

DOE/SF/00824--T3

Atomics International Division  
Rockwell International

## SUPPORTING DOCUMENT

NUMBER

(TI-099-241-005)

REV LTR/CHG

SEE SUMMARY OF CH

## PROGRAM TITLE

CLINCH RIVER BREEDER REACTOR PLANT

## DOCUMENT TITLE

Effect of Sodium Pool Temperature on Grapple  
Drive Stem Temperatures at Seals in CRBRP  
IVTM

## DOCUMENT TYPE

TECHNICAL INFORMATION

## KEY NOUNS

IVTM, SEALS

## ORIGINAL ISSUE DATE

6-10-74

GO NO.

09002

S/A NO.

41291

PAGE 1 OF 12

TOTAL PAGES

REL. DATE

6-26-74 BK

PREPARED BY/DATE

T. T. Shimazaki J.S. 6/11/74

DEPT

716

MAIL ADDR

T006

IR&D PROGRAM? YES ☐ NO ☒ IF YES, ENTER TPA NO. \_\_\_\_\_

## APPROVALS

O. P. Steele III *O.P. Steele* 6/11/74K. Foster *K. Foster* 6/18/74

## SECURITY CLASSIFICATION

(CHECK ONE BOX ONLY)

UNCL

CONF.

SECRET

AEC

☒☐☐

DOD

☐☐☐

(CHECK ONE BOX ONLY)

RESTRICTED

DATA

DEFENSE

INFO.

AUTHORIZED  
CLASSIFIER

DATE

## DISTRIBUTION

*	NAME	MAIL ADDR
	Berg, G.	LB31
	Bilibin, K.	LB26
	Crosgrove, R.	LB10
	Foster, K. (6)	LB10
	Kellogg, L.	LA49
	Kurzeka, W.	T006
	Moody, E.	LB25
	Shimazaki, T.	T006
	Steele, O.P. III	T006

DISTRIBUTION OF THIS DOCUMENT IS UNLIMITED

## ABSTRACT

The effect of sodium pool temperature on the grapple drive stem temperatures at the seals of the CRBRP (Clinch River Breeder Reactor Plant) IVTM (In-Vessel Transfer Machine) has been calculated.

Reducing the sodium pool temperature from 500F to 400F reduces the maximum grapple drive stem temperature at the seals from 510F to 472F on the initial up-stroke, and from 285F to 225F when system is at dynamic thermal equilibrium. The time the stem can remain in lowered position without stem temperature exceeding 300F at seals when stem is raised, increases from 4 minutes to 20 minutes, (the system being initially at dynamic thermal equilibrium).

## DISCLAIMER

This book was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

Am03 76SF00824  
**MASTER**

RESERVED FOR PROPRIETARY/LEGAL NOTICES

**THIS REPORT MAY NOT BE PUBLISHED WITHOUT THE  
APPROVAL OF THE PATENT BRANCH, AEC.**

This report was prepared as an account of work sponsored by the United States Government. Neither the United States nor the United States Atomic Energy Commission, nor any of their employees nor any of their contractors, subcontractors, or their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product or process disclosed, or represents that its use would not infringe privately owned rights.

\* TITLE PAGE ONLY

## **DISCLAIMER**

**This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency Thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.**

## **DISCLAIMER**

**Portions of this document may be illegible in electronic image products. Images are produced from the best available original document.**

## TABLE OF CONTENTS

<u>Section</u>		<u>Page</u>
I	INTRODUCTION	3
II	RESULTS	3
III	CONCLUSIONS	11
IV	REFERENCES	12

## FIGURES

1.	Support Body, Stem Guide Tube, Guide Sleeve and Nozzle Temperatures when System is at Dynamic Thermal Equilibrium; and Head and Shield Temperature Distributions Used	4
2.	Maximum, Raised Position Grapple Drive Stem Temperature when System is at Dynamic Thermal Equilibrium.	5
3.	Fuel Transfer Cycle for IVTM	6
4.	Stem Temp. Increase when Held in Lowered Position with Sodium at 400F; System Initially at Dynamic Thermal Equilibrium.	8
5.	Stem Temperature Increase when Held in Lowered Position with Sodium at 500F; System Initially at Dynamic Thermal Equilibrium	9

