

Energy

S
O
L
A
R



525
11/27/84

myf (3)

DR# 0633-5

DOE/ET/20356-16
(DE85000328)

STAND-ALONE FLAT-PLATE PHOTOVOLTAIC POWER SYSTEMS:
SYSTEM SIZING AND LIFE-CYCLE COSTING METHODOLOGY
FOR FEDERAL AGENCIES

By
C. S. Borden
K. Volkmer
E. H. Cochrane
A. C. Lawson

May 1984

Work Performed Under Contract No. AI01-76ET20356

Jet Propulsion Laboratory
Pasadena, California

Technical Information Center
Office of Scientific and Technical Information
United States Department of Energy

DISCLAIMER

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

DISCLAIMER

Portions of this document may be illegible in electronic image products. Images are produced from the best available original document.

DISCLAIMER

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

This report has been reproduced directly from the best available copy.

Available from the National Technical Information Service, U. S. Department of Commerce, Springfield, Virginia 22161.

Price: Printed Copy A06
Microfiche A01

Codes are used for pricing all publications. The code is determined by the number of pages in the publication. Information pertaining to the pricing codes can be found in the current issues of the following publications, which are generally available in most libraries: *Energy Research Abstracts (ERA)*; *Government Reports Announcements and Index (GRA and I)*; *Scientific and Technical Abstract Reports (STAR)*; and publication NTIS-PR-360 available from NTIS at the above address.

00-000000

Stand-Alone Flat-Plate Photovoltaic Power Systems: System Sizing and Life-Cycle Costing Methodology for Federal Agencies

C.S. Borden
K. Volkmer
E.H. Cochrane
A.C. Lawson

May 1984

Prepared for
U.S. Department of Energy
Through an Agreement with
National Aeronautics and Space Administration
by
Jet Propulsion Laboratory
California Institute of Technology
Pasadena, California

JPL Publication 84-37

MASTER

ABSTRACT

A simple methodology to estimate photovoltaic system size and life-cycle costs in stand-alone applications is presented in this document. It is designed to assist engineers at Government agencies in determining the feasibility of using small stand-alone photovoltaic systems to supply ac or dc power to the load. Photovoltaic system design considerations are presented as well as the equations for sizing the flat-plate array and the battery storage to meet the required load. Cost effectiveness of a candidate photovoltaic system is based on comparison with the life-cycle cost of alternative systems. Examples of alternative systems addressed herein are batteries, diesel generators, the utility grid, and other renewable energy systems. A companion document, Flat-Plate Photovoltaic Power Systems Handbook for Federal Agencies (Reference 10), is recommended for discussion of issues for evaluating the viability of potential photovoltaic applications; descriptions of present photovoltaic system applications; synthesis of lessons learned from photovoltaic system design, installation, and operation; and identification of procurement strategies for Federal agencies.

FOREWORD

This system sizing and life-cycle costing methodology provides a tool for Federal agencies to use in estimating photovoltaic system size and life-cycle costs for non-utility grid-interactive applications. It is specifically intended for use by the Federal Government since use by non-Government entities would require additional considerations such as the effect of taxes. It is not intended for detailed system design, but rather provides a Government engineer, having limited background in photovoltaic technology, with the concepts required to estimate the photovoltaic system size and corresponding life-cycle cost. The methodology is appropriate for sizing remote photovoltaic systems that use fixed flat-plate photovoltaic collector technology with or without battery storage. In addition, the procedures for determining initial capital costs and life-cycle costs can be used to estimate funding requirements for system procurement.

To evaluate the life-cycle costs for a photovoltaic system, a comparison must be made with those of any alternative system. The methodology permits calculations of the life-cycle cost of both a photovoltaic power system and that of any alternative system.

Should questions arise from the use of this methodology, contact the Federal Photovoltaic Utilization Program Office at the Jet Propulsion Laboratory, 4800 Oak Grove Drive, Pasadena, California, 91109, telephone (818) 577-9523 or FTS 961-9523.

ACKNOWLEDGMENT

The U.S. Department of Energy Federal Photovoltaic Utilization Program, under the direction of Mr. Michael Pulscak, Program Manager, provides for the acquisition and installation of photovoltaic systems within various Federal agencies. This methodology has been prepared as part of this program.

CONTENTS

I.	INTRODUCTION	1-1
A.	ABOUT THIS DOCUMENT	1-1
1.	Purpose	1-1
2.	Scope	1-1
3.	Organization of the Document	1-1
B.	POTENTIAL APPLICATIONS FOR PHOTOVOLTAIC POWER SYSTEMS	1-2
C.	PHOTOVOLTAIC POWER SYSTEM DESCRIPTION	1-2
1.	The Solar Cell, Module, and Array	1-2
2.	The Photovoltaic System	1-3
3.	Insolation Characteristics and Their Effect on System Sizing	1-5
II.	SYSTEM SIZING	2-1
A.	RATIONALE	2-1
B.	SUMMARY OF THE PHOTOVOLTAIC SYSTEM SIZING METHODOLOGY	2-1
C.	PHOTOVOLTAIC SYSTEM SIZING PROCEDURE	2-5
1.	Calculate the Load	2-5
2.	Determine Local Insolation	2-6
3.	Calculate "Worst-Month" Insolation and Load	2-6
4.	Determine Array and Battery Storage Sizing Factors	2-8
5.	Calculate Array Power and Area	2-11
6.	Calculate Battery Storage Size	2-13
7.	Determine Voltage Regulator Size	2-14
8.	Determine Inverter or Converter Size	2-14

III.	SYSTEM COST ANALYSIS	3-1
A.	SCOPE	3-1
B.	COST ANALYSIS METHODOLOGY	3-1
	1. Photovoltaic System Life-Cycle Cost	3-1
	2. Alternative Power System Life-Cycle Cost	3-6
C.	PHOTOVOLTAIC VERSUS ALTERNATIVE POWER SYSTEM COST COMPARISON	3-7
IV.	REFERENCES	4-1

APPENDIXES

A.	PHOTOVOLTAIC SYSTEM SIZING AND COSTING EXAMPLE	A-1
B.	ESTIMATION OF LOAD FRACTIONS SUPPLIED BY PHOTOVOLTAIC ARRAY AND BATTERY STORAGE	B-1
C.	COMPARISON OF SIZING METHODOLOGY WITH ALTERNATIVE APPROACHES	C-1
D.	AVERAGE DAILY INSOLATION TABLES FOR UNITED STATES SITES . . .	D-1

Figures

1-1.	Typical Solar Cell	1-3
1-2.	The Output of a Solar Cell Varies with Changes in the Environment: (a) Temperature and Solar Cell Voltage are Inversely Related, (b) Irradiance and Solar Cell Current are Directly Related	1-4
1-3.	Photovoltaic Module and Array: (a) Solar Cells Packaged into a Photovoltaic Module, (b) Modules are Grouped into an Array to Increase Power Output	1-5
1-4.	Stand-Alone Photovoltaic System Configuration to Serve a dc Load	1-5
1-5.	Stand-Alone Photovoltaic System Configuration to Serve an ac Load	1-6
1-6.	Clear Sky Array Power Output Profile	1-6
1-7.	Effect of Season and Region on Insolation Level (a) Winter, (b) Summer	1-7

1-8.	Insolation Available to the Array Under Clear Sky and Cloudy Conditions	1-8
1-9.	Relative Energy Output at Various Array Tilt Angles	1-9
2-1.	Sequence of Steps in Sizing a Remote, Stand-Alone Photovoltaic System	2-2
2-2.	Photovoltaic System Model Showing Key System Sizing Parameters	2-3
2-3.	Determining Array and Battery Storage Sizing Factors (at LOEP = 0.1) for Various Worst-Month Insolation Values . . .	2-9
3-1.	Approach for Determining Photovoltaic Power System Cost Effectiveness	3-2
3-2.	Life-Cycle Cost Comparison of Photovoltaic System (LCC _{PV}) and Non-Photovoltaic System (LCC _{ALT})	3-8
A-1.	Photovoltaic System Sizing Procedure	A-2
A-2.	Determining Array and Battery Storage Sizing Factors (at LOEP = 0.1) for Various Worst-Month Insolation Values. . .	A-6
A-3.	Approach for Determining Photovoltaic System Cost Effectiveness	A-8
B-1.	Idealized Energy Usage by Time-of-Day for a Given Month . . .	B-1

Tables

2-1.	Example of Method for Determining the Appropriate Insolation and Load Combinations for Sizing the Array and Battery Storage	2-7
A-1.	Photovoltaic System Sizing Parameters: Relevant Ranges and Default Values	A-3
A-2.	Monthly Insolation and Example Energy Load Values for Three Array Tilt Angles for China Lake, California	A-4
A-3.	Photovoltaic System Cost Parameters: Relevant Ranges and Default Values	A-9
A-4.	Cost Elements.	A-10
C-1.	Array and Battery Storage Sizing Comparison	C-2

SECTION I

INTRODUCTION

A. ABOUT THIS DOCUMENT

1. Purpose

Photovoltaic (PV) power systems are potentially a cost-effective alternative to conventional power sources (e.g., diesel generators, batteries) in a variety of remote applications where the operation, maintenance, and fuel costs of the conventional sources are high. This document describes a photovoltaic system sizing and life-cycle costing methodology that has been prepared to assist Federal Government agencies in determining the feasibility of using stand-alone photovoltaic systems that can supply either ac or dc power to a specified load. In addition, the procedure for determining initial capital costs and life-cycle costs can be used to estimate funding requirements for system procurement.

2. Scope

The methodology in this report applies to stand-alone fixed flat-plate photovoltaic systems (which include the array, voltage regulator, battery storage, and dc-ac inverter or dc-dc converter) as well as various possible alternatives such as battery storage, diesel generators, other renewable energy technologies, and extension of the utility grid to the remote site. The methodology, therefore, permits a comparison of the economic viability of photovoltaics with that of the possible alternatives, thereby facilitating final selection of the preferred generating option.

This document considers only the relative cost effectiveness as a selection factor in comparing photovoltaic and its alternatives. Additional non-cost-related factors in selecting a power system such as land limitations, limitations on noise generation, physical accessibility for maintenance, etc., although critical in some applications, are beyond the scope of this document.

Finally, this methodology applies to flat-plate photovoltaic-only systems. It does not address hybrid arrangements that combine photovoltaics with another conventional generation mode into a single power system. Sizing the various generating elements of a hybrid system can be accomplished only after a preliminary trade study to determine the most cost-effective configuration for the overall power system, given an intended load.

3. Organization of the Document

The remainder of Section I presents a description of photovoltaic technology and its application to typical remote loads. In addition, the various characteristics of solar irradiation (i.e., insolation) are described. Special attention is paid to insolation characteristics that may affect the manner in which the photovoltaic system is sized for an intended load.

Section II covers photovoltaic array and battery storage system sizing. Required inverter/converter and voltage regulator sizes are also addressed. Once the size calculations have been made, Section III is used to determine the life-cycle cost of both the photovoltaic power system and any alternatives being considered. A comparison of these life-cycle costs will provide the basis for selecting the power generation technology most appropriate for a given application.

B. POTENTIAL APPLICATIONS FOR PHOTOVOLTAIC POWER SYSTEMS

Photovoltaic power systems may be considered potentially viable for a number of remote applications. Typical loads that represent current and potential near-term photovoltaic applications are listed below:

- (1) Telecommunications.
Example: radio repeater.
- (2) Navigational aids.
Examples: beacon, buoy, lighthouse.
- (3) Aviation aids.
Examples: radar beacon, anemometer.
- (4) Environmental sensors.
Examples: radiation sampler, noise monitor.
- (5) Intrusion detectors.
Examples: entry monitor, electric fence.
- (6) Battery charging.
- (7) Lighting.
- (8) Refrigeration.
Example: medical supplies refrigerator.
- (9) Space conditioning.
Examples: small cooler, ventilator.
- (10) Water pumping.
- (11) Water purification/desalination.
- (12) Cathodic protection (corrosion protection).
Examples: transmission tower, bridge, well, pipeline.

C. PHOTOVOLTAIC POWER SYSTEM DESCRIPTION

1. The Solar Cell, Module, and Array

Photovoltaic systems are electrical generating systems based on photovoltaic, or solar, cells (Figure 1-1). The cells convert photons from incident sunlight directly into dc electricity. The solar cell typically

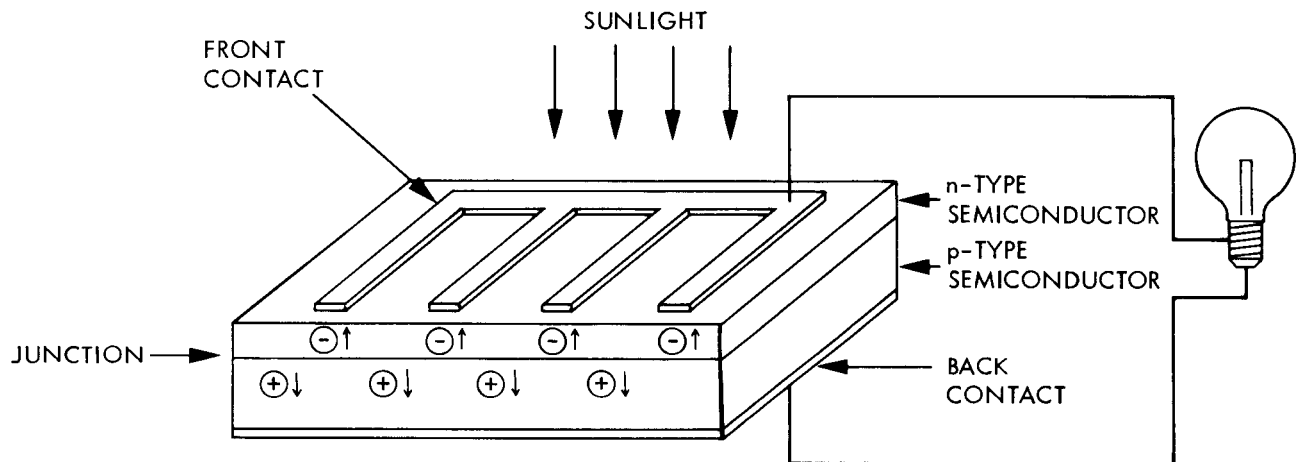


Figure 1-1. Typical Solar Cell

consists of two different types of semiconductor material, called n-type and p-type. Energy carried by the photons frees positive and negative charges within the cell material. The junction between the n- and p-type materials creates an electric field, causing the freed charges to separate across the junction and resulting in a voltage across the cell. Electrical contacts placed on the p-side and on the n-side of the solar cell allow the current generated within the cell to be applied to an external load.

The amount of electric current generated by a solar cell is primarily dependent on the intensity of solar radiation striking its exposed area. The open-circuit voltage produced, however, is primarily dependent on the temperature of the cell. Voltage and cell temperature are inversely related [i.e., an increase in temperature lowers both the output voltage and the output power, thereby reducing the cell's efficiency (Figure 1-2)].

Because the power output of a single solar cell is small [approximately 1 watt for a typical cell (100 cm², 10% efficient)], a number of cells are interconnected in series and parallel and sold as a package called a photovoltaic module (Figure 1-3a). These, in turn, can be wired together into an array (Figure 1-3b) to generate the amount of power required by the application.

2. The Photovoltaic System

A practical stand-alone photovoltaic power system typically requires several elements in addition to the array in order to satisfy the intended load. A typical configuration for a dc load is shown in Figure 1-4.

Battery storage, most commonly involving a lead-acid battery in present applications, stores electrical energy produced by the solar array in daytime for use during the night or under cloudy conditions. To be considered practical for remote applications, a storage battery should have a long life, require low maintenance, and be able to survive a number of deep discharge cycles with subsequent recharge by the array.

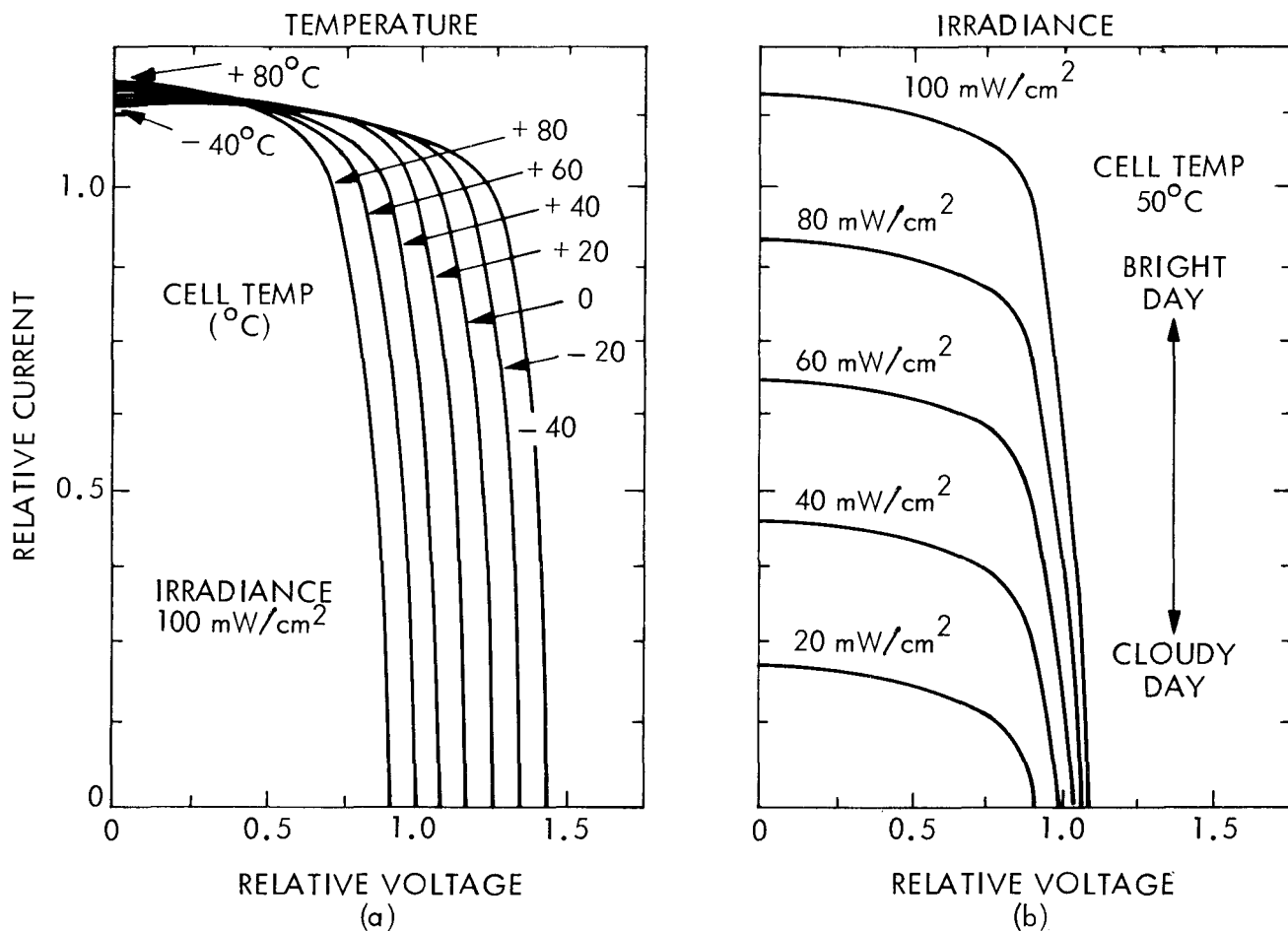


Figure 1-2. The Output of a Solar Cell Varies with Changes in the Environment: (a) Temperature and Solar Cell Voltage are Inversely Related, (b) Irradiance and Solar Cell Current are Directly Related

Another important component of a photovoltaic power system using storage is a voltage regulator that controls the output voltage from the array when used to charge the battery. The regulator also limits the loss of water that would occur from gassing of the battery if it were permitted to become overcharged. At night or on cloudy days, a blocking diode (see Figure 1-4) prevents the electrical energy stored within the battery from discharging through the voltage regulator or the array.

A system serving a dc load may require a dc-dc converter to match the system output voltage to the rated voltage of the load.

Some photovoltaic applications do not necessarily require battery storage. An example of this is water pumping, which needs only a photovoltaic array, a water pump, a water storage tank, and minimum power regulation. In this case, water is pumped into the storage tank during sunlight hours. The storage tank then acts as a reservoir, providing water during non-sunny periods.

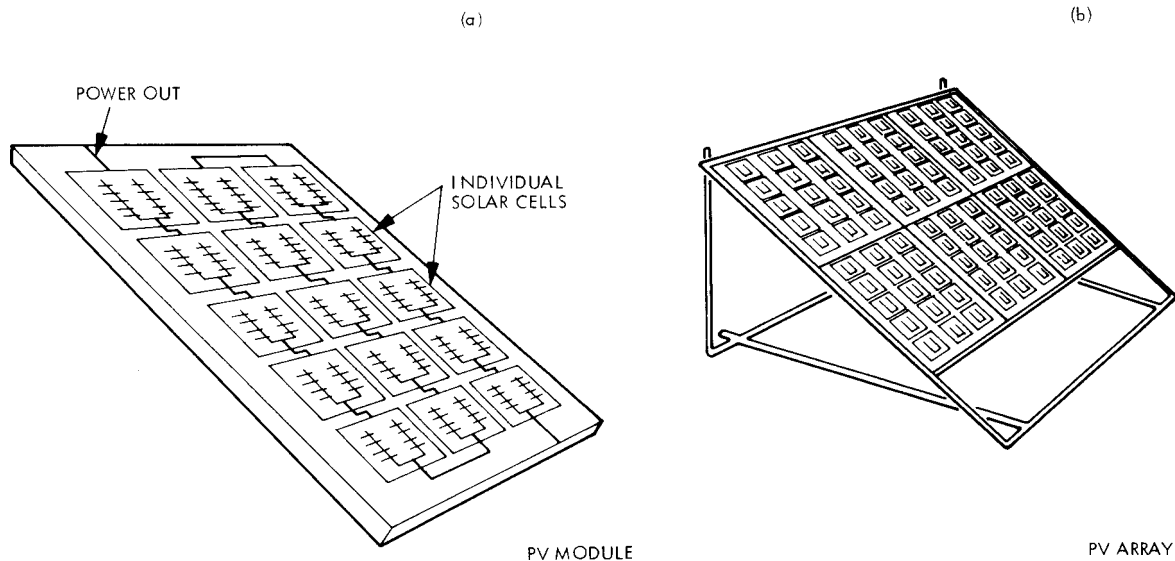


Figure 1-3. Photovoltaic Module and Array: (a) Solar Cells Packaged into a Photovoltaic Module, (b) Modules are Grouped into an Array to Increase Power Output

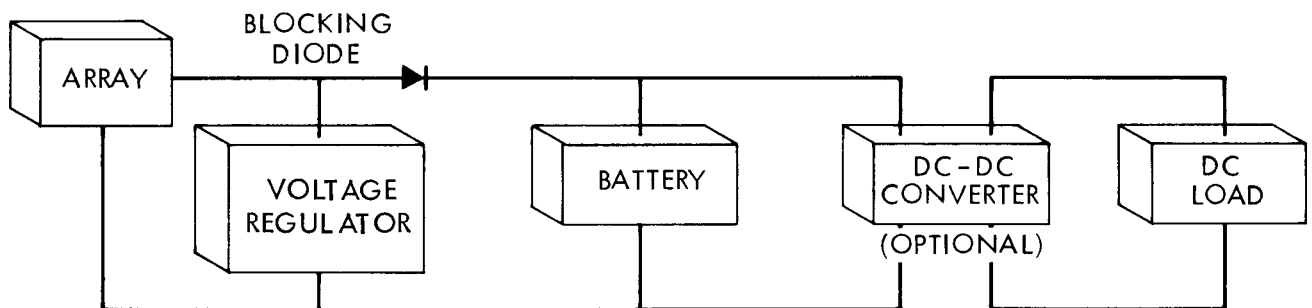


Figure 1-4. Stand-Alone Photovoltaic System Configuration to Serve a dc Load

Other applications may require power conditioning to provide the required power characteristics to an ac load. In this case, an inverter is used to convert the dc voltage from the array into an ac voltage (Figure 1-5).

3. Insolation Characteristics and Their Effect on System Sizing

Array and battery storage size requirements to adequately serve the load energy requirement ultimately depend on the amount of insolation at the location of the site. Since the amount of energy received from the sun will depend on location, season, weather, and array orientation, it is essential to account for these factors in sizing the system. Furthermore, since the intended load may also vary seasonally, sizing will normally require a systematic accounting approach to ensure that sufficient solar energy will be captured by the array to achieve acceptable system reliability throughout the year.

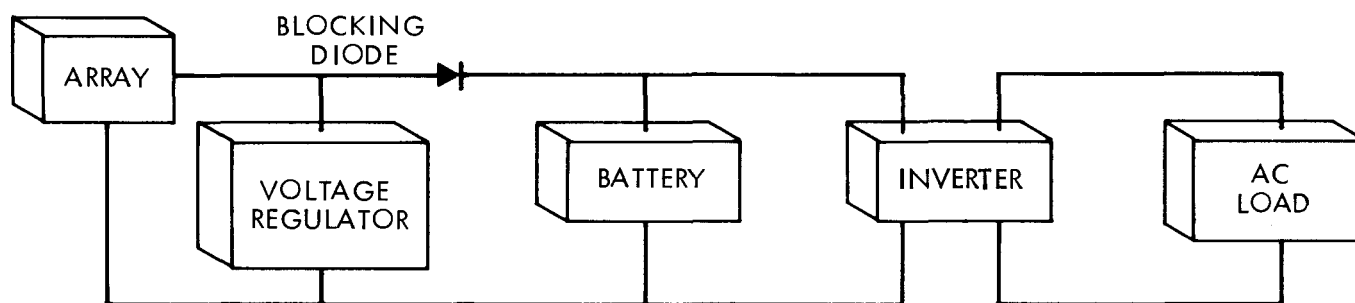


Figure 1-5. Stand-Alone Photovoltaic System Configuration to Serve an ac Load

Insolation characteristics important for sizing photovoltaic system components include the following: diurnal variation, regional and seasonal variability, weather, and array orientation relative to the direction of the sun. These characteristics are described below:

- (1) Diurnal Variation. The most important characteristic of insolation is its diurnal pattern. The expected power available to a fixed flat-plate array over a 24-hour period under clear sky conditions will follow a curve similar to that in Figure 1-6. Any load that does not closely approximate this power output profile, or accommodate deviations from it, will necessitate battery storage or other backup to the photovoltaic system.
- (2) Regional and Seasonal Variability. A second major factor in sizing the system is the regional and seasonal variability in insolation. Figure 1-7a shows the total insolation on a fixed collector tilted at latitude during the winter in the contiguous United States. Note that the insolation in $\text{kWh/m}^2\text{-day}$ varies by up to a factor of 2.5, depending on region. Also, note in Figure 1-7b the manner in which the total insolation differs between winter and summer for a given location. The summer-to-winter difference in insolation in prime locations such as the northern portions of California and Nevada, for example, is seen to be a factor of

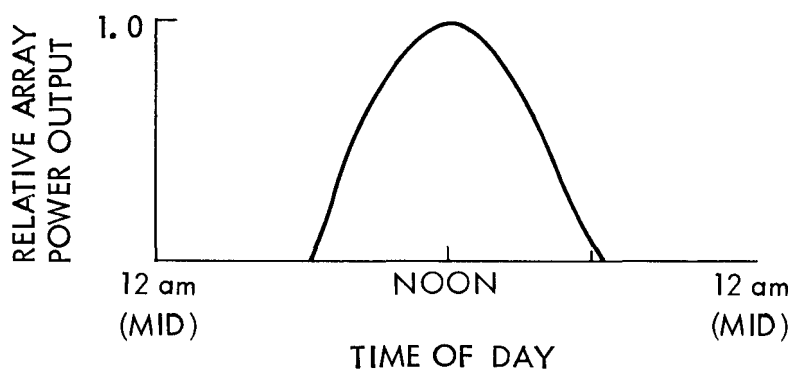


Figure 1-6. Clear Sky Array Power Output Profile

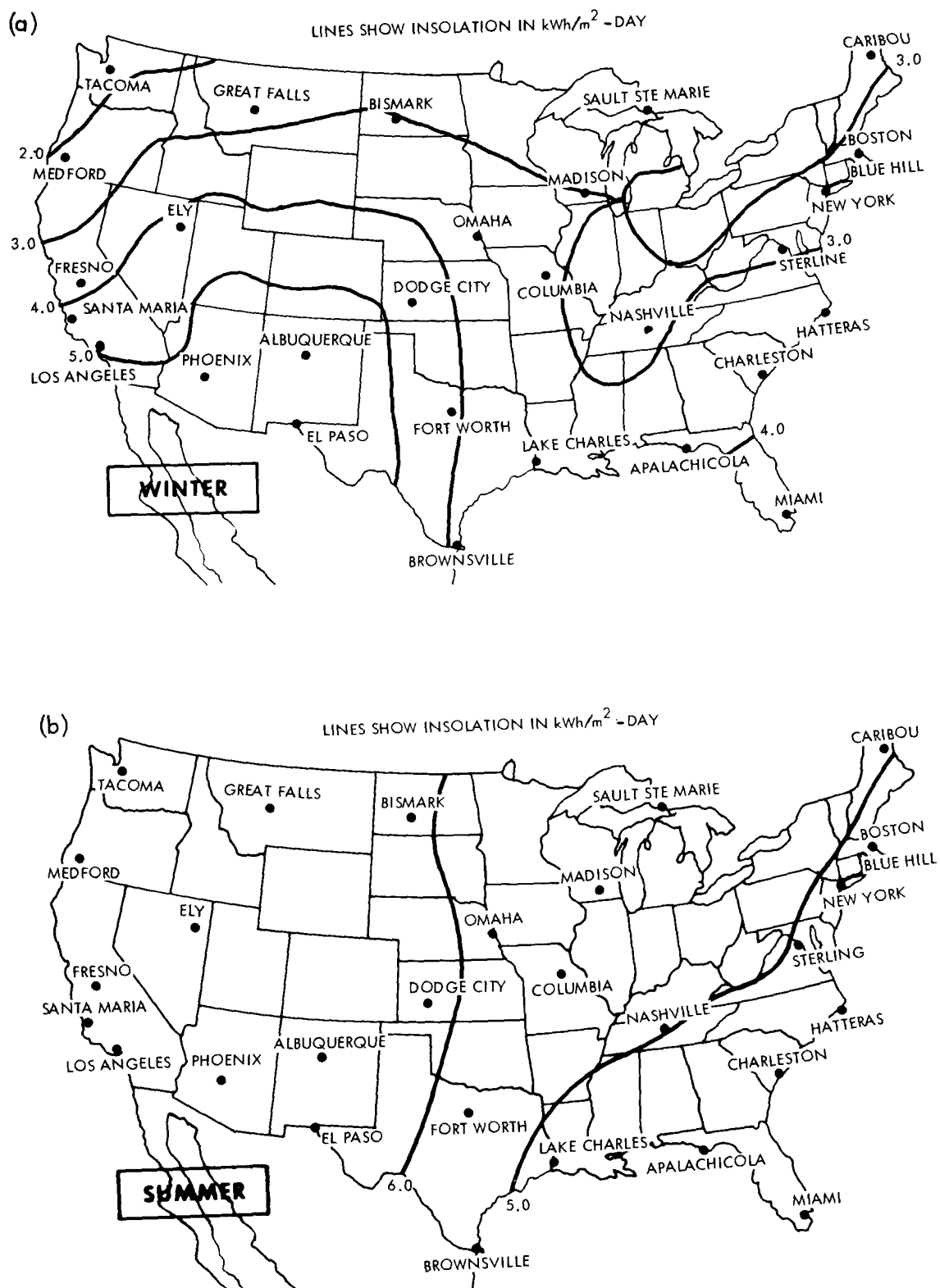


Figure 1-7. Effect of Season and Region on Insolation Level
(a) Winter, (b) Summer. (Reference 1)

between 1.5:1 and 2:1. These differences must be identified and allowed for in order to correctly size a system for a given load and location.

As noted previously, these variations will require that the sizing method accounts for these differences to ensure that the solar energy incident on the array is sufficient to serve the planned load during all months of the year.

- (3) Weather. Cloudy weather will considerably reduce the amount of insolation and, thus, the output from the photovoltaic system (see Figure 1-8). (The output typically will not drop to zero since flat-plate systems generate power roughly in proportion to the amount of light falling on the surface of the photovoltaic cells.) Since cloudy weather can occasionally persist for several days in any location, photovoltaic systems serving most loads will require storage or other electrical backup to ensure reliable power. In sizing a photovoltaic system, the amount of storage is primarily determined by the probable amount of cloudy weather at a given site during the worst month of the year. The method for sizing the battery storage in Section II.C.6 is based on estimates of this probability derived from historical weather records. Although previous weather history is not a perfect predictor of future weather patterns, it does serve as a useful guideline for estimating photovoltaic system requirements.
- (4) Orientation of the Array. Since there are seasonal differences in the daily path of the sun across the sky, the amount of solar energy striking a fixed array will vary seasonally according to its orientation. Note that these effects are due only to annual changes in sun angle and are distinct from typical seasonal

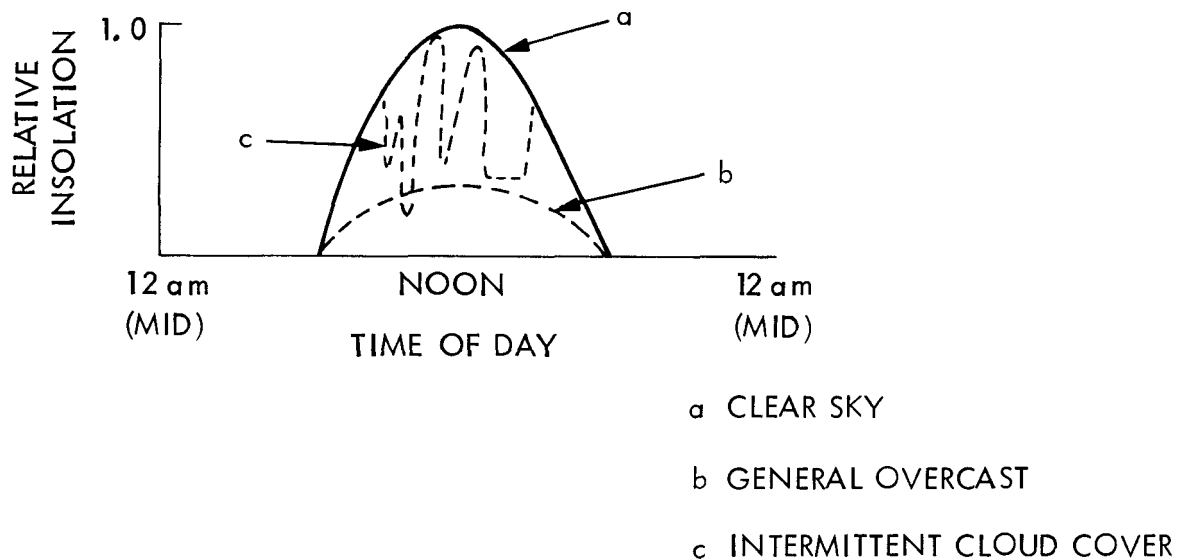


Figure 1-8. Insolation Available to the Array Under Clear Sky and Cloudy Conditions

changes in insolation due to changing weather patterns. Figure 1-9 illustrates the effect of array tilt on power output.¹ In this figure, array outputs are normalized and appear as fractions of the output from an array at latitude tilt.

