
Evaluation of Severe Accident Risks: Quantification of Major Input Parameters

MACCS Input

Manuscript Completed: November 1990
Date Published: December 1990

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Prepared for
Division of Systems Research
Office of Nuclear Regulatory Research
U.S. Nuclear Regulatory Commission
Washington, DC 20555
NRC FIN A1853

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ABSTRACT

Estimation of offsite accident consequences is the customary final step in a probabilistic assessment of the risks of severe nuclear reactor accidents. Recently, the Nuclear Regulatory Commission reassessed the risks of severe accidents at five U.S. power reactors (NUREG-1150). Offsite accident consequences for NUREG-1150 source terms were estimated using the MELCOR Accident Consequence Code System (MACCS). Before these calculations were performed, most MACCS input parameters were reviewed, and for each parameter reviewed, a best-estimate value was recommended. This report presents the results of these reviews. Specifically, recommended values and the basis for their selection are presented for MACCS atmospheric and biospheric transport, emergency response, food pathway, and economic input parameters. Dose conversion factors and health effect parameters are not reviewed in this report.

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1. INTRODUCTION

Estimation of offsite accident consequences is the customary final step in a probabilistic assessment of the risks of severe nuclear reactor accidents. For NUREG-1150 source terms [1,2], offsite accident consequences were estimated using the MELCOR Accident Consequence Code System (MACCS) [3-5]. In preparing for the performance of those calculations, most input parameters for the MACCS offsite consequences analysis code were reviewed, and for each parameter reviewed, a best estimate value and an uncertainty range were estimated. The following chapters summarize these reviews. Sample MACCS input files for the NUREG-1150 calculations are presented in Appendix A. The remainder of this chapter provides a brief overview of offsite consequence modeling.

1.1 Offsite Accident Progression

Should a severe reactor accident culminate in containment failure, winds would transport the radioactive gases and aerosols in the plume released to the atmosphere away from the reactor site. Downwind populations would be exposed to radiation, and land, buildings, and crops would be contaminated by radioactive materials deposited from the plume. Estimation of the range and probability of the health effects induced by the radiation exposures, and of the economic costs and losses that would result from the contamination of land, buildings, and crops is the object of an ex-plant consequence analysis [6,7].

1.2 Input Data and Quantities Calculated

MACCS calculations require the following data:

- The inventory at accident initiation (reactor scram) of those radioactive isotopes important for the calculation of ex-plant consequences (e.g., an end-of-cycle reactor core contains about 10^8 Ci of ^{131}I).
- The atmospheric source term produced by the accident (number of plume segments released, sensible heat content of each plume segment, time and duration of release, time when offsite officials are warned that an emergency response should be initiated, and the fraction of each important nuclide's scram inventory released with each plume segment).
- Meteorological data characteristic of the site region--usually one year of hourly windspeed, atmospheric stability, and rainfall readings recorded at the site or at a nearby National Weather Service station. Although one year of hourly readings contains 8760 weather sequences, most consequence calculations examine only a representative subset of these sequences (typically about 150 sequences). The representative subset is selected by stratified sampling of the 8760 sequences after sorting of the sequences into categories defined by windspeed, atmospheric stability, and the location (downwind distance) of rain.

- The *population distribution* about the reactor site (the distribution is usually constructed from census data on a polar coordinate grid having 16 angular sectors aligned with the 16 compass directions and some number of radial intervals that extend outward to 500 miles).
- *Emergency response assumptions* (evacuation time and average speed, effectiveness and occurrence of sheltering, criteria and timing for post-accident relocation of people, decontamination criteria and effectiveness, temporary interdiction criteria for land and buildings, and disposal criteria for contaminated crops).
- *Land usage* (habitable land fractions, farmland fractions), and *economic data* (worth of crops, land, and buildings) for the region about the reactor site.

Given these data, MACCS predicts

- Downwind *transport, dispersion, and deposition* of the radioactive materials released to the atmosphere from the failed containment.
- Short-term and long-term *radiation doses* received by exposed populations via direct (cloudshine, inhalation, groundshine, resuspension) and indirect (ingestion) pathways.
- Mitigation of those doses by *emergency response actions* (evacuation, sheltering, and relocation of people; disposal of milk, meat, and crops; decontamination, temporary interdiction, and condemnation of land and buildings).
- *Fatalities and injuries* expected within one year of the accident (early health effects) and the latent *cancer deaths* expected over the lifetime of the exposed individuals.
- *Offsite costs* of emergency response actions, and of the decontamination, temporary interdiction, and condemnation of milk, crops, land, and buildings.

1.3 Phenomena Modeled

1.3.1 Atmospheric Transport [8,9]

As in most consequence codes [10-14], MACCS neglects wind trajectories. The 16 compass sector population distributions are assumed to constitute a representative set of downwind exposed populations. The exposure probability of each of the 16 compass sector population distributions is assumed to be given by the frequency with which wind blows from the site into the sector (i.e., compass sector site wind rose frequencies). Windspeed determines the rate of downwind transport. Release duration and windspeed determine plume length. Dispersion of the plume in the downwind direction is neglected. Dispersion in the vertical and crosswind directions is estimated using a Gaussian plume model and therefore varies with windspeed and atmospheric stability. Vertical plume expansion is capped by the mixing depth (seasonal mixing layer height).

1.3.2 Deposition

Aerosols are removed from the plume by washout, which varies with rainfall rate, and by diffusion to, impaction on, and gravitational settling onto surfaces. The combined removal rate because of diffusion, impaction, and settling is modeled using an empirical, particle-size-dependent, dry deposition velocity. Runoff of rain and weathering decrease surface concentrations of radioactive aerosols deposited on the ground. Decrease of radioactivity because of radioactive decay is also modeled (only parent and daughter nuclides are followed, since doses from second generation daughters are insignificant).

1.3.3 Emergency Response

Population doses are mitigated by user-specified emergency response actions (evacuation, sheltering, and post-accident relocation of people; decontamination, temporary interdiction, and condemnation of land and buildings; disposal of contaminated meat, milk, and crops).

1.3.4 Dosimetry and Health Effects

Populations located on the MACCS computational grid receive doses from the passing plume (cloudshine), by exposure to materials deposited on the ground (groundshine), by inhalation of airborne radioactive materials (from the plume or from mechanical or wind driven resuspension of materials deposited on the ground), and by ingestion of contaminated water and foods. Contaminated water and foods may also be consumed by populations off of the computational grid.

Health effects are calculated from doses to specific organs [15]. Doses to specific organs are calculated using dose conversion factors [16]. Early injuries and fatalities (those that occur within one year of the accident) are estimated using nonlinear dose-response models. A recent expert review of radiation induced health effects [17] recommended the use of Hazard functions (H_i) when calculating early injuries or fatalities due to damage to organ i . Thus, the risk (r) per person of contracting a given early health effect is given by

$$r = 1 - \exp \left(\sum_i -H_i \right)$$

$$H_i = \ln 2 (D_i/D_{50,i})^\beta$$

$$H_i = 0 \text{ if } D_i \leq D_{th,i}$$

where D_i is the dose received by the impaired organ, $D_{th,i}$ is the damage threshold (dose threshold values are poorly known and variable over any population cohort), $D_{50,i}$ is the dose that induces the specified health effect in half of the exposed population (LD₅₀ value for deaths), and β is a parameter that determines the slope of the dose-response curve. Sums of Hazard functions are used (1) to model any health effect that has D₅₀ values that vary significantly with exposure period, and (2) to model early fatalities where death may be caused by the impaired functioning of several organs.

Linear-quadratic, zero-threshold, dose-response models are recommended by several recent reviews of mortality caused by radiation-induced cancers [18-20]. However, the quadratic portion of the model is not important, when long-term individual exposures are limited to 25 rems in 30 years, as is done in most consequence calculations. Accordingly, cancer fatality predictions are linear with dose. Cancer fatality predictions are not always linear with source term magnitude because dose is avoided by crop disposal and by decontamination and interdiction of land and buildings.

1.3.5 Economic Effects

Economic consequences [21] are estimated by summing the following costs: evacuation costs, temporary relocation costs (food, lodging, lost income), costs of decontaminating land and buildings, the value of crops destroyed because they were contaminated by direct deposition or root uptake, the value of farmland and of nonfarm commercial, public, and individual property that is condemned. Costs for damage to the reactor, the purchase of replacement power, medical care, life-shortening, and litigation are not calculated by MACCS.

1.4 Computational Framework

Figure 1-1 depicts the progression of a consequence calculation for one source term, one weather sequence, and one exposed population distribution. However, severe accidents can lead to source terms of quite different magnitudes (e.g., negligible at TMI, substantial at Chernobyl), and the weather conditions at the time of the release can greatly alter consequence magnitudes (e.g., intense rain at the time of the release or plume transport out to sea would largely eliminate health effects, while rainout of the plume onto a downwind city would greatly increase early fatalities).

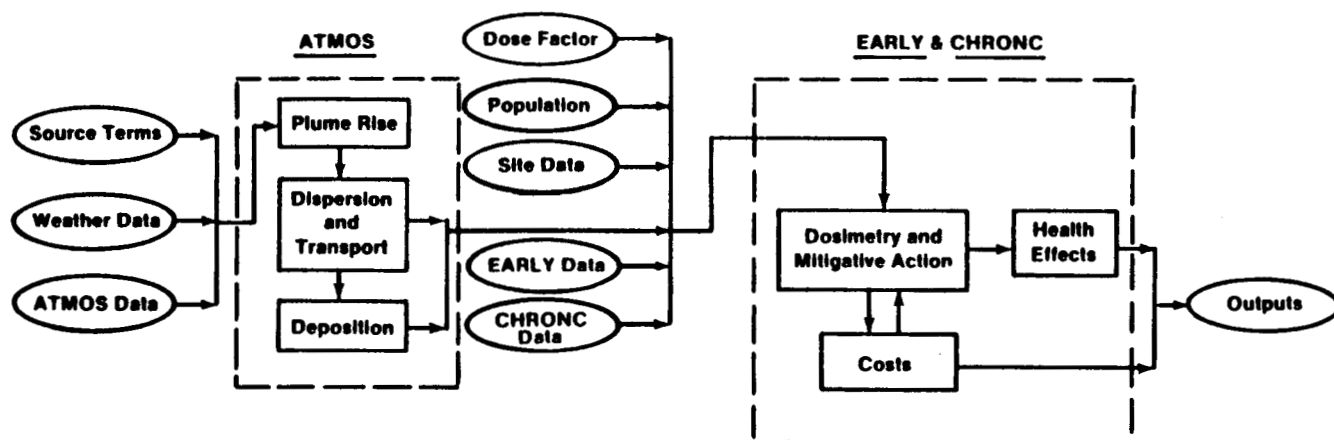


Figure 1-1. Progression of a Consequence Calculation.

Because consequences vary with source term magnitude, weather, and population density, to develop statistical distributions of consequence measures (doses, health effects, costs) that depict the range and probability of consequences for the reactor being examined, consequence assessments must examine all possible combinations of representative sets of source terms, weather sequences, and exposed populations. Usually distributions that display the variation of consequences with weather and population density are first developed for each representative source term. Then an integral depiction of consequences may be constructed by weighted summation of these source term dependent distributions, with each distribution weighted by the estimated absolute probability of occurrence of its underlying source term.

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2. TRANSPORT PARAMETERS

MACCS allows a release of radioactive materials to the atmosphere to be divided into plume segments, which can have different compositions, release durations, and energies (amounts of sensible heat). Plume segment lengths are determined by the product of the segment's release duration and the average windspeed during release. The initial vertical and horizontal dimensions of each plume segment are user specified. If release occurs into a building wake, then wake dimensions can be used to set the initial crosswind dimensions of the plume. If not, a point source can be specified.

A liftoff criterion (a critical windspeed that increases as plume buoyancy increases [1]) determines whether buoyant plumes are subject to plume rise. When the windspeed at release equals or exceeds the critical windspeed, plume rise is prevented. When the windspeed at release is less than the critical windspeed, plume rise is allowed, and the height to which a buoyant plume rises is determined using equations recommended by Briggs [2,3].

After release, windspeed determines the rates at which plume segments transport in the downwind direction, and wind direction at the time of release determines the direction of travel. As is done by most consequence codes [4,5], MACCS neglects wind trajectories. The sixteen compass sector population distributions are assumed to constitute a representative set of downwind exposed populations. The exposure probability of each of the 16 compass sector population distributions is assumed to be given by the frequency with which wind blows from the site into the sector (i.e., compass sector site wind rose frequencies).

During transport, dispersion in the vertical and horizontal (crosswind) directions is estimated using a Gaussian plume model [6]. Thus, dispersion rates depend on windspeed and on atmospheric stability. The crosswind Gaussian distribution of each plume segment is approximated by a multistep histogram. Although horizontal dispersion of plume segments is unconstrained, vertical dispersion is bounded by the ground and by the depth of the mixing layer (as specified by annual or seasonal mixing layer heights [7]), which are modeled as totally reflecting layers using mirror image sources [6]. Since the number of reflections increases as travel times lengthen, the vertical distribution of each plume segment eventually becomes uniform and is so modeled thereafter [8].

In MACCS, aerosols are removed from the plume by washout, which varies with rainfall rate [9], and by diffusion to, impaction on, and gravitational settling onto surfaces. The combined removal rate due to diffusion, impaction, and settling is modeled using an empirical, dry deposition velocity [10]. Because dry deposition velocity varies with particle size, if the aerosol size distribution is divided into ranges, a dry deposition velocity must be specified for each range.

Water bodies (rivers, great lakes, oceans) are contaminated by direct deposition of radioactive materials onto their surfaces, by runoff of contaminated rain that falls on land, and by washoff from land by uncontaminated rain of previously deposited contamination. Weathering, resuspension, runoff, washoff, and radioactive decay decrease surface

concentrations of radioactive materials deposited on the ground. Weathering is modeled using Gale's equation [11]. Resuspension is modeled using resuspension factors [10] that attempt to represent the average effect of resuspension by many processes at very different rates throughout large regions. Runoff is modeled by assuming that some fixed fraction of all materials initially deposited onto land is rapidly transferred to water bodies either during the initial rain event or by rain events that occur very soon after the initial deposition [12]. Washoff is modeled as a first order removal process that is integrated over all time after the initial deposition [12]. Decrease of radioactivity due to radioactive decay treats only first generation daughter products, since doses from second generation daughters are insignificant.

2.1 Reactor Dimensions

2.1.1 Recommendation.

Table 2.1 gives the values recommended for initial plume (reactor wake) dimensions for the MACCS NUREG-1150 calculations.

Table 2.1. Values for Initial Plume Dimensions

Reactor	BUILDH ^a			BUILDW ^b		
	Value	Range	Distribution	Value	Range	Distribution
Surry	50	10-50	Uniform	40	10-?	Uniform
Sequoyah	40	10-40	Uniform	40	10-225	Uniform
Peach Bottom	50	10-50	Uniform	50	10-200	Uniform
Grand Gulf	60	10-60	Uniform	40	10-175	Uniform

^a BUILDH - Building height

^b BUILDW - Building width

2.1.2 Discussion

In MACCS, the values specified for BUILDH and BUILDW determine the initial size of the plume upon escape from the wake of the reactor. Specifically, initial values for σ_z and σ_y , the vertical and crosswind standard deviations of the Gaussian plume, are calculated using the following relations [13a]:

$$\text{BUILDH} = 2.15 \sigma_z$$

$$\text{BUILDW} = 4.3 \sigma_y$$

These equations allow mixing of the plume into the reactor wake to be modeled by first setting crosswind plume dimensions upon escape from the wake equal to the crosswind dimensions of the wake and then backcalculating an upwind virtual point source for a plume with these dimensions.

Both theory [13b] and experiments [1] suggest that a plume released from a building under turbulent conditions will be entrained by the building's wake and before escaping from that wake will become well mixed throughout its volume. As long as windspeeds are significant, entrainment and thorough mixing occur not only when the release occurs from the lee face of the building, but also from its side, top, or upwind face. However, when conditions are not turbulent, the plume is observed to escape from the wake before becoming well mixed throughout its full volume.

These observations suggest that selecting values for BUILDH and BUILDW may not be straightforward. For example, for release from a rectangular building under turbulent conditions, the crosswind dimensions of the wake will depend on the orientation of the wind relative to the building. Moreover, when turbulence is minimal, initial plume dimensions upon escape from the building wake may be much smaller than the crosswind dimensions of the wake itself. Indeed, if windspeeds are very low, initial plume dimensions may be much closer to the dimensions of the hole in the building from which the plume issues, than to the dimensions of the building's wake.

Experiments also indicate that when prevailing conditions are turbulent, plume growth is so rapid that downwind size soon becomes independent of size upon escape from the building wake. Therefore, use of initial plume dimensions appropriate for release under nonturbulent conditions will not lead to significant errors if applied to releases under turbulent conditions. But failure dimensions are not known for NUREG-1150 source terms and no simple model for mixing into a portion of a building wake is available. Therefore, the specification of plume dimensions upon escape from the building wake when conditions are nonturbulent must be largely a guess.

Since some mixing into the building wake will occur whenever the prevailing wind is not stagnant, use of dimensions significantly larger than the dimensions of the containment failure seems appropriate. This will also be correct for blowdown plumes where dissipation of the energy of the jet produces substantial expansion of the plume (e.g., a jet that issues from a 1 m² hole will produce a plume with a cross-sectional area of about 100 m² after expansion dissipates the initial energy of the jet [14]). Therefore, somewhat arbitrarily, after rounding to the nearest multiple of 10 m, the dimensions of the reactor containment as read from FSAR drawings [15-18] are given above for BUILDH and BUILDW.

2.1.3 Correlations

BUILDH and BUILDW will be strongly correlated with prevailing atmospheric stability. Specifically, when unstable (Classes A-C) or neutral (Class D) atmospheric conditions prevail, the plume will become well mixed throughout the wake cavity before it escapes from the building wake. Therefore, when unstable or neutral conditions prevail, values at the upper end of the ranges specified above for BUILDH and BUILDW should be used. Conversely, when stable atmospheric conditions prevail (Classes E and F), the plume may either not be completely entrained into the building wake or, if completely entrained, may not become well mixed throughout its volume before escaping.

Therefore, when stable atmospheric conditions prevail, values at the lower end of the ranges specified above for BUILDH and BUILDW should be used. Because BUILDH and BUILDW are both correlated in the same way with atmospheric stability, they are also positively correlated with each other. For blowdown plumes, BUILDH and BUILDW will also be strongly and positively correlated with the energy of the blowdown jet. Finally, for plumes not initialized by blowdown, the nature of the correlation of BUILDH and BUILDW with atmospheric stability may cause the distributions of these variables to be bimodal, having small values when stable conditions prevail and large values when neutral or unstable conditions prevail.

2.2 Plume Rise

2.2.1 Recommendation

The values in Table 2.2 are recommended for plume rise scaling factors.

Table 2.2. Plume Rise Scaling Factors

Variable	Summary
SCLCRW	<p>Linear scaling factor on the critical wind speed (U_c) used in MACCS to determine whether buoyant plumes will be trapped in the turbulent wake of the reactor building complex. For any release, if the wind speed is greater than U_c, the plume is assumed to be trapped in the building wake, thereby preventing plume rise. By scaling the value of U_c, the MACCS user can examine the effect of the critical windspeed for escape from the building wake on the occurrence of plume rise.</p> <p>Base value: 1.0 Range: 0.5 to 2.0</p>
SCLADP	<p>Linear scaling factor on the amount of plume rise that will occur when the prevailing atmospheric conditions are characterized by stability class A, B, C, or D.</p> <p>Base value: 1.0 Range: 0.5 to 1.5</p>
SCLEFP	<p>Linear scaling factor on the amount of plume rise that will occur when the prevailing atmospheric conditions are characterized by stability class E or F.</p> <p>Base value: 1.0 Range: 0.5 to 1.5</p>

2.2.2 Discussion

The parameter values that determine plume rise are all hardwired in MACCS. The user can modify them only by using the scaling factors, SCLCRW, SCLADP, or SCLEFP. A short overview of the plume rise formula that these scaling factors modify is presented below.

SCLCRW is a factor that linearly scales the critical wind speed, U_c , that MACCS uses to determine if buoyant plumes escape from the turbulent wake of a reactor complex before they dissipate all of their buoyancy. The critical wind speed is defined by [1]:

$$U_c = (9.09 F/L)^{1/3}$$

where

F = buoyancy flux from the source = $8.8 \times 10^{-6} Q$,

Q = energy release rate (Joules/s), and

L = suitable length scale for the reactor building (m).

This expression was first suggested by Briggs [19] and later experimentally confirmed by Hall and Waters during wind tunnel experiments with 1/300 scale models [1]. However, it should be noted that the critical wind speed does not mark a sudden change in the plume position as ground level concentrations change relatively slowly with the buoyancy parameter, $F/U^3 L$. Since the coefficient 9.09 is uncertain by something like an order of magnitude, U_c must be uncertain by about a factor of two.

SCLADP is a factor that linearly scales the amount of plume rise predicted by MACCS when the prevailing atmospheric stability class is A through D. The plume rise formula for stability classes A through D used in MACCS is Equation 2.15 in Hanna et al. [3]:

$$\Delta h = \frac{1.6 F^{1/3} X^{2/3}}{U}$$

where

Δh = plume rise above release height (m),

F = buoyancy flux parameter (m^4/s^3) = $8.8 \times 10^{-6} Q$,

Q = energy release rate (Joules/s),

X = down wind distance (m), and

U = wind speed (m/s).

The above expression is the so-called "2/3 law," which agrees well with field studies and laboratory data. In Reference [3], the authors pointed out that the coefficient 1.6 can be expected to be accurate to $\pm 40\%$. Therefore, the value of Δh must be uncertain by at least a factor of 1.5.

SCLEFP is a factor that linearly scales the amount of plume rise predicted by MACCS when the prevailing atmospheric stability class is E or F. The plume rise formula for stability classes E and F is Equation 3.19 in Hanna et al. [3]:

$$\Delta h = 2.6 [F/(US)]^{1/3}$$

where

Δh = plume rise above release height (m),
 F = buoyancy flux parameter (m^4/s^3) = $8.8 \times 10^{-6} Q$,
 Q = energy release rate (Joules/s),
 U = wind speed (m/s), and
 S = stability parameter (see discussion for details)
 $= (g/T) (dT/dZ + 0.01 \text{ K/m})$.

where

g = gravitational constant = 9.8 m/s^2 ,
 T = ambient temperature (K), and
 dT/dZ = vertical temperature gradient for stability class E or F.

In NRC Regulatory Guide 1.23 [20], dT/dZ is expressed by

$dT/dZ = -0.5 \text{ to } 1.5 \text{ K/100 m}$, for class E
 $dT/dZ = 1.5 \text{ to } 4.0 \text{ K/100 m}$, for class F

By taking the midpoints of these ranges, we have

$dT/dZ = 0.5 \text{ K/100 m} = 0.005 \text{ K/m}$, for class E
 $dT/dZ = 2.75 \text{ K/100 m} = 0.0275 \text{ K/m}$, for class F

After substituting the above values for dT/dZ and 288 K (the reference temperature for the standard atmosphere) for T , we have

$S = 5.1 \times 10^{-4}$, for stability class E
 $S = 1.27 \times 10^{-3}$, for stability class F

These values are currently hardwired in MACCS. Note that S is a function of ambient temperature T , which could vary from 270 K to 308 K for a site with a temperate climate.

2.3 Plume Meander

2.3.1 Recommendation

Table 2.3 lists the values recommended for the parameters used in MACCS to correct Pasquill-Gifford σ_y values for the effects of horizontal meandering of plume segments:

Table 2.3. MACCS Correction Parameters

<u>Variable</u>	<u>Definition</u>	<u>Value</u>
TIMBAS	Release time for the Prairie Grass experiments (s)	180
XPFAC1	Release time exponent for releases shorter than BRKPNT	0.2
XPFAC2	Release time exponent for releases greater than or equal to BRKPNT	0.25
BRKPNT	Release time break point for changing from XPFAC1 to XPFAC2 (s)	3600

2.3.2 Discussion

MACCS uses the following equation to correct Pasquill-Gifford σ_y values for the effect of horizontal meandering of plume segments [21]:

$$\sigma_{y,MACCS}(x) = \sigma_{y,P-G}(x) [\Delta t_{seg}/\Delta t_{P-G}]^m$$

where x is the downwind distance of the plume segment from its point of release, $\sigma_{y,MACCS}(x)$ is the σ_y value used in MACCS, $\sigma_{y,P-G}(x)$ is the Pasquill-Gifford value for σ_y at the distance x , Δt_{seg} is the release duration of the plume segment, and $\Delta t_{P-G} = 10$ minutes [22,23,3b] is the release duration of the Prairie Grass Project [24] plumes, which are the experimental basis for the Pasquill-Gifford curves that express the increase of σ_y with downwind distance [25]. Parameter values for this equation have been reviewed by Gifford [26], who suggests that $m = 0.2$ when Δt is greater than 3 minutes but less than 1 hour, that $m = 0.25$ when $t = 1$ hour, and that $m = 0.3$ when $\Delta t = 100$ hours. Since in MACCS plume segment durations may not exceed 10 hours, $m = 0.25$ is recommended for plume segments having release durations between 1 and 10 hours.

2.4 Plume Dispersion

The power-law parameter values recommended in Table 2.4 for use in MACCS to estimate stability-class dependent values for σ_y and σ_z are the values developed by Tadmor and Gur [27]:

Table 2.4. Power-Law Parameter Values for MACCS

<u>Variable</u>	<u>Definition</u>																		
DPCYSIGA	Stability class dependent pre-exponential coefficient in the power-law expression for σ_y																		
	Values by Pasquill-Gifford Stability Class																		
	<table><tr><td><u>A</u></td><td><u>B</u></td><td><u>C</u></td><td><u>D</u></td><td><u>E</u></td><td><u>F</u></td></tr><tr><td>0.3658</td><td>0.2751</td><td>0.2089</td><td>0.1474</td><td>0.1046</td><td>0.0722</td></tr></table>	<u>A</u>	<u>B</u>	<u>C</u>	<u>D</u>	<u>E</u>	<u>F</u>	0.3658	0.2751	0.2089	0.1474	0.1046	0.0722						
<u>A</u>	<u>B</u>	<u>C</u>	<u>D</u>	<u>E</u>	<u>F</u>														
0.3658	0.2751	0.2089	0.1474	0.1046	0.0722														
DPCYSIGB	Stability class dependent exponent in the power-law expression for σ_y																		
	Values by Pasquill-Gifford Stability Class																		
	<table><tr><td><u>A</u></td><td><u>B</u></td><td><u>C</u></td><td><u>D</u></td><td><u>E</u></td><td><u>F</u></td></tr><tr><td>0.9031</td><td>0.9031</td><td>0.9031</td><td>0.9031</td><td>0.9031</td><td>0.9031</td></tr></table>	<u>A</u>	<u>B</u>	<u>C</u>	<u>D</u>	<u>E</u>	<u>F</u>	0.9031	0.9031	0.9031	0.9031	0.9031	0.9031						
<u>A</u>	<u>B</u>	<u>C</u>	<u>D</u>	<u>E</u>	<u>F</u>														
0.9031	0.9031	0.9031	0.9031	0.9031	0.9031														
DPCZSIGA	Stability class dependent pre-exponential coefficient in the power-law expression for σ_y																		
	Values by Pasquill-Gifford Stability Class																		
	<table><tr><td><u>A</u></td><td><u>B</u></td><td><u>C</u></td><td><u>D</u></td><td><u>E</u></td><td><u>F</u></td></tr><tr><td>0.9031</td><td>0.9031</td><td>0.9031</td><td>0.9031</td><td>0.9031</td><td>0.9031</td></tr><tr><td>0.00025</td><td>0.0019</td><td>0.2</td><td>0.3</td><td>0.4</td><td>0.2</td></tr></table>	<u>A</u>	<u>B</u>	<u>C</u>	<u>D</u>	<u>E</u>	<u>F</u>	0.9031	0.9031	0.9031	0.9031	0.9031	0.9031	0.00025	0.0019	0.2	0.3	0.4	0.2
<u>A</u>	<u>B</u>	<u>C</u>	<u>D</u>	<u>E</u>	<u>F</u>														
0.9031	0.9031	0.9031	0.9031	0.9031	0.9031														
0.00025	0.0019	0.2	0.3	0.4	0.2														
DPCZSIGB	Stability class dependent exponent in the power-law expression for σ_y																		
	Values by Pasquill-Gifford Stability Class																		
	<table><tr><td><u>A</u></td><td><u>B</u></td><td><u>C</u></td><td><u>D</u></td><td><u>E</u></td><td><u>F</u></td></tr><tr><td>2.1250</td><td>1.6021</td><td>0.8543</td><td>0.6532</td><td>0.6021</td><td>0.6020</td></tr></table>	<u>A</u>	<u>B</u>	<u>C</u>	<u>D</u>	<u>E</u>	<u>F</u>	2.1250	1.6021	0.8543	0.6532	0.6021	0.6020						
<u>A</u>	<u>B</u>	<u>C</u>	<u>D</u>	<u>E</u>	<u>F</u>														
2.1250	1.6021	0.8543	0.6532	0.6021	0.6020														

2.4.1 Discussion

In MACCS, horizontal and vertical dispersion of plume segments about their centerlines are calculated using Gaussian plume models [21]. These models assume that dispersion of plume materials produces normal distributions in the horizontal (y) and vertical (z) directions. Thus, the standard deviations (σ_y and σ_z) of these distributions determine the horizontal and vertical extent of each plume segment, and are calculated using the following:

$$\sigma_y = ax^b \qquad \sigma_z = cx^d \qquad (2.1)$$

where $a = \text{DPCYSIGA}$, $b = \text{DPCYSIGB}$, $c = \text{DPCZSIGA}$, $d = \text{DPCZSIGB}$, and x is the distance from the segment's release point to its present location. The values of the coefficients a , b , c , and d depend on atmospheric stability and thus vary with the six stability classes (Pasquill-Gifford classes A-F) used in MACCS. So whenever stability class changes, the apparent upwind location of the release (virtual source distance) must be recalculated by solving Equation 2.1 for x using the current value of σ_y or σ_z and the values of the parameters a , b , c , and d that correspond to the new atmospheric stability class.

Analytical fits of Equation 2.1 to experimental diffusion data measured in the field have been developed for all of the six Pasquill-Gifford stability classes by Tadmor and Gur [27], by Klug [28], and by Geiss [28]. The fits of Tadmur and Gur and of Klug are based on data gathered during the Prairie Grass Project [24]. The fits of Geiss are based on field studies of diffusion performed near the Julich Nuclear Research Center in Germany. The Prairie Grass experiments were conducted over flat terrain covered by prairie grass (low surface roughness). The releases were cold, of short duration (10 min.), and made at ground level. Downwind measurements were made to a distance of 0.8 km. The Julich experiments were conducted over farmland (medium surface roughness) and woodland (high surface roughness). The releases were cold, had one hour durations, and were made at three heights (50, 100, and 180 m). Downwind measurements were made to a distance of 11 km.

Table 2.5 presents the values of a, b, c, and d developed by Tadmor and Gur, by Klug, and by Geiss:

Table 2.5. Values for Constants in Equation 2.1

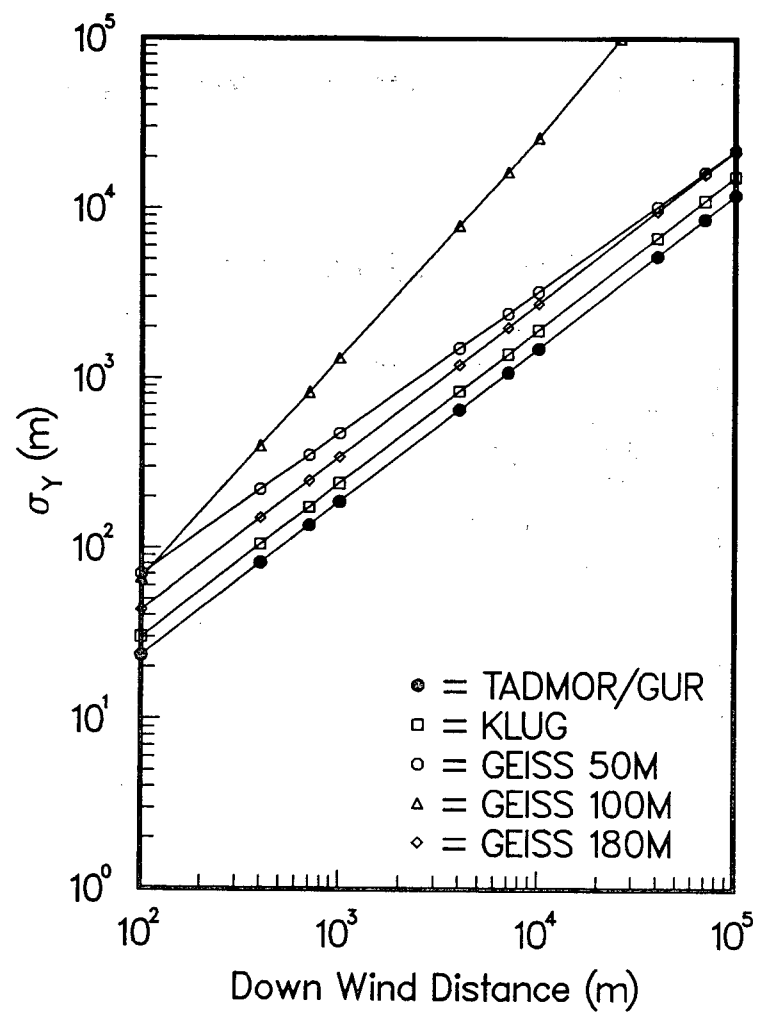
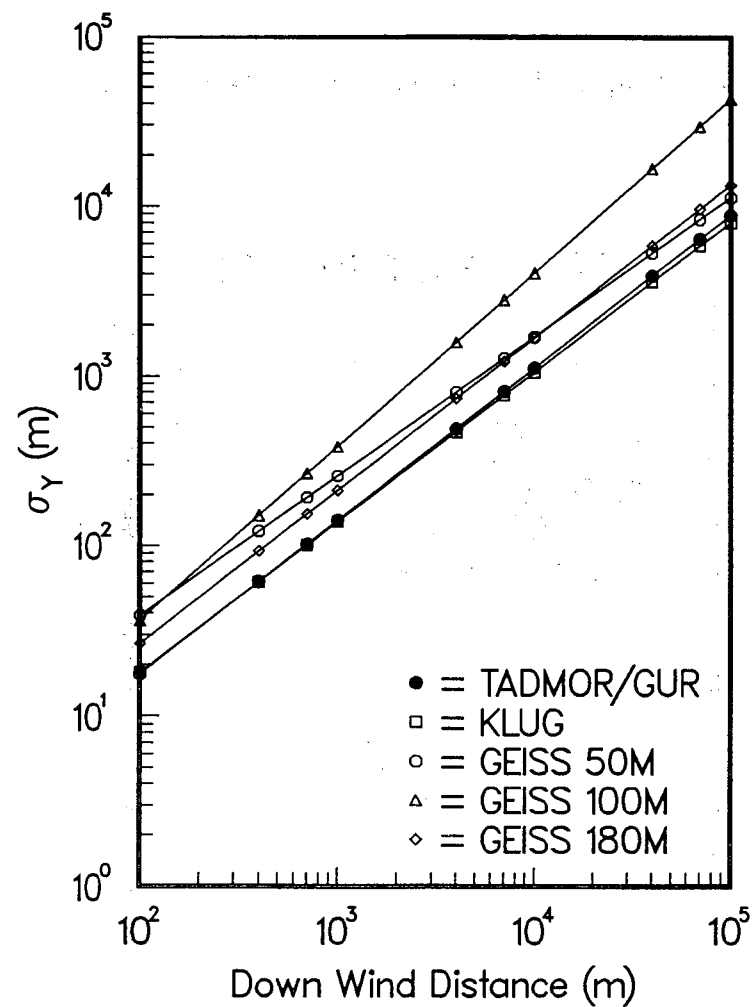
Study	Constant	Pasquill-Gifford Diffusion Class					
		A	B	C	D	E	F
Tadmor & Gur	a	0.3658	0.2751	0.2089	0.1474	0.1046	0.0722
	b	0.9031	0.9031	0.9031	0.9031	0.9031	0.9031
	c	0.00025	0.0019	0.2000	0.3000	0.4000	0.2000
	d	2.125	1.6021	0.8543	0.6532	0.6021	0.6020
Klug	a	0.4690	0.3060	0.2300	0.2190	0.2370	0.2730
	b	0.9030	0.8850	0.8550	0.7640	0.6910	0.5940
	c	0.0170	0.0720	0.0760	0.1400	0.2170	0.2620
	d	1.3800	1.0210	0.8790	0.7270	0.6100	0.5000
Geiss 50m	a	1.503	0.876	0.659	0.640	0.801	1.294
	b	0.833	0.823	0.807	0.784	0.754	0.718
	c	0.151	0.127	0.165	0.215	0.264	0.241
	d	1.219	1.108	0.996	0.885	0.774	0.662
Geiss 100m	a	0.170	0.324	0.446	0.504	0.411	0.253
	b	1.296	1.025	0.866	0.818	0.882	1.057
	c	0.051	0.070	0.137	0.265	0.487	0.717
	d	1.317	1.151	0.985	0.818	0.652	0.486
Geiss 180m	a	0.671	0.415	0.232	0.208	0.345	0.671
	b	0.903	0.903	0.903	0.903	0.903	0.903
	c	0.2045	0.0330	0.104	0.307	0.546	0.484
	d	1.500	1.320	0.997	0.734	0.557	0.500

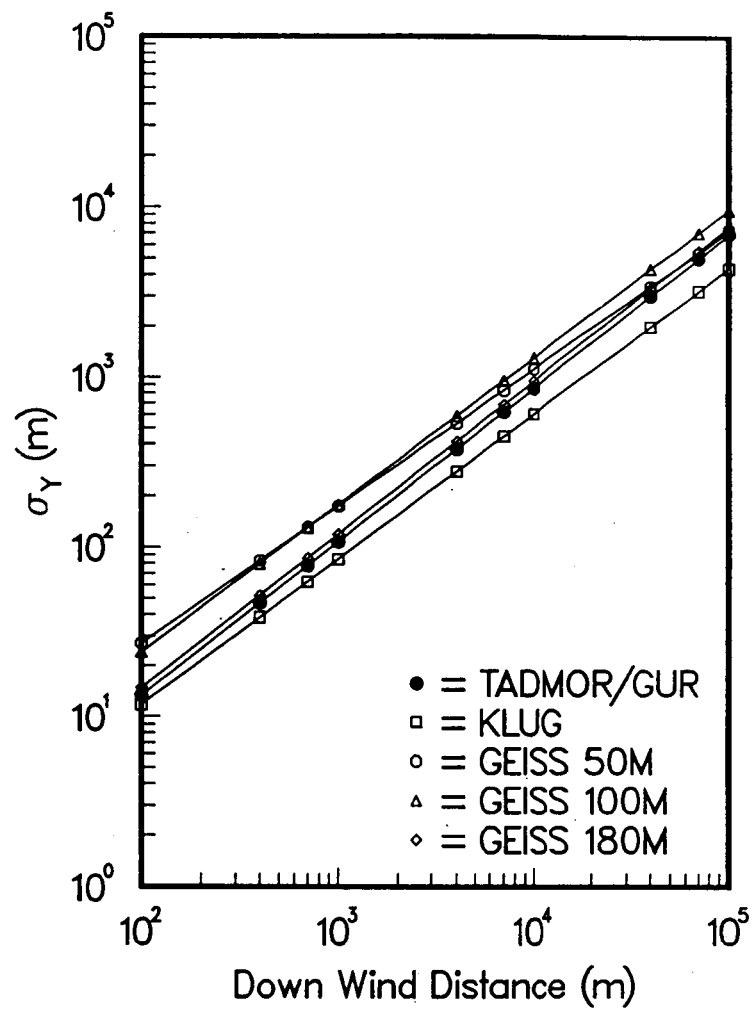
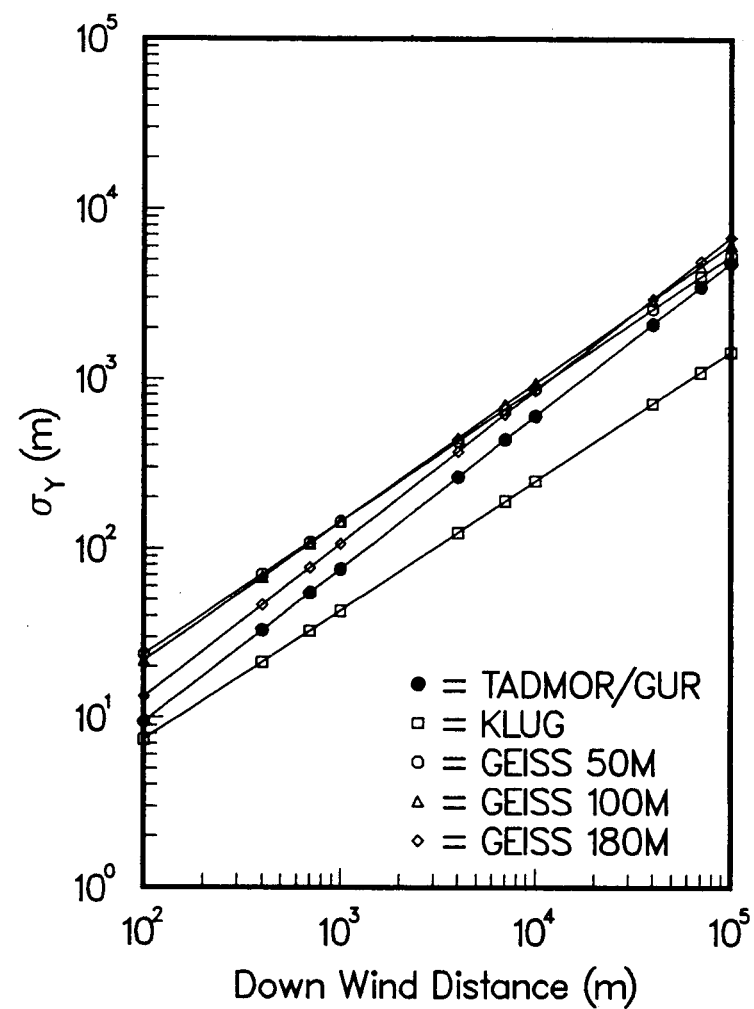
Figures 2.1 through 2.12 compare the effect of these five sets of parameter values on the increase of σ_y and σ_z with downwind distance. Figures 2.1 through 2.6 present the fits for σ_y . The fits for σ_z are presented in Figures 2.7 through 2.12.

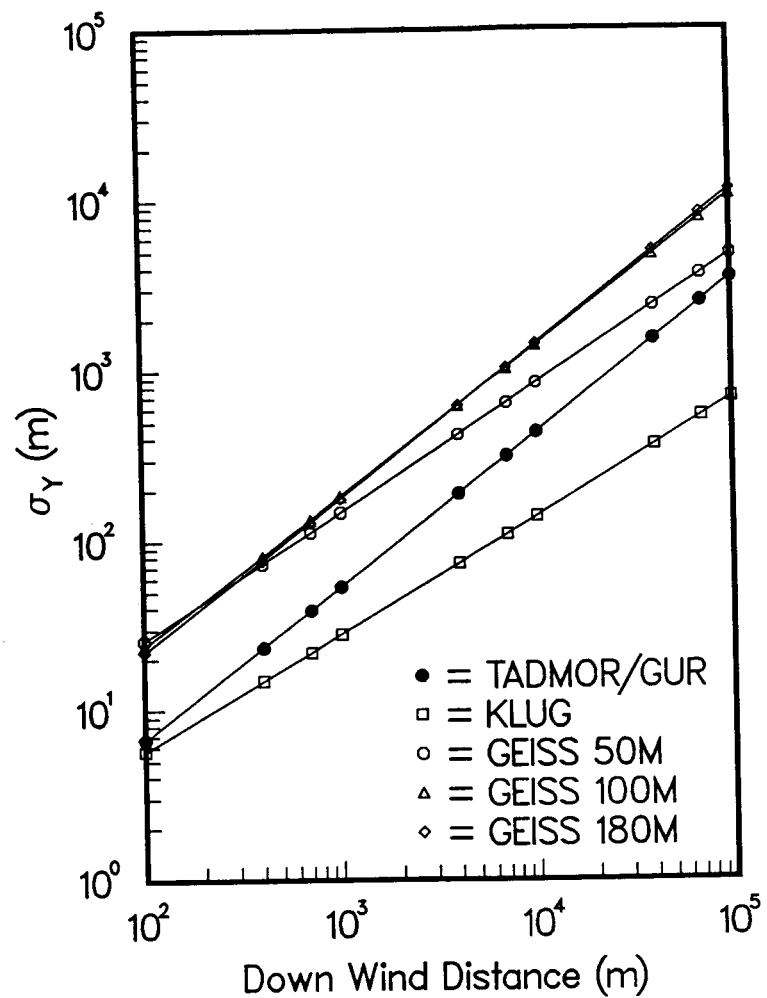
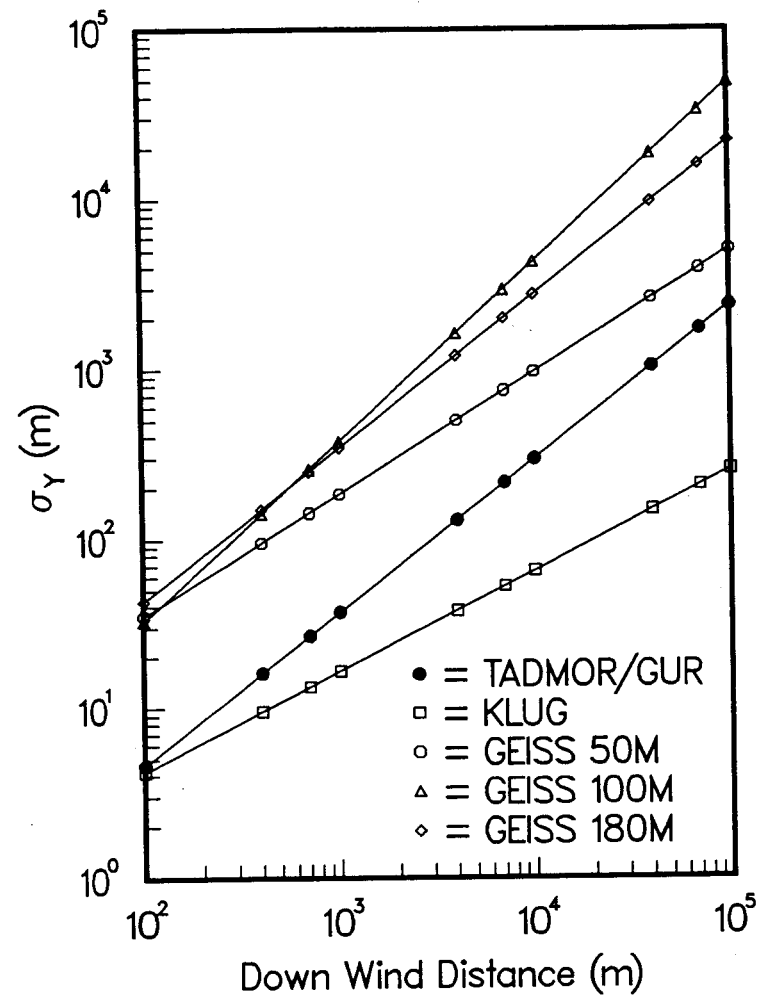
Because in MACCS reactor building dimensions determine the initial size (initial σ_y and σ_z values) of plume segments, the slope of the fits displayed in Figures 2.1 through 2.12 is important, but the magnitude of σ_y or σ_z (size of the plume) at a given distance is not. For example, if the width of the reactor building specified in MACCS input corresponds to an initial σ_y value of 250 m and the atmospheric stability at plume release is Class E, then Figure 2.5 shows that MACCS will calculate an initial upwind virtual source distance of 100 m if the Geiss 100 m σ_y fit is used, and an initial upwind virtual source distance of 400 m if the Tadmur and Gur σ_y fit is used. After this initialization step is completed, plume growth with downwind transport

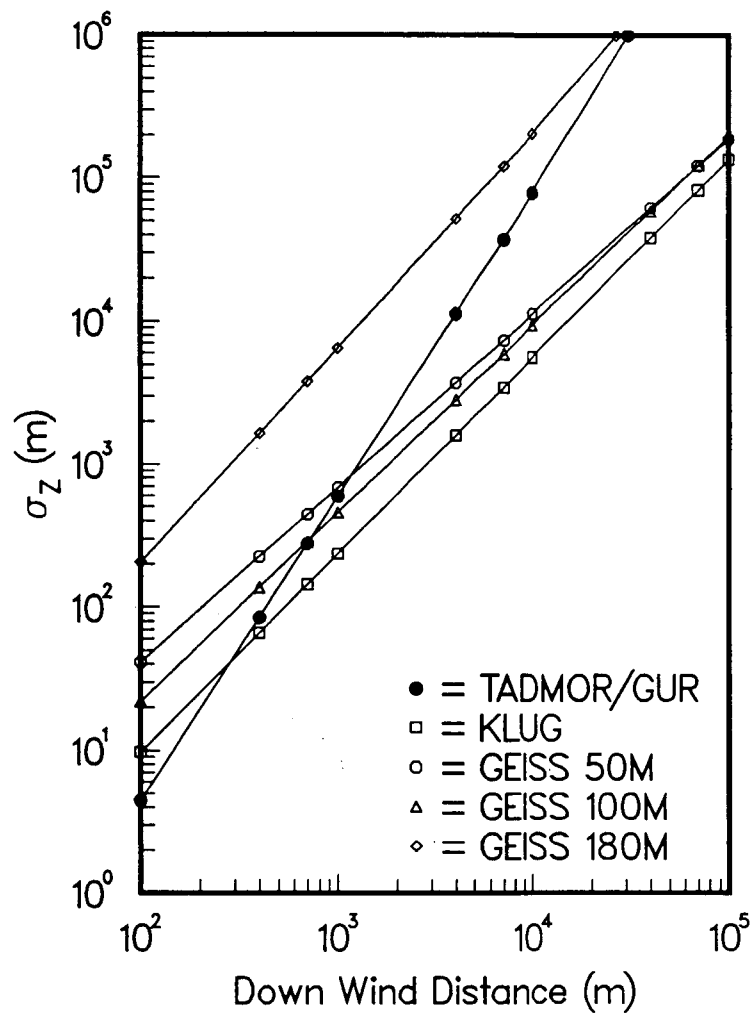
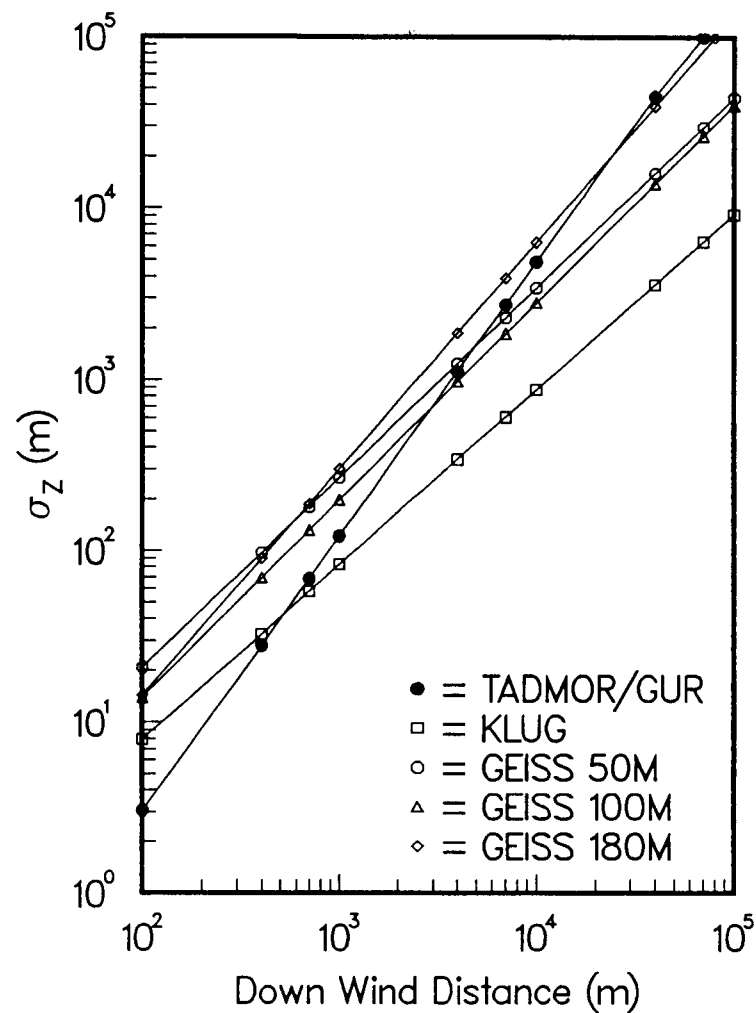
distance will be about the same using either σ_y fit, since both fits have about the same slope.

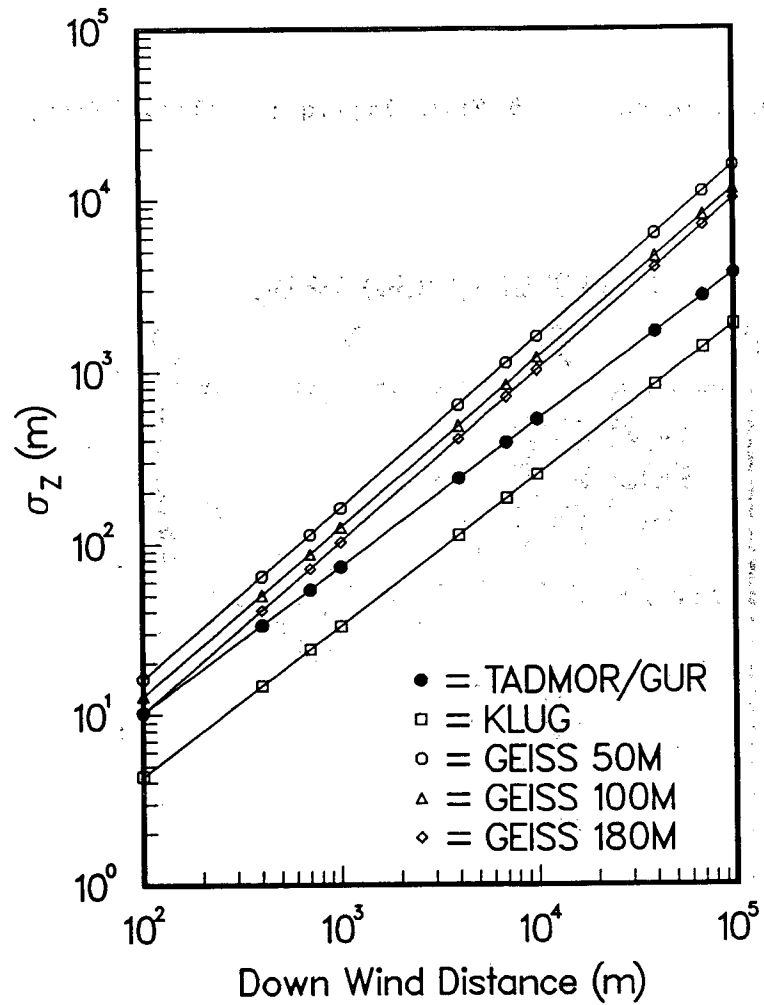
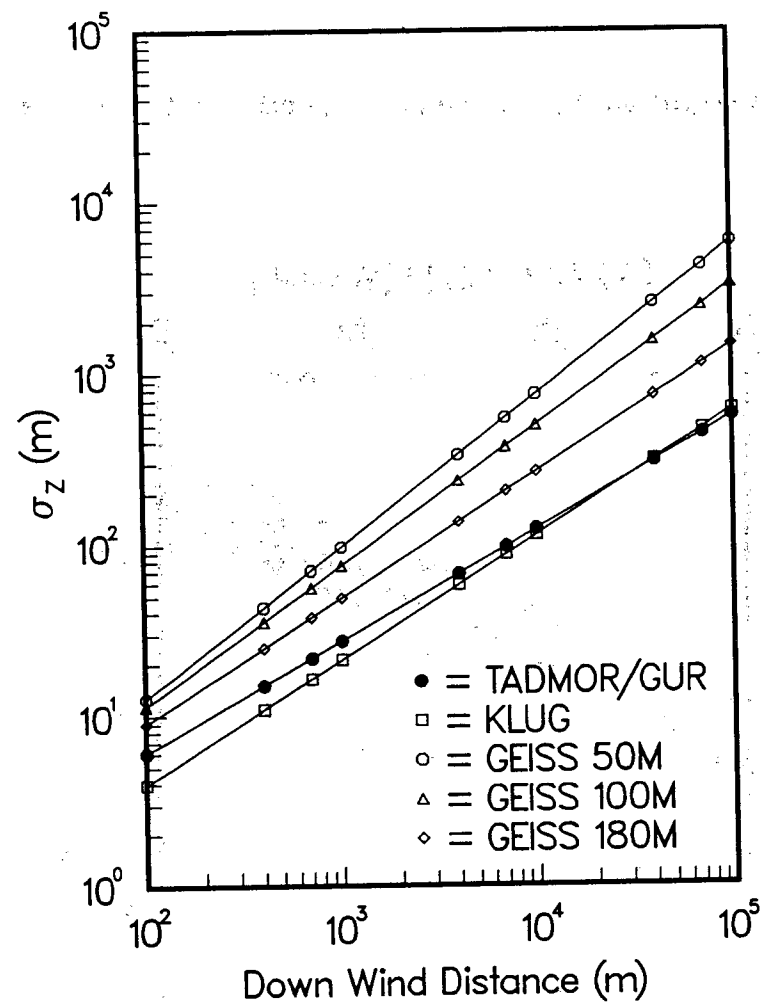
Figures 2.1 through 2.12 show that for any stability class, all the fits have similar slopes with but two exceptions: for stability classes A and B, the Geiss σ_y fits to 100 m releases and the Tadmor and Gur σ_z fits have significantly larger slopes than the other fits to those stability classes. The figures also show that the fits of Geiss to 180 m releases and the fits of Klug have slopes that are qualitatively representative of the envelope of slopes for the fits to any single stability class. Since buoyant plumes typically rise 180 m or so after release and most U.S. reactors are situated in regions having surface roughnesses greater than that of prairie grass, use of the Geiss 100 m fits seems indicated. Nevertheless, for the NUREG-1150 calculations, use of the Tadmur and Gur fits is recommended because relative to their uncertainties all of the fits are more or less equivalent and because the Tadmur and Gur fits have been used in most previous NRC consequence modeling studies.

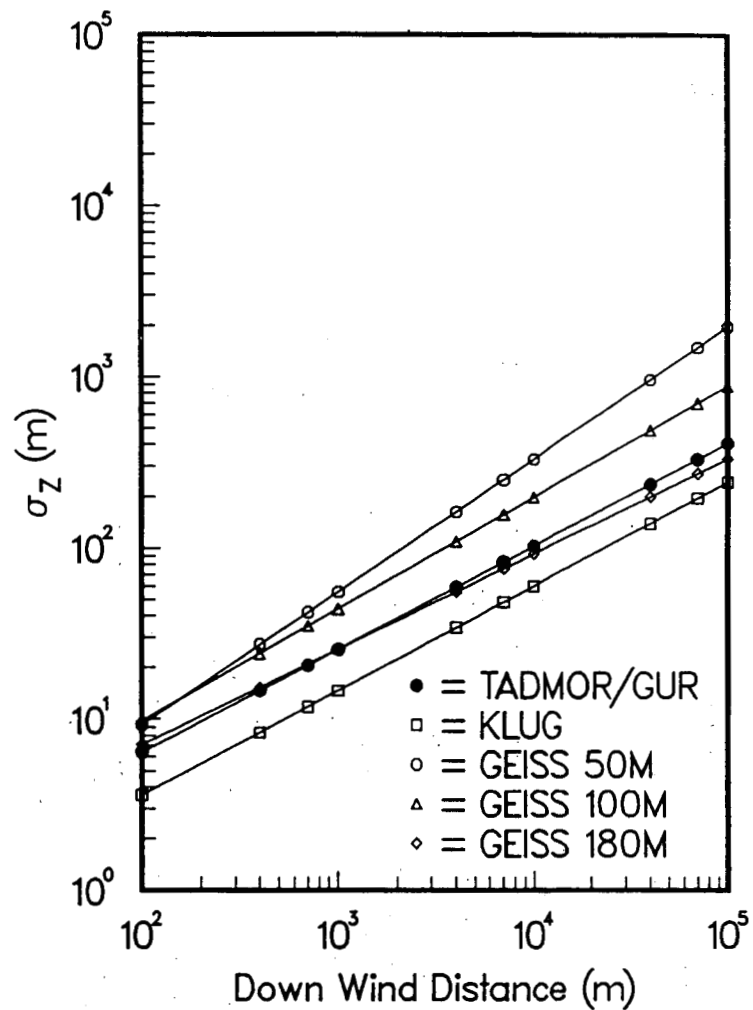
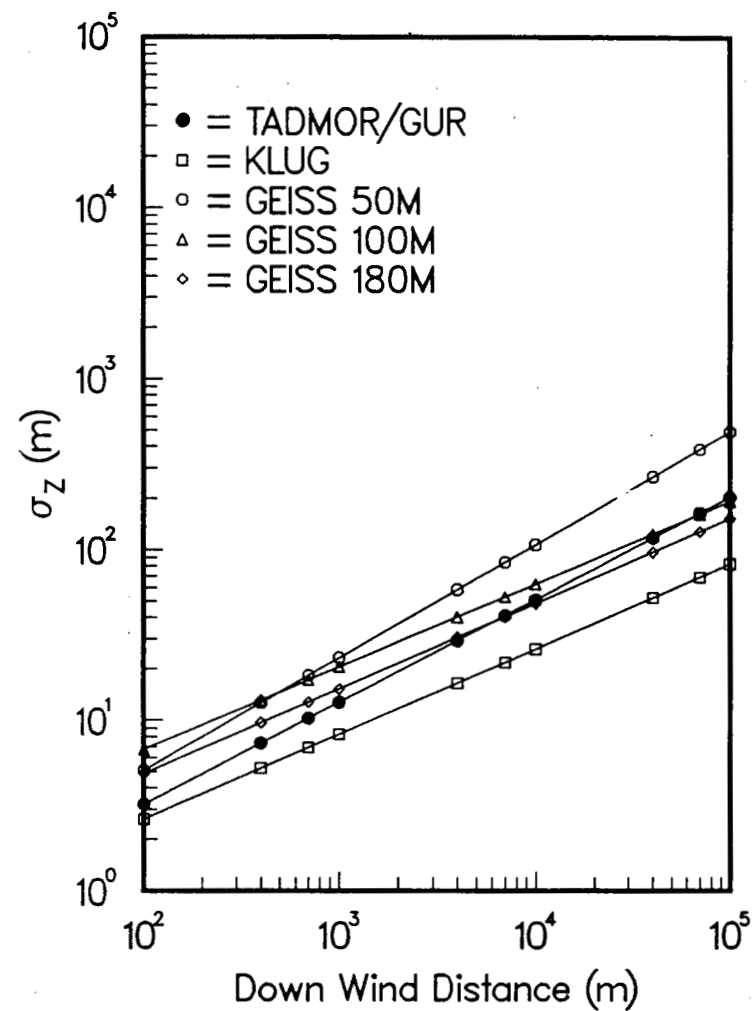
Figure 2-1. Stability Class A: σ_y vs Distance.Figure 2-2. Stability Class B: σ_y vs Distance.

