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ICECO-CEL:
A COUPLED EULERIAN-LAGRANGIAN CODE
FOR ANALYZING PRIMARY SYSTEM RESPONSE
IN FAST REACTORS

by

C. Y. Wang

BASE TECHNOLOGY



ARGONNE NATIONAL LABORATORY, ARGONNE, ILLINOIS

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C. Y. Wang

Reactor Analysis and Safety Division

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ABSTRACT

This report describes a coupled Eulerian-Lagrangian code, ICECO-CEL, for analyzing the response of the primary system during hypothetical core disruptive accidents. In the analysis, the implicit Eulerian method is used to calculate the fluid motion so that large fluid distortion, two-dimensional sliding interface, flow around corners, flow through coolant passageways, and out-flow boundary conditions can be adequately treated. The explicit Lagrangian formulation is employed to compute the response of the containment vessel and other elastic-plastic solids inside the reactor containment. Large displacements, as well as geometrical and material nonlinearities are considered in the analysis. Marker particles are utilized to define the free surface or the material interface, and to aid the visualization of the fluid motion.

In this report the basic equations and numerical techniques used in the Eulerian hydrodynamics and Lagrangian structural dynamics are described in detail. Treatment of the above-core hydrodynamics, sodium spillage, fluid cavitation, free-surface boundary conditions and heat transfer are also presented, together with the assumptions and limitations of the mathematical model used in the analysis. Many examples are given to illustrate the capabilities of the computer code. Comparisons of the code predictions with available experimental data are also made.

I. INTRODUCTION

Although the occurrence of energy excursions in a Liquid Metal Fast Breeder Reactor (LMFBR) has extremely low probability, safety analysis of LMFBR requires an analysis on the capability of the primary containment system to sustain the severe consequences of Hypothetical Core Disruptive Accidents (HCDAs). In the USA the safety criteria [1] requires that the primary containment be remained intact throughout the event of the energy excursion, and the fission-gas products and other harmful radioactive materials be prevented from release to the surrounding environs.

To accomplish this objective safety research groups throughout the world have been developing computer codes for analyzing the transient response of LMFBR subjected to postulated accident loads. Many of the codes currently in use are based on the Lagrangian formulations for both fluid and structural analysis, employing explicit time integration algorithm. The first Lagrangian Containment Code, REXCO-H [2], was developed in 1969 at Argonne National Laboratory. Since then a number of Lagrangian containment codes [3-6] have evolved. Other computer codes developed for different purposes [7-10] have also been applied to safety problems related to LMFBR containment.

Despite the fact that Lagrangian computer codes have been successfully used for analyzing the primary containment response under HCDAs. Their analyses are still limited to the early stages of the excursion, because excessive grid distortions will often deteriorate the accuracy of the numerical results. With the increasing concern for safety design of various LMFBRs and wide range of possible energy excursions, the issues of extended fluid motions accompanying by complex physical phenomena have gathered increasing importance. For instance, in a loop-type LMFBR shown in Fig. 1 concerns arose recently over the above-core hydrodynamics induced by the upper internal structure, the possibility of sodium spillage and its resulting sodium fires in the secondary containment, the expansion and contraction of the core-gas bubble, and the role of fluid cavitation on the containment response.

To assist the Lagrangian codes for analyzing the primary-system response during an HCDA a computer code, ICECO-CEL, is developed, where ICECO and CEL denote

Implicit Continuous-Fluid Eulerian Containment Code and Coupled Eulerian Lagrangian, respectively. This code is an extension of the ICECO code developed [11-14] early. It uses the implicit Eulerian hydrodynamic technique to treat the fluid motion, while employs explicit Lagrangian method to analyze the structural dynamics. These two analyses are coupled together at the interface where boundary conditions are rigorously satisfied. Thus, this program combines the advantages of both Eulerian and Lagrangian coordinate systems. The Eulerian coordinate system remains fixed in space, and can calculate violent fluid motion and fluid flow around irregular objects. The Lagrangian coordinate system moves with the material and can record the histories of the elastic-plastic solid for use in the constitutive equations of complex reactor structures.

In this report the governing equations for treating both fluids and solids are described in detail. Many sample problems are given and their results are discussed. Input instructions are also included.

II. METHODOLOGY

A. Basic Eulerian Hydrodynamics

1. The Partial Differential Equations

The basic differential equations used in the code are the conservation equations of continuum mechanics. Only nonturbulent flow is considered, and no external energy source is assumed to exist inside the flow region. Thus, the mass, momentum, and energy equations are:

$$\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x_i} (\rho u_i) = 0, \quad (1)$$

$$\frac{\partial}{\partial t} (\rho w_i) + \frac{\partial}{\partial x_j} (\rho w_i w_j) = \frac{\partial}{\partial x_i} \sigma_{ij} + \rho g_i, \quad (2)$$

$$\frac{\partial}{\partial t} (\rho E) + \frac{\partial}{\partial x_i} (\rho w_i E) = \frac{\partial}{\partial x_i} (\sigma_{ij} w_j) + \frac{\partial}{\partial x_i} \left(\mu B \frac{\partial I}{\partial x_i} \right) + \rho g_i w_i, \quad (3)$$

in which

$$E = I + \frac{1}{2} w_i w_i. \quad (4)$$

In Eqs. (1-4) ρ is the density; t the time; w_i the velocity component; g_i the component of gravity acceleration; μ the viscosity coefficient; E the specific total energy; I is the specific internal energy. The temperature in the heat conduction term has been eliminated by means of the constant coefficient B ; σ_{ij} is the stress tensor which is a function of the scalar pressure p and a deviatoric stress tensor $\bar{\sigma}_{ij}$, i.e.

$$\sigma_{ij} = -p \delta_{ij} + \bar{\sigma}_{ij}, \quad (5)$$

where δ_{ij} is Kronecker delta.

The deviatoric stress tensor can be written as

$$\bar{\sigma}_{ij} = \mu e_{ij} + \frac{1}{2} \lambda e_{\ell\ell} \delta_{ij},$$

and

(6)

$$e_{ij} = \frac{\partial w_j}{\partial x_i} + \frac{\partial w_i}{\partial x_j},$$

in which λ is another viscosity coefficient. Note that tensor notation is employed, so that repeated indices denote summations.

The coolant motion inside the reactor containment is assumed to be axisymmetric. Substitution of Eqs. (5) and (6) into (2) and (3). The mass, momentum, and energy equations are:

$$\frac{\partial \rho}{\partial t} + \frac{1}{r} \frac{\partial \rho u r}{\partial r} + \frac{\partial \rho v}{\partial z} = 0, \quad (7)$$

$$\frac{\partial \rho u}{\partial t} + \frac{1}{r} \frac{\partial \rho u^2 r}{\partial r} + \frac{\partial \rho u v}{\partial z} = - \frac{\partial}{\partial r} (p + q) + \mu \frac{\partial}{\partial z} \left(\frac{\partial u}{\partial z} - \frac{\partial v}{\partial r} \right), \quad (8)$$

$$\frac{\partial \rho v}{\partial t} + \frac{1}{r} \frac{\partial \rho u v r}{\partial r} + \frac{\partial \rho v^2}{\partial z} = \rho g - \frac{\partial}{\partial z} (p + q) - \frac{\mu}{r} \frac{\partial}{\partial r} \left[r \left(\frac{\partial u}{\partial z} - \frac{\partial v}{\partial r} \right) \right], \quad (9)$$

$$\begin{aligned} \frac{\partial \rho E}{\partial t} + \frac{1}{r} \frac{\partial \rho u E r}{\partial r} + \frac{\partial \rho v E}{\partial z} = & \rho v g + \frac{1}{r} \frac{\partial}{\partial r} \left\{ r \left[B \mu \frac{\partial I}{\partial r} - p u - \left(\frac{\lambda}{\lambda + 2\mu} \right) q u \right. \right. \\ & \left. \left. + \frac{\mu}{2} \frac{\partial}{\partial r} (2u^2 + v^2) + \mu v \frac{\partial u}{\partial z} \right] \right\} + \frac{\partial}{\partial z} \left\{ B \mu \frac{\partial I}{\partial z} - p v - \left(\frac{\lambda}{\lambda + 2\mu} \right) q v \right. \\ & \left. \left. + \frac{\mu}{2} \frac{\partial}{\partial z} (u^2 + 2v^2) + \mu u \frac{\partial v}{\partial r} \right\}, \end{aligned} \quad (10)$$

where

$$q \equiv -(\lambda + 2\mu) \left(\frac{1}{r} \frac{\partial u r}{\partial r} + \frac{\partial v}{\partial z} \right), \quad (11)$$

in which u and v are the velocity components in the r and z directions, respectively.

The equation of state is of the form

$$p = f(\rho, I). \quad (12)$$

The differential equations mentioned above are written in cylindrical coordinates and are used in the implicit Eulerian hydrodynamic methods [11,15]. Here, we refer to these equations as well as the governing finite-difference equation for the purpose of completeness.

2. The Finite-Difference Representations

Like most Eulerian hydrodynamic methods [11,15,17], the equations of mass and momentum are expressed in the advanced-time forms using an implicit-difference representation. Figure 2 shows an Eulerian finite-difference mesh, illustrating the centering of the physical variables relative to a typical cell. The velocities are defined at the cell boundaries with u at $i+\frac{1}{2}$ and v at $j+\frac{1}{2}$. Other field variables are all defined at the cell center.

To simplify the analysis, the description of the basic hydrodynamics and the detailed derivation of finite-difference expressions of mass and momentum equations will not be presented here, but are given in Refs. [11,13,15].

The equation of state of the coolant is

$$\bar{p}_{i,j} = p_{i,j}^n + c_{i,j}^n \left(\rho_{i,j}^{n+1} - \rho_{i,j}^n \right), \quad (13)$$

in which

$$c_{i,j}^n = \left(\frac{\partial p}{\partial \rho} \right)_{i,j},$$

is closely related to speed of sound; $\bar{p}_{i,j}$ is the advanced-time pressure; the superscripts $n+1$ and n will denote the $(n+1)$ -th and n -th time cycles in the following development; variables lacking superscripts will represent values of the n -th cycle.

Thus, eliminating the mass fluxes between the mass and momentum equations, in conjunction with the equation of state relating the advanced-time pressures and densities, results in a Poisson's equation governing the advanced-time pressures:

$$\bar{p}_{i,j} \left[\frac{1}{c_{i,j}^n} + 2\theta\psi\delta t^2 \left(\frac{1}{\delta r^2} + \frac{1}{\delta z^2} \right) \right] = G_{i,j} + \theta\psi\delta t^2 \left[\frac{r_{i-\frac{1}{2}} \bar{p}_{i-1,j} + r_{i+\frac{1}{2}} \bar{p}_{i+1,j}}{r_i \delta r^2} + \frac{\bar{p}_{i,j-1} + \bar{p}_{i,j+1}}{\delta z^2} \right], \quad (14)$$

where

$$G_{i,j} = G(R_{I+\frac{1}{2},j}; S_{i,j+\frac{1}{2}}; u, v, p, \rho, c^{-1}, \dots) ,$$

is the source term of the Poisson's equation which is evaluated from previous cycle values; R and S are the source terms of the momentum equations in the r and z directions, respectively; δt is the time step, δr and δz are respectively, the dimensions of a cell in the radial and axial directions; \bar{p} is the advanced-time pressure, corresponding to the pressure at the $(n+1)$ th cycle with superscript $n+1$ neglected, ψ and θ are the weighting constants of the momentum and mass equations which are utilized for the numerical treatment, as suggested in the ICE technique. These constants, with magnitudes between 0.0 and 1.0, represent the relative level of time centering of the pressure-gradient and mass-flux terms. For $\psi = 1.0$ the technique is purely implicit [15].

Noted that Eq. (14) is the governing difference equation for the advanced-time pressure in a cell completely filled with the fluid. It consists of five unknowns and is solved by the iteration technique.

If the fluid is bounded by the rigid walls and the wall boundaries coincide with the Eulerian grid lines, Eq. (14) is sufficient to determine the advanced-time pressure field. However, if the computational region involving flexible vessel or deformable internals, modification of source-term calculations is needed. For more details, the reader should refer to Ref. [13].

3. Particle Movement

After solving for the advanced-velocity field and other field variables, a new configuration of the flow field is generated by moving the marker particles to their new positions:

$$r_k^{n+1} = r_k^n + u_k \delta t ; \quad z_k^{n+1} = z_k^n + v_k \delta t ,$$

where u_k and v_k denote the velocity components for the k th particle. The values of u_k and v_k are obtained by averaging from the u and v fields, respectively. For example, if particle k is located within the cell where velocity components are defined at the nearby locations (see Fig. 3), u_k and v_k can be calculated by the area-weighting method:

$$u_k = \frac{A_1 u_1 + A_2 u_2 + A_3 u_3 + A_4 u_4}{\delta r \delta z},$$

and

(15)

$$v_k = \frac{B_1 v_1 + B_2 v_2 + B_3 v_3 + B_4 v_4}{\delta r \delta z}.$$

B. Integral Equations for Perforated Structure

Nuclear reactors usually have structure components with small coolant passageways, such as the core-support structure, upper internal structure and the reactor cover. The equations governing the fluid motion near these structures can be formulated rigorously if they have only one-dimensional movements. In general, the coolant flow through the coolant passageways can be analyzed by the conventional Eulerian and Arbitrary Lagrangian-Eulerian methods using various narrow cells to approach the size of the passageways. However, the resulting analysis has three drawbacks: (1) a large number of computational cells is required; (2) the time steps, usually proportional to the width of the narrow cell in accordance with the modified Courant stability condition, are limited to very small values; (3) undesirable errors may be induced if the variation of the cell width becomes too drastic.

To eliminate the difficulties mentioned previously, a hydrodynamic method for treating perforated structure is developed. It allows the use of large (wide) cells over the entire computational region. Thus, numerical calculations can be performed with fewer cells and thereby larger time steps. Consequently, the computational efficiency is optimized.

For the developments of flow through perforated structure it is desirable to replace the differential equations by the analogous integral equations, obtained by integrating over the respective control volume, V , and then converting the volume integral of divergences to surface integrals over the control surfaces. Thus, in integral form, the mass, momentum, and energy equations for a non-heat-conducting fluid are [16]:

$$\frac{\partial}{\partial t} \int_V \rho dV + \int_S \rho w_i n_i dS = 0 \quad , \quad (16)$$

$$\frac{\partial}{\partial t} \int_V \rho w_i dV + \int_S \rho w_i w_j n_j dS = \int_S \sigma_{ij} n_j dS + \int_V \rho g_i dV \quad , \quad (17)$$

and

$$\frac{\partial}{\partial t} \int_V \rho E dV + \int_S \rho w_i E n_i dS = \int_S \sigma_{ij} w_j n_i dS + \int_V \rho g_i w_i dV \quad , \quad (18)$$

where n_i is the outward normal of the surface S_i .

The control volumes employed for obtaining the radial velocity u , axial velocity v , and specific density ρ are essentially the same as those of the ICE technique. In other words, the control volume for derivation of u is centered at $(i+\frac{1}{2}, j)$, while control volumes for derivations of v and ρ are centered, respectively, at $(i, j+\frac{1}{2})$, and (i, j) . Also, to simplify the analysis of flow through the perforated structure we assume that the flow inside the coolant passageways is one-dimensional. Thus, based upon the integral equations mentioned above, the conservation equations of mass, momentum, and energy can be derived using the net fluid volume and the available flow areas. Similar concept has also been used by Sha et al. [17] in the three-dimensional thermal hydrodynamic analysis of reactor components.

C. The Above-Core Hydrodynamics

In the analysis of HCDAs one important area that so far has not been rigorously considered is the above-core hydrodynamics induced by the Upper Internal Structure (UIS). The shape of the UIS generally differs among various reactors. In the Fast Flux Test Facility (FFTF), the upper internal structure consists of three instrument trees located above the core. In the Clinch River Breeder Reactor (CRBR), the main body of the upper internal structure comprises of four support columns, an upper plate, and a lower plate holding numerous flow-guide passageways surrounded by the stagnant sodium as shown in Fig. 4. Since the passageways provide the only flow area for redirecting

the core sodium axially into the outlet plenum, the presence of the upper internal structure definitely has the effect of confining and retarding the HCDA bubble as well as slowing down the upward motion of the fluid. As a result, the HCDA energy release, the slug-impact loading, and the responses of the structural components and containment can be significantly influenced by this structure. Thus, to provide a more complete analysis of primary-containment response, the treatment of the upper internal structure should be incorporated into the computer model.

Since at the present time the structural dynamic program for treating the motion of the UIS is not available, the main body of the UIS is considered to be rigid and fixed in the space. The flow-area reduction due to presence of the support columns is ignored in the hydrodynamic calculations. The assembly portion of the UIS is considered as a perforated structure. The governing difference equations will be described below.

1. Fluid Motion Inside Coolant Passageways

The flow inside the coolant passageways is viscous but one-dimensional. The mass and momentum equations are:

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho \tilde{v}}{\partial z} = 0, \quad (19)$$

and

$$\frac{\partial \rho \tilde{v}}{\partial t} + \frac{\partial \rho \tilde{v}^2}{\partial z} = - \frac{\partial}{\partial z} (p + q) - f \frac{\rho \tilde{v} |\tilde{v}|}{2D}, \quad (20)$$

where \tilde{v} is the axial velocity, f is the friction factor depending on the wall roughness and the Reynolds number, and D is the average hydraulic diameter of the coolant passageways associated with each radial zone. The drag-force term in the momentum equation represents the friction retardation force acting on the coolant passageway wall. The absolute-value sign indicates that the drag force always acts opposite to the direction of the axial velocity component.

The viscous pressure q is given by

$$q = - \lambda \frac{\partial \tilde{v}}{\partial z}.$$

The finite difference forms of the axial momentum equations can be easily derived from the integral equation by summing term by term contributions of the convective fluxes and the surface forces on the bounding surfaces of a control volume ABCD shown in Fig. 5. The resulting equation is

$$\phi_i \frac{(\rho \tilde{v})_{i,j+\frac{1}{2}}^{n+1} - (\rho \tilde{v})_{i,j+\frac{1}{2}}^n}{\delta t} = \phi_i \left[\frac{\psi}{\delta z} (\bar{P}_{i,j} - \bar{P}_{i,j+1}) + \frac{1-\psi}{\delta z} (P_{i,j}^n - P_{i,j+1}^n) \right] + S_{i,j+\frac{1}{2}}, \quad (21)$$

were

$$S_{i,j+\frac{1}{2}} = \frac{\phi_i}{\delta z} \left\{ \left[(\rho \tilde{v}^2)_{i,j} - (\rho \tilde{v}^2)_{i,j+1} \right] + q_{i,j} - q_{i,j+1} \right\} - f \frac{\rho \tilde{v} |\tilde{v}|}{2D}. \quad (22)$$

The finite-difference mass equation becomes

$$\frac{\rho_{i,j}^{n+1} - \rho_{i,j}^n}{\delta t} = \frac{\theta}{\delta z} \left[(\rho \tilde{v})_{i,j-\frac{1}{2}}^{n+1} - (\rho \tilde{v})_{i,j+\frac{1}{2}}^{n+1} \right] + \frac{1-\theta}{\delta z} \left[(\rho \tilde{v})_{i,j-\frac{1}{2}}^n - (\rho \tilde{v})_{i,j+\frac{1}{2}}^n \right]. \quad (23)$$

The equation of state has the form

$$\bar{P}_{i,j} = P_{i,j}^n + c_{i,j}^n \left(\rho_{i,j}^{n+1} - \rho_{i,j}^n \right).$$

Thus, following the difference scheme of the implicit Eulerian hydrodynamics [11,13,15], a modified Poisson equation governing the advanced-time pressures in the coolant passageways can be obtained by eliminating the advanced-time densities and velocities in Eq. (23). This results in

$$\bar{P}_{i,j} \left[\frac{1}{c_{i,j}^n} + 2\theta\psi \frac{\delta t^2}{\delta z^2} \right] = H_{i,j} + \theta\psi\delta t^2 \left[\frac{\bar{P}_{i,j-1} + \bar{P}_{i,j+1}}{\delta z^2} \right], \quad (24)$$

where

$$H_{i,j} = \frac{P_{i,j}^n}{c_{i,j}^n} + \frac{\theta\delta t^2}{\delta z} \frac{1}{\phi_i} (S_{i,j-\frac{1}{2}} - S_{i,j+\frac{1}{2}}) + \frac{\delta t}{\delta z} \left[(\rho \tilde{v})_{i,j-\frac{1}{2}}^n - (\rho \tilde{v})_{i,j+\frac{1}{2}}^n \right] + \frac{\theta(1-\psi)}{\delta z^2} (P_{i,j-1}^n + P_{i,j+1}^n - 2P_{i,j}^n), \quad (25)$$

is the source term evaluated from previous-cycle pressures and velocities.

2. Fluid Motion Above the Perforated Structure

At the exit of the perforated structure the flow is two dimensional. The radial momentum equation can be derived using control volume ABCDEF shown in Fig. 5. The upper boundary of the UIS is assumed to be a porous polygon. Thus, in the calculation of the surface forces and the convected fluxes we homogenize the perforated structure member so that the total mass flux through the coolant passageways is uniformly distributed over the entire cell boundary. In other words, for the case shown in Fig. 6 we let

$$v_{i,j-\frac{1}{2}} = \phi_i \tilde{v}_{i,j-\frac{1}{2}}$$

Adding up the convective fluxes and the surface forces with respect to the bounding surfaces shown in Fig. 6, the radial momentum equation has the form

$$\begin{aligned} \frac{(\rho u)_{i+\frac{1}{2},j}^{n+1} + (\rho u)_{i+\frac{1}{2},j}^n}{\delta t} &= \frac{\psi}{\delta r} (\bar{p}_{i,j} - \bar{p}_{i+1,j}) + \frac{1-\psi}{\delta r} (p_{i,j}^n - p_{i+1,j}^n) \\ &+ R_{i+\frac{1}{2},j}, \end{aligned} \quad (26)$$

where

$$\begin{aligned} R_{i+\frac{1}{2},j} &= \frac{1}{r_{i+\frac{1}{2}} \delta r} \left[r_i (\rho u^2)_{i,j} - r_{i+1} (\rho u^2)_{i+1,j} \right] \\ &+ \frac{1}{\delta z} \left\{ \frac{1}{2r_{i+\frac{1}{2}}} \left[\phi_i r_i (\rho u \tilde{v})_{i,j-\frac{1}{2}} + \phi_{i+1} r_{i+1} (\rho u \tilde{v})_{i+1,j-\frac{1}{2}} \right] \right. \\ &\left. - (\rho uv)_{i+\frac{1}{2},j+\frac{1}{2}} \right\} + \frac{1}{\delta r} (q_{i,j} - q_{i+1,j}) + g_r \rho_{i+\frac{1}{2},j} \\ &+ \frac{\mu}{\delta z} \left[\frac{u_{i+\frac{1}{2},j+1} - u_{i+\frac{1}{2},j}}{\delta z} - \frac{v_{i+1,j+\frac{1}{2}} - v_{i,j+\frac{1}{2}}}{\delta r} \right. \\ &\left. - \frac{u_{i+\frac{1}{2},j} - u_{i+\frac{1}{2},j-1}}{\delta z} + \frac{\phi_{i+1} \tilde{v}_{i+1,j-\frac{1}{2}} - \phi_i \tilde{v}_{i,j-\frac{1}{2}}}{\delta r} \right]. \end{aligned} \quad (27)$$

The finite-difference representation of the axial momentum equation can be obtained from summation of the convective fluxes and the surface forces with respect to the control volume centering at $(i, j+\frac{1}{2})$, and has the form

$$\frac{(\rho v)_{i,j+\frac{1}{2}}^{n+1} - (\rho v)_{i,j+\frac{1}{2}}^n}{\delta t} = \frac{\psi}{\delta z} \left(\bar{P}_{i,j} - \bar{P}_{i,j+1} \right) + \frac{1-\psi}{\delta z} \left(P_{i,j}^n - P_{i,j+1}^n \right) + S_{i,j+\frac{1}{2}}, \quad (28)$$

where

$$\begin{aligned} S_{i,j+\frac{1}{2}} = & \frac{1}{r_i \delta r} \left[(\rho uvr)_{i-\frac{1}{2},j+\frac{1}{2}} - (\rho uvr)_{i+\frac{1}{2},j+\frac{1}{2}} \right] + \frac{1}{\delta z} \left[v_{i,j+\frac{1}{2}} (\rho_{i,j} v_{i,j-\frac{1}{2}} \right. \\ & \left. - \rho_{i,j+1} v_{i,j+\frac{3}{2}}) \right] + \frac{1}{\delta z} (q_{i,j} - q_{i,j+1}) + g_z \rho_{i,j+\frac{1}{2}} \\ & - \frac{\mu}{r_i \delta r} \left[r_{i+\frac{1}{2}} \left(\frac{u_{i+\frac{1}{2},j+1} - u_{i+\frac{1}{2},j}}{\delta z} - \frac{v_{i+1,j+\frac{1}{2}} - v_{i,j+\frac{1}{2}}}{\delta r} \right) \right. \\ & \left. - r_{i-\frac{1}{2}} \left(\frac{u_{i-\frac{1}{2},j+1} - u_{i-\frac{1}{2},j}}{\delta z} - \frac{v_{i,j+\frac{1}{2}} - v_{i-1,j+\frac{1}{2}}}{\delta r} \right) \right]. \end{aligned} \quad (29)$$

The finite-difference mass equation for cell (i,j) is

$$\frac{\rho_{i,j}^{n+1} - \rho_{i,j}^n}{\delta t} = \theta D_{i,j}^{n+1} + (1-\theta) D_{i,j}^n, \quad (30)$$

where

$$\begin{aligned} D_{i,j}^n = & \frac{1}{r_i \delta r} \left[r_{i-\frac{1}{2}} (\rho u)_{i-\frac{1}{2},j}^n - r_{i+\frac{1}{2}} (\rho u)_{i+\frac{1}{2},j}^n \right] \\ & + \frac{1}{\delta z} \left[\phi_i (\rho \tilde{v})_{i,j-\frac{1}{2}}^n - (\rho v)_{i,j+\frac{1}{2}}^n \right], \end{aligned} \quad (31)$$

represents the volumetric dilatation of cell (i,j) obtained from the previous-time cycle values, $D_{i,j}^{n+1}$ has exactly the same form but is evaluated at the (n+1)-th cycle.

The equation of state is

$$\bar{P}_{i,j} = P_{i,j} + c_{i,j}^n \left(\rho_{i,j}^{n+1} - \rho_{i,j}^n \right).$$

Eliminating the advanced-time densities and velocities in Eq. (30) we have a modified Poisson equation governing the new pressure field above the perforated UIS, which has the form

$$\bar{P}_{i,j} \left[\frac{1}{c_{i,j}^n} + 2\theta\psi\delta t^2 \left(\frac{1}{\delta r^2} + \frac{1}{\delta z^2} \right) \right] = H_{i,j} + \theta\psi\delta t^2 \left[\frac{r_{i-\frac{1}{2}} \bar{P}_{i-1,j} + r_{i+\frac{1}{2}} \bar{P}_{i+1,j}}{r_i \delta r^2} + \frac{\phi_i \bar{P}_{i,j-1} + (1-\phi_i) \bar{P}_{i,j} + \bar{P}_{i,j+1}}{\delta z^2} \right] \quad (32)$$

where

$$\begin{aligned} H_{i,j} = & \frac{P_{i,j}}{c_{i,j}} + \frac{\theta\delta t^2}{r_i \delta r} \left\{ \frac{1-\psi}{\delta r} \left[r_{i-\frac{1}{2}} (P_{i-1,j} - P_{i,j}) - r_{i+\frac{1}{2}} (P_{i,j} - P_{i+1,j}) \right] \right. \\ & + r_{i-\frac{1}{2}} R_{i-\frac{1}{2},j} - r_{i+\frac{1}{2}} R_{i+\frac{1}{2},j} \left. \right\} + \frac{\theta\delta t^2}{\delta z} \left\{ \frac{1-\psi}{\delta z} \left[\phi_i (P_{i,j-1} - P_{i,j}) \right. \right. \\ & - (1-\phi_i) g_z \delta z \rho_{i,j} - (P_{i,j} - P_{i,j+1}) \left. \right] + S_{i,j-\frac{1}{2}} - S_{i,j+\frac{1}{2}} \left. \right\} \\ & + \delta t D_{i,j}^n \end{aligned}$$

3. Fluid Motion Below the Perforated Structure

Below the perforated structure the flow is also two-dimensional. Here, we make the same assumption that the state of stress is continuous throughout the fluid element enclosed by the respective control volume for derivations of the momentum equations. Thus, similar to the formulation of difference equations above the perforated structure we assume that the coolant passages are uniformly dispersed over the upper cell boundary. Thus, we have

$$\hat{v}_{i,j+\frac{1}{2}} = \phi_i \tilde{v}_{i,j+\frac{1}{2}} \quad (33)$$

Similar to the development of equations for flows above the perforated UIS, the radial momentum equation becomes

$$\begin{aligned} \frac{(\rho u)_{i+\frac{1}{2},j}^{n+1} - (\rho u)_{i+\frac{1}{2},j}^n}{\delta t} = & \frac{\psi}{\delta r} (\bar{P}_{i,j} - \bar{P}_{i+1,j}) + \frac{1-\psi}{\delta r} (P_{i,j}^n - P_{i+1,j}^n) \\ & + R_{i+\frac{1}{2},j} \end{aligned} \quad (34)$$

where

$$\begin{aligned}
R_{i+\frac{1}{2},j} = & \frac{1}{r_{i+\frac{1}{2}} \delta r} \left[r_i (\rho u^2)_{i,j} - r_{i+1} (\rho u^2)_{i+1,j} \right] + \frac{1}{\delta z} \left\{ (\rho u v)_{i+\frac{1}{2},j-\frac{1}{2}} \right. \\
& \left. - \frac{1}{2r_{i+\frac{1}{2}}} \left[\phi_i r_i (\rho u \tilde{v})_{i,j+\frac{1}{2}} + \phi_{i+1} r_{i+1} (\rho u \tilde{v})_{i+1,j+\frac{1}{2}} \right] \right\} \\
& + \frac{1}{\delta r} (q_{i,j} - q_{i+1,j}) + g_r \rho_{i+\frac{1}{2},j} + \frac{\mu}{\delta z} \left[\frac{u_{i+\frac{1}{2},j+1} - u_{i+\frac{1}{2},j}}{\delta z} \right. \\
& \left. - \frac{\hat{v}_{i+1,j+\frac{1}{2}} - \hat{v}_{i,j+\frac{1}{2}}}{\delta r} - \frac{u_{i+\frac{1}{2},j} - u_{i+\frac{1}{2},j-1}}{\delta z} + \frac{v_{i+1,j-\frac{1}{2}} - v_{i,j-\frac{1}{2}}}{\delta r} \right], \quad (35)
\end{aligned}$$

is the source term with the form of \hat{v} defined in Eq. (33).

The finite-difference representation of the axial momentum equation is

$$\begin{aligned}
\phi_i \frac{(\rho \tilde{v})_{i,j+\frac{1}{2}}^{n+1} - (\rho \tilde{v})_{i,j+\frac{1}{2}}^n}{\delta t} = & \phi_i \left[\frac{\psi}{\delta z} (\bar{P}_{i,j} - \bar{P}_{i,j+1}) + \frac{1-\psi}{\delta z} (P_{i,j}^n - P_{i,j+1}^n) \right] \\
& + S_{i,j+\frac{1}{2}}, \quad (36)
\end{aligned}$$

where

$$\begin{aligned}
S_{i,j+\frac{1}{2}} = & \frac{\phi_i}{\delta z} \left[(\rho \tilde{v}^2)_{i,j} - (\rho \tilde{v}^2)_{i,j+1} \right] + \frac{1}{\delta z} (q_{i,j-1} - q_{i,j}) \\
& + \phi_i \frac{\rho_{i,j+1} + \rho_{i,j}}{2} q_z + (1-\phi_i) \rho_{i,j} q_z \\
& - \frac{\mu}{r_i \delta r} \left[r_{i+\frac{1}{2}} \left(\frac{u_{i+\frac{1}{2},j+1} - u_{i+\frac{1}{2},j}}{\delta z} - \frac{\hat{v}_{i+1,j+\frac{1}{2}} - \hat{v}_{i,j+\frac{1}{2}}}{\delta r} \right) \right. \\
& \left. - r_{i-\frac{1}{2}} \left(\frac{u_{i-\frac{1}{2},j+1} - u_{i-\frac{1}{2},j}}{\delta z} - \frac{\hat{v}_{i,j+\frac{1}{2}} - \hat{v}_{i-1,j+\frac{1}{2}}}{\delta r} \right) \right], \quad (37)
\end{aligned}$$

is the source term, \hat{v} again has the same form as of Eq. (33).

Similar to the momentum equations a weighting constant θ varying from 0.0 to 1.0 can be used for the finite-difference mass equation to indicate relative level between purely explicit and purely implicit forms. This yields

$$\frac{\rho_{i,j}^{n+1} - \rho_{i,j}^n}{\delta t} = \theta D_{i,j}^{n+1} + (1-\theta) D_{i,j}^n, \quad (38)$$

where

$$D_{i,j} = \frac{1}{r_i \delta r} \left[r_{i-\frac{1}{2}} (\rho u)_{i-\frac{1}{2},j} - r_{i+\frac{1}{2}} (\rho u)_{i+\frac{1}{2},j} \right] + \frac{1}{\delta z} \left[(\rho \tilde{v})_{i,j-\frac{1}{2}} - \phi_i (\rho \tilde{v})_{i,j+\frac{1}{2}} \right], \quad (39)$$

again denotes the volumetric dilatation of cell (i,j) with time index n and n+1 neglected in the expression.

Eliminating the advanced-time densities and velocities in the mass equation a modified Poisson equation characterizing the flow below the perforated structure is

$$\bar{P}_{i,j} \left[\frac{1}{c_{i,j}^n} + 2\theta\psi\delta t^2 \left(\frac{1}{\delta r^2} + \frac{1}{\delta z^2} \right) \right] = H_{i,j} + \theta\psi\delta t^2 \left[\frac{r_{i-\frac{1}{2}} \bar{P}_{i-1,j} + r_{i+\frac{1}{2}} \bar{P}_{i+1,j}}{r_i \delta t^2} + \frac{\bar{P}_{i,j-1} + \phi_i \bar{P}_{i,j+1} + (1-\phi_i) \bar{P}_{i,j}}{\delta z^2} \right], \quad (40)$$

in which

$$H_{i,j} = \frac{P_{i,j}}{c_{i,j}} + \frac{\theta\delta t^2}{r_i \delta r} \left\{ \frac{1-\psi}{\delta r} \left[r_{i-\frac{1}{2}} (P_{i-1,j} - P_{i,j}) - r_{i+\frac{1}{2}} (P_{i,j} - P_{i+1,j}) \right] + r_{i-\frac{1}{2}} R_{i-\frac{1}{2},j} - r_{i+\frac{1}{2}} R_{i+\frac{1}{2},j} \right\} + \frac{\theta\delta t^2}{\delta z} \left\{ \frac{1-\psi}{\delta z} \left[(P_{i,j-1} - P_{i,j}) - \phi_i (P_{i,j} - P_{i,j+1}) - (1-\phi_i) \rho_{i,j} g_z \delta z \right] + S_{i,j-\frac{1}{2}} - S_{i,j+\frac{1}{2}} \right\} + \delta t D_{i,j}^n, \quad (41)$$

is the source term; $D_{i,j}^n$ is defined in Eq. (39). Also, in calculating $H_{i,j}$ the momentum sources $R_{i-\frac{1}{2},j}$ and $S_{i,j-\frac{1}{2}}$ are also needed. The term $R_{i-\frac{1}{2},j}$ can be calculated from Eq. (35) by replacing index i with i-1; whereas $S_{i,j-\frac{1}{2}}$ can be evaluated from Eq. (9) of the ICE technique by changing j with j-1.

D. Moving Cover and Sodium Spillage

The Eulerian hydrodynamics is ideal for long-duration calculations for problems involving large material distortions. The basic hydrodynamic technique has an option for treating inflow and outflow boundary conditions. However, the size of the wall opening in the basic ICE method is limited to multiples of the cell size. In other words, if the wall opening is small, the Eulerian cell dimension must also be made small. In addition, the size of the opening in the basic hydrodynamic technique must remain constant. Thus, the opening does not vary with time, which is different from a gap generated by the slug-impact force on the reactor head cover at the head-vessel junction. Therefore, the basic hydrodynamic technique must be expanded in order to treat the coolant spillage problem more realistically.

In the Eulerian-Hydrodynamic analysis when the vessel head moves upward a set of irregular cells whose size varies in the axial direction according to the head displacement, is introduced on the top of the full-zone regular cell as shown in Fig. 7. Since in these irregular cells only the axial dimension of the cell varies, but the shape remains rectangular, it is possible to derive the governing difference equations with respect to these irregular cells. Several years ago, Chu [18] developed a quasi-Eulerian method which was used in conjunction with the ICECO code to study the effect of sodium spillage on slug impact. In that model the viscous stress tensor was neglected in the formulation, and a complete Donor-cell differencing scheme was utilized for evaluations of the source terms in the momentum equations and Poisson's equation.

Recently, the sodium-spillage model has been considerably revised and its scope of applicability is extended. The present model (1) provides a more compatible formulation so that in certain circumstances the equations can be directly reduced to those used in the Eulerian technique [11,13], (2) incorporates the correct, full viscous stress tensor, instead of a simple artificial viscosity, (3) introduces the option of using ZIP differencing scheme for calculating various source terms, and (4) includes provisions of computing coolant spillage through different leak paths.

Here, the control-volume technique is employed, in which the conservation equations are generalized to take into account the penetration holes and the side opening. The upper boundaries of the irregular cells are considered as inviscid, moving with the same velocity as the cover head. Thus, separation of the entire coolant-free surface with the reactor cover is not permitted after slug impact.

In the analysis, two fictitious cells, one on the top and one at the bottom of the irregular cell, are introduced for convenience of calculation (see Fig. 7). Fluid variables in the fictitious cells of both the irregular and regular cells are obtained from interpolation or extrapolation. To simplify the analysis we assume that (1) the penetration is located on the top center of the irregular cell for convenience of moving particles inside the top opening, (2) only one penetration is allowed for each cell, (3) the penetration is considered to open when the impulse on this penetration area exceeds a certain input value.

Thus, similar to the derivation of difference equations for the above-core hydrodynamics the governing difference equations near the reactor cover are formulated by summing up term by term contributions of the integral Eqs. (16-18). The radial momentum equation can be derived using control volume ABCDEF shown in Fig. 8. Again to ensure the stress continuity for calculating the viscous stress tensor it is necessary to distribute the velocity in the penetration opening uniformly throughout the upper cell boundary. For the case shown in Fig. 8, we let

$$\hat{v}_{i,j+\frac{1}{2}} = \eta_i (v_o)_{i,j+\frac{1}{2}} + (1-\eta_i) v_{i,j+\frac{1}{2}} \quad , \quad (42)$$

where \hat{v} is the mean value of the axial velocity component; η_i is the ratio of the penetration-opening area to the area of upper cell boundary; v_o is the fluid velocity at the penetration opening; v is the velocity of the moving cover. For convenience, we further define

$$\alpha_i = 0.5\eta_i r_i/r_{i+\frac{1}{2}} \quad \text{and} \quad \beta_{i+1} = 0.5\eta_{i+1} r_{i+1}/r_{i+\frac{1}{2}} \quad . \quad (43)$$

Thus, based on a control volume ABCDEF shown in Fig. 8, the radial momentum equation relative to the right-hand cell boundary has the form

$$\frac{(\rho u)_{i+\frac{1}{2},j}^{n+1} - (\rho u)_{i+\frac{1}{2},j}^n}{\delta t} = \frac{\psi}{\delta r} \left(\bar{p}_{i-1,j} - \bar{p}_{i,j} \right) + \frac{1-\psi}{\delta r} \left(p_{i-1,j}^n - p_{i,j}^n \right) + R_{i+\frac{1}{2},j}, \quad (44)$$

in which

$$\begin{aligned} R_{i+\frac{1}{2},j} = & \frac{1}{r_{i+\frac{1}{2}} \delta r} \left[r_i (\rho u^2)_{i,j} - (\rho u^2)_{i+1,j} \right] + \frac{1}{\delta y} \left[(\rho uv)_{i+\frac{1}{2},j-\frac{1}{2}} \right. \\ & - \alpha_i (\rho uv_o)_{i,j+\frac{1}{2}} - \beta_{i+1} (\rho uv_o)_{i+1,j+\frac{1}{2}} \\ & - (1-\alpha_i - \beta_{i+1}) (\rho uv)_{i+\frac{1}{2},j+\frac{1}{2}} \left. \right] + \frac{1}{\delta r} (q_{i,j} - q_{i+1,j}) + g_r \rho_{i+\frac{1}{2},j} \\ & + \frac{\mu}{\delta y} \left[\frac{u_{i+\frac{1}{2},j+1} - u_{i+\frac{1}{2},j}}{\delta z} - \frac{\hat{v}_{i+1,j+\frac{1}{2}} - \hat{v}_{i,j+\frac{1}{2}}}{\delta r} \right. \\ & \left. - \frac{u_{i+\frac{1}{2},j} - u_{i+\frac{1}{2},j-1}}{\delta z} + \frac{\hat{v}_{i+1,j-\frac{1}{2}} - \hat{v}_{i,j-\frac{1}{2}}}{\delta r} \right], \quad (45) \end{aligned}$$

is the source term with \hat{v} , α and β defined in Eqs. (42) and (43), respectively. Note that $R_{i+\frac{1}{2},j}$ is the source term, which has exactly the same form as the ICE technique in the case of full-cell openings (i.e., $\eta_i = \eta_{i+1} = 1$).

