
GO TO 250
240 NI=IGG
250 NTF1=IGM-NI+1

```

Figure B1. ANISN Sample Problem Input

	GC TO 250	
240	NI=IGG	
250	NTP1=ICM-NI+1	
	READ(4) (EBT(IGG), IGG=1, NTP1)	
	UC=EET(NTP1)	
	ICALL=1	
260	CONTINUE	
	IM2=IM+IM	ANSN2218
	E1=0.0	ANSN2219
	ICMC=1	ANSN2220
	DO 8003 I=1, IM	ANSN2221
	E1=E1 + CT(I)*DC(I)	ANSN2222
	NO(I)=ICMC	ANSN2223
	IF(I.LT.IM .AND. E1.LT.1.0)GO TO 8003	ANSN2224
	NO(ICMC + IM)=I+1	ANSN2225
	E1=0.0	ANSN2226
	ICMC=ICMC + :	ANSN2227
8003	CONTINUE	ANSN2228
	ICMC=NO(IM)	ANSN2229
	NGE=C	ANSN2230
	IF(IGE.EQ.2)MGE=1	ANSN2231
	IFLU1=IFLU	ANSN2232
	IF(IFLU.EQ.4)IFLU1=0	ANSN2233
	IGMPM=(IGMP-1)*MM	ANSN2234
	IGMPI=(IGMP-1)*IM	ANSN2235
	IGMI=(IIGG-1)*MM*IMP - MM	ANSN2236
	IF(IC.GT.1 .OR. IC.EQ.1 .AND. IFN.GE.1) GO TO 832	ANSN2237
C	*** FIRST GENERATION BOUNDARY FLUXES	ANSN2238
	IGMPMM=IGMPM + 1	ANSN2239
	DO 55 M=1, MM	ANSN2240
	IF(DSN(M))53,53,54	ANSN2241
53	B(IGMPMM)=XNN(1)	ANSN2242
	GO TO 55	ANSN2243
54	B(IGMPMM)=XNN(IM)	ANSN2244
55	IGMPMM=IGMPMM + 1	ANSN2245
832	IGMPII=IGMPI + 1	ANSN2246
	SCLMX=0.0	ANSN2247
	IF(IIC.GT.IIM/2 .AND. IIM.GE.20)IFLU1=3	ANSN2248
	DO 1001 I=1, IM	ANSN2249
	XN(IGMPII)=XNN(I)	ANSN2250
	IGMPII=IGMPII + 1	ANSN2251
C	*** ADD IN-GROUP SOURCE COMPONENT (PO)	ANSN2252
	ST(I)=SR(I)+ CS(I)*XNN(I)	ANSN2253
1001	XNN(I)=0.0	ANSN2254
	IF(ISCT.EQ.0)GO TO 1002	ANSN2255
	DO 1 I=1, IM	ANSN2256
	NLO=1	ANSN2257
	J=MA(I)	ANSN2258
	J=J5(J)	ANSN2259
	IF(J.EQ.C)GO TO 1	ANSN2260
	INN=I	ANSN2261
	IN=I	ANSN22 2

Figure B1 (contd.)

DO 2 N=1,J	ANSN2263
NFI=NLC + NGE*(N+1)/4	ANSN2264
DO 3 NN=NLC,NHI	ANSN2265
SAT(INN)=SA(INN) + CH(IN)*XNA(INN)	ANSN2266
XNA(INN)=0.0	ANSN2267
3 INN=INN+IM	ANSN2268
NLO=NFI+1	ANSN2269
2 IN=IN+IM	ANSN2270
1 CONTINUE	ANSN2271
1002 CONTINUE	ANSN2272
LC=LC+1	ANSN2273
KK=KK+1	ANSN2274
IF(IEL.NE.3 .AND. IBR.NE.3)GO TO 842	ANSN2275
C *** COMPUTE WHITE BOUNDARY FLUX	ANSN2276
XNII=0.0	ANSN2277
XNIO=0.0	ANSN2278
IGMPM=IGMPI + 1	ANSN2279
DO 45 M=1,M2	ANSN2280
IF(WD(M))46,46,47	ANSN2281
46 XNII=XNII + B(IGMPM)*ABS(WD(M))	ANSN2282
GO TO 45	ANSN2283
47 XNIO=XNIO + B(IGMPM)*WD(M)	ANSN2284
45 IGMPM=IGMPM + 1	ANSN2285
IF(IBL.EQ.3)XNII=XNII*ALFT(IIG)/ZZ3	ANSN2286
IF(IBR.EQ.3)XNIO=XNIO*APT(IIG)/ZZ3	ANSN2287
C *** BEGIN ANGLE LOOP FOR FLUX CALCULATION	ANSN2288
842 DO 5 M=1,MH	ANSN2289
LSNM=DSN(M)	ANSN2290
WM=W(M)	ANSN2291
IFM=(M-1)*IF	ANSN2292
IGMIP=ICMI + P	ANSN2293
C *** COMBINE PC AND PL SOURCE TERMS	ANSN2294
DO 6 I= 1, IM	ANSN2295
6 XNR(I) = ST(I)	ANSN2296
IF(ISCT.EQ.C)GO TO 9	ANSN2297
MN=M	ANSN2298
IN=1	ANSN2299
DO 8 N=1,J1	ANSN2300
DO 88 I=1,IM	ANSN2301
XNR(I)=XNR(I) + PNC(MN)*SAT(IN)	ANSN2302
88 IN=IN + 1	ANSN2303
8 MN=MN + M2	ANSN2304
C *** COMPUTE TRANSVERSE VEIL STREAMING CORRECTION	ANSN2305
9 EC=0.0	ANSN2306
IF(DPM1.EQ.C.0)GO TO 10	ANSN2307
IF(IGF.EQ.1)E8=SQRT(1.0 - DSNM*DSNM)/(0.5*IFM1)	ANSN2308
IF(IGE.NE.2)GO TO 10	ANSN2309
IF(WM.NP.C)GO TO 11	ANSN2310
KK=KK-1	ANSN2311
11 E8=LSN(KK)/(0.5*IFM1)	ANSN2312
C *** SET UP BOUNDARY CONDITIONS	ANSN2313
10 IF(LSNM.GE.0.C)GO TO 12	ANSN2314

Figure B1 (contd.)

ILS=IP	ANSN2315
IT=IF	ANSN2316
IOO=IP + 1	ANSN2317
IOI=IPR	ANSN2318
E1=KNIC	ANSN2319
GC TO 19	ANSN2320
12 IT=0	ANSN2321
ILS=-1	ANSN2322
IOO=0	ANSN2323
IOI=JPL	ANSN2324
E1=KNII	ANSN2325
19 IF(IC=-1)13,14,15	ANSN2326
12 XNM=C.C	ANSN2327
GC TO 17	ANSN2328
14 IGMPL=IGMPH + MR(M)	ANSN2329
XNM=B(IGMPL)	ANSN2330
GO TO 17	ANSN2331
15 XNM=E1	ANSN2332
