

**The CSRL-V ENDF/B-V 227-Group Neutron Cross-Section Library
and Its Application to Thermal-Reactor and
Criticality Safety Benchmarks***

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CONF-820566--6

DE82 017497

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- * Research was sponsored by (1) the Office of Nuclear Regulatory Research and the Office of Nuclear Material Safety and Safeguards, U. S. Nuclear Regulatory Commission under Interagency Agreements DOE 40-550-75 and 40-549-75, (2) the Electric Power Research Institute under EPRI Contract RP 975-3, and (3) the U. S. Department of Energy under contract (W-7405-eng-26) with Union Carbide Corporation.

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ABSTRACT

Characteristics and contents of the CSRL-V (Criticality Safety Reference Library based on ENDF/B-V data) 227-neutron-group AMPX master and pointwise cross-section libraries are described. Results obtained in using CSRL-V to calculate performance parameters of selected thermal reactor and criticality safety benchmarks are discussed.

I. INTRODUCTION

The U. S. Nuclear Regulatory Commission sponsored the development of a pseudo-problem-independent, comprehensive, 227-neutron-group, cross-section library derived primarily from ENDF/B-V data. The library, designated CSRL-V (Criticality Safety Reference Library based on ENDF/B-V data),^{1,2} is a data base in AMPX master format³ for the subsequent generation of problem-dependent fine- and/or broad-group cross sections for a broad range of applications, including reactor core and shielding analyses, criticality safety analyses, and shipping cask calculations. The CSRL-V library is available from the Radiation Shielding Information Center (RSIC) at the Oak Ridge National Laboratory (ORNL).³ Characteristics of CSRL-V, including the recent expansion of the library to include Bondarenko factor data for unresolved resonance processing, are described in Section II.

Problem-dependent cross sections derived from CSRL-V data can be used with the SCALE⁴ system and with codes such as KENO-IV,⁵ ANISN,⁶ XSDRNPM,⁷ VENTURE,⁸ DOT,⁹ MORSE¹⁰ or any computer code which uses data in the traditional multigroup cross-section table format. CSRL-V data can be coupled with photon-production and photon-interaction multigroup data produced with the AMPX system³ to produce coupled neutron-gamma cross-section libraries. Modules of the AMPX system offer a full spectrum of cross-section processing capabilities for the CSRL-V data, including energy group collapsing, interpolating on Bondarenko factors for self-shielding of unresolved resonance data and temperature corrections, resonance processing with the Nordheim integral method, reformatting, editing, etc. The AMPX system is available from RSIC.¹¹

CSRL-V has been used in a variety of benchmark calculations. Among the thermal reactor benchmarks calculated were selected CSEWG and Babcock & Wilcox lattice critical experiments. Criticality safety benchmarks calculated included homogeneous, uranyl fluoride and uranyl nitrate spheres with hydrogen-to-uranium ratios varying from 76 to 972. Representative results from the series of CSRL-V benchmark calculations are discussed in Section III.

II. CHARACTERISTICS OF CSRL-V

Favorable experiences gained from the generation and utilization of an ENDF/B-IV fine-group cross-section library generated with the AMPX system for criticality safety, reactor, and shielding studies¹²⁻¹⁴ (CSRL, circa 1975) influenced the processing procedures, the selection of the group structure, and the point-to-multigroup weighting functions used to generate CSRL-V. Basic sources of nuclear data, specifications, processing system, library formats and contents, and first-order data checks of CSRL-V are described in subsections below.

¹The United States Department of Energy has determined that fine-group and/or pointwise data derived from ENDF/B-V will, for the present, be limited to users within the United States and AECL (Chalk River), except for data derived from the ENDF/B-V Standards, Dosimetry, Actinide (special purpose), and Fission Product Files, which are available to everyone.

II.A. Materials

A list of the master cross-section data sets in the CSRL-V 227-group library is given in Table. 1. The library contains data for approximately 130 materials, including processed data for all evaluations in the ENDF/B-V General Purpose File.¹⁵ In addition, cross sections for selected materials not in the latest edition of ENDF/B were prepared from LENDL data,^{16,17} e.g., Ar, ⁴⁵Sc, ⁶⁴Zn, Ga, Sn, ¹⁹¹Ir, and ¹⁹³Ir. Hydrogen with water- and polyethylene-bound thermal scattering kernels, deuterium with D₂O-bound thermal kernels, carbon with a graphite thermal kernel, a special 1/V data set normalized to unity at 0.0253 eV, and a dose factor data set were also included in the library.