Likewise, the finite-difference representation of the axial momentum equation relative to the upper cell boundary $(i, j+\frac{1}{2})$ can be obtained using the control volume shown in Fig. 9, and has the form

$$\begin{aligned} \eta_i \frac{(\rho v_o)_{i,j+\frac{1}{2}}^{n+1} - (\rho v_o)_{i,j+\frac{1}{2}}^n}{\delta t} + (1-\eta_i) \frac{(\rho v)_{i,j+\frac{1}{2}}^{n+1} - (\rho v)_{i,j+\frac{1}{2}}^n}{\delta t} \\ = \frac{\eta_i}{dy} \left[\psi \left(\bar{p}_{i,j} - \bar{p}_{o_{i,j+1}} \right) + (1-\psi) \left(p_{i,j}^n - p_{o_{i,j+1}}^n \right) \right] \\ + \frac{1-\eta_i}{dy} \left[\psi \left(\bar{p}_{i,j} - \bar{p}_{i,j+1} \right) + (1-\psi) \left(p_{i,j}^n - p_{i,j+1}^n \right) \right] \\ + S_{i,j+\frac{1}{2}}, \quad (46) \end{aligned}$$

where

$$\begin{aligned}
S_{i,j+\frac{1}{2}} = & \frac{\eta_i}{dy} \left[(\rho v_o^2)_{i,j} - (\rho v_o^2)_{i,j+1} \right] + \frac{1-\eta_i}{dy} \left[(\rho v^2)_{i,j} - (\rho v^2)_{i,j+1} \right] \\
& + \frac{1}{r_i \delta r} \left[r_{i-\frac{1}{2}} (\rho uv)_{i-\frac{1}{2},j+\frac{1}{2}} - r_{i+\frac{1}{2}} (\rho uv)_{i+\frac{1}{2},j+\frac{1}{2}} \right] + \frac{1}{\delta y} (q_{i,j} - q_{i,j+1}) \\
& + \eta_i \frac{\rho_{o,i,j+1} + \rho_{i,j}}{2} g_z + (1-\eta_i) \frac{\rho_{i,j+1} + \rho_{i,j}}{2} \\
& - \frac{\mu}{r_i \delta r} \left[r_{i+\frac{1}{2}} \left(\frac{u_{i+\frac{1}{2},j+1} - u_{i+\frac{1}{2},j}}{\delta y} - \frac{\hat{v}_{i+1,j+\frac{1}{2}} - \hat{v}_{i,j+\frac{1}{2}}}{\delta r} \right) \right. \\
& \left. - r_{i-\frac{1}{2}} \left(\frac{u_{i-\frac{1}{2},j+1} - u_{i-\frac{1}{2},j}}{\delta r} - \frac{\hat{v}_{i,j+\frac{1}{2}} - \hat{v}_{i-1,j+\frac{1}{2}}}{\delta r} \right) \right] , \quad (47)
\end{aligned}$$

is the source term, ρ_o is the density outside the containment, dy is the axial size of the irregular cells, \hat{v} is again the mean value of the axial velocity component similar to the one expressed in Eq. (42); also, \bar{P}_o and P_o^n are the pressures outside the opening at the $(n+1)$ th and n th cycle, respectively.

Eliminating all the advanced-time densities and velocities in the mass equation similar to the scheme developed by Chu [18] a modified Poisson equation for the irregular cells, including the effects of penetration hole or side opening, is of the form

$$\begin{aligned}
\bar{P}_{i,j} \left[\frac{1}{c_{i,j}^n} + 2\theta\psi\delta t^2 \left(\frac{1}{\delta r^2} + \frac{1}{\delta y^2} \right) \right] = & H_{i,j} + \theta\psi\delta t^2 \left[\frac{r_{i-\frac{1}{2}} \bar{P}_{i-1,j} + r_{i+\frac{1}{2}} \bar{P}_{i+1,j}}{r_i \delta r^2} \right. \\
& \left. + \frac{\bar{P}_{i,j-1} + \eta_i \bar{P}_{o,i,j+1} + (1-\eta_i) \bar{P}_{i,j+1}}{\delta y^2} \right] , \quad (48)
\end{aligned}$$

in which

$$\begin{aligned}
H_{i,j} = & \frac{P_{i,j}}{c_{i,j}} + \frac{\theta\delta t^2}{r_i \delta r} \left\{ \frac{1-\psi}{\delta r} \left[r_{i-\frac{1}{2}} (P_{i-1,j} - P_{i,j}) - r_{i+\frac{1}{2}} (P_{i,j} - P_{i+1,j}) \right] \right. \\
& + r_{i-\frac{1}{2}} R_{i-\frac{1}{2}} - r_{i+\frac{1}{2}} R_{i+\frac{1}{2}} \left. \right\} + \frac{\theta\delta t^2}{\delta y} \left\{ \frac{1-\psi}{\delta y} \left[(P_{i,j-1} - P_{i,j}) \right. \right. \\
& \left. \left. - \eta_i (P_{i,j} - P_{o,i,j+1}) - (1-\eta_i) (P_{i,j} - P_{i,j+1}) \right] + S_{i,j-\frac{1}{2}} - S_{i,j+\frac{1}{2}} \right\} \\
& + \delta t D_{i,j}^n , \quad (49)
\end{aligned}$$

is the source term of the Poisson equation, $D_{i,j}^n$ is the volumetric dilatation [18] with all quantities evaluated at previous cycle n .

E. Flow Near Primary Vessel and Deformable Internals

The mathematical model for treating fluid-structure interactions near the primary vessel and deformable internals was described in ICECO-II report [13]. Here, we briefly mention the numerical treatment.

1. The Fluid-Vessel Interface

The interface between the fluid and the deformable vessel (such as the primary vessel, pipe wall, etc.) is treated as a free surface of the fluid but subjected to a pressure distribution that determines its motion. Such interfacial motion is made to conform with the motion of the structure generated by the internal hydrodynamic pressure loading. Since the viscosity of the fluid (like water or sodium) is very small, the sliding boundary condition is used at the interface which requires that the fluid is allowed to slide along the interface, but in the normal direction, the fluid and the structure are forced to move together.

A convenient way to satisfy the sliding boundary condition is by iteratively adjusting the pressure on the fluid interface by an amount proportional to the mass flow rate of the fluid normal to the boundary of the deformable structure. Thus, denoting h and $h+1$ the previous and new iterates, respectively, the relaxation equation for the pressure in the fluid-structure interfacial cell (k,l) is [13,19]

$$\bar{p}_{k,l}^{h+1} = \bar{p}_{k,l}^h - \frac{\rho \delta}{2\delta t} \left\{ \left[\bar{v}_p - \bar{v}_b \right] \cdot \bar{n} \right\}_{k,l} \quad (50)$$

In the above equation, \bar{v}_b is the velocity vector at the midpoint of the structure segment, \bar{v}_p is the velocity vector of the fluid particle, \bar{n} is the unit normal of the boundary pointing into the fluid, and δ is the smallest value between δr and δz . Thus, during the pressure iteration, one can see that if the particles attempt to cross the boundary the pressure in the boundary cell will be increased, forcing fluid to flow away from the boundary and vice versa.

2. Interaction of Fluids with Deformable Internals

Since fluids have different motions on both sides of the internal structure, the field variables such as p , ρ , u , and v in the cell containing structure are assumed to have different values. For instance, if the cell (i,j) contains the core barrel where both sides are submerged in the fluid the field variables should have two sets of values. The variables P^L , ρ^L , u^L , and v^L are calculated in such a way that the fluid on the left-hand side of the core barrel slides tangentially. Likewise, P^R , ρ^R , u^R , and v^R are obtained so that the fluid on its right-hand side also moves tangentially. Similarly, field variables can be obtained for the fluid located at the top or bottom of the structure. In general, for those variables at the exterior side of a Eulerian cell which cannot be computed by the conservation equation, extrapolation of their values from the interior region is necessary. The velocity components can be obtained from the mass conservation equation. These multi-valued velocity fields will be used consistently in the particle-movement and source-term modifications. They are also utilized in handling fluid motion at the geometrical discontinuities. For further details, see Ref. [13].

Analysis of fluid-structure interactions involving flexible internals is a complex problem. The analysis is further complicated if the structure possesses certain perforated openings, like the core-support-structure shown in Fig. 10. One way of dealing with this problem is to use the control-volume technique to derive the conservation equations and their difference representation with respect to the partial cell which is actually occupied by the fluid (such as CDEF shown in Fig. 10). However, because the structure component in general moves two dimensionally and the shape of the partial cell is highly irregular, the procedure of the control-volume technique is too cumbersome.

In order to accommodate the deformable internal and the perforated structures, we provide a scheme which still uses the relaxation equation to obtain the pressure adjacent to the structure but modifies that equation to account for the sodium flow through the openings. The basic idea is to homogenize the perforated structure member so that the total mass flux through the openings is uniformly distributed throughout the entire member. In other words, for those members containing openings, such as AB and CD in Fig. 10, we allow

fluid penetration and separation at the boundaries. To simplify the analysis, we further propose that: (a) fluids inside the coolant passage move one dimensionally, (b) sodium flows perpendicularly to the boundary at the entrance or exit, (c) the density variation inside the coolant passage is negligible, so that the amount of mass flowing into the passage is equal to the mass flowing out of the passage.

Thus, similar to Eq. (50) the modified relaxation equation for cell (k, ℓ) which contains of the boundary of an internal with or without perforated openings is

$$\bar{p}_{k,\ell}^{h+1} = \bar{p}_{k,\ell}^h - \frac{\delta}{2\delta t} \left\{ \rho \left(\bar{v}_p - \bar{v}_b \right) \cdot \bar{n} - \rho \phi \bar{v} \right\}_{k,\ell} \quad (51)$$

We recall that ϕ is the perforation ratio of the structural component, \bar{v} is the fluid velocity inside the coolant passageways and is evaluated from pressures on both sides of the structure [13].

F. Treatment of the Bubble-Coolant Interface and Free Surface

1. Marker Particle and Volume Fraction Methods

In calculating the high-energy excursion it is necessary to know the positions of the bubble-coolant interface and the coolant free surface so that pressures applied to the fluid boundaries can be calculated. Two different approaches are commonly used in the Eulerian hydrodynamics for calculating the positions of the fluid boundaries. These two approaches generally referred as the marker-particle method [20] and the volume-fraction method [21]. The marker-particle method uses Lagrangian particles to define the free surface and the interface. These particles, initially embedded in the fluid, are advected to their new positions using a simple kinematic relation between the fluid velocities in the local Eulerian cells. Consequently, fluid boundaries are clearly defined and good spatial resolution can be achieved. Since curved surface is allowed within one Eulerian cell this approach is potentially accurate regardless whether coarse or fine mesh is chosen in the analysis.

The volume-fraction method, on the other hand, utilizes fluid-volume fraction to determine the interface position and orientation. Normally, the free surface

within one Eulerian cell is considered as a straight line. Since no curvature of fluid boundary is allowed in the surface cell, position of free surface thus cannot be defined exactly. This approach is the equivalent of two marker particles per cell and generally works well if very fine mesh configurations are used in the analysis, but fails to provide good resolution if coarse mesh configuration is chosen.

Because of the difference mentioned above, the free surface is delineated by marker particles that move through the stationary network of cells. Each Eulerian cell is flagged to denote whether it is an empty cell (E) containing no fluid; a surface cell (S), which contains fluid but is next to an empty cell; or a full cell (F), which contains fluid and is not next to an empty cell.

2. Free-Surface Boundary Conditions

The correct free-surface boundary conditions are the continuities of the normal and tangential stresses suggested by Nichols and Hirt [20]. In general, for a viscous, compressible fluid the stress tensor is

$$\sigma_{ij} = -p\delta_{ij} + \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} - \frac{2}{3} \delta_{ij} \frac{\partial u_l}{\partial x_l} \right) + \xi \delta_{ij} \frac{\partial u_l}{\partial x_l}, \quad (52)$$

where δ_{ij} is the Kronecker delta, ξ is another second coefficient of viscosity and is defined as $\xi = \lambda + \frac{2}{3} \mu$.

Since most liquids the compressibilities are small, they may be regarded as practically incompressible. Thus, the stress tensor takes the form

$$\sigma_{ij} = -p\delta_{ij} + \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right). \quad (53)$$

Considering a free surface with a unit area n as illustrated in Fig. 6, it can be shown that, in terms of the stress tensor, the force acting on this surface is

$$\hat{F}_s = \hat{F}_r + \hat{F}_z, \quad (54)$$

where

$$\hat{F}_r = n_r (\sigma_{rr} \hat{e}_r + \sigma_{rz} \hat{e}_z) , \quad (55)$$

and

$$\hat{F}_z = n_z (\sigma_{rz} \hat{e}_r + \sigma_{zz} \hat{e}_z) . \quad (56)$$

Where \hat{F}_r and \hat{F}_z represent the force components acting on surfaces AC and BC which have outnormals parallel to the r- and z-axis, respectively.

Neglecting the viscosity of the gas the condition of normal force continuity yields

$$p - 2\mu \left[n_r^2 \frac{\partial u}{\partial r} + n_r n_z \left(\frac{\partial u}{\partial z} + \frac{\partial v}{\partial r} \right) + n_z^2 \frac{\partial v}{\partial z} \right] = p_a , \quad (57)$$

where p_a is the pressure applied at the free surface; n_r and n_z are the r and z components of the unit outward normal vector to the surface AB.

Similarly, the vanishing of the shear force on surface AB takes the form

$$2\mu \left[2n_r m_r \frac{\partial u}{\partial r} + \left(n_r m_z + n_z m_r \right) \left(\frac{\partial u}{\partial z} + \frac{\partial v}{\partial r} \right) + 2n_z m_z \frac{\partial v}{\partial z} \right] = 0 , \quad (58)$$

where m_r and m_z are the components of the unit tangential vector.

For problems involving shock-wave propagation the effect of viscosity, and hence of the boundary layer, is very small. The condition of normal force continuity at the free surface and the bubble-fluid interface implies that

$$p_{i,j} = p_a . \quad (59)$$

Also, if the curvature of the free surface is small, the condition of vanishing of tangential force is

$$\mu \left(\frac{\partial u_n}{\partial m} + \frac{\partial u_m}{\partial n} \right) = 0 , \quad (60)$$

where n denotes the outward normal direction and m the tangential direction to the local free surface. In the two-dimensional flow if the surface is nearly horizontal or vertical, the condition is

$$\frac{\partial u}{\partial z} + \frac{\partial v}{\partial r} = 0 \quad (61)$$

For the case shown in Fig. 11, the radial velocity $u_{i+1/2,j+1}$ is calculated from the finite-difference expression of the above expression:

$$u_{i+1/2,j+1} = u_{i+1/2,j} - \frac{\delta z}{\delta r} \left(v_{i+1,j+1/2} - v_{i,j+1/2} \right) \quad (62)$$

G. Wave Transient in Cavitated Liquids

During an HCDA pressure wave emanating from the reactor core encounters not only the surrounding structure, but also the coolant free surface from which it is reflected as a rarefaction wave. As the rarefaction wave propagates downward a tension regime is established over a large portion of the coolant domain. When a region of coolant passes into tension exceeding its tensile strength it is found from experiments that a rapid growth of bubbles is observed. These bubbles contain vapor and gas if any was previously dissolved in the liquid and are presumed to have previously existed as invisible "cavitation nuclei" distributed throughout the liquid. Thus, in order to provide an accurate analysis treatment of liquid cavitation must be considered.

Most hydrodynamic codes employ an equation of state which supplies a relationship between the pressure, density, and specific internal energy of the coolant. This equation of state together with conservation equations of mass, momentum, and energy permit the solution of the dynamic system. Compression equations of state have been determined for most liquids but very little is known about the equation of state of liquids in tension. One common approach for treating cavitation is analytically continuing the compressive equation of state into the tension regime and assuming a pressure cutoff at some point corresponding to the "tensile strength" of the liquid. Once the pressure cutoff is reached, variations in liquid volume (or density) do not affect the pressure, which remains at the cutoff value until the liquid recompacts. This model is usually referred to as the " p_{\min} model" [22-24]. The typical pressure-volume and pressure-density curves for the " p_{\min} model" are shown in Fig. 12.

Note that the " p_{\min} " model is the most simplest approach in which energy dissipations generated by the growth and collapse of the cavitated liquids are

neglected. Since no damping or dissipation involved in the analysis, numerical calculations employing the explicit solution algorithm thus have spurious oscillations.

Another approach considering damping term suggests that energy dissipation can occur in a cavitated liquid as a result of the finite rate at which cavitation bubbles grow and collapse. When this effect is taken into account the pressure-volume (p-v) paths for cavitated liquids become a hysteresis loop rather than the open curve in connection with the " p_{\min} " model. Thus, damping can be expected which could produce smoother pressure histories during recompaction of the cavitated liquid.

In this sophisticated cavitation model the dynamics of bubble growth is governed by the Rayleigh equation. Including surface tension and velocity damping this equation has the form

$$R \frac{d^2 R}{dt^2} + 2/3 \left(\frac{dR}{dt} \right)^2 = - \frac{1}{\rho} \left(p + \frac{2\sigma}{R} + 4 \frac{\mu \dot{R}}{R} \right), \quad (63)$$

where R is the average radius of the cavitated bubbles, ρ is the liquid density, p is the pressure, σ is the surface tension, μ is the viscosity.

Thus, if one attempts to include the bubble-growth rate in the numerical calculation, one must solve the Rayleigh equation along with conservation equations. This could further complicate the analysis. Nevertheless, this seems to be the only way to improve the solution of the explicit hydrodynamic codes.

Since the ICECO code uses the implicit integration scheme, the solution is stable and the adverse effect of fluid cavitation on the numerical results is less severe than those of the explicit containment codes. Therefore, the equation of state similar to the " p_{\min} " model shown in Fig. 12 has been incorporated into ICECO for calculating wave transient in the cavitated liquid.

H. Heat Transfer and Fuel-Coolant Interaction

Several years ago a fuel-coolant interaction (FCI) model [12] was incorporated into the ICECO code to study various heat transfer problems related to the

containment analysis. This model is the quasi-steady-state model (QSS) Ref. [25] in which the only resistance to heat transfer is assumed as due to the thermal conductivity of the fuel. Since the thermal conductivity of the liquid sodium is higher by an order of magnitude than that of the fuel, it is reasonable to neglect the thermal resistance due to sodium. The heat-transfer rate for the QSS model is given by the relation

$$\dot{q} = hA (T_f - T) \quad , \quad (64)$$

where

\dot{q} = heat-transfer rate,

T_f = fuel temperature,

T = sodium-coolant temperature,

and hA is a parametric heat-transfer coefficient based upon the fuel thermal conductivity and molten-fuel particle size in which

$$h = \frac{k_f}{r_f} \quad , \quad (65)$$

and

$$A = 4\pi r_f^2 \quad , \quad (66)$$

where k_f is the fuel thermal conductivity. In this study, the units are expressed in cgs units. The main hindrance to heat transfer is assumed to be due to the thermal conductivity of the fuel. Heat transferred to the sodium is distributed to all sodium in a fuel-coolant-interaction zone so that no thermal gradients exist in the sodium and it can be considered to be in thermodynamic equilibrium throughout the process. The heat of fusion of the fuel is neglected as a first approximation. Due to the nature of the lumped-parameter approach, the model roughly accounts for a finite, though unspecified, fragmentation rate. For more details, the reader should refer to Refs. [25-27].

I. The Equation of State of the Media

As described before the solution of the conservation equations requires an equation of state to describe the behavior of the reactor materials, particularly

in the reactor core and the coolant. The forms of equation of state which have been used are:

a. Murnaghan for fluids:

$$\bar{p} = p^n + c^n (\rho^{n+1} - \rho^n) , \quad (67)$$

in which

$$c^n = a_o^2 \left(1 + \frac{p_o^n \eta}{p_o a_o^2} \right) \frac{p_o}{\rho^n} , \quad (68)$$

is closely related to the speed of sound; a_o , p_o , and ρ_o are the speed of sound, pressure, and the density at the standard conditions, respectively; η is the isentropic exponent.

b. Isentropic equation of state for the core-gas bubble and the trapped air:

$$p = p_o \left(\frac{\bar{v}_o}{\bar{v}} \right)^\gamma , \quad (69)$$

where p_o and \bar{v}_o are the initial pressure and volume, respectively; γ is the isentropic exponent.

c. Pressure as a function of volume ratio \bar{v}/\bar{v}_o for core-gas bubble and air:

$$p = f \left(\frac{\bar{v}}{\bar{v}_o} \right) . \quad (70)$$

d. Pressure as a function of time:

$$p = f(t) . \quad (71)$$

e. Murnaghan for elastic-plastic solids and small distorted fluids:

$$p = \frac{B_o}{B_o'} \left[\left(\frac{\bar{v}_o}{\bar{v}} \right)^{B_o'} - 1 \right] , \quad (72)$$

in which B_o and B_o' are the bulk modulus and its pressure derivative, respectively.

Noted that equations related to fuel-coolant interactions described in the previous section are not included here.

J. Differencing Schemes and Convective Fluxes

There are various ways that the convective fluxes of the conservation equations can be written. The precise form although is irrelevant to the conceptual formulation used in the ICECO code but is crucial to the accuracy and numerical stability of the calculation. In the ICECO-H code [11] ZIP differencing scheme was used. Recently, capabilities of treating above-core hydrodynamics and sodium spillage have been added to the computer code. In these analysis, fluid motions in the vicinity of the upper internal structure and the reactor cover are sensitive to the directions of the flow. Therefore, a complete donor-cell differencing scheme was incorporated into the code as an option to the ZIP differencing scheme. Also a partial donor-cell differencing scheme has been added to the code to deal with the ongoing effort on the multi-material interactions. Thus, at the present time three types of flux expressions, i.e. ZIP, complete donor, and partial donor were already considered in the mathematical formulation.

According to the description of the ICE technique each of these three flux expressions has advantages and disadvantages. Here, we present various expressions for the convective fluxes $(\rho u^2)_{i,j}$ and $(\rho uv)_{i+\frac{1}{2},j-\frac{1}{2}}$ of the radial momentum equation and discuss the advantages and disadvantages of each expressions. Since in these flux terms certain variable is not defined at which the flux is to be evaluated some type of interpolation is needed.

The three flux expressions to be considered are described below.

ZIP:

$$(\rho u^2)_{i,j} = \rho_{i,j} u_{i-\frac{1}{2},j} u_{i+\frac{1}{2},j}$$

Complete Donor:

$$(\rho u^2)_{i,j} = \begin{cases} \rho_{i,j} u_{i-\frac{1}{2},j}^2 & \text{if } (u_{i-\frac{1}{2},j} + u_{i+\frac{1}{2},j}) > 0 \\ \rho_{i,j} u_{i+\frac{1}{2},j}^2 & \text{if } (u_{i-\frac{1}{2},j} + u_{i+\frac{1}{2},j}) < 0 \end{cases}$$

Partial Donor:

$$(\rho u^2)_{i,j} = \begin{cases} \rho_{i,j} u_{i-\frac{1}{2},j} (u_{i-\frac{1}{2},j} + u_{i+\frac{1}{2},j}) & \text{if } (u_{i-\frac{1}{2},j} + u_{i+\frac{1}{2},j}) > 0 \\ \rho_{i,j} u_{i+\frac{1}{2},j} (u_{i-\frac{1}{2},j} + u_{i+\frac{1}{2},j}) & \text{if } (u_{i-\frac{1}{2},j} + u_{i+\frac{1}{2},j}) < 0 \end{cases}$$

Also, for both complete and partial-donor differencing schemes:

$$(\rho uv)_{i+\frac{1}{2},j-\frac{1}{2}} = \begin{cases} \frac{1}{4} (v_{i,j-\frac{1}{2}} + v_{i+1,j-\frac{1}{2}}) (\rho_{i,j-1} + \rho_{i+1,j-1}) u_{i+\frac{1}{2},j-1} & \text{if } \frac{(v_{i,j-\frac{1}{2}} + v_{i+1,j-\frac{1}{2}})}{2} > 0 \\ \frac{1}{4} (v_{i,j-\frac{1}{2}} + v_{i+1,j-\frac{1}{2}}) (\rho_{i,j} + \rho_{i+1,j}) u_{i+\frac{1}{2},j} & \text{if } \frac{(v_{i,j-\frac{1}{2}} + v_{i+1,j-\frac{1}{2}})}{2} < 0 \end{cases}$$

The ZIP form is one order more accurate in δr and δz than the donor-cell flux. In addition, it has the advantages of eliminating a nonlinear contribution to instability [28]. For this reason the ZIP flux is often preferred for the momentum convection, except in problems the flow direction may play important role in the numerical solutions.

In the donor-cell expressions, either the complete- or partial-donor flux, the finite difference expression is not space-centered, and hence both have low order (in δr and δz) truncation errors. This contribute a positive diffusive effect and accordingly tend to automatically stabilize the numerical calculations. The magnitude can be excessive, thus leads to erroneous interpretations.

Our recommendation is to use ZIP differencing scheme in the majority calculations, such as the wave propagation, slug impact, expanding gas bubble, fluid-structure interaction, liquid cavitation, and the containment response. The only circumstances in which a complete-donor cell differencing scheme appears desirable is in the analysis of sodium spillage where violent fluid motion near the reactor cover may occur. In fact, except for problems dealing with the sodium spillage, all other problems presented in this report are all using the ZIP differencing scheme.

K. Lagrangian Formulation for Continua and Structures

Because of history dependence of the constitutive equations Lagrangian coordinate system is employed in the dynamic analysis of structure and solid continua. In view of complicated structure components involved in a typical reactor configuration, several separate programs are employed for analyzing the structural response. Several years ago, a finite-difference thin-shell program has been used in analyzing the response of the primary vessel. This program is now available as an option to the finite-element program in another version of ICECO code [13].

Presently, in the analysis of plug-jump and sodium-spillage problems, the motion of the reactor head, which is assumed to have only the rigid body motion under the constraint of the hold-down bolts, is calculated by a finite-difference program.

The shell structure in the reactor containment is now analyzed by a finite-element scheme developed by Belytschko and Hsieh [29-31]; whereas the elastic-plastic solid is analyzed by the finite-difference method utilized by Wilkins [7]. To facilitate the numerical treatment of boundary conditions and the arbitrary combination of the solid, the fluid, and the shell structure the equation of motion used in the finite-difference calculation for the solid media are formulated through the use of intermediate nodal forces. Thus, the equation of motion for solid and shells can be written as

$$M \ddot{u} = F^{\text{ext}} - F^{\text{int}}, \quad (73)$$

where M is the mass matrix; u the displacements; F^{ext} the discretized external

forces; and F^{int} the discretized internal forces; dots over the quantity denote time derivative. The equation of motion are integrated explicitly using a central difference scheme. Thus, velocities and displacements in the global coordinates are determined by the following relations

$$\begin{aligned}\dot{\underline{u}}(t + \Delta t) &= \dot{\underline{u}}(t) + \frac{1}{2} \Delta t [\ddot{\underline{u}}(t) + \ddot{\underline{u}}(t + \Delta t)] , \\ \underline{u}(t + \Delta t) &= \underline{u}(t) + \Delta t \dot{\underline{u}}(t) + \frac{1}{2} \Delta t^2 \ddot{\underline{u}}(t) .\end{aligned}\tag{74}$$

The oftenly used two elements, i.e. quadrilateral torodial continuum solid and conical shell elements, are briefly described. Other two elements, triangular and quadrilateral fluid elements, are given in Ref. [30].

1. Quadrilateral Continuum

The quadrilateral element can be used to model the elastic-plastic solids in the primary containment such as the radial shield and lead. It also can be used to simulate the compressible fluids with small distortion. In the analysis, the mass of each element is assumed to be equally distributed to its four vertice nodes. Thus the mass associated with each node point shown in Fig. 13 is

$$M_o = \frac{1}{4} \sum_{i=1}^4 M^{(i)} .$$

a. Nodal Force

The external forces are the pressure forces transmitted from the fluids. These forces are supplied by the fluid-dynamic calculation. The internal forces can be computed from the finite-difference representations similar to the method utilized by Wilkins [7]. In the Lagrangian formulation the equations of motion in the r and z directions are:

$$\begin{aligned}\ddot{r} &= \frac{1}{\rho} \left[\frac{\partial \sigma_{rr}}{\partial r} + \frac{\partial \sigma_{rz}}{\partial z} + \frac{\sigma_{rr} - \sigma_{\theta\theta}}{r} \right] , \\ \ddot{z} &= \frac{1}{\rho} \left[\frac{\partial \sigma_{rz}}{\partial r} + \frac{\partial \sigma_{zz}}{\partial z} + \frac{\sigma_{rz}}{r} \right] ,\end{aligned}\tag{75}$$

in which

$$\sigma_{rr} = \bar{\sigma}_{rr} - (p + q) ,$$

$$\sigma_{zz} = \bar{\sigma}_{zz} - (p + q) ,$$

$$\sigma_{\theta\theta} = \bar{\sigma}_{\theta\theta} - (p + q) ,$$

are the total stress components in the radial, axial, and circumferential directions, respectively; $\bar{\sigma}_{rr}$, $\bar{\sigma}_{zz}$, and $\bar{\sigma}_{\theta\theta}$ are the corresponding deviatoric stress components; σ_{rz} is the shearing stress; p is the pressure; q is the viscous pressure; ρ is the density; r and z are the nodal coordinates in the r and z directions, respectively.

In the finite-difference representation the equations of motion for a generic element shown in Fig. 13 are

$$\ddot{r} = -\frac{1}{2\Phi} \left[\sigma_{rr}^{(1)} z_{ab} + \sigma_{rr}^{(2)} z_{bc} + \sigma_{rr}^{(3)} z_{cd} + \sigma_{rr}^{(4)} z_{da} - \sigma_{rz}^{(1)} r_{ab} - \sigma_{rz}^{(2)} r_{bc} - \sigma_{rz}^{(3)} r_{cd} - \sigma_{rz}^{(4)} r_{da} \right] + \frac{1}{4} \sum_{i=1}^4 \left[(\sigma_{rr} - \sigma_{\theta\theta}) \frac{A^n}{M} \right]^{(i)} , \quad (76)$$

and

$$\ddot{z} = \frac{1}{2\Phi} \left[\sigma_{zz}^{(1)} r_{ab} + \sigma_{zz}^{(2)} r_{bc} + \sigma_{zz}^{(3)} r_{cd} + \sigma_{zz}^{(4)} r_{da} - \sigma_{rz}^{(1)} z_{ab} - \sigma_{rz}^{(2)} z_{bc} - \sigma_{rz}^{(3)} z_{cd} - \sigma_{rz}^{(4)} z_{da} \right] + \frac{1}{4} \sum_{i=1}^4 \left[\sigma_{rz} \frac{A^n}{M} \right]^{(i)} , \quad (77)$$

in which

$$\Phi = \frac{1}{4} \sum_{i=1}^4 (A^n \rho^n)^{(i)} , \quad (78)$$

$$z_{xy} = z_x - z_y \quad \text{and} \quad r_{xy} = r_x - r_y .$$

In the Eqs. (76-78) A^n is the area of the quadrilateral at previous cycle (n); $M^{(i)}$ is the original mass associated with i th element; also, Φ must be modified at the boundary of the Lagrangian domain [31].

Note from Eqs. (76,77) that the nodal accelerations are functions of the stresses in its four neighboring zones. This formula is quite restrictive in applying to the general problems. Particularly at the boundary of the structure where certain nodes may be connected by one or two quadrilaterals. Thus, to facilitate the treatment of boundary conditions and the arbitrary combination of the solid and thin shell elements the equation of motion are written through the use of the intermediate nodes forces of each element. Thus, for a typical element shown in Fig. 14, the internal nodal forces in the r and z directions are:

$$(F_1)_r^{\text{int}} = \frac{1}{2} [\sigma_{rr} (z_2 - z_4) - \sigma_{rz} (r_2 - r_4)] \bar{r} - X, \quad (79a)$$

$$(F_2)_r^{\text{int}} = \frac{1}{2} [\sigma_{rr} (z_3 - z_1) - \sigma_{rz} (r_3 - r_1)] \bar{r} - X, \quad (79b)$$

$$(F_3)_r^{\text{int}} = \frac{1}{2} [\sigma_{rr} (z_4 - z_2) - \sigma_{rz} (r_4 - r_2)] \bar{r} - X, \quad (79c)$$

$$(F_4)_r^{\text{int}} = \frac{1}{2} [\sigma_{rr} (z_1 - z_3) - \sigma_{rz} (r_1 - r_3)] \bar{r} - X, \quad (79d)$$

and

$$(F_1)_z^{\text{int}} = -\frac{1}{2} [\sigma_{zz} (r_2 - r_4) - \sigma_{rz} (z_2 - z_4)] \bar{r} - Y, \quad (80a)$$

$$(F_2)_z^{\text{int}} = -\frac{1}{2} [\sigma_{zz} (r_3 - r_1) - \sigma_{rz} (z_3 - z_1)] \bar{r} - Y, \quad (80b)$$

$$(F_3)_z^{\text{int}} = -\frac{1}{2} [\sigma_{zz} (r_4 - r_2) - \sigma_{rz} (z_4 - z_2)] \bar{r} - Y, \quad (80c)$$

$$(F_4)_z^{\text{int}} = -\frac{1}{2} [\sigma_{zz} (r_1 - r_3) - \sigma_{rz} (z_1 - z_3)] \bar{r} - Y, \quad (80d)$$

where

$$\bar{r} = \frac{M_0}{\rho^n A^n},$$

$$X = \frac{1}{4} (\sigma_{rr} - \sigma_{\theta\theta}) \frac{\phi}{\rho} \quad \text{and} \quad Y = \frac{1}{4} \sigma_{rz} \frac{\phi}{\rho}.$$

In Eqs. (79,80) subscripts r and z are used to denote the internal nodal forces in the radial and axial directions, respectively.

b. Stress and Yield Condition

The calculations of strain rates (or the velocity strains) are implemented by performing line integration along the counter 1234 of a typical Lagrangian element shown in Fig. 14. Evaluating at time $n+1/2$, they have the following form

$$\begin{aligned}\dot{e}_{rr} &= \frac{1}{2A} [(\dot{r}_2 - \dot{r}_4)(z_3 - z_1) - (\dot{r}_3 - \dot{r}_1)(z_2 - z_4)] , \\ \dot{e}_{zz} &= -\frac{1}{2A} [(\dot{z}_2 - \dot{z}_4)(r_3 - r_1) - (\dot{z}_3 - \dot{z}_1)(r_2 - r_4)] , \\ \dot{e}_{\theta\theta} &= \frac{\dot{V}}{V} - (\dot{e}_{rr} + \dot{e}_{zz}) ,\end{aligned}\tag{81}$$

and

$$\begin{aligned}\dot{e}_{rz} &= \frac{1}{2A} \{[(\dot{z}_2 - \dot{z}_4)(z_3 - z_1) - (z_2 - z_4)(\dot{z}_3 - \dot{z}_1)] \\ &\quad - [(\dot{r}_2 - \dot{r}_4)(r_3 - r_1) - (r_2 - r_4)(\dot{r}_3 - \dot{r}_1)]\} ,\end{aligned}$$

in which the dot over the quantity representing the time derivative of that quantity.

The incremental strains, Δe_{rr} , Δe_{zz} , $\Delta e_{\theta\theta}$, and Δe_{rz} and the incremental volume change ΔV at time $(n+1/2)$ can be simply computed from the respective rate change modifying by the time step [7].

The deviatoric stress components can be immediately calculated from

$$\begin{aligned}\bar{\sigma}_{rr}^{n+1} &= \bar{\sigma}_{rr}^n + 2\mu \left[\Delta e_{rr} - 1/3 \frac{\Delta V}{V} \right]^{n+1/2} + \delta_{rr}^n , \\ \bar{\sigma}_{zz}^{n+1} &= \bar{\sigma}_{zz}^n + 2\mu \left[\Delta e_{zz} - 1/3 \frac{\Delta V}{V} \right]^{n+1/2} + \delta_{zz}^n , \\ \bar{\sigma}_{\theta\theta}^{n+1} &= \bar{\sigma}_{\theta\theta}^n + 2\mu \left[\Delta e_{\theta\theta} - 1/3 \frac{\Delta V}{V} \right]^{n+1/2} , \\ \sigma_{rz}^{n+1} &= \sigma_{rz}^n + \mu [\Delta e_{rz}]^{n+1/2} + \delta_{rz}^n ,\end{aligned}\tag{82}$$

in which δ_{rr}^n , δ_{zz}^n , δ_{rz}^n are stress corrections due to rotation see Refs. [3,7].

These terms are required if a mass element has rotated in the r - z plane by an

angle during the time interval $\Delta t^{n+1/2} = t^{n+1} - t^n$, the stresses must be recalculated so that they will be referred to the r-z coordinates in their new position.

For the yield condition calculation a invariant J_2 is given by

$$2J_2^{n+1} = \left(\bar{\sigma}_{rr}^{n+1}\right)^2 + \left(\bar{\sigma}_{zz}^{n+1}\right)^2 + \left(\bar{\sigma}_{\theta\theta}^{n+1}\right)^2 + 2\left(\bar{\sigma}_{rz}^{n+1}\right)^2,$$

and

(83)

$$2J_2^{n+1} - 2/3 (\sigma_y^n)^2 = K^{n+1},$$

where σ_y^n is the yield stress obtained from the plastic stress-strain relationships. If $K^{n+1} \leq 0$ the deviatoric stresses as calculated in Eq. (82) are used to compute the internal nodal forces. However, if $K^{n+1} > 0$ the computed deviatoric stresses must be multiplied by a factor of $(2/3)^{1/2} \sigma_y^n / (2J_2^{n+1})^{1/2}$ to calculate the internal nodal forces.

2. Shell Element

In the ICECO code the reactor vessel, core barrel, and the core-support structure can be treated as thin axisymmetric shells or plates, in which the analysis accounts for the membrane and bending strengths of the shells, elastic-plastic material behavior, and large deformations under transient loading conditions.

A conical shell element developed by Belytschko and Hsieh [29] is utilized to model the thin shells or plates. This element is formulated using a convective (or corotational) coordinate system. In the analysis, each shell element is associated with a convective coordinate system that rotates but does not deform with the element. Strains are assumed to be linearly related to the displacement of the element relative to its convective coordinates. Similarly, the nodal forces are considered to be linearly related to the element stresses within its convective coordinates.

In the mathematical formulation the convected \hat{x} axis is taken to lie along the line joining the nodes. Cubic polynomial shape functions in \hat{x} are used for

the transverse displacements and a linear shape functions are employed for the axial displacement. Although the rotation within this type of element is not constant, the rotation with respect to the \hat{x} axis joining the two end nodes of the element is small, since the strains are assumed to be small. Hence the rotation of the \hat{x} axis, α , should be a good approximation of the rotational component of the element's displacement.

The deformation displacements are then the nodal rotations with respect to the \hat{x} axis shown in Fig. 15

$$\hat{\phi}_i = \phi_i - \alpha \quad (\alpha = 1, 2) \quad . \quad (84)$$

The midplane displacement thus can immediately be expressed in terms of the midplane strain $\hat{\epsilon}_m$.

In terms of the convective coordinates \hat{x} and \hat{y} the strain-displacement relations are

$$\begin{aligned} \hat{\epsilon}_x &= \hat{\epsilon}_m - \hat{y} \frac{\partial \hat{\phi}(\hat{x})}{\partial \hat{x}} \\ \hat{\epsilon}_\theta &= \frac{1}{r} \left(u_r - \hat{y} \cos \beta \frac{\partial u_y}{\partial \hat{x}} \right) \quad , \end{aligned} \quad (85)$$

where

$$\hat{\epsilon}_m = \frac{\partial u_x^{\text{def}}}{\partial \hat{x}} \quad ,$$

is the midplane strain; β is the angle of inclination; u_r and u_y are the global displacements in the radial and axial directions, respectively.

The cubic shape function transverse displacement field is

$$\hat{\phi}(\hat{x}) = \frac{\hat{\phi}_1}{\ell^2} (\ell^2 - 4\ell\hat{x} + 3\hat{x}^2) + \frac{\hat{\phi}_2}{\ell^2} (3\hat{x}^2 - 2\ell\hat{x}) \quad . \quad (86)$$

The stresses in the convective coordinates are then computed from the stress-strain laws. A multilinear segment representation [32] is employed to simulate the material nonlinearities. The equations for the internal node forces are

$$\begin{Bmatrix} m_1^P \\ m_2^P \\ \hat{f}_{2x}^P \end{Bmatrix} = -\frac{1}{\ell^2} \int_V \begin{bmatrix} (\hat{6x} - 2\ell) \hat{y} \\ (\hat{6x} - 2\ell) \hat{y} \\ \ell \end{bmatrix} \sigma_x dV \quad (87)$$

The other nodal forces are found by using self-equilibrium equations, and have the form

$$\hat{f}_{1y}^P = -\hat{f}_{2y}^P = \left(m_1^P + m_2^P \right) / \ell ,$$

and

$$\hat{f}_{1x}^P = -\hat{f}_{2x}^P .$$

(88)

The nodal forces are then transformed into the global coordinates. The internal nodal forces due to the circumferential stresses are computed by the standard linear nodal force-stress relation. Detail derivations can be seen in Refs. [29,30].