IGMPM=IGMPH + M	ANSN2333
IF(IOI.EQ.2)XNM=B(IGMPM)	ANSN2334
17 IF(WM.NE.0.0)GO TO 24	ANSN2335
DC 18 I=1,IX	ANSN2336
18 XNE(I)=0.0	ANSN2337
24 EE=XNM	ANSN2338
C *** BEGIN INTERVAL LOOP FOR FLUX CALCULATION	ANSN2339
IF(IPM.NE.1)GO TO 8644	ANSN2340
PAIGMM=PA(IGMIM + MM)	ANSN2341
C .....NOTE.....	
C.....SOME PATCHWORK CODING NOW IN S833	
C.....ALSO NOTE FIXED DIMENSION STMT. IN THIS ROUTINE <<<REDO LATER>>	
8644 DO 25 J=1,IX	ANSN2342
844 L = IABS(IOO-J)	ANSN2343
843 I = IABS(IT-J)	ANSN2344
K=IABS(ILS-J)	ANSN2345
IPMMI=IPMM+I	ANSN2346
IPMMK=IPMM+K	ANSN2347
IPMML=IPMM + L	ANSN2348
IF(DSNM.GT.0.0)GO TO 26	ANSN2349
C *** ADD SHELL SOURCE TO FLUX WHEN MU.LT.0	ANSN2350
IF(IPM-1)26,27,28	ANSN2351
28 IGMIMI=IGMIM + I*MM	ANSN2352
XNM=XNM + PA(IGMIMI)	ANSN2353
GO TO 26	ANSN2354
27 IF(IPP.EQ.I)XNM=XNM + PAIGMM	ANSN2355
C *** SAVE ANGULAR FLUX	ANSN2356
26 XND(IPMML)=E6	ANSN2357
C * * * * * ANISN FIVE MODE FLUX CALCULATION	*ANSN2358
C * * * * * E3 = CENTERED FLUX	*ANSN2359
C * * * * * E5 = ANGLE EXTRAPOLATED FLUX	*ANSN2360
C * * * * * E6 = SPACE EXTRAPOLATED FLUX	*ANSN2361
C * * * * * XNM = KNOWN SPACE BOUNDARY FLUX	*ANSN2362
C * * * * * PHIM = KNOWN ANGLE BOUNDARY FLUX	*ANSN2363

Figure B1 (contd.)

C	*****	XNRI = TOTAL SOURCE	ANSN2364
C	*****	E1 = SIGMA TOTAL	ANSN2365
	56	E1=CT(I)	ANSN2366
		IF(E1.EQ.0.0)E1=E1 + E6*V(I)	ANSN2367
		XNRI=XI/R(I)	ANSN236
C	SPUTTERING CHANGE - ADD CSD TERM TO TOTAL SOURCE		
		IF(IIG.NE.1) XNRI=XNRI+E3SAV2(I,M)*V(I)	
		DSKM=DS(IPMK)	ANSN2369
		DSLH=DS(IPML)	ANSN2370
		DSKM2=DSKM + DSLH	ANSN2371
		IF(WH.EQ.C.0 .OR. IGE.EQ.1)GO TO 6006	ANSN2372
C	*****	GENERAL DIRECTION FLUX CALCULATION - W.GT.0	ANSN2373
		PHIM=XNE(I)	ANSN2374
		DAIM=DA(IPMI)	ANSN2375
		DBIM=DB(IPMI)	ANSN2376
		DBIM2=DAIM + DBIM	ANSN2377
		IF(IFLU1-2)6001,6002,6003	ANSN237
C	*****	LINEAR MODEL	ANSN2379
	6001	E3=(XNRI + DSKM2*XNM + DBIM2*PHIM)/(E1 + DSKM2 + DBIM2)	ANSN23 0
		E5=E3 + E3 - PHIM	ANSN2381
		E6=E3 + E3 - XNM	ANSN2382
		IF(AMIN1(E5,E6) .GT. 0.0)GO TO 6007	ANSN2383
		IF(IFLU-1)6002,6007,6003	ANSN2384
C	*****	STEP FUNCTION MODEL	ANSN2385
	6002	E3=(XNRI + DSLM*XNM + DAIM*PHIM)/(E1 + DSKM + DBIM)	ANSN2386
		E5=E3	ANSN2387
		E6=E3	ANSN2388
		GC TO 6007	ANSN2389
C	*****	WEIGHTED DIFFERENCE MODEL	ANSN2390
C	*****	COMPUTE WEIGHTED SPACE TERMS	ANSN2391
	6003	IF(XNM.LE.0.0)GO TO 7001	ANSN2392
	7005	XNUM=E1 + DBIM + DBIM	ANSN2393
		XDEN=XNUM - DSLM - (DAIM*PHIM + XNRI)*0.9/XNM	ANSN2394
		IF(XDEN+XDEN .LE. XNUM) GO TO 7001	ANSN2395
		IF(XDEN-XNUM)7006,7003,7001	ANSN239
	7006	BBE=XNUM/XDEN	ANSN2397
	7004	XD1=DSLM - DSKM + DPM*DSKM	ANSN2398
		GO TO 7002	ANSN2399
	7003	XD1=DSLM	ANSN2400
		BBE=1.0	ANSN2401
		GO TO 7002	ANSN2402
	7001	XD1=DSKM2	ANSN2403
		BBE=2.0	ANSN2404
C	*****	COMPUTE WEIGHTED ANGLE TERMS	ANSN2405
	7002	IF(PHIM.LE.0.0)GO TO 7011	ANSN2406
	7015	XNUM=E1 + DSKM + DSKM	ANSN2407
		XDEN=XNUM - DAIM - (DSLM*XNM + XNRI)*0.9/PHIM	ANSN2408
		IF(XDEN+XDEN .LE. XNUM) GO TO 7011	ANSN2409
		IF(XDEN-XNUM)7016,7013,7011	ANSN2410
	7016	CCC=XNUM/XDEN	ANSN2411
	7014	XD2=DAIM - DBIM + CCC*DBIM	ANSN2412
		GO TO 6004	ANSN2413

Figure B1 (contd.)

7013	XD2=DAIM	ANSN2414
	CCC=1.0	ANSN2415
	GO TO 6004	ANSN2416
7011	XD2=DBIM2	ANSN2417
	CCC=2.0	ANSN2418
6004	$E3=(XNRI + XD1*XNM + XD2*PHIM)/(E1 + XD1 + XD2)$	ANSN2419
	$E5=CCC*(E3-PRIM) + PHIM$	ANSN2420
	$E6=BBB*(E3-XNM) + XNM$	ANSN2421
