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**LA-7455-MS**

Informal Report

## **Sorption-Desorption Studies on Argillite**

### **I. Initial Studies of Strontium, Technetium, Cesium, Barium, Cerium, and Europium**

**MASTER**

University of California



**LOS ALAMOS SCIENTIFIC LABORATORY**

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LA-7455-MS  
Informal Report  
UC-11 and UC-70  
Issued: March 1979

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**B. R. Erdal  
R. D. Aguilar  
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P. Q. Oliver  
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## SORPTION-DESORPTION STUDIES ON ARGILLITE

### 1. Initial Studies of Strontium, Technetium, Cesium, Barium, Cerium, and Europium

by

B. R. Erdal, R. D. Aguilar, B. P. Bayhurst,  
P. Q. Oliver, and K. Wolfsberg

#### ABSTRACT

Distribution ratios were determined for sorption-desorption of radioactive tracers between Eleana argillite available from the Nevada Test Site and a water prepared to be representative of the natural groundwater composition. The measurements were performed at 22°C and 70°C under atmospheric oxygen conditions. The order of increasing distribution coefficient by element at both temperatures is Tc(VII), Sr, Cs, Ba, Eu, and Ce. The effects of surface area and mineralogy were also investigated.

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#### SUMMARY

The most important barrier to the movement of dissolved radionuclides in geologic systems is retardation due to the interaction between the radionuclides and the geologic medium. This report summarizes initial investigations on the behavior of various radionuclides using Eleana argillite from the Nevada Test Site (NTS).

A batch technique has been developed for all sorption and desorption measurements. One-gram quantities of the crushed and sieved rock were pre-equilibrated for a minimum of 2 weeks with a water having a composition similar to the natural water. The spiked water was prepared by a similar pre-equilibration with ground but unsieved material. The evaporated radionuclides were then dissolved in this pre-equilibrated water. Twenty-ml portions of the spiked water were shaken with the pre-equilibrated rock for various contact times, the mixture was separated by four separate centrifugations at 16 000 rpm, and the solution was assayed for radioactivity. Due to the removal of some radionuclides by the container in which the measurements were performed, it was

necessary to sample all or part of the solid fraction in order to obtain accurate values. Techniques and calculational methods were developed for this purpose. The residue from the sorption measurements were employed for the desorption experiments using the same technique.

Various particle sizes ranging from 106 to 850  $\mu\text{m}$ , and both ambient and elevated ( $70^\circ\text{C}$ ) temperatures were used. Changes in the sorption-desorption behavior with time were examined for intervals of 1, 2, 4, and 8 weeks. The elements studied were Sr, Tc(VII), Cs, Ba, Ce(III), Eu(III), U(VI), Pu, and Am. The measurements were performed under atmospheric oxygen conditions.

The sorption ratio ( $R_d$  = activity per g of solid/activity per ml of water) increases slowly with time presumably due to the slow interaction of the rock surface with the groundwater. Surface alteration presumably is also the reason for the observation that it is more difficult to remove Cs, Sr, Ba, Ce, and Eu from the rock than it was to sorb these elements (desorption ratio greater than sorption ratio). Because there was little change in the surface area for the various particle size fractions studied, the sorption ratios did not vary strongly with particle size. The sorption ratio for Cs did not change with temperature, while the  $R_d$  values for Sr and Ba increased with increasing temperature and those for Ce and Eu decreased. Tc(VII) did not sorb appreciably.

## I. INTRODUCTION

A major requirement for the evaluation of the long-term safety of nuclear waste disposal in a geologic storage environment is a thorough understanding of the mechanisms and phenomenology of the sorption-desorption behavior of the various radionuclides that are biologically hazardous. This knowledge will help in the prediction of the fate of the radionuclides during the length of time required for radioactive decay to reduce the waste to safe levels.

This report presents the results of laboratory investigations of the sorption behavior of various radionuclides with the Eleana argillite found at the Nevada Test Site (NTS). The investigation was intended to satisfy two functions. First, site specific information on this medium was needed in order to help make a decision as to the feasibility of using the Eleana formation as a waste repository. Second, this work contributes to the large general data base of sorption information for a variety of representative geologic media.

The parameter most commonly used for describing equilibrium sorption-desorption ion-exchange reactions is the distribution coefficient,  $K_d$  (see for example, Ref. 1). The  $K_d$  is defined as the concentration per gram of a species on a solid phase divided by its concentration per ml in the liquid phase at equilibrium. This parameter currently is being used to describe the behavior of radionuclides in geologic systems (see, for example, Refs. 2-4) even though equilibrium may not have been established.

## II. GEOLOGIC MATERIAL PROPERTIES

### A. Mineralogy

Four different samples of the Eleana argillite were obtained from hole UE17e at the Nevada Test Site by A. R. Lappin, Sandia Laboratories, Albuquerque (SLA). The samples had all been wrapped in aluminum foil and waxed when they were originally taken. The depths from which they were removed were 121.8-122.2 m, 364.8-365.2 m, 548.2-548.4 m, and 717.2-717.3 m. They were labelled CN3, CN4, CN1, and CN2, respectively. Thin sections of this material were prepared and examined by optical microscopy to determine grain size and original mineralogy. The following were obtained by R. M. Vidale, Los Alamos Scientific Laboratory (LASL).

<u>Major minerals - detrital</u>	<u>Approx. Average Grain Diameter</u>
Quartz - angular, detrital in appearance	0.01 mm

Major minerals - metamorphic

These are very fine grained and approach  
the limit of microscope resolution

0.001 mm

Sericite

Chlorite, Opaques

Probable albite

Carbonate (siderite)

Pyrophyllite (by x-ray powder diffraction)

Opaques

After unwrapping the samples, CN1 and CN2 were reduced in size with hammers, with a Braun Chipmunk apparatus, and finally with a pulverizer having the plates set to produce a maximum grain size of about 1 mm. Each material was graded by use of Tyler sieves (ASTM E-11 specification) into the following size fractions: > 850  $\mu\text{m}$ , 500-850  $\mu\text{m}$ , 355-500  $\mu\text{m}$ , 250-355  $\mu\text{m}$ , 180-250  $\mu\text{m}$ , 150-180  $\mu\text{m}$ , 106-150  $\mu\text{m}$ , and < 106  $\mu\text{m}$ .

The 106-150  $\mu\text{m}$  and 355-500  $\mu\text{m}$  fractions of samples CN1 and CN2 were selected for subsequent use in some of the sorption studies. The fractions were washed briefly with deionized water to remove dust, and they were then dried in air, pumped in a vacuum desiccator containing Drierite for one hour, and dried in the desiccator for two days.

About 100 g of each of the original samples (CSI-4) were also pulverized in a ball mill, using tool-steel components, until the entire quantity passed through a 75- $\mu\text{m}$  sieve. They were then washed and dried as above.

A fourth set of samples was prepared by simply taking a few pieces of the original sample from the Braun Chipmunk from cores CN3 and CN4. These pieces, which had an approximate diameter of 2-5 mm, were simply washed and dried as before. These are hereafter named "chunk" samples.

A petrographic description of the fractions from one core is given in Table I (as determined by J. R. Smyth, LASL).

B. Cation Exchange Capacity

The cation exchange capacity (CEC) of each of the 106-150  $\mu\text{m}$  and 355-500  $\mu\text{m}$  fractions selected for study was measured using both cesium and strontium. The measurement was made<sup>5</sup> by shaking weighed 100-mg portions of the solids

TABLE I  
PETROGRAPHIC ANALYSIS OF CN1 FRACTIONS

	Percent in Sieve Fraction ( $\mu\text{m}$ )		
	106-150	250-355	355-500
Detrital Quartz	32	28	25
Other Detrital	2	3	4
Hematite	6	5	9
Clay Groundmass	60	64	62

with 20 mL of  $\approx 0.5$  M CsCl (pH=8.2) or  $\approx 0.5$  M SrAc<sub>2</sub> (pH=8.5) in deionized water for 8-14 days. The solutions were spiked with <sup>137</sup>Cs and <sup>85</sup>Sr, respectively, and the cation concentrations were determined by atomic absorption spectrophotometry. After the appropriate contact time, the phases were separated by centrifugation, the solids were washed briefly with water, and they were counted with a NaI(Tl) detector to ascertain the amount of strontium or cesium that had exchanged. The results from these measurements are given in Table II. The values indicate that samples from CN1 have a higher CEC than those from CN2. The CEC values determined using strontium tend to be higher than those obtained from cesium. However, due to the uncertainties in the technique, the differences may not be significant.

### C. Size Distribution Analysis

The size distributions of the particles in the selected fractions were measured by screening techniques by R. E. Honnella, LASL. For the range data, the sizes of the smallest screens through which 100% of the material passed were not recorded. However, the screen size listed in Table II as the upper bound for each sample is the size immediately larger than the size recorded as having collected the largest particles in a sample. The median values in Table II were calculated by linear interpolation between screen size data that most closely bracketed the median mass. Similarly, the upper and lower quartile values were calculated by linear interpolation between the screen data that immediately bracketed the 75% and 25% mass values, respectively. The semi-interquartile range as defined by Cramer<sup>6</sup> is a measure of the dispersion of the particle size distribution.

TABLE II  
CATION EXCHANGE CAPACITY AND SIEVE ANALYSIS

<u>Sample</u>	<u>Mesh Size (<math>\mu\text{m}</math>)</u>	<u>Cation Exchange Capacity (meg/100g)</u>		<u>Particle Size Distribution (<math>\mu\text{m}</math>)</u>		
		<u>Cs</u>	<u>Sr</u>	<u>Range</u>	<u>Median</u>	<u>Semi-inter- Quartile Range</u>
CN1	106-150	14	17	75-177	107	12
	355-500	14	16	300-595	415	39
CN1*	106-150			45-210	122	16
	355-500			250-595	426	38
CN2	106-150	8	10			
	106-150	8	10			

\*These samples were not treated by the washing and drying procedure before use; they were simply dried in the vacuum desiccator.

#### D. Surface Area

The surface area of the fractions has been determined by two different techniques, the BET method<sup>7</sup> and the ethylene glycol method.<sup>8-10</sup> The values are summarized in Table III. The BET method employed nitrogen as the absorbate. A portion of the ground and pulverized 106-150  $\mu\text{m}$  unwashed material from CN1 was also used as an intercomparison of BET values determined at LASL and Sandia (A. W. Lynch and R. G. Dosch) laboratories. The values were 12.5 and 9.9  $\text{m}^2/\text{g}$  from LASL and 10.2 and 9.1 from SLA, which indicates satisfactory agreement. Briefly the equilibrium ethylene glycol procedure<sup>8,9</sup> consists of wetting a dried and weighed sample of calcium saturated material with glycol. This is then followed by equilibration in an evacuated desiccator containing an anhydrous calcium chloride-ethylene glycol solvate. The equilibration is repeated until the weights become constant. This presumably indicates that only a monolayer remains. The results obtained using the standard procedure are shown in the fourth column of Table III.

TABLE III  
SURFACE AREA ( $\text{m}^2/\text{g}$ ) MEASUREMENTS

<u>Sample</u>	<u>Mesh Size (<math>\mu\text{m}</math>)</u>	<u>BET</u>	<u>Ethylene Glycol</u>	
			<u><math>\text{CaCl}_2</math> Pretreatment</u>	<u>No <math>\text{CaCl}_2</math> Pretreatment</u>
CN1	106-150	5.22	50,47	53
	355-500	7.61	45,64	~ 57
CN1*	106-150	12.5	51,48	
	355-500	9.9	64,49	
CN2	< 75		75	

\*These samples were not treated by the washing and drying procedure before use; they were simply dried in the vacuum desiccator.

The equilibrium ethylene glycol method<sup>8,9</sup> requires that the samples be saturated with calcium prior to treatment with the glycol. This is needed in order to make the systems homionic.<sup>10</sup> In order to verify this requirement, some surface areas were also determined without this pretreatment. This was also done to see if the prior treatment had degraded the samples. These data (see Table III) would seem to indicate that the pretreatment is necessary for argillite samples. This is not surprising since the clay content in the argillite is significant.

#### E. Groundwater Properties

The water used in these studies was made up in the laboratory to simulate the composition of a natural groundwater from hole UE16d at the NTS. The natural water composition represents an average sample taken by A. R. Lappin, SLA, from the depth interval 24.7-645.9 m. This water is not strictly an Eleana water since virtually all of the production was from the Tippipah formation and only a small amount of production was from the uppermost quartzites within the Eleana argillite in this hole. This water is therefore representative of waters that would enter the Eleana from above. The analysis of this water was performed

by R. L. McAvay, U. S. Geological Survey (see Table IV).

The composition of this natural water was simulated in the laboratory according to a prescription developed by Dosch, SLA. In this procedure, 187.1 mg  $\text{CaCO}_3$ , 32 mg  $\text{MgCO}_3$  was dissolved in 800 ml deionized water saturated with carbon dioxide. Then 1 ml NaF solution (1.26 mg/ml), 1.347 g  $\text{Na}_2\text{SiO}_3 \cdot 5\text{H}_2\text{O}$ , and 0.35 g  $\text{H}_2\text{SiO}_3$  were dissolved in 20 ml deionized water, and 10 ml was added to the first solution. Similarly, 50 ml of a solution containing KCl (0.25 mg/ml),  $\text{CaCl}_2$  (0.22 mg/ml), and  $\text{MgSO}_4$  (1.56 mg/ml) was added to the first solution, as were 1 ml  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$  solution (0.14 mg/ml), and 1 ml  $\text{SrCl}_2 \cdot 6\text{H}_2\text{O}$  solution (1.28 mg/ml). The solution was then diluted to 1.0 l with deionized water, followed by sparging with carbon dioxide for at least 12 h. After sparging the solution with nitrogen until a pH of about 8 was reached, it was allowed to air-equilibrate for at least one week prior to use. The typical atmospheric pressure at Los Alamos is  $\sim 580$  mm Hg.

Rock pre-equilibrated water was used in all the sorption measurements given in this report. This was prepared by contacting batches of the "synthetic" water with ground material that had not been sieved. The contact time was at least two weeks with a solution volume to solid ratio of 20 ml/g. The phases were separated by centrifugation at 7000 rpm followed by filtration through a 0.45  $\mu\text{m}$  Nuclepore filter paper. This procedure was used for preparation of waters pre-equilibrated at ambient temperature ( $22 \pm 2^\circ\text{C}$ ) and at elevated temperature ( $70 \pm 1^\circ\text{C}$ ). The same rock phase with fresh "artificial" water was used in all subsequent batches. Table IV summarizes the results of atomic absorption spectrophotometric analysis of these waters. The composition of the  $70^\circ\text{C}$  waters may be approaching steady state, but this is not true for the  $20^\circ\text{C}$  waters. Selected batches of these waters were also sent to the U. S. Geological Survey (R. L. McAvay) for analysis and these results are given in Table V. The pH of each of the waters was measured using glass electrodes, and standard reference electrodes.

### III. SORPTION OF STRONTIUM, CESIUM, BARIUM, CERIUM, AND EUPOPIUM

#### A. Measurement Techniques

##### 1. Preparation of Tagged Solutions

All traced waters used in these studies were prepared using the pre-equilibrated waters described previously and the following commercially available carrier-free or high specific activity radionuclides:  $^{85}\text{Sr}$ ,  $^{137}\text{Cs}$ ,  $^{133}\text{Ba}$ ,

TABLE IV  
ANALYSIS OF WATERS BY ATOMIC ABSORPTION SPECTROPHOTOMETRY

Constituent	USGS <sup>°</sup>	Lab <sup>*</sup>	(mg/l)											
			Batch 1		Batch 2		Batch 3		Batch 4		Batch 5			
			20°C**	70°C	20°C	70°C	20°C	70°C	20°C	70°C	20°C**	70°C		
Ca	79	70.8	15.1	19.6	15.5	16.6	23.4	23.1	22.3	19.7	17.6	19.6		
Mg	25	23.7	9.0	9.2	22.8	19.2	24.5	26.8	23.7	22.1	10.3	19.5		
K	6.6	7.6	7.9	8.1	8.0	7.8	6.9	6.7	6.3	6.1	6.9	5.9		
Si	31	43.4	3.3	5.8	8.8	5.6	12.9	10.5	22.5	15.3	6.4	13.7		
Na	30	28.5	85.1	83.4	44.1	55.5	33.3	36.1	31.1	31.1	85.5	29.9		
Fe	0.030													
Sr	0.420													
Cl	13													
F	0.6													
SO <sub>4</sub>	62													

<sup>°</sup>Composition of water obtained in the field (R. L. McAvay, USGS).

<sup>\*</sup>Composition before equilibration

<sup>\*\*</sup>Started with a fresh portion of rock

TABLE V  
USGS WATER ANALYSES

	Batch 4		Batch 5
	22°C	70°C (mg/ℓ)	22°C
Barium (Ba)	0.3	0.3	0.3
Calcium (Ca)	38	21	18
Iron (Fe)	0.02	0.02	0.02
Lithium (Li)	0.01	0.01	0.02
Magnesium (Mg)	23	21	9.8
Potassium (K)	6.9	6.6	7.7
Silicon (Si)	16	11	4.3
Sodium (Na)	32	33	96
Strontium (Sr)	0.60	0.40	0.57
Bicarbonate	190	130	260
Carbonate	0	0	0
Chloride	15	15	15
Fluoride	0.7	0.6	0.9
Sulfate	70	78	74
		(meq/ℓ)	
Total Cations	5.357	4.380	6.077
Total Anions	5.031	4.209	6.273

<sup>141</sup>Ce, and <sup>152</sup>Eu. The concentrations for these tracers are given in Table VI. The specific activities given are those provided by the manufacturer. The activities ( $\mu\text{Ci}/\text{mL}$ ) were measured on a calibrated Ge(Li) detector system (see below). The element concentrations given in Table VI only include that consciously added with the tracer. The appropriate volumes of tracers needed for a set of measurements were evaporated to dryness in a washed polyethylene tube overnight on a steam bath. Concentrated hydrochloric acid was added, and the mixture was taken dry again in order to convert the salts to chlorides. The appropriate volume of pre-equilibrated groundwater was added, and the mixture was stirred for  $\sim 24$  h. The mixture was centrifuged for one hour at 16 000 rpm, followed by filtration through a 0.45- $\mu\text{m}$  Nuclepore filter paper. The resulting tracer solution was used for the sorption measurements within about 0.5 day. An aliquot of the final solution was also removed for assay of the initial activity of each of the tracers in the solution. This aliquot was acidified with hydrochloric acid before assaying in order to stabilize the solution. The density of the final solution was also measured. During the tracer preparation, no cesium, strontium, or barium was lost, but about 50% of the cerium and europium was lost onto the filter paper.

One should note that the pre-equilibrated water itself may have considerable concentration of the carriers for each of these tracers. This concentration will be measured in the future when neutron activation analyses are made on each of the batches of water used in this study.

## 2. Sorption Measurements

Batch sorption experiments were performed by shaking weighed one-gram quantities of the crushed rock with 20 mL untraced pre-equilibrated water for a period of about two weeks. The samples were contained in stoppered 40 mL polyethylene centrifuge tubes at ambient temperature or in sealed polypropylene tubes at elevated temperature. All tubes were washed with deionized water prior to use. The phase were then separated by centrifuging at 16 000 rpm for one hour. The weight of the wash solution remaining with the solid phase was obtained by weighing the tube and solid before and after the pre-equilibration. A 20-mL volume of the tagged pre-equilibrated water was then added to the tube, the solid sample was dispersed with vigorous shaking, and the mixture was agitated gently for a given time. Typically, 1, 2, 4, and 8

TABLE VI  
ELEMENT CONCENTRATIONS

Tracer	Tracer		Traced Water	
	Specific Activity (mCi/g)*	Activity ( $\mu$ Ci/ml)	Concentration ( $\mu$ l/ml)	Element Concentration (molar)
$^{85}\text{Sr}$	300	21	1.5	$1.2 \times 10^{-6}$
$^{137}\text{Cs}$	CF	34	0.5	$1.4 \times 10^{-9}$
$^{133}\text{Ba}$	8120	51	0.3	$2.4 \times 10^{-8}$
$^{141}\text{Ce}$	600	110	1.	$1.3 \times 10^{-6}$
$^{152}\text{Eu}$	2638	32	1.	$8.0 \times 10^{-8}$

\* CF means carrier-free.

week contact times were used. The shaking rates were 200 oscillations per minute for the ambient temperature studies, and 80 oscillations per minute for the 70°C samples. A water bath shaker was used for the latter studies. At the end of the shaking period, the aqueous phase was separated from the solids by four centrifugings, each in a new polyethylene centrifuge tube, for one hour at 16 000 rpm. An aliquot of the final solution was then removed and placed in a standard scintillation counting polyvial. This solution was acidified with hydrochloric acid, and it was then assayed for the remaining activities. The pH of the solutions before and after contact with the rock were also recorded.

All solutions remaining from the sorption measurements, including the solution used for radioactivity assay, have been stored for future measurement of the final concentration of the major cations in these solutions. The procedures for these analyses are currently being developed on a Spectrametrics, Inc., model 3 spectrograph.

The same sorption procedure was also performed using a tube that did not have a solid phase present. This "control" sample was used to indicate if any of the radionuclides were likely to be removed by the container. In all cases (see below), the cesium, remained completely in solution. However, this was not

the case for barium, cerium, and europium, and for strontium at 70°C. It was felt that the amount of sorption on the container would vary, depending on whether or not solid material was present, since elements appear to adsorb on any available surface. Therefore, the presence of a solid phase would tend to reduce the fraction of the activity adsorbed on the container. This effect would be especially large when crushed rock solid phase are used since they have an appreciable surface area (see Table III).

In order to determine the amount of activity remaining with the solid phase, whether due to sorption, precipitation, centrifugation of a colloid with the solid, or by some other mechanism, a fraction (~ 25%) of the solid was removed for radioactivity assay. The solid phase was well mixed prior to removal of the fraction. The fraction of the solid removed was determined from the activity of  $^{137}\text{Cs}$  in the solid aliquot, in the solution, and in the initial activity. This method is reasonable since cesium did not adsorb on the container walls. A check was made by weighing the tube before and after removing the sample. Of course, the limitation in this method is how representative the fraction remained is of the entire solid.

The two selected sieve fractions from cores CN1 and CN2 were used for studies at ambient ( $22 \pm 2^\circ\text{C}$ ) and elevated ( $70 \pm 1^\circ\text{C}$ ) temperatures. The waters from the first pre-equilibration (Table IV) were used.

The  $< 75\text{-}\mu\text{m}$  samples from all four cores (CN1-CN4) and the chunk samples from CN3 and CN4 were treated in a similar manner using waters from the second pre-equilibration (Table IV).

### 3. Desorption Measurements

Desorption measurements were made for all samples previously used for the sorption measurements, except for the eight week sorption samples. The assay of activity on the solid sample was done as described earlier. A 15-ml volume of untagged pre-equilibrated water was used for each measurement in order to keep the volume to solid ratio  $\approx 20$ . Contact times of 2, 4, and 8 weeks were used for the 4, 2, and 1 week sorption measurements, respectively. The same procedure was used for separation of the phases and for radioactivity assay as was used in the sorption measurements. This includes the assay of the radioactivity on a fraction of the solid material.