Figure 2-3. Stability Class C: σ_y vs Distance.Figure 2-4. Stability Class D: σ_y vs Distance.

Figure 2-5. Stability Class E: σ_y vs Distance.Figure 2-6. Stability Class F: σ_y vs Distance.

Figure 2-7. Stability Class A: σ_z vs Distance.Figure 2-8. Stability Class B: σ_z vs Distance.

Figure 2-9. Stability Class C: σ_z vs Distance.Figure 2-10. Stability Class D: σ_z vs Distance.

Figure 2-11. Stability Class E: σ_z vs Distance.Figure 2-12. Stability Class F: σ_y vs Distance.

2.5 Dry Deposition Velocity

2.5.1 Recommendation

The values in Table 2.6 are recommended for the dry deposition velocity (VDEPOS).

Table 2.6. Dry Deposition Velocity

<u>Variable</u>	<u>Definition</u>	<u>Value</u>	<u>Range</u>
VDEPOS	Dry deposition velocity (cm/s)	0.3	0.03 - 3.0

2.5.1 Discussion

In MACCS, particulate matter is removed from plumes during downwind transport by washout and by dry deposition. Dry deposition is modeled using a mass transfer approach. Thus, the flux (ω) of particles to the ground due to dry deposition is calculated as the product of the ground level air concentration of the particles (X) and their dry deposition velocity ($v_d = \text{VDEPOS}$), where the dry deposition velocity is an empirical, particle-size-dependent parameter that represents the combined effects of diffusion to, impaction on, and settling onto surfaces:

$$\omega = v_d X$$

The magnitude of v_d depends on particle size, shape, and density, on atmospheric turbulence (wind speed, stability class), and on surface roughness (z_0) and friction velocity (u_*). Because aerosol size distributions were not developed for NUREG-1150 source terms, a single value for v_d had to be selected for the NUREG-1150 MACCS calculations and the value selected needed to reasonably represent the mean of the range of values that might actually occur.

This discussion of v_d is based on the following assumptions:

Rapid agglomeration of small particles before plume release from containment will largely eliminate particles smaller than 0.5 μm .

Gravitational settling will deplete the distribution of particles larger than 5 μm .

Fission product aerosols will have densities of a few grams per cubic centimeter (1 - 4 g/cm^3).

The value selected for v_d should well represent deposition to suburban areas because most population exposures will occur in suburban areas.

Both theoretical [10,29,30] and experimental [28,31,32,3] estimates of the magnitude of v_d are available. A theoretical model that gives v_d as a function of particle diameter, particle density, surface roughness, and

friction velocity has been developed by Sehmel and Hodgson [29]. Hobert et al. [30] found that $v_d = 0.0036 u_*$ with little dependence on particle size. The prevailing windspeed (u), its measurement height (z), surface roughness (z_0), and friction velocity (u_*) are related as follows [10]:

$$u = (u_*/k) \ln ((z+z_0)/z_0) \quad (2.5.1)$$

where $k = 0.4$ is von Karman's constant.

Table 2.7 presents values of z_0 and u_* for various surfaces

Table 2.7. Values of z_0 and u_*

Surface	z_0	u_*
Lawns	1	40
Tall Grass, Crops	10 - 15	70
Countryside	30	
Suburbs	100	
Trees, Forests	20 - 200	90
Cities	100 - 300	

If $z_0 = 100$ for suburbs and 5 m/s is a typical windspeed at a measurement height of 10 m, then from Equation 2.5.1 $u_* = 87$ cm/s and $v_d = 0.0036 u_* = 0.0036 (87 \text{ cm/s}) = 0.3 \text{ cm/s}$.

Figure 2.13 presents typical results for the Sehmel and Hodgson model for v_d for $u_* = 50$ cm/s. The figure shows that if $z_0 = 10$ cm, an aerosol distribution with a mean size (particle diameter) of $2 \mu\text{m}$ and a mean density of 2 g/cm^3 will have $v_d = 0.4$ cm/s. Figures from Sehmel [1] similar to this figure give $v_d = 3.0$ cm/s when $u_* = 100$ cm/s, $z_0 = 100$ cm, $r = 5 \mu\text{m}$, and $\rho = 4 \text{ g/cm}^3$; and $v_d = 0.03$ cm/s when $u_* = 30$ cm/s, $z_0 = 3$ cm, $r = 0.5 \mu\text{m}$, and $\rho = 1 \text{ g/cm}^3$.

DEPOSITION AND RESUSPENSION

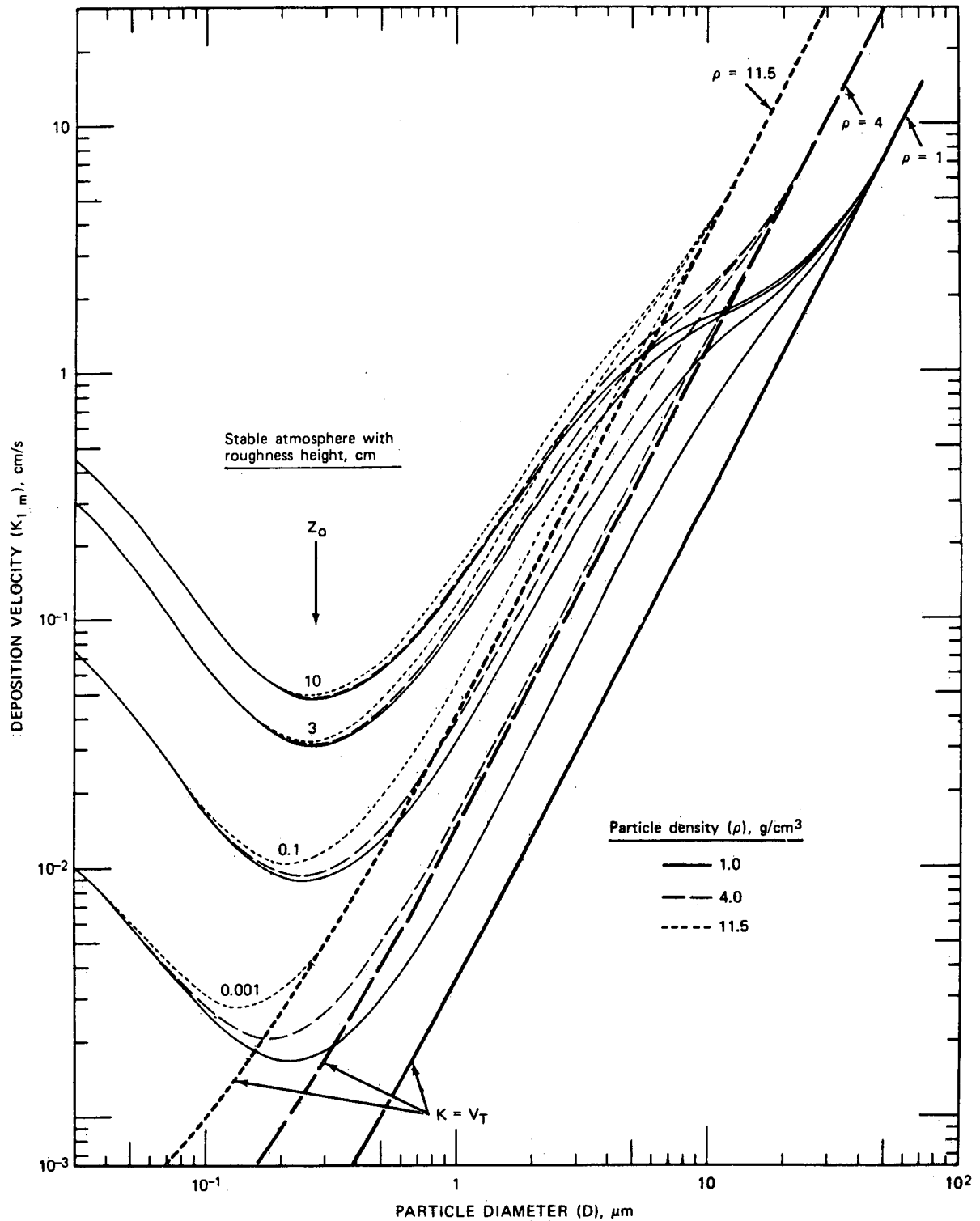


Figure 2.13. Predicted Deposition Velocities at 1 m for $u^* = 50$ cm/s and Particle Densities of 1.4 and 11.5 g/cm³.

Table 2.8 presents experimental values for v_d

Table 2.8. Experimental Values for v_d

<u>Aerosol Composition</u>	<u>Aerosol Size</u> (μm)	<u>Deposition Surface</u>	<u>Deposition Velocity</u>		<u>Reference</u>
			<u>Range</u> (cm/s)	<u>Arithmetic Mean^a</u> (cm/s)	
--	1	Grass		0.1	[28]
--	1		0.1 -1	0.5	[31]
Various ^b		Asphalt	0.01-0.3	0.15	[32]
		Concrete	0.005-0.2	0.1	
		Flagstones			
		Roofs	0.03-0.6	0.3	
		Bare Soils	0.1-0.6	0.3	
Various ^c		Trees	0.05-1	0.5	
		Forest	0.07-0.9	0.5	
		Grass	0.03-0.8	0.4	
--	0.1-10	Tall Grass	0.5-2	1.0	[3]
--	0.003-100		0.001-180	0.4 ^d	[10]

^a Arithmetic mean because for any aerosol size distribution mass will be concentrated among the larger particles that will have larger dry deposition velocities.

^b Aerosols containing Cs-134, Cs-137, I-131, La-140, La-141, Ce-141, Ce-144, Ru-106, Zr-95, and Nb-95.

^c Aerosols containing Cs-137 and I-131.

^d Geometric mean because of the large size range.

Examination of the table suggests that deposition to roads, lawns, and trees will occur with velocities of about 0.1, 0.3, and 0.5 cm/s. Therefore, if a typical residential suburb has roughly equal amounts of surface area provided by roads, lawns, and canopy (leaves on trees and shrubs), then $v_d = 0.3$. Therefore, since both theory and experiment suggest that $v_d =$ about 0.3 cm/s with a range of 0.03 to 3 cm/s, these values are recommended for use in the MACCS NUREG-1150 calculations.

2.6 Wet Deposition Parameters

2.6.1 Recommendation

The values in Table 2.9 are recommended for use in characterizing plume washout from rainfall.

Table 2.9. Plume Washout from Rainfall

<u>Variable</u>	<u>Summary</u>
CWASH1	Liner coefficient (s^{-1}) in expression defining rate constant for plume washout from rainfall (see Eq. 2.3). <u>Base value</u> : 9.5×10^{-5} . <u>Range</u> : $3 \times 10^{-5} - 3 \times 10^{-4}$. <u>Sampling Distribution</u> : Log uniform.
CWASH2	Exponential term in expression defining rate constant for plume washout due to rainfall (see Eq. 2.3). <u>Base value</u> : 0.8. <u>Range</u> : 0.7-0.9. <u>Sampling Distribution</u> : Uniform.

2.6.2 Rationale

The rain washout model in MACCS is of the form

$$dA/dt = -\lambda A, A(0) = A_0 \quad (2.2)$$

where

$A(t)$ = amount (Bq/m^2) of a radionuclide in the atmosphere above a region after a period of rainfall of length t (s),

λ = rate constant (s^{-1}) for radionuclide scavenging due to rainfall, and

A_0 = amount (Bq/m^2) of a radionuclide in the atmosphere above a region at the start of a period of rainfall (i.e., at $t = 0$ s).

In turn, λ is assumed to be a function of rainfall intensity. Specifically, λ is defined by

$$\lambda = aR^b \quad (2.3)$$

where R is the rainfall rate (mm/h) and $a = CWASH1$ and $b = CWASH2$ are empirically derived constants.

Additional background on this and other characterizations for rainfall scavenging is available elsewhere [9,33-36].

In MACCS, the constants a and b appearing in Equation 2.3 are used to characterize washout from rainfall. Brenk and Vogt [9] gave the following values for a and b ,

$$a = 1.2 \times 10^{-4}, \quad b = 0.5 \quad (2.4)$$

which have been used in past analyses with MACCS. In the NRPB review [33,31], it is concluded that the following ranges characterize values for a and b that are appropriate for use in a reactor accident code that must calculate washout under a variety of conditions:

$$3 \times 10^{-5} \leq a \leq 3 \times 10^{-4}, \quad 0.7 \leq b \leq 0.9 \quad (2.5)$$

For uncertainty studies, the above ranges will be used. Further, the following values at the center of the indicated ranges will be used as base values in the NUREG-1150 consequence analyses:

$$a = 9.5 \times 10^{-5}, \quad b = 0.8 \quad (2.6)$$

2.7 Weathering

2.7.1 Recommendation

The values in Table 2.10 are recommended for characterizing the "weathering" of external exposure in MACCS.

Table 2.10. Weathering of Radionuclides on Ground

Variable	Summary
NGWTRM	Number of different weathering processes selected for consideration. <u>Base Value</u> : 2.
GWCOEF1	Fraction of the deposition undergoing weathering process 1. <u>Base Value</u> : 0.5. <u>Range</u> : 0.25 to 0.75. <u>Sampling Distribution</u> : Uniform.
TGWHLF1	Weathering half-life (sec) for fraction of the deposition undergoing weathering process 1. <u>Base Value</u> : 1.6×10^7 s. <u>Range</u> : 7.8×10^6 to 2.3×10^7 . <u>Sampling Distribution</u> : Uniform.
GWCOEF2	Fraction of the deposition undergoing weathering process 2. <u>Value</u> : $1-A_1$.
TGWHLF2	Weathering half-life (sec) for fraction of the deposition undergoing weathering process 2. <u>Base Value</u> : 2.8×10^9 s. <u>Range</u> : 1.4×10^9 to 4.2×10^9 . <u>Sampling Distribution</u> : Uniform.

2.7.2 Rationale

The "weathering" model in MACCS for external exposure to deposited radionuclides is of the form

$$D(t) = D_0 e^{-\lambda t} \sum_{i=1}^n \left(A_i e^{-\lambda_i t} \right) \quad (2.7)$$

where

$D(t)$ = dose rate (Sv/s) from a ground-deposited radionuclide at time t (s) after its initial deposition,

D_0 = dose rate (Sv/s) at the time of initial deposition (i.e., at $t = 0$ s),

λ = decay constant (s^{-1}) for the radionuclide under consideration,

n = number of different weathering processes selected for consideration (e.g., short term and long term),

A_i = fraction of the deposition undergoing weathering process i (subject to the constraint that $A_1 + \dots + A_n = 1$), and

λ_i = decay constant (s^{-1}) for the portion of the external dose subject to weathering process i .

In turn, the λ_i are defined by

$$\lambda_i = \ln(2)/\tau_i \quad (2.8)$$

where

τ_i = weathering half-life (s), i.e., the time period over which the dose rate subject to weathering process i will decrease by 50%.

When only weathering processes are specified (i.e., NGWTRM = 2), then $T_1 = \text{TGWHLF1}$ and $T_2 = \text{TGNHLF2}$.

The use of weathering expressions of the form shown in Equation 2.7 for the assessment of time-dependent external exposure in reactor accident consequence assessments derives from a study by Gale et al. [37]. This study was performed in England and used experimental plots involving five different soil types to estimate the time-dependent external exposure from a deposition of ^{137}Cs . The results of this study lead to the following form of the expression in Equation 2.7:

$$D(t) = D_0 e^{-\lambda t} \left[A_1 e^{-\lambda_1 t} + A_2 e^{-\lambda_2 t} \right] \quad (2.9)$$

where

$$A_1 = 0.63,$$

$$\lambda_1 = \ln(2)/\tau_1 = \ln(2)/0.61 \text{ yr} = 1.13 \text{ yr}^{-1} = 3.65 \times 10^{-8} \text{ s},$$

$$A_2 = 0.37, \text{ and}$$

$$\lambda_2 = \ln(2)/\tau_2 = \ln(2)/92 \text{ yr} = 0.075 \text{ yr}^{-1} = 2.42 \times 10^{-9} \text{ s}.$$

The relationship in Equation 2.9 was used to estimate dose reduction in WASH-1400 and has also been used in many other reactor accident consequence assessments.

Until recently, the study by Gale et al. [37] appears to have been the only study providing any direct information of the time-dependent change in external exposure. However, several additional studies have recently been completed and will be briefly discussed. It is likely that more information on time-dependent weathering will become available in the future as the results of the Chernobyl accident are analyzed.

Warming [38,39] has performed several weathering experiments on impermeable surfaces in Denmark. The 1984 study involved the behavior of ^{86}Rb (an analogue for cesium) on concrete and asphalt surfaces. The following results were obtained. For one-year-old concrete, a maximum of 60% of the contamination (i.e., $A_1 = 0.6$) was weathered away with a half-life of 100 days

(i.e., $\tau_1 = 0.27$ yr). For "young" asphalt, 60% of the contamination (i.e., $A_1 = 0.6$) is removed with a half-life of 60 days (i.e., $\tau_1 = 0.16$ yr). An "old" concrete surface lost 40% (i.e., $A_1 = 0.4$) with a half-life of 100 days (i.e., $\tau_1 = 0.27$ yr). An "old" asphalt surface showed no signs of weathering (i.e., $A_1 = 0$). The 1982 study involved the behavior of ^{86}Rb , ^{130}Ru , and ^{44}Ba on asphalt surfaces. The combined results of this studied estimated A_1 to be 0.29 ± 0.18 and τ_1 to be 79 ± 55 days = 0.22 ± 0.15 yr.

Karlberg [40] studied the behavior of post-Chernobyl depositions on impermeable surfaces in Sweden. He provides the following summary for his results:

In general, the different nuclides seem to act in a similar way. The average remaining fraction after 12 months is around 0.4 except for paving stones, where the fraction is 0.8. For ^{103}Ru and $^{110}\text{Ag}^m$ on asphalt, the removal also seems to be less than for the other nuclides. A rough estimate of the remaining fraction and half-life times for 'short' weathering gives 0.3 and 104 days, 0.6 and 105 days, and 0.70 and 100 days for paving stones, asphalt, and concrete, respectively.

Thus, for various impermeable surfaces, Karlberg is observing values for A_1 that range from 0.2 to 0.7 and values for τ_1 that range from 0.27 yr to 0.38 yr. Further, Figure 2 in Karlberg's paper suggests that the corresponding values above a grass-covered area might be in the area of $A_1 = 0.15$ and $\tau_1 < 60$ days = 0.16 yr. The depositions considered by Karlberg involved rain during and after the passage of the plume and before the first measurements were made.

Jacob et al. [41] studied the behavior of post-Chernobyl depositions in southern Bavaria. They provide the following summary of their results:

Surface activities on paved areas have been determined by in situ measurements in Munich after a deposition of radionuclides from Chernobyl by heavy rain. No significant differences were found between asphalt, concrete, and granite pavements. In the first few days, about 50-70% of the caesium was removed by run-off with the depositing rain and by street cleaning. Barium behaved as cesium, about 80% of the ruthenium and about 90% of the iodine were removed. About 70% of the cesium initially retained disappears from the streets and squares with a half-life of about 80 days due to weathering and street cleaning. Cobbled pavement turned out to retain the radionuclides more effectively. In situ measurements on lawns supported the suggestion that the analytical approximation of Gale et al. under-estimates the external exposures from deposited cesium.

Thus, for impermeable surfaces, their results support a value of A_1 in the area of 0.9 and an effective value of τ_1 , which is considerably less than 80 days = 0.22 yr when the effects of early runoff are included. Their statement

with respect to Gale's equation is not entirely correct. In their comparison, they reduced the initial ground concentration by 30% because of infiltration effects. Such a reduction is not generally done when Gale's equation is used, and if this reduction had been omitted, use of Gale's equation would have provided an upper, rather than lower, bound on the external exposure rates observed by the authors.

Additional discussion of the time-dependent decrease in external exposure is given in Appendix C of Ostmeyer and Helton [42].

As can be seen from the studies just discussed, there exists considerable variation in the parameters associated with the Equation 2.7. This variation is due to many factors, including type of deposition surface, method of deposition, and the action of weather and other processes subsequent to deposition. Further, the uncertainty in these parameters for use in MACCS is compounded by the fact that consequence calculations involve both wet and dry deposition, weathering over a long time period, and environments that are a mixture of many different types of surfaces. With the preceding in mind, it was decided to pick values and ranges for use in MACCS that are representative of the observed values but do not allow any sort of rigorous statistical interpretation. Specifically, the following values are selected:

Table 2.11. MACCS Weathering Values

<u>Parameter</u>	<u>Value</u>	<u>Range</u>	<u>Distribution</u>
n	2		
A ₁	0.5	0.25-0.75	uniform
τ_1	0.5 yr	0.25-0.75	uniform
A ₂	1-A ₁		
τ_2	90 yr	45-135	uniform

In picking the preceding values, observed results for permeable surfaces (i.e., grass) were weighted more heavily than those for impermeable surfaces, since permeable surface area typically exceeds impermeable surface area (including in most urban and suburban areas). Because the half-lives of the radionuclides involved in external exposure calculations are relatively short (i.e., ≤ 30 yr), the parameter τ_2 is not very important.

2.8 Runoff and Washoff

2.8.1 Summary

Table 2.12 summarizes the base values and ranges for the variables for surface-water contamination.

Table 2.12. Base Value and Range for Variables Associated with Surface-Water Contamination

<u>Variable</u>	<u>Summary</u>
NUMWP	Number of radionuclides to be considered in the drinking-water pathway. <u>Base Value</u> : 4.
NAMWPI	Names of radionuclides to be considered in the drinking-water pathway. <u>Selected Radionuclides</u> : ^{89}Sr , ^{90}Sr , ^{134}Cs , ^{137}Cs .
WSHFRI1	Initial radionuclide wash-off fraction for ^{89}Sr . <u>Base Value</u> : 0.01. <u>Range</u> : 0.002 to 0.02. <u>Sampling Distribution</u> : Log Uniform.
WSHFRI2	Same variable as WSHFRI1 (but for ^{90}Sr).
WSHFRI3	Initial radionuclide wash-off fraction for ^{134}Cs . <u>Base Value</u> : 0.005. <u>Range</u> : 0.001 to 0.01. <u>Sampling Distribution</u> : Log Uniform.
WSHFRI4	Same variable as WSHFRI3 (but for ^{137}Cs).
WSHRTA1	Rate constant (yr^{-1}) for long-term wash-off for ^{89}Sr . <u>Base Value</u> : 0.004. <u>Range</u> : 0.0008 to 0.008. <u>Sampling Distribution</u> : Log Uniform.
WSHRTA2	Same variable as WSHRTA1 (but for ^{90}Sr).
WSHRTA3	Rate constant (yr^{-1}) for long-term wash-off for ^{134}Cs . <u>Base Value</u> : 0.001. <u>Range</u> : 0.0002 to 0.002. <u>Sampling Distribution</u> : Log Uniform.
WSHRTA4	Same variable as WSHRTA3 (but for ^{137}Cs).

Table 2.12. (cont'd)

Variable	Summary
WINGF1	Water ingestion factor for ^{89}Sr . <u>For Rivers</u> : Base value: 5×10^{-6} . Range: 1×10^{-6} to 1×10^{-5} . Sampling Distribution: Log Uniform. <u>For Large Lakes</u> : Base Value: 2×10^{-7} . Range: 1×10^{-7} to 1×10^{-6} . Sampling Distribution: Log Uniform.
WINGF2	Water ingestion factor for ^{90}Sr . <u>For Rivers</u> : Same variable as WINGF1. <u>For Large Lakes</u> : Base Value: 2×10^{-5} . Range: 1×10^{-5} to 1×10^{-4} . Sampling Distribution: Log Uniform.
WINGF3	Water ingestion factor ^{134}Cs . <u>For Rivers</u> : Base Value: 5×10^{-6} . Range: 1×10^{-6} to 1×10^{-5} . Sampling Distribution: Log Uniform. <u>For Large Lakes</u> : Base value: 2×10^{-6} . Range: 1×10^{-6} to 1×10^{-5} . Sampling Distribution: Log Uniform.
WINGF4	Water ingestion factor for ^{137}Cs . <u>For Rivers</u> : Same variable as WINGF3. <u>For Large Lakes</u> : Base Value: 4×10^{-6} . Range: 2×10^{-6} to 2×10^{-5} . Take as twice WINGF3 for lakes.

2.8.2 Rationale

The radionuclide wash-off model in MACCS is based on the relationship

$$dx/dt = -(\lambda + \lambda_b) x, \quad x(0) = (1 - \lambda_a) x_0 \quad (2.10)$$

where

$x(t)$ = amount (bq) of a radionuclide on land surfaces at time t (yr) after an initial deposition at time $t = 0$,

λ = decay constant (yr^{-1}) for radionuclide,

λ_a = fraction of initial radionuclide deposition that moves from land surfaces to surface-water bodies in a short time period after deposition,

λ_b = rate constant (yr^{-1}) for the long-term movement of the radionuclide from land surfaces to surface-water bodies, and

x_0 = initial radionuclide deposition (bq) on land surfaces.

The quantities λ_a and λ_b are the MACCS input variables WSHFRI and WSHRTA. The quantity x_0 is defined by

$$x_0 = \text{TOTDEP} * \text{FRACLD} \quad (2.11)$$

where

TOTDEP = total deposition (bq) predicted by MACCS for the radionuclide in the region under consideration and

FRACLD = fraction of region under consideration that is land; the remaining fraction $1 - \text{FRACLD}$ is assumed to be covered by surface-water bodies.

A single value can be used for FRACLD in a MACCS analysis or FRACLD can be specified for individual grid elements through the use of a Site Data File.

The amount of radionuclide moving from land surfaces to surface-water bodies is given by

$$\begin{aligned} D_1 &= \lambda_a x_0 + \int_0^{\infty} \lambda_b x(t) dt \\ &= (\lambda_a \lambda + \lambda_b) x_0 / (\lambda + \lambda_b) \end{aligned} \quad (2.12)$$

Further, the total deposition directly onto surface-water bodies is given by

$$D_2 = \text{TOTDEP} (1 - \text{FRACLD}) \quad (2.13)$$

Thus, the total amount of a radionuclide entering a surface-water system is given by

$$\text{DTOT} = D_1 + D_2 \quad (2.14)$$

The quantity in Equation 2.14 is then used to determine radionuclide consumption due to water ingestion.

For a given surface-water system, it is assumed that a constant fraction of a radionuclide entering the system will be ultimately consumed via the drinking-water pathway. This fraction is defined by the ratio

$$\text{WINGF} = \text{PTOT} / \text{DTOT} \quad (2.15)$$

where PTOT is the total amount (bq) of radionuclide consumed by the population via the surface-water pathway and DTOT is the total amount of radionuclide entering the surface-water system under consideration (see Equation 2.14).

Some type of analysis/modeling is required to define WINGF. This effort could range from the use of empirical data or simple compartment models to the development/application of quite sophisticated models for surface-water systems and their associated public water supply systems. However, in deciding on the amount of effort to invest in determining WINGF, it should be

kept in mind that the surface-water pathway is probably a small contributor to the total cancer risk from chronic exposure pathways [12,43].

We are interested in values for λ_a = WSHFRI, λ_b = WSHRTA, and WINGF. The quantities λ_a and λ_b are considered first. Table 2.13, which is taken from Helton et al. [12], provides a number of observed values for these quantities. Additional values are given in Table 2.14.

Helton et al. [12] concluded that only four radionuclides, ^{89}Sr , ^{90}Sr , ^{134}Cs , and ^{137}Cs , are needed to treat contamination of surface-water bodies. Based on the values for WSHFRI (λ_a) and WSHRTA (λ_b) in Tables 2.14 and 2.15 the following values are recommended for these variables and those nuclides:

Table 2.13. Values for WSHFRI (λ_a) and WSRTH (λ_b)

Isotope	WSHFRI (Range)	WSHRTA (Range)
^{89}Sr	0.01 (0.002 to 0.02)	0.004 (0.0008 to 0.008)
^{90}Sr	0.01 (0.002 to 0.02)	0.004 (0.0008 to 0.008)
^{134}Cs	0.005 (0.001 to 0.01)	0.001 (0.0002 to 0.002)
^{137}Cs	0.005 (0.001 to 0.01)	0.001 (0.0002 to 0.002)

* Considerable subjective judgment was used in selecting these values and ranges.

The development of values for WINGF is now considered. Helton et al. [12] present an exploratory study of the health effects of radionuclide wash-off into surface-water bodies. In that study of wash-off into river systems, WINGF is in effect defined by

$$\text{WINGF} = \text{WT} * \text{WC} * \text{POP} / \text{D} \quad (2.16)$$

where

WT = water treatment factor (i.e., the ratio of radionuclide concentration in water after water treatment to the concentration in water before treatment),

WC = individual water consumption ($\ell/\text{yr-ind}$),

POP = number of individuals obtaining drinking water from the river under consideration (ind), and

D = river discharge (ℓ/yr)

Two river systems were considered in Reference [12]: the lower Mississippi and Rhein-Meuse. Values for WINGF are now calculated using Equation 2.16 and parameter values taken from Reference [12].

Table 2.14. Removal Rates for Fallout Radionuclides Determined on a Regional Basis (Reference[12], Table 1).

Ref.	Nuclide	100 λ_a	100 λ_b	Location	Comment
Straub et al. [44]	^{90}Sr	1.7*		Continental United States	Three month period
	B-emitters	1.6		Continental United States	Nine month period
	^{90}Sr	3.9-12.2		Five watersheds in Ohio Valley	Three month period
*The values for λ_a may be overestimated as λ_a is defined by $\lambda_a=R/D$, where R and D are the removal in surface water and total deposition, respectively, for each time period considered. No credit is taken for removal of accumulated fallout.					
Miyake and Tsubota [45]	^{90}Sr		0.7-3.3	Ten watersheds in Japan	Mean value for ^{90}Sr is 1.5. Value for ^{137}Cs is estimated as that due to direct deposition on water bodies.
	^{137}Cs	1.7			
Yamagata et al. [46]	^{90}Sr	7.2	0.31	Japan	1 month period for λ_a
	^{137}Cs	1.3	0.06		
Jacobi et al. [47]	B-emitters	0.20-1.05	0.12-0.97	Twenty watersheds in West Germany	1 month period for λ_a . Extensive Study.
Jordan et al. [48,49]	^{90}Sr		0.036	Tropical rain forest, Puerto Rico	Derives λ_b for stable Sr and uses to predict behavior of ^{90}Sr .
Kamada et al. [50]	^{90}Sr		0.2-2*	Three watersheds in Japan	
*The values for λ_b may be overestimated as λ_b is defined by $\lambda_b=R/D$, where R and D are the annual radionuclide removal to surface water and total accumulated deposition, respectively.					
Miyake et al. [51]	^{239}Pu		0.12	Japan	
Kamada et al. [52]	^{90}Sr		0.2-2	Four watersheds in Japan	
Menzel [53]	^{90}Sr	0.59-2.17	0.17-0.75	Eight regions in United States	Two month period for λ_a . Extensive investigation.
Simpson et al. [54]	^{137}Cs		0.1	Hudson River watershed	
Carlsson [55]	^{137}Cs	1.9	0.56	Small watershed in Sweden	
Sprugel and Bartelt [56]	$^{239,240}\text{Pu}$		0.05	Ohio	
Aarkrog [57]	^{90}Sr	0.5	0.1	Denmark	Extensive investigation.
Linsley et al. [58]	^{90}Sr	10	1	Upland lake water supplies, England	^{90}Sr model for upland lake water slightly different from (2.1).
	^{90}Sr	1	0.067	River Thames, England	
	^{137}Cs	0.1	0.0067	River Thames, England	

Table 2.15. Additional Removal Rates for Radionuclides Determined on a Regional Basis

Ref.	Nuclide	100 λ_a	100 λ_b	Comment
[59,60]	^{137}Cs ^{131}I , ^{132}Te , ^{103}Ru	1 4-10		Northern Switzerland and southern Germany in first few weeks following depositions from the Chernobyl accident
[61]	^{137}Cs ^{239}Pu , ^{240}Pu ^{241}Am		0.02 0.02 0.02	Fallout in the Columbia River basin
[62]	^7Be ^{137}Cs ^{210}Pb	0.6-2.3	0.1 0.1	Alpine Rhone watershed in Switzerland. Suggests that value of λ_a for ^7Be may also be appropriate for Cs and Pb.
[63]	^{239}Pu , ^{240}Pu		0.4	Mississippi drainage basin
[64]	^{210}Pb		0.05	Susquehanna river system
[65]	Pu		0.002-0.08	Modeling study for the continental United States based on the universal soil loss equations

Mississippi for Sr

$$\begin{aligned} \text{WINGF} &= (0.87) (370 \text{ l/yr-ind}) (2.9\text{E}6 \text{ ind}) / (5.7 \times 10^{14} \text{ l/yr}) \\ &= 1.6 \times 10^{-6} \end{aligned} \quad (2.17)$$

Mississippi for Cs

$$\begin{aligned} \text{WINGF} &= (0.53) (370 \text{ l/yr-ind}) (2.9\text{E}6 \text{ ind}) / (5.7 \times 10^{14} \text{ l/yr}) \\ &= 1.0 \times 10^{-6} \end{aligned} \quad (2.18)$$

Rhein-Meuse for Sr

$$\begin{aligned} \text{WINGF} &= (1.0) (440 \text{ l/yr-ind}) (1.3\text{E}7 \text{ ind}) / (8.5 \times 10^{13} \text{ l/yr}) \\ &= 6.7 \times 10^{-5} \end{aligned} \quad (2.19)$$

Rhein-Meuse for Cs

$$\begin{aligned} \text{WINGF} &= (0.1) (440 \text{ l/yr-ind}) (1.3 \times 10^7 \text{ ind}) / (8.5 \times 10^{13} \text{ l/yr}) \\ &= 6.7 \times 10^{-6} \end{aligned} \quad (2.20)$$

Helton et al. [12] also considered the effects of a deposition onto Lake Michigan. The model used in this part of the analysis is equivalent to defining WINGF by

$$\begin{aligned} \text{WINGF} &= \left(\int_0^{\infty} e^{-\lambda t} dt / V \right) * \text{WT} * \text{WC} * \text{POP} \\ &= \frac{\text{WT} * \text{WC} * \text{POP}}{\lambda * V} \end{aligned} \quad (2.21)$$

where V is the volume (l) of the lake, λ is the rate constant (yr^{-1}) for removal from the lake (including radioactive decay, sedimentation, and outflow), and WT, WC, and POP are the same as in Equation 2.16. In turn, λ is defined by

$$\lambda = \ln(2) / \text{HL} \quad (2.22)$$

where HL is the effective half-life (yr) for the radionuclide under consideration. When Equation 2.21 and Equation 2.23 are combined, the following relationship is obtained:

$$\text{WINGF} = \frac{\text{HL} * \text{WT} * \text{WC} * \text{POP}}{\ln(2) * V} \quad (2.23)$$

Equation 2.14 and the data in Helton et al. [12] can now be used to estimate WINGF for a release to Lake Michigan.

Lake Michigan for ^{89}Sr

$$\begin{aligned} \text{WINGF} &= \frac{(0.14 \text{ yr}) (1.0) (370 \text{ l/yr-ind}) (1.0 \times 10^7 \text{ ind})}{\ln(2) * (4.87 \times 10^{15} \text{ l})} \\ &= 1.7 \times 10^{-7} \end{aligned} \quad (2.24)$$

Lake Michigan for ^{90}Sr

$$\begin{aligned} \text{WINGF} &= \frac{(15.4 \text{ yr}) (1.0) (370 \text{ l/yr-ind}) (1.1 \times 10^7 \text{ ind})}{\ln(2) * (4.8 \times 10^{15} \text{ l})} \\ &= 1.9 \times 10^{-5} \end{aligned} \quad (2.25)$$

Lake Michigan for ^{134}Cs

$$\begin{aligned} \text{WINGF} &= \frac{(0.13 \text{ yr}) (1.0) (370 \text{ l/yr-ind}) (1.1 \times 10^7 \text{ ind})}{\ln(2) * (4.87 \times 10^{15} \text{ l})} \\ &= 1.6 \times 10^{-6} \end{aligned} \quad (2.26)$$

Lake Michigan for ^{137}Cs

$$\begin{aligned} \text{WINGF} &= \frac{(3.5 \text{ yr}) (1.0) (370 \text{ l/yr-ind}) (1.1 \times 10^7 \text{ ind})}{\ln(2) * (4.87 \times 10^{15} \text{ l})} \\ &= 4.2 \times 10^{-5} \end{aligned} \quad (2.27)$$

Two additional, very crude calculations are now given for WINGF. The first uses Equation 2.16 and data for the entire United States. Specifically, the following data are used:

WT = 0.87 for Sr, 0.53 for Cs (same as used in Helton et al. [12],

WC = 370 l/yr-ind,

POP = 2.4×10^8 ind * 0.718 = 1.7×10^8 ind, where 2.4×10^8 ind is the population of the United States (Statistical Abstract of the United States 1988) and 0.718 is an approximation of the fraction of the total United States population that receives its water from surface-water bodies (Ref. [66], Table 6-39, p. 345), and

D = $(1,500 \times 10^6 \text{ acre ft/yr}) (1.234 \times 10^6 \text{ l/acre ft}) = 1.9 \times 10^{15} \text{ l/yr}$, where $1,500 \times 10^6$ is the annual discharge of rivers in the conterminous United States (Ref. [66], Table 2-2, p. 61).

Then the following approximations to WINGF are obtained:

Rivers in Conterminous United States for Sr

$$\begin{aligned} \text{WINGF} &= (0.87) (370 \text{ l/yr-ind}) (1.7 \times 10^8 \text{ ind}) / (1.9 \times 10^{15} \text{ l/yr}) \\ &= 2.9 \times 10^{-5} \end{aligned} \quad (2.28)$$

Rivers in Conterminous United States for Cs

$$\begin{aligned} \text{WINGF} &= (0.53) (370 \text{ l/yr-ind}) (1.7 \times 10^8 \text{ ind}) / (1.9 \times 10^{15} \text{ l/yr}) \\ &= 1.8 \times 10^{-5} \end{aligned} \quad (2.29)$$

The second calculation uses Equation 2.2 and the data for the entire United States. Specifically, the following variable values are assumed:

$$\text{WT} = 1 \text{ for Sr and Cs,}$$

$$\text{WC} = 370 \text{ l/yr-ind,}$$

$$\text{POP} = 1.7 \times 10^8 \text{ ind,}$$

$$\begin{aligned} \text{V} &= 4,500 \text{ mi}^3 * 3.38 \times 10^6 \text{ acre ft/mi}^3 * 1.234 \times 10^6 \text{ l/acre ft} \\ &= 1.9 \times 10^{16} \text{ l, where 4500 mi}^3 \text{ is the volume of freshwater lakes in} \\ &\quad \text{the conterminous United States (Ref. [66], Table 2-2, p. 61), and} \end{aligned}$$

$$\begin{aligned} \text{HL} &= 0.14 \text{ yr for } ^{89}\text{Sr}, 15.4 \text{ yr for } ^{90}\text{Sr}, 1.3 \text{ yr for } ^{134}\text{Cs}, 3.5 \text{ yr for } \\ &\quad ^{137}\text{Cs, where these are the values obtained in Helton et al. [12]} \\ &\quad \text{for Lake Michigan (values for smaller and/or other lakes could be} \\ &\quad \text{quite different; e.g., see Santschi et al. [59].} \end{aligned}$$

Then, the following approximations to WINGF are obtained:

Lakes in Conterminous United States for ^{89}Sr

$$\begin{aligned} \text{WINGF} &= \frac{(0.14 \text{ yr}) (1.0) (370 \text{ l/yr-ind}) (1.7 \times 10^8 \text{ ind})}{\ln(2) (1.9 \times 10^{16} \text{ l})} \\ &= 6.7 \times 10^{-7} \end{aligned} \quad (2.30)$$

Lakes in Conterminous United States for ^{90}Sr

$$\begin{aligned} \text{WINGF} &= \frac{(15.4 \text{ yr}) (1.0) (370 \text{ l/yr-ind}) (1.7 \times 10^8 \text{ ind})}{\ln(2) (1.9 \times 10^{16} \text{ l})} \\ &= 7.4 \times 10^{-5} \end{aligned} \quad (2.31)$$

Lakes in Conterminous United States for ^{134}Cs

$$\begin{aligned} \text{WINGF} &= \frac{(1.3 \text{ yr}) (1.0) (370 \text{ l/yr-ind}) (1.7 \times 10^8 \text{ ind})}{\ln(2) (1.9 \times 10^{16} \text{ l})} \\ &= 6.2 \times 10^{-6} \end{aligned} \quad (2.32)$$

Lakes in Conterminous United States for ^{137}Cs

$$\begin{aligned}\text{WINGF} &= \frac{(3.5 \text{ yr}) (1.0) (370 \text{ l/yr-ind}) (1.1 \times 10^7 \text{ ind})}{\ln(2) (1.9 \times 10^{16} \text{ l})} \\ &= 1.7 \times 10^{-5}\end{aligned}\quad (2.33)$$

Several simplistic calculations for WINGF have been given. These calculations are intended to provide only a ballpark estimate of the value of WINGF. The recommendations in Table 2.16 for WINGF are suggested for preliminary assessments of the drinking water pathway:

Table 2.16. Values for WINGF

Isotope	River (Range)	Lake (Range)
^{89}Sr	5×10^{-6} (1×10^{-6} - 1×10^{-5})	2×10^{-7} (1×10^{-7} - 1×10^{-6})
^{90}Sr	5×10^{-6} (1×10^{-6} - 1×10^{-5})	2×10^{-5} (1×10^{-5} - 1×10^{-4})
^{134}Cs	5×10^{-6} (1×10^{-6} - 1×10^{-5})	2×10^{-6} (1×10^{-6} - 1×10^{-5})
^{137}Cs	5×10^{-6} (1×10^{-6} - 1×10^{-5})	4×10^{-6} (2×10^{-6} - 2×10^{-5})

The values recommended here for "River" systems are somewhat lower than the screening estimates for WINGF because those calculations probably underestimated effects due to binding to sediments. The values for "Lake" are those obtained for Lake Michigan and they should be used only for a very large lake. The ranges are subjective estimates and are intended to be sampled with a log-uniform distribution.

Note: Although it was obtained too late to use in the development of the parameters presented here, a useful source of information on water use in the United States is Estimated Use of Water in the United States in 1985 by W. B. Solley, C. F. Merk, and R. R. Pierce (USGS Circular 1004, 1988).

2.9 Resuspension

2.9.1 Summary

Table 2.17 summarizes the base values and ranges for the variables for resuspension.

Table 2.17 Base Values and Ranges for Resuspension Variables

Variable	Summary
NRWTRM	Number of resuspension processes under consideration. <u>Base Value</u> : 3.
RWCOEF1	Resuspension coefficient for short term resuspension (m^{-1}). <u>Base Value</u> : 10^{-5} . <u>Range</u> : 10^{-6} - 10^{-4} . <u>Sampling Distribution</u> : Log Uniform. Rank correlation of 1 with RWCOEF2 and RWCOEF3; rank correlation of -0.75 with TRWHLH1, TRWHLH2 and TRWHLH3.
RWCOEF2	Resuspension coefficient for intermediate term resuspension (m^{-1}). <u>Base Value</u> : 10^{-7} . <u>Range</u> : 10^{-8} - 10^{-6} . <u>Sampling Distribution</u> : Log uniform. Correlation same as for RWCOEF1.
RWCOEF3	Resuspension coefficient for long term resuspension (m^{-1}). <u>Base Value</u> : 10^{-9} . <u>Range</u> : 10^{-8} - 10^{-10} . <u>Sampling Distribution</u> : Log uniform. Correlations same as for RWCOEF1.
TRWHLF1	Half-life (s) for resuspension coefficient RWCOEF1. <u>Base Value</u> : 1.6×10^7 (~6 mn). <u>Range</u> : 2.6×10^6 - 3.1×10^7 (~ 1-12 mn). <u>Sampling Distribution</u> : Log uniform. Rank correlation of 1 with TRWHLF2 and TRWHLF3; rank correlation of -0.75 with RWCOEF1, RWCOEF2 and RWCOEF3.
TRWHLF2	Half-life (s) for resuspension coefficient RWCOEF2. <u>Base Value</u> : 1.6×10^8 (~ 5 yr). <u>Range</u> : 3.1×10^7 - 3.1×10^8 (~ 1-10 yr). <u>Sampling Distribution</u> : Log uniform. Correlations same as for TRWHLF1.
TRWHLF3	Half-life (s) for resuspension coefficient RWCOEF3. <u>Base Value</u> : 1.6×10^9 (~50 yr). <u>Range</u> : 3.1×10^8 - 3.1×10^9 (~10-100 yr). <u>Sampling Distribution</u> : Log uniform. Correlations same as for TRWHLF1.

Comment: Since RWCOEF1, RWCOEF2, and RWCOEF3 are assumed to have a rank correlation of 1, a single variable can be sampled as a surrogate for all three. The same applies to TRWHLF1, TRWHLF2, and TRWHLF3. Thus, it is necessary to sample only two variables to implement these six variables.

2.9.2 Rationale

The resuspension model in MACCS is based on the resuspension factor approach. The resuspension factor $K(t)(m^{-1})$ is defined by

$$K(t) = a(t)/s(t) \quad (2.34)$$

where

$a(t)$ = air concentration (Bq/m^3) of resuspended activity at time t after an initial deposition and

$s(t)$ = initial surface deposition (Bq/m^2) corrected for radioactive decay.

Additional discussion is available in a number of reviews [10,42,67,68,69].

In MACCS, $K(t)$ is defined by

$$K(t) = \sum_{i=1}^n K_i \exp(-\lambda_i t) \quad (2.35)$$

where

n = NRWTRM = number of resuspension processes under consideration (e.g., short-term, intermediate-term, and long-term resuspension),

K_i = RWCOEF(i) = resuspension factor (m^{-1}) for the i th resuspension process, and

λ_i = $\ln(2)/\tau_i$ = rate constant (s^{-1}) for the time-dependent reduction in resuspension factor K_i

where

τ_i = TRWHLF(i) = resuspension half-life (s) (i.e., the time period over which the observed air concentration will decrease by 50%).

An excellent review of the data on resuspension is given by Sehmel [10]. As indicated by both the data in this review and statements by the author, there is great uncertainty in characterizing resuspension. For the resuspension model in MACCS, the data in Tables 12.7 and 12.9 of Sehmel will be used to characterize resuspension factors (i.e., the K_i in Equation 2.35). Further, the data in Table 12.8 of Sehmel will be used for guidance with respect to the rate constant λ_i .

Three time periods (i.e., $n=3$) will be considered in the definition of the resuspension factors: short term (i.e., K_1), intermediate term (i.e., K_2), and long term (i.e., K_3). The short-term and intermediate-term resuspension is assumed to correspond to the larger and intermediate sized factors in Sehmel, Table 12.9. The long-term resuspension corresponds to the values in Sehmel, Table 12.7 and the smaller to values in Sehmel, Table 12.9. Short-,

intermediate-, and long-term resuspension is intended to correspond respectively to resuspension which takes place over a few months, a few years, and a few tens of years after deposition.

Table 2.18 shows the values selected for the K_i and the τ_i .

Table 2.18. Values for K_i and τ_i

<u>Variable</u>	<u>Base Value</u>	<u>Range</u>	<u>Comment</u>
K_1	10^{-5}	$10^{-6} - 10^{-4}$	
τ_1	6 mon	1 - 12 mn	1 mon = 2.6×10^6 s
K_2	10^{-7}	$10^{-8} - 10^{-6}$	
τ_2	5 yr	1-10 yr	1 yr = 3.1×10^7 s
K_3	10^{-9}	$10^{-10} - 10^{-8}$	
τ_3	50 yr	10-100 yr	1 yr = 3.1×10^7 s

Although the values in Table 2.18 are not inconsistent with the available data, it must be recognized that these quantities are very uncertain.

Changes in environmental conditions are expected to have inverse effects on corresponding values of K_i and τ_i , but very similar effects on the set of K_i values, and also on the set of τ_i values. Thus, for sampling purposes, all values of K_i should be assumed to be strongly correlated (e.g., rank correlation of 1), all values of τ_i should be assumed to be strongly correlated (e.g., rank correlation of 1), and corresponding values of K_i and τ_i should be assumed to have a moderately strong, negative rank correlation (e.g., -0.75).

For comparison, values for K_i and τ_i used in the Reactor Safety Study (i.e., WASH-1400) and suggested in the review by Lassey [67] are listed in Tables 2.19 and 2.20.

Table 2.19. Values in Reactor Safety Study [11]

<u>Variable</u>	<u>Value</u>
K_1	10^{-5}
τ_1	1 yr
K_2	10^{-9}
τ_2	no decrease with time

Table 2.20. Values in Lassey [67]

<u>Variable</u>	<u>Value</u>
K_1	9×10^{-5}
τ_1	1.4 mn
K_2	1×10^{-5}
τ_2	1 yr
K_3	10^{-9}
τ_3	no decrease with time

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3. EMERGENCY RESPONSE PARAMETERS

3.1 Evacuation Parameters

3.1.1 Recommendation

The values in Table 3.1 for evacuation parameters are recommended for the MACCS NUREG-1150 calculations.

Table 3.1. Recommended Evacuation Parameter Values

<u>Variable</u>	<u>(Units)</u>	<u>Definition</u>	<u>Site</u>	<u>Value</u>	<u>Range^a</u>
EDELAY	(h)	Evacuation Delay Time	Sur	1.5	1.25 - 3.25
			GG	0.75	0.25 - 1.25
			PB	1.0	0.7 - 1.7
			Seq	1.8	0.5 - 2.0
ESPEED	(m s ⁻¹)	Radial Evacuation Speed	Sur	1.8	0.9 - 3.6
			GG	3.7	1.7 - 4.5
			PB	4.8	2.8 - 6.8
			Seq	1.8	1.2 - 6.7

^a All sampling distributions should be uniform over the stated ranges.

3.1.2 Data Sources

During 1985, NUS conducted a review for SNL of emergency response plans and estimates of evacuation times prepared for the utilities that run the five NUREG-1150 reactors (Surry, Grand Gulf, Sequoyah, Peach Bottom, and Zion) and, as was appropriate, discussed emergency response assumptions (e.g., evacuation delay period and average evacuation speed) with utility emergency response personnel. NUS submitted the results of this study to SNL in letter reports to which were appended copies of pertinent documentation (e.g., the utility studies of estimated Emergency Protection Zone [EPZ] clearance times) from which the data in the letter reports had been taken. The data presented here were drawn from the NUS reports and supporting documentation.

3.1.3 Surry

The Surry reactor is located on the south side of the James River. On the south side of the river within ten miles of the reactor (i.e., within the EPZ), population densities are low. However, on the north side of the river on the peninsula defined by the James and York rivers, population densities are high because of the presence of three cities: Williamsburg, Newport News, and Hampton. Should a severe accident ever occur at the Surry reactor, evacuation of this peninsula could be difficult because of the high population densities and because only two arteries (I64 and US60) are available to support the evacuation.

Table 3.2 presents EPZ populations for the five counties that neighbor the Surry site and estimates of preevacuation delay periods and average evacuation speeds for a Summer Sunday, a Winter Weekday, and Adverse Weather (winter ice storms).

Table 3.2. Surry Emergency Response Data

<u>County/Location</u>	<u>EPZ Pop (x10⁻³)</u>	<u>Summer Sunday</u>		<u>Winter Weekday</u>		<u>Adverse Weather</u>	
		<u>Delay (h)</u>	<u>Speed (mph)</u>	<u>Delay (h)</u>	<u>Speed (mph)</u>	<u>Delay (h)</u>	<u>Speed (mph)</u>
James City	16.5	3.25	4.0			1.25	1.6
Williamsburgh	11.6	2.25	5.7			1.25	2.2
York	8.6	1.25	4.4			1.25	2.5
Newport News	45.3	2.25	3.0			1.25	1.7
Surry/Isle of Wight	4.5	1.25	8.0			1.25	8.0
Total (Population weighted)	86.5	2.3	4.0			1.25	2.2
N of River	82.0	1.25	2.4	1.25	2.7	1.25	1.8
S of River	4.5	1.25	8.0	1.25	8.0	1.25	8.0
Total (Population weighted)	86.5	1.25	2.7	1.25	3.0	1.25	2.1

The population-weighted results for the five counties are probably superior to the population-weighted results for the data for North and South of the river. However, if the county data are used, estimates of the preevacuation delay period and average speed for a Winter Weekday must be developed that are consistent with the county data for a Summer Sunday and Adverse Weather.

The NUS study states that delays in excess of 1.25 h are expected only during the tourist season (summer months). Thus, a preevacuation delay period of 1.25 h should apply to Winter Weekdays, which agrees with the NUS estimates for delays N and S of the river on Winter Weekdays.

The NUS average speed of 3.0 mph estimated from the data for N and S of the river is inconsistent with the population weighted aggregate county data, since the average evacuation speed for the Winter Weekday (3.0 mph) estimated from the data for N and S of the river is lower than the average speed for a Summer Sunday (4.0 mph) estimated from the county data. If the Summer Sunday 4.0 mph speed derived from county data is scaled by the ratio of the Winter Weekday speed (3.0 mph) to the Summer Sunday speed (2.7 mph) developed from the N and S of the river data, then an average evacuation speed of 4.4 mph results.

Two-sevenths of the year are weekend days, and the summer tourist season is about four months long. Therefore, assume that Summer Sunday values apply 30 percent of the time.

$$0.3 = 0.5(2/7 + 4/12)$$

On the coast of Virginia, during the winter (December 21 through March 21) precipitation occurs about 8 percent of the time. If precipitation during the winter is assumed to mean that a severe ice storm has occurred, then during a full year at Surry, adverse weather will occur about 2 percent of the time. Finally, by difference, Winter Weekday values will apply 68 percent of the time.

Yearly average values for the preevacuation delay time and the average evacuation speed at the Surry site may now be estimated using the following equation:

$$0.3 S + 0.68 W + 0.02 A = \bar{X} \quad (3.1)$$

Table 3.3 presents the yearly average values obtained using this equation.

Table 3.3. Surry Evacuation Parameter Values Estimated from the Seasons and Time of Week

<u>Parameter</u>	<u>Summer Sunday</u>	<u>Winter Weekday</u>	<u>Adverse Weather</u>	<u>Yearly Average</u>
Delay (h)	2.3	1.25	1.25	1.57
Speed (mph)	4.0	4.4	2.2	4.24

Average evacuation speeds for the Surry EPZ can be estimated in at least two other ways. From a map of the peninsula near Williamsburg, one can estimate the following maximum travel distances within the EPZ for population located on the peninsula: maximum travel distance to I64 = 7 mi; and the maximum travel distance on I64 = 5 mi. Therefore, the average evacuation distance within the EPZ is about 6.0 mi = $(1/2)(7 + 5)$. The Surry "Estimation of Evacuation Times" report prepared by PRC Voorhees gives clear time distributions for a Summer Sunday and a Winter Weekday. The distributions show that 50% of the population in the EPZ will be ready to evacuate in 1.0 h and will have cleared the EPZ in 2.6 h. Their average evacuation time is therefore 1.6 h, and their average speed is 3.75 mph = 6.0 mi/1.6 h.

The PRC Voorhees report also presents vehicle capacities (vehicles per hour) for the roads that will be used to exit the EPZ for the counties that neighbor the Surry site, and for the number of vehicles available to support the evacuation in each county. From the number of vehicles available and the total EPZ population of each county, one can estimate that the average evacuating vehicle will be occupied by three people. Thus, from the county EPZ populations and vehicle capacities, one can estimate average evacuation times. Table 3.4 presents these estimates:

Table 3.4. Estimation of Surry Evacuation Times from Vehicle Capacities and Populations

County	EPZ Pop (x10-3)	Vehicle Capacity (x10-3)	Evacuation Time (h)
Surry/Wight	4.5	6.0	0.25
James/Williamsburgh	28.1	7.2	1.3
York	8.6	3.6	0.8
Newport News	45.3	9.6	1.6
Population weighted total	86.5		1.4

Since evacuation of the peninsula will determine average evacuation speeds within the EPZ, that speed can be estimated to be 4.29 mph = 6.0 mi/1.4 h, where 6.0 is the maximum travel distance within the EPZ on the peninsula.

Given the preceding results, a pre-evacuation delay period of 1.5 hours and an average evacuation speed of 4.0 mph (1.8 m s^{-1}) are recommended for NUREG-1150 calculations for the Surry site.

Table 3.5 presents the evacuation delay time and evacuation speed recommended for use at the Surry site and compares the recommended values to those specified by the NRC for use in the first pass NUREG-1150 calculations:

Table 3.5. Values Recommended for Surry Evacuation Parameters

	Recommended Value	NRC
Delay (h)	1.5	1.0
Speed (m s^{-1})	1.8	1.2

3.1.4 Grand Gulf

Evacuation time estimates for the Grand Gulf site are based on a state-of-the-art road network analysis. Data for pre-evacuation delay times and EPZ clearance times (delay time plus evacuation time) were developed for Weekdays, Weekend Days/Nights, and Adverse Weather (severe thunderstorms). Table 3.6 presents the evacuation data.

Table 3.6. Evacuation Data for Grand Gulf

Time/Condition	Average ^a		Evacuation		Maximum	Speed (mph)
	Delay Time (min)	Clear Time (min)	Time		Travel Distance (min)	
			(min)	(h)		
Weekday (WD)	45	160	115	1.92	10	5.21
Weekend/Night (WE/N)	45	105	60	1.0	10	10.0
Adverse Weather (A)	45	205	160	2.67	10	3.75

^aDelay times ranged from 15 to 75 minutes, so the average delay time is 45 minutes.

At the Grand Gulf site, precipitation at rates in excess of 0.1 in/h occurs about 2 percent of the time. If rain at rates that exceed 0.1 in/h is assumed to mean that a severe thunderstorm is occurring, then adverse weather will also occur at the Grand Gulf site about 2 percent of the time.

Yearly average pre-evacuation times and average evacuation speeds can be calculated from these data using the following equation:

$$0.02 A + 0.98 [0.5 N + 0.5(0.71 WD + 0.29 WE)] = \bar{X} \quad (3.2)$$

where $0.71 = 2/7$, and $0.29 = 5/7$. Substitution of the evacuation delay times and speeds listed in the preceding table into this equation yields a yearly average evacuation delay time of 45 min = 0.75 h and a yearly average evacuation speed of 8.2 mph = 3.7 m s^{-1} . Table 3.7 presents the evacuation delay time and evacuation speed recommended for use at the Grand Gulf site and compares the recommended values to those specified by the NRC for use in the first pass NUREG-1150 calculations:

Table 3.7. Values Recommended for Grand Gulf and Evacuation Parameters

<u>Parameter</u>	<u>Recommended Value</u>	<u>NRC</u>
Delay (h)	0.75	1.25 ^a
Speed (m s^{-1})	3.7	2.0
^a where 1.25 h = 75 min, the maximum pre-evacuation delay time.		

3.1.4 Peach Bottom

Estimates of total EPZ clearance times and pre-evacuation delay times (expressed in minutes after offsite warning) have been reported by the Philadelphia Electric Company for the five counties (Lancaster, York, Chester, Cecil, and Harford) that neighbor the Peach Bottom site. Values are reported for two types of weather (normal and adverse), two seasons of the year (winter and summer), and two times of day (daytime and nighttime). The estimates were developed using a state-of-the-art road network analysis. Table 3.8 presents estimates of the preevacuation delay time and the evacuation time, where

$$\text{Evacuation Time} = \text{Total EPZ Clearance Time} - \text{Pre-evacuation Delay Time}$$

for each county and set of conditions (prevailing weather, season, time of day). Also presented for each county are the distance to the EPZ boundary and the population within the EPZ.

Table 3.8. Peach Bottom Evacuation Data

	County					Population Weighted Average
	<u>Lancaster</u>	<u>York</u>	<u>Chester</u>	<u>Cecil</u>	<u>Harford</u>	
<u>Population</u>						
(0-12 mi x 10 ⁻³)	19.2	7.9	2.8	4.2	12.9	47.0
<u>Evacuation</u>						
<u>Distance</u> (mi)	13	12	15	12	12	12.6
<u>Daytime</u>						
Normal Weather						
Delay Time	85	80	88	75	80	82
Evacuation Time						
Winter	95	80	75	75	90	88
Summer	95	80	75	75	90	88
Adverse Weather						
Delay Time	100	95	98	85	95	96
Evacuation Time						
Winter	100	105	75	75	95	96
Summer	120	105	75	75	105	107
<u>Nighttime</u>						
Normal Weather						
Delay Time	40	40	53	40	40	41
Evacuation Time						
Winter	50	50	40	40	50	49
Summer	60	50	40	40	60	55
Adverse Weather						
Delay Time	40	40	53	40	40	41
Evacuation Time						
Winter	70	70	50	50	80	70
Summer	90	70	50	50	90	81

Yearly average values of pre-evacuation delay times and evacuation times can be calculated from this data using the following equation:

$$0.05[0.25(SDA + WDA + SNA + WNA)] + 0.95[0.25(SDN + WDN + SNN + WNN)] = \bar{X},$$

where

SDA = summer, daytime, adverse weather
WDA = winter, daytime, adverse weather
SNA = summer, nighttime, adverse weather
WNA = winter, nighttime, adverse weather

SDN = summer, daytime, normal weather
 WDN = winter, daytime, normal weather
 SNN = summer, nighttime, normal weather
 WNN = winter, nighttime, normal weather

and adverse weather (weather that reduces road capacities by 30%, e.g., snow, ice, rain, fog) is assumed to occur 5% of the time (precipitation occurs during about 8.5% of the hours in the year at the Peach Bottom site).

Substitution of the pre-evacuation delay times and evacuation times listed in the preceding table into this equation yields a yearly average preevacuation delay time of 62 min = 1.0 h and a yearly average evacuation time of 71 min = 1.18 h. Since the population weighted straight-line evacuation distance is 12.6 mi, this average evacuation time corresponds to an average evacuation speed of 10.7 mph = 4.8 m s⁻¹.