## I. INTRODUCTION

The results of an analysis of the grapple drive stem temperatures at the grapple drive stem reciprocating seals during fuel transfer operation of the IVTM (In-Vessel Transfer Machine) for the CRBRP (Clinch River Breeder Reactor Plant) are presented. The system analyzed is the same as the system analyzed in Ref. 1, with the following exceptions:

1. Sodium pool temperature of 400F as well as 500F, is analyzed.
2. The calculated temperature distributions in the top shield 48 hours after reactor shutdown (Ref. 2) are used. These temperature distributions are shown in Fig. 1.
3. The grapple drive stem stroke is 214.62 inches (Ref. 3).
4. The elevation of the lower end of the seals is 141 inches (Ref. 4).
5. The elevation of the sodium pool surface is minus (-) 87 inches (Ref. 4).

## II. RESULTS

Figure 2 shows the maximum temperature of the grapple drive stem in the raised position and Fig. 1 shows the temperature distribution in the structure surrounding the grapple drive stem, during fuel transfer operation, after enough fuel transfer cycles have been completed for the system to have reached dynamic thermal equilibrium. Dynamic thermal equilibrium is defined as that state when system temperatures at any particular point in the fuel transfer cycle remain the same in each succeeding fuel transfer cycle. The maximum temperature of the grapple drive stem in the raised position, shown in Fig. 2, occurs at 1337 seconds from the start of each fuel transfer cycle (see Fig. 3), i. e., when the stem just reaches the raised position for the last time in the fuel transfer cycle. It is seen in Fig. 2 that the maximum stem temperature seen by the seals is 225F if the sodium pool temperature is 400F, and 285F if the sodium pool temperature is 500F.

It can be deduced from the temperature distributions shown in Fig. 1, that the temperature of the seal housings in the upper end of the nozzle will be somewhat less than 200F if the sodium pool temperature is 400F and somewhat greater than 200F if the sodium pool temperature is 500F. It can also be deduced from the temperature distributions shown in Fig. 1 that the temperature of the hold-down actuating shafts, which have a

117 (121) 115 (119)

Fig. 1

Support Body, Stem Guide Tube, Guide Sleeve, & Nozzle Temperatures When System is at Dynamic Thermal Equilibrium; and Head and Shield Temperature Distributions Used

Note:

Numbers not in parenthesis are temperatures for 400°F sodium. Numbers in parenthesis are temperatures for 500°F sodium.

Elevation, inches

Stem guide tube  
Guide sleeve

Support body

Hold-down actuating shafts (stroke = 40½")

Nozzle

Head

Shield

Sodium

43 hrs. after reactor shutdown

400°F Sodium

500°F Sodium

Radius, inches

Head & shield temperature, °F



Fig. 2

Maximum Raised Position Grapple  
Drive Stem Temperature When System  
is at Dynamic Thermal Equilibrium

