

CONF-8705165--1

ELECTRON SPUTTERING IN THE ANALYTICAL ELECTRON MICROSCOPE:  
CALCULATIONS & EXPERIMENTAL DATA

Nestor J. Zaluzec and John F. Mansfield  
Electron Microscopy Center for Materials Research  
Materials Science Division  
Argonne National Laboratory  
Argonne, IL 60439, USA

CONF-8705165--1

DE87 011457

MARCH 1988

The submitted manuscript has been authored  
by a contractor of the U.S. Government  
under contract No. W-31-109-ENG-38.  
Accordingly, the U.S. Government retains a  
nonexclusive, royalty-free license to publish  
or reproduce the published form of this  
contribution or allow others to do so, for  
U.S. Government purposes.

\*Work supported by the U.S. Department of Energy, BES-Materials  
Sciences, under Contract W-31-109-Eng-38.

To be submitted to Proceedings of Workshop on Intermediate Voltage Microscopy  
and Its Application to Materials Science held at National Research Council of  
Canada, May 26-27, 1987.

DISCLAIMER

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

MASTER

DISSEMINATION OF THIS DOCUMENT IS UNLIMITED

# Electron Sputtering in the Analytical Electron Microscope: Calculations & Experimental Data

by

Nestor J. Zaluzec and John F. Mansfield

Electron Microscopy Center for Materials Research

Materials Science Division

Argonne National Laboratory

Argonne Illinois 60439 USA

## Introduction

The environment of the electron microscope is particularly severe when one considers the energy deposited in a specimen during typical experimental conditions. Conventional imaging experiments tend to employ electron current densities ranging from  $\sim 0.1$  to  $1 \text{ A/cm}^2$  while during microanalysis conditions probe current densities can range from  $10$  to values as high as  $10^5 \text{ A/cm}^2$ . At  $100 \text{ kV}$  this corresponds to power densities from  $100 \text{ Kilowatts/cm}^2$  to  $10^4 \text{ Megawatts/cm}^2$ . We have long known that these energy deposition rates can result in electron irradiation damage which can substantially alter the structure and composition of a specimen through either ionization damage in organics (Glaeser, 1978) or by displacement damage in inorganics (Hobbs, 1978) and/or combinations thereof. For the most part materials scientists operating an analytical electron microscope (AEM) in the  $100 - 200 \text{ kV}$  regime studying metallic and/or ceramic specimens have been spared the need to consider either of these effects as their specimens have tended to be sufficiently resilient. However, the advent of the new medium voltage

microscopes operating in the 300 - 400 kV regime with high brightness guns and clean or ultrahigh vacuum systems has necessitated a reevaluation of the effects of higher voltage operation in light of the destructive nature of the electron beam particularly under microanalysis conditions.

The advantages of increasing the accelerating voltage and decreasing the column vacuum have been discussed in detail elsewhere (Zaluzec 1978, Zaluzec, Taylor, Ryan & Philippides 1983, as well as in these proceedings). The detrimental implications of higher voltage operation relative to microanalysis are more subtle and were briefly discussed by Zaluzec and Mansfield (1986). In this earlier work, the calculated rates of displacement damage and atomic sputtering were compared with the characteristic signal generation rate. In this paper we expand upon that study with additional calculations relative to atomic sputtering as well as provide experimental verification of electron beam induced sputtering in the AEM.

### **Radiation Damage and Sputtering**

Radiation displacement damage occurs when kinetic energy is transferred from the incident electron beam to the atoms within the specimen. If the energy transferred is sufficient, then atoms may be displaced from their lattice sites; either to form point defects, which may subsequently migrate and cause elemental rearrangement, or to be sputtered from the solid.

These effects have been widely reported in the literature over the last ten years, however they have been mainly associated with High Voltage Electron Microscope (HVEM) studies (see for example Wiedersich et al 1977; Cherns et al 1976, 1977; Okamoto and Lam 1985). More recently electron probe related effects have been observed at 100 kV in dedicated STEM instruments by

Mochel et al (1983) and Thomas (1985) while radiation induced segregation was also observed by Mansfield et al (1986) during X-ray Energy Dispersive Spectroscopy (XEDS) analysis of an aluminium zinc alloy at 300 kV.