Table 3.9 presents the evacuation delay time and evacuation speed recommended for the Peach Bottom site and compares the recommended values to those specified by the NRC for use in the first pass NUREG-1150 calculations:

Table 3.9. Values Recommended for Peach Bottom
Evacuation Parameters

<u>Parameter</u>	<u>Recommended Value</u>	<u>NRC</u>
Delay (h)	1.0	1.25
Speed (m s ⁻¹)	4.8	2.0

3.1.5 Sequoyah

Estimates of clear times for the Sequoyah site are presented in the Multijurisdictional Emergency Response Plan prepared for that site by the State of Tennessee. That plan divides population into two groups, residents and transients, where transients are primarily people who visit the river to swim or picnic during summer months (June through September). For each of these population groups, and for both together, the plan estimates clear times for each of 28 sectors within the 10-m EPZ. These clear time estimates are presented in Table 3.10.

Table 3.10. Sequoyah Evacuation Data

Sector	Population		Clear Time (h)					
	Residents	Transients	Residents		Transients		Both	
			Normal	Adverse	Normal	Adverse	Normal	Adverse
A-1	1210	1500	5.25	6.00	2.50	3.25	6.00	6.75
A-2	490	600	5.25	6.00	2.50	3.25	6.00	6.75
A-3	3575		5.25	6.00			6.00	6.75
A-4	660		2.25	3.00			3.00	3.75
A-5	1100		4.25	5.00			5.00	5.75
A-6	1085	1350	3.88	4.63	2.50	3.25	4.63	5.38
B-1	850	2000	2.94	3.69	1.50	2.25	3.69	4.44
B-2	600	1050	2.67	3.42	1.50	2.25	3.42	4.17
B-3	845		2.83	3.58			3.58	4.33
B-4	410	900	2.50	3.25	1.50	2.25	3.25	4.00
B-5	1195		3.17	3.92			3.92	4.67
B-6	160		3.50	4.25			4.25	5.00
B-7	250		2.25	3.00			3.00	3.75
B-8	645		3.50	4.25			4.25	5.00
C-1	1040	750	3.50	4.25	1.50	2.25	4.25	5.00
C-2	1945	3700	3.50	4.25	2.50	3.25	4.25	5.00
C-3	1810		3.00	3.75			3.75	4.25
C-4	750		3.50	4.25			4.25	5.00
C-5	445		2.50	3.25			3.25	4.00
C-6	1670		3.13	3.88			3.88	4.63
C-7	1880	235	3.08	3.83	2.50	3.25	3.83	4.58
C-8	2440	4000	3.50	4.25	2.50	3.25	4.25	5.00
D-1	300	1250	5.25	6.00	2.50	3.25	6.00	6.75
D-2	3585	1500	5.25	6.00	3.88	4.63	6.00	6.75
D-3	3450		4.75	5.50			5.50	6.25
D-4	1650		4.00	4.75			4.75	5.50
D-5	10340		4.50	5.25			5.25	6.00
D-6	2880	5200	5.25	6.00	5.25	6.00	6.00	6.75
<u>Sum</u>	47260	24035						
Population								
<u>Weighted Sum</u>			4.17	4.92			4.90	5.65

The clear time estimates presented in Table 3.10 rest on the following four assumptions:

- (1) Whenever the residential population of the full EPZ is evacuated, the delay between notification to evacuate and the actual start of evacuation is 1.75 h.
- (2) When the full EPZ is evacuated, adverse weather (snow or flooding) lengthens evacuation times by 45 min.
- (3) Clear times for residents are lengthened by 45 m in. whenever the recreational transient population evacuates with the residential population.

(4) Delay times are not lengthened by adverse weather.

At Knoxville, TN, total yearly precipitation averages 47.29 inches and snow (as snow) averages 12.3 inches. Since the density of water is 1.0 g/cm^3 and the density of snow is about 0.1 g/cm^3 , the Knoxville data suggest that about 2.6 percent

$$2.6 = 100[12.3(0.1)/47.49(1.0)]$$

of all precipitation at the Sequoyah site will be snow. At the Sequoyah site, rain occurs during 7 percent of the hours of the year, and intense rain (rain rate greater than 6 mm/h for one h) occurs less than 0.15 percent of the time (during only 13 of 8760 h). If rain at a rate of 6 mm/h is assumed to indicate flooding, then adverse weather (flooding or snowfall) will occur at the Sequoyah site less than 3 percent of the time. Finally, if significant transient population is assumed to be present within the EPZ only on weekend days during the months of June through September, then the fraction of time when both the residential and the transient populations will evacuate together will be $0.1 = (4/12)(2/7)$.

The following equation can now be used to estimate a yearly average clear time for the entire Sequoyah EPZ:

$$f_A(f_R t_{RA} + f_B t_{BA}) + f_N(f_R t_{RN} + f_B t_{BN}) = \bar{X} \quad (3.3)$$

where

f_A = fraction time adverse weather prevails = 0.03,

f_N = fraction time normal weather prevails = 0.97,

f_R = fraction time only residential population evacuates = 0.9,

f_B = fraction time both residential and transient population evacuates = 0.1,

t_{RA} = clear time during adverse weather when only the residential population evacuates = 4.90 h,

t_{BA} = clear time during adverse weather when both the residential and the transient population evacuate = 5.65 h,

t_{RN} = clear time during normal weather when only the residential population evacuates = 4.17 h, and

t_{BN} = clear time during normal weather when both the residential and the transient population evacuates = 4.92 h.

Substitution of the parameter values given above now yields an average clear time of 4.27 hours and thus an average evacuation time of $2.52 \text{ h} = 4.27 \text{ h} - 1.75 \text{ h}$ where 1.75 h is the delay time before evacuation commences.

Accordingly, $3.97 \text{ mph} = 10 \text{ mi}/2.52 \text{ h} = 1.8 \text{ m s}^{-1}$ is a reasonable estimate of average evacuation speeds within the Sequoyah EPZ when the average is taken over all weather conditions and all evacuating populations. Table 3.11

presents the evacuation delay time and evacuation speed recommended for use at the Sequoyah site and compares the recommended values to those specified by the NRC for use in the first pass NUREG-1150 calculations:

Table 3.11. Values Recommended for Sequoyah Evacuation Parameters

<u>Parameter</u>	<u>Recommended Value</u>	<u>NRC</u>
Delay (h)	1.75	1.7
Speed (m s ⁻¹)	1.8	1.2

3.2 Shielding Factors and Breathing Rate

3.2.1 Recommendation

The shielding factor values and breathing rate in Table 3.12 are recommended for use in MACCS NUREG-1150 calculations. In Table 3.12, BRRATE = breathing rate, CSFACT = cloudshine shielding factor, GSFACT = groundshine shielding factor, PROTIN = inhalation protection factor, and SKPFAC = skin protection factor.

Table 3.12. Recommended Shielding Factor Values

<u>Variable</u>	<u>(Units)</u>	<u>Activity</u>	<u>Site</u>	<u>Value</u>	<u>Range*</u>
BRRATE	(liters/day)	All	All	2.3×10^4	$(0.9-2.6) \times 10^4$
CSFACT	(unitless)	Evacuation	All	1.0	n/a
		Normal Activity	All	0.75	0.6-0.95
		Active Sheltering	Zion	0.5	0.4-0.6
			GG	0.7	0.6-0.8
			PB	0.5	0.4-0.6
			Sur	0.6	0.5-0.7
			Seq	0.65	0.55-0.75
GSFACT	(unitless)	Evacuation	All	0.5	0.3-0.7
		Normal Activity	All	0.4	0.2-0.75
		Active Sheltering	Zion	0.1	0.03-0.2
			GG	0.25	0.1-0.4
			PB	0.1	0.02-0.2
			Sur	0.2	0.1-0.3
			Seq	0.2	0.1-0.35
PROTIN	(unitless)	Evacuation	All	1.0	n/a
		Normal Activity	All	0.5	0.15-1.0
		Active Sheltering	All	0.2	0.1-0.4
SKPFAC	(unitless)	Evacuation	All	1.0	n/a
		Normal Activity	All	0.5	0.15-1.0
		Active Sheltering	All	0.2	0.1-0.4

* All sampling distributions should be uniform over the stated ranges.

3.2.2 Discussion

MACCS requires that shielding factors be specified for people evacuating in vehicles (cars, buses), taking shelter in structures (houses, offices, schools), and continuing normal activities either outdoors, in vehicles, or indoors. Because inhalation doses depend on breathing rate, breathing rates must be specified for people who are continuing normal activities, taking shelter, and evacuating. Since indoor concentrations of gas-borne radioactive materials are usually substantially less than outdoor concentrations, MACCS also requires that inhalation and skin protection shielding factors (i.e., indoor/outdoor concentration ratios) be provided.

3.2.2.1 Breathing Rate

Breathing rates depend on activity, sex, and age. Adult men, women, and children, who sleep 8 hours per day and engage in light activity when awake, breathe respectively about 2.3×10^4 , 2.1×10^4 , and 1.5×10^4 liters of air per day [1]. Breathing rates for infants are substantially lower. Heavy activity increases breathing rates by about 50 percent. If fear is assumed not to increase the breathing rates of persons taking shelter or evacuating in vehicles, then the age and sex weighted breathing rate for light activity should be a reasonable number to use for persons responding to an accident. If 80 percent [2] of the population is assumed to be teenagers and adults (light activity breathing rate = 2.8×10^4 liters/day), 17 percent [2] is preteen children (light activity breathing rate = 1.8×10^4 liters/day), and 3 percent [2] is babies (waking breathing rate = 0.6×10^4 liters/day), the average light activity breathing rate is 2.6×10^4 liters/day. Since this value differs little from the daily breathing rate of an adult man (2.3×10^4 liters/day = 2.66×10^{-4} m³/s) typically used in ex-plant consequence calculations, the value for an adult man is selected for use in the NUREG-1150 calculations. For sensitivity studies, this parameter should be varied over the range 0.9×10^4 liters/day (sleeping population) to 2.6×10^4 liters/day (light activity).

3.2.2.2 Inhalation and Skin Protection Factors

Penetration of particulate matter into buildings is usually expressed as the ratio of the indoor particulate concentration to the outdoor concentration. Incomplete penetration lowers indoor inhalation and skin doses. Specifically, the Indoor Dose = (Outdoor Dose) (Indoor/Outdoor Ratio). Thus, the Indoor/Outdoor ratio gives the shielding factor provided by buildings for inhalation and skin exposures.

Indoor/Outdoor ratios of particulate matter in houses and buildings have been determined during several experimental studies [3-7]. These studies show that indoor/outdoor ratios depend strongly on particle size. Table 3.13 summarizes the results of these studies.

Table 3.13. Building Inhalation and Skin Shielding Factors
(Indoor/Outdoor Ratios)

Particle Size Range (μm)	Indoor/Outdoor Ratio	Reference
0.05 - 0.2	0.5	[7]
0.1 - 0.65	0.4	[3]
< 1	0.4	[4]
0.1 - 2	0.6	[6]
0.65 - 20	0.2	[3]
> 1	0.2	[4]
?	0.1 - 0.5	[5]

These data suggest that small particles (0.1 - 1 μm) will have an indoor/outdoor ratio of about 0.5, while large particles (1 - 20 μm) will have indoor/outdoor ratios of about 0.2. Since mass and therefore radioactivity will be concentrated in a distribution's large particles, use of a value smaller than 0.5 is indicated.

Indoor/Outdoor inhalation dose ratios have been calculated by Aldrich for a single compartment subject both to infiltration and ventilation [8]. As derived by Aldrich, this ratio is directly proportional to the fraction of the plume that penetrates the compartment (indoor/outdoor concentration ratio). Using best estimate values for model parameters (including a penetration fraction, indoor/outdoor concentration ratio, of 0.85), Aldrich found this dose ratio to have a value of about 0.6. Use of a penetration fraction of 0.3 would lower Aldrich's indoor/outdoor dose ratio to about 0.2.

Opening windows is observed rapidly to increase indoor/outdoor ratios. If windows are assumed to be open during the summer, then a time weighted summation of an indoor/outdoor ratio of 1.0 for the summer (3 months) and 0.2 for the rest of the year (9 months) yields an average indoor/outdoor ratio of 0.4.

Accordingly, for people in buildings, skin and inhalation protection factors of 0.2 (range 0.1 to 0.4) if actively taking shelter and 0.4 (range 0.1 to 1.0) if continuing normal activity are recommended. For people outdoors and evacuating in vehicles, skin and inhalation protection factors of 1.0 (no significant protection) should be assumed.

3.2.2.3 Reference Doses

External radiation doses to individuals are reduced by materials (e.g., hills, buildings, building walls if indoors) that are between the individual and the radiation source. The reduction, which is usually called the "shielding factor," is defined by the following equation:

$$S = D/D_{\text{ref}} \quad (3.4)$$

where S is the shielding factor, D is the dose received, and D_{ref} is the reference dose, which is the groundshine dose that would be received by an individual standing on a contaminated, completely smooth, infinite plane or

the cloudshine dose that would be received by an individual immersed in a contaminated infinite cloud (the effects of finite cloud dimensions and off-centerline locations on cloudshine doses are treated in MACCS using the semi-infinite cloud correction factor).

3.2.2.4 Outdoor Shielding Factors

People outdoors may be partially shielded from a contaminated cloud by buildings and hills. Since this shielding is likely to be pronounced only for people located in urban street canyons, a cloudshine shielding factor of 1.0 for people outdoors is recommended for use in best estimate MACCS calculations.

People who are outdoors are shielded from contaminated ground not only by buildings and hills but also by the roughness of the contaminated ground surfaces (e.g., dirt, lawns, pavement). The average shielding provided by suburban land will depend on how much of that land is typically devoted to houses, lawns, and pavement. Consider a 2000 ft² house (45 ft²) on a quarter acre (10⁴ ft²) lot fronted by a 3-ft-wide sidewalk and half of a 32-ft-wide road. If the roof of the house has a surface roughness like that of pavement, then the fraction of suburban land devoted to lawns is about 0.67, and the fraction devoted to pavement is about 0.33.

$$0.67 = \frac{(100)^2 - (45)^2}{100(100 + 3 + 16)} \quad (3.5)$$

Accordingly, using surface roughness shielding factors [9] of 0.8 for lawn and of 0.93 for pavement yields an average surface roughness shielding factor for suburban surfaces of 0.84.

The shielding from groundshine provided by buildings to people located outdoors can be estimated by a view factor calculation. For example, a square house, 45 ft on a side, located at the center of a square quarter acre lot will screen about 36 degrees of the horizon from the view of a person, who is standing at the intersection of the lot sideline with the centerline of the street that fronts the lot. Thus, assuming obstruction of view principally by the four nearest houses, groundshine reduction due to screening by buildings will be about $0.6 = 1 - 4(36/360)$.

Table 3.14 presents estimates for overall urban and suburban shielding factors for people located outdoors

Table 3.14. Urban and Suburban Skidding Factors for People Located Outdoors

<u>Location</u>	<u>Shielding Factor</u>	<u>Reference</u>
Urban Copenhagen	0.06	[10]
Street canyon	0.1	[11]
Suburban Copenhagen	0.6	[10]
Urban areas	0.3 - 0.7	[12]
Lawns, trees, and streets (after dry deposition)	0.5 - 2.0	[11]
Lawns and streets (deposition during heavy rain, little deposition to tree leaves)	0.2 - 0.5	[11]

If the following three assumptions are made,

- (1) the amount of material deposited on tree leaves is about the half the amount deposited on the ground,
- (2) the shielding factor for material deposited on tree leaves is 2.0 (this number is larger than 1.0 because the leaves of a tree are a smooth vertical planar source) and the roughness shielding factor for material deposited on suburban surfaces is 0.84, and
- (3) buildings and hills reduce exposures to materials deposited on tree leaves and on the ground by a factor of 0.6,

then, in agreement with Ostmeyer and Helton [1a], an overall shielding factor of 0.73 can be calculated for people located outdoors in suburban areas as follows:

$$0.73 = 0.6[0.33(2.0) + 0.67(0.84)] \quad (3.6)$$

Increasing the fraction of material deposited on tree leaves to 0.5 from 0.33 increases the overall shielding factor to 0.85. Decreasing the fraction deposited on tree leaves to 0.25, lowers the overall shielding factor to 0.68. Accordingly, an overall groundshine shielding factor of 0.7 for people located outdoors is suggested for use in best estimate MACCS calculations. For sensitivity studies a range of 0.2 - 1.0 should be assumed for this factor.

3.2.2.5 Mass Thickness

The shielding provided by a material is directly proportional to its mass thickness, which is the product of the density of the material and its thickness. Densities for typical building materials [13] are presented in Table 3.15.

Table 3.15. Densities of Building Materials

Material	Density (g/cm ³)
aluminum	2.6
asphaltum, tar	1.2
brick	1.8
concrete block	2.3
glass	2.6
gypsum (wallboard)	0.93
insulation	0.65
steel	7.8
Portland cement	3.1
wood (pine)	0.5

From these data, approximate mass thicknesses may be calculated for several types of wall construction typical of U.S. houses.

WOOD FRAME HOUSES FACED WITH WOOD, ALUMINUM, OR STUCCO

0.125" aluminum + 0.5" wood + 3.0" insulation + 0.5" wallboard

$$2.54[0.125(2.6) + 0.5(0.5) + 3.0(0.65) + 0.5(0.93)] = 7.6 \text{ g/cm}^2$$

0.5" wood siding + 0.5" wood + 3" insulation + 0.5" wallboard

$$2.54[0.5(0.5) + 0.5(0.5) + 3.0(0.65) + 0.5(0.93)] = 7.4 \text{ g/cm}^2$$

0.75" stucco + 0.5" wallboard + 3.0" insulation + 0.5" wallboard

$$2.54 [0.75(3.1) + 0.5(0.93) + 3.0(0.65) + 0.5(0.93)] = 13.2 \text{ g/cm}^2$$

BRICK AND CONCRETE BLOCK HOUSES

2.5" brick + 0.5" wallboard + 3.0" insulation + 0.5" wallboard

$$2.54[2.5(1.8) + 0.5(0.93) + 3.0(0.65) + 0.5(0.93)] = 18.7 \text{ g/cm}^2$$

0.75" stucco + 3.0" cement + 0.5" wallboard

$$2.54[0.75(3.1) + 3.0(2.3) + 0.5(0.93)] = 24.6 \text{ g/cm}^2$$

ROOFS

0.25" asphalt shingles + 0.5" wood + 0.5" wallboard

$$2.54[0.25(1.2) + 0.5(0.5) + 0.5(0.93)] = 2.6 \text{ g/cm}^2$$

FLOORS

0.5" wood + 0.5" wallboard

$$2.54[0.5(0.5) + 0.5(0.93)] = 1.8 \text{ g/cm}^2$$

In agreement with Ostmeyer and Helton [1b], these qualitative calculations suggest that 10 g/cm^2 is a typical mass thickness for wood frame houses faced with wood siding, aluminum siding, or stucco, and that 20 g/cm^2 is a typical mass thickness for brick or concrete block houses.

3.2.2.6 Vehicular Shielding Factors

An eighth of an inch of steel corresponds to a mass thickness of 2.5 g/cm^2 and an eighth of an inch of glass to a mass thickness of 0.8 g/cm^2 , neither of which is sufficient to provide significant shielding from a radioactive plume. Therefore, since the interior space of cars and buses will not exclude a

significant fraction of the plume, the value of the cloudshine shielding factor for vehicles should be assumed to be 1.0.

The shielding afforded by vehicles from exposure to contaminated ground has been examined experimentally by comparing the dose rate in the vehicle to the dose rate outside the vehicle [15,16]. Data for cars and buses are presented in Table 3.16.

Table 3.16. Vehicle Groundshine Shielding Factors

<u>Vehicle</u>	<u>Indoor/Outdoor Ratio</u>	<u>Reference</u>
Cars	0.6 - 0.7	[16]
	0.3 - 0.6	[17]
Buses	0.5 - 0.7	[16]
	0.3 - 0.4	[17]

A shielding factor referenced to a contaminated infinite smooth plane may be calculated from these numbers by multiplying by the surface roughness shielding factor for the land surrounding the roadway. Both for countryside and suburbia, the surface roughness shielding factor for grass should be used. Thus, assuming that (1) inside/outside vehicular dose ratios are respectively 0.5 and 0.6 for buses and cars, and that (b) 10 percent of the people in vehicles are in buses and the balance in cars, in agreement with Ostmeier and Helton [1c], a groundshine shielding factor of 0.5 for vehicles can be calculated as follows:

$$0.5 = 0.8[0.1(0.5) + 0.9(0.6)] \quad (3.7)$$

3.2.2.7 Structure Shielding

The degree of shielding afforded to persons within a structure depends strongly on the nature (construction type) of the structure, the location within the structure of the shielded person, and the amount of radioactive material that infiltrates the structure. Accordingly, the shielding afforded to persons, who actively take shelter in basements or interior rooms with building windows and doors closed, can be significantly greater than that afforded persons who continue normal activities.

Structures shield people from cloudshine because their walls attenuate radiation and because indoor gas-borne concentrations of plume materials are usually substantially less than those in the outdoor plume. Indoor concentrations are lower because infiltration is not complete and deposition to interior surfaces further reduces the gas-borne amounts of those materials that do infiltrate the structure. But the indoor volumes of typical houses will usually be small compared to the volume of the outdoor plume. Therefore, complete plume exclusion from typical houses will produce a reduction in dose of only about 0.95 [1d]. Since complete plume exclusion is unlikely, dose reduction due to plume exclusion can be neglected.

Shielding due to dose attenuation is calculated as the sum of the attenuation factors for the structural elements (walls, roofs, ground if in a basement) that lie between the shielded person and the plume with each attenuation factor weighted by the fraction of the plume shielded by that element. Consider a person standing in the middle of a single story square 2000 ft² house enveloped by a hemispherical plume. If approximated by a circle, the house will have a radius of 25 ft. Mensuration formulæ for spheres [20] show that the fraction of the hemispherical plume subtended by the walls of the house is given by the ratio of the wall height to the distance from the center of the house to the top of its walls. That distance is about 26 ft, where 26 is the hypotenuse of the right triangle having sides 8 and 25 ft long. Therefore, the walls of the single story square 2000 sq ft house will screen about $0.3 = 8/26$ of the hemispherical cloud from a person standing in the middle of the house. The remaining 0.7 of the hemisphere will be screened by the roof of the house. If this single story house has a full basement, then the ground, walls, and roof plus floor of the house will respectively screen the following fractions of the hemispherical cloud: 0.3, 0.23, and 0.47.

If the house has two 1000 ft² stories and thus an effective radius of 18 ft, for a person standing in the middle of the first floor, the fractions of the hemispherical plume screened by the walls and the roof will be 0.67 and 0.33. For a person standing in the middle of the second floor, the wall and roof screening fractions are 0.4 and 0.6. If the person is standing in the middle of the basement of the house, the fractions of the hemispherical plume screened by the ground, walls, and roof are 0.4, 0.4, and 0.2. Assuming complete screening by the ground and attenuation factors [1e] of 0.74 for wood frame walls, 0.52 for masonry walls, 0.92 for a roof, 0.87 for a roof plus one floor, and 0.81 for a roof plus two floors, now allows the following cloudshine shielding factors to be estimated for houses as in Table 3.17.

Table 3.17. Cloudshine Shielding Factors

<u>House</u>	<u>Construction</u>	<u>Location</u>	<u>Factor</u>
1-story	wood frame	1st floor	0.87
		basement	0.58
	masonry	1st floor	0.80
		basement	0.53
2-story	wood frame	2nd floor	0.85
		1st floor	0.78
		basement	0.46
	masonry	2nd floor	0.76
		1st floor	0.64
		basement	0.37

Assuming that most people are downstairs during waking hours and upstairs when sleeping yields overall normal activity cloudshine attenuation factors of $0.80 = 0.67(0.78) + 0.33(0.85)$ for two story wood frame houses and $0.68 = 0.67(0.64) + 0.33(0.76)$ for two story masonry houses.

Now consider a two story school or office building with an effective radius of 25 ft. If walls, floors, and roofs all have mass thicknesses of about 20

g/cm^2 , then the value of the cloudshine attenuation factor will be 0.52 for people on the second floor and 0.39 for people on the first floor, where

$$0.39 = 0.53(0.52) + 0.47(0.24)$$

The fraction of the cloud subtended by walls is 0.53, and 0.24 is the shielding provided by a roof plus a floor (total mass thickness of 40 g/cm^2). Now if people in the building are evenly distributed between the first and second floors, an overall cloudshine attenuation factor of 0.46 can be calculated for schools and small office buildings. Larger effective building radii and poured concrete (rather than concrete block) walls will reduce this value. Therefore, a cloudshine shielding factor of 0.4 for schools and small office buildings is recommended for use in MACCS. For sensitivity studies, a range of 0.2 (cloudshine shielding factor for large office buildings [18]) to 0.5 (cloudshine shielding factor for single story school or office building) should be assumed.

Structure shielding to cloudshine has been examined by Burson and Profio [18] who assumed different building dimensions and mass thicknesses in their calculations then were assumed above. Table 3.18 presents the shielding factor recommendations of Burson and Profio both as originally developed by those authors (the number not in parentheses) and as obtained using the same mass thicknesses assumed above (the number in parentheses).

Table 3.18. Cloudshine Shielding Factors Recommended by Burson and Profio [18] for People Located in Buildings

<u>Structure</u>	<u>Location</u>	<u>Factor</u>
House		
Wood Frame	Ground Floor	0.9 (0.8)
	Basement	0.6 (0.5)
Masonry	Ground Floor	0.6 (0.7)
	Basement	0.4 (0.45)
Office Building	Interior	0.2 (0.4)

Since cloudshine structure shielding factors are certainly not precise to two significant figures, values in Table 3.19 are recommended for use in MACCS.

Table 3.19. Recommended Cloudshine Shielding Factor for People Located in Buildings

<u>Activity</u>	<u>Structure</u>	<u>Stories</u>	<u>Factor</u>
Normal	Wood Frame House	2	0.8
		1	0.9
	Masonry House	2	0.7
		1	0.8
	School or Office	2	0.4
Sheltering	Wood Frame House	2	0.5
		1	0.6
	Masonry House	2	0.4
		1	0.5
	School or Office	2	0.4

In contrast to cloudshine, where the dose from gas-borne materials that have infiltrated a structure is usually small compared to the dose received from the plume that envelopes the structure, for the groundshine dose received from indoor deposits of infiltrated materials can be important when compared to the groundshine dose received from materials deposited outdoors. The contribution of indoor deposits to total groundshine doses (the dose from all deposited materials whether deposited outdoors or indoors) has been examined by Ostmeyer and Helton [1f] and by Jacob and Meckbach [11]. Jacob and Meckbach note that as structure shielding increases, the dose from indoor deposits becomes increasingly important. For example, in a structure that has a groundshine shielding factor of 0.015, indoor exposures are increased by about a factor of two, if the indoor deposit is 2 percent of the outdoor deposit [11]. In agreement with Ostmeyer and Helton [1g], Jacob and Meckbach [11] also estimate that an indoor deposit that is 10 percent of that outdoors will double the indoor dose if the structure's groundshine shielding factor is 0.07.

The dose from indoor deposits can be indirectly modeled by increasing the value of the groundshine shielding factor as required to produce a total dose equal to that which would result from all deposited materials (both those deposited on outdoor surfaces and those deposited on indoor surfaces). For wood frame houses (mass thickness = 10 g/cm²) and masonry houses (mass thickness = 20 g/cm²), Ostmeyer and Helton estimate [1h] that if indoor deposits are half those outdoors, the total indoor dose from all deposited materials (both indoors and outdoors) is well approximated by increasing the structure's groundshine shielding factor 0.1 unit.

Groundshine shielding has been reviewed by Burson and Profio [18] and by Ostmeyer and Helton [1f] and recent European studies of groundshine shielding factors have been summarized by Roed [19]. Table 3.20 presents pertinent results from these studies.

Table 3.20. Groundshine Shielding Factors for Buildings

Ref	Houses						School/Office			Basement		
	Wood Frame			Masonry			L	C	U	L	C	U
	L	C	U	L	C	U						
O	0.4	0.5	0.6	0.3	0.35	0.4	0.15	0.4	0.5	0.02	0.08	0.08
B	0.2	0.4	0.5	0.04	0.2	0.4	0.01	0.05	0.08	0.02	0.04	0.07
B+d	0.3	0.4	0.6	0.14	0.3	0.5	0.11	0.15	0.18	0.12	0.14	0.17
R		0.44			0.19			0.1				
R+d		0.54			0.29			0.2				

In the table, the shielding factor value in the C column is the central (best) estimate value and the L (lower) and U (upper) values define the estimated range of the factor. In the column labeled Ref, O denotes Ostmeyer and Helton [1a], B Burson and Profio [18], and R Roed [19]. Since the values of Ostmeyer and Helton reflect correction for indoor deposits (i.e., groundshine shielding factor incremented 0.1 unit to correct for 50 percent infiltration) while those of Burson and Profio and of Roed do not, the table also presents the values of Burson and Profio and of Roed incremented by 0.1 unit (B+d and R+d on the table) to permit comparison to the values of Ostmeyer and Helton. Finally, the values in the table attributed to Roed were calculated assuming mass thicknesses of 10 g/cm² (wood frame houses), 20 g/cm² (masonry houses), and 35 g/cm² (office building with solid concrete walls, i.e., not concrete block) using the following dependence of groundshine shielding factor (S_{gd}) on exterior wall thickness (m_t)

$$S_{gd} = \exp (-0.083 m_t) \quad (3.8)$$

which was developed from data taken from Roed [19].

Inspection of the preceding table suggests that reasonable values for groundshine shielding factors for normal activity (indoor deposits half those outside) are 0.5 for wood frame houses, 0.3 for masonry houses, 0.3 for schools and small office buildings, and 0.1 for basements. For sheltering, the following values are recommended: 0.4 for wood frame houses, 0.2 for masonry houses, 0.2 for schools and small office buildings, and 0.05 for basements.

Normal Activity. Because people continuing normal activities may be in more than one location, the shielding factor for normal activity, S_N , must be constructed as a weighted sum of the shielding factors for people outdoors, S_O , in vehicles, S_V , and indoors in schools and office buildings, S_B , and in houses, S_H . Thus,

$$S_N = F_O S_O + F_V S_V + F_B S_B + F_H S_H \quad (3.9)$$

where F_O , F_V , F_B , and F_H are the fractions of the population that continue normal activities outdoors, in vehicles, indoors in schools and office buildings, and indoors in houses.

Because differences in dimensions and building materials cause individual house shielding factors to vary significantly, the shielding factor for houses, S_H , must be constructed as a weighted sum over types of houses. Here, for simplicity, only two types of houses will be considered:

- (1) Wood frame houses faced with wood, aluminum, or stucco,
- (2) Concrete block houses, and wood frame houses faced with masonry (e.g., brick).

Because the shielding afforded by a structure changes as a person moves about within the structure (walls afford more shielding than windows, basements more than attics), location within structures will affect the value of structure shielding factors. Only two locations, in basements and not in basements, will be considered here. Lastly, because the shielding afforded by structures does not decrease exposures to radioactive materials that penetrate the structure, ventilation and infiltration will increase the values of structure shielding factors. Accordingly,

$$S_H = f_W S_W + f_{Wb} S_{Wb} + f_M S_M + f_{Mb} S_{Mb} \quad (3.10)$$

where f is the fraction of all houses that provide the degree of shielding S , the subscript b indicates a basement, and the subscripts W and M respectively denote wood frame houses not faced by masonry and concrete block and masonry faced houses, respectively.

Since most people performing normal activities in houses are not located in basements, f_{Wb} and f_{Mb} should be set to zero when Equation 3.10 is used to calculate structure shielding factors for normal activity. Since all houses do not have basements, when this equation is used to calculate house shielding factors for people who have taken shelter, nonzero values should be used for f_{Wb} and f_{Mb} that reflect the degree of utilization of available basements.

Values for the fractions F_0 , F_V , F_B , and F_H are developed by considering how much time different groups of people spend in different locations. At least three groups of people need to be considered: workers, school age children, and people who spend most of their time at home (i.e., preschool children, homemakers, retired persons, the unemployed). Table 3.21 presents census data for 1986 [2] from which population fractions for these three population groups may be constructed.

Table 3.21. Census Data for Population Groups

<u>Group</u>	<u>Age Range</u>	<u>Number (millions)</u>
Preschool	< 5	18.1
School	5 - 17	45.1
Adult	18 - 64	148.6
<u>Retired</u>	<u>> 64</u>	<u>29.2</u>
All		241.0

In 1986, 109.6 million Americans were employed [2]. Therefore, about 39.0 million Americans ($39.0 = 148.6 - 109.6$) between the ages of 18 and 64 must either be homemakers or unemployed, which means that about 86.3 million Americans spend most of their time at home ($86.3 = 18.1 + 39.0 + 29.2$). Thus, workers constitute $45.5\% = 100 (109.6/241.0)$ of the total 1986 population, school age children $18.7\% = 100 (45.1/241.0)$, and homebodies $35.8\% = 100 = (86.3/241.0)$.

Table 3.22 presents plausible estimates of the number of hours in a day on weekdays and weekends during winter and during the rest of the year that individuals in each of the three population groups defined above spend sleeping (N), indoors in houses (I), indoors in schools and office buildings (B), in vehicles (V), and outdoors (O).

Table 3.22. Estimates of Time Spent in Different Locations by Population Groups

Group	Season	Weekdays					Weekends				
		N	I	B	V	O	N	I	B	V	O
Workers	(R) Not Winter	8	6	8	1	1	8	9	0	2	5
	(W) Winter	8	6	8	1	1	8	13	0	1	2
School Children	(R) Not Winter	8	5	4	1	6	8	7	0	2	7
	(W) Winter	8	7	6	1	2	8	12	0	1	3
Homebodies	(R) Not Winter	8	12	0	2	2	8	9	0	2	5
	(W) Winter	8	13	0	2	1	8	13	0	1	2

The fraction of the time that the general population spends in houses, in schools or office buildings, in vehicles, or outdoors is now given by

$$F_t = \frac{1}{24} \{ 0.75[(F_1)(h_{1R}) + (F_2)(h_{2R}) + (F_3)(h_{3R})] + 0.25[(F_1)(h_{1W}) + (F_2)(h_{2W}) + (F_3)(h_{3W})] \} \quad (3.8)$$

where $F_1 = 0.455$, $F_2 = 0.187$, and $F_3 = 0.358$; the subscripts 1, 2, and 3 denote workers, school children, and homebodies; and the subscripts R and W denote "not winter" (that is spring, summer, and fall) and "winter." Substitution of numbers from Table 3.22 yields the values in Table 3.23 for the fractions of time spent by the general population in houses, in schools and offices, in vehicles, and outdoors.

Table 3.23. Time Fractions by Locations for the General Population

Population	Location	Weekday	Weekend	Total
All	Houses	0.67	0.74	0.69
	Buildings	0.19	0.0	0.14
	Vehicles	0.057	0.073	0.06
	Outdoors	0.084	0.19	0.11

Robinson and Converse [20] have developed values for fractions of the time spent in houses, buildings, vehicles, and outdoors by adults less than 65 years old. Since adults less than 65 years old are comprised of 109.6 million workers plus the 39.0 million adult homebodies, the following equation can be used to develop values for time fractions for these adults to compare to the results of Robinson and Converse,

$$F_t = \frac{1}{24} \{ 0.75[(F_{1A})(h_{1R}) + (F_{3A})(h_{3R})] + 0.25[(F_{1A})(h_{1W}) + (F_{3A})(h_{3W})] \} \quad (3.9)$$

where $F_{1A} = 0.74 = 109.6/148.6$ and $F_{3A} = 0.26 = 39.0/148.6$ are the fractions of the adult population that are workers less than 65 years old and homebodies less than 65 years old. Table 3.24 presents time fractions for adults less than 65 years old and compares the values for total time to those of Ref. [20].

Table 3.24. Time Fractions by Location
for Working Adults

<u>Population</u>	<u>Location</u>	<u>Weekday</u>	<u>Weekend</u>	<u>Total</u>	<u>Total R&C</u>
Adults < 65	Houses	0.65	0.75	0.68	0.69
	Buildings	0.247	0.0	0.18	0.20
	Vehicles	0.053	0.073	0.06	0.05
	Outdoors	0.05	0.177	0.09	0.06

The good agreement in this table between the calculated results and those of Robinson and Converse suggests that the estimates of hours spent in different locations that were presented in Table 3.22 are reasonable. Thus, the following time fractions for the general population are recommended for use in MACCS: Houses = 0.7, Schools and Office Buildings = 0.15, Vehicles = 0.05, and Outdoors = 0.1.

1983 data on new detached housing (i.e., not apartments) has been published by the FHA [21] and 1980 data on existing housing (single and multiunit structures) have been published by the Department of Commerce [22]. If, as was done by Aldrich [8], it is assumed that the characteristics of new detached housing in a state or metropolitan area applies to all detached houses in that state or area and that most multiunit structures have basements and masonry walls (brick faced or concrete block), then the following formula can be used to estimate the percentage of housing units in a state or metropolitan area that have basements or are constructed with masonry walls:

$$\% X = (\% \text{ houses})(\text{fraction new with } X) + (\% \text{ apartments}) \quad (3.10)$$

where X is either basements or masonry walls. Table 3.25 presents the FHA [21] and Department of Commerce [22] data needed by Equation 3.10 and the percent masonry housing and percent basements at the five NUREG-1150 sites as calculated using Equation 3.10 and as developed using 1970 and 1971 data either by the Reactor Safety Study [23] or by Aldrich [8].

Table 3.25. Regional Building Data

Site	State/City	% Units at Address		% Masonry				% Basements			
		one [22]	> one	FHA [21]	Calc	RSS [23]	Ch	FHA [21]	Calc	Ald [8]	Ch
Zion	WI	76	24	16	36	<20		81	86	90	
	Chicago	46	54		61		50				85
	IL	64	36	15	46	40-60		43	64	77	
GG	MI	82	18	56	64	40-60	60	0	18	5	5
PB	PA	77	23	41	55	60-80	55	87	90	89	90
Surry	VA	79	21	14	32	40-60	35	41	53	42	45
Seq	TN	80	20	50	60	40-60	55	12	30	28	30

* GG = Grand Gulf, PB = Peach Bottom, Seq = Sequoyah, RSS = Reactor Safety Study [23], Calc = as calculated with Eq. 7, Ald = Aldrich [8], and Ch = choice (recommended value).

Shielding Factors for Normal Activity and for Sheltering. Values for all of the parameters in Equations 3 and 4 have now been selected. Therefore, parameter values can be calculated for persons who continue normal activity (N) and for persons who actively take shelter (S). Values for three shielding factors, cloudshine (C), groundshine (G), and inhalation/skin (I), are calculated for each activity (normal activity and sheltering). For each shielding factor, three values, an upper bound (H), a best estimate (B), and a lower bound (L), are calculated. Because housing stock varies by location, values are calculated for each NUREG-1150 reactor site (Zion, Grand Gulf, Peach Bottom, Surry, and Sequoyah).

Upper and lower bounds are estimated by assuming that the accident occurs at an unfavorable time (after school during the rush hours on a summer weekday) and at a favorable time (during school hours on a winter weekday). For the summer weekday after school during the rush period (the unfavorable upper bound situation), it is assumed that that school children are now outdoors and most office workers are in vehicles commuting to their homes. For the winter weekday with school in session (the favorable lower bound situation), it is assumed that about two-thirds of the population that on average would be outdoors or in vehicles is now indoors in schools or office buildings. These assumptions yield the upper and lower bound values listed in Table 3.26 for the fractions of the general population that are outdoors (F_O), in vehicles (F_V), in buildings (F_B), and in houses (F_H).

Table 3.26. Upper and Lower Bounds for Population Fractions

Scenario	F_O	F_V	F_B	F_H
Upper Bound (H)	0.4	0.15	0.05	0.4
Lower Bound (L)	0.03	0.02	0.3	0.65

The parameter values used to calculate shielding factors for normal activity and for active sheltering are now presented in Table 3.27 and the resulting site specific average shielding values for normal activity and for active sheltering are presented in Table 3.27. In Table 3.27, the column headers are the parameters defined for Equations 3.9 and 3.10. In Table 3.28, Average indicates the average of the site specific values and is given only when the site specific values were quite similar; NRC indicates the value of the indicated shielding factor used in the first pass NUREG-1150 calculations; and Choice indicates the value recommended on the basis of these calculations. In both tables, the line headers are defined as follows: C = cloudshine, G = groundshine, I = inhalation/skin, N = normal activity, S = active sheltering, H = upper bound, B = control estimate, and L = lower bound. Thus, CNH = cloudshine, normal activity, upper bound and the B that comes next = cloudshine, normal activity, central estimate, and so forth.

Table 3.27. Input Data for Calculation of Shielding Factors
Using Equations 3.9 and 3.10

Peach Bottom															
	F _O	S _O	F _V	S _V	F _B	S _B	F _H	f _W	S _W	f _{Wb}	S _{Wb}	f _M	S _M	f _{Mb}	S _{Mb}
CNH	0.4	1.0	0.15	1.0	0.05	0.5	0.4	0.45	0.95	0.0	0.0	0.55	0.85	0.0	0.0
B	0.1	1.0	0.05	1.0	0.15	0.4	0.7	0.45	0.85	0.0	0.0	0.55	0.75	0.0	0.0
L	0.03	1.0	0.02	1.0	0.3	0.3	0.65	0.45	0.75	0.0	0.0	0.55	0.65	0.0	0.0
SH	0.0	0.0	0.0	0.0	0.2	0.5	0.8	0.04	0.95	0.41	0.65	0.05	0.85	0.5	0.55
B	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.04	0.85	0.41	0.55	0.05	0.75	0.5	0.45
L	0.0	0.0	0.0	0.0	0.2	0.3	0.8	0.04	0.75	0.41	0.45	0.05	0.65	0.5	0.35
GNH	0.4	1.0	0.15	0.7	0.05	0.5	0.4	0.45	0.6	0.0	0.0	0.55	0.5	0.0	0.0
B	0.1	0.7	0.05	0.5	0.15	0.3	0.7	0.45	0.5	0.0	0.0	0.55	0.3	0.0	0.0
L	0.03	0.2	0.02	0.2	0.3	0.1	0.65	0.45	0.3	0.0	0.0	0.55	0.15	0.0	0.0
SH	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.04	0.5	0.41	0.08	0.05	0.4	0.5	0.08
B	0.0	0.0	0.0	0.0	0.2	0.2	0.8	0.04	0.4	0.41	0.05	0.05	0.2	0.5	0.05
L	0.0	0.0	0.0	0.0	0.2	0.01	0.8	0.04	0.2	0.41	0.02	0.05	0.05	0.5	0.02
INH	0.4	1.0	0.15	1.0	0.05	1.0	0.4	0.45	1.0	0.0	0.0	0.55	1.0	0.0	0.0
B	0.1	1.0	0.05	1.0	0.15	0.4	0.7	0.45	0.4	0.0	0.0	0.55	0.4	0.0	0.0
L	0.03	1.0	0.02	0.9	0.3	0.1	0.65	0.45	0.1	0.0	0.0	0.55	0.1	0.0	0.0
SH	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.04	0.4	0.41	0.4	0.05	0.4	0.5	0.4
B	0.0	0.0	0.0	0.0	0.2	0.2	0.8	0.04	0.2	0.41	0.2	0.05	0.2	0.5	0.2
L	0.0	0.0	0.0	0.0	0.2	0.1	0.8	0.04	0.1	0.41	0.1	0.05	0.1	0.5	0.1
Surry															
	F _O	S _O	F _V	S _V	F _B	S _B	F _H	f _W	S _W	f _{Wb}	S _{Wb}	f _M	S _M	f _{Mb}	S _{Mb}
CNH	0.4	1.0	0.15	1.0	0.05	0.5	0.4	0.65	0.95	0.0	0.0	0.35	0.85	0.0	0.0
B	0.1	1.0	0.05	1.0	0.15	0.4	0.7	0.65	0.85	0.0	0.0	0.35	0.75	0.0	0.0
L	0.03	1.0	0.02	1.0	0.3	0.3	0.65	0.65	0.75	0.0	0.0	0.35	0.65	0.0	0.0
SH	0.0	0.0	0.0	0.0	0.2	0.5	0.8	0.36	0.95	0.29	0.65	0.19	0.85	0.16	0.55
B	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.36	0.85	0.29	0.55	0.19	0.75	0.16	0.45
L	0.0	0.0	0.0	0.0	0.2	0.3	0.8	0.36	0.75	0.29	0.45	0.19	0.65	0.16	0.35
GNH	0.4	1.0	0.15	0.7	0.05	0.5	0.4	0.65	0.6	0.0	0.0	0.35	0.5	0.0	0.0
B	0.1	0.7	0.05	0.5	0.15	0.3	0.7	0.65	0.5	0.0	0.0	0.35	0.3	0.0	0.0
L	0.03	0.2	0.02	0.2	0.3	0.1	0.65	0.65	0.3	0.0	0.0	0.35	0.15	0.0	0.0
SH	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.36	0.5	0.29	0.08	0.19	0.4	0.16	0.08
B	0.0	0.0	0.0	0.0	0.2	0.2	0.8	0.36	0.4	0.29	0.05	0.19	0.2	0.16	0.05
L	0.0	0.0	0.0	0.0	0.2	0.01	0.8	0.36	0.2	0.29	0.02	0.19	0.05	0.16	0.02
INH	0.4	1.0	0.15	1.0	0.05	1.0	0.4	0.65	1.0	0.0	0.0	0.35	1.0	0.0	0.0
B	0.1	1.0	0.05	1.0	0.15	0.4	0.7	0.65	0.4	0.0	0.0	0.35	0.4	0.0	0.0
L	0.03	1.0	0.02	0.9	0.3	0.1	0.65	0.65	0.1	0.0	0.0	0.35	0.1	0.0	0.0
SH	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.36	0.4	0.29	0.4	0.19	0.4	0.16	0.4
B	0.0	0.0	0.0	0.0	0.2	0.2	0.8	0.36	0.2	0.29	0.2	0.19	0.2	0.16	0.2
L	0.0	0.0	0.0	0.0	0.2	0.1	0.8	0.36	0.1	0.29	0.1	0.19	0.1	0.16	0.1

Table 3.27. (Continued)

<u>Zion</u>															
	F _O	S _O	F _V	S _V	F _B	S _B	F _H	f _W	S _W	f _{Wb}	S _{Wb}	f _M	S _M	f _{Mb}	S _{Mb}
CNH	0.4	1.0	0.15	1.0	0.05	0.5	0.4	0.5	0.95	0.0	0.0	0.5	0.85	0.0	0.0
B	0.1	1.0	0.05	1.0	0.15	0.4	0.7	0.5	0.85	0.0	0.0	0.5	0.75	0.0	0.0
L	0.03	1.0	0.02	1.0	0.3	0.3	0.65	0.5	0.75	0.0	0.0	0.5	0.65	0.0	0.0
SH	0.0	0.0	0.0	0.0	0.2	0.5	0.8	0.08	0.95	0.42	0.65	0.08	0.85	0.42	0.55
B	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.08	0.85	0.42	0.55	0.08	0.75	0.42	0.45
L	0.0	0.0	0.0	0.0	0.2	0.3	0.8	0.08	0.75	0.42	0.45	0.08	0.65	0.42	0.35
GNH	0.4	1.0	0.15	0.7	0.05	0.5	0.4	0.5	0.6	0.0	0.0	0.5	0.5	0.0	0.0
B	0.1	0.7	0.05	0.5	0.15	0.3	0.7	0.5	0.5	0.0	0.0	0.5	0.3	0.0	0.0
L	0.03	0.2	0.02	0.2	0.3	0.1	0.65	0.5	0.3	0.0	0.0	0.5	0.15	0.0	0.0
SH	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.08	0.5	0.42	0.08	0.08	0.4	0.42	0.08
B	0.0	0.0	0.0	0.0	0.2	0.2	0.8	0.08	0.4	0.42	0.05	0.08	0.2	0.42	0.05
L	0.0	0.0	0.0	0.0	0.2	0.01	0.8	0.08	0.2	0.42	0.02	0.08	0.05	0.42	0.02
INH	0.4	1.0	0.15	1.0	0.05	1.0	0.4	0.5	1.0	0.0	0.0	0.5	1.0	0.0	0.0
B	0.1	1.0	0.05	1.0	0.15	0.4	0.7	0.5	0.4	0.0	0.0	0.5	0.4	0.0	0.0
L	0.03	1.0	0.02	0.9	0.3	0.1	0.65	0.5	0.1	0.0	0.0	0.5	0.1	0.0	0.0
SH	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.08	0.4	0.42	0.4	0.08	0.4	0.42	0.4
B	0.0	0.0	0.0	0.0	0.2	0.2	0.8	0.08	0.2	0.42	0.2	0.08	0.2	0.42	0.2
L	0.0	0.0	0.0	0.0	0.2	0.1	0.8	0.08	0.1	0.42	0.1	0.08	0.1	0.42	0.1
<u>Grand Gulf</u>															
	F _O	S _O	F _V	S _V	F _B	S _B	F _H	f _W	S _W	f _{Wb}	S _{Wb}	f _M	S _M	f _{Mb}	S _{Mb}
CNH	0.4	1.0	0.15	1.0	0.05	0.5	0.4	0.4	0.95	0.0	0.0	0.6	0.85	0.0	0.0
B	0.1	1.0	0.05	1.0	0.15	0.4	0.7	0.4	0.85	0.0	0.0	0.6	0.75	0.0	0.0
L	0.03	1.0	0.02	1.0	0.3	0.3	0.65	0.4	0.75	0.0	0.0	0.6	0.65	0.0	0.0
SH	0.0	0.0	0.0	0.0	0.2	0.5	0.8	0.38	0.95	0.02	0.65	0.57	0.85	0.03	0.55
B	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.38	0.85	0.02	0.55	0.57	0.75	0.03	0.45
L	0.0	0.0	0.0	0.0	0.2	0.3	0.8	0.38	0.75	0.02	0.45	0.57	0.65	0.03	0.35
GNH	0.4	1.0	0.15	0.7	0.05	0.5	0.4	0.4	0.6	0.0	0.0	0.6	0.5	0.0	0.0
B	0.1	0.7	0.05	0.5	0.15	0.3	0.7	0.4	0.5	0.0	0.0	0.6	0.3	0.0	0.0
L	0.03	0.2	0.02	0.2	0.3	0.1	0.65	0.4	0.3	0.0	0.0	0.6	0.15	0.0	0.0
SH	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.38	0.5	0.02	0.08	0.57	0.4	0.03	0.08
B	0.0	0.0	0.0	0.0	0.2	0.2	0.8	0.38	0.4	0.02	0.05	0.57	0.2	0.03	0.05
L	0.0	0.0	0.0	0.0	0.2	0.01	0.8	0.38	0.2	0.02	0.02	0.57	0.05	0.03	0.02
INH	0.4	1.0	0.15	1.0	0.05	1.0	0.4	0.4	1.0	0.0	0.0	0.6	1.0	0.0	0.0
B	0.1	1.0	0.05	1.0	0.15	0.4	0.7	0.4	0.4	0.0	0.0	0.6	0.4	0.0	0.0
L	0.03	1.0	0.02	0.9	0.3	0.1	0.65	0.4	0.1	0.0	0.0	0.6	0.1	0.0	0.0
SH	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.38	0.4	0.02	0.4	0.57	0.4	0.03	0.4
B	0.0	0.0	0.0	0.0	0.2	0.2	0.8	0.38	0.2	0.02	0.2	0.57	0.2	0.03	0.2
L	0.0	0.0	0.0	0.0	0.2	0.1	0.8	0.38	0.1	0.02	0.1	0.57	0.1	0.03	0.1

Table 3.27. (Concluded)

<u>Sequoyah</u>															
	F _O	S _O	F _V	S _V	F _B	S _B	F _H	f _W	S _W	f _{Wb}	S _{Wb}	f _M	S _M	f _{Mb}	S _{Mb}
CNH	0.4	1.0	0.15	1.0	0.05	0.5	0.4	0.45	0.95	0.0	0.0	0.55	0.85	0.0	0.0
B	0.1	1.0	0.05	1.0	0.15	0.4	0.7	0.45	0.85	0.0	0.0	0.55	0.75	0.0	0.0
L	0.03	1.0	0.02	1.0	0.3	0.3	0.65	0.45	0.75	0.0	0.0	0.55	0.65	0.0	0.0
SH	0.0	0.0	0.0	0.0	0.2	0.5	0.8	0.31	0.95	0.14	0.65	0.38	0.85	0.17	0.55
B	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.31	0.85	0.14	0.55	0.38	0.75	0.17	0.45
L	0.0	0.0	0.0	0.0	0.2	0.3	0.8	0.31	0.75	0.14	0.45	0.38	0.65	0.17	0.35
GNH	0.4	1.0	0.15	0.7	0.05	0.5	0.4	0.45	0.6	0.0	0.0	0.55	0.5	0.0	0.0
B	0.1	0.7	0.05	0.5	0.15	0.3	0.7	0.45	0.5	0.0	0.0	0.55	0.3	0.0	0.0
L	0.03	0.2	0.02	0.2	0.3	0.1	0.65	0.45	0.3	0.0	0.0	0.55	0.15	0.0	0.0
SH	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.31	0.5	0.14	0.08	0.38	0.4	0.17	0.08
B	0.0	0.0	0.0	0.0	0.2	0.2	0.8	0.31	0.4	0.14	0.05	0.38	0.2	0.17	0.05
L	0.0	0.0	0.0	0.0	0.2	0.01	0.8	0.31	0.2	0.14	0.02	0.38	0.05	0.17	0.02
INH	0.4	1.0	0.15	1.0	0.05	1.0	0.4	0.45	1.0	0.0	0.0	0.55	1.0	0.0	0.0
B	0.1	1.0	0.05	1.0	0.15	0.4	0.7	0.45	0.4	0.0	0.0	0.55	0.4	0.0	0.0
L	0.03	1.0	0.02	0.9	0.3	0.1	0.65	0.45	0.1	0.0	0.0	0.55	0.1	0.0	0.0
SH	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.31	0.4	0.14	0.4	0.38	0.4	0.17	0.4
B	0.0	0.0	0.0	0.0	0.2	0.2	0.8	0.31	0.2	0.14	0.2	0.38	0.2	0.17	0.2
L	0.0	0.0	0.0	0.0	0.2	0.1	0.8	0.31	0.1	0.14	0.1	0.38	0.1	0.17	0.1

Table 3.28. Recommended Shielding Factor Values

	Zion	Grand Gulf	Peach Bottom	Surry	Sequoyah	Average	NRC	Choice
CNH	0.94	0.93	0.93	0.94	0.93	0.93		0.95
B	0.77	0.76	0.77	0.78	0.77	0.77	0.75	0.75
L	0.59	0.59	0.59	0.60	0.59	0.59		0.60
SH	0.62	0.80	0.60	0.72	0.74			0.80
B	0.52	0.70	0.50	0.62	0.64			
L	0.42	0.60	0.40	0.52	0.54			0.40
GNH	0.75	0.75	0.75	0.76	0.75	0.75		0.75
B	0.42	0.41	0.41	0.44	0.41	0.42	0.33	0.40
L	0.19	0.18	0.18	0.20	0.18	0.19		0.20
SH	0.19	0.42	0.17	0.31	0.35			0.35
B	0.11	0.25	0.10	0.20	0.21			
L	0.03	0.09	0.02	0.07	0.07			0.02
INH	1.00	1.00	1.00	1.00	1.00	1.00		1.00
B	0.49	0.49	0.49	0.49	0.49	0.49	0.75	0.50
L	0.14	0.14	0.14	0.14	0.14	0.14		0.15
SH	0.40	0.40	0.40	0.40	0.40	0.40		0.40
B	0.20	0.20	0.20	0.20	0.20	0.20		0.20
L	0.10	0.10	0.10	0.10	0.10	0.10		0.10

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4. MACCS FOOD PATHWAY INPUT PARAMETERS

4.1 Introduction

Within the MACCS code, of the consequences from the ingestion of food contaminated by radionuclides deposited onto farmland following an accidental release are measured. These consequences can be divided into two general categories:

- (1) societal dose received from the ingestion of contaminated food and the health effects from that dose, and
- (2) economic costs from the mitigative actions to limit the dose to some user-defined level of acceptability.

In addition, a further distinction is made within the MACCS code between the dose received via the food pathway from crops being grown at the time of the release (i.e., the growing season submodel) and the dose received subsequent to the current growing season from food grown on land contaminated by the release (i.e., the long-term submodel). This distinction becomes evident in the preparation of the food pathway input parameters. Doses are calculated and mitigative actions determined for each of these submodels.

In general, the following model is used to determine the dose received via the food pathway. The dose received by organ k from the ingestion of nuclide i found in food arising from crop j , $D_{i,j,k}$, can be expressed as

$$D_{i,j,k} = GC_i \cdot A \cdot FA_j \cdot TF_{i,j} \cdot DF_{i,k}$$

where

GC_i = ground concentration of nuclide i (Bq/m²),

A = farmland area (m²),

FA_j = fraction of farmland used to grow crop j (unitless),

$TF_{i,j}$ = transfer factor, i.e., the fraction of deposited material incorporated onto or into the edible portion of crop j and ultimately eaten by man (unitless), and

$DF_{i,k}$ = dose received by organ k from ingested nuclide i (Sv/Bq).

The resulting dose to organ k from ingested nuclide i becomes

$$D_{i,k} = GC_i \cdot DF_{i,k} \cdot \sum_j (A \cdot FA_j \cdot TF_{i,j}) \quad (4.1)$$

Equation 4.1 is used both to project the potential dose for the determination of necessary mitigative actions and to determine the societal health effects resulting from the actual dose received.

The food pathway parameters will be discussed in three major groups. Section 4.1 describes the general parameters to define the food pathway model, i.e., information about the nuclides to be considered and the crop categories to be used. Section 4.2 discusses the components of the transfer factor, $TF_{i,j}$, in Equation 4.1. In Section 4.3, the input parameters specifically required in determining the necessary mitigative actions are discussed. The input parameters within each section are presented in alphabetical order for ease of location. Each parameter is described as well as its recommended values. Because there is uncertainty inherent in the derivation of the input parameter values, most tables containing the recommended values will also contain a range of possible parameter values. This range for the input parameters will be enclosed in parentheses or, in some cases, indicated explicitly. The recommended values for each parameter are followed by a discussion of the methodology used and the assumptions made in deriving the values currently recommended.

4.2 Food Pathway Definition Input Parameters

Several input parameters are required for the definition of the MACCS food pathway model. The values selected for some of these parameters will determine the dimensions for all subsequent food pathway input parameters.

4.2.1 NFICRP

NFICRP = number of crop categories to be used

The recommended value for NFICRP is 7.

Discussion

The recommended crop categories are listed in Table 4.1 with the major crops included within each category.

Table 4.1. Crop Categories

<u>Pasture</u>	<u>Stored Forage</u>	<u>Grain</u>	<u>Legumes & Nuts</u>	<u>Leafy Green Veg</u>	<u>Roots & Tubers</u>	<u>Other Food</u>
Various grasses	Alfalfa Clover Sorghum	Wheat Oats Barley Corn (incl. sweet corn) Sorghum	Soybeans Peanuts Snap beans Dried beans Peas Nuts	Lettuce Cabbage Broccoli Spinach Celery Cauliflower Greens	Potatoes Carrots Beets Sugar Onion	Fruits: Apples Grapes Citrus Fruits: Oranges Grapefruits Lemons Vegetables: Tomatoes Cucumbers Peppers

Several factors were considered in dividing the crops into the seven distinct categories in Table 4.1. The evaluation of the input parameters for the food pathway in the MACCS code tends to be somewhat labor intensive, so the intent was to keep the derivation of input parameters as simple and straightforward as possible.

The first factor considered was the harvesting pattern for the various crop categories. Pasture is the only crop for which harvesting is considered continuous. It is also assumed that all radioactive material deposited onto pastureland during a given growing season will be consumed by grazing animals before the end of that growing season. In addition, it is assumed that the rate at which the pasture is harvested is constant over the entire season. In contrast, harvest is assumed to be a discrete process for all nonpasture crops. This significant difference in harvesting patterns served as the basis for the first major subdivision into crop categories, that is,

- (1) Pasture, and
- (2) Nonpasture crops.

To make an additional distinction between the nonpasture crops, consideration was given to how the edible portion of the nonpasture crops becomes contaminated during deposition. In certain crops, the edible portion is not exposed to the environment, and contamination occurs only by the translocation of the radioactive material deposited onto plant surfaces into the edible portion of the plant. Examples of this type of crop are grains, legumes, nuts, roots, and tubers. For all other nonpasture crops, the edible portion of the plant is directly exposed to the radioactive material during deposition. These crops include stored forage and all fruits and vegetables. By differentiating between nonpasture crops in which the edible portion is directly contaminated and those in which the edible portion is not subject to direct contamination, the crops were then further subdivided into the following categories:

- (1) Pasture
- (2) Nonpasture

- Indirect contamination of the edible portion
(grains, legumes, nuts, roots, and tubers)

- Direct contamination of the edible portion
(stored forage, fruits, and vegetables)

Within each of these broad groups of nonpasture crops, a further distinction can be made when consideration is given to the plant surface characteristics. For all crops, an increased roughness of the plant surfaces directly affects the efficiency with which the plant retains the radioactive material until the time of harvest.

For crops in which the edible portion is not exposed to the environment, an increase in the amount of material retained on the plant surfaces increases the translocation that can occur. The beard structure of grains further enhances the efficiency of the translocation process. The plant surfaces of legumes, nuts, roots, and tubers are similar and characteristically have less surface roughness than the plant surfaces of grains.

For crops in which the edible portion is exposed to the outside environment, an increased roughness in the plant surfaces will increase the amount of material physically retained on those surfaces until the crop is harvested. A distinction was thus made between green leafy vegetables and stored forage, in which the edible portion has significant surface roughness, and all other fruits and vegetables for which the edible portion has a relatively smooth surface or a "rind" that will be removed during preparation.

By considering the differences in the surface roughness of both plants and their edible portions, the crops categories were further refined as follows:

- (1) Pasture
- (2) Nonpasture

- Indirect contamination of the edible portion

- High plant surface roughness
(grains)

- Low plant surface roughness
(legumes, nuts, roots, tubers)

- Direct contamination of the edible portion

- High surface roughness of the edible portion
(stored forage, green leafy vegetables)

- Low surface roughness of the edible portion
(fruits and vegetables)

Finally, two additional factors were given consideration in arriving at the crop categories currently being used. The first, biological dissimilarity of the edible portion of the plant, led to a distinction between seeds (legumes

and nuts) and roots (roots and tubers). The second factor, crop utilization, gave rise to the distinction being made between stored forage (consumed only by animals) and green leafy vegetables (consumed only by man).

By giving consideration to these distinctions between crop types, the following crop categories evolved:

- (1) Pasture
- (2) Nonpasture
 - Indirect contamination of the edible portion
 - High plant surface roughness
(grains)
 - Low plant surface roughness
 - Reproductive plant part
(legumes and nuts)
 - Absorptive or energy storing plant part
(roots and tubers)
 - Direct contamination of the edible portion
 - High plant surface roughness
 - Consumed only by animals
(stored forage)
 - Consumed only by man
(green leafy vegetables)
 - Low plant surface roughness
(other food)

Of the crop categories, pasture crops and stored forage are eaten by animals that in turn are food for man, but they are not eaten by man directly. On the other hand, green leafy vegetables, roots, tubers, and "other" crops are not consumed by animals, but are consumed directly by man. Grains and legumes and nuts are consumed by both man and animals, which is important in evaluating the input parameters for the food pathway.

