

HOT CORROSION/EROSION TESTING OF MATERIALS FOR
APPLICATION TO ADVANCED POWER CONVERSION SYSTEMS
USING COAL-DERIVED FUELS
TASK II - FLUIDIZED BED COMBUSTION

FINAL REPORT
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I. ABSTRACT

The objective of this program was to provide an experimental basis for specifying materials for heat exchangers and gas turbines exposed to a pressurized fluidized bed combustor environment. A 1000 hour test was completed which:

- Exposed heat exchanger materials both within the fluidized bed and in the freeboard of a pressurized fluidized bed combustor at temperatures ranging from 1050°F to 1600°F for up to 1117 hours.
- Provided the first successful long term exposure of turbine blade materials subjected to PFBC flue gas where the particulates were removed solely by cyclones.

This report describes the operating conditions and major observations during this test period. Subsequent reports (1,2) will provide detailed metallurgical analysis of the test specimens to quantitatively determine the degree of hot gas corrosion and erosion present.

OPERATING CONDITIONS

Typical operating conditions for the PFBC miniplant combustor during this test period were 9 atm pressure, 915 to 950°C (1680-1740°F) bed temperature, 1.8 m/sec (6 ft/sec) fluidizing velocity, 15 to 25% excess air. Emission levels of SO₂ were 250 to 300 ppm and NO_x was approximately 100 ppm - both well below current EPA standards. Approximately 2 ppm of sodium and 0.5 ppm potassium was detected as alkali in the flue gas. Particulate concentration typically ranged from 0.025 to 0.07 gr/SCF.

RESULTS

Turbine Blade Section

During the 1000 hour test, operating conditions varied sufficiently to significantly alter the particulate loading and mean particle diameter of the particulate entering the turbine section. This permitted several observations to be made:

- Most of the turbine blade specimens visually appeared to be in satisfactory condition showing little, if any, erosion.
- Particulate loading and/or particle size had a profound effect on the degree of deposition and erosion on the turbine blades.

- In general, erosion was not visually apparent when 3 stages of conventional cyclones were used to clean the PFBC flue gas. However, upsets could cause marked erosion if the grain loading and particulate size increased only by small amounts.

Heat Exchanger Specimens

The heat exchanger specimens appeared to be in satisfactory condition both in bed and above the fluidized bed. However, several in-bed probes showed some visible signs of corrosion (one probe actually failed). The above-bed probes showed little, if any, visible corrosion or erosion.

CONCLUSIONS

- These tests indicated the possibility that conventional cyclones alone may be sufficient to protect gas turbine blade materials exposed to PFBC flue gas. This needs to be validated by further experimentation and metallurgical analysis of the test specimens.
- There seems to be satisfactory heat exchanger materials for above-bed use and probably in-bed use. Further experimentation and metallurgical analysis of the test specimens will better quantify the lifetime which can be expected.

II. SCOPE OF WORK

INTRODUCTION

Pressurized fluidized bed combustion offers the potential of an efficient and compact coal combustion technique also capable of providing pollution control. The technology involves the combustion of coal in a bed of particles maintained in a state of fluidization by the air required for combustion. The use of limestone or other suitable sorbent as the bed material permits the capture and removal of sulfur dioxide concurrently with the combustion process.

The objective of this program was to expose specimens of potential PFBC heat exchanger alloys (supplied by Westinghouse Research Center) and gas turbine materials (supplied by General Electric Company) to a pressurized fluidized bed coal combustion environment for 1100 hours. The Exxon Miniplant provided a test site for this test facility. The intent of the PFBC exposure tests was to compile a sound engineering data base for the characterization of the corrosion/erosion behavior of a number of commercially available alloys when exposed to a pressurized fluidized bed combustion environment. These pressurized fluidized bed combustion exposures will provide corrosion/erosion data and comparisons of materials for application to advanced power systems using coal-derived fuels.

TEST PROGRAM AND OPERATING CONDITIONS

The initial 100 hours of testing represented the shakedown phase of the program. It was intended to assess the performance of the heat exchanger specimen probes and the turbine test section and to evaluate the compatibility of these components with the miniplant combustor operating conditions and controls. It also provided an early opportunity for General Electric and Westinghouse to evaluate materials after a short test run. The shakedown run was completed and the results were reported in the first task report, March 1978.

Following the shakedown run are the extended exposure tests of the heat exchanger materials supplied by Westinghouse Research and the gas turbine materials supplied by General Electric Company. Total exposure times were intended to be up to 1000 hours, with the tests interrupted at the 250, 500 and 700 accumulated hour intervals to allow removal, inspection and re-insertion of the material specimens.

The target Exxon FBC miniplant operating conditions for the extended hot corrosion/erosion run were - pressure: 8.7-9.1 atmospheres; combustor bed temperature: 1700-1750°F (925-950°C); superficial bed velocity: 6 ft/sec (1.8 m/sec); excess air: 15-20%. Illinois No. 6 coal and the sorbent Pfizer dolomite was used. GE turbine test section inlet conditions were 9 atmospheres pressure, 1550°F gas temperature and 0.72 to 0.92 lb/sec gas mass flow rate.

DESCRIPTION OF PFBC MINIPLANT

The Exxon miniplant combustor is a 32 ft (10 m) tall vessel with a 24 inch (61 cm) pressure shell, refractory lined to a 13 inch (33 cm) inside diameter. It was modified by fabricating and inserting new sections to accommodate the 12 in-bed and 9 above-bed heat exchanger specimens (Figure 1).

Figure 2 is a flow schematic of the PFBC miniplant. Main fluidizing air for the combustor is supplied at pressures to 10 atmospheres and controlled flow rates of 600 to 1100 SCFM. Coal and dolomite (or limestone) are proportioned, premixed and continuously injected into the combustor at a port 11 inches (28 cm) above the distributor grid. The air passes up through the distributor grid where it fluidizes the bed material and provides the air required for combustion.

Heat extraction in the combustor is achieved by cooling coils through which water is circulated; they are mounted on flanges and immersed in the fluidized bed. The coils, fabricated from type 316 stainless steel 1/2 inch Sch. 40 pipe, are arranged in a serpentine, vertical orientation. Each coil covers a vertical distance of 18 inches and consists of 5.9 ft² (0.55 m²) of surface area. Three coils were inserted in the combustor for the shakedown run - one below the new lower probe section and two above. This coil surface area was calculated to provide desired combustor temperatures for the shakedown run conditions. From the shakedown run it was ascertained that two coils would suffice and subsequently the uppermost one was removed.

Flue gas exits the combustor and flows through three stages of cyclones (Figure 2) for particulate removal. The solids collected by the first stage cyclone are returned to the combustor 20 inches above the grid. Solids, mainly flyash, collected by the second and third cyclones are collected by means of a lock hopper system. The expanded bed height is controlled by continuously rejecting solids at a controlled rate through a port at the 90 inch (2.3 m) elevation. Final particulate removal was achieved by passing the flue gases through three conventional cyclones. The first cyclone recycled material back to the combustor while the remaining two cyclones rejected the solids through lock hoppers.

Pressure control is accomplished by bleeding a small amount of flue gas through a by-pass line around the turbine test section (Figure 3). The by-pass stream is expanded through a choked nozzle with make up air supplying the back pressure control. A measuring orifice was installed downstream of the turbine test section. During a run, both turbine mass flow and inlet temperature are scanned once a minute and recorded on magnetic tape. Particulate and analytical sampling trains are also located downstream of the turbine section at 200 kPa pressure.

Figure 1
Combustor Corrosion Probe Location

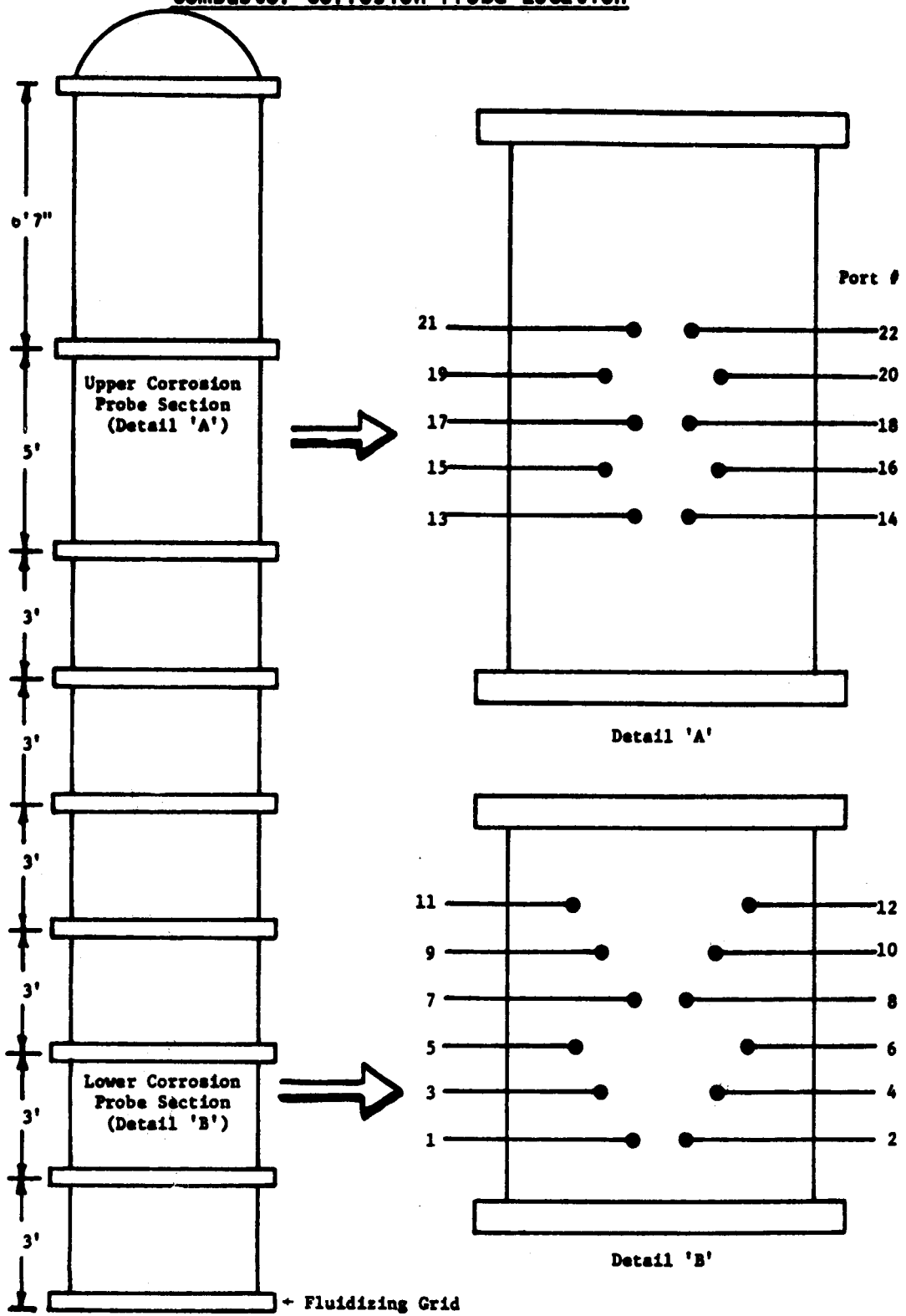
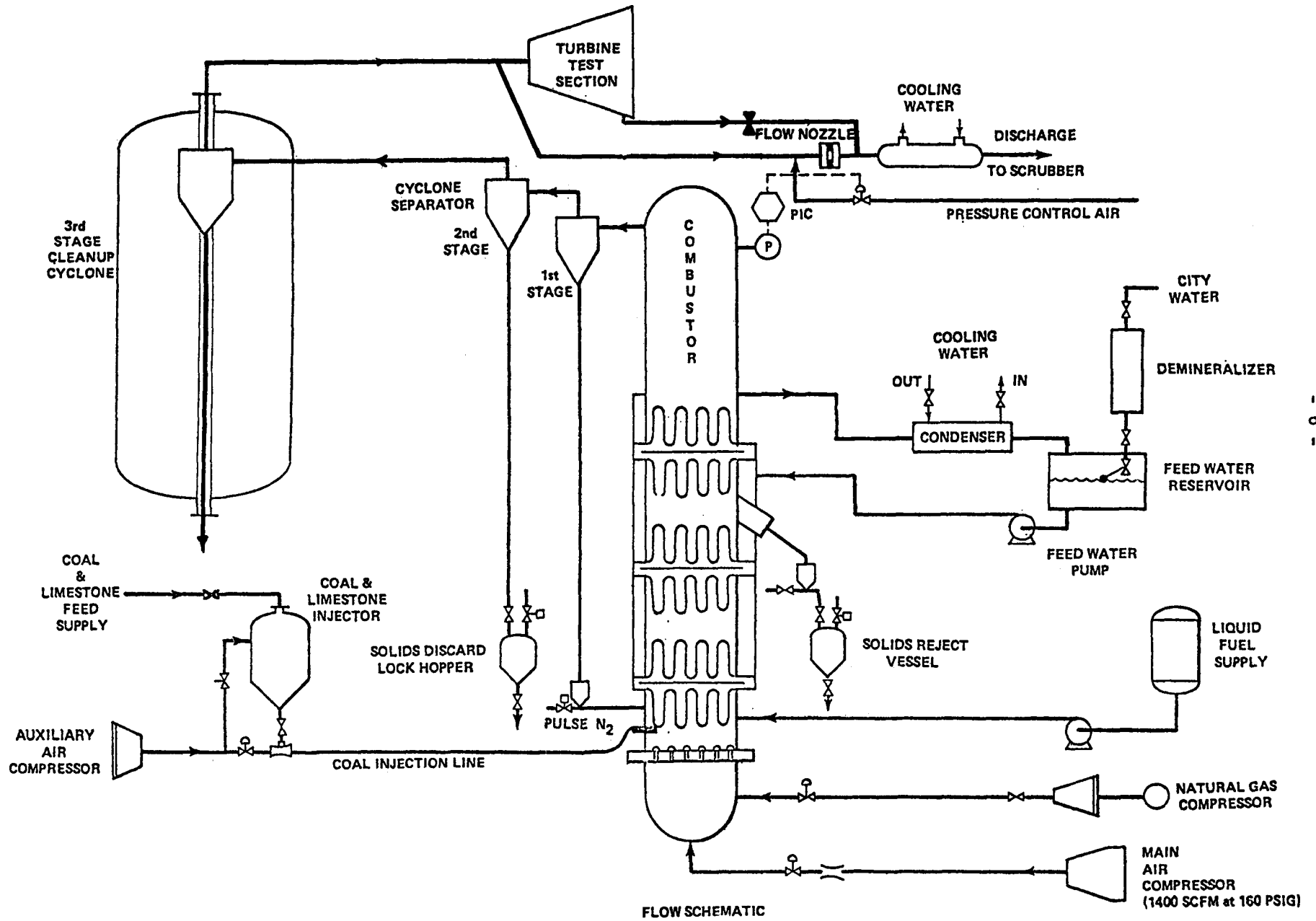


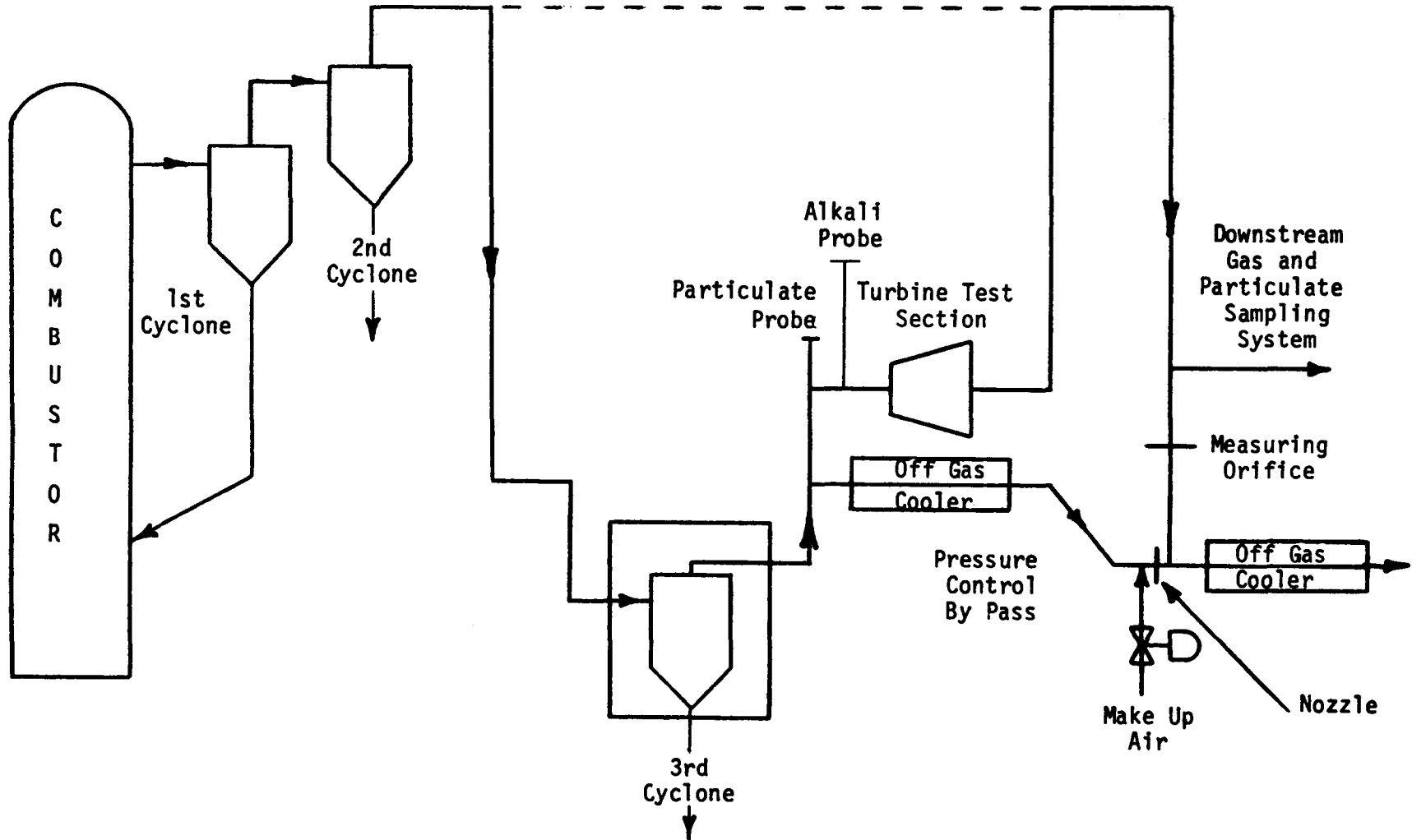
Figure 2
FLUIDIZED BED COMBUSTION MINIPLANT



FLOW SCHEMATIC

Figure 3

Miniplant Hot Gas Flow Schematic



III. EQUIPMENT AND TECHNIQUES

HEAT EXCHANGER SPECIMEN PROBES

The specimens prepared by Westinghouse for the PFBC combustor fireside corrosion/erosion exposures are 1.25 inch OD x 1.00 inch ID by 3 inch long cylinders with thermocouples inserted in the walls. Specimens of 2 different alloys selected for a given test matrix temperature are welded together, plugged at the end and welded to a tube section to form a bayonet probe. This specimen probe consists of a central cooling tube, thermocouple conduits, cooling air inlet and outlet and a flange for connection to the miniplant combustor port (Figure 4). The temperature of each specimen probe is controlled independently by regulating the flow rate of cooling air delivered to that probe. Each probe has a separate temperature control loop (Figure 4) consisting of a temperature controller, transducer (current-to-pneumatic) and control valve. Cooling air to the in-bed probes is supplied by an air compressor and a blower supplies air to the probes in the free board. This provides a reliable, independent and readily adjustable temperature control for the 21 specimen probes (each with 2 alloy specimens) inserted in the combustor. It permits control of 12 in-bed specimen probes at mean temperatures of 1050°F, 1200°F, 1400°F and 1600°F and 9 above-bed specimen probes at temperatures of 1200°F, 1400°F and 1600°F, with 3 specimen probes at each temperature.

The alloy-temperature matrix for in-bed and above-bed Exxon miniplant PFBC exposure tests is shown in Table 1.

Table 1

Heat Exchanger Materials
Alloy-Temperature Matrix

<u>Alloy</u>	<u>Specimen Temperature (°F)</u>			
	<u>In-Bed Only</u>	<u>In-Bed and Above-Bed</u>		
	<u>1050°</u>	<u>1200</u>	<u>1400</u>	<u>1600</u>
2 1/4 Cr - 1 Mo	X			
9 Cr - 1 Mo	X			
304 Stainless Steel		X		
Incoloy 800		X	X	
Hastelloy X			X	X
Haynes 188				X

The heat exchanger specimen probes were installed in the combustor according to the location schedule presented in Table 2. Probes in ports #1 to 12 are immersed in the fluidized bed (i.e., "in-bed" probes). The nominal composition of the probe alloy specimens are listed in Table 3.

Individual heat exchanger specimen temperatures are recorded on a 100-point data logger - a Doric "Digitrend 210" with alarm capabilities. This unit provides a time-temperature record of the heat exchanger probe

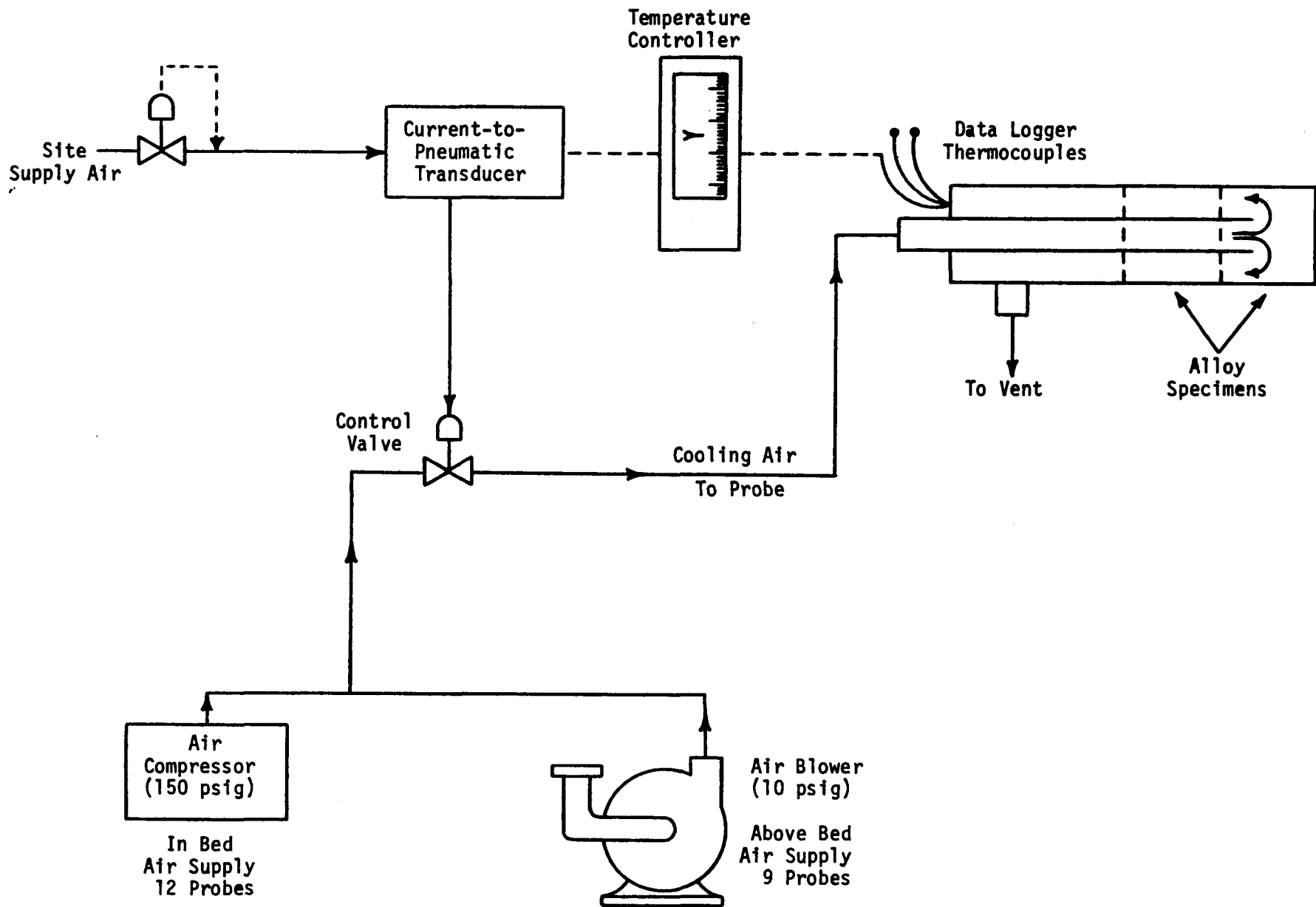


Figure 4

ER&E Miniplant PFBC Hot Corrosion Specimen Probe Temperature Control System

Table 2
Material Description and Location

<u>Combustor Port #</u>	<u>Specimen Material</u>		<u>Target Operating Temperature</u>	
	<u>(Outer)*</u>	<u>(Inner)*</u>	<u>°F</u>	<u>°C</u>
1	H	X	1600	871
2	X	8	1400	760
3	X	H	1600	871
4	8	X	1400	760
5	X	H	1600	871
6	8	X	1400	760
7	8	3	1200	649
8	9	2	1050	566
9	3	8	1200	649
10	2	9	1050	566
11	3	8	1200	649
12	2	9	1050	566
13	H	X	1600	871
14	8	X	1400	760
15	X	H	1600	871
16	8	X	1400	760
17	X	H	1600	871
18	X	8	1400	760
19	3	8	1200	649
20	8	3	1200	649
22	3	8	1200	649

Materials:

H - Haynes 188	1600
X - Hastelloy X	1600 and 1400
8 - Incoloy 800	1400 and 1200
9 - 9 Cr - 1 Mo	1050
2 - 2-1/4 Cr - 1 Mo	1050
3 - 304 stainless steel	1200

* Inner specimen is closest to center of combustor

* Outer specimen is closest to combustor wall

Table 3

Typical Composition of Alloys Tested in PFBC

<u>Heat Exchanger Probes</u>	<u>Composition (%)</u>											
	<u>C</u>	<u>Cr</u>	<u>Ni</u>	<u>Fe</u>	<u>Co</u>	<u>Mo</u>	<u>W</u>	<u>Al</u>	<u>Ti</u>	<u>Mn</u>	<u>Si</u>	<u>Others</u>
2 1/4 Cr - 1 Mo	0.1	2.2	--	Bal.	--	1	--	--	--	0.4	0.3	--
9 Cr - 1 Mo	0.1	9	--	Bal.	--	1	--	--	--	0.5	0.5	--
Type 304 SS	0.08	18	10	Bal.	--	--	--	--	--	1	0.5	--
Incoloy 800	0.04	20.5	32	46	--	--	--	0.4	0.4	0.7	0.4	0.3 Cu
Hastelloy X	0.1	21.5	Bal.	18.5	2.1	9	0.7	--	--	0.6	0.4	0.002 B
Haynes 188	0.08	22.2	22.3	1.8	Bal.	--	14	--	--	0.7	0.4	0.005 B
<u>Turbine Blade Alloys</u>												
U-700	0.07	15	55	0.1	17	5.0	--	4.0	3.5	<0.1	<0.1	<0.04 Zr, 0.15 B
IN-738	0.1	16	64	0.2	8.5	1.8	2.6	3.5	3.5	0.01	0.05	2.5 Nb, Ta
FSX-414	0.2	29	10.8	1.2	50	--	7	--	--	0.8	1.0	0.008 B
<u>Blade Claddings</u>												
IN-671	0.05	48	51	0.4	--	--	--	--	0.2	0.04	0.3	
S-57	0.1	25	10	0.5	Bal.	--	--	3	--	--	--	5 Ta, 0.15 Y
GE-2541	0.1	25	--	Bal.	--	--	--	4	--	--	--	1 Y

'
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specimens at specified intervals. If the temperature of any specimen deviates from a pre-selected acceptable range, the data logger system will (1) alarm, (2) print out all specimen temperatures and the time once, and (3) continue to print the temperatures of the specimens outside of the control span until the proper specimen test temperature is restored.

GAS TURBINE TEST SECTION

The turbine test section is intended to provide a region with representative flow velocities to furnish engineering information on the possible corrosion/erosion deterioration of gas turbine materials exposed to the exhaust gas from a pressurized fluidized bed coal combustor. A photograph of the turbine test section components in their proper flow sequence is presented in Figure 5.

The General Electric test section for gas turbine materials corrosion/erosion evaluation incorporates both buckets and nozzle test specimens (Figures 6 and 7). The bucket (impulse profile) specimens are arranged in 3 cascades (6 specimens in each cascade) forming 3 right angle turns in the flow stream. A fourth cascade, which returns the flow to its original direction, consists of 6 nozzles (reaction profiles) which accelerate the exit flow to a 1.0 Mach number. The rectangular duct is 5/8 inch deep and 2-5/8 inch wide at the bucket cascade section. All profile chords are 1.0 inch.

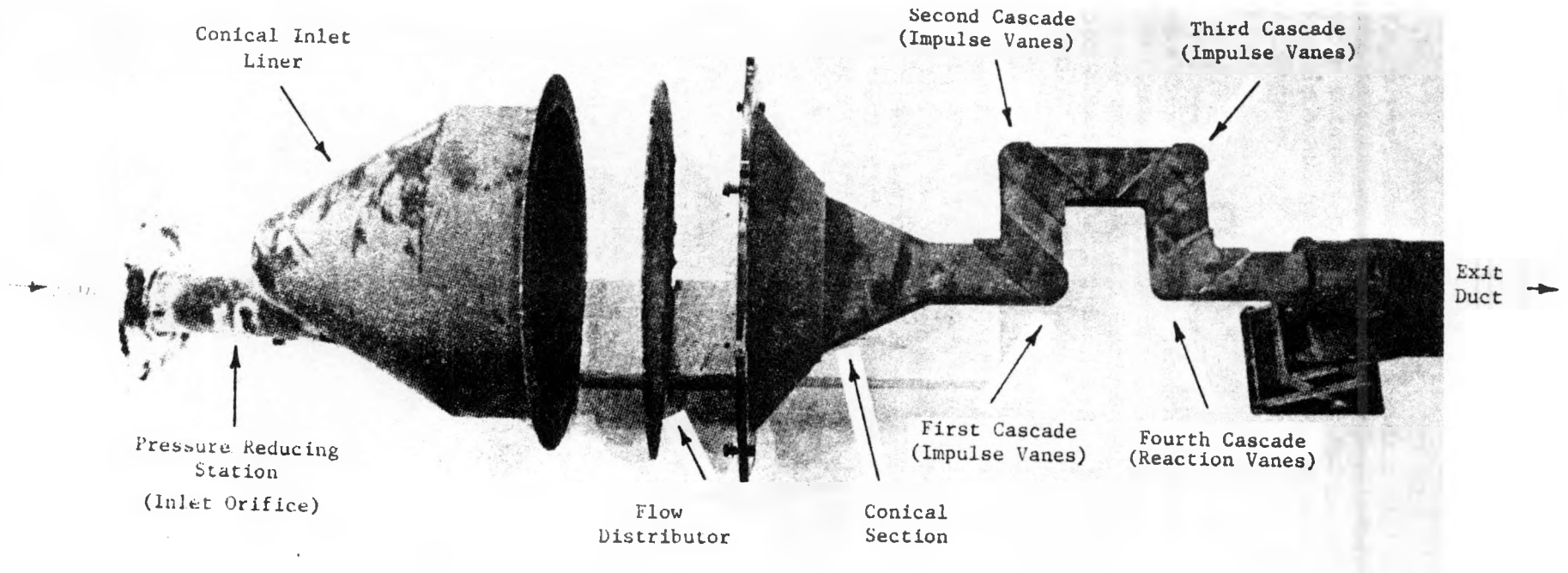
GE supplied bare and clad alloy airfoil specimens. The bare, base alloy specimens were IN-738, U-700 and FSX-414. The IN-738 were clad with IN-671, S-57 and GE 2541, and the FSX-414 were clad with GE 2541. One blade with IN-738 as the base alloy was coated with RT-22 (platinum-aluminide). The nominal composition of the alloys and claddings is presented in Table 3.

Enclosing the flow duct containing the airfoil specimens is a pressure shell which comprises the GE turbine test section. A pressure reducing section is an integral part of the turbine test section and located just upstream of the test passage. This is intended to adjust the turbine test section pressure so that proper blade velocities will be attained at miniplant test conditions.

The turbine test section was installed in the discharge line immediately downstream of the granular bed filter vessel (now housing the third stage cyclone). A new section of discharge pipe was fabricated and refractory lined to permit the insertion of the turbine test section.

Turbine test section flow control and combustor pressure control is accomplished by diverting a fraction of the flue gas through a by-pass loop around the turbine test section (Figure 3). The by-pass stream is expanded through a choked nozzle, with makeup air supplying the back pressure control. A measuring orifice was installed downstream of the turbine test section, so that turbine mass flow rate can be determined.