Under typical weather conditions, the maximum annual energy output from a fixed array occurs when the array is tilted at an angle equal to the latitude where it is sited. However, if the load varies seasonally, latitude tilt may not be the most cost-effective angle for the array; i.e., the smallest array size that satisfies the load. The method for selecting the correct tilt angle for sizing purposes will be described under II.C.3, Calculate "Worst-Month" Insolation and Load.

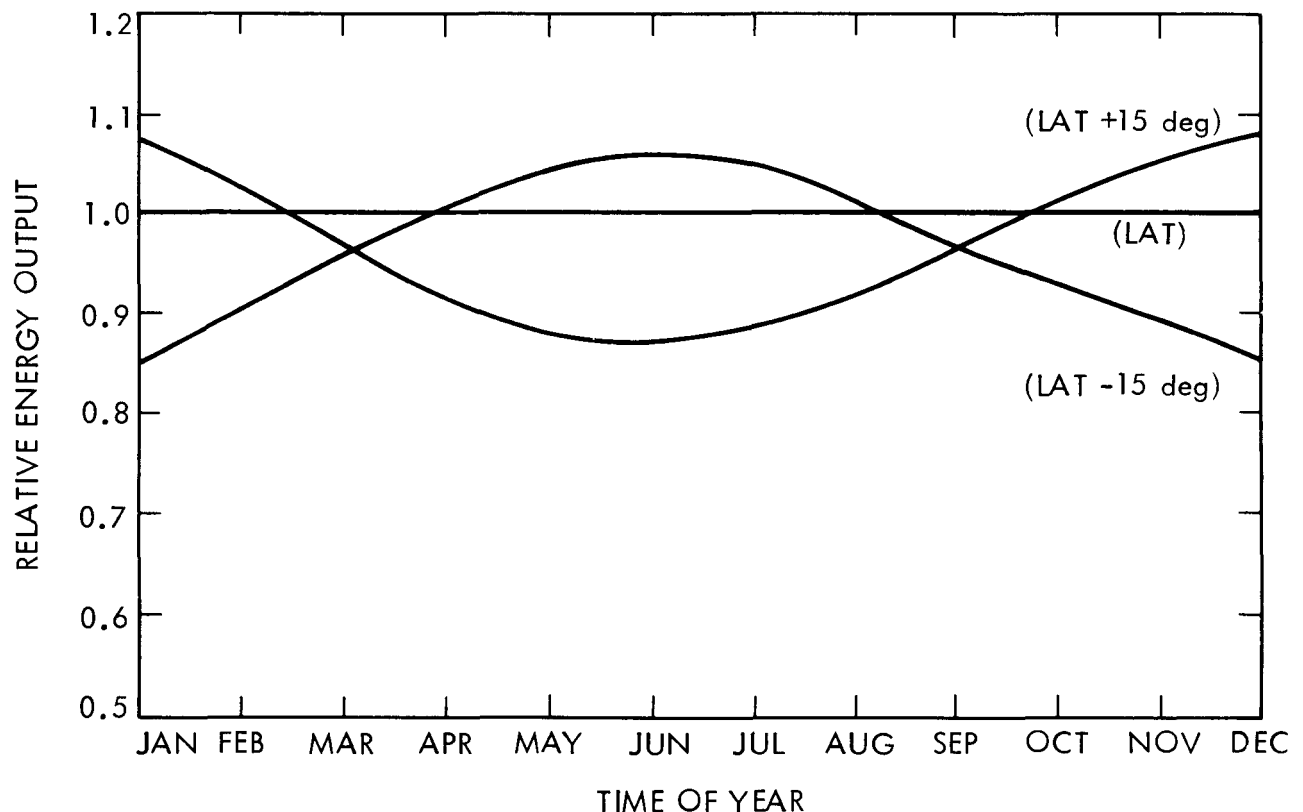


Figure 1-9. Relative Energy Output at Various Array Tilt Angles.
(Adapted From Reference 2)

¹Array tilt is measured from the horizontal. In the northern hemisphere, the array faces toward the south; in the southern hemisphere, it faces toward the north.

SECTION II

SYSTEM SIZING

A. RATIONALE

The term "sizing," as it is used in this document, means estimating the required size or capacity of all major photovoltaic system elements so that the system will be able to satisfactorily serve the intended load.² The sizing methodology described in this section is based on a target level of photovoltaic system reliability that is equivalent to conventional diesel or battery alternatives. The size estimates obtained by this methodology are used to cost the system according to the method described in Section III. The cost estimates, in turn, are compared with estimates for other possible power generating options in order to determine whether selection of a photovoltaic power system is justified on a comparative life-cycle cost basis.

The sizing methodology is restricted to stand-alone systems serving either ac or dc loads. If the application involves both ac and dc loads, the method may be applied by sizing the system for the ac and dc loads separately and then combining the results. This methodology is intended primarily to treat photovoltaic systems with storage since the majority of remote load applications will require at least part of their total energy needs at night or during cloudy day periods of reduced system output. Some applications, however, do not require regular power availability and may be served adequately by photovoltaic systems without battery storage capabilities. The primary example of this kind of application is a water pumping system in which water to serve periods of low pump output is stored in a reservoir or storage tank. The methodology will also address applications of this kind.

The required sequence of steps in the sizing methodology to be described is summarized in Figure 2-1.

B. SUMMARY OF THE PHOTOVOLTAIC SYSTEM SIZING METHODOLOGY

Figure 2-2 schematically depicts a photovoltaic system serving a load. This simple representation illustrates the key factors involved in system sizing. Radiant energy from the sun, or insolation (I) is converted to dc electrical energy by the array at a conversion efficiency e_a . A fraction of the load energy, f_a , may be received from the dc array output through an inverter if the load is ac, or directly if the load is dc. A dc-dc converter is used if the load operates at a dc voltage above that produced by the array configuration. The remaining load fraction, f_b , is received from the storage batteries that are periodically recharged by the array during periods when array output exceeds the load requirements. Conversion efficiencies for the voltage regulator, battery, and inverter or converter are e_{vr} , e_b , and

²Major system elements include the array, voltage regulator, battery storage, and dc-ac inverter or dc-dc converter.

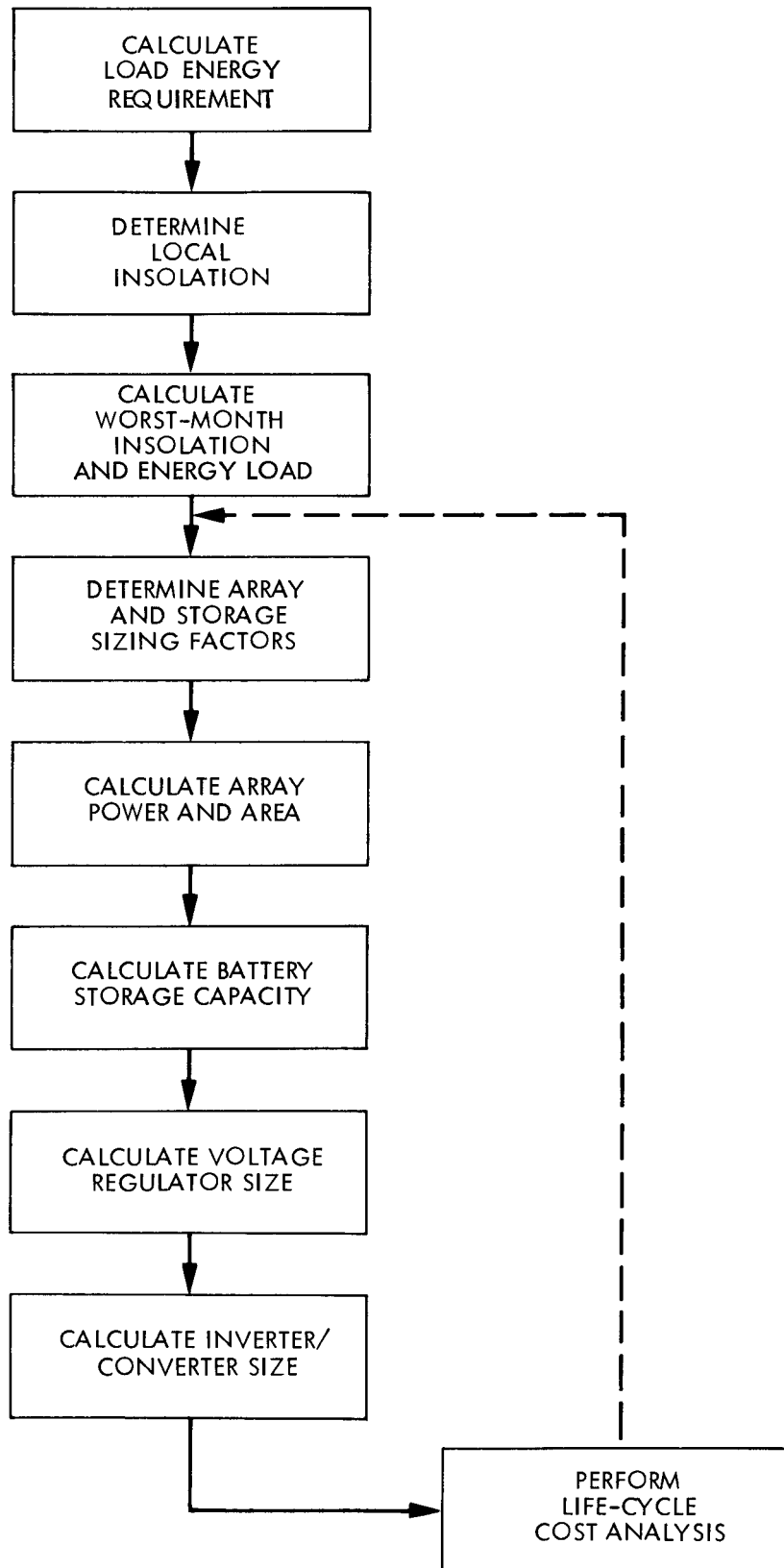


Figure 2-1. Sequence of Steps in Sizing a Remote, Stand-Alone Photovoltaic System

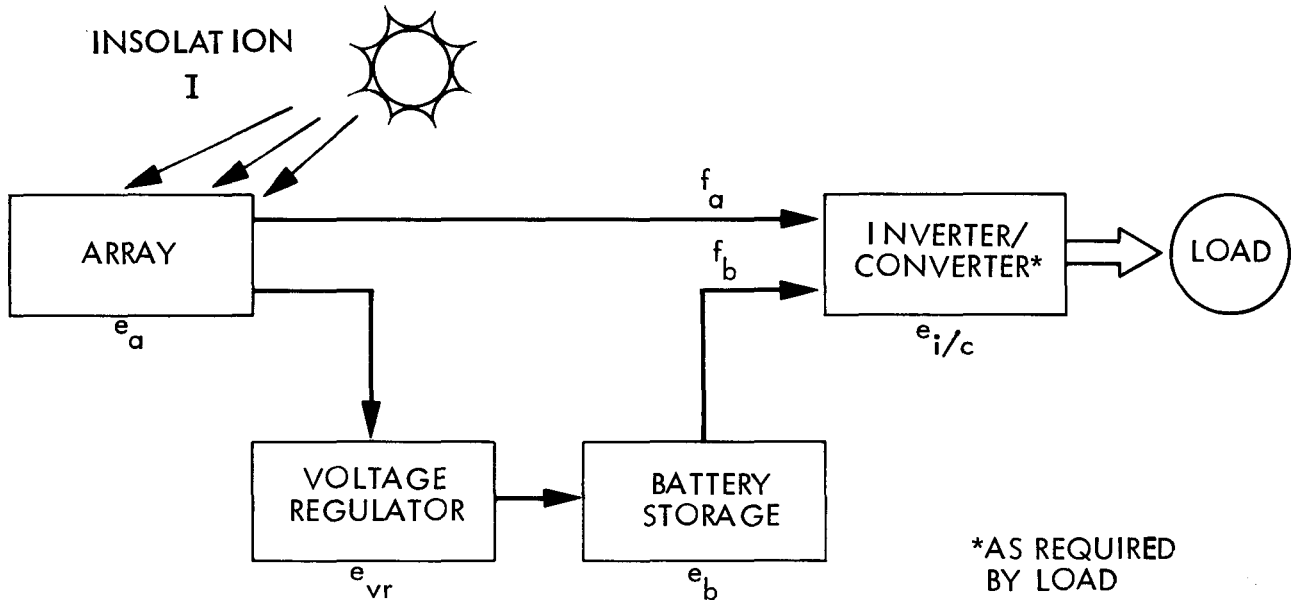


Figure 2-2. Photovoltaic System Model Showing Key System Sizing Parameters

e_i/c , respectively.³ As appropriate, these terms should be used in system sizing to account for losses occurring in these system elements during system operation.

The steps in the sizing methodology shown in Figure 2-1 are summarized below (complete details of the sizing procedure are presented in Section II.C.):

- (1) Calculate the Load. The average daily energy load in kilowatt-hours is calculated for each month of the year. In the simplest case, a single load element draws constant power at all times. If several load elements are present, the individual elements must be summed. If the load totals vary from day to day, an average daily load over each month of the year will be required.
- (2) Determine the Local Insolation. The appropriate amount of input energy (i.e., insolation, I) to the photovoltaic system at the application site may be obtained from tables in Appendix D for various array tilt angles. As insolation values will vary from month to month, average daily values for all months are included in the tables.

³In cases where neither an inverter or converter is required by the system, the e_i/c term in the sizing calculations is equal to 1.0 (i.e., no conversion losses). Similarly, if no storage is required, both e_{vr} and e_b are set equal to 1.0.

- (3) Calculate "Worst-Month" Insolation and Load Values. The sizing approach requires identification of the load and insolation values expected during the "worst month" of the year. This is done by constructing a table of average insolation and load values for each month of the year and then determining the month with the lowest ratio of insolation to load. The insolation and load values for the selected worst month are used in subsequent steps to calculate required array size and battery storage capacity.
- (4) Determine Array and Battery Storage Sizing Factors. The approach used in the methodology to size the array and storage is to apply previously determined "sizing factors" in the array and storage calculations in order to scale the system to achieve a desired level of autonomy (i.e., availability). These factors are displayed in a nomograph to facilitate selection of the appropriate sizing factor values for use in subsequent array and battery size calculations.⁴
- (a) In some sizing applications, the user may specify the level of system autonomy by placing a requirement on the number of sunless days during which the system must be able to satisfy the intended load. The sizing method in this document may also be applied in that case.
- (b) Estimate the load fractions supplied by the array and battery storage. Since energy supplied by the array directly to the load suffers less power loss than that passing through the battery storage, the fraction flowing to the load by each pathway should be estimated. In cases where these estimates are especially difficult to make, the user may follow a conservative sizing approach by letting the fraction from the array equal zero and the fraction from the battery equal one.
- (5) Calculate Array Power and Area. Calculating array size means calculating both its required peak power output in watts and its corresponding area in square meters. The array sizing calculations incorporate the worst-month load, array sizing factor based on the worst-month insolation, efficiencies of all major system elements, and a term to account for long-term array degradation.
- A modification of the sizing methodology may be applied to certain specialized applications that require no battery storage to back up the photovoltaic array, such as the case of pumping water to a storage reservoir.
- (6) Calculate Battery Storage Size. Calculating battery storage size requires scaling the storage to supply the daily energy load for a sufficient period of time to assure that the photovoltaic system meets the load requirements at least 96 to 98% of the time (or

⁴This approach has been adapted from Reference 3.

equivalently, a 0.1 "loss of energy probability" (LOEP) during the worst month of the year). Alternatively, the storage can be sized to supply the load for a specified number of sunless days. In either case, the actual rated capacity is adjusted to ensure battery operation within acceptable depth of discharge limits.

- (7) Calculate the Voltage Regulator Size. The battery charging voltage regulator is sized to handle the maximum amount of array output power (dc) that is not being used to supply the load. For conservatism, this will be considered to be the full rated peak array output power to account for situations in which the load has been disconnected.
- (8) Calculate the Inverter/Converter Size. The inverter or converter, if either is required, is rated according to its output capacity in watts or kilowatts ac or dc, respectively. These units are sized to match or exceed the maximum steady state load power requirement (or maximum surge current for inductive loads) occurring at any time during the expected system life.

The remainder of Section II describes the sizing procedure in detail.

C. PHOTOVOLTAIC SYSTEM SIZING PROCEDURE

This section describes the procedure for sizing the photovoltaic system using the steps identified in Figure 2-1. An example implementation of this procedure, along with sample data, is shown in Appendix A. The associated life-cycle cost analysis procedure is described in Section III.

1. Calculate the Load

Sizing the photovoltaic system first requires a calculation of the average daily energy load for each month of the year. The daily energy load for a single device or element is calculated as the power it draws in kilowatts times the number of hours that it is in service during every 24-hour period. If more than one load element is to be served, the total daily energy load is obtained by summing the individual loads as shown in Equation (1).

$$L_{td} = \sum_{i=1}^n P_i D_i / 1000 \quad (1)$$

where

L_{td} = total daily energy load in kilowatt-hours per day

P_i = power drawn by load element i while it is in service, in watts

D_i = amount of time per day in hours that load element i is in service

n = number of separate load elements

For loads that vary from day to day, an average daily load is calculated for each month of the year. An average daily load for a given month is the sum of all daily loads divided by the number of days in the month.⁵ If the load consists of both ac and dc elements, the load calculations and subsequent system sizing procedures should be applied separately to the ac and dc loads. The final array and battery sizes are then obtained by summing the separate array and battery sizes calculated for the ac and dc elements.

Note that this assumes that system and load are co-located. If the distance from a power source to dc load is increased beyond a few meters, resistive wiring losses will begin to become apparent. These losses will necessitate a compensating increase in the required system size. If deemed significant, the user of this methodology may allow for dc wiring losses by increasing the calculated load size served by the photovoltaic system to include the I^2R power losses calculated for the dc run.

2. Determine Local Insolation

Average daily insolation values for each month of the year must be determined for the application site. Appendix D contains insolation values for three possible array tilt angles for a variety of United States sites. Insolation for United States sites not listed may be estimated by interpolation between nearest tabulated values. Other sources may be consulted for non-United States locations. Insolation values determined for the site will be used in the next step of the sizing methodology.

3. Calculate "Worst-Month" Insolation and Load

This methodology requires the remote, stand-alone photovoltaic system to be sized to meet the load during the "worst month" of the year. The worst month is the one with the smallest ratio of energy falling on the array (insolation) to the energy required by the load. If the system is sized to meet the load during the worst month, it will automatically be sized adequately for all other months.⁶ The worst-month insolation and load values (i.e., values for which the insolation-load ratio is the smallest) are most conveniently identified by setting up a table that lists daily average insolation for each month along with daily average load.

⁵If the daily load variation is sufficiently large, or if load peaks appear on consecutive days, it may be necessary to use the peak load levels in place of monthly averages. Otherwise, the system may be inadequately sized to accommodate cloudy periods coinciding with these high load periods.

⁶System designers will often reduce the required array size and system cost by relying on "long term storage" in which energy stored during months of high insolation will be held for use during months of low insolation. In the present sizing method, the worst-month approach has been adopted to provide a somewhat more conservative size estimate.

In Table 2-1, the insolation data (in kWh/m²-day) are those listed in Appendix D for China Lake, California; the load data (in kWh/day) were chosen arbitrarily to illustrate the procedure. Note that in the table, the load data are listed next to insolation data corresponding to three different array tilt angles. The sizing procedure uses these insolation-load ratios in order to accommodate non-constant insolation and loads over the year. The three tilt angles, tilt equal to latitude, latitude +15 deg, and latitude -15 deg, will typically bound the range of array orientations required to best match the load whether the load is constant year round, winter peaking, or summer peaking. Using the tabular approach described below will assure a good estimate of the minimum array size necessary to serve the load regardless of the annual load pattern.

Table 2-1. Example of Method for Determining the Appropriate Insolation and Load Combinations for Sizing the Array and Battery Storage. (Sample Insolation Data are for China Lake, California.) Note that the example load is month-dependent, i.e., not constant (see text for details).

Month	Tilt Angle = Latitude -15 deg	Tilt Angle = Latitude	Tilt Angle = Latitude +15 deg
	Insolation (I) ÷ Load (L _{td}) = ____	Insolation (I) ÷ Load (L _{td}) = ____	Insolation (I) ÷ Load (L _{td}) = ____
January	3.88 ÷ 2.8 = 1.39	4.38 ÷ 2.8 = 1.56	4.63 ÷ 2.8 = 1.65*
February	4.77 ÷ 2.8 = 1.70	5.13 ÷ 2.8 = 1.83	5.20 ÷ 2.8 = 1.86
March	6.19 ÷ 2.5 = 2.48	6.34 ÷ 2.5 = 2.54	6.13 ÷ 2.5 = 2.45
April	7.33 ÷ 2.5 = 2.93	7.07 ÷ 2.5 = 2.83	6.46 ÷ 2.5 = 2.58
May	7.88 ÷ 2.5 = 3.15	7.26 ÷ 2.5 = 2.90	6.32 ÷ 2.5 = 2.53
June	8.30 ÷ 2.5 = 3.32	7.50 ÷ 2.5 = 3.00	6.38 ÷ 2.5 = 2.55
July	8.07 ÷ 2.5 = 3.23	7.43 ÷ 2.5 = 2.97	6.45 ÷ 2.5 = 2.58
August	8.63 ÷ 2.5 = 3.45	8.34 ÷ 2.5 = 3.34	7.61 ÷ 2.5 = 3.04
September	7.16 ÷ 2.0 = 3.58	7.36 ÷ 2.0 = 3.68	7.14 ÷ 2.0 = 3.57
October	5.88 ÷ 2.0 = 2.94	6.41 ÷ 2.0 = 3.21	6.57 ÷ 2.0 = 3.29
November	4.53 ÷ 2.0 = 2.27	5.17 ÷ 2.0 = 2.59	5.51 ÷ 2.0 = 2.76
December	3.82 ÷ 2.8 = 1.36	4.43 ÷ 2.8 = 1.58	4.78 ÷ 2.8 = 1.71

To determine the worst-month insolation and load values, Table 2-1 is applied as follows. In the columns below each tilt angle, enter the insolation value for each month as it appears in Appendix D for the appropriate application site. To the right of each insolation value, enter the calculated daily average load value for each month (see Step 1). The same load values should appear in each of the three tilt angle columns. Note that in the case of a constant, year-round load, all load values in the table will be identical. For each pair of insolation and load values, calculate the ratio of insolation to load, as shown. For each tilt angle column, select and circle the smallest resulting ratio. There may be duplicate values in one or more columns. Next, select the largest of the circled values. This value is indicated by "*." This value is a best estimate of the worst-month insolation/load ratio for the example application. Insolation and load values obtained in this manner are used in the following sizing steps. In Table 2-1, these values appear in boxes. Note that in this example, the array tilt angle selected is latitude +15 deg, denoting the choice that the array is oriented to serve a winter peaking load.

4. Determine Array and Battery Storage Sizing Factors

The next step in the sizing procedure is to determine the factors for array and battery sizing to be used in subsequent calculations of the actual array size and battery storage capacity.⁷ These factors have been derived from prior analyses of how the photovoltaic system loss of energy probability (LOEP) depends on array and battery size for a range of possible worst-month insolation levels (Reference 4).⁸ By determining the required size of array and battery storage per unit of load, dependent on the worst-month insolation, the proper array and battery sizes can then be calculated using insolation and load values determined in Step 3, above.

This probability value is the "worst-month LOEP;" i.e., the probability that the system will be unable to meet load requirements during the month having the smallest insolation/load ratio. The methodology in this document is based on a worst-month LOEP value of 0.1. This LOEP value for the worst insolation month corresponds to a monthly average LOEP of approximately 0.02-0.04. This value will provide a service availability roughly equivalent to that of conventional competitor power systems such as diesel, etc. If comparing photovoltaic to other renewable energy systems, an equivalent availability analysis is required for the other technologies. Reference 3 also presents results for LOEP values of 0.01 and 0.001; i.e., higher system availabilities. (Generalized approaches are described in References 4 and 5 which allow sizing the system to any LOEP value that may be required by the specific application.) It should be noted that the LOEP is based on the characteristics of insolation only and does not take into account photovoltaic equipment reliability.

⁷Adapted from Reference 3.

⁸The loss of energy probability is an estimate of the probability that during a given time period, the energy output of the power system will be insufficient to meet the energy load demand.

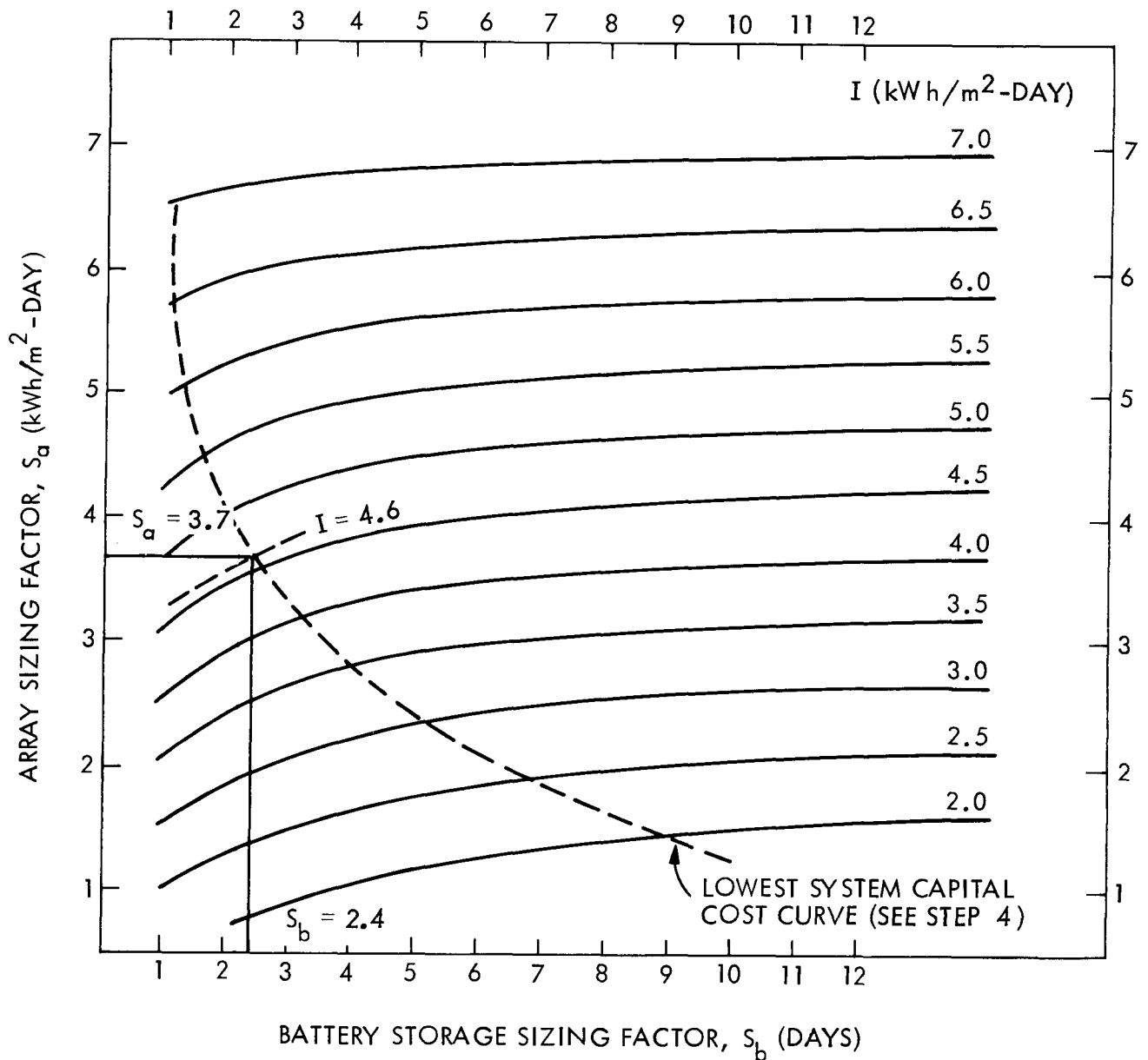


Figure 2-3. Determining Array and Battery Storage Sizing Factors (at LOEP = 0.1) for Various Worst-Month Insolation Values. (Adapted from Reference 3)

The sizing factors for the array and battery storage appear in Figure 2-3 in the form of a nomograph. In the nomograph, the solid curves each correspond to an insolation value as marked. Each solid curve shows the relationship between the array sizing factor, S_a , and the battery storage sizing factor, S_b , for that insolation value. S_a and S_b values to be used in subsequent array sizing calculations are selected by first choosing the solid curve whose worst-month insolation value equals that found by the method in Step 3. Interpolation may be used to obtain more precise results. A trial point on the selected solid curve is chosen next: the point of

intersection of the dashed line with the solid curve is the best initial choice. (The significance of the dashed line will be discussed below.) The array sizing factor, S_a , is found by extending a horizontal line from that point on the curve to the scale on the left of the nomograph. Similarly, the battery sizing factor, S_b , is found by extending a vertical line down from the same point on the solid curve to the scale at the bottom of the nomograph.

An example is shown in Figure 2-3 for the case in which the worst-month insolation = 4.6 (see Table 2-1). Any point on a given insolation curve will result in a worst-month LOEP exactly equal to 0.1. Different points on the insolation curve, however, will result in different combinations of array and battery sizes. For example, selecting a point on the solid curve farther to the left will result in a system with larger array and smaller battery storage, although it will still provide the same level of power availability (i.e., the same LOEP).

System capital cost will vary for different battery and array size combinations. For this reason, a dashed line intersecting the solid curves also appears in the nomograph. The intersection of the dashed line with the relevant insolation level defines the sizing factors that lead to lowest photovoltaic system capital costs for each insolation curve as derived from earlier photovoltaic component cost experience in remote, stand-alone system applications (Reference 3). The dashed line may thus be used as a guide for the initial selection of sizing factor values.

It should be recognized, however, that use of this dashed curve will not necessarily result in a lowest life-cycle cost estimate since it is based only on initial system capital costs. Other life-cycle cost factors such as operation, maintenance, and various financial parameters, have not been incorporated into the nomograph. Furthermore, since photovoltaic array costs are expected to decline in the future more rapidly than battery costs, the lowest capital cost system configuration is likely to be determined from points on the curves to the left of the present dashed line. The recommended approach in using this methodology is to initially select the point of intersection of the dashed line and the solid line nearest the worst-month insolation for the site. After determining the corresponding S_a and S_b values and calculating the array and battery storage sizes, the life-cycle cost should be computed according to the procedure in Section III. If it is found in this initial cost estimate that the photovoltaic system appears less economical than its competitors, additional array/battery size combinations should be examined. In this case, points on the solid curve to the left and right of the original point are chosen, corresponding array and storage sizes are calculated, and new life-cycle costs estimated. This process may be repeated until an approximate lowest (i.e., local optimum) life-cycle cost is obtained.

a. Determine Sizing Factors for a Specified Number of Sunless Days.
A photovoltaic system will frequently have to be sized under the condition that the system must be able to serve the load for a specified number of consecutive sunless days (or days of autonomy). The nomograph in Figure 2-3 may also be applied in these circumstances, but its use is somewhat different.

In this case, the specified number of sunless days is simply used as the battery sizing factor, S_b . The user is cautioned that the chosen S_b must be at least as large as the S_b displayed in Figure 2-3 to ensure adequate power to serve the load and recharge batteries at the stated level of reliability (i.e., LOEP = 0.1). From the point on the scale in Figure 2-3 where S_b is equal to the number of sunless days, a vertical line is drawn to intersect the solid curve whose value is closest to the appropriate worst-month insolation. From this intersection point, a line drawn left to the S_a scale determines the proper value of S_a . Sizing the system according to a specified number of sunless days generally will not yield the lowest capital-cost system having a given LOEP. However, specialized requirements of the application (e.g., very high reliability requirements as in the case of microwave repeaters) will sometimes dictate this approach.

b. Estimate Load Fractions Supplied by the Array and Storage. The energy load fraction supplied by the array, f_a , is that portion of the load energy that flows directly from the array, via an inverter or converter if one is used. The fraction f_b is the portion of the load supplied from battery storage. By definition, $f_a + f_b = 1$. Energy that flows from the array through battery storage is subjected to greater losses than that flowing directly from array to load. Therefore, the relative sizes of f_a and f_b will affect the required size of the array.

The equation to be used to calculate the array size in this methodology (Equation (2)) contains the load fractions f_a and f_b . However, precise calculation of the load fractions is difficult due to varying photovoltaic output by time of day and can be additionally complicated for complex or irregular load profiles. A means of estimating these fractions is described in Appendix B. The user may prefer to use the simplifying assumption that all of the array energy passes through the battery storage before passing to the load; i.e., letting $f_a = 0$ and $f_b = 1$. This is a conservative approach that tends to overestimate the system size since in most applications the load in part is supplied directly from the array, thus avoiding storage losses. For today's component efficiencies, the degree of oversizing will range from 0 to 25%, respectively, for the case of a nighttime-only load and the case in which load and array output are perfectly matched. The degree of oversizing for a constant, 24-hours/day load is typically less than 10%.

