

CRITICAL CURRENT AND FLUX PINNING

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BY CRYSTAL DEFECTS IN MELT-TEXTURED  $\text{YBa}_2\text{Cu}_3\text{O}_x$ <sup>\*</sup>

(INVITED PRESENTATION)

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# CRITICAL CURRENT AND FLUX PINNING BY CRYSTAL DEFECTS IN MELT-TEXTURED $\text{YBa}_2\text{Cu}_3\text{O}_x$

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## ABSTRACT

Sintered  $\text{YBa}_2\text{Cu}_3\text{O}_x$  bars 50 mm in length have been partially melted to develop highly textured microstructures. The bars exhibited large magnetic hysteresis and transport  $J_c$  values relative to conventional bulk  $\text{YBa}_2\text{Cu}_3\text{O}_x$ . Transmission electron microscopy observations revealed unique grain boundary features which are likely to be responsible for reduced weak-link effects. A high concentration of dislocations and some  $\text{Y}_2\text{Ba}_2\text{Cu}_3\text{O}_7$  particles were present in sample matrices. After high-temperature annealing, the intragranular  $J_c$  of the melt-textured material was considerably reduced. This reduction in  $J_c$  suggested that crystal defects such as dislocations were responsible for the stronger flux pinning in the melt-textured samples.

## INTRODUCTION

The critical current density ( $J_c$ ) of conventionally sintered bulk  $\text{YBa}_2\text{Cu}_3\text{O}_x$  is too low for most envisioned applications (1,2). In addition, the  $J_c$  values of these forms decreases rapidly in applied magnetic fields (3). The low  $J_c$  values are attributable to effects from high crystal anisotropy, flux creep, and weak-links associated with grain boundaries. Various partial-melting methods have been found to produce  $\text{YBa}_2\text{Cu}_3\text{O}_x$  with large, well-aligned grains; substantial improvements in  $J_c$ , especially in magnetic field, have resulted (3-8). Because many of the melt-textured materials carry so much current, it can be quite difficult to make accurate measurements of transport  $J_c$ .

values. Magnetic hysteresis measurements and the Bean model (9) are, therefore, generally used to calculate  $J_c$  (3-8).

It has not been determined conclusively whether the large, in-field  $J_c$  values of more than  $10^4$  A/cm<sup>2</sup> at 77 K for melt-textured specimens are due to inherent improvements in intragranular  $J_c$  or to enlarged current loops associated with strong linking of grains. In this paper, experimental results of superconducting properties and microstructural characteristics are reported for melted-textured  $\text{YBa}_2\text{Cu}_3\text{O}_x$  bars. Results are compared with those obtained for conventionally sintered bars. Microstructural effects on transport  $J_c$  and magnetic hysteresis are discussed.

## EXPERIMENTS

All specimens were prepared from  $\text{YBa}_2\text{Cu}_3\text{O}_x$  powder synthesized by solid-state reaction of  $\text{Y}_2\text{O}_3$ ,  $\text{BaCO}_3$ , and  $\text{CuO}$ . Well-mixed powders were calcined for 4 h at 800°C in flowing oxygen at a reduced pressure of about  $2.6 \times 10^2$  Pa. The powder was phase-pure by X-ray diffraction and differential thermal analysis (10). Bars were cold-pressed in a 50-mm by 7.6-mm steel die. The bars were placed on  $\text{Al}_2\text{O}_3$  setters and sintered at 985°C in flowing oxygen.

The sintered bars were melt-textured in air in a vertical tube furnace. A thin silver coating was sputtered onto the surfaces of some bars to promote melting. The texturing heat treatment was as follows: rapid insertion into a furnace at 1150°C, hold for 0.2 h, cool in 0.1 h to 1050°C, cool to 950°C at 1°C/h. Subsequent annealing in pure oxygen at 450°C increased the oxygen content to the desired level.

Small portions of a few specimens were crushed in an agate mortar and pestle so that intragranular  $J_c$  could be examined. The specimens were first cooled in liquid nitrogen to minimize formation of dislocations during crushing. Half of the powder from a crushed melt-textured sample was annealed in air for 80 h at 880°C in an

attempt to remove dislocations. The other half was given only an oxygenation anneal. For all powders, the final anneal was at 450°C in oxygen for 4 h. Powder particle sizes were measured from scanning electron microscopy (SEM) photographs.

