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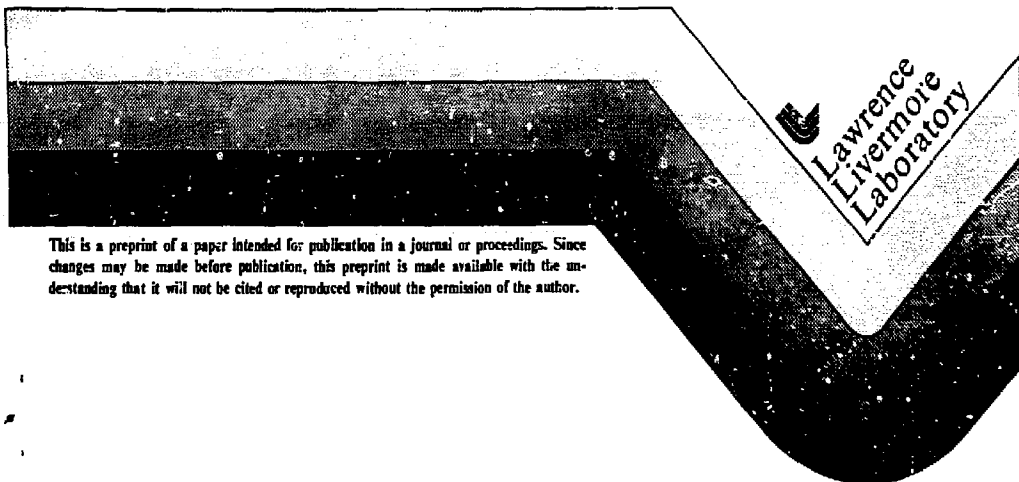
A Review of 1064-nm Damage Tests of
Electron-Beam Deposited $\text{Ta}_2\text{O}_5/\text{SiO}_2$
Antireflection Coatings

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A Review of 1064-nm Damage Tests of Electron-Beam Deposited
 $\text{Ta}_2\text{O}_5/\text{SiO}_2$ Antireflection Coatings

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ABSTRACT

Damage tests of $\text{Ta}_2\text{O}_5/\text{SiO}_2$ antireflection films deposited under a variety of conditions showed that thresholds of films deposited at 175 C were greater than thresholds of films deposited at either 250 C or 325 C. Deposition at high rate and low oxygen pressure produced highly absorptive films with low thresholds. Thresholds did not correlate with film reflectivity or net stress in the films, and correlated with film absorption only when the film absorption was greater than 10^4 ppm. Baking the films for four hours at 400 C reduced film absorption, altered net film stress, and produced an increase in the average damage threshold.

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1. Introduction

This study was conducted to determine the influence of deposition parameters on laser damage thresholds of silica/tantala antireflection (AR) coatings, and to determine what, if any, correlation exists between damage threshold and 1) the substrate material and the method of substrate polishing, 2) the net film stress, 3) the average absorption of the film, and 4) the reflectivity of the film.

2. Samples

The samples were four-layer silica/tantala AR films deposited by electron-beam evaporation. An undercoat¹ layer of silica with an optical thickness of a halfwave at 1064-nm was deposited between the AR film and the substrate.

Three sets of coatings were produced. The first set (A) of coatings was deposited in separate runs under each of eighteen different deposition conditions corresponding to the unique combinations of three deposition temperatures (175 C, 250 C and 325 C), three values of oxygen pressure during the deposition of the tantala layers (0.5×10^{-4} , 1.0×10^{-4} and 2.0×10^{-4} Torr) and two rates of deposition (1.5 Å/sec and 5 Å/sec). In each run, coatings were deposited on two fused silica substrates to be used for damage samples, and on thin fused silica substrates to be used in measurements of coating stress and absorption. These eighteen runs were then repeated to provide information on the reproducibility of the results. These repeat samples constitute the second set (B) of coatings.