#### 4. Assay of Radioactivity

The solution samples were all counted on a calibrated, 14%, coaxial Ge(Li) detector. An 11% Ge(Li) detector system was used for the solid fractions. The two different detector systems were carefully intercalibrated. The 4096 channel spectra were recorded in multichannel analyzers that are connected to a common PDP-9 computer, where they were analyzed on-line by RAYGUN, our in-house gamma-ray spectroscopy program. This program is designed for use on a minicomputer and it includes spectral interpretation. Its operation involves: 1) a search for background and peak (nonbackground) regions; 2) a preliminary peak search in the nonbackground regions; 3) construction of a step function under the peak(s) in each region; 4) construction of an underlying continuum by smoothing the background together with the step functions; 5) a search for peak regions and peaks with stricter criteria; 6) determination of peak positions and areas and correction for photopeak efficiency; if a multiplet is encountered, separation of the peaks by using peak shape information; 7) a search of the appropriate gamma-ray branching ratio library to find those nuclides and gamma-rays that appear to be in the spectrum, eliminating those that are not plausible; 8) set up an interference matrix,  $[A_{ij}]$ , where  $A_{ij}$  = branching ratio for the  $i^{th}$  peak identified corresponding to the  $j^{th}$  nuclide identified; 9) by a least-squares iteration, determine a solution to

$$Y_i = \sum_j A_{ij} X_j$$

where  $Y_i$  = observed intensity of the  $i^{th}$  peak and  $X_j$  = disintegration rate for the  $j^{th}$  nuclide; 10) correction of the disintegration rate observed for each radionuclide at the counting time to a specified time; 11) performance of an error analysis and output of the results in suitable form. A minimum of two counts, separated by at least one day were taken for each sample. The results from the RAYGUN analyses for each count were simply averaged prior to use.

#### 5. Calculations

The equilibrium distribution coefficient,  $K_d$ , for the distribution of activity between two phases is conventionally defined as:

$$K_d = \frac{\text{activity in solid phase per unit mass of solid}}{\text{activity in solution per unit volume of solution}}$$

It is not known whether equilibrium is achieved for the types of measurements reported here. However, the distribution of activities between the phases was measured, and throughout this report the resulting value is called the sorption ratio,  $R_d$ , which is otherwise identical to  $K_d$ , but does not imply equilibrium.

The following equation was used to calculate the sorption ratios for all cesium analyses and for strontium at ambient temperature:

$$R_d = \frac{R \cdot A_f - A_t}{A_f} \cdot \frac{V}{W}, \quad (1)$$

where

$A_f$  = the activity per ml of a given radionuclide in the tagged water (feed) added to the sample

$A_t$  = the activity per ml in the supernatant solution after the required contact time

$W$  = the weight (grams) of solid material used

$V$  = the total final volume of supernatant solution

$R$  = the dilution factor to take into account the residual solution from the wash.

The amount of residual solution ( $V_r$ ) left with the solid material was calculated from the weight increase of the sample plus container ( $g_r$ ) after the prewashed, and the measured density ( $\rho_r$ ) of the solutions used:

$$V_r = g_r / \rho_r.$$

Therefore, for these measurements (20.0 ml spiked water volume)

$$V = 20.0 + V_r$$

and

$$R = 20.0 / (20.0 + V_r).$$

The activities in the control samples were not used in the calculations. However, the results would not be changed since no container effect was observed in these experiments.

The standard deviation for each measurement was obtained from the errors associated with the activity measurements (generally less than 2%), the 3% uncertainty assumed for  $g_r$ , a 0.5 mg uncertainty in  $W$ , and a 0.5% uncertainty in the volumes. The errors were propagated using the rule for change of variables in a moment matrix assuming independence of the variables and using Eq. 1.

For the barium, cerium, and europium cases and the strontium at 70°C, a different calculational method was used. Since a container problem has never been observed for cesium, the sorption ratio for cesium was used as an internal monitor. The activity of the element of interest and of cesium in the solid and liquid samples was measured. The sorption ratio is

$$R_d = \frac{A_s}{A_t} \cdot \frac{V}{W}, \quad (2)$$

where  $A_s$  = activity on the solid. If a ratio of  $R_d$  values is calculated using Eq. 2 one has, after rearrangement,

$$R_{dx} = \frac{\left( \frac{A_{sx}}{A_{sm}} \right)}{\left( \frac{A_{tx}}{A_{tm}} \right)} R_{dm}, \quad (3)$$

where the  $x$  and  $m$  refer to the element of interest and cesium, respectively. This equation was used to calculate sorption ratio for the element of interest since the  $R_d$  for cesium was calculated using Eq. 1, in the same experiment.

The standard deviation was calculated using the same procedure as previously given but with Eq. 3.

For the desorption measurements, the sorption ratio was again calculated assuming that the cesium did not sorb on the container. The activity,  $A_{sm}^0$ , of  $^{137}\text{Cs}$  on the solid at the beginning of a desorption measurement was calculated using

$$A_{sm}^0 = A_m^0 (1-f_m) (1-f_d)$$

where

$A_m^0$  = the initial  $^{137}\text{Cs}$  activity at the beginning of the sorption measurement,

$f_m$  = the fraction of  $^{137}\text{Cs}$  activity remaining in solution after the sorption measurement, and

$f_d$  = the fraction of the solid removed from the sample prior to beginning the desorption measurement.

The cesium sorption ratio was then calculated by

$$R_{dm} = \frac{A_{sm}^0 - A_{tm} \cdot V}{A_{tm} \cdot V} \frac{V}{(1-f_d) W},$$

where

$$V = 15.0 + V_r.$$

The sorption ratios for all other species in the desorption measurement were then calculated using the sorption ratio for cesium and Eq. 3. An error analysis similar to that described earlier was also performed.

### B. Results and Conclusions

The results for the sorption ratio measurements for ambient temperature conditions are given in Tables VII-X, while those obtained at elevated temperature are given in Tables XI-XIV. If no sorption ratio is listed in these tables for a given contact time, this is due to the difficulty of measuring the activity in the solution. This means that either the sorption ratio is too large or that the decay time was too long (particularly important for  $^{141}\text{Ce}$ ). Limits for the  $R_d$  values have not been estimated.

The initial pH values of the tagged pre-equilibrated water used for the measurements involving the 106-150  $\mu\text{m}$  and 355-500  $\mu\text{m}$  fractions from CN1 and CN2 were 8.65 and 8.70 for the ambient and elevated temperature measurements, respectively. The final pH values for these samples are given in Tables XV and XVI. The initial pH values of the tagged pre-equilibrated water used for the measurements for the < 75  $\mu\text{m}$  fractions and the "chunk" samples were  $\approx$  8.6 and 8.63 for the 20°C and 70°C conditions, respectively, and the final pH values for these experiments are given in Tables XVII-XVIII. The tables also include a parameter, L/S, which is simply the ratio of the  $R_d$  value calculated using Eq. 1 (i.e., no correction for container effects) to the  $R_d$  calculated using Eq. 3 (i.e., corrected for container effects). The observation that few of the L/S values are less than one indicates that the sampling of the solid phase was satisfactory for these measurements. Table XIX gives the final pH values for all control samples and also the percentage of the activity of each of the nuclides that remained in solution. The  $R_d$  values are shown graphically in Figs. 1-30.

Equation 1 was used to calculate the sorption ratios for cesium under all conditions employed since the container effect was very low. This equation was

TABLE VII  
SORPTION RATIOS, SAMPLE CN1, AMBIENT TEMPERATURE

Fraction ( $\mu\text{m}$ )	Sorption Time (days)	Desorption Time (days)	Sorption Ratio, $R_d$ (m $\ell$ /g) <sup>*</sup>				
			Cs	Sr	Ba	Ce(III)	Eu(III)
106-150	6.75		590 (2.1)	69.4 (2.6)	413 (3.6)	4410 (4.1)	4340 (4.4)
		55.65	2810 (7.3)	50.0 (6.8)	831 (5.9)		43 400 (8.9)
	13.74		864 (2.3)	76.0 (2.6)	507 (3.9)	8290 (4.7)	6310 (4.4)
		27.61	2130 (7.2)	46.8 (6.3)	732 (5.7)		58 400 (11)
	26.94		992 (2.5)	77.2 (2.4)	629 (4.1)	22 500 (6.2)	18 600 (6.2)
		13.63	2460 (7.3)	49.2 (6.3)	773 (5.8)		121 000 (15)
	55.73		1540 (2.4)	82.8 (2.6)	866 (3.6)	43 100 (9.6)	43 100 (7.0)
355-500	6.74		823 (2.5)	74.2 (2.6)	365 (4.2)	5780 (5.0)	7340 (5.6)
		55.65	2940 (7.2)	48.2 (6.1)	615 (5.5)		159 000 (21)
	13.73		854 (2.4)	74.3 (2.6)	441 (3.9)	6690 (5.0)	4920 (4.4)
		2761	2270 (7.2)	50.9 (6.4)	503 (5.7)		61 000 (12)
	26.94		1090 (2.5)	79.0 (2.4)	661 (4.1)	24 700 (8.2)	20 200 (7.9)
		13.63	2270 (7.2)	48.0 (6.0)	516 (5.6)		61 200 (9.9)
	55.72		2410 (2.5)	80.3 (2.5)	1000 (3.7)	47 900 (12)	49 200 (8.5)

<sup>\*</sup>The values in parentheses are the standard deviations for a single measurement of the  $R_d$  values expressed in percent; these were obtained from the errors associated with the activity measurements and estimated uncertainties for the various parameters entering into the calculation; these estimated uncertainties were propagated using the rule for change of variables in a moment matrix assuming independence of the variables.

TABLE VIII  
SORPTION RATIOS, SAMPLE CN2, AMBIENT TEMPERATURE

Fraction ( $\mu\text{m}$ )	Sorption Time (days)	Desorption Time (days)	Sorption Ratio, $R_d$ (mL/g)*				
			Cs	Sr	Ba	Ce(III)	Eu(III)
106-150	6.74		606 (2.2)	107 (2.5)	773 (3.8)	2860 (4.1)	2250 (3.9)
		55.65	4920 (7.3)	97.3 (6.7)	1770 (6.2)		60 200 (9.6)
	13.70		981 (2.5)	127 (2.4)	1160 (4.1)	3490 (4.4)	2580 (4.1)
		27.61	3020 (7.3)	90.1 (6.8)	1560 (6.3)		67 200 (11)
	26.90		2280 (2.8)	137 (2.3)	2190 (4.7)	55 400 (10)	44 600 (9.7)
		13.63	4070 (7.3)	76.7 (6.3)	1660 (6.1)		
355-500	55.69		2510 (2.7)	147 (2.4)	24 100 (4.1)	71 600 (12)	68 400 (8.7)
		6.70	671 (2.2)	96.9 (2.3)	527 (4.0)	3930 (4.5)	4520 (4.4)
	13.69		4210 (7.3)	73.5 (6.5)	882 (5.9)		89 100 (13)
		27.61	991 (2.5)	111 (2.4)	730 (4.0)	6720 (4.7)	5780 (4.5)
	26.89		3050 (7.3)	84.1 (6.4)	10 000 (6.0)	43 700 (18)	39 000 (11)
		13.63	1320 (2.2)	118 (2.2)	1010 (3.7)	22 300 (5.6)	18 700 (5.2)
	55.68		3560 (7.2)	63.8 (5.6)	860 (5.4)		102 000 (12)
			2570 (2.8)	118 (2.4)	1320 (4.2)	80 200 (19)	50 200 (11)

\* See footnote to Table VII.

TABLE IX  
SORPTION RATIOS, < 75- $\mu$ m FRACTIONS, AMBIENT TEMPERATURE

Core	Sorption Time (days)	Desorption Time (days)	Sorption Ratio, $R_d$ (mL/g)*				
			Cs	Sr	Ba	Ce(III)	Eu(III)
CN1	7.11		2630 (2.6)	163 (2.2)	6490 (4.8)	48 000 (6.2)	39 500 (6.5)
		57.56	3640 (7.2)	208 (6.1)	10 100 (6.0)		116 000 (9.5)
	7.08		2480 (3.2)	169 (2.4)	6770 (5.9)	39 600 (7.2)	32 800 (7.2)
		57.56	4010 (7.3)	218 (6.9)	10 600 (6.7)		101 000 (9.0)
	13.96		2750 (2.5)	177 (2.2)	7410 (4.5)	53 800 (5.8)	47 900 (5.4)
		27.58	3930 (7.3)	212 (6.0)	9920 (6.6)		101 000 (11)
	13.93		2300 (2.7)	191 (2.3)	6460 (5.0)	36 200 (5.8)	30 600 (5.4)
		27.58	3870 (7.3)	215 (6.0)	10 300 (6.3)	129 000 (26)	93 000 (10)
	27.91		2600 (3.2)	220 (2.4)	8310 (6.0)	54 800 (8.0)	46 100 (7.6)
		13.54	3550 (7.3)	222 (5.9)	11 600 (6.3)		158 000 (12)
CN2	27.88		2500 (3.3)	208 (2.5)	8670 (6.5)	90 700 (13)	83 600 (11)
		13.54	3470 (7.2)	225 (11)	9900 (9.9)		109 000 (12)
	56.19		2400 (2.3)	246 (2.1)	9990 (4.3)	127 000 (16)	113 000 (8.6)
	56.17		2430 (2.3)	226 (2.2)	9720 (4.3)	146 000 (22)	97 600 (8.6)
	7.10		805 (2.2)	168 (2.1)	1480 (3.7)	2240 (3.9)	1870 (3.6)
		57.56	3600 (7.2)	206 (6.6)	10 700 (6.4)		118 000 (10)
	13.95		2700 (2.9)	234 (2.3)	7760 (5.4)	19 600 (5.3)	16 100 (4.8)
		27.58	4220 (7.4)	239 (6.4)	11 700 (7.2)		90 400 (12)
CN2	27.90		1850 (2.9)	245 (2.4)	6190 (5.5)	23 300 (6.2)	18 400 (5.4)
		13.54	3610 (7.3)	247 (6.3)	11 700 (6.5)	100 000 (19)	86 900 (8.7)
	56.19		2550 (2.4)	257 (2.1)	11 600 (4.7)	117 000 (15)	88 600 (7.3)

TABLE IX (cont'd)  
SORPTION RATIOS, <75- $\mu$ m FRACTIONS, AMBIENT TEMPERATURE

Core	Sorption Time (days)	Desorption Time (days)	Sorption Ratio, $R_d$ (mL/g)*				
			Cs	Sr	Ba	Ce(III)	Eu(III)
CN3	7.10		2840 (2.7)	147 (22)	4850 (4.7)	34 300 (5.6)	30 500 (5.6)
		57.56	4200 (7.2)	169 (6.4)	7320 (6.1)		94 500 (9.3)
	13.95		2030 (2.6)	147 (2.3)	3390 (4.3)	11 800 (4.6)	10 600 (4.2)
		27.58	4930 (7.4)	167 (6.3)	7340 (6.6)		97 400 (12)
	27.90		2460 (3.2)	162 (2.4)	4260 (5.5)	32 200 (7.2)	20 600 (6.5)
		13.54	3890 (7.3)	167 (6.3)	6760 (6.4)		73 900 (8.7)
CN4	56.18		2940 (2.4)	180 (2.1)	6410 (4.1)	77 000 (12)	82 400 (6.7)
		961 (2.5)	163 (2.4)	1690 (4.5)		3060 (4.5)	2740 (4.3)
	7.09		3400 (7.2)	208 (6.0)	8420 (6.9)		98 100 (8.2)
		57.56	2520 (2.7)	212 (2.3)	6590 (4.9)	15 800 (5.0)	14 500 (4.6)
	13.94		4190 (7.3)	192 (5.4)	8950 (5.8)	84 300 (22)	60 700 (8.0)
		27.58	1840 (2.9)	194 (2.4)	5460 (5.4)	22 800 (9.9)	19 500 (9.3)
CN4	27.90		3310 (7.2)	213 (514)	9780 (5.8)	75 000 (19)	59 100 (12)
		13.54	2440 (2.4)	238 (2.1)	9910 (4.6)	82 900 (13)	83 000 (7.3)

\* See the footnote to Table VII.

TABLE X  
SORPTION RATIOS, CHUCK SAMPLES, AMBIENT TEMPERATURE

Core	Sorption Time (days)	Desorption Time (days)	Sorption Ratio, $R_d$ (mL/g)*			
			Cs	Sr	Ba	Ce(III)
CN3	7.08		2150 (2.6)	53.3 (2.7)	295 (4.2)	35 800 ( 20)
		57.56	8410 (7.3)	47.8 (7.0)	939 (6.1)	
	13.93		3430 (3.8)	56.4 (2.7)	380 (5.7)	155 000 ( 31)
		27.58	7700 (7.4)	46.8 (7.1)	700 (6.3)	113 000 ( 15)
	27.88		2790 (3.3)	56.4 (2.7)	334 (5.0)	
		13.54	6480 (7.3)	53.3 (7.8)	632 (6.8)	
CN4	56.16		4090 (2.7)	56.6 (2.5)	515 (4.1)	
		7.07	521 (2.1)	42.5 (2.9)	212 (3.7)	15 200 (4.6)
	13.92		3540 (7.2)	44.4 (6.2)	580 (5.3)	13 000 (4.3)
		27.58	1090 (2.8)	47.1 (2.9)	279 (4.4)	21 500 (8.2)
	27.88		3990 (7.3)	47.3 (6.4)	3640 (6.1)	19 500 ( 11)
		13.54	1710 (2.5)	46.1 (2.9)	295 (3.9)	
	56.16		3030 (7.2)	44.9 (9.5)	554 (7.7)	
			4970 (2.9)	51.5 (2.5)	565 (4.3)	

\* See the footnote to Table VII.

TABLE XI  
SORPTION RATIOS, SAMPLE CN1, 70°C

Fraction ( $\mu\text{m}$ )	Sorption Time (days)	Desorption Time (days)	Sorption Ratio, $R_d$ (mL/g)*				
			Cs	Sr	Ba	Ce(III)	Eu(III)
106-150	7.06		663 (2.3)	108 (4.4)	1160 (4.0)	3790 (4.5)	4070 (4.0)
		55.65	2000 (7.2)	133 (6.8)	14 500 (7.1)		29 900 (7.6)
	13.87		708 (2.5)	137 (5.3)	2170 (4.8)	1260 (4.9)	1850 (4.4)
		27.65	2430 (7.2)	110 (6.3)	9020 (6.4)	13 900 (19)	18 900 (6.3)
	27.94		879 (2.1)	136 (3.9)	5460 (4.4)	9930 (5.4)	9630 (4.4)
		13.63	1810 (7.2)	131 (5.1)	10 600 (5.7)	17 700 (18)	21 100 (5.5)
	55.80		983 (2.2)	200 (3.9)	8550 (4.2)	1360 (4.2)	2050 (3.4)
		55.65	859 (2.4)	119 (4.4)	1220 (4.0)	5530 (4.5)	5830 (4.0)
355-500	7.05		1870 (7.2)	95.4 (7.0)	12 700 (6.7)	8110 (22)	10 300 (6.4)
		13.86	1080 (2.2)	118 (4.2)	1780 (3.8)	3420 (4.2)	3810 (3.6)
	27.93		2240 (7.2)	82.9 (6.7)	8150 (6.8)	5450 (12)	6050 (6.4)
		13.63	1172 (2.1)	129 (3.8)	4730 (4.2)	4020 (4.2)	3790 (3.6)
	55.84		1880 (7.2)	119 (6.0)	8370 (6.5)	18 000 (15)	24 700 (6.3)
			1250 (2.4)	150 (4.0)	8780 (4.7)	2700 (4.6)	3390 (3.7)

\* See the footnote to Table VII.

TABLE XII  
SORPTION RATIOS, SAMPLE CN2, 70°C

Fraction ( $\mu\text{m}$ )	Sorption Time (days)	Desorption Time (days)	Sorption Ratio, $R_d$ (mL/g)*				
			Cs	Sr	Ba	Ce(III)	Eu(III)
106-150	7.01		1090 (2.5)	172 (4.5)	1390 (4.2)	1270 (5.1)	805 (4.2)
		55.65	2730 (7.2)	114 (6.3)	3040 (5.8)	11 900 (18)	12 000 (5.9)
	13.82		1270 (2.5)	208 (4.5)	2790 (4.4)	1380 (5.1)	1210 (4.4)
		27.65	3540 (7.3)	145 (7.2)	3520 (6.8)	8290 (15)	8390 (6.9)
	27.88		1510 (2.4)	204 (4.2)	3040 (4.2)	1080 (4.8)	1050 (4.0)
		13.63	3100 (7.3)	184 (6.1)	4460 (6.2)		57 700 (7.1)
	55.80		1910 (3.1)	242 (4.9)	5300 (5.8)	15 300 (19)	13 100 (7.4)
		7.00	1210 (2.5)	197 (5.2)	1720 (4.4)	7880 (5.0)	9000 (4.0)
	55.65		2420 (7.2)	85.1 (6.4)	1590 (5.7)	4650 (18)	6500 (5.8)
		13.81	1480 (2.4)	181 (4.3)	1230 (4.1)	2340 (4.8)	2500 (4.2)
	27.65		3620 (7.3)	107 (6.8)	1810 (6.2)		14 500 (6.9)
		27.88	1520 (2.4)	166 (4.4)	1610 (4.1)	1510 (4.6)	1760 (4.0)
	13.63		2740 (7.2)	130 (5.9)	2170 (5.6)		59 500 (6.8)
		55.80	1830 (3.1)	185 (5.1)	2950 (5.1)	5000 (11)	5800 (5.6)

\*See the footnote to Table VII.