5. Calculate Array Power and Area

Calculating the array size means calculating both its peak power output in watts and its area in square meters. Both results are required for system costing.

The array size calculation requires the worst-month load value, L_{td} (determined in step 3), the array sizing factor, S_a (found from Figure 2-3), and the load fractions f_a and f_b . Also, the efficiencies of the storage batteries, voltage regulator, and inverter or converter are required. Typical values of these efficiencies appearing in Appendix A may be used in case they are not otherwise available. Finally, a factor, F , will be included in the

array calculation to account for array degradation over the lifetime of the system. This factor initially oversizes the array slightly to ensure that the system will meet load requirements until the end of its design life despite gradual array power output degradation.

The required array power is now calculated from Equation (2).

$$P_a = \frac{L_{td} \times 1000}{S_a \times F \times e_{i/c} [f_b (e_{vr} \times e_b) + f_a]} \quad (2)$$

where

P_a = array power in watts

L_{td} = energy load value in kilowatt-hours/day

S_a = array sizing factor in kilowatt-hours per square meter per day

$e_{i/c}$ = inverter or converter efficiency at maximum steady state load, if used; otherwise, $e_{i/c} = 1$

F = factor to account for array degradation over the system lifetime

e_{vr} = efficiency of voltage regulator if used; otherwise, $e_{vr} = 1$

e_b = battery efficiency

f_a = fraction of load energy supplied directly by the array

f_b = fraction of the load energy supplied from battery storage

1000 = 1000 watts/m²; a term to convert S_a into an equivalent number of hours per day that 1000 watts/m² insolation would be received by the array

This equation may also be applied to systems without storage. As in the case with storage, the array output energy on an average daily basis must match the average daily load energy requirements. Equation (2) can be applied by setting $f_b = 0$, $f_a = 1$, $e_b = 1$, and S_a = the worst-month insolation value. Note that in this case the LOEP of the photovoltaic system has not been estimated; thus, this case departs from the comparable-reliability sizing approach that underlies the balance of the document.

Array area is based on the array power level determined in Equation (2) and is shown in Equation (3) below:

$$A_a = \frac{P_a}{e_m [1 + P_{TC} (T_{op} - 28^{\circ}\text{C})] \times 1000} \quad (3)$$

where

A_a = array area in square meters

P_a = array power in watts obtained from Equation (2)

e_m = module efficiency at standard test conditions (STC)

P_{TC} = module temperature coefficient; typically = $-0.005/^{\circ}\text{C}$

T_{op} = actual module operating temperature in degrees Celsius. For temperate climates, use the nominal operating cell temperature (800 mW/cm², 20°C ambient, 1 m/s wind speed, 1.5 air mass) (NOCT). For hot climates (peak summer temperature over 110 to 115°F), use NOCT +10°C

1000 = 1000 W/m² at standard test conditions

6. Calculate Battery Storage Size

The next step in sizing the system is to calculate the required size of the battery storage in kilowatt-hours. Battery storage size is based on S_b from Figure 2-3 (or on a prior specification of the number of sunless days) and an allowance for the "depth of discharge" limit on the batteries. Operating within this limit prolongs battery life and protects the batteries in applications subject to freezing temperatures. Calculating the required battery capacity also requires the worst-month load value previously used in the array sizing equations. Finally, the inverter or converter efficiency used to calculate storage size is the same value used for the array calculation.

The required battery storage size is calculated using Equation (4).

$$E_b = \frac{L_{td} \times S_b}{d \times e_{i/c}} \quad (4)$$

where

E_b = rated battery energy storage in kWh

L_{td} = worst-month average daily load value in kWh/day
(see Step 3)

S_b = battery sizing factor in days

d = maximum allowable depth of discharge

$e_{i/c}$ = efficiency of the inverter or converter. If neither is used, $e_{i/c} = 1$

7. Determine Voltage Regulator Size

The battery charging voltage regulator is sized to handle the maximum amount of array output power likely to be available for charging the batteries. For conservatism, the regulator [or battery protector as it is known for small systems (<3 kW)] must be able to handle the array output at noon on a cold, clear day with the load disconnected. The voltage regulator is therefore sized to match array output at standard test conditions (1 kW/m², 28°C cell temperature).

8. Determine Inverter or Converter Size

The inverter or converter typically is sized according to the maximum steady-state load power requirement in watts, ac or dc, respectively. However, if the photovoltaic system is to be used to power an inductive load, the inverter must be able to supply the full surge current required by the load. In the case of an induction motor, the starting current can be as large as 4 to 5 times the rated motor requirements.

SECTION III

SYSTEM COST ANALYSIS

A. SCOPE

Cost effectiveness is the primary criterion for evaluation of candidate photovoltaic system applications. This section presents the life-cycle costing methodology to be used for determining photovoltaic system cost effectiveness. The methodology is intended primarily for estimating the viability of a photovoltaic power system compared to a non-photovoltaic power alternative, rather than precise energy cost estimation. Furthermore, it is solely intended for use by Government agencies since use by private entities would involve additional considerations such as the effect of taxes.

B. COST ANALYSIS METHODOLOGY

To determine whether a photovoltaic system is cost effective in a given application, the life-cycle cost of the photovoltaic system should be compared to the life-cycle cost of the alternative power system such as diesel generator, batteries, utility grid connection, or renewable energy technologies (see Figure 3-1). For the purpose of this comparison, the capabilities of satisfying load (i.e., availability) of all power systems being evaluated are assumed to be identical. The sizing analysis in Section II has been designed to ensure that photovoltaic system performance is adequate to satisfy the specified load.

1. Photovoltaic System Life-Cycle Cost

Photovoltaic power system life-cycle cost is estimated from the initial cost of the system installed at the site and the present value of all recurrent costs associated with system operation. Photovoltaic systems are typically capital intensive (i.e., they require a large initial capital expenditure), but have low operating costs (i.e., zero fuel cost and small expenditures for replacement, operation, and maintenance). The sum of capital and recurrent expenditures represents the equivalent amount of money required at the time of system installation to completely cover all costs associated with the photovoltaic system, including a return on the investment, over its operating lifetime.⁹ Life-cycle cost of the alternative to a photovoltaic system similarly combines the associated first cost and operating cost for comparison with the photovoltaic option.

⁹The "lifetime" of a photovoltaic, or any other power system, may be interpreted as the "financial lifetime" for the purposes of a life-cycle cost analysis. As such, the photovoltaic system operating lifetime provides a guideline, but not a constraint, on the lifetime chosen for the life-cycle cost analysis. Equal lifetimes must be chosen between competing technologies in the cost analysis described in this document.

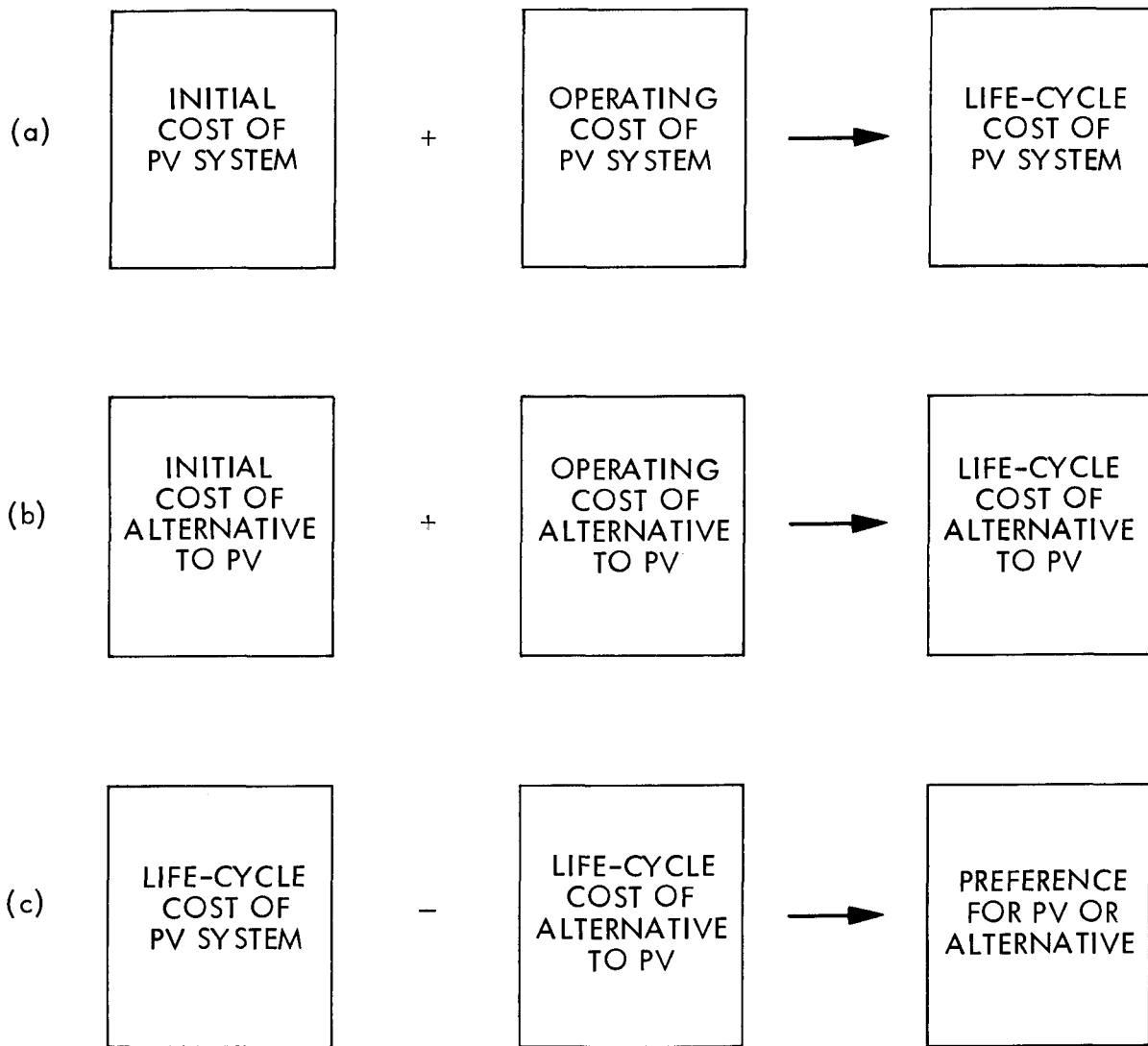


Figure 3-1. Approach for Determining Photovoltaic Power System Cost Effectiveness

The initial cost of a photovoltaic system can be determined from the cost of the array (in \$/W); power-related balance-of-system cost [i.e., battery storage in \$/kWh; voltage regulator in \$/W regulator input power, and inverter (or converter) costs in \$/W ac (or dc)]; area-related balance-of-system costs (i.e., structures and wiring costs in \$/m² of array); system installation and testing cost in percent of equipment cost, and any indirect costs (i.e., engineering and management fees, delivery, and contingency) in percent of equipment cost. Equation (5a) describes the analytical relationships and Equation (5b) displays the detailed procedure for estimating initial installed photovoltaic system cost (IC).

Initial cost = [1 + indirect (%) + installation (%)]

$$\times [\text{delivered equipment cost (\$)}] \quad (5a)$$

$$\begin{aligned} IC = & (1 + IND + INST) [(MOD \times P_a) + (ABOS \times A_a) + (CONV \times W_{DC}) \\ & + (INV \times W_{AC}) + (REG \times W^*) + (BAT \times BWh)] \end{aligned} \quad (5b)$$

where

IND = fractional indirect costs on equipment including engineering, management, and contingency fees

INST = fractional cost on equipment for installation, site preparation, testing, and checkout cost of the system

MOD = module cost in dollars per peak watt of array

P_a = peak watts of solar array (dc)

ABOS = area-related balance-of-system cost per square meter of array including cost of array structure, land, wiring, connectors, etc.

A_a = array area in square meters

CONV = converter cost per peak watt (dc)

W_{DC} = rated size of converter in peak watts (dc)

INV = inverter cost per peak watt (ac)

W_{AC} = rated size of the inverter in peak watts (ac). If more than one inverter is used, sum the peak watts of each. If commercially available inverters do not match the load requirement exactly, select the smallest unit sufficiently large to satisfy the load

REG = voltage regulator cost per peak watt (dc) of maximum regulator input power. (Note that cost may vary as a function of input voltage level)

W^* = maximum voltage regulator input power

BAT = battery cost per kilowatt-hour of energy storage

BWh = battery storage size in kilowatt-hours

Equipment cost estimates are assumed to include delivery to the site. All dollar amounts should be expressed in the same "base year" (e.g., 1984) for

consistency. Current dollar cost estimates based on prior year information will need to be escalated to the appropriate "base-year" level.

In addition to the initial installed system cost described above, recurrent costs associated with photovoltaic system operations are to be included in the estimation of life-cycle cost. Estimates of operation, maintenance, and replacement costs are based on hardware performance characteristics and system operating strategy. Expenditures are primarily for battery replacement (if battery storage is included in the system design) and array, inverter or converter, and battery operation and maintenance. The photovoltaic system operating strategy (e.g., the system may or may not be required to operate autonomously for a prolonged period of time) will affect both the initial system cost and the recurrent costs.

Battery lifetimes are typically between 5 to 10 years depending on manufacturer-specific battery characteristics, number of discharge cycles, design depth of discharge, and operating temperature. In contrast, the anticipated life of a photovoltaic array is estimated to be about 30 years. Battery replacement at regular intervals are, therefore, required throughout the operating lifetime of the photovoltaic array. The cost for each replacement of storage batteries (BR) is shown in Equation (6):

$$BR = (BAT \times BWh) (1 - SV) + LREP \quad (6)$$

where

BAT X BWh = delivered cost of batteries from Equation (5b)

SV = fractional salvage value of batteries at time of replacement

LREP = labor cost of battery replacement (in base-year dollars)

Salvage value of the batteries is typically based on prices in the scrap metal market (e.g., for lead or nickel) at the time of replacement. The present value of the sum of all battery replacements (RPV) over the photovoltaic system lifetime, escalated and discounted to account for the timing of the expenditure, is estimated using Equation (7) as follows:

$$RPV = \sum_{j=1}^{nrep} BR \times \left(\frac{1 + esc_b}{1 + dr} \right)^{j \times k} \quad (7)$$

where

j = counter for number of battery replacements (1, nrep)

k = battery lifetime (years)

$j \times k$ = constrained to be strictly less than photovoltaic system lifetime or lifetime used in life-cycle cost analysis (years)

BR = single-time battery replacement cost from Equation (6) in base-year dollars

esc_b = real (above inflation) annual escalation rate for storage batteries (fraction)

dr = discount rate (cost of money to system owner, typically defined as 10% (real) for Government applications)

Expenditures for replacement of capital equipment (other than batteries) with lifetimes shorter than the assumed photovoltaic system lifetime can also be determined using Equation (7), appropriately modified to reflect their cost and timing. For the purpose of this document, such replacements are considered minimal and are incorporated in the annual operation and maintenance cost equation described below.

Regular operation and maintenance costs can be estimated on an annual cost basis. These costs include expenditures for activities such as array, battery, and inverter maintenance; component replacements (other than batteries); and grounds, structural and electrical upkeep. Annual operation and maintenance costs (OM) can be estimated on the basis of the number of required visits to the site per year times the cost per trip in base-year dollars. A heuristic frequently used to estimate annual operation and maintenance expenditures is to assume that annual expenses are a fixed percentage of the initial cost of equipment. The present value of the cost of operation and maintenance procedures is the derived annual amount summed over the system lifetime, including any real escalation and discounting of expenditures over time. Annual expenditures are, therefore, growing in dollar amount at the constant rate of real escalation, if any. Present value of operation and maintenance cost (OMPV) is presented in Equation (8) as follows:

$$OMPV = OM \times \left(\frac{1 + esc_{om}}{dr - esc_{om}} \right) \times \left[1 - \left(\frac{1 + esc_{om}}{1 + dr} \right)^N \right], \text{ if } dr \neq esc_{om} \quad (8)$$

or

$$OMPV = OM \times N, \text{ if } dr = esc_{om}$$

where

OM = annual operation and maintenance cost in base year dollars

esc_{om} = real (above inflation) annual escalation rate for operation and maintenance activities (fraction), typically 0%

dr = real discount rate (fraction); typically 10%

N = system lifetime (years)

Photovoltaic system life-cycle cost (LCC) can now be determined from its constituent parts described above. Life-cycle cost is displayed in Equation (9) as the sum of the initial installed system cost, Equation (5) and the present value of recurrent costs, Equation (7) plus Equation (8).

$$LCC = IC + RPV + OMPV \quad (9)$$

All costs are in base year dollars. Typical values for parameters in Equation (5b) are presented in an example in Appendix A. As a guide for photovoltaic system cost analysis, initial installed system costs (IC) presently range from approximately \$17 to \$25/watt.

2. Alternative Power System Life-Cycle Cost

Photovoltaic system cost effectiveness is determined by comparison of the photovoltaic system life-cycle cost with the life-cycle cost of the competing energy technology. For a given application, photovoltaics may be competing with fossil fuel, battery, utility grid, or other renewable energy alternatives. In this section of the report, the cost of alternative technologies to photovoltaics are characterized. Section III.B.3 selects the least-cost non-photovoltaic alternative as the basis for the cost-competitiveness assessment.

Small stand-alone photovoltaic systems are potentially competitive with a number of alternatives including diesel generators, batteries, extension of a distant utility grid, and other current solar technologies. The life-cycle cost estimated for each alternative is consistent with the photovoltaic cost approach shown in Equation (9). Initial installed costs (IC), present value of capital replacements over the system lifetime (RPV), and present value of operation and maintenance costs (OMPV) are summed to their respective life-cycle cost. For the purpose of this analysis, the capability of all power systems to satisfy load (i.e., their availability) is assumed to be identical.

Diesel power generation systems require initial capital expenditures for diesel generators, a fuel storage system, and installation (IC). Diesel generators will require periodic repair, overhaul, and replacement within the time frame of the analysis (approximately 20 to 30 years). Recurrent maintenance and fuel costs for these types of systems are also of great importance. In many remote, stand-alone applications, the cost of fuel, labor, transportation and materials can be significant. Estimation of annual diesel generator operation and maintenance costs (OM) should be based on actual cost data.

Initial capital costs for battery systems are estimated in a manner similar to the battery cost term in Equation (5b), $Bat \times BWh$, plus the cost of associated control equipment, indirect costs, and installation. However, the battery system in this case must be sized to satisfy the entire load, accounting for system inefficiencies and assumed interval between recharges. Battery lifetimes are less than that of photovoltaic systems and thus will require replacement at regular time intervals within the assumed 20 to 30 year photovoltaic system lifetime. Battery electrical characteristics, cycling requirements, depth of discharge, and operating temperature contribute to the estimate of battery life. The present value of the cost of replacement is calculated as described in Equations (6) and (7). Remaining salvage value of used batteries is explicitly taken into account. Operation and maintenance costs, Equation (8), include battery inspections, recharge, and equalization at regular intervals depending on battery capacity, load being served, and depth of discharge.

Extension of an existing utility grid line can be very expensive for a remote application with a relatively small load. The costs for extending grid power to a remote site and for the kilowatt-hour meter are treated as initial capital costs (IC). Cost estimates for this equipment can be obtained from the local utility company. Once the utility line is installed, the primary recurrent cost is the cost of energy to serve the load. Current utility rate structures provide the basis for this cost over the photovoltaic system lifetime (OMPV). Note that in some locations, utility reliability may also be a factor in the comparison between photovoltaics and utility-supplied power.

Life-cycle cost estimates for other renewable energy alternatives (non-photovoltaic) require cost information as described in Equation (9). Specific system design and associated cost inputs will need to be developed by the organization performing the system comparison.

In addition to competing with the capital and operating costs associated with installing capacity to satisfy a new load is the potential for photovoltaics to operate in a fuel-displacement mode for an already existing application. Energy cost-intensive technologies in remote areas may provide a potentially cost effective use for photovoltaic technology. Though there would be no savings for initial capital expenditure on the alternative technology, the photovoltaic system would provide savings on operation and maintenance cost (OMPV) and, potentially, on delaying capital replacement (RPV) of the non-photovoltaic alternative. In this fuel-displacement mode, daytime photovoltaic system output can be used to satisfy coincident load. Battery storage can be added if it is found to be cost effective in this application. Either with or without battery storage, reliability of the alternative technology combined with the photovoltaic system would be enhanced.

C. PHOTOVOLTAIC VERSUS ALTERNATIVE POWER SYSTEM COST COMPARISON

Photovoltaic system cost competitiveness can be determined by comparison with the least-cost non-photovoltaic power system that satisfies all performance and reliability requirements. Using the approach displayed in Figure 3-1(c), and repeated in Figure 3-2, the life-cycle cost of the non-photovoltaic system

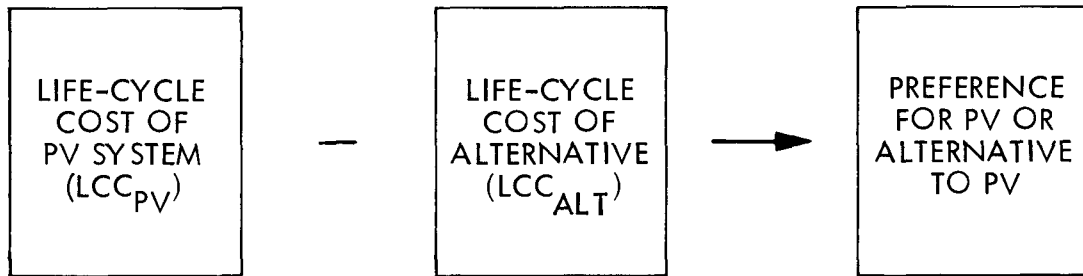


Figure 3-2. Life-Cycle Cost Comparison of Photovoltaic System (LCC_{PV}) and the Non-Photovoltaic System (LCC_{ALT})

(LCC_{ALT}) is subtracted from the life-cycle cost of the photovoltaic system (LCC_{PV}). Three outcomes are possible:

- (1) $LCC_{PV} - LCC_{ALT} < \$0$. The photovoltaic system is cost effective compared to the alternative system. The absolute value of the difference is a first-order measure of the preference for photovoltaics.
- (2) $LCC_{PV} - LCC_{ALT} > \$0$. The photovoltaic system is more expensive than the alternative; thus, it is not cost effective.
- (3) $LCC_{PV} - LCC_{ALT} = \$0$. The photovoltaic and alternative systems are of equal cost in present value terms.

This differential cost (or net present value) measure of cost competitiveness provides the basis for deciding to pursue or terminate photovoltaic system analysis and design activities. If in the initial estimate of photovoltaic system life-cycle cost the system is determined not to be cost effective, the sizing procedure should be repeated from the estimation of array and battery sizing factors (see discussion, Section II-4).

If the photovoltaic system is determined to be cost effective (or reasonably close to cost effective) for a specific application, it is useful to perform a sensitivity analysis on important cost parameters over an appropriate range of values. This sensitivity analysis is useful to the decision maker since small variations in cost drivers, such as escalation in diesel fuel or electricity prices over the system lifetime and the price of photovoltaic modules, can significantly alter the relative preference for competing power systems. The result of this analysis is an understanding of the effect of uncertainty in parameter values on photovoltaic system cost effectiveness.

SECTION IV

REFERENCES

1. Solar Photovoltaic Applications Seminar: Design, Installation and Operation of Small, Stand-Alone Photovoltaic Power Systems, U.S. Department of Energy, DOE/CS/32522-T1, July 1980.
2. Designing Small Photovoltaic Power Systems, Monegon, Ltd; Gaithersburg, Maryland, May 1981.
3. Rosenblum, L., Practical Aspects of Photovoltaic Technology, Applications, and Cost, NASA CR-168025, December 1982.
4. Macomber, H.L., Ruzek, J.B., Photovoltaic Stand-Alone Systems, DOE/NASA/0195-1, NASA CR-165352 M206, August 1981.
5. Bucciarelli, L.L., Jr., "Estimating Loss of Power Probabilities of Stand-Alone Photovoltaic Solar Energy Systems," Solar Energy, Vol. 32, No. 2, pp. 205-209, 1984.
6. Photovoltaic Product Directory and Buyers Guide, Pacific Northwest Laboratories, Battelle Memorial Institute, prepared for U.S. Department of Energy, PNL-5052, April 1984.
7. Simon, F., "Conceptual Design of Photovoltaic Medical Systems for Rural Health Applications," NASA LeRC Report No. 4210-055, March 1981.
8. Smith, J.H., Handbook of Solar Energy Data for South-Facing Surfaces in the United States, Vol. 1, DOE/JPL-1012-25, January, 1980.
9. Cartwright, K., Carmichael, H.E., Kamien, J.H., and Siegel, B., Comparison of Photovoltaic and Diesel Engine Systems for Village Power Applications, Aerospace Corporation for NASA Lewis Research Center, May 1980.
10. Cochrane, E.H., Lawson, A.C., and Savage, C.H., Flat-Plate Photovoltaic Power Systems Handbook for Federal Agencies, JPL Publication 84-35, DOE/ET 20356-14, April 1984.

APPENDIX A
PHOTOVOLTAIC SYSTEM SIZING
AND COSTING EXAMPLE

APPENDIX A

PHOTOVOLTAIC SYSTEM SIZING AND COSTING EXAMPLE

This appendix presents an example of sizing and costing a hypothetical photovoltaic system using the methodology described in this report. Estimates of currently relevant photovoltaic system parameter values are shown as a guide for users of the methodology. A sample comparison of photovoltaic system cost effectiveness compared to competing technologies is then presented.

To illustrate the system sizing procedure, an example is presented based on the sample case described in Section II of this report. The application is a small, seasonally variable load located near China Lake, California. Determination of photovoltaic system size follows the step-by-step procedure described in Section II of this document and repeated in Figure A-1. Typical values (and ranges) for several of the photovoltaic system sizing parameters are displayed in Table A-1. The table should be consulted frequently in using this appendix for a description of each parameter name.

Step 1: Calculate Load

Total daily energy load (L_{td}) is determined from Equation (1) as follows:

$$L_{td} = \sum_{i=1}^n P_i D_i / 1000 \quad (1)$$

It is assumed that each season has a separate, single ($n = 1$) ac load (P) for 8 hours/day (D) during daytime hours. The power drawn by the single load i for each month is:

350 watts:	December, January, February
312.5 watts:	March, April, May, June, July, August
250 watts:	September, October, November

The corresponding daily energy load (L_{td}) is 2.8 kilowatt-hours, 2.5 kilowatt-hours, and 2.0 kilowatt-hours, respectively.

Step 2: Determine Local Insolation

Appendix D contains the daily average insolation values for each month of the year and for three array tilt angles for a number of United States sites. Locate the site insolation values for China Lake, California, on page D-2. These values will be used in the following step of the methodology.

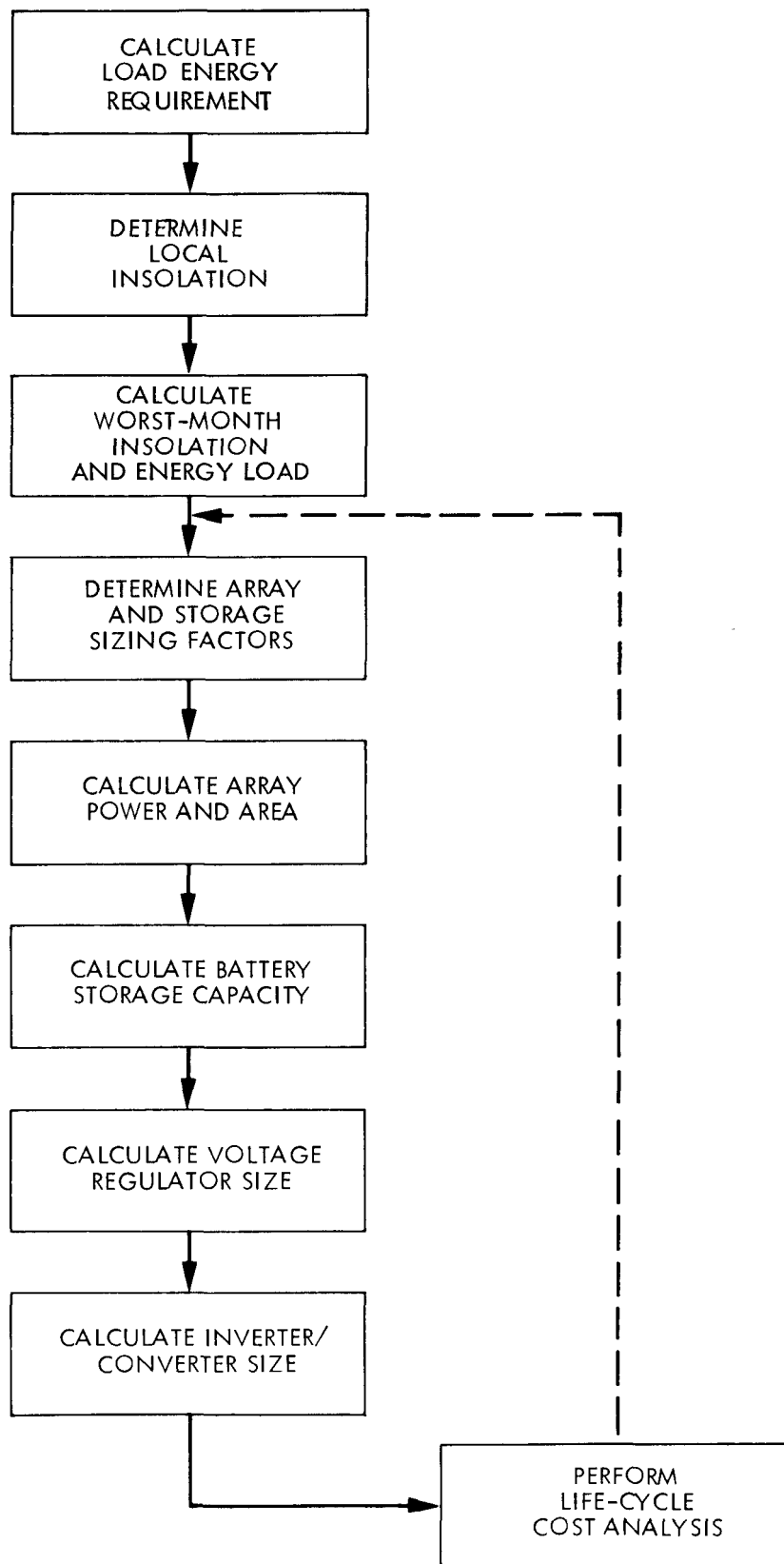


Figure A-1. Photovoltaic System Sizing Procedure

Table A-1. Photovoltaic System Sizing Parameters: Relevant Ranges and Default Values

Parameter	Parameter Name	Units	Range	Value
Array area	A_a	m^2	--	a
Battery depth of discharge	d	fraction	0.05-0.80	0.60
Load i duration	D_i	hours/day	--	b
Battery efficiency	e_b	fraction	0.80-0.90	0.88
Inverter/converter efficiency	$e_{i/c}$	fraction	0.85-0.97	0.93
Module efficiency	e_m	fraction	0.06-0.11	0.10
Voltage regulator efficiency	e_{vr}	fraction	0.85-0.93	0.91
Degradation factor	F	fraction	0.75-0.95	0.85
Load fraction: array	f_a	fraction	--	c
Load fraction: batteries	f_b	fraction	--	c
Worst-month insolation	I	kWh/m^2 -day	--	d,e
Worst-month load	L_{td}	kWh/day	--	b,e
Load i power requirement	P_i	watts	--	b
Array power requirement	P_a	watts	--	f
Module temperature coefficient	P_{TC}	fraction/ $^{\circ}C$	-0.005	-0.005
Array sizing factor	S_a	kWh/m^2 -day	--	g
Battery sizing factor	S_b	days	--	g
Module operating temperature	T_{op}	$^{\circ}C$	45-55	48 or 55 ^h

^aSee Equation (3).

^bSee Equation (1).

^cSee Appendix B.

^dSee Appendix D.

^eSee Table 2-1.

^fSee Equation (2).

^gSee Figure 2-3.

^hTemperate climate = 48 $^{\circ}C$ and hot climate = 55 $^{\circ}C$.

Step 3: Calculate Worst-Month Insolation and Load

Construct a table of monthly insolation and load values using the information generated from steps 1 and 2. Display them as shown in Table A-2, below. (This example is the same as shown in Table 2-1). For each month and tilt angle, divide the insolation value by the load and enter the ratio into the table.

For each tilt angle column shown in Table A-2, identify the month with the smallest ratio of insolation-to-load. Next, select the largest one of these values (identified by "*"). The insolation ($I = 4.6$) and load ($L_{td} = 2.8$) values corresponding to this particular value are the ones to be used in later sizing steps. This allows the system (array and battery) to be sized sufficiently large to supply the load for the worst month (i.e., month of lowest insolation relative to load) and allows some optimization of array and

Table A-2. Monthly Insolation and Example Energy Load Values for Three Array Tilt Angles for China Lake, California

Month	Tilt Angle = Latitude -15 deg	Tilt Angle = Latitude	Tilt Angle = Latitude +15 deg
	Insolation (I) ÷ Load (L_{td}) = ____	Insolation (I) ÷ Load (L_{td}) = ____	Insolation (I) ÷ Load (L_{td}) = ____
January	$3.88 \div 2.8 = 1.39$	$4.38 \div 2.8 = 1.56$	$4.63 \div 2.8 = 1.65^*$
February	$4.77 \div 2.8 = 1.70$	$5.13 \div 2.8 = 1.83$	$5.20 \div 2.8 = 1.86$
March	$6.19 \div 2.5 = 2.48$	$6.34 \div 2.5 = 2.54$	$6.13 \div 2.5 = 2.45$
April	$7.33 \div 2.5 = 2.93$	$7.07 \div 2.5 = 2.83$	$6.46 \div 2.5 = 2.58$
May	$7.88 \div 2.5 = 3.15$	$7.26 \div 2.5 = 2.90$	$6.32 \div 2.5 = 2.53$
June	$8.30 \div 2.5 = 3.32$	$7.50 \div 2.5 = 3.00$	$6.38 \div 2.5 = 2.55$
July	$8.07 \div 2.5 = 3.23$	$7.43 \div 2.5 = 2.97$	$6.45 \div 2.5 = 2.58$
August	$8.63 \div 2.5 = 3.45$	$8.34 \div 2.5 = 3.34$	$7.61 \div 2.5 = 3.04$
September	$7.16 \div 2.0 = 3.58$	$7.36 \div 2.0 = 3.68$	$7.14 \div 2.0 = 3.57$
October	$5.88 \div 2.0 = 2.94$	$6.41 \div 2.0 = 3.21$	$6.57 \div 2.0 = 3.29$
November	$4.53 \div 2.0 = 2.27$	$5.17 \div 2.0 = 2.59$	$5.51 \div 2.0 = 2.76$
December	$3.82 \div 2.8 = 1.36$	$4.43 \div 2.8 = 1.58$	$4.78 \div 2.8 = 1.71$

battery size as influenced by the potential benefit of varying array tilt angle. In this example, the array tilt angle of latitude +15 deg is preferred based on January insolation and load conditions.