The amount of kinetic energy ( $T_T$ ) transferred by an incoming electron (mass  $m_0$ ) to the nucleus of a specimen atom depends upon its kinetic energy  $T_E = eV_0$  ( $e$ =electronic charge,  $V_0$ = accelerating potential), the mass of the nucleus ( $M$ ) and the direction of scattering ( $\phi$ ) and can be written:

$$T_T = [2 * T_E * (T_E + 2 * m_0 c^2) * \sin^2(\phi/2)] / [M c^2] \quad 1.$$

The maximum energy transfer occurs for the forward scattering geometry ( $\phi=180^\circ$ ), which is the condition that we will use in all the calculations, presented herein. Atomic displacement occurs when the incident electron transfers sufficient energy ( $T_d$ ) to permanently displace or remove an atom from its normal lattice site. For the case of sputtering in the AEM, we only consider the removal of atoms from the electron exit surface of the specimen. Since the atoms at this surface are not totally surrounded as in the "bulk", the sputtering energy required to remove them ( $T_s$ ) is necessarily less than that required to form defects within the solid. As an upper limit one can estimate that  $T_s \sim T_d/2$ . Phenomenologically,  $T_s$  can also be related to the sublimation energy of a material, this could lower estimates of  $T_s$  by as much as another factor of 2. Table 1 compares the maximum kinetic energy transferable to various atoms at accelerating voltages of 100 - 400 kV, with values of the

experimentally derived displacement energy  $T_d$  and the sputtering energy

$T_d/4 < T_s < T_d/2$ . As one can see from this table the amount of energy transferred ( $T_T$ ) to many elements in the 100- 400 kV range is equal to or greater than  $T_s$  and therefore sufficient to warrant further investigation particularly for elements of atomic number  $< 30$ .

In order to estimate the cross sections ( $\sigma$ ) for sputtering, we will assume values of  $T_s \sim T_d/2$  and then interpolate values of  $\sigma$  from Oen's tables (1973).

Sputtering cross sections obtained in this manner are plotted in Figure 1 for the elements Aluminium, Titanium, Nickel and Niobium. The sputtering rate ( $R_s$ ) is given by the product of the cross-section ( $\sigma$ ) and the probe current density ( $J$ ). Although the cross-sections shown in figure 1 are somewhat low (1-100 Barns) the probe current density found under microanalysis conditions can be sufficient to make the sputtering rates significant. For example, one calculates that at 400 kV for a probe current density of  $30 \text{ A/cm}^2$  the sputtering rates for Aluminium, Titanium, Nickel and Niobium are 0.020, 0.025, 0.011, and 0.002 displacements/atom/sec, respectively. Assuming that each displacement of a surface atom is sufficient to cause its removal then the magnitude of this displacement or sputtering rate (  $\sim 0.02 - 0.002$  atomic layers per second ) should be readily observable. With the advent of the high brightness  $\text{LaB}_6$  and Field Emission Guns having current densities as much as 10 to 1000 times greater, one clearly has the potential to encounter enormous sputtering rates during microanalysis. This, of course, assumes that the environmental conditions within the microscope at the specimen are sufficiently "clean" that hydrocarbon contamination in the vicinity of the probe doesnot overwhelm the process of surface sputtering.

## Experimental

A thin foil of a polycrystalline aluminium-magnesium alloy was prepared by co-evaporation in a UHV evaporation system on NaCl. After removal of the NaCl by clean distilled water the specimen was mounted upon 3 mm Copper grid and subsequently transferred to the AEM. The specimen was irradiated with a 180nm diameter probe in a Philips EM420T for approximately 4000 seconds at 120kV using a tungsten hairpin filament electron source. The electron probe current was measured with a post-specimen Faraday cup, located in the camera chamber of microscope, where it was determined that during the sputtering experiment the probe current density was constant at  $\sim 28 \text{ A/cm}^2$ . Figure 2 shows a micrograph of the irradiated area before (2a) and after (2b) the 4000 sec irradiation, clearly seen is the "thinning" of the selected area. No specimen contamination during microanalysis of this specimen was observed at any time during this study in the AEM.

The change in relative thickness of the sample was monitored by continuously measuring the low loss region of the electron energy loss spectrum of the irradiated area and using the expression:

$$T/\lambda = \ln(I_0/I_t) \quad 2.$$

where  $T$ =specimen thickness,  $\lambda$ =mean free path of the inelastically scattered electrons,  $I_0$ =intensity of the zero loss peak, and  $I_t$ =intensity of the total inelastic spectrum. The values of  $\ln(I_0/I_t)$  were plotted as a function of irradiation time and the resulting graph is shown in figure 3. This plot

illustrates that there was a continuous reduction in the sample thickness during the irradiation which we attribute to sputtering.