Figure 5
Turbine Test Section



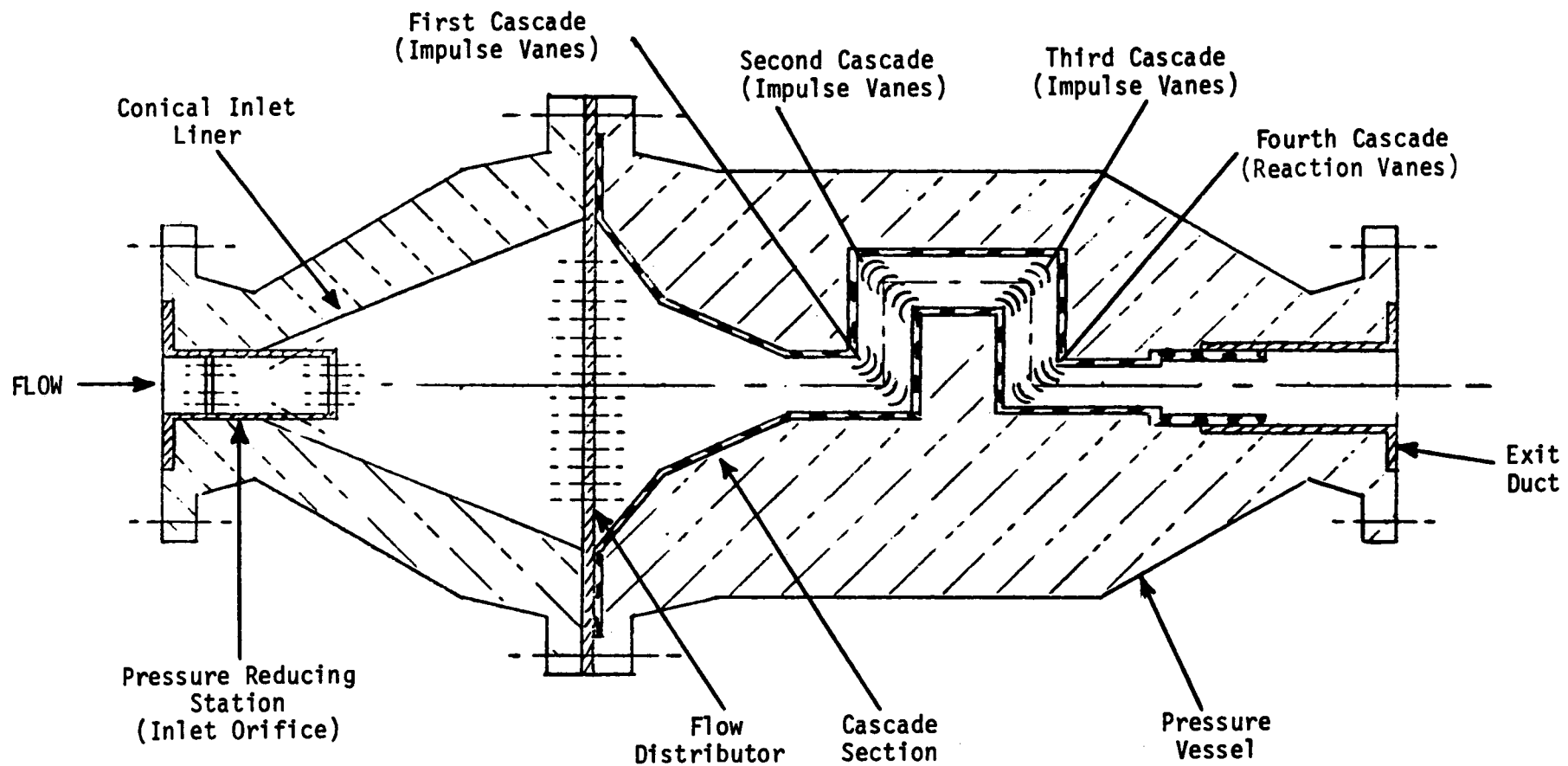


Figure 6

Turbine Test Section Schematic

FLOW CONDITIONS

Pressure - 9 atm
 Temperature - 1550°F
 Gas Flow Rate - 0.72-0.92 lb/sec
 550-722 scfm

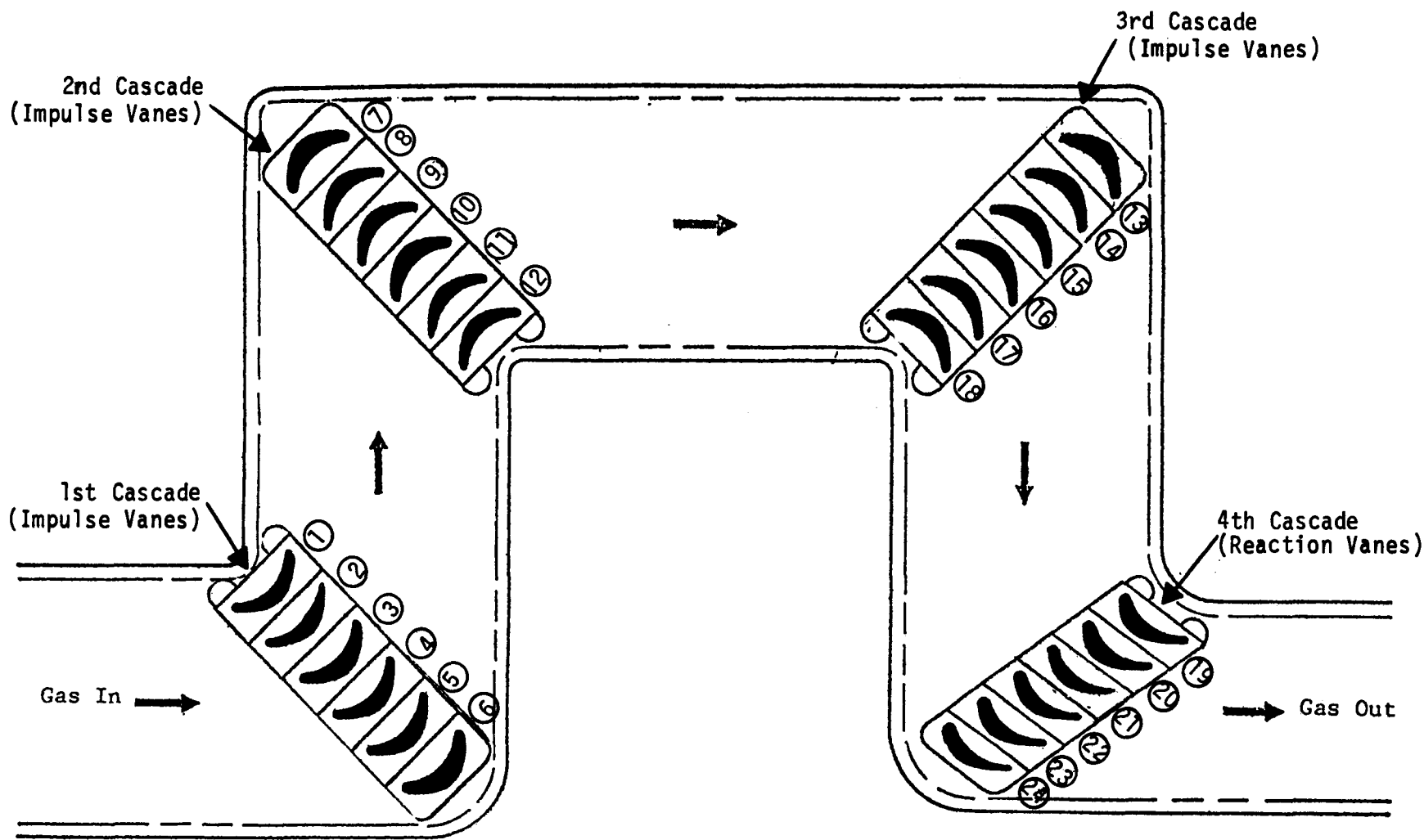


FIGURE 7 SCHEMATIC OF CASCADES IN TURBINE TEST SECTION

The study of turbine blade hot corrosion is deeply concerned with the possible attack of alkali salts on the blade materials. Since a commercial system would be designed to operate at high temperatures, the mini-plant system was modified to attempt to maintain the flue gas at a temperature of at least 1550°F at the turbine test section inlet. To satisfy these temperature conditions it was found necessary and practicable to combust some methane in the discharge piping. This compensates for the thermal losses in the pipe lines and the third cyclone vessel and assures that temperatures upstream of the turbine test section remain above 1550°F (see section on Methane Injection).

HOT GAS CLEANUP

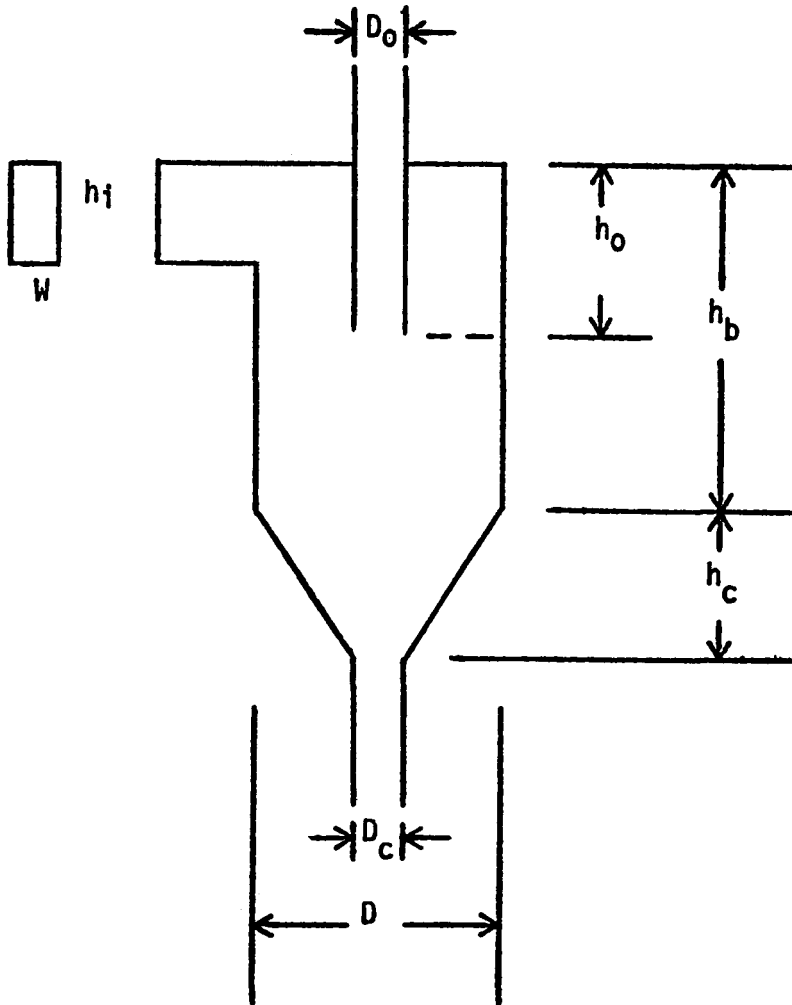
Estimates of the allowable particulate concentration in the flue gas entering the turbine range from 0.04 to 0.001 g/Nm³ (0.02 to 0.0004 grains/SCF). To meet these estimated requirements, the flue gas leaving a pressurized combustor must first be precleaned in two stages of cyclones and then sent to a third stage high efficiency device for final cleaning. The efficiency of the third stage device must be in the range of 95 to 99.7% to be within the currently estimated particulate loading target range.

Initially, particulate removal was to be achieved by using two stages of conventional cyclones followed by a granular bed filter of a design developed by the Ducon Company. This granular bed was to have been tested at Exxon Research and Engineering Company under sponsorship to the U.S. Environmental Protection Agency (Contract 68-02-1312). However, during this test program of the granular bed filter a number of major operating difficulties were encountered which led to the abandonment of the device as a third stage cleanup device. These problems included (1) the formation of a hard filter cake particulate retaining screens of the granular bed filter reducing gas throughput rates; (2) the excessive loss of filter bed material after retaining screens had been removed and freeboard increased; (3) a retention of a significant amount of particulate in the filter bed which, then, uniformly distributed through the filter bed causing a decrease in collection efficiency with time; (4) an inability to achieve outlet concentrations less than 0.05 gr/SCF for a significant period and (5) high vulnerability to process upsets causing shutdown of the system. A detailed description of the granular bed filter test program is given elsewhere (3).

Because correction of the operating problems of the granular bed filter were beyond the scope of the EPA program, a third stage cyclone replaced the granular bed filter in order to provide the final particulate cleanup. Throughout some 2000 hours of testing under various conditions the third cyclone has averaged an efficiency of 90% ± 3%. This conventional cyclone was used in conjunction with the first two stages of cyclones to provide particulate cleanup of the PFBC flue gas for these hot gas corrosion turbine tests. The dimensions of the cyclone are shown in Figure 8. Normal operating conditions for the cyclone are listed in Table 4.

Figure 8

Miniplant Third Cyclone Dimensions



W	h_i	h_o	h_b	h_c	D	D_o	D_c	
1.5	3.0	4.5	16	8	6.07	2.47	3.55	inches
3.81	7.6	11.4	41	20	15.4	6.27	9.02	cm

Table 4

Normal 3rd Cyclone
Operating Conditions

Pressure	900 kPa
Temperature	870°C
Inlet Velocity	50 m/sec
Inlet Loading	1.1 g/Nm ³
Inlet Average Particle Size	3-4 μm

METHANE INJECTION

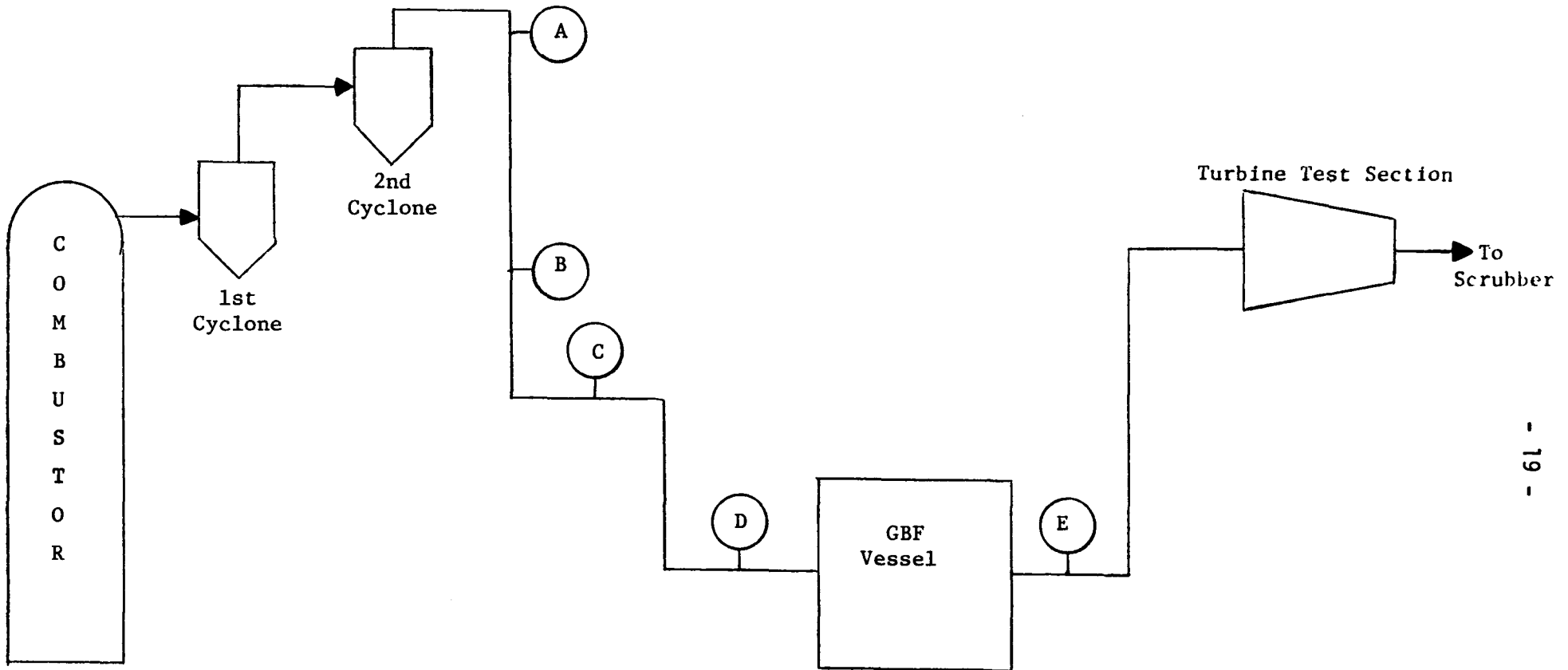
In order to simulate gas turbine operation, care must be taken to prevent the gas temperature from dropping below 843°C (1550°F). Below this temperature gas phase alkali will condense on duct walls or particulate matter. This would unrealistically reduce the gas phase alkali concentration to which the turbine blades are exposed. For this purpose a total of five (5) natural gas injection nozzles were installed in the flue gas line. Four (4) of the ports are located between the second and third cyclone and the fifth between the third cyclone (in the GBF vessel) and the turbine test section (Figure 9). The five ports are staggered to maintain gas temperatures between 1560°F and 1650°F (850°C and 900°C). The total amount of natural gas (typically 60 to 90 Ndm³/min) is controlled to maintain a set third cyclone inlet temperature. The flow distribution between the five nozzles is manually controlled. The injection nozzle consists of a closed end 3/8 inch alonized tube projecting to the duct centerline with a 0.10 cm diameter hole facing downstream. The probes are purged with nitrogen when not in use.

Temperature measurements have revealed that the methane gas does not begin to burn until it is several inches downstream of the injection point. Combustion then occurs uniformly over the next 5 feet before it is complete as indicated by a temperature decline.

The only effect of natural gas injection that has been measured besides a 0.5 to 1% reduction in flue gas oxygen is a drastic reduction in CO. During run 81, CO emissions fell from 525 ppm 1-1/2 hours after coal injection was begun to 30 ppm after methane injection into the flue gas lines was started. Reduction in CO emissions was also observed in runs 79 and 80 with methane injection. CO emissions observed in the past for mini-plant runs without methane injection were in the range of 100 to 200 ppm. For the runs with methane injection, the residence time of the flue gas in the piping at the temperature range of 1500 to 1730°F (816 to 943°C) was about twice as long as for runs without methane injection. Thus, methane injection could provide increased opportunity for burnout of CO.

Figure 9

Location of Methane Injection Nozzles



Methane Injection
Nozzle

Distance Downstream
of 2nd Cyclone (ft)

A	7.5
B	22.0
C	32.0
D	47.0
E	60.0

PARTICULATE SAMPLING AND MEASUREMENT

Particulate Sampling

Since the start of the 1000 hour exposure test program, two particulate sampling systems have been used to measure flue gas particulate loadings into the turbine test section. The oldest system, also used during the shakedown run, is located downstream of the turbine test section. This is near the point where the gas is sampled for flue gas composition. The other measurement system is only several feet upstream of the turbine test section. This system was initially designed to be used with a Southern Research Institute 5-cyclone train or a University of Washington 7-stage impactor for high temperature and high pressure particulate sampling.

The particulate sampling system located downstream of the turbine test section consists of a 1/2 inch (0.035 in wall) 316 stainless steel tube facing into the flow. A high temperature valve provides shut off for the changing of the Balston total filter during a run. After the Balston filter there are various coolers and a water knockout followed by a manual flow control globe valve. After the expansion valve, the flow may either be sent to a wet test meter for direct measurement, or the flow rate may be measured through a rotameter and the total flow obtained by integration over the sampling time. This system is shown schematically in Figure 10. Note both the probe and the filter are purged when not in use.

The other system upstream of the turbine test section is referred to as the cyclone and impactor particulate sampling system (CIPSS). The CIPSS was initially intended to accommodate any sampling device. A Southern Research Institute 5-cyclone sampling train and a University of Washington 7-stage impactor have been used in this system to sample the flue gas for particulate. The use of both the SRI cyclone and the UoW impactor is still experimental, so none of the results obtained are reported here. With a minor piping change the pressure vessel used to house the other sampling systems was by-passed and a 7 inch Balston total filter was installed in its place. This filter made use of the remainder of the sampling train (cooler, knockout, flow control valve, etc.) as shown in Figure 11. The section of the CIPSS before the sampling device is similar to the other sampling system with two exceptions. First the probe is 3/8 inch (0.035 in wall) 316 stainless steel tubing. Second the line is fairly long and thereby necessitates electrical heating to prevent condensation.

The locations of these particulate sampling systems are shown in Figure 3. During the corrosion test program both the Balston filter and the CIPSS particulate sampling systems were used. The CIPSS system was used with one Balston total filter. Once the validity of the modified CIPSS system results were confirmed by comparing them to a Balston filter sampling system results taken concurrently, the CIPSS system was used preferentially. This was done primarily because the sample flow of the high pressure gas upstream of the turbine test section was easier to regulate than that of the lower pressure gas downstream.

Figure 10

BALSTON FILTER PARTICULATE SAMPLING SYSTEM

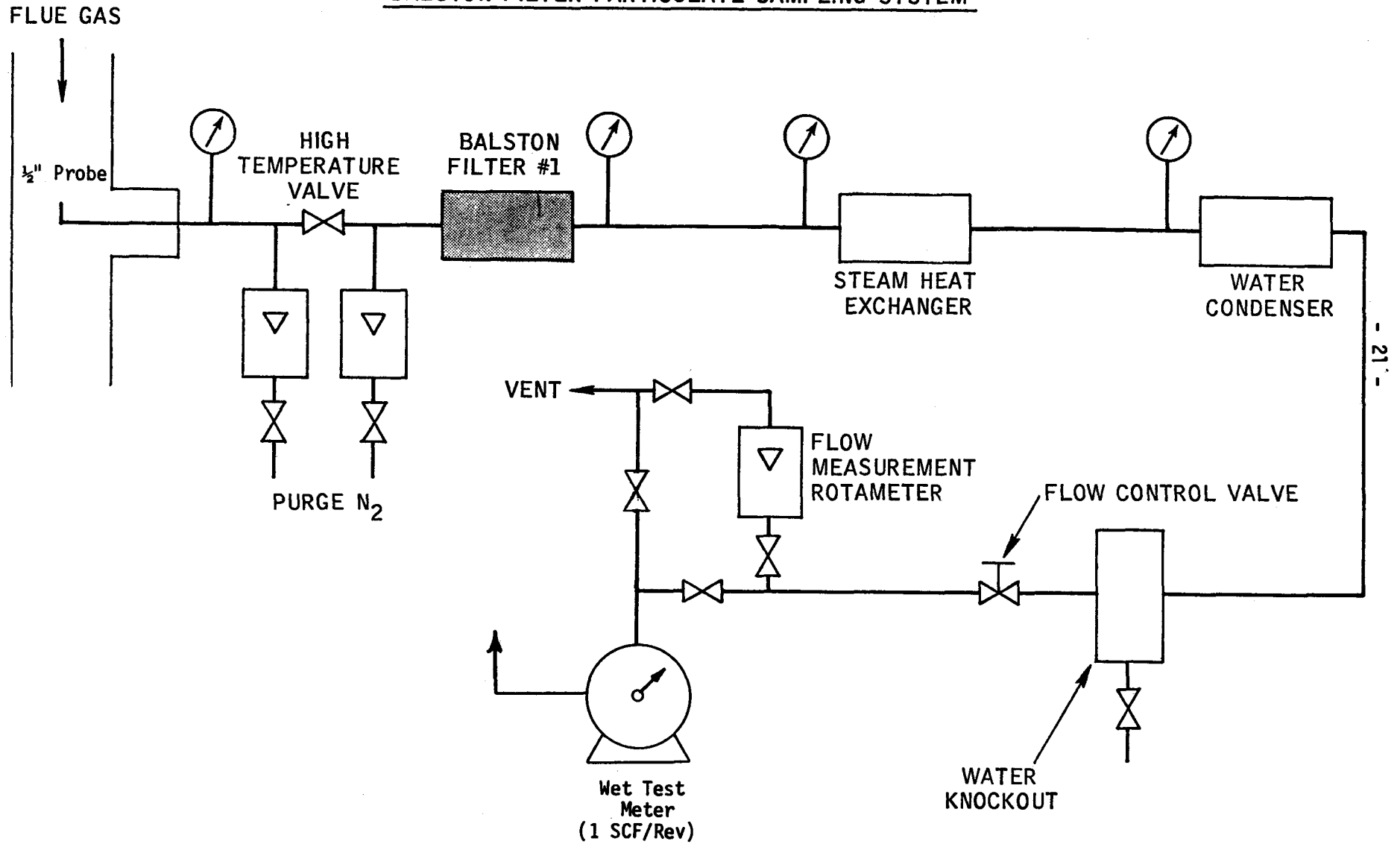
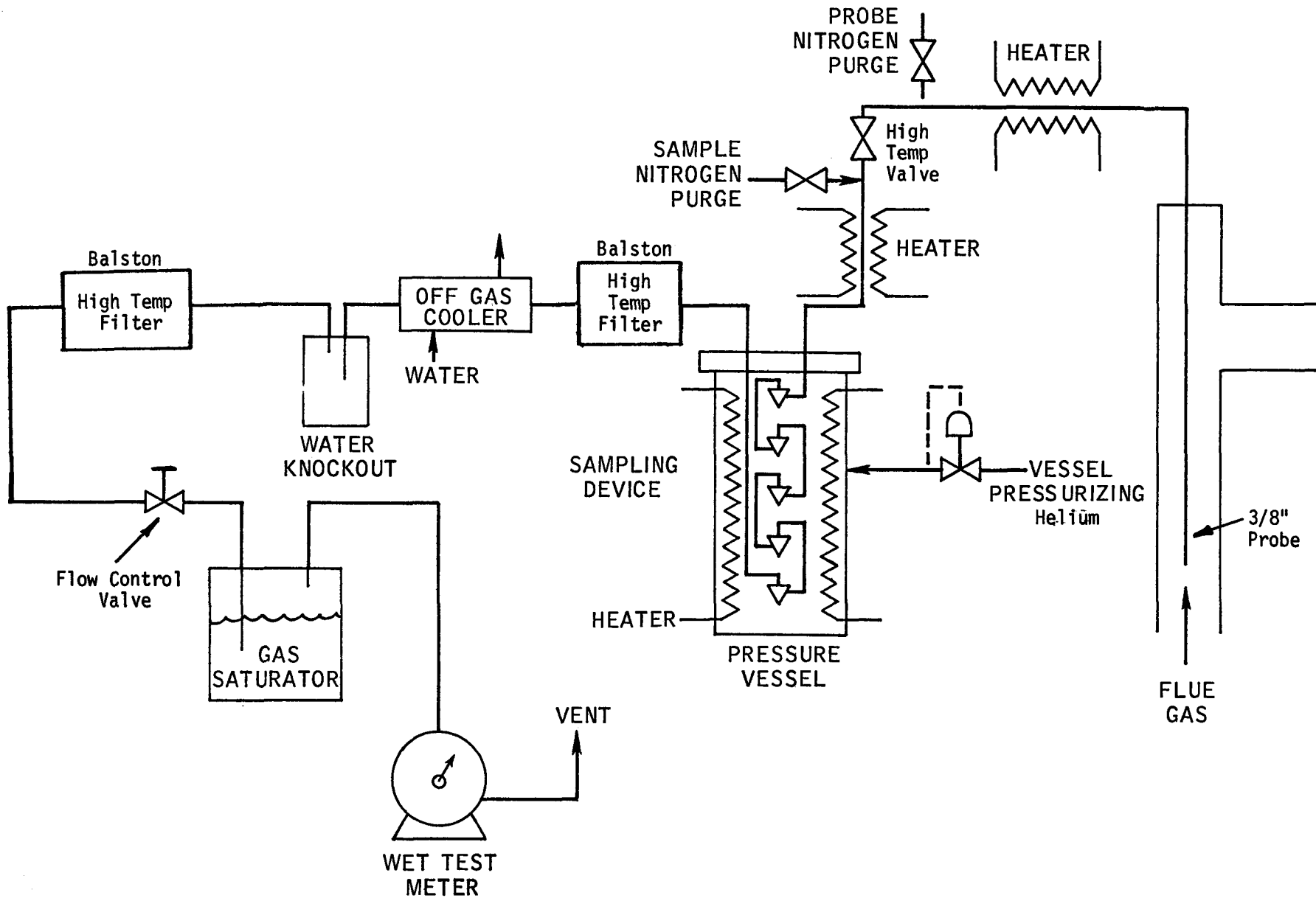


Figure 11
CYCLONE AND IMPACTOR PARTICULATE SAMPLING SYSTEM



Particulate Size Measurement

Particle size measurements for all of the 1000 hour exposure tests were done with a combination sonic sifter/Coulter Counter technique. Samples with significant concentrations of particles larger than 40 μm were first screened through a sonic sifter. The -325 US Mesh (44 μm) fraction from the sifter was analyzed with the Coulter Counter Model TA II with a 100 μm aperture. Material sized in this manner includes all second cyclone dump material, and some third cyclone dump material. Finer material, without significant material larger than 40 μm , is analyzed only with the Coulter Counter.

Balston filter particulates are carefully removed from the filter cake. Care must be taken to avoid mechanically brushing the filter cartridge material to prevent contamination. The particulate is redispersed in Isoton II with a dispersant in a sonic bath. This mixture is further diluted and analyzed with a 30 μm aperture probe on the Coulter Counter. If there is a reasonable amount of material larger than 12 μm , the sample is also analyzed with a 100 μm probe. The two size distributions are then combined with the dual aperture sizing technique developed by Coulter Counter Electronics, Inc.

Particle size distributions obtained with the above procedures for run 78 second and third cyclone dump material have been compared to distributions obtained with other size measurement equipment. Samples of the material were sent to General Electric who obtained size distributions with their Bahco particle size analyzer. The Bahco measures the aerodynamic equivalent diameter, whereas the Coulter Counter measures volumetric equivalent diameter. The size distributions for the second and third stage cyclone dump material are shown in Figures 12 and 13.

Continuous Particulate Monitor

A continuous, on-line particulate monitoring system was evaluated during run 80. The monitoring system (manufactured by IKOR, Inc., Gloucester, Massachusetts) makes use of the surface charge that particulates acquire during their flow through the combustion unit. The unit showed unexpected sensitivity to gas temperatures which made comparison of the signal amplitude with gravimetric sampling difficult. This indicated that while a gross change in particulate loading could be identified, the IKOR probe, in its present condition, could not be employed as a reliable device for controlling or monitoring particulate loading for the PFBC technology.

The IKOR system consists of two components. One of the components is a control and recording system; the other is a 1/4 inch diameter type 316 stainless steel rod which acts as the probe. The probe is inserted normal to the gas flow and acts as a site for particulate impaction. Each particle impacting on this probe transfers its accumulated charge to the probe. This

Figure 12

**Comparison of Particle Size Distribution
Via Bahco Vs. Coulter Counter of
Secondary Cyclone Dump Material (Run #78)**

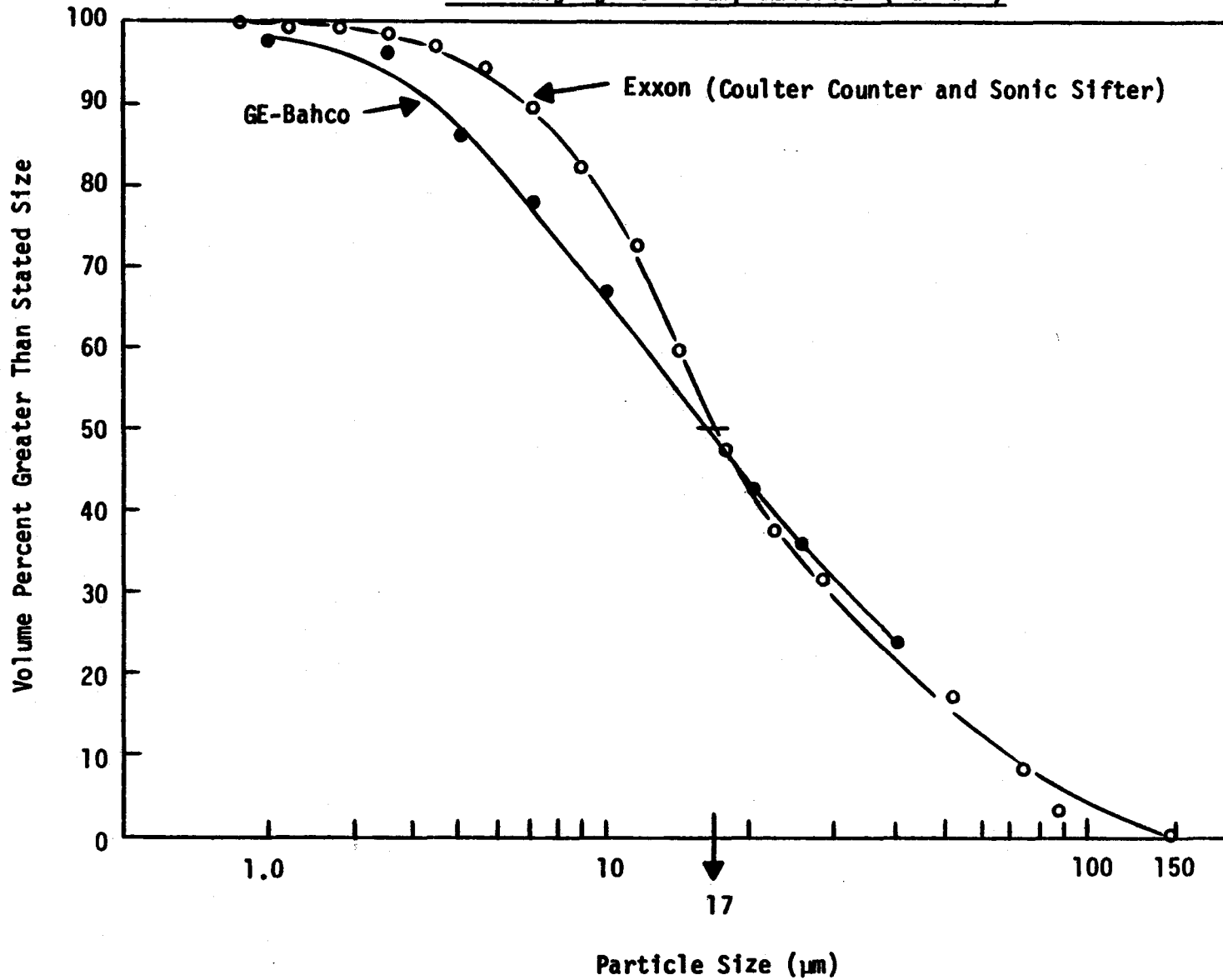
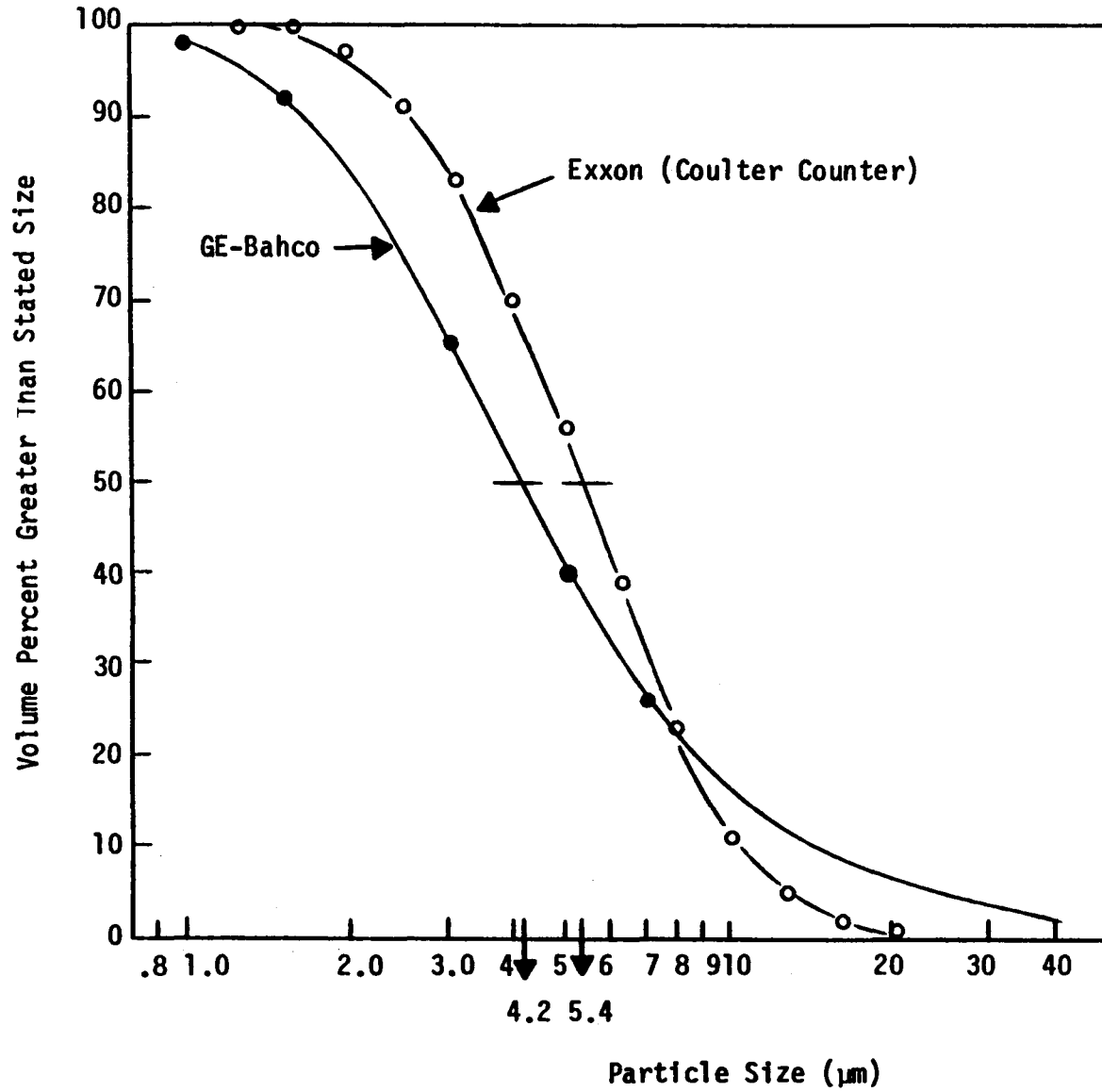


Figure 13

Comparison of Particle Size Distribution
Via Bahco Vs. Coulter Counter of
Tertiary Cyclone Dump Material (Run #78)



charge transfer effect generates an integrated output signal that is proportional to particulate mass flow in the gas stream. The magnitude of the integrated signal is correlated with a particulate loading measurement taken during the same time period. A strip chart is used to record and display the output.