Step 4: Determine Array and Storage Sizing Factors

Using the results from Table A-2, insert the relevant insolation value (4.6 kWh/m²-day) into Figure 2-3 (repeated as Figure A-2). For an initial estimate of array and battery sizing factors (S_a) and (S_b), respectively, locate the intersection of insolation (I) equal to 4.6 and the dashed line. The resulting array sizing factor S_a is 3.7 and battery sizing factor S_b is 2.4.

Based on the monthly load and insolation levels, the fraction of the load supplied directly by the array (f_a) can be estimated. For this example, 50% of the load served directly by the array is predicted (see step 1 for the assumptions on loads). Therefore, array fraction $f_a = 0.5$ and battery fraction $f_b = 0.5$.

Step 5: Calculate Array Power and Area

Array size (P_a) is now calculated using Equation (2) as follows:

$$\begin{aligned}
 P_a &= \frac{L_{td} \times 1000}{S_a \times F \times e_{i/c} [f_b (e_{vr} \times e_b) + f_a]} \quad (2) \\
 &= \frac{2.8 \times 1000}{3.7 \times 0.85 \times 0.93 [0.5(0.91 \times 0.88) + 0.5]} \\
 &= 1063 \text{ watts}
 \end{aligned}$$

Array area (A_a) associated with this array size is determined using Equation (3) below:

$$\begin{aligned}
 A_a &= \frac{P_a}{e_m [1 + P_{TC} (T_{op} - 28^\circ\text{C})] \times 1000} \quad (3) \\
 &= \frac{1063}{0.10 [1 - 0.005(55 - 28)] \times 1000} \\
 &= \frac{1063}{86.5} = 12.3 \text{ m}^2
 \end{aligned}$$

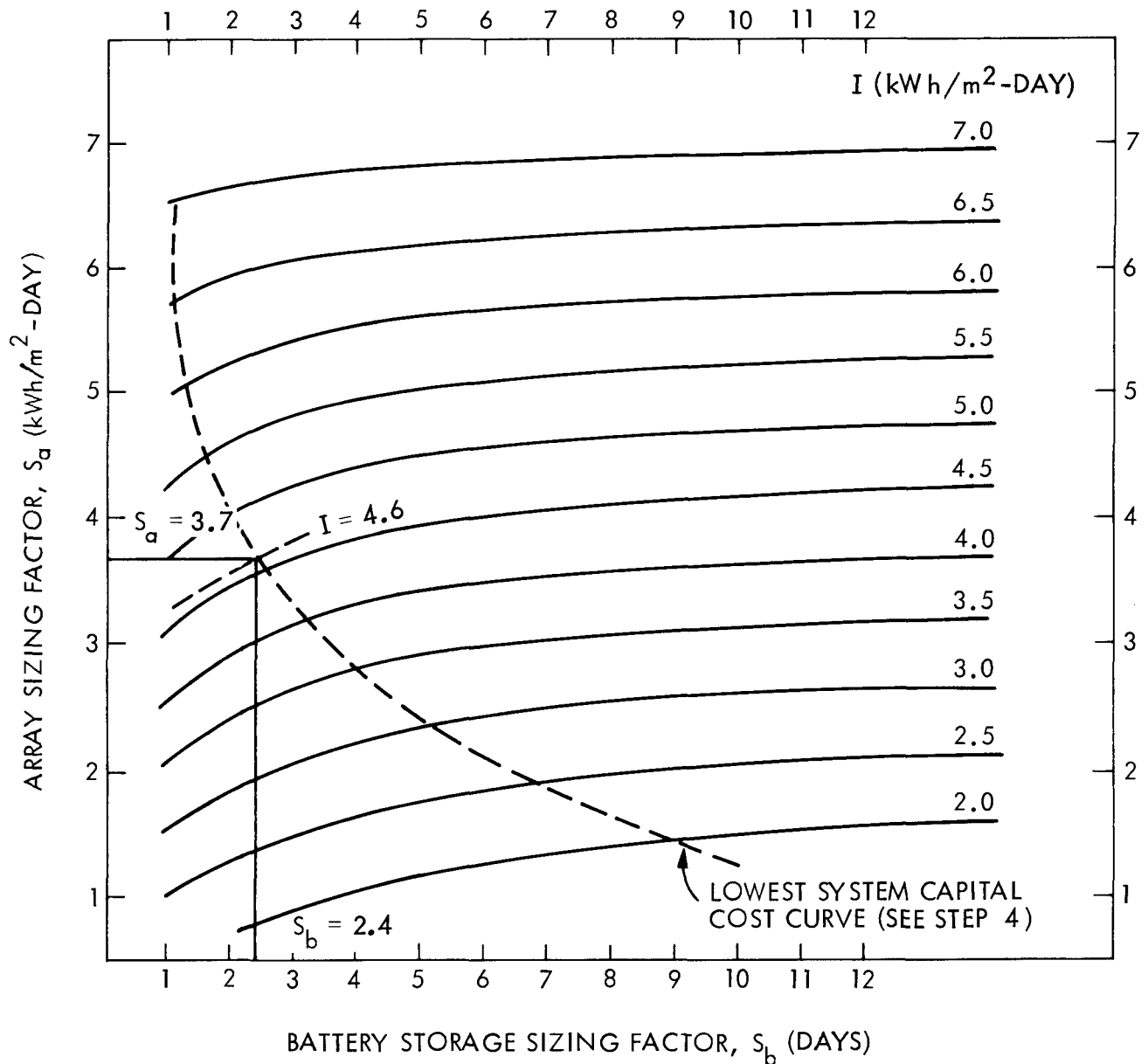


Figure A-2. Determining Array and Battery Storage Sizing Factors (at LOEP = 0.1) for Various Worst-Month Insolation Values. (Adapted from Reference 3)

For the purpose of this example, China Lake, California, is considered a hot climatic area. Therefore, module operating temperature (T_{op}) reflects the high point of the temperature range (55°C) rather than the typical value of 48°C (which reflects nominal operating cell temperature (NOCT) at 800 W/m², 20°C ambient air temperature, and air mass 1.5).

Step 6: Calculate Battery Storage Capacity

Battery storage (E_b) required for this application is based on the average daily load for the worst month of the year (L_{td} , from step 3), the battery sizing factor (S_b) based on the system reliability chart (Figure A-2), battery depth of discharge limit (d), and inverter efficiency ($e_{i/c}$). These factors are combined in Equation (4) as follows:

$$\begin{aligned} E_b &= \frac{L_{td} \times S_b}{d \times e_{i/c}} \\ &= \frac{2.8 \times 2.4}{0.6 \times 0.93} = 12.0 \text{ kWh} \end{aligned} \tag{4}$$

Step 7: Calculate Voltage Regulator Size

The voltage regulator is sized at the peak array output at standard test conditions (1 kW/m^2 and 28°C cell temperature) and assumes no load. Voltage regulator size is, therefore, 1063 watts.

Step 8: Calculate Inverter/Converter Size

In order to satisfy the peak power requirements of the load, 350 watts during the winter months, an inverter size of 350 W ac is required, assuming that the load is not inductive.

Having completed the sample photovoltaic system sizing analysis, the estimation of system life-cycle cost follows. As necessary, array and battery size refinements may be made so that life-cycle cost is reduced while retaining equivalent reliability (see the life-cycle costing iteration step in Figure A-1).

The cost analysis is composed of three parts. First, photovoltaic system life-cycle costs are estimated. Second, the cost of alternative energy systems in competition with photovoltaics are determined. Finally, the alternative energy generation systems are compared on the basis of least cost. Figure A-3 displays the procedure.

Typical values and ranges for the current cost of photovoltaic equipment (in 1984 dollars, delivered to the site) and operational attributes (e.g., battery lifetime) are presented in Table A-3. Data is based on available information for small stand-alone systems, current cost estimates, and catalog information (e.g., see Reference 6). The table should also be consulted throughout this appendix for a description of each parameter name.

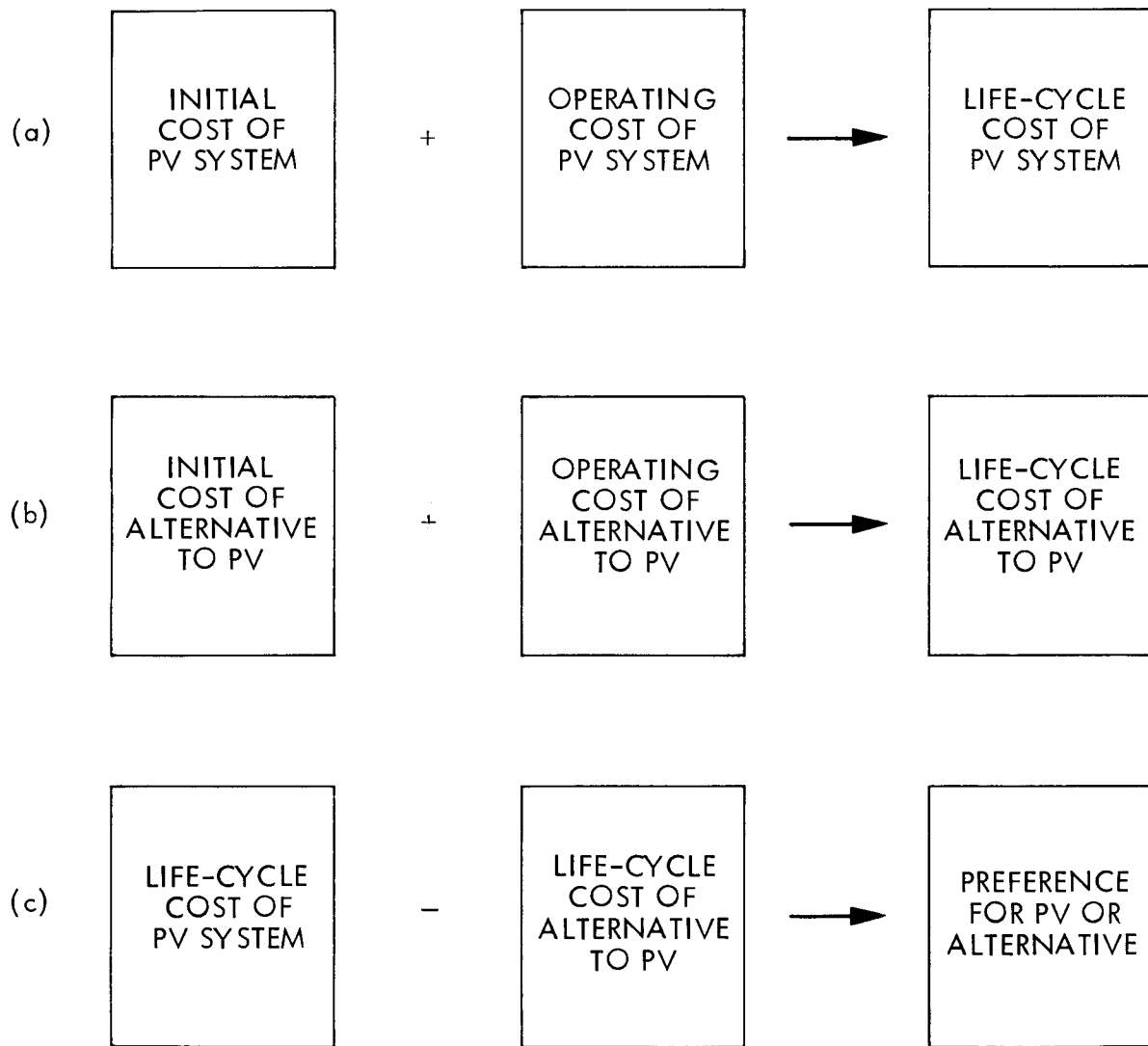


Figure A-3. Approach for Determining Photovoltaic System Cost Effectiveness

Photovoltaic system life-cycle cost is determined in three steps: estimation of initial cost, estimation of operating costs, and summation to life-cycle cost. These steps are illustrated below:

Step 1. Estimate Initial Cost of Photovoltaic System

The initial cost of a photovoltaic system (IC) includes expenditures for capital equipment, installation, testing, and any indirect costs as shown in Equation (5a) below:

$$\begin{aligned} \text{Initial cost} &= [1 + \text{indirect (\%)} + \text{installation (\%)}] \\ &\quad \times [\text{delivered equipment cost (\$)}] \end{aligned} \quad (5a)$$

Table A-3. Photovoltaic System Cost Parameters:
Relevant Ranges and Default Values

Parameter	Parameter Name	Units	Range	Value
Array-related BOS cost	ABOS	$\$/M^2$	20-300 ^a	150
Array area	A_a	M^2	--	^b
Battery cost	BAT	$\$/kWh$	50-250	80
Battery storage size	BWh	kWh	--	^c
Converter cost	CONV	$\$/W_{dc}$	0.70-200	0.80
Discount rate (real)	dr	fraction	0.10 ^d	0.10
Battery cost escalation rate (real)	esc_b	fraction	0-0.03	0
OM cost escalation rate (real)	esc_{om}	fraction	0-0.1	0
Indirect cost	IND	fraction	0.10-0.25	0.16
Installation and testing cost	INST	fraction	0.20-0.50	0.30
Inverter cost	INV	$\$/W_{ac}$	0.30-0.80	0.40
Battery lifetime	k	years	5-10	10
Labor cost for battery replacement	LREP	\$	0 ^e	0 ^e
Module cost	MOD	$\$/P_a$	7-10	10
Photovoltaic system lifetime	N	years	20-30	30
Number of battery replacements	nrep	number	2-5	2
Annual OM cost	OM	\$ or fraction	0.005-0.03 ^f	^f
Voltage regulator cost	REG	$\$/W^*$	0.20-0.50	0.45
Battery salvage value	SV	fraction	0-0.2	0.1
Peak watts ac	W_{ac}	watts	--	^g
System peak watts dc	W_{dc}	watts	--	^g
Array peak watts dc	P_a	watts	--	^h
Voltage regulator input power	W^*	watts	--	ⁱ

^aLow-end value reflects very low cost structures and zero land cost.

^bSee Equation (3).

^cSee Equation (4).

^dFor Government applications, a 10% real discount rate is used.

^eIncluded in annual OM cost.

^fRelevant for fraction of delivered equipment cost; see Equation (5a).

Range is based on photovoltaic systems without batteries.

^gSee Section II.C.8.

^hSee Equation (2).

ⁱSee Section II.C.7.

Indirect costs (IND) include engineering, management, and contingency fees and are assumed to be a fractional multiple of delivered equipment cost. Similarly, the cost of installation, site preparation, and test of the photovoltaic system (INST) is assumed to be a fractional multiple of delivered equipment cost. All costs associated with the initial installation of the photovoltaic system, excluding the cost of equipment itself, are to be included in the multipliers described above.

Delivered equipment cost represents the initial capital expenditures for all photovoltaic power-related equipment, structures, inverter or converter, protection equipment (e.g., voltage regulator), and battery-related equipment. Each cost element is described in terms of its "natural units" for costing purposes as shown in Table A-4.

The initial installed cost (IC) of the photovoltaic system can now be presented as in Equation (5b):

$$\begin{aligned}
 \text{IC} = & (1 + \text{IND} + \text{INST}) [(\text{MOD} \times P_a) + (\text{ABOS} \times A_a) + (\text{CONV} \times W_{\text{DC}}) \\
 & + (\text{INV} \times W_{\text{AC}}) + (\text{REG} \times W^*) + (\text{BAT} \times \text{BWh})]
 \end{aligned}
 \tag{5b}$$

Table A-4. Cost Elements

Cost Element	Cost Basis	Engineering Units
Module	Dollars per peak watt of array (MOD)	Peak watts of array power output (P_a)
Area-related balance of system	Dollars per square meter of array (ABOS)	Array area in square meters (A_a)
Inverter or converter	Dollars per rated peak watt ac (INV) or dc (CONV), respectively	Rated size of inverter, watts ac (W_{AC}) or converter, watts dc (W_{DC})
Regulator	Dollars per watt of maximum regulator input power (REG)	Maximum regulator input power, watts (W^*)
Battery-related equipment	Dollars per kilowatt-hour of storage (BAT)	Battery storage size in kilowatt-hours (BWh)

Using the assumed values from Table A-3 and from the sizing analysis, initial installed cost is calculated to be:

$$\begin{aligned} IC &= (1 + 0.16 + 0.30) [(10 \times 1063) + (150 \times 12.3) + (0) \\ &\quad + (0.40 \times 350) + (0.45 \times 1063) + (80 \times 12.0)] \\ &= (1.46) [\$14,053] = \$20,517 \end{aligned}$$

The initial installed system cost (IC) per peak watt of array (P_a) for this example is:

$$\frac{\$20,517}{1063 \text{ watts}} = \$19.30/\text{watt}$$

This falls within the present-day range of \$17 to \$25/watt initial system cost.

Step 2: Estimate Photovoltaic System Operating Costs

In addition to the initial installed system cost described above, recurrent costs associated with photovoltaic system operations are to be included in the estimation of life-cycle cost. Estimates of operation, maintenance and replacement costs are based on hardware performance characteristics and system operating strategy. Expenditures are primarily for battery replacement (if battery storage is included in the system design) and array, power conditioning unit, and battery operation and maintenance.

The cost of each battery replacement (BR) in base year dollars is estimated from the initial cost of batteries shown in Equation (5b), $BAT \times BWh$, less an allowance for salvage value (SV), plus the labor cost for replacement (LREP). This is displayed in Equation (6):

$$BR = (BAT \times BWh) (1 - SV) + LREP \quad (6)$$

Using the financial inputs from Table A-3, battery replacement cost is:

$$\begin{aligned} BR &= (80 \times 12.0)(1-0.1) + 0 \\ &= \$864 \end{aligned}$$

Over the photovoltaic system operating lifetime, a number of battery replacements (n_{rep}) will need to be made. The present value of these

replacements (RPV), escalated (at the real rate, esc_b) and discounted (at a real rate, dr) to account for the timing of the expenditure, is estimated using Equation (7) as follows:

$$RPV = \sum_{j=1}^{nrep} BR \times \left(\frac{1 + esc_b}{1 + dr} \right)^j \times k \quad (7)$$

where k is the battery lifetime. Using the baseline inputs, assuming two replacements during the system lifetime, the present value of battery replacements is:

$$RPV = \sum_{j=1}^2 (864) \times \left(\frac{1.0}{1.1} \right)^j \times 10 = \$462$$

The present value of expenditures for replacement of capital equipment (other than batteries) with lifetimes shorter than the assumed photovoltaic system lifetime can also be determined using Equation (7), appropriately modified to reflect their cost and timing. For the purpose of this example, such replacements are considered minimal and are incorporated in the annual operation and maintenance cost equation described below.

Regular operation and maintenance costs can be estimated on an annual cost basis. These costs include expenditures for activities such as array, battery, and inverter maintenance; component replacements (other than batteries); and grounds, structural, and electrical upkeep. Annual operation and maintenance costs (OM) can be estimated on the basis of the number of required visits to the site per year times the cost per trip in base year dollars. A heuristic frequently used to estimate operations and maintenance expenditures is to assume that annual expenses are a fixed percentage of the initial cost of equipment. The present value of the cost of operation and maintenance procedures is the derived annual amount summed over the system lifetime, including any real escalation (esc_{om}) and discounting (dr) of expenditures over the photovoltaic system lifetime (N). Annual expenditures are, therefore, growing in dollar amount at the constant rate of real escalation, if any. Present value of operation and maintenance cost (OMPV) is presented in Equation (8) as follows:

$$OMPV = OM \times \left(\frac{1 + esc_{om}}{dr - esc_{om}} \right) \times \left[1 - \left(\frac{1 + esc_{om}}{1 + dr} \right)^N \right], \quad \text{if } dr \neq esc_{om} \quad (8)$$

or

$$OMPV = OM \times N, \quad \text{if } dr = esc_{om}$$

For this example, annual operation and maintenance cost is assumed to include site visits once every 2 months for 4 hours per visit at a cost of \$25 per hour. Annual operation and maintenance cost (OM) is therefore \$600. The present value (OMPV) of these expenditures is:

$$\begin{aligned} \text{OMPV} &= 600 \times \left(\frac{1.0}{0.10 - 0} \right) \times \left[1 - \left(\frac{1.0}{1.1} \right)^{30} \right] \\ &= \$5656 \end{aligned}$$

Step 3: Sum to Life-cycle Cost

Photovoltaic system life-cycle cost (LCC) can now be determined from its constituent parts described above. Life-cycle cost is displayed in Equation (9) as the sum of the initial installed system cost, Equation (5), and the present value of recurrent costs, Equation (7) plus Equation (8).

$$\begin{aligned} \text{LCC} &= \text{IC} + \text{RPV} + \text{OMPV} \\ &= \$20,517 + \$462 + \$5656 \\ &= \$26,635 \end{aligned} \tag{9}$$

The life cycle cost in this example is expressed in 1984 dollars.

Cost estimates for alternative power systems in competition with photovoltaics are now required. For illustrative purposes, life-cycle cost estimates are prepared for batteries and diesel generators. Load energy and power requirements are identical to the assumptions used in the photovoltaic system sizing and life-cycle cost assessment.

1. Battery Cost Example

Battery storage size in kWh is based on the energy load, days of storage required between recharging, battery depth of discharge, and inverter or converter efficiency. The sizing algorithm is shown below:

$$\text{Battery size} = \frac{\text{Energy load} \times \text{days of storage}}{\text{Maximum depth of discharge} \times \text{inverter/converter efficiency}}$$

where the maximum daily energy load battery depth of discharge and inverter/converter efficiency are the same as in the photovoltaic example; and required days of storage is based on a first order trade-off between the initial cost of storage and the required recharging and maintenance costs (at the assumed labor rates and maintenance frequency).

Therefore,

$$\text{Battery size} = \frac{2.8 \times \text{days of storage}}{0.6 \times 0.93}$$

Since the operating costs associated with service personnel used to recharge and maintain batteries can be extremely high, sufficient battery storage to supply one month's energy load is assumed in this example. A smaller battery size would require more frequent visits and, thus, be more expensive from a life-cycle cost perspective. It is further assumed that once-a-month site visits for maintenance are required to ensure adequate system performance to satisfy the load. Battery size is thus:

$$\begin{aligned} \text{Battery size} &= \frac{2.8 \times 30}{0.6 \times 0.93} \\ &= 150 \text{ kWh} \end{aligned}$$

Using battery cost estimates from Table A-3, including indirect and installation costs, initial battery system capital cost (IC) is:

$$\text{IC} = (1 + 0.16 + 0.30) (150 \text{ kWh} \times \$80/\text{kWh}) = \$17,520$$

The cost of battery replacement (BR) every k years is based on Equation (6) and the battery assumptions in Table A-3.

$$\text{BR} = (\text{Battery size} \times \text{battery cost per kWh}) \times (1 - \text{salvage fraction}) + \text{labor cost}$$

$$= (150 \times 80) (1 - 0.1) + 0 = \$10,800$$

For this example, labor cost is assumed to be included in the regular operation and maintenance expenditure. In present value terms, battery replacement present value (RPV) per Equation (7) is:

$$\text{RPV} = \sum_{j=1}^{\text{nrep}} \text{BR} \times \left(\frac{1 + \text{esc}_b}{1 + \text{dr}} \right)^{j \times k}$$

Using the values from the previous tables,

$$\begin{aligned} \text{RPV} &= \sum_{j=1}^2 \$10,800 \times \left(\frac{1.0}{1.1} \right)^{j \times 10} \\ &= \$10,800 (0.39 + 0.15) = \$5830 \end{aligned}$$

Annual cost for operation and maintenance includes battery recharging and maintenance on the batteries and balance of system. For this example, monthly site visits are assumed, consistent with the sizing and cost trade-off described above. Each visit requires one maintenance person for 8 hours at \$25 per hour. Annual operation and maintenance cost (OM) for 12 site visits is therefore:

$$OM = 8 \text{ hours/visit} \times \$25/\text{hour} \times 12 \text{ visits/year} = \$2400$$

The cost of equipment used for recharging and maintenance is typically included in the estimate of the labor rate. Over the assumed 30 year lifetime, the present value of operation and maintenance cost (OMPV) is:

$$\begin{aligned} OMPV &= \$2400 \times \left(\frac{1 + \text{esc}_b}{dr - \text{esc}_b} \right) \times \left[1 - \left(\frac{1 + \text{esc}_b}{1 + dr} \right)^N \right] \\ &= \$2400 \times \left(\frac{1.0}{0.10 - 0} \right) \times \left[1 - \left(\frac{1.0}{1.1} \right)^{30} \right] \\ &= \$22,625 \end{aligned}$$

The life-cycle cost (LCC) of the battery system alternative is the sum of the initial installed capital cost (IC), present value of battery replacement cost (RPV), and the present value of operation and maintenance costs (OMPV) as shown below:

$$\begin{aligned} LCC &= IC + RPV + OMPV \\ &= \$17,520 + \$5830 + \$22,625 \\ &= \$45,975 \end{aligned}$$

This life-cycle cost value will be used in the subsequent cost comparison of energy generation system alternatives.

2. Diesel Generator Cost Example

Though the peak power required by the load is 350 W, a standard, small size production diesel generator is typically 3 to 4 kW. In this example, a single 4 kW Kohler diesel generator has been chosen. All unit

capital costs and maintenance requirements are identified in Reference 9. Installed costs in 1980 dollars are shown below:

Diesel generator	\$ 4566
Fuel tank, 500 gallons	400
Valves/piping	125
Mounting frame	50
Engine shelter	750
	<u>\$ 5891</u>

For consistency with the cost estimates for competing technologies, diesel generating installed costs can be inflated from 1980 to 1984 dollars using the Gross National Product Implicit Price Deflator (which results in a multiplier equal to 1.30). Installed cost is therefore $(1.30)(\$5891) = \7658 . This value is assumed to include the cost of system installation. Therefore, diesel generator system initial capital cost (IC) increments this amount only by the indirect cost fraction (16%) as shown below:

$$IC = (1.16)(\$7658) = \$8883$$

The Kohler diesel is a long-life unit that is assumed to require replacement costs equal to the cost of one unit after 15 years. Present value of replacements (RPV) is, therefore, the initial generator cost in 1980 dollars inflated to 1984 dollars by the 1.30 multiplier and discounted for 15 years as:

$$\begin{aligned}
 RPV &= \$4566 (1.30) \left(\frac{1 + \text{esc}_{om}}{1 + dr} \right)^{15} \\
 &= \$4566 (1.30) \left(\frac{1.0}{1.10} \right)^{15} = \$1421
 \end{aligned}$$

Annual expenditures for ongoing operation and maintenance are estimated based on: (1) the operating strategies described and costed in the referenced report, and (2) consistent labor hours and costs for the photovoltaic and battery examples in this appendix. Maintenance schedule and costs in 1984 dollars are shown below:

200 hours	\$29 parts + 4 hours labor	= \$ 129 = \$0.65/hour
500 hours	2 days labor (16 hours)	= \$ 400 = \$0.80/hour
10,000 hours	\$1000 for parts and labor	= \$1000 = <u>\$0.10/hour</u>
		\$1.55/hour

The assumed load operates 8 hours/day, 365 days/year, or 2920 hours/year. Annual maintenance expense is, therefore:

$$\$1.55 \times 2920 = \$4526/\text{year}$$

Annual fuel costs are estimated from the yearly hours of energy load, diesel engine fuel consumption, and fuel price. Kohler engine fuel consumption for the assumed load is 0.19 gallons/hour. Fuel price is assumed to be \$1/gallon. Annual fuel cost is:

$$2920 \text{ hours/year} \times 0.19 \text{ gallons/hour} \times \$1/\text{gallon} = \$555/\text{year}$$

The present value of operation and maintenance costs (OMPV) over the 30 year lifetime is:

$$\begin{aligned} \text{OMPV} &= (\$4526 + \$555) \left(\frac{1 + \text{esc}_{\text{om}}}{\text{dr} - \text{esc}_{\text{om}}} \right) \times \left[1 - \left(\frac{1 + \text{esc}_{\text{om}}}{1 + \text{dr}} \right)^N \right] \\ &= \$5081 \left(\frac{1.0}{0.10 - 0.0} \right) \times \left[1 - \left(\frac{1.0}{1.1} \right)^{30} \right] \\ &= \$47,914 \end{aligned}$$

Diesel generator system life-cycle cost (LCC) is the sum of the initial cost (IC), present value of replacements (RPV), and operation and maintenance (OMPV) costs as shown below:

$$\begin{aligned} \text{LCC} &= \text{IC} + \text{RPV} + \text{OMPV} \\ &= \$8883 + \$1421 + \$47,914 \\ &= \$58,218 \end{aligned}$$

The life-cycle cost comparison between photovoltaic and the battery and diesel alternatives can now be finalized. Life-cycle costs are summarized below:

Photovoltaics	\$26,635
Batteries only	\$45,975
Diesel generator	\$58,218

By inspection, the photovoltaic system is shown to be the least-cost alternative. On this basis, a decision to pursue photovoltaic system analysis and design activities is warranted. As stated in the text, however, it may be additionally useful to perform sensitivity analyses on important cost parameters to understand the effect of uncertainty in parameter values on photovoltaic system cost effectiveness.

APPENDIX B
ESTIMATION OF LOAD FRACTIONS
SUPPLIED BY PHOTOVOLTAIC ARRAY
AND BATTERY STORAGE

APPENDIX B

ESTIMATION OF LOAD FRACTIONS SUPPLIED BY PHOTOVOLTAIC ARRAY AND BATTERY STORAGE

An operating photovoltaic system is typically required to satisfy coincident load as well as to recharge battery storage. By using the photovoltaic array to satisfy load directly, rather than going through battery storage, power losses due to round-trip battery inefficiencies are avoided. Therefore, for the purpose of sizing a photovoltaic system, it may be important to explicitly consider this to avoid unintended oversizing and thus increased life-cycle cost.

Load can be served by either the photovoltaic array or battery storage as shown in Figure B-1.

Relating Figure B-1 to the discussion in Section II.C.4.b and to Equation (2) in Section II.C.5, the fraction of load supplied directly by the photovoltaic array is the cross-hatched area, denoted as f_a . The remaining fraction of the load is supplied by batteries, f_b .

Quantifying array output supplied directly to the load, f_a , is a non-trivial exercise due to the highly stochastic nature of array output and potentially variable loads. As part of a system design optimization effort, but not as part of the present methodology, the most precise way of estimating array output sent directly to the load is by means of a computer simulation of site-specific weather conditions, array output, and user load over a typical year calculated on an hourly basis. Using this information, array size can be calculated using Equation (2). Since this approach is inappropriate for use

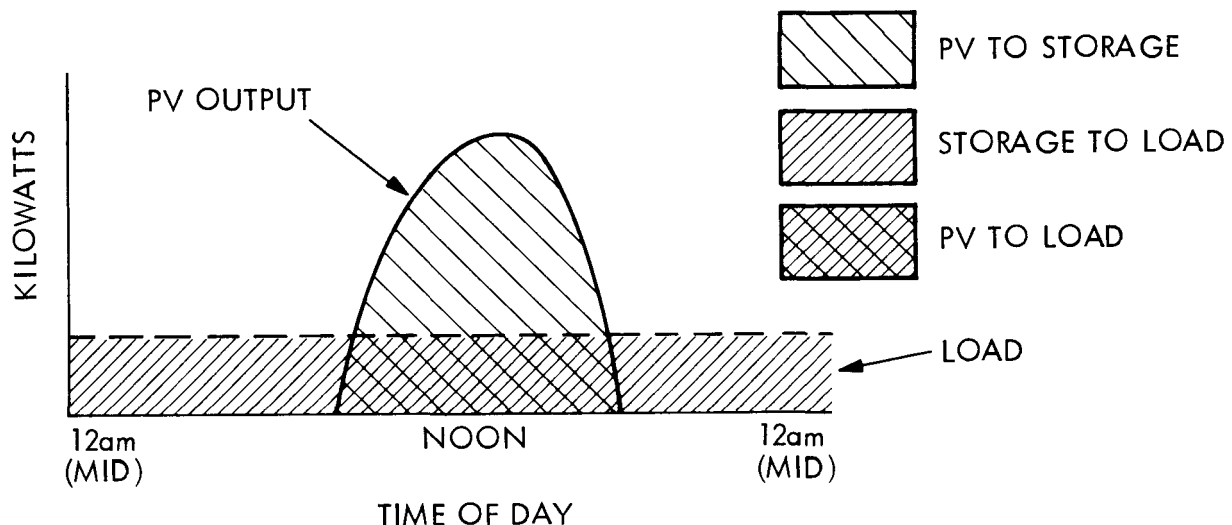


Figure B-1. Idealized Energy Usage by Time-of-Day for a Given Month

in combination with the sizing and costing methodology described earlier, two alternative approaches are described below:

- (1) Bound and Estimate Load Fraction Supplied by Photovoltaic Array.
In this case, the fraction of energy supplied directly to the load by the photovoltaic array can vary between 0% (for nighttime only demand) and 100% (for demand perfectly matched to photovoltaic output). For the 0% array-to-load assumption, all array output must pass through the battery and all battery-resultant efficiency losses incurred. Conversely, if all array output supplies the load directly, no battery efficiency penalties apply. In general, most photovoltaic systems operate between these two extremes.