4.2.2 NFIISO

NFIISO = number of nuclides for which data will be specified for the food pathway

The recommended value for NFIISO is 6.

Discussion

When NFIISO = 6, the recommended food pathway nuclides are Sr-89, Sr-90, Cs-134, Cs-137, I-131, and I-133. It is expected that these radionuclides will dominate the food pathway doses across the entire spectrum of potential reactor accident scenarios [1:40].

4.2.3 NTTRM

NTTRM = Number of terms used in the growing crop retention model that describes the weathering loss mechanism

The recommended value for NTTRM is 2.

Discussion

The growing season crop retention model calculates the fraction of the radioactive material deposited onto the surface of growing plants that will be retained following an exponential weathering loss resulting from exposure of the plant to the environment. By using two terms in the growing crop retention model, it is possible to separate the deposited material into the portion that will weather rapidly with a relatively short half-life and the remaining material that will adhere more stubbornly to the plant surfaces and weather more slowly.

The fractions of the material weathering with each pattern and the half-lives associated with each weathering pattern are supplied by the input parameters CTCOE and CTHALF as described in Section 4.3.

4.2.4 TGSBEG and TGSEND

TGSBEG_j = day of the year marking the start of the growing season for crop j

TGSEND_j = day of the year marking the end of the growing season for crop j

Table 4.10 gives recommended values for TGSBEG_j and TGSEND_j.

Discussion

Since the fraction of radioactive material deposited directly onto growing crops that remains on the crop at the time of harvest is time dependent, it must be determined when during the growing season the deposition occurred. The elapsed time before harvest, T_e , is then the difference between the day on which the crop is harvested, TGSEND, and the day on which deposition, T_a , (i.e., the day on which the accidental release occurred). Therefore,

$$T_e = TGSEND - T_a$$

This elapsed time is used within the MACCS code to determine the amount of radioactive material deposited onto plant surfaces that will be weathered away before the crop is harvested.

The values recommended for TGSBEG and TGSEND are summarized in Table 4.2.

Table 4.2. Values for TGSBEG and TGSEND

<u>Crop</u>	<u>TGSBEG_j</u>	<u>TGSEND_j</u>	<u>(Dates)</u>
Pasture	90	270	(3/31-9/27)
Stored Forage	150	240	(5/30-8/28)
Grains	150	240	
Legumes & Nuts	150	240	
Leafy Green Vegetables	150	240	
Root Vegetables	150	240	
Other Food	150	240	

4.3 Transfer Factor Component Input Parameters

Calculation of the dose to organ k from nuclide i , $D_{i,k}$ in Equation 4.1, requires the determination of the transfer factors, $TF_{i,j}$, which define the fraction of nuclide i deposited onto cropland used to grow crop j that is incorporated into the edible portion of the crop and ultimately consumed by man.

Figure 4.1 depicts the overall transfer of deposited radionuclides to man as modeled by MACCS. Each transfer path is labeled using the MACCS input parameters that either define the transfer along the path or, as in the case of CTCOE and CTHALF, calculate within the MACCS code the fraction of the available material transferred at that segment of the pathway. Tables 4.3 to 4.6 give the recommended values.

Two submodels within the MACCS food pathway model describe the transfer of deposited radioactive material to the edible portion of the crop. The first of these, the growing season submodel, describes the transfer of radionuclides deposited directly onto the surfaces of crops growing at the time of the release. The second, the long-term submodel, describes the transfer of radionuclides deposited onto soil that will subsequently enter the food chain via root uptake by plants or by direct ingestion of the contaminated soil by grazing animals. Within each of these submodels, crops are considered to enter the food chain in one of three ways: (1) the crop may be consumed directly by man, (2) it may be consumed by meat-producing animals with the meat in turn being consumed by man, or (3) it may be consumed by milk-producing animals with the milk in turn being consumed by man.

The derivation of values for each of the input parameters depicted in Figure 4.1 is discussed fully in the remainder of this section. These input parameters are considered in alphabetical order.

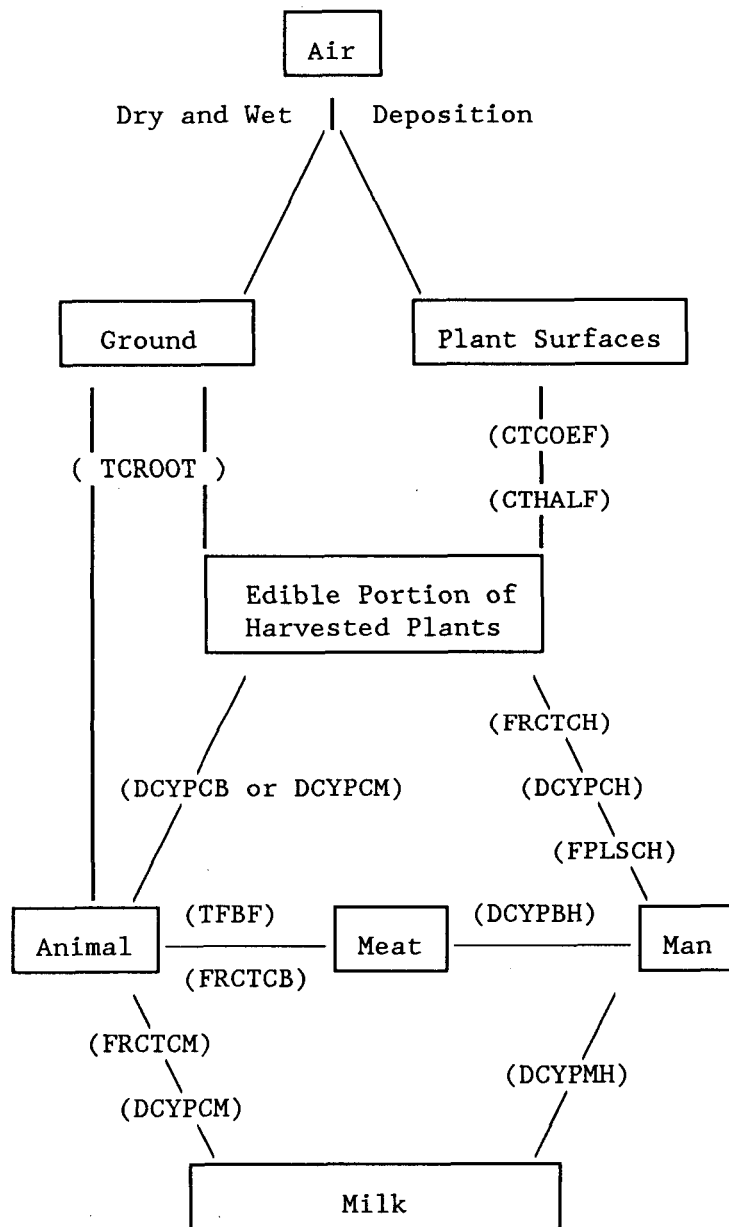


Figure 4.1 Transfer of Released Radionuclides to Man Via the Food Pathway as Depicted in the MACCS Code.

4.3.1 CTCOEF and CTHALF

$CTCOEF_n$ = fraction of material weathering with a half-life $CTHALF_n$

$CTHALF_n$ = half-life for the nth exponential term of the weathering model

Table 4.3. Recommended Values for CTCOE_{F1}

<u>Crop</u>	<u>Strontium</u>	<u>Cesium</u>	<u>Iodine</u>
Pasture	0.30 (0.23-0.38)	0.30 (0.23-0.38)	0.30 (0.23-0.38)
Stored Forage	0.20 (0.15-0.24)	0.20 (0.15-0.24)	0.20 (0.15-0.24)
Grain	0.010 (0.0075-0.013)	0.050 (0.038-0.063)	0.0
Legumes	0.0050 (0.0038-0.0063)	0.010 (0.0075-0.013)	0.0
Green Leafy Vegetables	0.24 (0.18-0.30)	0.24 (0.18-0.30)	0.24 (0.18-0.30)
Roots & Tubers	0.0006 (0.00045-0.00075)	0.025 (0.019-0.031)	0.0
Other Food	0.020 (0.15-0.24)	0.020 (0.15-0.24)	0.020 (0.15-0.24)

Table 4.4. Recommended Values for CTHALF₁*

<u>Crop</u>	<u>Strontium</u>	<u>Cesium</u>	<u>Iodine</u>
Pasture	1.2096x10 ⁶	1.2096x10 ⁶	1.2096x10 ⁶
Stored Forage	1.2096x10 ⁶	1.2096x10 ⁶	1.2096x10 ⁶
Grain	3.1536x10 ¹³	3.1536x10 ¹³	1.0
Legumes	3.1536x10 ¹³	3.1536x10 ¹³	1.0
Green Leafy Vegetables	1.2096x10 ⁶	1.2096x10 ⁶	1.2096x10 ⁶
Roots & Tubers	3.1536x10 ¹³	3.1536x10 ¹³	1.0
Other Food	1.2096x10 ⁶	1.2096x10 ⁶	1.2096x10 ⁶

* Half-lives in seconds: 14 days = 1.2096x10⁶
1 million years = 3.153x10¹³.

Table 4.5. Recommended Values for CTCOE_{F2}

<u>Crop</u>	<u>Strontium</u>	<u>Cesium</u>	<u>Iodine</u>
Pasture	0.076 (0.058-0.096)	0.076 (0.058-0.096)	0.076 (0.058-0.096)
Stored Forage	0.050 (0.038-0.063)	0.050 (0.038-0.063)	0.050 (0.038-0.063)
Grain	0.0	0.0	0.0
Legumes	0.0	0.0	0.0
Green Leafy Vegetables	0.060 (0.046-0.076)	0.060 (0.046-0.076)	0.060 (0.046-0.076)
Roots & Tubers	0.0	0.0	0.0
Other Food	0.050 (0.038-0.063)	0.050 (0.038-0.063)	0.050 (0.038-0.063)

Table 4.6. Recommended Values for CTHALF₂*

<u>Crop</u>	<u>Strontium</u>	<u>Cesium</u>	<u>Iodine</u>
Pasture	4.3200x10 ⁶	4.3200x10 ⁶	4.3200x10 ⁶
Stored Forage	4.3200x10 ⁶	4.3200x10 ⁶	4.3200x10 ⁶⁶
Grain	1.0	1.0	1.0
Legumes	1.0	1.0	1.0
Green Leafy Vegetables	4.3200x10 ⁶	4.3200x10 ⁶	4.3200x10 ⁶
Roots & Tubers	1.0	1.0	1.0
Other Food	4.3200x10 ⁶	4.3200x10 ⁶	4.3200x10 ⁶

* Half-lives in seconds: 50 days = 4.3200x10⁶.

A uniform sampling distribution is recommended for all CTCOEF and CTHALF. Recall that the numbers within the parentheses represent the possible range of values for each parameter value.

Discussion

Between the time of deposition of radioactive material onto plant surfaces and the time when the plants are harvested, part of the radioactive material will be lost from the plant surfaces by the following processes (1) weathering, (2) radioactive decay, (3) translocation to interior portions of the plant, and (4) harvesting.

The fraction of the radioactive material initially deposited onto plant surfaces that remains in or on the edible portions of the harvested plant is called the direct deposition transfer factor.

The magnitude of the direct deposition transfer factor depends on the time during the growing season when the accident (deposition) occurs. For crops in which the edible portion is exposed to the outside environment, the losses from weathering and decay will increase with time. Therefore, decreasing the time between deposition and harvest will result in an increase in the direct deposition transfer factor.

It is assumed that pasture undergoes continuous harvesting throughout the growing season. Deposition early in the pasturing season will increase both the time available for nuclide loss from weathering and decay and will also increase the time available for the consumption of contaminated pasture by grazing animals. Since consumption of nuclides by grazing is faster than the removal by either weathering or radioactive decay, the size of the direct deposition transfer factor will increase as the time available for grazing increases.

Weathering has been observed to cause a loss of radioactive material on plant surfaces due to the simultaneous occurrence of several exponential processes. Therefore, the removal of radioactivity from plant surfaces by weathering can be treated as a sum of terms that have the following form:

$$\sum_n \{CTCOEF_n \cdot \text{EXP}[-(\ln 2/CTHALF_n)]\} \quad (4.2)$$

where

$CTCOEF_n$ = fraction of material deposited per unit area of cultivated field that is removed by weathering with a half-life $CTHALF_n$

In addition,

$$CTCOEF_n = IF \cdot AF_n$$

where

IF = interception fraction, i.e., the fraction of the material deposited onto the field that is intercepted by crop surfaces

AF_n = availability fraction, i.e., the fraction of the material deposited onto crop surfaces from which the material is removed by weathering with the half-life CTHALF_n

and

$$\sum_n AF_n = 1$$

The edible portion of some crops is not exposed to the outside environment. For these crops, the retention of radioactivity in the edible portions will be determined by translocation of the material from plant surfaces to the edible portion. When this is the case, the weathering model as described above will not be applicable. Instead, an empirical transfer factor is used that has been derived from fallout studies. The empirical transfer factor represents the combined effects of interception, weathering, and translocation to the edible portion of the plant. For convenience, this empirical factor can be input as a value of CTCOEF_n. Since this empirical value includes the effects of weathering, the exponential part of weathering decay expression associated with this empirical value for CTCOEF_n is reduced to a value of unity by setting CTHALF_n, in Equation 4.2, equal to one million years (i.e., 3.1536×10^{13} seconds). In addition, all but the first term of the weathering equation are set to zero by setting CTCOEF_n for $n > 1$ equal to 0.0 and letting the associated value of CTHALF_n for $n > 1$ be 1 second. In effect, this transforms the exponential equation into a constant (i.e., CTCOEF₁) for those crops in which the edible portion is not exposed to the outside environment.

Finally, the removal of radioactivity is treated explicitly for all crops. It is currently assumed that there are two exponential weathering terms for all crop categories with appropriate adjustments made for the crops in which the edible portion is not exposed to the outside environment. When using a two exponential term weathering model, it becomes necessary to derive two values for each crop/nuclide combination that indicates the CTCOEF_n for each exponential expression. In addition, each of these terms will also require a value of CTHALF_n that describes the weathering half-life for that nuclide/crop combination for that component of the weathering process.

The following crops have edible portions that are exposed to the outside environment: pasture, stored forage, green leafy vegetables, and "other food." Given that the "other food" crop category consists primarily of fruits and vegetables in the light of per capita consumption data [2], the entire category will be treated as though the edible portion is exposed to the outside environment. As previously stated, $CTCOEF_n$ is the product of the interception fraction and the availability fraction. In addition, a half-life will be needed for each of the two exponential terms in the weathering equation. Based on studies by Simmonds and Linsley [3,4], the following values and associated ranges recommended for the interception fraction, availability fraction, and weathering half-lives are as summarized in Table 4.7. The higher interception fractions for pasture and spinach seems to be justified by Vuori's [5] study of fallout data following the Chernobyl accident.

Table 4.7. Interception Fraction, Availability Fraction, and Half-Lives

Variable	Value	Range of Values
Interception fraction		
Pasture	0.38	0.29-0.48
Stored Forage	0.25	0.20-0.28
Green Leafy Vegetables	0.30	0.23-0.38
Other Food	0.25	0.20-0.28
Availability fraction	0.80	0.75-0.85
for short-term weathering		
Availability fraction	0.20	0.15-0.25
for long-term weathering		
Half-life for short-term weathering (day)	14.0	13.0-19.0
Half-life for long-term weathering (day)	50.0	13.0-19.0

These data lead to the values in Table 4.8 for the variables $CTCOEF$ and $CTHALF$ for all nuclides being treated in the MACCS code. The remaining crop categories (i.e., grains, legumes, and roots and tubers) have edible portions not exposed to the environment, and the values for $CTCOEF_1$ will therefore represent empirical transfer factors as derived from fallout data. To ensure that MACCS will treat these factors as constants, the other related

Table 4.8. Values for CTCOEF and CTHALF*

	<u>Pasture</u>	<u>Stored Forage</u>	<u>Green Leafy Vegetables</u>	<u>Other Food</u>
CTCOEF ₁	0.30	0.20	0.24	0.20
CTCOEF ₂	0.076	0.05	0.060	0.05
CTHALF ₁	14 d.	14 d.	14 d.	14 d.
CTHALF ₂	50 d.	50 d.	50 d.	14 d.

* These values are converted to seconds for use in the MACCS code.

input variables take on the following values:

CTHALF₁ = 1 million years (i.e., 3.154×10^{13} s),
 CTCOEF₂ = 0.0
 CTHALF₂ = 1 s

Since the iodine isotopes considered have very short half-lives, it has been assumed that these isotopes will not be found in the edible portion of the plant at the time of harvest. Therefore, the value for CTCOEF₁ for both I-131 and I-133 will be 0.0.

In a review of the available data on direct deposition transfer factors to be used for CTCOEF₁, Ostmeier and Helton [1] arrived at empirical direct deposition transfer factors for grain and legumes. Coughtrey and Thorne [6] discussed the analogous empirical direct deposition transfer factor for roots and tubers. For each of these transfer factors, a range of possible values for each element/crop combination was chosen by assuming a 25% uncertainty range.

A summary of these empirical transfer factors and the associated range of possible values is given in Table 4.9.

Table 4.9. Summary of Empirical Transfer Factors

<u>Crop</u>	<u>Empirical Transfer Factors</u>	
	<u>Strontium</u>	<u>Cesium</u>
Grain	0.010 (0.0075-0.013)	0.050 (0.038-0.063)
Legumes	0.005 (0.0038-0.0063)	0.010 (0.0075-0.013)
Roots & Tubers	0.00060 (0.00045-0.00075)	0.025 (0.019-0.031)

4.3.2 DCYPBH

DCYPBH_i = Fraction of radionuclide i present in meat at the time of slaughter that is retained and consumed by man (accounts for losses from both decay and processing).

Table 4.10 shows the recommended values for DCYPBH_i.

Table 4.10. Recommended Values for DCYPBH_i

<u>Nuclide</u>	<u>DCYPBH</u>
Sr-89	0.77 (0.58-0.96)
Sr-90	1.0
Cs-134	1.0
Cs-137	1.0
I-131	0.18 (0.14-0.23)
I-133	0.0

A uniform sampling distribution is recommended for DCYPBH_i.

Discussion

DCYPBH_i can be expressed as

$$\text{DCYPBH}_i = \frac{\text{FINAL}_i}{\text{INITIAL}_i},$$

where

FINAL_i = Concentration of radionuclide i in the feed at the time of consumption by the animal (Ci/kg) (accounts for both decay and processing losses)

INITIAL_i = Concentration of radionuclide i in the meat at the time of slaughter (Ci/kg)

A value for DCYPBH is obtained for each nuclide i by evaluating the following expression:

$$DCYPBH_i = \text{EXP} \{ - [(\ln 2 / THALF_i) \cdot TDELAY] \} \quad (4.3)$$

where

$THALF_i$ = radiological half-life of isotope i

$TDELAY$ = delay time between the production and consumption of the food product

The values for $DCYPBH_i$ were obtained using Equation 4.3 with two assumptions. The first assumption is that 20 days elapse between the time of production and the consumption of meat and meat products as recommended in the Regulatory Guide 1.109 [7: Table E-15]. That delay time seems reasonable for all meat products purchased fresh by the consumer. The second assumption is that there is no significant difference in the delay time between production and consumption of beef, pork, and poultry; therefore, the loss from decay will be basically the same for all meat products.

In finding the range of values for this variable, it was assumed that the estimated value would most probably be accurate to 25%.

4.3.3 DCYPCB and DCYPCM

$DCYPCB_{i,j}$ and $DCYPCM_{i,j}$ give the fraction of radionuclide i present in crop j at the time of harvest that is ingested respectively by meat-producing or milk-producing animals.

$DCYPCB_{i,j}$ = Transfer factor for meat-producing animals

$DCYPCM_{i,j}$ = Transfer factor for milk-producing animals

Because dairy and beef cattle have similar consumption patterns for different crop types, $DCYPCB_{i,j}$ and $DCYPCM_{i,j}$ have the same values. The recommended values are presented in Tables 4.11 and 4.12. Since there are no processing losses between harvest and consumption by cattle, $DCYPCB_{i,j}$ and $DCYPCM_{i,j}$ treat only losses resulting from radioactive decay.

A uniform sampling distribution is recommended for $DCYPCB_{i,j}$ and $DCYPCM_{i,j}$.

Discussion

Because $DCYPCB_{i,j}$ and $DCYPCM_{i,j}$ have the same values for any nuclide/crop pair, they are both denoted in the following discussion by $DCYPCA_{i,j}$.

Table 4.11. Recommended Values for DCYPCB_{i,j} and DCYPCM_{i,j} for Crops Consumed by Cattle

<u>Nuclide</u>	<u>Pasture</u>	<u>Stored Forage</u>	<u>Grains</u>	<u>Legumes and Nuts</u>
Sr-89	1.0	0.37 (0.28-0.46)	0.20 (0.15-0.25)	0.20 (0.15-0.25)
Sr-90	1.0	0.99	0.99	0.99
Cs-134	1.0	0.92 (0.69-1.0)	0.85 (0.64-1.0)	0.85 (0.64-1.0)
Cs-137	1.0	0.99	0.99	0.99
I-131	1.0	0.063 (0.047-0.079)	0.032 (0.024-0.040)	0.032 (0.024-0.040)
I-133	1.0	0.0068 (0.0051-0.0085)	0.0034 (0.0025-0.0043)	0.0034 (0.0025-0.0043)

Table 4.12. Recommended Values for All Nuclides for Crops Not Consumed by Cattle

<u>Nuclide</u>	<u>Leafy Green Vegetables</u>	<u>Roots & Tubers</u>	<u>Other Food</u>
All	0.0	0.0	0.0

Thus,

$$DCYPCA_{i,j} = \frac{CONSUMED_{i,j}}{HARVEST_{i,j}}$$

where

CONSUMED_{i,j} = concentration (Ci/kg) of radionuclide i in crop j when consumed by animals (accounts for losses because of radioactive decay) and

HARVEST_{i,j} = concentration (Ci/kg) of radionuclide i in crop j at harvest.

Crops used to feed livestock will generally follow the same storage pattern regardless of whether the animal that consumes the crop is a milk- or beef-producing animal. For this reason, these two variables will have the same value for any nuclide/crop pair.

The values derived are based on the assumption that the consumption patterns for the crops in each crop category are similar from year to year. Three the crop categories have no significant consumption by animals, Leafy Green Vegetables, Roots and Tubers, and Other Food, and therefore are assigned a transfer factor of 0.0.

For pasture, grazing is the method of harvesting, and there is therefore no delay time between harvesting and consumption. Since herds are usually sized to the fields on which they graze, all radionuclides deposited onto the pasture grass are assumed to be consumed by the end of the pasturing season. For this reason, for pasture the value for the ratio of the amount of the nuclide consumed to the amount of the nuclide present at the time of harvest is 1.0 for all nuclides.

It is assumed that stored forage will be used on a continuous basis during the time when the animals are not grazing on pasture. The length of time over which this continuous feeding takes place is the difference between 365 days and the length of the pasturing season (growing season) for pasture. If FT_s is the time period over which the feeding of stored forage takes place, then letting the length of the growing season for pasture be 180 days (see TGSBEG and TGSEND), $FT_s = 365 - 180 = 185$ days.

For both grains and legumes, it is assumed that harvest occurs once a year, and the crops will be fed to animals in a continuous manner throughout the year until their next harvest. Accordingly, if the time over which grain and legumes are fed is denoted by FT_g , then $FT_g = 365$ days.

For a crop that is not harvested continuously (single harvest time), if an exact delay time (TDELAY) between harvest and consumption can be assigned the transfer factor, $TF_{i,j}$, for a given crop j for nuclide i is evaluated as follows:

$$TF_{i,j} = \text{EXP} \{ -[(\ln 2 / \text{THALF}_i) \cdot \text{TDELAY}_j] \} \quad (4.4)$$

where

THALF_i = radiological decay half-life for nuclide i and

TDELAY_j = time delay between harvest and consumption of crop j by animals.

$TF_{i,j}$ represents the fraction of the radioactive material present in the crop at the time of harvest that remains when the crop is consumed. The losses of radioactive material over that period of time is the result of radioactive decay.

For a crop that is continuously consumed, the transfer factor, $TF_{i,j}$, is calculated as the product of the consumption rate for the crop and the integral of the rate of transfer over the entire period of time the crop is being consumed. The transfer factor for a given crop category for a specific nuclide is then calculated using the following expression:

$$TF_{i,j} = CR_j \cdot \int_0^{T_j} \text{EXP}\{-[(\ln 2/THALF_i) \cdot t]\} dt$$

where

CR_j = consumption rate for crop j (day^{-1})

$THALF_i$ = radiological decay half-life for nuclide i

T_j = length of overall period during which crop j is consumed

If it is assumed that consumption takes place at a constant rate over the designated period, T_j , then $CR_j = 1/T_j$, and the expression for the transfer factor becomes

$$\begin{aligned} TF_{i,j} &= DCYPCA_{i,j} \\ &= \frac{1}{T_j} \cdot \int_0^{T_j} \text{EXP}\{-[(\ln 2/THALF_i) \cdot t]\} dt \\ &= \frac{1 - \text{EXP}\{-[(\ln 2/THALF_i) \cdot T_j]\}}{T_j \cdot (\ln 2/THALF_i)} \end{aligned} \quad (4.5)$$

For the period of consumption, T_j , the values FT_s and FT_g were used. That is,

$T_j = FT_s = 185$ days for Stored Forage

$= FT_g = 365$ days for Grains, Legumes, and Seeds

The range of possible values in each case was arrived at by assuming that the best estimate values are probably accurate to 25%.

4.3.4 DCYPCH

$DCYPCH_{i,j}$ = fraction of radionuclide i present in crop j at the time of harvest remains in food at the time of consumption by man (accounts for losses from radioactive decay)

The transfer factor, $DCYPCH_{i,j}$, accounts only for losses of radioactive material attributable to radioactive decay. Losses of material which occurs during the processing of food before it is eaten is accounted for by the transfer factor $FPLSCH_{i,j}$. Table 4.13 summarizes the recommended values of $DCYPCH_{i,j}$ for crops consumed by man, and Table 4.14 summarizes the values for crops not consumed by man.

Table 4.13. Recommended Values of $DCYPCH_{i,j}$ for Crops Consumed by Man

Nuclides	Grains	Legumes and Nuts	Green Leafy Vegetables	Roots & Tubers	Other Food
Sr-89	0.18 (0.14-0.22)	0.18 (0.14-0.22)	0.67 (0.50-0.84)	0.18 (0.14-0.22)	0.21 (0.16-0.26)
Sr-90	0.99 (0.97-1.0)	0.99 (0.97-1.0)	1.0	0.99 (0.97-1.0)	0.99 (0.97-1.0)
Cs-134	0.84 (0.63-1.0)	0.84 (0.63-1.0)	0.96 (0.76-1.0)	0.84 (0.63-1.0)	0.85 (0.64-1.0)
Cs-137	0.99 (0.77-1.0)	0.99 (0.77-1.0)	1.0	0.99 (0.77-1.0)	0.99 (0.77-1.0)
I-131	0.0099 (0.0074-0.012)	0.0099 (0.0074-0.012)	0.21 (0.052-0.37)	0.0099 (0.0074-0.012)	0.024 (0.017-0.030)
I-133	0.0	0.0	0.0	0.0	0.0

Table 4.14. Recommended Values for $DCYPCH_{i,j}$ for Crops Not Consumed by Man

Nuclide	Pasture	Stored Forage
All	0.0	0.0

The uniform sampling distribution is recommended for $DCYPCH_{i,j}$.

Discussion

DCYPCH_{i,j} can be defined as

$$\text{DCYPCH}_{i,j} = \frac{\text{INTAKE}_{i,j}}{\text{HARVEST}_{i,j}},$$

where

INTAKE_{i,j} = concentration (Ci/kg) of radionuclide i in crop j when consumed by man

HARVEST_{i,j} = concentration (Ci/kg) of radionuclide i in crop j at harvest

For the variable DCYPCH_{i,j}, it is necessary to determine a value for each crop category and radionuclides considered.

Since neither Pasture nor Stored Forage is consumed directly by man, a value of 0.0 is assigned to the variable DCYPCH for these crop categories over all the nuclides considered.

The values derived by Ostmeyer and Helton [1] were based on the assumption that there was a 14-day delay between harvest and consumption of all crops except grain. Grain was assumed to be put into storage upon harvest and then continuously released for consumption over the course of the year prior to the next harvest.

The revised values were derived by taking a more comprehensive look at the current marketing practices for each crop category. It is acknowledged that processing (canning and freezing) as well as storage will considerably change the delay time from harvest to consumption. A brief discussion follows of the observed practices and the assumptions made for each crop category.

Grains are harvested once a year and placed in storage to be released continuously to produce the edible products. It was assumed that the harvest of any given year would be completely depleted by the time of harvest the following year. This is considered a conservative model for grain usage, since the current stores would indicate that the actual delay time before consumption may well be considerably longer than the assumed delay time. Sweet corn has been included in the grain category to allow using similar transfer factors for the concentration of radionuclides found in the edible portion. This does not disrupt the model for crop usage, since sweet corn represents only 1.5% of the total grains consumed by man. In addition, only 30% of the sweet corn is consumed fresh, and the remaining 70% is processed [2:Table 213]. In effect, processing allows for the same continuous consumption over the year that is used in the model for all grain. It has been further assumed that there is a minimum processing and delivery time of 14 days before the grain products would be available for consumption.

The model used for grains was also used for two other categories of crops: (1) Legumes and Nuts and (2) Roots and Tubers. Continuous consumption for crops in these categories is assumed to begin 14 days after the crop is harvested and extends until the next year's harvest is ready for consumption, that is, until 14 days after the next harvest. The total time over which consumption of these crops occurs is therefore 365 days.

Storage and consumption patterns for the crop categories Green Leafy Vegetables and Other Food fall into three broad categories. Some produce is delivered fresh to market and consumed within 14 days. Some produce is placed in refrigerated storage for up to 6 months. Finally, some produce is undergoes additional processing (i.e., freezing, canning, or drying), which significantly increases its shelf life. For the processed produce, it has been assumed that the processing and delivery to the consumer will require 14 days and that the supply of processed products will be consumed continuously over the course of the next year.

By surveying agricultural data, it can be shown that 70% of the Green Leafy Vegetables will be consumed fresh after approximately a 14-day delay to the consumer. Another 25% of the crop will be placed in refrigerated storage and used over the course of six months. The final 5% will undergo additional processing and be used continuously until the time of the next harvest a year later. This information can be found in Ref. [2]: Table 161, p. 218; Table 244, p. 178; Table 205, p. 152; Table 209, p. 154; Table 246, p. 180.

For the Other Food crop category, a review of agricultural data [2: Tables 246, 258, 277, and 295] shows that 5% will be consumed fresh (after 14 days), while 95% undergoes additional processing that allows continuous utilization over the course of the year prior to the next harvest. This information is taken from Ref. [2]: Table 258, p. 189; Table 295, p. 211; Table 277, p. 199; Table 246, p. 180.

The information on consumption patterns for the various crop categories is summarized in Table 4.15. These percentages are used to evaluate a weighted average for the fraction of radionuclide i present in crop j at harvest that will be consumed by man, $DCYPCH_{i,j}$. Therefore, $DCYPCH_{i,j}$ will be derived as follows:

$$DCYPCH_{i,j} = FF_j \cdot TFF_i + FR_j \cdot TFR_i + FP_j \cdot TFP_i, \quad (4.6)$$

where

FF_j = fraction of crop j consumed fresh within 14 days of harvest

- FR_j = fraction of crop j refrigerated and consumed continuously over a 6-month time period beginning 14 days after harvest,
- FP_j = fraction of crop j processed and continuously consumed over a 1-year time period beginning 14 days after harvest,
- TFF_i = transfer factor that represents the fraction of radionuclide i present at harvest that would ultimately be consumed by man if the entire crop is consumed as fresh produce
- TFR_i = transfer factor that represents the fraction of radionuclide i present at harvest that would ultimately be consumed by man if the entire crop has been refrigerated and then is consumed continuously over 6 months
- TFP_i = transfer factor that represents the fraction of radionuclide i present at harvest that would ultimately be consumed by man if the entire crop undergoes further processing and then is consumed continuously over a period of 1 year

Table 4.15. Consumption Patterns

Crop	Fresh (% eaten after 14-day delay)	Refrigerated (% eaten over 6 mo)	Processed (% eaten over 1 yr)
Grains	0	0	100
Legumes & Nuts	0	0	100
Green Leafy Vegetables	70	25	5
Roots & Tubers	0	0	100
Other Food	5	0	95

All transfer factors that are part of Equation 4.5 are used to describe the fraction of radioactive material present in the edible portion of the crop at the time of harvest and retained following radioactive decay. As was noted earlier, the losses from the processing of food are handled by the parameter FPLSCH.

If an exact delay time between harvest and consumption can be assigned, as has been done for TFF_i, the fraction of radionuclide i present at harvest that is consumed by man would be calculated as follows:

$$TFF_i = \text{EXP} \{ -[(\ln 2 / T_{HALF_i}) \cdot T_{DELAY}] \} \quad (4.7)$$

where

$THALF_i$ = radiological decay half-life for the nuclide i (day^{-1})

$TDELAY$ = time delay between harvest and consumption (day)

If a portion of the crop is stored or preserved for utilization over an extended period, the consumption is considered to be continuous. The transfer factors, TFR and TRP, will be the product of the daily consumption rate of the food and the integral of the rate of transfer over the entire period of time the crop is being consumed. If it is assumed that consumption of the crop occurs at a constant rate over a given time period, T_j , then the consumption rate for crop j , CR_j , is

$$CR_j = 1 / T_j \quad (\text{day}^{-1})$$

Then the transfer factors TFR and TFP can be calculated using the following equation.

$$\begin{aligned} TRF_{i,j} &= TRP_{i,j} = CR_j \int_{T_1}^{T_2} \text{EXP}(-[(\ln 2 / THALF_i) \cdot t]) dt \\ &= \frac{1}{T_j} \cdot \int_{T_1}^{T_2} \text{EXP}(-[(\ln 2 / THALF_i) \cdot t]) dt \\ &= \frac{THALF_i}{T_j \cdot \ln 2} \cdot \left[\text{EXP} \left[-\frac{\ln 2}{THALF_i} \cdot T_2 \right] - \text{EXP} \left[-\frac{\ln 2}{THALF_i} \cdot T_1 \right] \right] \quad (4.8) \end{aligned}$$

where

T_j = length of the consumption period (day)

CR_j = consumption rate for crop j (day^{-1}) = $\frac{1}{T_j} = \frac{1}{T_2 - T_1}$

$THALF_i$ = radiological decay half-life for nuclide i (day)

T_1 = the shortest time after harvest that crop j will be consumed (days)

T_2 = the longest time after harvest that the crop will be consumed (days)

The values of T_j , T_1 , and T_2 used for the various consumption patterns are given in Table 4.16.

Table 4.16. Values for Time Variables

<u>Time</u>	<u>Foods Consumed Fresh</u>	<u>Foods Refrigerated and Consumed Over 6 Months</u>	<u>Foods Processed and Consumed Over 1 Year</u>
T_1	0	14	14
T_2	14	197	379
T_j	14	183	365

The range of possible values in each case was arrived at by assuming that the best estimate values being used are most probably accurate to within 25% of their actual value.

4.3.5 DCYPMH

$DCYPMH_i$ = fraction of radionuclide i present in milk at the time of production that is retained in the milk until the time of consumption by man (accounts for losses from both radioactive decay and processing)

The recommended values for $DCYPMH_i$ are as in Table 4.17.

Table 4.17. Recommended Values for $DCYPMH_i$

<u>Nuclide</u>	<u>DCYPMH</u>	<u>Range of Values</u>
Sr-89	0.66	0.50-0.83
Sr-90	1.0	
Cs-134	1.0	
Cs-137	1.0	0.21-0.35
I-131	0.28	
I-133	0.002	
		0.0015-0.0025

The uniform sampling distribution is recommended for DCYPMH.

Discussion

$DCYPMH_i$ can be defined as

$$DCYPMH_i = \frac{FINAL_i}{INITIAL_i}$$

where

$FINAL_i$ = concentration (Ci/L) of radionuclide i in milk at the time of consumption by man

$INITIAL_i$ = concentration (Ci/L) of radionuclide i in milk at the time it is produced

Values for this variable are found for each nuclide treated by the food pathways model by evaluating the following expression

$$DCYPMH_i = \text{EXP} \{ -[(\ln 2 / THALF_i) \cdot TDELAY] \}$$

where

$THALF_i$ = radiological half-life of nuclide i (days)

$TDELAY$ = delay time between the production and consumption of the dairy product (days)

The values first used for this variable were obtained by the assuming that all milk produced was consumed as fluid. Furthermore, a delay time ($TDELAY$) of four days was used as recommended in the Regulatory Guide 1.109 [7:Table E-15].

An investigation of the utilization of milk in the United States [2:Table 480] showed that milk products could be divided into three groups according to their shelf-life. These groups, the milk products included in each group, and the percentage of the total amount of milk that is accounted for by each group are shown in Table 4.18.

Since the products with the long shelf-life represent such a small percentage of the total milk produced, it was decided to combine it with those products having an intermediate shelf-life and to consider the entire group as having an intermediate shelf-life.

The derivation of the values for $DCYPMH_i$ now takes the form:

$$DCYPMH_i = FR_S \cdot \text{EXP} \left[- \frac{\ln 2}{THALF_i} \cdot T_S \right] + FR_L \cdot \text{EXP} \left[- \frac{\ln 2}{THALF_i} \cdot T_L \right] \quad (4.9)$$

where

- FR_S = fraction of milk production used in products with a short shelf-life
- FR_I = fraction milk production used in products with an intermediate shelf-life (including long shelf-life products)
- T_S = delay time between production of milk and consumption of those products with a short shelf-life (days)
- T_I = delay between production of milk and consumption of those products with an intermediate shelf-life (days)
- THALF_I = as defined previously (days)

Delay times needed to be established for the two groups. Milk consumed as a fluid accounts for nearly 80% of those products with a short shelf-life. Therefore, milk was assumed to be representative of short-shelf life products. It was found through the Associated Milk Producers that 2 or 3 days are required to get the milk to the shelf, and that a freshness date of at least 2 weeks is applied at the time of packaging, 1 or 2 days following production. Based on this information, the 4-day delay time originally used to calculate DCYPMH seemed somewhat short for this product group. A modified delay time of 7 days was, therefore, used to derive the current values of DCYPMH. Still, it seems likely that even the revised delay time may be too short.

Cheese and butter dominate the product group with intermediate shelf-life (which now also includes canned and dehydrated products). Cheese accounts for

Table 4.18. U.S. Milk Utilization

Group	Products	Total Production (%)
Short Shelf-Life	Fluid Milk Cottage Cheese Bulk Condensed Milk Ice Cream	49
Intermediate Shelf-Life	Cheese American Other Butter	49
Long Shelf-Life	Canned Milk Dry Milk Other Dehydrated Products	2

59% of the milk used for these products, and butter accounts for 37%. After curing for at least 60 days, cheese is given a freshness date of 60 days at the time of packaging. Butter, on the other hand, takes 5 or 6 days to produce, is readily frozen, which greatly enhances its shelf-life, and is given a freshness date of 60 days at the time of packaging. Using this information, it was decided to use value for the delay time for these products of 65 days.

In summary, the data in Table 4.19 were used to determine the value of the variable $DCYPMH_i$ for each nuclide i using Equation 4.9.

Table 4.19. Consumption Intervals for Milk Products

Product Group	Milk Production (%)	Delay Time (Days)*
Short Shelf-Life	50	7
Intermediate Shelf-Life	50	65
* Time from production to consumption.		

It has been assumed for the nuclides with relatively long half-lives that the entire amount of radioactivity present at the time of production will in fact be consumed.

The range of possible values for $DCYPMH$ was derived based on the estimate that the actual value would probably lie within 25% of the calculated value.

4.3.6 FPLSCH

$FPLSCH_{i,j}$ = fraction of radionuclide i present in crop j at harvest that is retained until consumption by man (does not account for losses from radioactive decay, which are handled separately by the parameter $DCYPCH$)

The recommended values for $FPLSCH$ are summarized in Tables 4.20 and 4.21. A uniform sampling distribution is recommended for $FPLSCH$.

Discussion

The variable $FPLSCH_{i,j}$ can be defined as follows:

$$FPLSCH_{i,j} = \frac{FINAL_{i,j}}{INITIAL_{i,j}}$$

where

$FINAL_{i,j}$ = concentration (Ci/kg) of radionuclide i in the edible portion of crop j at consumption by man when there are no losses caused by radioactive decay

$INITIAL_{i,j}$ = concentration (Ci/kg) of radionuclide i in the edible portion of crop j at harvest

Since neither pasture nor stored forage is consumed by man, each of these crops are assigned a processing retention factor of 0.0 over all nuclides. Processing loss factors for crops consumed by man were developed using data compiled by Boone et al. [8].

Table 4.20. Recommended Values for $FPLSCH_{i,j}$ for Crops Consumed by Man

<u>Nuclide</u>	<u>Grains</u>	<u>Legumes & Nuts</u>	<u>Green Leafy Vegetables</u>	<u>Roots & Tubers</u>	<u>Other Food</u>
Sr-89	0.25 (0.19-0.31)	0.8 (0.6-1.0)	0.5 (0.38-0.63)	0.8 (0.6-1.0)	0.71 (0.53-0.89)
Sr-90	0.25 (0.19-0.31)	0.8 (0.6-1.0)	0.5 (0.38-0.63)	0.8 (0.6-1.0)	0.71 (0.53-0.89)
Cs-134	0.25 (0.19-0.31)	0.8 (0.6-1.0)	0.5 (0.38-0.63)	0.8 (0.6-1.0)	0.71 (0.53-0.89)
Cs-137	0.25 (0.19-0.31)	0.8 (0.6-1.0)	0.5 (0.38-0.63)	0.8 (0.6-1.0)	0.71 (0.53-0.89)
I-131	0.33 (0.25-0.41)	0.8 (0.6-1.0)	0.5 (0.38-0.63)	0.8 (0.6-1.0)	0.71 (0.53-0.89)
I-133	0.33 (0.25-0.41)	0.8 (0.6-1.0)	0.5 (0.38-0.63)	0.8 (0.6-1.0)	0.71 (0.53-0.89)

Table 4.21. Recommended Value of $FPLSCH_{i,j}$ for Crops Not Consumed by Man

	<u>Pasture</u>	<u>Stored Forage</u>
All nuclides	0.0	0.0

The retention factor for grain is quite low because of the high degree of refinement of grains during the production of the refined products that dominate the per capita consumption of grain. This retention factor may be expected to increase as eating patterns change toward whole grain products as witnessed recently.

On the other hand, in the processing of legumes and nuts, the edible portion is consumed without such refinement. Therefore, all crops in this category except snap beans have a retention factor of 1.0. The edible pod of the snap bean is exposed to the environment during the growing season and will therefore be contaminated directly, and the bean itself will be contaminated by translocation. According to Boone et al. [10], only 50% of the radioactive material present at harvest will be retained in the bean after processing. Snap bean consumption accounts for approximately 40% of the human intake from this crop category. A weighted averaging approach was used in arriving at the overall retention factor for the legume and nut crops. That is,

$$FPLSCH = (0.60)(1.0) + (0.40)(0.50) = 0.80$$

For green leafy vegetables, translocation is not an important factor in the contamination resulting from direct deposition. Furthermore, half the radioactive material present on the edible portions of green leafy vegetables will be removed during washing and cooking.

Part of the contamination of the roots and tubers is from direct contact with contaminated soil, but translocation transfers an even greater amount of radioactive material from above-ground plant parts into the roots. Washing and peeling will remove the material in the skin of these vegetables, but processing will not decrease the amount of translocated material.

The Other Food category consists primarily of a wide variety of fruits and vegetables that can be grouped into three broad subcategories, each of which has a characteristic retention factor for radioactivity after processing:

- (1) Foods that have a rind or peel not considered to be edible and therefore removed before consumption. Examples are citrus fruits and melons. The contamination in the edible portion of the plant consists of material translocated to the flesh of the fruit. Retention fraction = 0.80
- (2) Fruits and vegetables that are contaminated by direct deposition and also contain radioactive material translocated to the interior portion of the fruit. The entire harvested portion of the crop is edible (for example, apples, pears, etc.). Since the skin is smooth and the fruit will be washed before consumption, much of the radioactive material present at the time of harvest will be removed. Retention fraction = 0.50
- (3) Tomatoes are especially susceptible to translocation to all edible portions, including the seeds. Therefore, even though their skin is smooth and easily washed, the retention fraction is greater than for the fruits and vegetables in subgroup 2. Retention fraction = 0.80

Approximately 70% of the crops in this category have a retention factor of 0.80, while the other 30% have a retention factor of 0.50. By weighting these two groups appropriately, an overall retention factor can be calculated as $FPLSCH = 0.70 (0.80) + 0.30 (0.50) = 0.7$.

The ranges of values were found by assuming that the calculated value is most probably correct to 25%.

4.3.7 FRCTCB, FRCTCH, FRCTCM

$FRCTCB_j$ = fraction of crop j consumed by meat-producing animals,

$FRCTCH_j$ = fraction of crop j consumed by man,

$FRCTCM_j$ = fraction of crop j consumed by milk-producing animals.

The recommended values for FRCTCH, FRCTCM, and FRCTCB are as given in Table 4.22. When sampling is to be done over the range of possible values, it is recommended that a uniform sampling distribution be assumed.

Table 4.22. Values for FRCTCH, FRCTCM, and FRCTCB

Crop	FRCTCH	FRCTCM	FRCTCB
Pasture	0.0	0.10 (0.075-0.125)	0.90 (0.875-0.925)
Stored Forage	0.0	0.13 (0.098-0.16)	0.87 (0.84-0.902)
Grain	0.35 (0.26-0.44)	0.040 (0.030-0.050)	0.61 (0.51-0.71)
Legumes and Nuts	0.24 (0.18-0.30)	0.046 (0.035-0.058)	0.714 (0.642-0.785)
Green Leafy Veg.	1.0	0.0	0.0
Roots & Tubers	1.0	0.0	0.0
Other Food	1.0	0.0	0.0

The recommended values were derived by analyzing current agricultural statistics [2] and using the summary of livestock ingestion rates as summarized by Boone et al. [8] as adapted from Ng [9]. A partial list of the reference tables [1] used to compile the data for the various crops and animals is given in Table 4.23. Since the health effects in MACCS are considered in the societal sense, the products exported are also included in defining the amounts of each crop category consumed by man and by animals. With the exception of soybeans, it has been assumed that utilization of the part of the crop exported follows the same pattern as domestic utilization. On the other hand, the utilization pattern for domestic use versus the

Table 4.23. Crop Utilization Patterns

Crop	Domestic		Export		Ref. 1	
	Food (lbs)	Feed (lbs)	Food (lbs)	Feed (lbs)	Table	Page
Wheat	3.75x10 ¹⁰	2.70x10 ¹⁰	4.87x10 ¹⁰	3.53x10 ¹⁰	5	4
Rye	1.96x10 ⁸	8.40x10 ⁸	1.06x10 ⁷	4.54x10 ⁷	19	16
Barley	8.35x10 ⁹	1.33x10 ¹⁰	1.70x10 ⁹	2.66x10 ⁹	58	44
Sorghum	5.60x10 ⁸	2.18x10 ¹⁰	3.50x10 ⁸	1.37x10 ¹⁰	67	51
Oats	2.50x10 ⁹	1.49x10 ¹⁰	8.96x10 ⁶	5.50x10 ⁷	50	39
Rice	5.58x10 ⁹	0.0	6.50x10 ⁹	0.0	28	20
Corn	2.73x10 ¹⁰	1.09x10 ¹¹	1.04x10 ¹⁰	4.14x10 ¹⁰	41	31
Sweet Corn	2.89x10 ⁹	0.0	0.0	0.0	213	157
Soybeans	7.18x10 ⁹	6.46x10 ¹⁰	1.89x10 ¹⁰	3.52x10 ¹⁰	170	127
Peanuts	1.52x10 ⁹	5.81x10 ⁸	7.26x10 ⁷	2.82x10 ⁷	160	121
Snap beans	1.27x10 ⁹	0.0	0.0	0.0	204	151
Peas	3.65x10 ⁸	0.0	0.0	0.0	223	163
Dried beans	1.55x10 ⁹	0.0	0.0	0.0	376	255
Nuts	5.19x10 ⁸	0.0	0.0	0.0	343	237
					345	237
					348	238
					351	240

utilization pattern for exported soybeans is significantly different. According to the American Soybean Association the patterns of soybean utilization are as indicated in Table 4.24.

Table 4.24. Crop Utilization

<u>Market</u>	<u>Food (%)</u>	<u>Feed (%)</u>
Domestic	10	90
Export	35	65

These utilization patterns for soybeans have been incorporated into Table 4.22, the summary table of crop utilization.

Using the summary data for crop utilization within the general categories of Grains and Legumes & Nuts, overall utilization can be summarized as in Table 4.25.

Table 4.25. Utilization of Grains, Legumes, and Nuts

<u>Crop Category</u>	<u>Food (%)</u>	<u>Feed (%)</u>
Grains	35	65
Legumes & Nuts	24	76

Boone et al. [8] compiled a summary of the daily consumption rates of various animals for a variety of crops. The rates for cattle, hogs, chickens, and dairy cattle from this summary are given below. In addition, a consumption rate for turkeys has been added, since they are being considered as part of the crop-meat-man pathway. To obtain a daily consumption rate for turkeys, the following assumptions were made:

- (1) Turkeys and chickens have similar biological and metabolic characteristics.
- (2) Similar amounts of feed will produce a similar weight-gain in both types of poultry.
- (3) The diet of both chickens and turkeys are similar in content.

As a result of these assumptions and the use of weight-at-slaughter statistics, it was determined that the daily consumption of a turkey is 2.6 times the daily consumption of a chicken. This factor was then used to determine the daily consumption rate for turkeys of the various crops based on the daily consumption by chickens. An overall summary of the daily consumption rates (lbs/day) is summarized in Table 4.26.

Table 4.26. Daily Consumption Rates of Feeds by Animals
in Pounds per Day

Feed	Cattle				
	Dairy	Beef	Hogs	Chickens	Turkeys
Pasture	8.55	8.55	0.0	0.0	0.0
Hay	14.90	10.80	0.0	0.0	0.0
Corn Silage	5.84	4.54	0.0	0.0	0.0
Sorghum Silage	1.33	0.966	0.0	0.0	0.0
Wheat	0.0509	0.0375	0.0675	0.00126	0.00328
Oats	0.131	0.0970	0.175	0.00328	0.00854
Rye	0.0888	0.0653	0.118	0.00232	0.00603
Barley	0.0372	0.0274	0.492	0.000922	0.00240
Sorghum	0.0599	0.0441	0.0794	0.00149	0.00387
Corn	4.48	3.30	5.92	0.111	0.289
Soybeans	1.06	0.783	1.41	0.0265	0.688
Peanuts	0.00992	0.00729	0.00131	0.000246	0.000640

Since the consumption rates for the different types of animals are given on a daily basis, it is necessary to determine how many of each type of animal there are on any given day to determine the total daily consumption by all such animals. For dairy cows and beef cattle, statistical data [2] provide those numbers. However, in the case of hogs and poultry, the age of the animal at the time of slaughter is less than one year. Therefore, for hogs and poultry, the "standing crop" (i.e., the number extant) on any given day is less than the total number produced during the year and is found by dividing the total number produced annually by the "number of crops per year", where

$$\text{Number of crops per year} = \frac{12 \text{ months}}{\text{Age at time of slaughter (mo)}}$$

A summary of the "standing crop" for each type of food-producing animal is given in Table 4.27.

By multiplying the daily consumption rate for a particular species of animal by the "standing crop" of that species, the total daily consumption of that crop by that type of animal can be found. With this total daily consumption for each crop category, it is then possible to determine the percentage of each crop category consumed by each species of food-producing animal. The

percentages obtained are given in Table 4.28. Finally, by using Table 4.25 in conjunction with Table 4.28, it is possible to arrive at the fraction of the crop which is consumed by man, dairy animals, and meat-producing animals.

The range of possible values was derived by assuming that the smallest fraction would most probably not vary by more than 25% of its calculated value. The variation for the larger fractions was then calculated such that

Table 4.27. "Standing Crops" (Animals)

<u>Animal</u>	<u>Total No. During Year</u>	<u>Age at Slaughter (mo)</u>	<u>Number of "Crops"</u>	<u>Standing Crop</u>	<u>Table</u>	<u>Page</u>
Cattle						
Dairy	1.114x10 ⁷	24	1.0	1.114x10 ⁷	388	261
Beef	1.029x10 ⁸	96	1.0	1.029x10 ⁸	388	261
Hogs	9.847x10 ⁷	6	2.4	4.103x10 ⁷	407	276
Chickens	4.415x10 ⁹	3	4.0	1.104x10 ⁹	508	358
					511	360
Turkeys	1.698x10 ⁸	6	2.0	8.490x10 ⁷	524	367

Table 4.28. Crop Consumption by Animal

<u>Crop Category</u>	<u>Cattle</u>		<u>Hogs (%)</u>	<u>Chickens (%)</u>	<u>Turkeys (%)</u>
	<u>Dairy (%)</u>	<u>Beef (%)</u>			
Pasture	10	90	0	0	0
Stored Forage	13	87	0	0	0
Grain	6	42	30	15	6
Legumes & Nuts	6	43	31	16	4
Green Leafy	0	0	0	0	0
Vegetables					
Roots & Tubers	0	0	0	0	0
Other Food	0	0	0	0	0

the ranges would be proportional to their sizes, but would not allow the total consumption of any crop to exceed 100%.

4.3.8 TCROOT

$TCROOT_{i,j}$ = fraction of the nuclide i deposited onto soil used to grow crop j that will ultimately be consumed by man as a result of the long-term uptake by plant roots or by direct consumption of the soil by grazing animals.

Table 4.29 shows the recommended values for $TCROOT_{i,j}$ for the Sr and Cs nuclides and Table 4.30 shows the recommended values for $TCROOT_{i,j}$ for the I nuclides.

Table 4.29. Recommended Values for $TCROOT_{i,j}$ for Sr and Cs Nuclides

Crop	Sr-89	Sr-90	Cs-134	Cs-137
Pasture	0.00041 (0.00030- 0.00051)	0.026 (0.014- 0.049)	0.0013 (0.0010- 0.0016)	0.0069 (0.0047- 0.0102)
Stored Forage	0.0013 (0.00095- 0.0016)	0.090 (0.05- 0.17)	0.00071 (0.00048- 0.0010)	0.0015 (0.00092- 0.0027)
Grain	0.000043 (0.000033- 0.000053)	0.0033 (0.0019- 0.0063)	0.000035 (0.000024- 0.000051)	0.000076 (0.000046- 0.00013)
Legumes	0.00037 (0.00028- 0.00047)	0.028 (0.016- 0.054)	0.000093 (0.000062 0.00014)	0.00020 (0.00012- 0.00035)
Green Leafy Vegetables	0.00017 (0.00013- 0.00021)	0.013 (0.0071- 0.024)	0.000014 (0.0000094- 0.000020)	0.000030 (0.000018- 0.000051)
Roots & Tubers	0.00011 (0.000083- 0.00014)	0.0084 (0.0047- 0.0016)	0.000056 (0.000038- 0.000080)	0.00012 (0.000072- 0.00021)
Other Food	0.000008 (0.0000063- 0.00041)	0.00066 (0.00036- 0.0013)	0.00011 (0.000071- 0.00015)	0.00023 (0.00014- 0.00041)

Table 4.30. Recommended Values for
TCROOT_{i,j} for I Nuclides

<u>Crop</u>	<u>I-131</u>	<u>I-133</u>
Pasture	0.000016	0.0000017
All others	0.0	0.0

A uniform sampling distribution is recommended for TCROOT_{i,j}.

Discussion

$$\text{TCROOT}_{i,j} = \text{IRU}_{i,j} + \text{ISI}_{i,j} \quad (4.10)$$

where

IRU_{i,j} = time-integrated root uptake rate for nuclide i deposited onto soil
used to grow crop j

ISI_{i,j} = time-integrated soil ingestion rate for nuclide i deposited onto
pasture

The principal mechanism by which nuclides are transferred from soil to plants is via root uptake. Transfer to plant surfaces may also occur by rainsplash and by the deposition of materials resuspended from surface soil. A rate at which nuclides are transferred from the soil to plants via each of these mechanisms can be established. The overall transfer rate is then just the weighted sum of these individual rates.

For the pasture, an additional term is used in deriving the data for TCROOT. To account for the fact that grazing cattle will ingest a certain amount of soil along with the plant material they consume, a time-integrated soil ingestion factor is added to the time-integrated root uptake rate. It is assumed that pasture undergoes continuous harvest (grazing by animals) and that all nuclides deposited onto pasture will be consumed by the end of the growing season. Therefore, the transfer factors (DCYPCB and DCYPCM) for nuclides deposited onto pasture and consumed by meat- or milk-producing animals is unity. The overall transfer factor for soil ingestion by grazing animals can be obtained by treating the ingestion of soil by grazing animals as though the ingested soil was first transferred to the surface of pasture grass then and consumed. The soil ingestion component, ISI, of the transfer factor TCROOT will be 0.0 for all crops except pasture.

According to Ostmeyer and Helton [1], the rate of transfer from soil to plants by either rainsplash or resuspension is negligible compared the rate of transfer via root uptake. The values for TCROOT were thus derived using only root uptake transfer factors.

If the nuclides deposited onto the soil were to remain at a constant level over time, the long-term transfer factor would simply be the product of the annual uptake rate and the length of time being considered. However, in actuality, the availability of the deposited material decreases over time. This decrease is a reflection of the following physical and chemical processes: (1) radioactive decay, (2) percolation of material to the region below the root zone, (3) irreversible chemical binding of the nuclides to components of the soil, (4) previous root uptake of nuclides, and (5) soil ingestion by grazing animals.

Because the availability of the material does not remain constant, it is necessary to integrate the uptake rate over time. If an exponential depletion rate is assumed, then the time-integrated root uptake transfer factor, IRU, can be expressed as

$$IRU_{i,j} = RU_{i,j} \cdot \int_0^T \text{EXP}\{-[(RU_{i,j} + RD_i + RP_i + RB_i + RSI_{i,j}) \cdot t]\} dt \quad (4.11)$$

where

$RU_{i,j}$ = rate at which nuclide i is incorporated into the edible portion of crop j via root uptake from the soil (yr^{-1})

RD_i = radiological decay rate for nuclide i (yr^{-1})

RP_i = rate at which nuclide i percolates to a region below the root zone (yr^{-1})

RB_i = rate at which nuclide i chemically binds irreversibly with soil components (yr^{-1})

$RSI_{i,j}$ = rate at which nuclide i is removed via soil ingestion from the soil used to grow crop j (yr^{-1})

T = the time period of interest for the transfer of deposited nuclides via root uptake from the soil to the edible portion of the plant (yr)

The time-integrated soil ingestion factor is obtained in an analogous manner with several differences. Soil ingestion occurs only from the surface soil, and therefore, the unavailability of material for ingestion by grazing cattle relates to the "loss" of the material from surface soil. Several factors contribute to the unavailability of material for ingestion. They are radiological decay, percolation of the nuclides out of the surface soil, removal of material via root uptake, and removal of material via ingestion by grazing animals.

Even though irreversible chemical binding may occur to the soil in the surface soil compartment (the top 1 cm), this irreversibly bound material is still available to be ingested. Therefore, the rate at which chemical binding occurs does not appear in the derivation of the transfer factor, ISI. ISI can be derived as follows:

$$ISI_{i,j} = RSI_{i,j} \cdot \int_0^T \text{EXP}\{-[(SRU_{i,j} + RD_i + SRP_i + RSI_{i,j}) \cdot t]\} dt \quad (4.12)$$

where

$RSI_{i,j}$ = rate at which nuclide i is removed via soil ingestion from the surface soil compartment on land used to grow crop j (yr^{-1})

$SRU_{i,j}$ = rate at which nuclide i is incorporated into the edible portion of crop j via root uptake from the surface soil compartment (yr^{-1})

RD_i = radiological decay rate for nuclide i (yr^{-1})

SRP_i = rate at which nuclide i percolates to a region below the surface soil compartment (yr^{-1})

T = the time period of interest for the transfer of deposited nuclides via soil ingestion of soil on which pasture is grown (yr)

When the time period of concern for the long-term doses arising from the food pathway is taken to be all time following the accident (i.e., letting $T = \infty$), $TCROOT_{i,j}$ will be evaluated as follows:

$$TCROOT_{i,j} = IRU_{i,j} + ISI_{i,j}$$

and

$$TCROOT_{i,j} = \frac{RU_{i,j}}{RU_{i,j} + RD_i + RP_i + RB_i + RSI_{i,j}} + \frac{RSI_{i,j}}{SRU_{i,j} + RD_i + SRP_i + RSI_{i,j}} \quad (4.13)$$

The values for $RU_{i,j}$ are derived from fallout data. Root uptake by plants is usually described using an empirical concentration ratio (CR) defined as

$$CR = \frac{\text{Radionuclide activity per unit mass (dry) of plant (Bq/kg)}}{\text{Radionuclide activity per unit mass (dry) of soil (Bq/kg)}}$$

The root uptake rate, RU, is then defined as

$$RU_{i,j} = CR_{i,j} \cdot \frac{CM_j}{SM}$$

where

CM_j = annual yield of crop j (kg yr⁻¹ /m²)

SM = soil mass in root uptake compartment (kg/m²)

The soil mass (SM) is taken to be an average value of 240 kg/m².

A summary of concentration ratios can be found in Till and Meyer [10:Table 5.17], and a summary of crop yield values can be found in Boone et al. [8]. A value for CM for each crop category is obtained by a weighted average over the predominant crops in each category. The values used for CR and CM for Sr and Cs nuclides are given in Table 4.31. The CR values for the short-lived I nuclides are assumed to be 0.0, which in turn implies that the IRU values for the I nuclides is 0.0 for all crops.

Table 4.31. Values for Concentration Ratios (CR) and Crop Yield Values (CM)

Crop	CR		CM
	Strontium	Cesium	(kg/yr•m ²)
Pasture	2.0	0.01	0.175
Stored Forage	3.0	0.2	0.50
Grains	0.2	0.02	0.25
Legumes	2.0	0.06	0.22
Green Leafy Veg.	2.0	0.02	0.10
Roots & Tubers	0.5	0.03	0.26
Other Foods	0.2	0.03	0.05

By using these values for CR and CM, the corresponding values for RU were established. These RU values are summarized in Table 4.32. The range of

values derived by assuming that the correct value would lie within 25% of the value estimated for RU.