The stainless steel probe, which was located in the off gas line about seven feet downstream of the GE turbine test section, survived the 215 hour test without noticeable damage. The gas temperature at the probe location was in the range of 1500-1525°F.

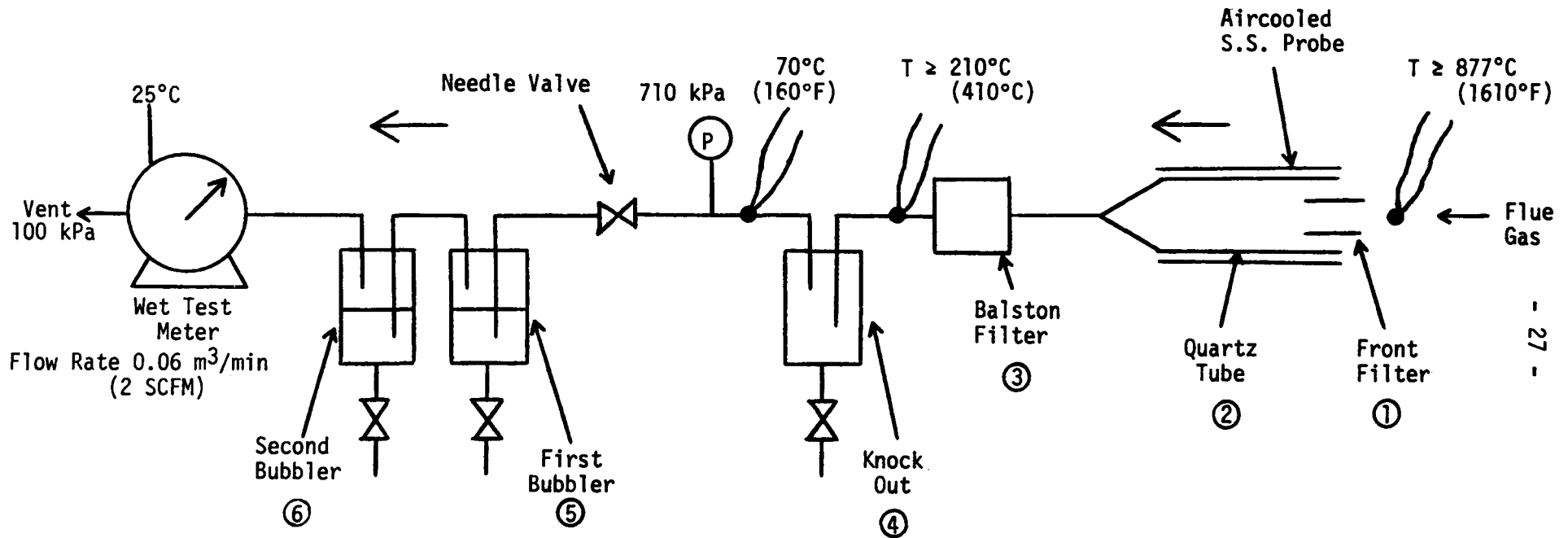
ALKALI PROBE TRAIN

An alkali probe train was designed and constructed by Exxon Research to enable acquisition of a hot pressurized flue gas sample before entering the turbine test section. The probe was designed to measure vapor phase Na and K concentrations of the flue gas at 1550°F and 9 atm pressure. Figure 14 is a schematic of the alkali probe train. The temperatures shown are those for test 4 of run 78, these are representative of normal operating conditions.

The hot pressurized flue gas enters the probe at system temperature and pressure and is prefiltered through three layers of astroquartz. Na and K vapors in the flue gas are then condensed on the walls of an air cooled quartz tube, which lowers the flue gas temperature from approximately 1550°F to 400°F. Alkali metals which condense on particulates in the flue gas are collected in a Balston filter after exiting the quartz tube. Flow is manually controlled by a needle valve and measured by a wet test meter.

Figure 14

Schematic of Alkali Probe Train
Alkali Test 4 During Run 78



- ① Front filter + particulates
- ② Quartz tube
- ③ Balston filter + particulates
- ④ Knock out solution
- ⑤ First distilled and deionized water bubbler
- ⑥ Second distilled and deionized water bubbler

IV. PRELIMINARY AND SHUTDOWN TESTS

PREPARATION RUNS

A preliminary hot test was undertaken to test the temperature control for the Westinghouse Research specimen probes. The initial twenty-one (21) heat exchanger specimen probes supplied by Westinghouse Research were installed - twelve (12) in the bed region and 9 in the freeboard region (Figure 1). (Table 2 lists the 21 probe material specimens, their combustor location and intended operating temperature.) The turbine test section was not installed during these preliminary tests.

The test indicated that high pressure air was necessary to effectively cool all 21 probes. Control of the high temperature bed probes and all of the freeboard probes appeared feasible using air pressure at 10 psig but cooling the in-bed probes at the lower temperatures, namely 1050°F and 1200°F, required an alternate source of high pressure air (150 psig) since the large volume of air necessary for cooling at these lower temperatures resulted in high pressure drops across the control valves and test probe. By-pass loops around the control valves were not necessary when this high air pressure air (150 psig) was used. Stable control was maintained by throttling the cooling air upstream of the control valve. The above-bed probes were cooled by air from a blower operating at 10 psig. Tests had shown that temperature control at 1400°F and 1200°F was excellent in the freeboard region. When the probes were at 1600°F, smaller trims were installed in the control valves in order to achieve steady control at this temperature.

Natural gas, i.e., methane, injection into the flue gas line between the second stage cyclone and the granular bed filter was investigated as a means of maintaining the flue gas temperature above 1550°F before entering the turbine test section. Natural gas was injected 7.5 feet downstream of the second stage cyclone and the effect on the line temperature profile was observed. As seen in Figure 15, most of the natural gas appears to have burned within 5 feet of the injection point. Injection of 2.8 SCFM of natural gas into 620 SCFM of flue gas raised the line temperature from 1380°F to 1525°F 50 feet downstream of the injection point. The presence of "hot spots" near the injection nozzle caused by the instantaneous combustion of the natural gas was also investigated. Figure 16 shows that the gas does not begin to burn until it is several inches downstream of the injection point. Combustion then occurs uniformly over the next 5 feet before it is complete, as indicated by a temperature decline. As a result of these tests, a total of five (5) equally spaced injection nozzles were installed in the flue gas line between the second stage cyclone and the turbine test section (Figure 9). This enabled the flue gas to be maintained above 1550°F throughout the entire run of pipe without the occurrence of large temperature spikes.

Figure 15

Methane Injection - Temperature Profiles

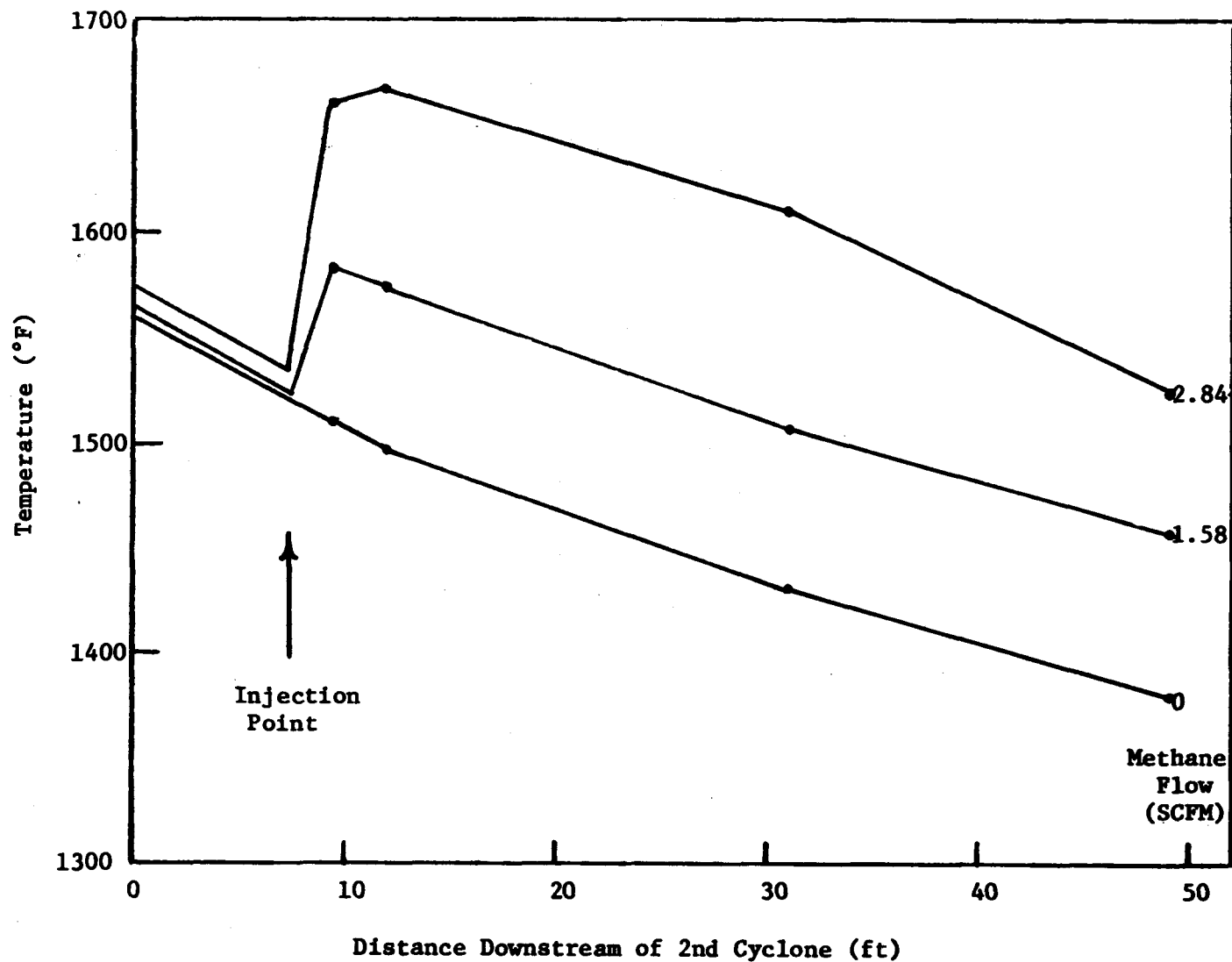
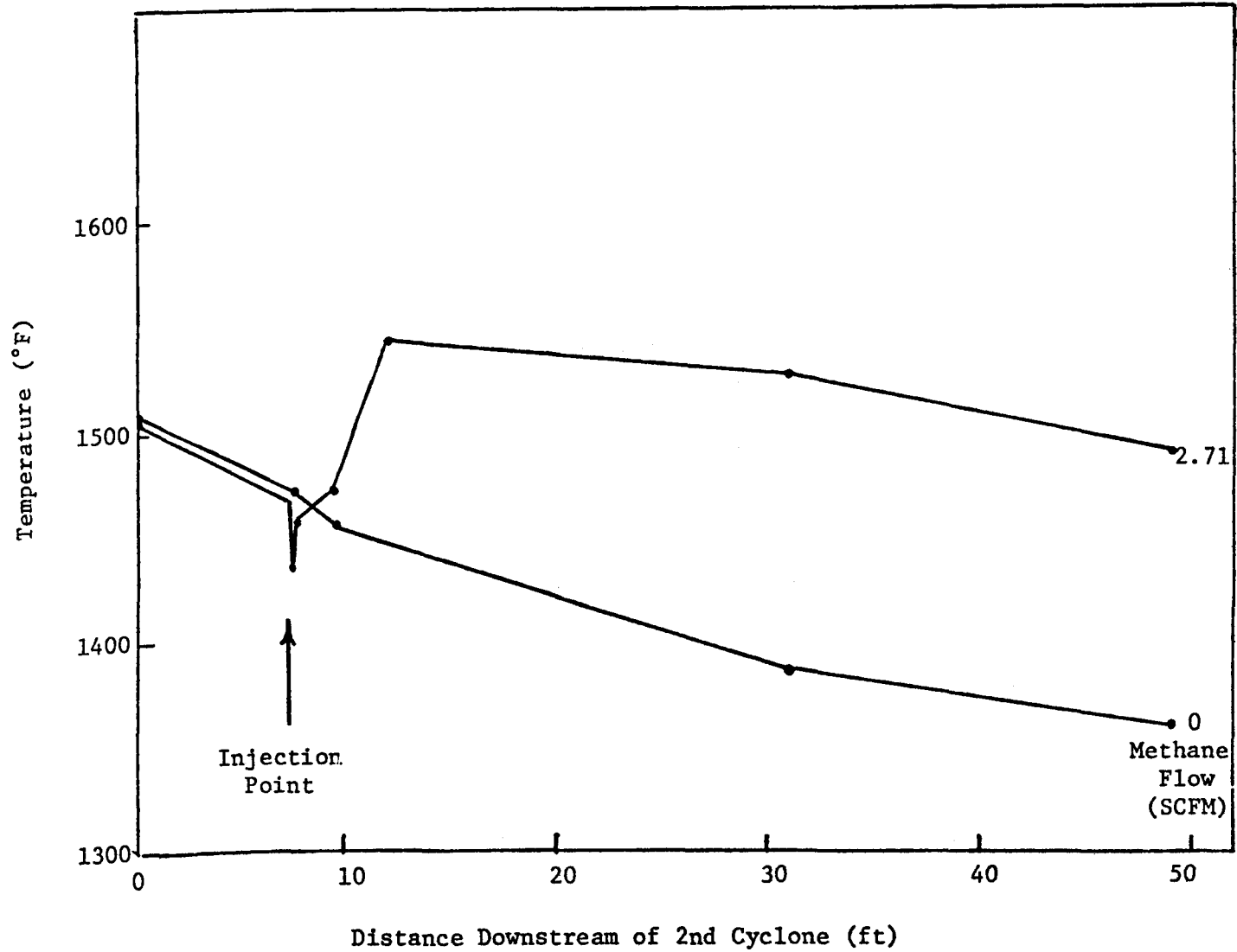


Figure 16

Methane Injection - Temperature Profiles



SHAKEDOWN TEST #1

Preparation for the 100 hour shakedown run included installation of the following major items: 21 heat exchanger specimen probes in the combustor, the turbine test section and associated discharge line modifications, a new pressure control system employing a by-pass loop around the turbine test section, and new combustor heat exchanger coils located above and below the in-bed heat exchanger specimen probes.

The turbine test section supplied by General Electric was installed in the discharge line immediately downstream of the granular bed filter (Figure 3). A new section of discharge pipe was fabricated and refractory lined to permit the insertion of the turbine test section. During a run both turbine mass flow and inlet temperature are scanned once a minute and recorded on magnetic tape. Particulate and analytical sampling trains were also located downstream of the turbine section at 200 kPa pressure.

Three (3) sets of granular bed filters, each containing 3 beds, were installed in the filter vessel downstream of a high efficiency cyclone (see Table 4 for dimensions). Improved blow back seals were adapted to each element, and methane addition and flow control capability was provided for each element. An oxygen sensor was interlocked with the methane addition system to alarm and shut off the methane injection if the oxygen level in the flue gas went below 1 percent. The cyclone, piping, and filter shrouds within the GBF vessel were wrapped with high temperature blanket insulation.

Preparations for the intended 100 hour shakedown run were completed on November 23, 1977 and test operations started on November 28th with the heat up of the granular bed filter vessel. The shakedown test (Miniplant Run 66) had to be terminated after 17 hours of operation due to excessive pressure drop across the granular bed filter. At one point, the filter pressure drop climbed as high as 207 kPa (30 psi). The blow back flow (cleaning cycle) was then increased in an attempt to lower the ΔP . A significant amount of filter media was lost because of the higher blow back velocity. However, the filter ΔP was lowered to approximately 7 kPa (10 psi) and remained constant until a fire in the coal feed injector vessel, caused by the pressure upsets during the high flow blow backs of the filter, forced the termination of the run.

Inspection of the filter elements after the run showed substantial plugging of the bottom support screen, the inlet retaining screens were relatively clean. This plugging caused the high pressure drop across the filter.

During the last 2 hours of the run the particulate concentration was measured at 0.06 gr/SCF. A summary of the operating conditions and emissions during the run is given in Table 5.

Table 5

Miniplant Operating Conditions and Emissions

Nominal Operating Conditions	<u>Shakedown Runs</u>				
	Run 66	Run 67.1	Run 67.2	Run 67.3	Run 67.4
Date 1977	11/29	12/12-12/13	12/13-12/14	12/15	12/15-12/16
Run Length (hrs)	17	28	25	10	37
Pressure (kPa)	930	930	930	930	930
Temperature (°C)	918	915	915	915-875	875
Superficial Velocity (m/sec)	1.6	1.7	1.7	1.6	1.6
Expanded Bed Height (m)	3.2	3.3	3.4	3.2	3.0
Excess Air % (Air/Fuel Ratio)	10	19	14	14	31
Coal Feed Rate (kg/hr)	130	118	130	125	115
Nominal Ca/S Molar Feed Ratio	1.25	1.25	1.25	1.25	1.25
<u>Flue Gas Emissions</u>					
SO ₂ (ppm)	370	675	625	612	650
NO _x (ppm)	20	100	65	65	105
CO (ppm)	205	300	160	312	200
CO ₂ (%)	12	14	15	12	12
O ₂ (%)	1.9	3.0	2.5	2.5	~5

Note: Run 67.1 - From startup to shutdown when larger pressure control nozzle was installed
 Run 67.2 - Steady state combustor operation at 915°C
 Run 67.3 - Transition period when combustor temperature was lowered from 915°C to 875°C
 Run 67.4 - Steady state combustor operation at 875°C maintained till shutdown

Eighteen of the 21 heat exchanger probes exhibited excellent temperature control throughout the run. However, control of the three in-bed probes intended for 1400°F conditions was somewhat erratic due to insufficient pressure of the air supply blower.

Temperature measurements of the probes controlled at the various temperatures showed the following gradients throughout the length of the probe, i.e., from "inner" to "outer" specimen.

1600°F	In-Bed	= 25°
	Above Bed	= 45°-60°
1400°F	In-Bed	= 200°
	Above Bed	= 40°-65°
1200°F	In-Bed	= 40°-140°
	Above Bed	= 225°-315°
1050°F	In-Bed	= 225°

Steady state was never established at the turbine test section inlet during this run, and the test was terminated before inlet temperature and pressure reached design specifications. Maximum inlet temperature was just under 1300°F (700°C) and maximum pressure just under 8.6 atm. Mass flow rate through the turbine test section started at 0.82 #/sec (650 SCFM), but continually decreased to 0.68 #/sec (540 SCFM) by the end of the run.

Examination of the turbine pressure reducing station following the run indicated that the orifice plate was partly plugged with small pieces of refractory which had broken off from the spool piece connecting the turbine test section. The obstruction of the flow area accounted for the declining flow rate through the turbine test section.

100 HOUR SHAKEDOWN TEST

Preparations for a second attempt at accomplishing the 100 hour shakedown test were completed in early December. The 100 hour shakedown test (Miniplant Run No. 67) commenced on December 12 and concluded at 11 P.M. on December 16, 1977.

Illinois No. 6 coal and Pfizer 1337 dolomite were fed to the combustor at a nominal calcium to sulfur molar ratio of 1.25. An analysis of the coal combusted is presented in Table 6.

The test was made using the third stage cyclone located in the GBF pressure vessel as the tertiary cleanup device. Because of the difficulties encountered in the previous test, the granular bed filters were eliminated. Methane was injected at 5 locations in the flue gas line between the second stage cyclone and the turbine test section. This enabled the flue gas to be maintained above 1550°F at the entrance to the turbine test section.

Table 6

Coal and Sorbent Analyses

(Used in Shakedown Runs #66 and 67; Nov-Dec, 1977)

Illinois No. 6 Analysis

Sample No. → Basis →	1		2		3		Avg.	
	<u>As Rec'd</u>	<u>Dry</u>	<u>As Rec'd</u>	<u>Dry</u>	<u>As Rec'd</u>	<u>Dry</u>	<u>As Rec'd</u>	<u>Dry</u>
Moisture (%)	2.00	-	2.00	-	2.05	-	2.02	-
Ash (%)	10.56	10.78	10.06	10.27	8.94	9.13	9.85	10.06
Sulfur (%)	4.14	4.22	4.12	4.20	3.95	4.03	4.06	4.15
Heating Value (BTU/#)	12,353	12,605	12,425	12,679	12,580	12,843	12,453	12,709

Pfizer 1337 Dolomite Calcined Analysis

	<u>CaO</u>	<u>MgO</u>	<u>Cl</u>	<u>Na</u>	<u>K</u>	<u>Fe₂O₃</u>	<u>SiO₂</u>	<u>Al₂O₃</u>	<u>S</u>
Weight Percent	56.6	42.69	0.25	1800 ppm	190 ppm	1.75	0.86	2.58	0.63

The combustor was operated at an average temperature of 1700°F for the first three days, but had to be lowered the last two days to maintain 9 atm pressure. Operations had to be interrupted for several hours because of a plugging problem in the turbine pressure reducing station. During the shut down, a larger pressure control nozzle was installed to allow for increased by-pass flow around the turbine test section without an increase in the combustor pressure.

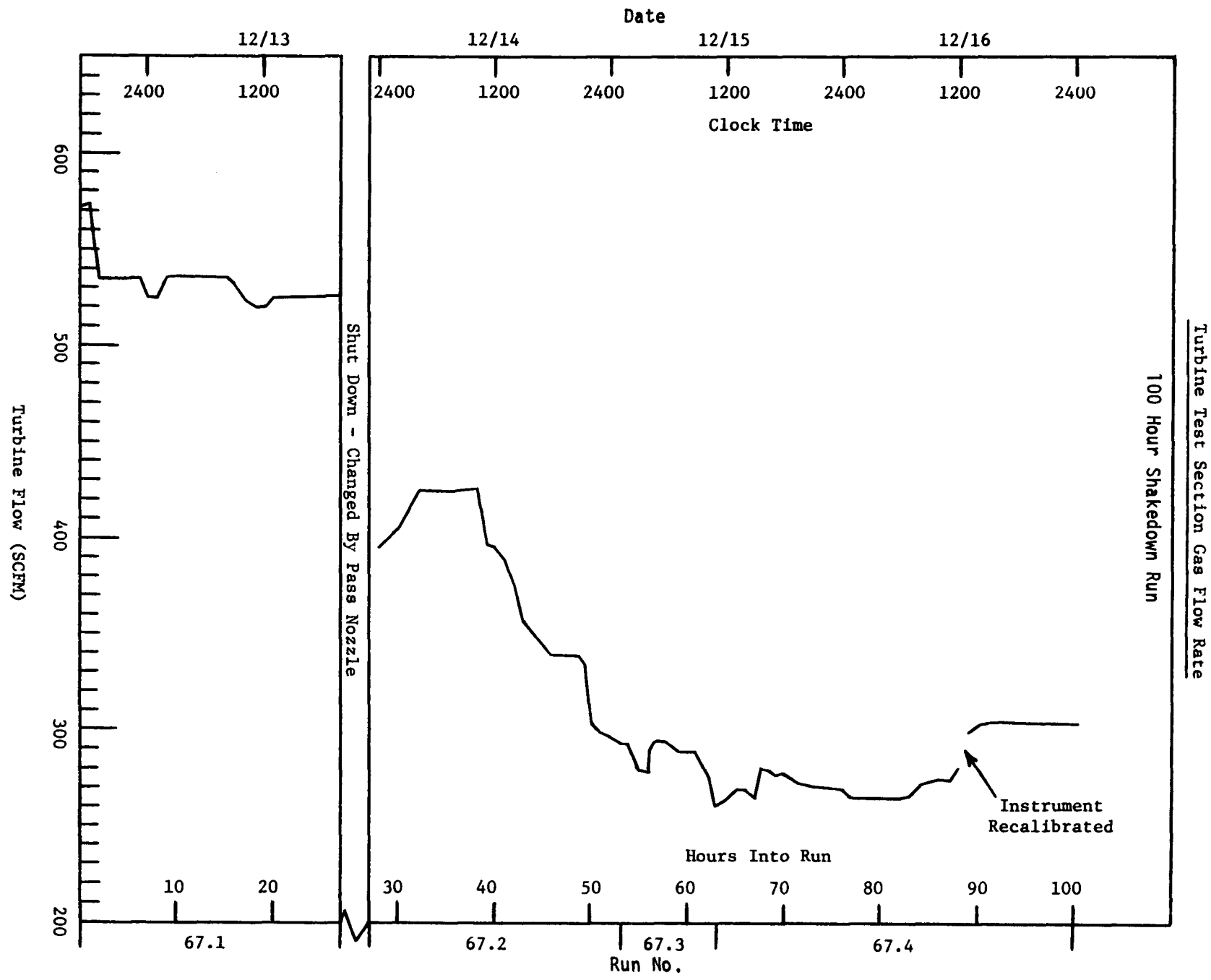
A summary of the operating conditions and gaseous emissions during this test is given in Table 5. The run can be broken down into four parts with respect to operating conditions and turbine flow rates. The first 28 hours of the run (run 67.1) represents the time from initial heat up of the unit to the first shutdown when a larger pressure control nozzle was installed. During the next 25 hours (run 67.2) steady state combustor operations were maintained. Flow through the turbine continued to decline during this part of the run as seen in Figure 17. This was the result of plugging of the pressure reducing station. The temperature at the turbine test section had to be lowered during the run to maintain a 9 atm combustor pressure. This was accomplished by ceasing methane injection into the off gas piping, and later lowering the combustor operating temperature. During this transition period of approximately 10 hours (run 67.3) the combustor temperature was lowered from 1680°F to 1607°F. Flue gas temperatures show this effect, increasing initially with unit heat up and then decreasing to a constant level after 70 hours (Figure 18). Steady state operations were maintained for the remainder of the 100 hours (run 67.4).

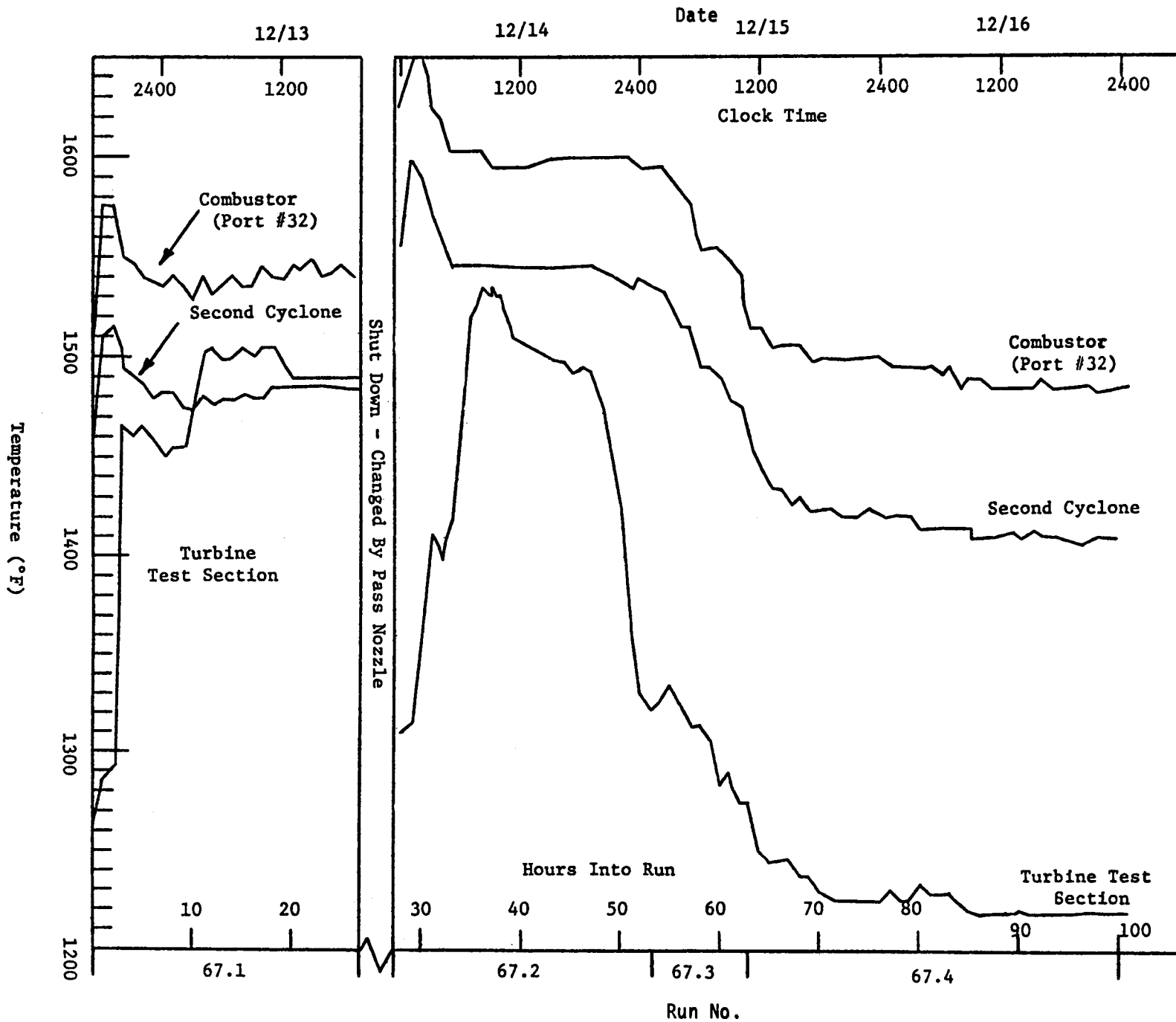
Turbine Test Section

The gas flow rate through the turbine section was lower than General Electric specifications during most of the run. Figure 17 shows the turbine gas flow rate dropping off during the first 50 hours of the run. The flow rate was fairly stable at 300 SCFM for the remainder of the run. Inspection of the turbine pressure reducing station following the run revealed that the inlet orifice plate was partly plugged with small pieces of refractory which had broken off from the spool piece connecting the turbine test section. Flyash adhered to the refractory pieces caught in the inlet orifice plate and eventually obstructed approximately 75% of the flow area. About 35 gm of flyash and 15 gm of stone were removed from the pressure reducing section after the run. Significant amounts of flyash were also found on some internal surfaces of the turbine test section. Approximately 150 gram of flyash was found adhered to the downstream face of the flow distributor plate. The upstream face of the plate was very clean (Figure 19). Another 130 gm of the flyash was found impinged on the conical portion of the cascade section. The particle size analysis for these samples are presented in Table 7. The turbine blade specimens used for the shakedown phase were removed, photographed and returned to GE for metallurgical analysis.

During the shakedown test there were several intervals where the particulate loading increased. Upon microscopic examination after the test some of the airfoil leading edges displayed a knife edge erosion configuration.

Figure 17





Flue Gas Temperature History
 Shakedown

Figure 18

Figure 19

Turbine Test Section Flow Distributor
Plate and Conical Inlet After Shakedown (Upstream Face)



Table 7
Particulate Size Distribution

Shakedown Run

Sample	44	10	8	6	4	2	1	Microns
	Percent Finer Than							
TTS Pressure Reduction Section	85	75	67	56	36	14	5	
TTS Rear of Flow Distributor	93	74	62	44	20	5	1	
TTS Cascade Housing	89	69	59	46	27	7	2	
Balston Filter #1 (61 Hours Into Run)	--	90	86	80	73	62	29	
Cyclone #3 Dump #33	98	76	67	55	37	13	1	

Views of the leading and trailing edges of the 4 turbine cascades after 100 hours of exposure appear in Appendix A, Figures A-1 to A-4. The deposition on the trailing edge can be clearly seen. Deposition was much heavier than after the first 17 hour shakedown tests.

Particulate Sampling

The flue gas particulate loading was measured throughout the run using 3 methods. As in prior runs, most of the samples were taken from an isokinetic slip stream using two Balston filters operating above the gas dew point. Three EPA Method V samples were taken from the cooled flue gas just upstream of the scrubber. Another sample was obtained using a set of 5 cyclones supplied by Southern Research Institute. All three methods consistently agreed with particulate concentrations ranging from 0.03 to 0.08 gr/SCF (Table 8). A similarly low particulate loading of 0.056 gr/SCF was measured using the Balston filters in run 66. Particle size analysis for the Balston filters collection of run 67 is presented in Table 7.

Chemical analysis of the flyash collected during the 100 hour shakedown run is listed in Table 9 according to collection point and run segment.

Table 8
Flue Gas Particulate Loading
Shakedown Run

Run #	Sampling Start Time	Sampling Duration	Sampling Method	Result	
	(Hours Into Run)	(hrs)		(grains/SCF)	(g/m ³)
67.1	6	2	Balston Filters	0.057	0.13
	17	2	EPA Method V	0.07	0.16
	17	2	Balston Filters	0.053	0.12
67.2	30	2	Balston Filters	0.081	0.18
	41	2	Balston Filters	0.058	0.13
	43	2	EPA Method V	0.05	0.1
67.3	53	2	Balston Filters	--	(1) --
	61	2	Balston Filters	0.066	0.15
67.4	72	13	Southern Research Cyclones	0.030	(2) 0.07
	87	3	EPA Method V	0.04	0.08

(1) Flue gas sample flow rate cannot be determined.

(2) Flue gas sample flow rate was lower than specified by the cyclone manufacturer.