The third set (C) of samples was fabricated after damage tests of coatings in sets A and B indicated that the optimum deposition parameters were a substrate temperature of 175 C, an oxygen pressure of 1×10^{-4} Torr, and a rate of 1.5 Å/sec. Using these deposition parameters, three additional coating runs were made. In each of these runs, coatings were deposited onto two conventionally polished fused silica substrates, two conventionally polished BK-7 glass substrates, and two bowl-feed polished BK-7 substrates.

Substrates were made of Suprasil II fused silica (a product of Amersil, Inc.) or PH-3 quality BK-7 glass. Bowl-feed polishing was done by Optical Coating Laboratory, Inc. In the bowl-feed process, the slurry is recirculated and breaks into successively finer particles.² Details of the process are proprietary and may vary among vendors. Conventional polishing was done by Zygo, Inc., using standard fresh-feed procedures specified by LLNL for high power laser components.

3. Data and Discussion

Laser-damage thresholds were measured³ with 1-ns, 1064-nm pulses focused to provide an approximately Gaussian beam which was 2.5 mm in diameter at the sample surface. Each test site on a sample was irradiated once. The sites were examined and photographed before and after irradiation, using a Nomarski microscope at a magnification of 100 X. Damage was defined to be any permanent alteration of the surface that was detectable by the Nomarski inspection.

For each shot, we recorded the beam profile and the pulse energy, and computed the peak on-axis fluence. Threshold was defined to be midway between the lowest fluence that caused damage and the highest fluence that caused no damage.

Damage thresholds for samples in sets A and B are shown in Table 1. Films deposited at 175 C had thresholds that were generally greater than thresholds of films deposited at 250 C or 325 C. The films with the lowest thresholds were those deposited at the greatest rate (5 Å/sec) and lowest oxygen pressure (0.5×10^{-4} Torr).

Thresholds for samples in set C are given in Table 2 and summarized in Table 3. For both fused silica and BK-7 substrates, thresholds were greatest for films deposited on bowl-feed-polished surfaces.⁴

The absorption and net stress of the films in sets A and B were determined by measurements made on thin witness samples that were coated in each run. Film absorption was measured by laser calorimetry.⁵ Net stress was determined by using a Fizeau interferometer to measure stress-induced deformation⁶ of the witness. Measured values of stress and absorption are given in Table 4. Absorption was largest for films deposited at the higher rate and at low oxygen pressure, which suggests that the absorption was due to incomplete oxidation of the film materials. Net stress was greater in films deposited at 175 C than in films deposited at either 250 C or 325 C, but not strongly dependent on either deposition rate or oxygen pressure.

After these initial tests, we baked a subset of the films in air for four hours at 400 C and remeasured the damage threshold, absorption, and stress. Values measured before and after baking are shown in Table 5.

As a result of the bake, stress was reduced in magnitude and converted from compressive to tensile. Absorption was greatly reduced in some films and thresholds were, on the average, slightly increased. However, inspection of the data in Table 5 indicates slight, if any, correlation between thresholds and either net stress or film absorption in either baked or unbaked films.

Finally, a Beckman DK2A two-beam spectrophotometer was used to measure the reflectance of each film in sets A and B. Reflectance values ranged from 0.01 to 0.18 percent except for one film with large absorption whose reflectance was 0.33 percent. This demonstrates that, low reflectance can be obtained in films deposited under a variety of deposition conditions; however, measurement of reflectance does not identify films with high damage thresholds.

4. Conclusions

Thresholds of silica/tantala antireflection films deposited by electron-beam evaporation on bowl-feed polished silica substrates were greatest when the films were deposited at low temperature (175 C) at low rate (1.5 Å/sec), and in the presence of adequate oxygen (1×10^{-4} Torr). Thresholds did not correlate with the measured net stress or the film reflectance, and correlated with film absorption only when the film absorption was greater than 10^4 ppm. Baking films for four hours at 400 C reduced film absorption, altered film stress, and produced some increase in the average damage threshold.