Table 4.32. Values for Root Uptake (RU)

Crop	RU		
	Strontium	Cesium	Iodine
Pasture	0.0015 (0.0011-0.0019)	0.0000073 (0.0000054-0.0000091)	0.0
Stored Forage	0.0063 (0.0047-0.0079)	0.00042 (0.00032-0.00053)	0.0
Grain	0.00021 (0.00016-0.00026)	0.000021 (0.000016-0.000026)	0.0
Legumes	0.0018 (0.0014-0.0023)	0.000055 (0.000041-0.000069)	0.0
Green Leafy Vegetables	0.00083 (0.00062-0.0010)	0.0000083 (0.0000062-0.000010)	0.0
Roots & Tubers	0.00054 (0.00041-0.00068)	0.000033 (0.000025-0.000041)	0.0
Other Foods	0.000042 (0.000031-0.000053)	0.000063 (0.000047-0.000079)	0.0

The rate at which nuclide i becomes unavailable for root uptake from radioactive decay, RD_i , can be defined as

$$RD_i = \ln 2 / THALF_i$$

where

$THALF_i$ = radiological half-life of nuclide i (yr)

Because radioactive half-lives are precisely known, no range of values has been established for RD_i . The values of RD_i are summarized in Table 4.33.

The percolation rate is strongly dependent on soil characteristics; therefore, these values are quite uncertain. The range of possible values was established by assuming that the actual value would most likely lie within 25% of the predicted value. The half-lives of the iodine isotopes considered are so short that radioactive decay is the primary mechanism by which these

nuclides become unavailable for root uptake. Thus, no percolation rate has been established for iodine nuclides.

Table 4.33. Values for Radioactive Decay

<u>Nuclide</u>	<u>RD</u>
Sr-89	4.860
Sr-90	0.024
Cs-134	0.340
Cs-137	0.023
I-131	31.500
I-133	292.000

The percolation rates, RP, for strontium and cesium established by Hoffman and Baes [11] are summarized in Table 4.34.

Table 4.34. Percolation Rate for Sr and Cs

<u>Element</u>	<u>RP</u>
Strontium	0.0021
Cesium	0.0096

In addition, the derived values for RP apply to the entire root zone (the top 15 cm of soil compartment). Since the surface soil compartment is assumed to reach a depth of 1 cm, the value of SRP, the percolation rate for the surface soil compartment, could be assumed to be one-fifteenth of the value RP established for the root zone. This does not seem too unreasonable, since the percolation distance would be one critical factor in the percolation rate. Still, this approximation may be somewhat conservative, since the surface soil compartment is much more susceptible to weathering than is the root uptake soil compartment.

Table 4.35 gives a summary of the values for RP, the percolation rate from the root uptake zone, and SRP, the percolation rate from the surface soil compartment.

Table 4.35. Values for ITF and ISI

<u>Element</u>	<u>ITF</u>	<u>ISI</u>
	<u>RP</u>	<u>SRP</u>
Strontium	0.0096 (0.0072-0.012)	0.14 (0.11-0.18)
Cesium	0.0021 (0.0016-0.0026)	0.032 (0.024-0.040)

Ostmeyer and Helton [1] established the rate of soil ingestion, RSI, for all nuclides for pasture. Since no soil ingestion occurs during the harvest of the nonpasture crops, the corresponding values of RSI is 0.0 yr^{-1} . Table 4.36 shows the values for RSI for all nuclides.

Table 4.36. Values for RSI for All Nuclides

<u>Crop</u>	<u>RSI</u>
Pasture	0.0005 (0.0004-0.0006)
Nonpasture	0.0

The range of possible values for the soil ingestion rate was established by assuming the actual value would most probably lie within 25% of the estimated value.

4.3.9 TFBF

TFBF_i = fraction of the daily consumption of nuclide i by meat-producing animals that remains in the meat at the time of slaughter

Table 4.37 shows the recommended values for TFBF_i . A uniform sampling distribution is recommended for TFBF_i .

Discussion

$$\text{TFBF}_i = \frac{\text{OUTPUT}_i}{\text{EATEN}_i}$$

Table 4.37. Recommended Values for $TFBF_i$

<u>Nuclide</u>	<u>TFBF</u>	<u>Range of Values</u>
Sr-89	0.00022	0.000094 - 0.00038
Sr-90	0.00022	0.000094 - 0.00038
Cs-134	0.023	0.020 - 0.035
Cs-137	0.024	0.020 - 0.035
I-131	0.0024	0.00082 - 0.0037
I-133	0.0011	0.00041 - 0.0013

where

$OUTPUT_i$ = amount of radionuclide i in meat produced by meat animals (C_i)

$EATEN_i$ = amount of radionuclide i in feed consumed by meat animals (C_i)

The value of this transfer factor is derived by evaluating the following expression:

$$TFBF_i = TR \cdot M \cdot ETF_i,$$

where

TR = fraction of animals slaughtered per day (day^{-1})

M = quantity of meat produced by those animals at slaughter (kg)

ETF_i = equilibrium transfer factor to meat for the radionuclide i (day/kg)

Previously, $TFBF_i$ was calculated using only beef in the calculations. By using recent agricultural data [2:Tables 455 and 516], it can be shown that beef accounts for only 42% of the meat produced, pork an additional 29%, and poultry the final 29%. The amount of poultry produced is composed of 84% chicken and 16% turkey. In light of these data, it was decided to consider all three meat sources (beef, pork, and poultry) in deriving a value for $TFBF$.

A transfer factor is obtained for each of these meat sources and an overall transfer is developed by taking a weighted average of these animal-specific transfer factors. That is,

$$TFBF_i = FB \cdot TFB_i + FPK \cdot TFPK_i + FC \cdot TFC_i + FT \cdot TFT_i$$

where

FB = fraction of meat produced that is beef (i.e., 0.42)

FPK = fraction of meat produced that is pork (i.e., 0.29)

FC = fraction of meat produced that is chicken (i.e., 0.24)

FT = fraction of meat produced that is turkey (i.e., 0.05)

TFB_i = transfer factor for nuclide i by beef

$TFPK_i$ = transfer factor for nuclide i by pork

TFC_i = transfer factor for nuclide i by chicken

TFT_i = transfer factor for nuclide i by turkey

Equilibrium transfer factors (ETF_i) for Sr, Cs, and I were derived by Ng et al. [12] and are presented in Table 4.38.

Table 4.38. Equilibrium Transfer Factors (ETFs)

<u>Element</u>	<u>Animal Product</u>	<u>ETF</u>	<u>Range of Values*</u>
Sr	Beef	0.00030	0.000064 - 0.00057
	Pork	0.0029	0.0012 - 0.0040
	Poultry	0.032	0.018 - 0.080
Cs	Beef	0.020	0.0072 - 0.093
	Pork	0.30	0.26 - 0.38
	Poultry	4.4	4.3 - 4.5
I	Beef	0.0072	0.0072 - 0.020
	Pork	0.027	0.0010 - 0.027
	Poultry	0.20	0.0080 - 0.20

* The range of possible values was established by Ng.

Due to the physiological similarity between different poultry types, the ETF_i values established by Ng for chicken have been used for both chicken and turkey.

These ETF_i values were derived for stable strontium and cesium and for I-131, and therefore represent biological losses for strontium and cesium but not radioactive decay losses. For iodine, the radioactive decay constant for I-131 has been included. For I-133, it is therefore necessary to adjust value of TF to reflect the significantly shorter half-life of this isotope.

To find an adjusted ETF value to incorporate specific radioactive decay rates, it is possible to begin with the assumption that

$$\frac{dQ_i(t)}{dt} = \frac{R_i}{M} - \lambda_i \cdot Q_i(t) \quad (4.14)$$

where

$Q_i(t)$ = concentration of the nuclide i in the meat at time t (Ci/kg)

R_i = ingestion rate for nuclide i (Ci/day)

M = the total weight of the meat in an animal at the time of slaughter (kg)

λ_i = decay constant reflecting both radiological decay and biological losses of nuclide i (day^{-1})

Therefore,

$$\frac{dQ_i(t)}{\lambda_i Q_i(t) - \frac{R_i}{M}} = - dt \quad (4.15)$$

By letting $u = \frac{R_i}{M} - \lambda_i Q_i(t)$ then $\frac{du}{dQ_i(t)} = -\lambda_i$ and $\frac{du}{-\lambda_i} = dQ_i(t)$

Therefore, by substitution into Equation 4.15

$$\frac{du}{\lambda_i u} = - dt \quad \text{and} \quad \frac{\ln(\lambda_i u)}{\lambda_i} = -t + C \quad \text{and} \quad \ln(\lambda_i u) = -\lambda_i t + C$$

$$\text{then } \lambda_i u = e^{-\lambda t} + C = e^C e^{-\lambda t} \quad \text{and} \quad u = \frac{e^C}{\lambda_i} e^{-\lambda t}$$

Therefore,

$$\frac{R_i}{M} - \lambda_i Q_i(t) = \frac{e^C}{\lambda_i} e^{-\lambda t} \quad \text{and} \quad Q_i(t) = \frac{R_i}{\lambda_i M} + \frac{e^C}{\lambda_i^2} e^{-\lambda t}$$

and in the equilibrium state

$$ETF_i = \lim_{t \rightarrow \infty} Q_i(t) = \frac{R_i}{\lambda_i M} \quad (4.16)$$

Since

$$ETF_i = \frac{Q_i(t)}{R_i} = \frac{\text{Concentration of nuclide } i \text{ in meat (Ci/kg)}}{\text{Daily ingestion rate of nuclide } i \text{ by the animal (Ci/day)}}$$

in the equilibrium state, it follows from Equation 4.16 that

$$ETF_i = \frac{Q_i(t)}{R_i} = \frac{\frac{R_i}{\lambda_i M}}{R_i} = \frac{1}{\lambda_i M} \quad (4.17)$$

For ETF_i as derived by Ng et al. [12], λ_i represents the biological decay constant for both strontium and cesium and represents the sum of the biological decay constant and the I-131 radiological decay constant for the iodine ETF_i . The revised $RETF_i$ can be defined as

$$RETF_i = \frac{1}{M (\lambda_{b,i} + \lambda_{d,i})} \quad (\text{day/kg}) \quad (4.18)$$

$\lambda_{b,i}$ = biological decay constant for nuclide i for the animal being considered (day⁻¹)

$\lambda_{d,i}$ = radiological decay constant for nuclide i (day⁻¹)

To derive the revised $RETf_i$ for a specific nuclide i, it will be assumed that the the Ng value, ETF_i , is based on nuclide with the radiological decay rate, λ_1 . Therefore,

$$ETF_i = \frac{1}{M (\lambda_1 + \lambda_{b,i})} \quad (4.19)$$

To establish the $RETf_i$, the biological decay rate will be needed. By solving Equation 4.19 for $\lambda_{b,i}$, we find

$$\lambda_{b,i} = \frac{1}{M \cdot ETF_i} - \lambda_1$$

Therefore, by Equation 4.17,

$$\begin{aligned} RETf_i &= \frac{1}{M (\lambda_{b,i} + \lambda_{d,i})} \\ &= \frac{1}{M \left[\left[\frac{1}{M \cdot ETF_i} - \lambda_1 \right] + \lambda_{d,i} \right]} \\ &= \frac{1}{M \left[\frac{1 - \lambda_1 \cdot M \cdot ETF_i + \lambda_{d,i} \cdot M \cdot ETF_i}{M \cdot ETF_i} \right]} \\ &= \frac{ETF_i}{1 + [M \cdot ETF_i \cdot (\lambda_{d,i} - \lambda_1)]} \end{aligned}$$

where

ETF_i = original equilibrium transfer factor as established by Ng (day/kg)

M = amount of meat produced by animals at time of slaughter (kg)

λ_1 = radioactive decay constant of used to establish the original ETF_i (day⁻¹)

$\lambda_{d,i}$ = radioactive decay constant for nuclide i (day⁻¹)

It has been noted that the ETF for strontium and cesium were established using the stable elements. This implies that λ_1 for both these cases would be nearly zero, and the expression for $RETF_i$ would simplify for strontium and cesium isotopes and becomes

$$RETF_i = \frac{ETF_i}{1 + (\lambda_{d,i} * M * ETF_i)} \quad (4.20)$$

The ETF for iodine was established using data for I-131, and therefore, in Equation 4.19,

$$\lambda_1 = \frac{\ln 2}{8.04}$$

Therefore, for any other isotope of iodine

$$RETF_i = \frac{ETF_i}{1 + \left[M \cdot ETF_i \cdot \left(\lambda_{d,i} - \frac{\ln 2}{8.04} \right) \right]} \quad (4.21)$$

Using Equations 4.20 and 4.21 and the values and ranges of ETF_i established by Ng et al. [12], the values and associated ranges for the revised equilibrium factors, $RETF_i$, were established and are summarized in Table 4.39. These values for $RETF_i$ were in turn used in deriving the transfer factor TBF_i for each nuclide i .

The variable M, the amount of meat produced by the animal at the time of slaughter, is needed both in the calculation of $RETF_i$ and the calculation of $TFBF_i$. Based on agricultural data [2:Tables 444 and 516], the values for M summarized in Table 4.40 were used.

Table 4.39. Values for Revised Equilibrium Transfer Factors

Nuclide	Cattle	Hog	Chicken	Turkey
Sr-89	0.00030 (0.000064-0.00057)	0.0029 (0.0012-0.0040)	0.032 (0.018-0.079)	0.032 (0.018-0.079)
Sr-90	0.00030 (0.000064-0.00057)	0.0029 (0.0012-0.0040)	0.032 (0.018-0.080)	0.032 (0.018-0.080)
Cs-134	0.020 (0.0072-0.091)	0.29 (0.26-0.37)	4.4 (4.3-4.5)	4.3 (4.2-4.4)
Cs-137	0.20 (0.0072-0.093)	0.30 (0.26-0.38)	4.4 (4.3-4.5)	4.4 (4.3-4.5)
I-131	0.0072 (0.0072-0.020)	0.027 (0.0010-0.027)	0.20 (0.0080-0.20)	0.20 (0.0080-0.20)
I-133	0.0033 (0.0033-0.0047)	0.011 (0.00095-0.011)	0.17 (0.0079-0.17)	0.11 (0.077-0.11)

Table 4.40. Meat Produced at Slaughter

Animal	Dressed Weight (kg)	Cutting Losses (%)	Edible Products Weight (kg) *
Cattle	269.0	15	229.0
Hogs	84.02	10	70.62
Chickens	1.34	10	1.188
Turkeys	6.96	10	6.183

Also needed for the calculation of $TFBF_i$ are values for the variable TR, the fraction of animals slaughtered per day. By using agricultural data on meat production [2:Tables 388, 398, 406, 407, 415, 502, 511, 516, 521, and 523], the values for TR in Table 4.41 were derived.

Recently there has been fallout data being made available following the Chernobyl accident. These data were reviewed by Nair and Iijima [13] and

estimates were made for several ETF_i . For Cs-137, they found an ETF of 0.02 day/kg for beef and a factor of 0.3 day/kg for pork, both of which closely agree with the ETFs as established by Ng [12].

A range of values for the equilibrium transfer factors was given by Ng. These ranges were used to determine the possible ranges for the variable $TFBF_i$.

Table 4.41. Values for the Fraction of Animals Slaughtered per Day (TR)

	<u>Beef</u>	<u>Pork</u>	<u>Poultry</u>	
			<u>Chicken</u>	<u>Turkey</u>
TR (day ⁻¹)	0.0011	0.0024	0.0026	0.0026

4.3.10 TFMLK

$TFMLK_i$ = fraction of the amount of radionuclide i present in the feed consumed by milk-producing animals that is present in the milk produced

Table 4.42 gives the recommended values for $TFMLK_i$. A uniform sampling distribution is recommended for $TFMLK_i$.

Table 4.42. Recommended Values for $TFMLK_i$

<u>Nuclide</u>	<u>$TFMLK_i$</u>	<u>Range of Values</u>
Sr-89	0.022	(0.0072-0.061)
Sr-90	0.022	(0.0072-0.061)
Cs-134	0.11	(0.040-0.26)
Cs-137	0.11	(0.040-0.26)
I-131	0.13	(0.036-0.46)
I-133	0.062	(0.018-0.22)

Discussion

$$TFMLK_i = \frac{OUTPUT_i}{EATEN_i}$$

where

OUTPUT_i = amount of nuclide i in milk produced

EATEN_i = amount of nuclide i in feed consumed

This variable is evaluated in the following manner for each nuclide i:

$$TFMLK_i = ETF_i \cdot MP$$

where

ETF_i = equilibrium transfer coefficient for nuclide i into milk (day/L)

MP = average daily total milk production (L/day)

Using recent agricultural data it was found the the average daily production is 16.01 L/day/cow [2:Table 471]. Therefore a value of MP = 16 was used for these calculations.

The equilibrium transfer factor, ETF_i, for the nuclide i is given below as summarized by Ng [12]. It is expected that there will be considerable variation in all ETF values. A summary of the possible range of values for the ETF for each of the elements is given below as adapted from Hoffman and Baes [11] by Ng [12].

Table 4.43. ETF for Nuclides

<u>Element</u>	<u>ETF (L/day)</u>	<u>Range of Values</u>
Strontium	0.0014	(0.00045-0.0038)
Cesium	0.0071	(0.0025-0.016)
Iodine	0.0099	(0.0027-0.035)

These values for ETF are based on stable element concentrations in associated milk and feed. Radioactive decay within the animal has an important impact on the ETF values for the short-lived radionuclides. The ETF values to be used for the I-131 and I-133 were adjusted to reflect these losses. The transfer coefficient can be thought of as the time-integrated transfer fraction for a unit nuclide intake by an animal [12]. In a development of the model used to describe the crop-animal-milk pathway, Ostmeier and Helton [1] conclude that when intake is considered to be constant with time the intake-to-milk equilibrium transfer coefficient can be derived as follows:

$$ETF_i = \sum_{k=1}^n \frac{A_k}{\lambda_{b,k} + \lambda_i} \quad (4.22)$$

where

A_k = concentration coefficient associated with a single acute exposure (L^{-1})

$\lambda_{b,k}$ = biological decay constant for the associated concentration coefficient A_k (day^{-1})

λ_i = radiological decay constant for the nuclide i (day^{-1})

This formulation accounts for the decrease in elemental concentration patterns over time from radioactive decay. Ng et al. [12] gave the values for stable iodine in Table 4.44.

Table 4.44. Values for Stable Iodine

<u>k</u>	<u>A_k</u>	<u>BDC_k</u>
1	0.0055	0.69
2	0.00017	0.088

Using the λ_i values of 0.086 and 0.80 for I-131 and I-133 respectively, the adjusted ETF_i values for these two nuclides are then as shown in Table 4.45.

Table 4.45. Adjusted ETF Values

<u>Nuclide</u>	<u>Adjusted ETF Value</u>
I-131	0.0081 (0.0022-0.029)
I-133	0.0039 (0.0011-0.014)

The range of possible values for ETF as noted above served as the basis for determining the adjusted range of values for ETF. This was accomplished by using similar ratios between the ETF values for stable iodine and the adjusted ETF value for each nuclide.

The values and ranges used in determining the values of the variable $TFMLK_i$ for each nuclide i are summarized in Table 4.46.

Table 4.46. ETF Values for $TFMLK_i$

<u>Nuclide</u>	<u>ETF Value (L/d)</u>	<u>Range of Value</u>
Sr-89	0.0014	(0.00045-0.0038)
Sr-90	0.0014	(0.00045-0.0038)
Cs-134	0.0071	(0.0025-0.016)
Cs-137	0.0071	(0.0025-0.016)
I-131	0.0081	(0.0022-0.029)
I-133	0.0039	(0.0011-0.014)

In a review of fallout data following the Chernobyl accident by Nair and Iijima [13], an equilibrium transfer factor of 0.002 d/L was suggested for I-131, which is somewhat less than the transfer factor derived here. This may be a notable development, since milk is the primary means within the food pathway by which iodine may be ingested. If this value is correct, the value of $TFMLK$ for I-131 would then become 0.032.

4.4 Mitigative Action Input Parameters

Within the MACCS code, the dose received by society is restricted by user-established dose criteria. For the food pathway model, two distinct criteria can be established: one for the growing season submodel and one for the long-term submodel. Various mitigative action options are available within the code for each of these submodels within the code. Each of the mitigative actions are designed to attenuate the societal dose received following an accidental release.

Several input parameters are required by the MACCS code to assure that the dose to be received via the food pathway will remain below the criteria. These input parameters are discussed in this section.

4.4.1 GCMAXR, PSCMLK, and PSCOTH

$GC\text{MAXR}_i$ = maximum allowable concentration for ground on which crops are grown that assures the lifetime dose criteria will be met (Bq/m^2)

$P\text{SCMLK}_i$ = maximum allowable concentration for ground on which crops are grown that assures the emergency dose criteria will be met without milk disposal (Bq/m^2)

$P\text{SCOTH}_i$ = maximum allowable concentration for ground on which crops are grown that assures the emergency dose criteria will be met without crop disposal (Bq/m^2)

Table 4.47 gives the recommended values for $GC\text{MAXR}_i$, $P\text{SCMLK}_i$, and $P\text{SCOTH}_i$.

Table 4.47. Recommended Values for $GC\text{MAXR}_i$, $P\text{SCMLK}_i$, and $P\text{SCOTH}_i$

<u>Nuclide</u>	<u>GCMA XR</u>	<u>PSCMLK</u>	<u>PSCOTH</u>
Sr-89	1.79×10^8	2.16×10^7	2.16×10^7
Sr-90	3.67×10^4	2.41×10^5	2.41×10^5
Cs-134	4.07×10^6	2.18×10^5	2.18×10^6
Cs-137	1.76×10^6	2.66×10^5	2.66×10^{10}
I-131	1.00×10^{20}	1.34×10^6	7.9510×6
I-137	1.00×10^{20}	1.05×10^{10}	1.02×10^{11}

It can be assumed the actual value for these variables will most probably lie within 25% of the calculated value. This assumption served as the basis for deriving a possible range of values for each nuclide/parameter pair.

Discussion

To assure that the dose received by individual remains below the user-defined dose criterion, the dose equation (i.e., Equation 4.1) is solved to find a maximum allowable ground concentration that would ensure the dose limit would not be exceeded. That is,

$$GCMAXR_i = \frac{DL_{i,k}}{DF_{i,k} \cdot \sum_j (A \cdot FA_j \cdot TF_{i,j})} \quad (4.23)$$

To determine these maximum allowable ground concentrations, a dose limit for a maximally exposed individual was used. That is, the ground concentration was calculated for an individual whose entire intake of food was assumed to originate on contaminated ground. The maximally exposed individual can be either an infant whose food intake consists entirely of milk or an adult whose intake of food is based on a "typical" market basket.

Since the dose is being limited for an individual, parameters in Equation 4.23 assume the following definitions:

$DL_{i,k}$ = dose limit for the maximally exposed individual (Sv)

$DF_{i,k}$ = dose conversion factor for the target organ k arising from the ingestion of nuclide i (Sv/Bq)

A = total cropland area required to grow crops to provide the food for the annual market basket for a maximally exposed individual (m^2)

FA_j = fraction of area A needed to grow crop j (unitless)

$TF_{i,j}$ = fraction of the amount of nuclide i deposited following the release that will ultimately be consumed by man (unitless)

Separate maximum allowable ground concentrations are derived for the long-term and growing season food pathway submodels. Associated with each of these submodels is an allowable dose (user input dose criterion).

$GCMAXR_i$ is the maximum allowable ground concentration established for nuclide i to meet the lifetime exposure criteria. It is applied to the long-term food pathway submodel.

For the growing season food pathway submodel, two maximum allowable ground concentrations are established. $PSCMLK_i$ is applied to the crop-milk-man pathway and assures that a maximally exposed infant (i.e., an infant drinking milk only from animals raised and fed on contaminated ground). $PSCOTH_i$ assures that the maximally exposed individual would not exceed the allowable dose when the nonmilk portion of his annual intake is added to the milk consumed when the ground concentration for milk production is $PSCMLK_i$.

Each of these allowable ground concentrations is determined for each nuclide is considered in the food pathway model. They are used within the MACCS code to determine mitigative action to assure the individual dose received as a result of the release of radioactive material will remain within the preestablished exposure criteria.

PSCMLK_i is used to determine the necessity of disposing of the milk being produced on contaminated ground. No disposal of milk is deemed to be necessary if the following condition is met:

$$\sum_i \frac{\text{PSCMLK}_i}{\text{GC}_i} \leq 1 \quad (4.24)$$

where

GC_i = the actual ground concentration of nuclide i following the release (Bq/m²)

Analogously, PSCOTH_i is used to determine the necessity of disposing of crops contaminated by direct deposition of radioactive material onto the plant surfaces following the release. No crop disposal is deemed necessary if the following condition is met:

$$\sum_i \frac{\text{PSCOTH}_i}{\text{GC}_i} \leq 1 \quad (4.25)$$

The parameter GCMAXR_i is used to ensure that the lifetime exposure from radionuclides ingested via the food pathway will meet the established criteria. No mitigative actions will be required if the following condition is met:

$$\sum_i \frac{\text{GCMAXR}_i}{\text{GC}_i} \leq 1 \quad (4.26)$$

If the ground concentration following the release is too high for this criteria to be met, several mitigative actions are evaluated for effectiveness in reducing the projected dose to within allowable standards. The first of the mitigative actions evaluated is decontamination of the cropland. If decontamination alone is insufficient to produce the required results, it is determined whether restricting crop production to allow natural depletion of the radioactive material would bring the dose received to within the lifetime criteria. Currently a maximum of eight years is permitted for interdiction of crop growth.

To calculate the effectiveness of an interdiction of crops for t years, the ground concentration following decontamination is attenuated by an overall annual depletion rate, $QROOT_i$, and the dose is again projected to determine whether the lifetime criteria have been fulfilled. That is,

$$GCI_{i,t} = GCD_i \cdot \text{EXP} (- QROOT_i \cdot t)$$

where

$GCI_{i,t}$ = ground concentration of nuclide i following t years of interdiction (Bq/m^2)

GCD_i = ground concentration of nuclide i following decontamination (Bq/m^2)

$QROOT_i$ = annual natural depletion rate for nuclide i (i.e., the depletion resulting from radioactive decay, percolation from the root zone, irreversible chemical binding with the soil, previous loss from the root zone from root uptake, and the loss from soil ingestion by grazing animals) (yr^{-1})

t = number of years over which interdiction is being considered (yr)

Following the calculation of the ground concentration following each additional year of interdiction (up to a maximum of eight years), a check is made to see whether the lifetime dose criteria are met, that is,

$$\sum_{k=1}^n \frac{GCMAXR_i}{GCI_{i,k}} \leq 1 \quad n \leq 8$$

If eight years proves to be insufficient for natural depletion to bring ground concentrations to within acceptable levels, the farmland will be condemned. That is, it will be purchased and restricted from production.

A complete discussion of the derivation of the values used for the input parameters $GCMAXR_i$, $PSCOTH_i$, and $PSCMLK_i$ is given in Appendix C of the MACCS Model Description [14]. Because of the lengthy discussion needed to describe these calculations adequately, that discussion will not be repeated in this document.

4.4.2 QROOT

$QROOT_i$ = annual depletion rate of nuclide i from the root zone

Table 4.48 gives the recommended values for QROOT for each nuclide i . A uniform sampling distribution is recommended for $QROOT_i$.

Table 4.48. Recommended Values for QROOT

<u>Nuclide</u>	<u>QROOT</u>	<u>Range of Possible Values</u>
Sr-89	4.9	
Sr-90	0.065	(0.041-0.090)
Cs-134	0.59	(0.51-0.69)
Cs-137	0.28	(0.19-0.38)
I-131	32.0	
I-133	290.0	

Discussion

$$QROOT_i = RRU_i + RD_i + RP_i + RB_i \quad (4.27)$$

where

$QROOT_i$ = annual rate of depletion of nuclide i from the root zone (yr^{-1})

RRU_i = annual rate of depletion from root uptake of the nuclide from the root zone (yr^{-1})

RD_i = annual rate of depletion from radioactive decay (yr^{-1})

RP_i = annual rate of depletion from percolation into soil below root zone (yr^{-1})

RB_i = annual rate of depletion from irreversible chemical binding of the nuclide with soil components (yr^{-1})

A single value of this variable is derived for each nuclide considered in the food pathway.

The annual rate at which plants remove strontium and cesium from the root zone via root uptake for the various crop categories is discussed and summarized by Ostmeier and Helton [1] whose recommended values are presented in Table 4.49.

Table 4.49. Root Uptake (RU) by Crop and Element

<u>Crop</u>	<u>Rate of Root Uptake</u>	
	<u>Sr</u>	<u>Cs</u>
Pasture	0.0017	0.000083
Stored Forage	0.0042	0.00021
Grains	0.00021	0.000021
Leafy Vegetables	0.0013	0.000013
Other Foods	0.00083	0.000042

Even though not all the crop categories considered were included in this summary, the cross section is wide enough that a weighted average of these values was used to determine the annual rate of depletion from soil via root uptake. As a result, the following values given for RU in Table 4.50 were obtained.

Table 4.50. Values for Root Uptake (RU)

<u>Element</u>	<u>RU</u>	<u>Range of Values</u>
Strontium	0.0016	(0.00021-0.0042)
Cesium	0.000074	(0.000013-0.00021)

No value for RU was derived for iodine isotopes because their short half-lives mean that these isotopes do not contribute significantly to the root uptake dose.

The annual rate at which a nuclide i disappears from the root zone due to radioactive decay (RD_i) is dependent on its radiological half-life. RD_i can be defined as follows:

$$RD_i = \frac{\ln 2}{THALF_i}$$

where

$THALF_i$ = radiological half-life of nuclide i (yr)

Values for RD_i are given in Table 4.51.

Table 4.51. Values for Radioactive Decay, RD_i (yr^{-1})

<u>Nuclide</u>	<u>RD</u>
Sr-89	4.86
Sr-90	0.024
Cs-134	0.34
Cs-137	0.023
I-131	31.5
I-133	292.0

Because radioactive half-lives are precisely known, no ranges are given for the values of RD_i .

The percolation rate for strontium and cesium have been established by Hoffman and Baes [11]. For strontium, this rate is given as $0.0021\ yr^{-1}$, and for cesium, it is given as $0.0096\ yr^{-1}$. The percolation rate is strongly dependent on soil characteristics; therefore, these values represent an approximate rate and are quite uncertain. A range of possible values was established by assuming that the actual value would most likely lie within 25% of the estimated value. No value for RP was derived for the iodine isotopes being considered since their depletion rate is dominated almost totally by radioactive decay. The values and possible ranges of values used for RP are summarized as in Table 4.52.

Table 4.52. Values for Rate of Percolation (RP_i)

<u>Element</u>	<u>DRP</u>	<u>Range of Values</u>
Strontium	0.0096	(0.0072-0.012)
Cesium	0.0021	(0.0016-0.0026)

When attempting to establish the rate of depletion from the root zone because of irreversible chemical binding with the soil, it becomes apparent that the binding rates for both strontium and cesium are strongly dependent on soil

characteristics. Based on investigations by Squire [15], Squire and Middleton [16], and Lassey [17], and a discussion by Coughtrey and Thorne [8], it seems reasonable to assume that 10-20% of the strontium in the soil will become chemically bound to the soil particles at a rate of about 1-5% per year. Cesium reacts even more dramatically with clay, and approximately 85-95% will become chemically bound to the clay particles and this binding will essentially be complete in three years. Chemical binding is not an important consideration for the iodine isotopes being considered, since radioactive decay is the primary mechanism by which they are depleted from the environment.

Based on this information, the values and ranges in Table 4.53 were established for the annual rate at which the nuclides become unavailable for root uptake because of irreversible binding with the soil.

Table 4.53. Values for Binding Rate, RB

<u>Element</u>	<u>RB</u>	<u>Range of Values</u>
Strontium	0.030	(0.01-0.05)
Cesium	0.25	(0.17-0.32)

Using the indicated derived values and ranges for the depletion rates from root uptake, radioactive decay, percolation out of the root zone, and chemical binding with the soil, the recommended values for the total depletion rates were found as the sum of the component parts as indicated in Equation 4.23.

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5. ECONOMIC PARAMETERS

5.1 Nonfarm Parameters: Recommended Values

Table 5.1 lists the values of nonfarm economic parameters recommended for use in MACCS.

Table 5.1. Economic Parameter Values for MACCS

Variable	(Units)	Site	Value	Range*	Definition
DPRATE	(per yr)	All	0.2	0.1 - 0.3	Property depreciation rate
DSRATE	(per yr)	All	0.12	0.7 - 0.17	Investment rate of return
EVACST	(\$/day)	All	\$27	\$25 - \$30	Per diem living expenses for evacuees
FRNFIM		All	0.8	0.7 - 0.9	Nonfarm
POPCST	(\$)	All	\$5000	\$3500 - \$7500	Relocation costs for owners of interdicted property
RELCST	(\$/day)	All	\$27	\$25 - \$30	Per diem living expenses for relocated population
VALWNR	(\$)	Grand Gulf	\$53K	\$43K - \$63K	Per capita value of nonfarm wealth
		Peach Bottom	\$79K	\$69K - \$89K	
		Surry	\$84K	\$74K - \$94K	
		Sequoyah	\$66K	\$56K - \$76K	
		Zion	\$76K	\$66K - \$86K	
		US	\$80K	\$60K - \$100K	

* All sampling distributions should be uniform over the stated ranges.

5.2 Nonfarm Parameters: Discussion

Most of the data presented in the following discussion were taken from Statistical Abstract of the United States for 1988. A few figures were taken from Fortune (April 25, 1988) and Forbes (January 11, 1989; June 27, 1988) magazines.

The economic model in the MACCS code treats following costs:

- (1) Daily food and lodging costs per person for short-term relocation of people who evacuate or relocate during the emergency phase of the accident (e.g., the first seven days after the accident),

- (2) Decontamination costs for property that can be returned to use,
- (3) Economic losses incurred while property is temporarily interdicted so that a period of decay following maximum decontamination can reduce yearly doses to acceptable levels (e.g., 5.5 rem in eight years), and
- (4) Economic losses from the permanent interdiction of property.

The model divides economic costs into two groups, farm costs and nonfarm costs. Farm costs are always calculated per hectare of farmland (worth of farmland and improvements per hectare, crop worth per hectare). Nonfarm costs are always calculated per person (temporary and permanent relocation costs per person, tangible worth of nonfarm property per person, decontamination costs of nonfarm property per person), where nonfarm property includes residential, commercial, and public land, improvements, equipment, and possessions.

5.2.1 Relocation Costs

Burke [1] estimated per diem relocation costs (housing, food, transportation) per person to be \$23.70 in 1982 dollars. Correction to 1986 (1986 CPI = 328; 1982 CPI = 289; ratio = 1.13) gives \$26.90 per day per person. Fifty dollars per night for a four-person motel room, and \$3.50, \$4.50, and \$7.00 per person for breakfast, lunch, and dinner plus \$1.50 per day for public transportation, gives \$29.00 per day per person. Burke estimated that mass care per diem costs would be about half the cost of commercial care (hotels and restaurants) and that about one fifth of all relocated persons would be accommodated in mass care facilities. If per diem costs are \$29 per person for 80 per cent of the relocated population and \$14.50 per person for the remaining 20 per cent, an average per diem relocation cost of \$26 per person results, which agrees well with Burke's result after correction to 1986 dollars. Therefore, a per diem relocation cost of \$27 per person is recommended for use in the final NUREG-1150 calculations.

5.2.2 Decontamination Costs

The MACCS decontamination model assumes that for both farm and nonfarm property several (no more than three) decontamination methods will be available. For each decontamination method, the model requires a cost (per hectare for farm property and per person for nonfarm property) and a decontamination factor, F_D , where

$$F_D = C_i/C_f$$

and C_i and C_f are the surface contamination levels before and after the decontamination step. Although the costs of the decontamination methods for farm and nonfarm property need not be the same, the set of decontamination factors used for farm property must be the same as the set used for nonfarm property.

5.2.3 Temporary Interdiction Losses

When property is temporarily interdicted, three costs are incurred for nonfarm property and two for farm property. For nonfarm property, the three costs are lost wages per person moved, lost return on investment on the interdicted

property, and the cost of the repairs required to return the property to use once the interdiction period ends. For farm property, the second and third costs apply but the first does not (because only the nonfarm economic model treats people).

Burke [1] examined the relocation costs that would be incurred by a person forced to relocate because his home had been interdicted. Since most of his possessions have been contaminated, Burke concluded that moving costs would be small when compared to lost wages, which he estimated to total about \$4000 based on the assumption that each worker relocated would be out of work for 100 to 180 days. Since per capita income in 1986 was \$14,600, if 140 days of lost wages are assumed (the average duration of unemployment from 1972 through 1986 was 15 weeks or 105 days, Reactor Safety Study [2] assumed that interdicted businesses would require about six months to reopen in a new location) and lost wages per person relocated would be \$5600. Correction of Burke's estimate of \$4000 based on 1982 data to 1986 yields \$4500. Accordingly, a moving cost of \$5000 is recommended for use in the final NUREG-1150 calculations.

Assume that all property (land, buildings, equipment, etc.) can be viewed as an investment that yields a rate of return, r , and depreciates at a rate, p , if left untended for some length of time, t . If, for example, the property is interdicted for t years, then two costs are incurred: (1) lost return on investment and (2) repair costs.

Consider a property composed of land (present value L) and improvements (present value I). The total present value of the property is $L + I = V$, and the fraction of the total present value that is improvements is $I/V = f$. If this property is now interdicted for t years, the lost return on investment is $V_t - V$, where $V_t = V e^{rt}$ and the repair costs that will be incurred at the end of the interdiction period are $I - I_t$, where $I_t = I e^{-pt}$. Therefore,

$$\text{Loss on Investment} = V_t - V = V e^{rt} - V = V (e^{rt} - 1)$$

$$\text{Repair Costs} = I - I_t = I - I e^{-pt} = I (1 - e^{-pt})$$

Let the present values of the lost return on investment and the repair costs be V' and I' . Then

$$V' e^{rt} = V_t - V = V (e^{rt} - 1)$$

$$V' = V (1 - e^{-rt})$$

$$I' e^{rt} = I - I_t = I (1 - e^{-pt})$$

$$I' = I e^{-rt} (1 - e^{-pt})$$

and C' , the present value of the total losses incurred during the interdiction period (t), is

$$\begin{aligned} C' &= V' + I' = V (1 - e^{-rt}) + I e^{-rt} (1 - e^{-pt}) \\ &= V - e^{rt} [V (1 - f + f e^{-pt})] \end{aligned}$$

which agrees with Burke et al. [1] and with the Reactor Safety Study [2].

To apply the preceding model, values for V, f, r, and p are needed. Since MACCS calculates farm costs on a per hectare basis and nonfarm costs on a per person basis, the values of V needed are the value of farm property per hectare (per acre) and of nonfarm property per person. State and national data for farm property are available from Statistical Abstract of the United States [3] and are discussed in other data packages. A value for the per person worth of nonfarm residential, commercial, and public property can be estimated from the following data, which were taken from Ref. [3]:

Reproducible Tangible Wealth	= $\$1.98 \times 10^{13}$
Urban and Built-Up Land	= 4.64×10^4 acres
Total Farm Assets	= $\$7.89 \times 10^{11}$
Farm Land	= $\$5.54 \times 10^{11}$
Farm Household Possessions	= $\$3.05 \times 10^{10}$
1987 U.S. Population	= 2.44×10^8

Now assuming that nonfarm land costs about \$90,000 per acre (typical suburban residential lots are 0.2 acre, land usually constitutes about one fifth of the cost of a house, and the 1986 median value of houses was \$92,000), the per person worth of nonfarm residential, commercial, and public property, that is V, is given by

$$\begin{aligned} V &= [\text{reproducible tangible wealth} \\ &\quad + \text{value of suburban land} \\ &\quad - \text{value of farm assets} \\ &\quad + \text{value of farm household possessions}]/[\text{U.S. population}] \\ &= [\$1.98 \times 10^{13} \\ &\quad + (4.64 \times 10^4 \text{ acres})(\$9 \times 10^4 \text{ acre}^{-1}) \\ &\quad - \$7.89 \times 10^{11} \\ &\quad + \$3.05 \times 10^{10}]/[2.44 \times 10^8 \text{ people}] \\ &= \$7.8 \times 10^4 \end{aligned}$$

Therefore, V is about \$80,000 per person.

The value of V is likely to vary significantly by state. This variation can be approximated by multiplying the \$80,000 value by the ratio of a state's per capita income to the national per capita income. The pertinent data are given in Table 5.2.

Table 5.2. Value to Region

Reactor	Region	(\$1000) Per Capita Income	V (\$1000)
	US	\$14.6	\$80
Seq	TN	12.0	66
	AL	11.3	62
Zion	WI	13.9	76
	Chicago	13.2	72
	IL	15.6	85
GG	MI	9.7	53
	LA	11.2	61
PB	PA	14.2	79
	MD	16.9	93
Sur	VA	15.4	84

Since investment property is usually purchased by borrowing money (mortgages, equipment loans), r , the total rate of return on any property must be calculated as the dollar weighted sum of the property owner's rate of return on equity (r_E) and the debt holder's rate of return on debt (r_D). Specifically,

$$r = fr_E + (1-f)r_D,$$

where $f = E/V$, E is the owner's equity in the property, V is the total value of the property, and $V - E = D$ is the debt on the property (for all manufacturing companies, $D/E = 1.8$ and thus $f = 0.36$; for the Fortune 500 companies, $D/E = 1.2$ and $f = 0.45$).

Several measures of the rate of return on debt or equity are given in Table 5.3:

Table 5.3. Rates of Return

Measure	Percent
Conventional Mortgage Rate (1970 - 1986)	11.9
Return on Equity	
Forbes Stock Fund Composite (1977 - 1987)	16.4
Standard and Poors 500 (1977 - 1987)	16.9
Fortune 500 (1977 - 1987)	17.2
Fortune 500 (1983 - 1987)	12.8
Fortune 500 (1986)	11.6
Fortune 500 (1987)	13.2
All Manufacturing (1985)	11.6
All Manufacturing (1986)	11.6

These data suggest that 12% is a representative rate of return on both mortgages and equity. Therefore, r equals 12%, which is the value of r used in Reactor Safety Study [2], where r was viewed as the carrying cost (expressed as a percent of value) for interdicted residential property (mortgage rate of 9% plus real estate tax rate of 3%).

Finally, no data on depreciation rates (p) for untended property are available. Reactor Safety Study assumed a value of 20% per year for p after noting that depreciation rates for property that is maintained are typically 3% to 5% per year.

5.3 Farm Parameters: Recommended Values

Table 5.4 gives the recommended values for VALUE and FRFIM.

Table 5.4. Recommended Values for VALWF and FRFIM

<u>Site</u>	<u>VALWF (\$/ha)</u>	<u>FRFIM (\$/ha)</u>
Grand Gulf (Mississippi)	1824	0.30
Peach Bottom (Pennsylvania)	4469	0.25
Sequoyah (Tennessee)	2708	0.27
Surry (Virginia)	2952	0.25
Zion (Wisconsin)	1754	0.49
VALWF - Value of farm wealth in region (includes all improvements belonging to both public and private sector)		
FRFIM - Fraction of farm wealth in region from improvements (includes buildings, equipment, infrastructure (such as roads, utilities, etc.))		

5.3.1 Discussion

The total value of farm machinery and implements in 1988 is 84.5 billion dollars according to the U.S. Department of Commerce [4:Table 1086]. Since there are 1002 million acres of farmland in the U.S. [4:Table 1057], the value of machinery and implements per acre is \$84.3 or \$208.2 per/hectare.

The value of farm land and buildings in 1988 [4:Table 1066] in the states being considered can be summarized as in Table 5.5.

Table 5.5. Value of Farm Land and Buildings (1988)

<u>State</u>	<u>Value of Land & Buildings (\$/ha)</u>
Mississippi	654
Pennsylvania	1725
Tennessee	1012
Virginia	1111
Wisconsin	626

The data in Table 5.5 were used to determine the value of the variable VALWF for each of the states considered in Table 5.6.

Table 5.6. Values for VALWF by State

<u>State</u>	<u>Value of Land & Buildings (\$/ha)</u>	<u>VALWF(\$/ha)</u>
Mississippi (Grand Gulf)	1615	1824
Pennsylvania (Peach Bottom)	4261	4469
Tennessee (Sequoyah)	2500	2708
Virginia (Surry)	2744	2952
Wisconsin (Zion)	1546	1754

Based on information from the USDA for 1984 [4:Table 543], Table 5.7 shows the value that was determined for the percentage of the total value of the farm that is accounted for by the buildings for each state being considered.

Table 5.7. Value of Buildings

<u>State</u>	<u>Value of Land and Buildings*</u>	<u>Value of Buildings</u>	<u>Total Value Represented by Buildings (%)</u>
Mississippi	13814	1975	14.3
Pennsylvania	12015	3196	26.6
Tennessee	12743	2829	22.0
Virginia	10192	2140	21.0
Wisconsin	17436	4830	27.7
* in millions of dollars			

This percentage was then used with the values derived for VALWF to determine the current value of buildings/acre, as well as the total value of buildings and equipment/hectare as in Table 5.8.

Table 5.8. Value of Buildings per Acre

<u>State</u>	<u>Value of Buildings (\$/ac)</u>	<u>Value of Buildings (\$/ha)</u>	<u>Value of Buildings & Equipment (\$/ha)</u>
Mississippi	138	341	549
Pennsylvania	367	906	1114
Tennessee	211	521	729
Virginia	218	538	746
Wisconsin	265	655	863

The values of FRFIM in Table 5.9 were derived as the fraction of VALWF that is represented by improvements (buildings and equipment).

Table 5.9. Values of FRFIM

<u>State</u>	<u>FRFIM</u>
Mississippi (Grand Gulf)	0.30
Pennsylvania (Peach Bottom)	0.25
Tennessee (Sequoyah)	0.27
Virginia (Surry)	0.25
Wisconsin (Zion)	0.49

REFERENCES

- [1] R. P. Burke et al., Economic Risks of Nuclear Power Reactor Accidents, NUREG/CR-3673, Sandia National Laboratories, Albuquerque, NM 1984.
- [2] U.S. Nuclear Regulatory Commission, Reactor Safety Study, Appendix VI, "Calculation of Reactor Accident Consequences," WASH-1400, Washington, DC, 1975.
- [3] Statistical Abstract of the United States, 1988, U.S. Department of Commerce.
- [4] Agricultural Statistics 1984, United States Department of Agriculture, Washington, DC, 1984.

1. The first part of the document is a list of names and addresses of the members of the committee.

2. The second part of the document is a list of names and addresses of the members of the committee.

APPENDIX A: Sample NUREG-1150 MACCS Input Files

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A.1 ATMOS

```

*****
* FILE NAME: 1150AT.INP
*
* GENERAL DESCRIPTIVE TITLE DESCRIBING THIS "ATMOS" INPUT
*
RIATNAM1001 'ATMOS INPUT FOR FINAL NUREG-1150 CALCULATIONS'
*
* FLAG TO INDICATE THAT THIS IS THE LAST PROGRAM IN THE SERIES TO BE RUN
*
OCENDAT1001 .FALSE. (SET THIS VALUE TO .TRUE. TO SKIP EARLY AND CHRONC)
*****
* GEOMETRY DATA BLOCK, LOADED BY INPGEO, STORED IN /GEOM/
*
* NUMBER OF RADIAL SPATIAL ELEMENTS
*
GENUMRAD001 26
*
* SPATIAL ENDPOINT DISTANCES IN MILES
*
*   END001    0.25    0.5    0.75    1.0    1.5
*   END002    2.0    2.5    3.0    3.5    5.0
*   END003    7.0    10    13    16    20
*   END004    25    30    40    50    70
*   END005   100   150   200   350   500
*   END006  1000
*
* SPATIAL ENDPOINT DISTANCES IN KILOMETERS
*
*   SITE                GG    LS    PB    SEQ    SUR    ZION
*   EXCLUSION ZONE DISTANCE (MI) 0.432 0.320 0.510 0.364 0.323 0.249
*   EXCLUSION ZONE DISTANCE (KM) 0.696 0.515 0.820 0.585 0.520 0.400
*   EXCLUSION ZONE + 1.0 MI (KM) 2.305 2.124 2.429 2.194 2.129 2.009
*
*GESPAEND001    .40    .80    1.21    1.61    2.41 * STANDARD GRID
*GESPAEND001    .40    .70    1.21    1.61    2.31 * GRAND GULF
*GESPAEND001    .16    .52    1.21    1.61    2.13 * LA SALLE
*GESPAEND001    .40    .82    1.21    1.61    2.43 * PEACH BOTTOM
*GESPAEND001    .16    .59    1.21    1.61    2.20 * SEQUOYAH
*GESPAEND001    .16    .52    1.21    1.61    2.13 * SURRY
*GESPAEND001    .40    .80    1.21    1.61    2.01 * ZION
*
* PEACH BOTTOM
*
GESPAEND001    .40    .82    1.21    1.61    2.43
GESPAEND002    3.22    4.02    4.83    5.63    8.05
GESPAEND003   11.27   16.09   20.92   25.75   32.19
GESPAEND004   40.23   48.28   64.37   80.47  112.65
GESPAEND005  160.93  241.14  321.87  563.27  804.67
GESPAEND006  1609.34
*****
* NUCLIDE DATA BLOCK, LOADED BY INPISO, STORED IN /ISOGRP/, /ISONAM/
*
* NUMBER OF NUCLIDES
*
ISNUMISO001 60
*
* NUMBER OF NUCLIDE GROUPS
*
ISMAXGRP001 9
*
* WET AND DRY DEPOSITION FLAGS FOR EACH NUCLIDE GROUP
*
*   WETDEP    DRYDEP
*
ISDEPFLA001 .FALSE. .FALSE.
ISDEPFLA002 .TRUE. .TRUE.

```

ISDEPFLA003	.TRUE.	.TRUE.
ISDEPFLA004	.TRUE.	.TRUE.
ISDEPFLA005	.TRUE.	.TRUE.
ISDEPFLA006	.TRUE.	.TRUE.
ISDEPFLA007	.TRUE.	.TRUE.
ISDEPFLA008	.TRUE.	.TRUE.
ISDEPFLA009	.TRUE.	.TRUE.

*

* NUCLIDE GROUP DATA FOR 9 NUCLIDE GROUPS

*

	NUCNAM	PARENT	IGROUP	HAFLIF	
ISOTPGRP001	CO-58	NONE	6	6.160E+06	
ISOTPGRP002	CO-60	NONE	6	1.660E+08	
ISOTPGRP003	KR-85	NONE	1	3.386E+08	
ISOTPGRP004	KR-85M	NONE	1	1.613E+04	
ISOTPGRP005	KR-87	NONE	1	4.560E+03	
ISOTPGRP006	KR-88	NONE	1	1.008E+04	
ISOTPGRP007	RB-86	NONE	3	1.611E+06	
ISOTPGRP008	SR-89	NONE	5	4.493E+06	
ISOTPGRP009	SR-90	NONE	5	8.865E+08	
ISOTPGRP010	SR-91	NONE	5	3.413E+04	
ISOTPGRP011	SR-92	NONE	5	9.756E+03	NEW
ISOTPGRP012	Y-90	SR-90	7	2.307E+05	
ISOTPGRP013	Y-91	SR-91	7	5.080E+06	
ISOTPGRP014	Y-92	SR-92	7	1.274E+04	NEW
ISOTPGRP015	Y-93	NONE	7	3.636E+04	NEW
ISOTPGRP016	ZR-95	NONE	7	5.659E+06	
ISOTPGRP017	ZR-97	NONE	7	6.048E+04	
ISOTPGRP018	NB-95	ZR-95	7	3.033E+06	
ISOTPGRP019	MO-99	NONE	6	2.377E+05	
ISOTPGRP020	TC-99M	MO-99	6	2.167E+04	
ISOTPGRP021	RU-103	NONE	6	3.421E+06	
ISOTPGRP022	RU-105	NONE	6	1.598E+04	
ISOTPGRP023	RU-106	NONE	6	3.188E+07	
ISOTPGRP024	RH-105	RU-105	6	1.278E+05	
ISOTPGRP025	SB-127	NONE	4	3.283E+05	
ISOTPGRP026	SB-129	NONE	4	1.562E+04	
ISOTPGRP027	TE-127	SB-127	4	3.366E+04	
ISOTPGRP028	TE-127M	NONE	4	9.418E+06	
ISOTPGRP029	TE-129	SB-129	4	4.200E+03	
ISOTPGRP030	TE-129M	NONE	4	2.886E+06	
ISOTPGRP031	TE-131M	NONE	4	1.080E+05	
ISOTPGRP032	TE-132	NONE	4	2.808E+05	
ISOTPGRP033	I-131	TE-131M	2	6.947E+05	
ISOTPGRP034	I-132	TE-132	2	8.226E+03	
ISOTPGRP035	I-133	NONE	2	7.488E+04	
ISOTPGRP036	I-134	NONE	2	3.156E+03	
ISOTPGRP037	I-135	NONE	2	2.371E+04	
ISOTPGRP038	XE-133	I-133	1	4.571E+05	
ISOTPGRP039	XE-135	I-135	1	3.301E+04	
ISOTPGRP040	CS-134	NONE	3	6.501E+07	
ISOTPGRP041	CS-136	NONE	3	1.123E+06	
ISOTPGRP042	CS-137	NONE	3	9.495E+08	
ISOTPGRP043	BA-139	NONE	9	4.986E+03	NEW
ISOTPGRP044	BA-140	NONE	9	1.105E+06	
ISOTPGRP045	LA-140	BA-140	7	1.448E+05	
ISOTPGRP046	LA-141	NONE	7	1.418E+04	NEW
ISOTPGRP047	LA-142	NONE	7	5.724E+03	NEW
ISOTPGRP048	CE-141	LA-141	8	2.811E+06	PARENT ADDED
ISOTPGRP049	CE-143	NONE	8	1.188E+05	
ISOTPGRP050	CE-144	NONE	8	2.457E+07	
ISOTPGRP051	PR-143	CE-143	7	1.173E+06	
ISOTPGRP052	ND-147	NONE	7	9.495E+05	
ISOTPGRP053	NP-239	NONE	8	2.030E+05	
ISOTPGRP054	PU-238	CM-242	8	2.809E+09	

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ISOTPGRP055    PU-239    NP-239    8    7.700E+11
ISOTPGRP056    PU-240    CM-244    8    2.133E+11
ISOTPGRP057    PU-241    NONE      8    4.608E+08
ISOTPGRP058    AM-241    PU-241    7    1.366E+10
ISOTPGRP059    CM-242    NONE      7    1.408E+07
ISOTPGRP060    CM-244    NONE      7    5.712E+08
*****
* WET DEPOSITION DATA BLOCK, LOADED BY INPWET, STORED IN /WETCON/
*
* WASHOUT COEFFICIENT NUMBER ONE, LINEAR FACTOR
*
WDCWASH1001    9.5E-5    (HELTON AFTER JONES, 1986)
*
* WASHOUT COEFFICIENT NUMBER TWO, EXPONENTIAL FACTOR
*
WDCWASH2001    0.8      (HELTON AFTER JONES, 1986)
*****
* DRY DEPOSITION DATA BLOCK, LOADED BY INPDY, STORED IN /DRYCON/
*
* NUMBER OF PARTICLE SIZE GROUPS
*
DDNPSGRP001    1
*
* DEPOSITION VELOCITY OF EACH PARTICLE SIZE GROUP (M/S)
*
DDVDEPOS001    0.01    (VALUE SELECTED BY S. ACHARYA, NRC) #
*****
* DISPERSION PARAMETER DATA BLOCK, LOADED BY INPDIS, STORED IN /DISPY/, /DISPZ/
*
* SIGMA = A X ** B WHERE A AND B VALUES ARE FROM TADMOR AND GUR (1969)
*
* LINEAR TERM OF THE EXPRESSION FOR SIGMA-Y, 6 STABILITY CLASSES
*
* STABILITY CLASS: A      B      C      D      E      F
*
DPCYSIGA001    0.3658    0.2751    0.2089    0.1474    0.1046    0.0722
*
* EXPONENTIAL TERM OF THE EXPRESSION FOR SIGMA-Y, 6 STABILITY CLASSES
*
* STABILITY CLASS: A      B      C      D      E      F
*
DPCYSIGB001    .9031    .9031    .9031    .9031    .9031    .9031
*
* LINEAR TERM OF THE EXPRESSION FOR SIGMA-Z, 6 STABILITY CLASSES
*
* STABILITY CLASS: A      B      C      D      E      F
*
DPCZSIGA001    2.5E-4    1.9E-3    .2      .3      .4      .2
*
* EXPONENTIAL TERM OF THE EXPRESSION FOR SIGMA-Z, 6 STABILITY CLASSES
*
* STABILITY CLASS; A      B      C      D      E      F
*
DPCZSIGB001    2.125    1.6021    .8543    .6532    .6021    .6020
*
* LINEAR SCALING FACTOR FOR SIGMA-Y FUNCTION, NORMALLY 1
*
DPYSCALE001    1.
*
* LINEAR SCALING FACTOR FOR SIGMA-Z FUNCTION,
* NORMALLY USED FOR SURFACE ROUGHNESS LENGTH CORRECTION.
* (Z1 / Z0) ** 0.2, FROM CRAC2 WE HAVE (10 CM / 3 CM) ** 0.2 = 1.27
*
DPZSCALE001    1.27
*****
* EXPANSION FACTOR DATA BLOCK, LOADED BY INPEXP, STORED IN /EXPAND/

```

See letter from M.A. Cunningham (NRC) to F.T. Harper (SNL) dated Aug. 7, 1990 filed in NRC Public Document Room.

```

*
* TIME BASE FOR EXPANSION FACTOR (SECONDS)
*
PMTIMBAS001    600.    (10 MINUTES)
*
* BREAK POINT FOR FORMULA CHANGE (SECONDS)
*
PMBRKPNT001    3600.    (1 hour)
*
* EXPONENTIAL EXPANSION FACTOR NUMBER 1
*
PMXPFAC1001      0.2
*
* EXPONENTIAL EXPANSION FACTOR NUMBER 2
*
PMXPFAC2001      0.25
*****
* PLUME RISE DATA BLOCK, LOADED BY INPLRS, STORED IN /PLUMRS/
*
* SCALING FACTOR FOR THE CRITICAL WIND SPEED FOR ENTRAINMENT OF A BOUYANT PLUME
* (USED BY FUNCTION CAUGHT)
*
PRSCLCRW001      1.
*
* SCALING FACTOR FOR THE A-D STABILITY PLUME RISE FORMULA
* (USED BY FUNCTION PLMRIS)
*
PRSCLDAP001      1.
*
* SCALING FACTOR FOR THE E-F STABILITY PLUME RISE FORMULA
* (USED BY FUNCTION PLMRIS)
*
PRSCLEFP001      1.
*****
* WAKE EFFECTS DATA BLOCK, LOADED BY INPWAK, STORED IN /BILWAK/
*
*      SITE      GG    PB    SEQ    SUR
*      WIDTH (M)  40    50    40    40
*      HEIGHT (M) 60    50    40    50
*
* BUILDING WIDTH (METERS)
*
WEBUILDW001    50.  *  PEACH BOTTOM
*
* BUILDING HEIGHT (METERS)
*
WEBUILDH001    50.  *  PEACH BOTTOM
*****
* RELEASE DATA BLOCK, LOADED BY INPREL, STORED IN /RELEAS/
*
* SPECIFIC DESCRIPTIVE TEXT DESCRIBING THIS PARTICULAR SOURCE TERM
*
RDATNAM2001 'NUREG-1150 PEACH BOTTOM SOURCE TERM PB-15-1'
*
* TIME (SECONDS) AFTER ACCIDENT INITIATION WHEN THE ACCIDENT REACHES GENERAL
* EMERGENCY CONDITIONS (AS DEFINED IN NUREG-0654), OR WHEN PLANT PERSONNEL
* CAN RELIABLY PREDICT THAT GENERAL EMERGENCY CONDITIONS WILL BE ATTAINED.
*
RDOALARM001    1.40E4
*
* SELECTION OF RISK DOMINANT PLUME
*
RDMAXRIS001      1
*
* NUMBER OF PLUME SEGMENTS THAT ARE RELEASED
*

```



```

RDNUMREL001  2
*
* REPRESENTATIVE TIME POINT FOR DISPERSION AND RADIOACTIVE DECAY
*
RDREFTIM001  0.0  0.5  (CORRESPONDING TO HEAD AND MIDPOINT WEATHER)
*
* HEAT CONTENT OF THE RELEASE SEGMENTS (WATTS)
* A VALUE SPECIFIED FOR EACH OF THE RELEASE SEGMENTS
*
RDPLHEAT001  1.40E7  1.49E6  *  8.0E8 CAL/240 SEC, 5.0E9 CAL/1.4E4 SEC
                                4.184 CAL/SEC = 1.0 WATT
*
* HEIGHT OF THE PLUME SEGMENTS AT RELEASE (METERS)
* A VALUE SPECIFIED FOR EACH OF THE RELEASE SEGMENTS
*
RDPLHITE001  30.  30.
*
* DURATION OF THE PLUME SEGMENTS (SECONDS)
* A VALUE SPECIFIED FOR EACH OF THE RELEASE SEGMENTS
*
RDPLUDUR001  240.  1.40E4
*
* TIME OF RELEASE FOR EACH PLUME (SECS FROM SCRAM)
* A VALUE SPECIFIED FOR EACH OF THE RELEASE SEGMENTS
*
RDPDELAY001  2.51E4  2.58E4
*
* RELEASE FRACTIONS FOR NUCLIDE GROUPS IN RELEASE
*
* GENERIC SOURCE TERM A
*
*      GROUP:  XE/KR  I      CS      TE      SR      RU      LA      CE      BA
*
RDRELFRC001  0.66  8.5E-3  9.4E-3  0.019  0.026  3.5E-3  2.8E-3  5.4E-3  0.026
RDRELFRC002  0.34  0.49   0.54   0.61   0.72   9.3E-3  0.062  0.12   0.62
*
* 3578 MWTH BWR CORE INVENTORY, 80 0/0 CAPACITY, 3/3 SHUTDOWN INVENTORY
*      SUPPLIED BY D.E. BENNETT, 6/17/86
*
*      NUCNAM      CORINV(BQ)
*
RDCORINV001  CO-58      2.024E+16
RDCORINV002  CO-60      2.423E+16
RDCORINV003  KR-85      3.317E+16
RDCORINV004  KR-85M     1.206E+18
RDCORINV005  KR-87      2.193E+18
RDCORINV006  KR-88      2.960E+18
RDCORINV007  RB-86      1.856E+15
RDCORINV008  SR-89      3.673E+18
RDCORINV009  SR-90      2.599E+17
RDCORINV010  SR-91      4.771E+18
RDCORINV011  SR-92      4.984E+18
RDCORINV012  Y-90       2.783E+17
RDCORINV013  Y-91       4.482E+18
RDCORINV014  Y-92       5.004E+18
RDCORINV015  Y-93       5.690E+18
RDCORINV016  ZR-95      5.899E+18
RDCORINV017  ZR-97      6.073E+18
RDCORINV018  NB-95      5.581E+18
RDCORINV019  MO-99      6.436E+18
RDCORINV020  TC-99M     5.554E+18
RDCORINV021  RU-103     4.877E+18
RDCORINV022  RU-105     3.254E+18
RDCORINV023  RU-106     1.327E+18
RDCORINV024  RH-105     2.429E+18
RDCORINV025  SB-127     3.077E+17

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RDCORINV026	SB-129	1.068E+18
RDCORINV027	TE-127	2.979E+17
RDCORINV028	TE-127M	4.010E+16
RDCORINV029	TE-129	1.002E+18
RDCORINV030	TE-129M	2.634E+17
RDCORINV031	TE-131M	5.058E+17
RDCORINV032	TE-132	4.944E+18
RDCORINV033	I-131	3.417E+18
RDCORINV034	I-132	5.020E+18
RDCORINV035	I-133	7.172E+18
RDCORINV036	I-134	7.850E+18
RDCORINV037	I-135	6.751E+18
RDCORINV038	XE-133	7.182E+18
RDCORINV039	XE-135	1.707E+18
RDCORINV040	CS-134	5.596E+17
RDCORINV041	CS-136	1.501E+17
RDCORINV042	CS-137	3.350E+17
RDCORINV043	BA-139	6.612E+18
RDCORINV044	BA-140	6.522E+18
RDCORINV045	LA-140	6.655E+18
RDCORINV046	LA-141	6.145E+18
RDCORINV047	LA-142	5.912E+18
RDCORINV048	CE-141	5.922E+18
RDCORINV049	CE-143	5.765E+18
RDCORINV050	CE-144	3.841E+18
RDCORINV051	PR-143	5.643E+18
RDCORINV052	ND-147	2.522E+18
RDCORINV053	NP-239	7.516E+19
RDCORINV054	PU-238	5.226E+15
RDCORINV055	PU-239	1.325E+15
RDCORINV056	PU-240	1.659E+15
RDCORINV057	PU-241	2.856E+17
RDCORINV058	AM-241	2.903E+14
RDCORINV059	CM-242	7.667E+16
RDCORINV060	CM-244	4.137E+15

*

* SCALING FACTOR TO ADJUST THE CORE INVENTORY

*

REACTOR	PWR	BWR	GG	LS	PB	SEQ	SUR	ZION
TYPE			B	B	B	P	P	P
POWER LEVEL (MWTH)	3412	3578	3833	3292	3293	3423	2441	3250
SCALING FACTOR	1.0	1.0	1.071	0.920	0.920	1.003	0.715	0.953

*

RDCORSCA001 0.920 * PEACH BOTTOM

*

* PARTICLE SIZE DISTRIBUTION OF EACH NUCLIDE GROUP

* YOU MUST SPECIFY A COLUMN OF DATA FOR EACH OF THE PARTICLE SIZE GROUPS

*

RDPSDIST001	1.
RDPSDIST002	1.
RDPSDIST003	1.
RDPSDIST004	1.
RDPSDIST005	1.
RDPSDIST006	1.
RDPSDIST007	1.
RDPSDIST008	1.
RDPSDIST009	1.