	GO TO 6007	ANSN2422
C	***** INITIAL DIRECTION FLUX CALCULATION - W.EQ.0	ANSN2423
C	***** ON SLAB FLUX CALCULATION - IGE.EQ.1	ANSN2424
6006	IF(IFLU-2)6011,6012,6013	ANSN2425
C	***** LINEAR MODEL	ANSN2426
6011	$E3=(XNRI + DSKM2*XNM)/(E1 + DSKM2)$	ANSN2427
	E5=E3	ANSN2428
	$E6=E3 + E3 - XNM$	ANSN2429
	IF(E6.GT.0.0)GO TO 6007	ANSN2430
	IF(IFLU-1)6012,6007,6013	ANSN2431
C	***** STEP FUNCTION MODEL	ANSN2432
6012	$E3=(XNRI + DSLM*XNM)/(E1 + DSLM)$	ANSN2433
	E5=E3	ANSN2434
	E6=E3	ANSN2435
	GO TO 6007	ANSN2436
C	***** WEIGHTED DIFFERENCE MODEL	ANSN2437
C	***** COMPUTE WEIGHTED SPACE TERMS	ANSN2438
6013	IF(XNM.LE.0.0)GO TO 7021	ANSN2439
7025	DBIM2=DSLM - DSKM	ANSN2440
	XNUM=E1 + DBIM2	ANSN2441
	$XDEN=XNUM - DSLM - XNRI*0.9/XNM$	ANSN2442
	IF(XDEN+XDEN .LE. XNUM) GO TO 7021	ANSN2443
	IF(XDEN-XNUM)7026,7023,7021	ANSN2444
7026	BBB=XNUM/XDEN	ANSN2445
7024	$XD1=DBIM2 + BBB*DSKM$	ANSN2446
	GO TO 7022	ANSN2447
7023	XD1=DSLM	ANSN2448
	BBB=1.0	ANSN2449
	GO TO 7022	ANSN2450
7021	XD1=DSKM2	ANSN2451
	BBB=2.0	ANSN2452
7022	$E3=(XNRI + XD1*XNM)/(E1 + XD1)$	ANSN2453
	E5=E3	ANSN2454
	$E6=BBB*(E3-XNM) + XNM$	ANSN2455
6007	CONTINUE	ANSN2456
C	SPUTTERING CHANGE - SAVE CSD FOR CURRENT GROUP	
6008	$E3SAV(I,M)=E3*SIGSD(IIG)$	
	$E3=E3*WM$	ANSN2457
	$XNE(I)=E5$	ANSN2458
	$XNM=E6$	ANSN2459
C	*** COMPUTE TOTAL FLUX (SCALAR)	ANSN2460
	$XNM(I)=XNM(I) + E3$	ANSN2461
	IF(ISCT.EQ.0)GO TO 33	ANSN2462
C	*** COMPUTE P-L CURRENTS	ANSN2463

Figure B1 (contd.)

IR=I	ANSN2464
MR=M	ANSN2465
DO 32 M=1, JT	ANSN2466
XNA(IM)=XNA(IM) + PNC(M)*E3	ANSN2467
IR=IR + IM	ANSN2468
32 MR=MR + MM	ANSN2469
33 IF(DSNM.LT.0.0)GO TO 25	ANSN2470
C *** ADD SHELL SOURCE TO FLUX WHEN MU.GT.0	ANSN2471
IF(IPM-1)25,34,35	ANSN2472
35 IGMPI=IGMIP - : : :	ANSN2473
XNM=XNM + PA(IGMPI)	ANSN2474
GO TO 25	ANSN2475
34 IF(IPP.EQ.I)XNM=XNM + PAIGMM	ANSN2476
25 CONTINUE	ANSN2477
C *** SAVE BOUNDARY FLUX	ANSN2478
IGMPM=IGMPH + M	ANSN2479
B(IGMPM)=E6	ANSN2480
C *** SAVE LAST ANGULAR FLUX	ANSN2481
IPML=IPMM + IABS(100-IP)	ANSN2482
XND(IPML)=E6	ANSN2483
5 CONTINUE	ANSN2484
845 E1=0.0	ANSN2485
E2=0.0	ANSN2486
IF(IBL.EG.1)GO TO 3337	ANSN2487
J=1	ANSN2488
DO 37 M=1, MM	ANSN2489
E1=E1 + WD(M)*XND(I)	ANSN2490
37 I=I + IP	ANSN2491
3337 J=IP	ANSN2492
DO 337M=1, MM	ANSN2493
E2=E2 + WD(M)*XND(J)	ANSN2494
337 J=J + IP	ANSN2495
C *** COMPUTE LEAKAGE	ANSN2496
RL=E2*AA(IP)	ANSN2497
XLL=E1*AA(1)	ANSN2498
XNLGG=RL - XLL	ANSN2499
833 IIC=IIC+1	ANSN2500
E1=0.0	ANSN2501
ESC=C.0	ANSN2502
ESM=0.0	ANSN2503
EAM=0.0	ANSN2504
C *** COMPUTE CONVERGENCE NUMBERS	ANSN2505
IGMPII=IGMPI + 1	ANSN2506
DO 38 I=1, IM	ANSN2507
E4=XNM(I) - XN(IGMPII)	ANSN2508
IGMPII=IGMPII + 1	ANSN2509
E2=CS(I)*E4	ANSN2510
E1=E1+E2	ANSN2511
ESM=ESM + ABS(E2)	ANSN2512
EAM=EAM + ABS(E4)*(CT(I)-CS(I))	ANSN2513
E4=ABS(E4 / XNM(I))	ANSN2514
IF(E4.LT.ESC)GO TO 38	ANSN2515

Figure B1 (contd.)

IFDMX=I	ANSN2516
ESC=E4	ANSN2517
30 CONTINUE	ANSN2518
ESM=AMAX1(ESM,EAP)	ANSN2519
C *** COMPUTE INNER ITERATION SCALE FACTOR	ANSN2520
E1=Z21/(Z21-E1)	ANSN2521
IF(E1.LE.0.0.OR.E1.GT.10.0)E1=10.0	ANSN2522
IF(ICMC.EQ.1)GO TO 124	ANSN2523
C *** COMPUTE SPACE DEPENDENT SCALE FACTORS	ANSN2524
C *** COMPUTE LEAKAGE TERMS AND SHELL SOURCE CONTRIBUTION TO Q	ANSN2525
DO 100 I=1,ICMC	ANSN2526
DC(IM +I)=0.0	ANSN2527
XNR(I)=0.0	ANSN2528
100 XNE(I)=0.0	ANSN2529
IGMPII=IGMPI + 1	ANSN2530
DO 101 I=1,IM	ANSN2531
II=NO(I)	ANSN2532