TABLE XIII  
SORPTION RATIOS, <75- $\mu\text{m}$  FRACTIONS, 70°C

Core	Sorption Time (days)	Desorption Time (days)	Sorption Ratio, $R_d$ (mL/g)*				
			Cs	Sr	Ba	Ce(III)	Eu(III)
CN1	8.02		1320 (2.2)	420 (4.0)	5460 (4.3)	2100 (4.1)	2320 (3.7)
		57.70	3040 (7.2)	567 (6.6)	58 300 (9.4)		39 500 (6.6)
	17.84		1250 (2.3)	453 (4.3)	17 500 (5.7)	20 500 (5.1)	22 300 (4.7)
		28.56	2360 (7.3)	504 (6.6)	81 900 (15)		95 400 (11)
	33.01		2120 (2.5)	507 (4.1)	31 900 (7.0)	16 500 (6.2)	20 400 (4.9)
		14.60	2070 (7.2)	562 (6.2)	62 700 (11)	40 200 (14)	46 400 (7.2)
CN2	59.94		1780 (2.2)	767 (4.3)	73 700 (10)	66 800 (13)	58 700 (7.1)
		8.02	1810 (2.6)	514 (4.7)	3100 (4.5)	2600 (4.6)	2600 (4.2)
	17.84		4750 (7.3)	423 (8.1)	69 800 (11)		50 000 (8.7)
		28.56	2027 (2.8)	585 (4.9)	12 500 (5.8)	4700 (5.0)	5800 (4.6)
	33.01		3470 (7.3)	430 (7.0)	56 300 (12)	40 800 (24)	92 700 (11)
		14.60	2810 (2.7)	575 (4.5)	34 800 (7.7)	24 500 (7.5)	27 800 (6.0)
	59.94		3140 (7.3)	503 (6.7)	55 600 (11)	49 900 (20)	74 400 (9.3)
			3200 (2.5)	666 (4.5)	52 000 (8.0)	29 000 (9.2)	32 800 (5.3)

TABLE XIII (cont'd)  
SORPTION RATIOS, <75- $\mu$ m FRACTIONS, 70°C

Core	Sorption Time (days)	Desorption Time (days)	Sorption Ratio, $R_d$ (mL/g)*				
			Cs	Sr	Ba	Ce(III)	Eu(III)
CN3	8.02	1970 (3.0)	411 (5.2)	7720 (5.4)	3060 (5.0)	3680 (4.7)	
		57.70	4960 (7.3)	454 (7.1)	63 200 (11)		63 000 (9.4)
	17.83	2250 (2.8)	543 (4.9)	19 600 (6.5)	17 800 (5.8)	19 000 (5.0)	
		28.56	3730 (7.3)	479 (6.0)	44 400 (9.4)		72 000 (12)
	33.01	2990 (2.8)	655 (4.7)	27 300 (6.8)	17 200 (6.1)	20 500 (5.3)	
		14.60	3630 (7.3)	489 (6.8)	38 100 (9.6)	35 300 (16)	41 500 (8.1)
CN4	59.93	4020 (2.7)	881 (4.5)	45 100 (8.1)	32 300 (16)	32 500 (7.8)	
		8.01	1760 (2.9)	369 (5.0)	6360 (5.6)	1900 (4.9)	2090 (4.6)
	17.83	4610 (7.3)	543 (6.7)	10 200 (15)			141 000 (14)
		28.56	1730 (2.6)	439 (5.2)	21 100 (6.7)	8230 (5.6)	10 000 (4.8)
	33.01	3590 (7.4)	527 (6.5)	13 100 (23)			143 000 (15)
		14.60	2490 (2.6)	577 (4.5)	64 300 (10)	72 200 (11)	64 300 (7.2)
	59.93	3020 (7.2)	553 (6.2)	87 100 (12)			105 000 (10)
		3000 (2.5)	882 (4.4)	41 700 (8.2)	21 700 (9.1)	21 800 (5.2)	

\* See the footnote to Table VII.

TABLE XIV  
SORPTION RATIOS, CHUNK SAMPLES, 70°C

Core	Sorption Time (days)	Desorption Time (days)	Sorption Ratio, $R_d$ (mL/g)*				
			Cs	Sr	Ba	Ce(III)	Eu(III)
CN3	8.01	57.70	1610 (2.6)	123 (4.6)	469 (4.2)	806 (4.4)	1630 (4.2)
			3230 (7.3)	104 (6.6)	730 (5.8)		9130 (6.4)
	17.82	28.56	1780 (2.9)	151 (4.8)	654 (4.5)	1130 (5.1)	1750 (4.7)
			2730 (7.3)	100 (6.1)	536 (5.6)	14 500 (16)	14 400 (6.6)
	33.00	14.60	1750 (2.6)	124 (4.1)	1177 (4.0)	2680 (4.9)	6410 (4.6)
			2260 (7.2)	93.0 (6.1)	852 (5.7)	3020 (6.3)	4720 (5.7)
CN4	59.92	8.00	1840 (2.2)	142 (3.6)	1320 (3.4)	2710 (5.0)	5650 (3.9)
			1410 (2.7)	99.2 (4.7)	433 (4.4)	1680 (4.8)	2200 (4.4)
	17.82	57.70	2980 (7.3)	100 (6.7)	2950 (5.9)		9030 (6.3)
			1290 (2.5)	98.9 (4.3)	752 (3.9)	631 (4.4)	1150 (4.1)
	33.00	28.56	2150 (7.3)	86.4 (6.0)	2430 (5.7)	4300 (8.6)	6430 (5.9)
			1440 (2.5)	105 (4.0)	1280 (3.9)	6570 (6.0)	10 600 (5.2)
	59.92	14.60	1960 (7.2)	84.6 (6.3)	1730 (5.8)	2810 (6.9)	4050 (5.8)
			1550 (2.3)	134 (3.7)	2090 (3.7)	6520 (9.2)	11 370 (5.3)

\* See the footnote to Table VII.

TABLE XV  
pH AND L/S VALUES, AMBIENT TEMPERATURE

Core	Fraction ( $\mu\text{m}$ )	Sorption Time (days)	Final pH	L/S			Final Desorption pH
				Ba	Ce	Eu	
CN1	106-150	6.75	8.93	1.02	2.12	2.27	8.58
		13.74	8.88	1.05	1.17	1.16	8.70
		26.94	8.73	1.08	1.03	0.98	8.76
		55.73	9.06	1.01	1.08	1.07	
	355-500	6.74	8.93	1.18	1.41	1.39	8.60
		13.73	8.92	1.03	1.58	1.50	8.76
		26.94	8.83	0.93	1.57	1.48	8.76
		55.72	8.79	0.99	1.19	1.16	
CN2	106-150	6.74	9.02	0.97	1.24	1.17	8.64
		13.70	8.89	1.00	1.44	1.35	8.85
		26.90	8.86	0.86	1.19	1.16	8.81
		55.69	8.82	0.90	1.32	1.28	
	355-500	6.70	8.98	1.03	1.68	1.54	8.68
		13.69	8.93	1.06	1.45	1.37	8.87
		26.89	8.93	1.00	1.24	1.19	8.81
		55.68	9.04	0.98	1.59	1.66	
CN3	Chunk	7.08	8.52	1.04	1.36	1.42	8.66
		13.93	8.56	0.97	1.29	1.25	8.83
		27.88		1.06			8.83
		56.16		1.02			
CN4	Chunk	7.07	8.58	1.09	0.88	0.90	8.63
		13.92	8.56	1.11	1.21	1.24	8.86
		27.88		1.10			8.86
		56.16		1.03			

TABLE XVI  
pH AND L/S VALUES, 70°C

Core	Fraction ( $\mu\text{m}$ )	Sorption Time (days)	Final pH	L/S				Final Desorption pH
				Sr	Ba	Ce	Eu	
CN1	106-150	7.06	8.93	2.10	0.99	0.75	0.78	7.94
		13.87	8.88	2.42	1.04	1.45	1.43	8.02
		27.94	8.79	2.46	1.09	1.35	1.74	8.74
		55.80	8.60	2.33	0.99	1.39	1.45	
	355-500	7.05	8.94	1.98	0.81	0.53	0.55	8.16
		13.86	8.93	2.50	0.96	0.77	0.79	8.59
		27.93	8.83	2.03	1.01	1.05	1.03	8.70
		55.84	8.76	2.24	1.02	1.19	1.21	
CN2	106-150	7.01	8.90	2.12	1.14	3.81	3.92	8.12
		13.82	8.81	2.75	1.06	4.08	4.31	8.36
		27.88	8.67	2.29	1.13	3.77	3.96	8.60
		55.80	8.50	2.24	1.04	2.35	2.37	
	355-500	7.00		2.02	0.59	0.52	0.55	8.08
		13.81	8.84	2.70	1.15	2.48	2.68	8.36
		27.88	8.73	2.45	1.11	1.88	1.96	8.57
		55.80	8.56	2.58	1.13	2.46	2.60	
CN3	Chunk	8.01	8.54	2.75	1.00	1.15	1.22	8.24
		17.82	8.42	2.69	0.93	2.75	2.51	8.28
		33.00	8.62	2.67	0.84	2.43	2.05	8.53
		59.92	8.52	2.64	0.93	3.17	2.80	
CN4	Chunk	8.00	8.54	2.82	1.10	1.23	1.35	8.30
		17.82	8.55	2.97	1.19	5.25	4.39	8.60
		33.00	8.77	2.84	1.09	2.18	1.97	8.57
		59.92	8.63	2.83	1.15	3.71	2.73	

TABLE XVII  
pH AND L/S VALUES, <75- $\mu$ m FRACTIONS, AMBIENT TEMPERATURE

Core	Sorption Time (days)	Final pH	L/S			Final Desorption pH
			Ba	Ce	Eu	
CN1	7.11	8.58	1.02	1.05	1.05	8.54
	7.08	8.64	1.01	1.03	1.03	8.74
	13.96	8.61	0.99	1.01	1.01	8.72
	13.93	8.73	0.96	0.86	0.86	8.91
	27.91	8.81	0.98	0.90	0.91	8.82
	27.88	8.81	1.01	0.91	0.89	8.84
	56.19	8.62	1.00	0.98	0.99	
	56.17	8.71	1.00	0.99	1.00	
CN2	7.10	8.62	1.07	1.24	1.27	8.65
	13.95	8.65	0.93	0.74	0.73	8.86
	27.90	8.82	0.91	0.93	0.95	8.85
	56.19	8.72	1.01	0.98	0.98	
CN3	7.10	8.62	0.99	0.96	0.97	8.66
	13.95	8.59	0.94	0.67	0.66	8.83
	27.90	8.81	0.98	0.87	0.87	8.83
	56.18	8.69	0.97	0.91	0.91	
CN4	7.09	8.61	1.10	1.30	1.33	8.72
	13.94	8.66	0.96	0.83	0.81	8.89
	27.90	8.77	1.00	1.05	1.06	8.86
	56.18	8.71	1.01	1.03	1.03	

TABLE XVIII  
pH AND L/S VALUES <75- $\mu$ m FRACTIONS, 70°C

Core	Sorption Time (days)	Final pH	L/S				Final Desorption pH
			Sr	Bg	Ce	Eu	
CN1	8.02	8.51	2.45	1.23	1.82	1.76	8.64
	17.84	8.61	2.43	1.04	0.93	0.93	8.31
	33.01	8.71	2.42	1.13	1.41	1.35	8.53
	59.94	8.52	2.12	1.00	0.89	1.15	
CN2	8.02	8.54	2.47	1.00	1.34	1.32	8.47
	17.84	8.52	2.52	0.86	1.19	1.17	8.35
	33.01	8.87	2.44	1.08	1.49	1.47	8.44
	59.94	8.52	2.43	1.08	1.17	1.19	
CN3	8.02	8.49	2.71	0.69	0.77	0.72	8.39
	17.83	8.44	2.49	0.81	0.62	0.64	8.26
	33.01	8.64	2.48	0.95	1.24	1.24	8.36
	59.93	8.43	2.34	1.16	1.93	2.56	
CN4	8.01	8.61	2.56	0.94	1.24	1.22	8.26
	17.83	8.61	2.57	0.78	1.07	1.06	8.08
	33.01	8.78	2.50	0.88	0.98	0.97	8.38
	59.93	8.48	2.36	1.25	1.63	1.68	

TABLE XIX  
PERCENT RECOVERY AND pH VALUES FOR CONTROL SAMPLES

Temp. (°C)	Batch Number of the water*	Contact Time (days)	Final pH	Percent Remaining in Solution				
				Cs	Sr	Ba	Ce	Eu
20	1	6.73		102	102	101	8.80	71.9
		13.73	8.91	98.6	98.6	98.3	8.39	67.3
		26.89	8.95	99.5	98.8	98.9	5.86	61.8
		55.68	9.01	97.9	98.3	96.9	4.47	48.5
	2	7.11		99.8	99.4	101	51.9	82.2
		13.86		102	93.4	89.2	5.34	6.27
		27.82	8.81	103	86.9	76.1	8.87	7.50
		56.11	8.82	106	90.2	80.7	1.54	0.24
70	1	7.00		99.9	75.8	80.0	2.50	2.21
		13.81	8.95	100	56.4	62.1	5.50	11.2
		27.88	8.97	100	31.2	42.4	0.28	0.62
		55.79	8.96	97.0	22.2	33.7	0.17	0.08
	2	8.00	8.59	102	84.3	85.4	0.26	0.54
		17.81	8.52	99.9	61.0	70.4	0.02	0.10
		32.99	8.72	99.8	34.6	52.1		

\* See Table IV.

also used for strontium under ambient conditions. However, Eq. 3 was used for all other calculations since the container effect on these cations was significant (Table XIX).

Upon examination of Tables VII-XIV one can make several general observations. The scatter in the sorption ratios is sometimes larger than the quoted experimental uncertainties, assuming that one could expect a constant or monotonic behavior with time. This indicates that strictly identical samples or conditions were not always attained. The  $R_d$  values for most species increase with time. This could be due to alteration of the minerals even at the rather low temperatures involved in these measurements or to relatively slow ion exchange.

Steady state seems to be attained more quickly at the higher temperatures, at least for cesium, strontium, and barium. Essentially the same  $R_d$  value is obtained at the two temperatures for each of these three cations. The sorption ratios for cerium and europium seem to vary inversely with temperature. Presumably the cerium and europium are more soluble at the higher temperature since they have the tendency to form hydroxides in the pH  $\approx 8$  solutions used.

There does not seem to be a strong correlation between the sorption capability of the material and the depth at which the samples were taken. There are indications that CN1 is a poorer sorber than CN2 for the cations studied, but the differences are small. The cation exchange capacity of CN1 is somewhat higher than that of CN2 (see Table II). This indicates that, as expected, the Eleana argillite is rather uniform in its geologic character.

At least qualitatively, an increase in the surface area is accompanied by an increase in the sorption ratio. However, the changes are not very large since the surface area did not change strongly with sieve fraction. Therefore, the differences observed may be due entirely to other factors, such as the differences in the mineral composition of the sieve fractions. Since the permeability of the argillite is low, it is not surprising that the  $R_d$  values for the chunk samples are significantly different than those obtained from the ground samples.

The agreement between the late time sorption and desorption  $R_d$  values is usually rather good. However, some desorption values are significantly greater (see the Ce and Eu data) than those reached by sorption. One can speculate that the observation may be a consequence of the following phenomena. The solution from which sorption takes place may contain different species of the

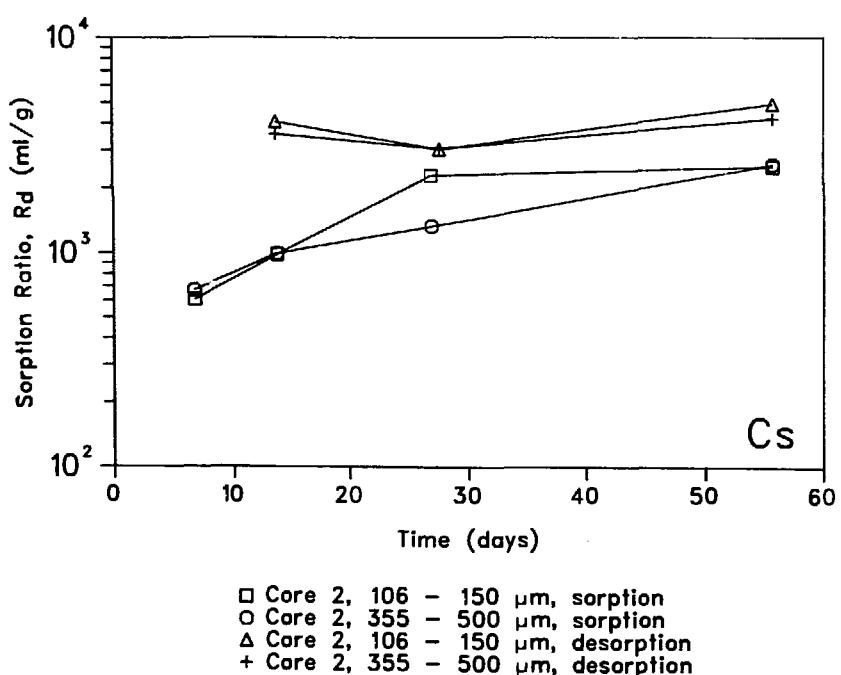
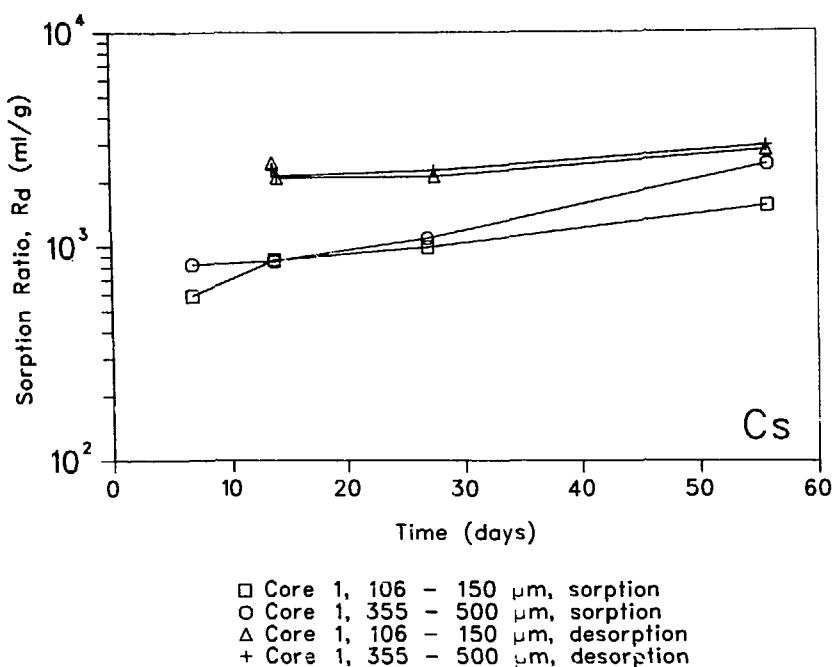


Fig. 1. Cesium sorption-desorption ratio data, selected sieve fractions, ambient temperature.

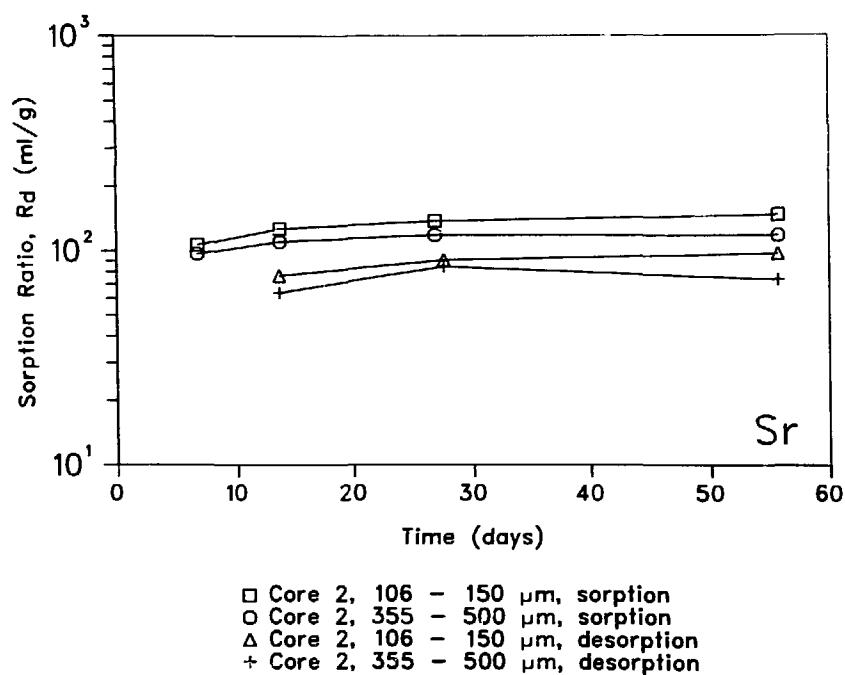
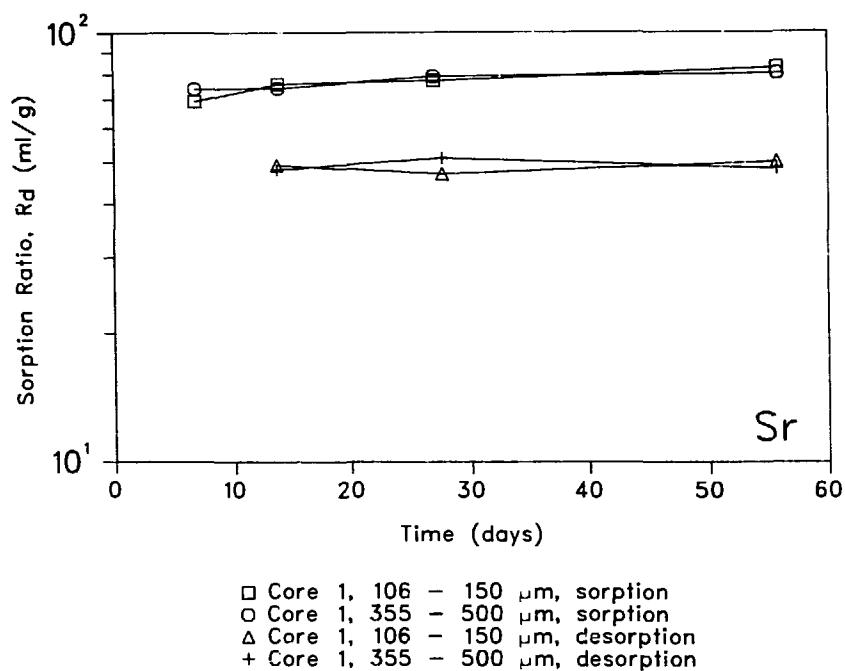


Fig. 2. Strontium sorption-desorption ratio data, selected sieve fractions, ambient temperature

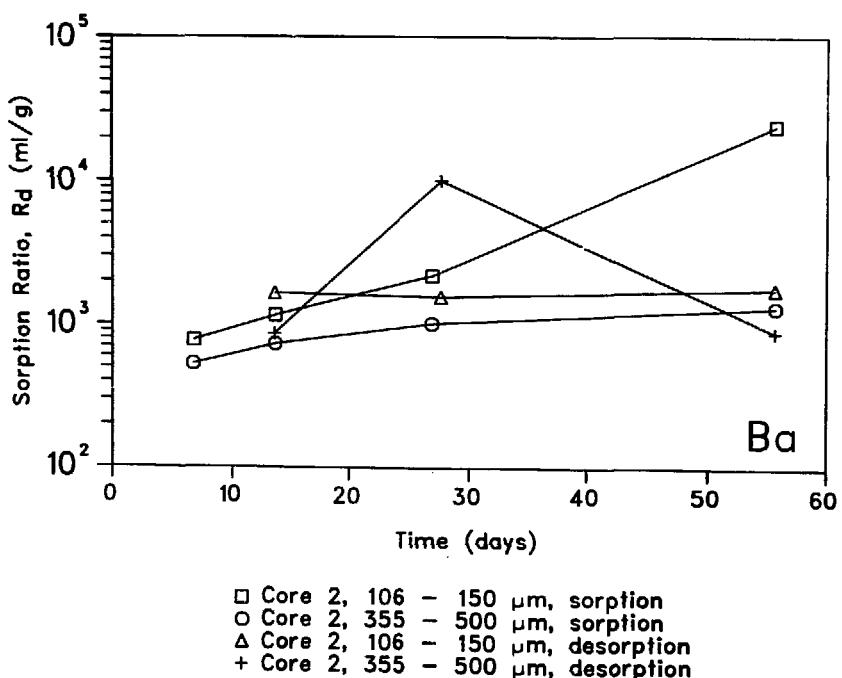
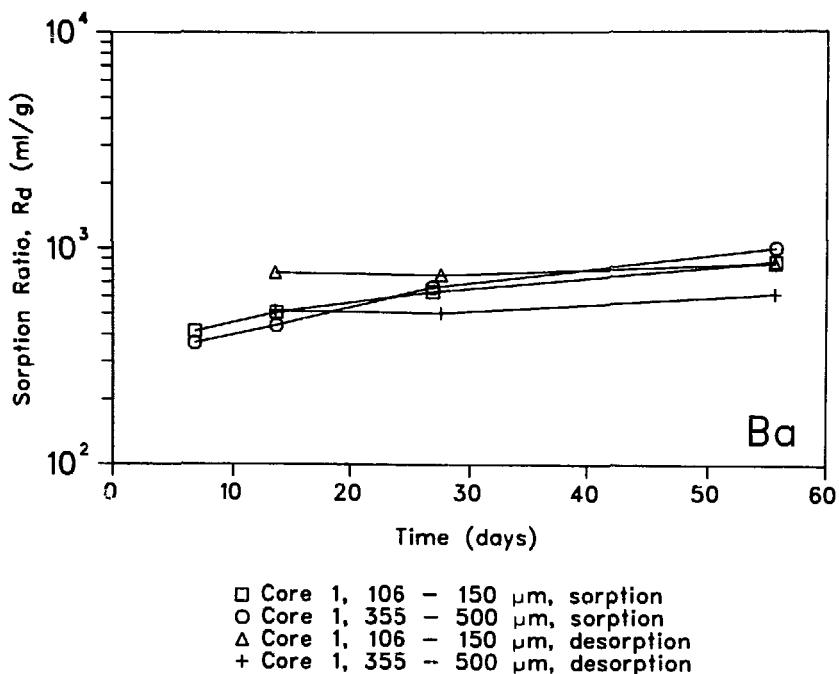


Fig. 3. Barium sorption-desorption ratio data, selected sieve fractions, ambient temperature.