A semi-quantitative analysis of the change in thickness can be made by assuming that the value of  $\lambda$  for the alloy is nearly the same as that for pure aluminium (~120nm). Thus assuming that the thickness calculated from the time zero spectrum is the original thickness, then this data yields an initial thickness of 62.4nm and a final thickness of 42.0 nm. This represents a ~20 nm (33%) reduction in sample thickness in the area under the probe due to the irradiation.

For comparison, the reduction in thickness by sputtering can be also estimated using calculated sputtering rates discussed above. Cross-sections for sputtering at 120kV were interpolated from Oen's calculations for pure Aluminium and Magnesium. The interpolation for pure Al is relatively unambiguous and yields a value of ~ 62 barns. Magnesium, however, is more difficult as the data is rapidly varying in the region in which we are interested, here the cross section is estimated to lie between 75 and 150 barns. For an irradiation time of 4000 seconds, with a probe current density of  $28 \text{ A/cm}^2$ , the amount of each element sputtered would have been ~43 layers of Al and ~52-104 layers of Mg. If we assume for the purposes of comparison that each atomic layer is ~ 0.3 nm thick equally populated by Al and Mg, then one calculates an overall reduction in thickness of ~15 - 28 nm which compares favorably to the experimentally determined mass loss of 20 nm.

The loss of mass, during microanalysis, from a specimen would on purely statistical considerations merely require an extended acquisition time in most microanalysis situations. However, examination of XEDS spectra recorded both

at the beginning and the end of the irradiation (figure 4) revealed that there was also preferential removal of Magnesium. Thus, the sample composition was changing during the irradiation, an effect which is to be expected considering the fact that the atomic sputtering rates for the two species are different.

### **Conclusions**

Experimental measurement of the atomic sputtering of specimens during microanalysis in a conventional 120kV AEM, has verified that electron sputtering can be an important effect during microanalysis. Calculations indicate that for the new generation of medium voltage analytical electron microscope this effect will become even more pronounced and must not be neglected during analysis. Preferential sputtering of different atomic species was observed and can have major implications to the accuracy of quantitative microanalysis.

### **Acknowledgement**

This work was supported by the U.S. Department of Energy, BES Materials Sciences, under contract number W-31-109-ENG-38 at Argonne National Laboratory.



## References

- Cherns, D., Minter, F. J. and Nelson, R. S., Nucl. Inst. & Methods 132 (1976) p369.
- Cherns, D., Finnis, M. W. and Matthews, M. D., Phil. Mag. 35 (1977) p693
- Glaeser R. M, in Introduction to Analytical Electron Microscopy, ed. Hren, Joy, and Goldstein (1978) Chapter 16, Plenum Press
- Hobbs L.W. in Introduction to Analytical Electron Microscopy, ed. Hren, Joy, and Goldstein (1978) Chapter 17 Plenum Press
- Mansfield, J. F., Okamoto, P. R., Rehn, L. E. and Zaluzec, N. J., accepted for publication in Ultramicroscopy 1986.
- Mochel M.E., Humphreys C.J. , Eades J. A., Mochel J.M. , Petford A.M., Applied Physics Letters, Vol 42 (4), p 392 (1983)
- Oen, O. S., ORNL Report #TM-4897, (1973).
- Thomas, L. E., Ultramicroscopy 18 (1985)
- Wiedersich H., Okamoto P.R. , Lam N.Q. in Radiation Effects in Breeder Reactor Structural Materials, ed. M.L. Bleiberg and J.W. Bennett (AIME, New York) 1977 p 801-819
- Zaluzec, N. J. 9th Int. Cong. on E. M., Toronto, Canada, (1978) p548.
- Zaluzec, N. J., Taylor, A., Ryan, E. A. and Philippides, A., Proc 7th HVEM Meeting, Univ. of Calif., Berkeley, Ca., #LBL-16031 Conf.-830819 (1983) p79.
- Zaluzec, N. J., Mansfield, J. F., Okamoto, P. R. and Lam, N. Q., Inst. Phys. Conf. Series No78 (1985), Chapter
- Zaluzec, N.J. and Mansfield J.F., Proceedings of the 44th EMSA meeting Albuquerque N.M, 1986 p.708 , San Francisco Press ed. G.W. Bailey

## **Keywords**

Analytical Electron Microscope (AEM)

Radiation Damage

Atomic Displacement, Atomic Sputtering, Preferential Sputtering

Electron Energy Loss Spectroscopy EELS

X-ray Energy Dispersive Spectroscopy XEDS

## **Figure Captions**

**Figure 1** Sputtering cross-sections for Aluminium, Titanium, Nickel and Niobium as a function of the incident beam accelerating voltage evaluated for  $T_s = T_d/2$ .