L. Stability Consideration

For the consideration of numerical stability, the time step δt_h chosen for the hydrodynamic analysis must satisfy the modified "Courant Condition." The restriction is that fluid must not be permitted to flow across more than one computational cell in one time step; that is

$$\delta t_h < \min \left(\frac{\delta r}{|u|_{\max}}, \frac{\delta z}{|v|_{\max}} \right) . \quad (89)$$

Since in the plug jump (movable head) problem the axial dimension of the quasi-Eulerian cell varies with the head displacement and is much smaller than the axial dimension of the regular cell, the time step used at the inception of slug impact is further restricted by

$$\delta t_h < \frac{\delta y}{|v_y|_{\max}} , \quad (90)$$

where δy is the axial dimension of the quasi-Eulerian cell, and v_y is the axial velocity component in the quasi-Eulerian cell. Typically, δt_h is chosen

equal to one-fourth to one-third of the minimum cell transient time obtained either from Eq. (89) or (90).

For the coupled fluid-structure analysis, the time step δt_s employed for the structural dynamic program must satisfy the following requirements

$$\delta t_s = \beta \frac{l}{c_l} , \quad (91)$$

and

$$\delta t_s = \beta \frac{l}{6c_b} . \quad (92)$$

Equation (91) applies to all elements, Eq. (92) only to flexural shell element. Here β is a reduction factor usually between 0.5 and 0.8; l is the distance between two nodes; c_l and c_b are longitudinal and flexural wave velocities, respectively, and are defined in Ref. [30].

Because the hydrodynamic program uses implicit integration scheme while the structural dynamic program utilizes explicit integration procedure, δt_h is larger than δt_s . Thus, within each time step several structural dynamic calculations must be performed in order to match one hydrodynamic calculation. The number of structural calculations (or known as sub-cycles) N can be determined by

$$N = I (\delta t_h / \delta t_s) + 1 , \quad (93)$$

where I denotes the integer part of the ratio.

In certain circumstances, the viscosity coefficients λ and μ should be used to damp out the pressure oscillation, particularly in a high-energy excursion. Thus, similar to the treatment of the ICECO technique, the coefficients and μ should be large enough so that

$$\lambda, \mu \geq 3/2 \rho |\bar{v}|^2 \delta t + \rho_{\max} (\nabla \cdot \bar{v}) (\delta r^2, \delta z^2)_{\max} . \quad (94)$$

M. Solution Procedure

We have presented the equations governing the advanced-pressure field for the entire computing domain. In summary the govern difference equations for different regions are: (1) Poisson equation [i.e. Eq. (14)] for the cell full of fluids. (2) Modified Poisson equations [Eqs. (24), (32), (40)] for cells inside or near the perforated upper internal structures. (3) Modified Poisson equation [i.e. Eq. (48)] for the quasi-Eulerian irregular cells under the reactor cover. (4) Relaxation equation [Eq. (50)] for cells near the deformable external boundary. (5) Generalized relaxation equation [Eq. (51)] for cells containing boundaries of deformable internals.

In the analysis, Eqs. (14), (24), (32), (40), (48), (50), and (51) are solved together by the regular iterative technique, which sweep through all the regular and irregular cells in the directions of increasing i and j . During each iteration sweep, say at iteration cycle $h+1$, the new value of $(p_{i,j}^{n+1})^{h+1}$ is obtained from the corresponding governing equation and is used to replace the old value of $(p_{i,j}^{n+1})^{h+1}$. The iteration is terminated when the new values do not differ much from the old values. In other words, the convergence is achieved when

$$\left| \begin{array}{c} | p_{\text{new}}^{n+1} - p_{\text{old}}^{n+1} | \\ | p_{\text{new}}^{n+1} + p_{\text{old}}^{n+1} | \end{array} \right| \leq \epsilon ,$$

has been satisfied for all cells. Here ϵ is usually of the order 20×10^{-4} or equal to some other suitable small number.

Figure 16 is a flow chart representing the computation procedure.

III. APPLICATIONS

A. Response of Pool-Type LMFBR

This study deals with the analysis of wave propagations in a pool-type LMFBR, serving as part of the supporting effort for the PCRV adaptation. The emphasis is on the analyses of the expanding core-gas bubble, together with the response of the reactor internals. Because of relative large dimensions of trapped air and the reactor configuration, excessive interface distortion and long-duration calculation are often involved. Under these conditions, the ICECO code is well-suited for such analysis. Furthermore, the code is attractive since it can treat two-dimensional sliding interfaces, flow around corners, large-amplitude free-surface motion, and can provide a stable solution over the entire spectrum of excursions.

The initial configuration used in the analysis is shown in Fig. 17. In the analysis, the vessel boundary and the core-support structure are both considered as rigid the radial shield and the core barrel are treated as deformable. In order to have better resolution at the material interfaces dense particles are placed at the bubble boundary and the free surface. The initial pressure inside the reactor core is about 27 MPa.

A sequence of analytical configurations at the specified times is given in Fig. 18. This shows the expansion of the core-gas bubble and the impact of fluid onto the reactor cover. The distortion of the bubble-coolant interface and the movement of the coolant around the upper edge of the core barrel are also clearly shown. Figure 19 gives radial displacement history of the upper core barrel. As it can be seen the solution is very stable.

The code is very efficient. The CPU time is only 20 minutes. The solution extends to $t = 110$ ms that is long enough to include all the important transients generated during the excursion.

B. Above-Core Hydrodynamics Induced by Upper Internals

Sample problems are given to study the mitigating effect of the perforated upper internal structure on the containment response as well as various modeling techniques available.

1. The Effect of Upper Internal Structure on the Wave Propagation

Here, we investigate the effect of the UIS on the wave propagation, pressure loadings, and containment response during an HCDA. The initial reactor configuration chosen for this study is shown in Fig. 20. To reduce the number of parameters involved in the analysis we considered the core barrel and core-support structure, as well as the reactor cover, to be rigid. The reactor vessel is made of elastoplastic material. The stress-strain relationship describing the vessel properties was approximated by two straight-line segments. Two calculations are performed: one with and the other without the UIS. In the calculation with the UIS, the perforation ratios for the first four cells from the centerline are 0.40, 0.30, 0.20, and 0.10 respectively. The initial pressure inside the core gas bubble is 30 MPa.

Figure 21 compares the total forces on the reactor cover as a function of time for the two cases studied. As can be seen the UIS has a pronounced mitigating effect on the slug-impact load. For the case with this structure the peak force is smaller than without this particular structure.

Figure 22 presents the reactor configurations at three different times for the case with the UIS. The configuration shows how the bubble expands and how the vessel deforms during an excursion. In addition, Fig. 22 indicates significant flow blockage near the bottom plate of the UIS.

To assess the effect of the upper internal structure on the core-gas bubble expansion and energy release we have found from the results that in the calculation without this structure the HCDA bubble volume and the axial kinetic energy of the fluid at the time of the slug impact are 4649 cm^3 and 49.15 MJ, respectively. For the calculation with the upper internal structure the corresponding values reduce to 4438 cm^3 and 41.38 MJ, respectively. This demonstrates

that the upper internal structure also has capability of confining the HCDA bubble expansion and reducing the axial energy of the coolant slug.

2. Optional Modelings for the Upper Internal Structures

As mentioned before the ICECO code also can model the UIS by rigid obstacles. Thus, two more cases are investigated, using two different modelings. In the first case, the coolant passageways and the UIS are modeled by rigid obstacles with an equivalent perforation ratio of 0.38. In the second case, the UIS is modeled by the rigid obstacles with zero perforation ratio, which corresponds to the case where the UIS passageways were completely plugged by the upper core materials during a whole core disassembly accident. Figures 23 and 24 gives, respectively, reactor configurations at three different times. They show how the core-gas-bubble expands, and how the above-core coolant moves during the excursion. We have found that in the case with coolant passageways the peak value of the impact force is 12.10 MN, which falls in between the peak values of the two calculations given previously in Fig. 21. Whereas the peak value corresponding to the case without coolant passageway is 7.8×10^2 MN. As expected, it is less than all the respective values obtained from the calculations with the coolant passageways.

C. Sodium Spillage From the Primary Containment

1. Sodium Spillage During an Energetic HCDA

Analysis of sodium spillage was performed for a 1000-MWe loop-type reactor as shown in Fig. 25a. The reactor configuration is 8.8 m in diameter, which consists of an 8.25-cm thick flexible vessel wall, a fixed reactor head. Two leak paths are assumed to exist during the slug impact. The first one is located in the reactor cover, representing the penetration opening generated at the periphery of the small and intermediate rotating plugs of the reactor cover. Such penetration, initially closed, is modeled to open when the impulse reached a prescribed value. The second leak path is located at the vessel-head junction to simulate the gap created by the ruptured seal. Since the primary emphasis of this study was placed on sodium spillage through the two leak paths, calculation was begun at slug impact and with a uniform gas bubble in this

simplified reactor configuration. The axial velocity of the sodium slug is 50 m/sec and the initial core pressure is 4 MPa.

Figure 25b presents the reactor configuration at 50 ms. The displacement of the reactor cover and sodium ejections from the top penetration and side opening can be clearly seen. Figure 26 shows sodium velocities of the top penetration and the side opening. The results are presented to 50 ms, based upon the fact that the velocity at the penetration reaches its minimum value. Figure 27 presents the total coolant masses ejected from both top penetration and the side opening. Because the size of the side opening increases sharply during the excursion, larger amount of ejected sodium was observed at the vessel-head junction. The quantity and the velocity of the sodium ejected from the primary vessel is a primary concern in assessing the integrity of the secondary containment.

2. Integrated Analysis of Containment Response and Sodium Spillage

An integrated analysis of containment response and sodium spillage in a typical LMFBR is presented. The reactor configuration used in this study is shown in Fig. 28. It consists of a reactor core, a primary vessel, a moveable vessel head, and the holddown bolts. The core barrel and the core-support structure are assumed to be rigid. Consequently large impact force is expected and the results are conservative. Two penetration holes are located in the vessel head (shown by the dotted lines) to indicate the locations of leak paths. These penetrations are closed initially but will become open after being acted upon by the impulses of 3.5×10^9 and 1.5×10^9 dyne-sec, respectively. The holddown bolts are assumed to respond elastic-plastically.

Figure 29 presents reactor configurations at 18.9 and 22.6 ms. The expansion of the gas bubble, the fluid motion around the corner of the core barrel, as well as the deformation of the upper containment vessel can be clearly seen. Marker-particle configurations also show some interesting phenomena after the slug impact. In Fig. 29a the penetrations no longer can sustain the impulses generated by the slug impact and suddenly become open. Figure 29b shows that the reactor cover moves upward and certain amounts of coolant already spilled

out from both the penetrations and the side opening at the vessel-cover junction. The computation terminated at about 23 msec at which time the primary containment already reaches the dynamic equilibrium. The sodium spillage phenomenon is of primary importance for the initiation of sodium fires in the secondary containment.

D. The Effect of Core-Support-Structure Openings on the Containment Response

During an HCDA, the pressure wave emanating from the reactor core can propagate into the lower reactor plenum through the core-support-structure (CSS) openings and thereby cause a pressure increase in that region. In the conventional Lagrangian analysis of the primary containment response, the sodium flow through the coolant passageways of the core support structure did not take into consideration the difficulties of large material distortions induced by the openings. Although the solution gave conservative results for the slug-impact load and the upper vessel deformation, it underestimated the pressure loading at the inlet-nozzle region. In order to understand the influence of the CSS openings on the responses of the containment and components, as well as on the wave motion in the reactor plenum, we present here an analysis which accounts for the coolant flow through the CSS openings, and compare the results concerning the pressure loadings and bottom-vessel deformations for the cases with and without openings in the CSS.

The reactor configuration chosen for the analysis is shown in Fig. 30. It consists of the reactor core, coolant, radial shield, core barrel, core-support structure, and the primary vessel. The core support structure is modeled as a composite structure made of plates and shells as in the actual structure.

In the calculation, we assume that the flow areas associated with each radial structure member is different from one another, and that the perforated ratio for the four Eulerian cells close to the symmetrical axis decrease outward in the radial direction.

Reactor configurations obtained from the calculation with the CSS openings show different flow characteristics near the core-support structure.

Because of the presence of the openings in the CSS immediately below the core region, the fluid can penetrate and separate at the boundaries. This is evident from Fig. 31, which gives the reactor configurations at three different times. From these configurations, one can see how the fluid flows across the CSS in the upper plenum and how the fluid flows away from the boundary due to fluid jetting in the reactor lower plenum. One can also see that, at other structural members without perforated openings, the fluid slides along the solid boundaries during the excursion.

Figure 32 shows the pressure loadings in the reactor plenum for the cases with and without openings. Figure 33 presents the axial deformation of the bottom vessel. Obviously, if the openings of the CSS are not considered, the pressure loading in the reactor lower plenum and the axial deformation of reactor bottom are underestimated. The degree of the underestimation is, of course, dependent on the perforation ratio of the core-support structure.

The pressure loadings near the outlet nozzle and the total forces on the reactor cover obtained from these two cases are also investigated. As we anticipate, the results reveal that the peak pressure and the peak force are larger when there are no openings than when openings exist. However, the differences are very small.

E. Heat Transfer - The Effect of Condensation on the Pressure Loading

In this study, the effect of condensation in the fuel-coolant-interaction (FCI) zone on the pressure loading over the extended period of time in a single-subassembly hexcan is analyzed. The computational model is shown in Fig. 34a, in which the FCI zone represents a hypothetical accident due to failure of seven pins. From symmetry considerations, only the top half of the hexcan is considered. For the calculations of heat transfer in the FCI zones, the quasi-steady-state model was used. The initial sodium temperature was 672°K; the fuel temperature was 3115°K (molten). The volume fraction of sodium and fuel was 0.0962 each. The rest was assumed to be the steel. Two computations are performed, one with condensation and the other without. To be able to compare the slug energy when the sodium reaches the top of the hexcan, a fictitious cover was assumed on the top of the hexcan.

The pressure histories in the FCI zone, as well as at location 1 for both cases, are shown in Fig. 34b through 34d, where pressure pulses due to the compression wave A from the liquid expansion, the inertia wave B from the sodium momentum and the reflected wave C from the slug impact can be seen. The effect of condensation is readily observed after onset of vaporization. It also delays the slug impact time from 7.78 msec to 8.23 msec, and reduces the peak impact forces from 141.6×10^9 dynes to 113.7×10^9 dynes. The reduction of the peak vapor pressure in the FCI zone due to condensation is about 12.2 bars. Comparing the pressure histories in Fig. 34c with that in the FCI zone, it is noted that the pressure wave attenuation is very small in the initial liquid-expansion phase, but it becomes significant after sodium vapor appears in the FCI zone. It is also noted from Fig. 34d that the pressure pulse due to the reflected wave in the case of condensation (shown by the solid line) has been drastically reduced.

Figure 35 gives the marker-particle configurations of the hexcan at three different times. It shows the extended motions of the sodium, together with highly expanded FCI zones.

IV. CODE VALIDATIONS

Several examples concerning with comparisons of code predictions with exact solution of theoretical method or experimental data and other program results are given. Due to space limitations only important results are provided.

A. Shock-Tube Problem

This example deals with a shock-tube problem as given in the Problem #1 of the APRICOT program [22]. The problem provides a sensitive test of the dispersion and numerical noise introduced at discontinuities, in particular at the shock wave and at the rarefaction. Figure 36 shows the configuration of the shock tube that has a rigid tube wall and two rigid end caps and is divided into two gas regions by a diaphragm. The internal energies and temperatures are the same on both sides; the density and pressure on the left side (designated by subscript l) are twice the values on the right side (designated by subscript r). At time $t = 0$, the diaphragm is removed. A shock wave initiated at the interface is propagated toward the right side, while a rarefaction wave moves in the opposite direction.

This problem has been analysed both in one and two-space dimensions, using ZIP, partial donor-cell and complete donor-cell differencing schemes. Results from 2-D analyses indicated that the transverse fluid motion is very weak, and that the 2-D solutions closely resemble the 1-D solution. Also, the difference of solutions obtained by these three different schemes is also very small, hence we present the solution obtained from the complete donor-cell scheme.

Figure 37 presents the pressure profile at $t = 500 \mu s$, using time step of $1 \mu s$ in the calculation. The theoretical solution is also included by the dotted lines. The computed pressure profile is in excellent agreement with the theoretical solution. Also, the solution is quite stable, even without using any viscosity. Figure 38 gives pressure profiles for various time steps, illustrating the importance of the time step on the numerical solution. As can be seen that if the time step is too large (e.g., $50 \mu s$) not only instability occurs, but also dispersion takes place at the shock and rarefaction wave fronts.

B. ANL Experiment on Bubble Expansion and Contraction

To further validate the code prediction on bubble dynamics, the code was used to correlate the bubble motion of an ANL experiment performed for studying the motion of an HCDA bubble. The test apparatus used in the experiment is shown in Fig. 39. The test vessel, containing a 12-in.-high column of water, was initially closed and covered by a thin diaphragm membrane. The diaphragm was broken by the diaphragm break rod which falls on signal under the effect of gravity. This permits the high-pressure air to expand rapidly into the liquid region. The behavior of the expanding bubble was recorded photographically and a pressure gauge is set up at Location A to obtain the pressure history.

Figure 40 presents the bubble configurations and fluid motions at seven different times. These configurations show how the free surface moves and how the bubble expands and contracts. First, the gas bubble expands spherically and reaches its maximum radius at about 22 msec. Then a dent is generated at the bubble vertex, and the bubble becomes toroidal in shape. The dent at the bubble vertex is caused by the fluid hydrodynamic pressure, which exceeds the bubble internal pressure and thus causes the reversal of the fluid motion. Because of the further depression of the dent, the gas bubble becomes unstable and collapses shortly after 41.89 msec, at which time several fluid particles already have been observed inside the gas-bubble region.

Experimentally recorded bubble motions at seven different instants are exhibited in Fig. 41. These configurations show how the bubble expands and contracts during the course of motion. The maximum bubble also occurs at 22 msec. To compare the results, the positions of the bubble wall along the symmetric axis obtained by the analysis are also shown in this figure.

Figure 42 shows the pressure histories at Location A obtained from the experimental record and the analysis. The results agreed well, except that at the early stage of motion the experimental trace had rapid pressure oscillation.

The good agreement of the analytical results with experimental data indicates that the code is a promising tool for investigating bubble motion during an HCDA, and that the bubble shape is, in general, not spherical.

C. SRI Test on Wave Propagation in an Elastic-Plastic Pipe

The code was used to simulate the piping experiment conducted by Stanford Research Institute (SRI) [33]. To validate the fluid-structure-interaction analysis as well as to illustrate the code performance on the fluid transient in the piping component.

In the experiment, the pressure pulse was generated by a pulse gun which was attached to a length of Nickel-200 pipe. The pipe was 3 in. OD, 40 mils thick, and 10 ft. long, and filled with water as shown in Fig. 43. Figure 44a shows the pressure-time history at position 1 in the pulse gun, which was used as the source pressure in the numerical calculation.

Figure 44b-d shows the computed pressure-time histories at pipe locations 1A, 2, and 3, along with the mean values of the SRI experimental pulses. The peak magnitudes and the pulse shapes, as well as the loading and unloading times, agreed well with the experimental results. Because of the effect of plastic deformation, both the computed and test results reveal that the pressure peak is significantly attenuated as the pressure wave propagates to the downstream of the pipe. Since the plastic waves travel much more slowly than the elastic waves, the pressure pulse which causes the pipe to yield is noticeably dispersed as it travels to the downstream.

Figure 45 gives the time histories of the radial deformations of the deformable pipe at six positions at about 4 msec. The SRI posttest measurements of the pipe wall are also given. At positions close to the source, the computed radial deformations compare well with the measured deformations. At positions away from the source, the pipe deformations are overestimated, as noted at positions 60.96 and 91.44 cm away from the source. The overestimation is probably due to the fact that the positions away from the source are still subjected to certain amounts of pressures, and thus their deformations are not completely recovered. Nevertheless, the analytical solution indeed agrees reasonably well with the experimental results.

D. SNR-300 Tests on Wave Propagations in Primary Containment

To validate the two dimensional analyses of fluid transients and fluid-structure interactions, the ICECO code was applied to the German LMFBR demonstration plant SNR-300.

Three test configurations of the SNR-300 reactor models shown in Fig. 46 will be considered in this paper. The first two models differ only by the rigidity of their radial boundary and the description of the source. The third model is essentially the same as that in Fig. 46b, except that two cylindrical vessels are used. In all cases, the basic test configuration consists of a spherical pressure-volume source immersed within a pool of water, which in turn, is held by a cylindrical container with rigid ends. From the free surface of the water to the top of the container, the space is occupied by air. The cylindrical walls of the containers are pre-compressed by the rigid end plates with holddown bolts. Rubber seals separate the cylindrical walls from the end plates.

The pressure-volume relationships of the source are derived independently and are given in Tables 1 and 2. The dynamic response of the structural material is also separately established by appropriate dynamic tests.

In the analytical model, a spherical-shaped source is used to represent the explosive charge. The position of the outside cylindrical boundary corresponds to the mean radius of the vessel. Other assumptions pertain to these three tests are: (a) the top and bottom boundaries are assumed to be stationary, (b) the cylindrical vessel boundary at the bottom is constrained axially and is free to move radially, and (c) the top vessel boundary is assumed to be free of any constraints.

1. The Thick-Vessel Model

In the thick-vessel test shown in Fig. 46a, the cylindrical vessel was assumed to deform elastically. The pressure-volume characteristics of the source are given in Table 1.

Table 1

Source Characteristics for the Thick-Vessel Model

Pressure, Bar	Volume Ratio (V/V_0)
411.0	1.0
330.0	1.3
263.0	1.72
182.0	2.37
152.0	3.13
124.0	4.11
109.0	5.18
85.0	6.7
65.5	8.93
50.0	12.0
44.0	13.9
36.0	17.0
30.5	20.9
27.0	24.0
23.5	27.8
20.0	31.5
19.2	34.8

Table 2

Source Characteristics for the Thin-Vessel Model

Pressure, Bar	Volume Ratio (V/V ₀)
426.8	1.0
380.8	1.18
278.9	1.60
199.3	2.12
111.7	2.75
71.4	3.47
42.0	5.0
22.0	8.0
12.2	12.0
7.0	18.0
3.8	28.0
1.95	45.0
1.1	68.5

The experimental results of Test 114, a representative test pertaining to the thick-vessel configuration, have been published [34]. A sampling of those data is reproduced here for comparison with the ICECO and REXCO results. Comparisons of the pressure histories at the bottom of the tank ($r = 10$ cm and $z = 0$) and at the cylindrical wall ($r = 25.5$ cm and $z = 36$ cm) opposite the source are given in Figs. 47 and 48.

Fairly good agreement of experiment and analysis is obtained for the first high-pressure rise in Fig. 47. The experimental pressure appears to be somewhat overestimated at the early part of the pressure pulse and largely underestimated later by the analytical results. The overestimation of the recorded pressure pulse is attributed to the difference of the boundary conditions at the vessel bottom. In the analysis the bottom vessel is assumed free to move radially, whereas in the experiment the bottom vessel is constrained by the rubber seal. This rubber seal, although has little radial resistance, definitely could create higher reflected pressure near the vessel-plate junction and thus cause the overestimation of experimental pressure. This boundary effect has small influence away from the bottom, as can be seen from the pressure histories at the vessel wall opposite the source shown in Fig. 48. The overall rise and fall of the pressure correlate very well between experiment and analysis.

2. The Thin-Vessel Configuration^{*}

The assumptions made in the ICECO model are similar to those for the thick-elastic-vessel configuration, except that the thin vessel is permitted to deform plastically. The stress-strain curve assumed for the thin vessel is confined to a bilinear representation. The elastic portion with modulus $E = 20000$ kp/mm² extends to the stress of 44 kp/mm²; beyond the yield stress, a plastic modulus $E_p = 40.96$ kp/mm² is assumed. The pressure-volume source characteristics used with the model shown in Fig. 46b are taken from Ref. [34] and given in Table 2.

^{*} Note that the mathematical model used for the sodium-spillage analysis is not the one described in Sec. II.D, but is the one inherited from the conventional Eulerian hydrodynamic methods.

In the original solution of the thin vessel problem (see Ref. 13, p. 43) it was assumed that air occupies the space between the surface of the water and the bottom of the cover, and spillage of the fluid does not take place [13]. This ICECO solution is reproduced in Fig. 49, showing in sequence the configurations: (a) the initial grid of the analytical model, (b) the configuration at about the maximum vessel deformation, opposite the source, (c) the initiation of impact, and (d) the maximum deformed configuration at the top of the vessel. It is clearly observed that during the initial stage of vessel deformation at the bottom and opposite the source, it deforms not only in the radial direction but also axially. The axial deformation of the vessel at the top is of the order of about 25 mm before the slug impact. Making an allowance for the contraction of the bolts during the initial deformation of the vessel, which would be a small fraction of one centimeter, we can see an initial opening on the top before impact takes place. The effectiveness of the rubber seals in a case like this should be negligible. Therefore, spillage of fluid for the thin vessel model could be considerable and the displacement at the top of the vessel may be quite different than what is shown in Fig. 49.

The uncertainty of water spillage through the existing gap at the top of the vessel on the deformation of the vessel led to two additional runs of ICECO. One run permitted fluid spillage over the top of the vessel during slug impact. Since the Eulerian grid was stationary and the vessel top moved within the grid, some initial matching of grid size was made so that spillage would be through at approximately a full grid dimension. The axial grid size was chosen as exactly half of that of the previous model. Consequently, the difference of this run was that the axial grid size was doubled, and air plus water was free to flow radially through the top-most grid during and after the slug impact. The progression of slug impact, fluid spillage and vessel deformation at the top is shown in Figs. 50a through 50d. It may be observed that the top of the vessel now deforms less than in the previous solution shown in Fig. 49. In fact, while the top of the vessel without spillage and air above the water surface was about 17.5%, the permanent set with spillage and no air on the top was found to be about 12%.

As another variation dealing with slug impact and consequent vessel deformation at the top, an ICECO run was made assuming that no air existed at the top

of the water surface, but spillage of the fluid was not considered. This variation thus only eliminated the air from the first solution depicted in Fig. 49. The resultant vessel deformation of this run was found to be between those derived from the first two solutions. The final vessel deformations of all three analytical solutions are shown in Fig. 51, together with the experimental results presented in Ref. [34].

3. The Double-Vessel Model

The combination of two codes REXCO and ICECO is utilized in this problem to yield the final analytical deformation of the cylindrical vessels. This is necessary because of basic or current limitations of the individual codes. The complexity revolves around the double-connected regions of water, spillage and even mixing of both fluid domains. The REXCO code, which is based on Lagrangian formulation, is handicapped by large deformations which would be a part of spillage over the top of inner vessel during slug impact. The ICECO code at this point of development does not treat an internal thin vessel. Thus, the analytical modeling of the two-vessel problem is decomposed into two parts: the first part involves the REXCO code and provides the initial solution to the problem. The second part makes use of the ICECO code and continues the solution to the end. The source characteristics for both models are the same as for the thin-vessel model discussed before. A bilinear behavior of the vessel is assumed; an elastic portion with $E = 2 \times 10^4$ kp/mm^2 extends to a yield stress of 39.2 kp/mm^2 after which a plastic modulus of 37.3 kp/mm^2 is assumed.

The initial stage of the excursion by means of REXCO is extended to the time when the vessels at the bottom and opposite the source have deformed to their equilibrium. At this time (1.4 ms) the REXCO output is converted for input of ICECO. An averaging procedure is applied within the fluid to approximate the initial velocities, densities and pressures for the initial conditions of the ICECO solutions.

The ICECO solution commences with a single fluid domain, a single vessel and simulates slug impact and the resultant fluid spillage. A special assumption made in the ICECO solution is that at the restart the vessel is taken to be

undeformed. The lower part of this new vessel extending to 0.62 m is now assumed very thick (0.5 m). Above this point, the vessel retains its actual thickness. The reasons for specifying a rigid vessel portion at the bottom is because at 1.4 ms, the vessel had deformed permanently and further deformation would not be expected; the thick-vessel portion would confine the deformations to small elastic oscillations which should not be detrimental to the overall solution. The actual thickness of the vessel at the top should enable permanent plastic deformation to take place during slug impact. The junction of the thin-thick portions is placed supposedly sufficiently far from the top so that the effective artificial reinforcement of the thick-vessel portion should be small. The final vessel deformations are thus derived from the combined REXCO and ICECO solutions are shown in Fig. 52 also containing the experimental data for Ref. [34]. The single vessel ICECO model thus provides the top deformation of the inner vessel.

E. UKAEA-JRC COVA Experiment of High-Energy Excursion Involving Shock Waves and Cavitations

This example problem deals with ICECO predictions on high-energy excursion to validate the mathematical treatment of shock-wave propagation and liquid cavitation. Although high-energy excursion has an extremely low probability of occurrence, it has large adverse consequences. The trend toward probabilistic risk analysis has led to the study of such excursion for assuring the integrity of the containment system.

Experimentation concerning high-energy excursions was conducted by the UKAEA and JRC-Ispra as part of the Code Validation (COVA) program [35]. The experiment includes the detonations of high explosive charges within a water-filled overstrong cylindrical vessel, as shown in Fig. 53a. This particular experiment consists of nine identical tests, three performed at AWRE-Foulness, three at AEE-Winfrith, and three at JRC-Ispra. Pressure and impulse measurements were taken at twenty locations on the floor, wall, and roof at three different planes.

Statistical analysis shows that the recorded data are of high quality. Thus, this COVA experiment has been chosen as a typical problem in the APRICOT program [22,36].

Results [36] of the APRICOT code-comparison exercise revealed that on the floor and the wall most Lagrangian hydrodynamic code provided solution in fair agreement with experimental data. However, the majority of the Lagrangian calculations overpredicted the impulses on the floor, particularly near the center of the tank. They also produced quite spikey pressure histories on the roof, even some using the sophisticated cavitation model developed by Rayleigh to account for the rate of growth and collapse of cavitated bubbles in water.

Here, numerical calculations were made with the ICECO code, using ZIP differencing scheme. All calculations cover important physical events without utilizing any complementary mechanism, such as artificial viscosities, rezoning, mesh stabilization and regularization, as well as prescribed grid motion. Water cavitation and spalling are treated by the "Pmin" model mentioned in Sec. II.G.

We have found from the results that (1) the ICECO code not only predicts correctly the pressure pulses on the floor and the side wall, but provides good resolutions of wave profile on the roof; and (2) the material properties of the vessel wall play an important role in calculating the impulse on the floor. Consequently, the discrepancy between the Lagrangian analyses and experimental data can be resolved if the vessel wall is assumed to be deformable.

For completeness, two calculations of the COVA experiments were made with the ICECO code, using vessel material properties as a parameter. One calculation considered the vessel wall to be rigid; the other assumed the vessel wall to be elastic, with the wall thickness taken to be 4 cm.

In the analysis, the physical system is discretized into 25×42 Eulerian cells as suggested by the APRICOT committee. This mesh configuration is relatively coarse in which the explosive charge was initially represented by two Eulerian cells. The initial pressure of the explosive charge is 116.04 k bar. Results are briefly described below.

1. Rigid-Wall Solution

Correlations of the computed pressures and impulses with the experimental results of all gauge positions are made. Wave shapes and arrival times are also compared. In general, the code can predict exceptionally well with the pressure pulses on the floor and wall, including both the incident shock waves, and reflections from the floor and wall and slug impact. However, on the floor the calculated pressure pulses generated from the wall of the tank are higher than those recorded in the experiment due to rigid-wall assumption. Because of space limitation, pressure pulses on the floor and wall are not presented here but are given in Ref. [37].

The computed and measured impulses on the floor, wall, and roof are given in Fig. 53b-d. In general the calculated impulses are in good agreement with the experimental results. However, the predicted floor impulses are higher than those measured, especially near the center of the tank. As mentioned before, this is due to the rigid-wall assumption which causes the overestimation of the reflected pulses, and in turn, the final impulse values.

Figure 53e depicts the reactor configuration at 1.0 msec, showing also the early stage of the bubble configuration. Because of strong wave reflections from the floor and the wall of the tank several jet-like spikes were observed which penetrate the boundary of the gas bubble. Since the code has an accurate scheme for treating highly contorted coolant surface, the collapsing of the gas bubble at this stage of excursion can be avoided and numerical calculations can be carried out continuously without any interruption.

The phenomenon of roof impact in the COVA experiment is very complex, due to the presence of cavitation and spalling at the coolant free surface. This complex phenomenon, in conjunction with the explicit integration algorithm for the conservation equations, impose certain difficulties in the numerical calculations obtained by the Lagrangian codes. Thus, nearly all the Lagrangian analyses showed considerably spikey pressure histories on the roof even sophisticated cavitation model and large amount of artificial viscosities are used as the smoothing mechanisms. Since the ICECO code uses the implicit integration scheme, the solution is stable and the adverse effect of fluid cavitation on

the numerical results is less severe than those of the explicit Lagrangian calculations. This can be seen from Fig. 54, which depicts respectively the experimental and computed pressures at roof gauge #18, located 16.0 cm away from the axis of the tank (see Fig. 53a). It indicates that the predicted pressure deviates only slightly from the recorded one and correlates well with the experimental data.

2. Deformable-Wall Solution

From the results of rigid-wall analyses obtained from ICECO and other Lagrangian codes it is shown that although the propagation of the primary pulse to the tank wall and floor was calculated accurately, secondary pulses to the wall, arising from reflections from the wall and the axis of the tank were overestimated in the code predictions. The overestimated secondary pulses further lead to the overprediction of impulses delivered to the floor of the tank, particularly near the centerline.

Recently, we have found that the material properties of the overstrong vessel play a significant role in calculating the strength of the reflected waves, and that even the relatively thick wall used in the COVA experiments can temporarily absorb a significant portion of the incident energy and delay releasing this energy for several hundred microseconds. This gives a partial explanation of the unexpectedly low secondary pulses observed in the experiment. Thus, the calculation was rerun with the ICECO code, allowing the vessel wall to deform elastically. The results are given below.

Figure 55 shows pressure and impulse histories at gauge #1, in which the two ICECO calculations are compared with experimental results. The diagrams on the right-hand side of these figures show the improvements achieved by considering the thick wall to be elastic. Figure 56 shows the impulses at gauge positions 1-7 for the two cases studied, together with the experimental results. The impulses obtained from the elastic-wall analysis agree very well with the recorded data.

F. SRI Complex Vessel Test SM-2 on Structural Response to a HCDA

Recently, a series of experiments (referred as SM tests) have been performed by SRI International using a 1/20 scale model of the Clinch River Breeder Reactor (CRBR) to study the effects of various structural components on the cover loading and vessel response [38]. These experiments consist of five tests. Test SM-1 was a static test of the reactor cover. The other four tests SM-2 to SM-5 were dynamic tests performed on the scale model of the CRBR. This report describes the ICECO code predictions of the SM-2 test.

The test model of SRI SM-2 is shown in Fig. 57. The reactor vessel was made from Ni-200 to simulate the stress-strain relationship of the Type 304 stainless steel at the reactor operating temperature. The core barrel was a thin aluminum cylinder while the radial shield was made of a stack of segmented steel rings. A Mylar diaphragm is placed above the charge canister to prevent water from entering into the source region. Water was used to simulate the coolant. Eight pressure gauges and ten strain gauges were used in the experiment to record pressure pulses and dynamic strains. Their positions are shown in Fig. 57.

The mathematical model used in the ICECO analysis is shown in Fig. 58a, where the fluid is denoted by marker particles. The initial position of the core-gas bubble is represented by approximately 18 Eulerian cells located at the lower left corner. The properties of the reactor vessel and core barrel were taken from the test data provided by SRI. The radial shield was treated as an elasto-plastic material with low yield strength. It should be mentioned that the value of the yield stress of the shield material was calculated from the frictional forces between the segmented rings, and that once the pressure force exceeds the frictional force, the segmented rings are allowed to slide and to become separate.

Two types of input data can be used to describe the behavior of the core gas; the pressure-volume (p-v) relationship and the pressure-time (p-t) history of the core gas. Calculations using the p-v as the input may not be accurate enough if errors have occurred in the measurement of core-gas-volume increase during the process of source pressure determination. On the other hand, the

p-t history of the core gas can be taken directly from the pressure transducer readings of the experiment. Thus, the p-t history could provide a more accurate input and is used here. Because of space limitation, only important results are presented in this report.

Figure 58b shows the computer generated reactor configurations after the slug impact. The deformations of the core barrel and reactor vessel as well as the expansions of the core-gas bubble can be clearly seen. Figure 59 shows a comparison of pressure histories of gauge P5. As can be seen, the agreement between the analytical result and the experimental measurement is very good. Figure 60 compares the calculated vessel and core-barrel deformations with the post-test measurement. The agreement is exceptionally good, particularly the lower portion of the reactor vessel.

V. THE COMPUTER PROGRAM

The computer program ICECO-CEL (ICECO-III) is written in FORTRAN IV for the IBM 370/195 computer to analyze the fluid transients, fluid-structure interaction, and the structural response. To assist the user in understanding the program, we first briefly present information concerning the identification of the cell flag, the particle set-up procedure, the slug-impact indication index, modelings of the flexible vessel, deformable internal and movable head cover, as well as the hydrodynamic-structural coupling and etc.

A. Cell Identification

Several types of flags are used in the computer program to appropriately identify the Eulerian cell, gas-bubble location, the orientation of the boundary segment of the structure, and the free-surface orientation. Here, we briefly describe these flags.

1. General Cell Flag

First, the cell flag is a numerical number assigned to each Eulerian cell to indicate the cell type. This number will be included in the detailed printout along with other physical variables. From the cell flag as well as the marker-particle configuration generated by the film subroutine, one can visualize the domain of the fluid and the configurations of the gas bubble, the core-gas region, and the boundary of the structures. The cell within a computing region may be one of the following types: (1) A Dummy (D) or a fictitious cell does not contain fluid and falls outside the system boundary. This cell is equivalent to the boundary cell of the MAC method and is used solely for computation purpose ($F = 1.0$). (2) A full (F) cell contains fluid and has no empty cells for neighbors on any of its four faces ($F = 2.0$); thus, this cell denotes part of the fluid region. (3) A surface (S) cell partially contains fluid, but has at least one empty cell among the neighbors on its four edges ($F = 3.0$); this cell defines the free surface or the bubble-coolant interface. (4) An empty (E) cell does not contain fluid ($F = 4.0$), and represents the region of gas bubble or the cover gas. (5) An obstacle (OB) cell represents rigid obstacle and does not contain fluid ($F = 5.0$). (6) A boundary (B) cell

contains a segment of the deformable vessel ($F = 6.0$). (7) An arbitrarily-shaped boundary (AB) cell has boundary of a rigid structure with boundary not coinciding with the Eulerian grid ($F = 7.0$). (8) An internal boundary (IB) cell possesses a boundary segment of the deformable internal structure ($F = 8.0$). (9) A quasi-Eulerian (Q) cell is an irregular cell underneath the reactor cover where sodium spillage and plug jump may occur ($F = 9.0$). (10) A perforated structure (PS) cell contains either an interior portion or a boundary segment of the perforated structure such as the upper internal ($F = 10.0$). (11) An internal structure (IS) cell contains interior of a thick solid structure but not the boundary ($F = 11.0$). Note that there is no fluid (marker particles) in this cell, and that the flag of this cell is time dependent as the structure moves across the fixed Eulerian coordinates.

Secondly, a bubble flag is used to denote which empty or surface cell represents the core-gas bubble and which represents the cover-gas region. This additional flag is necessary since the computer program has no way of knowing which empty cell belongs to the gas bubble. Particularly, in the case of bubble migration, the core-gas bubble and the trapped air can be separated by a thin liquid film. Thus, the source flag will give proper location of the gas bubble as well as the cover gas so that the corresponding pressure can be assigned to. Here, an empty cell ($F = 4.0$) or a surface cell ($F = 3.0$) may be one of two types: (1) A gas-bubble cell or a bubble-coolant interface cell ($LF = 1$). (2) A cover-gas cell or a free surface cell ($LF = 2$).

2. Boundary-Cell Flag

A moving (or arbitrarily-shape) boundary can be specified by a locus of node points described by the Lagrangian coordinates. These nodes are normally placed along the Eulerian grid lines. The boundary is therefore defined by a polygonal Lagrangian line, which was made up of straight line segments connecting these node points. A moving polygonal line intersecting the fixed Eulerian mesh will create numerous time-dependent irregular cells. To match the boundary condition at the midpoint of each segment, appropriate boundary flags must be established.

A boundary flag identifies the Eulerian cell that contains the solid materials and provides geometrical information of how vessel segment is oriented with respect to the Eulerian cell. At present, 15 flags have been considered for all possible intersections of the Lagrangian boundary with the fixed Eulerian grids. These flags are given in Fig. 61 where the boundaries of the structure are indicated by cross-hatch lines. If additional flags are needed, they can easily be incorporated into the computer program.