* OUTPUT CONTROL DATA BLOCK, LOADED BY INPOPT, STORED IN /ATMPT/

*

OCIDEBUG001 0

*

* NAME OF THE NUCLIDE TO BE LISTED ON THE DISPERSION LISTINGS

*

OCNUCOUT001 CS-137

```

* METEOROLOGICAL SAMPLING DATA BLOCK
*
* METEOROLOGICAL SAMPLING OPTION CODE:
*
* METCOD = 1, USER SPECIFIED DAY AND HOUR IN THE YEAR (FROM MET FILE),
*          2, WEATHER CATEGORY BIN SAMPLING,
*          3, 120 HOURS OF WEATHER SPECIFIED ON THE ATMOS USER INPUT FILE,
*          4, CONSTANT MET (BOUNDARY WEATHER USED FROM THE START),
*          5, STRATIFIED RANDOM SAMPLES FOR EACH DAY OF THE YEAR.
*
M1METCOD001  2
*
* LAST SPATIAL INTERVAL FOR MEASURED WEATHER
*
M2LIMSPA001  25
*
* BOUNDARY WEATHER, NO RAIN, WIND SPEED = 0.5 M/S, A-STABILITY,
* MIXING HEIGHT = 1000 M, APPLIES TO THE LAST SPATIAL INTERVAL
* (500 - 1000 MILES)
*
* BOUNDARY WEATHER MIXING LAYER HEIGHT
*
M2BNDMXH001  1000. (METERS)
*
* BOUNDARY WEATHER STABILITY CLASS INDEX
*
M2IBDSTB001  1      (A-STABILITY)
*
* BOUNDARY WEATHER RAIN RATE
*
M2BNDRAN001  0.      (0 MM / HOUR = NO RAIN)
*
* BOUNDARY WEATHER WIND SPEED
*
M2BNDWND001  0.5     (M / S)
*
* NUMBER OF SAMPLES PER BIN
*
M4NSMPLS001  4 (THIS NUMBER SHOULD BE SET TO 4 FOR RISK ASSESSMENT)
*
* NUMBER OF BINS TO BE SAMPLED (WHEN NSMPLS = 0)
*
*M4NSBINS001  6
*
*          BIN NUMBER      SAMPLE SIZE
*          INDXBIN          INWGHT
*M4SMPLDF001  3             8
*M4SMPLDF002  4            16
*M4SMPLDF003  5            12
*M4SMPLDF004  6             4
*M4SMPLDF005  7             4
*M4SMPLDF006  8             4
*
* NUMBER OF RAIN DISTANCE INTERVALS FOR BINNING
*
M4NRNINT001  6
*
* ENDPOINTS OF THE RAIN DISTANCE INTERVALS (KILOMETERS)
*
* NOTE: THESE MUST BE CHOSEN TO MATCH THE SPATIAL ENDPOINT DISTANCES
* SPECIFIED FOR THE ARRAY SPAEND (10 % ERROR IS ALLOWED).
*
*          2.0   3.5   7.0   13.0   25.0   50.0   MILES
*
M4RNDSTS001  3.22  5.63  11.27  20.92  40.23  80.47  KM
*

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* NUMBER OF RAIN INTENSITIY BREAKPOINTS
*
M4NRINTN001    3
*
* RAIN INTENSITY BREAKPOINTS FOR WEATHER BINNING (MILLIMETERS PER HOUR)
*
M4RNRATE001    1.  2.  3.
*
* INITIAL SEED FOR RANDOM NUMBER GENERATOR
*
M4IRSEED001    1
.
```

A.2 EARLY

```

*****
* FILE NAME: 1150ER.INP
*
* GENERAL DESCRIPTIVE TITLE DESCRIBING THIS "EARLY" INPUT FILE
*
MIEANAM1001 'EARLY INPUT FOR FINAL NUREG-1150 CALCULATIONS'
*
* FLAG TO INDICATE THAT THIS IS THE LAST PROGRAM IN THE SERIES TO BE RUN
*
MIENDAT2001 .FALSE. (SET THIS VALUE TO .TRUE. TO SKIP CHRONC)
*
* DISPERSION MODEL OPTION CODE: 1 * STRAIGHT LINE
*                                2 * WIND-SHIFT WITH ROTATION
*                                3 * WIND-SHIFT WITHOUT ROTATION
*
MIIPLUME001 2
*
* NUMBER OF FINE GRID SUBDIVISIONS USED BY THE MODEL
*
MINUMFIN001 7 (3, 5 OR 7 ALLOWED)
*
* LEVEL OF DEBUG OUTPUT REQUIRED, NORMAL RUNS SHOULD SPECIFY ZERO
*
MIIPRINT001 0
*
* FLAG INDICATING IF WIND-ROSES FROM ATMOS ARE TO BE OVERRIDDEN
*
MIOVRRID001 .FALSE. (USE THE WIND ROSE CALCULATED FOR EACH WEATHER BIN)
*
* LOGICAL FLAG SIGNIFYING THAT THE BREAKDOWN OF RISK BY WEATHER CATEGORY
* BIN ARE TO BE PRESENTED TO SHOW THEIR RELATIVE CONTRIBUTION TO THE MEAN
*
* RISBIN
*
MIRISCAT001 .FALSE.
*****
* POPULATION DISTRIBUTION DATA BLOCK, LOADED BY INPOP, STORED IN /POPDAT/
*
PDPOPFLG001 FILE
*
*PDPOPFLG001 UNIFORM
*PDIBEGIN001 1 (SPATIAL INTERVAL AT WHICH POPULATION BEGINS)
*PDPOPDEN001 50. (POPULATION DENSITY (PEOPLE PER SQUARE KILOMETER))
*****
* ORGAN DEFINITION DATA BLOCK, LOADED BY INORGA, STORED IN /EARDIM/ AND /ORGNAM/
*
* NUMBER OF ORGANS DEFINED FOR HEALTH EFFECTS
*
ODNUMORG001 9
*
* NAMES OF THE ORGANS DEFINED FOR HEALTH EFFECTS
*
ODORGNAM001 'SKIN', 'EDEWBODY', 'LUNGS', 'RED MARR', 'LOWER LI', 'STOMACH',
ODORGNAM002 'THYROIDH', 'BONE SUR', 'BREAST'
*ODORGNAM003 'EMBRYO', 'FETAL BONE', 'FETAL OTHR', 'GONADS',
*****
* SHIELDING AND EXPOSURE FACTORS, LOADED BY INDFAC, STORED IN /EADFAC/
*
* THREE VALUES OF EACH PROTECTION FACTOR ARE SUPPLIED,
* ONE FOR EACH TYPE OF ACTIVITY:
*
* ACTIVITY TYPE:
* 1 - EVACUEES WHILE MOVING
* 2 - NORMAL ACTIVITY IN SHELTERING AND EVACUATION ZONE
* 3 - SHELTERED ACTIVITY
*

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* CLOUD SHIELDING FACTOR
*
*   SITE      GG   PB   SEQ   SUR   ZION
*   SHELTERING 0.7  0.5  0.65  0.6  0.5
*
*           EVACUEES   NORMAL   SHELTER
*
SECSFACT001      1.      0.75      0.5      *   PEACH BOTTOM SHELTERING VALUE
*
* PROTECTION FACTOR FOR INHALATION
*
SEPROTIN001      1.      0.41      0.33      *   VALUES FOR NORMAL ACTIVITY
*                                           AND SHELTERING SELECTED
*                                           BY S. ACHARYA, NRC.
*
* BREATHING RATE (CUBIC METERS PER SECOND)
*
SEBRRATE001  2.66E-4  2.66E-4  2.66E-4
*
* SKIN PROTECTION FACTOR
*
SESKPFAC001      1.      0.41      0.33      *   VALUES FOR NORMAL ACTIVITY
*                                           AND SHELTERING SELECTED
*                                           BY S. ACHARYA, NRC.
*
* GROUND SHIELDING FACTOR
*
*   SITE      GG   PB   SEQ   SUR   ZION
*   SHELTERING 0.25  0.1  0.2  0.2  0.1
*
SEGSHFAC001      0.5      0.33      0.1      *   VALUE FOR NORMAL ACTIVITY
*                                           SELECTED BY S. ACHARYA, NRC;
*                                           PEACH BOTTOM SHELTERING VALUE.
*
* RESUSPENSION INHALATION MODEL CONCENTRATION COEFFICIENT (/METER)
*
*   RESCON = 1.E-4 IS APPROPRIATE FOR MECHANICAL RESUSPENSION BY VEHICLES.
*   RESHAF = 2.11 DAYS CAUSES 1.E-4 TO DECAY IN ONE WEEK TO 1.E-5, THE VALUE
*   OF RESCON USED IN THE FIRST TERM OF THE LONG-TERM RESUSPENSION EQUATION
*   USED IN CHRONC.
*
SERESCON001  1.E-4      (RESUSPENSION IS TURNED ON)
*
* RESUSPENSION CONCENTRATION COEFFICIENT HALF-LIFE (SEC)
*
SERESHAF001  1.82E5      (2.11 DAYS)
*****
* EVACUATION ZONE DATA BLOCK, LOADED BY EVNETW, STORED IN /NETWOR/, /EOPTIO/
*
* SPECIFIC DESCRIPTION OF THE EMERGENCY RESPONSE STRATEGY BEING USED
*
EZEANAM2001 'EVACUATION TO 10 MILES WITH HOT SPOT AND NORMAL RELOCATION'
*
* THE TYPE OF WEIGHTING TO BE APPLIED TO THE EMERGENCY RESPONSE SCENARIOS
*   YOU MUST SUPPLY A VALUE OF 'TIME' OR 'PEOPLE'
*
EZWTNAME001  'PEOPLE'
*
* WEIGHTING FRACTION APPLICABLE TO THIS SCENARIO
*
EZWTFRAC001  1.0      (100% OF THE PEOPLE WITHIN 10 MILES EVACUATE)
*
* LAST RING IN THE MOVEMENT ZONE
*
EZLASMOV001  15      (EVACUEES ARE DIRECTED AWAY FROM THE PATH OF
*                     THE RELEASE AFTER TRAVELLING TO 20 MILES)

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```

*
* FIRST SPATIAL INTERVAL IN THE EVACUATION ZONE
*
EZINIEVA001    1          (NO INNER SHELTER ZONE)
*
* OUTER BOUNDS OF THE 3 EVACUATION ZONES (0 MEANS THE ZONE IS NOT DEFINED)
*
EZLASEVA001    0  0  12  (EVACUATION FROM A SINGLE ZONE OUT TO 10 MILES)
*
*      SITE          GG    PB    SEQ    SUR
*      EDELAY (HR)    1.25  1.5   2.3   2.0
*      ESPEED (M/S)   3.7   4.8   1.8   1.8
*
*      EDELAY = CLDELAY + 0.5 HR
*
*      CLDELAY = DELAY BETWEEN WARNING OF PUBLIC TO BEGIN
*                EVACUATION AND TIME EVACUATION ACTUALLY BEGINS,
*                VALUES USED ARE DEVELOPED FROM SITE SPECIFIC
*                CLEAR TIME STUDIES
*
*      0.5 HR = MEAN (EXPECTED) TIME FROM OCCURENCE GENERAL EMERGENCY
*                CONDITIONS TO WARNING OF PUBLIC (SYRENS, BROADCAST)
*
* EVALUATION DELAY TIMES (SECONDS) FOR THE 3 EVACUATION ZONES
*
EZEDELAY001    0.  0.  5400.  * PEACH BOTTOM
*
* RADIAL EVACUATION SPEED (METERS / SECOND)
*
EZESPEED001    4.8  * PEACH BOTTOM
*
*****
* EMERGENCY RESPONSE DEFINITION, LOADED BY INPENR, STORED IN /SRZONE/,/PHASE2/
*
* TIME TO TAKE SHELTER IN THE INNER SHELTER ZONE (SECONDS FROM ALARM)
*
SRTTOSH1001    0.  (THIS ZONE IS NULL BECAUSE INIEVA=0)
*
* SHELTER TIME IN THE INNER SHELTER ZONE (SECONDS)
*
SRSHELT1001    0.  (THIS ZONE IS NULL BECAUSE INIEVA=0)
*
* LAST RING OF THE OUTER SHELTER ZONE
*
SRLASHE2001    0  (THIS ZONE IS NULL)
*
* TIME TO TAKE SHELTER IN THE OUTER SHELTER ZONE (SECONDS FROM ALARM)
*
SRTTOSH2001    0.  (THIS ZONE IS NULL)
*
* SHELTER TIME IN THE OUTER SHELTER ZONE (SECONDS)
*
SRSHELT2001    0.  (THIS ZONE IS NULL)
*
* DURATION OF THE EMERGENCY PHASE (SECONDS FROM PLUME ARRIVAL)
*
SRENDEMP001    604800.  (ONE WEEK)
*
* CRITICAL ORGAN FOR RELOCATION DECISIONS
*
SRCRIORG001    'EDEWBODY'
*
* HOT SPOT RELOCATION TIME (SECONDS FROM PLUME ARRIVAL)
*
SRTIMHOT001    43200.  (ONE-HALF DAY)
*

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* NORMAL RELOCATION TIME (SECONDS FROM PLUME ARRIVAL)
*
SRTIMNRM001  86400.      (ONE DAY)
*
* HOT SPOT RELOCATION DOSE CRITERION THRESHOLD (SIEVERTS)
*
SRDOSHOT001  0.5      (PROJECTED WHOLE BODY DOSE OF 50 IN 1 WEEK TRIGGERS
*                      RELOCATION AT ONE-HALF DAY)
*
* NORMAL RELOCATION DOSE CRITERION THRESHOLD (SIEVERTS)
*
SRDOSNRM001  0.25      (PROJECTED WHOLE BODY DOSE OF 25 IN 1 WEEK TRIGGERS
*                      RELOCATION AT ONE DAY)
*
*****
* EARLY FATALITY MODEL PARAMETERS, LOADED BY INEFAT, STORED IN /EFATAL/
*
* NUMBER OF EARLY FATALITY EFFECTS
*
EFNUMEFA001  3
*
*                      LD50 by t
*      ORGNAM      EFFACA  EFFACB  EFFTHR  1  7 14 30 200 365
*
EFATAGRP001 'RED MARR'      4.      6.      1.5      4      8 16
EFATAGRP002 'LUNGS'      10.0      7.      5.0     10     160    370 920
EFATAGRP003 'LOWER LI'    15.      10.      7.5     15     35
*
* NOTE: LUNG PARAMETERS TAKEN FROM LETTER FROM B. SCOTT TO N. WALD DATED
*       3/7/87; SHAPE FACTOR OF 7 IS APPROPRIATE FOR EXTERNAL AND INTERNAL
*       DOSE DELIVERED AT THE SAME TIME.
*
*****
* EARLY INJURY MODEL PARAMETERS, LOADED BY INEINJ, STORED IN /EINJUR/
*
* NUMBER OF EARLY INJURY EFFECTS
*
EINUMEIN001  7
*
*                      D50 vs t
*      EINAME      ORGNAM  EISUSC EITHRE EIFACA EIFACB  1  7 10 21
*
EINJUGRP001 'PRODRMAL VOMIT' 'STOMACH' 1.      .5      2.      3.      2  5
EINJUGRP002 'DIARRHEA'      'STOMACH' 1.      1.      3.      2.5     3  6
EINJUGRP003 'PNEUMONITIS'   'LUNGS'  1.      5.     10.      7.      = DEATH
EINJUGRP004 'SKIN ERYTHEMA'  'SKIN'  1.      3.      6.      5.      6  20
EINJUGRP005 'TRANSEPIDERMAL' 'SKIN'  1.     10.     20.      5.     20  80
EINJUGRP006 'THYROIDITIS'   'THYROIDH' 1.     40.    240.      2.      240
EINJUGRP007 'HYPOTHYROIDISM' 'THYROIDH' 1.      2.     60.      1.3     60
*EINJUGRP008 'FETAL DEATH'   'EMBRYO' 0.012 0.1      2.      2.2    TO 270d
*EINJUGRP009 'MENTAL RETARD' 'EMBRYO' 0.0048 0.      2.5     1.      TO 175d
*EINJUGRP010 'MICROCEPHALY' 'EMBRYO' 0.0053 0.05    0.7      0.4    TO 119d
*
* NOTE: THYROIDH ACUTE DOSE CONVERSION FACTORS ARE USED TO CALCULATE
*       THYROID INJURIES. WHEN THESE DOSE FACTORS WERE CALCULATED,
*       INHALATION DOSE FACTORS FOR IODINE ISOTOPES WERE REDUCED BY A
*       FACTOR OF FIVE TO ACCOUNT FOR THE REDUCED EFFECTIVENESS OF DOSE FROM
*       IODINE ISOTOPES. 0.0048 = 0.012 X 0.4; 0.0053 = 0.012 X (17X7)/270.
*
*****
* ACUTE EXPOSURE CANCER PARAMETERS, LOADED BY INACAN STORED IN /ACANCR/.
*
* NUMBER OF ACUTE EXPOSURE CANCER EFFECTS
*
LCNUMACA001  7
*
* DOSE THRESHOLD FOR LINEAR DOSE RESPONSE (SV)
*
LCACTHRE001  1.5
*
*      ACNAME      ORGNAM  ACSUSC DOSEFA DOSEFB CFRISK CIRISK

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LCANCERS001	'LEUKEMIA'	'RED MARR'	1.	.39	.61	3.7E-3	3.7E-3
LCANCERS002	'BONE'	'BONE SUR'	1.	.39	.61	1.5E-4	1.5E-4
LCANCERS003	'BREAST'	'BREAST'	1.	1.	0.	6.0E-3	1.7E-2
LCANCERS004	'LUNG'	'LUNGS'	1.	.39	.61	5.1E-3	5.7E-3
LCANCERS005	'THYROID'	'THYROIDH'	1.	1.	0.	7.2E-4	7.2E-3
LCANCERS006	'GI'	'LOWER LI'	1.	.39	.61	1.5E-2	2.5E-2
LCANCERS007	'OTHER'	'LOWER LI'	1.	.39	.61	7.5E-3	1.3E-2
*LCANCERS008	'SKIN'	'SKIN'	1.	1.0	0.0	0.0	6.7E-3
*LCANCERS009	'LEUK UTERO'	'FETAL BONE'	0.012	0.4	0.0	3.0E-2	3.0E-2
*LCANCERS010	'OTHR UTERO'	'FETAL OTHR'	0.012	0.4	0.0	3.0E-2	3.0E-2
*LCANCERS011	'DOMINANT'	'GONADS'	1.	0.5	0.5	0.0	1.4E-2
*LCANCERS012	'X-LINKED'	'GONADS'	1.	0.5	0.5	0.0	4.4E-2
*LCANCERS013	'ANEUPLOIDY'	'GONADS'	1.	1.	0.0	0.0	5.0E-4
*LCANCERS014	'TRANSLOCAT'	'GONADS'	1.	0.5	0.5	0.0	2.0E-3
*LCANCERS015	'M-FACTOR'	'GONADS'	1.	0.5	0.5	0.0	1.4E-2
*LCANCERS016	'PREG LOSS'	'GONADS'	1.	0.74	0.26	0.0	3.5E-2

* NOTE: THYROIDH LIFETIME DOSE CONVERSION FACTORS ARE USED TO CALCULATE THYROID CANCERS. WHEN THESE DOSE FACTORS WERE CALCULATED, INHALATION AND INGESTION DOSE FACTORS FOR IODINE ISOTOPES WERE REDUCED BY A FACTOR OF THREE TO ACCOUNT FOR THE REDUCED EFFECTIVENESS OF DOSE FROM IODINE ISOTOPES. $0.74 = (17 + 9)/(17 + 9 + 9)$ AND $0.26 = 1.0 - 0.74$. GONADS DOSE FACTOR = (TESTES DOSE FACTOR + OVARIES DOSE FACTOR)/2. SKIN CANCER IS ASSUMED TO BE LINEAR (SEE NUREG/CR-4214 PAGE II-122). GENETIC EFFECTS ARE INTEGRATED OVER ALL FUTURE GENERATIONS (SEE HARVARD REPORT FOR FRACTIONS IN EACH GENERATION).

* RESULT 1 OPTIONS BLOCK, LOADED BY INOUT1, STORED IN /INOUT1/
* TOTAL NUMBER OF A GIVEN EFFECT (LATENT CANCER, EARLY DEATH, EARLY INJURY)

* NUMBER OF DESIRED RESULTS OF THIS TYPE

TYPE1NUMBER	35
TYPE1OUT001	'ERL FAT/TOTAL' 1 26 (0 TO 1000 MILES)
TYPE1OUT002	'ERL INJ/PRODRMAL VOMIT' 1 26
TYPE1OUT003	'ERL INJ/DIARRHEA' 1 26
TYPE1OUT004	'ERL INJ/PNEUMONITIS' 1 26
TYPE1OUT005	'ERL INJ/THYROIDITIS' 1 26
TYPE1OUT006	'ERL INJ/HYPOTHYROIDISM' 1 26
TYPE1OUT007	'ERL INJ/SKIN ERYTHEMA' 1 26
TYPE1OUT008	'ERL INJ/TRANSEPIDERMAL' 1 26
TYPE1OUT009	'CAN FAT/TOTAL' 1 26
TYPE1OUT010	'CAN FAT/LUNG' 1 26
TYPE1OUT011	'CAN FAT/THYROID' 1 26
TYPE1OUT012	'CAN FAT/BREAST' 1 26
TYPE1OUT013	'CAN FAT/GI' 1 26
TYPE1OUT014	'CAN FAT/LEUKEMIA' 1 26
TYPE1OUT015	'CAN FAT/BONE' 1 26
TYPE1OUT016	'CAN FAT/OTHER' 1 26
TYPE1OUT017	'CAN INJ/TOTAL' 1 26
TYPE1OUT018	'ERL FAT/TOTAL' 1 19 (0 TO 50 MILES)
TYPE1OUT019	'ERL INJ/PRODRMAL VOMIT' 1 19
TYPE1OUT020	'ERL INJ/DIARRHEA' 1 19
TYPE1OUT021	'ERL INJ/PNEUMONITIS' 1 19
TYPE1OUT022	'ERL INJ/THYROIDITIS' 1 19
TYPE1OUT023	'ERL INJ/HYPOTHYROIDISM' 1 19
TYPE1OUT024	'ERL INJ/SKIN ERYTHEMA' 1 19
TYPE1OUT025	'ERL INJ/TRANSEPIDERMAL' 1 19
TYPE1OUT026	'CAN FAT/TOTAL' 1 19
TYPE1OUT027	'ERL FAT/TOTAL' 1 12 (0 TO 10 MILES)
TYPE1OUT028	'ERL INJ/PRODRMAL VOMIT' 1 12
TYPE1OUT029	'ERL INJ/DIARRHEA' 1 12
TYPE1OUT030	'ERL INJ/PNEUMONITIS' 1 12
TYPE1OUT031	'ERL INJ/THYROIDITIS' 1 12

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TYPE1OUT032      'ERL INJ/HYPOTHYROIDISM'      1  12
TYPE1OUT033      'ERL INJ/SKIN ERYTHEMA'        1  12
TYPE1OUT034      'ERL INJ/TRANSEPIDERMAL'       1  12
TYPE1OUT035      'CAN FAT/TOTAL'               1  12
*****
* RESULT 2 OPTIONS BLOCK, LOADED BY INOUT2, STORED IN /INOUT2/
* FURTHEST DISTANCE AT WHICH A GIVEN RISK OF EARLY DEATH IS EXCEEDED.
*
* NUMBER OF DESIRED RESULTS OF THIS TYPE
*
TYPE2NUMBER      1
*
*          FATALITY RISK THRESHOLD
*
TYPE2OUT001      0.
*****
* RESULT 3 OPTIONS BLOCK, LOADED BY INOUT3, STORED IN /INOUT3/
* NUMBER OF PEOPLE WHOSE ACUTE DOSE TO A GIVEN ORGAN EXCEEDS A GIVEN THRESHOLD.
*
* NUMBER OF DESIRED RESULTS OF THIS TYPE
*
TYPE3NUMBER      2
*
*          ORGAN NAME      DOSE THRESHOLD (SV)
*
TYPE3OUT001      'RED MARR'          1.5
TYPE3OUT002      'LUNGS'            5.0
*****
* RESULT 4 OPTIONS BLOCK, LOADED BY INOUT4, STORED IN /INOUT4/
* 360 DEGREE AVERAGE RISK OF A GIVEN EFFECT AT A GIVEN DISTANCE.
*
* POSSIBLE TYPES OF EFFECTS ARE:
*
*   'ERL FAT/TOTAL'
*   'ERL INJ/INJURY NAME'
*   'CAN FAT/CANCER NAME'
*   'CAN FAT/TOTAL'
*
* NUMBER OF DESIRED RESULTS OF THIS TYPE
*
TYPE4NUMBER      5
*
*          RADIAL INDEX      TYPE OF EFFECT
*
TYPE4OUT001      1          'ERL FAT/TOTAL'
TYPE4OUT002      2          'ERL FAT/TOTAL'
TYPE4OUT003      3          'ERL FAT/TOTAL'
TYPE4OUT004      4          'ERL FAT/TOTAL'
TYPE4OUT005      5          'ERL FAT/TOTAL'
*****
* RESULT 5 OPTIONS BLOCK, LOADED BY INOUT5, STORED IN /INOUT5/
*
* TOTAL POPULATION DOSE TO A GIVEN ORGAN BETWEEN TWO DISTANCES.
*
* NUMBER OF DESIRED RESULTS OF THIS TYPE
*
TYPE5NUMBER      3
*
*          ORGAN          I1DIS5          I2DIS5
*
TYPE5OUT001      'EDEWBODY'          1          12      (0-10 MILES)
TYPE5OUT002      'EDEWBODY'          1          19      (0-50 MILES)
TYPE5OUT003      'EDEWBODY'          1          26      (0-1000 MILES)
*****
* RESULT 6 OPTIONS BLOCK, LOADED BY INOUT6, STORED IN /INOUT6/
*

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* CENTERLINE DOSE TO AN ORGAN VS DIST BY PATHWAY, PATHWAY NAMES ARE AS FOLLOWS:

* PATHWAY NAME:

* 'CLD' - CLOUDSHINE
 * 'GRD' - GROUNDSHINE
 * 'INH ACU' - "ACUTE DOSE EQUIVALENT" FROM DIRECT INHALATION OF THE CLOUD
 * 'INH LIF' - "LIFETIME DOSE COMMITMENT" FROM DIRECT INHALATION OF THE CLOUD
 * 'RES ACU' - "ACUTE DOSE EQUIVALENT" FROM RESUSPENSION INHALATION
 * 'RES LIF' - "LIFETIME DOSE COMMITMENT" FROM RESUSPENSION INHALATION
 * 'TOT ACU' - "ACUTE DOSE EQUIVALENT" FROM ALL PATHWAYS
 * 'TOT LIF' - "LIFETIME DOSE COMMITMENT" FROM ALL PATHWAYS

* NUMBER OF DESIRED RESULTS OF THIS TYPE

TYPE6NUMBER 0

	ORGNAM	PATHNM	I1DIS6	I2DIS6	
*TYPE6OUT001	'RED MARR'	'TOT ACU'	1	19	(0-50 MILES)
*TYPE6OUT002	'LUNGS'	'TOT ACU'	1	19	(0-50 MILES)
*TYPE6OUT003	'EDEWBODY'	'TOT LIF'	1	26	(0-1000 MILES)

* RESULT 7 OPTIONS BLOCK, LOADED BY INOUT7, STORED IN /INOUT7/

* CENTERLINE RISK OF A GIVEN EFFECT VS DISTANCE

* NUMBER OF DESIRED RESULTS OF THIS TYPE

TYPE7NUMBER 0

	NAME	I1DIS7	I2DIS7	
*TYPE7OUT001	'ERL FAT/TOTAL'	1	19	(0-50 MILES)
*TYPE7OUT002	'CAN FAT/TOTAL'	1	26	(0-1000 MILES)

* RESULT 8 OPTIONS BLOCK, LOADED BY INOUT8, STORED IN /INOUT8/

* POPULATION WEIGHTED FATALITY RISK BETWEEN 2 DISTANCES

* NUMBER OF DESIRED RESULTS OF THIS TYPE

TYPE8NUMBER 2

	NAME	I1DIS8	I2DIS8	
TYPE8OUT001	'ERL FAT/TOTAL'	1	5	(0-EXCL ZONE + 1 MI)
TYPE8OUT002	'CAN FAT/TOTAL'	1	12	(0-10 MILES)

A.3 CHRONC

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*****
* FILE NAME: 1150CH.INP
*
* GENERAL DESCRIPTIVE TITLE DESCRIBING THIS "CHRONC" INPUT FILE
*
CHCHNAME001 'CHRONC INPUT FOR FINAL NUREG-1150 CALCULATIONS'
*****
* EMERGENCY RESPONSE COST DATA BLOCK
*
* EVACUATION COST (DOLLARS/PERSON-DAY)
*
CHEVACST001 27.00
*
* RELOCATION DOST (DOLLARS/PERSON-DAY)
*
CHRELCST001 27.00
*****
* LONG TERM PROTECTIVE ACTION DATA BLOCK
*
* END OF THE INTERMEDIATE PHASE PERIOD (SECONDS FROM ACCIDENT INITIATION)
*
CHTMIPND001 604800. (7 DAYS, NO INTERMEDIATE PHASE)
*
* ACTION PERIOD (PROJECTION PERIOD) FROM THE START OF THE LONG TERM PHASE,
* THE POINT AT WHICH THE LONG TERM DOSE CRITERION IS EVALUATED (SECONDS)
*
CHTMPACT001 1.58E8 (5 YEARS)
*
* DOSE CRITERION FOR INTERMEDIATE PHASE RELOCATION (SV)
*
CHDSCRTI001 1.0E5 (NO INTERMEDIATE PHASE RELOCATION)
*
* DOSE CRITERION FOR LONG TERM PHASE RELOCATION (SV)
*
CHDSCRLT001 0.04 (2 REM IN FIRST YEAR, 0.5 REM PER YEAR FOR YRS 2 - 5)
*
* CRITICAL ORGAN NAME FOR LONG-TERM ACTIONS
*
CHCRTOCR001 'EDEWBODY'
*
*****
* DECONTAMINATION PLAN DATA BLOCK
*
* NUMBER OF LEVELS OF DECONTAMINATION
*
CHLVLDEC001 2
*
* DECONTAMINATION TIMES (SECONDS) CORRESPONDING TO THE LVLDEC LEVELS
* OF DECONTAMINATION
*
CHTIMDEC001 5.184E6 1.0368E7 (60, 120 DAYS)
*
* DOSE REDUCTION FACTORS CORRESPONDING TO THE LVLDEC LEVELS OF DECONTAMINATION
*
CHDSRFCT001 3. 15.
*
* COST OF FARM DECONTAMINATION PER UNIT AREA (DOLLARS/HECTARE)
* FOR THE VARIOUS LEVELS OF DECONTAMINATION
*
CHCDFRM0001 562.5 1250.
*
* COST OF NONFARM DECONTAMINATION PER PERSON (DOLLARS/PERSON)
* FOR THE VARIOUS LEVELS OF DECONTAMINATION
*
CHCDNFRM001 3000. 8000.

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*
* FRACTION OF FARMLAND DECONTAMINATION COST DUE TO LABOR
* FOR THE VARIOUS DECONTAMINATION LEVELS
*
CHFRFDL0001  0.3      0.35
*
* FRACTION OF NON-FARM DECONTAMINATION COST DUE TO LABOR
* FOR THE VARIOUS DECONTAMINATION LEVELS
*
CHFRNFDL001  0.7      0.5
*
* FRACTION OF TIME WORKERS IN FARM AREAS SPEND IN DECONTAMINATION WORK
* FOR THE VARIOUS DECONTAMINATION LEVELS
*
CHTFWK0001  0.10     0.33
*
* FRACTION OF TIME WORKERS IN NON-FARM AREAS SPEND IN DECONTAMINATION WORK
* FOR THE VARIOUS DECONTAMINATION LEVELS
*
CHTFWKNF001  0.33     0.33
*
* AVERAGE COST OF DECONTAMINATION LABOR (DOLLARS/MAN-YEAR)
*
CHDLBCST001  35000.
*****
* INTERDICTION COST DATA BLOCK
*
* DEPRECIATION RATE DURING INTERDICTION PERIOD (PER YEAR)
*
CHDPRATE001  0.20
*
* SOCIETAL DISCOUNT RATE DURING INTERDICTION PERIOD (PER YEAR)
*
CHDSRATE001  0.12
*
* URBAN POPULATION REMOVAL COST (DOLLARS/PERSON)
*
CHPOPCST001  5000.
*****
* GROUNDSHINE WEATHERING DEFINITION DATA BLOCK
*
* NUMBER OF TERMS IN THE GROUNDSHINE WEATHERING RELATIONSHIP (EITHER 1 OR 2)
*
CHNGWTRM001  2
*
* GROUNDSHINE WEATHERING COEFFICIENTS
*
CHGWCOEF001  0.5      0.5      (GAYLE'S EQUATION)
*
* HALF LIVES CORRESPONDING TO THE GROUNDSHINE WEATHERING COEFFICIENTS (S)
*
CHTGWHLF001  1.6E7  2.8E9      (GAYLE'S EQUATION)
*****
* RESUSPENSION WEATHERING DEFINITION DATA BLOCK
*
* NUMBER OF TERMS IN THE RESUSPENSION WEATHERING RELATIONSHIP
*
CHNRWTRM001  3
*
* RESUSPENSION CONCENTRATION COEFFICIENTS (/ METER)
* RELATIONSHIP BETWEEN GROUND CONCENTRATION AND INSTANTANEOUS AIR CONC.
*
CHRWCOEF001  1.0E-5  1.0E-7  1.0E-9
*
* HALF-LIVES CORRESPONDING TO THE RESUSPENSION CONCENTRATION COEFFICIENTS (S)
*

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CHTRWHLF001  1.6E7    1.6E8    1.6E9    (6 MONTHS, 5 YEARS, 50 YEARS)
*****
* SITE REGION DESCRIPTION DATA BLOCK
*
* FRACTION OF AREA THAT IS LAND IN THE REGION
*
CHFRACLD001  1.0E-35    (VALUE NOT USED SINCE SITE FILE PROVIDED)
*
* FRACTION OF LAND DEVOTED TO FARMING IN THE REGION
*
CHFRCFRM001  1.0E-35    (VALUE NOT USED SINCE SITE FILE PROVIDED)
*
* AVERAGE VALUE OF ANNUAL FARM PRODUCTION IN THE REGION (DOLLARS/HECTARE)
* (CASH RECEIPTS FROM FARMING PLUS VALUE OF HOME CONSUMPTION)/(LAND IN FARMS)
*
CHFRMPRD001  0.          (VALUE NOT USED SINCE SITE FILE PROVIDED)
*
* FRACTION OF FARM PRODUCTION RESULTING FROM DAIRY PRODUCTION IN THE REGION
* (VALUE OF MILK PRODUCED)/(CASH RECEIPTS FROM FARMING PLUS VALUE OF HOME...)
*
CHDPFRCT001  0.          (VALUE NOT USED SINCE SITE FILE PROVIDED)
*
* VALUE OF FARM WEALTH (DOLLARS/HECTARE): AVERAGE VALUE OF FARM LAND
* AND BUILDINGS PER HECTARE TO 100 MILES
*
* SITE          GG      LS      PB      SEQ      SUR      ZION
* VALWF ($/HECTARE) 2561  3305  3421  1855  2613  2897
*
CHVALWF0001  3421. * PEACH BOTTOM
*
* FRACTION OF FARM WEALTH IN IMPROVEMENTS FOR THE REGION
*
* SITE  GG      LS      PB      SEQ      SUR      ZION
* FRFIM 0.3    0.19  0.25  0.27  0.25  0.49
*
CHFRFIM0001  0.25 * PEACH BOTTOM
*
* NON-FARM WEALTH, PROPERTY AND IMPROVEMENTS FOR THE REGION (DOLLARS/PERSON)
* THE VALUE OF ALL RESIDENTIAL, BUSINESS, AND PUBLIC ASSETS WHICH WOULD BE
* LOST IN THE EVENT OF PERMANENT INTERDICTION OF THE AREA
*
* SITE          GG      PB      SUR      SEQ      ZION
* VALWNF ($K)  53      78      84      66      76
*
CHVALWNF001  78000. * PEACH BOTTOM
*
* FRACTION OF NON-FARM WEALTH IN IMPROVEMENTS FOR THE REGION
*
CHFRNFIM001  0.8
*****
* SPECIAL OPTIONS DATA BLOCK
*
* DETAILED PRINT OPTION CONTROL SWITCHES, LOOK AT THE CODE BEFORE TURNING ON!!
* (KCEPNT, KDFPNT, KDPNT, KGCPNT, KLTPNT, KWTPNT, KSWRSK, KSWDSC)
*
CHKSWTCH001  0 0 0 0 0 0 0 0 0 0 0 0
*****
* WATER PATHWAY NUCLIDE DEFINITIONS FOR CHRONC
*
* NUMBER OF NUCLIDES IN THE WATER INGESTION PATHWAY MODEL
*
CHNUMWPI001  4
*
* TABLE OF NUCLIDE DEFINITIONS IN THE WATER INGESTION PATHWAY MODEL
* WATER PATHWAY NUCLIDES MUST BE A SUBSET OF THE INGESTION MODEL NUCLIDES
*

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* IF A SITE DATA FILE IS DEFINED, THE DATA DEFINING THE WATERSHED INGESTION
 * FACTOR IS SUPERSEDED BY THE CORRESPONDING DATA IN THE SITE DATA FILE

* WINGF VALUES BY DRAINAGE SYSTEM

NUCLIDE	SR-89	SR-90	CS-134	CS-137
RIVER	5.0E-6	5.0E-6	5.0E-6	5.0E-6
GREAT LAKE	2.0E-7	2.0E-7	2.0E-6	4.0E-6
OCEAN	0.0	0.0	0.0	0.0

* ALL NUREG-1150 SITES HAVE RIVER DRAINAGE SYSTEMS EXCEPT LASALLE AND ZION

WATER NUCLIDE	INITIAL WASHOFF FRACTION	ANNUAL WASHOFF RATE	INGESTION FACTOR ((BQ INGESTED)/ (BQ IN WATER))
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	NAMWPI	WSHFRI	WSHRTA	WINGF
CHWTRISO001	SR-89	0.01	0.004	5.0E-6
CHWTRISO002	SR-90	0.01	0.004	5.0E-6
CHWTRISO003	CS-134	0.005	0.001	5.0E-6
CHWTRISO004	CS-137	0.005	0.001	5.0E-6

 * CROP PATHWAY DEFINITIONS FOR CHRONC

* MODIFIED 14 OCT 88, BY JLS, VALUES CHANGED TO THOSE DEVELOPED BY J. ROLLSTIN

* NUMBER OF DEFINED CROPS IN THE CHRONC FOOD INGESTION MODEL

* CHNFICRP001 7 (UP TO 10 ALLOWED)

* NOTE TO USER: THE CODE MAKES SPECIAL TREATMENT OF CROP NAMES BEGINNING WITH
 * 'PASTURE' DUE TO THE CONTINUOUS NATURE OF THE HARVESTING PROCESS.

* IF THE USER WISHES TO DEFINE A NEW CROP CATEGORY FOR RANGELAND PASTURE,
 * IT SHOULD BE CALLED 'PASTURE-RANGE' OR 'PASTURE-DRY'

* TABLE OF CROP DEFINITIONS FOR THE CHRONC FOOD INGESTION MODEL

* FRACTION OF CROP CONSUMED BY

CROP NAME	MAN	DAIRY	MEAT
		ANIMALS	ANIMALS
NAMCRP	FRCTCH	FRCTCM	FRCTCB
CHCRPTBL001 'PASTURE	0.0	0.1	0.9
CHCRPTBL002 'STORED FORAGE	0.0	0.13	0.87
CHCRPTBL003 'GRAINS	0.35	0.040	0.61
CHCRPTBL004 'GRN LEAFY VEGETABLES	1.0	0.0	0.0
CHCRPTBL005 'OTHER FOOD CROPS	1.0	0.0	0.0
CHCRPTBL006 'LEGUMES AND SEEDS	0.24	0.046	0.714
CHCRPTBL007 'ROOTS AND TUBERS	1.0	0.0	0.0

 * CHRONC INGESTION PATHWAY NUCLIDE DEFINITIONS

* NUMBER OF NUCLIDES IN THE CHRONC FOOD INGESTION MODEL

* CHNFIISO001 6 (UP TO 10 ALLOWED, BEWARE THAT DAUGHTER BUILDUP IS NOT TREATED)

* TABLE OF NUCLIDE DEFINITIONS IN THE CHRONC INGESTION PATHWAY MODEL

* NUCLIDES THAT WERE DEFINED IN THE WATER PATHWAY DATA ABOVE MUST BE
 * A SUBSET OF THE CHRONC INGESTION FOOD PATHWAY NUCLIDES. THE WATER
 * PATHWAY NUCLIDES MUST BE LISTED FIRST IN THIS DATA BLOCK AND IN THE
 * SAME ORDER AS THEY WERE LISTED IN THE WATER PATHWAY DATA BLOCK

RETENTION FACTORS	TRANSFER FACTORS [(BQ TRANSFERED)/
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*          INGESTION  PROCESSING AND DECAY  (BQ INGESTED)]
*          NUCLIDE    MILK/MAN  MEAT/MAN    MILK      MEAT
*
*          NAMIPI      DCYPMH    DCYPBH      TFMLK    TFBF
CHISODEF001  SR-89      0.66      0.77      0.022    0.00022
CHISODEF002  SR-90      1.0       1.0       0.022    0.00022
CHISODEF003  CS-134     1.0       1.0       0.11     0.023
CHISODEF004  CS-137     1.0       1.0       0.11     0.024
CHISODEF005  I-131      0.28      0.18      0.13     0.0024
CHISODEF006  I-133      0.002     0.0       0.062    0.0011
*****
*  TRANSFER FACTOR FROM SOIL TO PLANT BY ROOT-UPTAKE (AND BY SOIL INGESTION FOR
*  GRAZING ON PASTURE) INTEGRATED OVER ALL TIME [(BQ TRANSFERED)/(BQ DEPOSITED)]
*
*
*          NUCLIDE  PASTURE  STORED  GREEN  OTHER  LEGUMES  ROOTS
*                   FORAGE  GRAINS  LEAFY  FOOD   AND     AND
*                   VEG     CROPS  SEEDS  TUBERS
*
*          NAMISO    TCROOT  TCROOT  TCROOT  TCROOT  TCROOT  TCROOT  TCROOT
CHTCROOT001  SR-89    4.1E-4  1.3E-3  4.3E-5  1.7E-4  8.6E-6  3.7E-4  1.1E-4
CHTCROOT002  SR-90    2.6E-2  9.0E-2  3.3E-3  1.3E-2  6.6E-4  2.8E-2  8.4E-3
CHTCROOT003  CS-134   1.3E-3  7.1E-4  3.5E-5  1.4E-5  1.1E-4  9.3E-5  5.6E-5
CHTCROOT004  CS-137   6.9E-3  1.5E-3  7.6E-5  3.0E-5  2.3E-4  2.0E-4  1.2E-4
CHTCROOT005  I-131    1.6E-4  0.0     0.0     0.0     0.0     0.0     0.0
CHTCROOT006  I-133    1.7E-6  0.0     0.0     0.0     0.0     0.0     0.0
*****
*  RADIOACTIVE DECAY RETENTION FACTORS (I.E., 1 - F WHERE F = FRACTION OF
*  RADIOACTIVITY LOST BY DECAY) FOR NUCLIDES IN CROPS FROM TIME OF HARVEST
*  TO TIME OF CONSUMPTION BY HUMANS (FRACTION RETAINED)
*
*
*          NUCLIDE  PASTURE  STORED  GREEN  OTHER  LEGUMES  ROOTS
*                   FORAGE  GRAINS  LEAFY  FOOD   AND     AND
*                   VEG     CROPS  SEEDS  TUBERS
*
*          NAMISO    DCYPCH  DCYPCH  DCYPCH  DCYPCH  DCYPCH  DCYPCH  DCYPCH
CHDCYPCH001  SR-89      0.0     0.0     0.18    0.67    0.21    0.18    0.18
CHDCYPCH002  SR-90      0.0     0.0     0.99    1.0     0.99    0.99    0.99
CHDCYPCH003  CS-134     0.0     0.0     0.84    0.96    0.85    0.84    0.84
CHDCYPCH004  CS-137     0.0     0.0     0.99    1.0     0.99    0.99    0.99
CHDCYPCH005  I-131     0.0     0.0     0.0099  0.21    0.024   0.0099  0.0099
CHDCYPCH006  I-133     0.0     0.0     0.0     0.0     0.0     0.0     0.0
*****
*  CROP PROCESSING AND PREPARATION RETENTION FACTORS FOR NUCLIDES IN FOOD
*  CROPS CONSUMED BY HUMANS (FRACTION RETAINED).  FACTORS REFLECT LOSS OF
*  NUCLIDES FROM FOODS DUE TO PROCESSING (E.G., WASHING OF FRUIT, PEELING
*  OF POTATOES, LOSSES DURING CANNING) AND FOOD PREPARATION (COOKING) FROM
*  THE TIME OF PROCESSING OF THE HARVESTED CROP TO THE TIME OF CONSUMPTION
*  BY HUMANS.  FACTORS DO NOT REFLECT LOSSES DUE TO RADIOACTIVE DECAY.
*
*
*          NUCLIDE  PASTURE  STORED  GREEN  OTHER  LEGUMES  ROOTS
*                   FORAGE  GRAINS  LEAFY  FOOD   AND     AND
*                   VEG     CROPS  SEEDS  TUBERS
*
*          NAMISO    FPLSCH  FPLSCH  FPLSCH  FPLSCH  FPLSCH  FPLSCH  FPLSCH
CHFPLSCH001  SR-89      0.0     0.0     0.25    0.5     0.71    0.8     0.8
CHFPLSCH002  SR-90      0.0     0.0     0.25    0.5     0.71    0.8     0.8
CHFPLSCH003  CS-134     0.0     0.0     0.25    0.5     0.71    0.8     0.8
CHFPLSCH004  CS-137     0.0     0.0     0.25    0.5     0.71    0.8     0.8
CHFPLSCH005  I-131     0.0     0.0     0.33    0.5     0.71    0.8     0.8
CHFPLSCH006  I-133     0.0     0.0     0.33    0.5     0.71    0.8     0.8
*****
*  RETENTION FACTORS FOR NUCLIDES IN CROPS FROM TIME OF HARVEST TO TIME OF
*  CONSUMPTION BY MILK-PRODUCING ANIMALS (FRACTION RETAINED).  FACTOR REFLECTS
*  LOSSES DUE TO RADIOACTIVE DECAY.
*
*
*          GREEN  OTHER  LEGUMES  ROOTS

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*
*          NUCLIDE   PASTURE   STORED   GREEN   OTHER   LEGUMES   ROOTS
*          NUCLIDE   PASTURE   FORAGE   LEAFY   FOOD    AND      AND
*          NUCLIDE   PASTURE   FORAGE   VEG     CROPS   SEEDS   TUBERS
*
*          NAMISO    DCYPCM   DCYPCM   DCYPCM   DCYPCM   DCYPCM   DCYPCM
CHDCYPCM001 SR-89      1.0     0.37    0.20    0.0     0.0     0.20    0.0
CHDCYPCM002 SR-90      1.0     0.99    0.99    0.0     0.0     0.99    0.0
CHDCYPCM003 CS-134     1.0     0.92    0.85    0.0     0.0     0.85    0.0
CHDCYPCM004 CS-137     1.0     0.99    0.99    0.0     0.0     0.99    0.0
CHDCYPCM005 I-131     1.0     0.063   0.032   0.0     0.0     0.032   0.0
CHDCYPCM006 I-133     1.0     0.0068  0.0034  0.0     0.0     0.0034  0.0
*****
* RETENTION FACTORS FOR NUCLIDES IN CROPS FROM TIME OF HARVEST TO TIME OF
* CONSUMPTION BY MEAT-PRODUCING ANIMALS (FRACTION RETAINED). FACTOR REFLECTS
* LOSSES DUE TO RADIOACTIVE DECAY.
*
*          NUCLIDE   PASTURE   STORED   GREEN   OTHER   LEGUMES   ROOTS
*          NUCLIDE   PASTURE   FORAGE   LEAFY   FOOD    AND      AND
*          NUCLIDE   PASTURE   FORAGE   VEG     CROPS   SEEDS   TUBERS
*
*          NAMISO    DCYPCB   DCYPCB   DCYPCB   DCYPCB   DCYPCB   DCYPCB
CHDCYPCB001 SR-89      1.0     0.37    0.20    0.0     0.0     0.20    0.0
CHDCYPCB002 SR-90      1.0     0.99    0.99    0.0     0.0     0.99    0.0
CHDCYPCB003 CS-134     1.0     0.92    0.85    0.0     0.0     0.85    0.0
CHDCYPCB004 CS-137     1.0     0.99    0.99    0.0     0.0     0.99    0.0
CHDCYPCB005 I-131     1.0     0.063   0.032   0.0     0.0     0.032   0.0
CHDCYPCB006 I-133     1.0     0.0068  0.0034  0.0     0.0     0.0034  0.0
*****
* DEFINE THE DIRECT DEPOSITION TO CROPS TRANSFER FUNCTION
*
* NUMBER OF TERMS IN THE DIRECT DEPOSITION TO CROPS TRANSFER FUNCTION
*
CHNTRTRM001      2
*
* LOSSES DUE TO WEATHERING FROM PLANT SURFACES AND DURING TRANSLOCATION
* FROM PLANT SURFACES TO INTERIOR EDIBLE PORTIONS OF PLANTS ARE MODELLED
* USING THE FOLLOWING EQUATION:
*
* FRACTION RETAINED = CTCOEFL*EXP(-LN2/CTHALF1) + CTCOEF2*EXP(-LN2/CTHALF2)
*
* FOR PASTURE, STORED FORAGE, GREEN LEAFY VEGETABLES, AND OTHER FOOD CROPS,
* THIS EQUATION IS USED AS A TWO TERM WEATHERING EQUATION. FOR GRAINS,
* LEGUMES AND SEEDS, AND ROOTS AND TUBERS WHERE RADIOACTIVITY IS CONSUMED
* ONLY IF TRANSLOCATED TO EDIBLE PORTIONS OF THE PLANT, THIS EQUATION IS
* REDUCED TO A TRANSLOCATION TRANSFER FACTOR BY SETTING CTCOEF2 TO ZERO,
* CTHALF2 TO ONE SECOND, AND CTHALF1 TO ABOUT ONE MILLION YEARS (1E13
* SECONDS). WHEN USED TO MODEL TRANSLOCATION, THE VALUE OF THE TRANSLOCATION
* TRANSFER FACTOR IS DEVELOPED FROM FALLOUT DATA AND IS INPUT AS THE VALUE
* OF CTCOEFL.
*
* TWO TIME PERIODS ARE USED FOR WEATHERING, THE FIRST IS 14 DAYS LONG (1.21E6
* SECONDS) AND THE SECOND IS 50 DAYS LONG (4.32E6 SECONDS).
*
* DIRECT DEPOSITION TRANSFER COEFFICIENTS [(BQ TRANSFERED)/(BQ DEPOSITED)]
* BY CHRONC INGESTION MODEL NUCLIDE
*
*          TERM 1  NUCLIDE  PASTURE  STORED  GREEN  OTHER  LEGUMES  ROOTS
*          TERM 1  NUCLIDE  PASTURE  FORAGE  LEAFY  FOOD   AND     AND
*          TERM 1  NUCLIDE  PASTURE  FORAGE  VEG    CROPS  SEEDS   TUBERS
CHCTCOEF101 SR-89      0.3      0.2     0.01   0.24   0.2     0.005   0.0006
CHCTCOEF102 SR-90      0.3      0.2     0.01   0.24   0.2     0.005   0.0006
CHCTCOEF103 CS-134     0.3      0.2     0.05   0.24   0.2     0.01    0.025
CHCTCOEF104 CS-137     0.3      0.2     0.05   0.24   0.2     0.01    0.025
CHCTCOEF105 I-131     0.3      0.2     0.0    0.24   0.2     0.0     0.0
CHCTCOEF106 I-133     0.3      0.2     0.0    0.24   0.2     0.0     0.0
* TERM 2
CHCTCOEF201 SR-89      0.076    0.05    0.0    0.06   0.05    0.0     0.0

```

CHCTCOEF202	SR-90	0.076	0.05	0.0	0.06	0.05	0.0	0.0
CHCTCOEF203	CS-134	0.076	0.05	0.0	0.06	0.05	0.0	0.0
CHCTCOEF204	CS-137	0.076	0.05	0.0	0.06	0.05	0.0	0.0
CHCTCOEF205	I-131	0.076	0.05	0.0	0.06	0.05	0.0	0.0
CHCTCOEF206	I-133	0.076	0.05	0.0	0.06	0.05	0.0	0.0

*

* CROP TRANSFER HALF-LIVES BY CHRONC INGESTION MODEL NUCLIDE (SECONDS)

*

*

TERM 1	NUCLIDE	PASTURE	STORED FORAGE	GRAINS	GREEN LEAFY VEG	OTHER FOOD CROPS	LEGUMES AND SEEDS	ROOTS AND TUBERS
CHCTHALF101	SR-89	1.21E6	1.21E6	1E13	1.21E6	1.21E6	1E13	1E13
CHCTHALF102	SR-90	1.21E6	1.21E6	1E13	1.21E6	1.21E6	1E13	1E13
CHCTHALF103	CS-134	1.21E6	1.21E6	1E13	1.21E6	1.21E6	1E13	1E13
CHCTHALF104	CS-137	1.21E6	1.21E6	1E13	1.21E6	1.21E6	1E13	1E13
CHCTHALF105	I-131	1.21E6	1.21E6	1.0	1.21E6	1.21E6	1.0	1.0
CHCTHALF106	I-133	1.21E6	1.21E6	1.0	1.21E6	1.21E6	1.0	1.0

* TERM2

CHCTHALF201	SR-89	4.32E6	4.32E6	1.0	4.32E6	4.32E6	1.0	1.0
CHCTHALF202	SR-90	4.32E6	4.32E6	1.0	4.32E6	4.32E6	1.0	1.0
CHCTHALF203	CS-134	4.32E6	4.32E6	1.0	4.32E6	4.32E6	1.0	1.0
CHCTHALF204	CS-137	4.32E6	4.32E6	1.0	4.32E6	4.32E6	1.0	1.0
CHCTHALF205	I-131	4.32E6	4.32E6	1.0	4.32E6	4.32E6	1.0	1.0
CHCTHALF206	I-133	4.32E6	4.32E6	1.0	4.32E6	4.32E6	1.0	1.0

* TABLE OF CROP DATA (GROWING SEASON AND FARMLAND SHARE) IN THE REGION.

*

* IF A SITE DATA FILE IS BEING USED (AS SPECIFIED ON THE EARLY USER INPUT FILE),
 * THEN DATA FROM THE SITE FILE (AND NOT THE DATA BELOW) IS USED FOR THE
 * CALCULATION OF DOSES AND COSTS FROM THE AGRICULTURE MODEL AND THE NUMBERS
 * BELOW ARE IGNORED.

*

* IF A SITE DATA FILE IS NOT BEING USED, THE DATA BELOW IS USED IN ITS STEAD.

*

FARMLAND SHARE VALUES (FRCTFL) BY SITE AND CROP CATEGORY

*

SITE	GG	LS	PB	SEQ	SUR	ZION
PASTURE	0.70	0.47	0.38	0.69	0.41	0.45
STORED FORAGE	0.05	0.10	0.13	0.006	0.13	0.11
GRAINS	0.18	0.26	0.23	0.16	0.21	0.26
GRN LEAFY VEGETABLES	0.0005	0.0003	0.002	0.0007	0.002	0.0004
OTHER FOOD CROPS	0.004	0.001	0.004	0.005	0.004	0.001
LEGUMES AND SEEDS	0.13	0.13	0.16	0.15	0.15	0.13
ROOTS AND TUBERS	0.0008	0.002	0.004	0.001	0.003	0.002

*

GROWING

SEASON (DAYS) FARMLAND

*

CROP NAME START END SHARE

*

NAMCRP	TGSBEG	TGSEND	FRCTFL
CHCRPRGN001 'PASTURE	' 90.	270.	0.38
CHCRPRGN002 'STORED FORAGE	' 150.	240.	0.13
CHCRPRGN003 'GRAINS	' 150.	240.	0.23
CHCRPRGN004 'GRN LEAFY VEGETABLES	' 150.	240.	0.002
CHCRPRGN005 'OTHER FOOD CROPS	' 150.	240.	0.004
CHCRPRGN006 'LEGUMES AND SEEDS	' 150.	240.	0.16
CHCRPRGN007 'ROOTS AND TUBERS	' 150.	240.	0.004

* PROTECTIVE ACTION GUIDES FOR THE DIRECT DEPOSITION PATHWAY TO
 * MILK AND ITS PRODUCTS AND TO OTHER CROPS AND THEIR PRODUCTS
 * BY FOOD INGESTION MODEL NUCLIDE (PERMISSIBLE SURFACE
 * CONCENTRATION IN BECQUERELS PER SQUARE METER)

*

* PERMISSIBLE SURFACE CONCENTRATIONS WERE DERIVED BY INVERTING
 * THE FOOD PATHWAY MODEL THEREBY MAKING THE DOSE TO AN ORGAN THE

* INDEPENDENT VARIABLE AND GROUND CONCENTRATION THE DEPENDENT
 * VARIABLE. PERMISSIBLE GROUND CONCENTRATIONS WERE CALCULATED
 * ASSUMING (1) ALLOWABLE FIRST YEAR (I.E., DIRECT DEPOSITION)
 * ORGAN DOSES OF 15 REM PER YEAR TO THYROID AND 5 REM PER YEAR
 * TO ANY OTHER ORGAN; AND (2) ALLOWABLE DOSES IN SUBSEQUENT YEARS
 * (I.E., ROOT UPTAKE PATH) OF 1.5 REM TO THYROID AND 0.5 REM TO
 * ANY OTHER ORGAN.

	NUCLIDE	MILK AND PRODUCTS	OTHER CROPS AND PRODUCTS
	NAMIPI	PSCMLK	PSCOTH
CHPAGMCP001	SR-89	2.1E06	2.2E06
CHPAGMCP002	SR-90	4.6E04	5.1E04
CHPAGMCP003	CS-134	1.4E05	9.6E04
CHPAGMCP004	CS-137	1.9E05	1.3E05
CHPAGMCP005	I-131	1.0E05	9.2E06
CHPAGMCP006	I-133	1.2E09	1.0E20 1.0E20 = NO LIMIT

 * PROTECTIVE ACTION GUIDES FOR LONG-TERM TRANSFER TO FARM CROPS
 * FROM ROOT AND OTHER SOIL UPTAKE FROM SURFACE CONTAMINATION
 * BY CHRONC INGESTION MODEL NUCLIDE (PERMISSIBLE SURFACE
 * CONCENTRATION IN BEQUERELS PER SQUARE METER) AND THE ASSOCIATED
 * ANNUAL DEPLETION RATE FOR THE NUCLIDE IN THE SOIL.