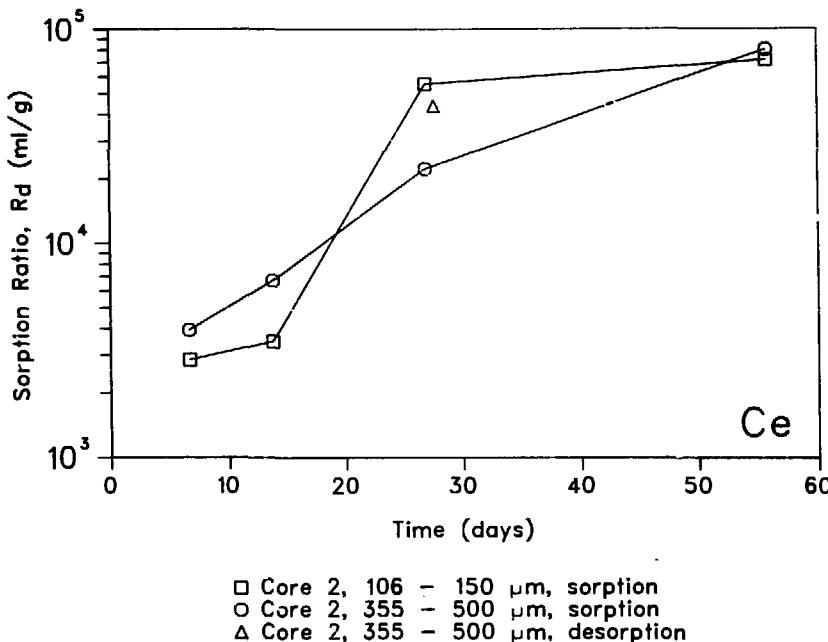
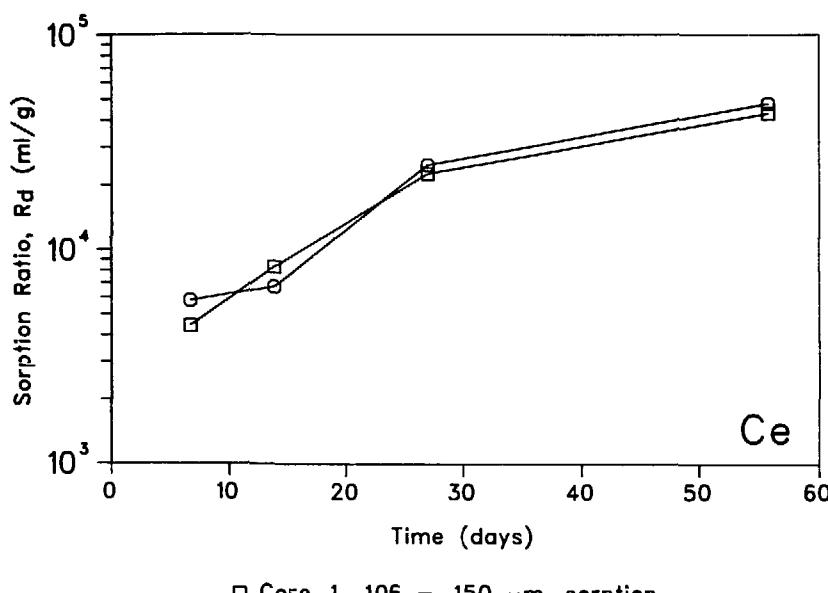


Fig. 4. Cerium sorption-desorption ratio data, selected sieve fractions, ambient temperature.

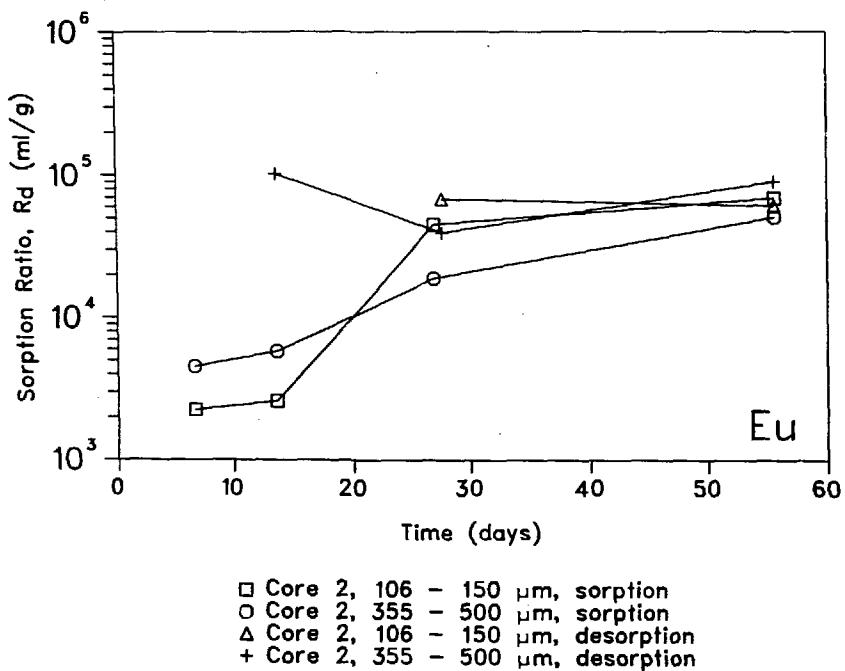
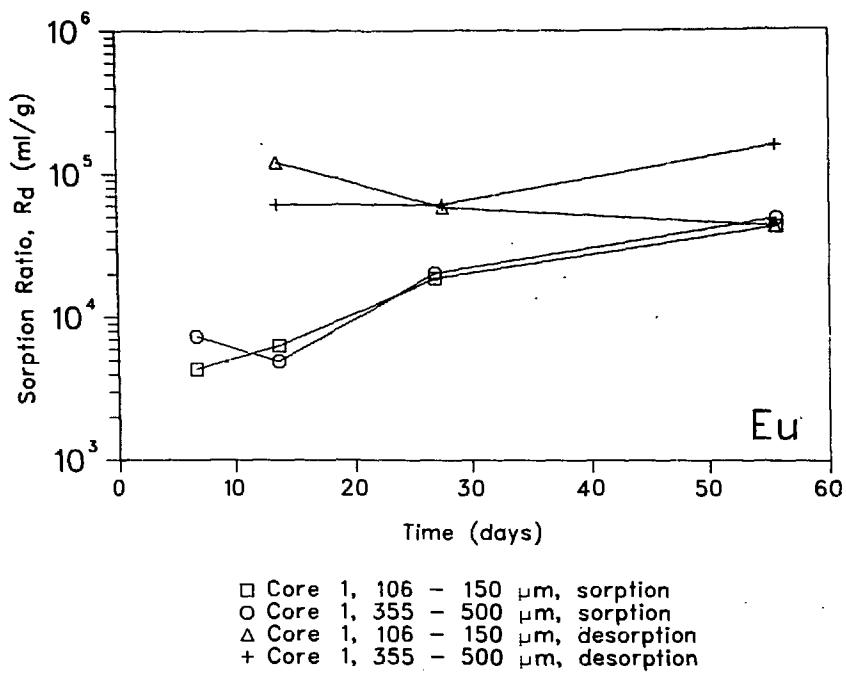
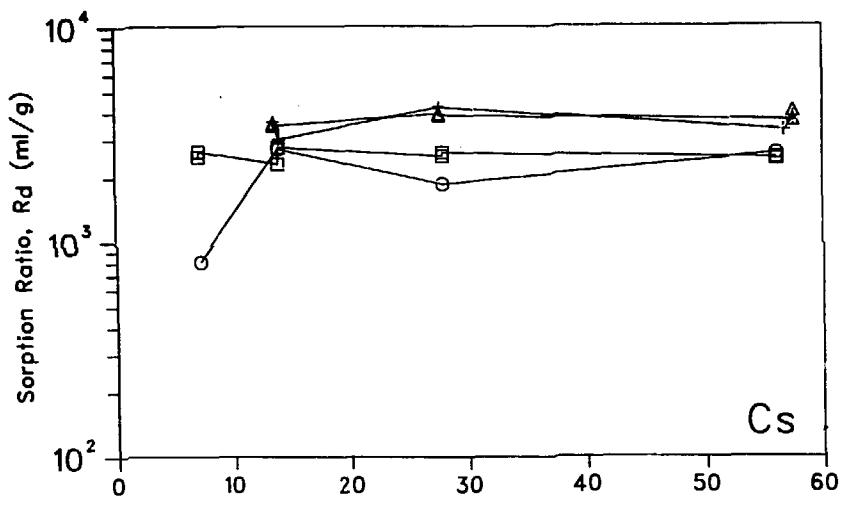


Fig. 5. Europium sorption-desorption ratio data, selected sieve fractions, ambient temperature.



□ Core 1, -75  $\mu\text{m}$ , sorption  
 ○ Core 2, -75  $\mu\text{m}$ , sorption  
 △ Core 1, -75  $\mu\text{m}$ , desorption  
 + Core 2, -75  $\mu\text{m}$ , desorption

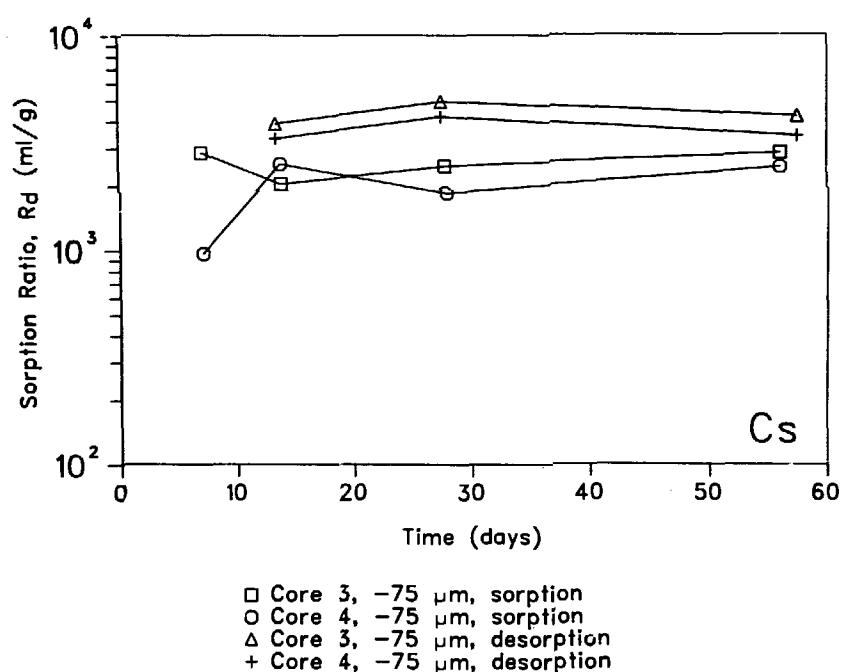


Fig. 6. Cesium sorption-desorption ratio data, <75- $\mu\text{m}$  fractions, ambient temperature.

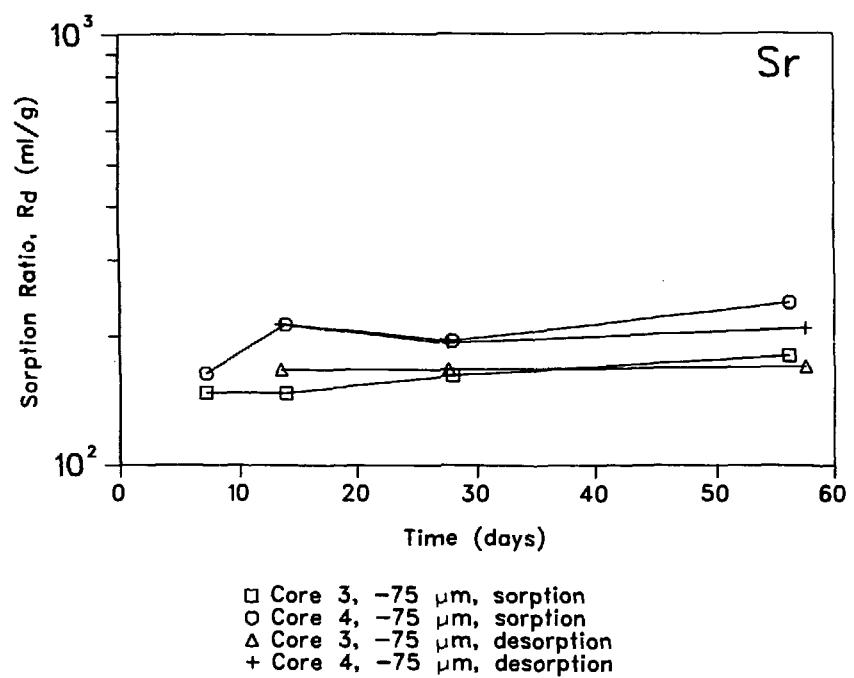
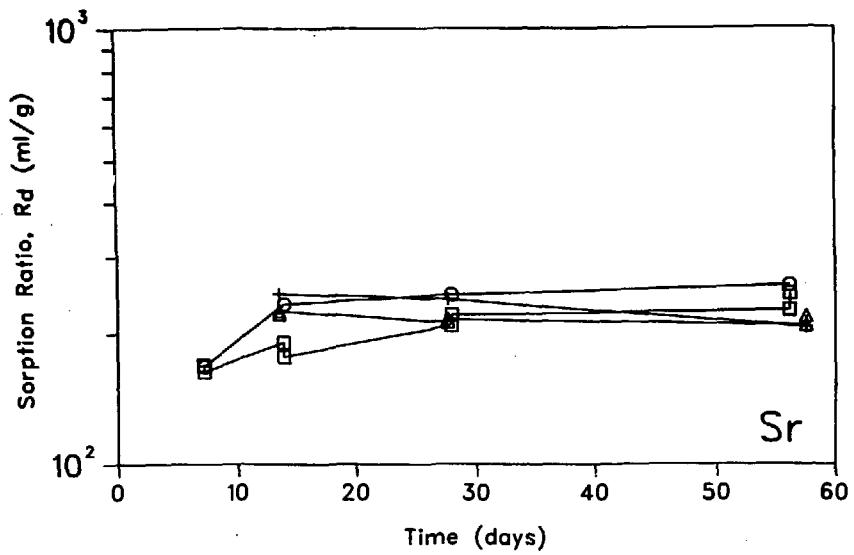


Fig. 7. Strontium sorption-desorption ratio data,  $<75\text{-}\mu\text{m}$  fractions, ambient temperature.

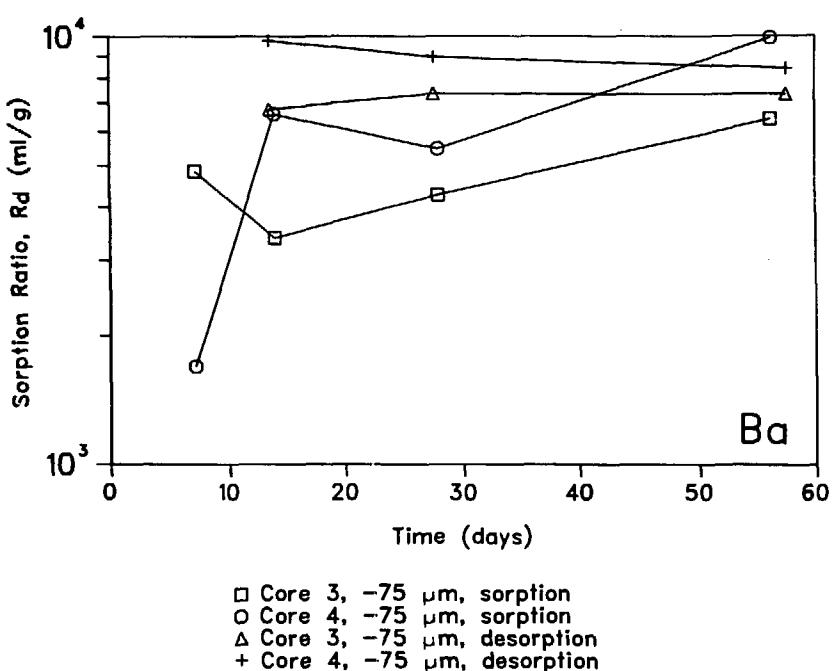
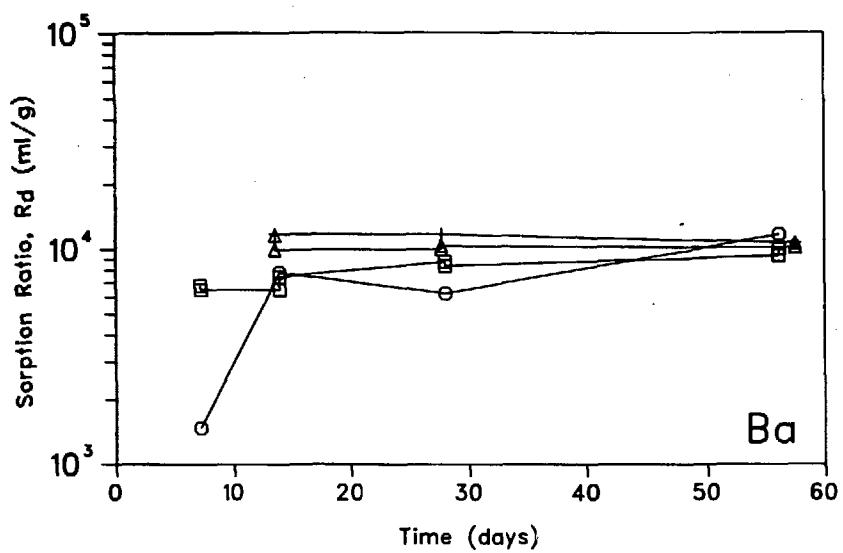


Fig. 8. Barium sorption-desorption ratio data <75- $\mu\text{m}$  fractions, ambient temperature

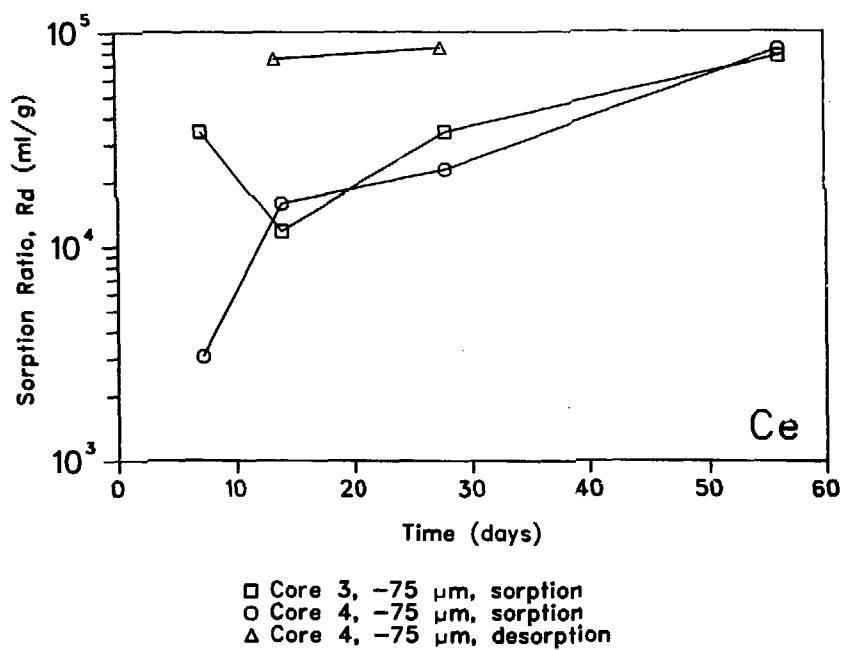
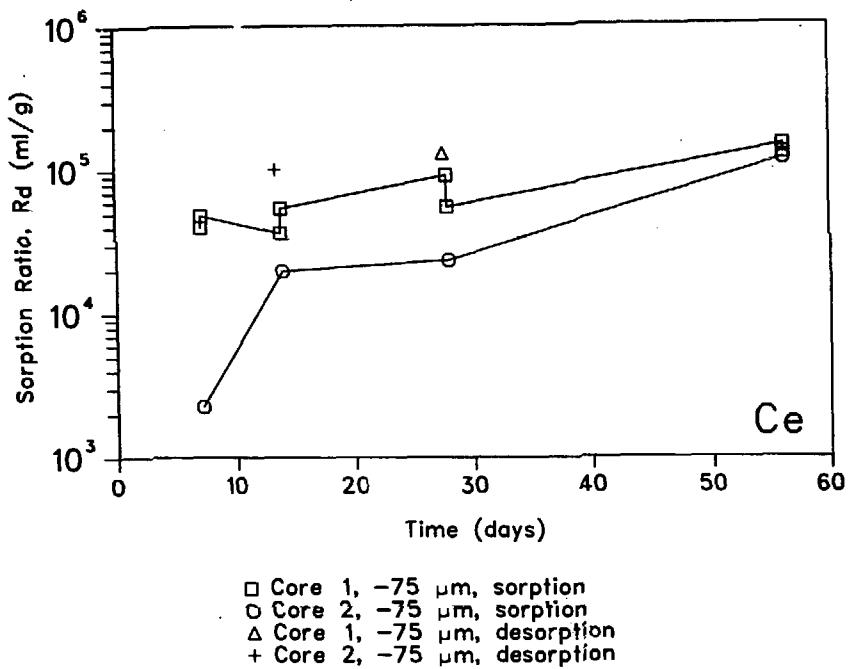


Fig. 9. Cerium sorption-desorption ratio data,  $<75\text{-}\mu\text{m}$  fractions, ambient temperature.