Table 9

Run 67 - Fly Ash Chemical Analyses

	<u>Ca</u>	<u>S</u>	<u>SO₄</u>	<u>CO₃</u>	<u>C</u>	<u>Mg</u>
<u>Run 67.1</u> (Dumps)						
2nd Cyclone (5-9)	7.3	5.39	14.01	0.45	4.69	3.1
2nd Cyclone (10-14)	7.1	5.03	16.4	0.51	4.2	3.4
3rd Cyclone (5-9)	6.7	6.05	19.85	0.03	1.26	3.9
3rd Cyclone (10-14)	6.8	6.90	20.61	0.01	1.23	4.1
<u>Run 67.2</u>						
2nd Cyclone (18-22)	8.4	5.26	16.37	0.84	3.43	4.3
2nd Cyclone (23-27)	8.4	5.44	17.68	0.49	3.66	4.2
3rd Cyclone (18-22)	6.9	8.02	23.29	0.13	2.26	3.5
3rd Cyclone (23-27)	6.8	6.19	18.64	0.08	1.16	3.4
<u>Run 67.3</u>						
2nd Cyclone (28-32)	7.3	4.99	15.34	0.51	4.01	3.6
3rd Cyclone (28-32)	6.1	8.02	21.53	0.21	0.40	3.6
<u>Run 67.4</u>						
2nd Cyclone (42-46)	4.3	5.17	15.66	0.49	4.78	2.1
2nd Cyclone (47-51)	6.9	5.78	16.19	0.48	4.53	3.4
3rd Cyclone (41-45)	6.7	9.3	28.78	0.09	1.06	5.0
3rd Cyclone (46-50)	6.9	8.78	28.29	0.04	1.15	4.9

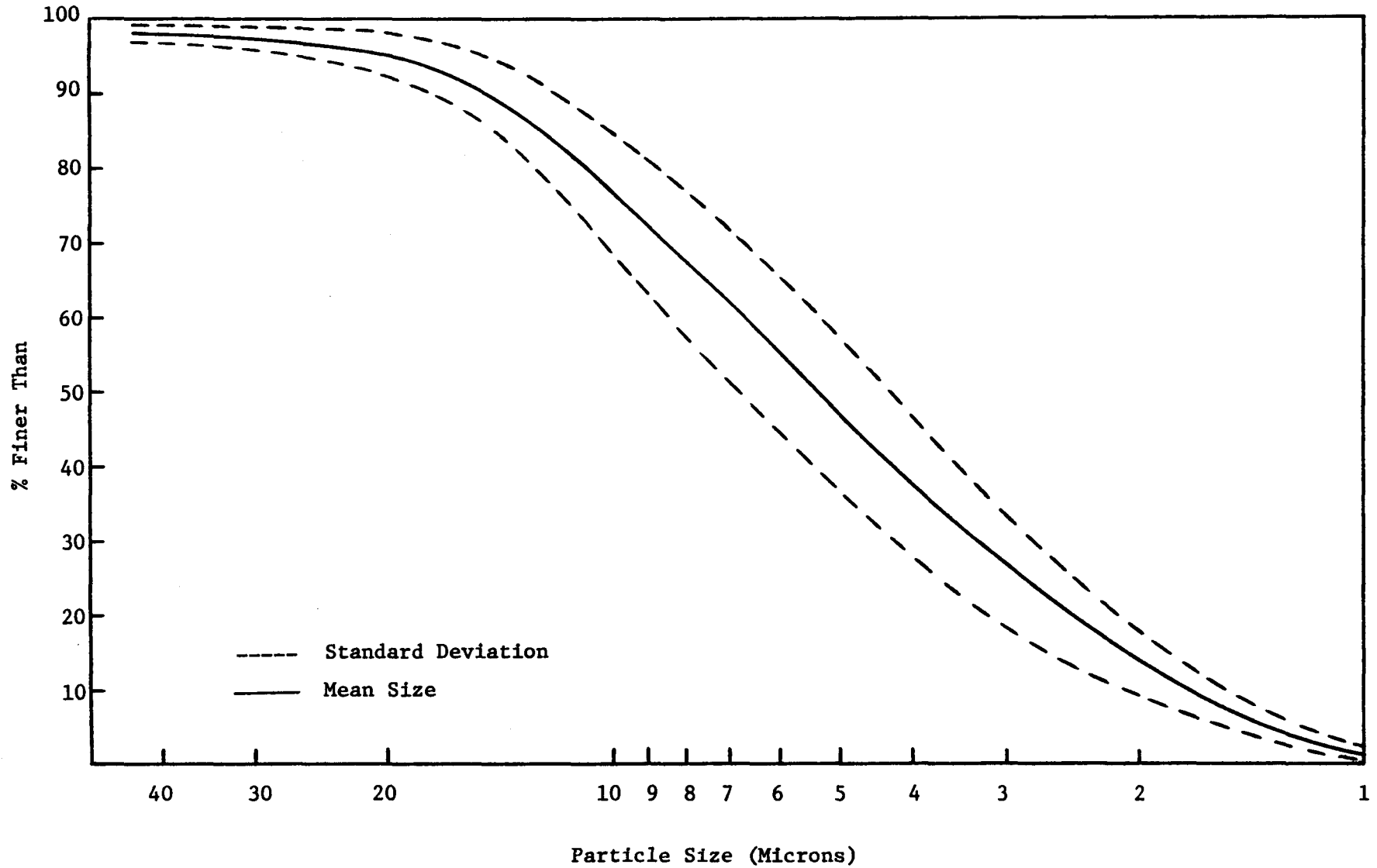
The particle size distribution of particulates captured by the third stage cyclone during the 100-hour shakedown run (run 67) is shown in Figure 20. The solid line represents the mean size distribution of 8 cyclone lock hopper dumps. The dashed line represents the standard deviation. The mean particle size distribution is consistent with calculated values for a conventional cyclone with those dimensions. The standard deviation is approximately $\pm 10\%$, and probably represents the limit of accuracy of the current particle size analysis technique; this consists of a wet sieving with a 325 US mesh (44 μm) screen. The minus 325 mesh is then used for Coulter Counter analysis.

Heat Exchanger Probes

All 21 heat exchanger probes exhibited excellent temperature control throughout the run. However, the above bed 1600°F probes were somewhat cooler than desired in the later part of the run because the combustor environment was at a slightly lower temperature than the control point.

Figure 20

Run 67 Tertiary Cyclone Captured Particulates
Mean Particle Size Distribution



Temperature data for the twenty-one (21) heat exchanger probes exposed during the 100 hour shakedown run are presented in Appendix Table A-1. Temperatures at two locations in each probe were recorded every 10 minutes for the first 25 hours; the time interval was increased to every 20 minutes for the remainder of the 100 hour run. In these tables the recorded temperatures have been averaged for five (5) hour segments of the run. Also listed are the standard deviations for that time period as well as the maximum and minimum temperatures experienced by the specimen material during those five (5) hours.

This collated temperature data of the heat exchanger probes generally reveals excellent temperature control of the individual specimens. Based on this data at steady combustor conditions 40% of the individual specimens would not experience a temperature span greater than 20°F; 70% not greater than a 30°F span, and 100% not greater than a 60°F span. During steady state periods more than 75 percent of the specimens were maintained within a 20°F temperature range.

Appendix figures A-5 through A-11 are typical time-temperature histories of the different specimen probes controlled at the four (4) specified temperatures. The figures are as follows:

Figure 5	Probe 1	1600°F	In Bed
Figure 6	Probe 13	1600°F	Above Bed
Figure 7	Probe 6	1400°F	In Bed
Figure 8	Probe 14	1400°F	Above Bed
Figure 9	Probe 11	1200°F	In Bed
Figure 10	Probe 20	1200°F	Above Bed
Figure 11	Probe 8	1050°F	In Bed

As seen in these figures, temperature gradients throughout the length of the probe, i.e., from "inner" to "outer" specimen, exist even after extended exposure times. ("Inner" refers to the tube specimen nearest the center of the combustor.) The mean temperature of two specimens on a probe characteristically differed by the an average of 20° to 180°F. In this run temperature control of the probe was maintained so as to prevent either of the two specimens from exceeding the designated temperature.

The heat exchanger probes have been photographed in groups of three (3) according to their operating temperatures and location in the combustor. These photographs are presented in the appendix, Figures A-12 through A-18.

V. PFBC EXPOSURE TEST RESULTS

TEST SUMMARY

The 1000 hour exposure test was completed in several segments between June 1978 and June 1979. The longest continuous run was 250 hours. Other runs were between 217 and 100 hours in duration. A chronological summary of the PFBC hot corrosion/erosion testing is presented in Table 10. During the 5 runs that comprise the 1000 hour test run conditions were acceptably steady. Many flue gas, particulate, coal and sorbent samples were taken. Most of these samples were analyzed and are included in the run summaries in Table 11.

Run 78 was the first run of the 1000 hour exposure test. This run marked the longest continuous operation of the miniplant - 250 hours. The combustor was operated at an average temperature of 1700°F throughout the 11 day period, and at a constant 9 atm pressure. Operations had to be interrupted several times due to coal feeding problems caused by line erosion. The total lost time after the unit was lined out was 6 hours. Run conditions were well controlled during the test with mass flow and temperature in the gas turbine test section reasonably steady. The turbine test section flow rate averaged 720 SCFM. Natural gas injection at 5 locations in the flue gas line between the second stage cyclone and the turbine test section maintained the flue gas above 1580°F before entering the test section. Flue gas temperature profiles at three times in the run are shown in Figure 21. Examination of the flue gas piping following the run revealed a large accumulation of flyash around thermocouple No. 5, resulting in an erroneous gas temperature reading. The thermocouple had become so inbedded in the deposits that it became isolated from the gas stream and was indicating a low temperature. Historical data indicated that the temperature drop across the 2nd cyclone is approximately 25°F. This temperature drop was used to correct the temperature profile. The corrected profile is shown in Figure 21. Correcting for this temperature measurement error, it would take approximately 40 hours before all points in the system were at a minimum of 1550°F. A graph of the combustor temperature at various times during the run is shown in Figure 22. The large temperature drop near the top of the combustor noticed during shakedown was eliminated with the removal of miniplant cooling coil 3B.

Run 78 was broken down into 10 parts to facilitate the data handling process. Illinois No. 6 coal and Pfizer No. 1337 dolomite were used in this run at a nominal calcium to sulfur molar feed ratio of 1.45. The SO₂ retention levels in the run averaged about 90%. This exceeds slightly the latest new source performance standard of 85% SO₂ removal specified by the EPA. During run 78, SO₂ emissions fluctuated more than expected. The variations in gas residence time and problems with the flue gas sampling system were responsible for most of the variations observed.

Table 10
 PFBC Miniplant
Hot Corrosion/Erosion Testing Summary

<u>Test Dates</u>	<u>Run No.</u>	<u>Run Length (Hours)</u>	<u>Cumulative Run Time (Hours)</u>	<u>Remarks</u>
November 29, 1977	66	17	17	Shakedown - 1st Attempt
December 12-16, 1977	67	100	117	Shakedown Completed
June 19-30, 1978	78	250	250	Specimens Removed & Inspected
July 31 - August 5	79	100	350	
September 13-22	80	215	565	Specimens Removed & Inspected
October 9-16	81	170	735	Specimens Removed & Inspected No deposits on turbine blades
May 29 - June 10, 1979	106	265	1000	Five hour interval of high particulate loading (plugged cyclone) Exposure testing completed. All specimens removed for metallurgical analysis.

Table 11

Miniplant Operating Conditions and Emissions

Nominal Operating Conditions	Run 78.1	78.2	78.3	78.4	78.5	78.6	78.7	78.8	78.9	78.10
Date (1978)	6/19-6/20	6/21	6/22	6/23	6/24	6/25	6/26	6/27	6/28	6/29-6/30
Run Length (hrs)	25	25	25	25	25	25	25	25	25	25
Pressure (psig)	120	120	120	120	120	120	120	120	120	120
Temperature (°F)	1640	1660	1670	1680	1690	1710	1720	1720	1720	1720
Superficial Velocity (ft/sec)	5.9	6.0	6.0	6.0	6.1	6.1	5.8	6.2	5.8	5.9
Expanded Bed Height (ft)	12.4	11.6	9.4	11.2	10.2	10.9	10.7	9.4	9.5	12.4
Excess Air %	34	25	23	21	15	25	15	15	15	34
Coal Feed Rate (lb/hr)	224	266	261	270	245	290	292	288	288	288
Nominal Ca/S Molar Feed Ratio	1.25	1.45	1.45	1.45	1.45	1.45	1.45	1.45	1.45	1.45
<u>Flue Gas Emissions</u>										
SO ₂ (ppm)	286	231	169	157	460	270	113	363	260	286
NO _x (ppm)	45	38	41	42	37	32	28	41	36	15
CO (ppm)*	679	679	613	655	644	667	590	724	596	679
CO ₂ (%)	12.5	14.0	13.7	14.3	14.3	15.3	14.0	15.6	16.0	12.5
O ₂ (%)	5.5	4.2	4.0	3.7	2.8	4.3	3.2	3.2	2.8	5.5
SO ₃ (ppm by wet chemistry)	0.6	--	9.9	--	--	--	12.8	--	--	0.4

 * CO analyzer appeared to be malfunctioning, reported levels may be high.

Table 11 (Cont'd)

Miniplant Operating Conditions and Emissions

Nominal Operating Conditions	Run 79	80.1	80.2	81	106.1	106.2	106.3
Date	7/31-8/4/78	9/13-16/78	9/16-22/78	10/9-16/78	5/29/79	5/31	6/2-10/79
Run Length (hrs)	100	100	115	170	43	5	217
Pressure (psig)	120	119	119	119	116	116	117
Temperature (°F)	1717	1704	1670	1710	--	--	--
Superficial Velocity (ft/sec)	6.2	5.8	5.8	5.9	5.61	5.31	5.38
Expanded Bed Height (ft)	10.1	12.7	7.0	N.A.	7.90	10.66	10.00
Excess Air %	24	27	18	25-30	15.6	5.8	9.0
Coal Feed Rate (lb/hr)	290	359	370	250	306	318	316
Nominal Ca/S Molar Feed Ratio	1.45	1.41	1.41	1.45	1.45-1.20	1.20	1.25
<u>Flue Gas Emissions</u>							
SO ₂ (ppm)	293	217	152	250-325	21.4	37.8	91.4
NO _x (ppm)	56	78	121	40-130	47.5	42.4	64.1
CO (ppm)*	--	--	--	--	332	507	540
CO ₂ (%)	14.6	13.0	12.4	13	14.8	16.4	13.4
O ₂ (%)	4.2	5.0	3.5	4.5-5.0	4.1	2.1	3.1
SO ₂ (ppm by wet chemistry)							
SO ₃ (average ppm)	~6.0	~3.0	~0.0				

 N.A. = Data Not Available

* CO analyzer malfunctioned.

Figure 21

Flue Gas Temperature History - Run 78

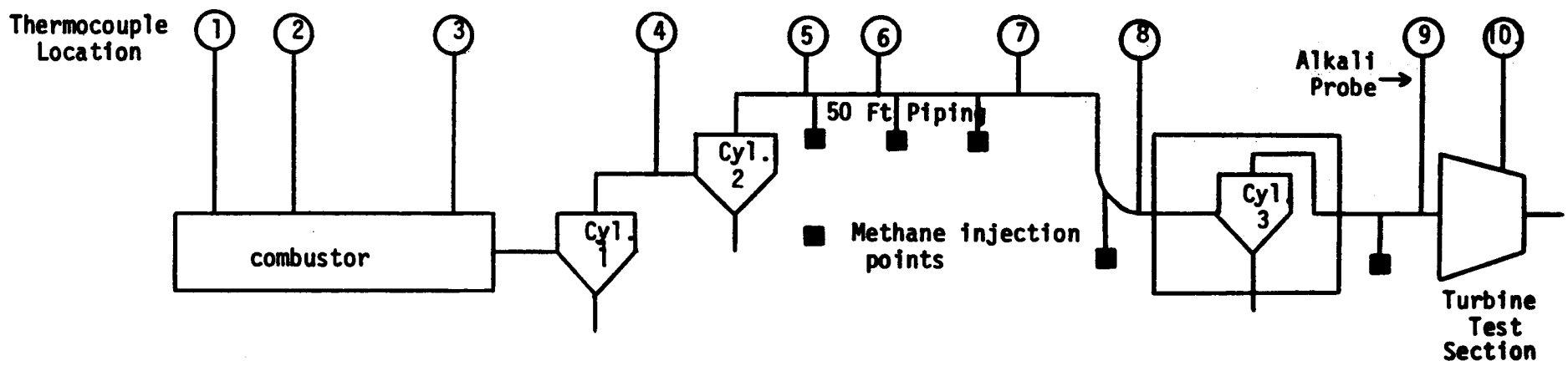
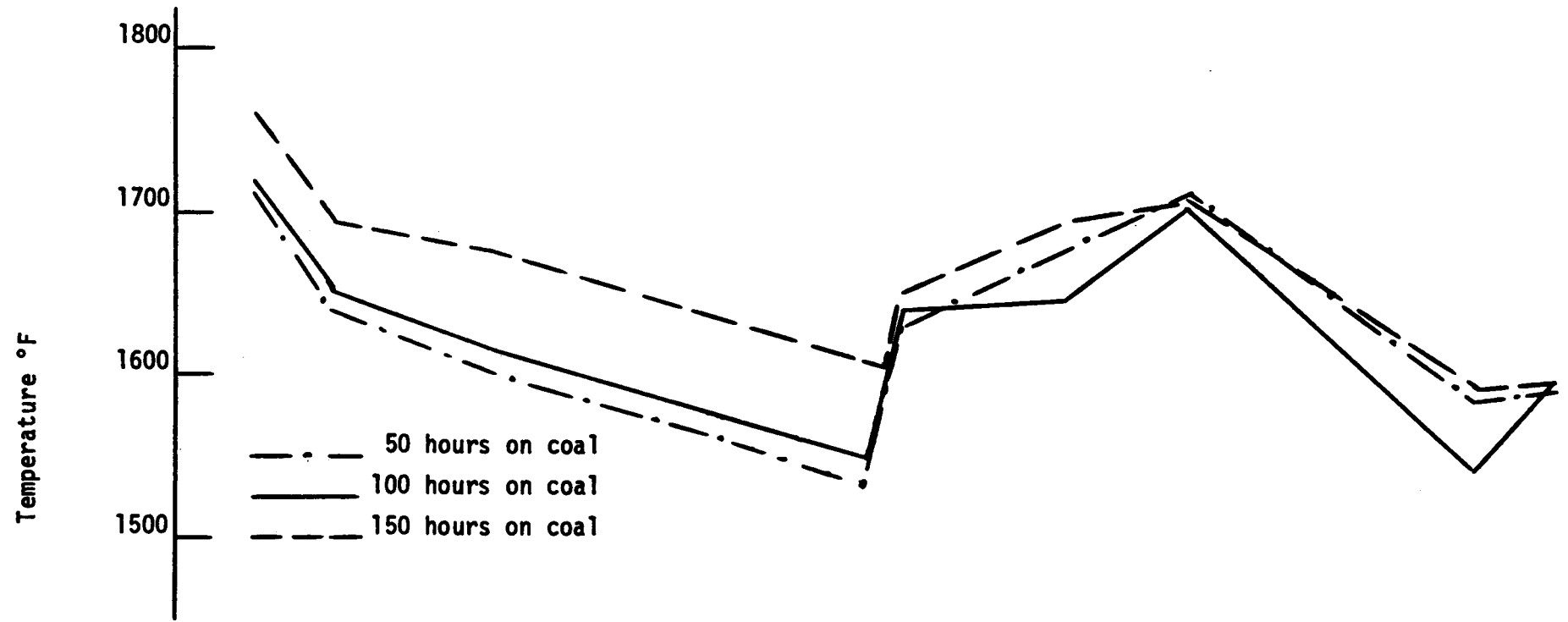
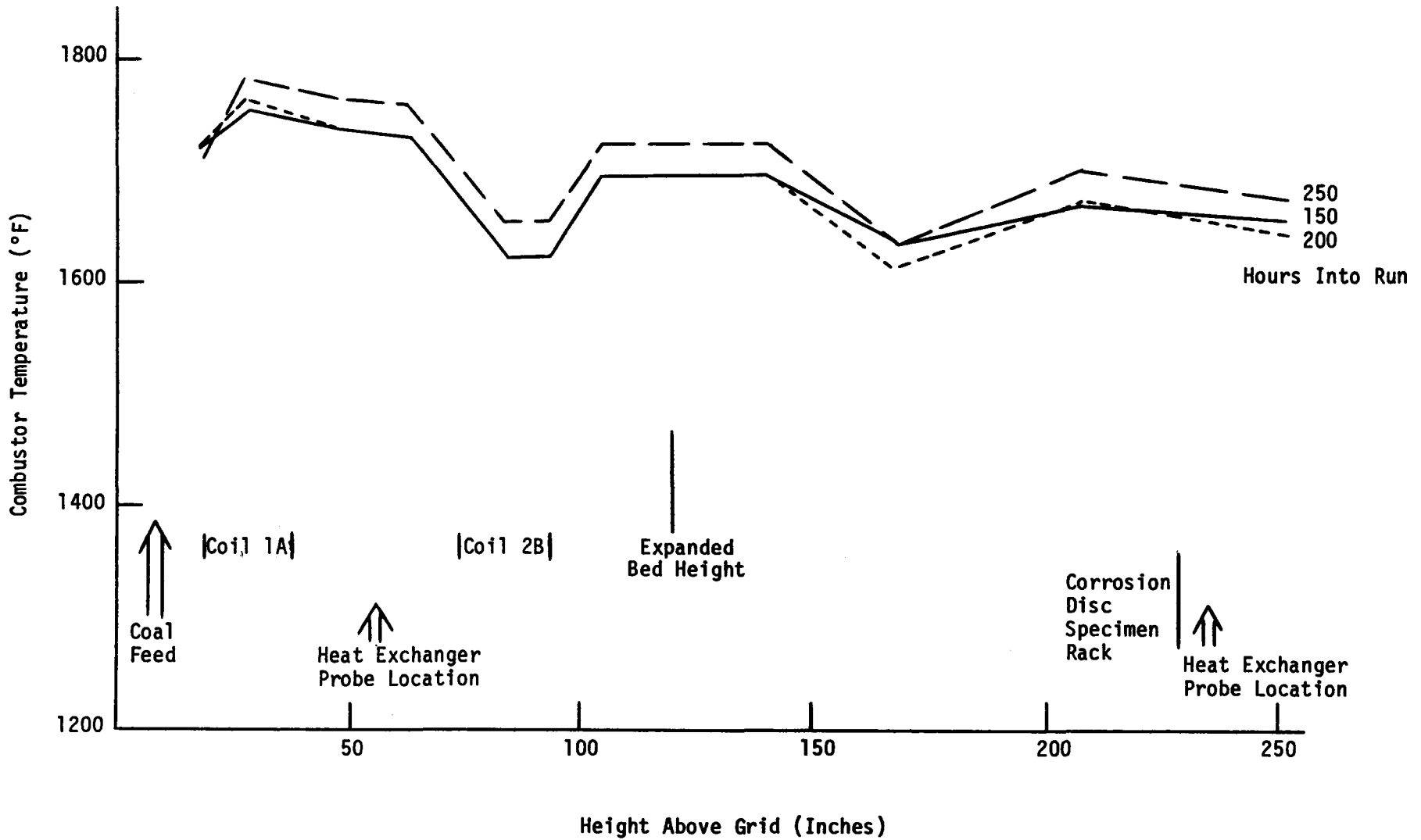


Figure 22

Miniplant Run 78: Combustor Temperature Profile



The change in gas residence time resulted from a drift in bed height during the run. This accounted for many of the perturbations in SO₂ emissions. Operating problems with the flue gas sampling system accounted for the remaining variations. These operating problems were caused by gas dryer leakage and water condensation in the sampling line. When these problems occurred, SO₂ measurements were backed up with wet chemistry analysis which confirmed the steadier SO₂ emission measurements which were obtained during routine periods.

Several analyses of the coal combusted during run 78 showed an average moisture content of 13%. This was the first time that coal with such a high moisture content was fed into the combustor, and surprisingly, did not present any feeding problems. The coal had been screened to remove the -50 mesh fines and this undoubtedly helped avoid feeding problems. Chemical and particle size analyses of the coal and dolomite used in this and all subsequent runs is presented in Tables 12, 13 and 14.

General Electric and Westinghouse inspected their specimens after this run. As per the test plan, several turbine blade specimens and several boiler tube specimens were replaced at the conclusion of this run. All of the specimens removed appeared to be in good condition. No visible signs of corrosion or erosion were present.

Run 79 was the second segment of the materials corrosion test program. It commenced on July 31, 1978 and was terminated after 100 hours of operation because of a plug in the solids discharge line from the first (recycle) cyclone. The system was shut down in anticipation of an increased grain loading resulting from the plug which disabled the first cyclone. General Electric and Westinghouse did not inspect the specimens following this run.

Run conditions were well controlled during the test. Mass flow rate and temperature in the turbine test section were reasonably steady. Temperature at the turbine test section was maintained at approximately 1600°F throughout the run while the turbine flow rate averaged 685 SCFM. The combustor was operated at an average temperature of 1715°F throughout the 5 day period, and at a constant 9 atm pressure. Flue gas temperature profiles during this miniplant run are shown in Figure 23.

Illinois No. 6 coal and Pfizer No. 1337 dolomite were used in this run at a nominal calcium to sulfur molar feed ratio of 1.45; SO₂ retention levels averaged about 90%. Chemical analysis of the coal and dolomite used in this run is presented in Table 12.

The third segment of the test program, Miniplant run 80, was voluntarily terminated after 215 hours of successful operation. This brought the total exposure time for the gas turbine specimens to 565 hours. Superficial inspection of the turbine blade specimens again showed no signs of erosion or corrosion. All the heat exchanger probes looked satisfactory except for one in port no. 6 which showed signs of considerable wastage.

Table 12

Coal and Sorbent Analyses

Condition →	Illinois Coal No. 6 Analysis					
	78.1		78.2-78.10		79	
	As Received	Dry	As Received	Dry	As Received	Dry
Basis →						
Volatile Matter, %	39.95	41.25	37.57	43.04	37.71	43.10
Fixed Carbon, %	45.32	46.80	40.74	46.73	41.81	47.78
Moisture, %	3.16	--	12.82	--	12.5	--
Ash, %	11.57	11.95	8.88	10.19	7.98	9.12
Total Carbon, %	65.58	67.65	57.76	65.16	60.63	68.21
Hydrogen, %	5.63	5.81	5.02	5.66	5.48	6.17
Sulfur, %	4.17	4.31	3.52	4.04	3.33	3.81
Nitrogen, %	2.41	2.49	2.26	2.55	1.17	1.32
Oxygen, %	7.55	7.79	11.00	12.41	10.11	11.37
Heating Value, BTU/lb.	12,042	12,435	10,988	12,604	11,043	12,620

Table 12 (Cont'd)

Coal and Sorbent Analyses

Condition →	Illinois Coal No. 6 Analysis					
	80.1-80.2		81		106	
	As Received	Dry	As Received	Dry	As Received	Dry
Volatile Matter, %	38.72	42.44	36.98	42.46	37.10	41.85
Fixed Carbon, %	39.88	48.20	42.0	48.22	43.65	49.25
Moisture, %	12.86	--	12.9	--	11.36	--
Ash, %	8.54	9.36	8.12	9.33	7.89	8.90
Total Carbon, %	67.67	58.97	58.81	67.52	67.39	75.04
Hydrogen, %	5.81	5.06	4.78	5.49	5.10	5.68
Sulfur, %	3.53	3.87	3.37	3.87	3.52	3.97
Nitrogen, %	1.29	1.12	1.09	1.25	1.33	1.48
Oxygen, %	11.99	10.45	10.94	12.56	4.43	4.93
Heating Value, BTU/lb.	11,528	12,631	10,892	12,505	11,969	12,374

Table 13
Coal Particle Size Distribution

U.S. Sieve #	50	40	30	25	20	8
	% Finer Than					
Run 78.1	0.5	2.7	18.2	27.7	40.5	99.7
Run 106	0.5	2.8	10.1	13.5	20.5	99.7

Table 14

Pfizer 1337 Dolomite Calcined Analysis Run 79

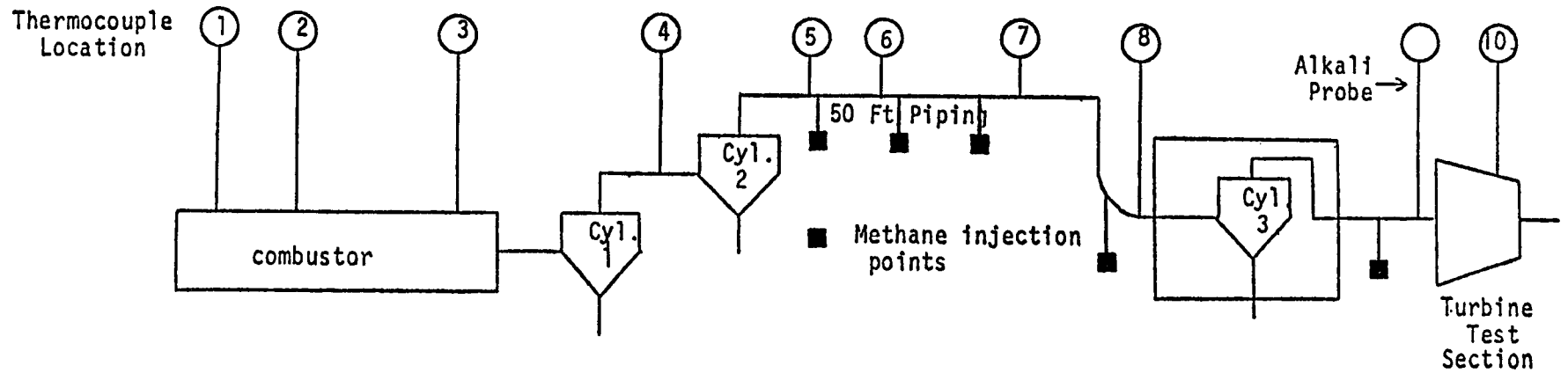
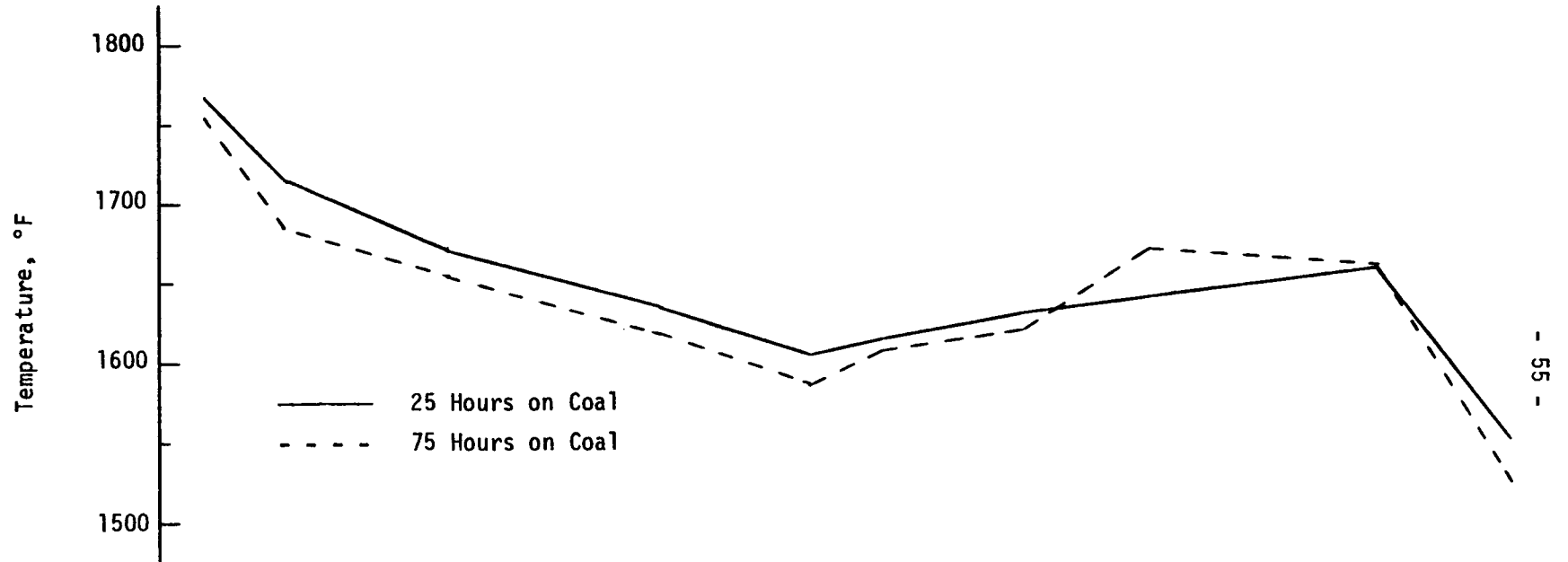
<u>Run</u>	<u>CaO</u>	<u>MgO</u>	<u>Cl</u>	<u>Na</u>	<u>Weight % K</u>	<u>Fe₂O₃</u>	<u>SiO₂</u>	<u>Al₂O₃</u>	<u>S</u>
78.1-78.3	56.60	42.69	0.25	1800 ppm	190 ppm	1.75	0.86	2.58	0.63
78.4-79	55.31	44.10	0.09	325 ppm	439 ppm	0.23	0.82	0.32	0.17
80-81	61.33	37.96	0.09	1030 ppm	<400 ppm	0.27	0.36	0.21	0.12
106	55.78	37.04	0.09	300 ppm	100 ppm	0.23	0.59	0.45	0.003

Particle Size Distribution

<u>U.S. Sieve #</u>	<u>25</u>	<u>20</u>	<u>18</u>	<u>16</u>	<u>12</u>	<u>8</u>
	<u>% Finer Than</u>					
Run 78.4	0.5	0.7	1.5	21.5	38.2	92.2

Figure 23

Run 79: Flue Gas Temperature History



Temperatures at the turbine test section inlet ranged from 1570°F to 1620°F throughout the run. Flue gas temperature profiles for the mini-plant are shown in Figure 24. The run had to be interrupted for 2 hours at the 82 hour mark to replace a leaking lock hopper valve. After the interruption, the turbine flow rate dropped by 12% from the previous level of 690 SCFM to 620 SCFM.

Examination of the flue gas piping following the run revealed a large accumulation of particulates at the entrance to the turbine test section, apparently caused by the formation of condensate during the shutdown and subsequent startup.

The fourth segment of the PFBC hot corrosion/erosion testing program terminated after 170 hours of successful operation. This run (#81) brought the total hours of miniplant exposure testing to 735 hours, exclusive of the shakedown runs. Run conditions were well controlled during the test with mass flow rate and temperature in the turbine test section reasonably steady. Temperature at the turbine test section (Figure 25) was maintained at approximately 1560°F throughout the run while the turbine flow averaged 700 SCFM. The turbine test inlet temperature was slightly lower than during prior tests. This is due mainly to the greater heat loss experienced in the cold weather (October). A longer time period was required to reach thermal equilibrium, however the gas was at or near 1550°F for most (60+%) of the run.

The final segment of the exposure tests (run 106) was completed on June 10, 1979. Run #106 started under operating conditions similar to those employed in the previous test (run #81). Combustor temperatures were approximately 1715°F and very uniform and the pressure was 9 atmospheres. What differed was that the elutriation rates and cyclone collections, both second and third, were unusually high at the start of the run. That may have been due to the old bed material used at the start of the run, which was more friable than new material. The particulate loadings at the turbine test section were slightly higher than usual 0.03 to 0.08 gr/SCF, compared to the 0.025 to 0.035 values obtained in recent runs. After 41 hours of operation, the grain loading from the third stage cyclone increased to approximately 0.46 gr/SCF. Because of this, the run was terminated after 48 hours and the cyclones and turbine blades were examined. Based on cyclone lock hopper collections and particulate measurements, it was concluded that the turbine blade specimens were exposed to these high particulate concentrations for not longer than 7 hours, and most probably 5 to 6 hours. Inspection of the third stage cyclone found that it was almost fully blocked - both in the barrel and in the inlet transition piece - by caked, easily removed, flyash fines.