The assumption that all array output goes through the battery in those applications where the array could supply the load directly is a simplifying assumption that would cause the photovoltaic system to be somewhat oversized relative to the requirements of the load. Conservative approaches have already been incorporated in the methodology to ensure adequate system size. The user should be careful not to unintentionally bias system size larger than required due to this photovoltaic array-to-load factor.

At one boundary condition, the array is sized correctly for 0% (nighttime only demand) array-to-load case compared to the required size, assuming all energy goes through the battery. Conversely, with a perfect match between array and load, the array would be oversized approximately 25% based on the current baseline values for voltage regulation and round-trip battery storage efficiencies (see Appendix A). A more realistic estimate of array oversizing is between these two values. For example, the degree of oversizing for a constant, 24 hours/day load is typically less than 10%.

- (2) Calculate Load Fraction Supplied by Photovoltaic Array Using a Simplified Procedure. A simple algorithm can be constructed to help estimate the load fraction supplied directly by the photovoltaic array under some rather limiting constraints. Assuming clear-sky conditions, an idealized time-of-day profile of array output can be constructed, as shown in Figure B-1, for each month of the year. Then, a representation of the deterministic time-of-day load for each month is incorporated. The load need not be constant by time-of-day or between months. For the "worst" month (see Section II.B.3), estimate the fraction of the load supplied by the array, f_a . This is the cross-hatched area divided by the total load. Insert this fraction into Equation (2). Battery sizing is not affected by this procedure. Repeat this procedure for each month of the year to ensure that array-to-load differences are adequately incorporated. Select the maximum array size, P_a , from Equation (2) to adequately cover each month of the year for the selected array tilt angle.

Use of this procedure requires acceptance of certain limitations. Most importantly, to the extent that there is any variability in time-of-day photovoltaic output (or load) such that the load cannot be served according to the idealized pattern displayed in Figure B-1, this algorithm will overestimate the amount of array power sent directly to the load. Based on the degree of variability, this overestimate will result in the array and battery to be sized smaller than required to meet the load by some varying amount.

APPENDIX C
COMPARISON OF SIZING METHODOLOGY
WITH ALTERNATIVE APPROACHES

APPENDIX C

COMPARISON OF SIZING METHODOLOGY WITH ALTERNATIVE APPROACHES

This section compares the results of applying the sizing methodology in this document with the results of several other sizing approaches. Each methodology has been applied to the same application load example. The example is derived from Reference 3, and was discussed along with the alternative sizing methods.

The application load for this comparison is a constant power load of 4.2 kWh/day. The site has a worst-month insolation value of 2.3 kWh/m²-day. Additional data used for the initial sizing are as follows:

$$f_b = 0.6 \quad (\text{i.e., the fraction of the load met by the battery. Therefore, } f_a = 1 - f_b = 0.4)$$

$$e_{vr} \cdot e_b = 0.80$$

$$e_{i/c} = 0.93$$

Application of the sizing methodology as described in Section II is simplified by the constant load and the prior stipulation of the worst-month insolation. Therefore, $L_{td} = 4.2$ kWh/day and $I = 2.3$ kWh/M²/day. The array sizing factor, S_a , corresponding to $I = 2.3$ in Figure 2-3, is 1.7. No array degradation factor appears in the other sizing approaches. For comparison of the present method, therefore, $F = 1.0$.

The array power from Equation (2) is therefore:

$$\begin{aligned} P_a &= \frac{L_{td} \times 1000}{S_a \times F \times e_{i/c} [f_b (e_{vr} \times e_b) + f_a]} \\ &= \frac{4.2 \times 1000}{1.7 \times 1.0 \times 0.93 [0.6 (0.8) + 0.4]} \\ &= \frac{4200}{1.7 \times 1.0 \times 0.93 \times 0.88} = \frac{4200}{1.39} \end{aligned}$$

Therefore,

$$P_a = 3020 \text{ W (peak) ac}$$

Note that if an array degradation factor, F, equal to 0.85 is included, the result becomes:

$$P_a = 3550 \text{ W (peak) ac}$$

The battery storage sizing factor, S_b , from Figure 2-3 is 7.5. The required battery storage capacity, assuming an 80% depth of discharge (d), is therefore:

$$\begin{aligned} E_b &= \frac{L_{td} \times S_b}{d \times e_{f/c}} \\ &= \frac{4.2 \times 7.5}{0.8 \times 0.93} \\ &= 42 \text{ kWh} \end{aligned}$$

These results are compared with three other approaches in the table below:

Table C-1. Array and Battery Storage Sizing Comparison

Method	Reference	Array Size, W_p	Battery Storage Size, kWh
NASA	7	3000	42
ROSSA	3	3140	42
Solarex ^a	7	3150	30
FPUP (present document)	--	3020	42

^aSolarex designed and built a system with this array and storage size for the site in question. This system was designed for a load of 4.0 kWh/day rather than for 4.2, as in the other examples.

This comparison shows that the present sizing method yields results similar to those of three other approaches when applied to this load and

location. It should be recognized, however, that different sizing approaches will frequently yield different results due to the built-in design margin or loss-of-energy probability (LOEP) selected as the basis of the sizing approach. These differences argue for the use of an LOEP-based sizing approach in order to ensure that power system alternatives being sized for comparison purposes are all sized to the same level of estimated performance.

APPENDIX D
AVERAGE DAILY INSOLATION TABLES
FOR UNITED STATES SITES
(ADAPTED FROM REFERENCE 8)

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL	AVERAGE		
ARRAY	TILT	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL	DAY		
														(KWH/SQ. M)	(KWH/SQ. M)		
JUNEAU	AK	LATITUDE:		58 DEGREES		22 MINUTES											
LATITUDE	-15:	1.04	1.70	2.57	3.72	4.07	4.28	4.02	3.47	2.73	1.74	1.24	.68	951.8	2.6		
LATITUDE	:	1.16	1.81	2.57	3.53	3.71	3.86	3.67	3.28	2.72	1.83	1.39	.78	922.7	2.5		
LATITUDE	+15:	1.22	1.82	2.43	3.18	3.24	3.32	3.20	2.96	2.58	1.83	1.45	.83	853.6	2.3		
KING SALMON	AK	LATITUDE:		58 DEGREES		41 MINUTES											
LATITUDE	-15:	1.25	2.22	3.68	4.40	4.73	4.68	4.38	3.73	3.54	3.08	2.07	1.08	1183.5	3.2		
LATITUDE	:	1.39	2.36	3.72	4.19	4.32	4.22	4.00	3.54	3.57	3.32	2.35	1.25	1164.2	3.2		
LATITUDE	+15:	1.46	2.37	3.56	3.78	3.77	3.63	3.48	3.19	3.41	3.36	2.49	1.34	1090.5	3.0		
KODIAK	AK	LATITUDE:		57 DEGREES		45 MINUTES											
LATITUDE	-15:	1.13	1.92	3.50	4.38	4.35	4.65	4.46	4.20	3.55	3.06	1.90	.99	1160.0	3.2		
LATITUDE	:	1.26	2.03	3.53	4.16	3.98	4.20	4.08	3.99	3.58	3.29	2.15	1.13	1137.8	3.1		
LATITUDE	+15:	1.31	2.02	3.37	3.76	3.47	3.61	3.55	3.60	3.42	3.32	2.27	1.20	1062.9	2.9		
NOME	AK	LATITUDE:		64 DEGREES		30 MINUTES											
LATITUDE	-15:	.34	1.56	3.29	4.63	5.14	5.40	4.57	3.74	3.53	2.59	1.16	.01	1095.5	3.0		
LATITUDE	:	.38	1.65	3.32	4.39	4.69	4.85	4.15	3.54	3.58	2.79	1.32	.01	1055.8	2.9		
LATITUDE	+15:	.40	1.65	3.17	3.96	4.06	4.14	3.60	3.19	3.42	2.82	1.39	.01	968.4	2.7		
BIRMINGHAM	AL	LATITUDE:		33 DEGREES		34 MINUTES											
LATITUDE	-15:	2.75	3.53	4.44	5.39	5.72	5.83	5.58	5.57	5.01	4.54	3.44	2.70	1658.7	4.5		
LATITUDE	:	3.02	3.73	4.49	5.19	5.31	5.33	5.17	5.36	5.08	4.87	3.84	3.05	1657.0	4.5		
LATITUDE	+15:	3.14	3.74	4.31	4.75	4.68	4.63	4.57	4.91	4.89	4.94	4.03	3.23	1577.2	4.3		
MOBILE	AL	LATITUDE:		30 DEGREES		41 MINUTES											
LATITUDE	-15:	3.11	3.92	4.74	5.51	5.78	5.69	5.30	5.25	4.89	4.72	3.64	2.94	1688.3	4.6		
LATITUDE	:	3.43	4.16	4.80	5.31	5.37	5.22	4.93	5.06	4.95	5.06	4.07	3.32	1694.8	4.6		
LATITUDE	+15:	3.58	4.19	4.63	4.87	4.75	4.55	4.36	4.64	4.77	5.14	4.28	3.53	1620.9	4.4		
MONTGOMERY	AL	LATITUDE:		32 DEGREES		18 MINUTES											
LATITUDE	-15:	2.87	3.66	4.56	5.56	5.85	5.99	5.67	5.62	5.01	4.67	3.59	2.87	1703.1	4.7		
LATITUDE	:	3.17	3.88	4.61	5.36	5.43	5.47	5.26	5.42	5.08	5.01	4.02	3.25	1703.0	4.7		
LATITUDE	+15:	3.29	3.89	4.43	4.91	4.78	4.75	4.64	4.96	4.89	5.08	4.22	3.45	1622.1	4.4		
FORT SMITH	AR	LATITUDE:		35 DEGREES		20 MINUTES											
LATITUDE	-15:	3.03	3.75	4.56	5.23	5.90	6.33	6.37	6.11	5.27	4.64	3.55	2.94	1756.2	4.8		
LATITUDE	:	3.37	3.98	4.61	5.03	5.46	5.76	5.88	5.89	5.35	4.98	3.99	3.34	1754.8	4.8		
LATITUDE	+15:	3.52	4.00	4.43	4.60	4.81	4.98	5.16	5.38	5.15	5.05	4.20	3.56	1669.3	4.6		

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE	ARRAY TILT	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
LITTLE ROCK	AR	LATITUDE: 34 DEGREES			44 MINUTES										
	LATITUDE -15:	2.93	3.73	4.54	5.21	5.95	6.38	6.27	6.04	5.30	4.71	3.47	2.84	1746.4	4.8
	LATITUDE :	3.24	3.96	4.59	5.01	5.51	5.82	5.80	5.82	5.38	5.06	3.89	3.22	1744.7	4.8
	LATITUDE +15:	3.39	3.98	4.41	4.59	4.85	5.03	5.09	5.32	5.19	5.14	4.09	3.43	1659.4	4.5
PHOENIX	AZ	LATITUDE: 33 DEGREES			26 MINUTES										
	LATITUDE -15:	4.19	5.21	6.36	7.67	8.26	8.28	7.66	7.46	7.13	6.11	4.83	4.02	2348.9	6.4
	LATITUDE :	4.74	5.62	6.51	7.40	7.60	7.48	7.06	7.20	7.32	6.66	5.52	4.66	2366.3	6.5
	LATITUDE +15:	5.02	5.72	6.31	6.76	6.60	6.36	6.15	6.57	7.10	6.83	5.89	5.03	2260.9	6.2
PRESCOTT	AZ	LATITUDE: 34 DEGREES			39 MINUTES										
	LATITUDE -15:	4.30	5.14	6.30	7.44	8.11	8.34	7.12	6.82	6.97	6.09	4.94	4.15	2304.2	6.3
	LATITUDE :	4.88	5.54	6.45	7.18	7.47	7.53	6.57	6.58	7.16	6.64	5.66	4.83	2327.1	6.4
	LATITUDE +15:	5.18	5.64	6.24	6.56	6.50	6.41	5.74	6.01	6.94	6.81	6.05	5.23	2229.6	6.1
TUCSON	AZ	LATITUDE: 32 DEGREES			7 MINUTES										
	LATITUDE -15:	4.42	5.35	6.47	7.66	8.23	8.24	7.21	7.06	6.90	6.08	4.94	4.18	2335.1	6.4
	LATITUDE :	5.00	5.77	6.63	7.39	7.57	7.44	6.65	6.81	7.07	6.62	5.65	4.85	2356.1	6.5
	LATITUDE +15:	5.30	5.87	6.42	6.74	6.57	6.33	5.81	6.22	6.84	6.79	6.02	5.25	2255.1	6.2
WINSLOW	AZ	LATITUDE: 35 DEGREES			1 MINUTES										
	LATITUDE -15:	4.19	5.15	6.34	7.47	8.01	8.19	7.24	7.00	6.90	6.01	4.90	4.04	2295.2	6.3
	LATITUDE :	4.75	5.55	6.49	7.21	7.37	7.39	6.67	6.74	7.07	6.54	5.61	4.69	2314.0	6.3
	LATITUDE +15:	5.03	5.64	6.28	6.57	6.40	6.29	5.81	6.15	6.84	6.70	5.99	5.07	2213.3	6.1
YUMA	AZ	LATITUDE: 32 DEGREES			40 MINUTES										
	LATITUDE -15:	4.45	5.43	6.70	7.84	8.42	8.50	7.56	7.56	7.20	6.23	5.04	4.26	2410.2	6.6
	LATITUDE :	5.05	5.87	6.88	7.57	7.75	7.68	6.97	7.31	7.40	6.80	5.77	4.97	2434.4	6.7
	LATITUDE +15:	5.37	5.98	6.67	6.91	6.73	6.53	6.08	6.67	7.18	6.98	6.17	5.38	2331.3	6.4
BAKERSFIELD	CA	LATITUDE: 35 DEGREES			25 MINUTES										
	LATITUDE -15:	3.15	4.19	5.63	6.85	7.75	8.31	8.29	7.97	7.19	5.79	4.03	2.92	2194.8	6.0
	LATITUDE :	3.50	4.46	5.74	6.60	7.14	7.50	7.62	7.69	7.39	6.30	4.56	3.33	2187.2	6.0
	LATITUDE +15:	3.67	4.50	5.54	6.03	6.22	6.38	6.61	7.01	7.16	6.45	4.83	3.55	2068.6	5.7
CHINA LAKE	CA	LATITUDE: 35 DEGREES			41 MINUTES										
	LATITUDE -15:	3.88	4.77	6.19	7.33	7.88	8.30	8.07	8.63	7.16	5.88	4.53	3.82	2328.1	6.4
	LATITUDE :	4.38	5.13	6.34	7.07	7.26	7.50	7.43	8.34	7.36	6.41	5.17	4.43	2338.3	6.4
	LATITUDE +15:	4.63	5.20	6.13	6.46	6.32	6.38	6.45	7.61	7.14	6.57	5.51	4.78	2227.5	6.1

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC		
DAGGETT	CA	LATITUDE:		34 DEGREES		52 MINUTES									
	-15:	4.02	4.92	6.29	7.44	8.01	8.36	8.03	7.82	7.20	5.98	4.68	3.90	2334.1	6.4
	:	4.55	5.30	6.44	7.18	7.38	7.55	7.40	7.56	7.41	6.53	5.35	4.52	2348.6	6.4
	+15:	4.82	5.38	6.24	6.56	6.42	6.43	6.43	6.90	7.19	6.69	5.71	4.89	2241.3	6.1
EL TORO	CA	LATITUDE:		33 DEGREES		40 MINUTES									
	-15:	3.85	4.65	5.60	6.25	6.39	6.65	7.29	7.00	6.07	5.17	4.24	3.73	2036.4	5.6
	:	4.33	4.98	5.71	6.02	5.91	6.05	6.73	6.76	6.20	5.59	4.81	4.30	2051.4	5.6
	+15:	4.57	5.05	5.52	5.51	5.20	5.22	5.87	6.17	5.99	5.69	5.10	4.63	1963.7	5.4
FRESNO	CA	LATITUDE:		36 DEGREES		46 MINUTES									
	-15:	2.72	3.89	5.59	6.89	7.69	8.26	8.31	8.04	7.27	5.81	3.90	2.50	2158.6	5.9
	:	3.01	4.14	5.70	6.64	7.08	7.46	7.64	7.76	7.48	6.33	4.41	2.83	2146.5	5.9
	+15:	3.14	4.17	5.51	6.07	6.18	6.36	6.63	7.08	7.26	6.48	4.68	3.00	2025.7	5.5
LONG BEACH	CA	LATITUDE:		33 DEGREES		49 MINUTES									
	-15:	3.77	4.56	5.61	6.28	6.37	6.48	7.09	6.83	5.94	5.05	4.14	3.62	2001.8	5.5
	:	4.24	4.89	5.72	6.06	5.90	5.91	6.55	6.59	6.06	5.45	4.69	4.18	2015.9	5.5
	+15:	4.48	4.95	5.53	5.54	5.18	5.11	5.73	6.02	5.86	5.55	4.98	4.49	1929.4	5.3
LOS ANGELES	CA	LATITUDE:		33 DEGREES		56 MINUTES									
	-15:	3.78	4.57	5.65	6.32	6.36	6.43	7.12	6.76	5.88	5.02	4.16	3.65	1999.6	5.5
	:	4.25	4.89	5.76	6.10	5.89	5.86	6.57	6.52	5.99	5.41	4.72	4.21	2014.3	5.5
	+15:	4.48	4.96	5.57	5.58	5.18	5.07	5.75	5.96	5.79	5.51	5.00	4.53	1928.6	5.3
NEEDLES	CA	LATITUDE:		34 DEGREES		46 MINUTES									
	-15:	4.15	5.23	6.49	7.59	8.19	8.44	7.84	7.45	7.21	6.07	4.87	4.09	2362.5	6.5
	:	4.70	5.65	6.65	7.33	7.54	7.62	7.22	7.19	7.42	6.62	5.58	4.76	2381.9	6.5
	+15:	4.98	5.76	6.45	6.69	6.56	6.48	6.29	6.57	7.20	6.79	5.96	5.16	2277.5	6.2
OAKLAND	CA	LATITUDE:		37 DEGREES		44 MINUTES									
	-15:	3.05	3.97	5.22	6.32	6.85	7.12	7.19	6.78	6.19	4.89	3.66	2.98	1955.4	5.4
	:	3.40	4.23	5.31	6.09	6.32	6.46	6.62	6.53	6.33	5.28	4.13	3.40	1951.7	5.3
	+15:	3.56	4.27	5.12	5.56	5.54	5.55	5.78	5.96	6.12	5.37	4.37	3.64	1851.7	5.1
RED BLUFF	CA	LATITUDE:		40 DEGREES		9 MINUTES									
	-15:	2.53	3.58	4.95	6.36	7.39	7.87	8.31	7.79	7.00	5.24	3.29	2.44	2033.9	5.6
	:	2.80	3.79	5.02	6.11	6.80	7.11	7.63	7.51	7.19	5.68	3.70	2.77	2013.7	5.5
	+15:	2.92	3.81	4.83	5.57	5.93	6.07	6.61	6.85	6.96	5.79	3.89	2.94	1893.3	5.2

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC		
SACRAMENTO	CA	LATITUDE:		38 DEGREES		31 MINUTES									
LATITUDE	-15:	2.55	3.69	5.27	6.63	7.55	8.11	8.35	7.92	7.11	5.47	3.53	2.45	2090.9	5.7
LATITUDE	:	2.81	3.91	5.36	6.38	6.95	7.33	7.67	7.65	7.31	5.94	3.98	2.77	2073.2	5.7
LATITUDE	+15:	2.93	3.94	5.17	5.83	6.06	6.25	6.65	6.97	7.09	6.07	4.20	2.94	1951.6	5.3
SAN DIEGO	CA	LATITUDE:		32 DEGREES		44 MINUTES									
LATITUDE	-15:	3.90	4.70	5.64	6.25	6.18	6.26	6.74	6.65	5.95	5.16	4.31	3.79	1994.8	5.5
LATITUDE	:	4.39	5.04	5.75	6.03	5.72	5.72	6.23	6.42	6.07	5.58	4.89	4.37	2014.9	5.5
LATITUDE	+15:	4.63	5.11	5.56	5.52	5.04	4.95	5.46	5.87	5.87	5.68	5.19	4.71	1934.5	5.3
SAN FRANCISCO	CA	LATITUDE:		37 DEGREES		37 MINUTES									
LATITUDE	-15:	3.04	3.93	5.22	6.31	6.90	7.19	7.41	7.00	6.35	4.94	3.64	2.94	1975.5	5.4
LATITUDE	:	3.39	4.19	5.30	6.08	6.36	6.52	6.82	6.75	6.49	5.33	4.11	3.36	1970.1	5.4
LATITUDE	+15:	3.55	4.22	5.11	5.55	5.57	5.60	5.95	6.16	6.28	5.43	4.34	3.59	1867.3	5.1
SANTA MARIA	CA	LATITUDE:		34 DEGREES		54 MINUTES									
LATITUDE	-15:	3.51	4.31	5.56	6.25	6.60	7.12	7.22	6.88	6.11	5.26	4.11	3.52	2023.8	5.5
LATITUDE	:	3.93	4.61	5.66	6.03	6.11	6.46	6.67	6.64	6.25	5.70	4.66	4.06	2032.8	5.6
LATITUDE	+15:	4.14	4.66	5.47	5.51	5.36	5.56	5.82	6.06	6.04	5.82	4.95	4.36	1940.4	5.3
SUNNYVALE	CA	LATITUDE:		37 DEGREES		25 MINUTES									
LATITUDE	-15:	3.17	4.04	5.32	6.39	7.05	7.42	7.55	7.17	6.41	5.03	3.74	3.02	2019.1	5.5
LATITUDE	:	3.54	4.31	5.41	6.15	6.50	6.72	6.95	6.91	6.55	5.43	4.22	3.45	2013.9	5.5
LATITUDE	+15:	3.72	4.34	5.21	5.62	5.68	5.76	6.05	6.30	6.34	5.53	4.46	3.69	1908.7	5.2
COLORADO SPRINGS	CO	LATITUDE:		38 DEGREES		49 MINUTES									
LATITUDE	-15:	4.17	4.81	5.66	6.39	6.60	7.17	6.86	6.72	6.51	5.72	4.50	3.92	2100.9	5.8
LATITUDE	:	4.74	5.18	5.77	6.15	6.09	6.50	6.32	6.48	6.67	6.23	5.16	4.57	2126.1	5.8
LATITUDE	+15:	5.04	5.27	5.57	5.62	5.34	5.59	5.53	5.91	6.45	6.38	5.50	4.95	2042.8	5.6
DENVER	CO	LATITUDE:		39 DEGREES		45 MINUTES									
LATITUDE	-15:	4.01	4.65	5.65	6.24	6.62	7.12	7.05	6.82	6.45	5.55	4.29	3.75	2076.2	5.7
LATITUDE	:	4.56	5.01	5.76	6.00	6.11	6.46	6.50	6.57	6.60	6.04	4.90	4.36	2095.9	5.7
LATITUDE	+15:	4.84	5.08	5.56	5.48	5.35	5.55	5.67	6.00	6.39	6.17	5.22	4.72	2009.0	5.5
GRAND JUNCTION	CO	LATITUDE:		39 DEGREES		7 MINUTES									
LATITUDE	-15:	3.65	4.56	5.70	6.59	7.38	7.86	7.65	7.28	6.86	5.70	4.41	3.66	2171.0	5.9
LATITUDE	:	4.12	4.89	5.81	6.34	6.79	7.10	7.03	7.02	7.03	6.20	5.03	4.25	2180.1	6.0
LATITUDE	+15:	4.35	4.96	5.61	5.78	5.92	6.06	6.12	6.39	6.81	6.34	5.36	4.58	2078.0	5.7

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC		
PUEBLO	CO	LATITUDE: 38 DEGREES 17 MINUTES													
	LATITUDE -15:	4.12	4.73	5.68	6.46	6.69	7.36	7.15	6.97	6.55	5.67	4.49	3.86	2122.9	5.8
	LATITUDE :	4.68	5.09	5.79	6.22	6.17	6.67	6.59	6.72	6.71	6.16	5.12	4.48	2142.6	5.9
	LATITUDE +15:	4.97	5.16	5.59	5.68	5.40	5.71	5.74	6.13	6.49	6.30	5.46	4.85	2053.1	5.6
HARTFORD	CT	LATITUDE: 41 DEGREES 56 MINUTES													
	LATITUDE -15:	2.14	2.85	3.51	4.33	4.86	5.11	5.11	4.70	4.22	3.53	2.27	1.81	1352.9	3.7
	LATITUDE :	2.35	3.00	3.53	4.15	4.49	4.66	4.72	4.51	4.26	3.76	2.51	2.02	1337.8	3.7
	LATITUDE +15:	2.44	2.99	3.37	3.78	3.96	4.05	4.16	4.11	4.08	3.79	2.61	2.13	1262.1	3.5
GUANTANAMO BAY	CU	LATITUDE: 19 DEGREES 54 MINUTES													
	LATITUDE -15:	4.66	5.38	6.17	6.69	6.36	6.10	6.50	6.31	5.84	5.17	4.76	4.39	2079.2	5.7
	LATITUDE :	5.27	5.79	6.31	6.48	5.93	5.62	6.06	6.12	5.96	5.56	5.40	5.07	2115.9	5.8
	LATITUDE +15:	5.60	5.90	6.12	5.95	5.23	4.89	5.33	5.62	5.77	5.67	5.74	5.47	2046.1	5.6
WASHINGTON-STERLINDC		LATITUDE: 38 DEGREES 57 MINUTES													
	LATITUDE -15:	2.44	3.15	3.98	4.77	5.32	5.76	5.62	5.30	4.81	4.02	2.86	2.16	1528.7	4.2
	LATITUDE :	2.69	3.32	4.01	4.58	4.93	5.26	5.20	5.10	4.87	4.29	3.19	2.43	1518.5	4.2
	LATITUDE +15:	2.80	3.33	3.85	4.19	4.35	4.56	4.58	4.66	4.68	4.34	3.34	2.57	1437.8	3.9
WILMINGTON	DE	LATITUDE: 39 DEGREES 40 MINUTES													
	LATITUDE -15:	2.49	3.25	4.11	4.85	5.30	5.71	5.65	5.32	4.76	3.97	2.90	2.26	1539.3	4.2
	LATITUDE :	2.76	3.43	4.14	4.65	4.90	5.21	5.22	5.11	4.82	4.25	3.23	2.55	1530.0	4.2
	LATITUDE +15:	2.87	3.44	3.97	4.25	4.32	4.51	4.59	4.66	4.63	4.29	3.39	2.70	1449.3	4.0
APALACHICOLA	FL	LATITUDE: 29 DEGREES 44 MINUTES													
	LATITUDE -15:	3.16	3.98	4.94	6.02	6.45	6.08	5.60	5.39	5.16	4.93	3.94	3.12	1788.9	4.9
	LATITUDE :	3.49	4.22	5.01	5.81	5.98	5.56	5.21	5.21	5.24	5.31	4.42	3.54	1795.8	4.9
	LATITUDE +15:	3.65	4.25	4.84	5.32	5.26	4.83	4.61	4.78	5.05	5.40	4.67	3.77	1716.4	4.7
DAYTONA BEACH	FL	LATITUDE: 29 DEGREES 11 MINUTES													
	LATITUDE -15:	3.56	4.29	5.19	6.02	6.07	5.57	5.51	5.36	4.94	4.45	3.89	3.32	1769.5	4.8
	LATITUDE :	3.96	4.56	5.28	5.81	5.63	5.11	5.12	5.18	5.00	4.75	4.35	3.77	1780.2	4.9
	LATITUDE +15:	4.15	4.60	5.09	5.32	4.96	4.46	4.53	4.75	4.81	4.80	4.58	4.02	1705.4	4.7
JACKSONVILLE	FL	LATITUDE: 30 DEGREES 30 MINUTES													
	LATITUDE -15:	3.40	4.16	5.14	5.95	6.03	5.73	5.56	5.42	4.85	4.40	3.81	3.18	1753.7	4.8
	LATITUDE :	3.77	4.42	5.22	5.74	5.60	5.25	5.17	5.23	4.91	4.71	4.27	3.61	1761.6	4.8
	LATITUDE +15:	3.95	4.46	5.03	5.26	4.94	4.57	4.57	4.80	4.73	4.76	4.50	3.85	1685.2	4.6

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC		
-----		-----												-----	-----
MIAMI	FL	LATITUDE:		25 DEGREES		48 MINUTES									
LATITUDE	-15:	3.74	4.50	5.27	5.90	5.71	5.25	5.46	5.17	4.76	4.46	3.99	3.69	1761.3	4.8
LATITUDE	:	4.17	4.80	5.36	5.70	5.33	4.84	5.09	5.00	4.83	4.76	4.47	4.21	1781.2	4.9
LATITUDE	+15:	4.38	4.85	5.18	5.24	4.72	4.24	4.52	4.60	4.65	4.82	4.71	4.50	1715.6	4.7
ORLANDO	FL	LATITUDE:		28 DEGREES		33 MINUTES									
LATITUDE	-15:	3.68	4.37	5.29	6.06	6.14	5.60	5.56	5.33	4.99	4.61	4.08	3.50	1801.8	4.9
LATITUDE	:	4.10	4.65	5.38	5.86	5.71	5.14	5.18	5.15	5.06	4.94	4.59	3.99	1817.2	5.0
LATITUDE	+15:	4.31	4.70	5.19	5.37	5.03	4.49	4.58	4.73	4.87	5.01	4.85	4.26	1744.9	4.8
TALLAHASSEE	FL	LATITUDE:		30 DEGREES		23 MINUTES									
LATITUDE	-15:	3.30	4.05	4.98	5.84	5.98	5.73	5.39	5.36	5.03	4.78	3.86	3.16	1748.3	4.8
LATITUDE	:	3.66	4.31	5.06	5.63	5.55	5.25	5.02	5.17	5.10	5.13	4.33	3.58	1757.6	4.8
LATITUDE	+15:	3.82	4.34	4.87	5.16	4.89	4.57	4.44	4.74	4.91	5.21	4.56	3.81	1682.6	4.6
TAMPA	FL	LATITUDE:		27 DEGREES		58 MINUTES									
LATITUDE	-15:	3.68	4.39	5.30	6.09	6.18	5.65	5.42	5.26	4.95	4.73	4.08	3.49	1802.0	4.9
LATITUDE	:	4.10	4.68	5.40	5.88	5.74	5.19	5.05	5.09	5.02	5.07	4.59	3.98	1819.3	5.0
LATITUDE	+15:	4.31	4.73	5.22	5.40	5.07	4.53	4.48	4.67	4.84	5.15	4.85	4.25	1748.7	4.8
ATLANTA	GA	LATITUDE:		33 DEGREES		39 MINUTES									
LATITUDE	-15:	2.80	3.55	4.47	5.43	5.72	5.81	5.59	5.51	4.89	4.50	3.55	2.76	1661.6	4.6
LATITUDE	:	3.08	3.75	4.52	5.23	5.31	5.31	5.19	5.31	4.96	4.82	3.98	3.12	1661.3	4.6
LATITUDE	+15:	3.21	3.76	4.34	4.79	4.68	4.62	4.58	4.86	4.77	4.89	4.18	3.32	1582.5	4.3
AUGUSTA	GA	LATITUDE:		33 DEGREES		22 MINUTES									
LATITUDE	-15:	2.94	3.72	4.59	5.58	5.75	5.78	5.55	5.37	4.84	4.57	3.69	2.97	1684.7	4.6
LATITUDE	:	3.25	3.94	4.64	5.37	5.34	5.29	5.15	5.17	4.89	4.90	4.14	3.37	1687.5	4.6
LATITUDE	+15:	3.38	3.96	4.46	4.92	4.71	4.59	4.55	4.74	4.71	4.97	4.36	3.58	1610.3	4.4
MACON	GA	LATITUDE:		32 DEGREES		42 MINUTES									
LATITUDE	-15:	2.97	3.70	4.65	5.60	5.81	5.83	5.50	5.53	4.92	4.63	3.74	2.94	1699.3	4.7
LATITUDE	:	3.28	3.92	4.71	5.39	5.39	5.34	5.11	5.33	4.99	4.97	4.20	3.34	1703.3	4.7
LATITUDE	+15:	3.42	3.94	4.53	4.94	4.76	4.64	4.51	4.88	4.80	5.05	4.42	3.55	1626.3	4.5
SAVANNAH	GA	LATITUDE:		32 DEGREES		8 MINUTES									
LATITUDE	-15:	3.06	3.77	4.75	5.66	5.72	5.60	5.49	5.21	4.63	4.48	3.70	3.02	1677.2	4.6
LATITUDE	:	3.38	3.99	4.81	5.46	5.31	5.13	5.10	5.02	4.68	4.79	4.15	3.43	1681.1	4.6
LATITUDE	+15:	3.52	4.01	4.63	5.00	4.68	4.47	4.50	4.59	4.49	4.85	4.36	3.65	1605.4	4.4