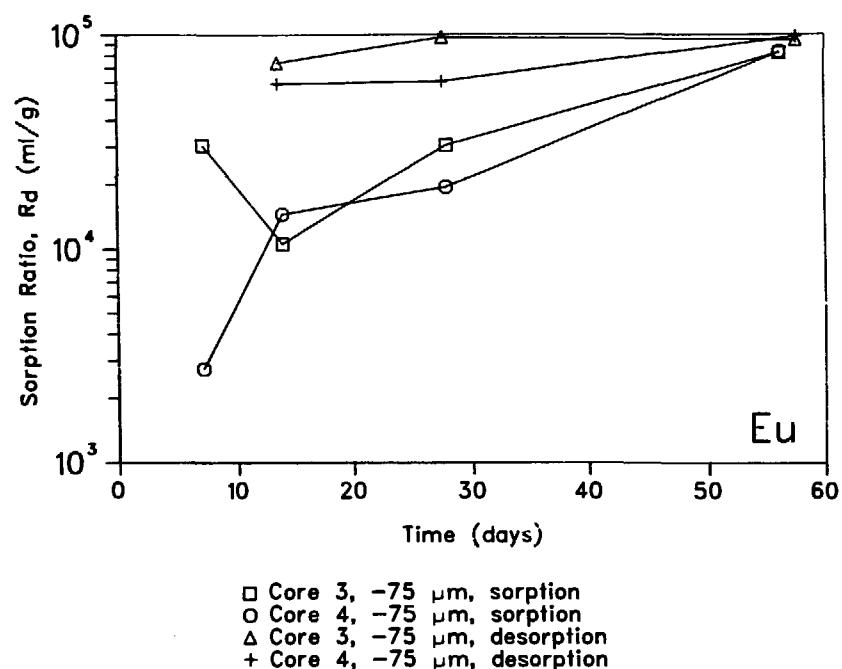
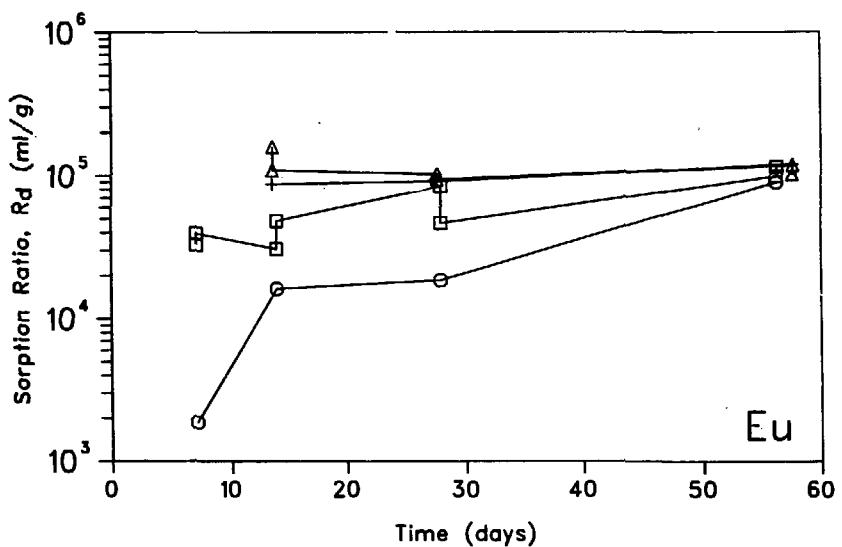


Fig. 10. Europium sorption-desorption ratio data, <75- $\mu$ m fractions, ambient temperature.

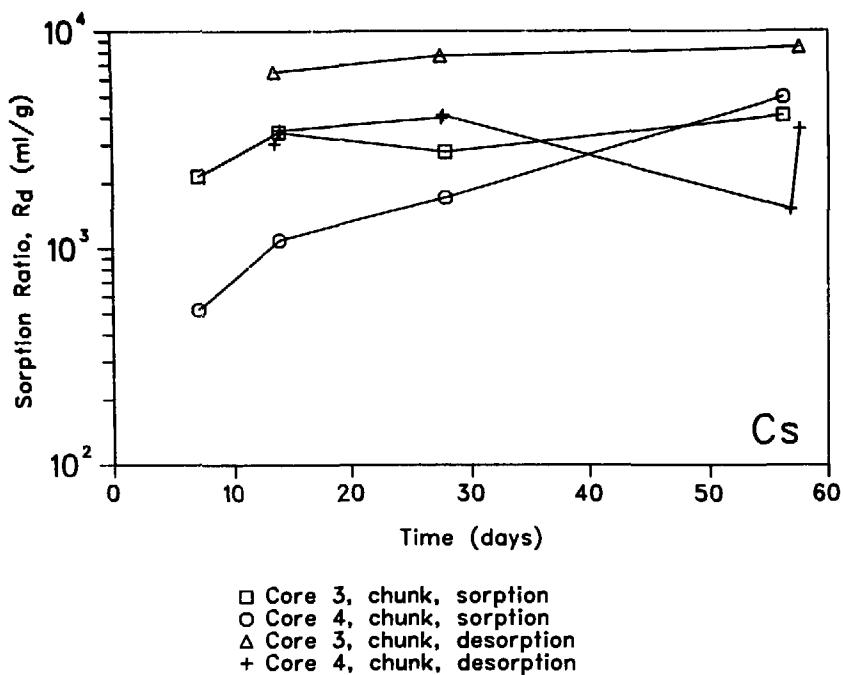


Fig. 11. Cesium sorption-desorption ratio data, chunk samples, ambient temperature

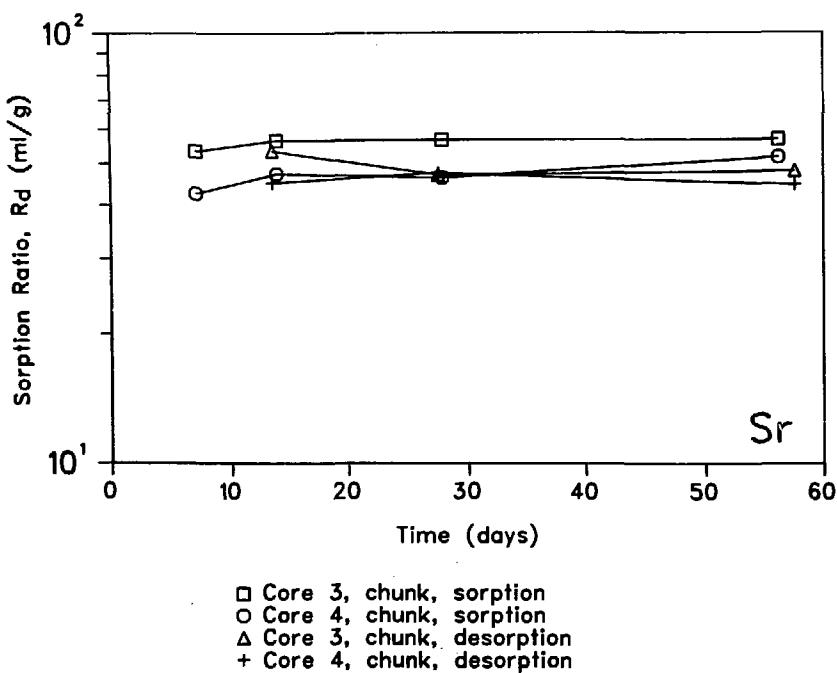


Fig. 12. Strontium sorption-desorption ratio data, chunk samples, ambient temperature.

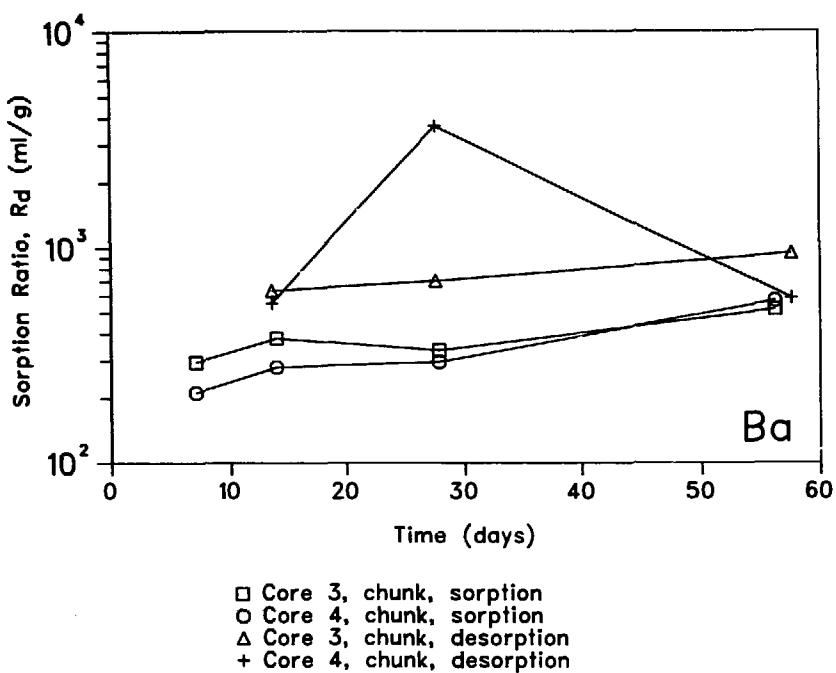


Fig. 13. Barium sorption-desorption ratio data, chunk samples, ambient temperature.

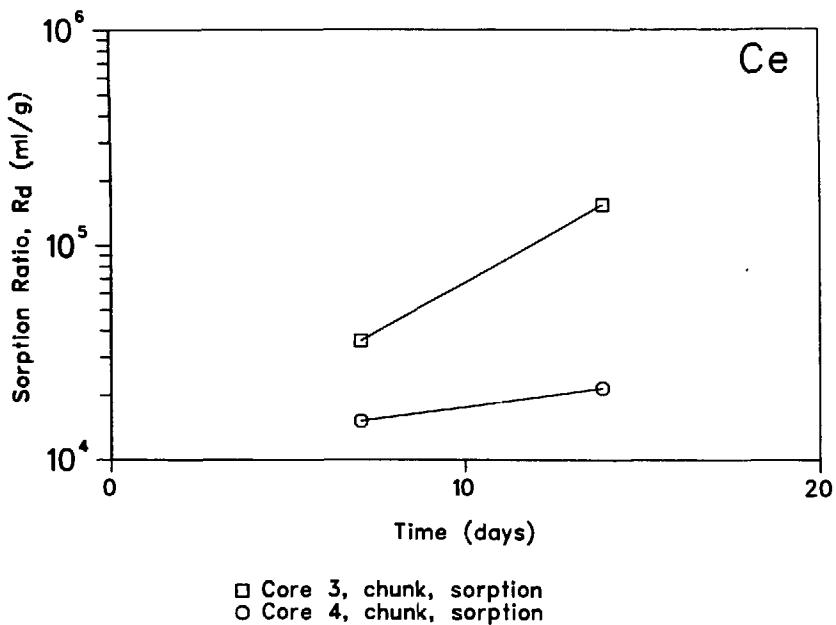


Fig. 14. Cerium sorption-desorption ratio data, chunk samples, ambient temperature.

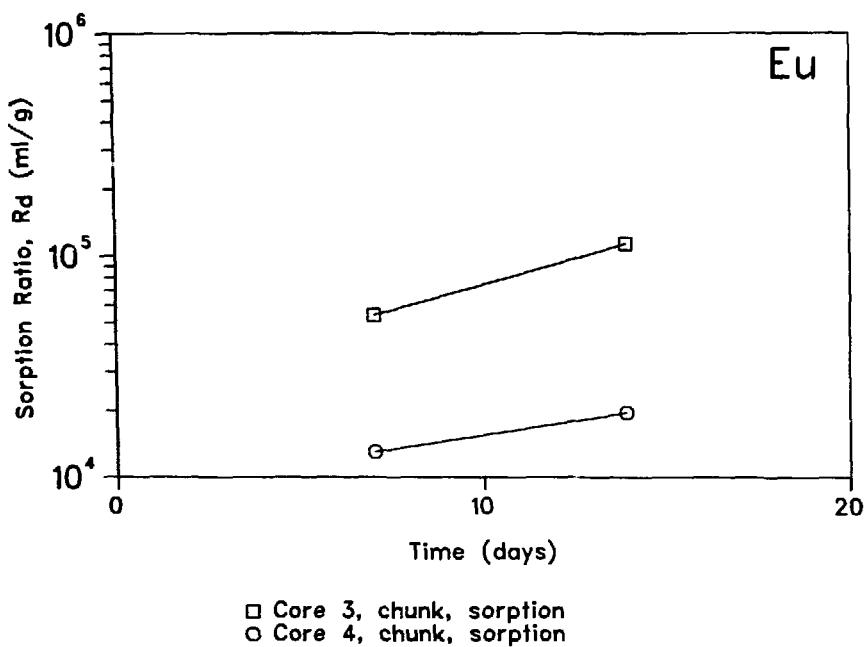


Fig. 15. Europium sorption-desorption ratio data, chunk samples, ambient temperature.

same element (for example, ions of different oxidation states, differently complexed ions, and various degrees of hydration or polymerization). If the exchange between such species is very slow and they exhibit different sorption characteristics, only one species may sorb strongly while the other remains in solution. The nonsorbing species is then absent in the desorption experiment. Of course, one could also explain this observation by postulating a significant alteration of the mineralogy in such a manner as to greatly increase the clay and zeolite fractions on the surface of the solid phase. Since, clays and zeolites have a strong affinity for cations, one would then expect a higher sorption ratio.

The need to sample the solid phase in order to measure the sorption ratio for those species having container problems is very clear. Of course, the addition of the solid should reduce the percentage of the activity going to the wall due to the greater surface area of the solid. However, for argillite the magnitude of the effect of the container is sometimes significant, as indicated by the L/S ratio in the tables.

In order to check briefly on the effect of the water and solid pre-equilibration, three measurements were made in which neither the rock nor the

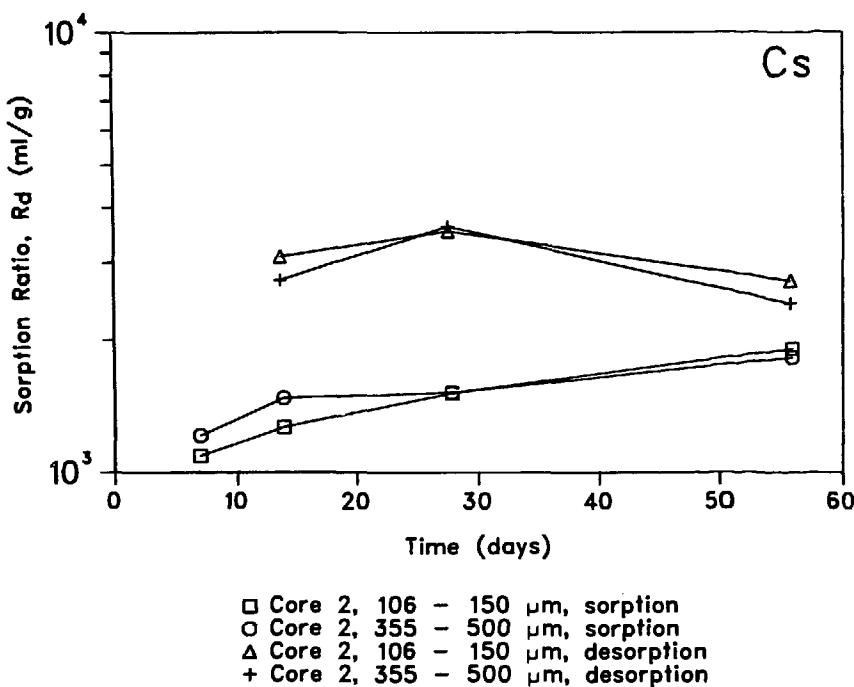
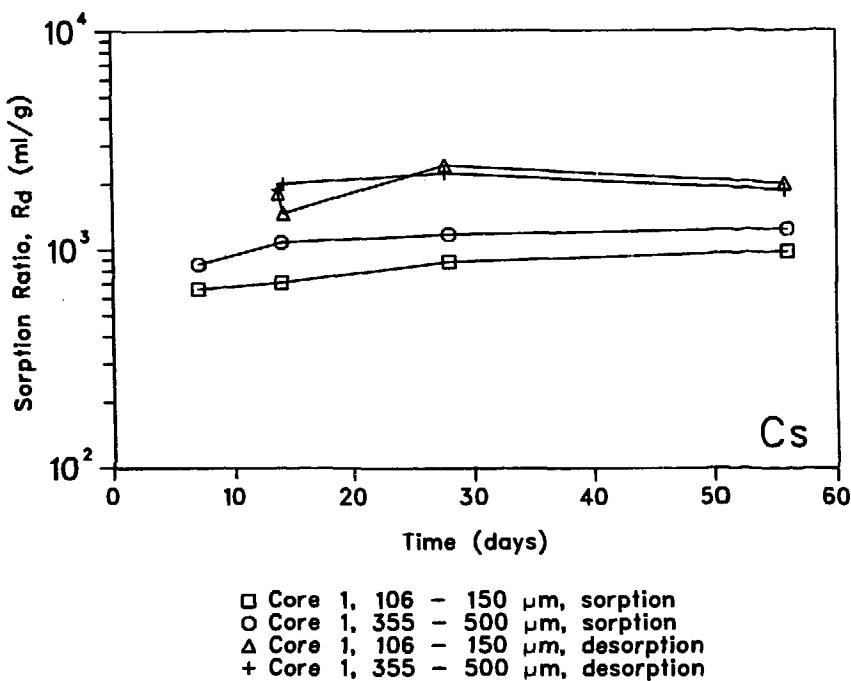
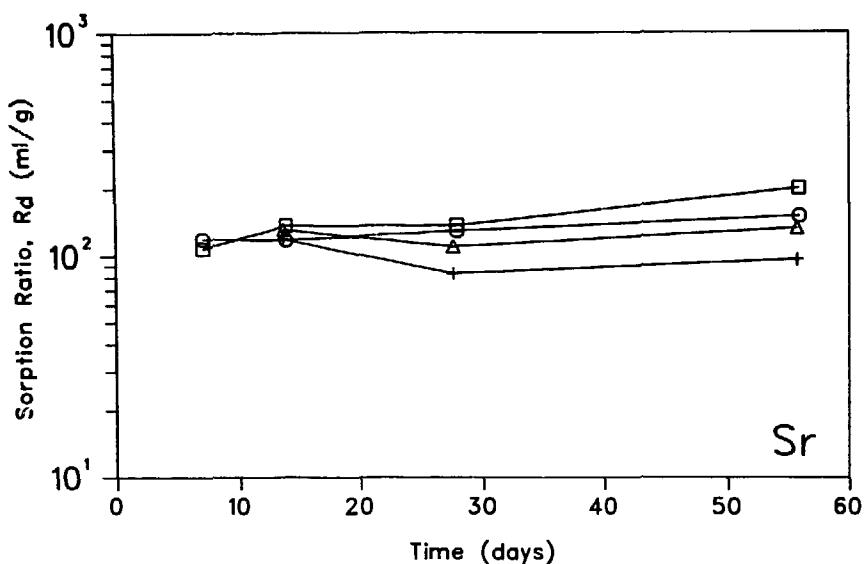
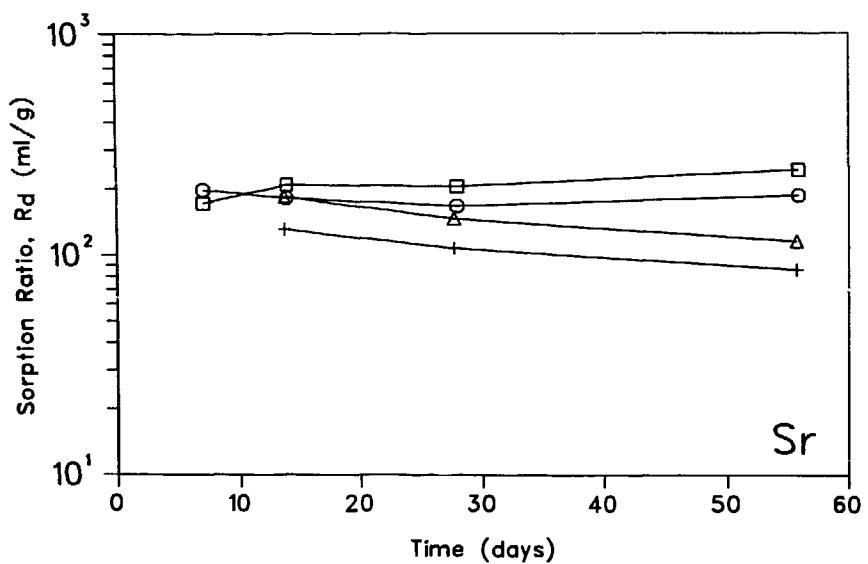


Fig. 16. Cesium sorption-desorption ratio data, selected sieve fractions, 70°C.



□ Core 1, 106 - 150  $\mu$ m, sorption  
 ○ Core 1, 355 - 500  $\mu$ m, sorption  
 △ Core 1, 106 - 150  $\mu$ m, desorption  
 + Core 1, 355 - 500  $\mu$ m, desorption



□ Core 2, 106 - 150  $\mu$ m, sorption  
 ○ Core 2, 355 - 500  $\mu$ m, sorption  
 △ Core 2, 106 - 150  $\mu$ m, desorption  
 + Core 2, 355 - 500  $\mu$ m, desorption

Fig. 17. Strontium sorption-desorption ratio data, selected sieve fractions, 70°C.