During the shutdown, the turbine test section was dismantled and inspected and two blades removed and replaced. The test section was reassembled. The run resumed and progressed smoothly until a voluntary

Figure 24

Run 80: Flue Gas Temperature History

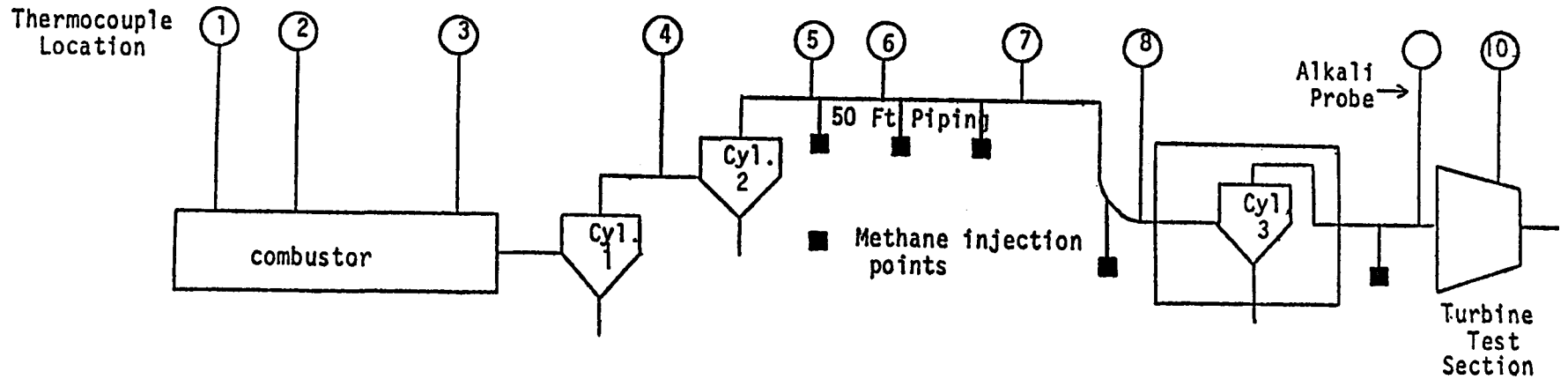
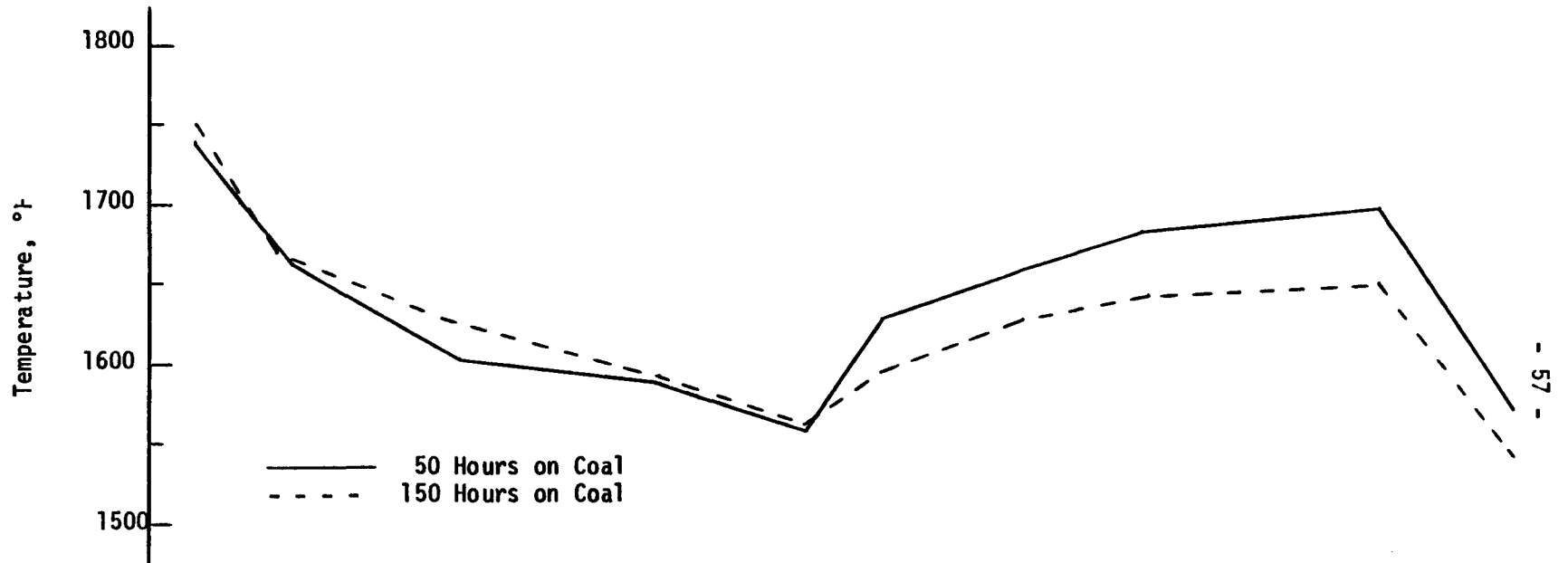
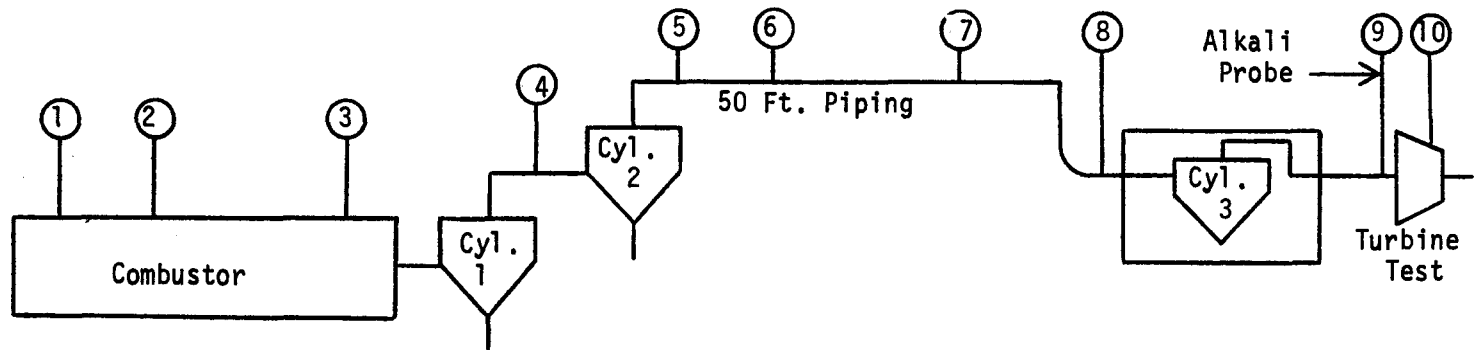
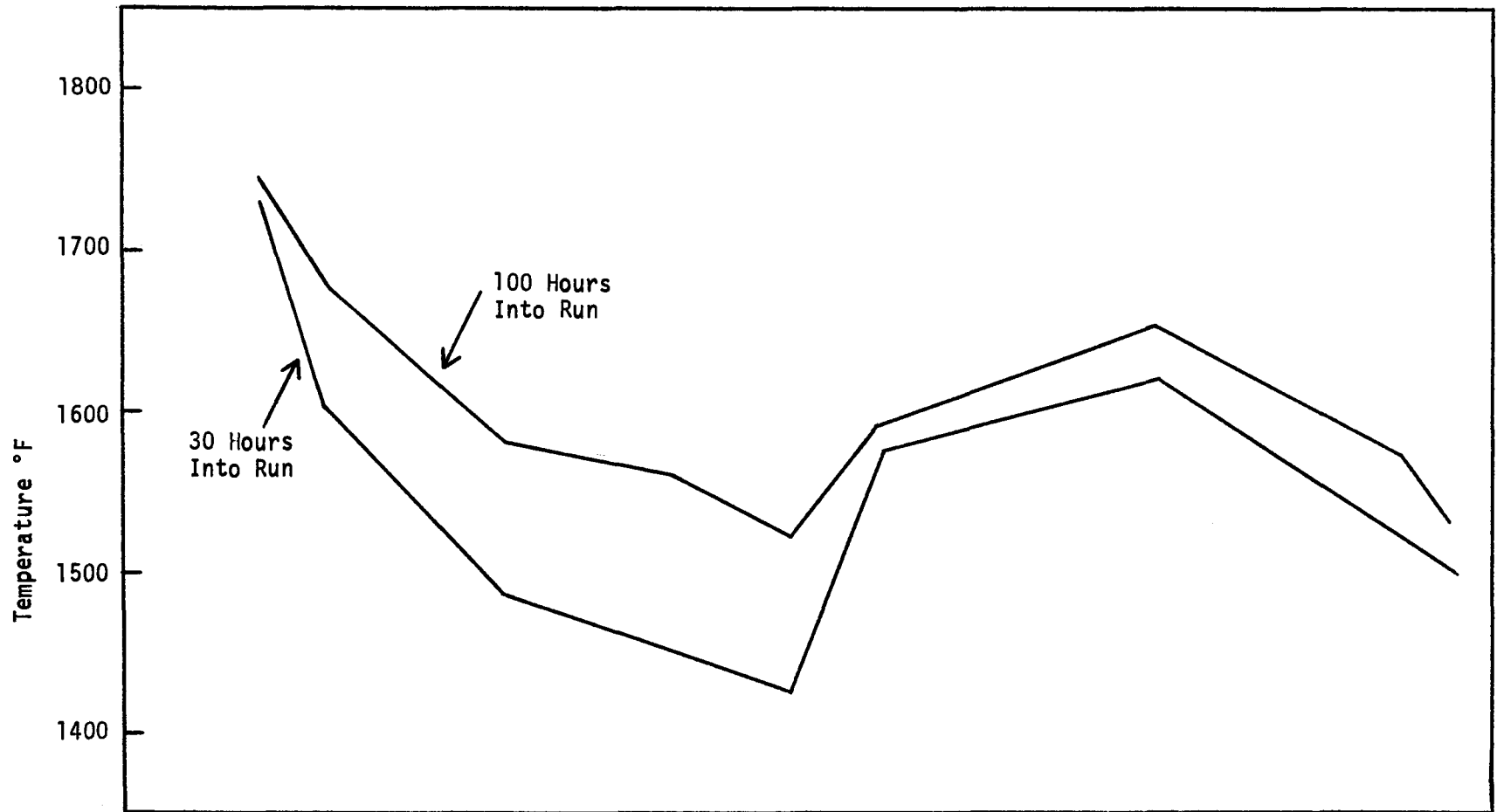


Figure 25

Run 81 Flue Gas Temperature History



shutdown after a total of 265 hours. Turbine flow remained the same throughout the run at ~630 SCFM. The temperature of the flue gas at various points also did not change (Figure 26).

One unusual aspect of this run was the much higher than expected SO₂ retention. The low SO₂ emissions (high retention) during the first segment of the run can be explained in part by the high elutriation rate. This would increase the gas residence time as well as the sorbent utilization. During the initial segment of the run the Ca/S was reduced from 1.45 to 1.25 to increase the SO₂ emissions. The feed was not changed during the shutdown. After the restart, when elutriation rates were normal, SO₂ emissions were still much lower than expected. The sulfur retention remained at or above 97% for the entire run. The reason for this is not known.

FLUE GAS EMISSIONS

The flue gas from the Miniplant is continuously analyzed for O₂, NO_x, CO, CO₂ and SO₂ with standard IR and UV gas analyzers. During long operations of the Miniplant, the analyzers are calibrated at least once per day. During the 1000 hour exposure tests, the on-line analyzers were also randomly compared to other analyzers normally used in the bench unit, as well as with gas chromatography or wet chemistry samples. The results of these various methods are shown in Table 15.

During the corrosion testing flue gas emissions were continuously monitored and averaged over periods reported in the prior section. In general the SO₂ emission of 260 ppm represented a very high reduction level comparable to the 90% reduction standard proposed by the EPA. During the last 265 hours of exposure retention levels were 98% (90 ppm SO₂ emission). The reason for this high retention is still unclear. The NO_x emission throughout the 1000 hours was 35-50 ppm. Mostly the flue gas consisted of 14% CO₂, and 5% O₂ throughout the series of tests.

Some components of the flue gas are only sampled in a batch wise manner. These include flue gas alkali as well as particulates. The alkali measurement train described in an earlier section has been used to take several samples just upstream of the turbine test section. The breakdown of where in the train the various amounts of alkali were detected is shown in Table 16. The test temperatures are shown in Figure 14.

The four good samples for Na, K, and Cl emissions were fairly consistent. During runs 78, 79 and 80, 1.8 to 3.2 ppmw Na, 0.3 to 0.5 ppmw K and 47 to 54 ppmw Cl were found in the flue gas. Most of the Na and K collected in the alkali probe train was found in particulates collected at low temperature (230°C) on the Balston filter. More K did condense on the front screen during runs 78 and 80 than during run 79. No difference was observed for the Na vapor. The Cl collected in the train was found only in the knock out condensate.

Figure 26

Run 106 Flue Gas Temperature History

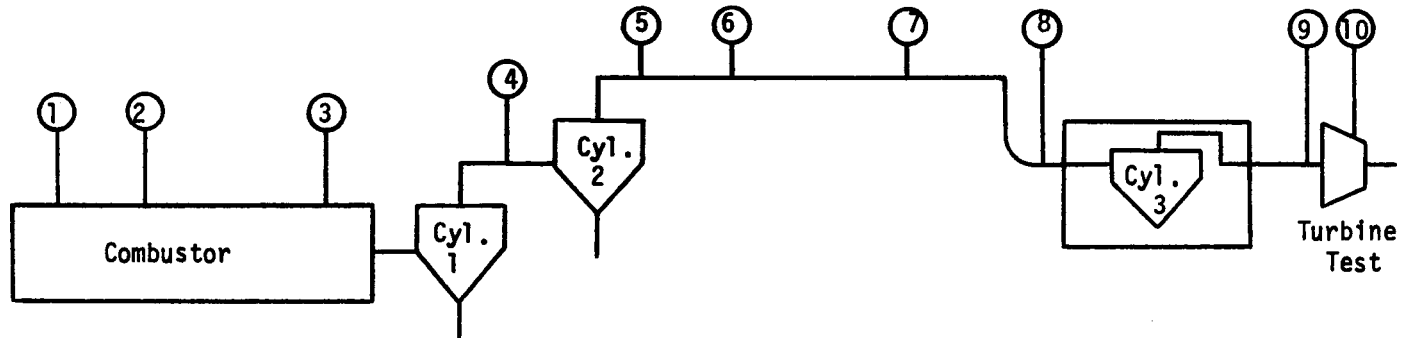
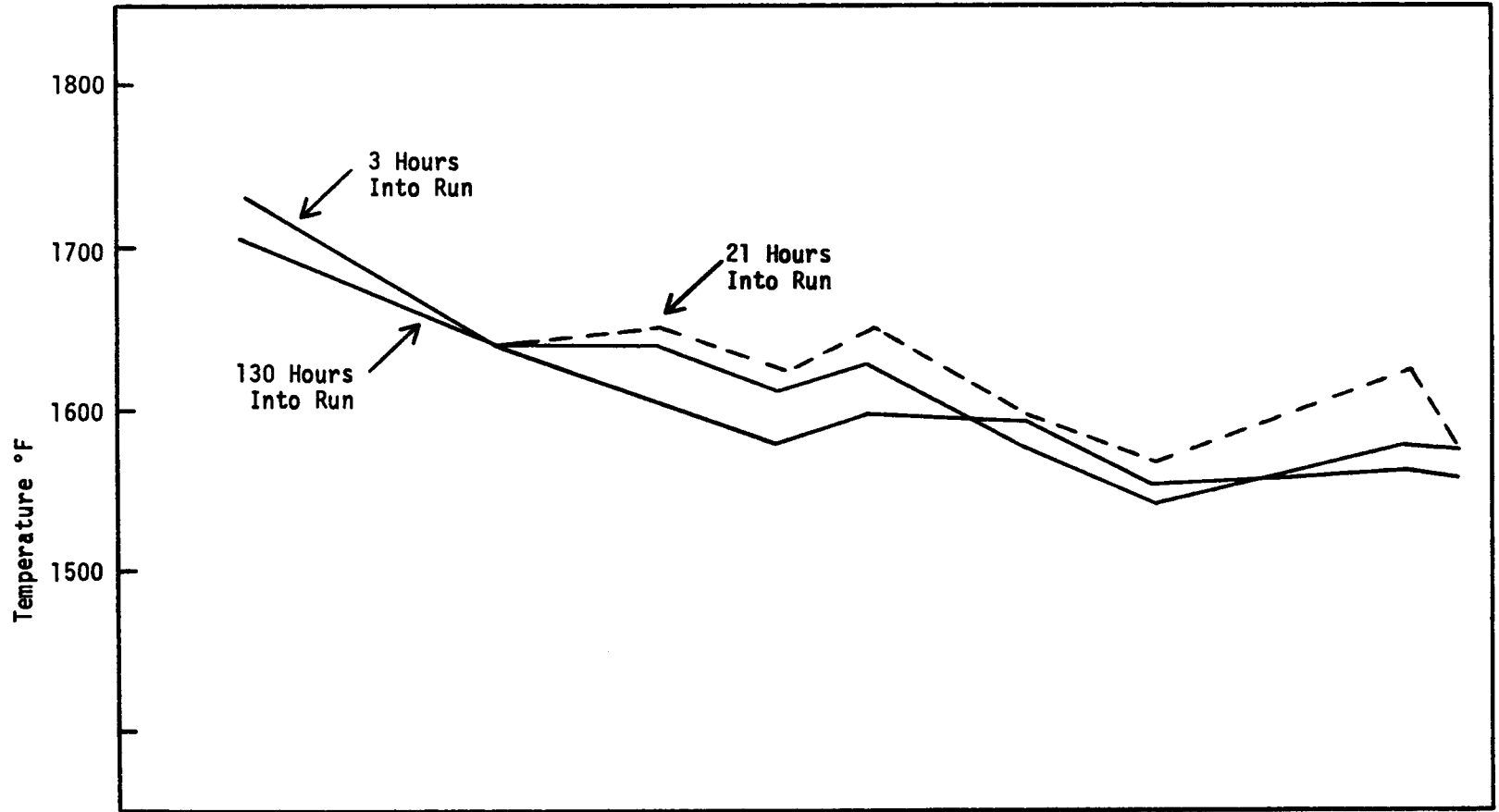


Table 15

Flue Gas Emissions During Run 81

<u>Date</u> <u>(1978)</u>	<u>Time</u>	<u>Analysis</u>	<u>NO</u> <u>ppm</u>	<u>CO₂</u> <u>%</u>	<u>CO</u> <u>ppm</u>	<u>O₂</u> <u>Teledyne</u> <u>%</u>	<u>O₂</u> <u>Beckman</u> <u>%</u>	<u>SO₂</u> <u>ppm</u>	<u>SO₃</u> <u>ppm</u>
10-09	11:20-12:00	Miniplant	115	10	---	---	9	50-600+	---
		Bench Unit	120	13	525	6.5	---	80-400	---
10-09	13:00-13:30	Miniplant	---	11	---	---	7.7	240	---
		Bench Unit	140	13	30	5.2	---	240	---
10-12	09:20-10:20	Miniplant	---	--	---	---	---	322	---
		Wet Chem.(a)	---	--	---	---	---	324	7
10-12	11:30-12:00	Miniplant	120	13.5	---	5	5	270	---
		Bench Unit	138	13	30	5	---	280	---

Gas Chromatographic Analyses of Flue Gas During Run 78.3

<u>Date</u> <u>(1978)</u>	<u>S Analyses of Dry Flue Gas</u>				<u>Hydrocarbon Analyses of</u> <u>Wet Flue Gas</u>		
	<u>SO₂</u> <u>ppm</u>	<u>H₂S</u> <u>ppm</u>	<u>COS</u> <u>ppm</u>	<u>CS₂</u> <u>ppm</u>	<u>CH₄</u> <u>ppm</u>	<u>C₂H₆</u> <u>ppm</u>	<u>C₃ to C₆</u> <u>ppm</u>
06-22	117	1	N.D.	N.D.	18	14	N.D.

 (a) Controlled condensation method for SO₃; EPA method 8 for SO₂.

N.D. = Not Detected

Table 16

Na and K Emissions in Flue Gas
Alkali Probe Test - Runs 79 and 80

<u>Alkali Train Location</u>	<u>Run 78</u>		<u>Run 79.1</u>		<u>Run 79.2</u>		<u>Run 80</u>	
	<u>Wt. % K Collected</u>	<u>Wt. % Na Collected</u>	<u>Wt. % K Collected</u>	<u>Wt. % Na Collected</u>	<u>Wt. % K Collected</u>	<u>Wt. % Na Collected</u>	<u>Wt. % K Collected</u>	<u>Wt. % Na Collected</u>
Front Filter (Including Particulates)	36.8	6.8	5	1	6	1	13	1
Quartz Tube	3.2	0.7	14	2	8	2	30	2
Balston Filter Particulates	59.0	88.6	80	96	83	95	52	94
Knock Out Solution	1.0	3.9	1	1	3	2	5	3
ppmw in Flue Gas	0.54	2.06	0.28	1.84	0.38	3.23	0.32	2.88

PARTICULATE LOADING

Particulate loadings were carefully monitored throughout the 1000 hours of testing. Samples were taken with both particulate sampling systems described in an earlier section. A listing of all samples as well as all particle size distributions is in Appendix B. A summary of the particulate loadings is shown in Figure 27. Another summary of the size distribution limit (90% vol. finer than) is shown in Figure 28. Summaries of particulate in 5 principal size ranges at the outlet of the recycle cyclone and the two cleanup cyclones are shown in Tables 17, 18 and 19. The gas which exits the third cyclone is expanded through the turbine test section.

Particulate loadings for run 78 ranged from 0.014 to 0.056 gr/SCF (32 to 128 mg/m³). Samples were taken both at high pressure upstream of the turbine test section and at low pressure downstream of the turbine test section. The samples from both locations were fairly well in agreement. The volume mean size of particulates captured by both sampling systems was 2 μ .

A routine cleaning and inspection of the third cyclone following run 78 revealed a thermal stress failure (hole) in the dipleg just before it exits the granular bed filter vessel. This failure was due to thermal stresses of expansion and contraction during the intermittent operations of the miniplant. The dipleg was repaired and a section of flexible tube was inserted in the system to allow for thermal expansion. The hole in the dipleg was small, but it may have allowed a very small stream of particulate rich gas to mix with the clean gas and thereby increased the loadings.

During run 79 only three particulate samples were taken. The loadings were unusually low, possibly due to the thorough cleaning and repair that the tertiary cyclone underwent just prior to the run. The average particle loading was 0.012 gr/SCF. This is the lowest sustained particulate loading average ever achieved in the miniplant. Near the end of the run particulate loadings increased. This was due to the plugging of the primary (recycle) cyclone. The run was terminated a few hours ahead of schedule to prevent possible damage to the turbine test section.

During run 80 particulate measurements were again taken with Balston total filters at the 2 sampling locations -- upstream and downstream of the GE turbine test section. Particulate loadings were consistently between 0.014 and 0.028 gr/SCF (33 and 55 mg/Nm³) throughout the run. The material captured after the turbine had an average particle size of 0.92 μ m whereas that captured before the turbine had an average size of 1.1 μ m. The particulates collected during run 80 were generally finer than those collected during prior runs at similar conditions with the Illinois No. 6 coal. The reason for this discrepancy is not known.

Figure 27

Hot Corrosion Runs Particulate Loading Summary

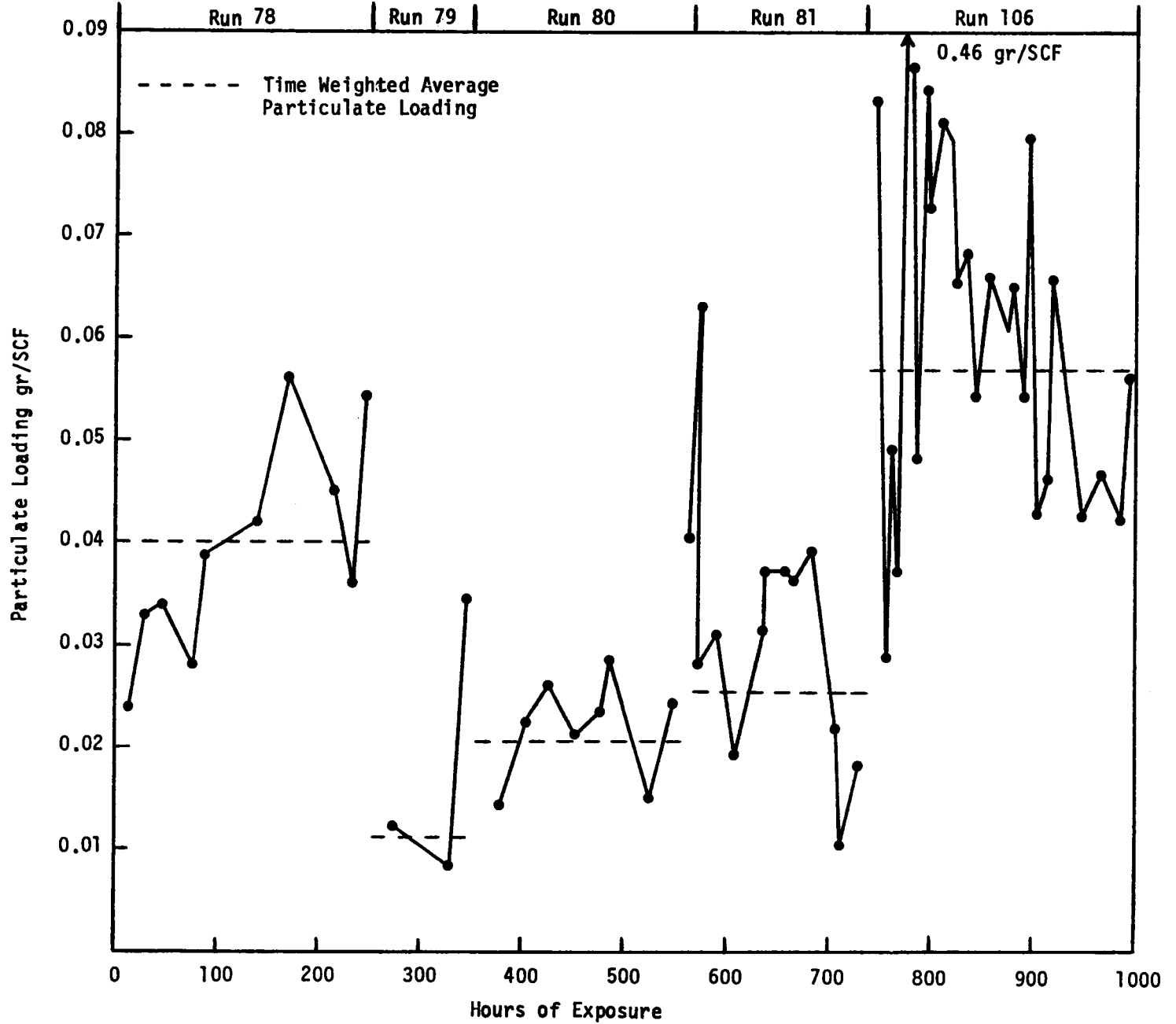


Figure 28
Particulate Size Limit Summary

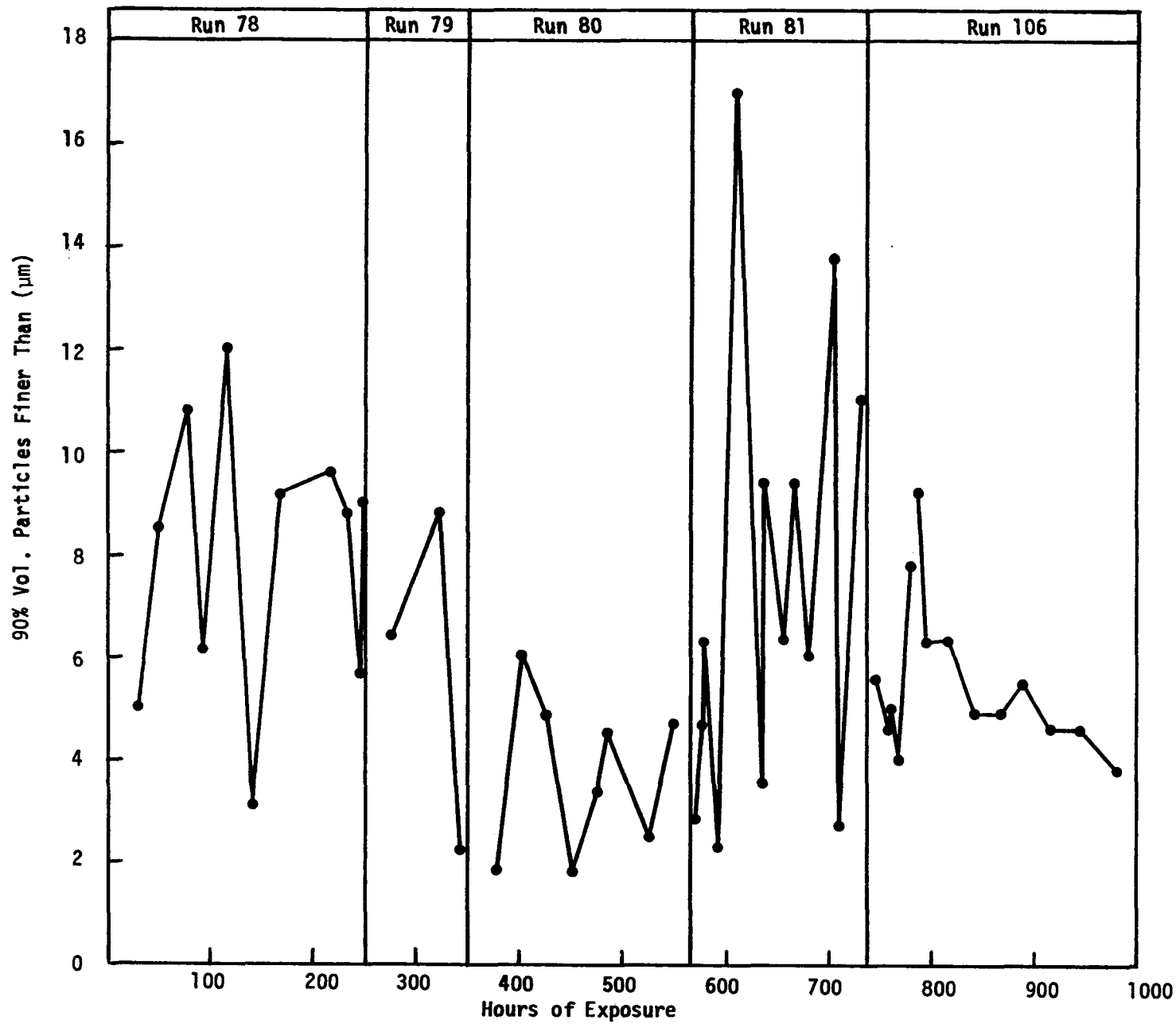


Table 17

First Cyclone Gas Outlet Particulate
Concentration Summary

<u>Run No.</u>	<u>0-5 μm</u>		<u>5-10 μm</u>		<u>10-20 μm</u>		<u>20-40 μm</u>		<u>> 40 μm</u>		<u>Total Loading gr/SCF</u>
	<u>gr/SCF</u>	<u>%</u>	<u>gr/SCF</u>	<u>%</u>	<u>gr/SCF</u>	<u>%</u>	<u>gr/SCF</u>	<u>%</u>	<u>gr/SCF</u>	<u>%</u>	
78.4	0.51	10.0	1.08	21.4	1.62	31.9	0.63	12.5	1.22	24.2	5.06
78.7	0.32	4.9	0.90	13.7	1.83	27.8	0.93	14.1	2.60	39.5	6.58
78.10	0.60	10.4	1.25	21.7	1.89	32.6	0.45	7.9	1.59	27.5	5.79
79	0.31	3.9	0.75	9.5	2.08	26.4	1.37	17.4	3.37	42.9	7.87
80.2	0.25	5.7	0.62	13.7	1.24	27.6	0.73	16.3	1.66	36.8	4.50
81	0.49	8.1	0.71	11.7	1.24	20.5	0.34	5.6	3.28	54.1	6.07
106.1	2.06	17.7	2.65	22.8	3.14	27.0	1.64	14.1	2.13	18.3	11.62
10.63	0.53	8.1	1.01	15.5	1.92	29.5	1.08	16.6	1.96	30.15	6.50

Table 18

Secondary Cyclone Gas Outlet Particulate
Concentration Summary

<u>Run No.</u>	<u>0-5 μm</u>		<u>5-10 μm</u>		<u>10-20 μm</u>		<u>20-40 μm</u>		<u>> 40 μm</u>		<u>Total Loading gr/SCF</u>
	<u>gr/SCF</u>	<u>%</u>	<u>gr/SCF</u>	<u>%</u>	<u>gr/SCF</u>	<u>%</u>	<u>gr/SCF</u>	<u>%</u>	<u>gr/SCF</u>	<u>%</u>	
78.4	0.207	52.9	0.148	37.7	0.037	9.4	0.0	0.0	0.0	0.0	0.392
78.7	0.137	53.3	0.101	39.1	0.020	7.6	0.0	0.0	0.0	0.0	0.258
78.10	0.241	63.0	0.124	32.4	0.017	4.6	0.0	0.0	0.0	0.0	0.382
79	0.170	61.9	0.084	30.7	0.020	7.4	0.0	0.0	0.0	0.0	0.274
80.2	0.125	68.7	0.051	27.9	0.006	3.5	0.0	0.0	0.0	0.0	0.182
81	0.243	69.3	0.074	21.2	0.030	8.6	0.003	0.0	0.0	0.0	0.350
106.1	1.72	49.8	1.11	32.1	0.53	15.4	0.09	2.6	0.0	0.0	3.45
106.3	0.29	46.0	0.22	34.9	0.12	19.0	0.0	0.0	0.0	0.0	0.623

Table 19

Third Cyclone Gas Outlet Particulate
Concentration Summary

<u>Run No.</u>	<u>0-5 μm</u>		<u>5-10 μm</u>		<u>10-20 μm</u>		<u>20-40 μm</u>		<u>> 40 μm</u>		<u>Total Loading gr/SCF</u>
	<u>gr/SCF</u>	<u>%</u>	<u>gr/SCF</u>	<u>%</u>	<u>gr/SCF</u>	<u>%</u>	<u>gr/SCF</u>	<u>%</u>	<u>gr/SCF</u>	<u>%</u>	
78.4	0.033	85.4	0.005	12.5	0.001	2.1	0.0	0.0	0.0	0.0	0.039
78.7	0.040	72.3	0.012	20.7	0.004	7.0	0.0	0.0	0.0	0.0	0.056
78.10	0.047	87.0	0.005	9.8	0.002	3.2	0.0	0.0	0.0	0.0	0.054
79	0.010	84.0	0.002	13.5	0.0	2.5	0.0	0.0	0.0	0.0	0.012
80.2	0.026	92.0	0.002	7.3	0.0	0.7	0.0	0.0	0.0	0.0	0.028
81	0.030	95.9	0.001	3.6	0.0	0.5	0.0	0.0	0.0	0.0	0.031
106.1	0.070	84.1	0.009	10.8	0.005	6.0	0.0	0.0	0.0	0.0	0.083
106.3	0.058	92.1	0.004	6.4	0.001	1.6	0.0	0.0	0.0	0.0	0.063

During run 81 twelve particulate measurements were taken with the Balston total filter sampling systems. The primary "recycle" cyclone dipleg plugged almost at the start of the run. This was the same problem that prematurely shutdown run 79. The run was continued to scheduled shutdown, when particulate measurements showed that the average loading (0.026 gr/SCF) was only slightly higher than during runs 79 and 80 (0.011 and 0.021 gr/SCF respectively). This average loading was significantly lower than during run 78 (0.04 gr/SCF). All of these runs were made under otherwise similar combustor operating conditions.

Particle size distributions obtained from the Balston filter particulates with the Coulter Counter revealed a similar average size (1.36 μm) to runs 78, 79 and 80 (1.9, 1.1 and 1.2 μm respectively). The difference was in the large end of the distribution. 5% of the particles were larger than 12 μm during run 81, whereas 5% were larger than 11, 10, and 5.4 μm respectively for the prior runs in the series. This can be seen in Figure 28 and Appendix B.

