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DEVELOPMENT OF A TEMPORALLY AND SPATIALLY
RESOLVED GRAZING INCIDENCE SPECTROMETER*

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Abstract

In this report we present design considerations for a grazing incidence spectrometer which will resolve both temporally and spatially the emission from a wide variety of plasmas. The basis of the design involves use of microchannel plates (MCPs) which are curved to conform to the Rowland circle of the spectrometer. The spectra are obtained when the anode is properly biased. The use of multiple anodes allows gating and with appropriate delays results in sequential time resolution of a few nanoseconds. Simultaneous gating of the anodes with spatial resolution of $<100\mu$ for any given time frame can also be obtained. The efficiency of this spectrometer is also compared with conventional grazing incidence spectrometers.

Introduction

We have been using grazing incidence spectrometers (GIS) as diagnostic tools for studying a wide variety of plasmas, looking at both line and continuum radiation. These spectrometers offer excellent spectral resolution ($\Delta\lambda/\lambda=10^{-3} - 10^{-4}$) and the grazing incidence geometry gives reflectivity in the 10-500Å range not attainable with any other instrument. The standard operating modes for this instrument are as a scanning monochromator, which uses time-dependent photon counting techniques, but integrated over a narrow wavelength range, and as a spectrograph which utilizes film to offer maximal resolution over a very broad spectral range but has decreased sensitivity and necessitates long integrated measurements. To incorporate the advantages of both of these modes of operation we are currently assembling a camera GIS which will allow us to acquire spectra over a wide spectral range (10-1000Å) with excellent resolution in a photon counting mode with equal rates, time range and spectral resolution.

The system incorporates a camera GIS and a multi-channel complement of detectors with interchangeable mounts. The detection system is a vacuum tube multi-channel plate (MCP) which will have a channel count capability of 1000 or more channels (see Fig. 1). The 100 channel width MCP will be mounted with several interchangeable probe strips as shown in Fig. 2 which can be gated in a time range to measure the increased sensitivity (with or without spatial resolution), or sequentially yielding time resolved spectra. During a test run a high voltage pulser feeding the anodes (with a peak rate 100 Mc/sec) can be used in parallel or series with an array of timing devices, changing the geometry as table as shown in Fig. 3. The output electron gun then projects the used onto a phosphor whose light output is guided by a fiber optic up to the film plane where standard films can be used. An inverse

future development will be to replace the film with solid-state CCD's for increased sensitivity and direct on-line digital read out.

Sensitivity and Time Resolution

The pulsed spectrometer system works, in its most sensitive mode, by pulsing individual photons incident on each channel of the MCP while its anode is biased positively. A bias voltage of 1kV across the MCP gives rise to 1.5 x 10⁵ electrons per detected photon. Pulsing the anode at 5kV gives about 100 eV storage energy at the phosphor at

$$E = \frac{qV}{2} = \frac{1.6 \times 10^{-19} \times 5 \times 10^4}{2} = 4.0 \times 10^{-15} \frac{\text{ergs}}{\text{ph}} \times (1.6 \times 10^{-19} \frac{\text{J}}{\text{eV}})^{-1} = \frac{25 \text{ ergs}}{(\text{ph-ph})}$$

where ph is the photon efficiency for $P=11$ or $P=40$ phosphor is 10 percent of the total area of light written into the P aperture of the fibre. The area of the P aperture between .01 and .08 degrees' at the film plane is 1.57×10^{-4} cm² for a 100 μ fibre. A 100 μ Pan-X film exposed to .1 ph region gives a 100 μ area of 1.57 x 10⁻⁴ cm² of film and 1.1 μ ph-ph-region. The 100 μ ph-ph-region is 1.57 x 10⁻⁴ cm² of light per region for a 100 μ ph-ph-region. The 100 μ ph-ph-region is 1.57 x 10⁻⁴ cm² of light per region for a 100 μ ph-ph-region.