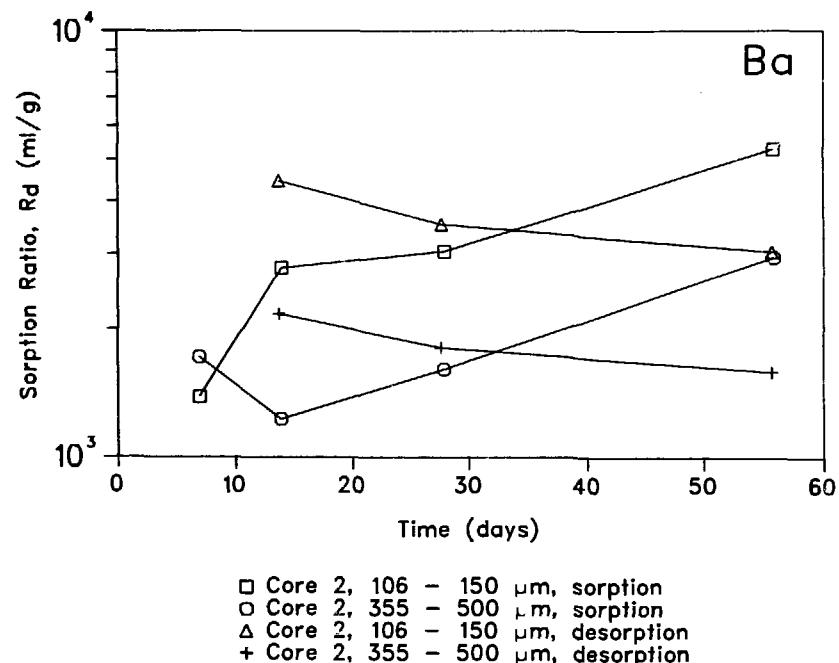
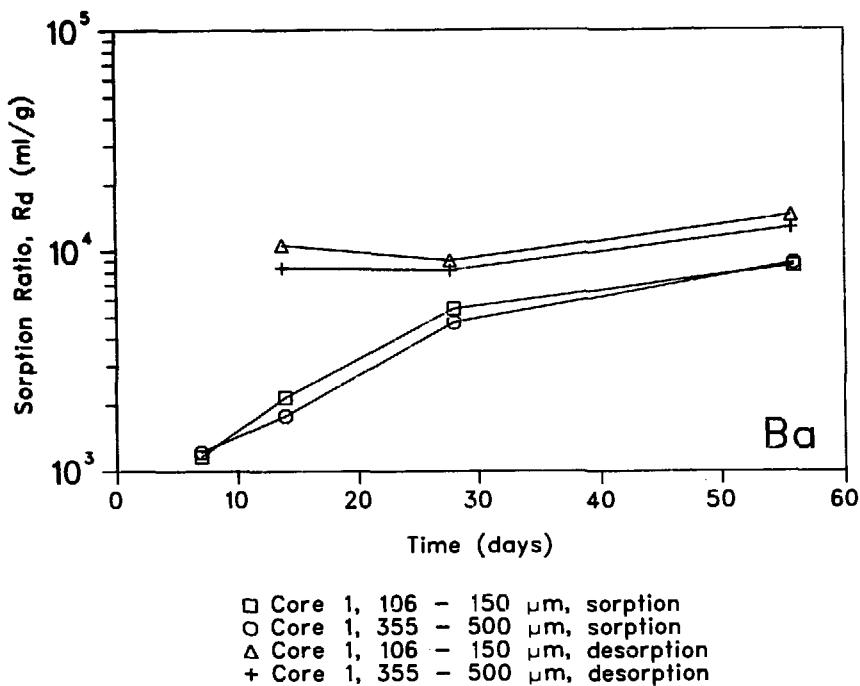


Fig. 18. Barium sorption-desorption ratio data, selected sieve fractions, 70°C.

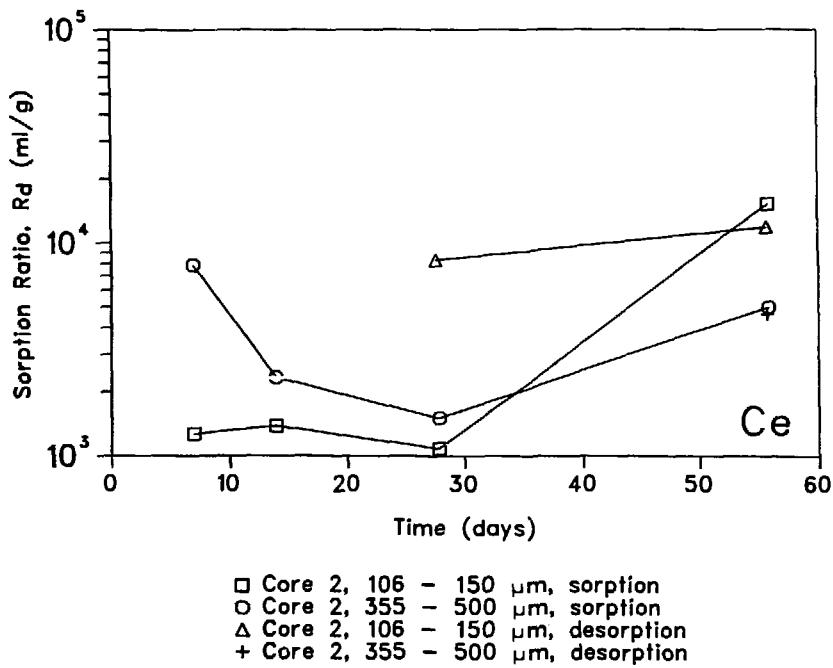
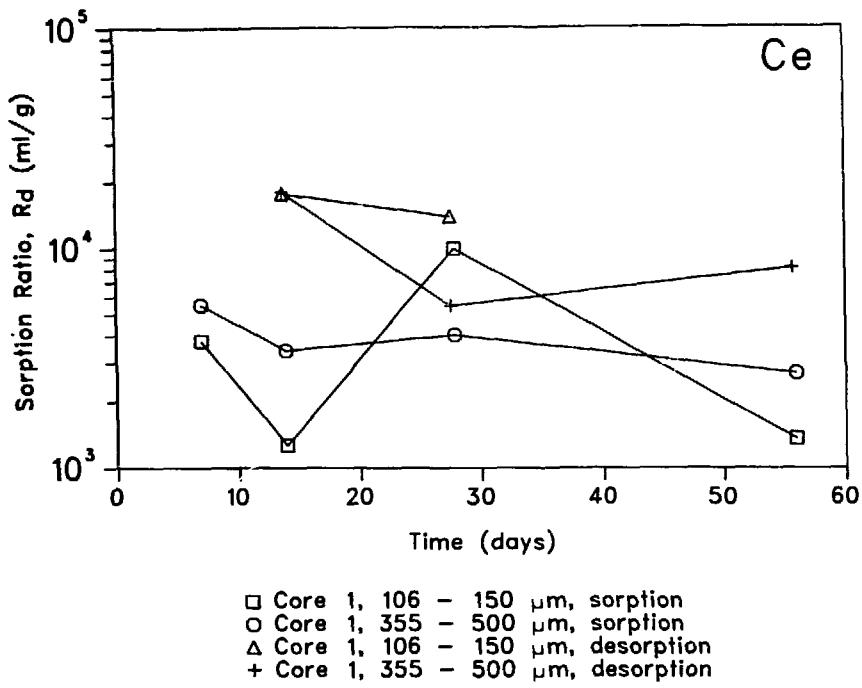


Fig. 19. Cerium sorption-desorption ratio data, selected sieve fractions, 70°C.

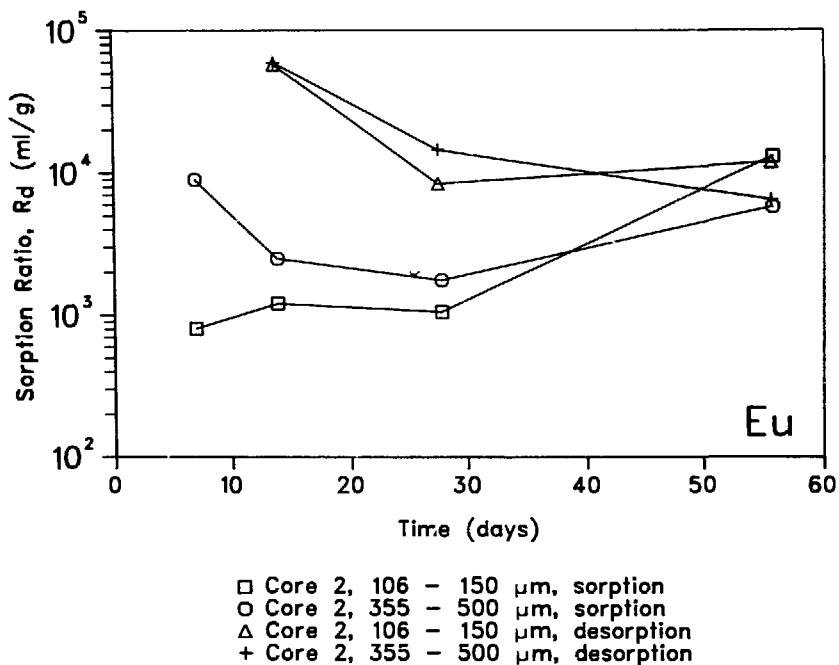
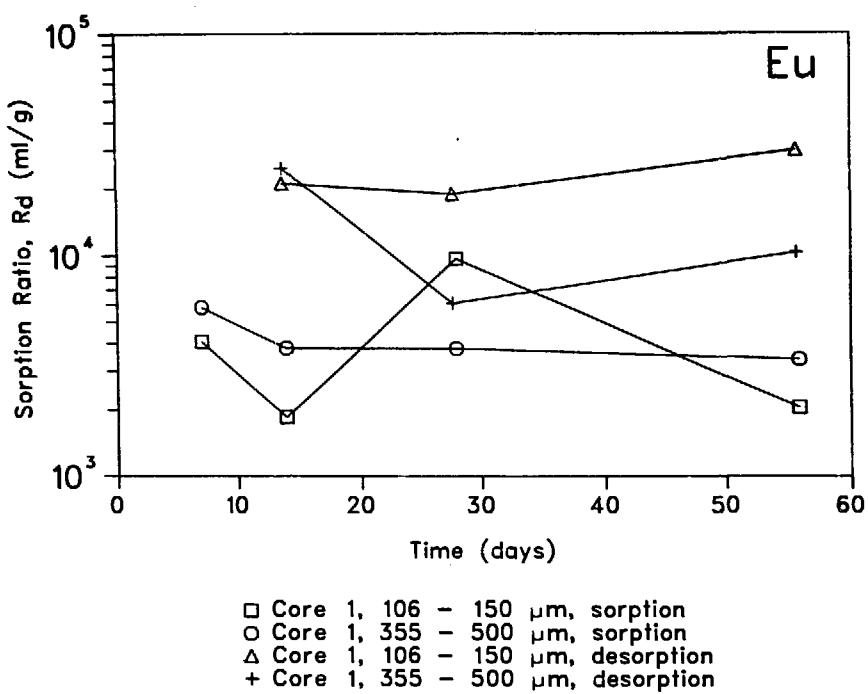


Fig. 20. Europium sorption-desorption ratio data, selected sieve fractions, 70°C.

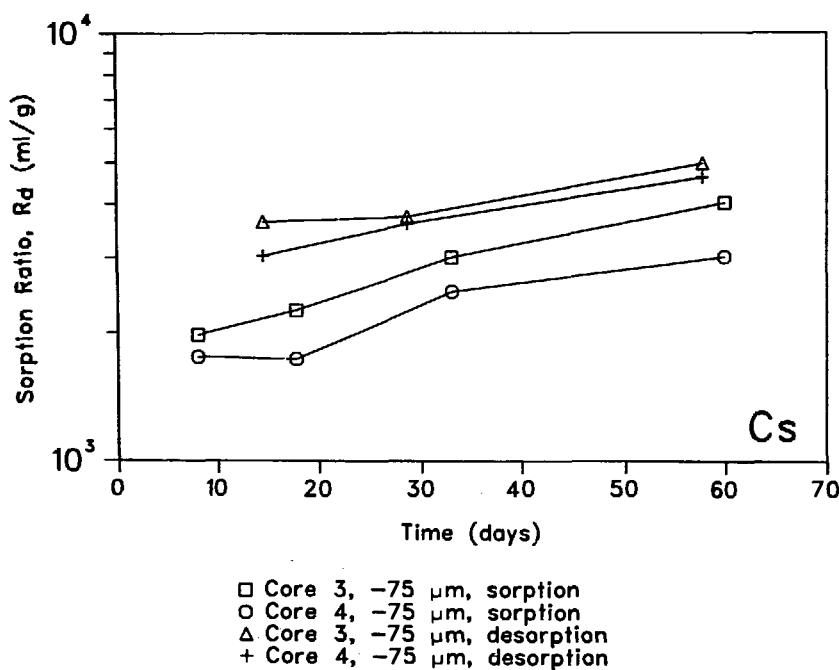
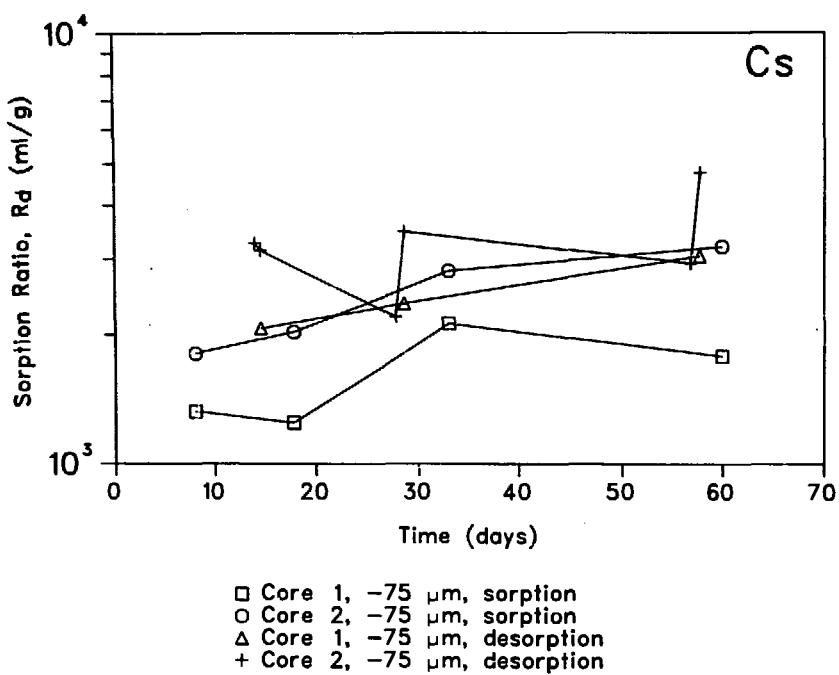


Fig. 21. Cesium sorption-desorption ratio data, <75- $\mu\text{m}$  fractions, 70°C.

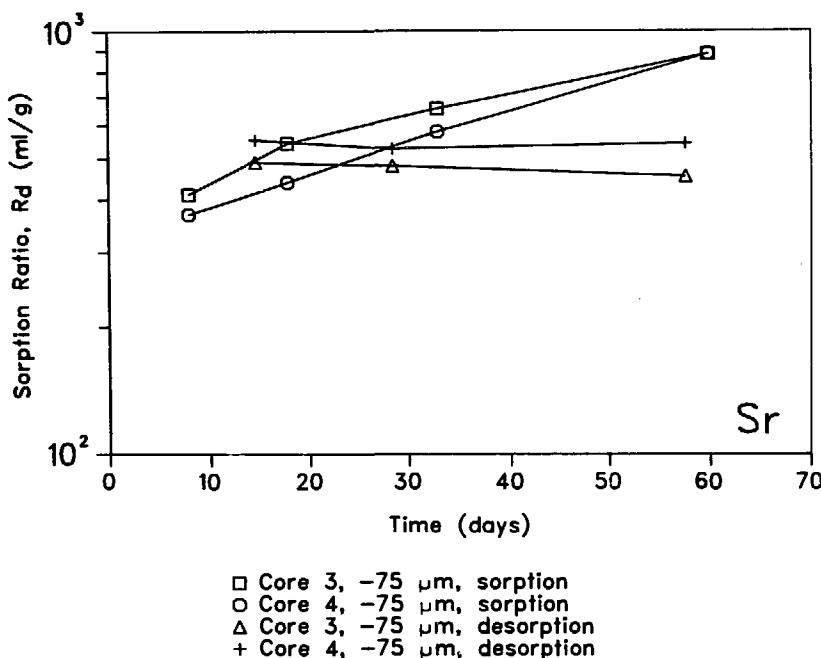
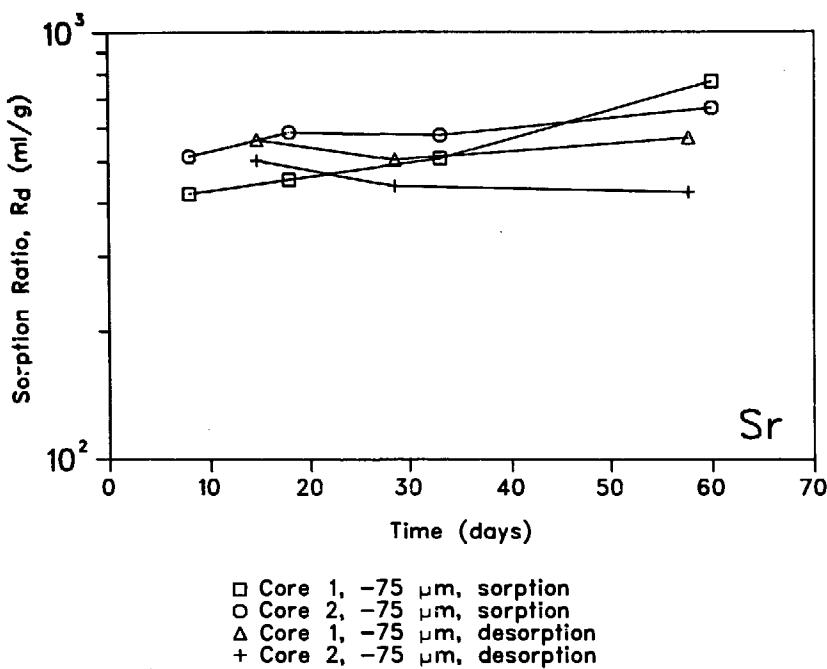


Fig. 22. Strontium sorption-desorption ratio data, <75- $\mu$ m fractions, 70°C.

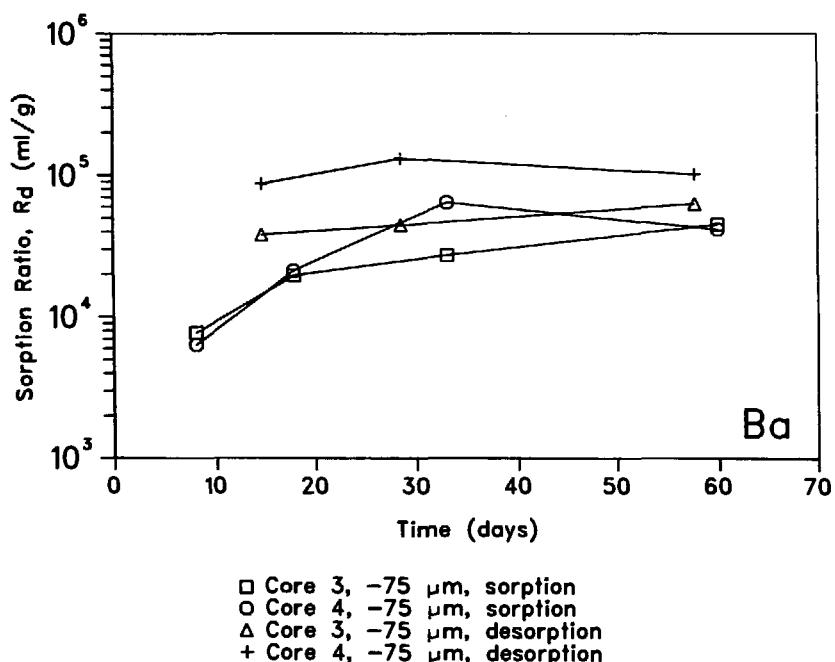
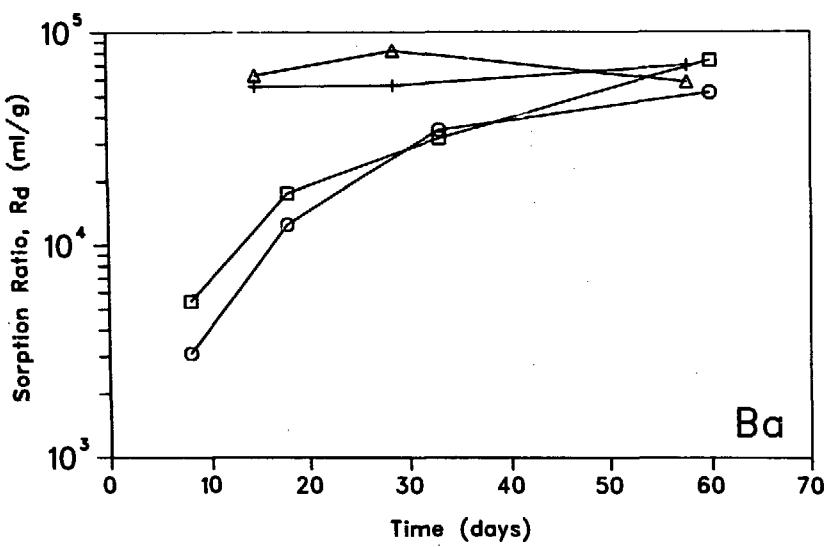


Fig. 23. Barium sorption-desorption ratio data,  $\triangleleft 75$ - $\mu$ m fractions, 70°C.

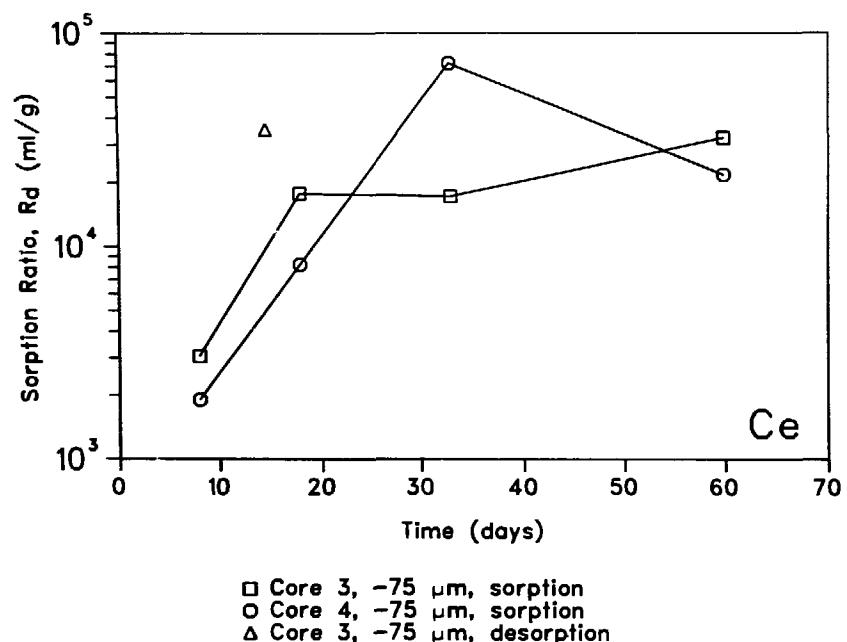
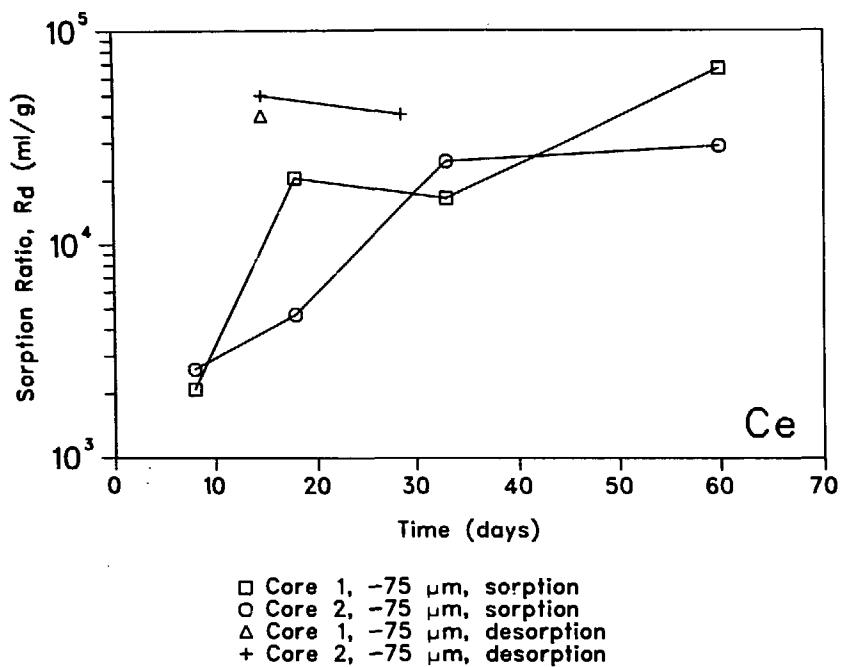


Fig. 24. Cerium sorption-desorption ratio data,  $<75$ - $\mu$ m fractions, 70°C.