An important point to note is that after run 81 the turbine test blades and the miniplant ducting did not exhibit as much particulate deposition as during previous long runs. After runs 78, 79 and 80 the miniplant exhaust ducting had to be cleaned to remove particulate deposition. After run 81, the ducts were clean. This may be attributed to the abrasive action of the larger particles that resulted from the blockage of the primary cyclone dipleg.

At the start of run 106.1 particulate loadings from the combustor were extremely high. This was probably due to the use of an old starting bed. For several hours one order of magnitude higher than normal particulate concentrations into the tertiary cyclone deposited a layer of particulates on the flue gas ducts and the body of the cyclone. Later in the run, when cyclone inlet loadings were nearly normal, some of that coating must have dislodged and plugged the tertiary cyclone. The run was interrupted after 48 hours when tertiary cyclone outlet loadings (0.46 gr/SCF) were similar to the normal inlet loading (0.5-0.8 gr/SCF). This outlet loading during run 106.2 was no more than 7 hours and probably only 5 to 6 hours in duration.

Following the shutdown, the cyclone was inspected and the body, and dipleg were found almost completely plugged with caked -- but not fused -- particulates. Only a small hole was available for the flue gas to pass through the cyclone. This hole almost directly connected the inlet and the outlet of the cyclone. These particulates were easily removed and the system was put back together for a restart. The turbine test section was also disassembled and showed some erosion on many of the leading edges of the blades.

Following cleanout of the miniplant ducting, the run was resumed and designated 106.3. This time particulate loadings, though still higher than during prior tests, were within acceptable ranges. The average particle loadings for runs 106.1, 106.2 and 106.3 were 0.050, 0.46, and 0.068 gr/SCF respectively. The average particle sizes were 1.88, 3.5 and 1.76 μm

respectively. During run 106.1 and 106.3 the particle size distribution was similar to that seen during run 80.

While three stages of cyclones seem to be sufficient to protect the gas turbine from massive erosion, the level of cleanup (0.035 gr/SCF) was not sufficient to meet the new source performance standard for particulates set by the EPA (approximately 0.015 gr/SCF). However, one could surmise that improvements or optimization of cyclone performance could be accomplished to meet both requirements i.e., protection of the gas turbine and environmental regulations. This may afford a major capital cost reduction in the PFBC process.

CYCLONE PERFORMANCE

During this hot gas corrosion/erosion study of turbine blade materials, high cyclone efficiencies allowed the use of two stages of cyclone cleanup before the turbine test section. Particulate loadings as low as 0.01 gr/SCF were achieved, which infers both cyclones operated at efficiencies in excess of 90%. These high efficiencies are not readily predicted and warrant further study.

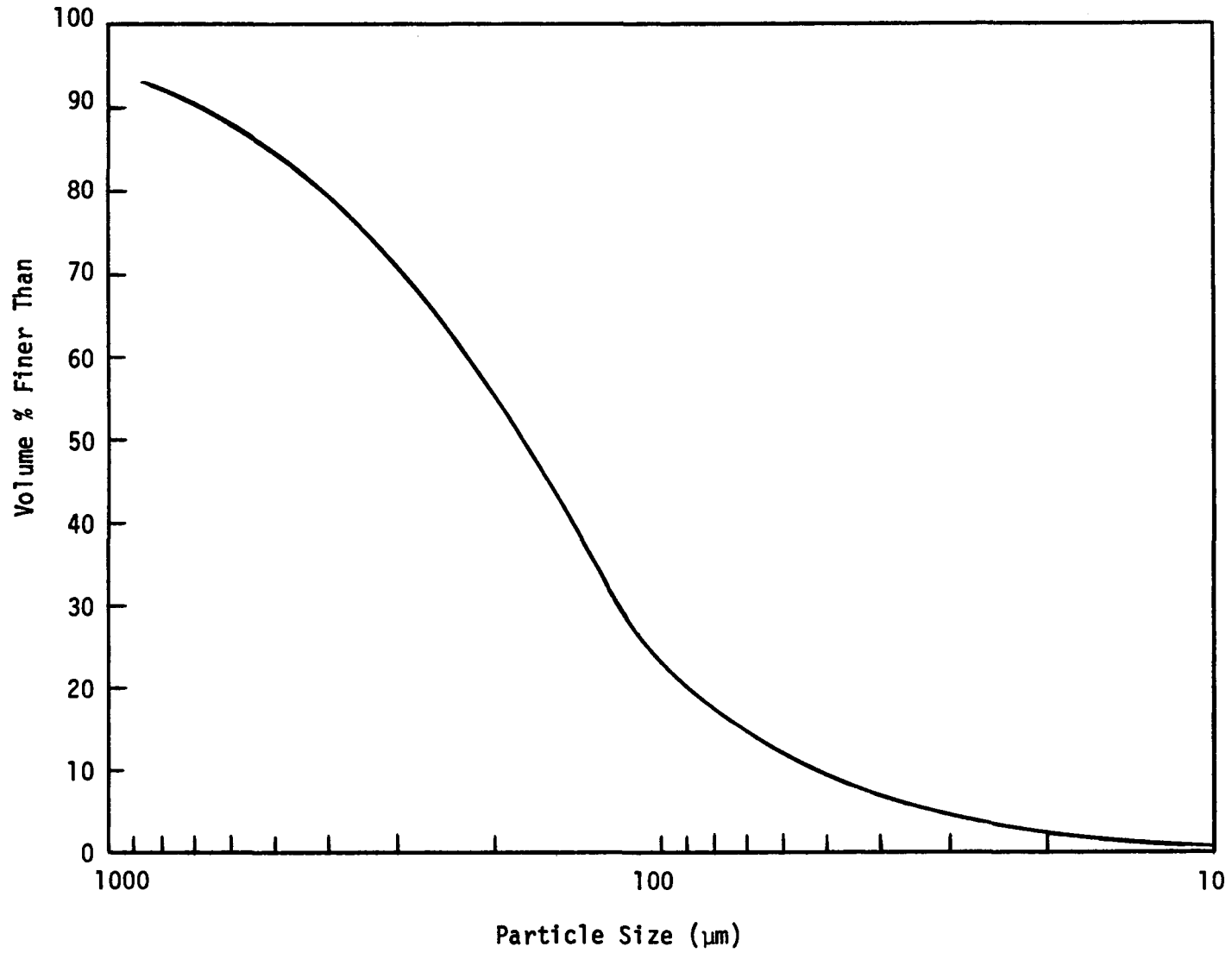
The efficiency of the primary "recycle" cyclone is intentionally low by design, so that larger particles can be recirculated to the fluidized bed combustor. There is no convenient way of measuring particulates in the gas entering or exiting the cyclone due to its location with respect to the combustor. During run 81, when the dipleg plugged, some of the material removed from the dipleg was subjected to particle size analysis. This is not representative of true recycle operation. A graph of the size distribution is shown in Figure 29.

The second cyclone in the series of three, captures material which is then collected in a lock hopper. This, plus knowledge of the outlet particulate concentration makes possible efficiency calculations based on a mass balance. Typically the cyclone is 90 to 95% efficient. This is with inlet loadings of 5 to 8 gr/SCF with an average particle diameter of 17 to 22 μ .

The third cyclone in the train receives an inlet loading of 0.5 to 0.7 gr/SCF with an average size of 3 to 4 μ m. This cyclone is located in a large pressure vessel. The dimensions of this cyclone are shown in Figure 8. The cyclone normally operates at 880°C, 900 kPa pressure and inlet velocities of 50 m/s. Flue gas can be sampled for particulates both before and after the cyclone. During runs 78 through 81, isokinetic samples were taken with Balston total filters only on particulates in the gas exiting the cyclone. This sample gas was withdrawn through an isokinetic stationary probe. After the one to two hour sample was taken, the filter cartridge was weighed and particulates were removed from the filter cake for Coulter Counter size analysis.

Figure 29

**Primary Cyclone Return Line
Particle Size Distribution (Run 81)**



The size distribution of the material captured by the cyclone was analyzed with a combination of a sonic sieve and the Coulter Counter. A mass balance was completed around the cyclone to determine inlet size and concentration. In this way cyclone fractional (grade) efficiencies were obtained under the assumption that there was no accumulation or attrition in the cyclone. The validity of these calculations has been confirmed with concurrent inlet and outlet samples and mass balance calculations. Independent studies by other contractors have also confirmed the high cyclone efficiencies (4). A graph of the tertiary cyclone grade efficiency during run 79 and 80 is shown in Figure 30. The grade efficiency for all runs in this series is shown in Table 20.

The cyclone collection efficiency data confirm the ability of the miniplant cyclone train to very effectively capture particles greater than 10 microns. Particles in the 5-10 micron range are captured with a 95-99% efficiency, and particles in the 2-5 micron range with a 75 to 95% efficiency. This intimates that if a fourth cyclone were to be added, practically all particles larger than 10 microns could be captured and a substantial portion of the 5-10 μ m population would also be removed. Since particles greater than 10 microns are prime suspects in causing turbine blade erosion, a four cyclone train could cleanup the flue gas to a suitable level for gas turbines.

HEAT EXCHANGER PROBES

Probes consisting of the alloy combinations listed in Table 1 were positioned in the combustor ports and exposed at the intended set point temperatures. A maximum of 21 probes were inserted in the combustor at a given time during the test program. At each temperature level, two probes were exposed for the entire 1000 hour test plus 117 shakedown hours. Thus, a total of 14 probes containing 28 specimens resided within the combustor for the duration of the test. Five of the seven probes which were inserted at the start of the test were exposed for 367 hours and then replaced with 7 new probes which remained in the combustor for 485 hours. The remaining probes were exposed for periods from 100 to 423 hours. A tabulation of the heat exchanger probe details and exposure times appears in Table 21. A probe test history is presented graphically in Figure 31.

Temperature data for the 31 different heat exchanger probes exposed during the PFBC hot corrosion/erosion program are presented in Appendix C Tables C-1 through C-5. Temperatures at two locations in each probe were recorded every 20 minutes during the run. In these tables the recorded temperatures have been averaged for five (5) hour segments of the run. Also listed are the standard deviations for that time period as well as the maximum and minimum temperatures experienced by the specimen material during those five (5) hours.

Figure 30

**Particle Capture Efficiency of
the Tertiary Miniplant Cyclone**

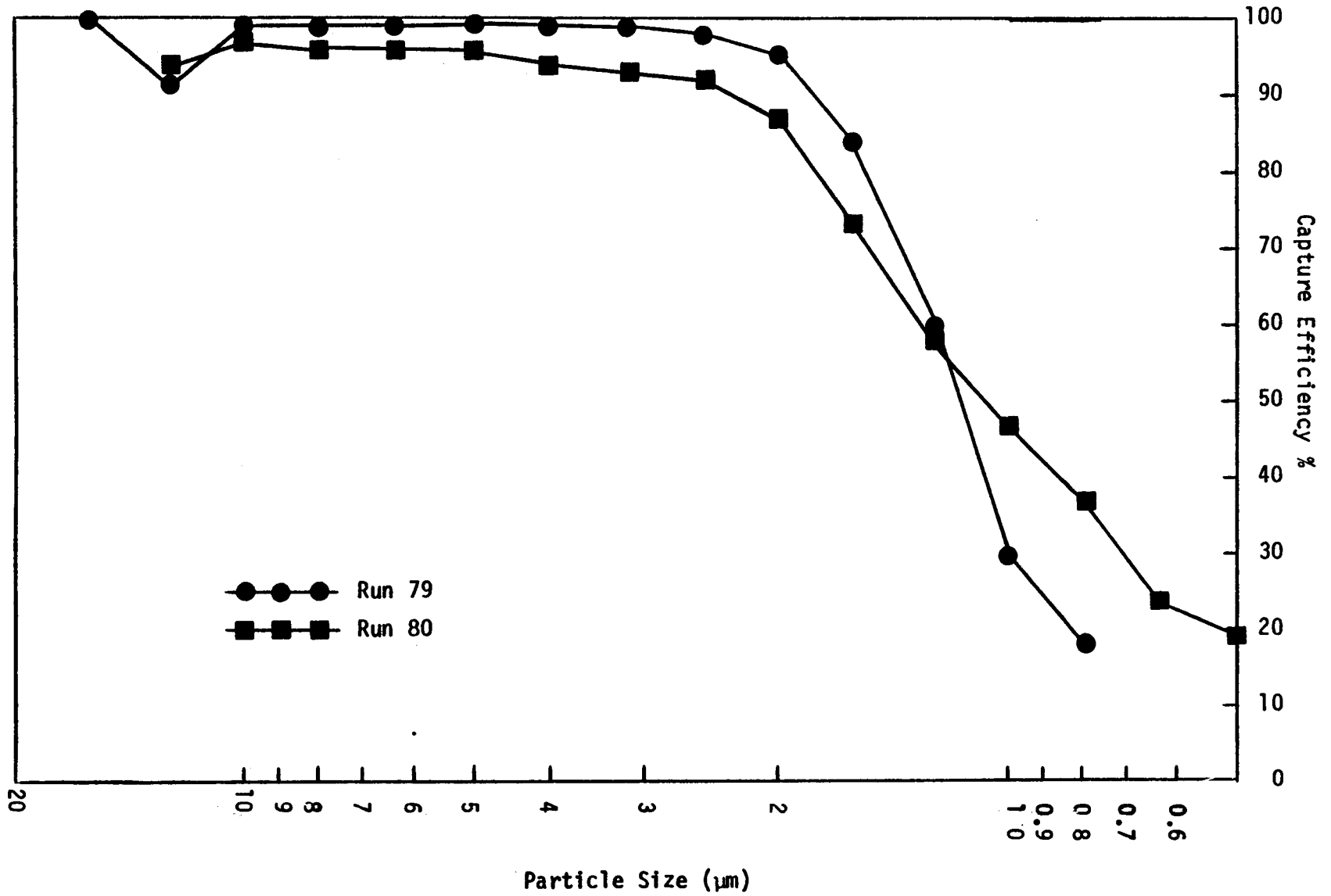


Table 20

Third Cyclone Grade Efficiency Summary

Run	Stated Particle Size (Microns) Collected with Efficiency (%)																
	0.5	0.63	0.794	1.0	1.26	1.59	2.0	2.52	3.17	4.0	5.04	6.35	8.00	10.08	12.7	16.0	20.2
78.2	40	39	45	61	78	87	94	95	95	95	95	95	95	95 ⁺	99 ⁺	99 ⁺	99 ⁺
78.4	5	10	22	41	69	86	93	95	96	97	96	97	96	96	99 ⁺	99 ⁺	99 ⁺
78.10	37	30	53	58	78	86	90	93	94	94	94	94 ⁺	94 ⁺	94 ⁺	99 ⁺	99 ⁺	99 ⁺
79	0	0	32	48	81	94	98	99	99	99	99 ⁺	99 ⁺	99 ⁺	99 ⁺	99 ⁺	99 ⁺	99 ⁺
79	0	0	5	13	39	74	93	97	99	99	99 ⁺	99 ⁺	99 ⁺	99 ⁺	99 ⁺	99 ⁺	99 ⁺
80.2	20	24	37	47	58	74	87	92	93	94	96	96	97	99 ⁺	99 ⁺	99 ⁺	99 ⁺
81 *	0	0	14.1	79.9	83	90	94	97	98	98	99	99	99	99 ⁺	99 ⁺	99 ⁺	99 ⁺
106.1	--	--	--	--	94	93	94	96	98	98	98	99	99	99 ⁺	99 ⁺	99 ⁺	99 ⁺
106.3	--	--	--	--	66	63	66	74	78	85	91	95	96	97	97	99 ⁺	99 ⁺
106.3	--	--	--	--	42	55	77	91	94	96	96	97	96	98	99 ⁺	99 ⁺	99 ⁺

 * Primary cyclone disabled.

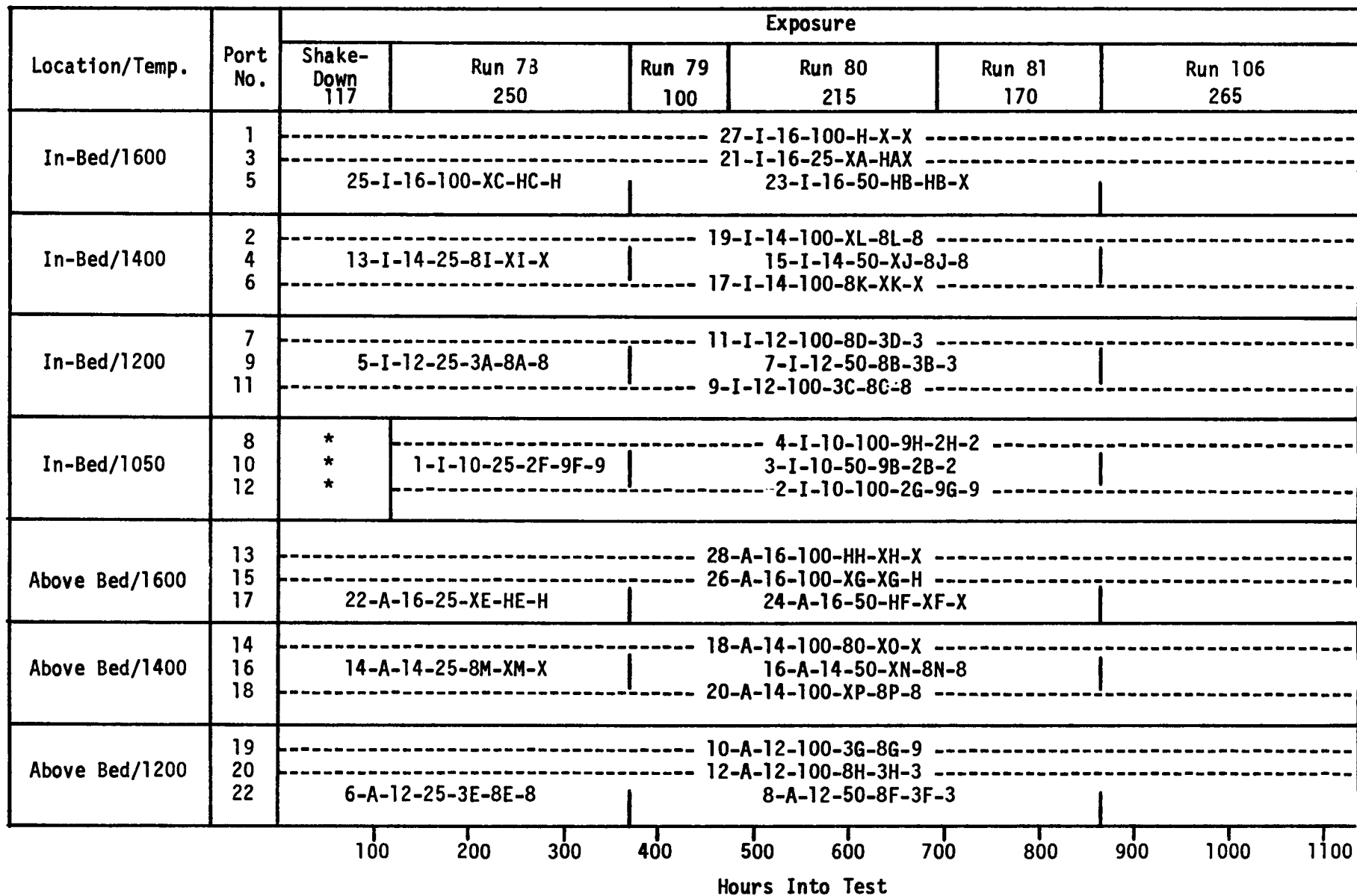
Table 21

Heat Exchanger Specimen Probe Summary

<u>Port No.</u>	<u>Probe No.</u>	<u>Set Point Temp (°F)</u>	<u>Alloy Position</u>		<u>Run Exposed</u>	<u>Total Hours</u>
			<u>Near Wall</u>	<u>Inner Bed</u>		
<u>In-Bed Specimens</u>						
1	27	1600	Haynes 188	Hastelloy X	66,67,78,79,80,81,106	1117
2	19	1400	Hastelloy X	Inconel 800	66,67,78,79,80,81,106	1117
3	21	1600	Hastelloy X	Haynes 188	66,67,78,79,80,81,106	1117
4	13	1400	Inconel 800	Hastelloy X	66,67,78	367
4	15	1400	Hastelloy X	Inconel 800	79,80,81	485
5	25	1600	Hastelloy X	Haynes 188	66,67,78,*	423
5	23	1600	Haynes 188	Hastelloy X	79,80,81	485
6	17	1400	Inconel 800	Hastelloy X	66,67,78,79,80,81,106	1117
7	11	1200	Inconel 800	SS 304	66,67,78,79,80,81,106	1117
8	4D	1050	9 Cr - 1 Mo	2-1/4 Cr - 1 Mo	66,67	117
8	4H	1050	9 Cr - 1 Mo	2-1/4 Cr - 1 Mo	78,79,80,81,106	1000
9	5	1200	SS 304	Inconel 800	66,67,78	367
9	7	1200	Inconel 800	SS 304	79,80,81	485
10	1A	1050	2-1/4 Cr - 1 Mo	9 Cr - 1 Mo	66,67	117
10	1F	1050	2-1/4 Cr - 1 Mo	9 Cr - 1 Mo	78	250
10	3	1050	9 Cr - 1 Mo	2-1/4 Cr - 1 Mo	79,80,81	485
11	9	1200	SS 304	Inconel 800	66,67,78,79,80,81,106	1117
12	2C	1050	2-1/4 Cr - 1 Mo	9 Cr - 1 Mo	66,67,*	123
12	2G	1050	2-1/4 Cr - 1 Mo	9 Cr - 1 Mo	78,79,80,81,106	1000
<u>Above-Bed Specimens</u>						
13	28	1600	Haynes 188	Hastelloy X	66,67,78,79,80,81,106	1117
14	18	1400	Hastelloy X	Inconel 800	66,67,78,79,80,81,106	1117
15	26	1600	Hastelloy X	Haynes 188	66,67,78,79,80,81,106	1117
16	14	1400	Inconel 800	Hastelloy X	66,67,78	367
16	16	1400	Hastelloy X	Inconel 800	79,80,81	485
17	22	1600	Hastelloy X	Haynes 188	66,67,78	367
17	24	1600	Haynes 188	Hastelloy X	79,80,81	485
18	20	1400	Hastelloy X	Inconel 800	66,67,78,79,80,81,106*	1146
19	10	1200	SS 304	Inconel 800	66,67,78,79,80,81,106	1117
20	12	1200	Inconel 800	SS 304	66,67,78,79,80,81,106	1117
22	6	1200	SS 304	Inconel 800	66,67,78	367
22	8	1200	Inconel 800	SS 304	79,80,81	485

Figure 31

Westinghouse Heat Exchanger Probe Test History



* Exposed for shakedown only - see Table 21.

This collated temperature data generally reveals excellent temperature control of the individual specimens. At steady state condition 60% of the specimens had a temperature deviation from the mean less than 20°F, 90% less than 30°F, and all less than 50°F.

The probes were inspected following each run. All the specimens basically survived intact, except for the inner specimen on probe #6. This probe was comprised of Inconel 800 and Hastelloy X and controlled at 1400°F. The Hastelloy X showed considerable wastage near the capped end and developed a hole in that region after run 80 (at 565 hours). The remaining 2 in-bed probes of this type (materials and temperature) as well as the 3 above-bed probes appeared in good condition. A small portion of the probe around the perforation was removed for metallurgical analysis and the probe repaired for further testing. The probe completed the tests without further incident.

Photographs of the 14 heat exchanger probes that completed the 1000 hour testing (1117 hours total) are presented in Appendix C Figures C-1 through C-7. The photos are grouped according to probe operating temperature and bed location. For comparison, photographs taken of the probes after run 80 (682 hours for the original specimens) are presented in Appendix C Figures C-8 through C-14. Upon completion of the test program the heat exchanger probes were sent to Westinghouse R&D Center for complete metallurgical analysis. From a cursory observation of the probes it appears that the ferritic alloys and some Hastelloy X specimens experienced the most attack. Table 22 presents a brief summary of the probe specimen appearance at the conclusion of the testing. The 14 probes inspected were all exposed for 1117 hours. The above-bed probe specimens generally appeared in better condition than the in-bed probes.

TURBINE BLADE SPECIMENS

The turbine test section was positioned in the miniplant discharge piping for the entire PFBC hot corrosion/erosion testing program. The blades exposed during the initial 117 ("shakedown") hours were returned to GE for metallurgical analysis. The extended testing was started with an entirely new set of specimen blades, some bare and some clad.

Among the 24 airfoil specimens starting the test were 9 unclad base alloy specimens (4 of IN-738, 3 of U-700 and 2 of FSX-414). The other IN-738 blades were clad with either IN-671, S-57 or GE-2541. Blades of FSX-414 were clad with GE-2541. One blade with IN-738 as the base alloy was coated with RT-22 (platinum-aluminide).

Of the original airfoil specimens in the 24 cascade positions, 13 specimens were exposed for the full 1000 hours. Another 27 specimens were located in the remaining 11 positions for periods as short as 48 hours to as much as 750 hours. These blades were selectively replaced at various stages of the test. A tabulation of the specimen materials identification, cascade location, and exposure times is given in Table 23. Figure 7 (Section III) depicts the specimen location in the cascades and Figure 32 is a graph of the specimen location and exposure history.

Table 22

Heat Exchanger Probe Appearance
at Test Conclusion

<u>Specimen Alloy</u>	<u>Temp (°F)</u>	
		<u>In-Bed</u>
2-1/4 Cr - 1 Mo/9 Cr - 1 Mo	1050	Thick, hard deposits and considerable oxide spalling
304 SS/Inconel 800	1200	Substantial oxidation of both specimens
Inconel 800/Hastelloy X	1400	Hastelloy X pitted and 1 Hastelloy X perforated
Hastelloy X/Haynes 188	1600	Hastelloy X oxidized slightly more than Haynes 188
		<u>Above-Bed</u>
304 SS/Inconel 800	1200	Smooth, deep reddish deposits
Inconel 800/Hastelloy X	1400	Some oxidation, especially on lower surfaces
Hastelloy X/Haynes 188	1600	Thin, brownish deposits

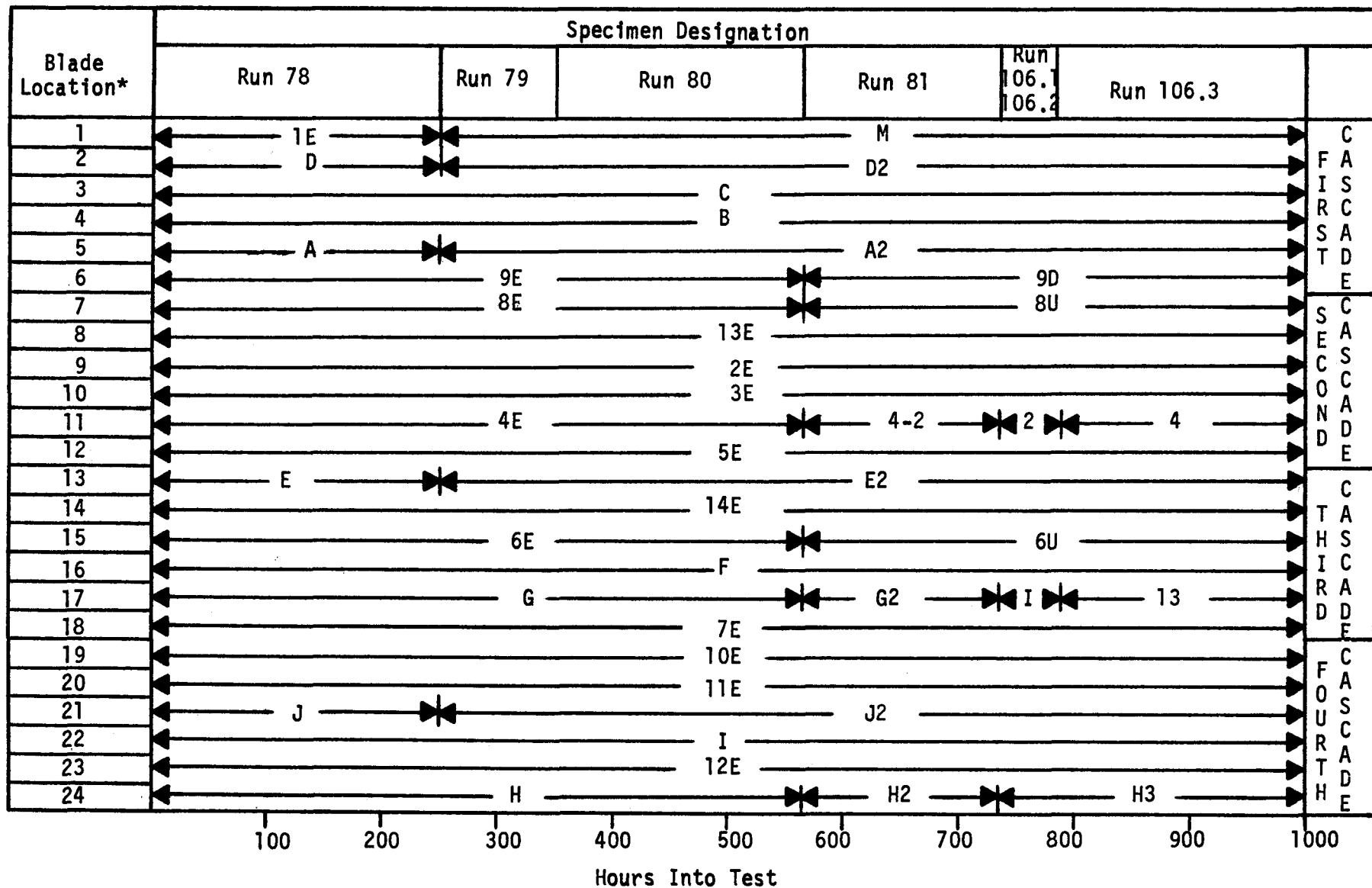
Table 23

GE Turbine Test Blade Specimens
Exposed During the 1000 Hour Test

<u>Location No.</u>	<u>Base Alloy</u>	<u>Cladding/Coating</u>	<u>Specimen No.</u>	<u>Runs Exposed</u>	<u>Hours Exposure</u>
1	IN-738	IN-671	1E	78	250
2	IN-738	--	D	78	250
3	U-700	--	C	78-106	1000
4	IN-738	--	B	78-106	1000
5	FSX-414	--	A	78	250
6	IN-738	S51/A1	9E	78-80	565
7	IN-738	GE-2541 PM	8E	78-80	565
8	FSX-414	PFB-6PM/A1	13E	78-106	1000
9	IN-738	S57/A1	2E	78-106	1000
10	IN-738	GE-2541 PM	3E	78-106	1000
11	IN-738	IN-671	4E	78-80	565
12	IN-738	PFB-6A1	5E	78-106	1000
13	U-700	--	E	78	250
14	FSX-414	GE-2541 PM	14E	78-106	1000
15	IN-738	PFB-6/A1	6E	78-80	565
16	IN-738	RT-22	F	78-106	1000
17	IN-738	--	G	78-80	565
18	IN-738	PFB-6	7E	78-106	1000
19	IN-738	GE-2541 PM	10E	78-106	1000
20	IN-738	IN-671	11E	78-106	1000
21	IN-738	--	J	78	250
22	FSX-414	--	I	78-106	1000
23	FSX-414	PFB-6PM/A1	12E	78-106	1000
24	U-700	--	H	78-80	565
1	IN-738	--	M	79-106	750
2	IN-738	--	D2	79-106	750
5	FSX-414	--	A2	79-106	750
13	U-700	--	E2	79-106	750
21	IN-738	--	J2	79-106	750
6	IN-738	S57/A1	9D	81-106	435
7	IN-738	GE-2451	8U	81-106	435
11	IN-738	IN-671	4-2	81	170
15	IN-738	PFB-6/A1	6U	81-106	435
17	IN-738	--	G2	81	170
24	U-700	--	H2	81	170
11	IN-738	IN-671	2	106.1- 106.2	48
17	IN-738	--	I	106.1- 106.2	48
24	U-700	--	H3	106	265
11	IN-738	--	4	106.3	217
17	FSX-414	--	13	106.3	217

Figure 32

Turbine Test Section Specimen History



*See Figure 7

The turbine blade specimens were routinely brushed with a soft bristle brush and inspected after 250, 565, 735 and 783 hours of exposure. After 735 hours of PFBC exposure the turbine blade specimens revealed no obvious signs of attack. At the 250 and 565 hour inspections there was substantial deposition of flyash on the suction (i.e., convex) surface of the airfoils near the trailing edge. Figures 33, 34 and 35 show the second cascade specimens after 250, 565 and 735 hours exposure, respectively. Note that the particulate deposition present on the trailing edges of the blades in Figure 33 and 34 is not present in Figure 35. The photograph in Figure 35 was taken after run 81, during which the primary "recycle" cyclone plugged and increased the mean particle size and particulate loading at the turbine test section. This scouring effect did not cause visible erosion. However, it did act to remove or prevent the accumulation of deposits on the blades.

Run 106 started at the 735 hour mark but had to be interrupted after only 48 hours (at the 783 hour mark) because abnormally high particulate loadings were detected at the turbine test section. The high particulate loadings were found to be caused by blockage of the third stage cyclone. It is deduced that the turbine blade specimens were exposed to an order of magnitude increase in particulate concentration (Figure 27) for not longer than 7 hours and most probably 5 to 6 hours.

Examination of the turbine blades revealed that some specimens experienced noticeable erosion during this 48 hour interval, almost certainly mostly occurring in those final 5 to 6 hours. Practically no flyash deposits were found on the blade specimens. This corroborates previous experience, where the existence of higher particulate loading can scour the deposits from the blades. The blade specimens were gently cleaned and weighed. Many specimens experienced a weight loss of almost 0.10 grams. The erosion was most prominent on the leading edge of the airfoils. The blades with the most noticeable erosion wastage were in the following cascade sites (see Figure 7).

<u>Cascade</u>	<u>Location</u>
1st	3, 4, 5
2nd	9 (slight)
3rd	17, 16
4th	20, 21, 22, 23 (esp. 21)

The blades in the fourth cascade, which are the only reaction type airfoil profiles and where the flow velocities approach sonic, experienced the most prominent erosion. The most severely eroded specimen was in position 21 (Figure 7), which lost about 0.3 grams. All the reaction blades in the center of the 4th cascade also exhibited erosion on the pressure side - from the leading edge to about the center of the airfoil.