In calculating fluid-structure interactions involving deformable internals, it is desirable to introduce multivalued variables such as u , v , p , ρ near the deformable structure as described detailedly in the ICECO-II Report, ANL-78-103 [13]. To accomplish this objective, a criterion (or a flag) must be established to indicate the position of the fluid relative to the structure. Here, we refer to Fig. 61 shown previously and assume that the fluid is at the left when the flag KF equals to 1, 9, 11, 59, 69, or 79; the fluid is at top when KF equals to 8, 12, or 13; at right when KF equals to 4, 6, or 14; and at bottom when KF equals to 2, 3, or 7.

3. Surface-Cell Flag

In the analysis velocity components are defined at the middle points of cell boundaries as shown previously in Fig. 2. In a surface cell, the position where the velocity is defined may be outside the fluid region. This happens often when a surface cell has empty neighbors. Here two flagging schemes are established to identify the number and position(s) of the velocity components located outside the fluid region.

a. Conventional Flagging Scheme

The conventional flagging scheme is the one being used in the Eulerian hydrodynamic methods such as MAC [39], SMAC [40], ICE, and their extended technique. The scheme simply searches the positions of the empty cells relative to a surface cell. Figure 62 presents 12 cell flags, indicating possible arrangement of empty cells relative to a surface cell. These flags, representing by different numerals, provide locations (shown by dots) of velocities outside the fluid boundary.

b. Detailed Flagging Scheme

Since the conventional flag depends on the positions of empty cells relative to a surface cell rather than on the position and orientation of the free surface, the solution obtained is approximate. The detailed flagging scheme approximately calculates the free-surface orientations and finds which velocity locations are outside the fluid region similar to the manner of determining the boundary flags in the fluid-structure interaction. Presently, 12 different flags (see Fig. 63) are designed for the surface cell with the heavily line indicates the free surface boundary and the arrow points into the fluid region. This flagging scheme has not been generalized enough to take care of all the problems. Thus when apply this scheme we should note that: (1) It can only be applied to the case the bubble is surrounded by the fluids. In other words, the first and last marker particles defined the bubble boundary must be on the symmetrical axis. (2) The marker particles described the bubble boundary and the free surface (if any) must be numbered in such a way that as one advances from i -th particle to $(i+1)$ -th particle the fluid is on the left of the interface. (3) The scheme cannot be applied if the distance between two consecutive interfacial particles are greater than one cell.

In general, the numerical solution based on the conventional flagging scheme can give satisfactory results for majority cases. However, in the situation the bubble-coolant interface has large curvature the refined flag might provide a better solution.

B. Other Information

1. Surface-Cell Velocity Calculation

Once the locations of the unknown velocity components are determined by either one of the two flagging schemes, their values are computed similar to those of the MAC method in treating the open sides of the free surface cells. For one unknown velocity case (configurations 1, 2, 4, 8 in Figs. 62 and 63), or two adjacent unknown velocities case (configurations 3, 6, 9, 12), the appropriate u and/or v may be calculated precisely from the mass equation. For the case of three unknown velocities (configurations 7, 11, 13, 14) we customarily

assume the interface is flat and first compute two u or two v based on the inviscid boundary condition; then compute the remaining one unknown using the mass conversation equation.

2. Marker-Particle Setup and Slug Impact

To create the fluid inside the computing region, the particle-setup cards are needed. The computing program requires one card for each set of marker particles. The shape of the particle set is limited to being rectangular, as illustrated in Fig. 64.

For each set of marker particles, the number of particles to be created in the r and z directions should be specified through parameters NX and NY . Four dimensions - XO , YO , DXK , and DYK - are also needed to describe the geometry of a given particle set. The FORTRAN variables XO and YO represent the coordinates of the first particle; DXK and DYK denote the space increments in the r (or x) and z (or y) directions, respectively.

Both the interior and interfacial particles are denoted by the same FORTRAN variable. To distinguish these particles, the particle sets defining the core-gas bubble should be read in first and the particles representing the interface between the coolant and the cover gas should be read in next. After the input of interfacial particles, the interior particles can be input in any order. The particles used to define bubble boundary and the free surface must be set up or numbered in such a way that as one advances from (i) th to $(i+1)$ th particles the fluid region is at the left-hand side of the interface boundary.

At the beginning of slug impact, the marker particles originally positioned on the free surface move upward and impact the reactor cover. In the numerical approach, the Eulerian cell underneath the cover head will be changed from a surface cell to a full cell and allowed to produce a pressure on the cover. Since the free surface generally exhibits a curvature, and slug impact occurring in the cell underneath the cover takes place at a different instant, a criterion must be established so that the programs will know when to change the cell flag and shift the pressure calculation. This criterion can be specified through the parameter $KIMP$, which means the minimum number of particles for

each cell required to contact the vessel head to imply the slug impact. In a two-dimensional excursion, this parameter can be set equal to one-half of the number of particles located at the free surface in each surface cell. In the one-dimensional case, the slug impact begins when all free-surface particles have been pushed upward and have contacted the cover. Nevertheless, the specification of this parameter depends on the physical judgment of the user.

3. The Computing Domain and Modeling Technique

The computing mesh used in the ICECO analysis is similar to the MAC method in which a belt of dummy (fictitious) cell outside the boundaries of the real computing mesh are used for the computational purpose. The mesh boundaries are assumed to be the rigid walls so that the normal velocities are set equal to zero at all the calculation cycles in order to conserve momentum exactly. This setup is intended for the hydrodynamic problems with boundaries coincide with the mesh boundaries. Thus, one can easily figure out the minimum cell numbers for a given domain by adding two cells in both the radial and axial directions.

However, for problems involving flexible external boundaries shown in Fig. 65, attention should be given regarding how to determine the minimum cell numbers in order to conserve the storage. The guideline is that one should keep at least one column (or one row in the case of movable head and curved reactor bottom) of empty cells between the dummy cells and the cell containing the rightmost (or uppermost) external boundary segments. The reason of the arrangement is that the velocities outside the boundaries (shown by arrows) are needed in matching the boundary conditions at the fluid-structure interfaces, and that these velocities generally have nonzero values which are different from the zero velocity set at the mesh boundaries. With this background in mind, one can compute a priori the required cell numbers for problems involving small or moderate displacement of external boundaries. In the case of large displacement, one may either leave more than two empty cells outside the boundaries or perform a few try runs to find out the cell numbers containing the farthest boundary segment and decide the required cell numbers from there.

Another thing noteworthy to mention is the initial positions of the flexible external boundaries. Again, referring to Fig. 65 our guideline is to place the external boundaries (such as vessel, bottom of the cover if movable, and reactor bottom, etc.) slightly off the grid lines at where velocity components (shown by dots) are rigorously computed from the momentum equations. Thus, in the fluid-structure-interaction analysis the velocity vector of the virtual particle located at the midpoints of the boundary segment will depend less significantly on the velocities outside the boundaries. Although we cannot avoid this situation entirely since the boundary could move in an arbitrary manner, at least we treat the interaction precisely at the beginning of the deforming stage.

Finally, for problem involving deformable internals we should also keep in mind that the present computer program can only handle small displacement of reactor internals. Also, the program has the restriction that the internal boundary cell contains only one midpoint of the boundary segment, as shown in Fig. 66. Therefore, in the numerical modeling we should lump the radial shield and the core barrel together and skillfully avoid the situation where one Eulerian cell has two interfacial segments.

4. Hydrodynamic-Structure Connectivity

In the coupled fluid-structure problem involving interactions of coolant with primary vessel and various deformable internals it is necessary to transmit certain information back and forth between the hydrodynamic and structural calculations. These two calculations are combined as follows: (1) the hydrodynamic program first computes pressure on the load line representing the fluid-structure (or Eulerian-Lagrangian) interface, (2) the pressure is treated as input external (or driving) force to the structural program, (3) the structural program returns the displacements, velocities, and accelerations at the fluid-structure interface to the hydrodynamic program, and (4) the hydrodynamic program performed iteration on the advanced-time pressures using the returned values and computes a new improved pressure at the boundary. The procedure of (1) to (4) is repeated until a prescribed terminating cycle (or time) is reached.

To provide proper communications between the hydrodynamic and structural calculations we have established two numbering systems for hydrodynamic and structural computations, respectively. The first one is point/segment system for hydrodynamic calculations. The second one is the node/element system used for finite-element discretization of the structure.

In the hydrodynamic calculation using point/segment system the fluid is assumed to be on the left-hand side of the load line that connects the beginning and the terminating points. On each load line the 'point' and hence the 'segment' must be numbered in a consecutive manner. Thus, two point numbers are given at the intersection of two load lines, as shown in Fig. 67a. In this figure ordinary numbers indicate 'point' numbers, numbers with prime (showing only the first and the last one each load line) are the 'segment' numbers.

In the structural calculation conventional node/element numbering system is used. The 'node' number on the pressure load line is restricted by the numbering rules of the finite-element discretization, in which only one nodal number (excluding the dummy nodes for the shell element) can be given at the intersection. Figure 67b shows the numbering system for the finite-element structural dynamic calculation. Here, the circled numbers represent 'node' numbers; the starred numbers indicate 'element' number. Understandably, numbers indicating 'dummy' nodes as required by the finite-element thin shell calculations are excluded for the purpose of simplification.

The format and algorithm for reading-in the segments/points numbering are the same as for reading-in the nodes numbering. Hence, automatic generation of the numbering can be used when the numbering is increased by a constant. The format and algorithm for reading the segment/points connectivity information are the same as for reading-in the finite element element/nodes relationship. Again, automatic generation of these data can be utilized if all the numbers are increased by one.

C. Computer Output

1. Input Verification Printout

The code is user-oriented. It is constructed in such a way that the user can easily understand and verify his input cards. Thus, all the information generated by the input cards at the beginning of cycle are printed with headings. These printouts are briefly described below.

a. Data for Hydrodynamics

Complete input cards for hydrodynamics are printed in accordance with the input instruction, including the card number and variables FORTRAN names. Such output provides important information concerning: (1) title of the run; (2) the size of the computation region; (3) specification of plot to be done by the CALCOMP plotter, index for problem continuation; (4) important indexes or parameters indicating whether or not the problem involves slug impact, fluid-structure interaction, moving cover and sodium spillage, deformable internals, flow through perforated structure, and etc.; (5) characteristics of the source pressure; (6) coordinate-system options, rigid-obstacle options, rigid thin shell (or plate) options, ZIP or donor-cell differencing options, and etc.; (7) marker-particle configuration; (8) information for deformable internal structure, moving cover and sodium spillage, flow through perforated structures.

b. Data for Structural Dynamics

(1) Number of nodes, elements, materials, nodes at which special displacement conditions are specified, structural time increment, and the number of load lines; (2) properties of material used; (3) a table of three columns showing the radial (x) and the axial (y) coordinates of all nodal points; (4) a table of eleven columns showing the element number, its associated four nodes (N1-N4), three blank numbers for future use, problem-characteristic number (PTYP), material type number (MTYP), and the element type number (ND); (5) a table of four columns showing the node number at which special displacement constraints are set and describing the constraints. One in the x column indicates that

motion in the radial direction is not permitted. One in the y column indicates that motion in the axial direction is not permitted. The angle column shows the angle between a direction along which motion of the node is not permitted and the global x coordinates; (6) hydrodynamic-structure connectivity, point/segment and node/element relations; (7) table of Q array and the required array storage.

2. General Printout

a. All Problems

At every NDTGEN cycle the program prints: (1) under title 'KT CK' the number of marker particles per each Eulerian cell that have contacted with the cover; such printout appears if slug impact is expected and no quasi-Eulerian (irregular) cells are involved; (2) the radial, axial, and total fluid-kinetic energy, total energy in the system, total fluid internal energy, original core energy, and energy balance discrepancy; (3) pressure, energy of the core-gas bubble, volume of gas bubble at the previous (n^{th}) and advanced-time ($(n+1)^{\text{th}}$) cycles, as well as the original core volume; (4) information similar to (3) for the trapped air; (5) pressure in the core-gas bubble, trapped air, and time if pressure-time (p-t) histories are used as source pressures; in this case printout items (2)-(4) mentioned above are omitted; (6) cycle number, time, and time step; (7) solution time in the structural program, allowable time step, number of subcycles, time step of structural analysis; (8) time, number of iterations needed, calculated maximum convergence criterion, and fluid volume.

b. Moving-Cover and Sodium-Spillage Analysis

If problem involves moving cover and sodium spillage that is analyzed by the control-volume technique, the program prints: (1) at every cycle under title 'penetration x x is opened', the radial cell number of the penetration, the calculated and the allowable impulse if the penetration becomes open; (2) at every NDTGEN cycle under title 'COVER' the cover axial cell number (JC), cover height, total force on the cover, cover position, cover velocity, cover acceleration, bolt force, pressure in cell (4,JC), pressure in cell (4,JC-1),

flag of cell (4,JC), flag of cell (4,JC-1); (3) for every NDTGEN cycle and every contacting particle under title 'REFLAG CK CONTACT' the particle number, its radial cell number (I), number of particles contacting the cover associated with cell I, particle's radial position, particle's axial position, cover axial position, axial velocity at bottom of the irregular cell, and the cover velocity.

3. Optional Printout

Optional printouts are determined by each frequency specified in card type 11 in the input instruction. The contents of these printouts are briefly described below.

a. Detailed Cell-Variable Output

For every NDTCP cycle the program prints the detailed information for each Eulerian cell, including the radial cell number I, the axial cell number J, sonic speed c , fluid velocity in the coolant passageway \tilde{v} , radial velocity u , source term of the radial momentum equation R , source term of the axial momentum equation, pressure p , source term of the Poisson equation G (or H in this report), cell flag F , free surface or boundary flag KF , bubble flag LF , flag NF for cell around the deformable internals.

b. Particle-Position Output

For every NDTPP cycle the program prints marker-particle information, including particle number, its radial position, and axial position.

c. Boundary-Flag Output

For every NDTFLG cycle the program prints boundary flags information of each segment in a six column tabulated form under the title 'BDYFLG', including segment number M , its radial cell number I , axial cell number J , first boundary flag $KF1$, second boundary flag $KF2$, radial position of the first point $RV(M)$, axial position of the first point $ZV(M)$, radial position of the second point $RV(M+1)$, axial position of the second point $ZV(M+1)$, segment slope A , segment axial distance B , and cell flag $F(IJ)$.

d. Deformable-Internal Output

For every NDTINT cycle the program prints multivalued variables near the reactor internals in fifteen columns, including radial cell number I; axial cell number J; fluid densities on the left- and right-hand sides of the internal $\rho(LR)$; fluid densities above and below the internal $\rho(TB)$; radial velocities on the left- and right-hand sides of the structure $U(LR)$; radial velocities above and below the internal $U(TB)$; source term of the radial momentum equation R; axial velocities on the left- and right-hand sides of the structure $V(LR)$; axial velocities above and below the structure $V(TB)$; source term of the axial momentum equation S; pressures on the left- and right-hand sides of the internal $P(LR)$; pressures above and below internal $p(TB)$; hydrodynamic pressure p; boundary flag of the first interface KF1; boundary flag of the second interface KF2; segment number of the first interface IV1; segment number of the second interface IV2.

Note that the format of variable printout may be changed from time to time. However we don't anticipate any difficulty of understanding the meaning of these variables. For instance if radial velocity U is printed in four rows under heading U(LTRB), then these four values indicate the radial velocities corresponding to the fluid at the left, top, right, and bottom side of the structure, respectively. Similar designation applied to other field variables.

4. Pictorial Display

a. FILM Output

The program provides reactor configuration generated by the FILM at every NDTP cycle. Thus, structural deformation, marker-particle movements, core expansions, and flow patterns can be seen on a series of these displays.

b. Results for CALCOMP Plot

After the calculation is terminated, the program prints out all the information stored on binary tape 2 to be used later for plotting purposes. The information is printed in the form: (1) problem title; (2) number of cycles

stored and number of values stored; (3) a table of 10 columns consisting of cycle number, time in seconds, and eight columns of values stored. This information is printed repeatedly until all values are printed. Each column of values is headed by KXP(I), KYP(I), and KZP(I) identifying the zone and the type of variable stored as supplied in card Type 4.

D. Program Execution and Limitations

As will be described later that the dimensions of common blocks inside the computer code is not dynamically allocated. We intend to make the dynamic allocations of the program in the near future so that one can save the core storage for different applications. However, the available load module has a capacity of executing problems with 420 Eulerian cells and 4000 marker particles, which is large enough for most containment analyses. Nevertheless, adjusting dimensions of several important common blocks, such as X00, BOXJ, SS, and BOXH in subroutines MAIN and OTAPE to save core storage is possible. Such adjustment can be easily done through (1) updating procedure, or (2) changing common-block dimensions in those four subroutines and linking those updated members with the existing load module. To accomplish this procedure, let us introduce the functions of these common blocks and subroutines.

1. Changes of Common Blocks for Saving Computer Storage

a. COMMON/X00/

Consisting variables for analyses involving hydrodynamics, coolant-vessel interaction, rigid cell boundaries, above-core hydrodynamics.

b. COMMON/BOXJ/

Consisting variables for fluid-structure interaction with deformable internals.

c. COMMON/SS/

Consisting variables for cover jump and sodium spillage analysis which involves quasi-Eulerian irregular cells underneath the reactor cover.

d. COMMON/BOXH/

Consisting variables of marker particles involving outflow in the sodium-spillage analysis.

e. COMMON/ALLOC/QWHAMS(9000), MAXQ

Consisting variables for structural dynamic calculation with MAXQ = 9000 specified internally in subroutine MAIN.

2. Adjustment of Subroutines Needed for Saving the Computer Storage

a. MAIN: presets dimensions of important variable and parameter in several common blocks; common blocks needed to be adjusted are X00, BOXJ, SS, BOXH, and ALLOC, as well as the value of MAXQ.

b. OTAPE: writes or reads tapes for the purpose of continuation of a run; common blocks needed to be adjusted are X00, BOXJ, BOXH. Note that adjustment of these common blocks are needed only if continuation of a computational run is involved.

3. Limitations

<u>Number of</u>	<u>Not to Exceed</u>
Eulerian cells	420
Cells in the radial direction	30
Cells in the axial direction	100
Marker particles	4000
Data points per run for each CALCOMP display	1000
Different plots for CALCOMP display	100
Data points on pressure-volume ratio $\left[p \sim \left(\frac{V}{V_0} \right) \right]$ curve	150
Data points on pressure-time (P-t) curve	150
Pressure sources	2
Rigid obstacles	350
Rigid thin membrane (or plate) located at cell boundary	100

<u>Number of</u>	<u>Not to Exceed</u>
Eulerian cells describing the source regions	100
Eulerian cells for perforated internal structures	100
Load lines or interfaces of fluid and deformable structures	10
Points, segments	100
Nodes, elements	100
Stress-strain coordinates for holddown bolts	15
Piecewise linear segments for stress-strain curve of each thin shell	5
Materials involved in the structural-dynamic analysis	20

The program has other limitations. These are (1) source region must be greater than one Eulerian cell, (2) marker particle must be used whether the flow is confined or involves a free surface, (3) slug impact can be analyzed only in the positive z direction, (4) the flow must be laterally confined, and (5) deformation of the internal structure must be small.

The limitation on the deformations of the reactor internals needs further explanation. Note that the ICECO code uses Eulerian coordinates in the fluid calculations. These coordinates are fixed in the space. In reactor containment the reactor vessel and internal structures are not rigidly fixed in space. As they displaced under the applied pressure loads, their boundaries will intersect the Eulerian grid lines, creating irregular cells. The treatment of the irregular cells at the fluid-structure interface is very complex. Particularly, for the deformable internals the analysis usually involves multi-valued field variables near the structures. Since treatment of reactor internals with large displacement is a formidable task to accomplish, present program can only treat small displacements of the reactor internals.

VI. INPUT INSTRUCTION

The input data cards consists of two parts: (1) hydrodynamics, and (2) structural dynamics. The data cards in these two parts are numbered independently to each other so that any adding or deleting of card in one part will not effect the sequence of the other.

A. Hydrodynamics Input*

0

Note: The following card types are required as input information to the program and are listed in the order in which they must appear in the data deck.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
1		(20A4)		
	1-80		TITLE	80 characters of alphanumerics for problem identification. Column 1 must be blank.
2		(4I6)		
	1-6		IBAR	\bar{I} , number of cells in the r (or x) direction, including two boundary cells for calculation purpose ($IBAR \geq 3$).
	7-12		JBAR	\bar{J} , number of cells in the z (or y) direction, including two boundary cells for calculation purpose ($JBAR \geq 3$).
	13-18		INDMAT	Index for allocating dimensions of field variables for multi-material interaction.

Note: If $IBAR = 3$, the flow is one dimensional and the boundary of the fluid domain is rigid in the r (or x) direction.

* Note that in this load module the capabilities of treating cavitation and heat transferred are not included.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
2 (contd.)				<p>INDMAT = 0: Field variables for multi-material calculation having minimum dimensions.</p> <p>INDMAT = 1: Field variables for multi-material calculation having normal dimensions. At the present time INDMAT = 1 is not available.</p>
19-24			IDEFST	<p>Index for allocating dimensions of field variables for internal deformable structure.</p> <p>IDEFST = 0: Field variables for deformable internals having minimum dimensions.</p> <p>* IDEFST = 1: Field variables for deformable internals having normal dimensions. IDEFST is closely associated with IVESSL = 4 specified on card of Type 6.</p>
<u>Note:</u> See Section V for other changes needed to conserve core storage.				
2A		(2I6)		Card for multi-material interaction used only when INDMAT = 1 on card of Type 2.
1-6			NMAT	Number of different fluids (excluding the core-gas bubble and the trapped air) involved in the calculation.
7-12			NBAR	Total fluid particles involved in the analysis for designing different fluids.
3		(2I6)		Cards for displaying curves.
1-6			NPP	Number of curves (or field variables) to be written on plot tape 2 and to be displayed later by the CALCOMP plotter. The values (or data points) for each curves are printed at the end of each run at

* If IVESSL = 4 is specified on card Type 6, IDEFST must be set equal to 1.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
3 (contd.)				every NDTCLC cycle ($100 \geq \text{NPP} \geq 0$) specified on card 11. $\text{NPP} = 0$; printed values and CALCOMP plot are neglected.
	7-12		NPRS	Index for the specification of the initial value for each individual curve. $\text{NPRS} = 0$; the initial values of all the NPP curves are zero. $\text{NPRS} \neq 0$: the initial value of each curve may not be zero. In this case, specify the initial value of each curve on the cards of Type 29.
4		(18I4)		Specification of the values of be displayed by the CALCOMP plotter.
	1-4		KXP ₁	Used only when $\text{NPP} > 0$ on card of Type
	5-8		KYP ₁	3.
	9-12		KZP ₁	KXP _m , KYP _m , and KZP _m define the values to be stored for the CALCOMP plotter: $m = 1, \dots, \text{NPP}$ ($100 \geq \text{NPP} \geq 0$). Six sets of KXP _m , KYP _m , and KZP _m values per card. Use as many cards of Type 4 as needed.

Specification

KXP_m is the radial cell number I_m , and KYP_m is the axial cell number J_m . KZP_m defines the values for that cell.

KZP_m = 1: Pressure, in dynes/cm².

KZP_m = 2: Radial velocity component, in cm/sec. 0

KZP_m = 3: Axial velocity component, in cm/sec.

<u>Card</u> <u>Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN</u> <u>Name</u>	<u>Description</u>
4 (contd.)				<p> $KZP_m = 4$: Here $KXP_m = 100 \cdot J_m + I_{n1}$, and $KYP_m = 100 \cdot J_m + I_{n2}$. The value is the force in dynes as applied by the pressure in cells (I_{n1}, J_m), (I_{n1+1}, J_m) through (I_{n2}, J_m) on the upper area of the above cells. </p> <p> $KZP_m = 5$: Here $KXP_m = 100 \cdot I_m + J_{n1}$, and $KYP_m = 100 \cdot I_m + J_{n2}$. The value is the force in dynes as applied by pressure in cells (I_m, J_{n1}) through (I_m, J_{n2}) on the right-side area of the above cells. </p> <p> $KZP_m = 6$: Here $KXP_m = 100 \cdot J_m + I_{n1}$, and $KYP_m = 100 \cdot J_m + I_{n2}$. The value is the upward force in dynes applied on the perforated plate. The plate is oriented horizontally and is spanned from cell (I_{n1}, J_m) to (I_{n2}, J_m) which may have full-cell openings. </p> <p> $KZP_m = 7$: Pressure on the structural seg- ment, in dynes/cm. </p> <p> $KXP_m = 0$ or arbitrary. $KYP_m =$ the segment number. </p> <p> $KZP_m = 8$: Radial velocity at the mid- point of the structural segment, in cm/sec. </p> <p> $KXP_m = 0$. $KYP_m =$ segment number. </p> <p> $KZP_m = 9$: Axial velocity of the mid- point of the structural segment, in cm/sec. </p>

<u>Card</u>	<u>Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTTRAN</u> <u>Name</u>	<u>Description</u>
4					
					(contd.)
				$KXP_m = 0.$	
				$KYP_m =$ segment number.	
				$KZP_m = 10:$ Radial displacement of the structural node <u>point</u> , in cm.	
				$KXP_m = 0.$	
				$KYP_m =$ node point number.	
				$KZP_m = 11:$ Axial displacement of the structural node point, in cm.	
				$KXP_m = 0.$	
				$KYP_m =$ point number.	
				$KZP_m = 12:$ Circumferential strain of the structural node.	
				$KXP_m =$ the component number (see Fig. 68).	
				$KYP_m =$ the element number.	
				$KZP_m = 13:$ Meriendianal strain of the structural element, in %.	
				$KXP_m =$ the component number (see Fig. 68).	
				$KYP_m =$ the element number.	
				$KZP_m = 14:$ Total net force on the radial shield core barrel simulated by the rigid obstacles, in dynes/cm ² . Here $KXP_m = 100 \cdot I_m + J_{n1}$ and $KYP_m = 100 \cdot I_m + J_{n2}$. The value is the outward force in cells (I_{m-1}, J_{n1}) through (I_{m-1}, J_{n2}) subtract the inward force in cells (I_{m+1}, J_{n1}) through (I_{m+1}, J_{n2}). Note that I_m denote the radial cell number of the radial sheild.	
				$KZP_m = 15:$ Axial position of the marker particle, in cm.	
				$KYP_m =$ the particle number.	
				$KZP_m = 16:$ Total mass of fluid spillage through penetration opening on the vessel cover, in gm.	

<u>Card</u> <u>Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN</u> <u>Name</u>	<u>Description</u>
4 (contd.)				<p>KXP_m = the radial cell number with the opening.</p> <p>KZP_m = 17: Total mass of fluid spillage through vessel-head junction, in gm.</p> <p>KZP_m = 18: Total force acting on the movable head, in dynes.</p> <p>KZP_m = 19: Total force in the hold-down bolts if the head is movable, in dynes.</p> <p>KZP_m = 20: Axial displacement of the movable head, in cm.</p> <p>KZP_m = 21: Velocity of the movable head, in cm/sec.</p> <p>KZP_m = 22: Acceleration of the movable head, in cm/sec².</p> <p>KZP_m = 23: Pressure in the quasi-Eulerian cell generated by the movable head, in dynes/cm².</p> <p>KZP_m = 24: Radial velocity in the quasi-Eulerian cell defined at right-hand boundary, in cm/sec.</p> <p>KZP_m = 25: Axial velocity in the quasi-Eulerian cell defined at upper cell boundary, in cm/sec.</p> <p>KZP_m = 26: Impulse acting on the penetration opening of the vessel head, in dyne-sec/cm².</p> <p>KXP_m = the radial cell number having the opening.</p> <p>KZP_m = 27: Density in the quasi-Eulerian cell, in gm/cm³.</p> <p>KXP_m = the radial cell number.</p> <p>KZP_m = 28: Velocity in the penetration opening, in cm/sec.</p>

<u>Card</u> <u>Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN</u> <u>Name</u>	<u>Description</u>
4 (contd.)				<p> KXP_m = radial cell number. KYP_m = 0 or arbitrary. $KZP_m = 29: KXP_m = 100 \cdot J_m + I_{n1}$. $KYP_m = 100 \cdot J_m + I_{n2}$. The value is the downward force on the perforated structure. The structure is oriented horizontally and is spanned from cell (I_{n1}, J_m) to (I_{n2}, J_m). $KZP_m = 30$: (not available). Axial velocity in the perforated upper internal structure, in cm/sec. KXP_m = radial cell number. KYP_m = axial cell number. $KZP_m = 31$. Material strain energy, in dyne-cm. KXP_m = material number. KYP_m = 0 or arbitrary. $KZP_m = 32$. Total kinetic energy of the structural components. KXP_m = total number of material + 1. KYP_m = 0 or arbitrary. $KZP_m = 33$: stress or strain (see Fig. 68). KXP_m = the component number (see Fig. 68). KYP_m = the element number. </p>

- Note:**
- (a) Cards of Type 4 are not needed when $NPP = 0$ is specified on card of Type 3.
 - (b) If $NPRS \neq 0$ on card of Type 3, the initial value of each curve may be different from zero and hence should be specified on cards of Type 29.
 - (c) Calculations of the circumferential strain ($KZP = 12$) and the meriendianal strain ($KZP = 13$) are done in the finite element program. See Fig. 68 for determination of the component number.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
5		(2I6)		
	1-6		IOUT	<p>Parameter to determine restart-capability usage of auxiliary tapes 8 and 9.</p> <p>IOUT = 0: Tapes 8 and 9 are not used.</p> <p>IOUT = 1: After the computation is terminated, the program writes the output data on a binary tape 8 so that the problem may be continued later.</p> <p>IOUT = 2: Continuation of the problem from a previous run. Program reads the input data from a binary tape 9.</p> <p>IOUT = 3: Program combines both IOUT = 1 and IOUT = 2 capabilities. Program reads the input data from a binary tape 9 and also writes the output data on a binary tape 8 for later continuation.</p>
<p><u>Note:</u> For IOUT = 2 or 3, the input to the program is on tape 9; thus, only cards of Type 1-20 are required.</p>				
	7-12		IZIP	<p>Index for choosing the differencing scheme.</p> <p>IZIP = 0: ZIP differencing.</p> <p>IZIP = 1: Complete donor-cell differencing.</p> <p>IZIP = 2: Partial donor-cell differencing.</p>
	13-18		IFLMCV	<p>Index for plotting the reactor cover.</p> <p>IFLMCV = 0: Reactor cover is not plotted.</p> <p>IFLMCV = 1: Reactor cover is plotted.</p>
	19-24		INDPEF	<p>Index for analyzing perforated structures by the control-volume method.</p> <p>INDPEF = 0: No perforated structure.</p> <p>INDPEF = 1: (not available). With perforated structure analyzed by the</p>

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
5 (contd.)				control-volume method. Provide hydrodynamic information on cards of Type 49-53.
	25-30		JHEAD	Axial cell number at which the upper cell boundary coincides with the bottom of the reactor cover. JHEAD = JBAR-1 for rigid cover.
	31-36		NCONVG	Number of iterations the solution is forced to be converged after NCYCVG cycle of calculation (for debugging purpose). NCONVG = 0: No limitation on the number of iteration.
	37-42		ISTATE	Index for indicating type of fluid and its equation of state involved in the analysis. ISTATE = 0: Water or sodium. ISTATE = 1: Gas.
	43-48		MINITR	Minimum number of iterations for improving the solution of the coupled fluid-structure problem. MINITR = 0: No minimum iterations. MINITR > 0: Minimum number of iterations is MINITR. Input card 5A required.
	49-54		NCYCVG	Cycle number after which the solution is assumed to be converged after NCONVG iteration (for debugging purpose).
5A		(1E12.4)		
	1-12		VDIF	Velocity discrepancy associated with MINITR specified on card of Type 5.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
5A (contd.)				In the boundary cell if $ \bar{v}_p - \bar{v}_b $ is greater than VDIF the iteration will continue at least MINITR times to ensure the accuracy of the boundary treatment.
<u>Note:</u> Card of Type 5A is not required if MINITR = 0 specified on card Type 5.				
6		(12I6)		Parameter card.
	1-6		KY	Number of marker particles initially assigned to each full cell (KY > 0).
<u>Note:</u> Particles located at the upper and right edges of the cell (i, j) will belong to cell (i, j).				
	7-12		NLAST	Stop cycle; allows the problem to be terminated after stop cycle.
	13-18		IDT	Index for selecting the time step. IDT = 1: Constant time step is used. This time step should be specified on card of Type 18. IDT = 2: 12 varied time steps are used in the calculation. These steps should be specified on cards of Type 16 and 17, and will be changed automatically at 12 cycles (NCL1, NCL2, ..., NCL12) prescribed on cards of Type 15.
	19-24		IVIS	Viscosity index (a parameter for selecting the viscosity coefficients μ and λ of the fluid used in the calculation). IVIS = 0: Viscosities λ and μ are neglected. IVIS = 1: $\lambda = 0$, real value of μ is used. The value of μ is specified on card of Type 19.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
6 (contd.)				<p>IVIS = 2: $\mu = 0$, artificial coefficient λ is used.</p> <p>IVIS = 3: $\lambda = 0$, artificial coefficient μ is used.</p> <p>IVIS = 4: $\mu = 0$, real value of λ is used and should be specified on card of Type 19.</p> <p>IVIS = 5: Real values of both λ and μ are used, and these values should be specified on card of Type 19.</p> <p>IVIS = 6: Artificial viscosities λ and μ are used.</p>
25-30			ITAU	<p>Index controlling mass-diffusion coefficient.</p> <p>ITAU = 0: Mass-diffusion coefficient τ is taken to be zero.</p> <p>ITAU = 1: Constant value of τ is used. The value should be specified on card of Type 19.</p> <p>ITAU = 2: Artificial mass-diffusion coefficient is considered.</p>
31-36			NP	<p>Number of cells (or number of regions, NP, in case of $NP < 0$) with initial pressure, velocities, internal energy, etc., input individually. Thus, in the program the uniform initial conditions (pressure, velocities, and specified internal energy specified on card of Type 22) in these NP cells will be Overridden by the nonuniform initial conditions provided on cards of Type 30 or 30A.</p>

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTTRAN Name</u>	<u>Description</u>
6 (contd.)				
	37-42		INDOUT	<p>Outflow (fluid spillage) controlling index.</p> <p>INDOUT = 0: No fluid spillage.</p> <p>INDOUT = 1: Fluid spillage through one-cell opening at the upper containment wall immediate below the vessel head.</p> <p>INDOUT = 2: Fluid spillages through both penetrations and the side opening at the vessel-head junction. In this case, input data for penetrations and side opening are needed to be specified on cards of Type 42-46.</p>
	43-48		INDBC	<p>Index controlling outflow (fluid spillage) boundary condition.</p> <p>INDBC = 0: Outflow boundary condition is not specified; set INDOUT = 0.</p> <p>INDBC = 1: Downstream of the outflow boundary is assumed to be a pressure free and frictionless region; used when INDOUT > 0.</p> <p>INDBC > 1: Not available.</p>
	49-54		INDHT	<p>Index indicating whether source pressure is generated by the heat transfer mechanism (such as fuel-coolant interaction).</p> <p>INDHT = 0: Source pressure is not generated by the heat transfer mechanism.</p> <p>INDHT ≠ 0: (not available). Source pressure is generated by the heat-transfer mechanism.</p>

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
6 (contd.)				
	55-60		IVESSL	<p>Index indicating type of vessel boundary.</p> <p>IVESSL = 0: Vessel boundary is rigid and coincides with the grids of Eulerian cells.</p> <p>IVESSL = 1: Deformable vessel, vessel motion is computed by a finite-difference this shell program (not available).</p> <p>IVESSL = 2: Deformable vessel. Vessel motion is computed by a finite-element structural program, WHAMS. Provide input data for WHAMS.</p> <p>IVESSL = 3: Rigid vessel. The shape of the vessel can be arbitrarily such as the curved reactor bottom. The curved boundary will generate irregular Eulerian cells. Provide input data for irregular cells on cards Type 32 and 33.</p> <p>* IVESSL = 4: Deformable vessel and internal structures. Motion of the deformable structure is computed by a finite-element structural program, WHAMS. Provide additional data for hydrodynamics on cards Type 34-40, also provide data for WHAMS program.</p>
	61-66		ICOVER	<p>Index for indicating cover-head analysis.</p> <p>ICOVER = 0: Rigid cover. The bottom boundary of the reactor cover coincides with the Eulerian grid lines.</p> <p>ICOVER = 1: Movable cover. Provide data for cover and bolts on cards Type 42-44.</p>
7	(12I6)			
	1-6		IPART	<p>Index controlling marker particle and fluid-boundary movement.</p>

*The Index IVESSL = 4 can also be used in problems involving (1) multi-vessels located externally, and (2) vessel with orientation changing abruptly such as the curved reactor bottom.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
7 (contd.)				
				IPART = 0: Fluid movement is neglected. This approach is sometimes used in the pipe flow.
				IPART = 1: Fluid movement is considered.
7-12			INDPCT	Slug-Impact index. INDPCT = 0: No slug impact. INDPCT = 1: With slug impact.
13-18			KIMP	Number of marker particles contacting vessel cover required to indicate the beginning of slug impact (suggest KIMP = 1).
19-24			INDCOR	Number of source regions (or free sur- face plus interface) involved in the analysis. The first source region is the core-gas bubble; the second source region is the cover-gas region ($0 <$ $INDCOR \leq 2$). INDCOR = 1: Only reactor core considered as the source.
25-30			MPA	Number of particles used to define the boundary of the core-gas bubble (or the first source region).
31-36			MPB	Number of particles used to specify the free-surface position (that is, the in- terface between the cover-gas region and the sodium pool).
37-42			INTEG	Index for calculating the volume of the core-gas bubble. INTEG = 1: Calculating bubble volume with respect to the r axis.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
7 (contd.)				
				INTEG \neq 1: Calculating bubble volume with respect to the z axis.
43-48			INDMPA	<p>Index for film display of marker particles around the core.</p> <p>INDMPA = 0: Marker particles defining the core-gas bubble are not connected by straight lines.</p> <p>INDMPA = 1: Marker particles defining the core-gas bubble are connected by the straight lines through the FILM subroutine.</p>
49-54			ISHALW	<p>Index for excursion geometry.</p> <p>ISHALW = 0: Deep excursion in which regions of the core-gas bubble and the upper cover gas can be separated by a value of YMAX. In this case, specify YMAX on card of Type 12.</p> <p>ISHALW = 1: For shallow-coolant excursion in which the core-gas bubble and upper cover-gas regions cannot be separated by a prescribed value.</p>
55-60			INDKT	<p>Index indicating interfacial boundary condition during the slug impact.</p> <p>INDKT = 0: Particles on the coolant free surface once contact with the cover will remain in contact but can slide tangentially.</p> <p>INDKT = 1: (not available). Particles contact with the cover can separate from the cover.</p>

<u>Card</u> <u>Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN</u> <u>Name</u>	<u>Description</u>
7 (contd.)				
	61-66		IEXPN	<p>Index indicating the effect of the radial shield on the core-gas bubble expansion; used when core particles move to the right-hand side of the radial shield (such as in the SRI experiments).</p> <p>IEXPN = 0: Bubble-volume calculation is not effected by the radial shield.</p> <p>IEXPN = 1: Bubble-volume calculation is effected by the <u>rigid</u> radial shield. Supply information of the radial shield and core particles on card of Type 28D for correct volume computation.</p> <p>IEXPN = 2: Bubble-volume calculation is effected by the <u>flexible</u> radial shield. Supply information on card of Type 28E for correct volume computation.</p>
	67-72		IFLAG	<p>Index indicating the flagging scheme used at the free surface and the bubble-coolant interface.</p> <p>IFLAG = 0: Detailed flagging scheme similar to the one used at the curved vessel bottom.</p> <p>IFLAG = 1: Conventional flagging scheme such as the one used in the MAC method.</p>
<p><u>Note:</u> (a) When IFLAG = 0, the first and last marker particles of the core-gas bubble must be located on the symmetrical axis.</p> <p>(b) For the case of strong source pressure and large curvature at the bubble-coolant interface IFLAG = 0 may give better results.</p> <p>(c) See Section V for descriptions of the flagging schemes.</p>				
8	(5I6)			Source card.
	1-6		INDPT	Index to indicate the characteristic of source pressure.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
8 (contd.)				<p>INDPT = 0: Source pressures are calculated by pressure-volume (p-v) relationship.</p> <p>INDPT = 1: Source pressures are determined by the pressure-time (p-t) relationship.</p>
7-12			INDPTA	<p>Index to determine the p-t relationship at the core-gas bubble, or source region at the lower end of the fluid region.</p> <p>INDPTA = 0: Gas bubble is subjected to zero pressure.</p> <p>INDPTA = 1: Gas bubble is subjected to a constant-pressure PRESS specified on card of Type 23.</p> <p>INDPTA = 2: Gas bubble is subjected to a pressure $P = F_1(t)$, with number of data points specified by KCA, and the corresponding pressure and time values prescribed on cards of Type 9.</p> <p>INDPTA = 3: Gas bubble is subjected to a pressure calculated from $pV^Y = C$. Specify initial pressure, energy, and gas exponent on cards of Type 23.</p> <p>INDPTA = 4: Gas bubble is subjected to a pressure $P = F_1(V/V_0)$, with number of data points specified by KCA, and the corresponding pressure and volume-ratio (V/V_0) values prescribed on cards of Type 9.</p>
13-18			INDPTB	<p>Index to indicate the p-t relationship at the cover-gas region or at the upper end of the fluid region.</p> <p>INDPTB = 0: Cover-gas region is subjected to a zero pressure.</p>

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTTRAN Name</u>	<u>Description</u>
8 (contd.)				<p>INDPTB = 1: Cover-gas region is subjected to a constant pressure PRESSB specified on card of Type 24.</p> <p>INDPTB = 2: Cover-gas region is subjected to a pressure $p = F_2(t)$, with number of data points specified by KCB, and the corresponding pressure and time values prescribed on cards of Type 10.</p> <p>INDPTB = 3: Cover-gas region is subjected to a pressure calculated from $PV^Y = C$, specify initial, pressure energy, and gas exponent on cards of Type 24.</p> <p>INDPTB = 4: Gas-gas (or second source) region is subjected to a pressure $p = F_2(V/V_0)$, with number of data points specified by KCB, and the corresponding pressure and volume-ratio (V/V_0) values prescribed on cards of Type 10.</p>
	19-24		KCA	Number of data points on the $F_1(t)$ [or $F_1(V/V_0)$] curve applied at the core-gas bubble or at the lower end of the fluid region ($0 \leq KCA \leq 150$).
	25-30		KCB	Number of data points on the $F_2(t)$ [or $F_2(V/V_0)$] curve applied at the upper gas gap or the upper end of the fluid region ($0 \leq KCB \leq 150$).
9		(8F9.0)		
	1-9		PPA _i	$\left. \begin{array}{l} PPA_i \\ VVA_i \end{array} \right\}$ P_i and T_i ($i = 1, 2, \dots$) are the pressure and time (or volume ratio) values, respectively. These values are taken from the data points of pressure-versus-time (or
	10-18		VVA _i	

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTTRAN Name</u>	<u>Description</u>
9 (contd.)				
	etc.			volume ratio) curve specified for the core-gas bubble region.
<p><u>Note:</u> (a) There are KCA (see card Type 8) sets of pressure and time (or volume ratio) input, each card consists of 4 sets of them.</p> <p>(b) The times (or volume ratios) on cards of Type 9 are in increasing order.</p> <p>(c) Cards of Type 9 are required if either INDPTA = 2 or 4 specified on card Type 8.</p>				
10	(8F9.0)			
1-9		PPB _i	}	P _i and T _i (i = 1, 2, ...) are the pressure and time (or volume ratio) values, respectively. These values are taken from the data points of pressure-versus-time (or volume ratio) curve specified for the cover-gas region.
10-18		VVB _i		
etc.				
<p><u>Note:</u> (a) There are KCB (see card Type 8) sets of pressure and time (or volume ratio) input. Each card consists of 4 sets of them.</p> <p>(b) The times (or volume ratios) on cards of Type 10 are in increasing order.</p> <p>(c) Cards of Type 10 are required if either INDPTB = 2 or 4 is specified on card Type 8.</p>				
11	(5I6)			Frequency card.
1-6		NDTP		Frequency of film output. NDTP = 0: No film output. NDTP ≥ 1: Marker-particle configuration is displayed every NDTP cycle.
7-12		NDTCP		Frequency of output of physical variables for all Eulerian cells. These variables include u, v, c, p, and cell flag F.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
11 (contd.)				<p>NDTCP = 0: No variable output.</p> <p>NDTCP \geq 1: Cell-variable output every NDTCP cycle.</p>
13-18			NDTPP	<p>Frequency of the printout of marker-particle positions. The printout includes the numbering of the particles, and the radial and axial positions of each marker particle.</p> <p>NDTPP = 0: No particle-position printout.</p> <p>NDTPP \geq 1: Particle-position printout every NDTPP cycle.</p>
19-24			NDTCLC	<p>Frequency of data points to be plotted on each curve. Maximum number of data points for each curve is limited to 1000. Thus, if the computing cycles exceed 1000, frequency is needed so that each curve is made of 1000 data points or less.</p> <p>NDTCLC = 0: CALCOMP plot is neglected.</p> <p>NDTCLC \geq 1: Each curve is made of values obtained from every NDTCLC cycle.</p>
25-30			NDTGEN	<p>Frequency of general output. The printout includes the source informations, cycle number, time, iteration number, viscosities, and etc.</p> <p>NDTGEN = 0: No general printout.</p> <p>NDTGEN > 0: General printout every NDTGEN cycle.</p>
31-36			NGRID	<p>Frequency to omit the plotting of grid lines on the film output. NGRID must be multiple value of NDTP.</p>

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
11 (contd.)				
				NGRID \leq 1: Program reset NGRID = NDTP. NGRID $>$ 1: Grid lines are omitted at every NGRID cycle.
	37-42		NDTSTR	Frequency of output of the structural dynamics. NDTSTR = 0: No printout. NDTSTR $>$ 0: Printout at every NDTSTR cycle (not available).
	43-48		NDTFLG	Frequency of output for the boundary cell flag. NDTFLG = 0: No printout. NDTFLG $>$ 0: Printout at every NDTFLG cycle (not available).
	49-54		NDTINT	Frequency for printout hydrodynamics of deformable internal structures. NDTINT = 0: No printout. NDTINT $>$ 0: Printout at every NDTINT cycle (not available).
	55-60		NDTSSP	Frequency for printout hydrodynamics of sodium spillage. NDTSSP = 0: No printout. NDTSSP $>$ 0: Printout at every NDTSSP cycle (not available).
12	(6E12.4)			
	1-12		DR	δr (or δx), the cell size in the r (or x) direction, in centimeters.
	13-24		DZ	δz (or δy), the cell size in the z (or y) direction, in centimeters.
	25-36		PC	Problem-geometry parameter.