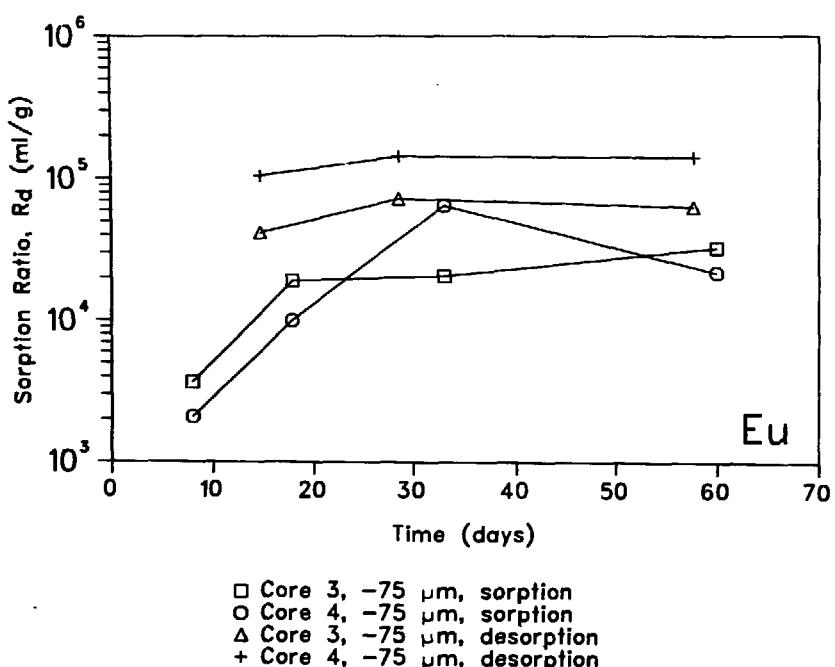
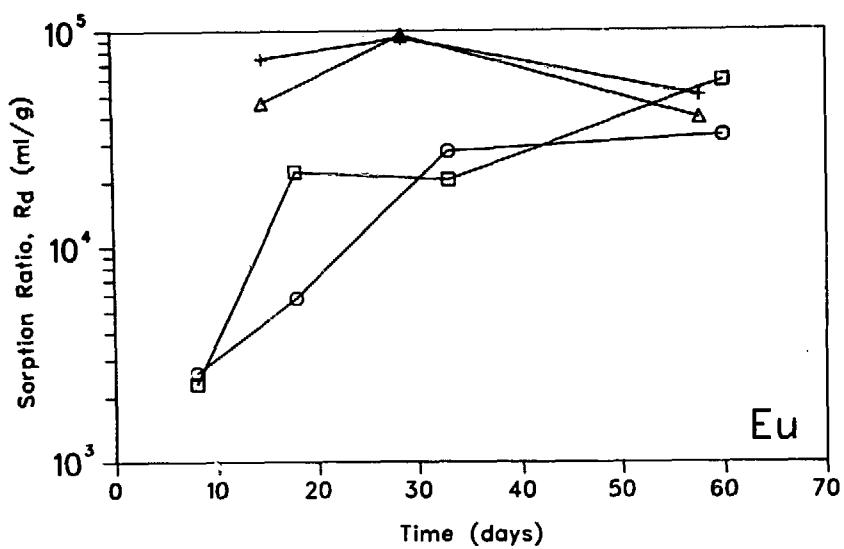


Fig. 25. Europium sorption-desorption ratio data, <75- $\mu$ m fractions, 70°C.

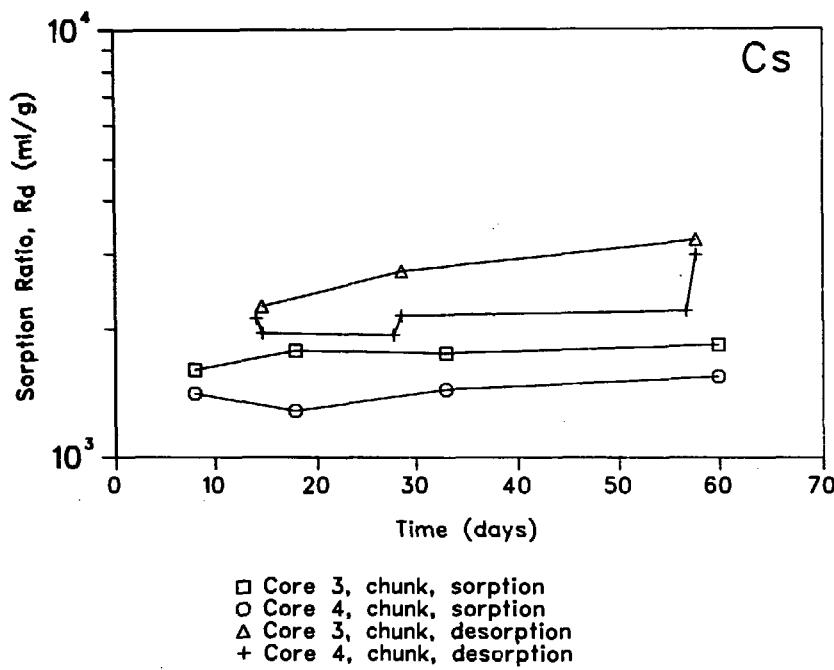


Fig. 26. Cesium sorption-desorption ratio data, chunk samples, 70°C.

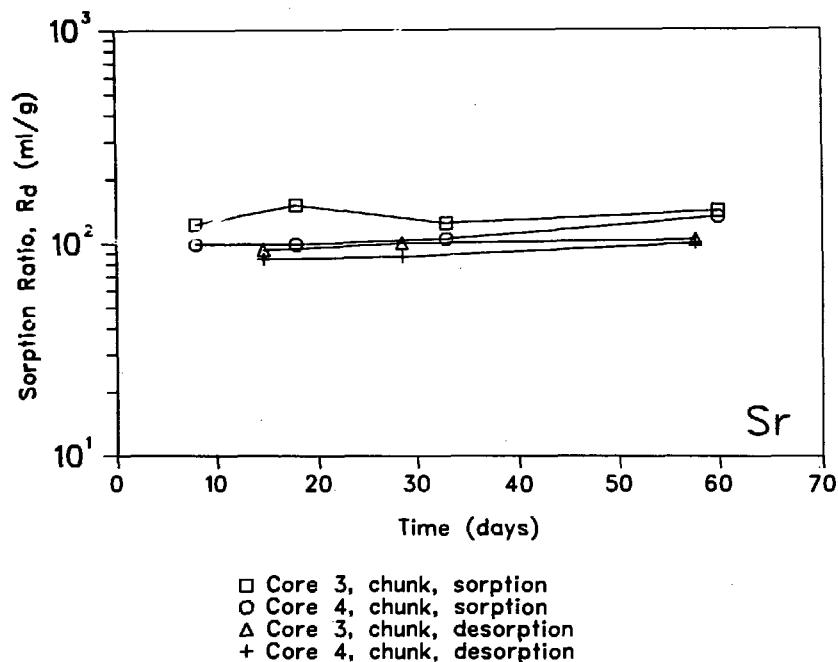


Fig. 27. Strontium sorption-desorption ratio data, chunk samples, 70°C.

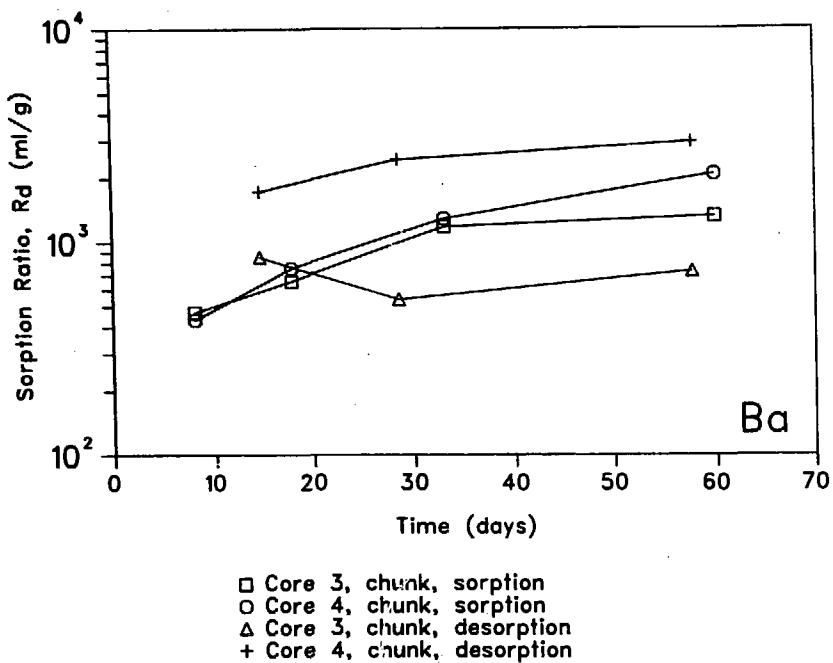


Fig. 28. Barium sorption-desorption ratio data, chunk samples, 70°C.

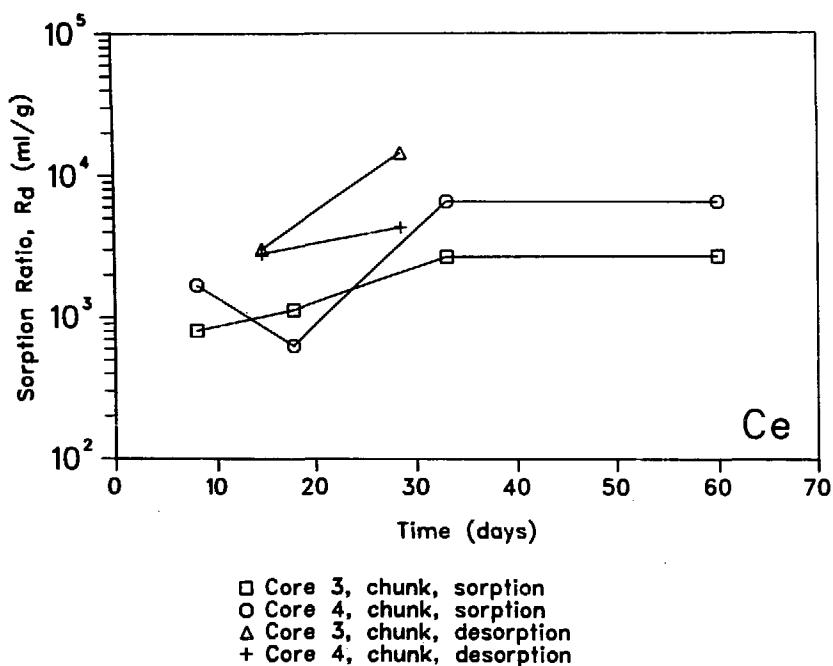


Fig. 29. Cerium sorption-desorption ratio data, chunk samples, 70°C.

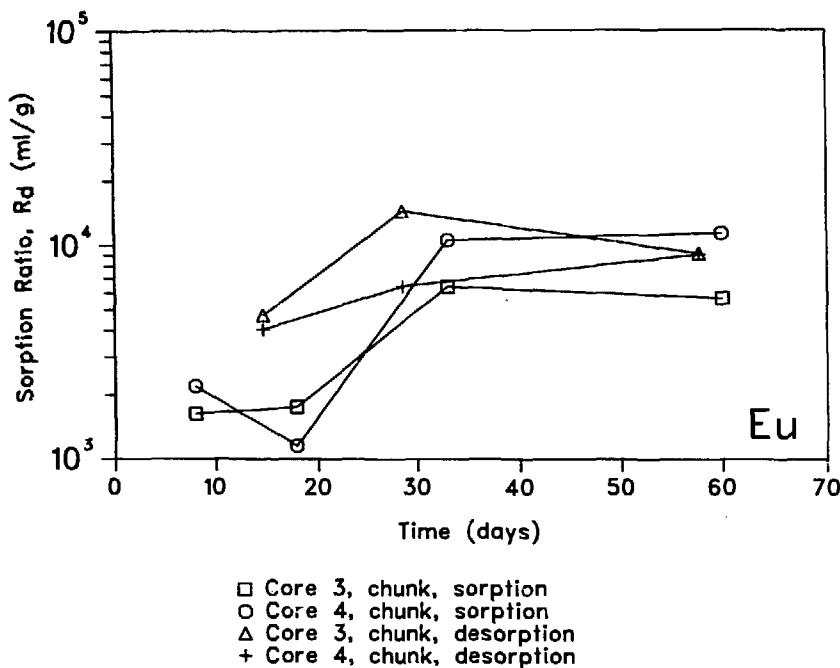


Fig. 30. Europium sorption-desorption ratio data, chunk samples, 70°C.

water was pre-equilibrated. Otherwise, exactly the same procedure as described previously was used. The contact times were 1, 2 and 4 weeks and the  $< 75\text{-}\mu\text{m}$  material prepared from CN1 was used. The measurements were run at ambient temperatures. The sorption ratios and associated data are given in Table XX and XXI. The measured  $R_d$  values are somewhat higher than those given in Table IX for the study on the same material with pre-equilibrated waters. This may be due to entrapment of the cations during the mass transfer processes that are occurring as the system approaches "equilibrium."

Table XXII gives the mean  $R_d$  values for the sorption measurements for each of the core samples at the two different temperatures. Even though there are some particle size effects on the sorption ratio, and also an increase in sorption with time, it is felt that a simple average is reasonably justified. These average values indicate that the elements arranged in the order of increasing sorption ratio at ambient and at 70°C is: Sr, Cs, Ba, Ce, Eu. The sorption of cerium and europium is about equal in magnitude.

#### IV. SORPTION OF TECHNETIUM

##### A. Measurement Technique

Measurements of the sorption behavior of technetium, under atmospheric

TABLE XX  
SORPTION RATIOS, CN1, < 75  $\mu\text{m}$  FRACTION,  
AMBIENT TEMPERATURE, NO PRE-EQUILIBRATION

Contact Time (days)	Sorption Ratio, $R_d$ (mL/g) <sup>*</sup>				
	Cs	Sr	Ba	Ce(III)	Eu(III)
6.91	2580 (2.8)	348 (2.2)	11000 (5.8)	94100 (8.8)	76100 (10)
13.83	3840 (3.0)	472 (2.1)	15900 (6.1)	162000 (11)	131000 (12)
27.85	3870 (3.6)	487 (2.5)	18300 (7.8)	171000 (21)	148000 (15)

\* See the footnote to Table VII.

TABLE XXI  
pH AND L/S VALUES FOR MEASUREMENTS IN TABLE XX

Contact Time (days)	Final pH*	L/S			Percent Remaining in Solution				
		Ba	Ce	Eu	Cs	Sr	Ba	Ce	Eu
6.91	8.83	1.02	0.96	0.97	0.61	4.3	0.14	0.02	0.02
6.91**	8.85				99.2	101	95.9	72.03	85.6
13.83	9.07	1.03	0.95	0.95	0.54	4.25	0.13	0.01	0.02
13.83**	9.01				92.3	93.9	89.1	62.25	78.3
27.85	9.45	1.02	0.96	0.97	0.52	4.01	0.11	0.01	0.01
27.85**	9.26				94.6	97.4	92.3	53.86	77.4

\* The initial pH was 8.46

\*\* Control samples

TABLE XXII  
MEAN SORPTION RATIOS

Sorption Ratio,  $R_d$  (mL/g)

Element	Core	22°C		70°C	
		Sorption	Desorption	Sorption	Desorption
Cs	CN1	1830 ± 200	3110 ± 710	1200 ± 120	1980 ± 610
	CN2	1580 ± 200	3810 ± 610	1881 ± 150	3280 ± 690
	CN3*	2540 ± 190	4340 ± 530	2810 ± 460	4110 ± 740
	CN4*	1940 ± 360	3630 ± 480	2240 ± 310	3740 ± 810
Sr	CN1	138 ± 14	133 ± 88	265 ± 57	256 ± 218
	CN2	156 ± 17	131 ± 76	335 ± 61	236 ± 166
	CN3*	159 ± 77	168 ± 7	622 ± 100	508 ± 40
	CN4*	202 ± 16	204 ± 11	567 ± 110	541 ± 13
Ba	CN1	4270 ± 970	5530 ± 5100	12 700 ± 5600	29 600 ± 29 300
	CN2	4900 ± 2000	5650 ± 5140	10 900 ± 5100	22 030 ± 29 300
	CN3*	4730 ± 640	7140 ± 330	24 900 ± 7800	48 600 ± 13 100
	CN4*	5920 ± 1690	9050 ± 680	33 400 ± 12 600	36 800 ± 43 600
Ce	CN1	47 400 ± 10 400	> 100 000	10 700 ± 5000	17 200 ± 12 300
	CN2	34 000 ± 11 000	72 000 ± 40 000	8660 ± 2990	26 000 ± 19 800
	CN3*	39 300 ± 13 600		17 600 ± 6000	26 600 ± 12 400
	CN4*	31 200 ± 17 700	79 600 ± 6600	26 000 ± 15 900	
Eu	CN1	40 300 ± 800	89 800 ± 45 000	10 700 ± 4400	32 500 ± 26 900
	CN2	26 800 ± 8400	81 600 ± 25 000	9360 ± 3330	41 700 ± 32 200
	CN3*	38 500 ± 15 400	88 600 ± 12 800	18 900 ± 5900	58 800 ± 15 700
	CN4*	30 000 ± 18 000	72 600 ± 22 100	24 500 ± 13 900	98 200 ± 75 900

\*The results obtained using the chunk samples were not included in the average.

oxygen conditions, have been made following exactly the same procedures as described earlier in this report (see section III.A). The measurements were made using the  $^{95m}\text{Tc}$  supplied by Argonne National Laboratory under contract with Battelle Pacific Northwest Laboratory. The fourth batch (see Table IV) of pre-equilibrated water was used. The initial pH values were 8.32 and 8.38 for the ambient and 70°C measurements, respectively. Since the container sorption problems for technetium were unknown,  $^{137}\text{Cs}$  was also added to the water (17  $\mu\text{Ci}$   $^{137}\text{Cs}/\ell$  final solution ( $1.4 \times 10^{-9}\text{M}$ )) using the evaporation procedure previously described. However, the  $^{95m}\text{Tc}$  was added by simply pipetting a fraction of the diluted tracer into the appropriate water prior to filtration. The pH did not require adjusting after this addition. The final concentration was 4.1  $\mu\text{Ci}$   $^{95m}\text{Tc}/\ell$  solution ( $1.9 \times 10^{-9}\text{M}$ ). The 106-150  $\mu\text{m}$  and 355-500  $\mu\text{m}$  fractions from CN1, the  $< 75\text{-}\mu\text{m}$  material from CN2, and the chunk samples from CN4 were used in the measurements which were performed at  $22 \pm 2^\circ\text{C}$  and  $70 \pm 1^\circ\text{C}$ .

## B. Results and Conclusions

The results for the  $R_d$  measurements for the ambient and elevated temperature conditions are given in Tables XXIII and XXIV, respectively. The sorption ratios for technetium were calculated using Eq. 1 since no container sorption was found for  $^{95m}\text{Tc}$ . The initial pH values of the solutions were 8.32 and 8.38, for the 20°C and 70°C experiments, respectively. The final pH values and the percentages of the activities remaining in solution after the appropriate contact time are given in Table XXV. The sorption ratio results are shown graphically in Figs. 31-34.

As expected there seems to be a correlation between the surface area and the technetium sorption ratio for the ground samples. However, the highest  $R_d$  values were observed for the chunk sample, which should have the lowest surface area. This may be due<sup>11</sup> to the presence of organic matter in the argillite.

The technetium sorption ratio decreases dramatically when the temperature is raised to 70°C. This may be due to increased solubility at the higher temperature.

The cesium sorption ratios obtained in this set of measurements are in reasonable agreement with those given earlier (Tables VII-XIV) for the same materials. The  $R_d$  values for the 106-150  $\mu\text{m}$  fractions from CN1 are higher,

TABLE XXIII  
Cs AND Tc SORPTION RATIOS, AMBIENT TEMPERATURE

Core	Fraction ( $\mu\text{m}$ )	Sorption Time (days)	Desorption Time (days)	Sorption Ratio, $R_d$ (mL/g)*	
				Cs	Tc(VII)
CN1	106-150	6.75		1320 (2.0)	11.8 (5.1)
			56.81	1970 (11)	126 (13)
		16.76		1370 (1.6)	11.9 (4.0)
			27.74	2810 (11)	110 (13)
		27.77		2350 (1.9)	15.9 (3.9)
	355-500		14.03	2090 (11)	95.4 (12)
		58.77		2740 (1.9)	16.2 (3.9)
		6.74		1070 (1.3)	15.4 (4.0)
			56.81	1570 (11)	165 (15)
		16.76		1930 (1.6)	21.5 (3.4)
CN2	< 75	27.76		4030 (12)	181 (13)
			27.74	2490 (2.6)	22.1 (3.6)
		58.77		2120 (10)	143 (13)
		6.73		3850 (2.1)	31.0 (3.0)
			56.81	1030 (12)	18.3 (3.9)
	58.75	16.75		3270 (11)	222 (14)
				1230 (1.5)	29.1 (3.0)
		27.76		27.73	204 (13)
				1600 (1.8)	34.7 (2.9)
		58.75		14.03	3000 (11)
CN4	Chunk	58.75		1830 (1.8)	193 (13)
		6.73		865 (1.2)	39.8 (3.0)
			56.81	1520 (9.6)	18.8 (3.6)
		16.74		1930 (1.8)	511 (21)
				4100 (12)	111 (2.3)
		27.75		3040 (1.6)	693 (17)

\*See the footnote to Table VII.