Figure 33

View of the Leading and Trailing
Edges of the Second Cascade
(Run 78)

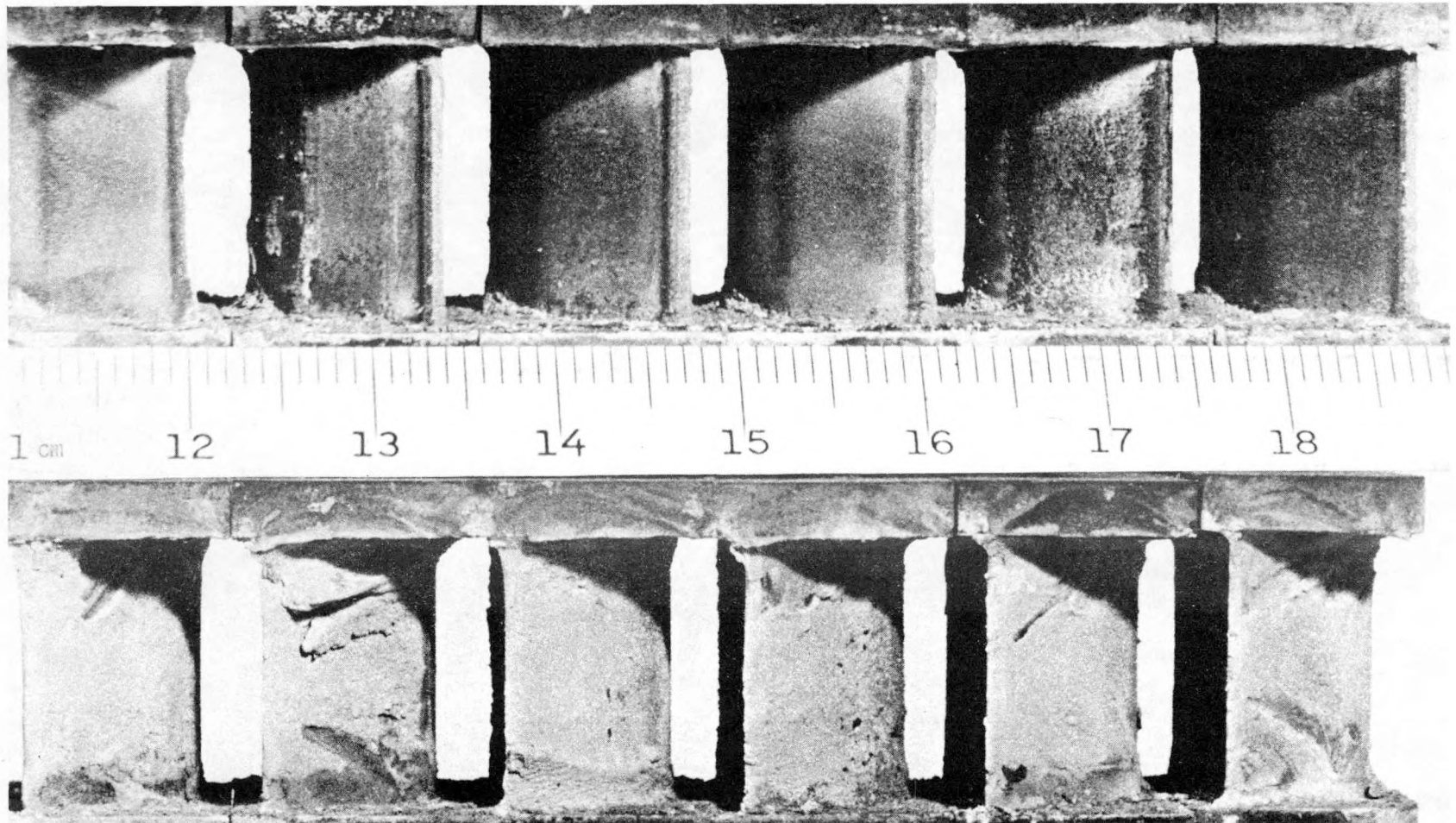


Figure 34

View of the Leading and
Trailing Edges of the Second Cascade

(Run 80)

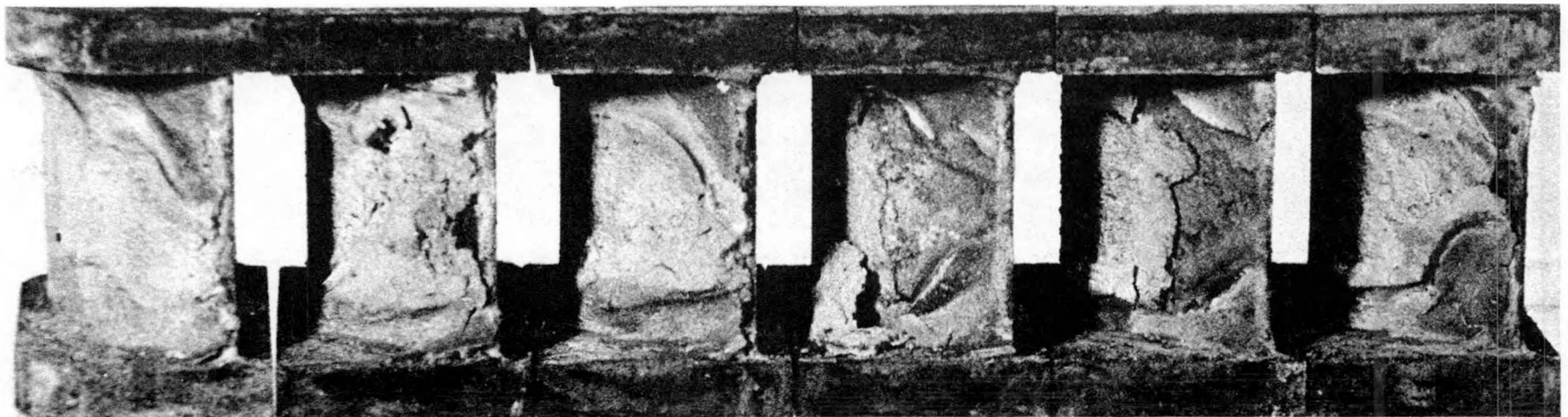
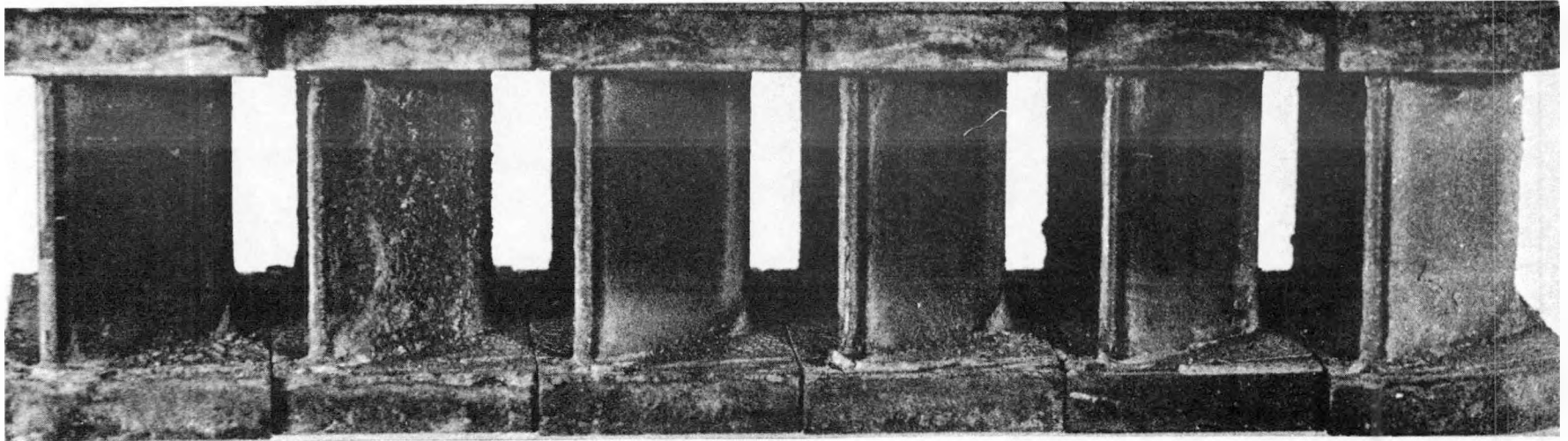
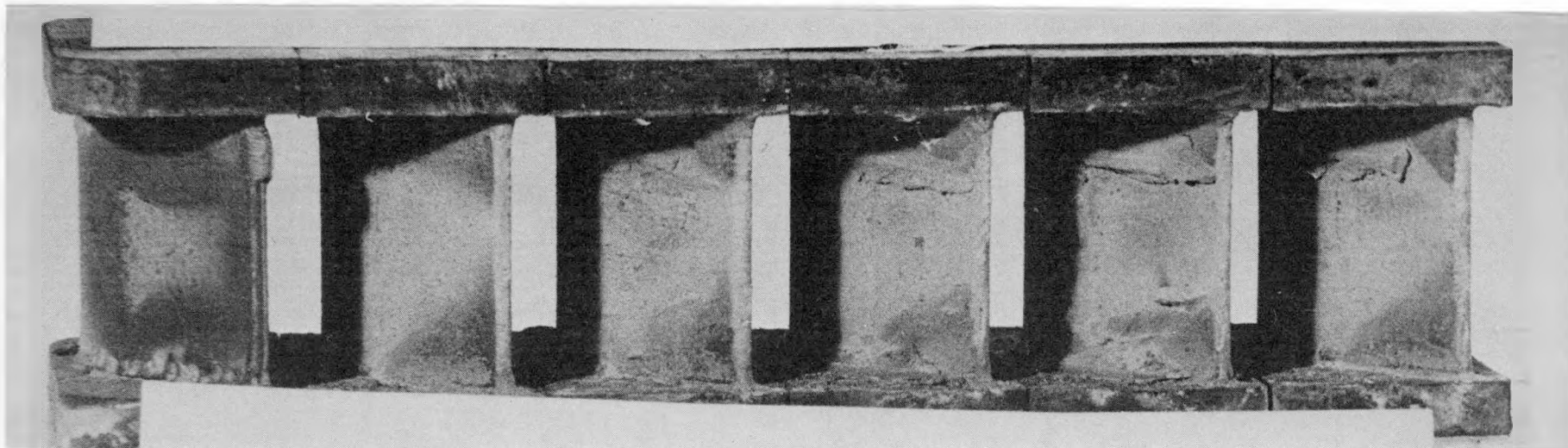
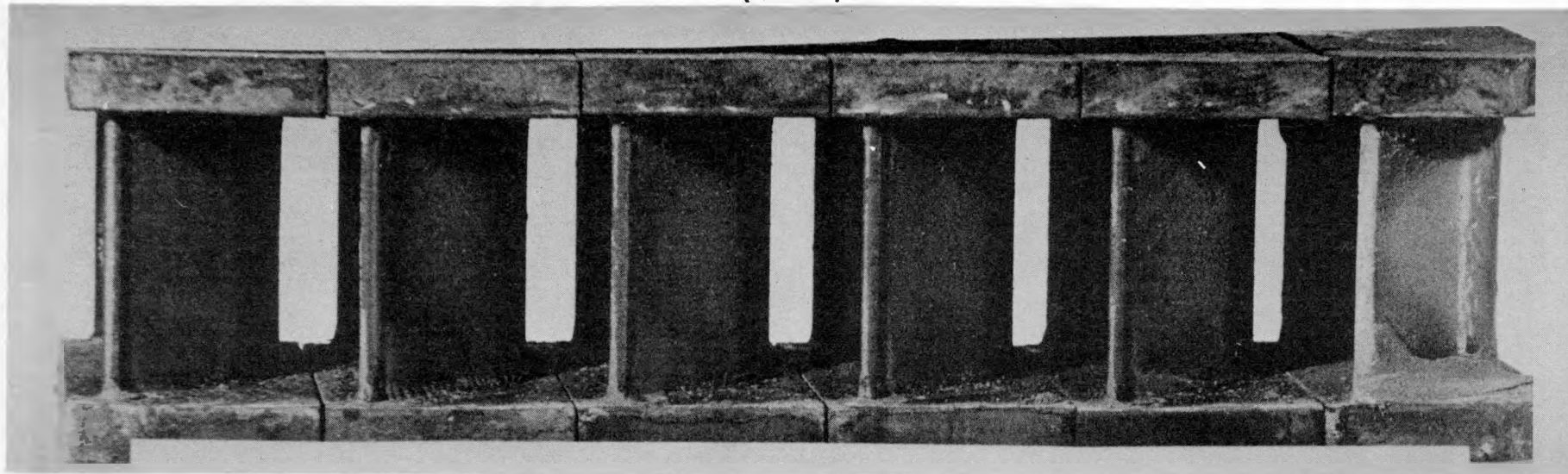


Figure 35

View of the Leading and
Trailing Edges of the Second Cascade

(Run 81)



At the start of run 106, three new blade specimens had been inserted; one in the 2nd cascade (position 11), one in the 3rd cascade (position 17), and one in the 4th cascade (position 24). The airfoil at position 17 revealed considerable erosion at the leading edge, especially considering only 48 hours of exposure. To provide a guideline to help characterize the effects of this high particulate loading episode, it was decided to remove the specimens from positions 11 and 17 so that they could be available for metallographic examination. Replacement airfoils for these locations were obtained from GE and placed in the passage. Run 106 resumed and operated smoothly for the final 217 hours.

Figure 36 is a photograph of the two blades in position 17 during run 106 along side one another, revealing the erosion on the leading edge of the first specimen (I). Note that the other blade, which was exposed ~5 times longer to particulate concentrations ~5 times lower showed no signs of erosion.

At the conclusion of the 1000 hour PFBC exposure tests the turbine blade specimens were photographed and returned to General Electric for metallurgical examination. Flyash deposits from each blade cascade were collected for particle size analysis. From a cursory inspection, the airfoils generally appear satisfactory. The 4th cascade specimens in locations 20, 21, 22, and 23 (Figure 7) still exhibited the most noticeable erosion. Indeed, the most airfoil erosion during the 1000 hours of exposure appeared to occur during this run just concluded, and in particular during the 5 or 6 hours of this run, when the third staged cyclone plugged.

The photograph in Figure 37 is the leading edge of specimen J2 as it appeared at the completion of the test. This specimen in the fourth (reaction) cascade, position 21, experienced the most severe erosion. All of the noticeable metal wastage apparently occurred during the high particulate loading period. Visual inspections and weight comparisons of blade specimen J2 before and after the final 217 hours of exposure did not disclose signs of further erosion.

Figures 38 and 39 show a top and bottom view of all of the blade specimens exposed during the final 217 hours (run 106.3). Although some erosion is evident, it is not catastrophic and appears mostly to have occurred during run 106.2, the high particulate loading period.

Throughout the 1000 hour exposure test, gas flow through the turbine test section was within the required range (Figure 40). Although the flow rate varied somewhat from run to run, during a given test it was fairly steady. During most runs a slight decrease in flow with time was experienced. This is attributed to particulate deposition on the pressure reducing section or on the blades themselves. The most dramatic drop in flow occurred after a 2 hour shutdown during run 81. The flow went from 680 to 625 SCFM. The 1-1/2 day shutdown during run 106 did not cause such a sharp decrease in flow rate. This was probably due to the fact the flue gas line and the turbine test section were dismantled and cleaned prior to restarting.

Figure 36

Specimens Occupying Position No. 17 During Run 106

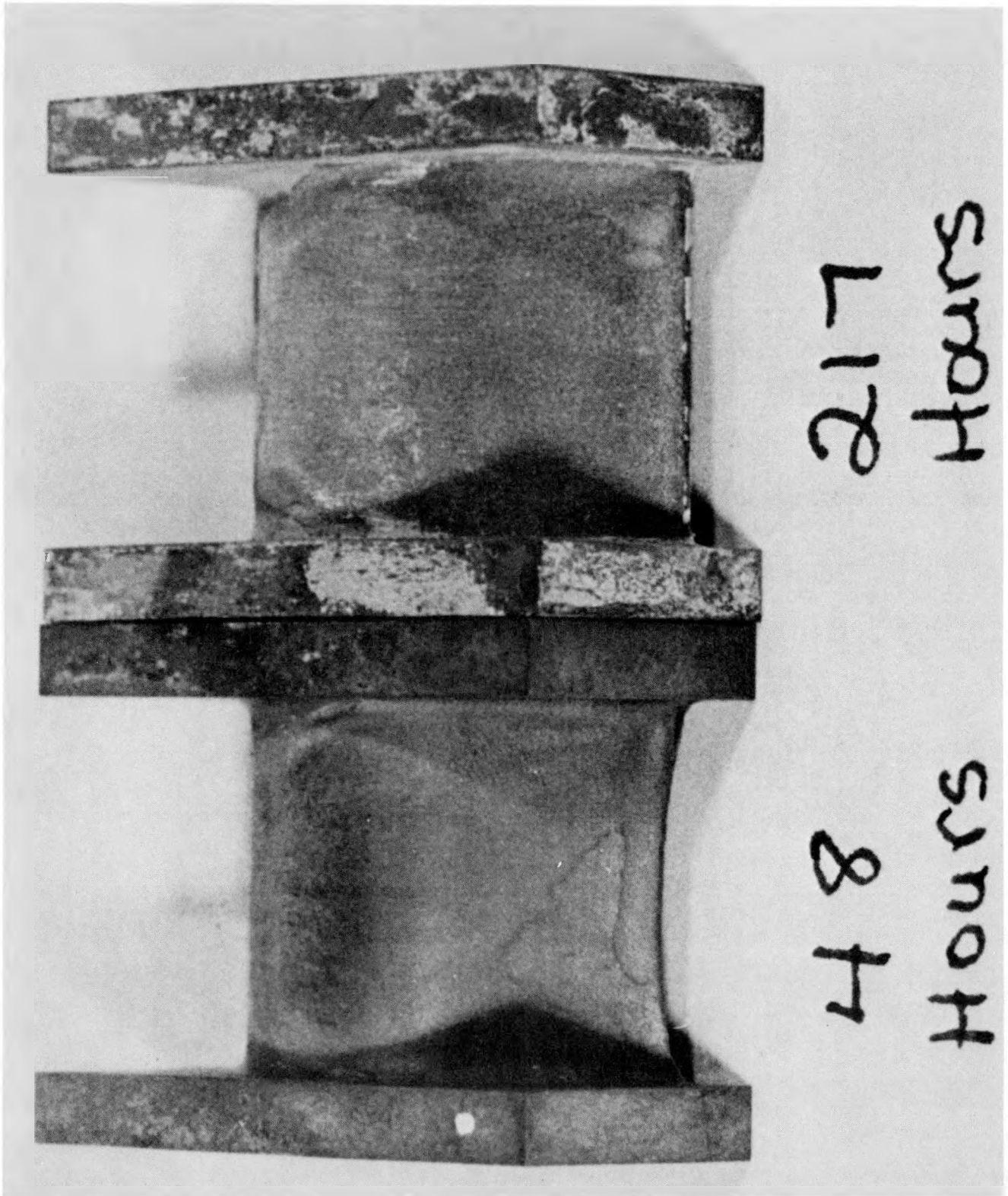


Figure 37

Blade Specimen J2 (21) After 1000 Hours

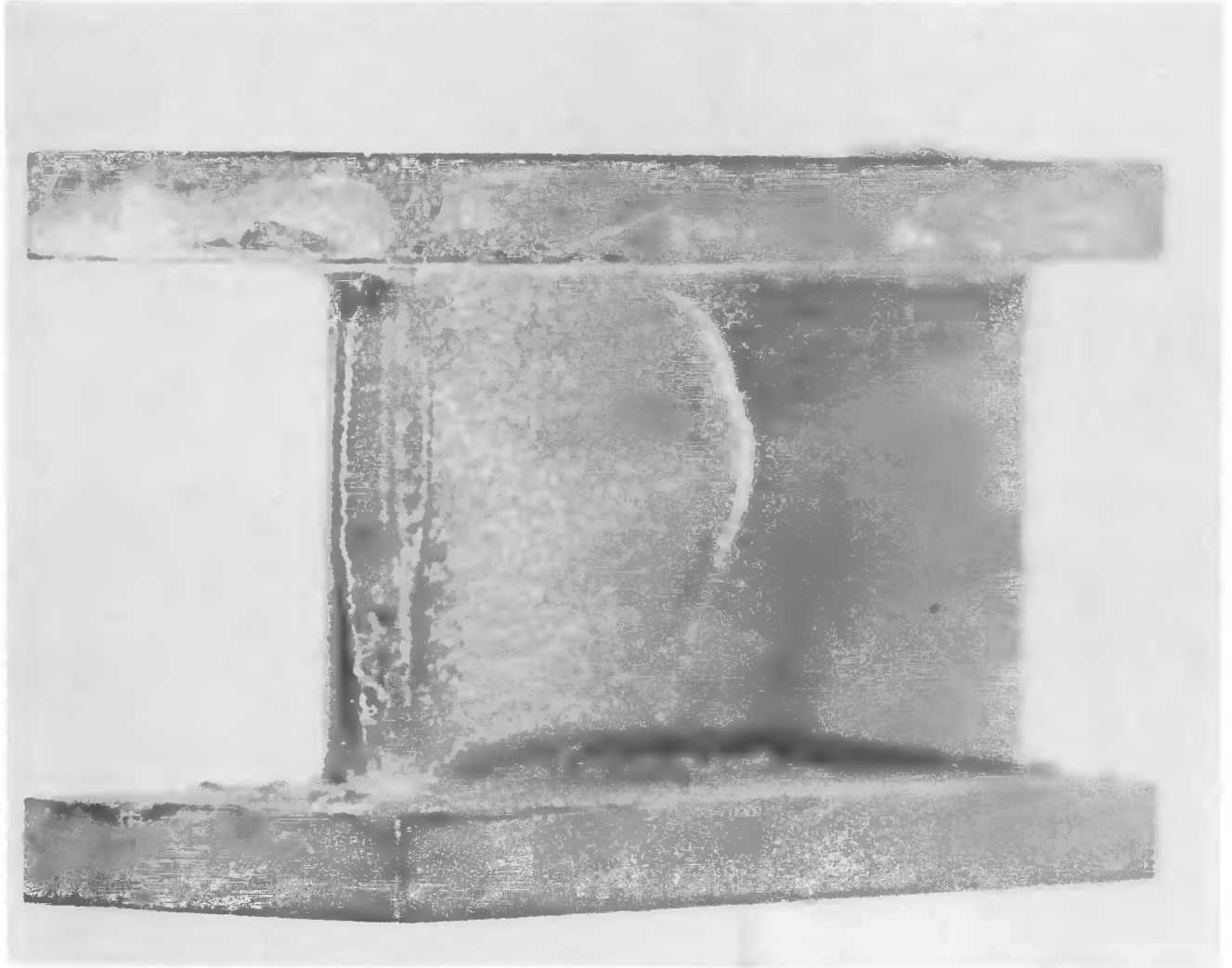


Figure 38

All Blade Specimens After 1000
Hour Tests (Convex Side)

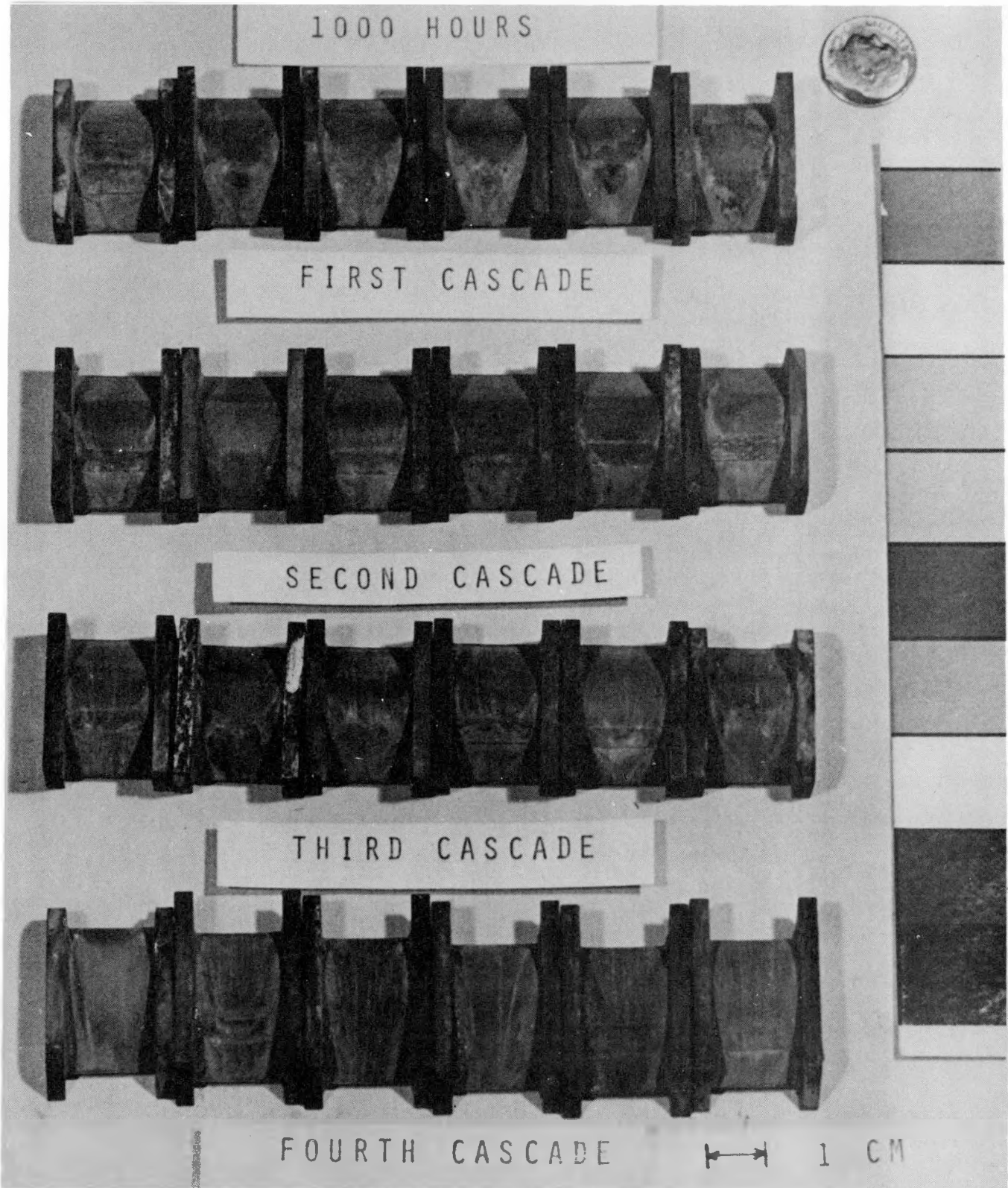


Figure 39

All Blade Specimens After 1000
Hour Tests (Concave Side)

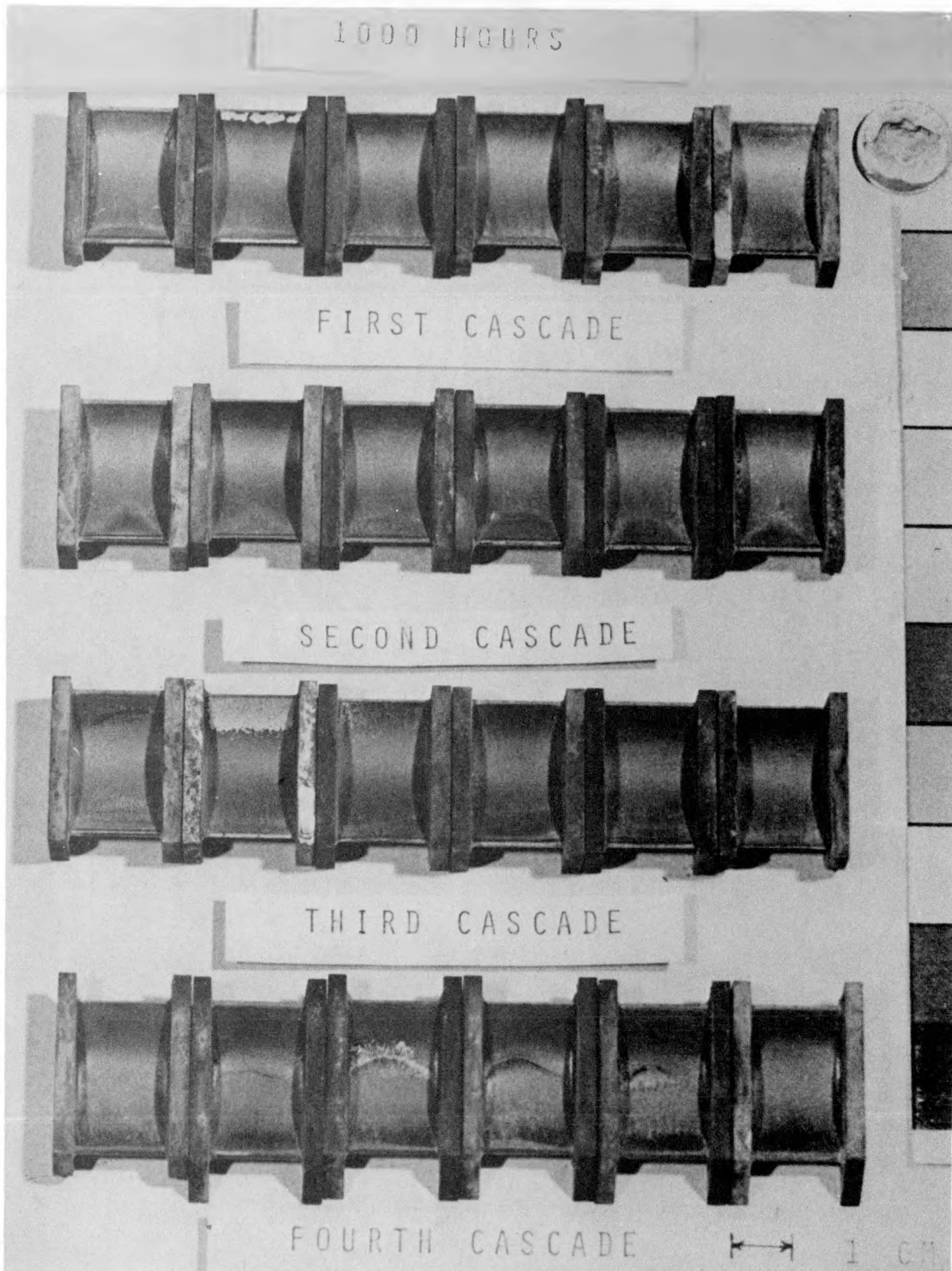
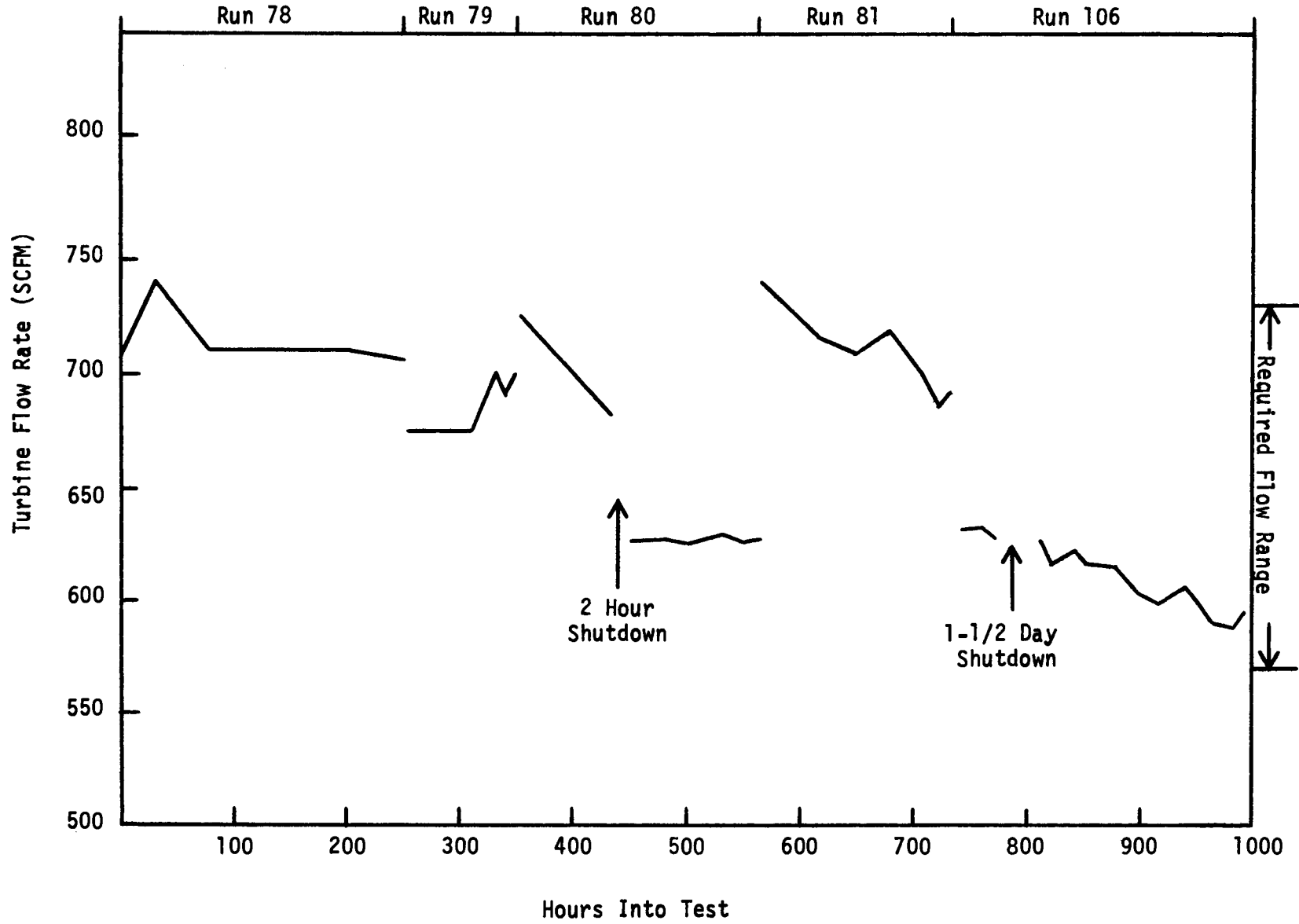


Figure 40

1000 Hour Turbine Flow Summary



CORROSION DISCS

During the 1000 hour hot corrosion exposure test, it was intended that combustor and discharge line conditions be constant. This provided an opportunity to obtain extended fireside corrosion data by also locating alloy specimens in the freeboard of the combustor. The same materials used for the turbine airfoil specimens were mounted on a support located inside the combustor. This permitted a comparison of the hot corrosion attack of the same material at two different regions within a PFBC.

Three sets of alloy discs (4 samples per set) were received from General Electric for exposure in the 1000 hour testing program. The alloys received were U-700, IN-738, and FSX-414. The first two are nickel based alloys similar to those tested in the turbine test section; the latter is a cobalt based alloy. The discs are approximately 1 inch in diameter by 1/16 inch thick. In the 250 hour run, two specimens from each alloy set were exposed in the combustor freeboard region in the vicinity of the heat exchanger probes. A plot of the combustor temperature profile at three times during the run is shown in Figure 22. This figure also shows the location of the corrosion discs and their approximate exposure temperatures. Visual examination of the discs after each run revealed no obvious signs of erosion or corrosion (Figure 41). Discs were periodically taken by General Electric for metallurgical analysis after various exposure times.