XNE(II)=XNE(II) + SR(I)	ANSN2533
C SPUTTERING CHANGE - PRESERVE BALANCE FOR CONVERGENCE TESTS	
DO 888 M=1,MM	
888 XNE(II)=XNE(II)+E3SAV2(I,M)*V(I)*W(M)	ANSN2534
XNR(II)=XNR(II) + CS(I)*(XN(ICAPII)-XNR(II))	ANSN2535
DC(IM +II)=DC(IM +II) + CS(I)*XNN(I)	ANSN2536
SP=0.0	ANSN2537
SM=0.0	ANSN2538
IF(IPM-1)108,102,103	ANSN2539
102 IF(IPP.NE.I)GO TO 108	ANSN2540
J=1	ANSN2541
GO TO 104	ANSN2542
103 J=I	ANSN2543
104 IGMIJ=IGMI + J*MM + 1	ANSN2544
DO 1011 M=1,MM	ANSN2545
E3=PA(IGMIJ)*ABS(WD(M))	ANSN2546
IGMIJ=IGMIJ+1	ANSN2547
IF(WD(M).LT.0.0)GO TO 105	ANSN2548
SP=SP + E3	ANSN2549
GO TO 1011	ANSN2550
105 SM=SM + E3	ANSN2551
1011 CONTINUE	ANSN2552
XNE(II)=XNE(II) + SM*AA(I+1)	ANSN2553
IF(I+1 .EQ. NO(IM+II))GO TO 106	ANSN2554
XNE(II)=XNE(II) + SP*AA(I+1)	ANSN2555
GO TO 108	ANSN2556
106 IF(II.NE.ICMC)XNE(II+1)=XNE(II+1) + SP*AA(I+1)	ANSN2557
108 IGMPII=IGMPII+1	ANSN2558
101 CONTINUE	ANSN2559
II1=1	ANSN2560
DO 109 I=1,ICMC	ANSN2561
DC(IM +I)=DC(IM +I)*0.25	ANSN2562
II2=NO(IM+I)	ANSN2563
II1S=II1	ANSN2564
II2S=II2	

Figure B1 (contd.)

XLM=0.0	ANSN2565
XLP=0.0	ANSN2566
DO 115 M=1,MM	ANSN2567
IF(WD(M).GT.0.0)GO TO 116	ANSN2568
XLP=XLP + XND(II2)*ABS(WD(M))	ANSN2569
GO TO 117	ANSN2570
116 XLM=XLM + XND(II1)*WD(M)	ANSN2571
117 II1=II1 + IP	ANSN2572
115 II2=II2 + IP	ANSN2573
II1=II2S	ANSN2574
ST(I)=-XLP*AA(II2S)	ANSN2575
109 SAT(I)=-XLM*AA(II1S)	ANSN2576
FLUXP=DC(IM +1)	ANSN2577
DO 118 I=1,ICMC	ANSN257
FLUXM=FLUXP	ANSN2579
IF(I.EQ.ICMC)GO TO 8001	ANSN2580
FLUXP=AMAX1(DC(IM +I),DC(IM +I+1))	ANSN2581
GO TO 8002	ANSN2582
8001 FLUXP=DC(IM +I)	ANSN2583
8002 ST(I)=ST(I)-FLUXP	ANSN2584
SAT(I)=SAT(I)-FLUXM	ANSN2585
118 XNR(I)=XNR(I) + XNE(I) - ST(I) - SAT(I)	ANSN2586
C ***	ANSN2587
C *** SOLVE TRI-DIAGONAL MATRIX	ANSN25
C ***	ANSN2589
C *** COMPUTE A(1) AND A(J)	ANSN2590
XNR(1)=XNR(1) + SAT(1)	ANSN2591
XNR(ICMC)=XNR(ICMC) + ST(ICMC)	ANSN2592
C *** REMOVE B TERMS FROM MATRIX	ANSN2593
J=1	ANSN2594
DO 111 I=2,ICMC	ANSN2595
COEF=SAT(I)/XNR(J)	ANSN2596
XNR(I)=XNR(I) - COEF*ST(J)	ANSN2597
XNE(I)=XNE(I) - COEF*XNE(J)	ANSN2598
111 J=J+1	ANSN2599
C *** SOLVE FOR F(I)	ANSN2600
I=ICMC	ANSN2601
DO 112 J=2,ICMC	ANSN2602
XNE(I)=XNE(I)/XNR(I)	ANSN2603
IF(XNE(I).LT.0.0)GO TO 124	ANSN2604
J=I-1	ANSN2605
112 XNE(I)=XNE(I) - XNE(I+1)*ST(I)	ANSN2606
XNE(1)=XNE(1)/XNR(1)	ANSN2607
IF(XNE(1).LT.0.0)GO TO 124	ANSN2608
C ***	ANSN2609
C *** MATRIX SOLVED	ANSN2610
C ***	ANSN2611
I=IM	ANSN2612
DO 119 J=1,IM	ANSN2613
II=NO(I)	ANSN2614
XNE(I)=XNE(II)	ANSN2615
119 I=I-1	ANSN2616

Figure B1 (contd.)

Figure A1 (contd.)

DO 114 I=1,IM	ANSN2617
114 SAT(I)=0.0	ANSN2618
GO TO 125	ANSN2619
C *** APPLY SPACE DEPENDENT SCALE FACTORS	ANSN2620
124 DO 123 I=1,IM	ANSN2621
123 XNE(I)=E1	ANSN2622
125 DO 39 I=1,IM	ANSN2623
IF(ABS(1.0 - XNE(I)).LT.SCLMX)GO TO 39	ANSN2624
SCLMX=ABS(1.0 - XNE(I))	ANSN2625
SCLXX=XNE(I)	ANSN2626
ISMX=I	ANSN2627
39 INN(I)=XNN(I)*XNE(I)	ANSN2628
122 IF(ISCT.EQ.C)GO TO 3399	ANSN2629
DO 339 I=1,IM	ANSN2630
IN=I	ANSN2631
DO 40 N=1,JI	ANSN2632
XNA(IN)=XNA(IN)*XNE(I)	ANSN2633
40 IN=IN + IM	ANSN2634
339 CONTINUE	ANSN2635
3399 E1=XNE(1)	ANSN2636
E2=XNE(IM)	ANSN2637
IGMPMM=IGMPM+1	ANSN2638
DO 41 M=1,MM	ANSN2639
IF(WD(M).GT.0.0)GO TO 441	ANSN2640
B(IGMPMM)=B(IGMPMM)*E1	ANSN2641
GO TO 41	ANSN2642
441 B(IGMPMM)=B(IGMPMM)*E2	ANSN2643
41 IGMPMM=IGMPMM + 1	ANSN2644
C *** TEST CONVERGENCE	ANSN2645