Small bars for property measurements were cut by diamond saw.  $J_c$ , determined with a voltage criterion of 1  $\mu$ V/cm, was measured by a standard four-terminal method at 77 K. The current and voltage leads were directly soldered to the sample with pure indium. An electromagnet was used to supply a steady applied field up to 1.5 T for the  $J_c$  measurements. The magnetic hysteresis and relaxation data were taken with a commercial superconducting quantum interference device (SQUID) at various temperatures up to 5 T. Transmission electron microscopy (TEM) was performed on a Philips 420 electron microscope.

## RESULTS AND DISCUSSION

Figure 1 shows the microstructure of a melt-textured (MT) sample observed by SEM. Figure 1a, a fracture surface, shows that the superconducting grains are well aligned along the ab plane and that twin boundaries are mostly normal to the grain boundaries. The concentration of  $Y_2BaCuO_5$  (211) is low in the MT samples: back-scattered electron imaging revealed only small amounts of 211 and CuO (Fig. 1b). This is in sharp contrast to previous results for zone-melted samples in which high levels of 211 were observed (3,6-8). This microstructural difference is possibly attributable to differences in cooling conditions and silver addition. The melt-textured samples also exhibit high homogeneity as indicated by magnetization measurements: the MT sample shows a sharp superconducting transition near 90 K (Fig. 2).

Transport  $J_c$  data and characteristics of the low-angle grain boundaries have been reported elsewhere (11). Most of the grain boundaries are well aligned. The angular differences between adjacent

grains are estimated to less than 3°. Transport  $J_c$ , measured by pulsed current, has reached  $4.4 \times 10^4 \text{ A/cm}^2$  at 77 K and 1.8 T. This high  $J_c$  value is comparable to other reports (5-8) and indicates a strong correlation with the observed low-angle grain boundaries.

Magnetization (M) versus applied field (H) data were also obtained to estimate the intragranular  $J_c$  based on the Bean critical-state model. However, owing to difficulties in measuring the size of the induced current loop  $d$ , the magnetization  $J_c$  could not be accurately determined. Thus, a different approach was taken. Small parts of samples were crushed into fine powders to separate the grains. M versus H measurements were performed on these powders. To determine whether the strong pinning in the MT samples is caused by high densities of crystal defects such as dislocations, some of the powder was annealed at 880° for 80 h to remove some of the defects. For comparison, an as-sintered bar was also crushed and measured. All three samples—as melt-textured (MT), melt-textured and high-temperature annealed (MTA), and as-sintered (ST)—received identical annealing in oxygen at 450° for 4 h.

Particle sizes of the powdered samples, as estimated by SEM, exhibited distributions. Average values for each powder were between 5 and 10  $\mu\text{m}$ . It is emphasized that annealing had no effect on particle size and that only relative changes in pinning strength were examined. An average particles size  $d$  was used for estimation of intragranular  $J_c$ . According to the Bean model,  $J_c = 30 \Delta M/d$ , where  $J_c$  is in  $\text{A/cm}^2$ ,  $\Delta M$  is the magnetic hysteresis difference in  $\text{emu/cm}^3$ , and  $d$  is the particle size in cm. It is noted that the  $d$  values obtained by powdering the bulk samples are smaller than the average grain sizes of the bulk samples. This ensures that few grain boundaries are likely to exist within the particles.

Figure 3 shows the calculated  $J_c$  versus H at 10 K up to 4.7 T. The MT sample has the highest  $J_c$  ( $1 \times 10^7 \text{ A/cm}^2$  at 2 T). After the high temperature anneal,  $J_c$  at the same field dropped to  $4 \times 10^6 \text{ A/cm}^2$ . For the as-sintered sample,  $J_c$  is  $6 \times 10^5 \text{ A/cm}^2$  at 2 T. This consistent

decrease in  $J_c$  clearly indicates microstructural differences between samples. Figure 4 is a TEM photograph showing a high density of dislocations in the matrix of a melt-textured bar. It has been reported that stacking-fault-type defects also exist in the melt-textured samples (12). Such crystal defects have rarely been observed in conventionally sintered samples. The origins of these defects is not clear. A possible explanation is that large numbers of dislocations can be generated by a high thermal gradient during partial melting (13). Sintering temperatures,  $\approx 950^\circ\text{C}$ , are usually much lower than the processing temperature,  $\approx 1050^\circ\text{C}$ , of melt texturing.