<u>Card</u> <u>Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN</u> <u>Name</u>	<u>Description</u>
12 (contd.)				
				PC = 0: Calculation performed in the cylindrical coordinates with axial symmetry (in r-z plane).
				PC = 1.0: Calculation performed in the plane coordinates (in x-y plane).
	37-48		PROB	Parameter to determine flow characteristic. PROB = 1.0: Incompressible-flow calculation; the equation of state is bypassed in the analysis. PROB = 2.0: Compressible-flow calculation.
	49-60		CONST	ρ_0 , density of the fluid at the standard conditions, in g/cm^3 ($\rho_0 > 0$).
	61-72		YMAX	A maximum value in the z (or y) direction where the maximum axial position of the bubble boundary is not expected to exceed during the expansion in the computing run, in cm. This height is used to differentiate the region of core-gas bubble and the cover gas. Thus, all empty cells and surface cells having axial coordinates ($z_{i,j}$ or $y_{i,j}$) smaller than YMAX will be assumed to be the gas-bubble region. All empty cells and surface cells having the axial coordinates greater than YMAX will be assumed to be the cover-gas region.
13		(I6)		
	1-6		NSOUR	Number of cells corresponding to the initial gas bubble where pressure calculated is the source pressure ($100 > \text{NSOUR} > 0$).

<u>Card</u> <u>Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN</u> <u>Name</u>	<u>Description</u>
13 (contd.)				
<u>Note:</u> Gas bubble must be greater than one cell size.				
14	(12I6)			
	1-6		KSOUX _i	I _i and J _i (i = 1, 2, ...) define, respec-
	7-12		KSOUY _i	tively, the radial and axial cell number
	.			used to represent the initial position
	.			of the core-gas bubble.

Note: Gas bubble must be greater than one cell size.

15	(12I6)		
	1-6	NCL1	NCL1, NCL2, ..., NCL12 are 12 prescribed
	7-12	NCL2	computational cycles at which the time
	.	.	step (δt) is expected to be changed for
	.	.	the numerical integration. The 12 time
	.	.	steps (DLT1, ..., DLT12) are specified
	67-72	NCL12	on the cards of Type 16 and 17.

Note: (a) This card is omitted if IDT = 1 is specified on card of Type 6.

(b) To start fluid motion, it is suggested that $NCL1 \geq 5$. In this case, the program will use a time step of 0.1×10^{-6} sec for the first five computation cycles.

16	(6E12.4)		
	1-12	DLT1	Time steps, in seconds; δt_i represents
	.	.	the corresponding time steps expected
	.	.	to be changed at the respective cycle
	.	.	NCL_i specified on card of Type 15.
	61-72	DLT6	Thus the program will use 0.1×10^{-6}
			sec if $NCL_1 > \text{cycle} > 1$; δt_1 if $NCL_2 >$
			$\text{cycle} > NCL_1$; δt_2 if $NCL_3 > \text{cycle} > NCL_2$;
			...; δt_6 if $NCL_7 > \text{cycle} > NCL_6$.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
17		(6E12.4)		
	1-12		DLT7	Time steps, in seconds, δt_i represents
	13-24		DLT8	the corresponding time steps expected
	.		.	to be changed at the respective cycles
	.		.	NCL_i ($i = 7, \dots, 12$) specified on cards
	.		.	of Type 15. Thus the program will use
	61-72		DLT12	δt_7 if $NCL_8 > \text{cycle} > NCL_7$; δt_8 if NCL_9
				$> \text{cycle} > NCL_8$; ...; δt_{12} if $\text{cycle} >$
				NCL_{12} .

Note: (a) Cards of Type 16 and 17 are omitted if $IDT = 1$ is specified on card of Type 6.

- (b) The size of the time step is also controlled by the stability criteria. If any time step prescribed on the cards of Type 16 and 17 is greater than the one satisfying the stability criteria, the program will use the step calculated by the stability criteria.
- (c) For the compressible-flow problem, it is suggested that the input time steps should not exceed about 10^{-4} sec. Also, time steps should increase gradually.

18		(3E12.4)		
	1-12		EPS	ϵ , convergence criterion for the iteration of pressure field. Usually ϵ is of the order of 5×10^{-4} .
	13-24		EPSS	P_{\min} , the minimum allowable pressure in the fluid region (usually zero), in dynes/cm ² .
	25-36		DTCON	δt , the constant time step, in seconds, used only when $IDT = 1$ is defined on card of Type 6. (If $IDT \neq 1$, let $DTCON = 0.1 \times 10^{-6}$ sec).
	37-42		TYPE	Parameter for indicating rigid obstacle option.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTTRAN Name</u>	<u>Description</u>
18 (contd.)				<p>TYPE = 0.0: No rigid obstacle in the computing region.</p> <p>TYPE = 1.0: With rigid obstacles in the computing region.</p>
<p><u>Note:</u> (a) If TYPE = 1.0 input data concerning number of cells occupied by the obstacles and perforated holes generated by the arrangement of obstacles should be specified on cards of Type 25, 26, and 27.</p> <p>(b) Each obstacle occupies one full cell, its boundaries coincide with grid lines.</p>				
19	(6E12.4)			
	1-12		VISR	μ , second (dynamic) viscosity coefficient of the fluid, in dyne-sec/cm ² . A real number.
	13-24		VOVISR	λ , first (volumetric) viscosity coefficient of the fluid, in dyne-sec/cm ² . Also a real number.
	25-36		TAU	τ , mass-diffusion coefficient (usually zero).
	37-48		PHI	ϕ , weighting constant for the pressure field in the finite-difference momentum equation. ($1.0 \geq \phi > 0$; usually $\phi = 1.0$).
	49-60		THETA	θ , weighting constant in the finite-difference mass equation. ($1.0 \geq \theta > 0$; usually $\theta = 1.0$).
	61-72		B	The quotient of γ to Prandtl number. B is a constant relating the temperature change with the variation of internal energy of a heat-conducting fluid; for a non-heat-conducting fluid, B = 0.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
20		(6E12.4)		
	1-12		GR	g_r , gravity in the r or x direction (either positive or negative), in dyne-cm/sec^2 .
	13-24		GZ	g_z , gravity in the z or y direction (either positive or negative), in dyne-cm/sec^2 .
	25-36		TS	Initial starting time of problem in seconds.
	37-48		TL	Maximum time, in seconds; allows the problem to be terminated after TL sec.
	49-60		XR	The width of the computing region (in r or x direction), in centimeters. This value does not include two boundary cells [XR = (IBAR - 2) x DR].
	61-72		YT	The height of the computing region (in z or y direction), in centimeters. This value does not include two boundary cells [YT = (IBAR - 2) x DZ].
21		(1I6)		
	1-6		NM	Number of marker-particle sets to be created. For <u>each</u> set of marker particles, the number of particles positioning in the r and z directions (NX and NY), and the initial coordinates and space increments must be specified on cards of Type 31.

Note: The fluid domains are identified by the marker-particle configuration; hence, particles must be used.

22	(5E12.4)			Specification of uniform initial condition.
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<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTTRAN Name</u>	<u>Description</u>
22 (contd.)				
	1-12		UINT	Initial velocity in the r (or x) direction, defined at the right-hand edge of the cell, in cm/sec.
	13-24		VINT	Initial velocity in the z (or y) direction, defined at the upper edge of the cell, in cm/sec.
	25-36		PINT	Initial pressure, defined at the cell center, in dynes/cm ² .
	37-48		EIINT	Initial specific internal energy, defined at the cell center, in cm ² /sec ² .
	49-60		ETINT	Initial specific total energy, defined at the cell center, in cm ² /sec ² .

Note: Usually UINT, VINT, PINT, EIINT, and ETINT all equal zero.

23	(5E12.4)			Card for core-gas bubble and coolant.
	1-12		PRESS	P_0 , initial pressure in the core-gas bubble, in dynes/cm ² .
	13-24		ENERGY	E_0 , initial total energy in the core-gas bubble, in dyne-cm. (Energy > 0; if energy = 0, the program will assume energy = 10 ¹² dyne-cm.)
	25-36		AO	a_0 , speed of sound of the fluid at standard condition, in cm/sec.
	37-48		GMA	η , isentropic exponent of the fluid. It is a constant equivalent to the pressure derivative of bulk modulus of elasticity of the fluid. This constant appears in the Murnagham equation of state and will be used to calculate the $c_{i,j}^n$ through the relation:

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
23 (contd.)				
				$c_{i,j}^n = \left[a_0^2 \left(1 + \frac{p_{i,j}^n}{a_0^2 p_0} \right) \frac{\rho_0}{\rho} \right]_{i,j}$
	49-60		GMAC	γ_c , adiabatic exponent of the core-gas bubble ($1.4 > \gamma_c \geq 1.0$). This constant is used to determine the pressure in the core-gas bubble through the adiabatic equation of state: $p v^{\gamma_c} = \text{constant.}$
24		(3E12.4)		Card for cover gas region.
	1-12		PRESSB	Initial pressure in the upper cover-gas region, in dynes/cm ² .
	13-24		ENGB	Initial energy in the cover-gas region, in dyne-cm.
	25-36		GMAG	γ_g , adiabatic constant for the cover gas ($1.4 \geq \gamma_g \geq 1$). This constant is needed if pressure in the cover-gas region is computed from the adiabatic equation of state: $p v^{\gamma_g} = \text{constant.}$
25		(2I6)		Card specifying number of obstacles and perforated holes (full cell size).
	1-6		NOBT	Number of Eulerian cells occupied by the rigid obstacles ($350 \geq \text{NOBT} \geq 0$).
	7-12		NCONTR	If perforated structure is involved in the analysis and is modelled by the rigid obstacles, NCONTR represents number of holes on the structure ($100 \geq \text{NCONTR} \geq 0$).

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
25 (contd.)				
<u>Note:</u> (a) Card of Type 25 is needed when TYPE = 1.0 specified on card 18. (b) Specify the positions of the obstacle cells and cells occupied by the perforated holes, respectively, on cards of Type 26 and 27.				
26	(12I6)			Obstacle location cards.
	1-6	KOBX _i	}	KOBX _i and KOBY _i (i = 1, 2, ...) define, respectively, the radial and axial cell number used to represent the position of Eulerian cell which is occupied by the _i th rigid obstacle.
	7-12	KOBY _i		
<u>Note:</u> (a) There are NOBT (see card Type 25) sets of radial and axial cell numbers. Each card of Type 26 consists of 6 sets of them. (b) Cards of Type 26 is required if Type = 1 is specified on card of Type 18.				
27	(12I6)			Perforated-hole location cards.
	1-6	KCONX _i	}	KCONX _i and KCONY _i (i = 1, 2, ...) define, respectively, the radial and axial cell number used to represent the position of the holes on the perforated plate.
	7-12	KCONY _i		
<u>Note:</u> (a) There are NCONTR (see card Type 25) sets of radial and axial cell numbers. Each card of Type 27 consists of 6 sets of them. (b) Cards of Type 27 is required only if TYPE = 1.0 (specified on card of Type 18) and NCONTR ≠ 0 (specified on card of Type 25).				
28A	(3I6)			Rigid thin membrane card.
	1-6	IPLATE		Index indicating rigid thin boundary option. IPLATE = 0: No rigid internal thin membrane (or plate). IPLATE = 1: With rigid thin membrane (or plate).

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
28A (contd.)				
	7-12		KBR	Number of thin rigid boundary perpendicular to the radial direction (parallel to the axial direction, such as core barrel).
	13-18		KBZ	Number of thin rigid boundary perpendicular to the axial direction (parallel to the radial direction, such as thin plate).

Note: (a) Rigid boundary option can be used to simulate shell or plate, either located internally or externally, but it must be located on the cell boundary.

(b) KBZ \neq 0 only available if IZIP = 1 is selected on card Type 5.

28B	(12I6)			Rigid thin shell location card.
	1-6	IBR _i	}	IBR _i and JBR _i (i = 1, 2, ..., KBR) define, respectively, the radial and axial cell number of an Eulerian cell which has a rigid shell locating at its right-hand cell boundary.
	7-12	JBR _i		
	etc.			

Note: (a) There are KBR (see card Type 28A) sets of radial axial cell number input. Each card Type 28B consists of 6 sets of them.

(b) Cards of Type 28B are required if KBR \neq 0 specified on card Type 28A.

28C	(12I6)			Rigid thin plate location card.
	1-6	IBZ _i	}	IBZ _i and JBZ _i (i = 1, 2, ..., KBZ) define, respectively, the radial and axial cell number of an Eulerian cell which has a rigid thin plate locating at its upper cell boundary.
	7-12	JBZ _i		
	etc.			

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTTRAN Name</u>	<u>Description</u>
28C (contd.)				
<u>Note:</u> (a) There are KBZ (see card Type 28A) sets of radial and axial cell numbers input. Each card Type 28C consists of 6 sets of them. (b) Cards of Type 28C are required if KBZ \neq 0 specified on card Type 28A. (c) KBZ \neq 0 only available if IZIP = 1 is selected on card Type 5.				
28D	(2I6, 2E12.4)			Card for core-volume calculation (for the case of rigid radial shield).
1-6			NTIP	In the case the radial shield is rigid but its boundary not coincides with the Eulerian grid lines, NTIP is the <u>Point</u> Number associated with the upper left corner. If the radial shield is modelled by rigid obstacles, NTIP is a dummy value.
7-12			NCOR	Particle number associated with the right-most marker particle located on the boundary of the core gas bubble. In the analysis this particle must be joined with the upper left corner of the radial shield to accurately calculate the core volume.
13-24			RVTIP	Radial coordinate of the upper left corner of the radial shield.
25-36			ZVTIP	Axial coordinate of the upper left corner of the radial shield.
<u>Note:</u> Card of Type 28D is required if IEXPN = 1 specified on card of Type 7.				
28E	(2I6)			Card for improved core-volume calculation (for the case of flexible radial shield).
1-6			NTIP	<u>Point</u> number on the Lagrangian Load Line, which define the upper left corner of the flexible radial shield.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
28E (contd.)				
	7-12		NCOR	Same description as NCOR on card of Type 28D.

Note: Card of Type 28E is required if IEXPN = 2 specified on card of Type 7.

29	(6E12.4)			Cards provide non-zero initial values for the plotting curves.
1-12		PRS _{1,1}		PRS _{m,1} is the initial value associated with each I _m and J _m defined in cards of Type 4. These values should be specified in the same order as on the cards of Type 4 and will be printed in the output.
13-24		PRS _{2,1}		
.		.		
.		.		
.		.		
67-72		PRS _{m,1}		

Note: (a) Cards of Type 29 are not needed if NPP = 0 or in NPRS = 0 is specified on card of Type 3.

(b) There are NPP (see card Type 3) initial values. Each card Type 29 consists of 6 of them.

30	(2I6, 5E12.4)			Nonuniform initial condition card (Case 1: NP \geq 0 on card of Type 6).
1-6		I		Cell number of the r (or x) direction.
7-12		J		Cell number in the z (or y) direction.
13-24		U _{I,J}		Velocity in the r (or x) direction, defined at right edge of the cell, in cm/sec.
25-36		V _{I,J}		Velocity in z (or y) direction, defined at the top edge of the cell, in cm/sec.
37-48		P _{i,j}		Pressure at the cell center, in dynes/cm ² .
49-60		EI _{i,j}		Specific internal energy, defined at the cell center, in cm ² /sec ² .
61-72		RHO _{i,j}		Density at the cell center, in gm/cm ³ .

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTTRAN Name</u>	<u>Description</u>
30 (contd.)				
<p><u>Note:</u> (a) Cards of Type 30 used only when $NP \geq 0$ on card of Type 6.</p> <p>(b) Total number of cards of TYPE 30A required is NP specified on card of Type 6.</p>				
30A (alternative)				Nonuniform initial condition card (Case 2: $NP < 0$ on card of Type 6). $ NP $ define the number of sections for specifying the initial conditions.
	1-3		I1	Starting cell number in the r (or x) direction.
	4-6		I2	End cell number in the r (or x) direction.
	7-9		J1	Starting cell number in the z (or y) direction.
	10-12		J2	Ending cell number in the z (or y) direction.
30B (alternative)				
	13-24		$U_{i,j}$	
	25-36		$V_{i,j}$	
	37-48		$P_{i,j}$	See card of Type 30A for descriptions.
	49-60		$EI_{i,j}$	
	61-72		$RHO_{i,j}$	

- Note: (a) Cards of Type 30B used only when $NP < 0$ specified on card of Type 6.
- (b) Total number of cards of Type 30B is $|NP|$ specified on cards of Type 6.
- (c) Here U, V, P, EI, RHO are the uniform condition throughout a region bounded by I1, I2, J1, and J2.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTTRAN Name</u>	<u>Description</u>
31	(2I6, 4E12.4)			Particles set-up cards.
	1-6		NX	Number of columns of marker particles to be created in the r (or x) direction.
	7-12		NY	Number of rows of marker particles to be created in the z (or y) direction.
	13-24		X0	r (or x) coordinate of first particle, in cm.
	25-36		Y0	z (or y) coordinate of first particle, in cm.
	37-48		DXK	Particle spacing in the r (or x) direction, in cm; negative value representing decrement.
	49-60		DYK	Particle spacing in the z (or y) direction, in cm; negative value representing decrement.

Note: (a) Card of Type 31 is needed for each set of particles.. Thus the total number of cards of this type is equal to the value of NM specified on card of Type 21.

(b) Particle sets indicating the initial position of bubble boundary must be specified first and should be numbered in the clockwise direction. The total number of particles used is equal to MPA defined on card of Type 7.

(c) Particle set defining the initial position of the free surface should be input next and should be numbered in the direction of decreasing r. The total number used is equal to MPB defined on card of Type 7.

32	(1I6)			
	1-6		NIRG	Number of irregular cell created by the arbitrarily shaped external boundaries ($50 \geq \text{NIRG} \geq 0$).

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
32 (contd.)				
<u>Note:</u> Cards of Type 39 is needed only if IVESSL = 3 specified on card of Type 6. Here the external boundaries can be of arbitrarily shape but are rigidly fixed in the space.				
33	(4E12.4)			Rigid irregular cell cards.
1-12		RB _i	}	RB _i and ZB _i define, respectively, the radial and axial coordinates of the beginning node point associated with the i th rigid irregular cell.
13-24		ZB _i		
25-36		RT _i	}	RT _i and ZT _i define, respectively, the radial and axial coordinates of the terminating node point associated with the i th rigid irregular cell.
37-48		ZT _i		

Note: (a) The number of cards of Type 33 required is NIRG specified on card of Type 32.

(b) This card is omitted if IVESSL \neq 3 on card of Type 6.

34	(7I6)			Card for hydrodynamics of the deformable internals.
1-6		NLOAD		Total number of load lines (Lagrangian boundary lines) along which the sliding boundary conditions are satisfied. Specify the beginning node point and terminating point of each load lines on cards of Type 35.
7-12		ISTR		Index indicating nature of the internal structure. ISTR = 0: Load lines do not enclose thick component which completely occupies one or more Eulerian cell. ISTR > 1: Load lines may enclose thick component which occupies one or more

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
34 (contd.)				Eulerian cell. In this case, specify the beginning and terminating node points of those load lines (either entire or part of the line) on card of Type 36.
13-18			NSEG	Number of segment at which sliding boundary condition is not required. This situation occurs when structural segment does not contact with the fluid. If NSEG > 0 specify these segments on cards of Type 37.
19-24			NCON	Number of straight lines to be connected in the film output (marker particle configuration plot) for convenience of indicating the internal component. If NCON > 0 specify the beginning and terminating points of each straight lines on card of Type 38. Note that these points must be located on the load lines.
25-30			NPZERO	Number of segments not subjected to the hydrodynamic pressure. This situation occurs if the structure segment does not contact with the fluid. If NPZERO > 0 specify segment numbers on card of Type 39.
31-36			NOPEN	Number of pair segments (one top and one bottom) on the core-support structure having perforated openings. If NOPEN > 0 specify segment number, perforated ratio, and other information on card of Type 40.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTTRAN Name</u>	<u>Description</u>
34 (contd.)				
	37-42		NBLDIS	Index indicating geometrical discontinuities generated by the deformable core barrel. NBLDIS = 0: No core-barrel. NBLDIS = 1: With core-barrel discontinuity. Provide input on cards of Type 41.
	43-48		ILOAD	Index for determining load line type. ILOAD = 0: Load line type (LTLOAD) determined internally. ILOAD = 1: Load line type prescribed by the user. Provide input on card 34A.

Note: (a) If ILOAD = 0 types of all the load lines are determined by the value of IVESSL on card 6; that is IVESSL < 4, $LTLOAD_i = 1$ (external structure); for IVESSL = 4, $LTLOAD_i = 2$ (internal structure).

	49-54		KFLD	Index for prescribing the boundary flags. KFLD = 0: Boundary flag determined internally. KFLD = 1: Boundary flag of certain load line is prescribed by the user. Provide input on card 34B.
34A	(12I6)			Load line type.
	1-6		$LTLOAD_i$	Integer indicating load line type.
	7-12			LTLOAD = 1: External structure. LTLOAD = 2: Internal structure.

Note: (a) Cards of Type 34A is required only if ILOAD \neq 0 on card 34.
(b) Use as many cards of Type 34A as required; $i = 1, 2, \dots, NLOAD$.
(c) LTLOAD = 2, multi-value field variables are used in the analysis.

Card Type	Columns	Format	FORTTRAN Name	Description
34B		(12I6)		Boundary flag of load line.
	1-6		IDEXLD _i	IDEXLD _i and KFLOAD _i provide index and boundary cell flag for the i th load line. IDEXLD _i = 1: The i th load line with pre-scribed boundary flag. KFLOAD _i : A numeral indicating orientation of the boundary segment.
	7-12		KFLOAD _i	
	etc.			
<u>Note:</u> (a) Cards of Type 34B is required only if KFLD ≠ 0 on card 34. (b) There are NLOAD (see card Type 34) sets of index and boundary-flag input. Each card consists of 4 sets of them. (c) See Section V for description of the boundary cell flag.				
35		(12I6)		Load line cards.
	1-6		NBEG _i	NBEG _i and NTER _i (i = 1, ... NLOAD) define, respectively, the beginning and terminating point numbers for the i th load line.
	7-12		NTER _i	
	etc.			
<u>Note:</u> There are NLOAD (see card 34) sets of input. Each card consists of 6 of them.				
36		(12I6)		Thick structure card.
	1-6		NSTRB _i	NSTRB _i and NSTRT _i define, respectively, the two points (not necessary to be the beginning and terminating points) on the load lines which may enclose component having thickness more than one Eulerian cell.
	7-12		NSTRT _i	
	.			
<u>Note:</u> There are ISTR (see card Type 34) sets of input. Each card consists of 6 of them.				
37		(12I6)		
	1-6		KSEG _i	Segment number where sliding boundary condition at the midpoint of that segment is not required.
	7-12			
	etc.			

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTTRAN Name</u>	<u>Description</u>
37 (contd.)				
<u>Note:</u> Use as many cards of Type 37 as required; 12 numbers per each card (1 = 1, 2, ..., NSEG).				
38	(12I6)			
1-6		NCONB _i	}	NCONB _i and NCONT _i (i = 1, 2, ..., NCON) define, respectively the beginning and terminating points on the i th load line to be connected in the film output. The cross hatch line used to indicate the radial shield.
7-12		NCONT _i		
etc.				
<u>Note:</u> There are NCON (see card Type 34) sets of beginning and terminating points. Each card of Type 38 consists of 6 of them.				
39	(12I6)			
1-6		KPZERO _i	}	Some structural segments do not contact with the fluid such as if the segments are the internal members of the structure. In this case, KPZERO _i (i = 1, 2, ..., NPZERO) defines the numbers of those segments.
7-12				
.				
.				
.				
<u>Note:</u> Use as many cards of Type 39 as required; i = 1, ..., NPZERO.				
40	(2I6, 5E12.4)			Perforated core support structure.
1-6		NOSEG1 _i	}	N1 _i and N2 _i (i = 1, 2, ... NOPEN) define, respectively, the bottom and the top segment numbers of the core-support structure.
7-12		NOSEG2 _i		
13-24		RATIO _i		φ _i , perforated ratio (ratio of opening area to the total area of the segment).
25-36		UOPEN _i		U _i , initial velocity in the openings, in cm/sec (normally zero).

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTTRAN Name</u>	<u>Description</u>
40 (contd.)				
	37-48		HIGHT _i	L _i , thickness or length of the opening passage, in cm.
	49-60		COEF _i	Frictional loss coefficient, used to calculate the pressure drop in the coolant passages.
	61-72		EXPONT _i	Exponential factor.

Note: (a) Cards of Type 40 are required if NOPEN > 0 specified on cards of Type 34.

(b) Total number of cards of type required is NOPEN.

41	(2I6)			
	1-6		NPTR	Point number define the upper right end of the flexible core barrel.
	7-12		NPTL	Point number define the upper left end of the flexible core barrel.

Note: Card of Type 41 is used if NBLDIS \neq 0 specified on card of Type 34.

42	(5I6)			Movable cover and sodium spillage.
	1-6		IOPEN	Radial cell number where sodium spillage through vessel-head junction or plug jump occurs. For rigid vessel, IOPEN = IBAR; for the flexible vessel, IOPEN = I _r + 1 in which I _r is the cell number of the rightmost quasi-Eulerian (irregular) cell adjacent to the vessel cell.
	7-12		JOPEN	Axial cell number where sodium spillage through vessel-head junction or plug jump occurs. For the rigid vessel or flexible vessel, JOPEN = J _z + 1, in which J _z is the axial cell number of the uppermost quasi-Eulerian (irregular) cell below the vessel head. Note that to allow

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
42 (contd.)				cover move upward we have to set JOPEN < JBAR.
	13-18		NTOPEN	Number of penetration openings on the vessel head. If NTOPE > 0, specify opening information on card Type 45.
	19-24		NSOPEN	Index indicating sodium spillage through vessel-head junction. NSOPEN = 0: No coolant spillage through side opening. NSOPEN = 1: With coolant spillage through side opening. Specify the vessel height on card Type 46.
	25-30		IFLMCV	Control index for plotting cover and bolts. IFLMCV = 0: Cover and bolts are not plotted in the film configuration. IFLMCV = 1: Cover and bolts are plotted in the film output.

Note: (a) Card Type 42 is required when either INDOUT > 1 or ICOVER ≠ 0 specified on card Type 6.

(b) When sodium spillage is considered (INDOUT > 1), reactor cover must be considered as movable (ICOVER > 0) even if rigid cover is used. Thus, cards of Type 43 and 44 should be included.

43	(2I6, 3E12.4)			Movable reactor cover.
	1-6		KCVR	Number of points on the force-displacement table for describing the response of the cover and bolts.
	7-12		ICONT	Index indicating relative position of the free surface and the cover head. ICONT = 0: Coolant not contacting with cover head initially.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTTRAN Name</u>	<u>Description</u>
43 (contd.)				ICONT = 1: Coolant contacting with cover head initially.
	13-24		CVRMAS	Cover mass, in gm.
	25-36		CVRZ	Initial axial position of the vessel cover, in cm.
	37-48		CVRDPH	Thickness of the cover, in cm.

Note: Cards of Type 43 is required when either INDOUT > 1 or ICOVER \neq 0 specified on card Type 6.

44	(I6, 2E12.4)			Bolts card.
	1-6		K	Point number.
	7-18		CF _K	Force, in dynes/cm ² .
	19-30		CD _K	Displacement, in cm.

Note: (a) Cards of Type 44 are required if either INDOUT > 1 (ICOVER > 0) or ICOVER \neq 0 specified on card Type 6.
 (b) Total number of card Type 44 required is KCVR specified on card Type 43.
 (c) The displacements on card Type 44 must be in increasing order.
 (d) To simulate the rigid cover one can specify large bolt force but small displacement.

45	(2I6, 2E12.4)			Penetration openings card.
	1-6		K	Radial cell number with penetration opening.
	7-12		KNN _K	Flag for K th radial cell. KNN = 1: With penetration.
	13-18		FNTP _K	Allowable impulse of penetration above which the penetration will become open, in dyne-sec/cm ² .
	19-24		FNTAR _K	Opening ratio.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTTRAN Name</u>	<u>Description</u>
45 (contd.)				
<u>Note:</u> (a) Cards of Type 45 is required only if INDOUT > 1 on card of Type 6. (b) Total number of card Type 45 required is NTOPEN specified on card Type 42.				
46		(E12.4)		
	1-12		HTMAX	Maximum vessel height, in cm. If cover height exceeds this value coolant spillage at the vessel-head junction will occur. Use only when NSOPEN = 1 specified on card Type 42.
<u>Note:</u> Cards of Type 47 and 48 are not used. They are reserved for problems involving multi-material interaction.				
49		(10I6)		Parameter card.
	1-6		IUIS	Index for indicating the characteristic of the Upper Internal Structure (UIS). IUIS = 0: No rigid, perforated UIS. IUIS = 1: With rigid, perforated UIS, input the radial and axial cell numbers for each perforated obstacle.
	7-12		ICSS	Index for indicating the characteristic of the Core-Support Structure (CSS). ICSS = 0: No rigid and perforated CSS. ICSS = 1: With rigid and perforated CSS, input the radial and axial cell numbers for each perforated obstacle.
	13-18		NPERF	Total number of perforated-obstacle cells.
	19-24		INDUIS	INDUIS = 1: Control-volume method for analyzing flows through the UIS. INDUIS \neq 1: Other methods (not available).

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTTRAN Name</u>	<u>Description</u>
49 (contd.)				
	25-30		INDCSS	INDCSS = 1: Control-volume method for analyzing flows through the CSS. INDCSS \neq 1: Other methods (not available).
	31-36		JREF	Axial cell number separating the UIS and the CSS. JREF - 1 < J_B , where J_B is the axial cell number below the perforated UIS.
	37-42		MOPEN	Number of columns of cells representing the perforated UIS.
	43-48		NOPE	Number of columns of cells representing the perforated CSS.
	49-54		NDGPEF	Frequency of printout for flow through the perforated structure.
	55-60		ITUBE	ITUBE = 1: Perforated UIS remains intact, only axial fluid motion is involved. ITUBE \neq 1: Not available.
50		(4I6)		Parameter card.
	1-6		IDPUIS	Index for pressure-loss calculation for the UIS. IDPUIS = 0: Pressure loss is not calculated. IDPUIS = 1: Pressure loss is calculated (not available).
	7-12		IDPCSS	Index for pressure-loss calculation for the CSS. IDPCSS = 0: Pressure loss is not calculated. IDPCSS = 1: Pressure loss is calculated (not available).
	13-18		IMVUIS	IMVUIS = 0: Particles move uniformly through the perforated UIS. IMVUIS \neq 0: Not available.

Card Type	Columns	Format	FORTTRAN Name	Description
50 (contd.)				
	19-24		IMVCSS	IMVCSS = 0: Particles move uniformly through the perforated CSS. IMVCSS \neq 0: Not available.
51	(12I6)			Perforated-structure location cards.
	1-6		IPERF _i	IPERF _i and JPERF _i (i = 1, 2...NPERF) define, respectively, the radial and axial cell number for representing the perforated UIS and CSS.
	7-12		JPERF _i	
	.		.	
	.		.	
<u>Note:</u> (a) There are NPERF (see card Type 49) sets of radial and axial cell numbers. Each card of Type 51 consists of 6 sets of them. (b) Card of Type 51 is required if NPERF \neq 0 is specified on card Type 49.				
52	(I6, 3E12.4)			Information for the Upper Internal Structure (UIS).
	1-6		K	Radial cell number.
	7-18		RATUIS _k	Perforation ratio for cells having radial cell number k.
	19-30		DIAUIS _k	Equivalent hydraulic diameter (in cm) for calculating the frictional loss in the UIS (not available).
	31-42		RGHUIS _k	Coefficient for indicating roughness corresponding to cells with radial cell number k (not available)
<u>Note:</u> (a) Cards of Type 52 are required if IUIS = 1 and INDUIS = 1 specified on card Type 49. (b) Total number of card Type 52 required is MOPEN specified on card Type 49.				
53	(I6, 3E12.4)			Information for the Core-Support Structure (CSS).

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
53 (contd.)				
	1-6		K	Radial cell number.
	7-18		RATCSS _k	Perforation ratio for cells having radial cell number k.
	19-30		DIACSS _k	Equivalent hydrodynamic diameter (in cm) for calculating the frictional loss in the CSS (not available).
	31-42		RGHCSS _k	Coefficient for indicating roughness corresponding to cells with radial cell number k (not available).

Note: (a) Cards of Type 53 are required if ICSS = 1 and INDCSS = 1 specified on card Type 49.

(b) Total number of card Type 53 required is NOPEN specified on card Type 49.

B. Finite-Element Structural Dynamics Input

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTTRAN Name</u>	<u>Description</u>
1		(20A4)		
	1-80		TITLE	80 characters of alpha-numerics for identification. Column 1 should be blank.
2		(5I5, 5X, E10.6, I5)		Parameter card.
	1-5		NNODE	Number of nodes. Note that for shell element each node is assigned a "real" node number and a "dummy" node number. Thus, number of nodes for shell elements must be twice the number of "real" nodes, which should be included in NNODE. $0 < \text{NNODE} \leq 500$ (see card Type 6).
	6-10		NELE	Number of elements. $0 < \text{NELE} \leq 500$ (see card Type 7).
	11-15		NUMMAT	Number of material types specified on card Types 4, 5a, 5b, 5c, or 4, 5x, and 5y. $0 < \text{NUMMAT} \leq 20$.
	16-20		NUMDIS	Number of nodes at which one or more displacement components are prescribed. $0 \leq \text{NUMDIS} \leq 250$ (see card Type 8).
	21-25		MXSTEP	At cycle MXSTEP printer-plotter and CALCOMP output as specified on card Types 10 and 11. MXSTEP must be an integral multiple of NPFREQ (see card Type 9).
	31-40		DELT	Time increment parameter (only used within WHAMS). DELT < 0.0: Program sets $\text{DELT}_{\text{max}} = -\text{DELT}$. DELT = 0.0: Program calculates DELT_{max} with no upper bound. DELT > 0.0: Program calculates DELT_{max} . If

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTTRAN Name</u>	<u>Description</u>
2 (contd.)				
	41-45		NPRES	$\text{DELT}_{\text{max}} > \text{DELT}$, program sets $\text{DELT}_{\text{max}} = \text{DELT}$. Number of load lines (see card Types 13-17) $0 < \text{NPRES} \leq 10$.
3	1-5		KONTRL(1)	KONTRL(1) = 1: Axisymmetric three dimensional problem. KONTRL(1) = 2: Plane stress two dimensional problem. KONTRL(1) = 3: Plane strain two dimensional problem.
4		(3I5)		Material cards.
	1-5		MTYPE	Material type number.
	6-10		NTYPE	NTYPE = 1: For flexural element (shell or beam element). NTYPE = 2: For triangular continuum element (solid or fluid element depending on bulk modulus K specified on card Type 5x). NTYPE = 3: For quadrilateral hydrodynamics element (not available). NTYPE = 4: For quadrilateral elastic-plastic (or fluid) element.
	11-15		NED	Number of straight line segment representing the stress-strain relationship of the flexural element ($\text{NED} \leq 5$, and used only for flexural element).

Note: (a) The flexural element (NTYPE = 1) is used to model the reactor vessel, core barrel, and core-support structure.