IF((XITR.EQ.0 .AND. IBR.EQ.0) .OR. IIC.GE.IIM)GO TO 42	ANSN2646
IF(ESM.GT.EPG .AND. ESC.GT.EPS .OR. XLAL.GT.0.0 .AND.	ANSN2647
1 ESC.GT.XLAL)GO TO 832	ANSN2648
42 K=1	ANSN2649
DO 43 M=1,MM	ANSN2650
WDM=WD(M)	ANSN2651
J=K+1	ANSN2652
DO 443 I=1,IM	ANSN2653
XNEI=XNE(I)	ANSN2654
IF(WDM.LT.0.0 .OR. I.EQ.1)XND(K)=XND(K)*XNEI	ANSN2655
IF(WDM.GT.0.0 .OR. I.EQ.IM)XND(J)=XND(J)*XNEI	ANSN2656
K=K+1	ANSN2657
C SPUTTERING CHANGE - SAVE CSD FOR NEXT GROUP	
E3SAV2(I,M)=E3SAV1(I,M)	
443 J=J+1	ANSN2658
K=J	ANSN2659
43 CONTINUE	ANSN2660
XNLGG=RL*E2 - XLL*E1	ANSN2661
IF(ICVT.NE.1)GO TO 999	ANSN2662
IF(IIG.EQ.1)WRITE(NOU,60)	ANSN2663
WRITE(NOU,70) IIG,JIC,IFDMX,ESC,ISMX,SCLXX,ICMC	ANSN2664
60 FORMAT(76X,' GROUP INNER MFD MAX. FLUX M&F MAX. SCALE COA	ANSN2665
*RSE'/83X,'ITERS INT. DIFFERENCE INT. FACTOR MESH')	ANSN2666

Figure B1 (contd.)

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70 FORMAT(76X,3I6,1PE13.5,I6,E13.5,I6) ANSN2667
999 RETURN ANSN2668
END ANSN2669
SUBROUTINE SUMMARY(XKI,FD,XN, VE,W,DSN,MA,MZ,CRX,Q,PA,DF,I2,CA,CF, ANSN3072
1CT,CS,V,AA,TAB,WD,XND,FXS,FIS,SNM,SFS,OTS,APS,FRT,TXN,DEN,RFL,RCT, ANSN3073
2RLK,XLL,XLK,XBB,RXN,IG1,I1,IH1,IGM1,M1,IM1) ANSN3074
C *** SUMMARY PRINTS ANGULAR FLUXES AND COMPUTES SUMMARY TABLES ANSN3075
C SPUTTERING CHANGE - SETUP ARRAYS, COMMON/SPUT/
REAL*8 EBT,UO
DIMENSION E(50,2),R(50,33),ETA(16,2),WT(16)
COMMON/SPUT/SIGSD(50),ZET(51),UO,NI
DIMENSION XKI(1),FD(1),XN(1:1), VE(1),W(1),DSN(1),MA(1),MZ(1) ANSN3076
1,CRX(IH1,IGM1,1),Q(I1,1),FA(M1,IM1,1),DF('),CA(1),CF(1),CT(1), ANSN3077
2 CS(1),V(1),AA(1),TAB(1),WD(1),XND(I2,1),FXS(IG1,1),FIS(IG1,1), ANSN3076
3 SNM(IG1,1),SFS(IG1,1),OTS(IG1,1),APS(IG1,1),XLK(IG1,1),XBB(IG1,1) ANSN3079
4,RXN(IG1,1),RFL(IG1,1),RCT(IG1,1),RLK(IG1,1),XLL(IG1,1),FRT(IG1,1) ANSN3080
5,TXN(IG1,1),DEN(IC1,1) ANSN3081
COMMON /BULKPR/ ANSN3082
$ D(1),LIM1,LXN1,LFD,LXN,LR,LVE,LW,LDSN,LMA,LMZ,LMB,LMC,LXND, ANSN3083
1LMTT,LCRX,LFIX,LFLT,LQ,LPA,LJ5,LRM,LDF,LJ3,LJ4,LJ3T,LART,LALFT, ANSN3084
2LFGP,LFGG,LEND,LV,LAA,LJD,LMP,LPC,LXJ,LCH,LCA,LCF,LCT,LCS,LTAB, ANSN3085
3LXND,LSA,LSAT,LRAV,LRA,LXNN,LXNE,LXNR,LXNA,LSR,LST,LQG,LFG,LSG, ANSN3086
4LXKF,LXNI,LXNO,LT3,LT5,LDA,LDB,LDC,LDS,LB,IGMP,IGMM,IIGG,NERR,IMJT ANSN3087
5,IHG,IMP,MP,NDS,NUS,SDG,SCG,AG,XNLGG,XNLG,SMG,ALA,ASR,EAM,EPG,EQ, ANSN3088
6E1,E2,E3,E4,E5,E6,E7,E8,E9,E10,E11,E12,E13,E14,E15,E16,E17,E18,E19 ANSN3089
7,E20,ESC,ESM,FVP,EVPP,FPT,IC,ICVT,IGP,JG,IHP,IIC,IIG,IP,IZT,I01, ANSN3090
8I02,I03,I04,I05,I06,I07,I08,I09,I00,JT,LC,MG,MI,ML,MM,NFN,XITR, ANSN3091
9XLAP,XLAPP,XLAR,XLA,XNIO,XNII,ZZ1,ZZ2,ZZ3,XNB,YKEP,YKIP,IH,I,K,L, ANSN3092
AM,J,N,NN,13V, ANSN3093
EID,ITH,ISCT,ISN,IGE,JBL,IBR,IZM,IM,IEVT,JGM,IHT,IHS,IHM,MS,MCR,MTP ANSN3094
C,MT,IDFM,IPVT,JQM,IPM,IPP,JIM,ID1,ID2,ID3,ID4,ICM,IDAT1,IDAT2,IPG, ANSN3095
DIFLU,IFN,IPRT,IXTR, ANSN3096
EEV,EVM,EPS,BF,DY,DZ,DFM1,XNF,PV,PYF,XLAL,XLAK,EQL,XNPM, ANSN3097
FT(12),WIN,NOU,NT1,NT2,NT3,NT4,NT5,NT6,NT7 ANSN3098
C SPUTTERING CHANGE - CALCULATE ANGULAR RESPONSE FUNCTION, R
NT=ICM-NI
JSN=ISN
WRITE(6,2000)N1,NT,JSN,UO
2000 FORMAT(1H1,I5,' ICN GROUPS;',I5,'TARGET ATOM GROUPS; S',I2,
1 ' UO=',D15.5)
JSN=JSN/2
NTP1=NT+1
JEN1=JSN+1
DO 105 I=1,JSN
105 WT(I)=W(I+1)
WRITE(6,2005)
2005 FORMAT('0 TARGET ATOM GROUP BOUNDARIES AND SN WEIGHTS')
WRITE(6,2010)(EBT(J),I=1,NTP1)
WRITE(6,201C)(WT(I),I=1,JSN)
2010 FORMAT(1H ,7E15.5)
DO 110 JG=1,NT
E(JG,1)=EFT(JG+1)