II.B. Group Structure

The CSRL-V 227-neutron-group structure includes 79 thermal groups in the 10⁻⁵ to 3.00 eV range to accommodate the effects of low-energy resonance and thermal-neutron upscatter. The 148 groups in the 3-eV to 20-MeV range permit fine-group consideration of the resonance structure of prominent nuclei, the thresholds of important reactions, and various fission spectra. Specifically, boundaries were chosen to fit the reaction thresholds and major resonance levels of the following nuclides: Be, ¹⁰B, C, N, O, F, Na, Mg, Al, Si, K, Ca, Cr, Mn, Fe, Ni, Cu, Zr, Mo, Ag, Cd, In, Sn, Ba, Gd, Hf, Pb, ²³²Th, ²³³U, ²³⁴U, ²³⁵U, ²³⁶U, ²³⁸U, ²³⁸Pu, ²³⁹Pu, ²⁴⁰Pu, and ²⁴¹Pu.

Of the 148 epithermal groups, 58 groups span the fission-neutron-energy range from 20 MeV to 8.03 keV. This energy range includes most of the cross-section structure for the light and intermediate-mass nuclides. It also includes inelastic scattering and fission thresholds for certain of the heavy nuclides. The 90 groups between 8.03 keV and 3.00 eV were chosen to bracket major resonance levels in the intermediate-mass and heavy nuclides.

In the thermal energy range, several of the fuel and neutron absorbing nuclides have large resonances which are broad relative to the neutron energy exchange per collision. The closely-spaced thermal groups are designed to account for the effects of those resonances in the presence of thermal upscatter.

Table 1. (cont.)

Ship's Name		Lat	Long	Altitude	Cob	Height-Pressure ⁶	Described Between Reddoubt Solar Band ⁵		
Ship's Name	Lat	Long	Altitude	Cob	Height-Pressure ⁶	1-4 Transmissions in this Band ¹	2-4 Transmissions in this Band ²	Percentage (%)	
30000	1305	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1310	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1315	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1320	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1325	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1330	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1335	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1340	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1345	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1350	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1355	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1400	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1405	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1410	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1415	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1420	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1425	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1430	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1435	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1440	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1445	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1450	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1455	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1500	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1505	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1510	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1515	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1520	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1525	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1530	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1535	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1540	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1545	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1550	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
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30000	1705	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1710	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1715	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1720	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
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30000	1730	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1735	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
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30000	1745	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1750	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1755	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1800	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1805	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1810	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1815	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1820	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1825	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1830	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1835	31	140	140	140	1.2, 4.5, 16.37, 22.37, 28.10, 40.4, 46.4, 57.7, 73.4, 83.1, 140.7, 149.9	2.16, 17.27, 28.26, 34.4, 41.36, 100.0	46	
30000	1								