	NUCLIDE	PERMISSIBLE SURFACE CONCENTRATION	ANNUAL DEPLETION RATE
	NAMIPI	GCMAXR	QROOT
CHPAGLTS001	SR-89	8.3E05	4.9
CHPAGLTS002	SR-90	4.0E03	0.065
CHPAGLTS003	CS-134	1.1E05	0.59
CHPAGLTS004	CS-137	1.2E05	0.28
CHPAGLTS005	I-131	2.1E07	32.0
CHPAGLTS006	I-133	1.6E12	290.0

 * DEFINE THE TYPE 9 RESULTS

* LONG-TERM POPULATION DOSE IN A GIVEN REGION BROKEN DOWN BY THE 12 PATHWAYS
 *
 * NUMBER OF RESULTS OF THIS TYPE THAT ARE BEING REQUESTED
 * FOR EACH RESULT YOU REQUEST, THE CODE WILL PRODUCE A SET OF 12

TYPE9NUMBER 2 (UP TO 10 ALLOWED)

	ORGNAM	INNER	OUTER
TYPE9OUT001	'EDEWBODY'	1	26 (0-1000 MILES)
TYPE9OUT002	'EDEWBODY'	1	19 (0-50 MILES)

 * ECONOMIC COST RESULTS IN A REGION BROKEN DOWN BY 12 TYPES OF COSTS

*
 * NUMBER OF RESULTS OF THIS TYPE THAT ARE BEING REQUESTED
 * FOR EACH RESULT YOU REQUEST, THE CODE WILL PRODUCE A SET OF 12

TYPL0NUMBER 2 (UP TO 10 ALLOWED)

	INNER	OUTER
TYPL0OUT001	1	26 (0-1000 MILES)
TYPL0OUT002	1	19 (0-50 MILES)