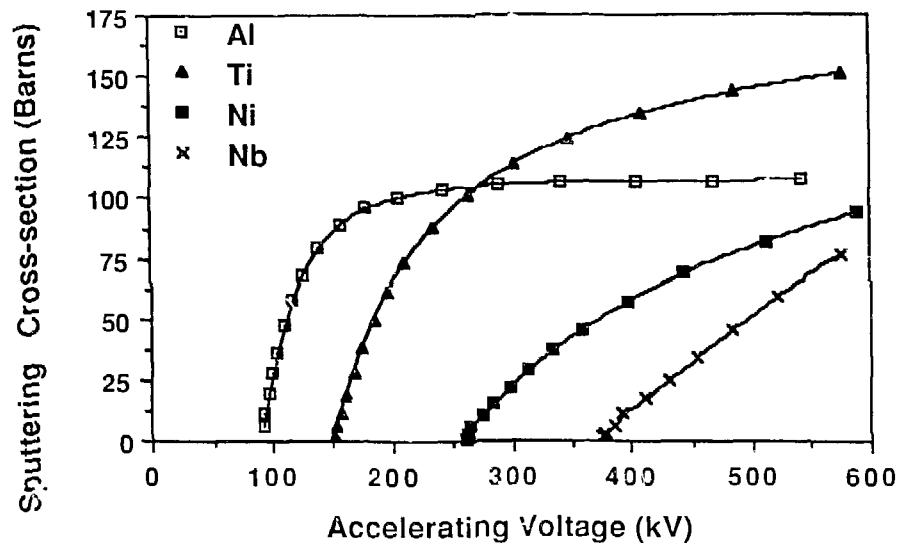
**Figure 2** Analyzed region of the Aluminium/Magnesium alloy before (a) and after (b) 4000 sec irradiation. Thinning due to sputtering is readily visible in the micrograph.

**Figure 3** Experimentally measured change in specimen thickness during irradiation, obtained by continuously measuring the relative intensity of the zero loss to inelastic scattering intensity ratio during electron irradiation.