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Country		Year	Latitude	Longitude	Depth (m)	Number of Specimens	Number of Specimens Preserved	Number of Specimens Examined	Percentage (%)	Temperature (°C)
1	2	3	4	5	6	7	8	9	10	11
12	13	14	15	16	17	18	19	20	21	22
23	24	25	26	27	28	29	30	31	32	33
34	35	36	37	38	39	40	41	42	43	44
45	46	47	48	49	50	51	52	53	54	55
56	57	58	59	60	61	62	63	64	65	66
67	68	69	70	71	72	73	74	75	76	77
78	79	80	81	82	83	84	85	86	87	88
89	90	91	92	93	94	95	96	97	98	99
100	101	102	103	104	105	106	107	108	109	110
111	112	113	114	115	116	117	118	119	120	121
122	123	124	125	126	127	128	129	130	131	132
133	134	135	136	137	138	139	140	141	142	143
144	145	146	147	148	149	150	151	152	153	154
155	156	157	158	159	160	161	162	163	164	165
166	167	168	169	170	171	172	173	174	175	176
177	178	179	180	181	182	183	184	185	186	187
188	189	190	191	192	193	194	195	196	197	198
199	200	201	202	203	204	205	206	207	208	209
210	211	212	213	214	215	216	217	218	219	220
221	222	223	224	225	226	227	228	229	230	231
232	233	234	235	236	237	238	239	240	241	242
243	244	245	246	247	248	249	250	251	252	253
254	255	256	257	258	259	260	261	262	263	264
265	266	267	268	269	270	271	272	273	274	275
276	277	278	279	280	281	282	283	284	285	286
287	288	289	290	291	292	293	294	295	296	297
298	299	300	301	302	303	304	305	306	307	308
309	310	311	312	313	314	315	316	317	318	319
320	321	322	323	324	325	326	327	328	329	330
331	332	333	334	335	336	337	338	339	340	341
342	343	344	345	346	347	348	349	350	351	352
353	354	355	356	357	358	359	360	361	362	363
364	365	366	367	368	369	370	371	372	373	374
375	376	377	378	379	380	381	382	383	384	385
386	387	388	389	390	391	392	393	394	395	396
397	398	399	400	401	402	403	404	405	406	407
408	409	410	411	412	413	414	415	416	417	418
419	420	421	422	423	424	425	426	427	428	429
430	431	432	433	434	435	436	437	438	439	440
441	442	443	444	445	446	447	448	449	450	451
452	453	454	455	456	457	458	459	460	461	462
463	464	465	466	467	468	469	470	471	472	473
474	475	476	477	478	479	480	481	482	483	484
485	486	487	488	489	490	491	492	493	494	495
496	497	498	499	500	501	502	503	504	505	506
507	508	509	510	511	512	513	514	515	516	517
518	519	520	521	522	523	524	525	526	527	528
529	530	531	532	533	534	535	536	537	538	539
540	541	542	543	544	545	546	547	548	549	550
551	552	553	554	555	556	557	558	559	560	561
562	563	564	565	566	567	568	569	570	571	572
573	574	575	576	577	578	579	580	581	582	583
584	585	586	587	588	589	590	591	592	593	594
595	596	597	598	599	600	601	602	603	604	605
606	607	608	609	610	611	612	613	614	615	616
617	618	619	620	621	622	623	624	625	626	627
628	629	630	631	632	633	634	635	636	637	638
639	640	641	642	643	644	645	646	647	648	649
650	651	652	653	654	655	656	657	658	659	660
661	662	663	664	665	666	667	668	669	670	671
672	673	674	675	676	677	678	679	680	681	682
683	684	685	686	687	688	689	690	691	692	693
694	695	696	697	698	699	700	701	702	703	704
705	706	707	708	709	710	711	712	713	714	715
716	717	718	719	720	721	722	723	724	725	726
727	728	729	730	731	732	733	734	735	736	737
738	739	740	741	742	743	744	745	746	747	748
749	750	751	752	753	754	755	756	757	758	759
760	761	762	763	764	765	766	767	768	769	770
771	772	773	774	775	776	777	778	779	780	781
782	783	784	785	786	787	788	789	790	791	792
793	794	795	796	797	798	799	800	801	802	803
804	805	806	807	808	809	810	811	812	813	814
815	816	817	818	819	820	821	822	823	824	825
826	827	828	829	830	831	832	833	834	835	836
837	838	839	840	841	842	843	844	845	846	847
848	849	850	851	852	853	854	855	856	857	858
859	860	861	862	863	864	865	866	867	868	869
870	871	872	873	874	875	876	877	878	879	880
881	882	883	884	885	886	887	888	889	890	891
892	893	894	895	896	897	898	899	900	901	902
903	904	905	906	907	908	909	910	911	912	913
914	915	916	917	918	919	920	921	922	923	924
925	926	927	928	929	930	931	932	933	934	935
936	937	938	939	940	941	942	943	944	945	946
947	948	949	950	951	952	953	954	955	956	957
958	959	960	961	962	963	964	965	966	967	968
969	970	971	972	973	974	975	976	977	978	979
980	981	982	983	984	985	986	987	988	989	990
991	992	993	994	995	996	997	998	999	1000	1001

• 2004-2005/2006

Sample	Number of Insects Examined	Number of Insects Infected	Percentage Infected	Number of Insects Examined	Number of Insects Infected	Percentage Infected	Number of Insects Examined		Percentage Infected
							Number of Insects Examined	Number of Insects Infected	
1	100	10	10%	100	10	10%	100	10	10%
2	100	20	20%	100	20	20%	100	20	20%
3	100	30	30%	100	30	30%	100	30	30%
4	100	40	40%	100	40	40%	100	40	40%
5	100	50	50%	100	50	50%	100	50	50%
6	100	60	60%	100	60	60%	100	60	60%
7	100	70	70%	100	70	70%	100	70	70%
8	100	80	80%	100	80	80%	100	80	80%
9	100	90	90%	100	90	90%	100	90	90%
10	100	100	100%	100	100	100%	100	100	100%

Footnotes for Table 1.

- a. All neutron data from ENDF/B-V unless otherwise noted.
- b. Unless otherwise noted, Bondarenko factors are available for MT's 1, 2, 4, 18 (for fissionable nuclei), 102, and 1000.
- c. An evaluation from the LENDL library, not an ENDF/B-V evaluation.
- d. The following code is used to identify the weighting functions:

<u>Code</u>	<u>Weight Function</u>
A	10^{-5} -0.1265 eV Maxwellian; 0.1265 eV-1.4 MeV 1/E; 1.4-20 MeV fission spectrum.
B	10^{-5} -0.1265 eV Maxwellian; 0.1265 eV-0.75 MeV 1/E; 0.75-20 MeV fission spectrum.
C	10^{-5} -0.1265 eV Maxwellian; 0.1265 eV-0.1 MeV 1/E; 0.1-20 MeV fission spectrum.