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References

1. Apfel, J. H.; Enemark, E. A.; Milam, D.; Smith, W. L.; and Weber, M. J., The Effects of Barrier Layers and Surface Smoothness on 150-ps, 1.064- μ m Laser Damage of AR-Coatings on Glass; Laser-Induced Damage to Optical Materials: 1977, proceedings of the 1977 Boulder Damage Conference, NBS Spec. Publ. 509, p. 255-260 (1977).
2. Dietz, R. W.; and Bennett, J. M., Bowl-feed Technique for Producing Supersmooth Optical Surfaces; Appl. Opt.(5): 881-882; 1966.
3. Lowdermilk, W. H.; and Milam, D., Laser-Induced Surface and Coating Damage; IEEE J. Quant. Elect. QE-17; 1888-1903; 1981.
4. Lowdermilk, W. H.; Milam, D.; and Rainer, F., Damage to Coatings and Surfaces by 1.06- μ m Pulses; Laser-Induced Damage to Optical Materials: 1979, proceedings of the 1979 Boulder Damage Conference, NBS Spec. Publ. 568, p. 391-403 (1980).
5. Allen, T. H.; Apfel, J. H.; and Carniglia, C. K., A 1.06- μ m Laser Absorption Calorimeter for Optical Coatings; Laser-Induced Damage to Optical Materials: 1978, proceedings of the 1978 Boulder Damage Conference, NBS Spec. Publ. 541, p. 33-36 (1978).

6. Ledger, A. M.; and Batista, R. C., Intrinsic and Thermal Stress Modeling for Thin-Film Multilayers; Laser-Induced Damage to Optical Materials: 1977, proceedings of the 1977 Boulder Damage Conference, NBS Spec. Publ. 509, p. 230-244 (1977).

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Table 1.

Damage Thresholds (1-ns, 1064-nm) of Ta₂O₅/SiO₂ AR coatings with $\lambda/2$ SiO₂ undercoats deposited onto bowl-feed polished fused silica at three substrate temperatures, three oxygen pressures, and two deposition rates.

| Deposition Rate (Å/s) | O ₂ Pressure x10 ⁻⁴ Torr | Substrate Temperature of 175 C | | Substrate Temperature of 250 C | | Substrate Temperature of 325 C | |
|--------------------------|---|-----------------------------------|-----------------------------------|-----------------------------------|-----------------------------------|-----------------------------------|-----------------------------------|
| | | Sample* | Threshold (J/cm ²) | Sample | Threshold (J/cm ²) | Sample | Threshold (J/cm ²) |
| 1.5 | 0.5 | A-1a | 13.0 ± 3.0 | A-4a | 7.1 ± 0.7 | A-7a | 6.6 ± 0.7 |
| | " | A-1b | 9.6 ± 1.0 | A-4b | 6.6 ± 1.0 | A-7b | 6.8 ± 1.0 |
| | " | B-1 | 9.0 ± 1.4 | B-4 | 5.7 ± 1.3 | B-7 | 3.5 ± 0.4 |
| " | 1.0 | A-2a | 18.7 ± 1.9 | A-5a | 6.9 ± 0.7 | A-8a | 4.7 ± 0.5 |
| | " | A-2b | 14.9 ± 1.5 | A-5b | 8.0 ± 0.8 | A-8b | 8.1 ± 0.8 |
| | " | B-2 | 10.3 ± 1.0 | B-5 | 6.1 ± 1.4 | B-8 | 6.3 ± 0.7 |
| " | 2.0 | A-3a | 12.9 ± 1.4 | A-6a | 6.7 ± 0.7 | A-9a | 6.6 ± 0.7 |
| | " | A-3b | 9.5 ± 1.5 | A-6b | 11.0 ± 1.1 | A-9b | - |
| | " | B-3 | 11.1 ± 1.2 | B-6 | 7.3 ± 0.9 | B-9 | 5.8 ± 0.9 |
| 5.0 | 0.5 | A-10a | 7.1 ± 0.8 | A-13a | 2.2 ± 0.3 | A-16a | 1.8 ± 0.6 |
| | " | A-10b | 6.8 ± 0.9 | A-13b | 3.0 ± 0.4 | A-16b | - |
| | " | B-10 | 4.9 ± 1.3 | B-13 | 6.0 ± 0.6 | B-16 | 3.9 ± 0.5 |
| " | 1.0 | A-11a | 6.7 ± 1.0 | A-14a | 5.3 ± 0.5 | A-17a | 5.4 ± 0.7 |
| | " | A-11b | 6.9 ± 0.7 | A-14b | 8.0 ± 0.8 | A-17b | 5.5 ± 0.6 |
| | " | B-11 | 9.0 ± 1.0 | B-13 | 6.9 ± 0.9 | B-17 | 5.9 ± 0.8 |
| " | 2.0 | A-12a | 11.3 ± 1.1 | A-15a | 9.5 ± 1.4 | A-18a | 6.5 ± 0.6 |
| | " | A-12b | 9.3 ± 1.2 | A-15b | 8.5 ± 0.8 | A-18b | 6.4 ± 0.6 |
| | " | B-12 | 5.5 ± 1.0 | B-15 | 5.1 ± 0.5 | B-18 | 5.5 ± 0.8 |