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL	AVERAGE DAY
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	(KWH/SQ. M)	(KWH/SQ. M)
BARBERS POINT	HI	LATITUDE: 21 DEGREES 19 MINUTES													
LATITUDE	-15:	4.06	4.75	5.29	5.79	6.13	6.26	6.28	6.22	5.85	5.15	4.39	3.97	1951.9	5.3
LATITUDE	:	4.54	5.07	5.38	5.61	5.72	5.74	5.85	6.02	5.96	5.53	4.94	4.54	1974.8	5.4
LATITUDE	+15:	4.78	5.14	5.21	5.16	5.05	4.98	5.15	5.53	5.77	5.63	5.23	4.86	1900.3	5.2
HILO	HI	LATITUDE: 19 DEGREES 43 MINUTES													
LATITUDE	-15:	3.69	4.04	4.29	4.52	4.85	5.17	5.07	5.02	4.94	4.46	3.64	3.37	1614.9	4.4
LATITUDE	:	4.09	4.29	4.35	4.39	4.56	4.79	4.76	4.88	5.01	4.76	4.03	3.81	1634.2	4.5
LATITUDE	+15:	4.29	4.32	4.21	4.06	4.08	4.21	4.25	4.50	4.85	4.81	4.23	4.04	1577.0	4.3
HONOLULU	HI	LATITUDE: 21 DEGREES 20 MINUTES													
LATITUDE	-15:	3.97	4.60	5.22	5.67	6.07	6.21	6.22	6.21	5.84	5.10	4.27	3.85	1924.4	5.3
LATITUDE	:	4.43	4.90	5.31	5.49	5.66	5.70	5.80	6.01	5.95	5.48	4.80	4.39	1944.7	5.3
LATITUDE	+15:	4.65	4.96	5.13	5.05	5.00	4.95	5.11	5.52	5.76	5.57	5.07	4.69	1869.8	5.1
BURLINGTON	IA	LATITUDE: 40 DEGREES 47 MINUTES													
LATITUDE	-15:	2.63	3.46	4.21	5.07	5.82	6.42	6.48	6.09	5.23	4.45	3.11	2.31	1684.2	4.6
LATITUDE	:	2.92	3.67	4.26	4.86	5.38	5.84	5.98	5.86	5.32	4.79	3.49	2.62	1674.1	4.6
LATITUDE	+15:	3.06	3.68	4.08	4.44	4.73	5.03	5.23	5.35	5.12	4.86	3.68	2.78	1584.1	4.3
DES MOINES	IA	LATITUDE: 41 DEGREES 32 MINUTES													
LATITUDE	-15:	2.71	3.52	4.31	5.16	5.80	6.43	6.51	6.12	5.36	4.57	3.16	2.42	1707.7	4.7
LATITUDE	:	3.02	3.74	4.35	4.94	5.35	5.84	6.00	5.88	5.45	4.92	3.55	2.75	1699.3	4.7
LATITUDE	+15:	3.16	3.76	4.18	4.51	4.70	5.04	5.25	5.36	5.25	5.00	3.74	2.93	1609.3	4.4
MASON CITY	IA	LATITUDE: 43 DEGREES 9 MINUTES													
LATITUDE	-15:	2.71	3.53	4.34	5.06	5.90	6.40	6.49	6.19	5.34	4.46	3.00	2.31	1697.1	4.6
LATITUDE	:	3.02	3.75	4.39	4.84	5.44	5.80	5.97	5.95	5.43	4.80	3.37	2.62	1685.9	4.6
LATITUDE	+15:	3.17	3.77	4.21	4.41	4.76	5.00	5.22	5.42	5.23	4.86	3.54	2.79	1593.7	4.4
SIOUX CITY	IA	LATITUDE: 42 DEGREES 24 MINUTES													
LATITUDE	-15:	2.73	3.49	4.31	5.24	5.91	6.44	6.60	6.20	5.36	4.51	3.17	2.40	1716.6	4.7
LATITUDE	:	3.04	3.71	4.35	5.03	5.45	5.84	6.08	5.96	5.45	4.86	3.57	2.73	1707.0	4.7
LATITUDE	+15:	3.18	3.72	4.17	4.58	4.78	5.03	5.31	5.43	5.25	4.93	3.76	2.90	1615.2	4.4
BOISE	ID	LATITUDE: 43 DEGREES 34 MINUTES													
LATITUDE	-15:	2.33	3.57	4.95	6.18	7.13	7.48	8.20	7.55	6.87	5.20	3.23	2.30	1980.0	5.4
LATITUDE	:	2.58	3.80	5.03	5.94	6.56	6.76	7.53	7.28	7.06	5.65	3.64	2.62	1962.5	5.4
LATITUDE	+15:	2.69	3.82	4.84	5.41	5.73	5.79	6.53	6.63	6.84	5.77	3.84	2.78	1847.2	5.1

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL	AVERAGE		
ARRAY	TILT	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL	DAY		
														(KWH/SQ. M)	(KWH/SQ. M)		
LEWISTON	ID	LATITUDE:		46 DEGREES		23 MINUTES											
LATITUDE	-15:	1.62	2.59	3.88	4.84	5.77	6.11	7.36	6.70	5.76	3.98	2.13	1.50	1593.0	4.4		
LATITUDE	:	1.76	2.71	3.91	4.63	5.31	5.54	6.76	6.44	5.87	4.27	2.37	1.68	1562.4	4.3		
LATITUDE	+15:	1.81	2.70	3.74	4.21	4.65	4.77	5.88	5.86	5.66	4.33	2.47	1.76	1458.1	4.0		
POCATELLO	ID	LATITUDE:		42 DEGREES		55 MINUTES											
LATITUDE	-15:	2.59	3.73	5.19	6.14	7.13	7.53	8.15	7.67	6.95	5.47	3.54	2.49	2028.8	5.6		
LATITUDE	:	2.89	3.97	5.28	5.90	6.57	6.81	7.49	7.40	7.14	5.95	4.01	2.85	2018.7	5.5		
LATITUDE	+15:	3.02	4.00	5.09	5.38	5.74	5.84	6.51	6.75	6.93	6.09	4.25	3.04	1907.2	5.2		
CHICAGO	IL	LATITUDE:		41 DEGREES		47 MINUTES											
LATITUDE	-15:	2.30	3.05	4.03	4.82	5.55	6.09	6.04	5.74	5.03	4.09	2.65	1.91	1562.9	4.3		
LATITUDE	:	2.54	3.22	4.06	4.62	5.13	5.54	5.57	5.51	5.11	4.39	2.96	2.14	1546.6	4.2		
LATITUDE	+15:	2.64	3.22	3.89	4.22	4.51	4.78	4.88	5.03	4.91	4.44	3.10	2.26	1457.9	4.0		
SPRINGFIELD	IL	LATITUDE:		39 DEGREES		50 MINUTES											
LATITUDE	-15:	2.58	3.41	4.08	4.97	5.78	6.35	6.38	5.98	5.33	4.40	3.09	2.28	1663.6	4.6		
LATITUDE	:	2.86	3.61	4.12	4.77	5.34	5.78	5.88	5.75	5.42	4.73	3.46	2.58	1653.3	4.5		
LATITUDE	+15:	2.98	3.63	3.95	4.36	4.70	4.99	5.15	5.25	5.22	4.80	3.63	2.74	1564.5	4.3		
FORT WAYNE	IN	LATITUDE:		41 DEGREES		0 MINUTES											
LATITUDE	-15:	1.95	2.73	3.50	4.46	5.18	5.57	5.53	5.27	4.65	3.80	2.31	1.65	1419.2	3.9		
LATITUDE	:	2.13	2.85	3.51	4.27	4.78	5.07	5.10	5.05	4.70	4.05	2.54	1.83	1397.2	3.8		
LATITUDE	+15:	2.19	2.84	3.35	3.89	4.21	4.40	4.48	4.60	4.51	4.09	2.64	1.91	1311.9	3.6		
INDIANAPOLIS	IN	LATITUDE:		39 DEGREES		44 MINUTES											
LATITUDE	-15:	2.09	2.88	3.67	4.58	5.23	5.66	5.59	5.42	4.79	3.95	2.55	1.84	1469.6	4.0		
LATITUDE	:	2.28	3.02	3.69	4.39	4.84	5.17	5.17	5.20	4.85	4.22	2.82	2.05	1452.7	4.0		
LATITUDE	+15:	2.36	3.02	3.53	4.01	4.27	4.48	4.54	4.75	4.66	4.26	2.95	2.15	1369.2	3.8		
SOUTH BEND	IN	LATITUDE:		41 DEGREES		42 MINUTES											
LATITUDE	-15:	1.77	2.57	3.56	4.57	5.34	5.83	5.75	5.55	4.76	3.78	2.25	1.52	1439.3	3.9		
LATITUDE	:	1.92	2.69	3.57	4.38	4.93	5.30	5.30	5.33	4.82	4.03	2.48	1.67	1414.3	3.9		
LATITUDE	+15:	1.97	2.67	3.42	4.00	4.34	4.59	4.66	4.86	4.63	4.07	2.58	1.73	1324.9	3.6		
DODGE CITY	KS	LATITUDE:		37 DEGREES		46 MINUTES											
LATITUDE	-15:	3.67	4.46	5.31	6.20	6.47	7.14	7.11	6.79	6.14	5.31	4.05	3.47	2012.6	5.5		
LATITUDE	:	4.15	4.78	5.40	5.97	5.98	6.48	6.55	6.54	6.27	5.76	4.60	4.01	2023.5	5.5		
LATITUDE	+15:	4.38	4.84	5.21	5.45	5.24	5.57	5.72	5.97	6.07	5.88	4.88	4.31	1933.0	5.3		

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC		
GOODLAND KS		LATITUDE: 39 DEGREES 22 MINUTES													
LATITUDE	-15:	3.67	4.28	5.19	6.05	6.39	7.13	7.19	6.81	6.07	5.34	4.07	3.47	1999.4	5.5
LATITUDE	:	4.15	4.58	5.27	5.82	5.90	6.46	6.62	6.56	6.20	5.80	4.63	4.01	2008.8	5.5
LATITUDE	+15:	4.38	4.63	5.08	5.31	5.17	5.54	5.77	5.98	5.98	5.92	4.92	4.32	1917.5	5.3
TOPEKA KS		LATITUDE: 39 DEGREES 4 MINUTES													
LATITUDE	-15:	3.03	3.72	4.50	5.39	5.93	6.44	6.59	6.32	5.54	4.72	3.55	2.76	1781.4	4.9
LATITUDE	:	3.38	3.95	4.55	5.18	5.48	5.85	6.08	6.08	5.64	5.08	4.00	3.15	1778.0	4.9
LATITUDE	+15:	3.55	3.98	4.37	4.73	4.81	5.04	5.31	5.54	5.43	5.16	4.22	3.36	1688.6	4.6
WICHITA KS		LATITUDE: 37 DEGREES 39 MINUTES													
LATITUDE	-15:	3.43	4.15	5.01	5.84	6.30	6.86	6.93	6.71	5.84	5.06	3.92	3.21	1926.1	5.3
LATITUDE	:	3.85	4.43	5.09	5.62	5.82	6.23	6.39	6.47	5.96	5.47	4.44	3.69	1931.4	5.3
LATITUDE	+15:	4.05	4.48	4.90	5.14	5.11	5.36	5.58	5.90	5.75	5.57	4.70	3.95	1841.3	5.0
LEXINGTON KY		LATITUDE: 38 DEGREES 2 MINUTES													
LATITUDE	-15:	2.25	2.95	3.85	4.81	5.39	5.74	5.72	5.52	4.85	4.15	2.83	2.12	1528.7	4.2
LATITUDE	:	2.46	3.10	3.88	4.62	4.99	5.23	5.28	5.30	4.91	4.43	3.14	2.37	1513.9	4.1
LATITUDE	+15:	2.54	3.09	3.71	4.22	4.40	4.54	4.64	4.84	4.72	4.47	3.29	2.50	1429.3	3.9
LOUISVILLE KY		LATITUDE: 38 DEGREES 11 MINUTES													
LATITUDE	-15:	2.26	3.00	3.87	4.78	5.31	5.76	5.67	5.51	4.86	4.14	2.82	2.14	1526.7	4.2
LATITUDE	:	2.47	3.15	3.89	4.59	4.92	5.26	5.24	5.29	4.92	4.42	3.13	2.40	1512.8	4.1
LATITUDE	+15:	2.55	3.14	3.73	4.19	4.34	4.56	4.61	4.83	4.73	4.47	3.27	2.53	1429.0	3.9
BATON ROUGE LA		LATITUDE: 30 DEGREES 32 MINUTES													
LATITUDE	-15:	2.92	3.74	4.64	5.38	5.77	5.86	5.38	5.37	4.93	4.71	3.48	2.83	1675.1	4.6
LATITUDE	:	3.22	3.96	4.70	5.19	5.36	5.37	5.01	5.18	5.00	5.06	3.88	3.19	1677.2	4.6
LATITUDE	+15:	3.35	3.98	4.53	4.76	4.74	4.67	4.43	4.75	4.81	5.13	4.07	3.39	1600.1	4.4
LAKE CHARLES LA		LATITUDE: 30 DEGREES 7 MINUTES													
LATITUDE	-15:	2.67	3.56	4.39	5.01	5.71	5.99	5.51	5.29	4.99	5.01	3.45	2.67	1651.9	4.5
LATITUDE	:	2.91	3.75	4.44	4.83	5.31	5.48	5.12	5.11	5.06	5.39	3.84	3.00	1650.6	4.5
LATITUDE	+15:	3.01	3.76	4.27	4.43	4.69	4.75	4.53	4.68	4.87	5.47	4.02	3.16	1571.8	4.3
NEW ORLEANS LA		LATITUDE: 29 DEGREES 59 MINUTES													
LATITUDE	-15:	3.09	3.93	4.74	5.70	6.08	6.11	5.60	5.49	5.09	4.81	3.66	2.98	1743.3	4.8
LATITUDE	:	3.41	4.17	4.81	5.50	5.65	5.59	5.21	5.30	5.17	5.17	4.09	3.37	1747.9	4.8
LATITUDE	+15:	3.56	4.20	4.63	5.05	4.98	4.85	4.61	4.86	4.99	5.25	4.30	3.58	1669.2	4.6

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE	ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
SHREVEPORT	LA	LATITUDE:	32 DEGREES 28 MINUTES													
LATITUDE	-15:		2.93	3.77	4.56	5.18	5.82	6.27	6.20	6.05	5.33	4.85	3.67	2.94	1753.2	4.8
LATITUDE	:		3.23	3.99	4.62	4.99	5.40	5.72	5.74	5.84	5.42	5.22	4.11	3.33	1753.8	4.8
LATITUDE	+15:		3.37	4.01	4.44	4.57	4.76	4.95	5.05	5.34	5.22	5.30	4.32	3.54	1670.6	4.6
BOSTON	MA	LATITUDE:	42 DEGREES 22 MINUTES													
LATITUDE	-15:		2.17	2.86	3.69	4.37	5.02	5.50	5.43	4.93	4.67	3.74	2.34	1.97	1421.2	3.9
LATITUDE	:		2.38	3.00	3.71	4.18	4.64	5.01	5.01	4.73	4.72	3.99	2.59	2.21	1405.3	3.9
LATITUDE	+15:		2.47	2.99	3.54	3.81	4.08	4.34	4.40	4.31	4.53	4.02	2.70	2.33	1325.0	3.6
BALTIMORE	MD	LATITUDE:	39 DEGREES 11 MINUTES													
LATITUDE	-15:		2.55	3.28	4.13	4.87	5.29	5.69	5.63	5.25	4.79	4.01	2.94	2.29	1544.2	4.2
LATITUDE	:		2.81	3.47	4.17	4.67	4.90	5.19	5.20	5.04	4.84	4.28	3.28	2.58	1534.8	4.2
LATITUDE	+15:		2.93	3.47	3.99	4.26	4.31	4.50	4.57	4.60	4.65	4.32	3.44	2.73	1453.9	4.0
PATUXENT RIVER	MD	LATITUDE:	38 DEGREES 17 MINUTES													
LATITUDE	-15:		2.59	3.33	4.17	5.02	5.45	5.73	5.61	5.33	4.85	4.05	3.10	2.42	1572.7	4.3
LATITUDE	:		2.86	3.52	4.21	4.82	5.04	5.23	5.19	5.12	4.91	4.32	3.47	2.74	1565.0	4.3
LATITUDE	+15:		2.98	3.53	4.04	4.40	4.44	4.53	4.56	4.67	4.72	4.36	3.64	2.91	1484.2	4.1
BANGOR	ME	LATITUDE:	44 DEGREES 48 MINUTES													
LATITUDE	-15:		2.25	3.09	4.11	4.83	5.39	5.63	5.80	5.45	4.80	3.69	2.36	2.02	1504.8	4.1
LATITUDE	:		2.49	3.27	4.15	4.62	4.97	5.12	5.34	5.22	4.86	3.95	2.63	2.29	1489.3	4.1
LATITUDE	+15:		2.60	3.27	3.98	4.21	4.36	4.43	4.68	4.76	4.67	3.98	2.75	2.43	1404.1	3.8
CARIBOU	ME	LATITUDE:	46 DEGREES 52 MINUTES													
LATITUDE	-15:		2.21	3.24	4.40	4.78	4.93	5.33	5.51	5.10	4.26	3.07	1.85	1.74	1413.0	3.9
LATITUDE	:		2.46	3.44	4.46	4.58	4.54	4.84	5.07	4.88	4.30	3.27	2.03	1.97	1394.9	3.8
LATITUDE	+15:		2.57	3.46	4.28	4.16	3.99	4.19	4.44	4.44	4.12	3.28	2.11	2.08	1312.1	3.6
PORTLAND	ME	LATITUDE:	43 DEGREES 39 MINUTES													
LATITUDE	-15:		2.12	2.79	3.54	4.31	4.86	5.18	5.15	4.87	4.32	3.51	2.18	1.81	1359.8	3.7
LATITUDE	:		2.33	2.93	3.56	4.13	4.49	4.72	4.75	4.67	4.36	3.74	2.41	2.03	1343.3	3.7
LATITUDE	+15:		2.43	2.93	3.40	3.76	3.95	4.10	4.17	4.25	4.18	3.77	2.51	2.14	1265.6	3.5
ALPENA	MI	LATITUDE:	45 DEGREES 4 MINUTES													
LATITUDE	-15:		1.67	2.55	3.85	4.71	5.36	5.69	5.87	5.35	4.39	3.23	1.81	1.49	1400.8	3.8
LATITUDE	:		1.82	2.66	3.88	4.50	4.94	5.16	5.40	5.12	4.43	3.42	1.98	1.70	1371.6	3.8
LATITUDE	+15:		1.87	2.65	3.71	4.10	4.33	4.46	4.73	4.66	4.24	3.44	2.04	1.81	1280.1	3.5

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL	AVERAGE DAY
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	(KWH/SQ. M)	(KWH/SQ. M)
DETROIT MI		LATITUDE: 42 DEGREES 25 MINUTES													
LATITUDE	-15:	1.83	2.71	3.61	4.63	5.32	5.66	5.70	5.24	4.65	3.69	2.19	1.58	1425.7	3.9
LATITUDE	:	1.99	2.84	3.63	4.43	4.92	5.15	5.26	5.02	4.70	3.93	2.42	1.75	1401.6	3.8
LATITUDE	+15:	2.05	2.83	3.47	4.04	4.32	4.46	4.61	4.58	4.51	3.96	2.51	1.83	1313.9	3.6
FLINT MI		LATITUDE: 42 DEGREES 58 MINUTES													
LATITUDE	-15:	1.65	2.53	3.46	4.42	5.15	5.49	5.59	5.19	4.43	3.49	1.94	1.60	1369.4	3.8
LATITUDE	:	1.79	2.64	3.47	4.24	4.76	5.00	5.16	4.98	4.48	3.72	2.13	1.82	1345.7	3.7
LATITUDE	+15:	1.83	2.62	3.31	3.86	4.19	4.34	4.53	4.54	4.30	3.75	2.20	1.94	1261.1	3.5
GRAND RAPIDS MI		LATITUDE: 42 DEGREES 53 MINUTES													
LATITUDE	-15:	1.78	2.57	3.69	4.68	5.46	5.93	5.95	5.62	4.71	3.63	2.03	1.60	1452.3	4.0
LATITUDE	:	1.98	2.69	3.71	4.48	5.04	5.40	5.49	5.39	4.77	3.87	2.23	1.83	1428.6	3.9
LATITUDE	+15:	2.08	2.68	3.55	4.09	4.43	4.67	4.81	4.92	4.58	3.90	2.32	1.95	1339.2	3.7
HOUGHTON MI		LATITUDE: 47 DEGREES 10 MINUTES													
LATITUDE	-15:	1.23	1.96	3.54	4.61	5.18	5.56	5.76	5.19	3.88	3.01	1.58	1.05	1297.0	3.6
LATITUDE	:	1.35	2.02	3.56	4.40	4.77	5.04	5.29	4.96	3.90	3.19	1.76	1.17	1262.7	3.5
LATITUDE	+15:	1.40	1.98	3.40	4.00	4.18	4.36	4.62	4.51	3.73	3.20	1.84	1.23	1172.0	3.2
SAULT STE. MARIE MI		LATITUDE: 46 DEGREES 28 MINUTES													
LATITUDE	-15:	1.52	2.56	3.93	4.66	5.26	5.49	5.74	5.16	4.00	2.96	1.58	1.48	1351.2	3.7
LATITUDE	:	1.64	2.69	3.96	4.45	4.85	4.98	5.28	4.94	4.03	3.14	1.72	1.69	1321.4	3.6
LATITUDE	+15:	1.69	2.68	3.79	4.05	4.25	4.31	4.62	4.49	3.86	3.15	1.76	1.80	1231.9	3.4
TRAVERSE CITY MI		LATITUDE: 44 DEGREES 44 MINUTES													
LATITUDE	-15:	1.53	2.27	3.72	4.69	5.39	5.80	5.96	5.44	4.40	3.25	1.74	1.37	1388.7	3.8
LATITUDE	:	1.70	2.36	3.74	4.49	4.97	5.27	5.49	5.21	4.45	3.46	1.90	1.55	1358.7	3.7
LATITUDE	+15:	1.77	2.33	3.58	4.09	4.36	4.55	4.81	4.75	4.26	3.47	1.96	1.64	1267.1	3.5
DULUTH MN		LATITUDE: 46 DEGREES 50 MINUTES													
LATITUDE	-15:	1.99	2.97	3.97	4.63	5.13	5.35	5.81	5.27	4.23	3.27	1.95	1.59	1405.7	3.9
LATITUDE	:	2.20	3.14	4.00	4.43	4.73	4.86	5.34	5.05	4.27	3.49	2.15	1.79	1383.8	3.8
LATITUDE	+15:	2.29	3.14	3.83	4.03	4.15	4.21	4.68	4.59	4.09	3.51	2.24	1.89	1298.1	3.6
INTERNATIONAL FALLS MN		LATITUDE: 48 DEGREES 34 MINUTES													
LATITUDE	-15:	1.93	3.05	4.13	4.94	5.38	5.62	6.04	5.60	4.45	3.32	1.86	1.63	1460.5	4.0
LATITUDE	:	2.13	3.24	4.17	4.73	4.95	5.10	5.55	5.36	4.51	3.55	2.06	1.84	1436.4	3.9
LATITUDE	+15:	2.22	3.25	3.99	4.29	4.33	4.40	4.85	4.88	4.32	3.57	2.14	1.95	1345.2	3.7

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC		
MINNEAPOLIS-ST. PAUMN		LATITUDE: 44 DEGREES 53 MINUTES													
LATITUDE	-15:	2.31	3.29	4.16	4.84	5.41	5.84	6.16	5.73	4.81	3.81	2.43	1.85	1541.8	4.2
LATITUDE	:	2.57	3.49	4.20	4.63	4.99	5.31	5.67	5.50	4.87	4.08	2.71	2.09	1525.4	4.2
LATITUDE	+15:	2.69	3.50	4.03	4.22	4.38	4.59	4.96	5.01	4.68	4.12	2.83	2.21	1437.2	3.9
ROCHESTER MN		LATITUDE: 43 DEGREES 55 MINUTES													
LATITUDE	-15:	2.31	3.16	4.02	4.70	5.28	5.76	5.95	5.60	4.72	3.77	2.42	1.88	1510.0	4.1
LATITUDE	:	2.56	3.35	4.06	4.50	4.87	5.24	5.49	5.38	4.79	4.03	2.70	2.12	1494.0	4.1
LATITUDE	+15:	2.67	3.36	3.89	4.10	4.28	4.54	4.81	4.90	4.60	4.07	2.82	2.24	1408.3	3.9
COLUMBIA MO		LATITUDE: 38 DEGREES 49 MINUTES													
LATITUDE	-15:	2.64	3.41	4.19	4.99	5.82	6.33	6.55	6.21	5.24	4.47	3.13	2.38	1686.8	4.6
LATITUDE	:	2.93	3.61	4.23	4.79	5.39	5.76	6.05	5.98	5.33	4.80	3.50	2.69	1676.9	4.6
LATITUDE	+15:	3.05	3.62	4.06	4.38	4.74	4.98	5.30	5.46	5.13	4.87	3.68	2.86	1587.2	4.3
KANSAS CITY MO		LATITUDE: 39 DEGREES 18 MINUTES													
LATITUDE	-15:	2.88	3.53	4.30	5.17	5.80	6.30	6.51	6.16	5.29	4.48	3.37	2.66	1718.9	4.7
LATITUDE	:	3.21	3.74	4.34	4.96	5.36	5.72	6.00	5.93	5.37	4.81	3.78	3.02	1712.9	4.7
LATITUDE	+15:	3.36	3.76	4.17	4.53	4.71	4.94	5.25	5.41	5.17	4.88	3.99	3.22	1624.9	4.5
SPRINGFIELD MO		LATITUDE: 37 DEGREES 14 MINUTES													
LATITUDE	-15:	2.89	3.55	4.34	5.23	5.82	6.28	6.37	6.14	5.28	4.53	3.36	2.70	1720.5	4.7
LATITUDE	:	3.21	3.76	4.38	5.02	5.38	5.72	5.88	5.91	5.36	4.87	3.76	3.06	1714.8	4.7
LATITUDE	+15:	3.36	3.77	4.21	4.59	4.73	4.94	5.15	5.40	5.16	4.94	3.95	3.26	1627.2	4.5
ST. LOUIS MO		LATITUDE: 38 DEGREES 45 MINUTES													
LATITUDE	-15:	2.72	3.46	4.28	5.12	5.79	6.34	6.34	5.99	5.28	4.45	3.20	2.42	1687.1	4.6
LATITUDE	:	3.02	3.66	4.33	4.92	5.36	5.77	5.85	5.76	5.37	4.79	3.59	2.74	1679.1	4.6
LATITUDE	+15:	3.16	3.68	4.15	4.50	4.71	4.99	5.13	5.26	5.17	4.85	3.77	2.91	1591.1	4.4
JACKSON MS		LATITUDE: 32 DEGREES 19 MINUTES													
LATITUDE	-15:	2.88	3.71	4.66	5.49	5.98	6.14	5.88	5.73	5.16	4.72	3.54	2.83	1726.7	4.7
LATITUDE	:	3.17	3.93	4.72	5.29	5.55	5.61	5.45	5.52	5.23	5.06	3.95	3.20	1725.1	4.7
LATITUDE	+15:	3.30	3.94	4.54	4.84	4.89	4.86	4.80	5.05	5.04	5.14	4.14	3.39	1641.5	4.5
MERIDIAN MS		LATITUDE: 32 DEGREES 20 MINUTES													
LATITUDE	-15:	2.84	3.66	4.51	5.33	5.73	5.96	5.62	5.60	4.96	4.66	3.51	2.79	1679.7	4.6
LATITUDE	:	3.13	3.88	4.57	5.14	5.32	5.45	5.21	5.39	5.03	5.00	3.92	3.15	1679.2	4.6
LATITUDE	+15:	3.25	3.89	4.39	4.71	4.69	4.73	4.60	4.94	4.84	5.07	4.11	3.34	1599.3	4.4

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC		
BILLINGS	MT	LATITUDE:		45 DEGREES		48 MINUTES									
	LATITUDE -15:	2.55	3.36	4.59	5.15	5.99	6.61	7.51	7.02	5.87	4.65	3.08	2.45	1792.7	4.9
	LATITUDE :	2.85	3.57	4.65	4.93	5.52	5.99	6.90	6.76	5.99	5.02	3.48	2.81	1781.6	4.9
	LATITUDE +15:	2.99	3.59	4.47	4.49	4.83	5.15	6.01	6.16	5.79	5.11	3.67	3.00	1683.0	4.6
CUT BANK	MT	LATITUDE:		48 DEGREES		36 MINUTES									
	LATITUDE -15:	2.28	3.20	4.50	5.10	5.93	6.22	7.25	6.68	5.57	4.36	2.89	2.17	1711.5	4.7
	LATITUDE :	2.55	3.40	4.56	4.87	5.45	5.63	6.65	6.42	5.68	4.71	3.26	2.49	1696.8	4.6
	LATITUDE +15:	2.67	3.42	4.38	4.43	4.77	4.84	5.79	5.85	5.47	4.78	3.44	2.66	1599.3	4.4
DILLON	MT	LATITUDE:		45 DEGREES		15 MINUTES									
	LATITUDE -15:	2.76	3.75	4.96	5.56	6.23	6.50	7.53	6.99	6.05	4.79	3.30	2.59	1858.4	5.1
	LATITUDE :	3.09	4.00	5.04	5.32	5.73	5.89	6.91	6.72	6.18	5.19	3.73	2.97	1850.8	5.1
	LATITUDE +15:	3.25	4.03	4.85	4.85	5.01	5.06	6.01	6.12	5.97	5.28	3.94	3.18	1751.6	4.8
GLASGOW	MT	LATITUDE:		48 DEGREES		13 MINUTES									
	LATITUDE -15:	2.13	3.08	4.37	5.09	5.73	6.22	6.93	6.53	5.48	4.34	2.82	2.12	1671.4	4.6
	LATITUDE :	2.37	3.26	4.42	4.87	5.27	5.62	6.36	6.27	5.58	4.68	3.17	2.43	1654.7	4.5
	LATITUDE +15:	2.48	3.27	4.24	4.42	4.61	4.84	5.54	5.71	5.38	4.75	3.34	2.59	1557.9	4.3
GREAT FALLS	MT	LATITUDE:		47 DEGREES		29 MINUTES									
	LATITUDE -15:	2.28	3.28	4.62	5.07	5.80	6.39	7.36	6.76	5.60	4.52	2.85	2.02	1723.5	4.7
	LATITUDE :	2.55	3.48	4.68	4.85	5.33	5.79	6.76	6.50	5.71	4.88	3.21	2.31	1707.5	4.7
	LATITUDE +15:	2.66	3.50	4.50	4.41	4.67	4.97	5.88	5.92	5.50	4.96	3.38	2.46	1608.4	4.4
HELENA	MT	LATITUDE:		46 DEGREES		36 MINUTES									
	LATITUDE -15:	2.18	3.13	4.44	5.04	5.82	6.20	7.36	6.70	5.67	4.41	2.90	2.13	1706.7	4.7
	LATITUDE :	2.43	3.32	4.50	4.82	5.36	5.62	6.76	6.44	5.79	4.76	3.26	2.43	1690.7	4.6
	LATITUDE +15:	2.53	3.33	4.32	4.39	4.69	4.84	5.88	5.87	5.58	4.83	3.44	2.59	1592.8	4.4
LEWISTOWN	MT	LATITUDE:		47 DEGREES		3 MINUTES									
	LATITUDE -15:	2.24	3.09	4.40	4.90	5.66	6.25	7.22	6.62	5.52	4.35	2.83	2.19	1684.1	4.6
	LATITUDE :	2.49	3.27	4.45	4.68	5.20	5.66	6.62	6.35	5.62	4.69	3.18	2.50	1667.2	4.6
	LATITUDE +15:	2.60	3.28	4.27	4.26	4.55	4.86	5.76	5.78	5.41	4.76	3.35	2.66	1569.7	4.3
MILES CITY	MT	LATITUDE:		46 DEGREES		26 MINUTES									
	LATITUDE -15:	2.43	3.32	4.61	5.23	5.94	6.52	7.22	6.88	5.80	4.59	3.10	2.38	1767.4	4.8
	LATITUDE :	2.71	3.53	4.67	5.01	5.47	5.90	6.63	6.61	5.92	4.96	3.51	2.72	1755.3	4.8
	LATITUDE +15:	2.84	3.54	4.48	4.56	4.78	5.07	5.77	6.02	5.71	5.04	3.70	2.91	1657.2	4.5

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC		
MISSOULA	MT	LATITUDE: 46 DEGREES 55 MINUTES													
	LATITUDE -15:	1.46	2.43	3.74	4.67	5.58	5.87	7.35	6.54	5.43	3.77	2.16	1.41	1537.4	4.2
	LATITUDE :	1.58	2.55	3.77	4.47	5.14	5.33	6.76	6.28	5.54	4.04	2.40	1.57	1506.6	4.1
	LATITUDE +15:	1.62	2.53	3.60	4.06	4.51	4.60	5.88	5.72	5.34	4.08	2.51	1.64	1405.2	3.8
ASHEVILLE	NC	LATITUDE: 35 DEGREES 26 MINUTES													
	LATITUDE -15:	2.93	3.65	4.54	5.41	5.57	5.63	5.47	5.27	4.73	4.40	3.56	2.82	1643.1	4.5
	LATITUDE :	3.25	3.86	4.59	5.20	5.16	5.15	5.07	5.07	4.79	4.72	3.99	3.20	1645.1	4.5
	LATITUDE +15:	3.40	3.88	4.42	4.76	4.55	4.48	4.47	4.64	4.60	4.78	4.21	3.41	1569.4	4.3
CAPE HATTERAS	NC	LATITUDE: 35 DEGREES 16 MINUTES													
	LATITUDE -15:	2.75	3.55	4.61	5.76	6.05	6.17	5.92	5.53	5.14	4.35	3.66	2.82	1714.8	4.7
	LATITUDE :	3.04	3.76	4.66	5.55	5.60	5.62	5.48	5.32	5.22	4.66	4.11	3.20	1711.1	4.7
	LATITUDE +15:	3.17	3.77	4.48	5.07	4.93	4.87	4.82	4.87	5.02	4.72	4.34	3.40	1625.9	4.5
CHARLOTTE	NC	LATITUDE: 35 DEGREES 13 MINUTES													
	LATITUDE -15:	2.91	3.64	4.57	5.50	5.72	5.83	5.64	5.50	4.93	4.51	3.62	2.88	1681.8	4.6
	LATITUDE :	3.22	3.85	4.62	5.29	5.30	5.32	5.23	5.29	5.00	4.83	4.06	3.28	1682.8	4.6
	LATITUDE +15:	3.36	3.87	4.44	4.84	4.67	4.62	4.60	4.84	4.81	4.90	4.28	3.49	1603.7	4.4
CHERRY POINT	NC	LATITUDE: 34 DEGREES 54 MINUTES													
	LATITUDE -15:	3.06	3.83	4.82	5.82	5.94	5.89	5.64	5.29	4.96	4.46	3.78	3.07	1721.2	4.7
	LATITUDE :	3.40	4.07	4.88	5.61	5.50	5.38	5.23	5.09	5.03	4.79	4.26	3.51	1726.8	4.7
	LATITUDE +15:	3.56	4.10	4.70	5.13	4.85	4.67	4.61	4.66	4.84	4.85	4.51	3.75	1649.7	4.5
GREENSBORO	NC	LATITUDE: 36 DEGREES 5 MINUTES													
	LATITUDE -15:	2.95	3.67	4.59	5.47	5.76	5.92	5.75	5.52	4.98	4.43	3.58	2.89	1689.5	4.6
	LATITUDE :	3.28	3.89	4.64	5.26	5.33	5.40	5.32	5.30	5.05	4.75	4.02	3.28	1689.4	4.6
	LATITUDE +15:	3.42	3.91	4.46	4.80	4.69	4.68	4.67	4.84	4.85	4.81	4.23	3.50	1608.9	4.4
RALEIGH-DURHAM	NC	LATITUDE: 35 DEGREES 52 MINUTES													
	LATITUDE -15:	2.83	3.55	4.44	5.34	5.58	5.66	5.47	5.22	4.81	4.25	3.40	2.74	1622.3	4.4
	LATITUDE :	3.13	3.75	4.49	5.14	5.18	5.17	5.07	5.03	4.87	4.55	3.81	3.11	1622.5	4.4
	LATITUDE +15:	3.27	3.77	4.32	4.70	4.57	4.50	4.48	4.60	4.69	4.60	4.01	3.31	1546.1	4.2
BISMARCK	ND	LATITUDE: 46 DEGREES 46 MINUTES													
	LATITUDE -15:	2.53	3.51	4.55	4.94	5.79	6.26	6.88	6.52	5.40	4.31	2.82	2.22	1697.8	4.7
	LATITUDE :	2.83	3.75	4.61	4.73	5.33	5.67	6.32	6.26	5.51	4.65	3.18	2.54	1686.3	4.6
	LATITUDE +15:	2.97	3.77	4.43	4.30	4.67	4.88	5.51	5.70	5.30	4.72	3.35	2.71	1592.8	4.4