In Fig. 5, flux pinning force density ( $F_p$ ) is plotted versus reduced field  $h(H/H_{c2})$ . The  $H_{c2}$  value was previously estimated for the polycrystalline  $\text{YBa}_2\text{Cu}_3\text{O}_x$  (14). As proposed by Fietz and Webb (15), the pinning force density  $F_p(h)$  can be expressed as:

$$F_p = (H_{c2})^n (T) f(h),$$

where the pinning function  $f(h)$  is directly related to the specific pinning mechanisms in the system. For all type II superconductors with high upper critical field  $H_{c2}$ , pinning force density has a maximum in the  $F_p$  versus  $h$  plot. Kramer (16) suggested that  $F_p$  contains two competing parts which are related to pinning strength and the plastic shear of the flux-line lattice, respectively. The Kramer model predicts that, as a metallurgical treatment results in fewer and weaker pinning centers in the material, the peak position  $F_{\max}$  shifts to lower values of  $h$  and the corresponding  $F_p$  values increase. Such a peak shift is observed, as shown in Fig. 5, which could be related to the pinning mechanism proposed by Kramer. For an MT sample, the  $F_p$  peak occurs at  $h = 0.012$  and has the highest value of  $250 \times 10^6 \text{ TA/cm}^2$ . After annealing the sample at  $880^\circ\text{C}$  for 80 h, concentrations of crystal defects such as edge dislocations and stacking faults are reduced.  $F_p$  is decreased to  $120 \times 10^6 \text{ TA/cm}^2$  and the peak of  $F_p$  is moved to a higher value  $h \approx 0.04$ .

The above results suggest that the strong flux pinning effects observed in the melt-textured sample are related to the high densities of crystal defects in the sample matrices. Although it has been proposed that oxygen inhomogeneity can cause strong pinning, it should not play an important role in this study since all samples had the same oxygen treatment. The various microstructures in these samples were established through different processing methods, and processing strongly affected critical current densities.

## CONCLUSIONS

A highly textured microstructure was obtained in melt-textured  $\text{YBa}_2\text{Cu}_3\text{O}_x$  bars. The transport  $J_c$  in magnetic fields up to 1.5 T was greatly improved at 77 K. TEM evidence suggests that this enhancement of  $J_c$  may be connected with presence of small-angle grain boundaries. High temperature annealing resulted in considerable reduction in  $J_c$  in the melt-textured sample at 10 K. This indicates that the strong flux pinning effects are due to high densities of crystal defects in the melt-textured samples.

## ACKNOWLEDGMENTS

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## FIGURES

Figure 1. SEM photographs of a melt-textured bar showing (a) secondary-electron image of fracture surface and (b) back-scattered electron image of polished surface; note that little 211 is present.

Figure 2. Magnetization versus temperature at 5 G for melt-textured samples.

Figure 3. Magnetization  $J_c$  versus applied field at 10 K for the powder samples indicated.

Figure 4. TEM micrograph showing edge dislocations in a melt-textured sample; the dislocation density has been estimated to be  $10^{10}/\text{cm}^2$ .

Figure 5. Flux pinning force density versus reduced field ( $h$ ) at 10 K for the samples indicated. The solid lines are a guide for the eye.