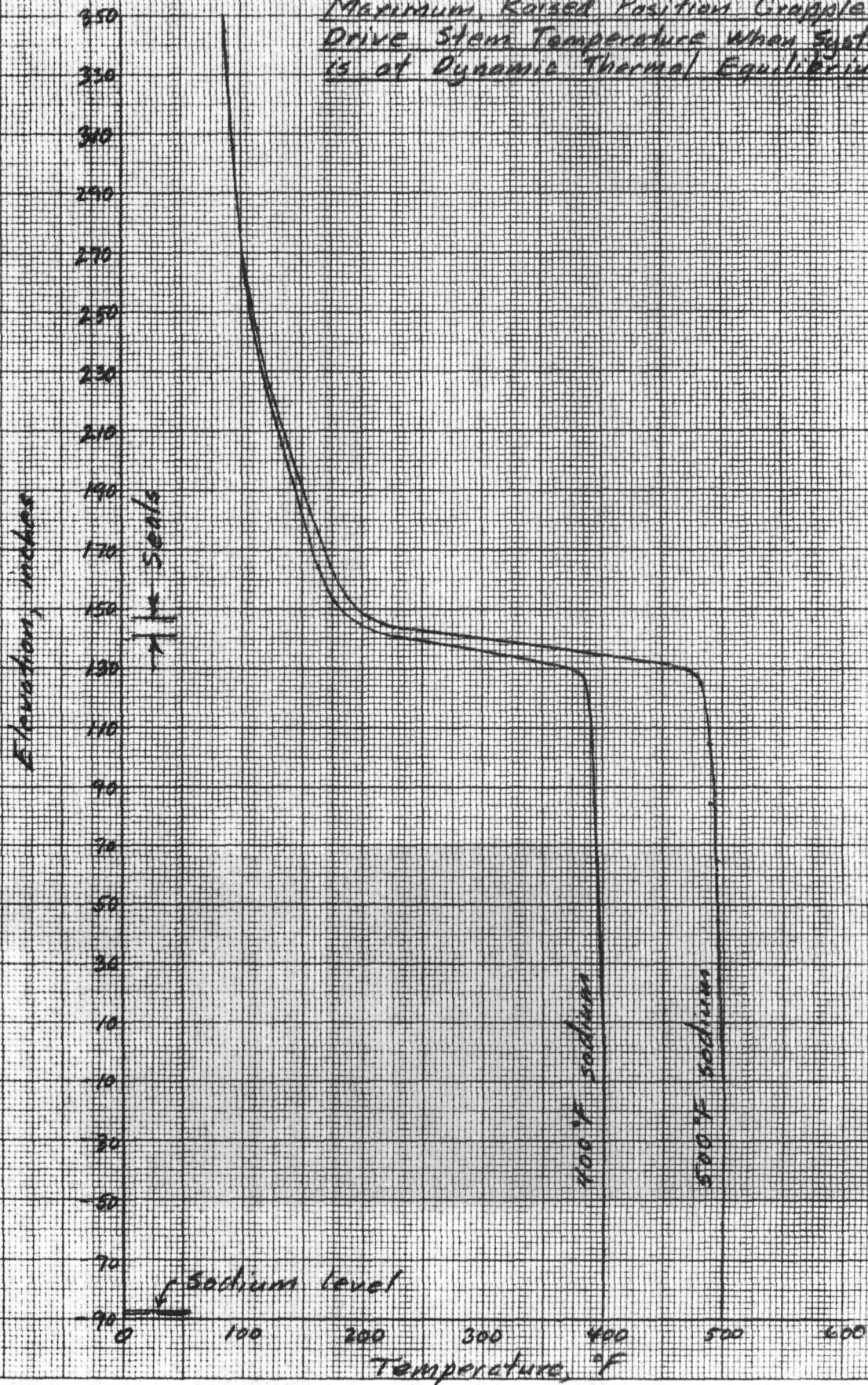
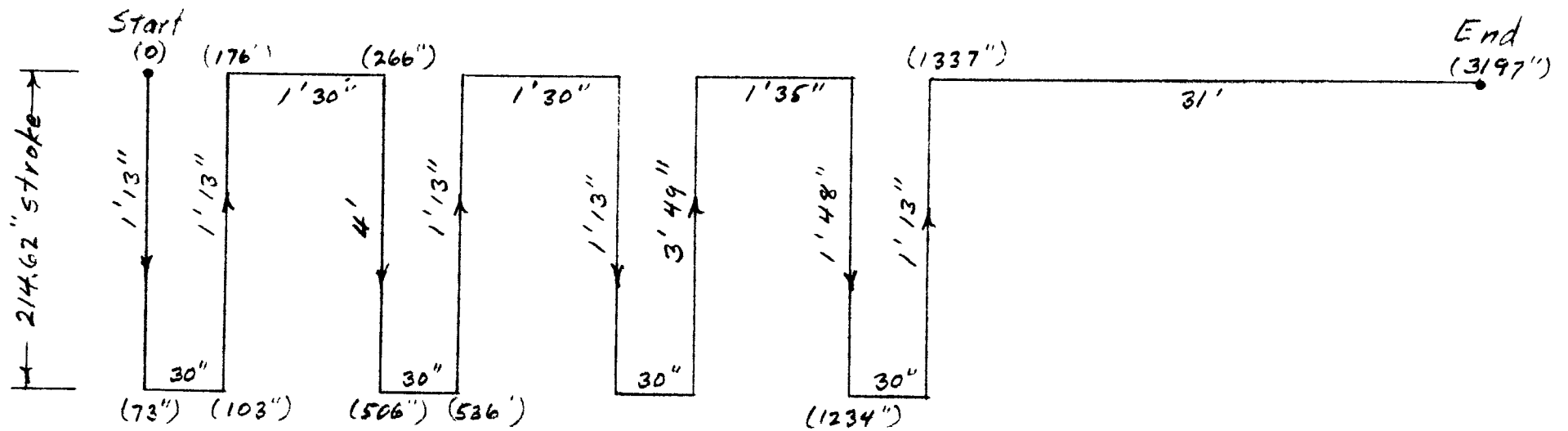


Fig. 3  
Fuel Transfer Cycle for IVTM





stroke of 40-1/2 inches, could exceed 300F at the seals when these shafts approach or reach the raised position whether the sodium pool temperature is 400 or 500F.