- e. Order of scattering in the fast range is P_5 ; in the thermal range, it's P_3 .
- f. See Appendix C of Ref. 1 for the definitions of the process identifiers (MT numbers).

II.C. Weighting Function

All materials in the CSRL-V library were processed with a fission-1/E-Maxwellian weighting function. Temperature of the fission spectrum component of the weighting function was 1.27×10^6 eV; temperature of the Maxwellian component was 300°K. The energy at which the fission component was joined to the 1/E component generally was 1.4 MeV for the light materials, 0.75 MeV for the intermediate-mass materials, and 0.1 MeV for the heavy materials. The 1/E component was joined to the Maxwellian component at 0.1265 eV for the processing of all materials.

II.D. Legendre Order of Scattering

The special 1/V data set and the ^{64}Zn , ^{191}Ir , and ^{193}Ir data sets were processed with a P_0 order of scattering. Group-to-group transfer matrices for ^1H , ^2H , and C were expanded to P_5 in the epithermal range and P_3 in the thermal range. All other materials were processed with a P_3 expansion.

II.E. Codes Used to Process CSRL-V

As shown in Fig. 1, current versions of modules from the AMPX and NJOY^{18,19} cross-section processing systems were used to process CSRL-V. ENDF/B-V evaluations containing resolved resonance data were "preprocessed" with NPTXS (AMPX) to make pointwise files (i.e., neutron energy, cross-section pairs) for the total, fission, elastic scattering, and (n, γ) reactions. The pointwise elastic scattering data were used to augment the ENDF data selected in a subsequent module (XLACS2) used to process the multigroup scattering matrices.

XLACS2 (AMPX) was used to produce full-energy-range multigroup neutron cross sections in AMPX master format (see below). The module processes ENDF/B resolved resonance data into a form suitable for use (i.e., resonance parameters) in the calculation of self-shielded cross sections with the Nordheim integral treatment²⁰ provided in the NITAWL (AMPX) module.

The NJOY modules UNRESR and UXSR, an improved version of UNRESR, were used to compute effective pointwise self-shielded cross sections for the unresolved resonance region. TABU (AMPX) was used to process the pointwise unresolved data into group-averaged Bondarenko²¹ data which were a function of material, process, temperature, background cross section, and energy. UNITAB (AMPX) was used to merge the Bondarenko data and the XLACS2-produced data into a final master data set.

XLACS2 has not been programmed to process Adler-Adler resonance data in ENDF formats. Consequently, NJOY was used to process the two ENDF/B-V evaluations which contain Adler-Adler data -- MAT 1393 (^{233}U) and MAT 1381 (^{241}Pu). The resulting CSRL-V data sets have Bondarenko factor data for both the resolved and unresolved energy ranges.

Other codes were used for data management and format conversion. NPCSL (NJOY) was used to convert binary pointwise data sets to BCD format. RIGEL, an ENDF code, was used to change the mode of ENDF data from binary to BCD, or vice versa. AJAX (AMPX) was used to merge AMPX master data sets. AIM (AMPX) was used to convert binary master libraries to BCD-formatted master libraries, or vice versa.

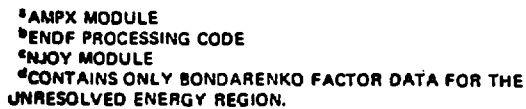


Fig. 1. Codes used to generate CSRL-V libraries

II.F. Thermal Range Processing

A feature of the code used to process the CSRL-V multigroup data (XLACS2) is the ability to process normal ENDF/B data in the fast and epithermal energy regions and to couple the data in a consistent fashion with thermal data taken from another ENDF/B evaluation to produce a single full-energy-range master data set. This means, for example, that a multithermal-group master data set can be prepared for hydrogen using the normal ENDF/B hydrogen evaluation for the energy region above the thermal-epithermal cutoff, i.e., for the fast groups, and using an ENDF thermal evaluation containing $S_{\alpha,\beta}$ data based on a water model for the region below the cutoff energy (the thermal groups). Two advantages of this approach are the convenience of dealing with a single set of processed data and the generation of multigroup cross sections representing the correct distributions for neutrons elastically or inelastically scattered into the thermal range. This procedure was used to process water-bound and polyethylene-bound hydrogen, CSRL-V ID's 1001 and 1301, D₂O-bound deuterium (1002), and graphite (6312).