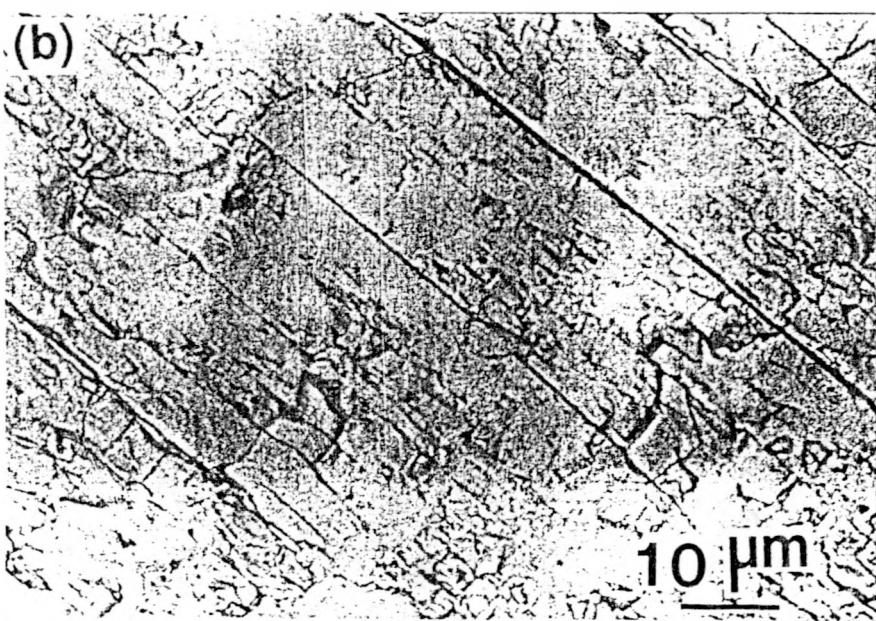
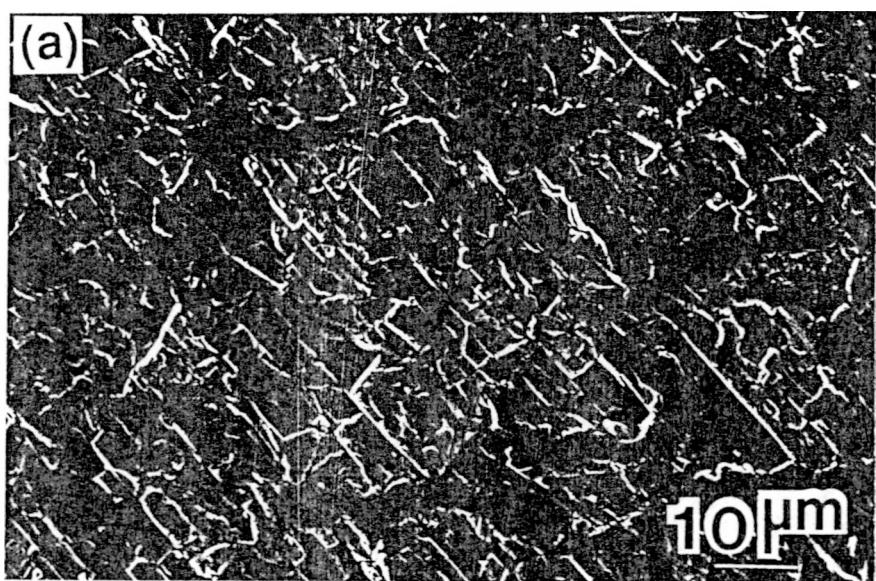