Figures 4 and 5 show for sodium pool temperatures of 400F and 500F, respectively, the change in temperature with time of the grapple stem if the stem is held in the lowered position for a prolonged period, the system having been initially at dynamic thermal equilibrium. Two ordinate scales are shown. The ordinate scale on the right side gives the correct elevation for the temperatures shown. The ordinate scale on the left side shows what the stem temperatures would be in the raised position if the stem is raised instantaneously. Inasmuch as it takes a finite amount of time for the stem to be raised, and since the stem cools during this time, the actual stem temperature, when in the raised position, would be lower than the temperatures shown. However, the difference, i.e., the amount of cooling, is not significant if the stem moves up at a speed of 15 ft/min.

The stem temperature distribution, labelled zero (0) minutes, is that computed at 1234 seconds from the start of the fuel transfer cycle (see Fig. 3), i.e., when the stem just reaches the lowered position for the last time in the fuel transfer cycle. Stem temperature distributions at times 10, 20, 30, and 60 minutes later, and when the system reaches thermal equilibrium, are also shown. The dip in stem temperature, at the lowered position elevation of around minus (-) 50 inches, in the 30 and 40 minute curves is due to the low heat capacity of the guide sleeve and stem guide tube (see Fig. 1) as compared with the heat capacity of the support body. It is seen that if the drive stem is held in the lowered position for 20 minutes or longer in the case of sodium pool temperature = 400F (Fig. 4), and for about 4 minutes or longer in the case of sodium pool temperature = 500F (Fig. 5), the seals will see a stem temperature of 300F or higher when the stem is raised.

If the stem is held in the lowered position until thermal equilibrium is reached (which, on the basis of the plots shown in Figures 4 and 5, would probably take at least a couple of hours), and the stem is then raised at a speed of 15 ft/min, it is seen from Figures 4 and 5 respectively, that, during this up-stroke, the temperature of the grapple drive stem sliding past the seals will range up to 472F if the sodium pool temperature is 400F, and up to 510F if the sodium pool temperature is 500F. This is expected to be the condition for the initial up-stroke.

Fig. 4

Stem Temperature Increase When Held in Lowered Position with Sodium at 400°F; System Initially at Dynamic Thermal Equilibrium