```

Figure B1 (contd.)

```

110  E(JG,2)=EET(JG)
      ETA(1,1)=0.0
      ETA(1,2)=2.*WT(1)
      DO 120 IA=2,JSN
      ETA(IA,1)=ETA(IA-1,2)
120  ETA(IA,2)=ETA(IA,1)+2.*WT(IA)
      JSN2=2*JSN+1
      NTOT=NI+NT
      DO 130 JG=1,NTOT
      DO 130 IA=1,JSN2
130  R(JG,IA)=0.0
      DO 140 JG=1,NT
      IGG=NI+JG
      DO 140 IA=1,JSN
      IAA=JSN1-IA+1
      EA=E(JG,1)*ETA(IA,1)**2
      EB=E(JG,2)*ETA(IA,1)**2
      EC=E(JG,1)*ETA(IA,2)**2
      ED=E(JG,2)*ETA(IA,2)**2
      IF(EA.GT.UO) GO TO 101
      IF(ED.LT.UO) GO TO 106
      IF(EC.GT.UO) GO TO 102
      ETAL=ETA(IA,1)**2
      IF(EB.LT.UO) ETAL=UO/E(JG,2)
      R(IGG,IAA)=(ETA(IA,2)**2+ETAL)/2./UO-1./E(JG,2)
      R(IGG,IAA)=R(IGG,IAA)/(1./E(JG,1)-1./E(JG,2))
      IF(EB.LT.UO) R(IGG,IAA)=R(IGG,IAA)*(ETA(IA,2)**2-ETAL)/
1  (ETA(IA,2)**2-ETA(IA,1)**2)
      GO TO 140
101  R(IGG,IAA)=1.0
      GO TO 140
102  EU=E(JG,2)
      IF(EB.GT.UO) EU=UO/ETA(IA,1)**2
      R(IGG,IAA)=UC*(1./E(JG,1)+1./EU)/2.-ETA(IA,1)**2
      IF(EB.LT.UO) R(IGG,IAA)=R(IGG,IAA)*(1./E(JG,1)-1./EU)/
1  (1./E(JG,1)-1./E(JG,2))
      R(IGG,IAA)=1.-R(IGG,IAA)/(ETA(IA,2)**2-ETA(IA,1)**2)
      GO TO 140
106  R(IGG,IAA)=0.0
140  CONTINUE
      WRITE(6,2015)
2015  FORMAT(///' ANGULAR LEAKAGE RESPONSE FOR SPATTERING PROBLEM'//)
      DO 170 JG=1,NTOT
      DO 169 IA=2,JSN1
      RTEMP=R(JG,IA)
      IATP=JSN2-IA+2
      R(JG,IA)=R(JG,IATP)
169  R(JG,IATP)=RTEMP
      WRITE(6,2020) JG,JSN2
170  WRITE(6,2010) (R(JG,IA),IA=1,JSN2)
2020  FORMAT('          R(',I2,',',IA),IA=1,',',I2)
      DO 1 IIC=1,IGM

```

ANSN3099

Figure B1 (contd.)

	IIGG=IIG	ANSN3100
	CALL WANDR1 ( 3 ,XND,IP*MM,2)	
	IF(ID1.EQ.C .OR. ID1.EQ.2)GO TO 2	ANSN3102
C	*** PRINT ANGULAR FLUX	ANSN3103
	WRITE (NOU,10)IIG	ANSN3104
	10 FORMAT(3F1 FLUX BY ANGLE AND POINT FOR GROUP I3)	ANSN3105
	CALL WOT(XND,MM,IP,1,'PNT.','ANGL',0,NOU)	
	2 IF(IDAT1.EQ.0)GO TO 3	ANSN5107
	IIGG=1	ANSN3108
	CALL WANDR1 (NT3,CRY,IHP*MT,2)	03439060
	IO1=MP*IMP	AKSN3110
	IF(IQM+IPM.NE.0) CALL WANDR1 (NT3,Q,IO1,2)	
C	*** COMPUTE SUMMARY TABLES	ANSN3112
	3 IH=IHM	ANSN3113
	4 K=IIG+IIS-IF	AKSN3114
	IF(K.LE.0)GO TO 5	ANSN3115
	IF(K.GT.IGM)GO TO 6	ANSN3116
	IF(ID/T1.NE.2)GO TO 7	ANSN3117
	K=1	AKSN3118
	CALL WANDR1 (NT1,XN,IM,2)	03453000
	IF(ISCT.GT.0)READ (NT1)	ANSN3120
	7 DO 8 I=1,IM	ANSN3121
	J=MA(I)	ANSN3122
	L=JABS(MZ(J))	ANSN3123
	J=MINO(J,I,ZH)	ANSN3124
	E4=V(I)	ANSN3125
	IF(IDPM.GT.0)E4=E4*TF(I)	ANSN3126
	IF(IH.NE.IHS)GO TO 39	ANSN3127
	CS(I)=ZN(I,K)	ANSN3128
	E1=CRX(IHT,IIGG,L)	ANSN3129
	E2=CRX(IHT-2,IIGG,L)	ANSN3130
	E2=0.0	ANSN3131
	IF(IDPM.EQ.0)GO TO 11	ANSN3132
	E1=E1*DF(I)	ANSN3133
	E2=E2*DF(I)	ANSN3134
C	*** TRANSVERSE BUCKLING CORRECTION	ANSN3135
	11 IF(DY.GT.0.0) E3=3.289866*E1/(DY*E1 +EF)**2	ANSN3136
	IF(DZ.GT.0.0) E3=E3 + 3.289866*E1/(DZ*E1 + RF)**2	ANSN3137
	CT(I)=(E1 + TAB(IIG) + E3)*CS(I) *V(I)	ANSN3138
	CA(I)=(E2 + TAB(IIG) + E3)*CS(I) *V(I)	ANSN3139
	GO TO 8	ANSN3140
C	*** FXS - FIXED SOURCE	ANSN3141
C	*** FIS - FISSION SOURCE	ANSN3142
C	*** SMN - SCATTER GAINS	ANSN3143
C	*** SFS - SELF SCATTER	ANSN3144
C	*** OTS - SCATTER LOSSES	AKSN3145
C	*** APS - ABSORPTIONS	AKSN3146
C	*** XLK - NET LEAKAGE	ANSN3147
C	*** XBB - NEUTRON BALANCE (GAINS/LOSSES)	ANSN3148
C	*** RXN - FLUX AT RIGHT BOUNDARY	ANSN3149
C	*** RFL - J+ AT RIGHT BOUNDARY	ANSN3150
C	*** RCT - J-NET AT RIGHT BOUNDARY	ANSN3151

Figure B1 (contd.)