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sensitivity with our current system (film only). To get a minimally detectable density of .1 using the most sensitive film (Kodak 101) requires $\approx 8 \times 10^6$ photons/cm². A typical resolution unit is approximately 10^{-2} cm x .5 cm or 5×10^{-3} cm², so 4×10^4 photons are needed per resolution unit for a minimum detectable signal. If the MCP detection efficiency is 1 percent we would get 400 counts (5 percent statistics) in the same resolution unit. A more reasonable MCP detection efficiency is 5 percent which implies an increase in detection sensitivity over 101 film of a factor of 100. In a given resolution unit there are 10^3 channels and each channel is capable of registering 10^2 electrons (or detecting 20 photons) before saturation. Thus, the instrument has at least three orders of magnitude dynamic range for a given resolution element.

In practical terms, this means that for an experiment involving a weakly emitting plasma that requires 10 counts to give a satisfactory time-integrated spectrum, the time resolution by a factor of 10 is now possible.

Finally, by using internationally experienced, well-trained¹ cameras and by using the state-of-the-art image technology suggested a list of a few camera and exposure times.

CONCLUSION

The response of the system can now be calculated for typical plasmas. In our case $\lambda_{p,500\text{\AA}}$, the plasma source spectral photon flux, is related to $\lambda_{p,500\text{\AA}}$, the number of counts/resolution unit by

$$N_{\text{counts}} = \lambda_{p,500\text{\AA}} \times \eta_{\text{MCP}} \times \eta_{\text{cam}} \times t \times \Omega$$

obtainable only if a mirror is not used, and is approximately $1 \times 10^{-8} \text{ cm}^2$ sr. If Ω_s calculated without a mirror is greater than Ω calculated with a mirror, one would not use a mirror. Typical values for the other parameters that determine n are

$$st = 2 \times 10^{-9} \text{ sec} - 2 \times 10^{-2} \text{ sec},$$

$$\lambda = .6 \text{ \AA} \text{ (im spectrometer, } 300 \text{ \AA/mm grating)}$$

$$\eta_{\text{opt}} = .01$$

$$R_g = .1$$

which gives $n = N_{\text{plasma}} \times st \times 6 \times 10^{-13} \text{ \AA cm}^2 \text{ sec sr}$ for a system which uses imaging optics.

Plasma sources can often be described as being optically thick blackbody radiators or optically thin line radiators. If we focus a blackbody radiator on the entrance slit of the spectrometer, N_{plasma} will be given by the Planck formula

$$N_{\text{plasma}}(\lambda) = \frac{2c}{4\pi hc/(\lambda^4 - 1)} \frac{\text{photons}}{\text{cm}^2 \text{ \AA sec sr}}$$

The maximum number of photons detected in a wavelength dispersive device will occur at a wavelength of

$$\lambda_{\text{max}} = 3.9 \text{ Kf/hc}$$

and the spectral photon radiance at this peak is given by (λ in μV)

$$N_{\text{plasma}}(\lambda_{\text{max}}) = 1.2 \times 10^{19} (\lambda)^4 \frac{\text{photons}}{\text{cm}^2 \text{ \AA sec sr}}$$

Assuming that such a source remains at a temperature T for a framing time of 10 nsec,

$$N = 10^{10} \lambda^{-1}$$

then implies that improved statistics could be obtained on a 3λ , 10 nsec emitter.

The calculations for spatially resolved spectroscopy. To do this we use a spectrograph (Fig. 1) and reduce the width of the slit from the .5 cm used in the Ω configuration. The magnification is the ratio of object to image distance, which is wavelength dependent.

To compute the number of counts/resolution unit detected in the portion of the entrance slit which images a given volume of plasma, Ω_y , one uses the same Ω for the nonspatially resolved case with a modified Ω (Fig. 4c)

$$\Omega = \Omega_{\Omega_y} \left(\frac{r_{\Omega_y}}{r_{\Omega}} \right)^2 \lambda_{\Omega}$$

where λ_{Ω} is the wavelength of the entrance slit

r_{Ω_y} = the spatially resolving slit width

r_{Ω} = distance to spatial resolution slit distance

r_{Ω_y} = distance to entrance slit distance

Ω_y = the surface area of the volume of

plasma being imaged visible to the

entrance slit.