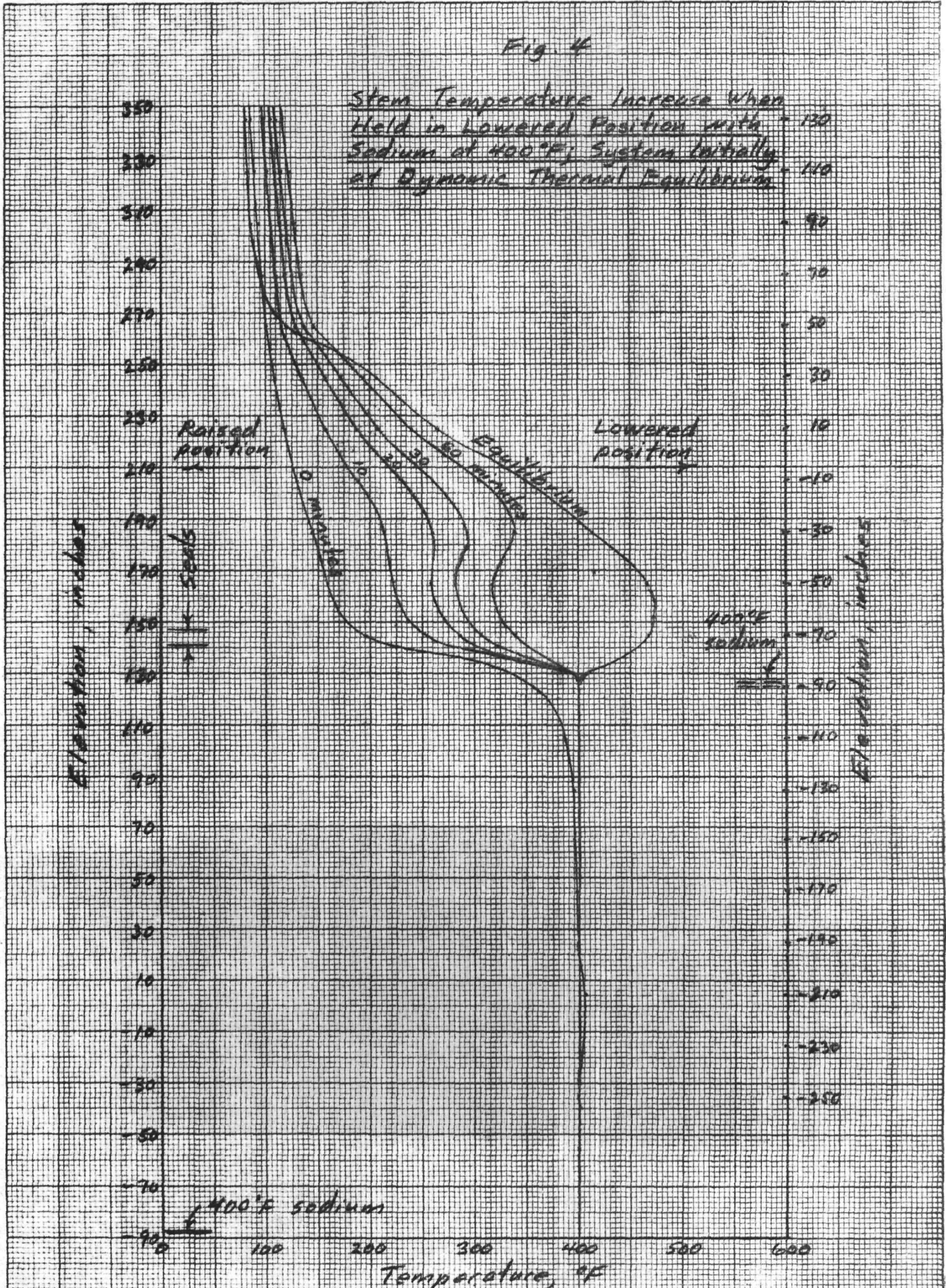
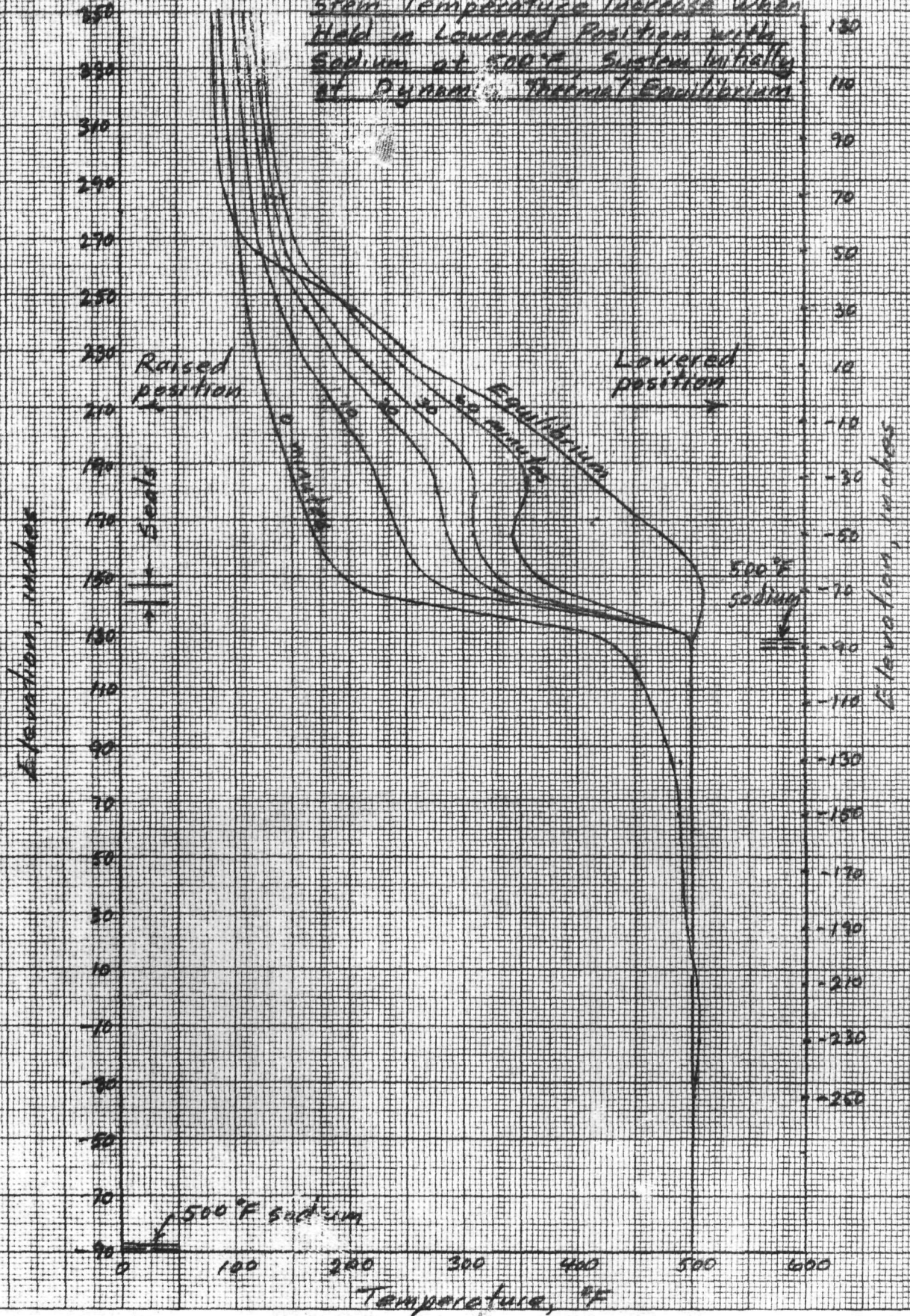