*Samples are designated by a symbol which indicates the coating set (A or B), the particular coating run (1 through 18), and an additional designator (a or b) to distinguish two parts made in a single coating run.

Table 2

Damage thresholds (1-ns, 1064-nm) of Ta₂O₅/SiO₂ AR coatings with $\lambda/2$ SiO₂ undercoats deposited on three types of substrates at T = 175 C, Rate = 1.5 Å/sec, and O₂ pressure = 1.0 x 10⁻⁴ torr. Eighteen coatings were made in three separate runs.

| Sample* | Substrate Material | Substrate Polish | Damage Threshold (J/cm ²) |
|---------|--------------------|------------------|---------------------------------------|
| C1-a | fused silica | conventional | 9.2 ± 0.9 |
| C1-b | " | " | 6.8 ± 1.3 |
| C1-c | BK-7 | " | 5.5 ± 0.9 |
| C1-d | " | " | 8.5 ± 1.2 |
| C1-e | " | bowl feed | 6.3 ± 0.6 |
| C1-f | " | " | 9.0 ± 1.0 |
| C2-a | fused silica | conventional | 5.8 ± 1.0 |
| C2-b | " | " | 3.7 ± 0.6 |
| C2-c | BK-7 | " | 7.0 ± 0.8 |
| C2-d | " | " | 5.8 ± 0.6 |
| C2-e | " | bowl feed | 10.2 ± 1.0 |
| C2-f | " | " | 13.1 ± 1.3 |
| C3-a | fused silica | conventional | 9.4 ± 1.0 |
| C3-b | " | " | 11.4 ± 1.2 |
| C3-c | BK-7 | " | 6.0 ± 0.8 |
| C3-d | " | " | 7.7 ± 0.8 |
| C3-e | " | bowl feed | 7.7 ± 0.8 |
| C3-f | " | " | 11.3 ± 1.2 |

*Sample designation indicates the coating run (C1, C2 or C3) and the particular substrate (a-f).

Table 3.

Summary of damage threshold data (1-ns, 1064-nm) for Ta₂O₅/SiO₂ AR coatings with $\lambda/2$ SiO₂ undercoats deposited on four types of surfaces. (T = 175 C, rate = 1.5 Å/sec, O₂ pressure = 1×10^{-4} Torr)

| Material | Polish | Number of Samples | Median Threshold (J/cm ²) | Range of Observed Thresholds (J/cm ²) |
|--------------|--------------|-------------------|---------------------------------------|---|
| fused silica | bowl-feed | 3 | 14.9 | 10.3 - 18.7 |
| BK-7 | " | 6 | 9.6 | 6.3 - 13.1 |
| fused silica | conventional | 6 | 8.0 | 3.7 - 11.4 |
| BK-7 | " | 6 | 6.5 | 5.5 - 8.5 |

Table 4.