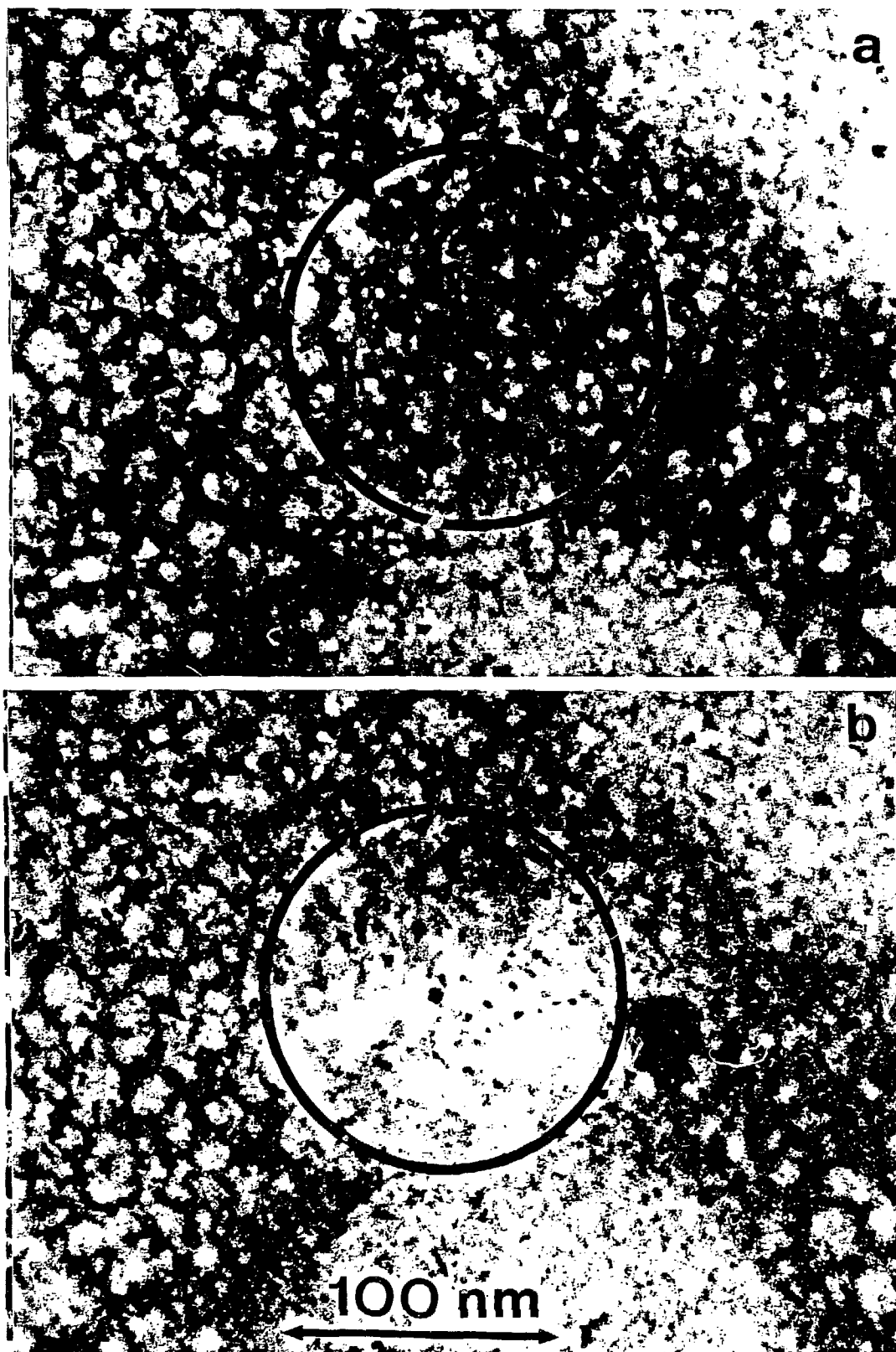
**Figure 4** Experimentally measured x-ray energy dispersive spectra before and after ~ 4000 sec irradiation. Note the change in the relative intensity ratio of Al to Mg  $K\alpha$  lines indicating a preferential loss of Mg due to sputtering. The Al  $K\alpha$  lines have been normalized to the same value for display purposes.

**Table 1**  
**Comparison of Maximum Transferable Kinetic Energy**  
**with Displacement and Sputtering Energies**  
**at 100, 200, 300 and 400 kV**

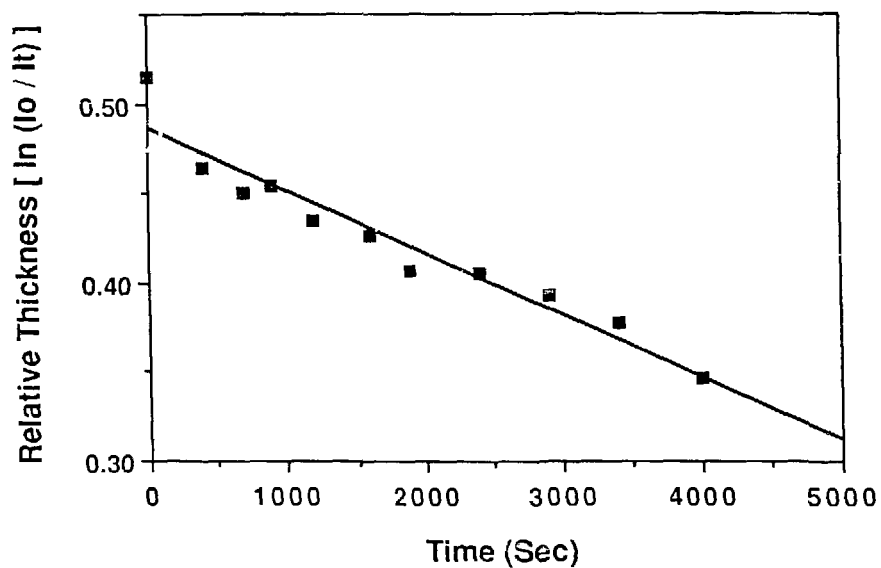
Element	$T_T$ [eV]				$T_d$ [eV]	$T_s$ [eV]
	100kV	200kV	300kV	400kV		
Al	8.93	19.5	31.6	45.3	16	4-8
Ti	5.00	11.0	17.8	25.5	15	4-8
V	4.73	10.3	16.72	24.0	29	7-14
Cr	4.63	10.1	16.38	23.5	22	5-11
Fe	4.31	9.40	15.25	21.8	16	4-8
Co	4.08	8.91	14.45	20.7	23	6-12
Ni	4.10	8.94	14.5	20.8	22	6-11
Cu	3.79	8.26	13.4	19.2	18	4-9
Zn	3.69	8.03	13.03	18.7	16	4-8
Nb	2.59	5.65	9.17	13.2	24	6-12
Mo	2.51	5.47	8.88	12.7	27	7-14
Ag	2.23	4.87	7.90	11.3	28	7-14
Cd	2.14	4.67	7.58	10.9	20	5-10
Ta	1.33	2.90	4.71	6.75	33	8-16
Pt	1.23	2.69	4.37	6.26	33	8-16
Au	1.22	2.67	4.32	6.2	36	9-18