Only the very light moderators need the special ENDF thermal evaluations for the preparation of multithermal-group cross sections. For those nuclides which have no special thermal evaluations, XLACS2 allows the following options for generating thermal scattering matrices based on the free gas treatment:

1. The code will generate free gas $S_{\alpha,\beta}$ data. This process was used with light nuclides -- $A \leq 19$.
2. The code will use an analytic free gas treatment to generate P_0 thermal matrices. The thermal values are normalized to the free-atom scattering cross section in the epithermal range. This process was used for nuclides with mass > 19 and with no resonances in the thermal range.
3. The same analytic routines used in #2 are used but the scattering matrices are normalized to the average values of the scattering cross section in the thermal range. (Note that this will not preserve the Doppler broadening inherent in the free gas equations unless it is present in the thermal point values.) This approach was used for nuclides with thermal resonances -- nuclides such as ²³⁵U and ²⁴⁰Pu.

II.G. Resolved Resonance Processing

Resolved resonance processing for CSRL-V involved the calculation of two arrays of cross-section data for the elastic scattering, n- γ capture, and fission reactions, i.e., XLACS2 calculates MT 2 and 1023 data for elastic scattering, MT 18 and 1022 data for fission, and MT 102 and 1021 data for n- γ capture. The MT 1021, 1022, and 1023 arrays contain the averaged values of the cross sections for the resonance bodies. These averaged values are weighted over the weighting spectrum specified for the XLACS2 problem.

The MT 18 and MT 102 arrays contain "everything" except the MT 1022 and MT 1021 data, respectively. "Everything" includes the following:

- a. The wings of the resonances (recall that the Nordheim treatment only applies to a region close to the resonance peak.)
- b. The contributions from all $\ell=1, 2, 3, \dots$ resonances.
- c. The interference terms (even in the resonance body) for the case of multilevel Breit-Wigner fits.
- d. The ENDF File 3 background data.

Conversely, the calculated MT 2 data are the sum of the above "everything" contributions and the 1023 data, i.e., the MT 2 data are for total elastic scattering.

Data calculated for MT 1, 27, and 101 follow the same rules as for MT 2, 18, and 102. For example,

$$(MT\ 27) = (MT\ 101) + (MT\ 18) \quad (1)$$

$$(MT\ 101) = \sum_{i=2}^{14} (MT\ 100+i) \quad (2)$$

II.H. Fission Spectrum

XLACS2 calculates a full group-to-group fission matrix as a prelude to calculating an averaged fission spectrum. This two-dimensional array is reduced to the one-dimensional array placed on the master library (MT 1018) by the following expression:

$$\bar{\chi}_g = \frac{\sum_{g'} v_{g'} \sigma_{g'}^f \phi_{g'} \chi(g' \rightarrow g)}{\sum_{g'} v_{g'} \sigma_{g'}^f \phi_{g'}} \quad (3)$$

II.I. Format of the CSRL-V Master Library

Among the many types of cross-section libraries that can be produced with the AMPX system (libraries such as ANISN-formatted libraries, CCC-formatted libraries, "working" libraries, etc.), the format of an AMPX master cross-section library is the most general way to store multigroup neutron cross-section data. Included in a master library are one-dimensional multigroup cross-section data, transfer matrices for elastic and inelastic scattering reactions and for neutron producing reactions [e.g., (n,2n)] with arbitrary orders of scatter for fast and thermal data where required, resonance self-shielding parameters (including Bondarenko factors) for subsequent problem-dependent processing, fission spectrum data, weighting

function data, etc. These data are available in a compacted magic word format to remove extraneous zeros and consequently to substantially reduce tape storage requirements. One-dimensional and transfer matrix data (two-dimensional data) in each CSRL-V master data set are identified by MT number in Table 1. Format of an AMPX master library is given in Ref. 1.

III. CSRL-V BENCHMARK CALCULATIONS

Data from CSRL-V have been used to calculate performance parameters for the CSEWG TRX-1 and TRX-2 benchmarks²² and for the Babcock & Wilcox B&W-XIII and B&W-XX benchmarks.²³ Results of the TRX calculations are summarized in Section III.A and the B&W calculations are summarized in Section III.B. Eigenvalue calculations for selected criticality safety benchmarks are discussed in Section III.C.