(b) The quadrilateral elastic-plastic element (NTYPE = 4) is suggested to model the radial shield or other heavy fluids.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
4 (contd.)				
(c) There should be one set of cards of Type 4, 5a, 5b, and 5c for the flexural element (NTYPE = 1) or one set of cards of Type 4, 5x, 5y for other elements (NTYPE \neq 1).				
5a	(6E10.4)			Material properties (for shell or beam element NTYPE = 1).
	1-10	ED(1)		ρ : Density, in g/cm^3 .
	11-20	ED(2)		σ_1 : Stress at point 1, in dyne/cm^2 .
	21-30	ED(3)		ϵ_1 : Strain at point 1.
	31-40	ED(4)		σ_2 : Stress at point 2, in dyne/cm^2 .
	41-50	ED(5)		Width of beam, in cm (only needed for plane stress problem).
	51-60	ED(6)		ϵ_2 : Strain at point 2.
5b	(6E10.4)			Material properties.
	1-10	ED(7)		ν : Poissons' ratio.
	11-20	ED(8)		t : Thickness of beam element, in cm. Only needed when not specified in dummy node data (card Type 7).
	21-30	ED(9)		Damping coefficient 1 (not available).
	31-40	ED(10)		Damping coefficient 2 (not available).
	41-50	ED(11)		Damping coefficient 3 (not available).
	51-60	ED(12)		Damping coefficient 4 (not available).
5c	(6E10.4)			Material properties.
	1-10	ED(13)		σ_3 : Stress at point 3, in dyne/cm^2 .
	11-20	ED(14)		ϵ_3 : Strain at point 3.
	21-30	ED(15)		σ_4 : Stress at point 4, in dyne/cm^2 .

Card Type	Columns	Format	FORTTRAN Name	Description
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5c
(contd.)

31-40			ED(16)	ϵ_4 : Strain at point 4.
41-50			ED(17)	σ_5 : Stress at point 5, in dyne/cm ² .
51-60			ED(18)	ϵ_5 : Strain at point 5.

Note: In the case of NED \leq 2 specified on card Type 4, card of Type 5c is simply a blank card.

5x		(6E10.4)		Material properties (for continuum elements NTYPE \neq 1).
1-10			E(1,MTYPE)	ρ : Density, in g/cm ³ .
11-20			E(2,MTYPE)	E: Young's modulus, in dyne/cm ² .
21-30			E(3,MTYPE)	σ_y : Initial yield stress, in dyne/cm ² .
31-40			E(4,MTYPE)	Ep: Plastic modulus, in dyne/cm ² .
41-50			E(5,MTYPE)	B_0 : Bulk modulus of elasticity, in dyne/cm ² (for NTYPE = 3, or 4).
51-60			E(6,MTYPE)	σ_{ult} : Ultimate stress, in dyne/cm ² .

Note: (a) For triangular solid element NTYPE = 2, set bulk modulus $B_0 = 0$.
 (b) For triangular fluid element (NTYPE = 2) or quadrilateral fluid element (NTYPE = 3) input density ρ and bulk modulus B_0 only, set other variables equal to zero.
 (c) If the quadrilateral elastic-plastic element is used to simulate fluid input density ρ , bulk modulus B_0 only. Set other variable equal to zero.

5y		(6E10.4)		Material properties.
1-10			E(7,MTYPE)	ν : Poisson's ratio.
11-20			E(8,MTYPE)	B' : The pressure derivative of the bulk modulus of elasticity, used for NTYPE = 4 only.
21-30			E(9,MTYPE)	Damping coefficient.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
5y (contd.)				
	31-40		E(10,MTYPE)	a_Q : Quadratic artificial viscosity coefficient for the quadrilateral elastic-plastic element ($a_Q \approx 1.2$).
	41-50		E(11,MTYPE)	a_L : Linear artificial viscosity coefficient for the quadrilateral elastic-plastic element ($a_L = 0.05 - 0.2$).
	51-60		E(12,MTYPE)	a_R : Rotational artificial viscosity coefficient for the quadrilateral elastic-plastic element.

Note: (a) ED(9,MTYPE) through ED(12,MTYPE) are reserved as the damping coefficients for elements other than the quadrilateral elastic-plastic element.

(b) One should refer to REXCO-HEP, ANL-75-19 (Ref. 3) for damping coefficient and a_Q , a_L , as well as a_R for the elastic-plastic element.

6	(I5, 5X, 2E10.4)			Node cards.
	1-5		N	Node number.
	11-20		XC(N)	X-coordinate of real nodes. For "dummy" nodes (see NNODE description, card of Type 2) thickness of beam may be specified through XC(N). In that case all beam elements joined to node N will have the same thickness at that point.
	21-30		YC(N)	Y-coordinate of real nodes.

Note: Nodal coordinates for nodes equispaced between two nodes will be automatically generated if the data cards for intermediate nodes are skipped.

7	(11I5)			Element cards.
	1-5		M	Element number.
	6-10		NODE(1,M)	Node N1 of element (a "real" node).

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
7 (contd.)				
	11-15		NODE(2,M)	Node N2 of element (a "real" node).
	16-20		NODE(3,M)	Node N3 of element (a "dummy" node for shell element).
	21-25		NODE(4,M)	Node N4 of element (a "dummy" node for shell element).
	41-45		NODE(8,M)	Node(8,M) = 1: Axisymmetric element. Node(8,M) = 2: Plane stress, two dimensional element. Node(8,M) = 3: Plane strain, two dimensional element.
	46-50		NODE(9,M)	Material type number for element M.
	51-55		NODE(10,M)	Element type number for element M. NODE(10,M) = 1: Flexural (shell) element. NODE(10,M) = 2: Triangle continuum element (solid or fluid). NODE(10,M) = 3: Quadrateral hydrodynamic element. NODE(10,M) = 4: Quadrateral elastic-plastic element.

Note: Node cards for elements which can be generated by adding one to all node numbers of the previous element need not be included. The node data for these elements will be generated automatically. However, if this is done the node card for the last element must be included.

8	(I10, E10.4)	NODDIS	Prescribed displacement cards. Use NUMDIS cards (see NUMDIS on card Type 2).	
1-7		N	The node at which one or more <u>displacement</u> components are prescribed to be zero or some non-zero value given in SUBROUTINE FREEFD.	

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
8 (contd.)				
	8		I	\bar{X} -component control; for dummy nodes this is the rotatory degree of freedom.
	9		I	\bar{Y} -component control. I = 0: The component is unconstrained. I = 1: The component is zero. I = 2: The component is a non-zero value which is prescribed in FREEFD as a function of time.
	10			Not used.
	11-20		ANGLE	Angle of inclination of local \bar{X} -axis relative to global x-axis measured counterclockwise in degrees. This local coordinate system enables displacement components other than x and y to be prescribed.

Note: (a) If NUMDIS = 0, skip this type of cards.
(b) Use as many cards of Type 8 as required, total NUMDIS cards.

9	(4I10)			Output control card.
	1-10		NPFREQ	Output frequency; time history records of specified nodal and element information will be printed every NPFREQ main time steps.
	11-20		NPRU	Number of nodal time history records, i.e., displacements, velocities, or accelerations $0 \leq \text{NPRU} \leq 20$. See card Type 10.
	21-30		NPRS	Number of element time history records, i.e., stresses, strains, etc. $0 \leq \text{NPRS} \leq 20$. See card Type 11.
	31-40		NPIC	Number of complete output pictures at specified time steps; a complete picture consists

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
9 (contd.)				of all nodal and element variables for a selection of stresses, displacements, etc. $0 \leq \text{NPIC} \leq 10$. See card Type 12.
<p><u>Note:</u> (a) The plotting subroutine has been taken out from the structural dynamic program. Thus, it is suggested that NPFREQ, NPRU, NPRS, and NPIC be all set equal to zero. However, we retain the description in case we decide to put the plotting subroutine back in the program.</p>				
10	(8I10)	UOUT		NPRU cards (see card 9). Use as many cards as needed, 8 items per card. If NPRU = 0, no cards of Type 10 are used.
	1-7	N		Node number at which a specified displacement, velocity or acceleration time history is to be output, each NPFREQ cycles.
	8	L		Component number: L = 1: x-component (or rotatory component for dummy nodes). L = 2: y-component.
	9	K		Nature of record: K = 0: Displacement record. K = 1: Velocity record. K = 2: Acceleration record.
	10	M		Plot control: M = 0: No plot. M = 1: Nodal time history is plotted on printer only. M = 2: Nodal time history is plotted on printer and CALCOMP. M = 3: Nodal time history is plotted on printer and punched on cards.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
10 (contd.)				
	11-17		N	Node number.
	18		L	Component number.
	19		K	Nature of record.
	20		M	Plot control.
	etc.			

Note: This card is not needed at the present time, since the plotting subroutine is not available in this program (see note of card Type 9).

11	(8I10)		SOUT	NPRS cards (see card Type 9). Use as many cards as needed, 8 items per card, NPRS items total. If NPRS = 0, no cards of Type 11 are used.
	1-7		N	Element for which a time history is to be output.
	8-9		L	Component number (see <u>Note:</u>).
	10		K	Plot control parameter (see card Type 10).
	11-17		N	Element number.
	18-19		L	Component number.
	20		K	Plot control parameter.
	etc.			

Note: (a) The component number (card Type 11, Cols. 8-9) is used to specify an element record as follows:

Plane element (triangle continuum, quadrilateral hydrodynamic, and elastic-plastic elements):

L = 1: Extensional strain $\hat{\epsilon}_{xx}$.

L = 2: Extensional strain $\hat{\epsilon}_{yy}$.

L = 3: Engineering shear strain $2\hat{\epsilon}_{xy}$.

L = 4: Hoop strain $\epsilon_{\theta\theta}$ (for axisymmetric problems).

<u>Card</u> <u>Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN</u> <u>Name</u>	<u>Description</u>
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11
(contd.)

L = 5 to 8: Stresses σ_x , σ_y , σ_{xy} and $\sigma_{\theta\theta}$ in the same order as the stresses of the flexural element.

Flexural element (beam and shell elements):

Since the integration for the nodal forces uses two points along the length and five points through the depth of an element. Figure 68 shows component numbers used to specify the element records. There are 50 records available for each flexural element.

(b) Card Type 11 is not needed at the present time (see note of card Type 9).

12	(2I10)		NPIC cards (see card Type 9). Use a number of cards of Type 12 equal to NPIC.
1-10		NPOUT	Time step at which a complete output as specified by KONT is desired.
11-20		KONT	<p>KONT = 1: Output displacements at all nodes.</p> <p>KONT = 2: Output above and coordinates of deformed structure (output of dummy nodes is meaningless for this card).</p> <p>KONT = 3: Output above plus velocities and accelerations at all nodes.</p> <p>KONT = 4: Output above plus all element information--stresses, strains, etc.</p> <p>KONT = 5: Same printed output as KONT = 2; in addition, CALCOMP plot of the deformed structure.</p> <p>KONT = 6: Same printed output as KONT = 3; in addition, CALCOMP plot of the deformed structure.</p>

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
12 (contd.)				KONT = 7: Same printed output as KONT = 4; in addition, CALCOMP plot of the deformed structure.
<u>Note:</u> Card Type 12 is not needed at the present time (see note of card Type 9).				
13	(6I5)			Load line card description (see NPRES on card Type 2).
	1-5		IDUM	Load line number.
	6-10		NDNOD	Number of points on load line (usually the number of "real" nodes on beam or shell).
	11-15		IVOL(I)	IVOL(I) = 1: Load line is part of an axisymmetric surface. IVOL(I) = 2: Load line is part of a plane surface (not available). I is the internal load number.
	16-20		INT1	Internal increment between <u>points</u> on load line for automatic load line point generation. If INT1 > 0, the load line point is generated by adding INT1 to the previous point number (NDNOD - 1) times starting with the first point specified on card Type 14. Set INT1 = 0 if automatic generation is not desired. Usually INT1 = 1.
	21-25		INT2	Internal spacing between <u>nodes</u> on load line for automatic load line node generation. If INT2 > 0, the load line node is generated by adding <u>INT2</u> to the previous node number (NDNOD - 1) times starting with the first node specified on card Type 15. Set INT2 = 0, if automatic generation is not desired. Usually INT2 = 1.

<u>Card Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN Name</u>	<u>Description</u>
13 (contd.)				
	26-30		INT3	Internal spacing between segments on load line for automatic load line segments generation. If $INT3 > 0$, the load line segment generated by adding $INT3$ to the previous segment number ($NDNOD - 2$) times starting with the first segment specified on card Type 16. Set $INT3 = 0$, if automatic generation is not desired. Usually $INT3 = 1$.
14		(I6I5)		
	1-5	KPRES(J)		Point on the load line; if all points can
	6-10	KPRES(J+1)		be generated from $KPRES(i)$ by incrementing
	etc.	J=1, NDNOD		by $INT1$, only $KPRES(i)$ need be included. Total number of points on all load lines is limited to 100.
15		(I6I5)		
	1-5	KNODE(J)		Nodes on the load line; if all nodes can
	6-10	KNODE(J)		be generated from $KNODE(i)$ by increment-
	etc.	J=1, NDNOD		ing by $INT2$, only $KNODE(i)$ need be included. Total number of nodes on all load lines is limited to 100.
16		(I6I5)		
	1-5	KSG(J)		Segments on the load line; if all segments
	6-10	J=1, NDNOD		can be generated from $KSG(i)$ by increment-
				ing by $INT3$, only $KSG(i)$ need be included. Total number of segments on all load lines is limited to 99.
17		(3I5)		Segment/point connectivity cards.
	1-5	LM		Segment number.

<u>Card</u> <u>Type</u>	<u>Columns</u>	<u>Format</u>	<u>FORTRAN</u> <u>Name</u>	<u>Description</u>
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17

(contd.)

6-10		IY(1,LM)	Point i of segment.
11-15		IY(2,LM)	Point j of segment.

- Note: (a) Connectivity cards for segments which can be generated by adding one to all numbers of the previous segment need not be included. The data for these segments will be automatically generated. However, if this is done, the connectivity card for the last segment must be included.
- (b) Card of Types 13 to 17 are to be used in sets, one set for each load line. Total number of sets is NPRES; $0 < \text{NPRES} \leq 10$.

VII. CONCLUSIONS

The ICECO-CEL (ICECO-III) Code is capable of providing accurate analysis of primary containment response to an HCDA. It can be used to analyze various transient phenomena, such as the wave propagation, slug impact, expanding gas bubble, fluid-structure interaction, containment response, sodium spillage, liquid cavitation, and the above-core hydrodynamics. The code has several special features: (1) It can provide a stable solution throughout the entire excursion without using any complementary mechanisms such as artificial viscosities, rezoning, mesh stabilization and regularization, as well as prescribing grid motion. This is a deciding advantage for applying the code to the parametric studies and production runs. (2) It treats complex fluid motion in the complicated LMFBR containment and yet still maintains the computational efficiency. The computing time for analyzing the response of a typical LMFBR given in Sect. III.B. is about 20 minutes on an IBM 370/195, which is comparable to the conventional explicit numerical technique. (3) It has an accurate scheme for treating highly contorted coolant surfaces. Thus, the collapsing of the core-gas bubble at the early stage of excursion can be avoided and numerical calculations can be carried out continuously without any interruption. (4) The developed algorithm has the capability of treating flow through coolant passageways of the upper internal structure located in the above-core region. Thus, it can give an accurate estimate of the mitigating effect of the upper internals on the slug-impact loads and the containment response, which is of significance in the safety analysis of LMFBRs. (5) It treats the sodium spillage through penetration openings on the reactor cover and the ruptured seal at the vessel-cover junction. This is not only important to the primary containment integrity, but is essential to the analysis of transport of radiological material to the secondary containment.

The accuracy of the code solutions have been validated against available experimental data, such as those obtained from the ANL bubble experiment, SRI piping test, SNR-300 breeder reactor, UKAEA-JRC COVA experiment, and SRI complex vessel test SM-2. The good agreement between the code predictions and the recorded data demonstrates that the ICECO-CEL code is an accurate and useful tool for the LMFBR safety analysis.

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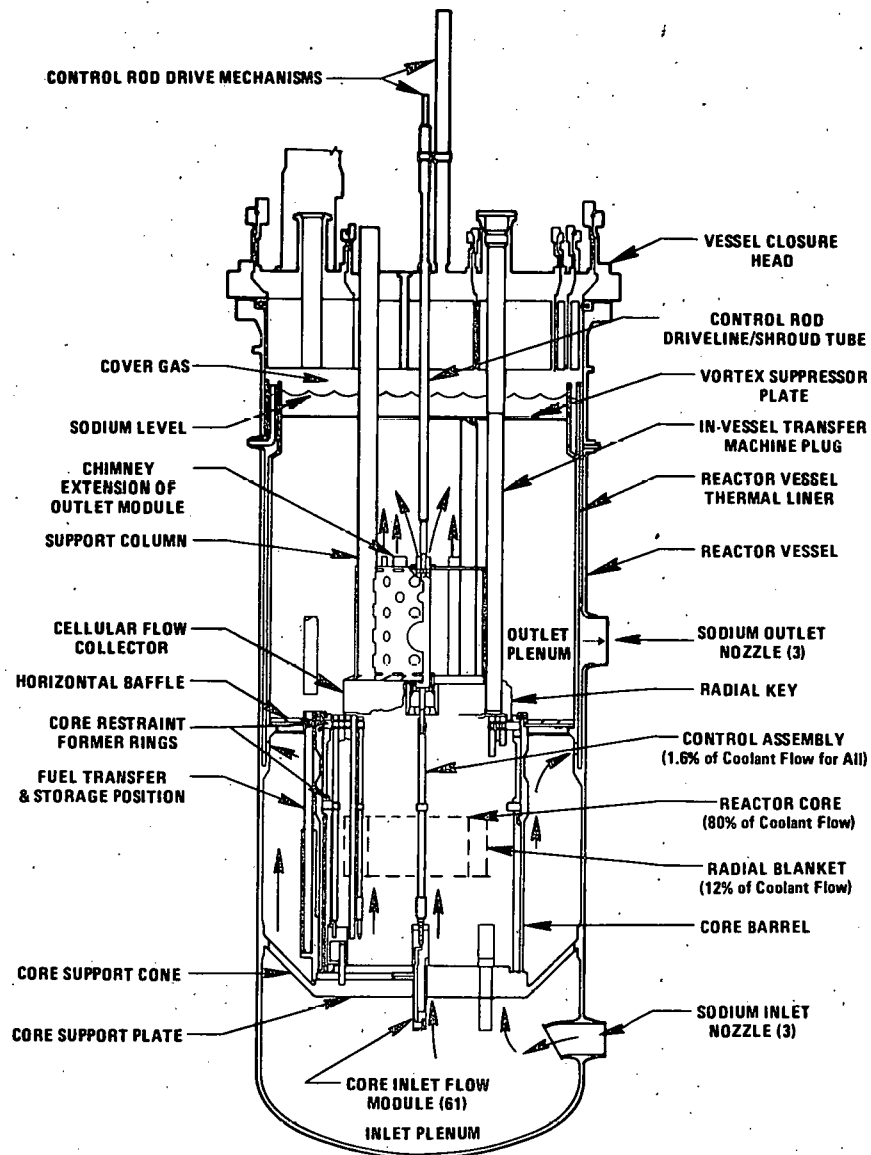


Fig. 1. Typical Configuration of an LMFBR

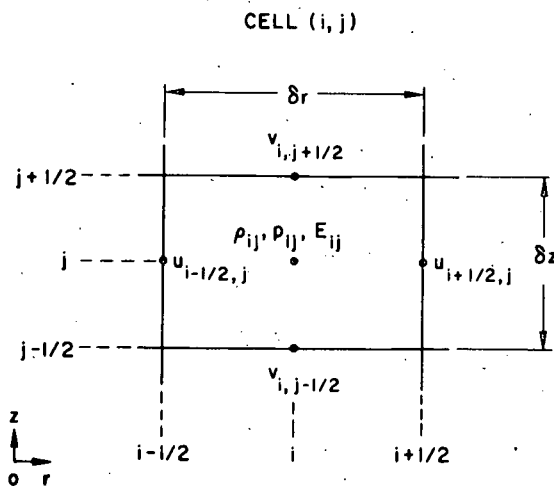


Fig. 2

The Location of the Cell Variables
in an Eulerian Computational Cell

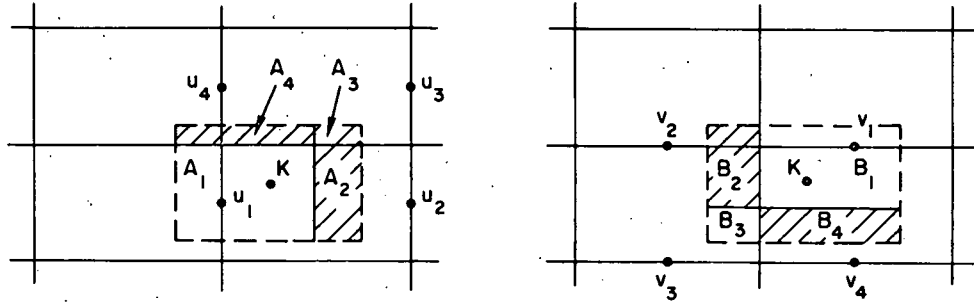


Fig. 3. Linear Interpolation for U_K and V_K with Position of K^{th} Particle as Shown

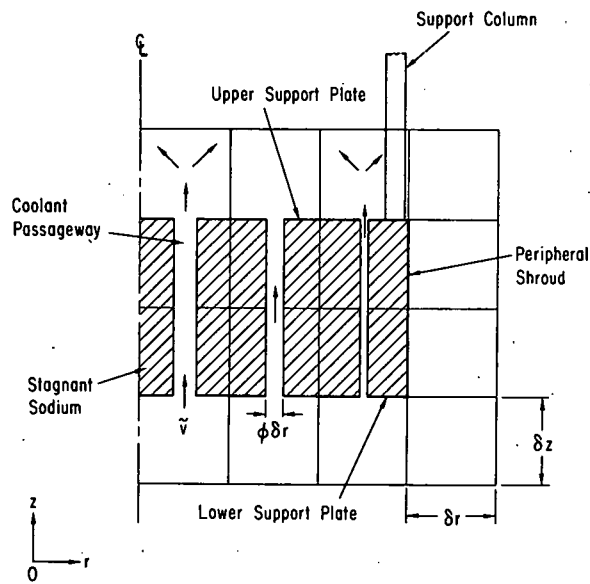
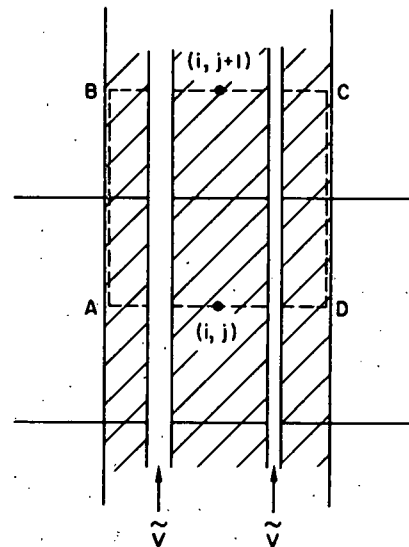


Fig. 4

Eulerian Computing Mesh for Upper Internal Structure

Fig. 5

Control Volume for Derivation of Axial Momentum Equation Inside Coolant Passageways



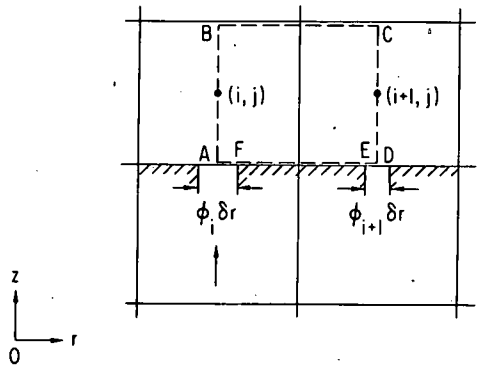


Fig. 6. Control Volume for Derivation of Radial Momentum Equation Above the Perforated Structure

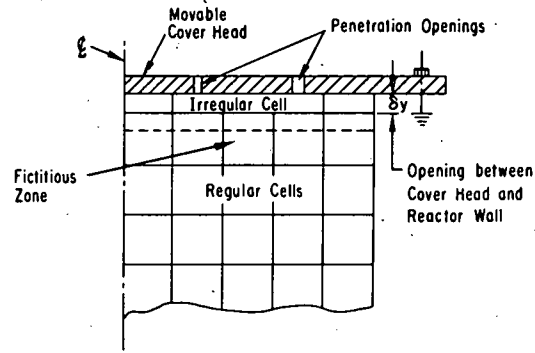


Fig. 7. Reactor Cover with Penetration Openings

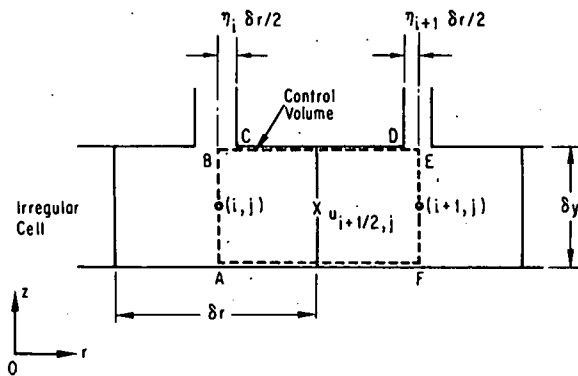


Fig. 8. Control Volume for Radial Momentum Equation Underneath the Cover

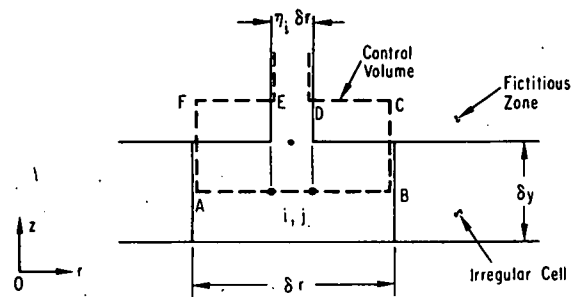


Fig. 9. Control Volume for Axial Momentum Equation Underneath the Cover

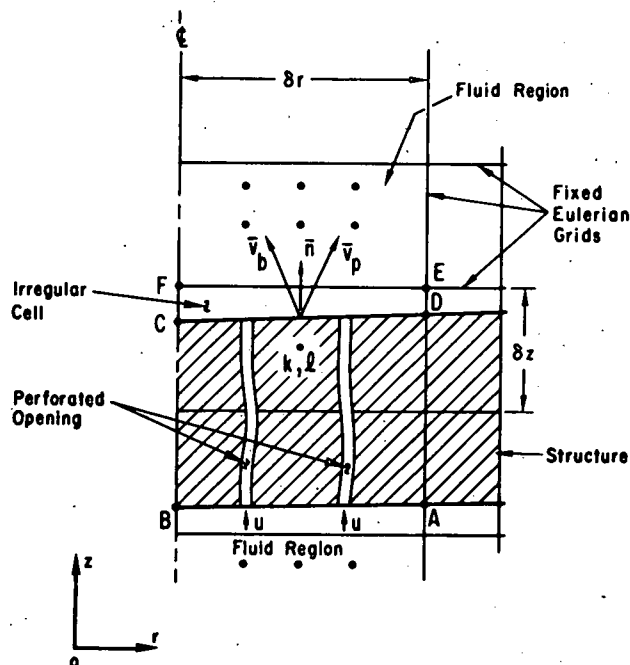


Fig. 10

Irregular Cell (k, l) Containing Deformable Structure with Perforated Openings

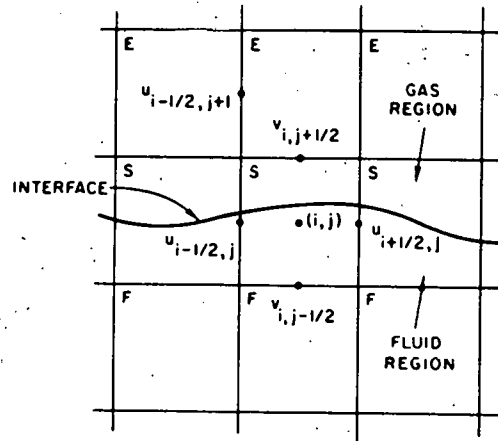
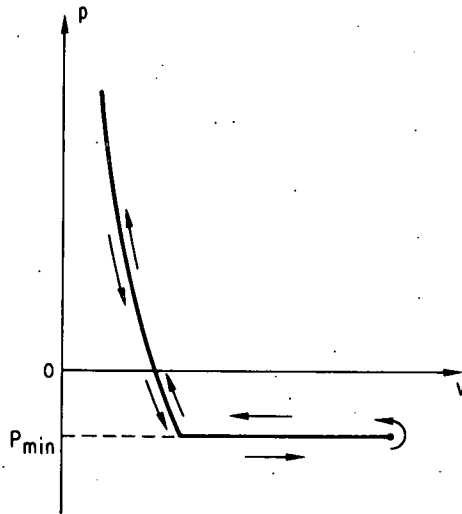


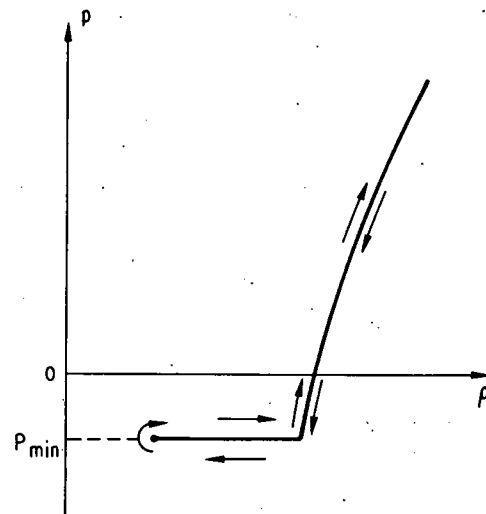
Fig. 11

Velocity Calculation in Vicinity of a Surface Cell

E: EMPTY CELL
S: SURFACE CELL
F: FULL CELL



(a)



(b)