Fig. 5

Stem Temperature Increase when  
Held in Lowered Position with  
Sodium at 500°F. System Initially  
at Dynamic Thermal Equilibrium



if it is desired to limit the maximum temperature of the grapple drive stem at the seals to 300F, it can be accomplished by stopping the up-stroke when the temperature of the grapple drive stem at the seals reaches 300F, and holding the stem at this position long enough for it to cool sufficiently before completing the up-stroke. It can be determined from Figs. 4 and 5 that the temperature of the grapple drive stem at the seals will reach 300F when the stem is raised to 75 inches below the raised position. On the basis of calculations made in Ref. 5 for an IVTM and support body having slightly different dimensions, the stem will have to be held in this position for about an hour in the case of sodium pool temperature = 500F (and somewhat less time in the case of sodium pool temperature = 400F) for it to cool enough to permit completion of the up-stroke without the temperature of the grapple drive stem exceeding 300F at the seals. The stem cools by virtue of heat transfer by conduction and radiation to the colder support body surrounding it. From this point on, the fuel transfer cycle shown in Fig. 3, can be followed without the temperature of the grapple drive stem exceeding 300F at the seals.

### III. CONCLUSIONS

Reducing the sodium pool temperature from 500F to 400F reduces the maximum grapple drive stem temperatures at the seals and increases the time the stem can remain in the lowered position without the stem temperature exceeding 300F at the seals when the stem is raised, to the following extent:

	<u>Sodium Pool Temperature</u>	
	<u>400F</u>	<u>500F</u>
1. Maximum stem temperature seen by seals during initial up-stroke.	472F	510F
2. Maximum stem temperature at seals when system is operating at dynamic thermal equilibrium.	225F	285F
3. Length of time stem can remain in lowered position without stem temperature exceeding 300F at seals when stem is raised (at 15 ft/min.); system initially at dynamic thermal equilibrium.	20 min.	4 min.



#### IV. REFERENCES

1. TI-099-241-002, "Thermal Analysis of Seals in CRBRP In-Vessel Transfer Machine", T. Shimazaki, 2-12-74.
2. ARD Letter WA40082, April 9, 1974
3. IL, Kellogg to Steele, "Phase IV, IVTM Seal and Bushing Test", May 10, 1974.
4. K. Bilibin, Personal communication, June 7, 1974.
5. TI-097-241-010, "In-Vessel Transfer Machine Seal Thermal Analysis", T. Shimazaki, 12-15-73.