III.A. CSEWG TRX-1 and TRX-2 Benchmarks

The CSEWG TRX-1 and TRX-2 benchmarks were water-moderated, fully reflected assemblies with aluminum-clad fuel rods of 1.3% ²³⁵U-enriched uranium. The 0.983-cm-diameter rods were arranged in triangular arrays with lattice spacings of 1.8060 and 2.1740 cm and with moderator/fuel volume ratios of 2.35 and 4.02 for TRX-1 and TRX-2, respectively. Integral parameters which were measured at the center of each lattice included the epithermal/thermal ratio of ²³⁸U capture (ρ^{28}) and of ²³⁵U fission (δ^{25}), the ratio of ²³⁵U capture to ²³⁵U fission (C^*), and the ratio of ²³⁸U fission to ²³⁵U fission (δ^{28}).

Problem-dependent cross sections processed from CSRL-V were used to calculate the benchmark performance parameters. A typical code calculational sequence is depicted in Fig. 2. Axial bucklings given in Ref. 22 were used to determine the representative assembly cylinder heights for the discrete ordinates calculations.

Calculated performance parameters for TRX-1 and TRX-2 are compared in Tables 2 and 3, respectively, with experimental values and with the average of ENDF/B-V calculations by laboratories which contributed to the CSEWG ENDF/B-V thermal benchmark studies.²⁴ CSRL-V calculations for TRX-1 were made with the 227-group CSRL-V data. TRX-2 calculations were made with a 27-group subset of the fine-group CSRL-V cross sections. The TRX-2 cell-averaged flux was used to collapse the CSRL-V data sets to the broad-group structure.

Comparison of the CSRL-V results with the CSEWG results shows that ρ^{28} for both TRX-1 and TRX-2 is higher (~2%) than the CSEWG average, which in turn is higher than the experimental ρ^{28} . This parameter strongly influences k_{eff} . The CSRL-V eigenvalue is ~0.3% lower than the CSEWG average k_{eff} for both TRX-1 and TRX-2. In depth studies are in progress to either substantiate the CSRL-V results or to identify the cause(s) of the discrepancies.

TYPICAL BENCHMARK CALCULATIONAL SEQUENCE

ORNL - ORO 60-12660

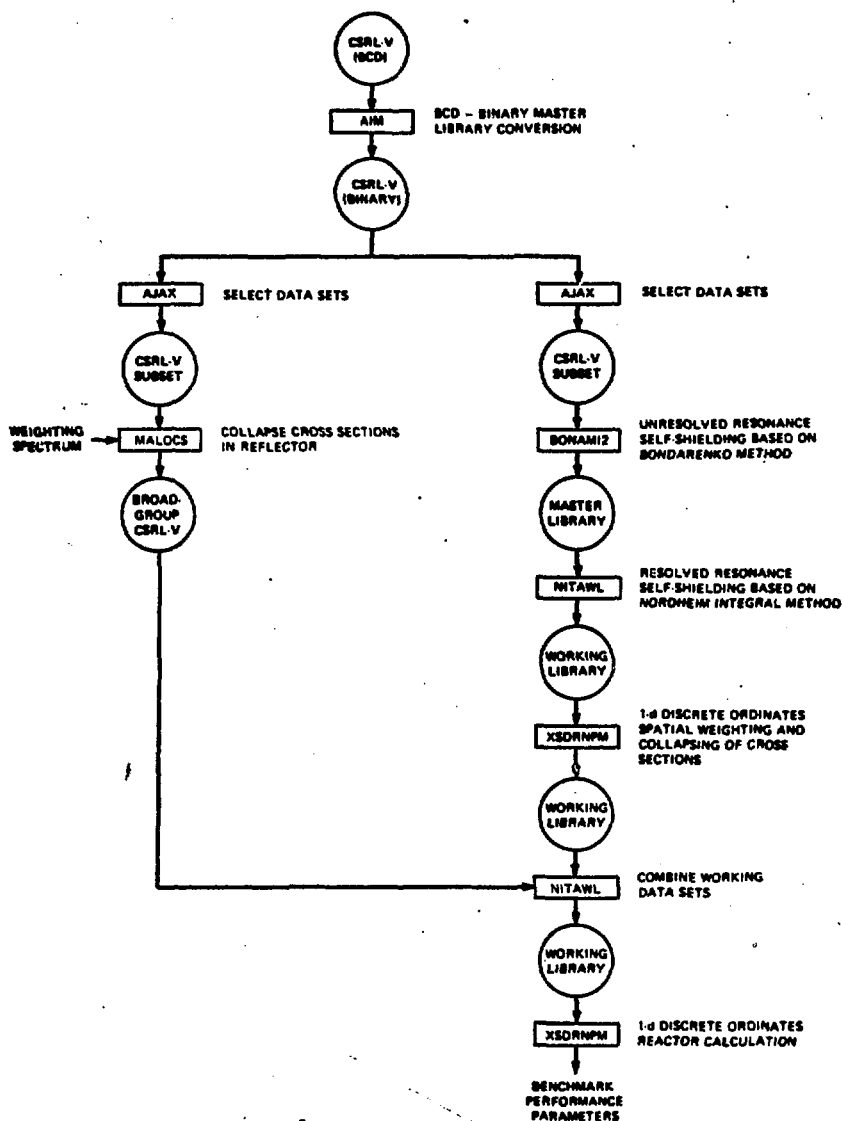


Fig. 2. Typical benchmark calculational sequence.