 * DEFINE A FLAG THAT CONTROLS THE PRODUCTION OF THE ACTION DISTANCE RESULTS

* SPECIFYING A VALUE OF .TRUE. TURNS ON ALL 8 OF THE ACTION DISTANCE RESULTS,

```

* A VALUE OF .FALSE. WILL ELIMINATE THE ACTION DISTANCE RESULTS FROM THE OUTPUT.
*
TYP11FLAG11 .TRUE.
*****
* IMPACTED AREA/POPULATION RESULTS IN A REGION BROKEN DOWN BY 6 TYPES OF IMPACTS
*
* NUMBER OF RESULTS OF THIS TYPE THAT ARE BEING REQUESTED
* FOR EACH RESULT YOU REQUEST, THE CODE WILL PRODUCE A SET OF 8
*
TYP12NUMBER    2          (UP TO 10 ALLOWED)
*
*              INNER      OUTER
*
TYP12OUT001     1          26    (0-1000 MILES)
TYP12OUT002     1          19    (0-50 MILES)

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A.4 DOSDATA

MACCS DOSE CONVERSION FILE: MOD SER #32, 1-NOV-88, 10:20:02
SANDIA NATIONAL LABORATORIES J. JOHNSON
12. ORGANS DEFINED IN THIS FILE:

STOMACH
SMALL IN
LUNGS
RED MARR
THYROID
LOWER LI
BONE SUR
BREAST
TESTES
OVARIES
EDEWBODY
THYROIDH

60 NUCLIDES DEFINED IN THIS FILE:

CO-58
CO-60
KR-85
KR-85M
KR-87
KR-88
RB-86
SR-89
SR-90
SR-91
SR-92
Y-90
Y-91
Y-92
Y-93
ZR-95
ZR-97
NB-95
MO-99
TC-99M
RU-103
RU-105
RU-106
RH-105
SB-127
SB-129
TE-127
TE-127M
TE-129
TE-129M
TE-131M
TE-132
I-131
I-132
I-133
I-134
I-135
XE-133
XE-135
CS-134
CS-136
CS-137
BA-139
BA-140
LA-140
LA-141
LA-142
CE-141
CE-143
CE-144

PR-143
ND-147
NP-239
PU-238
PU-239
PU-240
PU-241
AM-241
CM-242
CM-244

	CLOUDSHINE	GROUND SHINE 8HR	GROUND SHINE 7DAY	GROUND SHINE RATE	INHALED ACUTE	INHALED CHRONIC	INGESTION
CO-58							
STOMACH	3.520E-14	1.979E-11	4.023E-10	6.881E-16	1.558E-10	1.394E-09	3.853E-10
SMALL IN	3.203E-14	1.796E-11	3.652E-10	6.247E-16	3.307E-10	7.495E-10	1.130E-09
LUNGS	3.805E-14	2.143E-11	4.356E-10	7.452E-16	1.039E-09	1.601E-08	8.510E-11
RED MARR	3.869E-14	2.179E-11	4.430E-10	7.579E-16	1.577E-10	9.228E-10	2.601E-10
THYROID	4.788E-14	2.690E-11	5.469E-10	9.354E-16	-1.000E+00	8.704E-10	6.308E-11
LOWER LI	3.456E-14	1.942E-11	3.948E-10	6.754E-16	9.144E-10	1.989E-09	3.962E-09
BONE SUR	4.249E-14	2.389E-11	4.857E-10	8.308E-16	-1.000E+00	6.926E-10	1.252E-10
BREAST	4.566E-14	2.571E-11	5.228E-10	8.942E-16	-1.000E+00	9.367E-10	1.788E-10
TESTES	5.074E-14	2.845E-11	5.784E-10	9.894E-16	-1.000E+00	1.060E-10	1.614E-10
OVARIES	3.456E-14	1.942E-11	3.948E-10	6.754E-16	-1.000E+00	6.166E-10	1.041E-09
EDEWBODY	4.398E-14	2.459E-11	5.000E-10	8.553E-16	-1.000E+00	3.088E-09	8.206E-10
THYROIDH	4.788E-14	2.690E-11	5.469E-10	9.354E-16	6.142E-11	8.704E-10	6.308E-11
CO-60							
STOMACH	9.132E-14	4.602E-11	9.655E-10	1.598E-15	3.840E-10	2.726E-08	1.611E-09
SMALL IN	8.530E-14	4.301E-11	9.022E-10	1.494E-15	8.077E-10	7.046E-09	3.591E-09
LUNGS	9.862E-14	4.986E-11	1.046E-09	1.731E-15	5.186E-09	3.448E-07	8.768E-10
RED MARR	9.957E-14	5.032E-11	1.055E-09	1.747E-15	3.986E-10	1.718E-08	1.311E-09
THYROID	1.230E-13	6.219E-11	1.305E-09	2.159E-15	-1.000E+00	1.615E-08	7.843E-10
LOWER LI	9.069E-14	4.575E-11	9.597E-10	1.589E-15	2.386E-09	7.916E-09	1.113E-08
BONE SUR	1.056E-13	5.333E-11	1.119E-09	1.852E-15	-1.000E+00	1.353E-08	9.415E-10
BREAST	1.164E-13	5.872E-11	1.232E-09	2.039E-15	-1.000E+00	1.843E-08	1.100E-09
TESTES	1.297E-13	6.548E-11	1.373E-09	2.274E-15	-1.000E+00	1.697E-09	1.075E-09
OVARIES	8.879E-14	4.484E-11	9.406E-10	1.557E-15	-1.000E+00	4.753E-09	3.187E-09
EDEWBODY	1.125E-13	5.666E-11	1.189E-09	1.968E-15	-1.000E+00	5.948E-08	2.839E-09
THYROIDH	1.230E-13	6.219E-11	1.305E-09	2.159E-15	1.465E-10	1.615E-08	7.843E-10
KR-85							
STOMACH	7.674E-17	0.000E+00	0.000E+00	0.000E+00	6.757E-14	7.007E-14	0.000E+00
SMALL IN	6.881E-17	0.000E+00	0.000E+00	0.000E+00	6.781E-14	7.007E-14	0.000E+00
LUNGS	8.340E-17	0.000E+00	0.000E+00	0.000E+00	4.672E-13	4.708E-13	0.000E+00
RED MARR	8.562E-17	0.000E+00	0.000E+00	0.000E+00	6.808E-14	7.007E-14	0.000E+00
THYROID	1.037E-16	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	7.007E-14	0.000E+00
LOWER LI	7.484E-17	0.000E+00	0.000E+00	0.000E+00	6.781E-14	7.007E-14	0.000E+00
BONE SUR	9.767E-17	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	7.007E-14	0.000E+00
BREAST	1.037E-16	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	7.007E-14	0.000E+00
TESTES	1.123E-16	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	7.007E-14	0.000E+00
OVARIES	7.484E-17	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	7.007E-14	0.000E+00
EDEWBODY	2.315E-16	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	1.180E-13	0.000E+00
THYROIDH	1.037E-16	0.000E+00	0.000E+00	0.000E+00	6.689E-14	7.007E-14	0.000E+00
KR-85M							
STOMACH	5.232E-15	0.000E+00	0.000E+00	0.000E+00	6.098E-14	6.101E-14	0.000E+00
SMALL IN	4.566E-15	0.000E+00	0.000E+00	0.000E+00	6.101E-14	6.104E-14	0.000E+00
LUNGS	5.771E-15	0.000E+00	0.000E+00	0.000E+00	4.804E-13	4.804E-13	0.000E+00
RED MARR	5.549E-15	0.000E+00	0.000E+00	0.000E+00	6.369E-14	6.372E-14	0.000E+00
THYROID	7.737E-15	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	5.532E-14	0.000E+00
LOWER LI	5.105E-15	0.000E+00	0.000E+00	0.000E+00	5.912E-14	5.915E-14	0.000E+00
BONE SUR	8.467E-15	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	6.103E-14	0.000E+00
BREAST	8.593E-15	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	5.722E-14	0.000E+00
TESTES	7.959E-15	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	5.514E-14	0.000E+00
OVARIES	4.630E-15	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	5.995E-14	0.000E+00
EDEWBODY	7.222E-15	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	1.110E-13	0.000E+00
THYROIDH	7.737E-15	0.000E+00	0.000E+00	0.000E+00	5.529E-14	5.532E-14	0.000E+00
KR-87							
STOMACH	3.161E-14	0.000E+00	0.000E+00	0.000E+00	2.218E-13	2.218E-13	0.000E+00

SMALL IN	2.946E-14	0.000E+00	0.000E+00	0.000E+00	2.210E-13	2.210E-13	0.000E+00
LUNGS	3.393E-14	0.000E+00	0.000E+00	0.000E+00	2.386E-12	2.386E-12	0.000E+00
RED MARR	3.456E-14	0.000E+00	0.000E+00	0.000E+00	2.179E-13	2.179E-13	0.000E+00
THYROID	4.091E-14	0.000E+00	0.000E+00	0.000E+00-1.000E+00	2.149E-13	2.149E-13	0.000E+00
LOWER LI	3.133E-14	0.000E+00	0.000E+00	0.000E+00	2.250E-13	2.250E-13	0.000E+00
BONE SUR	3.678E-14	0.000E+00	0.000E+00	0.000E+00-1.000E+00	2.139E-13	2.139E-13	0.000E+00
BREAST	4.091E-14	0.000E+00	0.000E+00	0.000E+00-1.000E+00	2.139E-13	2.139E-13	0.000E+00
TESTES	4.439E-14	0.000E+00	0.000E+00	0.000E+00-1.000E+00	2.140E-13	2.140E-13	0.000E+00
OVARIES	2.933E-14	0.000E+00	0.000E+00	0.000E+00-1.000E+00	2.220E-13	2.220E-13	0.000E+00
EDEWBODY	3.958E-14	0.000E+00	0.000E+00	0.000E+00-1.000E+00	4.816E-13	4.816E-13	0.000E+00
THYROIDH	4.091E-14	0.000E+00	0.000E+00	0.000E+00	2.149E-13	2.149E-13	0.000E+00
KR-88							
STOMACH	1.064E-13	0.000E+00	0.000E+00	0.000E+00	3.745E-13	3.745E-13	0.000E+00
SMALL IN	1.001E-13	0.000E+00	0.000E+00	0.000E+00	3.780E-13	3.780E-13	0.000E+00
LUNGS	1.140E-13	0.000E+00	0.000E+00	0.000E+00	4.218E-12	4.218E-12	0.000E+00
RED MARR	1.156E-13	0.000E+00	0.000E+00	0.000E+00	3.666E-13	3.666E-13	0.000E+00
THYROID	1.367E-13	0.000E+00	0.000E+00	0.000E+00-1.000E+00	3.538E-13	3.538E-13	0.000E+00
LOWER LI	1.059E-13	0.000E+00	0.000E+00	0.000E+00	3.971E-13	3.972E-13	0.000E+00
BONE SUR	1.205E-13	0.000E+00	0.000E+00	0.000E+00-1.000E+00	3.508E-13	3.508E-13	0.000E+00
BREAST	1.357E-13	0.000E+00	0.000E+00	0.000E+00-1.000E+00	3.556E-13	3.556E-13	0.000E+00
TESTES	1.481E-13	0.000E+00	0.000E+00	0.000E+00-1.000E+00	3.512E-13	3.512E-13	0.000E+00
OVARIES	9.881E-14	0.000E+00	0.000E+00	0.000E+00-1.000E+00	3.890E-13	3.890E-13	0.000E+00
EDEWBODY	9.850E-14	0.000E+00	0.000E+00	0.000E+00-1.000E+00	8.454E-13	8.454E-13	0.000E+00
THYROIDH	1.367E-13	0.000E+00	0.000E+00	0.000E+00	3.537E-13	3.538E-13	0.000E+00
RB-86							
STOMACH	3.488E-15	1.806E-12	3.361E-11	6.310E-17	3.020E-10	1.453E-09	2.912E-09
SMALL IN	3.203E-15	1.670E-12	3.108E-11	5.835E-17	2.042E-10	1.347E-09	2.163E-09
LUNGS	3.742E-15	1.951E-12	3.631E-11	6.818E-17	1.595E-09	3.298E-09	2.137E-09
RED MARR	3.805E-15	1.979E-12	3.682E-11	6.913E-17	8.078E-10	2.362E-09	3.789E-09
THYROID	4.725E-15	2.460E-12	4.577E-11	8.593E-17-1.000E+00	1.333E-09	2.137E-09	2.137E-09
LOWER LI	3.425E-15	1.788E-12	3.327E-11	6.247E-17	2.041E-10	1.349E-09	2.167E-09
BONE SUR	4.059E-15	2.115E-12	3.935E-11	7.388E-17-1.000E+00	4.260E-09	6.841E-09	6.841E-09
BREAST	4.439E-15	2.305E-12	4.290E-11	8.054E-17-1.000E+00	1.336E-09	2.142E-09	2.142E-09
TESTES	4.947E-15	2.578E-12	4.797E-11	9.006E-17-1.000E+00	1.346E-09	2.160E-09	2.160E-09
OVARIES	3.393E-15	1.770E-12	3.293E-11	6.183E-17-1.000E+00	1.332E-09	2.137E-09	2.137E-09
EDEWBODY	4.722E-15	3.909E-12	7.274E-11	1.366E-16-1.000E+00	1.801E-09	2.545E-09	2.545E-09
THYROIDH	4.725E-15	2.460E-12	4.577E-11	8.593E-17	2.497E-10	1.333E-09	2.137E-09
SR-89							
STOMACH	5.042E-18	2.743E-15	5.505E-14	9.545E-20	1.904E-10	5.510E-10	9.321E-10
SMALL IN	4.598E-18	2.497E-15	5.011E-14	8.689E-20	2.759E-10	6.284E-10	1.433E-09
LUNGS	5.422E-18	2.952E-15	5.925E-14	1.027E-19	1.332E-09	2.186E-09	2.584E-10
RED MARR	5.518E-18	2.998E-15	6.017E-14	1.043E-19	9.360E-10	5.651E-09	3.261E-09
THYROID	6.849E-18	3.727E-15	7.480E-14	1.297E-19-1.000E+00	4.475E-10	2.584E-10	2.584E-10
LOWER LI	4.947E-18	2.697E-15	5.413E-14	9.386E-20	1.980E-09	3.586E-09	2.063E-08
BONE SUR	5.961E-18	3.235E-15	6.492E-14	1.126E-19-1.000E+00	8.355E-09	4.820E-09	4.820E-09
BREAST	6.437E-18	3.508E-15	7.041E-14	1.221E-19-1.000E+00	4.475E-10	2.584E-10	2.584E-10
TESTES	7.198E-18	3.909E-15	7.846E-14	1.360E-19-1.000E+00	4.475E-10	2.584E-10	2.584E-10
OVARIES	4.947E-18	2.688E-15	5.395E-14	9.354E-20-1.000E+00	4.476E-10	2.584E-10	2.584E-10
EDEWBODY	3.796E-16	1.457E-12	2.924E-11	5.069E-17-1.000E+00	1.787E-09	2.503E-09	2.503E-09
THYROIDH	6.849E-18	3.727E-15	7.480E-14	1.297E-19	8.878E-11	4.475E-10	2.584E-10
SR-90							
STOMACH	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.219E-10	2.365E-09	1.570E-09
SMALL IN	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.686E-10	2.402E-09	1.802E-09
LUNGS	0.000E+00	0.000E+00	0.000E+00	0.000E+00	7.464E-10	3.422E-09	1.333E-09
RED MARR	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.725E-09	3.051E-07	1.752E-07
THYROID	0.000E+00	0.000E+00	0.000E+00	0.000E+00-1.000E+00	2.328E-09	1.333E-09	1.333E-09
LOWER LI	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.611E-09	5.133E-09	1.943E-08
BONE SUR	0.000E+00	0.000E+00	0.000E+00	0.000E+00-1.000E+00	6.758E-07	3.881E-07	3.881E-07
BREAST	0.000E+00	0.000E+00	0.000E+00	0.000E+00-1.000E+00	2.328E-09	1.333E-09	1.333E-09
TESTES	0.000E+00	0.000E+00	0.000E+00	0.000E+00-1.000E+00	2.328E-09	1.333E-09	1.333E-09
OVARIES	0.000E+00	0.000E+00	0.000E+00	0.000E+00-1.000E+00	2.328E-09	1.333E-09	1.333E-09
EDEWBODY	9.537E-17	2.464E-13	3.113E-11	5.000E-18-1.000E+00	5.919E-08	3.518E-08	3.518E-08
THYROIDH	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.138E-10	2.328E-09	1.333E-09
SR-91							
STOMACH	3.581E-14	1.456E-11	3.424E-11	6.938E-16	1.653E-10	1.731E-10	8.625E-10
SMALL IN	3.254E-14	1.324E-11	3.112E-11	6.305E-16	2.333E-10	2.419E-10	1.353E-09

LUNGS	3.873E-14	1.575E-11	3.702E-11	7.501E-16	8.695E-10	9.243E-10	3.289E-11
RED MARR	3.936E-14	1.599E-11	3.760E-11	7.620E-16	7.944E-11	1.446E-10	1.233E-10
THYROID	4.869E-14	1.971E-11	4.633E-11	9.388E-16	-1.000E+00	4.434E-11	2.641E-11
LOWER LI	3.516E-14	1.425E-11	3.350E-11	6.787E-16	5.220E-10	6.234E-10	3.929E-09
BONE SUR	4.322E-14	1.756E-11	4.133E-11	8.375E-16	-1.000E+00	1.424E-10	9.812E-11
BREAST	4.662E-14	1.895E-11	4.458E-11	9.034E-16	-1.000E+00	4.814E-11	5.224E-11
TESTES	5.136E-14	2.089E-11	4.914E-11	9.957E-16	-1.000E+00	4.335E-11	4.141E-11
OVARIES	3.507E-14	1.425E-11	3.350E-11	6.787E-16	-1.000E+00	6.763E-11	2.120E-10
EDEWBODY	3.160E-14	1.404E-11	3.184E-11	6.435E-16	-1.000E+00	2.615E-10	6.790E-10
THYROIDH	4.869E-14	1.971E-11	4.633E-11	9.388E-16	3.583E-11	4.434E-11	2.641E-11
SR-92							
STOMACH	4.883E-14	1.157E-11	1.422E-11	8.403E-16	1.104E-10	1.108E-10	5.294E-10
SMALL IN	4.566E-14	1.081E-11	1.327E-11	7.864E-16	1.857E-10	1.861E-10	1.081E-09
LUNGS	5.264E-14	1.253E-11	1.539E-11	9.101E-16	7.106E-10	7.173E-10	1.948E-11
RED MARR	5.327E-14	1.266E-11	1.556E-11	9.196E-16	4.114E-11	4.213E-11	4.225E-11
THYROID	6.532E-14	1.556E-11	1.913E-11	1.129E-15	-1.000E+00	2.288E-11	1.418E-11
LOWER LI	4.852E-14	1.152E-11	1.415E-11	8.371E-16	3.252E-10	3.369E-10	2.179E-09
BONE SUR	5.644E-14	1.343E-11	1.653E-11	9.735E-16	-1.000E+00	5.591E-11	3.874E-11
BREAST	6.247E-14	1.481E-11	1.821E-11	1.075E-15	-1.000E+00	2.549E-11	2.743E-11
TESTES	6.913E-14	1.643E-11	2.020E-11	1.192E-15	-1.000E+00	2.176E-11	1.903E-11
OVARIES	4.725E-14	1.123E-11	1.381E-11	8.149E-16	-1.000E+00	3.134E-11	8.079E-11
EDEWBODY	6.019E-14	1.536E-11	1.953E-11	1.043E-15	-1.000E+00	1.741E-10	4.451E-10
THYROIDH	6.532E-14	1.556E-11	1.913E-11	1.129E-15	2.241E-11	2.288E-11	1.418E-11
Y-90							
STOMACH	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.745E-10	4.263E-10	1.060E-09
SMALL IN	0.000E+00	0.000E+00	0.000E+00	0.000E+00	8.713E-10	1.022E-09	2.557E-09
LUNGS	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.546E-09	9.309E-09	1.264E-14
RED MARR	0.000E+00	0.000E+00	0.000E+00	0.000E+00	8.668E-12	1.507E-11	3.664E-13
THYROID	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	5.183E-13	1.264E-14
LOWER LI	0.000E+00	0.000E+00	0.000E+00	0.000E+00	6.544E-09	1.262E-08	3.145E-08
BONE SUR	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	1.507E-11	3.664E-13
BREAST	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	5.184E-13	1.268E-14
TESTES	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	5.183E-13	1.264E-14
OVARIES	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	5.191E-13	1.438E-14
EDEWBODY	6.308E-16	2.379E-12	2.404E-11	8.623E-17	-1.000E+00	2.281E-09	2.905E-09
THYROIDH	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.153E-13	5.183E-13	1.264E-14
Y-91							
STOMACH	1.316E-16	6.690E-14	1.351E-12	2.328E-18	2.740E-10	3.431E-10	6.914E-10
SMALL IN	1.224E-16	6.234E-14	1.259E-12	2.169E-18	6.656E-10	8.421E-10	1.737E-09
LUNGS	1.424E-16	7.246E-14	1.463E-12	2.521E-18	6.923E-09	9.836E-08	2.017E-13
RED MARR	1.436E-16	7.310E-14	1.476E-12	2.543E-18	2.798E-11	3.174E-10	6.562E-12
THYROID	1.782E-16	9.060E-14	1.830E-12	3.152E-18	-1.000E+00	8.479E-12	1.288E-13
LOWER LI	1.306E-16	6.644E-14	1.342E-12	2.312E-18	6.908E-09	1.455E-08	3.027E-08
BONE SUR	1.528E-16	7.765E-14	1.568E-12	2.702E-18	-1.000E+00	3.166E-10	6.108E-12
BREAST	1.677E-16	8.540E-14	1.725E-12	2.971E-18	-1.000E+00	8.908E-12	5.545E-13
TESTES	1.874E-16	9.570E-14	1.933E-12	3.330E-18	-1.000E+00	6.404E-12	4.137E-13
OVARIES	1.284E-16	6.535E-14	1.320E-12	2.274E-18	-1.000E+00	8.190E-12	3.532E-12
EDEWBODY	5.509E-16	1.594E-12	3.218E-11	5.544E-17	-1.000E+00	1.312E-08	2.571E-09
THYROIDH	1.782E-16	9.060E-14	1.830E-12	3.152E-18	6.243E-13	8.479E-12	1.288E-13
Y-92							
STOMACH	9.228E-15	2.473E-12	3.125E-12	1.700E-16	1.703E-10	1.705E-10	1.420E-09
SMALL IN	8.498E-15	2.274E-12	2.875E-12	1.563E-16	2.382E-10	2.390E-10	2.000E-09
LUNGS	9.989E-15	2.671E-12	3.376E-12	1.836E-16	1.242E-09	1.249E-09	1.393E-12
RED MARR	1.012E-14	2.708E-12	3.423E-12	1.861E-16	2.061E-12	2.079E-12	4.930E-12
THYROID	1.249E-14	3.344E-12	4.227E-12	2.299E-16	-1.000E+00	1.054E-12	1.776E-13
LOWER LI	9.132E-15	2.440E-12	3.084E-12	1.677E-16	1.959E-10	2.090E-10	1.749E-09
BONE SUR	1.088E-14	2.920E-12	3.691E-12	2.007E-16	-1.000E+00	1.512E-12	1.754E-12
BREAST	1.186E-14	3.178E-12	4.017E-12	2.185E-16	-1.000E+00	1.503E-12	3.564E-12
TESTES	1.316E-14	3.529E-12	4.460E-12	2.426E-16	-1.000E+00	3.494E-13	1.399E-12
OVARIES	9.006E-15	2.413E-12	3.049E-12	1.658E-16	-1.000E+00	2.628E-12	1.971E-11
EDEWBODY	1.238E-14	5.018E-12	6.342E-12	3.449E-16	-1.000E+00	2.125E-10	5.153E-10
THYROIDH	1.249E-14	3.344E-12	4.227E-12	2.299E-16	1.049E-12	1.054E-12	1.776E-13
Y-93							
STOMACH	3.361E-15	1.321E-12	3.127E-12	5.961E-17	2.810E-10	2.896E-10	1.280E-09
SMALL IN	3.127E-15	1.223E-12	2.895E-12	5.518E-17	5.455E-10	5.711E-10	2.524E-09
LUNGS	3.647E-15	1.427E-12	3.377E-12	6.437E-17	2.190E-09	2.524E-09	8.661E-13

RED MARR	3.710E-15	1.448E-12	3.427E-12	6.532E-17	3.495E-12	4.018E-12	4.936E-12
THYROID	4.503E-15	1.771E-12	4.192E-12	7.991E-17	-1.000E+00	9.250E-13	1.259E-13
LOWER LI	3.361E-15	1.307E-12	3.094E-12	5.898E-17	1.398E-09	1.997E-09	8.844E-09
BONE SUR	4.059E-15	1.602E-12	3.793E-12	7.230E-17	-1.000E+00	3.134E-12	1.726E-12
BREAST	4.439E-15	1.757E-12	4.159E-12	7.927E-17	-1.000E+00	1.742E-12	3.121E-12
TESTES	4.788E-15	1.883E-12	4.458E-12	8.498E-17	-1.000E+00	6.650E-13	1.777E-12
OVARIES	3.203E-15	1.251E-12	2.961E-12	5.644E-17	-1.000E+00	5.307E-12	2.194E-11
EDEWBODY	4.977E-15	4.053E-12	9.594E-12	1.829E-16	-1.000E+00	5.829E-10	1.232E-09
THYROIDH	4.503E-15	1.771E-12	4.192E-12	7.991E-17	8.313E-13	9.250E-13	1.259E-13
ZR-95							
STOMACH	2.660E-14	1.509E-11	3.258E-10	5.232E-16	1.541E-10	1.085E-09	3.568E-10
SMALL IN	2.407E-14	1.363E-11	2.943E-10	4.725E-16	3.296E-10	9.802E-10	1.119E-09
LUNGS	2.876E-14	1.628E-11	3.516E-10	5.644E-16	1.505E-09	1.843E-08	2.342E-11
RED MARR	2.924E-14	1.656E-11	3.575E-10	5.740E-16	2.845E-10	3.207E-09	2.135E-10
THYROID	3.615E-14	2.049E-11	4.425E-10	7.103E-16	-1.000E+00	7.790E-10	8.238E-12
LOWER LI	2.607E-14	1.473E-11	3.181E-10	5.105E-16	1.573E-09	4.164E-09	7.778E-09
BONE SUR	3.203E-14	1.811E-11	3.910E-10	6.279E-16	-1.000E+00	2.172E-08	4.860E-10
BREAST	3.456E-14	1.948E-11	4.207E-10	6.754E-16	-1.000E+00	9.280E-10	1.047E-10
TESTES	3.837E-14	2.159E-11	4.661E-10	7.484E-16	-1.000E+00	3.023E-10	8.032E-11
OVARIES	2.616E-14	1.482E-11	3.199E-10	5.137E-16	-1.000E+00	8.361E-10	8.153E-10
EDEWBODY	3.299E-14	1.873E-11	4.043E-10	6.493E-16	-1.000E+00	4.327E-09	1.027E-09
THYROIDH	3.615E-14	2.049E-11	4.425E-10	7.103E-16	6.141E-11	7.790E-10	8.238E-12
ZR-97							
STOMACH	5.527E-14	2.431E-11	9.498E-11	1.083E-15	3.772E-10	4.175E-10	1.213E-09
SMALL IN	5.004E-14	2.202E-11	8.599E-11	9.807E-16	7.834E-10	8.857E-10	3.389E-09
LUNGS	5.975E-14	2.626E-11	1.026E-10	1.170E-15	2.836E-09	3.957E-09	1.759E-11
RED MARR	6.084E-14	2.673E-11	1.044E-10	1.191E-15	1.079E-10	1.396E-10	1.297E-10
THYROID	7.481E-14	3.301E-11	1.290E-10	1.471E-15	-1.000E+00	3.744E-11	2.662E-12
LOWER LI	5.419E-14	2.387E-11	9.324E-11	1.063E-15	2.609E-09	4.271E-09	1.795E-08
BONE SUR	6.691E-14	2.949E-11	1.153E-10	1.315E-15	-1.000E+00	1.217E-10	4.538E-11
BREAST	7.210E-14	3.172E-11	1.240E-10	1.414E-15	-1.000E+00	5.790E-11	8.094E-11
TESTES	7.937E-14	3.496E-11	1.366E-10	1.558E-15	-1.000E+00	2.986E-11	5.200E-11
OVARIES	5.415E-14	2.380E-11	9.302E-11	1.061E-15	-1.000E+00	1.696E-10	6.219E-10
EDEWBODY	8.623E-15	5.200E-12	1.857E-11	2.118E-16	-1.000E+00	1.067E-09	2.288E-09
THYROIDH	7.481E-14	3.301E-11	1.290E-10	1.471E-15	2.788E-11	3.744E-11	2.662E-12
NB-95							
STOMACH	2.778E-14	1.557E-11	3.063E-10	5.422E-16	1.287E-10	6.362E-10	2.796E-10
SMALL IN	2.515E-14	1.411E-11	2.776E-10	4.915E-16	2.838E-10	5.201E-10	9.116E-10
LUNGS	3.000E-14	1.684E-11	3.314E-10	5.866E-16	7.399E-10	8.319E-09	2.743E-11
RED MARR	3.051E-14	1.711E-11	3.367E-10	5.961E-16	1.212E-10	4.425E-10	1.993E-10
THYROID	3.773E-14	2.121E-11	4.173E-10	7.388E-16	-1.000E+00	3.582E-10	1.184E-11
LOWER LI	2.724E-14	1.529E-11	3.009E-10	5.327E-16	9.234E-10	1.928E-09	4.009E-09
BONE SUR	3.330E-14	1.866E-11	3.672E-10	6.501E-16	-1.000E+00	5.161E-10	2.965E-10
BREAST	3.583E-14	2.012E-11	3.959E-10	7.008E-16	-1.000E+00	4.062E-10	1.074E-10
TESTES	3.995E-14	2.230E-11	4.388E-10	7.769E-16	-1.000E+00	6.507E-11	9.664E-11
OVARIES	2.730E-14	1.529E-11	3.009E-10	5.327E-16	-1.000E+00	4.310E-10	8.030E-10
EDEWBODY	3.449E-14	1.937E-11	3.812E-10	6.748E-16	-1.000E+00	1.652E-09	7.029E-10
THYROIDH	3.773E-14	2.121E-11	4.173E-10	7.388E-16	4.278E-11	3.582E-10	1.184E-11
MO-99							
STOMACH	5.518E-15	3.820E-12	5.368E-11	1.100E-16	1.894E-10	2.325E-10	5.135E-10
SMALL IN	4.978E-15	3.408E-12	4.751E-11	9.894E-17	4.221E-10	5.189E-10	1.249E-09
LUNGS	5.993E-15	4.163E-12	5.884E-11	1.192E-16	1.592E-09	4.292E-09	1.506E-11
RED MARR	6.057E-15	4.111E-12	5.687E-11	1.202E-16	3.096E-11	5.074E-11	7.972E-11
THYROID	7.579E-15	5.376E-12	7.737E-11	1.513E-16	-1.000E+00	1.516E-11	1.034E-11
LOWER LI	5.422E-15	3.740E-12	5.251E-11	1.078E-16	2.860E-09	5.516E-09	1.367E-08
BONE SUR	6.913E-15	5.189E-12	7.849E-11	1.386E-16	-1.000E+00	4.290E-11	6.669E-11
BREAST	7.388E-15	5.483E-12	8.176E-11	1.487E-16	-1.000E+00	2.748E-11	3.422E-11
TESTES	7.991E-15	5.622E-12	8.026E-11	1.595E-16	-1.000E+00	1.220E-11	2.719E-11
OVARIES	5.359E-15	3.624E-12	4.983E-11	1.065E-16	-1.000E+00	9.503E-11	2.174E-10
EDEWBODY	7.164E-15	5.694E-12	7.867E-11	1.667E-16	-1.000E+00	1.075E-09	1.362E-09
THYROIDH	7.579E-15	5.376E-12	7.737E-11	1.513E-16	5.884E-12	1.516E-11	1.034E-11
TC-99M							
STOMACH	4.154E-15	1.731E-12	2.875E-12	9.196E-17	1.437E-11	1.519E-11	7.169E-11
SMALL IN	3.583E-15	1.498E-12	2.489E-12	7.959E-17	3.397E-12	3.520E-12	2.227E-11
LUNGS	4.598E-15	1.928E-12	3.203E-12	1.024E-16	2.924E-11	3.061E-11	3.151E-12
RED MARR	4.217E-15	1.755E-12	2.915E-12	9.323E-17	2.296E-12	2.389E-12	6.273E-12

THYROID	6.342E-15	2.656E-12	4.412E-12	1.411E-16	-1.000E+00	2.088E-11	8.449E-11
LOWER LI	4.027E-15	1.689E-12	2.806E-12	8.974E-17	3.371E-12	3.834E-12	2.545E-11
BONE SUR	7.230E-15	3.020E-12	5.017E-12	1.605E-16	-1.000E+00	1.784E-12	4.064E-12
BREAST	7.230E-15	3.050E-12	5.067E-12	1.620E-16	-1.000E+00	1.520E-12	3.563E-12
TESTES	6.437E-15	2.698E-12	4.482E-12	1.433E-16	-1.000E+00	5.222E-13	2.294E-12
OVARIES	3.615E-15	1.510E-12	2.509E-12	8.023E-17	-1.000E+00	1.703E-12	9.738E-12
EDEWBODY	5.729E-15	2.418E-12	4.017E-12	1.285E-16	-1.000E+00	7.451E-12	1.673E-11
THYROIDH	6.342E-15	2.656E-12	4.412E-12	1.411E-16	1.968E-11	2.088E-11	8.449E-11
RU-103							
STOMACH	1.662E-14	9.838E-12	1.950E-10	3.426E-16	1.212E-10	5.047E-10	3.143E-10
SMALL IN	1.487E-14	8.816E-12	1.747E-10	3.070E-16	2.683E-10	4.713E-10	8.509E-10
LUNGS	1.808E-14	1.075E-11	2.131E-10	3.745E-16	1.307E-09	1.560E-08	7.350E-11
RED MARR	1.849E-14	1.093E-11	2.166E-10	3.806E-16	8.176E-11	3.183E-10	1.666E-10
THYROID	2.246E-14	1.331E-11	2.638E-10	4.635E-16	-1.000E+00	2.564E-10	6.289E-11
LOWER LI	1.624E-14	9.656E-12	1.914E-10	3.363E-16	1.489E-09	3.135E-09	6.534E-09
BONE SUR	2.119E-14	1.258E-11	2.493E-10	4.381E-16	-1.000E+00	2.371E-10	9.661E-11
BREAST	2.257E-14	1.346E-11	2.671E-10	4.694E-16	-1.000E+00	3.103E-10	1.200E-10
TESTES	2.427E-14	1.442E-11	2.859E-10	5.023E-16	-1.000E+00	6.971E-11	1.220E-10
OVARIES	1.614E-14	9.565E-12	1.896E-10	3.331E-16	-1.000E+00	3.070E-10	5.712E-10
EDEWBODY	2.107E-14	1.249E-11	2.476E-10	4.351E-16	-1.000E+00	2.485E-09	8.278E-10
THYROIDH	2.246E-14	1.331E-11	2.638E-10	4.635E-16	2.856E-11	2.564E-10	6.289E-11
RU-105							
STOMACH	2.784E-14	9.261E-12	1.410E-11	5.581E-16	7.924E-11	8.095E-11	4.980E-10
SMALL IN	2.511E-14	8.313E-12	1.265E-11	5.010E-16	1.205E-10	1.248E-10	7.898E-10
LUNGS	3.019E-14	9.999E-12	1.525E-11	6.025E-16	5.005E-10	5.725E-10	6.210E-12
RED MARR	3.076E-14	1.021E-11	1.558E-11	6.152E-16	7.221E-12	7.688E-12	2.340E-11
THYROID	3.805E-14	1.258E-11	1.919E-11	7.579E-16	-1.000E+00	4.145E-12	1.813E-12
LOWER LI	2.727E-14	9.051E-12	1.379E-11	5.454E-16	2.058E-10	3.048E-10	1.339E-09
BONE SUR	3.456E-14	1.154E-11	1.775E-11	6.944E-16	-1.000E+00	4.616E-12	8.893E-12
BREAST	3.710E-14	1.232E-11	1.893E-11	7.420E-16	-1.000E+00	6.609E-12	1.591E-11
TESTES	4.027E-14	1.337E-11	2.040E-11	8.054E-16	-1.000E+00	1.523E-12	7.596E-12
OVARIES	2.714E-14	8.994E-12	1.365E-11	5.422E-16	-1.000E+00	1.590E-11	9.669E-11
EDEWBODY	3.519E-14	1.210E-11	1.848E-11	7.292E-16	-1.000E+00	1.235E-10	2.868E-10
THYROIDH	3.805E-14	1.258E-11	1.919E-11	7.579E-16	3.876E-12	4.145E-12	1.813E-12
RU-106							
STOMACH	7.293E-15	4.175E-12	8.726E-11	1.452E-16	6.984E-10	2.938E-09	3.119E-09
SMALL IN	6.564E-15	3.765E-12	7.869E-11	1.310E-16	1.589E-09	3.397E-09	5.548E-09
LUNGS	7.896E-15	4.531E-12	9.469E-11	1.576E-16	3.044E-08	1.037E-06	1.435E-09
RED MARR	8.054E-15	4.622E-12	9.660E-11	1.608E-16	8.744E-11	1.770E-09	1.483E-09
THYROID	9.862E-15	5.652E-12	1.181E-10	1.966E-16	-1.000E+00	1.733E-09	1.432E-09
LOWER LI	7.135E-15	4.093E-12	8.555E-11	1.424E-16	1.604E-08	3.713E-08	7.087E-08
BONE SUR	9.037E-15	5.187E-12	1.084E-10	1.804E-16	-1.000E+00	1.620E-09	1.445E-09
BREAST	9.672E-15	5.552E-12	1.160E-10	1.931E-16	-1.000E+00	1.798E-09	1.457E-09
TESTES	1.056E-14	6.053E-12	1.265E-10	2.106E-16	-1.000E+00	1.154E-09	1.474E-09
OVARIES	7.103E-15	4.075E-12	8.517E-11	1.417E-16	-1.000E+00	1.308E-09	1.656E-09
EDEWBODY	1.010E-14	9.017E-12	1.885E-10	3.137E-16	-1.000E+00	1.289E-07	7.419E-09
THYROIDH	9.862E-15	5.652E-12	1.181E-10	1.966E-16	4.022E-11	1.733E-09	1.432E-09
RH-105							
STOMACH	2.600E-15	1.488E-12	9.870E-12	5.581E-17	6.353E-11	7.262E-11	1.946E-10
SMALL IN	2.315E-15	1.327E-12	8.804E-12	4.978E-17	1.353E-10	1.578E-10	4.427E-10
LUNGS	2.841E-15	1.631E-12	1.082E-11	6.120E-17	4.985E-10	9.509E-10	3.847E-12
RED MARR	2.936E-15	1.682E-12	1.116E-11	6.310E-17	5.385E-12	7.746E-12	1.463E-11
THYROID	3.615E-15	2.071E-12	1.374E-11	7.769E-17	-1.000E+00	2.878E-12	2.894E-12
LOWER LI	2.556E-15	1.462E-12	9.701E-12	5.486E-17	7.389E-10	1.347E-09	3.781E-09
BONE SUR	3.647E-15	2.088E-12	1.385E-11	7.832E-17	-1.000E+00	4.441E-12	6.731E-12
BREAST	3.805E-15	2.189E-12	1.452E-11	8.213E-17	-1.000E+00	5.592E-12	8.959E-12
TESTES	3.837E-15	2.206E-12	1.464E-11	8.276E-17	-1.000E+00	2.827E-12	7.209E-12
OVARIES	2.416E-15	1.386E-12	9.197E-12	5.200E-17	-1.000E+00	2.105E-11	5.798E-11
EDEWBODY	3.449E-15	2.012E-12	1.335E-11	7.546E-17	-1.000E+00	2.573E-10	3.980E-10
THYROIDH	3.615E-15	2.071E-12	1.374E-11	7.769E-17	1.432E-12	2.878E-12	2.894E-12
SB-127							
STOMACH	2.337E-14	1.314E-11	1.623E-10	4.693E-16	2.278E-10	3.267E-10	5.597E-10
SMALL IN	2.106E-14	1.181E-11	1.459E-10	4.217E-16	5.199E-10	7.090E-10	1.630E-09
LUNGS	2.534E-14	1.420E-11	1.755E-10	5.074E-16	1.907E-09	6.915E-09	1.574E-11
RED MARR	2.584E-14	1.456E-11	1.799E-10	5.200E-16	9.334E-11	1.547E-10	1.317E-10
THYROID	3.171E-14	1.784E-11	2.205E-10	6.374E-16	-1.000E+00	6.144E-11	4.642E-12

LOWER LI	2.289E-14	1.287E-11	1.590E-10	4.598E-16	3.663E-09	7.432E-09	1.959E-08
BONE SUR	2.908E-14	1.634E-11	2.019E-10	5.835E-16	-1.000E+00	1.331E-10	5.225E-11
BREAST	3.111E-14	1.749E-11	2.161E-10	6.247E-16	-1.000E+00	9.102E-11	7.574E-11
TESTES	3.393E-14	1.909E-11	2.358E-10	6.818E-16	-1.000E+00	4.588E-11	5.894E-11
OVARIES	2.280E-14	1.278E-11	1.579E-10	4.566E-16	-1.000E+00	2.521E-10	6.148E-10
EDEWBODY	2.951E-14	1.702E-11	2.093E-10	6.088E-16	-1.000E+00	1.633E-09	1.948E-09
THYROIDH	3.171E-14	1.784E-11	2.205E-10	6.374E-16	2.443E-11	6.144E-11	4.642E-12
SB-129							
STOMACH	5.264E-14	1.651E-11	2.316E-11	9.830E-16	1.226E-10	1.235E-10	7.245E-10
SMALL IN	4.820E-14	1.512E-11	2.120E-11	9.006E-16	1.888E-10	1.912E-10	1.473E-09
LUNGS	5.676E-14	1.785E-11	2.503E-11	1.062E-15	8.374E-10	8.954E-10	9.379E-12
RED MARR	5.771E-14	1.811E-11	2.540E-11	1.078E-15	1.608E-11	1.654E-11	3.661E-11
THYROID	7.103E-14	2.233E-11	3.132E-11	1.329E-15	-1.000E+00	9.720E-12	1.464E-12
LOWER LI	5.169E-14	1.624E-11	2.278E-11	9.672E-16	2.014E-10	2.321E-10	1.929E-09
BONE SUR	6.247E-14	1.970E-11	2.764E-11	1.170E-15	-1.000E+00	1.481E-11	1.332E-11
BREAST	6.786E-14	2.143E-11	3.008E-11	1.272E-15	-1.000E+00	1.281E-11	2.560E-11
TESTES	7.515E-14	2.363E-11	3.315E-11	1.405E-15	-1.000E+00	5.415E-12	1.105E-11
OVARIES	5.137E-14	1.608E-11	2.255E-11	9.576E-16	-1.000E+00	2.148E-11	1.514E-10
EDEWBODY	6.528E-14	2.129E-11	2.998E-11	1.238E-15	-1.000E+00	1.740E-10	4.830E-10
THYROIDH	7.103E-14	2.233E-11	3.132E-11	1.329E-15	9.521E-12	9.720E-12	1.464E-12
TE-127							
STOMACH	1.639E-16	7.509E-14	1.679E-13	3.456E-18	4.321E-11	4.465E-11	2.425E-10
SMALL IN	1.462E-16	6.717E-14	1.502E-13	3.092E-18	6.822E-11	7.117E-11	3.896E-10
LUNGS	1.788E-16	8.198E-14	1.833E-13	3.773E-18	3.748E-10	4.258E-10	2.885E-12
RED MARR	1.836E-16	8.405E-14	1.879E-13	3.869E-18	3.342E-12	3.986E-12	6.413E-12
THYROID	2.245E-16	1.033E-13	2.310E-13	4.756E-18	-1.000E+00	1.844E-12	2.855E-12
LOWER LI	1.605E-16	7.371E-14	1.648E-13	3.393E-18	1.640E-10	2.275E-10	1.265E-09
BONE SUR	2.191E-16	1.006E-13	2.248E-13	4.630E-18	-1.000E+00	4.063E-12	6.424E-12
BREAST	2.312E-16	1.061E-13	2.372E-13	4.883E-18	-1.000E+00	1.878E-12	2.998E-12
TESTES	2.410E-16	1.109E-13	2.479E-13	5.105E-18	-1.000E+00	1.828E-12	2.940E-12
OVARIES	1.560E-16	7.165E-14	1.602E-13	3.298E-18	-1.000E+00	2.029E-12	4.040E-12
EDEWBODY	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	8.597E-11	1.874E-10
THYROIDH	2.245E-16	1.033E-13	2.310E-13	4.756E-18	1.590E-12	1.844E-12	2.855E-12
TE-127M							
STOMACH	4.566E-17	7.804E-14	2.953E-12	1.884E-18	8.892E-11	2.302E-10	2.115E-10
SMALL IN	3.165E-17	5.837E-14	2.406E-12	1.287E-18	1.832E-10	3.690E-10	4.338E-10
LUNGS	6.247E-17	1.013E-13	3.555E-12	2.616E-18	2.476E-09	3.337E-08	9.597E-11
RED MARR	2.632E-17	5.643E-14	2.669E-12	1.034E-18	2.769E-10	5.309E-09	5.373E-09
THYROID	1.237E-16	1.852E-13	5.663E-12	5.296E-18	-1.000E+00	9.635E-11	9.411E-11
LOWER LI	4.059E-17	7.121E-14	2.788E-12	1.662E-18	2.309E-09	5.719E-09	1.109E-08
BONE SUR	1.069E-16	1.615E-13	5.126E-12	4.503E-18	-1.000E+00	2.055E-08	2.086E-08
BREAST	3.038E-16	4.141E-13	1.042E-11	1.322E-17	-1.000E+00	1.097E-10	9.733E-11
TESTES	1.877E-16	2.688E-13	7.518E-12	8.118E-18	-1.000E+00	9.225E-11	9.303E-11
OVARIES	4.503E-17	7.676E-14	2.865E-12	1.877E-18	-1.000E+00	1.100E-10	1.248E-10
EDEWBODY	1.412E-16	1.758E-13	3.615E-12	6.111E-18	-1.000E+00	5.801E-09	2.224E-09
THYROIDH	1.237E-16	1.852E-13	5.663E-12	5.296E-18	1.337E-11	9.635E-11	9.411E-11
TE-129							
STOMACH	1.842E-15	2.273E-13	2.293E-13	3.805E-17	1.553E-11	1.553E-11	3.970E-10
SMALL IN	1.652E-15	2.027E-13	2.044E-13	3.393E-17	1.083E-11	1.083E-11	2.730E-10
LUNGS	2.007E-15	2.482E-13	2.503E-13	4.154E-17	1.526E-10	1.526E-10	4.910E-13
RED MARR	2.042E-15	2.501E-13	2.522E-13	4.186E-17	6.131E-13	6.131E-13	7.610E-13
THYROID	2.527E-15	3.145E-13	3.172E-13	5.264E-17	-1.000E+00	5.088E-13	3.350E-13
LOWER LI	1.804E-15	2.217E-13	2.235E-13	3.710E-17	1.838E-12	1.839E-12	3.700E-11
BONE SUR	2.375E-15	2.956E-13	2.981E-13	4.947E-17	-1.000E+00	7.058E-13	5.990E-13
BREAST	2.610E-15	3.334E-13	3.363E-13	5.581E-17	-1.000E+00	5.381E-13	6.050E-13
TESTES	2.737E-15	3.429E-13	3.458E-13	5.740E-17	-1.000E+00	4.522E-13	3.750E-13
OVARIES	1.782E-15	2.198E-13	2.216E-13	3.678E-17	-1.000E+00	5.052E-13	1.580E-12
EDEWBODY	2.685E-15	5.525E-13	5.572E-13	9.248E-17	-1.000E+00	2.085E-11	5.430E-11
THYROIDH	2.527E-15	3.145E-13	3.172E-13	5.264E-17	5.088E-13	5.088E-13	3.350E-13
TE-129M							
STOMACH	1.157E-15	1.240E-12	2.709E-11	2.359E-17	2.603E-10	4.813E-10	6.262E-10
SMALL IN	1.040E-15	1.104E-12	2.413E-11	2.099E-17	5.055E-10	7.966E-10	1.470E-09
LUNGS	1.262E-15	1.358E-12	2.966E-11	2.591E-17	4.429E-09	4.028E-08	1.588E-10
RED MARR	1.259E-15	1.344E-12	2.940E-11	2.524E-17	4.854E-10	3.038E-09	3.432E-09
THYROID	1.617E-15	1.753E-12	3.820E-11	3.393E-17	-1.000E+00	1.555E-10	1.566E-10
LOWER LI	1.132E-15	1.208E-12	2.639E-11	2.296E-17	4.897E-09	1.100E-08	2.464E-08

BONE SUR	1.443E-15	1.599E-12	3.496E-11	3.022E-17	-1.000E+00	7.149E-09	8.103E-09
BREAST	1.687E-15	1.936E-12	4.203E-11	3.869E-17	-1.000E+00	1.684E-10	1.657E-10
TESTES	1.754E-15	1.932E-12	4.207E-11	3.773E-17	-1.000E+00	1.390E-10	1.604E-10
OVARIES	1.138E-15	1.209E-12	2.640E-11	2.318E-17	-1.000E+00	1.783E-10	2.405E-10
EDEWBODY	1.644E-15	2.813E-12	6.190E-11	5.035E-17	-1.000E+00	6.466E-09	2.885E-09
THYROIDH	1.617E-15	1.753E-12	3.820E-11	3.393E-17	3.040E-11	1.555E-10	1.566E-10
TE-131M							
STOMACH	5.525E-14	2.755E-11	1.751E-10	1.048E-15	2.208E-10	2.758E-10	6.627E-10
SMALL IN	5.016E-14	2.504E-11	1.589E-10	9.528E-16	3.920E-10	4.928E-10	1.600E-09
LUNGS	5.966E-14	2.979E-11	1.895E-10	1.133E-15	1.244E-09	2.231E-09	6.208E-11
RED MARR	6.028E-14	3.011E-11	1.918E-10	1.145E-15	9.441E-11	1.386E-10	2.393E-10
THYROID	7.492E-14	3.757E-11	2.390E-10	1.430E-15	-1.000E+00	3.280E-08	3.908E-08
LOWER LI	5.424E-14	2.710E-11	1.722E-10	1.031E-15	1.333E-09	2.367E-09	8.102E-09
BONE SUR	6.713E-14	3.366E-11	2.159E-10	1.281E-15	-1.000E+00	2.608E-10	3.698E-10
BREAST	7.245E-14	3.646E-11	2.332E-10	1.387E-15	-1.000E+00	9.204E-11	1.342E-10
TESTES	7.928E-14	3.970E-11	2.529E-10	1.511E-15	-1.000E+00	4.542E-11	9.816E-11
OVARIES	5.350E-14	2.671E-11	1.695E-10	1.016E-15	-1.000E+00	2.335E-10	7.370E-10
EDEWBODY	6.458E-14	3.240E-11	2.070E-10	1.227E-15	-1.000E+00	1.634E-09	2.355E-09
THYROIDH	7.492E-14	3.757E-11	2.390E-10	1.430E-15	6.429E-09	3.280E-08	3.908E-08
TE-132							
STOMACH	6.976E-15	3.219E-11	5.471E-10	1.551E-16	2.302E-10	4.076E-10	4.855E-10
SMALL IN	6.152E-15	2.912E-11	4.957E-10	1.364E-16	3.127E-10	5.081E-10	7.662E-10
LUNGS	7.706E-15	3.493E-11	5.930E-10	1.722E-16	5.740E-10	1.641E-09	2.937E-10
RED MARR	7.642E-15	3.531E-11	6.006E-10	1.681E-16	2.500E-10	3.951E-10	4.064E-10
THYROID	1.021E-14	4.414E-11	7.469E-10	2.308E-16	-1.000E+00	5.284E-08	4.695E-08
LOWER LI	6.849E-15	3.154E-11	5.362E-10	1.519E-16	8.207E-10	1.574E-09	3.764E-09
BONE SUR	1.075E-14	4.024E-11	6.752E-10	2.419E-16	-1.000E+00	7.249E-10	8.537E-10
BREAST	1.154E-14	4.369E-11	7.321E-10	2.686E-16	-1.000E+00	3.312E-10	3.126E-10
TESTES	1.078E-14	4.683E-11	7.922E-10	2.461E-16	-1.000E+00	3.374E-10	3.256E-10
OVARIES	6.247E-15	3.114E-11	5.313E-10	1.395E-16	-1.000E+00	3.866E-10	5.058E-10
EDEWBODY	9.502E-15	4.131E-11	6.992E-10	2.153E-16	-1.000E+00	2.229E-09	2.132E-09
THYROIDH	1.021E-14	4.414E-11	7.469E-10	2.308E-16	2.263E-08	5.284E-08	4.695E-08
I-131							
STOMACH	1.291E-14	7.742E-12	1.238E-10	2.727E-16	5.997E-11	7.516E-11	3.059E-10
SMALL IN	1.154E-14	6.914E-12	1.106E-10	2.435E-16	1.572E-11	2.742E-11	4.471E-11
LUNGS	1.408E-14	8.444E-12	1.351E-10	2.974E-16	4.616E-10	6.565E-10	1.016E-10
RED MARR	1.449E-14	8.678E-12	1.388E-10	3.057E-16	3.518E-11	6.260E-11	9.444E-11
THYROID	1.776E-14	1.062E-11	1.699E-10	3.742E-16	-1.000E+00	2.911E-07	4.753E-07
LOWER LI	1.265E-14	7.589E-12	1.214E-10	2.673E-16	1.465E-11	2.593E-11	4.239E-11
BONE SUR	1.731E-14	1.044E-11	1.671E-10	3.678E-16	-1.000E+00	5.718E-11	8.699E-11
BREAST	1.830E-14	1.098E-11	1.757E-10	3.869E-16	-1.000E+00	7.861E-11	1.209E-10
TESTES	1.899E-14	1.143E-11	1.829E-10	4.027E-16	-1.000E+00	2.322E-11	3.777E-11
OVARIES	1.224E-14	7.337E-12	1.174E-10	2.584E-16	-1.000E+00	2.533E-11	4.067E-11
EDEWBODY	1.667E-14	1.009E-11	1.614E-10	3.553E-16	-1.000E+00	8.872E-09	1.434E-08
THYROIDH	1.776E-14	1.062E-11	1.699E-10	3.742E-16	1.279E-08	9.694E-08	1.583E-07
I-132							
STOMACH	8.308E-14	1.738E-11	1.909E-11	1.598E-15	9.896E-11	9.896E-11	6.320E-10
SMALL IN	7.547E-14	1.579E-11	1.735E-11	1.452E-15	1.245E-11	1.245E-11	3.160E-11
LUNGS	8.974E-14	1.879E-11	2.065E-11	1.728E-15	2.702E-10	2.703E-10	2.640E-11
RED MARR	9.132E-14	1.910E-11	2.099E-11	1.757E-15	1.401E-11	1.401E-11	2.450E-11
THYROID	1.126E-13	2.352E-11	2.584E-11	2.163E-15	-1.000E+00	1.726E-09	3.842E-09
LOWER LI	8.149E-14	1.703E-11	1.871E-11	1.566E-15	1.126E-11	1.127E-11	2.750E-11
BONE SUR	9.989E-14	2.090E-11	2.296E-11	1.922E-15	-1.000E+00	1.242E-11	2.190E-11
BREAST	1.078E-13	2.259E-11	2.481E-11	2.077E-15	-1.000E+00	1.412E-11	2.511E-11
TESTES	1.192E-13	2.493E-11	2.739E-11	2.293E-15	-1.000E+00	9.901E-12	2.220E-11
OVARIES	8.118E-14	1.700E-11	1.868E-11	1.563E-15	-1.000E+00	9.960E-12	2.340E-11
EDEWBODY	1.032E-13	2.203E-11	2.420E-11	2.025E-15	-1.000E+00	1.026E-10	1.814E-10
THYROIDH	1.126E-13	2.352E-11	2.584E-11	2.163E-15	3.442E-10	5.748E-10	1.279E-09
I-133							
STOMACH	2.121E-14	1.076E-11	4.720E-11	4.249E-16	1.023E-10	1.046E-10	5.533E-10
SMALL IN	1.915E-14	9.713E-12	4.252E-11	3.837E-16	2.006E-11	2.150E-11	4.041E-11
LUNGS	2.305E-14	1.172E-11	5.158E-11	4.630E-16	7.128E-10	8.162E-10	4.518E-11
RED MARR	2.350E-14	1.196E-11	5.196E-11	4.725E-16	2.454E-11	2.717E-11	4.313E-11
THYROID	2.873E-14	1.462E-11	6.491E-11	5.771E-16	-1.000E+00	4.855E-08	9.102E-08
LOWER LI	2.077E-14	1.052E-11	4.605E-11	4.154E-16	1.910E-11	2.049E-11	3.883E-11
BONE SUR	2.645E-14	1.350E-11	6.041E-11	5.327E-16	-1.000E+00	2.518E-11	4.080E-11

BREAST	2.829E-14	1.439E-11	6.509E-11	5.676E-16	-1.000E+00	2.931E-11	4.688E-11
TESTES	3.079E-14	1.566E-11	6.965E-11	6.183E-16	-1.000E+00	1.947E-11	3.632E-11
OVARIES	2.071E-14	1.052E-11	4.602E-11	4.154E-16	-1.000E+00	1.934E-11	3.573E-11
EDEWBODY	2.685E-14	1.427E-11	6.312E-11	5.637E-16	-1.000E+00	1.583E-09	2.800E-09
THYROIDH	2.873E-14	1.462E-11	6.491E-11	5.771E-16	4.778E-09	1.617E-08	3.031E-08
I-134							
STOMACH	9.672E-14	8.230E-12	8.245E-12	1.811E-15	7.081E-11	7.081E-11	5.480E-10
SMALL IN	8.847E-14	7.524E-12	7.537E-12	1.655E-15	5.521E-12	5.521E-12	1.600E-11
LUNGS	1.043E-13	8.893E-12	8.909E-12	1.957E-15	1.429E-10	1.429E-10	1.260E-11
RED MARR	1.059E-13	9.008E-12	9.025E-12	1.982E-15	6.067E-12	6.067E-12	1.090E-11
THYROID	1.306E-13	1.114E-11	1.116E-11	2.451E-15	-1.000E+00	2.848E-10	6.160E-10
LOWER LI	9.513E-14	8.100E-12	8.115E-12	1.782E-15	4.800E-12	4.800E-12	1.290E-11
BONE SUR	1.148E-13	9.787E-12	9.804E-12	2.153E-15	-1.000E+00	5.296E-12	9.290E-12
BREAST	1.246E-13	1.061E-11	1.063E-11	2.334E-15	-1.000E+00	6.153E-12	1.160E-11
TESTES	1.379E-13	1.175E-11	1.177E-11	2.584E-15	-1.000E+00	4.001E-12	8.860E-12
OVARIES	9.418E-14	8.028E-12	8.043E-12	1.766E-15	-1.000E+00	4.235E-12	1.100E-11
EDEWBODY	1.204E-13	1.042E-11	1.044E-11	2.292E-15	-1.000E+00	3.548E-11	6.630E-11
THYROIDH	1.306E-13	1.114E-11	1.116E-11	2.451E-15	5.697E-11	9.485E-11	2.051E-10
I-135							
STOMACH	6.093E-14	2.170E-11	4.265E-11	1.065E-15	9.819E-11	9.855E-11	5.403E-10
SMALL IN	5.689E-14	2.020E-11	3.951E-11	9.932E-16	1.878E-11	1.899E-11	4.108E-11
LUNGS	6.589E-14	2.354E-11	4.632E-11	1.154E-15	4.295E-10	4.396E-10	3.737E-11
RED MARR	6.658E-14	2.377E-11	4.682E-11	1.165E-15	2.194E-11	2.231E-11	3.638E-11
THYROID	8.172E-14	2.917E-11	5.765E-11	1.427E-15	-1.000E+00	8.435E-09	1.778E-08
LOWER LI	6.056E-14	2.154E-11	4.231E-11	1.057E-15	1.765E-11	1.784E-11	3.937E-11
BONE SUR	7.106E-14	2.561E-11	5.157E-11	1.242E-15	-1.000E+00	1.997E-11	3.342E-11
BREAST	7.823E-14	2.817E-11	5.639E-11	1.370E-15	-1.000E+00	2.334E-11	3.844E-11
TESTES	8.672E-14	3.094E-11	6.113E-11	1.514E-15	-1.000E+00	1.521E-11	3.213E-11
OVARIES	5.897E-14	2.091E-11	4.088E-11	1.029E-15	-1.000E+00	1.699E-11	3.616E-11
EDEWBODY	7.257E-14	2.643E-11	5.277E-11	1.285E-15	-1.000E+00	3.308E-10	6.041E-10
THYROIDH	8.172E-14	2.917E-11	5.765E-11	1.427E-15	1.434E-09	2.809E-09	5.920E-09
XE-133							
STOMACH	9.450E-16	0.000E+00	0.000E+00	0.000E+00	1.312E-13	1.451E-13	0.000E+00
SMALL IN	7.991E-16	0.000E+00	0.000E+00	0.000E+00	1.368E-13	1.498E-13	0.000E+00
LUNGS	1.113E-15	0.000E+00	0.000E+00	0.000E+00	3.516E-13	3.716E-13	0.000E+00
RED MARR	7.293E-16	0.000E+00	0.000E+00	0.000E+00	1.558E-13	1.686E-13	0.000E+00
THYROID	1.719E-15	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	1.381E-13	0.000E+00
LOWER LI	8.689E-16	0.000E+00	0.000E+00	0.000E+00	1.357E-13	1.486E-13	0.000E+00
BONE SUR	1.976E-15	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	1.616E-13	0.000E+00
BREAST	2.255E-15	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	1.415E-13	0.000E+00
TESTES	1.814E-15	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	1.392E-13	0.000E+00
OVARIES	8.340E-16	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	1.464E-13	0.000E+00
EDEWBODY	1.551E-15	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	1.762E-13	0.000E+00
THYROIDH	1.719E-15	0.000E+00	0.000E+00	0.000E+00	1.212E-13	1.381E-13	0.000E+00
XE-135							
STOMACH	8.213E-15	0.000E+00	0.000E+00	0.000E+00	2.546E-13	2.575E-13	0.000E+00
SMALL IN	7.293E-15	0.000E+00	0.000E+00	0.000E+00	2.560E-13	2.586E-13	0.000E+00
LUNGS	9.006E-15	0.000E+00	0.000E+00	0.000E+00	7.646E-13	7.685E-13	0.000E+00
RED MARR	9.228E-15	0.000E+00	0.000E+00	0.000E+00	2.532E-13	2.554E-13	0.000E+00
THYROID	1.167E-14	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	2.341E-13	0.000E+00
LOWER LI	8.118E-15	0.000E+00	0.000E+00	0.000E+00	2.479E-13	2.504E-13	0.000E+00
BONE SUR	1.202E-14	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	2.473E-13	0.000E+00
BREAST	1.253E-14	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	2.392E-13	0.000E+00
TESTES	1.227E-14	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	2.321E-13	0.000E+00
OVARIES	7.515E-15	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	2.525E-13	0.000E+00
EDEWBODY	1.103E-14	0.000E+00	0.000E+00	0.000E+00	-1.000E+00	3.151E-13	0.000E+00
THYROIDH	1.167E-14	0.000E+00	0.000E+00	0.000E+00	2.308E-13	2.341E-13	0.000E+00
CS-134							
STOMACH	5.581E-14	3.159E-11	6.615E-10	1.097E-15	3.462E-10	1.251E-08	2.009E-08
SMALL IN	5.042E-14	2.858E-11	5.984E-10	9.925E-16	3.382E-10	1.372E-08	2.178E-08
LUNGS	6.025E-14	3.424E-11	7.169E-10	1.189E-15	1.036E-09	1.173E-08	1.746E-08
RED MARR	6.152E-14	3.488E-11	7.303E-10	1.211E-15	9.057E-10	1.178E-08	1.868E-08
THYROID	7.579E-14	4.292E-11	8.986E-10	1.490E-15	-1.000E+00	1.113E-08	1.764E-08
LOWER LI	5.454E-14	3.095E-11	6.481E-10	1.075E-15	3.349E-10	1.372E-08	2.177E-08
BONE SUR	6.786E-14	3.844E-11	8.049E-10	1.335E-15	-1.000E+00	1.091E-08	1.731E-08
BREAST	7.293E-14	4.136E-11	8.661E-10	1.436E-15	-1.000E+00	1.082E-08	1.714E-08

TESTES	8.023E-14	4.556E-11	9.540E-10	1.582E-15	-1.000E+00	1.296E-08	2.058E-08
OVARIES	5.454E-14	3.105E-11	6.500E-10	1.078E-15	-1.000E+00	1.133E-08	1.798E-08
EDEWBODY	6.968E-14	3.966E-11	8.304E-10	1.377E-15	-1.000E+00	1.253E-08	1.975E-08
THYROIDH	7.579E-14	4.292E-11	8.986E-10	1.490E-15	4.736E-10	1.113E-08	1.764E-08
CS-136							
STOMACH	7.864E-14	4.255E-11	7.539E-10	1.490E-15	3.756E-10	1.965E-09	3.384E-09
SMALL IN	7.166E-14	3.884E-11	6.882E-10	1.360E-15	3.663E-10	2.114E-09	3.408E-09
LUNGS	8.498E-14	4.608E-11	8.165E-10	1.614E-15	7.041E-10	2.311E-09	2.617E-09
RED MARR	8.593E-14	4.653E-11	8.245E-10	1.630E-15	7.018E-10	1.855E-09	2.952E-09
THYROID	1.072E-13	5.830E-11	1.033E-09	2.042E-15	-1.000E+00	1.723E-09	2.736E-09
LOWER LI	7.737E-14	4.191E-11	7.427E-10	1.468E-15	3.617E-10	2.108E-09	3.404E-09
BONE SUR	9.481E-14	5.178E-11	9.176E-10	1.814E-15	-1.000E+00	1.691E-09	2.697E-09
BREAST	1.027E-13	5.604E-11	9.930E-10	1.963E-15	-1.000E+00	1.658E-09	2.636E-09
TESTES	1.126E-13	6.129E-11	1.086E-09	2.147E-15	-1.000E+00	1.881E-09	3.034E-09
OVARIES	7.642E-14	4.146E-11	7.347E-10	1.452E-15	-1.000E+00	1.673E-09	2.699E-09
EDEWBODY	9.792E-14	5.320E-11	9.427E-10	1.863E-15	-1.000E+00	1.990E-09	3.062E-09
THYROIDH	1.072E-13	5.830E-11	1.033E-09	2.042E-15	3.585E-10	1.723E-09	2.736E-09
CS-137							
STOMACH	2.010E-14	1.149E-11	2.430E-10	4.020E-16	2.251E-10	8.606E-09	1.390E-08
SMALL IN	1.812E-14	1.037E-11	2.194E-10	3.630E-16	1.956E-10	9.043E-09	1.436E-08
LUNGS	2.178E-14	1.243E-11	2.630E-10	4.350E-16	9.533E-10	8.799E-09	1.266E-08
RED MARR	2.217E-14	1.260E-11	2.666E-10	4.410E-16	5.625E-10	8.295E-09	1.316E-08
THYROID	2.730E-14	1.560E-11	3.301E-10	5.460E-16	-1.000E+00	7.919E-09	1.257E-08
LOWER LI	1.968E-14	1.123E-11	2.376E-10	3.930E-16	1.953E-10	9.063E-09	1.439E-08
BONE SUR	2.460E-14	1.406E-11	2.974E-10	4.920E-16	-1.000E+00	7.933E-09	1.258E-08
BREAST	2.643E-14	1.509E-11	3.192E-10	5.280E-16	-1.000E+00	7.823E-09	1.240E-08
TESTES	2.904E-14	1.655E-11	3.500E-10	5.790E-16	-1.000E+00	8.758E-09	1.390E-08
OVARIES	1.974E-14	1.123E-11	2.376E-10	3.930E-16	-1.000E+00	8.107E-09	1.286E-08
EDEWBODY	2.526E-14	1.459E-11	3.085E-10	5.104E-16	-1.000E+00	8.628E-09	1.355E-08
THYROIDH	2.730E-14	1.560E-11	3.301E-10	5.460E-16	2.960E-10	7.919E-09	1.257E-08
BA-139							
STOMACH	1.157E-15	1.742E-13	1.775E-13	2.467E-17	9.184E-11	9.184E-11	6.880E-10
SMALL IN	1.024E-15	1.539E-13	1.567E-13	2.178E-17	7.425E-11	7.425E-11	5.560E-10
LUNGS	1.278E-15	1.928E-13	1.964E-13	2.730E-17	2.529E-10	2.529E-10	4.450E-13
RED MARR	1.227E-15	1.841E-13	1.875E-13	2.607E-17	4.351E-12	4.351E-12	9.610E-13
THYROID	1.709E-15	2.598E-13	2.646E-13	3.678E-17	-1.000E+00	2.905E-12	3.210E-13
LOWER LI	1.138E-15	1.711E-13	1.743E-13	2.423E-17	1.573E-11	1.573E-11	1.000E-10
BONE SUR	1.826E-15	2.777E-13	2.829E-13	3.932E-17	-1.000E+00	4.354E-12	6.400E-13
BREAST	1.887E-15	2.911E-13	2.966E-13	4.122E-17	-1.000E+00	2.947E-12	5.700E-13
TESTES	1.763E-15	2.687E-13	2.737E-13	3.805E-17	-1.000E+00	2.870E-12	3.620E-13
OVARIES	1.034E-15	1.554E-13	1.583E-13	2.201E-17	-1.000E+00	3.054E-12	1.610E-12
EDEWBODY	2.164E-15	8.125E-13	8.276E-13	1.150E-16	-1.000E+00	4.686E-11	1.080E-10
THYROIDH	1.709E-15	2.598E-13	2.646E-13	3.678E-17	2.905E-12	2.905E-12	3.210E-13
BA-140							
STOMACH	6.405E-15	6.623E-12	5.941E-10	1.332E-16	1.416E-10	3.561E-10	5.836E-10
SMALL IN	5.708E-15	6.025E-12	5.512E-10	1.189E-16	2.874E-10	5.526E-10	1.691E-09
LUNGS	6.976E-15	7.209E-12	6.438E-10	1.455E-16	9.581E-10	1.678E-09	6.920E-11
RED MARR	7.071E-15	7.296E-12	6.525E-10	1.471E-16	4.739E-10	1.221E-09	4.219E-10
THYROID	8.752E-15	9.019E-12	7.951E-10	1.842E-16	-1.000E+00	2.721E-10	5.583E-11
LOWER LI	6.247E-15	6.515E-12	5.891E-10	1.300E-16	2.334E-09	4.364E-09	2.630E-08
BONE SUR	8.340E-15	8.317E-12	7.069E-10	1.754E-16	-1.000E+00	2.317E-09	5.331E-10
BREAST	8.942E-15	9.129E-12	7.788E-10	1.918E-16	-1.000E+00	3.023E-10	1.609E-10
TESTES	9.418E-15	9.696E-12	8.495E-10	1.991E-16	-1.000E+00	2.908E-10	1.467E-10
OVARIES	6.152E-15	6.374E-12	5.705E-10	1.284E-16	-1.000E+00	4.480E-10	9.877E-10
EDEWBODY	8.333E-15	8.930E-12	7.628E-10	1.875E-16	-1.000E+00	1.020E-09	2.545E-09
THYROIDH	8.752E-15	9.019E-12	7.951E-10	1.842E-16	6.819E-11	2.721E-10	5.583E-11
LA-140							
STOMACH	8.657E-14	4.027E-11	2.954E-10	1.497E-15	3.570E-10	4.664E-10	1.086E-09
SMALL IN	8.086E-14	3.754E-11	2.754E-10	1.395E-15	7.481E-10	9.753E-10	2.968E-09
LUNGS	9.354E-14	4.359E-11	3.198E-10	1.620E-15	2.048E-09	4.213E-09	4.000E-11
RED MARR	9.481E-14	4.419E-11	3.242E-10	1.643E-15	1.440E-10	2.124E-10	2.816E-10
THYROID	1.148E-13	5.366E-11	3.936E-10	1.995E-15	-1.000E+00	6.865E-11	6.386E-12
LOWER LI	8.593E-14	4.001E-11	2.935E-10	1.487E-15	2.946E-09	5.498E-09	1.750E-08
BONE SUR	1.008E-13	4.726E-11	3.467E-10	1.757E-15	-1.000E+00	1.406E-10	9.757E-11
BREAST	1.116E-13	5.212E-11	3.824E-10	1.937E-15	-1.000E+00	1.453E-10	1.800E-10
TESTES	1.227E-13	5.724E-11	4.199E-10	2.128E-15	-1.000E+00	5.875E-11	1.217E-10

OVARIES	8.276E-14	3.864E-11	2.835E-10	1.436E-15	-1.000E+00	4.534E-10	1.334E-09
EDEWBODY	1.071E-13	5.107E-11	3.746E-10	1.898E-15	-1.000E+00	1.315E-09	2.290E-09
THYROIDH	1.148E-13	5.366E-11	3.936E-10	1.995E-15	3.768E-11	6.865E-11	6.386E-12
LA-141							
STOMACH	1.566E-15	4.158E-13	6.939E-13	2.667E-17	9.818E-11	9.900E-11	9.310E-10
SMALL IN	1.475E-15	3.913E-13	6.421E-13	2.511E-17	1.430E-10	1.445E-10	1.370E-09
LUNGS	1.700E-15	4.510E-13	7.574E-13	2.892E-17	8.319E-10	8.904E-10	2.715E-13
RED MARR	1.712E-15	4.545E-13	7.461E-13	2.917E-17	5.104E-12	6.845E-12	1.073E-12
THYROID	2.099E-15	5.594E-13	9.643E-13	3.583E-17	-1.000E+00	2.447E-12	5.284E-14
LOWER LI	1.563E-15	4.152E-13	6.889E-13	2.664E-17	1.440E-10	1.672E-10	1.448E-09
BONE SUR	1.804E-15	4.812E-13	8.877E-13	3.073E-17	-1.000E+00	2.502E-11	6.220E-13
BREAST	2.001E-15	5.310E-13	9.646E-13	3.393E-17	-1.000E+00	2.669E-12	7.068E-13
TESTES	2.223E-15	5.890E-13	1.010E-12	3.773E-17	-1.000E+00	2.300E-12	3.183E-13
OVARIES	1.516E-15	4.021E-13	6.581E-13	2.581E-17	-1.000E+00	2.896E-12	3.757E-12
EDEWBODY	2.569E-15	1.848E-12	2.653E-12	1.192E-16	-1.000E+00	1.529E-10	3.750E-10
THYROIDH	2.099E-15	5.594E-13	9.643E-13	3.583E-17	2.195E-12	2.447E-12	5.284E-14
LA-142							
STOMACH	1.123E-13	1.396E-11	1.440E-11	1.744E-15	4.911E-11	4.911E-11	8.530E-10
SMALL IN	1.053E-13	1.307E-11	1.349E-11	1.633E-15	4.066E-11	4.066E-11	7.750E-10
LUNGS	1.195E-13	1.490E-11	1.537E-11	1.861E-15	3.508E-10	3.508E-10	8.370E-12
RED MARR	1.221E-13	1.521E-11	1.569E-11	1.899E-15	6.799E-12	6.799E-12	1.930E-11
THYROID	1.433E-13	1.792E-11	1.849E-11	2.239E-15	-1.000E+00	4.904E-12	1.160E-12
LOWER LI	1.113E-13	1.384E-11	1.427E-11	1.728E-15	1.143E-11	1.144E-11	1.901E-10
BONE SUR	1.262E-13	1.579E-11	1.629E-11	1.972E-15	-1.000E+00	5.372E-12	7.400E-12
BREAST	1.427E-13	1.780E-11	1.836E-11	2.223E-15	-1.000E+00	6.257E-12	1.540E-11
TESTES	1.560E-13	1.945E-11	2.006E-11	2.429E-15	-1.000E+00	2.103E-12	5.290E-12
OVARIES	1.037E-13	1.297E-11	1.338E-11	1.620E-15	-1.000E+00	5.887E-12	6.970E-11
EDEWBODY	1.366E-13	1.761E-11	1.816E-11	2.199E-15	-1.000E+00	5.587E-11	1.790E-10
THYROIDH	1.433E-13	1.792E-11	1.849E-11	2.239E-15	4.904E-12	4.904E-12	1.160E-12
CE-141							
STOMACH	2.388E-15	1.547E-12	3.029E-11	5.391E-17	9.040E-11	1.603E-10	2.240E-10
SMALL IN	2.074E-15	1.338E-12	2.619E-11	4.661E-17	2.167E-10	2.866E-10	5.893E-10
LUNGS	2.664E-15	1.729E-12	3.385E-11	6.025E-17	1.538E-09	1.669E-08	1.429E-12
RED MARR	2.419E-15	1.556E-12	3.047E-11	5.422E-17	2.434E-11	8.891E-11	3.396E-11
THYROID	3.678E-15	2.412E-12	4.721E-11	8.403E-17	-1.000E+00	2.543E-11	1.800E-13
LOWER LI	2.328E-15	1.502E-12	2.940E-11	5.232E-17	1.972E-09	4.100E-09	8.641E-09
BONE SUR	4.154E-15	2.703E-12	5.292E-11	9.418E-17	-1.000E+00	2.657E-10	2.375E-11
BREAST	4.249E-15	2.821E-12	5.523E-11	9.830E-17	-1.000E+00	4.456E-11	1.105E-11
TESTES	3.773E-15	2.484E-12	4.864E-11	8.657E-17	-1.000E+00	5.369E-12	7.580E-12
OVARIES	2.093E-15	1.356E-12	2.655E-11	4.725E-17	-1.000E+00	5.544E-11	1.076E-10
EDEWBODY	3.426E-15	2.229E-12	4.364E-11	7.766E-17	-1.000E+00	2.436E-09	7.850E-10
THYROIDH	3.678E-15	2.412E-12	4.721E-11	8.403E-17	3.186E-12	2.543E-11	1.800E-13
CE-143							
STOMACH	8.720E-15	4.926E-12	3.092E-11	1.858E-16	1.854E-10	2.121E-10	5.608E-10
SMALL IN	7.769E-15	4.380E-12	2.749E-11	1.652E-16	4.174E-10	4.914E-10	1.365E-09
LUNGS	9.545E-15	5.422E-12	3.403E-11	2.045E-16	1.512E-09	3.884E-09	3.829E-12
RED MARR	9.545E-15	5.330E-12	3.345E-11	2.010E-16	2.039E-11	2.953E-11	5.074E-11
THYROID	1.234E-14	7.087E-12	4.448E-11	2.673E-16	-1.000E+00	6.239E-12	4.351E-13
LOWER LI	8.498E-15	4.792E-12	3.007E-11	1.807E-16	2.311E-09	4.281E-09	1.167E-08
BONE SUR	1.195E-14	6.893E-12	4.326E-11	2.600E-16	-1.000E+00	1.647E-11	1.610E-11
BREAST	1.303E-14	7.675E-12	4.817E-11	2.895E-16	-1.000E+00	1.661E-11	2.327E-11
TESTES	1.319E-14	7.616E-12	4.780E-11	2.873E-16	-1.000E+00	5.816E-12	1.531E-11
OVARIES	8.245E-15	4.657E-12	2.923E-11	1.757E-16	-1.000E+00	7.556E-11	2.131E-10
EDEWBODY	1.169E-14	7.369E-12	4.697E-11	2.778E-16	-1.000E+00	9.190E-10	1.228E-09
THYROIDH	1.234E-14	7.087E-12	4.448E-11	2.673E-16	3.686E-12	6.239E-12	4.351E-13
CE-144							
STOMACH	1.793E-15	9.314E-13	2.002E-11	3.343E-17	6.003E-10	1.185E-09	1.110E-09
SMALL IN	1.636E-15	8.416E-13	1.811E-11	3.024E-17	1.461E-09	2.166E-09	3.711E-09
LUNGS	1.960E-15	1.025E-12	2.201E-11	3.675E-17	2.631E-08	7.896E-07	6.514E-12
RED MARR	1.882E-15	9.613E-13	2.070E-11	3.457E-17	4.025E-11	2.786E-09	8.660E-11
THYROID	2.505E-15	1.344E-12	2.880E-11	4.810E-17	-1.000E+00	2.908E-10	5.137E-12
LOWER LI	1.761E-15	9.113E-13	1.960E-11	3.272E-17	1.526E-08	3.410E-08	6.638E-08
BONE SUR	2.426E-15	1.328E-12	2.838E-11	4.738E-17	-1.000E+00	4.819E-09	1.304E-10
BREAST	2.649E-15	1.467E-12	3.136E-11	5.235E-17	-1.000E+00	3.478E-10	1.215E-11
TESTES	2.660E-15	1.426E-12	3.057E-11	5.105E-17	-1.000E+00	1.922E-10	1.013E-11
OVARIES	1.651E-15	8.577E-13	1.845E-11	3.081E-17	-1.000E+00	2.383E-10	6.961E-11

EDEWBODY	8.079E-16	5.398E-13	1.124E-11	1.875E-17	-1.000E+00	1.012E-07	5.710E-09
THYROIDH	2.505E-15	1.344E-12	2.880E-11	4.810E-17	3.907E-12	2.908E-10	5.137E-12
PR-143							
STOMACH	3.234E-22	1.802E-19	3.209E-18	6.310E-24	1.398E-10	1.661E-10	3.620E-10
SMALL IN	2.917E-22	1.630E-19	2.902E-18	5.708E-24	3.371E-10	4.126E-10	8.939E-10
LUNGS	3.488E-22	1.947E-19	3.467E-18	6.818E-24	1.960E-09	1.332E-08	6.518E-15
RED MARR	3.552E-22	1.983E-19	3.531E-18	6.944E-24	4.864E-12	1.497E-11	1.039E-12
THYROID	4.376E-22	2.454E-19	4.370E-18	8.593E-24	-1.000E+00	9.391E-14	6.518E-15
LOWER LI	3.158E-22	1.766E-19	3.144E-18	6.183E-24	3.304E-09	6.763E-09	1.466E-08
BONE SUR	3.900E-22	2.173E-19	3.870E-18	7.610E-24	-1.000E+00	1.495E-11	1.037E-12
BREAST	4.186E-22	2.345E-19	4.176E-18	8.213E-24	-1.000E+00	9.391E-14	6.519E-15
TESTES	4.630E-22	2.590E-19	4.611E-18	9.069E-24	-1.000E+00	9.390E-14	6.519E-15
OVARIES	3.168E-22	1.775E-19	3.160E-18	6.215E-24	-1.000E+00	9.390E-14	6.523E-15
EDEWBODY	1.771E-16	5.553E-13	9.887E-12	1.944E-17	-1.000E+00	2.190E-09	1.264E-09
THYROIDH	4.376E-22	2.454E-19	4.370E-18	8.593E-24	8.229E-14	9.391E-14	6.518E-15
ND-147							
STOMACH	4.313E-15	2.675E-12	4.589E-11	9.386E-17	1.419E-10	1.977E-10	3.571E-10
SMALL IN	3.805E-15	2.359E-12	4.046E-11	8.276E-17	3.388E-10	4.346E-10	9.403E-10
LUNGS	4.756E-15	2.982E-12	5.116E-11	1.046E-16	1.634E-09	1.060E-08	2.446E-12
RED MARR	4.471E-15	2.729E-12	4.682E-11	9.576E-17	3.426E-11	9.219E-11	5.042E-11
THYROID	6.279E-15	4.003E-12	6.868E-11	1.405E-16	-1.000E+00	1.825E-11	2.699E-13
LOWER LI	4.154E-15	2.567E-12	4.403E-11	9.006E-17	2.868E-09	5.843E-09	1.279E-08
BONE SUR	6.247E-15	4.003E-12	6.868E-11	1.405E-16	-1.000E+00	3.258E-10	2.219E-11
BREAST	6.818E-15	4.473E-12	7.674E-11	1.570E-16	-1.000E+00	3.465E-11	1.872E-11
TESTES	6.723E-15	4.302E-12	7.379E-11	1.509E-16	-1.000E+00	6.749E-12	1.364E-11
OVARIES	4.091E-15	2.539E-12	4.356E-11	8.911E-17	-1.000E+00	8.412E-11	1.790E-10
EDEWBODY	5.891E-15	3.991E-12	6.847E-11	1.400E-16	-1.000E+00	1.849E-09	1.184E-09
THYROIDH	6.279E-15	4.003E-12	6.868E-11	1.405E-16	4.598E-12	1.825E-11	2.699E-13
NP-239							
STOMACH	5.296E-15	3.236E-12	3.022E-11	1.180E-16	1.059E-10	1.291E-10	3.457E-10
SMALL IN	4.630E-15	2.818E-12	2.632E-11	1.027E-16	2.413E-10	2.988E-10	8.735E-10
LUNGS	5.898E-15	3.610E-12	3.371E-11	1.316E-16	9.586E-10	2.348E-09	2.402E-12
RED MARR	5.454E-15	3.314E-12	3.095E-11	1.208E-16	7.943E-11	2.075E-10	4.660E-11
THYROID	7.991E-15	4.915E-12	4.590E-11	1.792E-16	-1.000E+00	7.599E-12	2.063E-13
LOWER LI	5.137E-15	3.149E-12	2.941E-11	1.148E-16	1.509E-09	2.916E-09	8.684E-09
BONE SUR	8.815E-15	5.437E-12	5.077E-11	1.982E-16	-1.000E+00	2.027E-09	3.609E-11
BREAST	9.037E-15	6.028E-12	5.629E-11	2.198E-16	-1.000E+00	1.623E-11	1.714E-11
TESTES	8.245E-15	5.141E-12	4.801E-11	1.874E-16	-1.000E+00	2.296E-11	1.144E-11
OVARIES	4.725E-15	2.897E-12	2.705E-11	1.056E-16	-1.000E+00	7.449E-11	1.621E-10
EDEWBODY	7.350E-15	4.572E-12	4.270E-11	1.667E-16	-1.000E+00	6.760E-10	8.807E-10
THYROIDH	7.991E-15	4.915E-12	4.590E-11	1.792E-16	4.130E-12	7.599E-12	2.063E-13
PU-238							
STOMACH	6.723E-19	1.396E-15	2.935E-14	4.852E-20	2.725E-10	1.134E-09	1.277E-09
SMALL IN	4.566E-19	4.249E-16	8.939E-15	1.478E-20	6.381E-10	2.222E-09	3.186E-09
LUNGS	1.008E-18	3.021E-15	6.348E-14	1.050E-19	1.436E-06	3.186E-04	8.643E-14
RED MARR	4.535E-19	1.113E-15	2.340E-14	3.869E-20	2.552E-09	5.785E-05	1.266E-08
THYROID	1.465E-18	3.724E-15	7.825E-14	1.294E-19	-1.000E+00	3.852E-10	7.993E-14
LOWER LI	6.659E-19	1.780E-15	3.740E-14	6.183E-20	6.605E-09	3.294E-08	5.656E-08
BONE SUR	1.792E-18	5.057E-15	1.063E-13	1.757E-19	-1.000E+00	7.211E-04	1.576E-07
BREAST	1.547E-17	1.004E-13	2.110E-12	3.488E-18	-1.000E+00	4.394E-10	1.804E-13
TESTES	3.615E-18	1.862E-14	3.913E-13	6.469E-19	-1.000E+00	1.038E-05	2.318E-09
OVARIES	6.659E-19	1.716E-15	3.606E-14	5.961E-20	-1.000E+00	1.041E-05	2.325E-09
EDEWBODY	4.028E-18	2.290E-14	4.809E-13	7.951E-19	-1.000E+00	7.759E-05	1.337E-08
THYROIDH	1.465E-18	3.724E-15	7.825E-14	1.294E-19	1.480E-11	3.852E-10	7.993E-14
PU-239							
STOMACH	1.776E-18	1.489E-15	2.909E-14	5.169E-20	2.533E-10	1.069E-09	1.196E-09
SMALL IN	1.481E-18	9.863E-16	1.881E-14	3.425E-20	5.952E-10	2.097E-09	2.991E-09
LUNGS	2.074E-18	2.210E-15	4.401E-14	7.674E-20	1.352E-06	3.213E-04	7.881E-14
RED MARR	1.671E-18	1.379E-15	2.665E-14	4.788E-20	2.400E-09	6.568E-05	1.405E-08
THYROID	2.901E-18	2.877E-15	5.717E-14	9.989E-20	-1.000E+00	3.757E-10	7.495E-14
LOWER LI	1.735E-18	1.616E-15	3.182E-14	5.613E-20	6.175E-09	3.099E-08	5.316E-08
BONE SUR	3.425E-18	3.635E-15	7.276E-14	1.262E-19	-1.000E+00	8.167E-04	1.748E-07
BREAST	8.562E-18	3.991E-14	8.344E-13	1.386E-18	-1.000E+00	3.990E-10	1.207E-13
TESTES	3.710E-18	8.548E-15	1.762E-13	2.968E-19	-1.000E+00	1.197E-05	2.631E-09
OVARIES	1.573E-18	1.479E-15	2.915E-14	5.137E-20	-1.000E+00	1.194E-05	2.624E-09
EDEWBODY	3.646E-18	1.003E-14	2.107E-13	3.484E-19	-1.000E+00	8.299E-05	1.396E-08

THYROIDH	2.901E-18	2.877E-15	5.717E-14	9.989E-20	1.381E-11	3.757E-10	7.495E-14
PU-240							
STOMACH	6.976E-19	1.387E-15	2.914E-14	4.820E-20	2.553E-10	1.079E-09	1.201E-09
SMALL IN	4.820E-19	4.516E-16	9.487E-15	1.570E-20	6.007E-10	2.108E-09	3.005E-09
LUNGS	1.034E-18	2.949E-15	6.193E-14	1.024E-19	1.352E-06	3.213E-04	8.206E-14
RED MARR	4.661E-19	1.095E-15	2.301E-14	3.805E-20	2.400E-09	6.562E-05	1.405E-08
THYROID	1.522E-18	3.661E-15	7.689E-14	1.272E-19	-1.000E+00	3.758E-10	7.499E-14
LOWER LI	6.849E-19	1.744E-15	3.662E-14	6.057E-20	6.224E-09	3.112E-08	5.337E-08
BONE SUR	1.842E-18	4.948E-15	1.039E-13	1.719E-19	-1.000E+00	8.145E-04	1.746E-07
BREAST	1.490E-17	9.586E-14	2.013E-12	3.330E-18	-1.000E+00	4.333E-10	1.734E-13
TESTES	3.583E-18	1.789E-14	3.758E-13	6.215E-19	-1.000E+00	1.197E-05	2.631E-09
OVARIES	6.881E-19	1.689E-15	3.547E-14	5.866E-20	-1.000E+00	1.197E-05	2.632E-09
EDEWBODY	3.958E-18	2.190E-14	4.599E-13	7.604E-19	-1.000E+00	8.291E-05	1.397E-08
THYROIDH	1.522E-18	3.661E-15	7.689E-14	1.272E-19	1.381E-11	3.758E-10	7.499E-14
PU-241							
STOMACH	0.000E+00	8.927E-19	3.289E-16	0.000E+00	2.415E-12	2.455E-11	6.080E-12
SMALL IN	0.000E+00	7.733E-19	2.849E-16	0.000E+00	5.838E-12	2.436E-11	1.513E-11
LUNGS	0.000E+00	1.015E-18	3.739E-16	0.000E+00	8.545E-10	3.172E-06	4.468E-15
RED MARR	0.000E+00	8.539E-19	3.146E-16	0.000E+00	4.411E-13	1.426E-06	2.780E-10
THYROID	0.000E+00	1.430E-18	5.268E-16	0.000E+00	-1.000E+00	9.130E-12	1.011E-15
LOWER LI	0.000E+00	8.569E-19	3.157E-16	0.000E+00	6.199E-11	1.805E-10	2.694E-10
BONE SUR	0.000E+00	1.615E-18	5.950E-16	0.000E+00	-1.000E+00	1.776E-05	3.467E-09
BREAST	0.000E+00	1.860E-18	6.852E-16	0.000E+00	-1.000E+00	2.141E-11	2.780E-15
TESTES	0.000E+00	1.496E-18	5.510E-16	0.000E+00	-1.000E+00	2.753E-07	5.636E-11
OVARIES	0.000E+00	7.912E-19	2.915E-16	0.000E+00	-1.000E+00	2.755E-07	5.650E-11
EDEWBODY	7.153E-20	6.100E-17	1.281E-15	2.118E-21	-1.000E+00	1.334E-06	2.069E-10
THYROIDH	0.000E+00	1.430E-18	5.268E-16	0.000E+00	1.872E-15	9.130E-12	1.011E-15
AM-241							
STOMACH	4.883E-16	4.036E-13	8.475E-12	1.402E-17	5.091E-10	3.251E-09	1.345E-09
SMALL IN	4.122E-16	3.378E-13	7.095E-12	1.173E-17	8.464E-10	4.191E-09	3.330E-09
LUNGS	5.930E-16	4.958E-13	1.041E-11	1.722E-17	6.385E-07	1.837E-05	3.364E-11
RED MARR	3.203E-16	2.657E-13	5.580E-12	9.228E-18	4.847E-08	1.738E-04	1.448E-06
THYROID	9.418E-16	7.834E-13	1.645E-11	2.721E-17	-1.000E+00	1.596E-09	1.321E-11
LOWER LI	4.313E-16	3.588E-13	7.536E-12	1.246E-17	6.275E-09	3.161E-08	5.810E-08
BONE SUR	1.091E-15	9.112E-13	1.914E-11	3.165E-17	-1.000E+00	2.166E-03	1.802E-05
BREAST	1.259E-15	1.370E-12	2.876E-11	4.756E-17	-1.000E+00	2.666E-09	2.625E-11
TESTES	9.862E-16	8.738E-13	1.835E-11	3.035E-17	-1.000E+00	3.243E-05	2.693E-07
OVARIES	4.344E-16	3.606E-13	7.574E-12	1.253E-17	-1.000E+00	3.251E-05	2.706E-07
EDEWBODY	8.264E-16	7.533E-13	1.582E-11	2.616E-17	-1.000E+00	1.197E-04	9.819E-07
THYROIDH	9.418E-16	7.834E-13	1.645E-11	2.721E-17	2.761E-10	1.596E-09	1.321E-11
CM-242							
STOMACH	7.008E-19	1.652E-15	3.421E-14	5.740E-20	5.453E-10	1.627E-09	1.423E-09
SMALL IN	4.439E-19	4.317E-16	8.939E-15	1.500E-20	8.934E-10	2.656E-09	3.545E-09
LUNGS	1.081E-18	3.541E-15	7.333E-14	1.230E-19	6.144E-07	1.546E-05	8.833E-12
RED MARR	4.915E-19	1.296E-15	2.684E-14	4.503E-20	5.125E-08	3.908E-06	3.581E-08
THYROID	1.560E-18	4.581E-15	9.487E-14	1.592E-19	-1.000E+00	9.384E-10	8.805E-12
LOWER LI	7.135E-19	2.090E-15	4.328E-14	7.262E-20	6.546E-09	3.118E-08	6.234E-08
BONE SUR	1.899E-18	5.886E-15	1.219E-13	2.045E-19	-1.000E+00	4.862E-05	4.463E-07
BREAST	1.719E-17	1.059E-13	2.192E-12	3.678E-18	-1.000E+00	9.415E-10	8.935E-12
TESTES	4.186E-18	2.172E-14	4.498E-13	7.547E-19	-1.000E+00	5.695E-07	5.190E-09
OVARIES	7.040E-19	2.017E-15	4.177E-14	7.008E-20	-1.000E+00	5.699E-07	5.198E-09
EDEWBODY	4.502E-18	2.482E-14	5.139E-13	8.623E-19	-1.000E+00	4.663E-06	3.102E-08
THYROIDH	1.560E-18	4.581E-15	9.487E-14	1.592E-19	3.048E-10	9.384E-10	8.805E-12
CM-244							
STOMACH	5.105E-19	1.389E-15	2.914E-14	4.820E-20	5.191E-10	1.712E-09	1.356E-09
SMALL IN	3.000E-19	3.090E-16	6.480E-15	1.072E-20	8.501E-10	2.737E-09	3.362E-09
LUNGS	8.308E-19	3.052E-15	6.404E-14	1.059E-19	6.716E-07	1.925E-05	8.846E-12
RED MARR	3.583E-19	1.097E-15	2.301E-14	3.805E-20	5.102E-08	9.330E-05	7.766E-07
THYROID	1.186E-18	3.929E-15	8.244E-14	1.364E-19	-1.000E+00	1.015E-09	8.467E-12
LOWER LI	5.359E-19	1.791E-15	3.758E-14	6.215E-20	6.289E-09	3.147E-08	5.967E-08
BONE SUR	1.446E-18	5.072E-15	1.064E-13	1.760E-19	-1.000E+00	1.171E-03	9.748E-06
BREAST	1.509E-17	9.504E-14	1.994E-12	3.298E-18	-1.000E+00	1.052E-09	8.920E-12
TESTES	3.520E-18	1.919E-14	4.026E-13	6.659E-19	-1.000E+00	1.584E-05	1.319E-07
OVARIES	5.296E-19	1.727E-15	3.624E-14	5.993E-20	-1.000E+00	1.587E-05	1.324E-07
EDEWBODY	3.831E-18	2.208E-14	4.633E-13	7.662E-19	-1.000E+00	6.687E-05	5.429E-07
THYROIDH	1.186E-18	3.929E-15	8.244E-14	1.364E-19	2.909E-10	1.015E-09	8.467E-12

A.3 SITE

**Surry
Sequoyah
Peach Bottom
Grand Gulf**

MACCS SITE DATA FILE FOR SURRY (JLS, 11/10/88)

SECPop POP DISTRIBUTION FROM 1980 CENSUS DATA ALTERED USING 0-10 MI NRC DATA

26 SPATIAL INTERVALS

16 WIND DIRECTIONS

7 CROP CATEGORIES

4 WATER PATHWAY ISOTOPES

2 WATERSHEDS

59 ECONOMIC REGIONS

SPATIAL DISTANCES

0.16	0.52	1.21	1.61	2.13	3.22	4.02	4.83
5.63	8.05	11.27	16.09	20.92	25.75	32.19	40.23
48.28	64.37	80.47	112.65	160.93	241.14	321.87	563.27
804.67	1609.34						

POPULATION

0.	0.	0.	0.	0.	0.	4.	5.
6.	25.	3341.	7107.	2173.	0.	1305.	474.
2252.	2945.	5403.	20169.	112004.	3431358.	1355700.	2742710.
2487346.	104331.						
0.	0.	0.	0.	1.	2.	9.	13.
15.	63.	1667.	3550.	1330.	1072.	3198.	2425.
515.	9469.	5317.	7120.	13586.	198785.	1058744.	20508438.
3290082.	830354.						
0.	0.	0.	0.	0.	0.	5.	6.
8.	31.	822.	1752.	4543.	1713.	1597.	2296.
6535.	1775.	0.	8555.	48596.	119411.	233382.	3003954.
7620063.	1169436.						
0.	0.	0.	0.	0.	0.	1.	1.
2.	11.	543.	1157.	3820.	1621.	3364.	0.
0.	129.	6679.	11858.	0.	0.	0.	0.
0.	0.						
0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	4798.	10202.	10348.	10480.	9570.	0.
0.	2317.	1756.	0.	0.	0.	0.	0.
0.	0.						
0.	0.	0.	0.	0.	0.	1.	1.
1.	7.	8316.	17684.	16340.	30419.	39474.	74998.
24195.	80412.	57477.	0.	0.	0.	0.	0.
0.	0.						
0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	1722.	6433.	36763.	20632.
126203.	372471.	68327.	8599.	6339.	1057.	0.	0.
0.	0.						
0.	0.	0.	0.	0.	0.	2.	2.
3.	13.	127.	273.	1649.	4571.	3441.	7838.
11747.	19019.	3360.	36387.	10447.	12402.	0.	0.
0.	0.						
0.	0.	5.	4.	8.	23.	14.	20.
23.	93.	301.	650.	0.	0.	1264.	4065.
1106.	14665.	4071.	18006.	37417.	89072.	81626.	0.
0.	0.						
0.	0.	0.	0.	0.	0.	19.	25.
29.	117.	45.	105.	0.	510.	951.	1521.
1223.	17636.	4926.	30765.	53265.	289674.	216165.	479431.
280809.	8801784.						
0.	0.	0.	0.	1.	2.	14.	20.
23.	93.	155.	338.	125.	1079.	0.	1355.
2765.	154.	5296.	21409.	62228.	523803.	479588.	1538059.
1526840.	3099458.						
0.	0.	0.	0.	1.	2.	14.	20.
23.	93.	110.	240.	1056.	0.	50.	1396.
915.	3153.	4132.	16295.	35596.	239712.	709522.	2845970.
3957581.	10560254.						
0.	0.	0.	0.	0.	0.	25.	33.
38.	154.	30.	70.	450.	0.	980.	517.
155.	66531.	40902.	9557.	44818.	194801.	376828.	1492286.
2250273.	12145932.						

LAND FRACTION

REGION INDEX

WATERSHED INDEX

A-45

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1 1 1 1 1 1 2 2 2 2 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2
1 1 1 1 1 1 2 2 2 2 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2
1 1 1 1 1 1 2 2 2 2 1 1 1 1 1 2 2 2 2 2 2 2 2 2 2
1 1 1 1 1 1 2 2 2 2 2 2 2 2 2 2 1 1 1 2 2 2 2 2 2
1 1 1 1 1 1 1 1 1 1 2 2 1 1 1 1 1 1 1 1 2 2 2 2 2
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 2 2 2 2 2
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 2 2 2
1 1 1 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1 1 2 2 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1 1 2 2 2 2 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1 1 2 2 2 2 2 2 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1 1 2 2 2 2 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1 1 2 2 2 2 2 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1 1 2 2 2 2 2 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

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CROP SEASON AND SHARE

1 PASTURE	90.	270.	0.41
2 STORED FORAGE	150.	240.	0.13
3 GRAINS	150.	240.	0.21
4 GRN LEAFY VEGETABLES	150.	240.	0.002
5 OTHER FOOD CROPS	150.	240.	0.004
6 LEGUMES AND SEEDS	150.	240.	0.15
7 ROOTS AND TUBERS	150.	240.	0.003

WATERSHED DEFINITION -- INITIAL AND ANNUAL WASHOFF AND INGESTION FACTORS

1 SR-89	5.0E-6	0.0
2 SR-90	5.0E-6	0.0
3 CS-134	5.0E-6	0.0
4 CS-137	5.0E-6	0.0

REGIONAL ECONOMIC DATA

1 ALA	.354	.040	459.	1824.	62000.
2 ARIZ	.516	.104	110.	682.	74000.
3 ARK	.483	.041	466.	2049.	61000.
4 CALIF	.330	.144	1022.	4394.	93000.
5 COLO	.522	.048	211.	971.	83000.
6 CONN	.160	.294	1605.	4980.	107000.
7 DEL	.534	.042	1723.	3428.	82000.
8 FLA	.375	.080	832.	3341.	80000.
9 GA	.363	.060	613.	1885.	73000.
10 IDAHO	.279	.144	343.	1562.	61000.
11 ILL	.806	.044	709.	3900.	86000.
12 IND	.713	.079	611.	3283.	72000.
13 IOWA	.938	.060	695.	3133.	73000.
14 KANS	.917	.035	281.	1204.	81000.
15 KY	.571	.112	482.	1838.	61000.
16 LA	.354	.074	459.	3284.	61000.
17 MAINE	.079	.260	662.	1133.	70000.
18 MD	.429	.216	956.	4489.	93000.
19 MASS	.136	.249	1349.	2563.	97000.
20 MICH	.313	.247	658.	2187.	81000.
21 MINN	.597	.223	516.	2111.	82000.
22 MISS	.470	.054	403.	2084.	53000.
23 MO	.703	.102	322.	1647.	76000.
24 MONT	.657	.030	61.	563.	65000.
25 NEBR	.962	.031	318.	1148.	75000.
26 NEV	.127	.139	63.	601.	84000.
27 N.H.	.096	.482	518.	2018.	87000.
28 N.J.	.203	.129	1399.	6477.	102000.
29 N.MEX	.590	.144	53.	473.	63000.
30 N.Y.	.310	.589	711.	1378.	94000.
31 N.C.	.352	.065	860.	2658.	68000.
32 N.DAK	.924	.048	164.	948.	69000.
33 OHIO	.602	.175	581.	2686.	76000.
34 OKLA	.751	.060	204.	1508.	67000.
35 OREG	.292	.111	236.	1203.	73000.
36 PA	.303	.447	855.	2534.	78000.
37 R.I.	.108	.213	1062.	6438.	80000.
38 S.C.	.290	.084	472.	1843.	62000.
39 S.DAK	.915	.091	145.	587.	65000.

40	TENN	.509	.153	360.	1850.	66000.
41	TEX	.816	.064	164.	1492.	74000.
42	UTAH	.225	.259	123.	1286.	60000.
43	VT	.286	.789	628.	1472.	73000.
44	VA	.382	.198	371.	2075.	84000.
45	WASH	.377	.154	476.	1948.	82000.
46	W.VA	.246	.224	150.	1728.	58000.
47	WIS	.517	.591	723.	1751.	76000.
48	WYO	.561	.028	43.	380.	70000.
49	BRIT COL	.377	.154	476.	1948.	60000.
50	OCEAN	.000	.000	0.	0.	0.
51	SASKAT	.657	.030	61.	563.	60000.
52	MANITOBA	.924	.048	164.	948.	60000.
53	ONTARIO	.597	.223	516.	2111.	60000.
54	QUEBEC	.310	.589	711.	1378.	60000.
55	NOVA SCOT	.079	.260	662.	1133.	60000.
56	BAJA CAL	.330	.144	1022.	4394.	10000.
57	SONORA	.516	.104	110.	682.	10000.
58	CHIHUAHUA	.590	.144	53.	473.	10000.
59	COAHUILA	.816	.064	164.	1492.	10000.

END

MACCS SITE DATA FILE FOR SEQUOYAH (JLS, 11/10/88)
 SECPOP POP DISTRIBUTION FROM 1980 CENSUS DATA ALTERED USING NRC 0-10 MI DATA

26 SPATIAL INTERVALS

16 WIND DIRECTIONS

7 CROP CATEGORIES

4 WATER PATHWAY ISOTOPES

2 WATERSHEDS

59 ECONOMIC REGIONS

SPATIAL DISTANCES

0.16	0.59	1.21	1.61	2.20	3.22	4.02	4.83
5.63	8.05	11.27	16.09	20.92	25.75	32.19	40.23
48.28	64.37	80.47	112.65	160.93	241.14	321.87	563.27
804.67	1609.34						

POPULATION

0.	0.	1.	2.	3.	9.	17.	23.
27.	108.	94.	205.	1723.	2650.	2143.	3115.
0.	3480.	11182.	17930.	28763.	115019.	418223.	5029591.
4226619.	4488368.						
0.	0.	0.	0.	0.	0.	20.	26.
31.	123.	113.	247.	139.	0.	5298.	1568.
2201.	7260.	7325.	32422.	30166.	160847.	199147.	1890643.
6355716.	4462791.						
0.	0.	0.	0.	0.	0.	10.	13.
15.	62.	100.	219.	1268.	0.	842.	1545.
4148.	8158.	13530.	64005.	402619.	182881.	264818.	1337697.
4212858.	16777882.						
0.	0.	2.	2.	4.	12.	21.	29.
34.	139.	137.	303.	1791.	84.	2410.	1760.
3279.	25166.	14663.	20036.	90922.	166500.	427081.	1708718.
2761967.	33429318.						
0.	0.	4.	3.	6.	17.	19.	26.
31.	125.	109.	241.	8099.	4329.	4865.	3644.
1631.	4373.	5694.	10190.	40504.	307949.	679113.	2706447.
1836035.	61860.						
0.	0.	10.	8.	15.	42.	30.	39.
46.	185.	284.	616.	14472.	17775.	2090.	0.
2584.	1342.	11514.	18499.	39805.	264994.	248066.	1611099.
158953.	0.						
0.	0.	28.	21.	43.	108.	19.	26.
31.	124.	221.	479.	1696.	3491.	3673.	573.
2284.	1781.	5016.	12098.	124573.	247313.	116761.	926895.
20508.	0.						
0.	0.	10.	8.	15.	42.	30.	39.
46.	185.	317.	683.	4433.	1428.	1116.	4812.
8921.	35672.	8113.	18140.	440744.	1509163.	332123.	724766.
1849557.	7058200.						
0.	0.	13.	11.	21.	55.	34.	42.
51.	201.	350.	750.	3423.	13902.	1593.	10103.
5243.	23950.	9798.	83659.	74015.	179136.	445749.	722824.
88247.	0.						
0.	0.	10.	8.	15.	42.	24.	33.
38.	155.	1388.	2964.	18490.	16715.	47757.	20708.
13611.	14501.	10374.	25951.	87033.	219844.	165903.	817257.
727568.	0.						
0.	0.	0.	0.	0.	0.	20.	26.
31.	123.	1035.	2207.	11021.	32871.	58191.	25162.
5119.	10063.	8404.	43649.	85136.	336315.	718998.	539129.
2939755.	2621959.						
0.	0.	6.	6.	10.	28.	187.	229.
270.	1064.	1598.	3402.	25316.	8121.	4311.	247.
2740.	13641.	9228.	7319.	198972.	203432.	153718.	737715.
929605.	11056743.						
0.	0.	6.	6.	10.	28.	63.	78.
93.	366.	928.	1979.	0.	996.	0.	4192.
2202.	5408.	6558.	45279.	45072.	142776.	147560.	1566084.
1144300.	4699268.						

CROP SEASON AND SHARE

WATERSHED DEFINITION -- INITIAL AND ANNUAL WASHOFF AND INGESTION FACTORS

REGIONAL ECONOMIC DATA

A-50

40 TENN	.509	.153	360.	1850.	66000.
41 TEX	.816	.064	164.	1492.	74000.
42 UTAH	.225	.259	123.	1286.	60000.
43 VT	.286	.789	628.	1472.	73000.
44 VA	.382	.198	371.	2075.	84000.
45 WASH	.377	.154	476.	1948.	82000.
46 W.VA	.246	.224	150.	1728.	58000.
47 WIS	.517	.591	723.	1751.	76000.
48 WYO	.561	.028	43.	380.	70000.
49 BRIT COL	.377	.154	476.	1948.	60000.
50 OCEAN	.000	.000	0.	0.	0.
51 SASKAT	.657	.030	61.	563.	60000.
52 MANITOBA	.924	.048	164.	948.	60000.
53 ONTARIO	.597	.223	516.	2111.	60000.
54 QUEBEC	.310	.589	711.	1378.	60000.
55 NOVA SCOT	.079	.260	662.	1133.	60000.
56 BAJA CAL	.330	.144	1022.	4394.	10000.
57 SONORA	.516	.104	110.	682.	10000.
58 CHIHUAHUA	.590	.144	53.	473.	10000.
59 COAHUILA	.816	.064	164.	1492.	10000.

END

MACCS SITE DATA FILE FOR PEACH BOTTOM (JLS, 11/10/88)
 SECPop POP DISTRIBUTION FROM 1980 CENSUS DATA ALTERED USING NRC 0-10 MI DATA

26 SPATIAL INTERVALS

16 WIND DIRECTIONS

7 CROP CATEGORIES

4 WATER PATHWAY ISOTOPES

2 WATERSHEDS

59 ECONOMIC REGIONS

SPATIAL DISTANCES

0.40	0.82	1.21	1.61	2.43	3.22	4.02	4.83
5.63	8.05	11.27	16.09	20.92	25.75	32.19	40.23
48.28	64.37	80.47	112.65	160.93	241.14	321.87	563.27
804.67	1609.34						

POPULATION

0.	0.	0.	0.	0.	0.	20.	26.
31.	122.	406.	867.	2212.	5557.	68185.	42610.
36746.	25232.	43251.	88038.	210634.	215849.	547385.	1124293.
25330.	0.						
0.	0.	1.	1.	3.	7.	19.	26.
30.	123.	455.	977.	5385.	1870.	9336.	12012.
13500.	29877.	188747.	79915.	174604.	430572.	162914.	1349066.
393839.	0.						
0.	0.	1.	2.	4.	8.	24.	32.
37.	151.	413.	889.	1602.	2235.	3231.	10573.
14456.	22521.	91474.	220858.	495439.	1870811.	1387490.	5663616.
1201796.	326019.						
0.	0.	0.	1.	2.	4.	31.	39.
48.	187.	325.	700.	2912.	1710.	3207.	3038.
26164.	90241.	164108.	2425058.	987201.	10635304.	3591517.	4107688.
32847.	0.						
0.	0.	6.	5.	14.	21.	32.	41.
49.	195.	323.	698.	1871.	4260.	5207.	9780.
37964.	241423.	217733.	745625.	219373.	268826.	0.	0.
0.	0.						
0.	0.	0.	0.	0.	0.	32.	39.
46.	183.	354.	755.	4439.	760.	4691.	11312.
40619.	35254.	18393.	113077.	188361.	49837.	0.	0.
0.	0.						
0.	0.	0.	0.	0.	0.	28.	36.
43.	169.	406.	870.	3309.	3109.	5776.	1130.
3899.	10750.	14771.	72422.	79583.	9233.	0.	0.
0.	0.						
0.	0.	1.	2.	4.	8.	37.	46.
56.	219.	702.	1498.	1005.	4019.	24424.	5722.
856.	8539.	9246.	26850.	83286.	119486.	708.	0.
0.	0.						
0.	0.	4.	4.	11.	17.	14.	20.
23.	93.	1048.	2238.	4653.	5262.	9826.	24736.
5216.	3830.	3556.	39680.	50491.	79486.	699884.	908098.
91529.	0.						
0.	0.	8.	6.	20.	28.	16.	23.
27.	109.	476.	1024.	2497.	11148.	9730.	20245.
77714.	765820.	262612.	524192.	713496.	142725.	773884.	1665003.
1818021.	9939781.						
0.	0.	5.	5.	13.	19.	178.	219.
259.	1019.	510.	1090.	2522.	2254.	7890.	10533.
48267.	370900.	155161.	804528.	1197119.	135990.	265587.	2040215.
3539979.	10361091.						
0.	0.	4.	4.	11.	16.	30.	39.
46.	185.	317.	683.	1074.	2423.	1931.	3281.
4610.	26679.	45421.	93784.	130701.	137332.	106204.	1206559.
2351412.	10208089.						
0.	0.	9.	7.	21.	30.	49.	62.
73.	291.	475.	1019.	3353.	0.	2586.	9756.
4223.	44975.	27904.	69133.	177306.	198565.	501712.	1845582.
5452104.	13054765.						


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1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 2 2 2 2 2
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 2 2 2 2 2
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1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 2 2 2 2 2
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 2 2 2 2 2
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 2
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

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CROP SEASON AND SHARE

1 PASTURE	90.	270.	0.38
2 STORED FORAGE	150.	240.	0.13
3 GRAINS	150.	240.	0.23
4 GRN LEAFY VEGETABLES	150.	240.	0.002
5 OTHER FOOD CROPS	150.	240.	0.004
6 LEGUMES AND SEEDS	150.	240.	0.16
7 ROOTS AND TUBERS	150.	240.	0.004

WATERSHED DEFINITION -- INITIAL AND ANNUAL WASHOFF AND INGESTION FACTORS

1 SR-89	5.0E-6	0.0
2 SR-90	5.0E-6	0.0
3 CS-134	5.0E-6	0.0
4 CS-137	5.0E-6	0.0

REGIONAL ECONOMIC DATA

1 ALA	.354	.040	459.	1824.	62000.
2 ARIZ	.516	.104	110.	682.	74000.
3 ARK	.483	.041	466.	2049.	61000.
4 CALIF	.330	.144	1022.	4394.	93000.
5 COLO	.522	.048	211.	971.	83000.
6 CONN	.160	.294	1605.	4980.	107000.
7 DEL	.534	.042	1723.	3428.	82000.
8 FLA	.375	.080	832.	3341.	80000.
9 GA	.363	.060	613.	1885.	73000.
10 IDAHO	.279	.144	343.	1562.	61000.
11 ILL	.806	.044	709.	3900.	86000.
12 IND	.713	.079	611.	3283.	72000.
13 IOWA	.938	.060	695.	3133.	73000.
14 KANS	.917	.035	281.	1204.	81000.
15 KY	.571	.112	482.	1838.	61000.
16 LA	.354	.074	459.	3284.	61000.
17 MAINE	.079	.260	662.	1133.	70000.
18 MD	.429	.216	956.	4489.	93000.
19 MASS	.136	.249	1349.	2563.	97000.
20 MICH	.313	.247	658.	2187.	81000.
21 MINN	.597	.223	516.	2111.	82000.
22 MISS	.470	.054	403.	2084.	53000.
23 MO	.703	.102	322.	1647.	76000.
24 MONT	.657	.030	61.	563.	65000.
25 NEBR	.962	.031	318.	1148.	75000.
26 NEV	.127	.139	63.	601.	84000.
27 N.H.	.096	.482	518.	2018.	87000.
28 N.J.	.203	.129	1399.	6477.	102000.
29 N.MEX	.590	.144	53.	473.	63000.
30 N.Y.	.310	.589	711.	1378.	94000.
31 N.C.	.352	.065	860.	2658.	68000.
32 N.DAK	.924	.048	164.	948.	69000.
33 OHIO	.602	.175	581.	2686.	76000.
34 OKLA	.751	.060	204.	1508.	67000.
35 OREG	.292	.111	236.	1203.	73000.
36 PA	.303	.447	855.	2534.	78000.
37 R.I.	.108	.213	1062.	6438.	80000.
38 S.C.	.290	.084	472.	1843.	62000.
39 S.DAK	.915	.091	145.	587.	65000.

40 TENN	.509	.153	360.	1850.	66000.
41 TEX	.816	.064	164.	1492.	74000.
42 UTAH	.225	.259	123.	1286.	60000.
43 VT	.286	.789	628.	1472.	73000.
44 VA	.382	.198	371.	2075.	84000.
45 WASH	.377	.154	476.	1948.	82000.
46 W.VA	.246	.224	150.	1728.	58000.
47 WIS	.517	.591	723.	1751.	76000.
48 WYO	.561	.028	43.	380.	70000.
49 BRIT COL	.377	.154	476.	1948.	60000.
50 OCEAN	.000	.000	0.	0.	0.
51 SASKAT	.657	.030	61.	563.	60000.
52 MANITOBA	.924	.048	164.	948.	60000.
53 ONTARIO	.597	.223	516.	2111.	60000.
54 QUEBEC	.310	.589	711.	1378.	60000.
55 NOVA SCOT	.079	.260	662.	1133.	60000.
56 BAJA CAL	.330	.144	1022.	4394.	10000.
57 SONORA	.516	.104	110.	682.	10000.
58 CHIHUAHUA	.590	.144	53.	473.	10000.
59 COAHUILA	.816	.064	164.	1492.	10000.

END

MACCS SITE DATA FILE FOR GRAND GULF (JLS, 11/10/88)
 SECPPOP POP DISTRIBUTION FROM 1980 CENSUS DATA ALTERED USING NRC 0-10 MI DATA

26 SPATIAL INTERVALS								
16 WIND DIRECTIONS								
7 CROP CATEGORIES								
4 WATER PATHWAY ISOTOPES								
2 WATERSHEDS								
59 ECONOMIC REGIONS								
SPATIAL DISTANCES								
0.40	0.70	1.21	1.61	2.31	3.22	4.02	4.83	
5.63	8.05	11.27	16.09	20.92	25.75	32.19	40.23	
48.28	64.37	80.47	112.65	160.93	241.14	321.87	563.27	
804.67	1609.34							
POPULATION								
0.	0.	4.	3.	7.	16.	0.	1.	
2.	12.	30.	70.	0.	0.	67.	1304.	
0.	74.	743.	15484.	83209.	72162.	120923.	541090.	
3057152.	9822912.							
0.	0.	1.	2.	3.	9.	1.	3.	
4.	17.	45.	105.	0.	4637.	0.	15004.	
21111.	2866.	604.	10875.	31683.	110002.	126487.	1603453.	
1595033.	24970756.							
0.	0.	0.	0.	0.	0.	5.	6.	
8.	31.	95.	205.	713.	0.	1658.	4373.	
757.	3527.	3814.	12032.	35282.	62550.	175379.	1020222.	
2240248.	21211502.							
0.	0.	0.	0.	1.	4.	11.	16.	
19.	79.	85.	190.	0.	413.	0.	853.	
2232.	3387.	49094.	247241.	33956.	99583.	73501.	1699378.	
3829756.	18370806.							
0.	0.	1.	2.	3.	9.	13.	18.	
22.	87.	61.	139.	401.	327.	0.	0.	
893.	5713.	10673.	16982.	31249.	133852.	75589.	888587.	
1460466.	1943140.							
0.	0.	1.	0.	3.	6.	51.	65.	
77.	307.	109.	241.	0.	751.	63.	0.	
1185.	5028.	7940.	15118.	33308.	130847.	390071.	714008.	
368763.	8028641.							
0.	0.	1.	0.	3.	6.	201.	249.	
293.	1157.	1149.	2451.	0.	851.	0.	222.	
858.	1203.	21095.	19956.	49172.	94458.	284438.	656.	
0.	754387.							
0.	0.	0.	0.	1.	4.	14.	20.	
23.	93.	170.	370.	201.	0.	1430.	0.	
13.	3396.	1567.	22369.	42828.	544166.	811964.	11629.	
0.	0.							
0.	0.	1.	2.	3.	9.	6.	9.	
12.	48.	128.	282.	0.	0.	1492.	3370.	
0.	1858.	2341.	9365.	67097.	515206.	208032.	0.	
0.	0.							
0.	0.	0.	0.	1.	4.	3.	6.	
8.	33.	101.	224.	0.	927.	0.	1091.	
65.	28282.	3770.	5243.	35077.	369254.	56437.	0.	
0.	0.							
0.	0.	1.	0.	2.	2.	0.	0.	
0.	0.	79.	171.	0.	0.	0.	1339.	
0.	23126.	3047.	4072.	41214.	100210.	217276.	879780.	
399582.	639306.							
0.	0.	0.	0.	0.	0.	0.	0.	
0.	0.	63.	137.	1716.	465.	0.	525.	
663.	1298.	2246.	16476.	123117.	79084.	75399.	2976832.	
2081941.	284505.							
0.	0.	0.	0.	0.	0.	0.	0.	
0.	0.	25.	55.	0.	0.	117.	313.	
0.	5945.	2397.	10843.	28920.	64335.	236712.	2130706.	
1744285.	1801823.							

LAND FRACTION

REGION INDEX

WATERSHED INDEX

A-57

CROP SEASON AND SHARE

WATERSHED DEFINITION -- INITIAL AND ANNUAL WASHOFF AND INGESTION FACTORS

REGIONAL ECONOMIC DATA

A-58

40 TENN	.509	.153	360.	1850.	66000.
41 TEX	.816	.064	164.	1492.	74000.
42 UTAH	.225	.259	123.	1286.	60000.
43 VT	.286	.789	628.	1472.	73000.
44 VA	.382	.198	371.	2075.	84000.
45 WASH	.377	.154	476.	1948.	82000.
46 W.VA	.246	.224	150.	1728.	58000.
47 WIS	.517	.591	723.	1751.	76000.
48 WYO	.561	.028	43.	380.	70000.
49 BRIT COL	.377	.154	476.	1948.	60000.
50 OCEAN	.000	.000	0.	0.	0.
51 SASKAT	.657	.030	61.	563.	60000.
52 MANITOBA	.924	.048	164.	948.	60000.
53 ONTARIO	.597	.223	516.	2111.	60000.
54 QUEBEC	.310	.589	711.	1378.	60000.
55 NOVA SCOT	.079	.260	662.	1133.	60000.
56 BAJA CAL	.330	.144	1022.	4394.	10000.
57 SONORA	.516	.104	110.	682.	10000.
58 CHIHUAHUA	.590	.144	53.	473.	10000.
59 COAHUILA	.816	.064	164.	1492.	10000.

END