Coating absorption and net coating stress measured from witness samples coated in the eighteen coating runs comprising set A.

| Deposition Rate (Å/sec) | Substrate Temperature (C) | O ₂ Pressure (x10 ⁻⁴) Torr | Absorption (ppm) | | Net Stress (KPSI) | |
|----------------------------|------------------------------|--|------------------|-------|-------------------|-------|
| | | | Set A | Set B | Set A | Set B |
| 1.5 | 175 | 0.5 | 100 | 67 | 50 | 46 |
| " | " | 1.0 | 365 | 166 | 49 | 48 |
| " | " | 2.0 | 91 | 79 | 34 | 44 |
| " | 250 | 0.5 | 573 | 88 | 48 | 45 |
| " | " | 1.0 | 54 | 41 | 48 | 45 |
| " | " | 2.0 | 27 | 46 | 37 | 41 |
| " | 325 | 0.5 | 308 | 1770 | 37 | 47 |
| " | " | 1.0 | 38 | 22 | 38 | 40 |
| " | " | 2.0 | 26 | 29 | - | 46 |
| 5.0 | 175 | 0.5 | 2770 | 547 | 53 | 61 |
| " | " | 1.0 | 1730 | 1030 | 53 | 62 |
| " | " | 2.0 | 2180 | 1390 | 53 | 57 |
| " | 250 | 0.5 | 9450 | 4620 | - | 52 |
| " | " | 1.0 | 294 | 898 | 47 | 47 |
| " | " | 2.0 | 2240 | 46 | 49 | 48 |
| " | 325 | 0.5 | 23000 | 2300 | 26 | 25 |
| " | " | 1.0 | 39 | 44 | 39 | - |
| " | " | 2.0 | 27 | 692 | 49 | 44 |

Table 5.

Damage thresholds (1-ns, 1064-nm), net stress and absorption for fourteen Ta₂O₅/SiO₂ AR coatings measured before and after the coatings were baked in air for four hours at 400 C.

| Sample* | Rate (Å/sec) | Deposition Temp (C) | O ₂ Pressure (x10 ⁻⁴ Torr) | Thresholds(J/cm ²) | | Net Stress*(KPSI) | | Absorption(ppm) | |
|---------|-----------------|------------------------|---|--------------------------------|----------|-------------------|-------|-----------------|-------|
| | | | | pre-bake | baked | pre-bake | baked | pre-bake | baked |
| A-1a | 1.5 | 175 | 0.5 | 13.0±3.0 | 17.4±2.0 | 50 | -12 | 100 | 16 |
| A-3a | " | " | 2.0 | 12.9±1.4 | 20.1±2.0 | 34 | -1 | 91 | 20 |
| A-4a | " | 250 | 0.5 | 7.1±0.7 | 4.7±0.5 | 48 | -16 | 573 | 22 |
| A-5a | " | " | 1.0 | 6.9±0.7 | 7.6±0.8 | 48 | -13 | 54 | 22 |
| A-6a | " | " | 2.0 | 6.7±0.7 | 12.7±1.8 | 37 | -1 | 27 | 25 |
| A-7a | " | 325 | 0.5 | 6.6±0.7 | 6.8±0.7 | 37 | -14 | 308 | 23 |
| A-8a | " | " | 1.0 | 4.7±0.5 | 5.0±0.8 | 38 | -15 | 38 | 30 |
| A-10a | 5.0 | 175 | 0.5 | 7.1±0.8 | 8.4±0.8 | 53 | -17 | 2770 | 43 |
| A-11a | " | " | 1.0 | 6.7±1.0 | 9.0±1.0 | 53 | -16 | 1730 | 31 |
| A-12a | " | " | 2.0 | 11.3±1.1 | 13.0±1.3 | 53 | -10 | 2180 | 12 |
| A-14a | " | 250 | 1.0 | 5.3±0.5 | 3.9±0.7 | 47 | -20 | 294 | 41 |
| A-15a | " | " | 2.0 | 9.5±1.4 | 4.9±1.2 | 49 | -18 | 2240 | 30 |
| A-17a | " | 325 | 1.0 | 5.4±0.7 | 5.6±0.6 | 39 | -14 | 39 | 26 |
| A-18a | " | " | 2.0 | 6.5±0.6 | 6.1±0.8 | 49 | -13 | 27 | 11 |

* By convention, a positive value indicates compressive stress and a negative value indicates tensile stress.