Fig 1

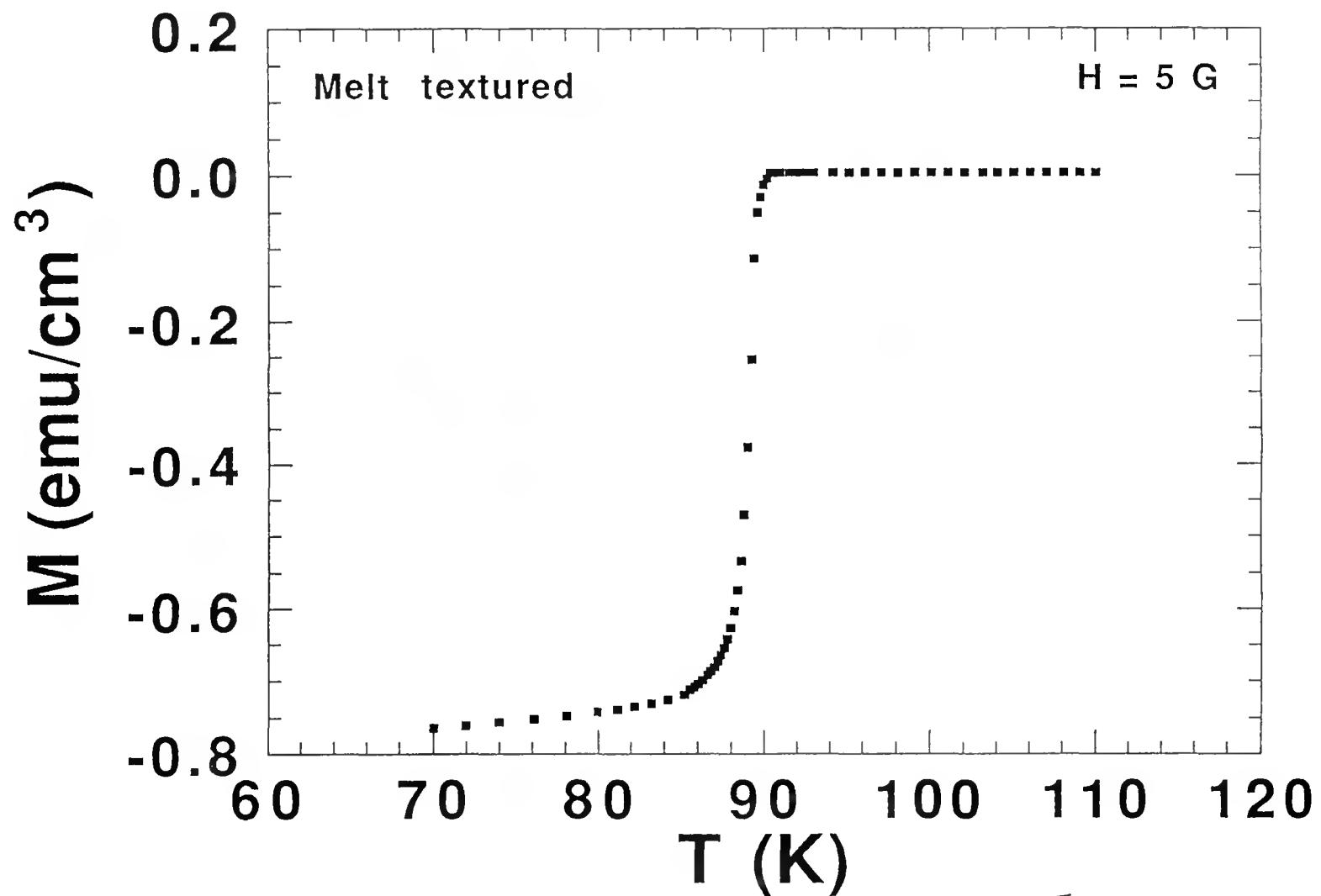


Fig 2