Fig. 12. Conventional Equation of State for Cavitated Fluid

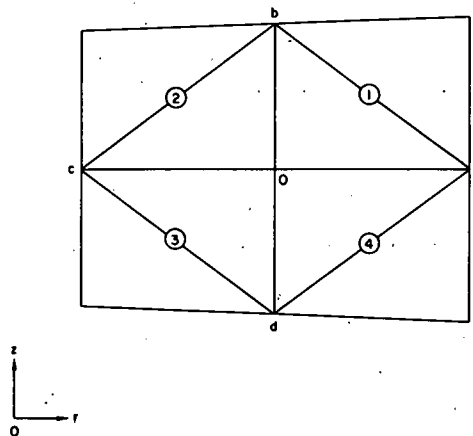


Fig. 13. Zone Configuration for Finite-Difference Equations

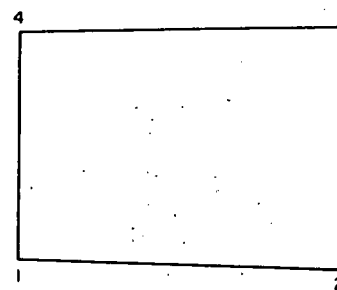


Fig. 14. Numbering Scheme for Calculating Node Forces

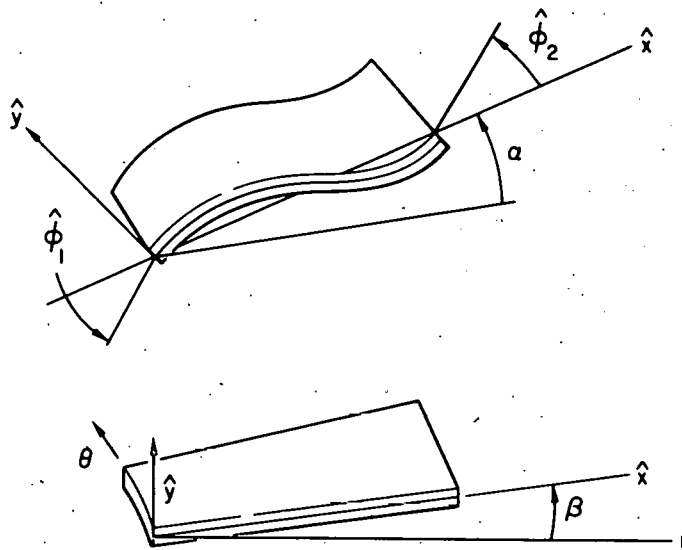


Fig. 15

Axisymmetric Shell Element

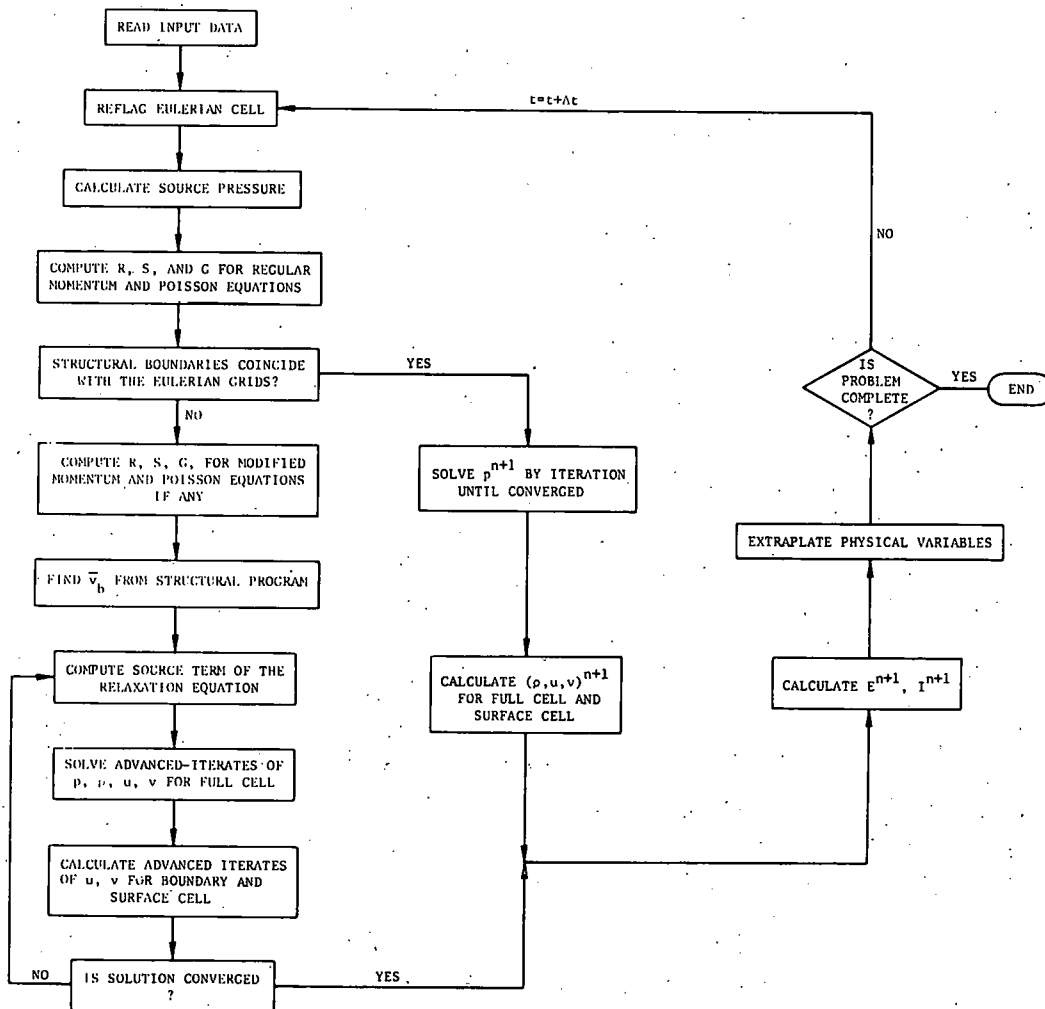


Fig. 16. Flow Chart Representing the Computational Procedure

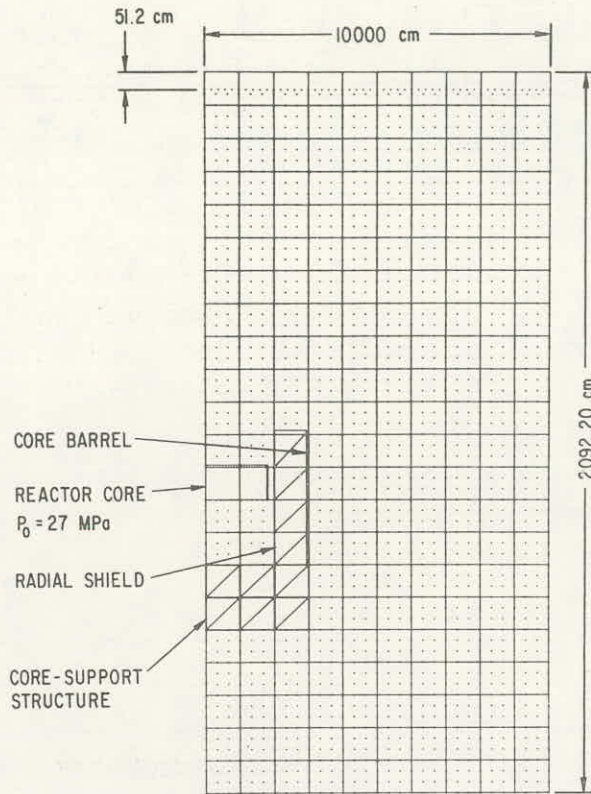


Fig. 17
Initial Configuration of
the Pool-Type LMFBR

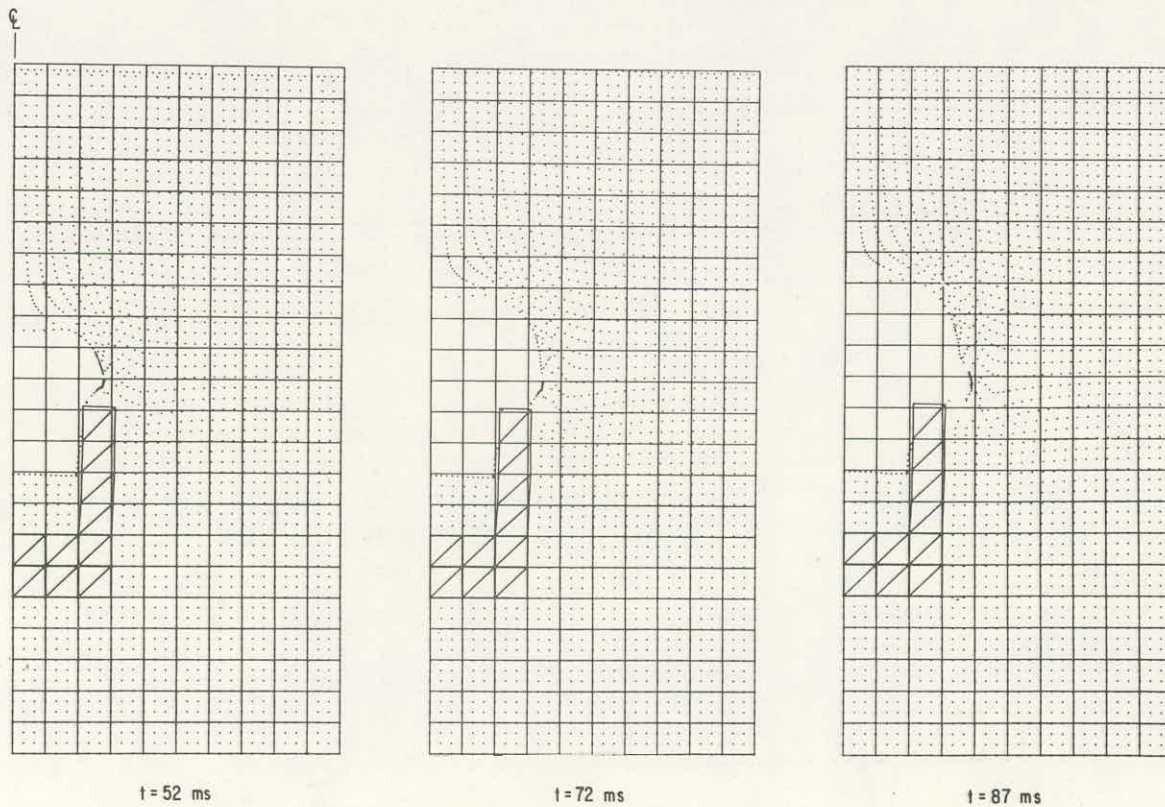


Fig. 18. Reactor Configurations at Several Different Times

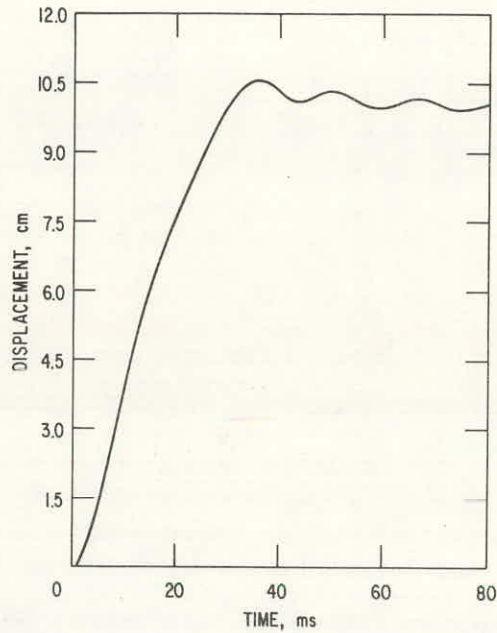


Fig. 19

Radial Displacement History of the
Upper End of the Core Barrel

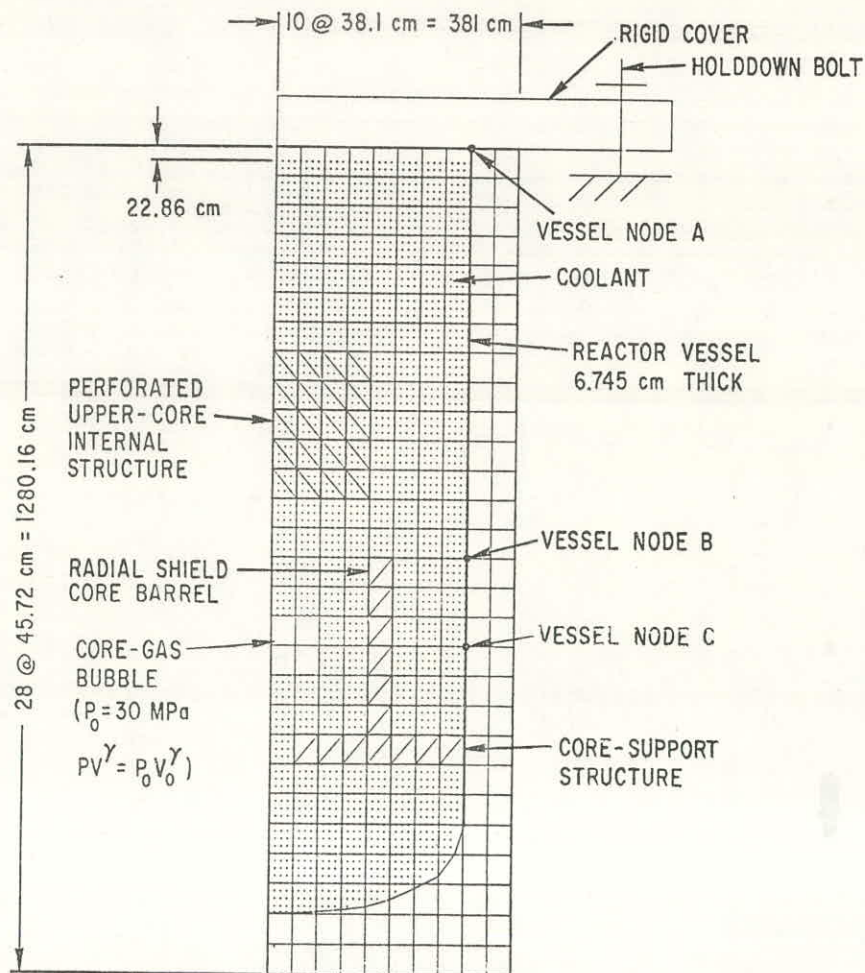


Fig. 20. Initial Reactor Configuration with the Upper Internal Structure

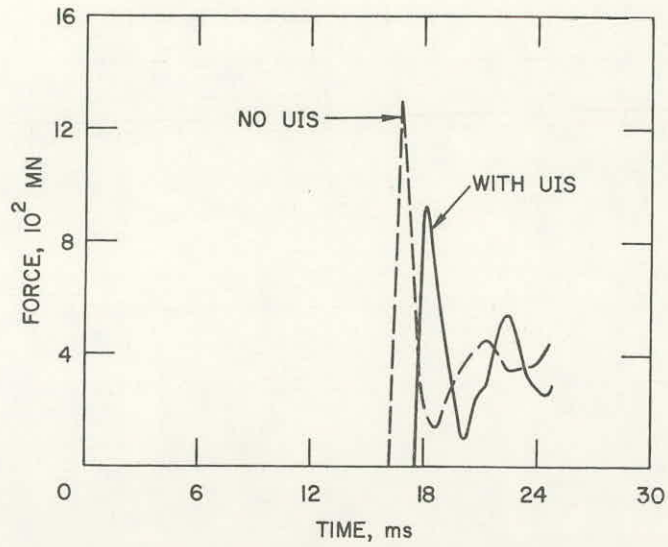


Fig. 21
Comparison of Total Force
on the Reactor Cover

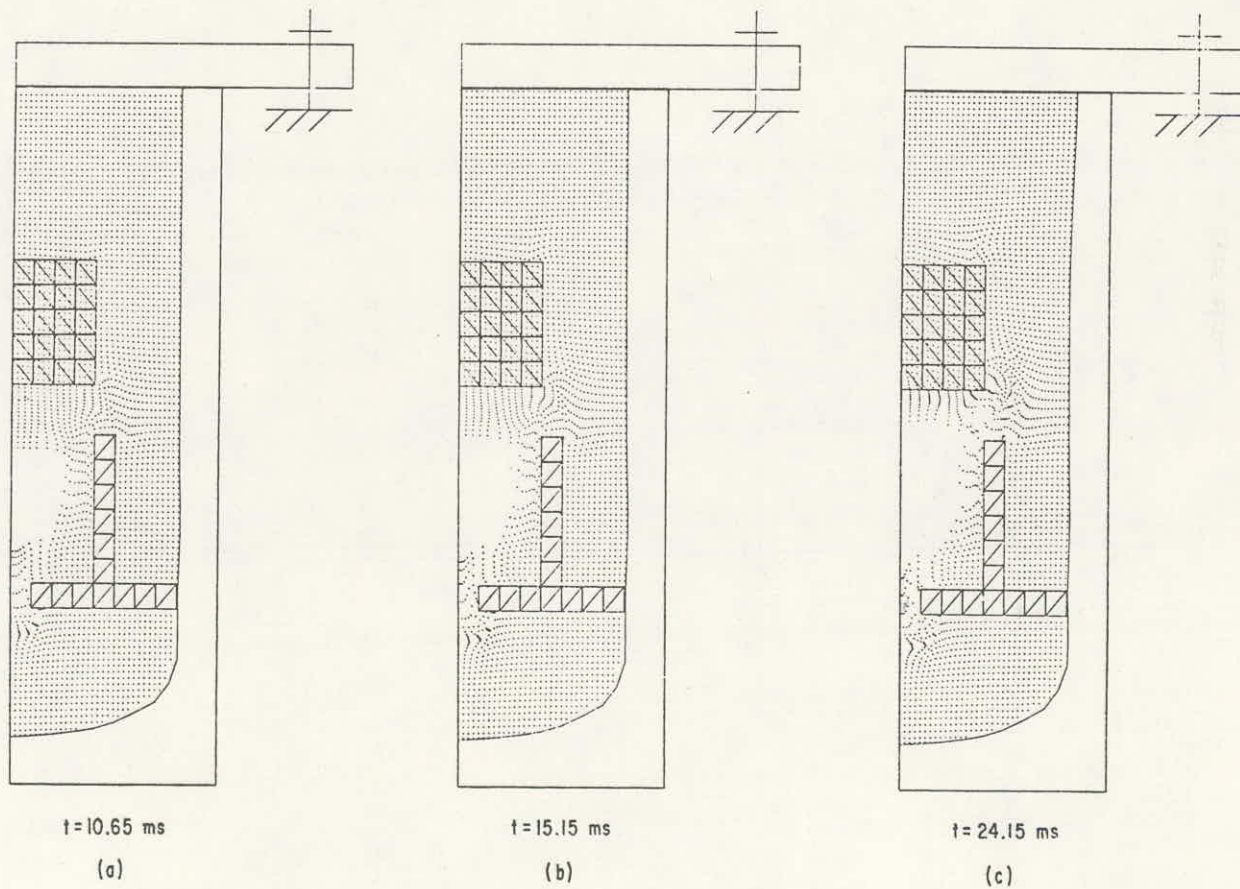


Fig. 22. Reactor Configurations at Three Different Times (Upper Internal Modeled as Perforated Structure)

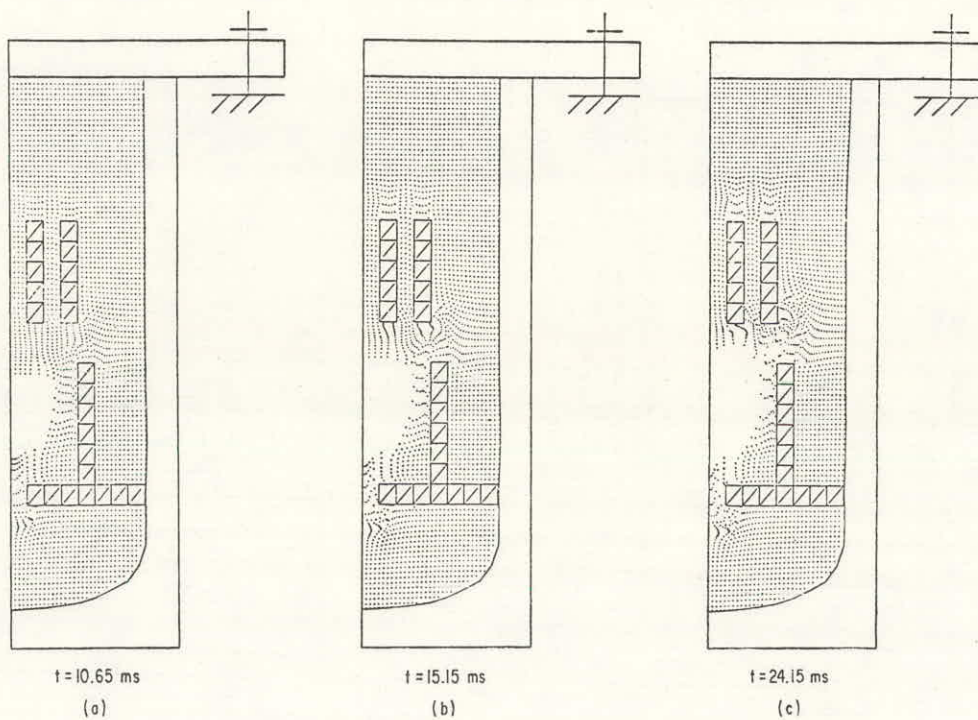


Fig. 23. Reactor Configurations at Three Different Times
(Upper Internal Modeled by Rigid Obstacles)

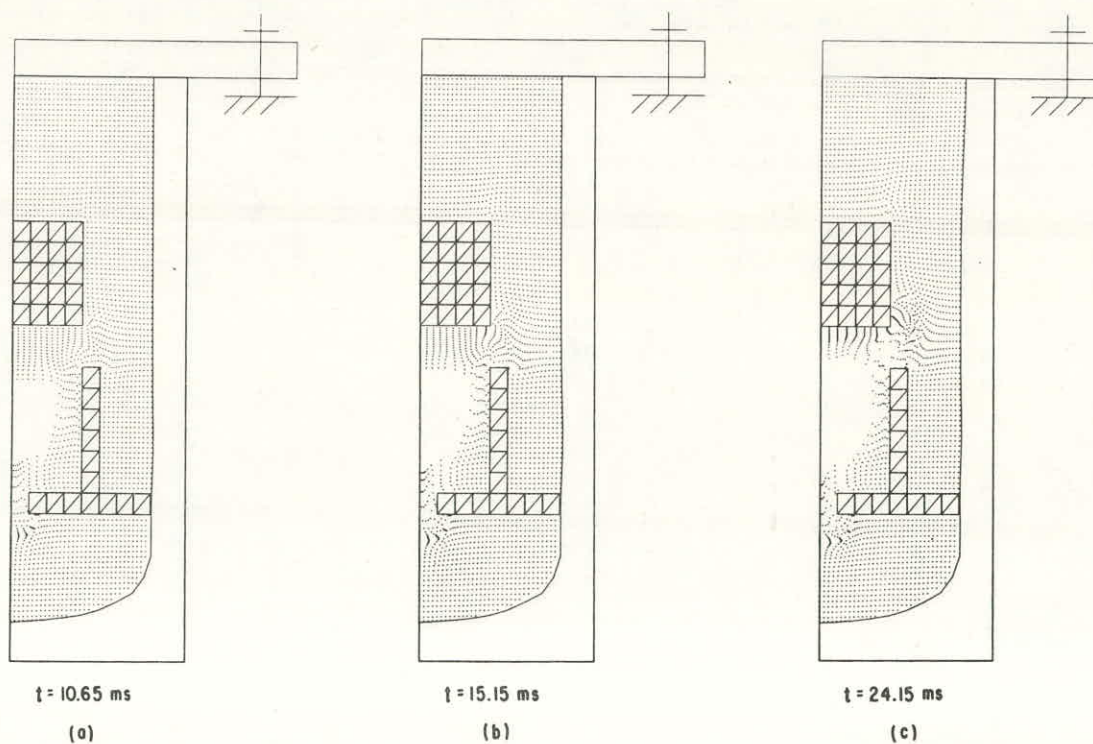


Fig. 24. Reactor Configurations at Three Different Times (UIS Passageways Were Plugged)

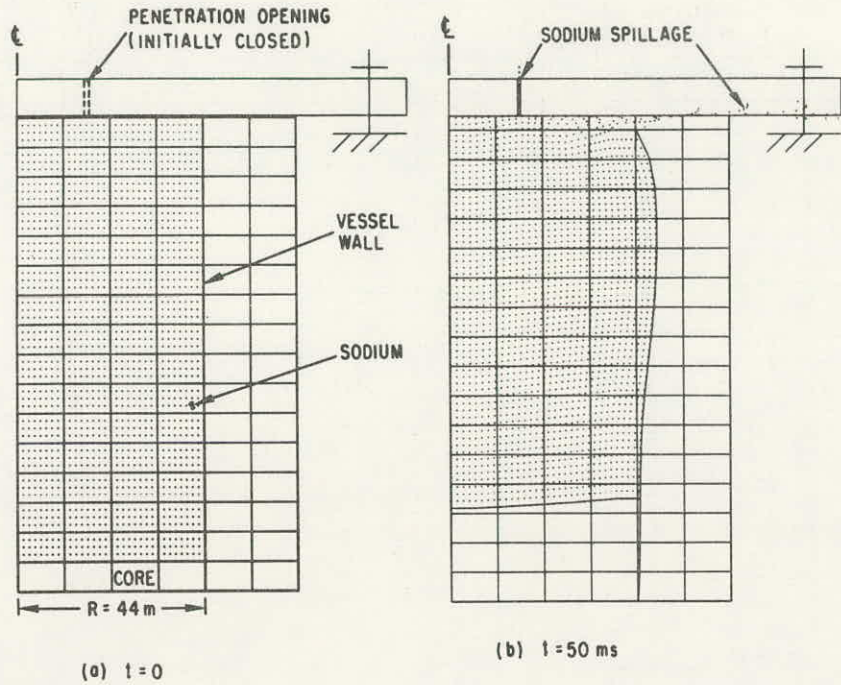


Fig. 25. (a) Configuration of a Simplified Reactor (Top Penetration Initially Closed), (b) Configuration of 50 ms Showing Coolant Spillage from Top Penetration and from Vessel-Heat Junction

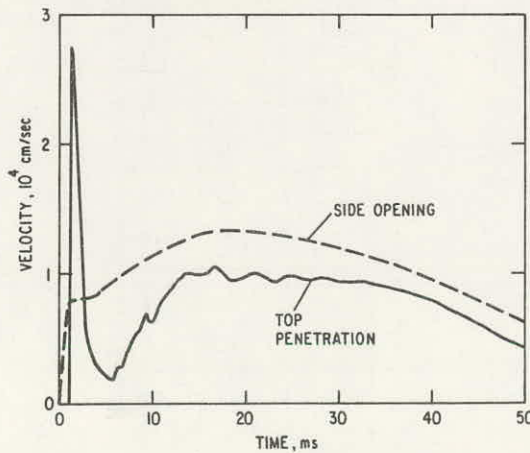
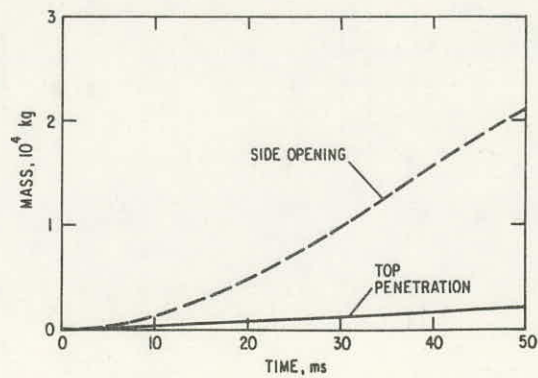


Fig. 26

Sodium Velocities at Top Penetration and Side Opening

Fig. 27
Total Spillage from Top Penetration and Side Opening



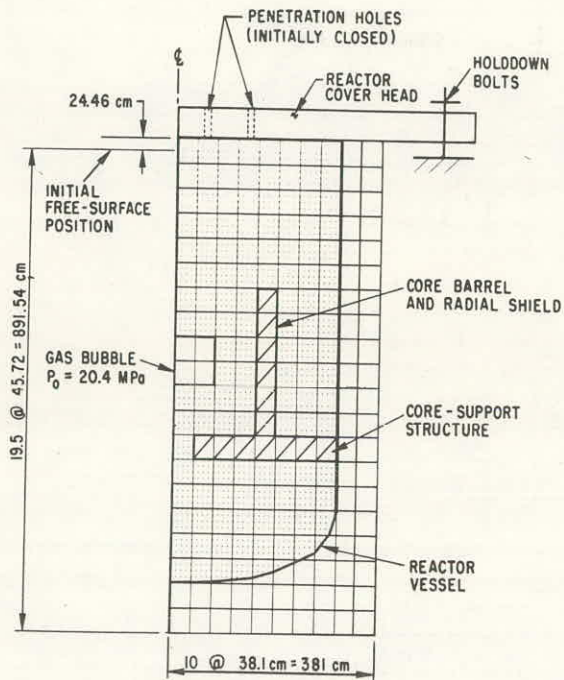


Fig. 28

Initial Configuration Used for Containment and Sodium-Spillage Analysis

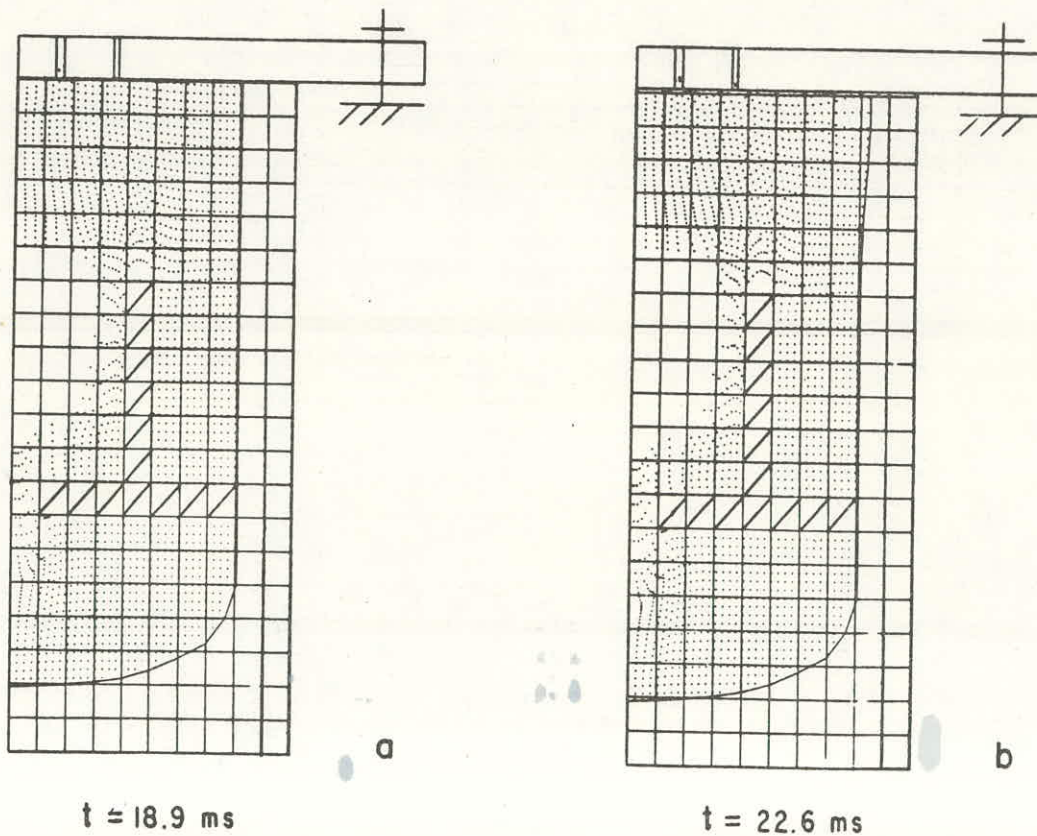


Fig. 29. Reactor Configurations at Two Different Times

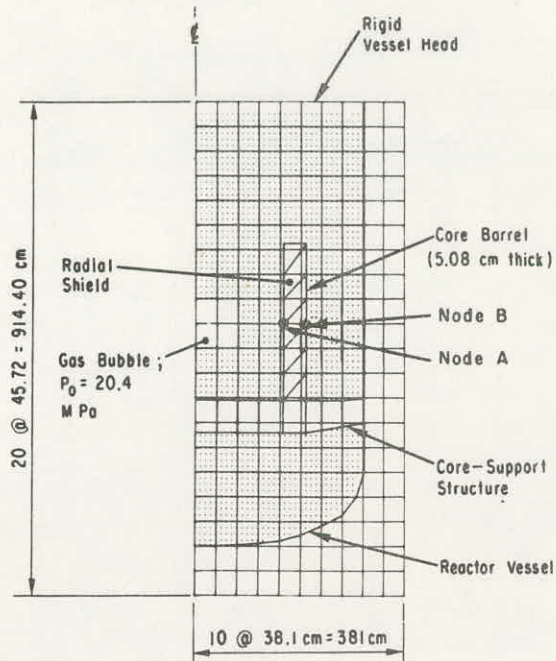


Fig. 30
Initial Configuration Used in the Analysis

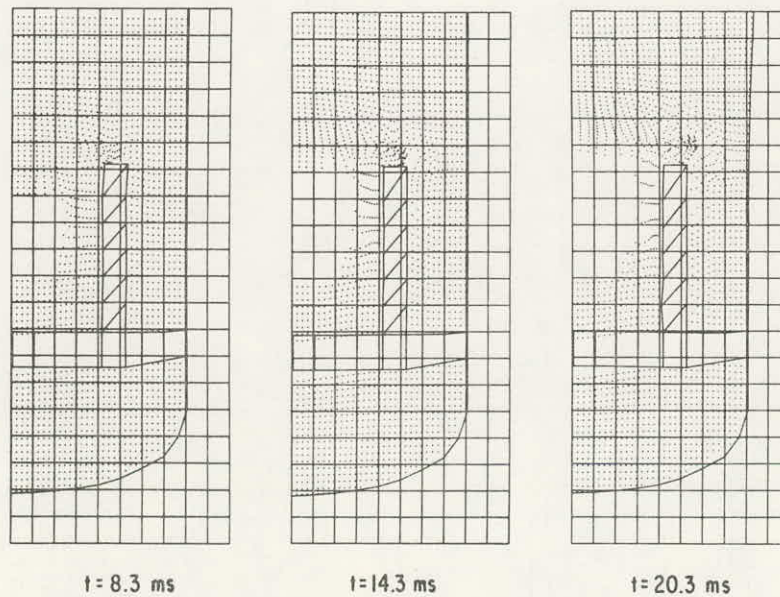
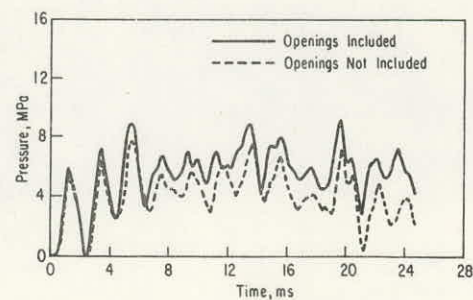


Fig. 31. Configurations at Various Times

Fig. 32
Pressure Loadings in the Reactor Lower Plenum



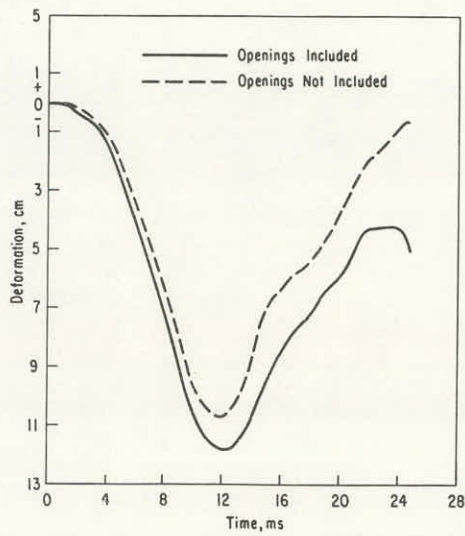


Fig. 33
Axial Deformation of Bottom Vessel

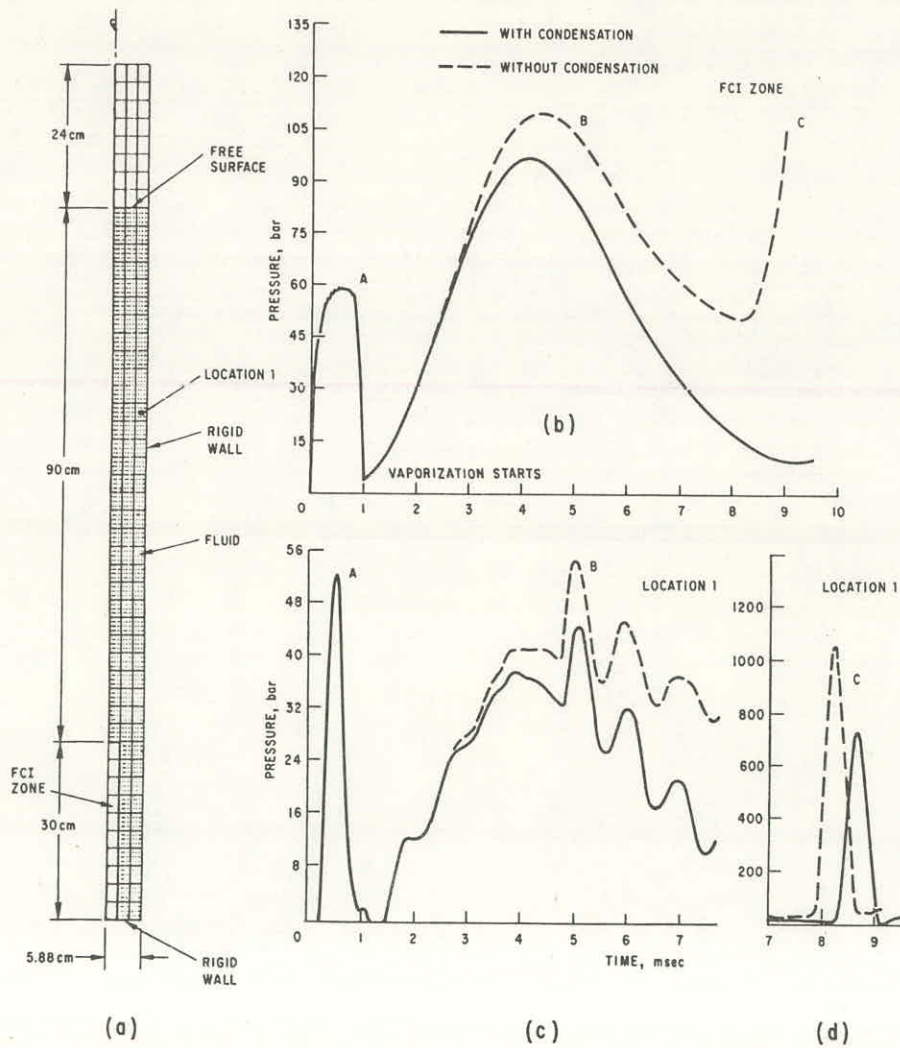


Fig. 34. Model of a Single Subassembly and Pressure Histories

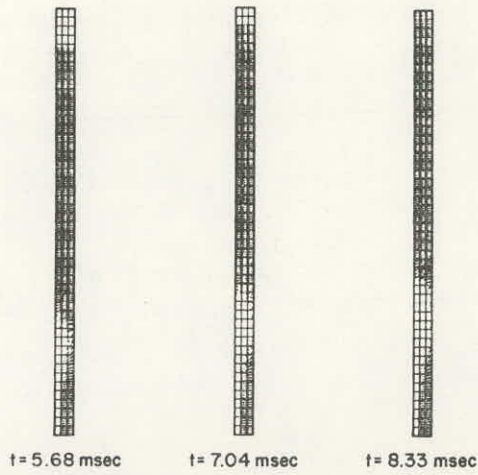


Fig. 35

Marker-Particle Configurations (with Condensation)

Fig. 36

Schematic of Shock Tube (not to Scale)

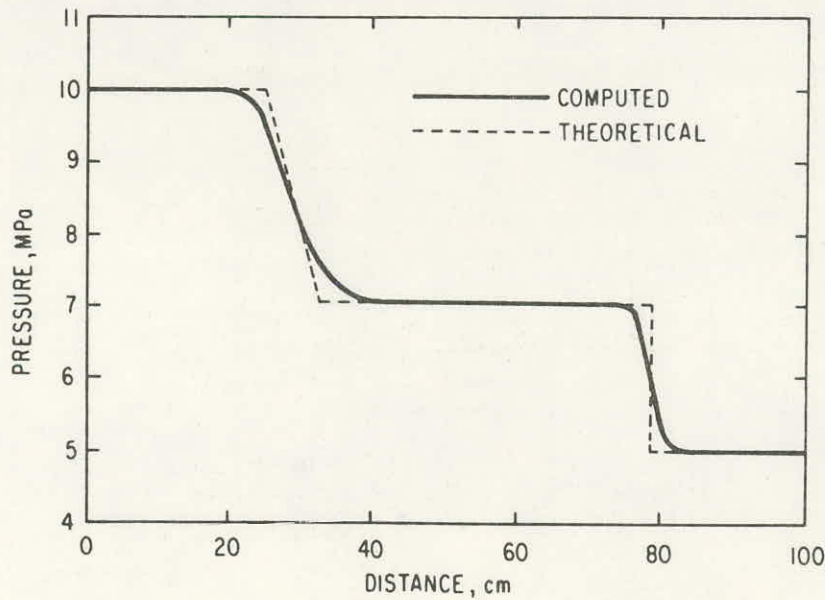
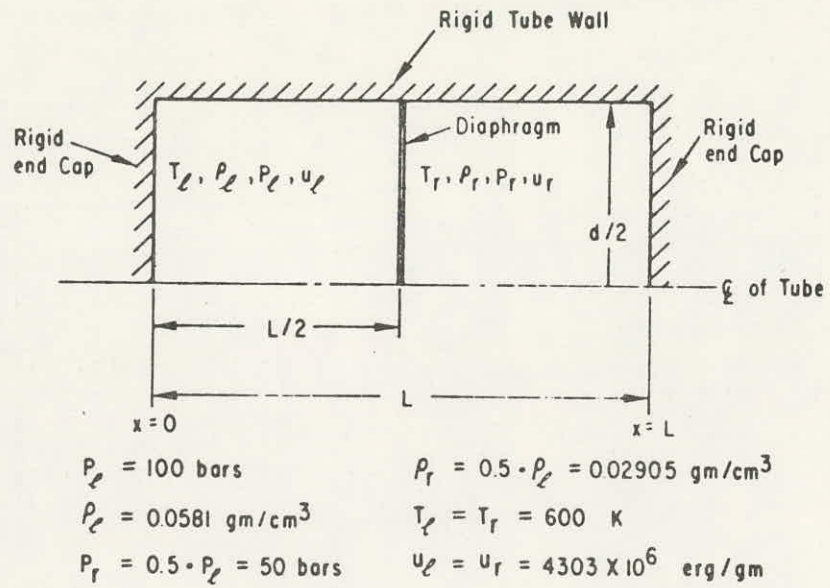


Fig. 37

Pressure Profile at $500 \mu\text{s}$

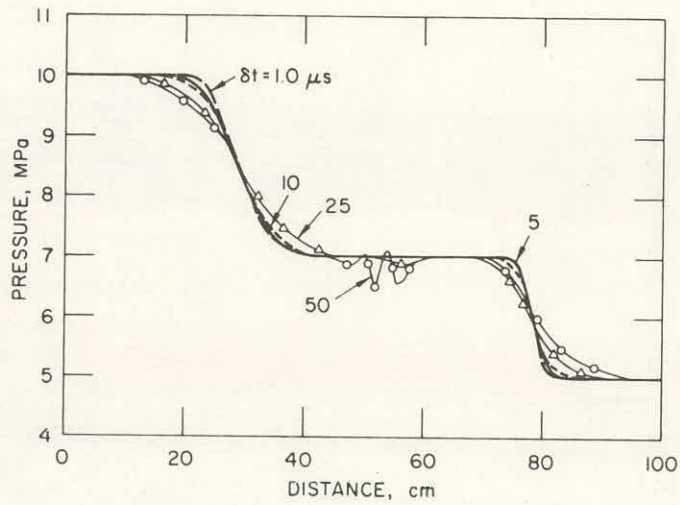
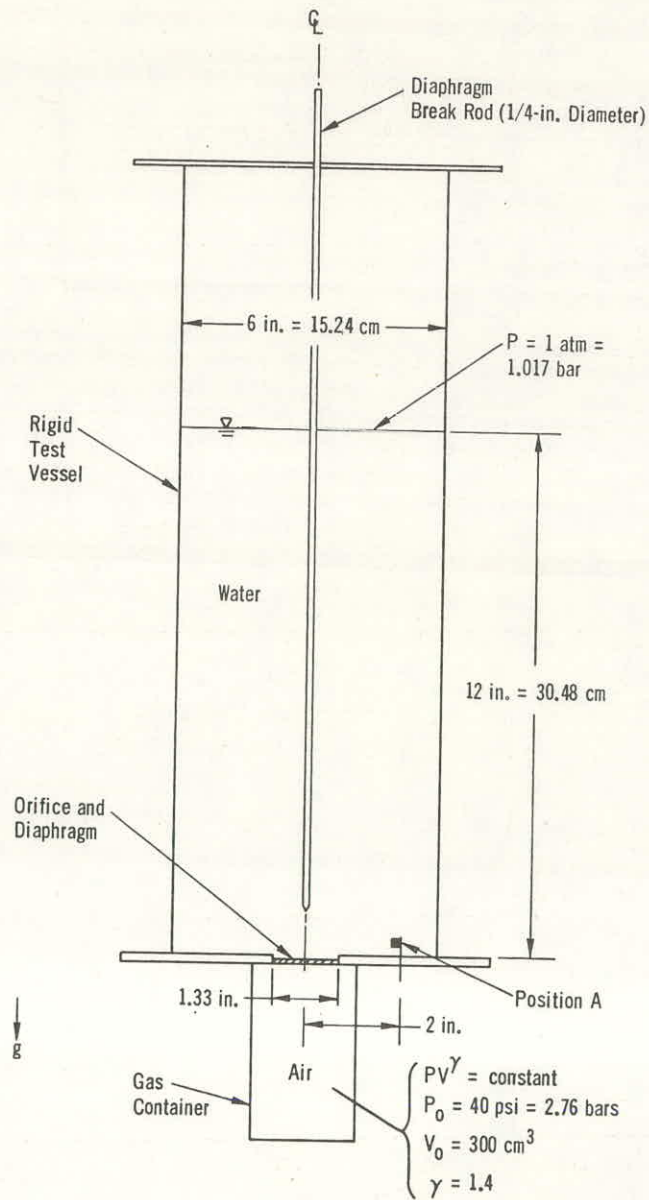


Fig. 38

Pressure Profiles at $500 \mu s$
for Various Time Steps

Fig. 39
Simplified Test Apparatus
for Bubble Motion



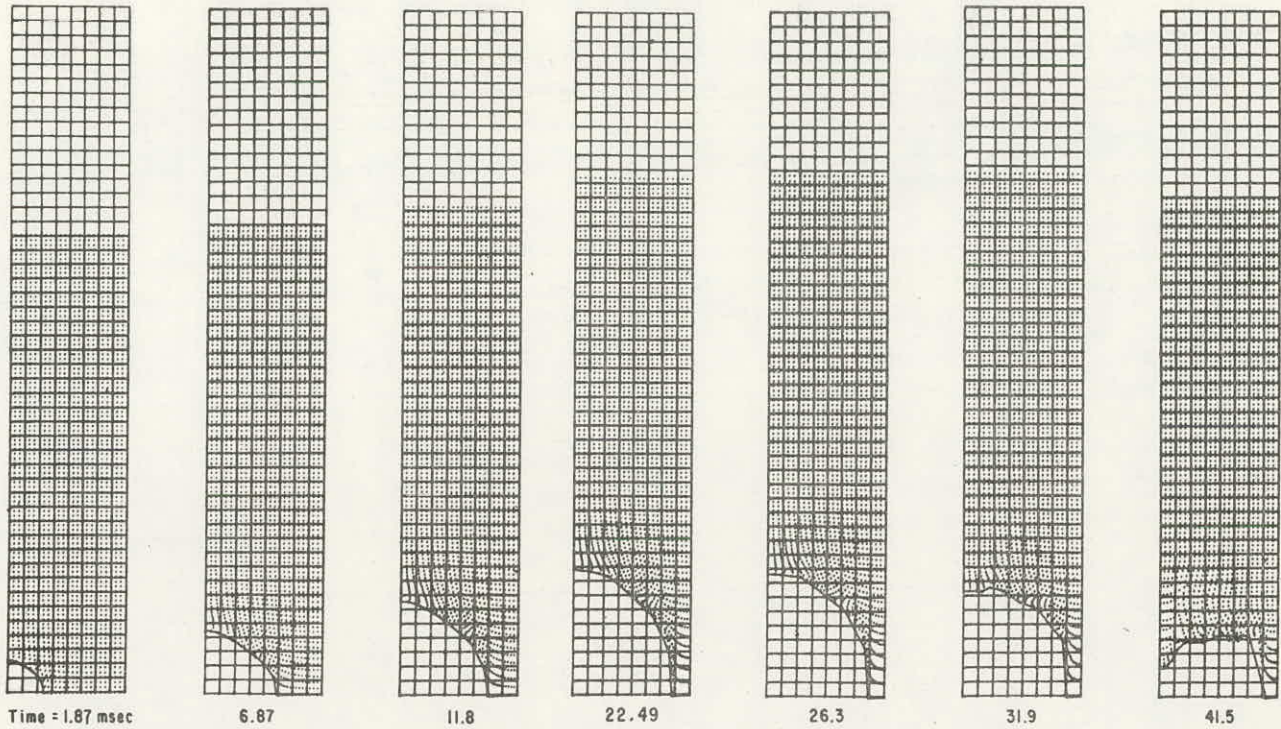


Fig. 40. Bubble and Coolant Configurations at Seven Different Times

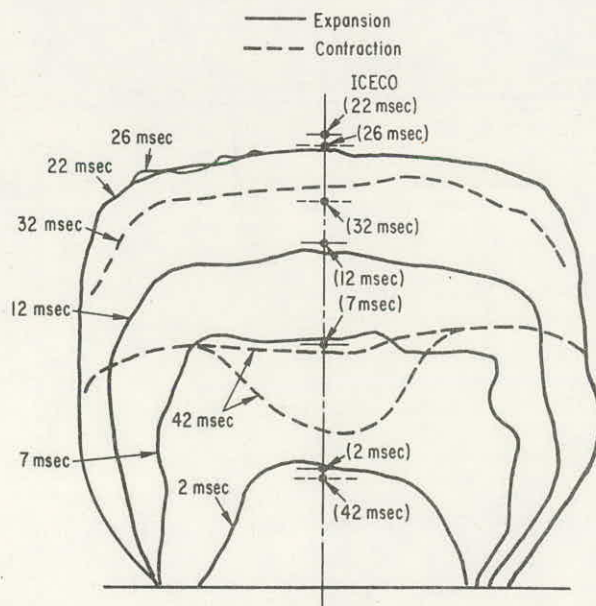


Fig. 41. Experimental Bubble Configurations at Seven Different Times

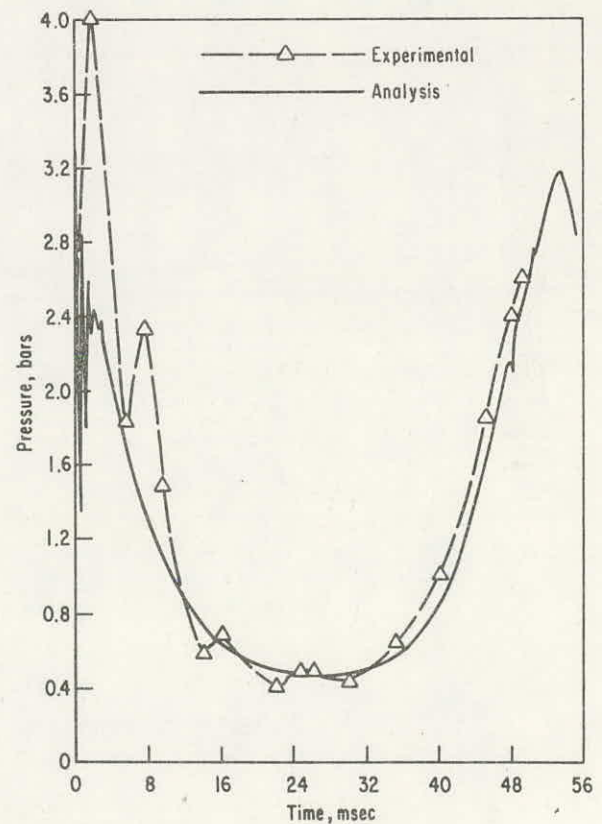


Fig. 42. Pressure Histories at Location A

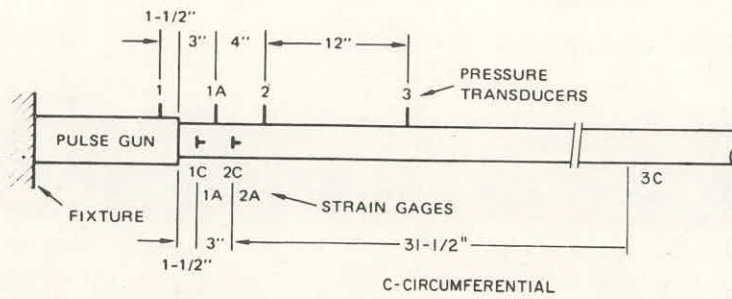


Fig. 43. Configuration of the Elastic-Plastic Pipe

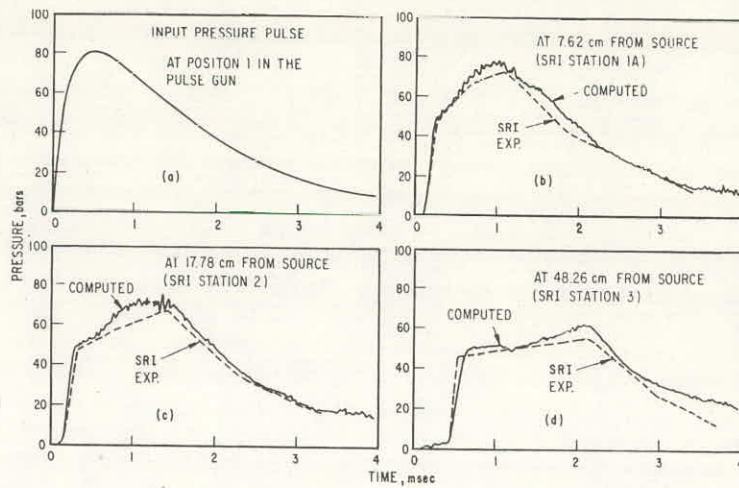


Fig. 44. Pressure Histories at Various Locations in the Elastic-Plastic Pipe

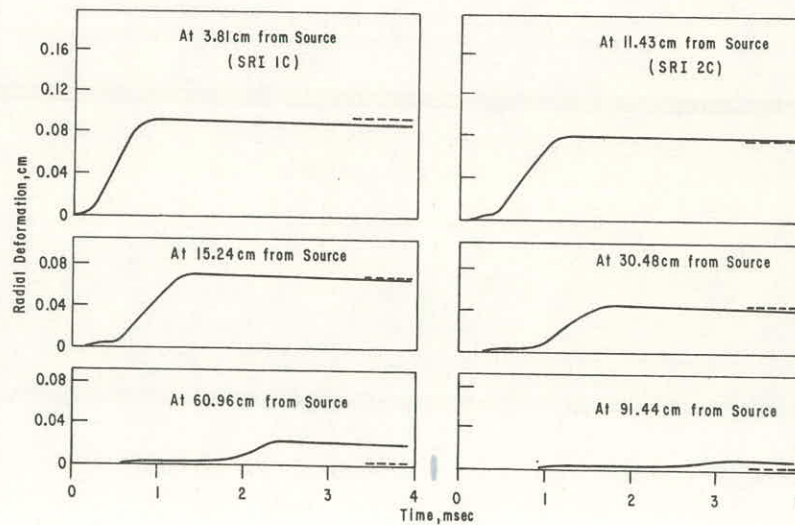


Fig. 45. Radial Deformations at Six Positions (— ICECO; --- SRI Test)