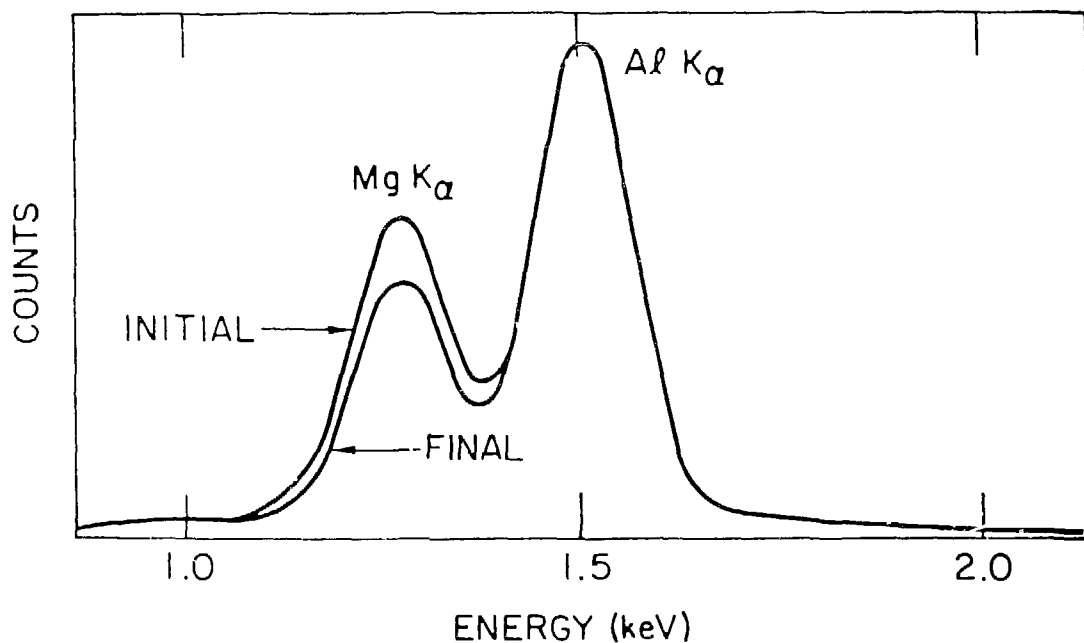
**Figure 1** Sputtering cross-sections for Aluminium, Titanium, Nickel and Niobium as a function of the incident beam accelerating voltage evaluated for  $T_s = T_d/2$ .



**Figure 2** Analyzed region of the Aluminium/Magnesium alloy before (a) and after (b) 4000 sec irradiation. Thinning due to sputtering is readily visible in the micrograph.



**Figure 3** Experimentally measured change in specimen thickness during irradiation, obtained by continuously measuring the relative intensity of the zero loss to inelastic scattering intensity ratio during electron irradiation.



**Figure 4** Experimentally measured x-ray energy dispersive spectra before and after  $\sim 4000$  sec irradiation. Note the change in the relative intensity ratio of Al to Mg K $\alpha$  lines indicating a preferential loss of Mg due to sputtering. The Al K $\alpha$  lines have been normalized to the same value for display purposes.