Consider as an example, a 100μ diameter, 100eV, 10 nsec blackbody emitter, spatially resolved with a 10μ image defining slit placed 5 cm from the source and 40 cm from the spectrometer entrance slit. Using the same values at R_g , ϵ_{det} , and $\Delta\lambda$ as before, we get for the number of counts at the blackbody peak/resolution unit,

$$n_p = 1.2 \times 10^{15} \Omega$$

assuming an entrance slit width w of 10^{-3} cm

$$\Omega_{sc} = 1.4 \times 10^{-12} \text{ cm}^2 \text{ sr}$$

and $n_p = 1 \times 10^3$ counts/resolution unit imaged at the peak of the blackbody spectrum ($\approx 25\text{\AA}$). The spatial resolution at the source is limited to $\approx 10\mu$ (the diffraction limit is 5μ at $25\text{\AA}$) which for the above geometry gives a magnification of $16\times$ at the microchannel plate (assuming a 3600 lines/mm grating at 45° degree incidence). The spatial resolution limit is the 2×10^4 elements that make up the vertical dimensions of the MCP for large objects, and the defining optics or slit size (keeping in mind the diffraction limit for longer wavelengths) for small objects magnified on the exit plane. A practical limit is probably 10μ .

An alternative mentioned above to the use of a cross slit for position sensitive information is a cylindrical mirror which would focus in the non-analyzing plane. This case gives much higher sensitivity at wavelengths above $500\text{\AA}$ and could be used if necessary in this region.

For an optically thin line radiator, approximately 10 counts are necessary to detect a line peak. Taking into account the 1 percent quantum efficiency of the MCP and 10 percent diffraction efficiency of the grating, this requires 10^4 photons incident on the grating. To resolve one millisecond this requires 10^7 photons/sec incident on the grating. The number of ions viewed, N_{ion} , is given by

$$N_{ion} = R \int n_i dl$$

where Ω is the acceptance angle of the spectrometer, R is the entrance slit to plasma distance, and $\int n_i dl$ is the integral of the ion density along the line of sight at the spectrometer. On the average, each ion will emit $\frac{\Omega A_{slit}}{4\pi}$ photons into the grating, where A_{slit} is the entrance slit area and R is again the plasma to entrance slit distance.

The brightness of a source minimally detectable with a 1 millisecond exposure time is then given by

$$\text{brightness} = N_{ion} \frac{A_{slit}}{4\pi R^2} = 1 \times 10^7 \frac{\text{photons}}{\text{sec}} \cdot \frac{\Omega A_{slit}}{4\pi} \int n_i dl$$

$$\frac{\text{brightness}}{\int n_i dl} = .04 \text{ photons/sec/sr}$$

where $\Omega = 10^{-3}$ rad and $A_{slit} = 10^{-3} \text{ cm}^2$. Thus for application to plasmas like the Tandem Mirror experiment at Livermore most of the common impurities could easily be resolved on a millisecond time scale.

Conclusion

We have shown that time resolved (high resolution) spectroscopy is possible in the 10 to 1000Å region using a grazing incidence spectrometer and pulsed channel plates. The system places very modest requirements on plasma brightness for efficient detection, and can be used in many different plasma regimes with lifetimes between 10^{-9} and 10^{-2} sec.

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Figure Captions

- Fig. 1. Schematic of the detector fitted with a microchannel plate.
- Fig. 2. Enlarged cross section of the detector showing the five anode strips.
- Fig. 3. Space pulse diagram; delays and pulse widths are determined by pulse lengths.
- Fig. 4. Spectrometer solid angles: a) with mirror to fill the optics, b) without mirror, c) with a position defining slit.



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Figure 1. Map of the study area.