C	*** RLK - RIGHT LEAKAGE	ANSN3152
C	*** XLL - LEFT LEAKAGE	ANSN3153
C	*** FRT - FISSION RATE	ANSN3154
C	*** TXN - TOTAL FLUX	ANSN3155
C	*** DEN - DENSITY	ANSN3156
	39 SWN(IIG,J)=SWN(IIG,J) + CRX(IH,IIGG,L)*XN(I,K)*EA	ANSN3157
	8 CONTINUE	ANSN3158
	5 IH=IH-1	ANSN3159
	IF(IE.GT.IHT)GO TO 4	ANSN3160
	6 IF(IDAT1.NE.2)GO TO 35	ANSN3161
	IF(WDS.LT.IIG .AND. JIG.NE.IGM)GO TO 43	ANSN3162
	REWIND NT1	ANSN3163
	GO TO 35	ANSN3164
	43 N=NDS + MIMO(NUS,IGM-IIG)	ANSN3165
	IF(ISCT.GT.0)N=N+N	ANSN3166
	DO 36 I=1,N	ANSN3167
	36 BACKSPACE NT1	ANSN3168
	35 E1=EV	ANSN3169
	IF(IEVT.NE.1)E1=1.0	ANSN3170
	IGI=(IIGG-1)*MP*IMP	ANSN3171
	DO 9 I=1,IM	ANSN3172
	J=MA(I)	ANSN3173
	K=IABS(MZ(J))	ANSN3174
	J=MIMO(J,IZM)	ANSN3175
	EA=V(I)	ANSN3176
	IF(IPM.GT.0)EA=EA*LP(I)	ANSN3177
	IF(ITH.EQ.0)GO TO 41	ANSN3178
	FIS(IIG,J)=FIS(IIG,J) + CRX(IHT-1,IIGG,K)*FD(I)*EA	ANSN3179
	GO TO 42	ANSN3180
	41 FIS(IIG,J)=FIS(IIG,J) + XKI(IIG)*FD(I)*V(I)/E1	ANSN3181
	42 SFS(IIG,J)=SFS(IIG,J) + CS(I)*CRX(IHS,IIGG,K) *EA	ANSN3182
	OTS(IIG,J)=OTS(IIG,J) + CT(I)	ANSN3183
	APS(IIG,J)=APS(IIG,J) + CA(I)	ANSN3184
	TXN(IIG,J)=TXN(IIG,J) + CS(I)*V(I)	ANSN3185
	JF(IQM.NE.0)FXS(IIG,J)=FXS(IIG,J) + Q(IGI+I,1)*V(1)	ANSN3186
	9 FRT(IIG,J)=FRT(IIG,J) + CS(I)*CRX(IHT-1,IIGG,K)*EA	ANSN3187
	DO 12 J=1,IZM	ANSN3188
	DEN(IIG,J)=TXN(IIG,J)/VE(IIG)	ANSN3189
	12 OTS(IIG,J)=OTS(IIG,J) - APS(IIG,J) - SFS(IIG,J)	ANSN3190
	IF(IPM.EQ.0)GO TO 13	ANSN3191
	J=MIMO(IZM,MA(IPP))	ANSN3192
	JJ=J	ANSN3193
	IF(IPP.NE.IM)JJ=MIMO(IZM,MA(IPP+1))	ANSN3194
	DO 17 I=1,IM	ANSN3195
	IF(IPM.EQ.1)GO TO 1007	ANSN3196
	J=MIMO(IZM,MA(I))	ANSN3197
	JJ=J	ANSN3198
	IF(I.NE.IM)JJ=MIMO(IZM,MA(I+1))	ANSN3199
1007	E3=0.0	ANSN3200
	E4=0.0	ANSN3201
	DO 16 M=1,MM	ANSN3202
	E2=PA(M,I,IIGG)*ABS(WD(M))	ANSN3203

Figure B1 (contd.)

IF(WD(M).LY.O.O)GO TO 1005	ANSN320A
E3=E3 + E2	ANSN3205
GO TO 16	ANSN3206
1005 E4=E4 + E2	ANSN3207
16 CONTINUE	ANSN3208
IF(IPM.EQ.1)GO TO 15	ANSN3209
IF(I.EQ.IM)GO TO 17	ANSN3210
FXS(IIG,JJ)=FXS(IIG,JJ) + E3*AA(I+1)	ANSN3211
17 FXS(IIG,J)=FXS(IIG,J) + E4*AA(I+1)	ANSN3212
GO TO 13	ANSN3213
15 IF(IPP.EQ.IM)GO TO 1006	ANSN3214
FXS(IIG,JJ)=FXS(IIG,JJ) + E3*AA(IPP+1)	ANSN3215
1006 FXS(IIG,J)=FXS(IIG,J) + E4*AA(IPP+1)	ANSN3216
13 DO 18 J=1,IZP	ANSN3217
IF(J.NE.IZP .AND. IZH.NE.1)GO TO 24	ANSN3218
I01=1	ANSN3219
I02=IM	ANSN3220
GO TO 25	ANSN3221
24 DO 19 I01=1,IM	ANSN3222
IF(J.EQ.MA(I01))GO TO 21	ANSN3223
19 CONTINUE	ANSN3224
21 I02=IP	ANSN3225
22 I02=I02-1	ANSN3226
IF(J.NE.MA(I02))GO TO 22	ANSN3227
25 DO 23 M=1,MM	ANSN3228
RXM(IIG,J)=RXM(IIG,J) + XND(I02+1,M)*W(M)	ANSN3229
IF(WD(M).GT.O.O)RFL(IIG,J)=RFL(IIG,J) + XND(I02+1,M)*WD(M)	ANSN3230
C SPATTERING CHANGE - FOLD R WITH RIGHT LEAKAGE	
RCT(IIG,J)=RCT(IIG,J)+XND(I02+1,M)*WD(M)*R(IIG,M)	
23 XLL(IIG,J)=XLL(IIG,J)+XND(I01,M)*WD(M)	ANSN3232
RLK(IIG,J)=RCT(IIG,J)*AA(I02+1)	ANSN3233
XLL(IIG,J)=XLL(IIG,J)*AA(I01)	ANSN3234
XLK(IIG,J)=RLK(IIG,J) - XLL(IIG,J)	ANSN3235
16 CONTINUE	ANSN3236
1 CONTINUE	ANSN3237
REWIND 3	
IF(IDAT1.NE.O)REWIND NT3	ANSN3239
37 DO 34 K=1,16	ANSN3240
L=(K-1)*IZP	ANSN3241
M=L+IZP	ANSN3242
10 26 J=1,IZP	ANSN3243
N=L+J	ANSN3244
DO 27 IIG=1,IGM	ANSN3245
E1=FXS(IIG,M)	ANSN3246
IF(J.EQ.IZP)GO TO 28	ANSN3247
FXS(IGP,N)=FXS(IGP,N) + E1	ANSN3248
IF(K.GT.9)GO TO 27	ANSN3249
FXS(IIG,M)=FXS(IIG,M) + E1	ANSN3250
GO TO 27	ANSN3251
28 FXS(IGP,M)=FXS(IGP,M) + E1	ANSN3252
27 CONTINUE	ANSN3253
26 CONTINUE	ANSN3254