Table 2. Integral Parameters for TRX-1

Parameter ^a	Experiment	Five-Lab Average ^b	CSRL-V	ENDF/B-V Calculation	
				$\left(\frac{\text{Calc.}}{\text{Exp.}}\right) - 1 \times 100$	
				5-Lab. Avg.	CSRL-V
ρ^{28}	1.320±0.021	1.359±0.016	1.388	3.0	5.2
δ^{25}	0.0987±0.0010	0.1003±0.0010	0.09984	1.6	1.2
δ^{28}	0.0946±0.0041	0.0989±0.0003	0.09824	4.5	3.8
C*	0.797±0.008	0.798±0.005	0.8081	0.1	1.4
k_{eff}	1.0	0.9961±0.0031	0.9929	-0.39	-0.71

^a Parameter definitions (measured at core center):

- ρ^{28} ≡ ratio of epithermal-to-thermal ²³⁸U capture
- δ^{25} ≡ ratio of epithermal-to-thermal ²³⁵U fissions
- δ^{28} ≡ ratio of ²³⁸U fissions to ²³⁵U fissions
- C* ≡ ratio of ²³⁸U captures to ²³⁵U fissions

^b Electric Power Research Institute (EPRI), ORNL (not this work), Brookhaven National Laboratory (BNL), Chalk River Nuclear Laboratories (CRNL), and Combustion Engineering, Inc. (CE) results as reported by Weisbin, Hardy et al. as a part of the CSEWG ENDF/B-V data testing program.²⁴

Table 3. Integral Parameters for TRX-2

Parameter	Experiment	ENDF/B-V Calculation			
		Four-Lab Average ^a	27-Group CSRL-V	$\left(\frac{\text{Calc.} - 1}{\text{Exp.}} \right) \times 100$	
				4-Lab. Avg.	27-Gp. CSRL-V
ρ^{28}	0.837 \pm 0.016	0.846	0.865	1.1	3.3
δ^5	0.0614 \pm 0.0008	0.0614	0.0612	0.0	-0.33
δ^{28}	0.0693 \pm 0.0035	0.0699	0.0696	0.9	0.43
C*	0.647 \pm 0.006	0.642	0.648	-0.8	0.15
k_{eff}	1.0	0.9984	0.9948	-0.16	-0.52

^a EPRI, ORNL (not this work), CRNL, and CE results reported by Weisbin, Hardy et al. as a part of the CSEWG ENDF/B-V data testing program.²⁴

III.B. B&W-XIII and B&W-XX Benchmarks

CSRL-V data were used to calculate eigenvalues for two slightly-enriched (2.46% ^{235}U) UO_2 , water-moderated critical assembly experiments reported by the Babcock & Wilcox Company — B&W-XIII and B&W-XX. The critical assembly was erected in a 5-foot-diameter by 6.5-foot-high aluminum core tank mounted inside an existing 9-foot-diameter tank. Fuel rods consisted of pellets in 1.206-cm-diameter, 156.4-cm-long, aluminum-clad cylinders arranged in a 1.511 cm lattice pitch. Nonmoderator-to-moderator volume ratio was 1.001. The two experiments differed in the presence (or absence) of boron in the moderator, the number of fuel rods and the radial and axial parameters as follows:

Core No.	Boron in moderator (gm B/l)	Number of fuel rods	Radial parameters (cm)		Axial parameters (cm)	
			Core radius	Reflector thickness	Moderator height	Reflector thickness
XIII	0	596	20.82	55.38	141.1	12.3
XX	1.675	5137	61.11	15.09	93.2	60.2

Calculated eigenvalues for B&W-XIII and B&W-XX are compared in Table 4 with eigenvalues calculated with two other ENDF/B-V cross-section libraries—the 97-group EPRI-CELL (E-C/PDQ) and a 127-group in-house library used in other thermal benchmarking studies. The E-C/PDQ values were obtained by EPRI by feeding cell-averaged, broad-group cross-sections computed with the EPRI-CELL code into a 1-d PDQ diffusion theory calculation. The 127-group results used a Bondarenko resonance shielding calculation with the same background cross sections (σ_0 's) as in the EPRI-CELL calculation, which partially accounts for the good agreement with the E-C/PDQ results. The cell-averaging and 1-d core calculation for the 127-group library was done with XSDRNPM. Note that again the CSRL-V NITAWL-XSDRNPM eigenvalue results are lower than the other methods.