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC		
FARGO	ND	LATITUDE: 46 DEGREES 54 MINUTES													
LATITUDE	-15:	2.18	3.15	4.25	5.00	5.75	6.05	6.67	6.32	5.19	4.13	2.49	1.95	1618.6	4.4
LATITUDE	:	2.42	3.34	4.30	4.79	5.29	5.49	6.13	6.07	5.28	4.44	2.79	2.22	1601.1	4.4
LATITUDE	+15:	2.53	3.35	4.12	4.36	4.64	4.73	5.35	5.53	5.08	4.51	2.93	2.36	1507.0	4.1
MINOT	ND	LATITUDE: 48 DEGREES 16 MINUTES													
LATITUDE	-15:	2.11	2.99	4.10	4.99	5.80	6.00	6.62	6.29	5.18	4.18	2.52	1.92	1606.1	4.4
LATITUDE	:	2.34	3.17	4.14	4.77	5.34	5.43	6.07	6.03	5.26	4.50	2.83	2.19	1586.7	4.3
LATITUDE	+15:	2.45	3.18	3.97	4.33	4.66	4.68	5.29	5.49	5.06	4.56	2.97	2.33	1491.4	4.1
GRAND ISLAND	NE	LATITUDE: 40 DEGREES 58 MINUTES													
LATITUDE	-15:	3.10	3.75	4.62	5.62	6.13	6.80	6.89	6.50	5.63	4.86	3.58	2.86	1837.6	5.0
LATITUDE	:	3.48	3.99	4.68	5.40	5.66	6.17	6.35	6.26	5.74	5.26	4.05	3.28	1836.5	5.0
LATITUDE	+15:	3.66	4.02	4.50	4.93	4.97	5.31	5.55	5.71	5.54	5.35	4.29	3.52	1745.5	4.8
NORTH OMAHA	NE	LATITUDE: 41 DEGREES 22 MINUTES													
LATITUDE	-15:	3.00	3.66	4.48	5.16	5.81	6.43	6.55	6.22	5.08	4.46	3.06	2.56	1719.8	4.7
LATITUDE	:	3.36	3.89	4.53	4.95	5.36	5.84	6.03	5.98	5.16	4.80	3.43	2.91	1712.3	4.7
LATITUDE	+15:	3.53	3.91	4.35	4.51	4.71	5.03	5.27	5.45	4.96	4.87	3.61	3.11	1622.5	4.4
NORTH PLATTE	NE	LATITUDE: 41 DEGREES 8 MINUTES													
LATITUDE	-15:	3.31	3.95	4.91	5.73	6.17	6.87	7.09	6.67	5.88	5.09	3.74	3.13	1905.3	5.2
LATITUDE	:	3.72	4.22	4.98	5.50	5.69	6.22	6.52	6.42	6.00	5.51	4.24	3.61	1907.1	5.2
LATITUDE	+15:	3.92	4.25	4.79	5.01	4.98	5.35	5.68	5.85	5.79	5.62	4.49	3.87	1814.5	5.0
SCOTTSBLUFF	NE	LATITUDE: 41 DEGREES 52 MINUTES													
LATITUDE	-15:	3.29	3.98	4.85	5.55	6.02	6.78	7.12	6.75	6.08	5.01	3.61	3.02	1889.5	5.2
LATITUDE	:	3.71	4.25	4.92	5.33	5.55	6.15	6.55	6.50	6.22	5.42	4.09	3.48	1892.9	5.2
LATITUDE	+15:	3.91	4.29	4.74	4.87	4.87	5.29	5.72	5.93	6.01	5.53	4.33	3.73	1802.4	4.9
CONCORD	NH	LATITUDE: 43 DEGREES 12 MINUTES													
LATITUDE	-15:	2.14	2.78	3.54	4.35	4.90	5.16	5.19	4.83	4.22	3.45	2.17	1.77	1355.8	3.7
LATITUDE	:	2.36	2.92	3.56	4.16	4.53	4.70	4.79	4.63	4.25	3.67	2.39	1.98	1337.6	3.7
LATITUDE	+15:	2.45	2.91	3.40	3.79	3.98	4.08	4.20	4.21	4.07	3.69	2.49	2.08	1258.8	3.4
LAKEHURST	NJ	LATITUDE: 40 DEGREES 2 MINUTES													
LATITUDE	-15:	2.47	3.13	3.96	4.78	5.17	5.38	5.26	5.04	4.55	3.88	2.81	2.22	1480.9	4.1
LATITUDE	:	2.73	3.30	3.99	4.58	4.78	4.90	4.86	4.83	4.60	4.13	3.13	2.50	1470.9	4.0
LATITUDE	+15:	2.84	3.30	3.82	4.18	4.21	4.26	4.28	4.41	4.41	4.17	3.28	2.65	1392.8	3.8

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC		
NEWARK	NJ	LATITUDE:		40 DEGREES		42 MINUTES									
LATITUDE	-15:	2.47	3.15	3.98	4.76	5.23	5.44	5.46	5.16	4.63	3.90	2.72	2.14	1493.2	4.1
LATITUDE	:	2.73	3.32	4.01	4.57	4.84	4.96	5.04	4.95	4.69	4.16	3.03	2.41	1483.1	4.1
LATITUDE	+15:	2.85	3.33	3.85	4.17	4.26	4.31	4.43	4.52	4.50	4.20	3.18	2.55	1404.2	3.8
ALBUQUERQUE	NM	LATITUDE:		35 DEGREES		3 MINUTES									
LATITUDE	-15:	4.35	5.22	6.28	7.29	7.83	8.09	7.67	7.50	7.07	6.17	4.98	4.23	2334.2	6.4
LATITUDE	:	4.94	5.62	6.43	7.03	7.21	7.30	7.06	7.24	7.26	6.73	5.70	4.92	2356.8	6.5
LATITUDE	+15:	5.24	5.72	6.22	6.42	6.27	6.22	6.14	6.60	7.03	6.90	6.09	5.33	2257.0	6.2
CLAYTON	NM	LATITUDE:		36 DEGREES		27 MINUTES									
LATITUDE	-15:	4.24	4.88	5.92	6.69	6.86	7.31	7.05	6.89	6.51	5.80	4.62	4.04	2155.5	5.9
LATITUDE	:	4.81	5.25	6.05	6.44	6.34	6.63	6.50	6.64	6.66	6.31	5.28	4.71	2179.6	6.0
LATITUDE	+15:	5.11	5.33	5.84	5.88	5.55	5.69	5.68	6.06	6.45	6.46	5.63	5.10	2092.3	5.7
FARMINGTON	NM	LATITUDE:		36 DEGREES		45 MINUTES									
LATITUDE	-15:	4.19	5.09	6.10	7.02	7.59	8.06	7.66	7.44	7.05	6.04	4.76	3.94	2280.6	6.2
LATITUDE	:	4.75	5.49	6.24	6.77	6.99	7.29	7.05	7.18	7.25	6.59	5.45	4.59	2301.7	6.3
LATITUDE	+15:	5.05	5.59	6.03	6.18	6.10	6.22	6.14	6.55	7.03	6.76	5.83	4.96	2203.8	6.0
ROSWELL	NM	LATITUDE:		33 DEGREES		24 MINUTES									
LATITUDE	-15:	4.30	5.20	6.33	7.21	7.58	7.90	7.52	7.29	6.73	5.88	4.73	4.12	2276.3	6.2
LATITUDE	:	4.87	5.61	6.48	6.96	6.99	7.14	6.93	7.03	6.89	6.40	5.40	4.78	2297.1	6.3
LATITUDE	+15:	5.16	5.71	6.27	6.35	6.10	6.10	6.04	6.42	6.67	6.55	5.76	5.17	2199.6	6.0
TRUTH OR CONSEQUENNM		LATITUDE:		33 DEGREES		14 MINUTES									
LATITUDE	-15:	4.64	5.53	6.62	7.60	7.89	8.01	7.28	7.20	6.82	6.10	5.13	4.37	2348.5	6.4
LATITUDE	:	5.28	5.98	6.79	7.33	7.27	7.24	6.72	6.95	6.98	6.64	5.88	5.09	2377.3	6.5
LATITUDE	+15:	5.61	6.09	6.58	6.69	6.32	6.18	5.86	6.34	6.76	6.81	6.29	5.52	2282.5	6.3
TUCUMCARI	NM	LATITUDE:		35 DEGREES		11 MINUTES									
LATITUDE	-15:	4.33	5.02	6.08	6.86	7.14	7.51	7.24	7.08	6.53	5.70	4.67	4.14	2201.1	6.0
LATITUDE	:	4.91	5.41	6.21	6.61	6.59	6.80	6.67	6.83	6.68	6.20	5.34	4.82	2223.5	6.1
LATITUDE	+15:	5.21	5.49	6.00	6.04	5.76	5.82	5.82	6.23	6.46	6.34	5.69	5.22	2132.1	5.8
ZUNI	NM	LATITUDE:		35 DEGREES		6 MINUTES									
LATITUDE	-15:	4.20	5.02	5.98	7.08	7.63	7.86	6.98	6.79	6.78	5.93	4.75	4.04	2223.0	6.1
LATITUDE	:	4.76	5.40	6.11	6.83	7.03	7.11	6.44	6.54	6.94	6.46	5.43	4.69	2243.3	6.1
LATITUDE	+15:	5.05	5.49	5.90	6.23	6.13	6.07	5.62	5.97	6.72	6.61	5.79	5.07	2148.6	5.9

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC		
ELKO	NV	LATITUDE:		40 DEGREES		50 MINUTES									
	-15:	3.25	4.31	5.44	6.34	7.17	7.67	8.18	7.84	7.28	5.80	4.01	3.16	2145.9	5.9
	:	3.65	4.62	5.55	6.10	6.61	6.94	7.52	7.57	7.50	6.33	4.57	3.65	2149.4	5.9
	+15:	3.85	4.67	5.35	5.57	5.77	5.94	6.53	6.90	7.28	6.49	4.86	3.92	2043.2	5.6
ELY	NV	LATITUDE:		39 DEGREES		17 MINUTES									
	-15:	3.84	4.69	5.93	6.68	7.17	7.61	7.60	7.46	7.31	6.04	4.48	3.63	2204.7	6.0
	:	4.34	5.04	6.06	6.43	6.60	6.88	6.99	7.19	7.52	6.59	5.12	4.21	2220.7	6.1
	+15:	4.60	5.11	5.85	5.87	5.76	5.89	6.08	6.56	7.29	6.75	5.46	4.54	2122.5	5.8
LAS VEGAS	NV	LATITUDE:		36 DEGREES		5 MINUTES									
	-15:	4.28	5.30	6.58	7.64	8.18	8.39	7.99	7.76	7.43	6.27	4.88	4.11	2398.8	6.6
	:	4.86	5.72	6.74	7.37	7.52	7.56	7.35	7.49	7.64	6.85	5.59	4.79	2418.3	6.6
	+15:	5.16	5.83	6.53	6.72	6.53	6.43	6.38	6.83	7.41	7.03	5.97	5.18	2311.4	6.3
LOVELOCK	NV	LATITUDE:		40 DEGREES		4 MINUTES									
	-15:	3.86	4.88	6.20	7.26	7.95	8.32	8.67	8.40	7.76	6.41	4.64	3.70	2376.4	6.5
	:	4.37	5.26	6.34	6.99	7.31	7.49	7.95	8.10	7.99	7.02	5.31	4.29	2387.9	6.5
	+15:	4.62	5.34	6.13	6.38	6.35	6.38	6.89	7.38	7.75	7.21	5.67	4.63	2274.7	6.2
RENO	NV	LATITUDE:		39 DEGREES		30 MINUTES									
	-15:	3.75	4.74	6.12	7.21	7.85	8.17	8.37	8.10	7.58	6.19	4.43	3.55	2316.2	6.3
	:	4.24	5.10	6.26	6.95	7.22	7.37	7.68	7.82	7.80	6.78	5.06	4.12	2326.3	6.4
	+15:	4.49	5.18	6.06	6.34	6.29	6.29	6.66	7.13	7.58	6.96	5.40	4.44	2215.6	6.1
TONOPAH	NV	LATITUDE:		38 DEGREES		4 MINUTES									
	-15:	4.23	5.20	6.54	7.47	7.99	8.41	8.38	8.14	7.63	6.45	4.90	4.10	2419.3	6.6
	:	4.81	5.62	6.71	7.20	7.35	7.58	7.69	7.86	7.85	7.06	5.62	4.78	2439.2	6.7
	+15:	5.10	5.71	6.49	6.57	6.39	6.44	6.67	7.16	7.62	7.26	6.01	5.18	2331.1	6.4
WINNEMUCCA	NV	LATITUDE:		40 DEGREES		54 MINUTES									
	-15:	3.26	4.27	5.48	6.59	7.37	7.79	8.36	7.97	7.35	5.81	4.01	3.18	2175.9	6.0
	:	3.67	4.58	5.59	6.34	6.78	7.04	7.68	7.69	7.57	6.34	4.56	3.67	2178.2	6.0
	+15:	3.87	4.63	5.40	5.79	5.92	6.02	6.67	7.02	7.35	6.50	4.85	3.95	2069.0	5.7
YUCCA FLATS	NV	LATITUDE:		36 DEGREES		57 MINUTES									
	-15:	4.25	5.07	6.39	7.42	7.98	8.27	8.21	7.90	7.44	6.25	4.75	4.07	2375.0	6.5
	:	4.84	5.47	6.55	7.17	7.35	7.47	7.55	7.63	7.66	6.84	5.45	4.75	2396.5	6.6
	+15:	5.14	5.57	6.35	6.54	6.40	6.37	6.56	6.96	7.45	7.03	5.83	5.14	2292.6	6.3

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL	AVERAGE DAY
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	(KWH/SQ. M)	(KWH/SQ. M)
ALBANY	NY	LATITUDE: 42 DEGREES 45 MINUTES													
LATITUDE	-15:	2.08	2.77	3.57	4.40	4.86	5.24	5.35	4.98	4.32	3.41	2.09	1.68	1363.8	3.7
LATITUDE	:	2.28	2.91	3.59	4.22	4.50	4.78	4.94	4.78	4.36	3.63	2.30	1.88	1344.6	3.7
LATITUDE	+15:	2.37	2.90	3.43	3.84	3.96	4.15	4.34	4.35	4.18	3.65	2.39	1.97	1264.5	3.5
BINGHAMTON	NY	LATITUDE: 42 DEGREES 13 MINUTES													
LATITUDE	-15:	1.84	2.20	3.05	4.07	4.63	5.09	5.14	4.71	4.13	3.20	1.80	1.48	1259.3	3.5
LATITUDE	:	2.05	2.27	3.04	3.89	4.28	4.64	4.74	4.51	4.16	3.39	1.96	1.67	1236.8	3.4
LATITUDE	+15:	2.15	2.23	2.89	3.55	3.77	4.03	4.17	4.11	3.98	3.40	2.01	1.77	1159.4	3.2
BUFFALO	NY	LATITUDE: 42 DEGREES 56 MINUTES													
LATITUDE	-15:	1.65	2.27	3.18	4.34	4.96	5.47	5.52	5.04	4.25	3.26	1.78	1.43	1315.2	3.6
LATITUDE	:	1.83	2.41	3.18	4.15	4.58	4.98	5.10	4.83	4.29	3.47	1.94	1.61	1291.3	3.5
LATITUDE	+15:	1.92	2.42	3.03	3.78	4.03	4.32	4.48	4.40	4.12	3.48	2.00	1.71	1209.3	3.3
CENTRAL PARK	NY	LATITUDE: 40 DEGREES 47 MINUTES													
LATITUDE	-15:	2.19	2.82	3.70	4.48	5.07	5.18	5.22	4.89	4.40	3.65	2.38	1.84	1395.3	3.8
LATITUDE	:	2.40	2.96	3.72	4.29	4.69	4.73	4.83	4.69	4.44	3.88	2.63	2.05	1380.0	3.8
LATITUDE	+15:	2.49	2.95	3.56	3.92	4.14	4.12	4.25	4.28	4.26	3.91	2.74	2.16	1302.0	3.6
LA GUARDIA	NY	LATITUDE: 40 DEGREES 46 MINUTES													
LATITUDE	-15:	2.45	3.16	4.02	4.79	5.24	5.47	5.52	5.23	4.66	3.90	2.71	2.16	1501.8	4.1
LATITUDE	:	2.71	3.34	4.05	4.60	4.85	4.98	5.10	5.02	4.72	4.17	3.02	2.44	1491.7	4.1
LATITUDE	+15:	2.82	3.34	3.89	4.20	4.27	4.33	4.49	4.58	4.53	4.21	3.16	2.59	1412.3	3.9
MASSENA	NY	LATITUDE: 44 DEGREES 56 MINUTES													
LATITUDE	-15:	1.84	2.56	3.63	4.48	5.03	5.39	5.45	4.99	4.23	3.17	1.83	1.43	1341.4	3.7
LATITUDE	:	2.02	2.68	3.65	4.29	4.64	4.90	5.02	4.78	4.28	3.37	2.00	1.58	1316.2	3.6
LATITUDE	+15:	2.09	2.67	3.49	3.91	4.08	4.25	4.41	4.35	4.10	3.39	2.07	1.66	1231.7	3.4
ROCHESTER	NY	LATITUDE: 43 DEGREES 7 MINUTES													
LATITUDE	-15:	1.77	2.16	3.25	4.43	4.98	5.50	5.53	5.06	4.29	3.27	1.80	1.43	1325.1	3.6
LATITUDE	:	1.97	2.23	3.25	4.24	4.60	5.00	5.09	4.85	4.33	3.47	1.96	1.61	1298.4	3.6
LATITUDE	+15:	2.06	2.19	3.09	3.86	4.05	4.33	4.47	4.42	4.15	3.48	2.02	1.71	1213.6	3.3
SYRACUSE	NY	LATITUDE: 43 DEGREES 7 MINUTES													
LATITUDE	-15:	1.68	2.21	3.19	4.38	4.89	5.38	5.46	5.01	4.32	3.26	1.77	1.45	1310.7	3.6
LATITUDE	:	1.82	2.29	3.19	4.18	4.52	4.90	5.03	4.80	4.36	3.45	1.93	1.64	1283.0	3.5
LATITUDE	+15:	1.86	2.25	3.03	3.81	3.97	4.24	4.42	4.37	4.18	3.46	1.98	1.74	1198.3	3.3

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC		
AKRON-CANTON															
	OH	LATITUDE:		40 DEGREES		55 MINUTES									
LATITUDE	-15:	1.79	2.49	3.41	4.45	5.17	5.58	5.54	5.28	4.64	3.71	2.23	1.54	1396.3	3.8
LATITUDE	:	1.94	2.59	3.42	4.27	4.79	5.09	5.12	5.07	4.69	3.96	2.45	1.69	1372.9	3.8
LATITUDE	+15:	1.99	2.57	3.27	3.90	4.22	4.42	4.50	4.63	4.50	3.99	2.55	1.76	1287.7	3.5
CINCINNATI															
	OH	LATITUDE:		39 DEGREES		4 MINUTES									
LATITUDE	-15:	2.08	2.82	3.60	4.56	5.17	5.57	5.47	5.37	4.70	3.97	2.55	1.90	1454.5	4.0
LATITUDE	:	2.26	2.95	3.62	4.37	4.78	5.08	5.06	5.15	4.76	4.23	2.82	2.11	1436.8	3.9
LATITUDE	+15:	2.33	2.93	3.46	3.99	4.21	4.40	4.45	4.70	4.56	4.27	2.94	2.21	1353.6	3.7
CLEVELAND															
	OH	LATITUDE:		41 DEGREES		24 MINUTES									
LATITUDE	-15:	1.80	2.29	3.26	4.43	5.21	5.59	5.67	5.24	4.54	3.56	2.05	1.55	1377.5	3.8
LATITUDE	:	2.00	2.37	3.26	4.24	4.82	5.09	5.23	5.03	4.58	3.79	2.25	1.76	1353.7	3.7
LATITUDE	+15:	2.10	2.33	3.11	3.87	4.24	4.41	4.59	4.58	4.40	3.82	2.32	1.87	1268.8	3.5
COLUMBUS															
	OH	LATITUDE:		40 DEGREES		0 MINUTES									
LATITUDE	-15:	1.91	2.58	3.45	4.42	5.09	5.49	5.43	5.41	4.63	3.83	2.35	1.70	1410.4	3.9
LATITUDE	:	2.07	2.68	3.46	4.23	4.71	5.00	5.01	5.19	4.68	4.08	2.59	1.87	1388.7	3.8
LATITUDE	+15:	2.13	2.66	3.30	3.86	4.15	4.34	4.41	4.73	4.49	4.12	2.69	1.95	1304.3	3.6
DAYTON															
	OH	LATITUDE:		39 DEGREES		54 MINUTES									
LATITUDE	-15:	2.07	2.79	3.62	4.60	5.26	5.68	5.60	5.43	4.77	3.93	2.48	1.80	1462.8	4.0
LATITUDE	:	2.26	2.93	3.64	4.41	4.87	5.18	5.18	5.21	4.83	4.19	2.75	2.00	1444.8	4.0
LATITUDE	+15:	2.33	2.92	3.48	4.03	4.30	4.49	4.56	4.76	4.64	4.23	2.86	2.10	1360.8	3.7
TOLEDO															
	OH	LATITUDE:		41 DEGREES		36 MINUTES									
LATITUDE	-15:	1.87	2.67	3.57	4.55	5.33	5.69	5.74	5.36	4.69	3.79	2.25	1.60	1434.9	3.9
LATITUDE	:	2.04	2.79	3.59	4.36	4.92	5.18	5.29	5.15	4.74	4.04	2.48	1.77	1411.6	3.9
LATITUDE	+15:	2.10	2.77	3.43	3.98	4.33	4.49	4.65	4.69	4.55	4.07	2.58	1.85	1324.2	3.6
YOUNGSTOWN															
	OH	LATITUDE:		41 DEGREES		16 MINUTES									
LATITUDE	-15:	1.77	2.21	3.13	4.18	4.91	5.33	5.37	4.97	4.35	3.48	1.99	1.53	1317.5	3.6
LATITUDE	:	1.97	2.28	3.13	4.00	4.54	4.86	4.96	4.76	4.39	3.70	2.17	1.73	1294.8	3.5
LATITUDE	+15:	2.06	2.25	2.98	3.65	4.00	4.21	4.36	4.34	4.20	3.72	2.24	1.84	1214.2	3.3
OKLAHOMA CITY															
	OK	LATITUDE:		35 DEGREES		24 MINUTES									
LATITUDE	-15:	3.30	3.99	4.89	5.60	5.91	6.49	6.57	6.37	5.47	4.78	3.82	3.16	1837.9	5.0
LATITUDE	:	3.69	4.25	4.96	5.39	5.47	5.91	6.07	6.13	5.57	5.15	4.31	3.61	1841.6	5.0
LATITUDE	+15:	3.87	4.28	4.78	4.93	4.82	5.10	5.31	5.60	5.37	5.23	4.55	3.86	1755.8	4.8

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC		
TULSA	OK	LATITUDE: 36 DEGREES				12 MINUTES									
LATITUDE	-15:	3.04	3.71	4.57	5.20	5.62	6.12	6.26	6.10	5.20	4.54	3.52	2.90	1729.3	4.7
LATITUDE	:	3.38	3.94	4.62	5.00	5.21	5.58	5.78	5.87	5.28	4.87	3.95	3.30	1728.5	4.7
LATITUDE	+15:	3.54	3.96	4.44	4.57	4.59	4.83	5.07	5.36	5.08	4.94	4.16	3.52	1645.0	4.5
ASTORIA	OR	LATITUDE: 46 DEGREES				9 MINUTES									
LATITUDE	-15:	1.66	2.23	3.20	4.19	5.00	4.91	5.45	5.07	4.57	3.16	1.93	1.29	1300.5	3.6
LATITUDE	:	1.85	2.32	3.20	3.99	4.61	4.47	5.01	4.85	4.63	3.35	2.13	1.42	1274.8	3.5
LATITUDE	+15:	1.94	2.29	3.05	3.63	4.04	3.87	4.39	4.41	4.43	3.37	2.21	1.48	1191.7	3.3
BURNS	OR	LATITUDE: 43 DEGREES				35 MINUTES									
LATITUDE	-15:	2.35	3.34	4.44	5.53	6.41	6.92	7.70	7.13	6.33	4.67	3.00	2.26	1831.1	5.0
LATITUDE	:	2.61	3.54	4.49	5.31	5.91	6.27	7.08	6.86	6.48	5.04	3.38	2.57	1813.6	5.0
LATITUDE	+15:	2.72	3.55	4.31	4.84	5.17	5.38	6.16	6.25	6.27	5.13	3.55	2.73	1707.5	4.7
MEDFORD	OR	LATITUDE: 42 DEGREES				22 MINUTES									
LATITUDE	-15:	1.76	2.99	4.16	5.47	6.33	6.90	7.73	7.20	6.08	4.22	2.35	1.54	1728.7	4.7
LATITUDE	:	1.91	3.15	4.19	5.25	5.83	6.25	7.10	6.93	6.22	4.53	2.60	1.70	1695.6	4.6
LATITUDE	+15:	1.96	3.15	4.02	4.78	5.11	5.37	6.18	6.32	6.00	4.58	2.71	1.77	1581.9	4.3
NORTH BEND	OR	LATITUDE: 43 DEGREES				25 MINUTES									
LATITUDE	-15:	2.03	2.89	3.90	5.03	5.79	6.04	6.57	6.03	5.24	3.85	2.57	1.91	1579.9	4.3
LATITUDE	:	2.23	3.04	3.92	4.82	5.33	5.49	6.05	5.80	5.33	4.12	2.86	2.15	1557.5	4.3
LATITUDE	+15:	2.31	3.04	3.75	4.39	4.68	4.74	5.28	5.28	5.12	4.16	3.00	2.27	1462.2	4.0
PENDLETON	OR	LATITUDE: 45 DEGREES				41 MINUTES									
LATITUDE	-15:	1.62	2.57	3.95	5.07	6.02	6.52	7.54	6.91	6.00	4.18	2.23	1.49	1649.4	4.5
LATITUDE	:	1.76	2.69	3.98	4.85	5.55	5.91	6.93	6.64	6.14	4.50	2.48	1.66	1618.1	4.4
LATITUDE	+15:	1.81	2.68	3.81	4.41	4.86	5.08	6.03	6.05	5.93	4.56	2.59	1.74	1510.0	4.1
PORTLAND	OR	LATITUDE: 45 DEGREES				36 MINUTES									
LATITUDE	-15:	1.59	2.25	3.31	4.37	5.18	5.37	6.38	5.70	4.68	3.16	1.88	1.46	1382.1	3.8
LATITUDE	:	1.76	2.34	3.31	4.18	4.77	4.89	5.87	5.46	4.74	3.35	2.07	1.66	1353.9	3.7
LATITUDE	+15:	1.84	2.31	3.16	3.80	4.19	4.23	5.13	4.97	4.55	3.37	2.15	1.77	1264.0	3.5
REDMOND	OR	LATITUDE: 44 DEGREES				16 MINUTES									
LATITUDE	-15:	2.43	3.31	4.50	5.68	6.50	6.94	7.68	7.11	6.25	4.52	2.95	2.30	1833.4	5.0
LATITUDE	:	2.70	3.50	4.55	5.45	5.98	6.28	7.05	6.84	6.39	4.88	3.31	2.62	1814.4	5.0
LATITUDE	+15:	2.82	3.52	4.36	4.96	5.23	5.39	6.13	6.23	6.17	4.95	3.49	2.78	1706.8	4.7

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC		
SALEM	OR	LATITUDE: 44 DEGREES 55 MINUTES													
	LATITUDE -15:	1.68	2.39	3.50	4.58	5.42	5.61	6.72	6.04	5.14	3.34	1.98	1.53	1461.0	4.0
	LATITUDE :	1.88	2.49	3.51	4.38	5.00	5.10	6.18	5.81	5.22	3.55	2.18	1.74	1434.1	3.9
	LATITUDE +15:	1.97	2.47	3.36	3.99	4.39	4.41	5.40	5.29	5.03	3.58	2.26	1.86	1340.9	3.7
ALLENTOWN	PA	LATITUDE: 40 DEGREES 39 MINUTES													
	LATITUDE -15:	2.33	3.01	3.86	4.63	5.07	5.38	5.47	5.10	4.49	3.79	2.57	2.00	1452.4	4.0
	LATITUDE :	2.57	3.17	3.89	4.44	4.69	4.91	5.05	4.89	4.54	4.04	2.85	2.24	1439.4	3.9
	LATITUDE +15:	2.67	3.17	3.72	4.05	4.14	4.27	4.44	4.46	4.36	4.07	2.98	2.36	1360.1	3.7
ERIE	PA	LATITUDE: 42 DEGREES 5 MINUTES													
	LATITUDE -15:	1.59	2.20	3.28	4.48	5.10	5.58	5.69	4.82	4.41	3.43	1.81	1.34	1332.2	3.6
	LATITUDE :	1.75	2.27	3.28	4.28	4.71	5.08	5.24	4.61	4.45	3.64	1.96	1.50	1303.8	3.6
	LATITUDE +15:	1.82	2.24	3.12	3.90	4.14	4.40	4.60	4.20	4.26	3.66	2.02	1.59	1217.3	3.3
HARRISBURG	PA	LATITUDE: 40 DEGREES 13 MINUTES													
	LATITUDE -15:	2.34	3.02	3.86	4.62	5.11	5.47	5.45	5.10	4.59	3.80	2.60	2.07	1462.7	4.0
	LATITUDE :	2.58	3.18	3.89	4.43	4.73	4.99	5.04	4.89	4.63	4.05	2.88	2.32	1449.2	4.0
	LATITUDE +15:	2.68	3.18	3.72	4.04	4.17	4.33	4.43	4.46	4.44	4.08	3.01	2.45	1369.0	3.8
PHILADELPHIA	PA	LATITUDE: 39 DEGREES 53 MINUTES													
	LATITUDE -15:	2.42	3.11	3.95	4.69	5.14	5.49	5.45	5.18	4.62	3.87	2.78	2.17	1488.2	4.1
	LATITUDE :	2.67	3.28	3.98	4.50	4.76	5.01	5.04	4.98	4.67	4.13	3.10	2.44	1478.5	4.1
	LATITUDE +15:	2.78	3.28	3.82	4.11	4.20	4.35	4.43	4.54	4.49	4.17	3.24	2.59	1400.4	3.8
PITTSBURGH	PA	LATITUDE: 40 DEGREES 30 MINUTES													
	LATITUDE -15:	1.75	2.36	3.32	4.30	4.96	5.34	5.23	4.97	4.36	3.63	2.20	1.68	1343.8	3.7
	LATITUDE :	1.88	2.45	3.33	4.12	4.59	4.87	4.83	4.77	4.41	3.87	2.42	1.91	1323.1	3.6
	LATITUDE +15:	1.92	2.42	3.17	3.76	4.05	4.23	4.25	4.35	4.22	3.89	2.51	2.03	1243.0	3.4
WILKES-BARRE-SCRANPA		LATITUDE: 41 DEGREES 20 MINUTES													
	LATITUDE -15:	1.98	2.69	3.54	4.39	4.92	5.33	5.41	5.00	4.37	3.70	2.18	1.67	1376.0	3.8
	LATITUDE :	2.16	2.82	3.55	4.20	4.55	4.86	4.99	4.79	4.41	3.94	2.40	1.84	1355.7	3.7
	LATITUDE +15:	2.22	2.80	3.39	3.83	4.01	4.22	4.39	4.37	4.22	3.97	2.49	1.93	1274.1	3.5
KOROR ISLAND	PN	LATITUDE: 7 DEGREES 20 MINUTES													
	LATITUDE -15:	4.14	4.72	5.04	5.36	5.05	4.72	4.65	4.70	4.73	4.56	4.29	3.93	1698.9	4.7
	LATITUDE :	4.60	5.03	5.15	5.23	4.77	4.41	4.40	4.59	4.82	4.87	4.78	4.45	1736.1	4.8
	LATITUDE +15:	4.84	5.10	5.00	4.85	4.27	3.91	3.95	4.27	4.68	4.95	5.04	4.75	1690.1	4.6