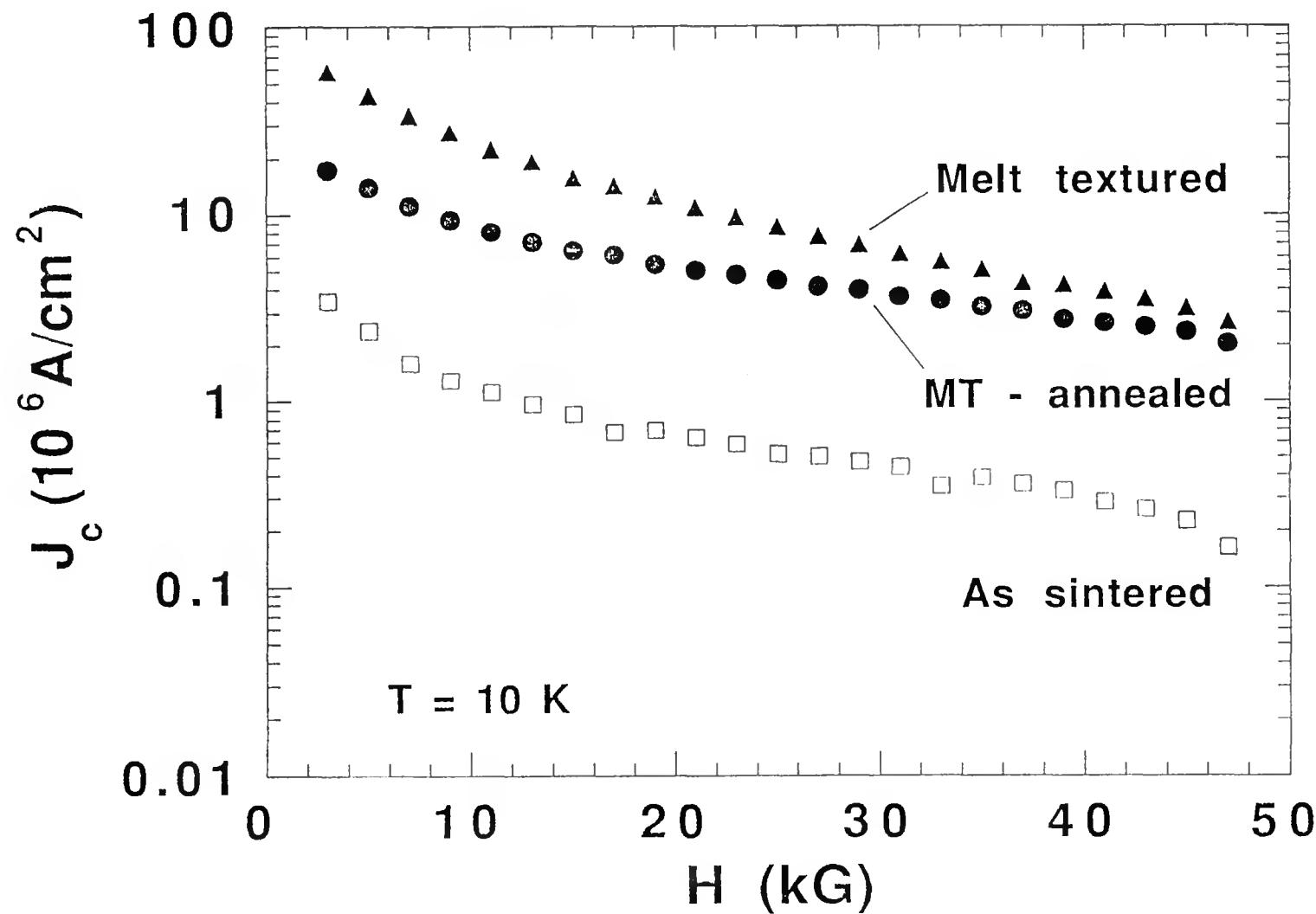


Fig 3

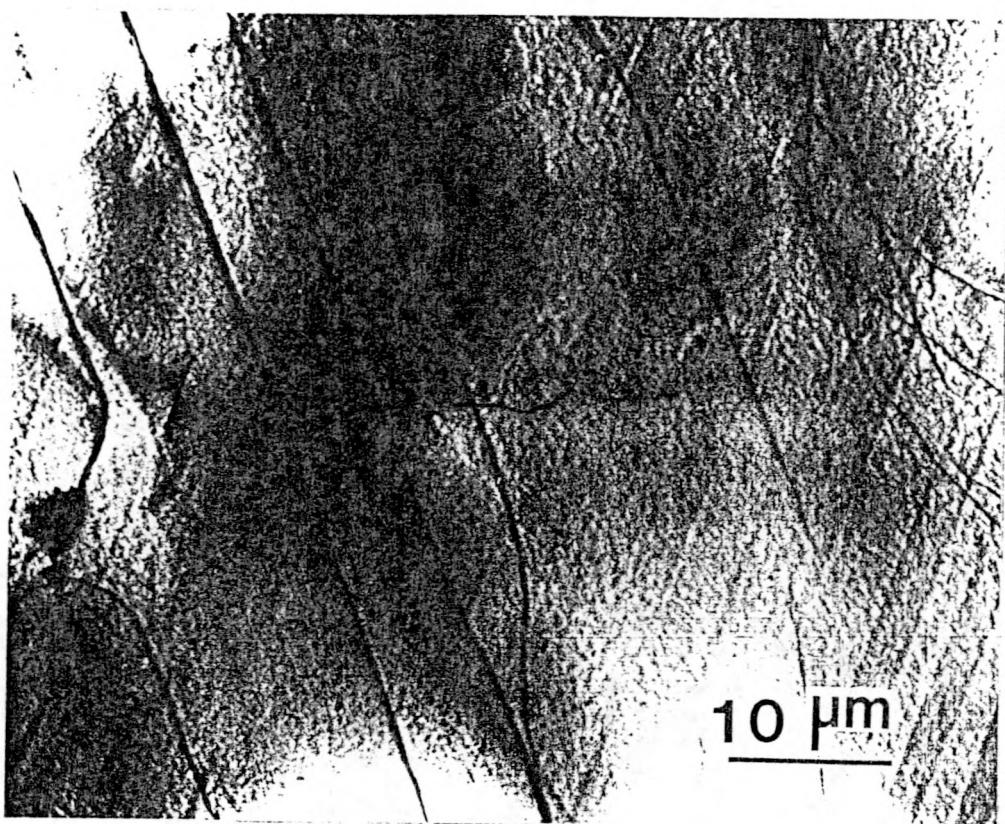