Table 4. Calculated Eigenvalues for B&W-XIII and -XX Lattices

Parameter	<u>Calculated Eigenvalue</u>				<u>$\left(\frac{\text{Calculated}}{\text{Experimental}} - 1 \right) \times 100$</u>			
	E-C/PDO	127-Group	XSDRN	CSRL-V	E-C/PDO	127-Group	XSDRN	CSRL-V
B&W-XIII k_∞	1.327	1.328	1.320	—	—	—	—	—
B&W-XIII k_{eff}	1.003	1.002	0.995	0.3	0.2	0.2	—0.5	—
B&W-XX	1.089	1.089	1.084	—	—	—	—	—
B&W-XX	1.002	1.000	0.995	0.2	0.0	0.0	—0.5	—

III.C. Criticality Safety Benchmarks

Adequacy of the CSRL-V group structure and validity of selected data sets from the library were further tested by a series of P_3 S_8 fine- and broad-group calculations of k -eff for a series of criticality safety benchmarks. Characteristics of five selected uranium solution experiments with various $H/^{235}U$ atom ratios are given in Table 5. The experiments were water-reflected and unreflected critical spheres of uranyl nitrate or uranyl fluoride aqueous solutions. Calculated eigenvalues for the benchmarks are given in Table 6. CSRL-V results are compared with results obtained using the 16-group P_1 Hansen-Roach cross-section library.²⁹

Table 5. Critical Conditions for Bare and Reflected Spheres

Experiment Designation	Sphere Radii (cm)		Atom Density ^a (atoms/bn.cm)										Reflector Condition	Reference
	Inner	Outer	²³⁵ U	²³⁵ U	²³⁸ U	²³⁵ U	H	O	F	H	O			
CS1	11.32 ^b	11.68	8.70-4	5.326-4	4.30-4	4.73-3	6.334-2	3.35-2	1.704-3				Reflected	15
CS2	13.20 ^b	13.33	2.87-4	2.429-4	1.31-4	1.34-3	6.353-2	3.36-2	3.214-4				Reflected	26
CS4	25.39 ^b		7.00-7	1.161-4	9.00-7	2.186-3	5.489-2	3.31-2	4.607-3				Bare	27
CS5	18.35 ^b	18.50	1.65-4	1.333-4	9.20-7	9.90-4	4.518-2	3.40-2		3.32-4				
CS7	34.60 ^b	34.92		6.794-3		4.83-4	6.603-2	3.39-2		2.35-4	1.28-3			

^a Sphere constructed of Al (6.016×10^{-2} atoms/bn cm).

^b Container wall, supporting members, and solution filling correction of

16.8¢ is made to calculated eigenvalues.

^c Atom densities given as a number and an exponent, e.g., 1.00-1 means 1.00×10^{-1} .

Table 6. Calculated Results for Uranium Solution Critical Experiments

Experiment Designation	Experiment Description	H/U-235 Atom Ratio	$k_{eff} \left(\frac{\text{Calculated}}{\text{Experimental}} - 1 \right) \times 100$	
			Hansen-Roach 16 Group, P ₁	CSRL-V
CS1	93.2% enriched uranyl fluoride solution spheres, infinite water reflector	76.1	0.0	0.19
CS2		269.8	-0.37	0.07
CS4	4.98% enriched uranyl fluoride solution sphere	490.0	-1.20	-0.30
CS5	93.2% enriched uranyl nitrate solution sphere	425.1	-0.79	0.15
CS7	Borated 93.2% enriched uranyl nitrate solution sphere	971.6	0.45	-0.58

IV. CONCLUSIONS AND FUTURE OBJECTIVES

The CSRL-V AMPX master and pointwise cross-section libraries are available on magnetic tape from the Radiation Shielding Information Center in a package identified as DLC-095/CSRL-V.^a Documentation for the library is given in Ref. 1.

CSRL-V eigenvalue results for the thermal reactor benchmarks were slightly lower than ENDF/B-V based results reported by others. Possible reasons for the differences are being investigated.

ENDF/B-V Special Purpose Dosimetry, Activation, and Gas Production Files are being processed for CSRL-V. Photon-production and photon-interaction libraries are in the planning stage.

^a Inquiries should be addressed to Radiation Shielding Information Center, P. O. Box X, Oak Ridge National Laboratory, Oak Ridge, TN 37830.

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