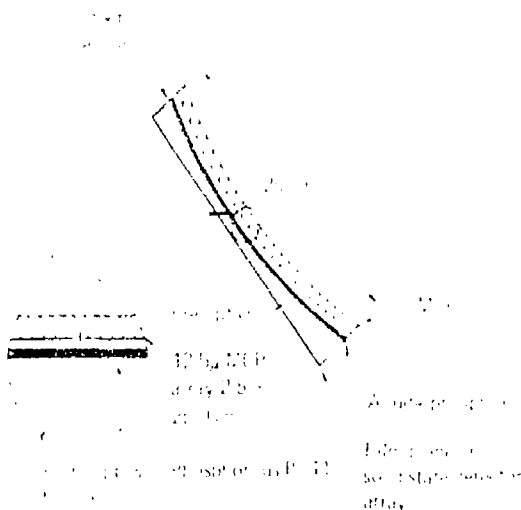
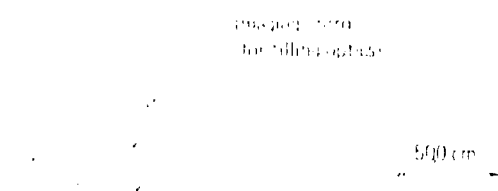


Figure 2

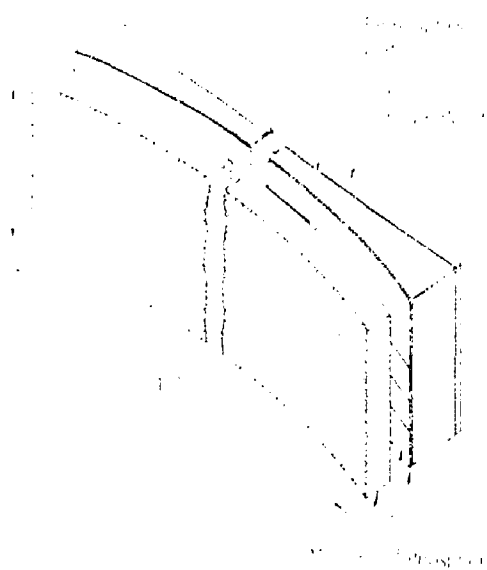


Figure 1
Box with lid

Figure 1

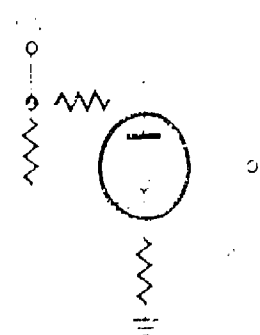


Figure 1

The circuit shown in Figure 1 is a simple resistive network. The central component is a voltage source or a dependent source, indicated by the horizontal line. The resistors are connected in a way that allows for the calculation of the current through the central component.

The circuit is analyzed using the following steps:

$$I = \frac{V}{R}$$

$$R = R_1 + R_2 + R_3$$

$$I = \frac{V}{R_1 + R_2 + R_3}$$

$$I = \frac{V}{R_1 + R_2 + R_3} = \frac{10V}{10\Omega + 10\Omega + 10\Omega} = \frac{10V}{30\Omega} = \frac{1}{3}A$$

Figure 1



Figure 4

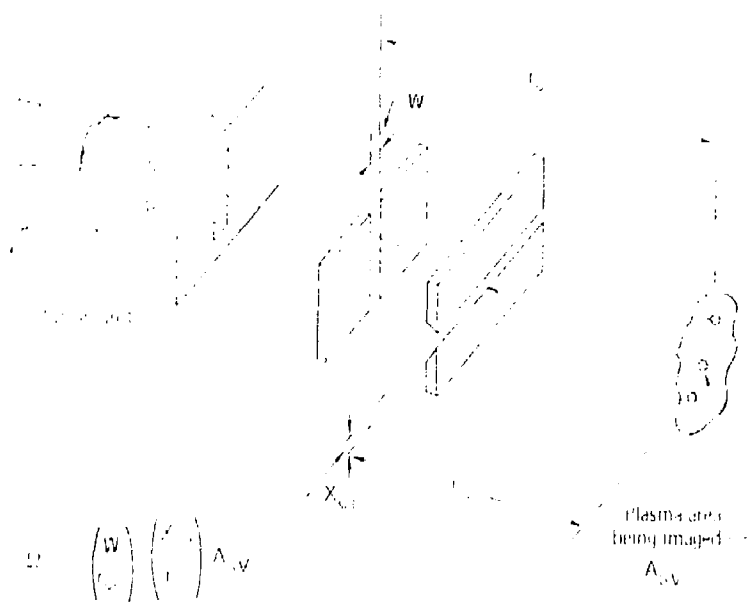


Figure 5