TABLE XXIV  
Cs AND Tc SORPTION RATIOS, 70°C

Core	Fraction ( $\mu\text{m}$ )	Sorption Time (days)	Desorption Time (days)	Sorption Ratio, $R_d$ (ml/g)*	
				Cs	Tc(VI)
CN1	106-150	6.72		620 (1.1)	1.24 (29)
			56.80	1380 (10)	- 3.98 (28)
		13.72		640 (1.1)	1.44 (25)
			27.73	1340 (10)	- 2.43 (48)
		27.77		662 (1.5)	1.57 (23)
	355-500		14.05	1460 (9.9)	- 1.75 (70)
		59.74		765 (1.5)	1.06 (34)
		6.71		972 (1.3)	1.72 (22)
			56.80	1930 (10)	- 1.77 (67)
		13.72		983 (1.5)	2.23 (16)
CN2	< 75		27.73	1890 (11)	1.57 (94)
		27.72		1110 (1.5)	2.03 (18)
			14.05	2000 (11)	0.04
		59.73		1150 (1.6)	1.61 (23)
		6.69		1930 (1.5)	0.94 (42)
			56.80	2930 (11)	- 8.86 (10)
		13.71		1950 (1.6)	1.90 (21)
			27.73	2200 (11)	- 4.38 (25)
		27.72		2060 (1.9)	3.14 (14)
			14.05	3260 (11)	5.81 (35)
CN4	Chunk	59.73		2340 (1.8)	2.15 (20)
		6.70		1050 (1.3)	5.36 (7.9)
			56.80	2200 (11)	17.8 (18)
		13.71		1020 (1.4)	6.70 (6.8)
			27.71	1930 (11)	33.5 (11)
		27.71		1130 (1.7)	9.56 (5.2)
			14.05	2120 (11)	45.3 (13)
		59.72		1220 (1.7)	12.4 (4.6)

\* See the footnote to Table VII.

TABLE XXV  
FINAL pH AND PERCENT REMAINING IN SOLUTION

Core	Fraction ( $\mu\text{m}$ )	Contact Time (days)	Temperature ( $^{\circ}\text{C}$ )	Final pH	Percent Remaining in Solution	
					Cs	Tc
CN1	106-150	6.75	20	8.75	1.52	63.3
		16.76		8.78	1.48	63.4
		27.77		8.46	0.85	55.9
		58.77		8.20	0.73	55.5
	355-500	6.74	20	8.62	1.85	56.8
		16.76		8.66	1.03	48.2
		27.76		8.41	0.80	47.5
		58.76		8.36	0.52	39.4
CN2	< 75	6.73	20	8.88	2.16	55.4
		16.75		8.76	1.84	44.2
		27.76		8.53	1.40	39.6
		58.75		8.47	1.24	36.7
CN4	Chunk	6.73	20	8.72	2.22	51.1
		16.74		8.70	1.01	15.0
		27.75		8.54	0.65	12.8
		58.75		8.44	0.71	8.1
CN1	106-150	6.72	70	8.87	3.17	94.3
		13.72		8.67	3.09	93.4
		27.72		8.00	2.96	92.8
		59.73		8.65	2.62	95.1
	355-500	6.71	70	8.82	2.04	92.2
		13.72		8.75	1.94	89.7
		27.72		8.20	1.79	90.8
		59.73		8.64	1.74	92.7
CN2	< 75	6.69	70	8.78	1.16	96.0
		13.71		8.02	1.16	92.3
		27.72		8.26	1.10	88.0
		59.73		8.46	0.98	91.5
CN4	Chunk	6.70	70	8.75	1.87	78.9
		13.71		8.25	1.96	75.2
		27.71		8.21	1.72	67.4
		59.72		8.56	1.65	62.2

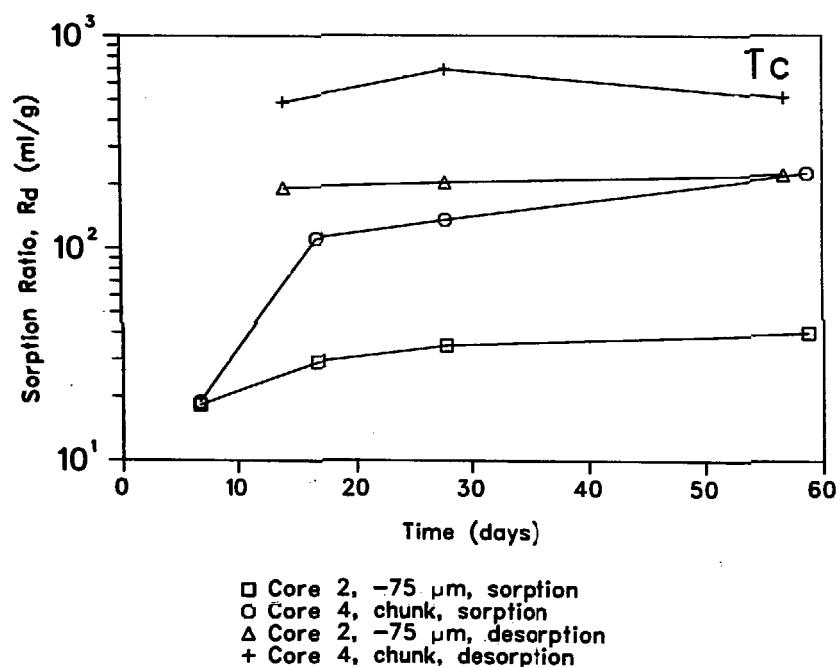
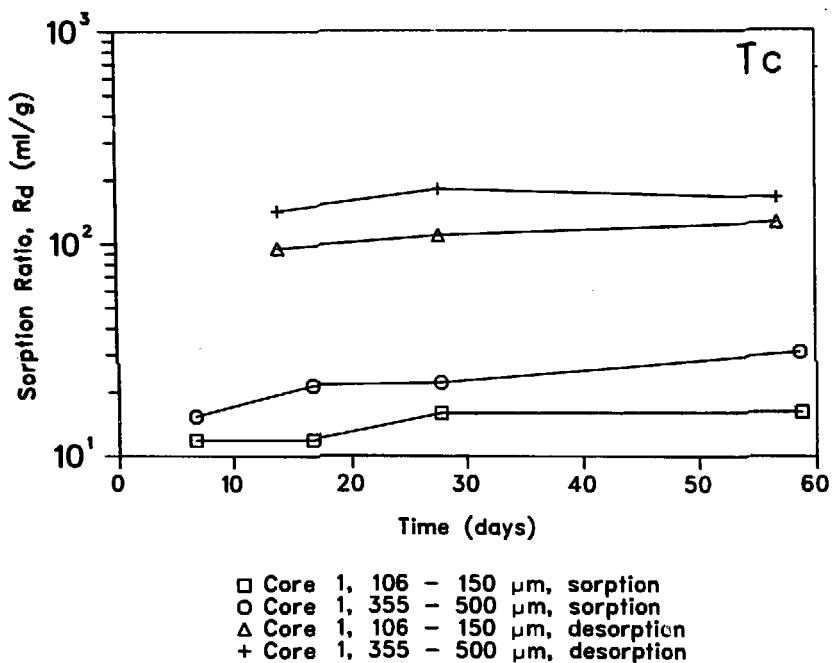


Fig. 31. Technetium sorption-desorption ratio data, ambient temperature.

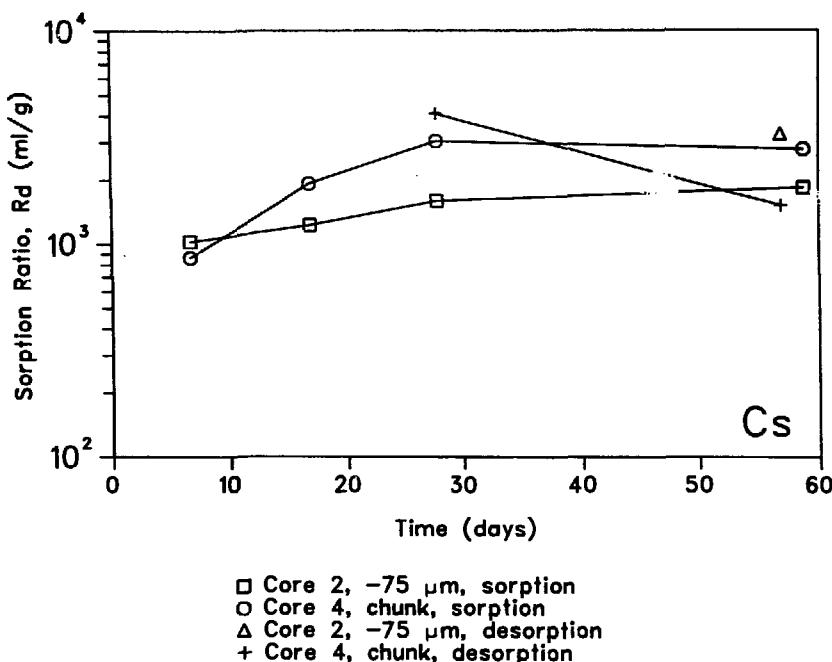
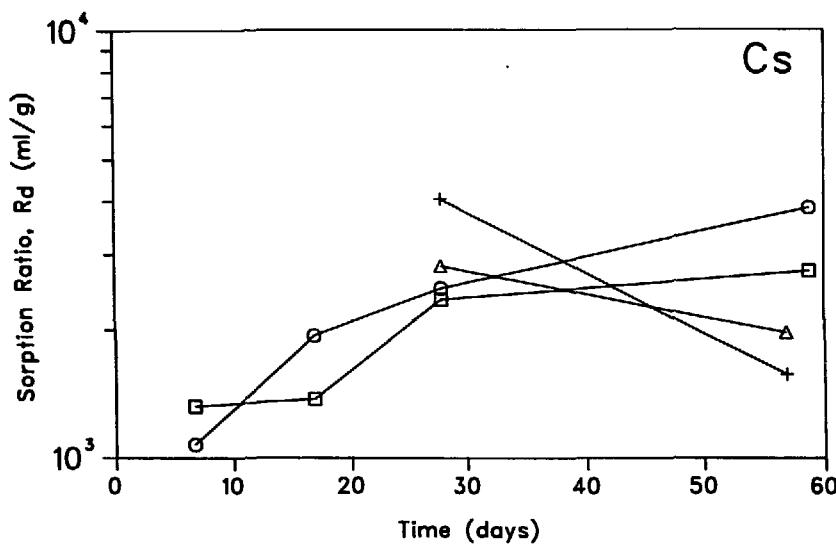


Fig. 32. Cesium sorption-desorption ratio data, ambient temperature.

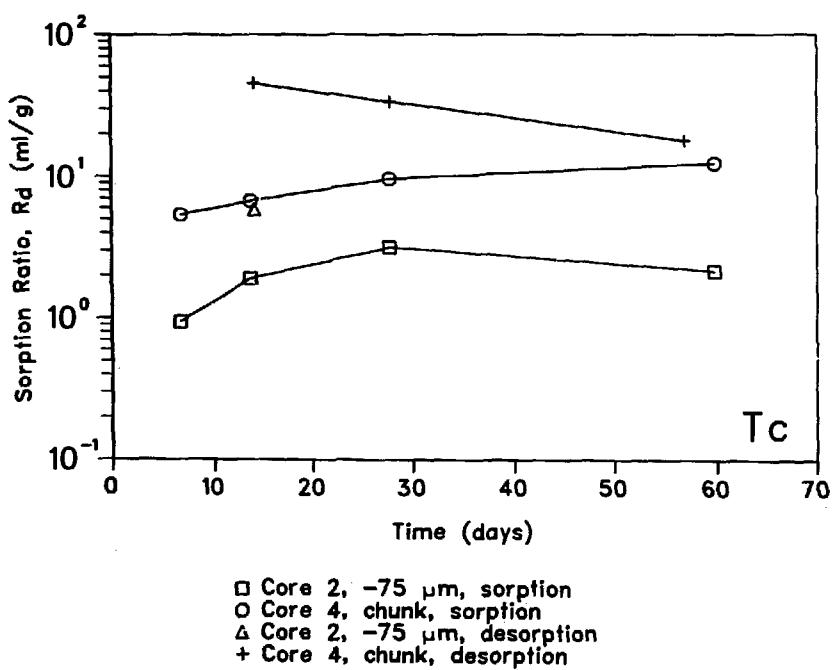
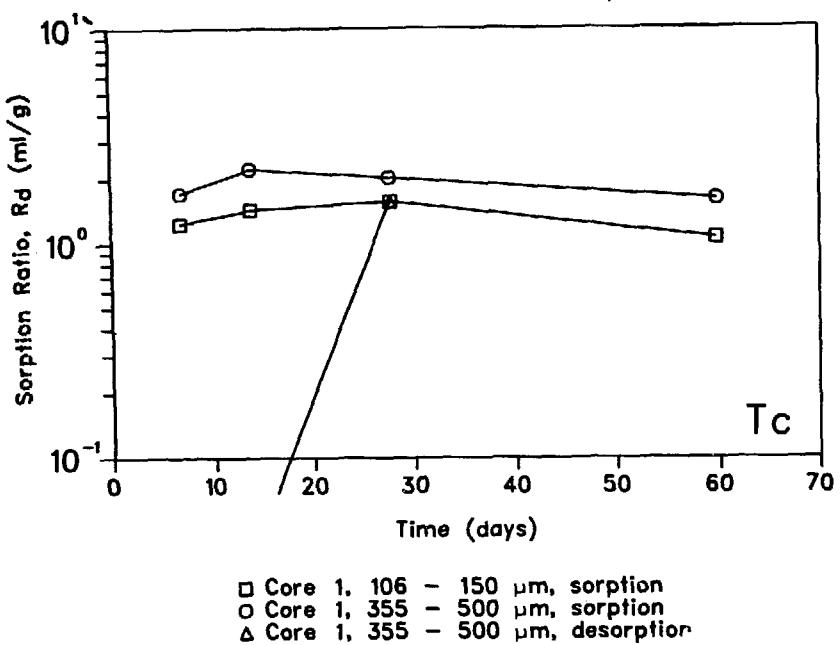


Fig. 33. Technetium sorption-desorption ratio data,  $70^{\circ}\text{C}$ .

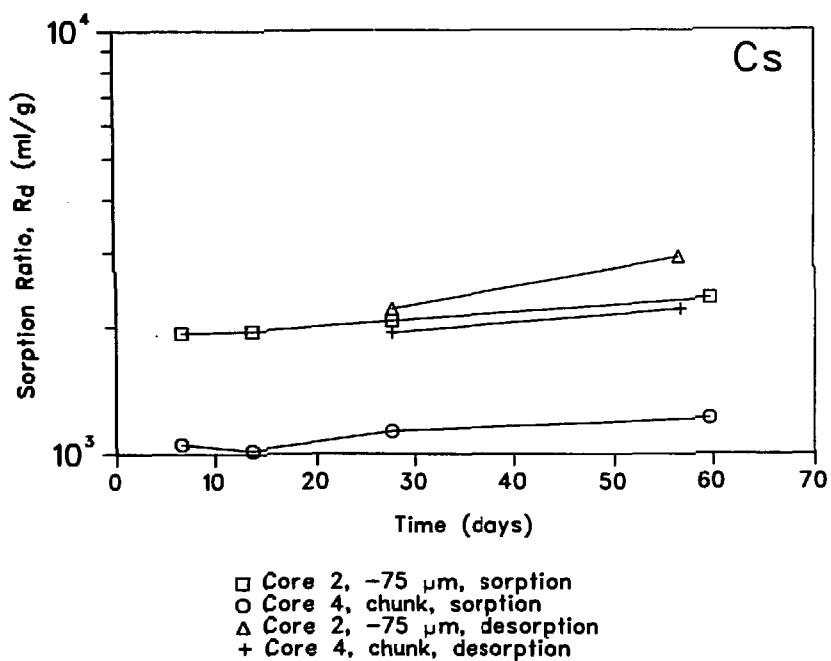
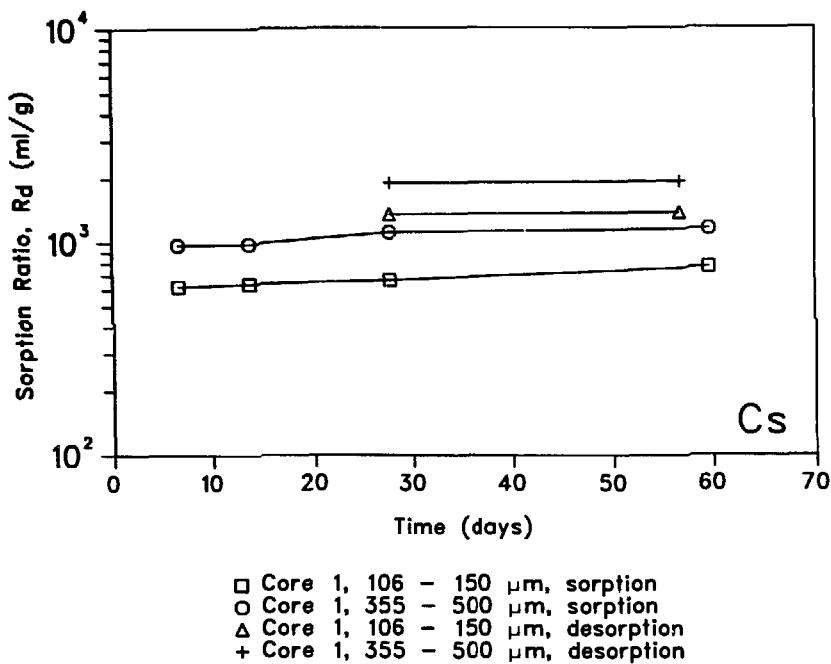


Fig. 34. Cesium sorption-desorption ratio data, 70°C.

however, than the earlier results. The agreement between the sets is encouraging since a different batch of water was used and the sieved fractions had been stored for several months between the two sets of experiments. One could expect some dehydration of the samples with time that could lead to changes in the mineralogy.

The mean sorption ratios for technetium for all measurements are  $47 \pm 15$   $\text{mL/g}$  and  $3.4 \pm 0.8$   $\text{mL/g}$  for the ambient and  $70^\circ\text{C}$  conditions, respectively. Similarly, the mean sorption ratios for cesium for these experiments are  $2270 \pm 940$   $\text{mL/g}$  and  $1580 \pm 690$   $\text{mL/g}$  for the two temperature conditions.

## V. SUMMARY

Table XXVI summarizes representative sorption ratios for each of the elements studied at ambient ( $22 \pm 2^\circ\text{C}$ ) and elevated ( $70 \pm 1^\circ\text{C}$ ) temperature.

## ACKNOWLEDGMENTS

The authors wish to thank A. R. Lappin and R. G. Dosch of the Sandia Laboratories for providing the Eleana argillite cores and for the water analysis and formulation.

Similarly, we wish to acknowledge R. J. Serne (Battelle Pacific Northwest Laboratory) and J. J. Hines (Argonne National Laboratory) who provided the  $^{95m}\text{Tc}$  utilized in this study.

The authors wish to thank D. C. Hoffman for many fruitful discussions and valuable advice. The authors also wish to acknowledge the following Los Alamos Scientific Laboratory personnel for the efforts mentioned: J. R. Smyth and R. M. Vidale (petrography), R. E. Honnell (size distribution analyses and BET surface area measurements), P. A. Elder and M. E. Lark (sample counting and  $\gamma$ -spectral analyses), A. E. Norris and R. E. Honnell (BET surface area and particle size analyses), and E. F. Willow and L. M. Wagoner (typing of drafts and final manuscript).

TABLE XXVI  
REPRESENTATIVE SORPTION RATIOS (mℓ/g)

Element	22 ± 2°C		70 ± 1°C	
	Sorption	Desorption	Sorption	Desorption
Sr	135 ± 10	126 ± 14	322 ± 37	268 ± 36
Tc(VII)	47 ± 15		3.4 ± 0.8	17 ± 8
Cs	1990 ± 120	3610 ± 210	1580 ± 90	2680 ± 140
Ba	3920 ± 710	5240 ± 790	13 200 ± 3000	31 300 ± 6700
Ce(III)	41 900 ± 6400	86 400 ± 14 000	10 800 ± 2500	17 400 ± 3900
Eu(III)	36 000 ± 5100	89 200 ± 6000	11 400 ± 2300	42 700 ± 7400

## REFERENCES

1. E. R. Thomkins and S. W. Mayer, "Ion Exchange as a Separations Method III. Equilibrium Studies of the Reactions of Rare Earth Complexes with Synthetic Ion Exchange Resins," *J. Am. Chem. Soc.* 69, 2859 (1947); "Ion Exchange as a Separations Method IV. Theoretical Analysis of The Column Separations Process," *J. Am. Chem. Soc.* 69, 2866 (1947).
2. J. F. Relyea, Di Rai, and R. J. Serne, "Interaction of Waste Radionuclide with Geomedia: Program, Approach, and Progress," *Proceedings of the Symposium on Science Underlying Radionuclide Waste Management, Materials Research Society*, Boston, Massachusetts, November 28-December 1, 1978.
3. G. H. Higgins, "Evaluation of the Ground-Water Contaminants Hazard from Underground Nuclear Explosions," *J. Geophys. Res.* 64, 1509 (1959).
4. D. H. Lester, G. Jansen, and H. C. Burkholder, "Migration of Radionuclide Chains Through an Absorbing Medium," in *Adsorption and Ion Exchange*, I. Zwiebel and N. H. Sweed, Eds. (AIChE Symposium Series 152, No. 71, New York, 1975) 202-213.
5. K. Wolfsberg, "Sorption-Desorption Studies of Nevada Test Site Alluvium and Leaching Studies of Nuclear Test Debris," *Los Alamos Scientific Laboratory report LA-7216-MS* (1978).
6. H. Cramer, *Mathematical Methods of Statistics* (Princeton University Press, 1946), p. 181.
7. S. Brunauer, P. H. Emmett, and R. Teller, "Adsorption of Gases in Multi-molecular Layers," *J. Am. Chem. Soc.* 60, 309 (1938).
8. R. S. Dyal and S. B. Hendricks, "Total Surface of Clays in Polar Liquids as a Characteristic Index," *Soil Sci.* 69, 421 (1950).

9. C. A. Bower and J. O. Goertzen, "Surface Area of Soils and Clays by an Equilibrium Ethylene Glycol Method," *Soil Sci.* 87, 289 (1959).
10. B. L. McNeal, "Effect of Exchangeable Cations on Glycol Retention by Clay minerals," *Soil Sci.* 97, 96 (1964).
11. D. Rhai and R. J. Serne, "Solid Phases and Solution Species of Different Elements in Geologic Environments," Battelle Pacific Northwest Laboratory report PNL-2651 (March 1978).