Fig 4

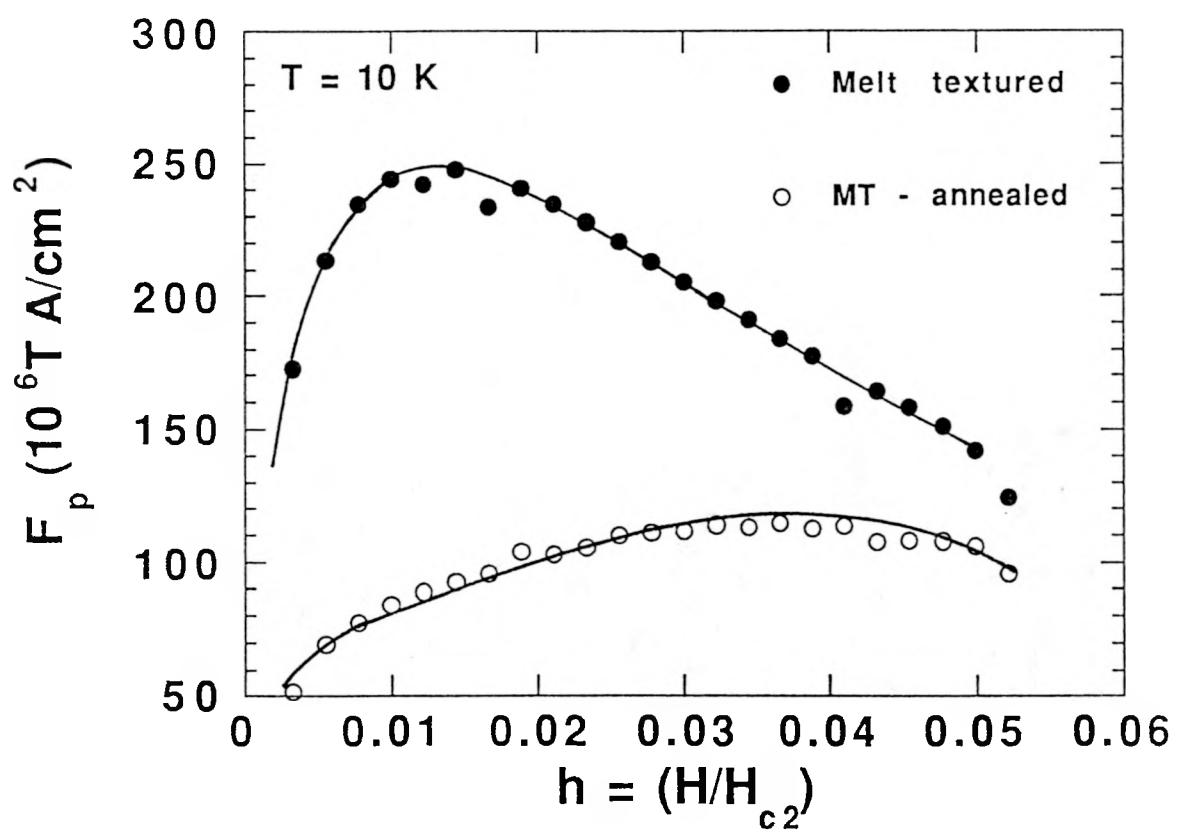


Fig 5