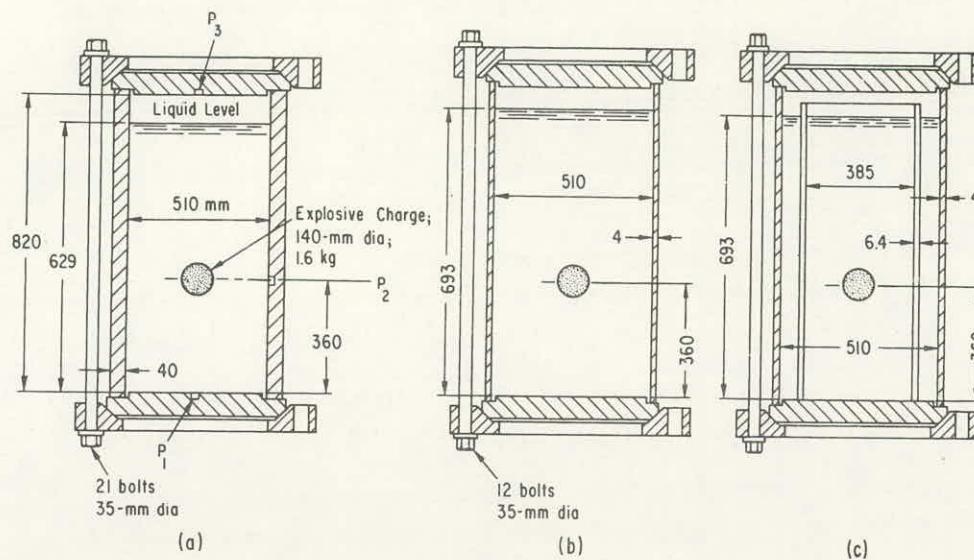


Fig. 46. Test Configurations of the SNR-300 Reactor Models

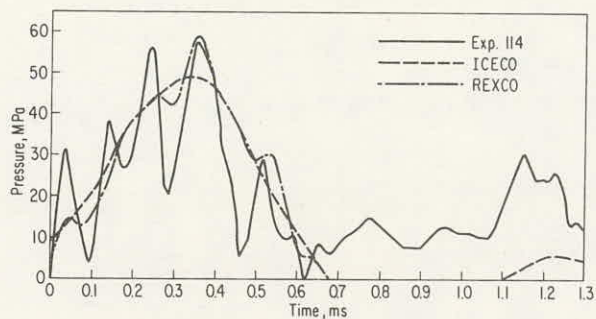
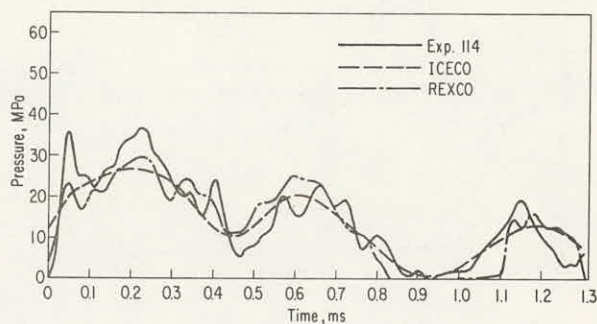
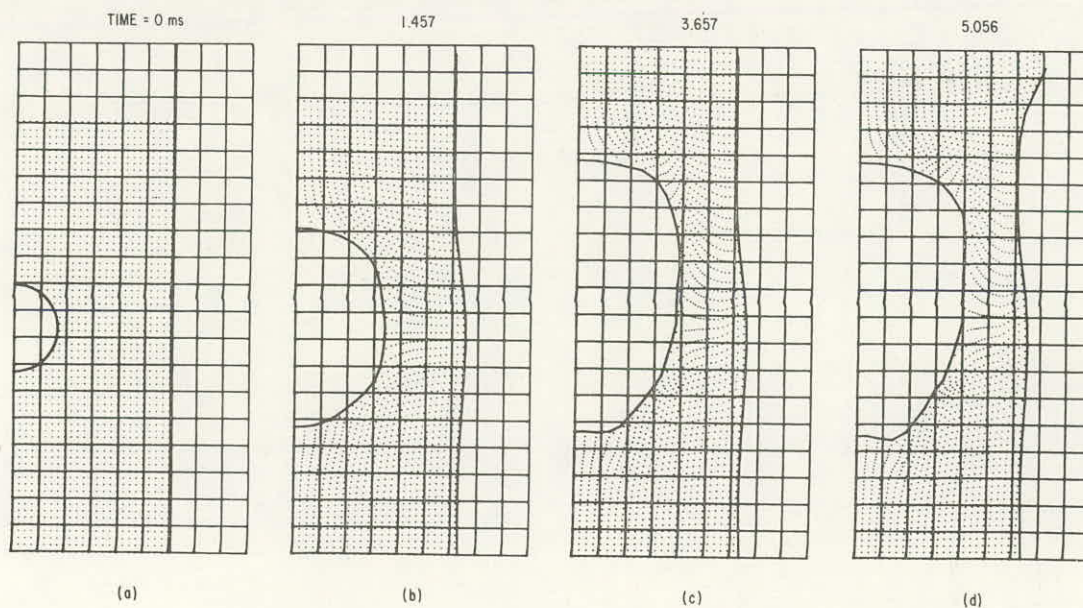
Fig. 47. Comparison of Pressure at $r = 10$ cm and $z = 0$. (Delay of 0.2 ms).Fig. 48. Comparison of Pressure at $r = 25.5$ cm and $z = 36$ cm. (Delay of 0.12 cm).

Fig. 49. Reactor Configurations at Three Different Times (No Spillage)

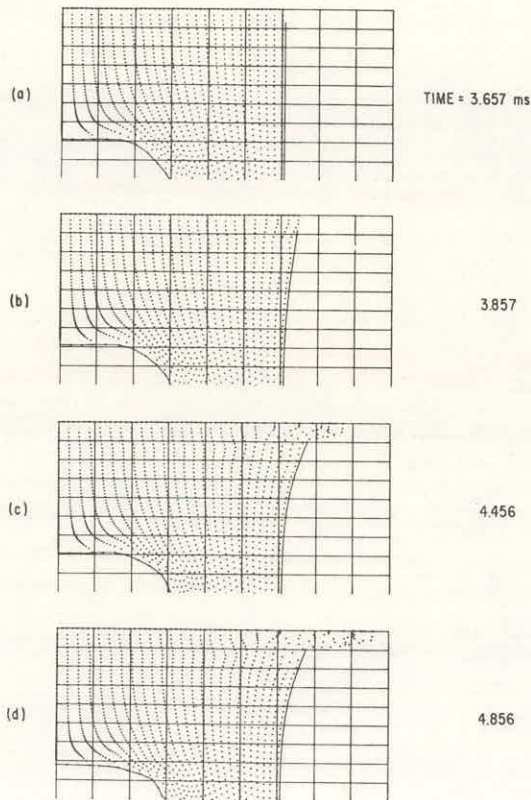


Fig. 50

Reactor Configurations at Three
Different Times (with Spillage)

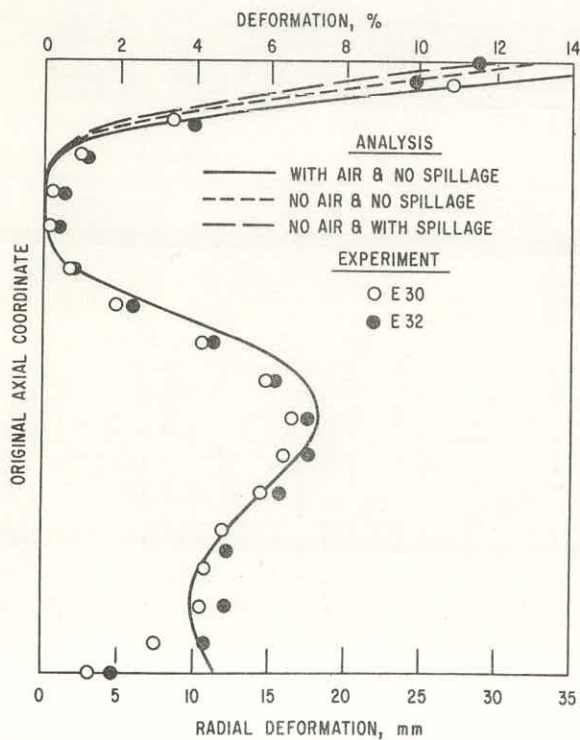


Fig. 51. Comparison of the Permanent Vessel
Deformations (Thin-Vessel Model)

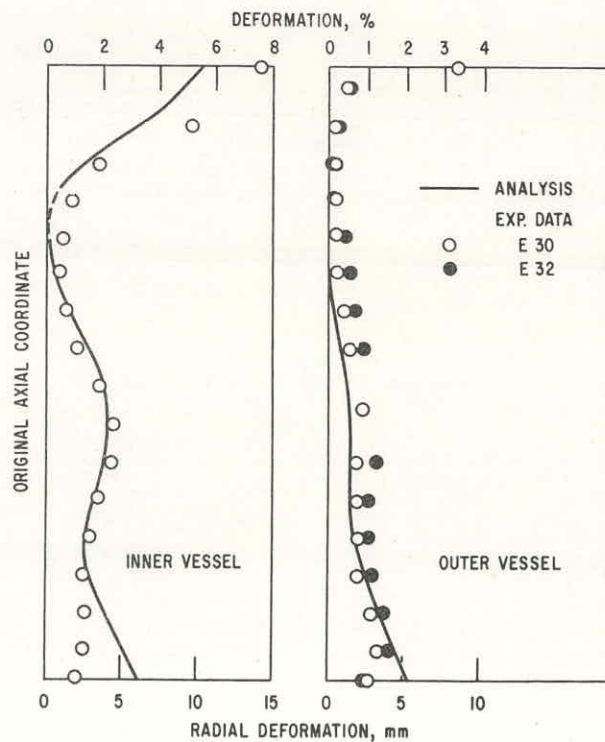
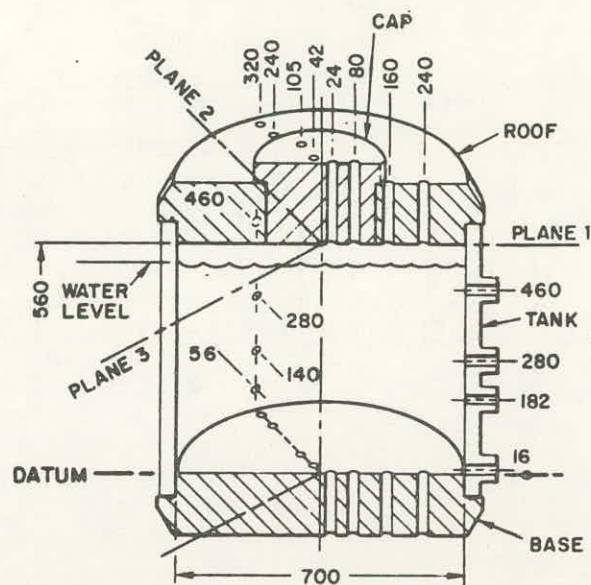
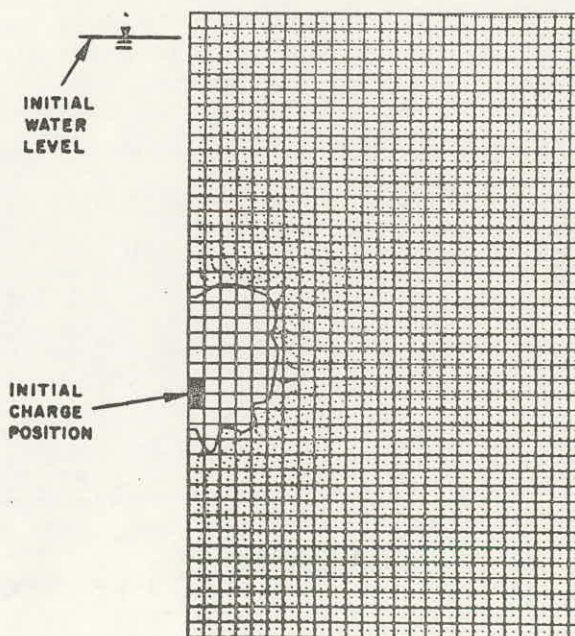
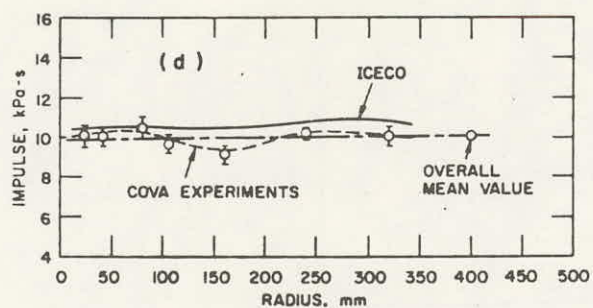
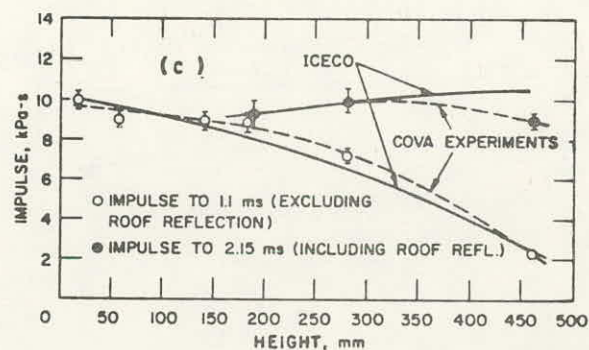
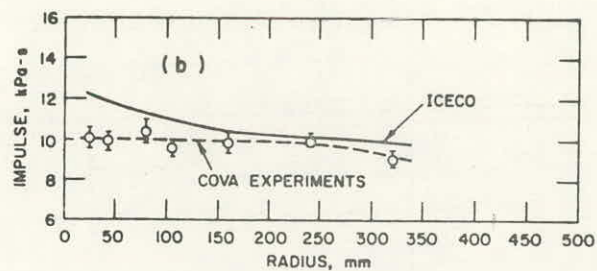


Fig. 52. Comparison of the Permanent Vessel
Deformation (Double-Vessel Model)



(a)



t = 1.0 ms

(e)

Fig. 53. (a) Test Model of the COVA Overstrong Vessel Experiment: (b-d) Impulses on the Floor, Wall, and the Roof, (e) Configuration at 1 ms

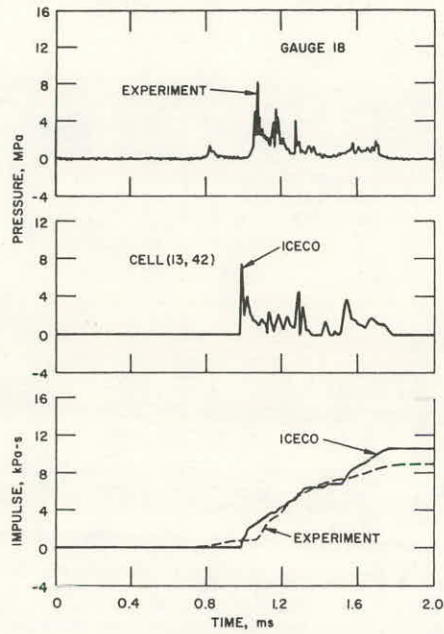


Fig. 54. Comparison of Pressure Histories at Roof Gauge #18 ($r = 160$ mm)

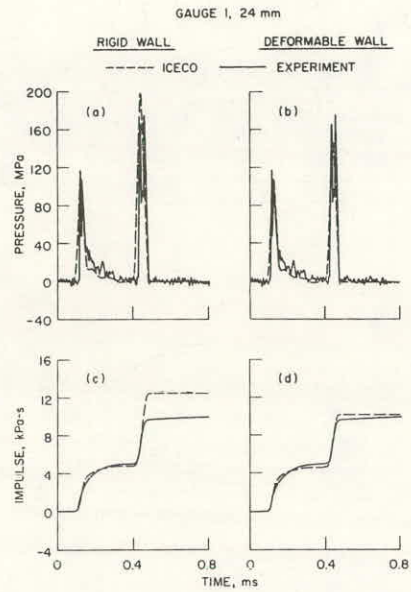


Fig. 55. Pressure and Impulse Histories for Floor Gauge #1 ($r = 24$ mm)

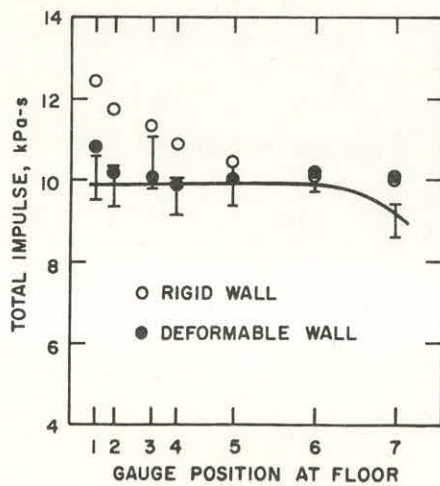


Fig. 56. Impulses at Floor Gauges

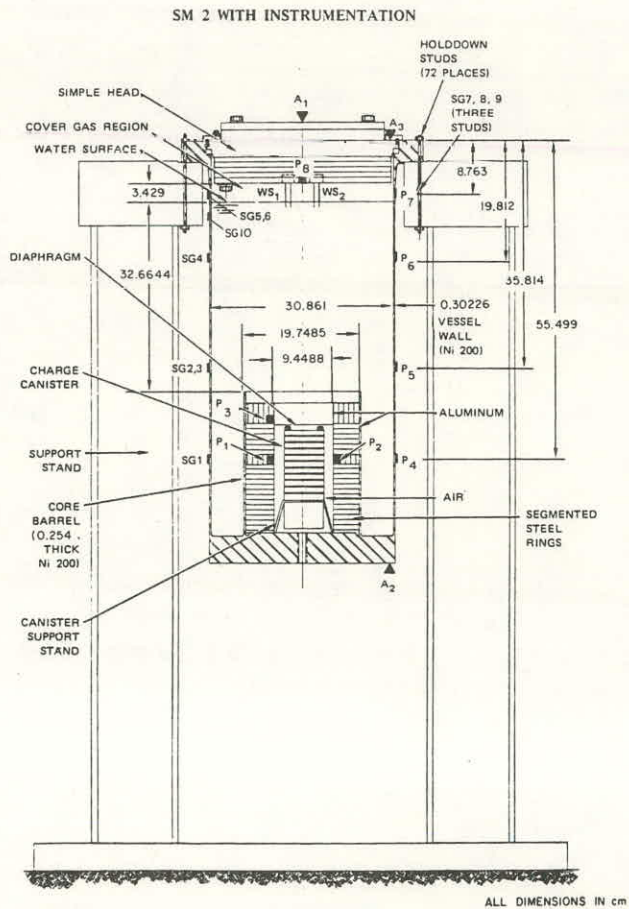


Fig. 57. SM-2 Test Model with Instrumentation

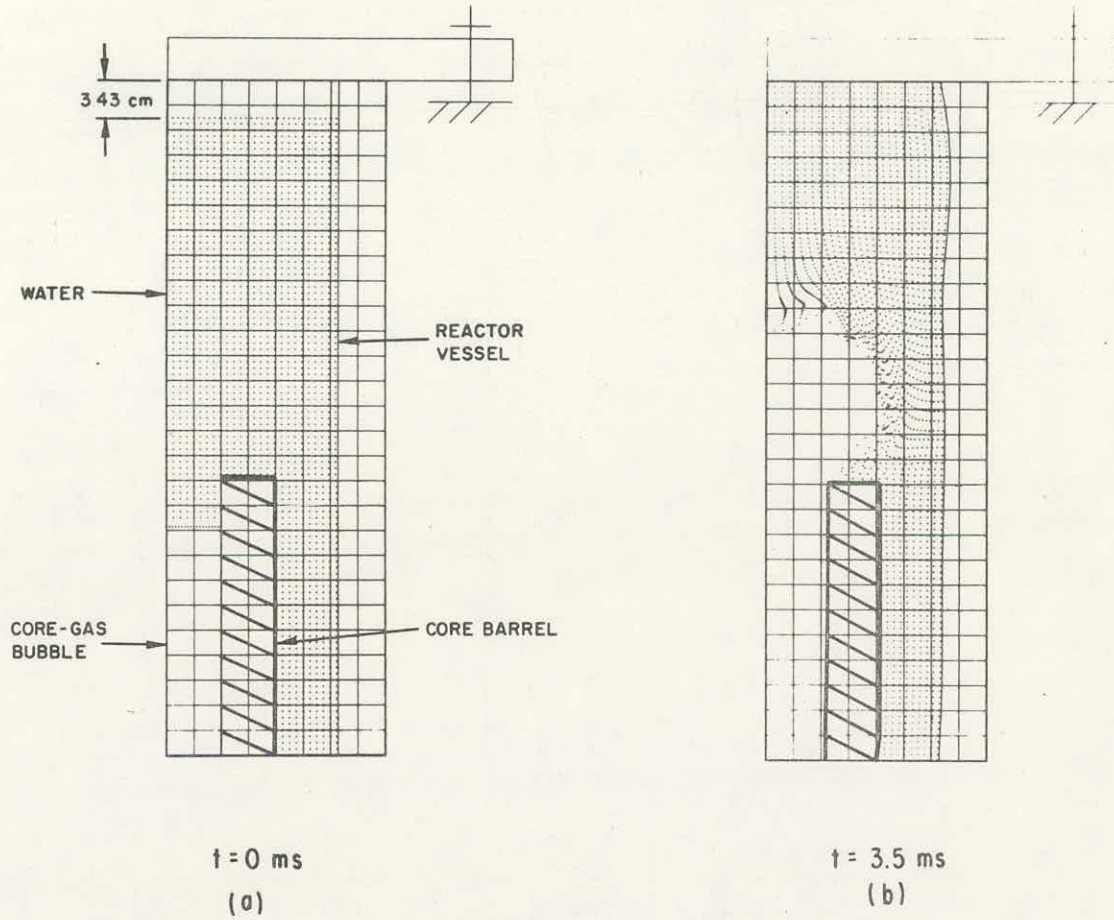


Fig. 58. Configurations at Two Different Times

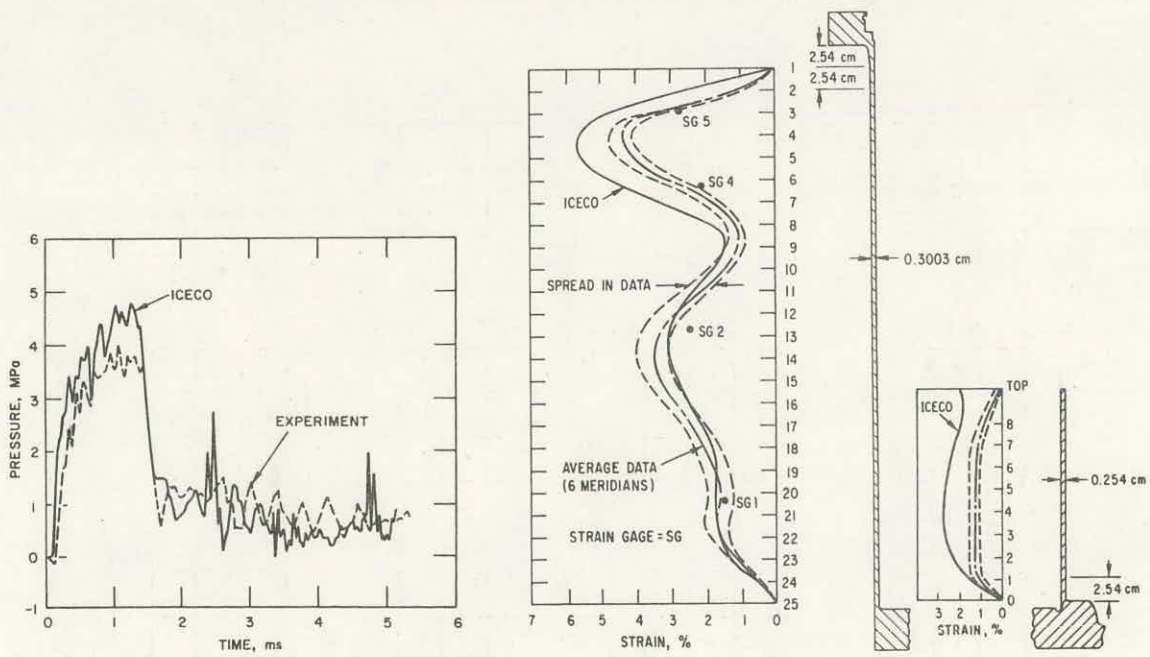


Fig. 59. Pressure Histories at Gauge P-5

Fig. 60. Deformed Shape Profile of SM-2

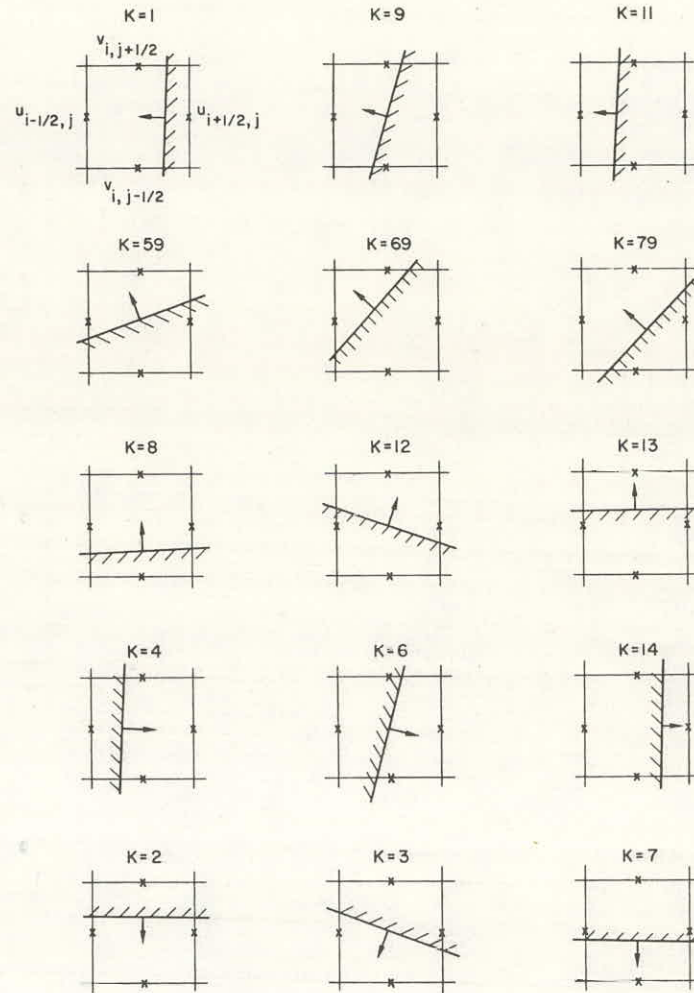


Fig. 61. Different Type of Flags at the Deformable Boundaries

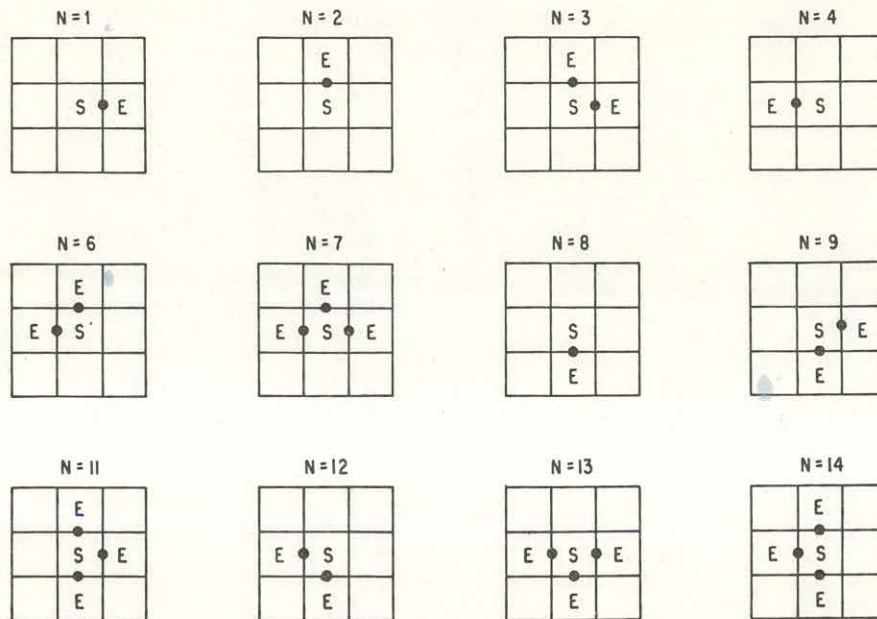


Fig. 62. Conventional Cell Flags Used Near the Free Surface

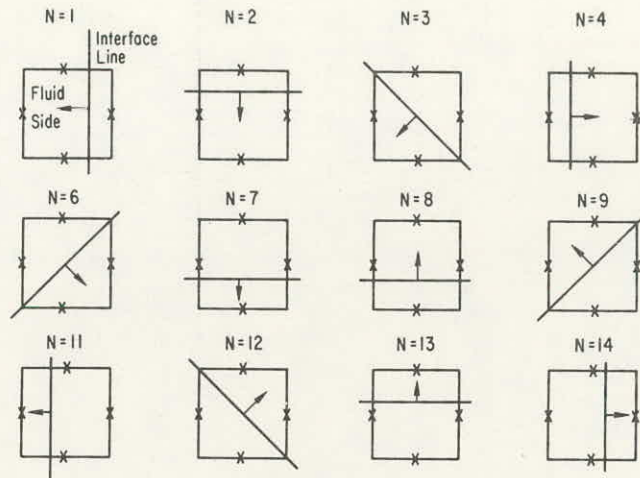


Fig. 63. Detailed Cell Flags Used Near the Free Surface

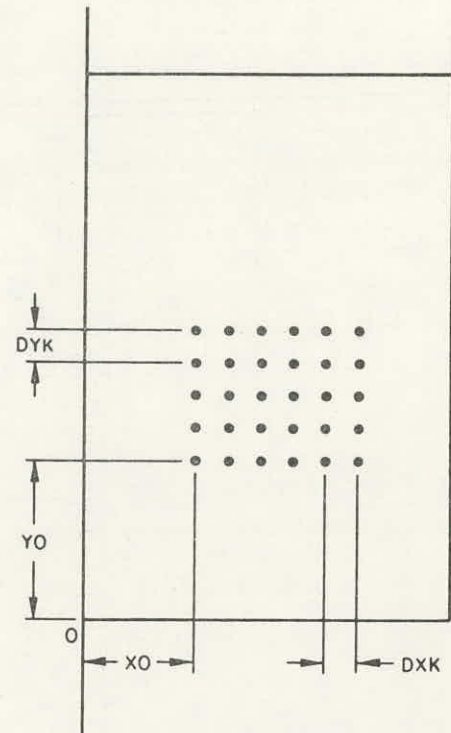


Fig. 64. Marker Particle Setup

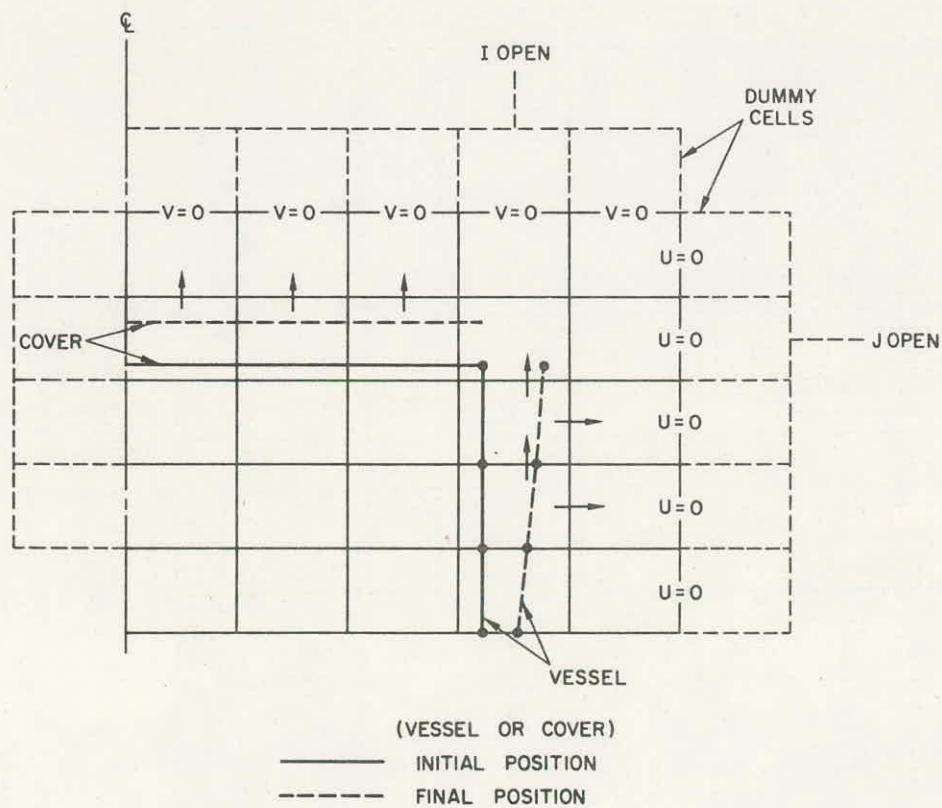


Fig. 65. Computing Mesh for Problems with Flexible External Boundaries

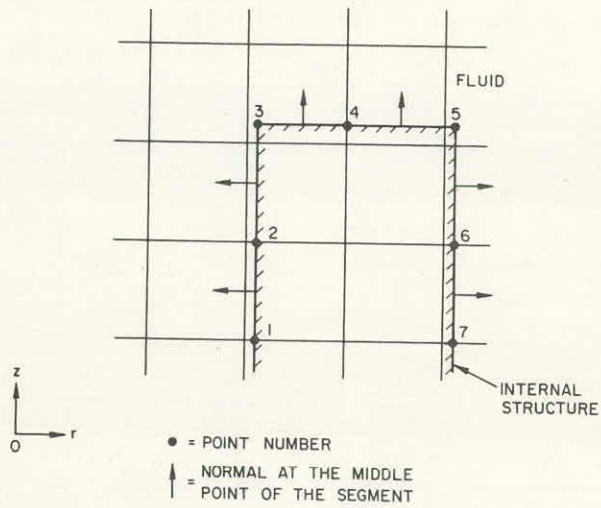


Fig. 66. Computing Mesh for Problems with Deformable Internals

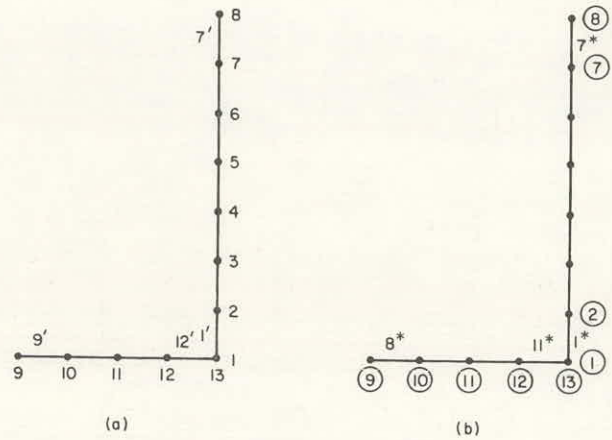
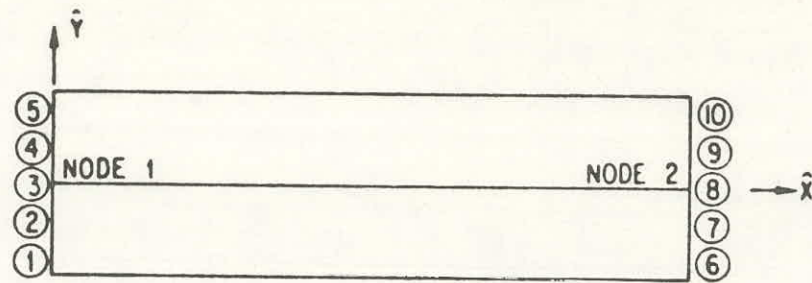


Fig. 67. Numbering System for Treating Fluid-Structure Interaction with Multiple Load Lines



	①	②	③	④	⑤	⑥	⑦	⑧	⑨	⑩
$\hat{\epsilon}_x$	1	2	3	4	5	6	7	8	9	10
$\hat{\sigma}_x$	11	12	13	14	15	16	17	18	19	20
$\hat{\epsilon}_\theta$	21	22	23	24	25	26	27	28	29	30
$\hat{\sigma}_\theta$	31	32	33	34	35	36	37	38	39	40
YIELD fct	41	42	43	44	45	46	47	48	49	50

Fig. 68. Component Number for the Time-History Plot

Distribution for ANL-81-9Internal:

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 E. S. Beckjord
 C. E. Till
 R. Avery
 L. Burris
 D. W. Cissel
 S. A. Davis
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 B. R. T. Frost
 L. G. LeSage
 R. A. Lewis
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 D. Okrent, U. California, Los Angeles

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the 1990s, the number of people in the world who are illiterate has increased from 1.2 billion to 1.5 billion. The number of illiterate people in the world is expected to reach 1.7 billion by the year 2015. The number of illiterate people in the world is expected to reach 1.7 billion by the year 2015. The number of illiterate people in the world is expected to reach 1.7 billion by the year 2015.