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL	AVERAGE DAY
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	(KWH/SQ. M)	(KWH/SQ. M)
KWAJALEIN ISLAND PN		LATITUDE: 8 DEGREES 44 MINUTES													
LATITUDE	-15:	4.69	5.32	5.57	5.50	5.23	5.20	5.16	5.34	5.01	4.64	4.35	4.28	1832.8	5.0
LATITUDE	:	5.27	5.72	5.69	5.37	4.94	4.84	4.88	5.21	5.11	4.96	4.86	4.89	1876.2	5.1
LATITUDE	+15:	5.58	5.82	5.53	4.97	4.41	4.27	4.36	4.82	4.96	5.04	5.13	5.26	1827.7	5.0
WAKE ISLAND PN		LATITUDE: 19 DEGREES 17 MINUTES													
LATITUDE	-15:	4.45	5.11	5.79	6.16	6.41	6.37	6.02	5.90	5.56	5.11	4.75	4.36	2007.1	5.5
LATITUDE	:	5.01	5.48	5.91	5.97	5.98	5.84	5.61	5.71	5.66	5.49	5.38	5.02	2039.2	5.6
LATITUDE	+15:	5.30	5.56	5.72	5.48	5.26	5.06	4.96	5.25	5.47	5.58	5.71	5.41	1969.7	5.4
SAN JUAN PR		LATITUDE: 18 DEGREES 26 MINUTES													
LATITUDE	-15:	4.33	4.96	5.69	5.95	5.68	5.67	5.86	5.80	5.33	4.89	4.47	4.05	1907.1	5.2
LATITUDE	:	4.85	5.31	5.81	5.77	5.32	5.24	5.48	5.62	5.42	5.24	5.03	4.63	1938.3	5.3
LATITUDE	+15:	5.12	5.38	5.63	5.31	4.72	4.58	4.85	5.17	5.24	5.32	5.33	4.97	1874.1	5.1
PROVIDENCE RI		LATITUDE: 41 DEGREES 44 MINUTES													
LATITUDE	-15:	2.30	2.95	3.72	4.53	5.14	5.38	5.25	4.95	4.43	3.77	2.48	2.01	1428.2	3.9
LATITUDE	:	2.53	3.10	3.74	4.34	4.75	4.90	4.85	4.75	4.47	4.02	2.76	2.26	1415.1	3.9
LATITUDE	+15:	2.64	3.10	3.58	3.96	4.18	4.26	4.27	4.33	4.29	4.06	2.88	2.39	1337.0	3.7
CHARLESTON SC		LATITUDE: 32 DEGREES 54 MINUTES													
LATITUDE	-15:	2.87	3.61	4.56	5.58	5.73	5.60	5.55	5.10	4.76	4.42	3.73	2.92	1656.9	4.5
LATITUDE	:	3.17	3.82	4.62	5.38	5.33	5.14	5.15	4.91	4.82	4.73	4.19	3.31	1660.5	4.5
LATITUDE	+15:	3.30	3.84	4.45	4.93	4.70	4.48	4.55	4.50	4.64	4.79	4.42	3.52	1585.6	4.3
COLUMBIA SC		LATITUDE: 33 DEGREES 57 MINUTES													
LATITUDE	-15:	3.01	3.76	4.66	5.64	5.85	5.91	5.68	5.50	4.97	4.57	3.76	3.01	1714.5	4.7
LATITUDE	:	3.34	3.99	4.72	5.44	5.42	5.41	5.27	5.30	5.04	4.91	4.23	3.43	1719.3	4.7
LATITUDE	+15:	3.49	4.02	4.55	4.98	4.78	4.69	4.65	4.85	4.85	4.98	4.47	3.65	1642.0	4.5
GREENVILLE-SPARTAN SC		LATITUDE: 34 DEGREES 54 MINUTES													
LATITUDE	-15:	2.93	3.66	4.60	5.50	5.67	5.82	5.65	5.50	4.88	4.50	3.66	2.84	1680.4	4.6
LATITUDE	:	3.25	3.88	4.66	5.30	5.26	5.32	5.24	5.30	4.94	4.83	4.11	3.22	1683.3	4.6
LATITUDE	+15:	3.39	3.90	4.48	4.85	4.64	4.62	4.62	4.85	4.75	4.90	4.34	3.43	1606.1	4.4
HURON SD		LATITUDE: 44 DEGREES 23 MINUTES													
LATITUDE	-15:	2.42	3.16	4.18	5.13	5.84	6.37	6.84	6.46	5.50	4.48	3.00	2.17	1692.0	4.6
LATITUDE	:	2.70	3.34	4.22	4.91	5.38	5.78	6.29	6.20	5.60	4.83	3.37	2.46	1677.5	4.6
LATITUDE	+15:	2.82	3.35	4.04	4.47	4.72	4.98	5.48	5.65	5.39	4.90	3.54	2.62	1582.2	4.3

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC		
PIERRE	SD	LATITUDE: 44 DEGREES 23 MINUTES													
LATITUDE	-15:	2.68	3.42	4.57	5.43	6.14	6.66	7.13	6.83	5.86	4.83	3.31	2.43	1806.6	4.9
LATITUDE	:	3.00	3.63	4.63	5.21	5.65	6.03	6.56	6.57	5.98	5.22	3.74	2.78	1797.0	4.9
LATITUDE	+15:	3.15	3.65	4.45	4.74	4.95	5.18	5.71	5.99	5.77	5.31	3.95	2.96	1699.3	4.7
RAPID CITY	SD	LATITUDE: 44 DEGREES 3 MINUTES													
LATITUDE	-15:	2.73	3.55	4.65	5.33	5.88	6.46	6.95	6.70	5.92	4.85	3.43	2.63	1799.9	4.9
LATITUDE	:	3.06	3.77	4.71	5.11	5.42	5.85	6.38	6.44	6.04	5.25	3.88	3.01	1794.2	4.9
LATITUDE	+15:	3.20	3.79	4.52	4.65	4.75	5.03	5.56	5.86	5.83	5.34	4.10	3.21	1700.4	4.7
SIOUX FALLS	SD	LATITUDE: 43 DEGREES 34 MINUTES													
LATITUDE	-15:	2.62	3.38	4.30	5.15	5.90	6.36	6.71	6.25	5.40	4.47	3.09	2.33	1704.4	4.7
LATITUDE	:	2.92	3.59	4.34	4.94	5.44	5.77	6.18	6.00	5.49	4.82	3.48	2.65	1693.6	4.6
LATITUDE	+15:	3.06	3.61	4.17	4.50	4.77	4.97	5.39	5.47	5.29	4.89	3.66	2.82	1601.3	4.4
CHATTANOOGA	TN	LATITUDE: 35 DEGREES 2 MINUTES													
LATITUDE	-15:	2.48	3.16	4.04	5.01	5.33	5.56	5.34	5.27	4.63	4.21	3.16	2.41	1540.7	4.2
LATITUDE	:	2.72	3.32	4.07	4.81	4.94	5.08	4.95	5.07	4.68	4.50	3.51	2.70	1533.0	4.2
LATITUDE	+15:	2.81	3.31	3.90	4.40	4.36	4.42	4.37	4.63	4.49	4.54	3.68	2.85	1454.4	4.0
KNOXVILLE	TN	LATITUDE: 35 DEGREES 49 MINUTES													
LATITUDE	-15:	2.48	3.21	4.12	5.19	5.56	5.77	5.56	5.41	4.84	4.31	3.15	2.40	1583.2	4.3
LATITUDE	:	2.72	3.38	4.16	4.99	5.16	5.27	5.15	5.21	4.90	4.62	3.51	2.70	1576.1	4.3
LATITUDE	+15:	2.82	3.38	4.00	4.57	4.55	4.58	4.54	4.76	4.71	4.67	3.68	2.86	1495.4	4.1
MEMPHIS	TN	LATITUDE: 35 DEGREES 3 MINUTES													
LATITUDE	-15:	2.73	3.52	4.42	5.30	5.81	6.19	6.07	5.93	5.14	4.63	3.37	2.65	1697.8	4.7
LATITUDE	:	3.01	3.71	4.46	5.10	5.38	5.64	5.62	5.71	5.21	4.97	3.76	2.99	1691.6	4.6
LATITUDE	+15:	3.13	3.72	4.29	4.66	4.73	4.88	4.93	5.21	5.01	5.04	3.95	3.18	1605.3	4.4
NASHVILLE	TN	LATITUDE: 36 DEGREES 7 MINUTES													
LATITUDE	-15:	2.30	3.06	3.91	5.01	5.62	5.94	5.83	5.66	4.91	4.32	2.95	2.18	1574.0	4.3
LATITUDE	:	2.51	3.21	3.93	4.81	5.21	5.42	5.40	5.44	4.97	4.62	3.27	2.43	1559.6	4.3
LATITUDE	+15:	2.59	3.20	3.77	4.40	4.59	4.69	4.74	4.97	4.77	4.67	3.42	2.55	1472.9	4.0
ABILENE	TX	LATITUDE: 32 DEGREES 26 MINUTES													
LATITUDE	-15:	3.63	4.34	5.42	5.94	6.28	6.70	6.59	6.32	5.49	4.90	4.03	3.57	1923.9	5.3
LATITUDE	:	4.06	4.63	5.51	5.72	5.82	6.10	6.09	6.09	5.58	5.27	4.54	4.10	1933.6	5.3
LATITUDE	+15:	4.27	4.68	5.32	5.24	5.12	5.26	5.34	5.57	5.38	5.36	4.80	4.40	1848.2	5.1

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC		
AMARILLO	TX	LATITUDE: 35 DEGREES 14 MINUTES													
	LATITUDE -15:	4.09	4.80	5.76	6.59	6.82	7.23	7.03	6.87	6.26	5.53	4.47	3.93	2112.4	5.8
	LATITUDE :	4.62	5.16	5.88	6.35	6.30	6.56	6.48	6.63	6.40	5.99	5.09	4.56	2130.9	5.8
	LATITUDE +15:	4.89	5.23	5.68	5.80	5.51	5.63	5.66	6.05	6.18	6.12	5.42	4.93	2041.5	5.6
AUSTIN	TX	LATITUDE: 30 DEGREES 18 MINUTES													
	LATITUDE -15:	3.24	4.00	4.81	5.13	5.66	6.30	6.49	6.19	5.43	4.83	3.76	3.21	1797.6	4.9
	LATITUDE :	3.58	4.25	4.87	4.95	5.26	5.75	6.01	5.98	5.52	5.18	4.20	3.64	1801.9	4.9
	LATITUDE +15:	3.74	4.28	4.69	4.54	4.65	4.98	5.27	5.47	5.33	5.26	4.42	3.88	1719.6	4.7
BROWNSVILLE	TX	LATITUDE: 25 DEGREES 54 MINUTES													
	LATITUDE -15:	3.20	3.86	4.78	5.52	5.97	6.48	6.84	6.44	5.58	4.96	3.74	3.08	1841.3	5.0
	LATITUDE :	3.54	4.09	4.85	5.34	5.56	5.93	6.34	6.23	5.68	5.34	4.17	3.47	1843.4	5.1
	LATITUDE +15:	3.69	4.12	4.68	4.91	4.91	5.14	5.56	5.71	5.49	5.43	4.38	3.68	1756.7	4.8
CORPUS CHRISTI	TX	LATITUDE: 27 DEGREES 46 MINUTES													
	LATITUDE -15:	3.23	3.97	4.73	5.23	5.77	6.39	6.75	6.35	5.62	4.99	3.81	3.11	1825.4	5.0
	LATITUDE :	3.57	4.21	4.80	5.05	5.37	5.84	6.25	6.14	5.72	5.37	4.26	3.51	1829.8	5.0
	LATITUDE +15:	3.73	4.24	4.62	4.64	4.75	5.06	5.49	5.62	5.53	5.46	4.48	3.73	1746.0	4.8
DALLAS	TX	LATITUDE: 32 DEGREES 51 MINUTES													
	LATITUDE -15:	3.21	3.91	4.86	5.23	5.82	6.47	6.54	6.30	5.47	4.77	3.73	3.19	1812.3	5.0
	LATITUDE :	3.57	4.15	4.93	5.04	5.41	5.91	6.05	6.08	5.56	5.13	4.19	3.64	1816.3	5.0
	LATITUDE +15:	3.74	4.18	4.75	4.62	4.77	5.11	5.31	5.56	5.37	5.21	4.42	3.89	1732.7	4.7
DEL RIO	TX	LATITUDE: 29 DEGREES 22 MINUTES													
	LATITUDE -15:	3.57	4.27	5.30	5.43	5.64	6.16	6.34	6.20	5.32	4.87	3.99	3.47	1844.1	5.1
	LATITUDE :	3.97	4.54	5.39	5.24	5.25	5.63	5.88	5.98	5.41	5.24	4.48	3.96	1855.9	5.1
	LATITUDE +15:	4.17	4.58	5.21	4.80	4.64	4.88	5.17	5.48	5.22	5.32	4.73	4.23	1777.7	4.9
EL PASO	TX	LATITUDE: 31 DEGREES 48 MINUTES													
	LATITUDE -15:	4.49	5.51	6.62	7.65	8.02	8.12	7.56	7.39	6.89	6.20	5.06	4.30	2367.7	6.5
	LATITUDE :	5.10	5.96	6.79	7.39	7.39	7.34	6.97	7.14	7.07	6.77	5.80	5.01	2395.1	6.6
	LATITUDE +15:	5.42	6.08	6.59	6.75	6.43	6.26	6.08	6.52	6.86	6.94	6.20	5.43	2297.8	6.3
FORT WORTH	TX	LATITUDE: 32 DEGREES 50 MINUTES													
	LATITUDE -15:	3.13	3.90	4.82	5.20	5.83	6.53	6.65	6.41	5.59	4.84	3.74	3.13	1820.3	5.0
	LATITUDE :	3.48	4.14	4.89	5.01	5.42	5.95	6.15	6.19	5.70	5.20	4.20	3.56	1823.3	5.0
	LATITUDE +15:	3.64	4.17	4.71	4.59	4.78	5.15	5.39	5.66	5.50	5.29	4.43	3.80	1738.1	4.8

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL	AVERAGE DAY
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	(KWH/SQ. M)	(KWH/SQ. M)
HOUSTON TX		LATITUDE: 29 DEGREES 59 MINUTES													
LATITUDE	-15:	2.84	3.64	4.33	4.86	5.48	5.79	5.65	5.39	4.94	4.57	3.46	2.76	1635.1	4.5
LATITUDE	:	3.11	3.85	4.38	4.69	5.11	5.31	5.25	5.21	5.01	4.90	3.85	3.10	1636.8	4.5
LATITUDE	+15:	3.24	3.86	4.22	4.31	4.53	4.62	4.64	4.78	4.83	4.97	4.04	3.29	1561.7	4.3
KINGSVILLE TX		LATITUDE: 27 DEGREES 31 MINUTES													
LATITUDE	-15:	3.29	4.02	4.75	5.28	5.77	6.22	6.51	6.12	5.39	4.88	3.76	3.12	1800.0	4.9
LATITUDE	:	3.63	4.26	4.81	5.10	5.37	5.69	6.04	5.92	5.48	5.24	4.20	3.53	1804.6	4.9
LATITUDE	+15:	3.80	4.29	4.64	4.69	4.75	4.94	5.31	5.42	5.29	5.32	4.42	3.75	1722.6	4.7
LAREDO TX		LATITUDE: 27 DEGREES 32 MINUTES													
LATITUDE	-15:	3.46	4.15	5.02	5.49	6.03	6.33	6.58	6.41	5.67	4.94	3.79	3.28	1862.0	5.1
LATITUDE	:	3.84	4.40	5.10	5.30	5.61	5.79	6.10	6.19	5.78	5.31	4.23	3.72	1868.4	5.1
LATITUDE	+15:	4.02	4.44	4.92	4.87	4.95	5.02	5.36	5.67	5.58	5.40	4.45	3.96	1784.3	4.9
LUBBOCK TX		LATITUDE: 33 DEGREES 39 MINUTES													
LATITUDE	-15:	4.25	5.04	6.18	7.04	7.40	7.69	7.44	7.19	6.39	5.65	4.68	4.05	2222.0	6.1
LATITUDE	:	4.82	5.43	6.32	6.80	6.83	6.97	6.86	6.94	6.54	6.13	5.34	4.71	2242.0	6.1
LATITUDE	+15:	5.11	5.52	6.11	6.21	5.96	5.97	5.98	6.34	6.33	6.27	5.70	5.09	2147.3	5.9
LUFKIN TX		LATITUDE: 31 DEGREES 14 MINUTES													
LATITUDE	-15:	2.99	3.84	4.65	5.20	5.76	6.24	6.18	5.98	5.20	4.95	3.73	3.02	1758.3	4.8
LATITUDE	:	3.30	4.06	4.71	5.01	5.35	5.70	5.73	5.77	5.28	5.33	4.17	3.42	1760.2	4.8
LATITUDE	+15:	3.44	4.09	4.53	4.59	4.72	4.93	5.04	5.28	5.08	5.41	4.39	3.64	1678.1	4.6
MIDLAND-ODESSA TX		LATITUDE: 31 DEGREES 56 MINUTES													
LATITUDE	-15:	4.30	5.12	6.36	7.08	7.50	7.76	7.36	7.15	6.37	5.71	4.75	4.17	2241.4	6.1
LATITUDE	:	4.87	5.51	6.52	6.84	6.93	7.04	6.80	6.91	6.52	6.21	5.42	4.84	2264.1	6.2
LATITUDE	+15:	5.16	5.61	6.32	6.26	6.05	6.02	5.94	6.31	6.31	6.36	5.78	5.24	2170.7	5.9
PORT ARTHUR TX		LATITUDE: 29 DEGREES 57 MINUTES													
LATITUDE	-15:	2.95	3.78	4.53	5.14	5.78	6.13	5.70	5.56	5.14	4.75	3.58	2.87	1701.5	4.7
LATITUDE	:	3.25	4.00	4.58	4.96	5.38	5.61	5.30	5.37	5.21	5.11	4.00	3.23	1704.2	4.7
LATITUDE	+15:	3.38	4.02	4.42	4.56	4.75	4.87	4.69	4.92	5.03	5.19	4.20	3.43	1626.2	4.5
SAN ANGELO TX		LATITUDE: 31 DEGREES 22 MINUTES													
LATITUDE	-15:	3.72	4.38	5.48	5.94	6.27	6.63	6.54	6.32	5.48	4.92	4.10	3.61	1929.2	5.3
LATITUDE	:	4.16	4.67	5.58	5.73	5.81	6.04	6.05	6.10	5.57	5.29	4.62	4.14	1940.3	5.3
LATITUDE	+15:	4.37	4.72	5.38	5.25	5.11	5.21	5.31	5.58	5.37	5.38	4.88	4.45	1856.2	5.1

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC		
SAN ANTONIO	TX	LATITUDE: 29 DEGREES 32 MINUTES													
LATITUDE	-15:	3.32	4.08	4.85	5.15	5.85	6.30	6.54	6.23	5.52	4.85	3.79	3.24	1818.1	5.0
LATITUDE	:	3.68	4.33	4.92	4.96	5.44	5.75	6.06	6.01	5.61	5.21	4.24	3.68	1823.7	5.0
LATITUDE	+15:	3.85	4.37	4.74	4.56	4.80	4.98	5.32	5.51	5.42	5.29	4.47	3.92	1741.4	4.8
SHERMAN	TX	LATITUDE: 33 DEGREES 43 MINUTES													
LATITUDE	-15:	3.15	3.82	4.69	5.19	5.71	6.42	6.41	6.26	5.48	4.80	3.73	3.09	1789.0	4.9
LATITUDE	:	3.50	4.05	4.75	5.00	5.30	5.85	5.93	6.03	5.58	5.16	4.19	3.53	1792.4	4.9
LATITUDE	+15:	3.66	4.08	4.57	4.58	4.68	5.06	5.20	5.52	5.38	5.25	4.43	3.76	1709.5	4.7
WACO	TX	LATITUDE: 31 DEGREES 37 MINUTES													
LATITUDE	-15:	3.18	3.95	4.84	5.17	5.48	6.41	6.56	6.31	5.47	4.78	3.72	3.20	1799.0	4.9
LATITUDE	:	3.53	4.19	4.91	4.98	5.09	5.85	6.08	6.09	5.56	5.14	4.17	3.64	1803.3	4.9
LATITUDE	+15:	3.69	4.22	4.73	4.57	4.50	5.06	5.33	5.57	5.37	5.22	4.39	3.89	1720.8	4.7
WICHITA FALLS	TX	LATITUDE: 33 DEGREES 58 MINUTES													
LATITUDE	-15:	3.47	4.18	5.10	5.70	6.22	6.73	6.68	6.39	5.57	4.91	3.93	3.39	1895.9	5.2
LATITUDE	:	3.87	4.46	5.18	5.49	5.77	6.13	6.17	6.16	5.67	5.29	4.44	3.90	1903.8	5.2
LATITUDE	+15:	4.07	4.50	5.00	5.03	5.07	5.29	5.41	5.63	5.48	5.39	4.70	4.18	1818.4	5.0
BRYCE CANYON	UT	LATITUDE: 37 DEGREES 42 MINUTES													
LATITUDE	-15:	4.14	4.97	6.13	7.05	7.60	8.03	7.51	7.14	7.09	6.10	4.74	3.98	2267.0	6.2
LATITUDE	:	4.70	5.36	6.27	6.80	7.01	7.26	6.92	6.89	7.28	6.67	5.43	4.63	2288.9	6.3
LATITUDE	+15:	4.99	5.45	6.07	6.21	6.11	6.20	6.03	6.29	7.06	6.84	5.80	5.02	2192.4	6.0
CEDAR CITY	UT	LATITUDE: 37 DEGREES 42 MINUTES													
LATITUDE	-15:	3.97	4.71	5.94	6.92	7.65	8.19	7.76	7.43	7.29	6.07	4.61	3.78	2262.1	6.2
LATITUDE	:	4.50	5.06	6.07	6.67	7.05	7.39	7.14	7.17	7.50	6.63	5.27	4.38	2278.0	6.2
LATITUDE	+15:	4.77	5.14	5.87	6.09	6.14	6.30	6.22	6.54	7.28	6.80	5.63	4.74	2176.3	6.0
SALT LAKE CITY	UT	LATITUDE: 40 DEGREES 46 MINUTES													
LATITUDE	-15:	2.96	4.07	5.40	6.32	7.36	7.76	8.08	7.61	7.05	5.64	3.86	2.84	2100.2	5.8
LATITUDE	:	3.31	4.35	5.50	6.08	6.78	7.02	7.42	7.34	7.25	6.14	4.38	3.26	2096.1	5.7
LATITUDE	+15:	3.48	4.39	5.31	5.55	5.92	6.00	6.45	6.69	7.03	6.29	4.65	3.48	1986.1	5.4
NORFOLK	VA	LATITUDE: 36 DEGREES 54 MINUTES													
LATITUDE	-15:	2.83	3.55	4.50	5.46	5.83	6.07	5.72	5.48	4.93	4.22	3.50	2.77	1669.8	4.6
LATITUDE	:	3.14	3.76	4.55	5.26	5.40	5.53	5.30	5.27	5.00	4.52	3.94	3.15	1668.1	4.6
LATITUDE	+15:	3.28	3.78	4.38	4.81	4.76	4.79	4.66	4.82	4.81	4.58	4.15	3.36	1587.1	4.3

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC		
RICHMOND	VA	LATITUDE: 37 DEGREES 30 MINUTES													
	-15:	2.65	3.35	4.25	5.10	5.44	5.68	5.47	5.22	4.77	4.05	3.16	2.52	1572.6	4.3
	:	2.93	3.54	4.29	4.90	5.04	5.18	5.07	5.01	4.83	4.32	3.53	2.85	1567.2	4.3
	+15:	3.05	3.54	4.12	4.48	4.44	4.50	4.46	4.58	4.64	4.36	3.71	3.03	1488.6	4.1
ROANOKE	VA	LATITUDE: 37 DEGREES 19 MINUTES													
	-15:	2.78	3.44	4.35	5.15	5.45	5.71	5.54	5.28	4.81	4.25	3.31	2.64	1604.6	4.4
	:	3.08	3.64	4.39	4.95	5.05	5.21	5.13	5.08	4.86	4.55	3.71	2.99	1601.9	4.4
	+15:	3.22	3.64	4.22	4.52	4.45	4.52	4.51	4.64	4.67	4.60	3.90	3.18	1523.8	4.2
BURLINGTON	VT	LATITUDE: 44 DEGREES 28 MINUTES													
	-15:	1.78	2.46	3.45	4.30	4.89	5.24	5.36	4.94	4.21	3.17	1.71	1.54	1311.3	3.6
	:	1.94	2.57	3.46	4.11	4.51	4.77	4.94	4.73	4.24	3.36	1.86	1.76	1286.8	3.5
	+15:	2.00	2.55	3.30	3.74	3.97	4.13	4.33	4.30	4.06	3.37	1.92	1.87	1204.5	3.3
OLYMPIA	WA	LATITUDE: 46 DEGREES 58 MINUTES													
	-15:	1.39	2.04	3.14	4.21	5.10	5.14	6.00	5.28	4.51	2.80	1.67	1.27	1297.0	3.6
	:	1.54	2.11	3.14	4.02	4.70	4.67	5.52	5.06	4.56	2.96	1.83	1.44	1266.6	3.5
	+15:	1.60	2.08	2.99	3.65	4.12	4.05	4.83	4.60	4.37	2.97	1.89	1.53	1179.3	3.2
SEATTLE-TACOMA	WA	LATITUDE: 47 DEGREES 27 MINUTES													
	-15:	1.38	2.02	3.19	4.35	5.36	5.46	7.10	5.56	4.50	2.95	1.69	1.23	1366.3	3.7
	:	1.52	2.10	3.19	4.16	4.93	4.96	6.51	5.32	4.55	3.13	1.86	1.39	1330.4	3.6
	+15:	1.58	2.07	3.04	3.78	4.32	4.28	5.67	4.84	4.36	3.14	1.92	1.48	1234.3	3.4
SPOKANE	WA	LATITUDE: 47 DEGREES 38 MINUTES													
	-15:	1.54	2.65	4.05	5.10	6.03	6.34	7.47	6.81	5.88	4.03	2.15	1.38	1628.7	4.5
	:	1.68	2.80	4.09	4.88	5.55	5.74	6.86	6.55	6.01	4.33	2.39	1.54	1596.9	4.4
	+15:	1.73	2.79	3.92	4.44	4.85	4.94	5.96	5.96	5.80	4.39	2.50	1.61	1489.2	4.1
WHIDBEY ISLAND	WA	LATITUDE: 48 DEGREES 21 MINUTES													
	-15:	1.60	2.29	3.53	4.57	5.52	5.51	6.24	5.50	4.69	3.02	1.92	1.27	1392.0	3.8
	:	1.79	2.40	3.55	4.36	5.07	5.00	5.73	5.27	4.75	3.21	2.13	1.41	1361.1	3.7
	+15:	1.88	2.38	3.39	3.96	4.44	4.32	5.00	4.79	4.56	3.22	2.22	1.48	1267.9	3.5
YAKIMA	WA	LATITUDE: 46 DEGREES 34 MINUTES													
	-15:	1.81	2.91	4.34	5.45	6.31	6.59	7.44	6.88	6.01	4.19	2.36	1.58	1702.5	4.7
	:	1.98	3.07	4.39	5.22	5.80	5.96	6.83	6.61	6.14	4.51	2.63	1.78	1674.1	4.6
	+15:	2.05	3.07	4.21	4.75	5.07	5.12	5.94	6.02	5.93	4.58	2.76	1.87	1565.2	4.3

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
EAU CLAIRE WI		LATITUDE:		44 DEGREES		52 MINUTES									
LATITUDE	-15:	2.23	3.20	4.10	4.77	5.24	5.67	5.89	5.48	4.54	3.63	2.23	1.76	1484.4	4.1
LATITUDE	:	2.48	3.39	4.14	4.57	4.84	5.16	5.43	5.26	4.59	3.88	2.48	1.98	1466.5	4.0
LATITUDE	+15:	2.58	3.40	3.97	4.16	4.25	4.46	4.75	4.79	4.41	3.91	2.58	2.09	1380.3	3.8
GREEN BAY WI		LATITUDE:		44 DEGREES		29 MINUTES									
LATITUDE	-15:	2.20	3.06	4.14	4.81	5.35	5.78	5.89	5.47	4.62	3.57	2.30	1.79	1491.8	4.1
LATITUDE	:	2.43	3.24	4.18	4.60	4.94	5.25	5.42	5.25	4.67	3.81	2.55	2.02	1472.1	4.0
LATITUDE	+15:	2.53	3.24	4.01	4.19	4.33	4.54	4.75	4.78	4.48	3.84	2.66	2.13	1384.0	3.8
LA CROSSE WI		LATITUDE:		43 DEGREES		52 MINUTES									
LATITUDE	-15:	2.32	3.22	4.10	4.75	5.33	5.78	5.93	5.62	4.68	3.73	2.42	1.87	1514.7	4.1
LATITUDE	:	2.58	3.41	4.14	4.55	4.92	5.25	5.46	5.39	4.74	3.99	2.69	2.10	1498.5	4.1
LATITUDE	+15:	2.69	3.42	3.96	4.15	4.33	4.54	4.79	4.91	4.55	4.02	2.81	2.22	1412.3	3.9
MADISON WI		LATITUDE:		43 DEGREES		8 MINUTES									
LATITUDE	-15:	2.48	3.37	4.21	4.64	5.41	5.90	6.01	5.73	4.89	3.92	2.42	1.94	1550.6	4.2
LATITUDE	:	2.75	3.57	4.25	4.44	4.99	5.36	5.54	5.50	4.95	4.20	2.68	2.18	1534.5	4.2
LATITUDE	+15:	2.87	3.58	4.07	4.04	4.38	4.63	4.85	5.01	4.75	4.24	2.80	2.30	1446.4	4.0
MILWAUKEE WI		LATITUDE:		42 DEGREES		57 MINUTES									
LATITUDE	-15:	2.24	3.01	4.01	4.79	5.50	5.99	6.11	5.77	4.92	3.88	2.52	1.85	1540.7	4.2
LATITUDE	:	2.47	3.18	4.04	4.59	5.08	5.45	5.63	5.55	4.99	4.16	2.80	2.08	1522.9	4.2
LATITUDE	+15:	2.57	3.18	3.87	4.18	4.46	4.71	4.94	5.06	4.80	4.20	2.93	2.19	1433.8	3.9
CHARLESTON WV		LATITUDE:		38 DEGREES		22 MINUTES									
LATITUDE	-15:	2.02	2.64	3.52	4.41	5.06	5.39	5.20	4.95	4.52	3.84	2.63	1.89	1402.6	3.8
LATITUDE	:	2.20	2.75	3.53	4.23	4.69	4.92	4.81	4.75	4.56	4.09	2.91	2.10	1386.2	3.8
LATITUDE	+15:	2.26	2.73	3.37	3.86	4.14	4.28	4.24	4.34	4.38	4.12	3.04	2.19	1307.2	3.6
HUNTINGTON WV		LATITUDE:		38 DEGREES		22 MINUTES									
LATITUDE	-15:	2.16	2.87	3.74	4.72	5.28	5.59	5.46	5.17	4.65	3.98	2.75	2.04	1474.5	4.0
LATITUDE	:	2.36	3.00	3.76	4.53	4.89	5.10	5.05	4.96	4.70	4.24	3.05	2.28	1459.7	4.0
LATITUDE	+15:	2.44	2.99	3.60	4.14	4.31	4.43	4.45	4.53	4.51	4.28	3.19	2.40	1378.1	3.8
CASPER WY		LATITUDE:		42 DEGREES		55 MINUTES									
LATITUDE	-15:	3.49	4.41	5.49	6.23	6.88	7.59	7.95	7.62	6.85	5.55	4.05	3.31	2114.3	5.8
LATITUDE	:	3.95	4.74	5.60	5.99	6.34	6.86	7.30	7.36	7.04	6.04	4.63	3.84	2121.9	5.8
LATITUDE	+15:	4.18	4.80	5.40	5.46	5.54	5.88	6.35	6.71	6.83	6.19	4.93	4.15	2021.2	5.5

AVERAGE DAILY INSOLATION BY MONTH (KWH/SQ. M)

SITE														ANNUAL TOTAL (KWH/SQ. M)	AVERAGE DAY (KWH/SQ. M)
ARRAY TILT		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC		
CHEYENNE		-----												-----	-----
	WY	LATITUDE:		41 DEGREES		9 MINUTES									
LATITUDE	-15:	3.77	4.50	5.34	5.90	6.19	6.83	6.93	6.60	6.33	5.44	4.15	3.58	1995.7	5.5
LATITUDE	:	4.27	4.83	5.44	5.66	5.71	6.19	6.37	6.34	6.47	5.91	4.73	4.16	2011.4	5.5
LATITUDE	+15:	4.52	4.90	5.24	5.16	5.00	5.32	5.56	5.78	6.26	6.03	5.03	4.49	1925.5	5.3
ROCK SPRINGS															
	WY	LATITUDE:		41 DEGREES		36 MINUTES									
LATITUDE	-15:	3.63	4.65	5.78	6.53	7.31	7.80	7.96	7.60	7.10	5.83	4.24	3.50	2190.3	6.0
LATITUDE	:	4.11	5.01	5.90	6.28	6.73	7.05	7.31	7.33	7.30	6.36	4.84	4.07	2200.7	6.0
LATITUDE	+15:	4.35	5.08	5.70	5.73	5.87	6.03	6.35	6.69	7.08	6.52	5.16	4.39	2098.0	5.7
SHERIDAN															
	WY	LATITUDE:		44 DEGREES		46 MINUTES									
LATITUDE	-15:	2.65	3.41	4.58	5.17	5.88	6.55	7.31	6.90	5.91	4.61	3.14	2.46	1784.6	4.9
LATITUDE	:	2.96	3.62	4.64	4.95	5.42	5.94	6.72	6.64	6.04	4.98	3.54	2.82	1775.2	4.9
LATITUDE	+15:	3.11	3.64	4.46	4.51	4.75	5.11	5.85	6.05	5.83	5.07	3.74	3.01	1678.9	4.6