Figure B1 (contd.)

```

3A CONTINUE
  DG 29 J=1,IZP
  CT(J)=0.0
  DO 29 IIG=1,IGP
  E1=FXS(IIG,J) + FIS(IIG,J) + SMN(IIG,J) + AMAX1(XLL(IIG,J),0.0)
  * AMIN1(RLK(IIG,J),0.0)
  E2=OTS(IIG,J) + APS(IIG,J) + AMAX1(RLK(IIG,J),0.0) -
  * AMIN1(XLL(IIG,J),0.0)
29 XBB(IIG,J)=E1/E2
  DG 1029 I=1,IM
  J=MA(I)
  CT(J)=CT(J) + V(I)
1029 CT(IZP)=CT(IZP) + V(1)
  DO 38 J=1,IZP
  32 IF(J.EQ.IZP)GO TO 31
C *** PRINT SUMMARY TABLES
  WRITE (NOU,20) J,IGP,CT(J)
20 FORMAT(18H1 SUMMARY FOR ZONE I3,4TH BY GROUP INCLUDING SUM FOR ALLANSW3275
  1 GROUPS IN LINE I3,' VOLUME=',1PE13.5)
  GO TO 33
31 WRITE (NOU,30) CT(IZP)
30 FGMAT(2GH1 SUMMARY FOR SYSTEM,' VOLUME=',1PE13.5)
33 WRITE (NOU,40) (I,FXS(I,J),FIS(I,J),SMN(I,J),SFS(J,J),OTS(I,J),APSAW3280
  1(I,J),RLK(I,J),XBB(I,J),I=1,IGP)
40 FORMAT(108H0 GRP. FIX SOURCE FISS SOURCE IN SCATTER SLF SCATAW3282
  1TER OUT SCATTER ABSORPTION LEAKAGE BALANCE/(I6,1PE13.5ANSW3283
  2))
  WRITE (NOU,50) (I,FXN(I,J),RFL(I,J),RCT(I,J),RLK(I,J),XLL(I,J),PRTAW3285
  1(I,J),TXN(I,J),DEN(I,J),I=1,IGP)
50 FORMAT(108H0 GRP. RT BDY FLUX RT BDY J+ RT BDY J RT LEAKAW3287
  1AGE LFT LEAKAGE FISS RATE TCTAL FLUX DENSITY/(I6,1PE13.5ANSW3288
  2))
38 CONTINUE
  IF(ID.LT.1000000)GO TO 999
  CALL FACTOR(MZ,D(LMB),D(LMC),D(LXMD),MA,V,XN,DF,TAB,IM,IGP)
999 RETURN
  END
//LKED.PROG DD DISP=SHR,DSN=X.WAR14636.WARPROG
  INCLUDE PRG(ANISM)
//GO.FT01F001 DD UNIT=SYSDA,SPACE=(TRK,(100,10),RLSE),
// DCB=(RECFM=VBS,LRECL=X,BLKSIZE=7208)
//GO.FT02F001 DD UNIT=SYSDA,SPACE=(TRK,(100,10),RLSE),
// DCB=(RECFM=VBS,LRECL=Y,BLKSIZE=7208)
//GO.FT03F001 DD UNIT=SYSDA,SPACE=(TRK,(100,10),RLSE),
// DCB=(RECFM=VBS,LRECL=X,BLKSIZE=7208)
//GO.FT04F001 DD DSN=T.TJH45255.XSPU,DISP=SHR
//GO.FT07F001 DD SYSOUT=B
//GO.FT03F001 DD UNIT=SYSDA,SPACE=(TRK,(100,10),RLSE),
// DCB=(RECFM=VBS,LRECL=X,BLKSIZE=7208)
//GO.FT09F001 DD UNIT=SYSDA,SPACE=(TRK,(100,10),RLSE),
// DCB=(RECFM=VBS,LRECL=X,BLKSIZE=7208)
//GO.FT05F001 DD #

```

Figure B1 (contd.)

SPUTTERING: H->N1 20GPS

15\$\$ 1 0 19 32 1 0 0 1 200 0 20 3 4 23 20 0 20 20 0 0 0 1 200 30 0 0  
0 0 1 0 0 0 3 1 0 0

16\*\* 2R0.0 0.001 ARC.0 1.0 0.0 0.5 0.0001 3R0.0 T

13\$\$ 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20

T

18\*\* 0.0 1.0 F0.0 T

3\*\* F0.0 T

1\*\* F0.0

4\*\* 99I0.0 99I1000. 2000.

5\*\* F1.0

6\*\*

0. .0067881 .0155634 .0237896 .0311572 .037399 .0422891 .0456508  
.0473626 .0473626 .0456508 .0422891 .037399 .0311572  
.0237896 .0155634 .0067881 1N16

7\*\*

-1. -.9947 -.972286 -.932815 -.877701 -.808937 -.729008 -.640801  
-.547506 -.452494 -.355198 -.270992 -.191062 -.122298 -.0671843  
-.0277125 -.00529954 1N16

8\$\$ F1

9\$\$ 1

10\$\$ 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20

11\$\$ FC

12\*\* F1.0

19\$\$ 19

T T

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