CONCLUSIONS

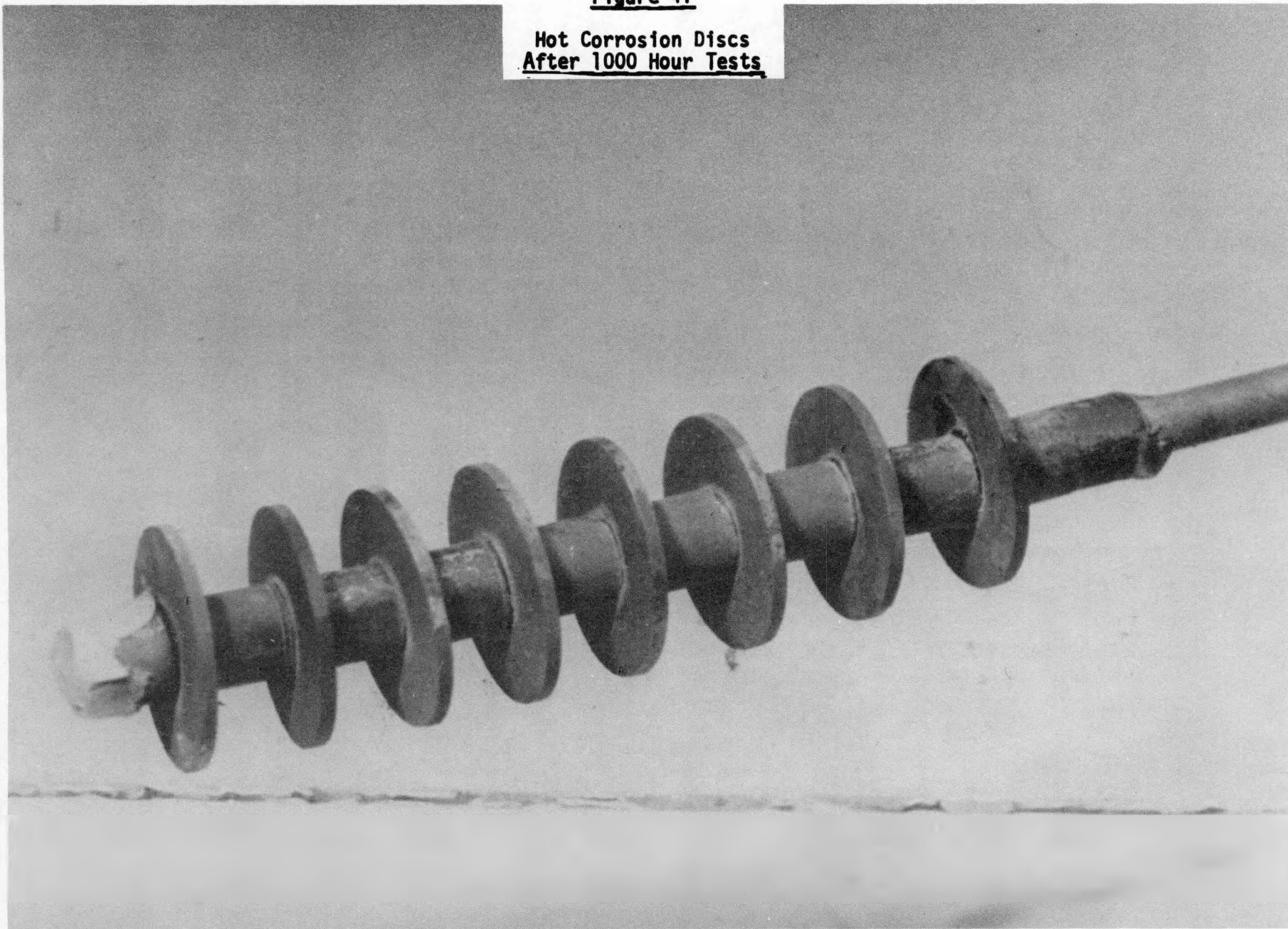
The 1100 hour test at the Exxon Miniplant facility has indicated that materials are available for use in the PFBC application as heat exchanger and turbine blades. This needs to be further substantiated by metallurgical testing which will be performed by Westinghouse Research and Development (1) and General Electric Company (2) on these specimens, as well as subsequent testing of materials in PFBC environments such as those presently being undertaken at the Coal Utilization Research Laboratory in England and by Curtiss-Wright. Furthermore, the indication is that particulate cleanup using conventional cyclones may be sufficient to provide adequate gas turbine protection for periods of time economically feasible in a PFBC application.

While cyclones seem to provide adequate protection for turbine blade materials, a number of significant problems may exist in terms of maintaining control. These are:

Particle grain loading and particle size need to be controlled to relatively low concentrations (0.025 to 0.07 gr/SCF), and mean particle size of approximately 1-2 microns if significant erosion is to be avoided.

Figure 41

Hot Corrosion Discs
After 1000 Hour Tests



- Based on the Miniplant tests, there is a suspicion, that very fine particulate (less than 1.1 microns) and low grain loadings may induce particle deposition in the ducting prior to the gas turbine as well as on the gas turbine blades. Subsequent spalling of this material may cause severe erosion problems. There may be a lower limit to which cleanup might be feasible. This needs to be further explored in subsequent tests.
- High particulate loading or large mean particle size which could result from relatively minor process or equipment malfunctions e.g., cyclone plugging, can cause erosion rates that would very rapidly decrease the efficiency of the gas turbine. Therefore, reliable particulate control and measurement systems are necessary to protect the gas turbine.

Corrosion and erosion problems are not severe for heat exchanger materials in the freeboard of the combustor. However, the degree of in-bed corrosion/erosion in the fluidized bed needs to be further quantified by metallurgical analysis before definitive recommendations can be made for suitable heat exchanger materials.

VI. BIBLIOGRAPHY

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3. Hoke, R. C., et al, "Miniplant Studies of Pressurized Fluidized-Bed Coal Combustion: Final Report," to be published under EPA Contract No. 68-02-1312.
4. "Evaluation of A Cyclonic Type Dust Collector for High Temperature High Pressure Particulate Control," M. Ernst, R. C. Hoke, V. J. Siminski, J. D. McCain, R. Parker, D. C. Drehmel, Presented for "The Second Symposium on the Transfer and Utilization of Particulate Control Technology," July 23-27, 1979 in Denver, Colorado.

APPENDIX A

TURBINE BLADES AND HEAT
EXCHANGER PROBES AFTER SHUTDOWN

Enclosed are photographs of the appearance of the turbine blade and heat exchange probes after shutdown. The temperature history of the probes during shutdown are also included.

Figure A-1

View of the Leading and
Trailing Edges of the First Cascade

100 Hour Shakedown



Figure A-2

View of the Leading and Trailing
Edges of the Second Cascade

100 Hour Shakedown

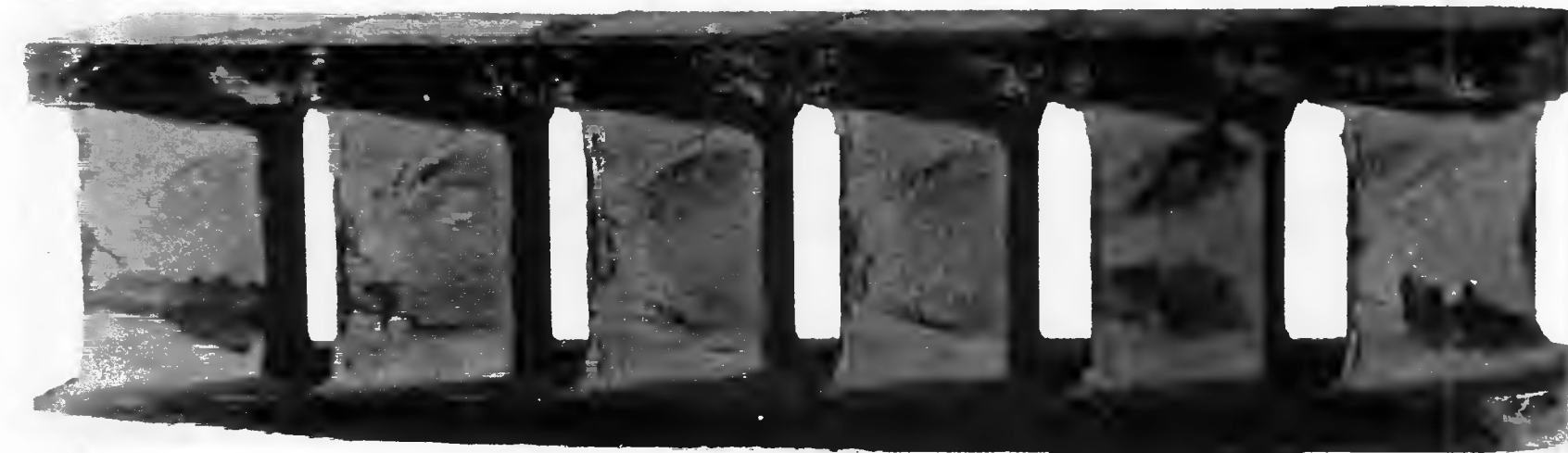
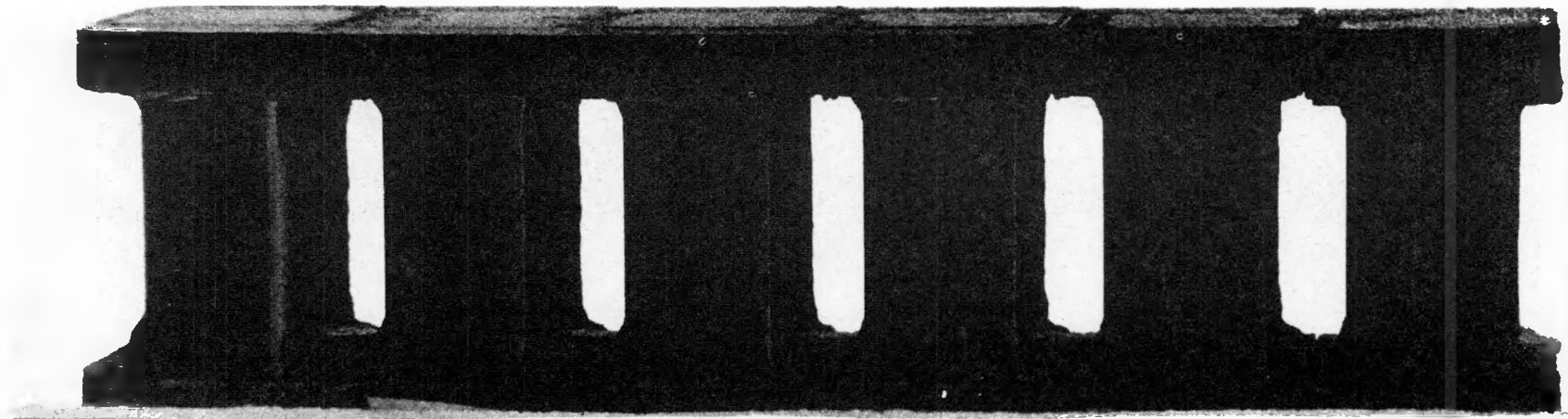


Figure A-3

View of the Leading and
Trailing Edges of the Third Cascade

100 Hour Shakedown

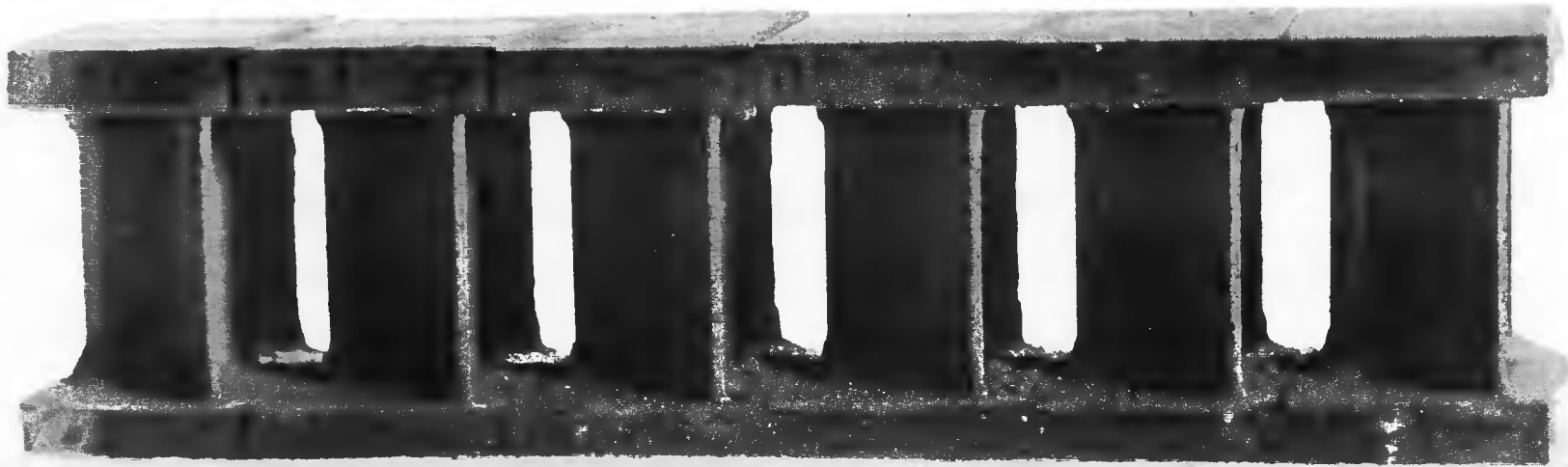


Figure A-4

View of the Leading and
Trailing Edges of the Fourth Cascade

100 Hour Shakedown

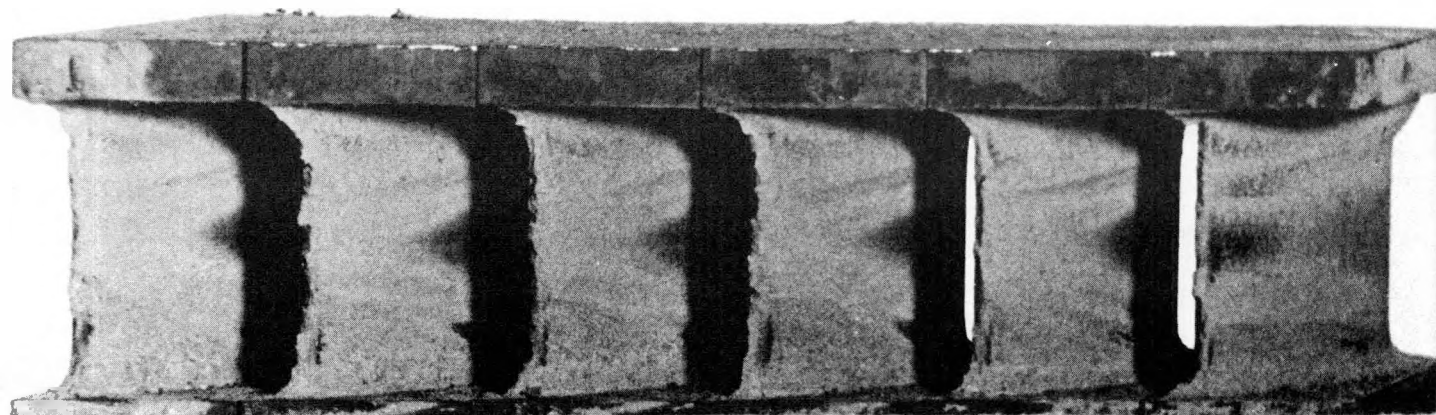
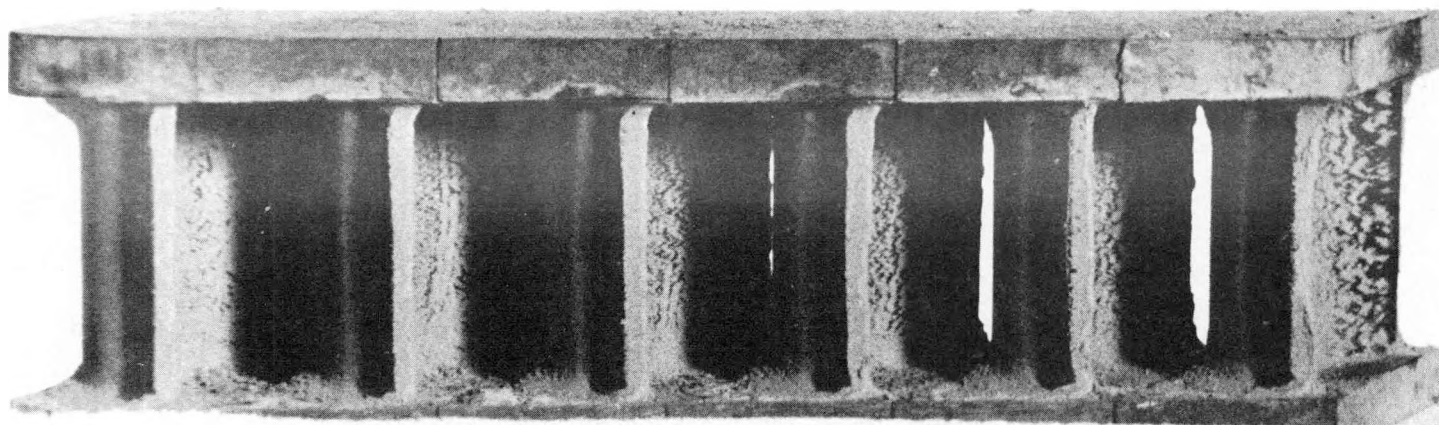


Figure A-5

Probe #1 1600°F In Bed (Shakedown Run 67)

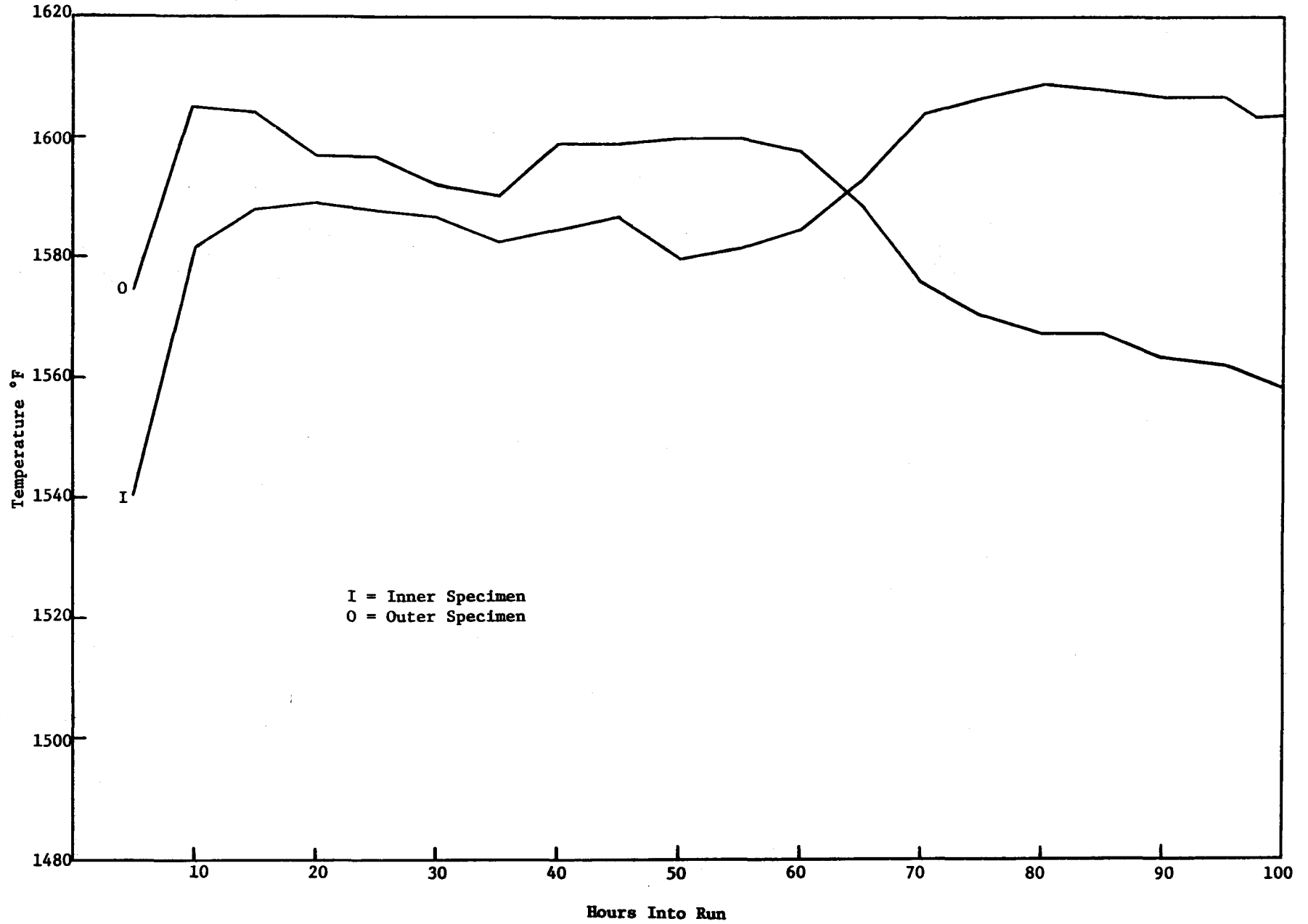


Figure A-6

Probe #13 1600°F Above Bed (Shakedown Run 67)

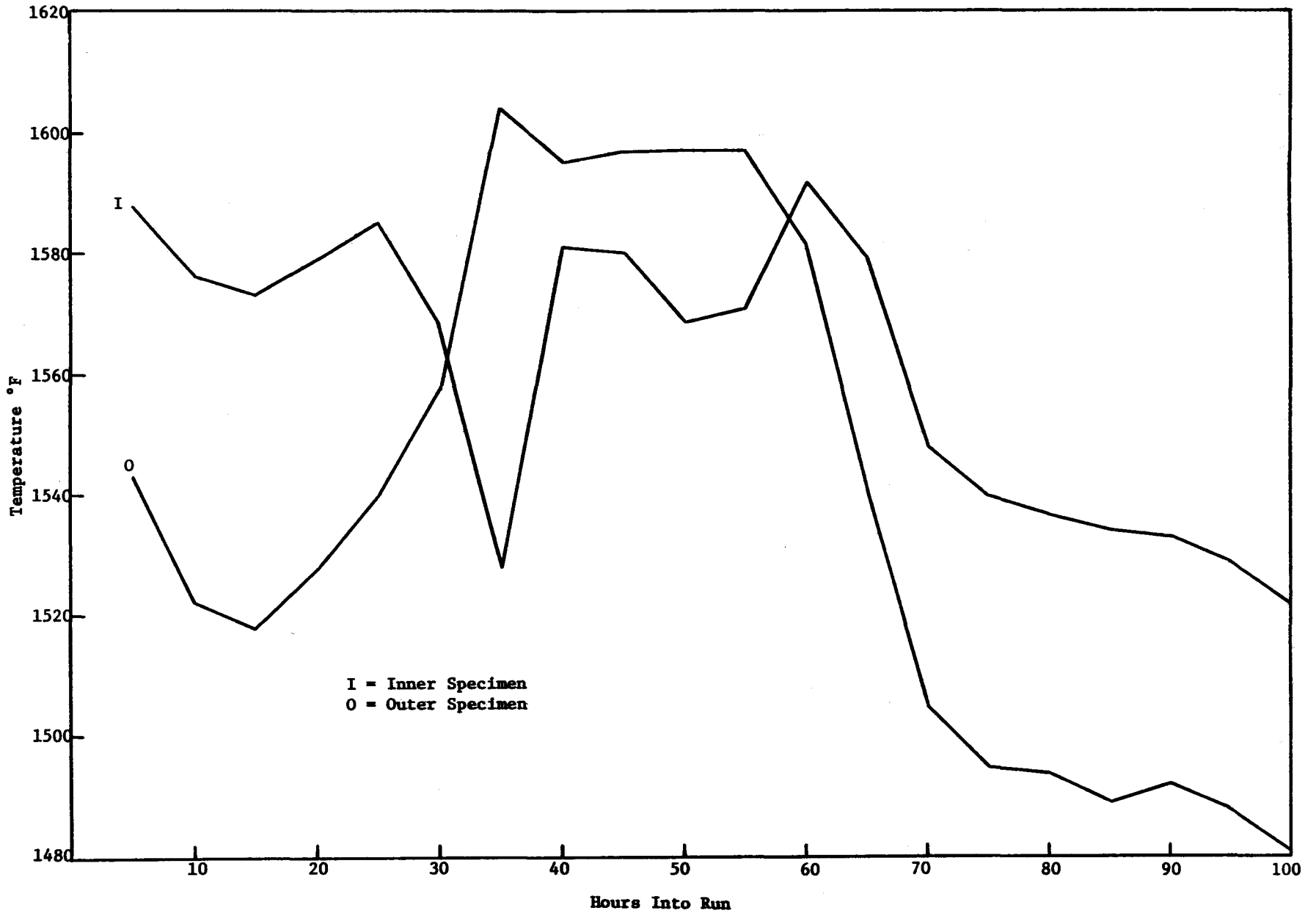


Figure A-7

Probe #6 1400°F In Bed (Shakedown Run 67)

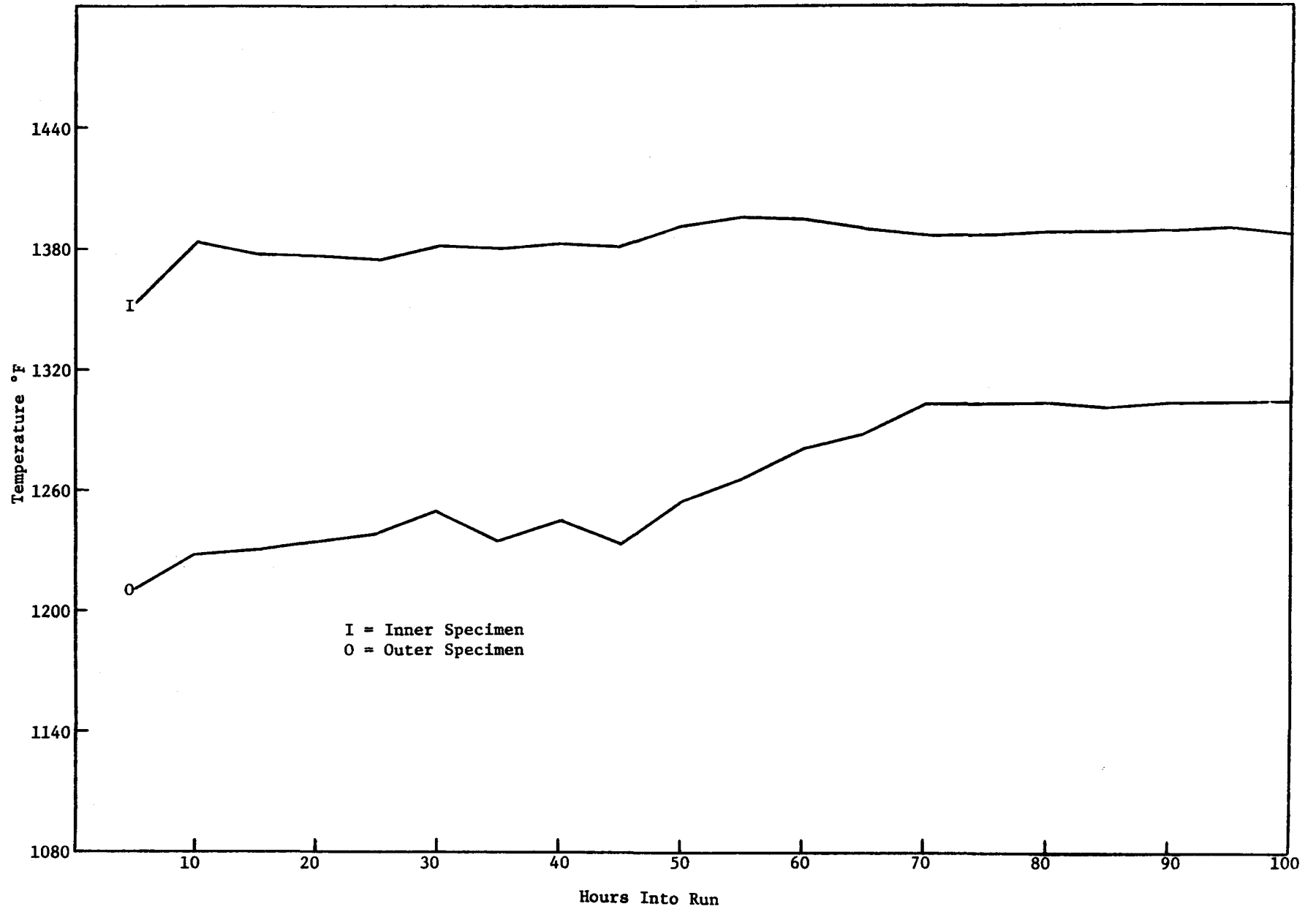


Figure A-8

Probe #14 1400°F Above Bed (Shakedown Run 67)

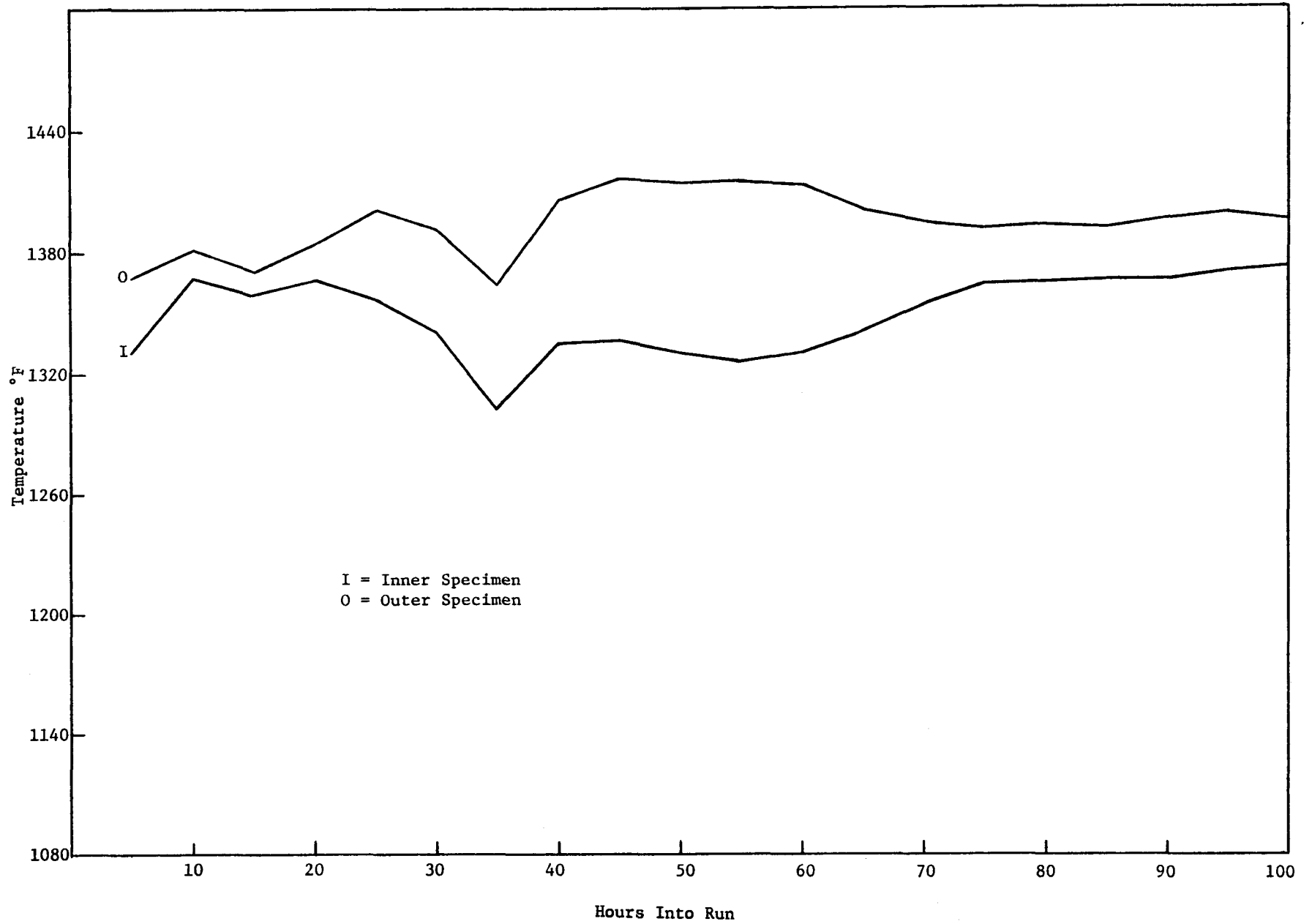


Figure A-9

Probe #11 1200°F In Bed (Shakedown Run 67)

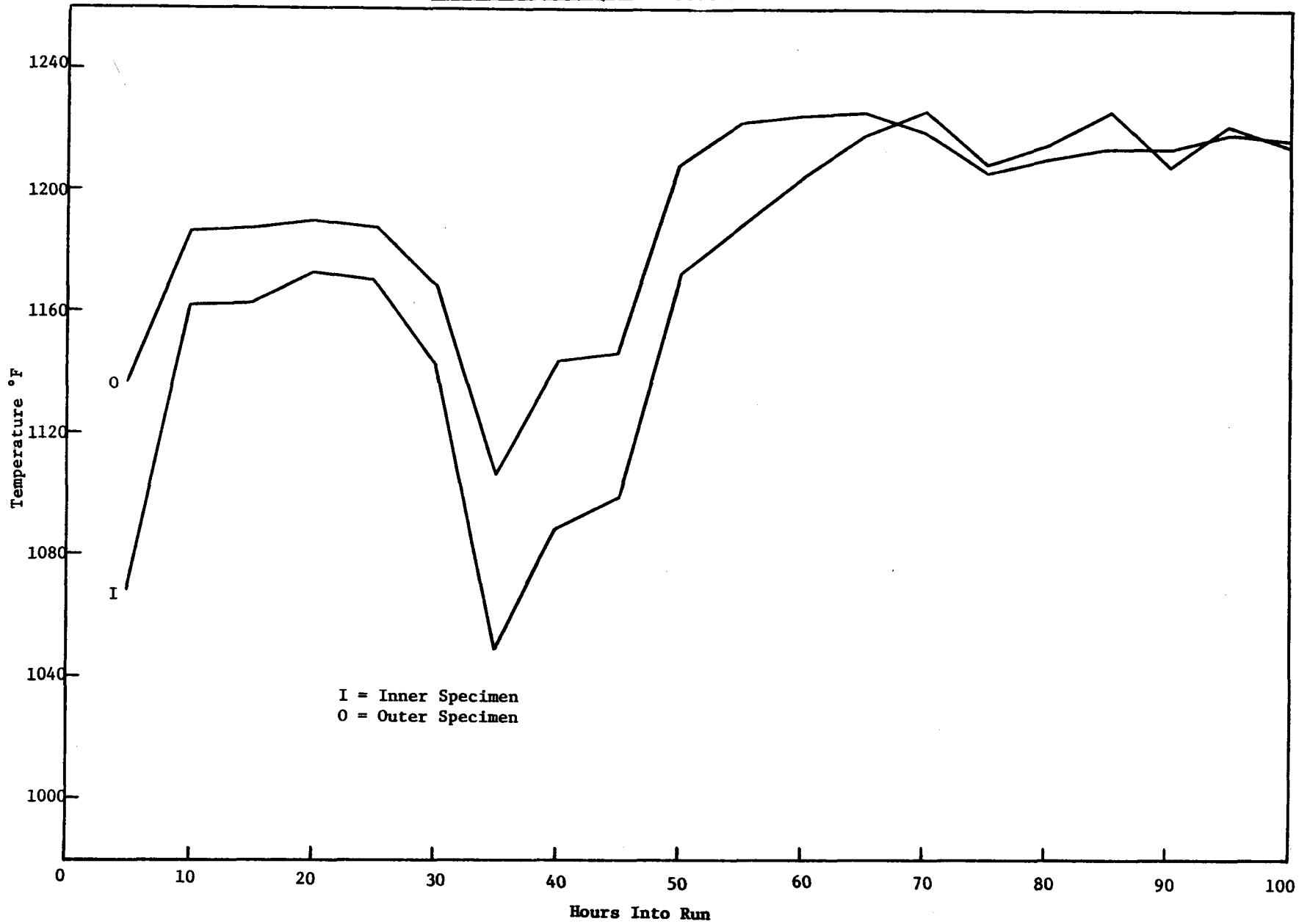


Figure A-10

Probe #20 1200°F Above Bed (Shakedown Run 67)

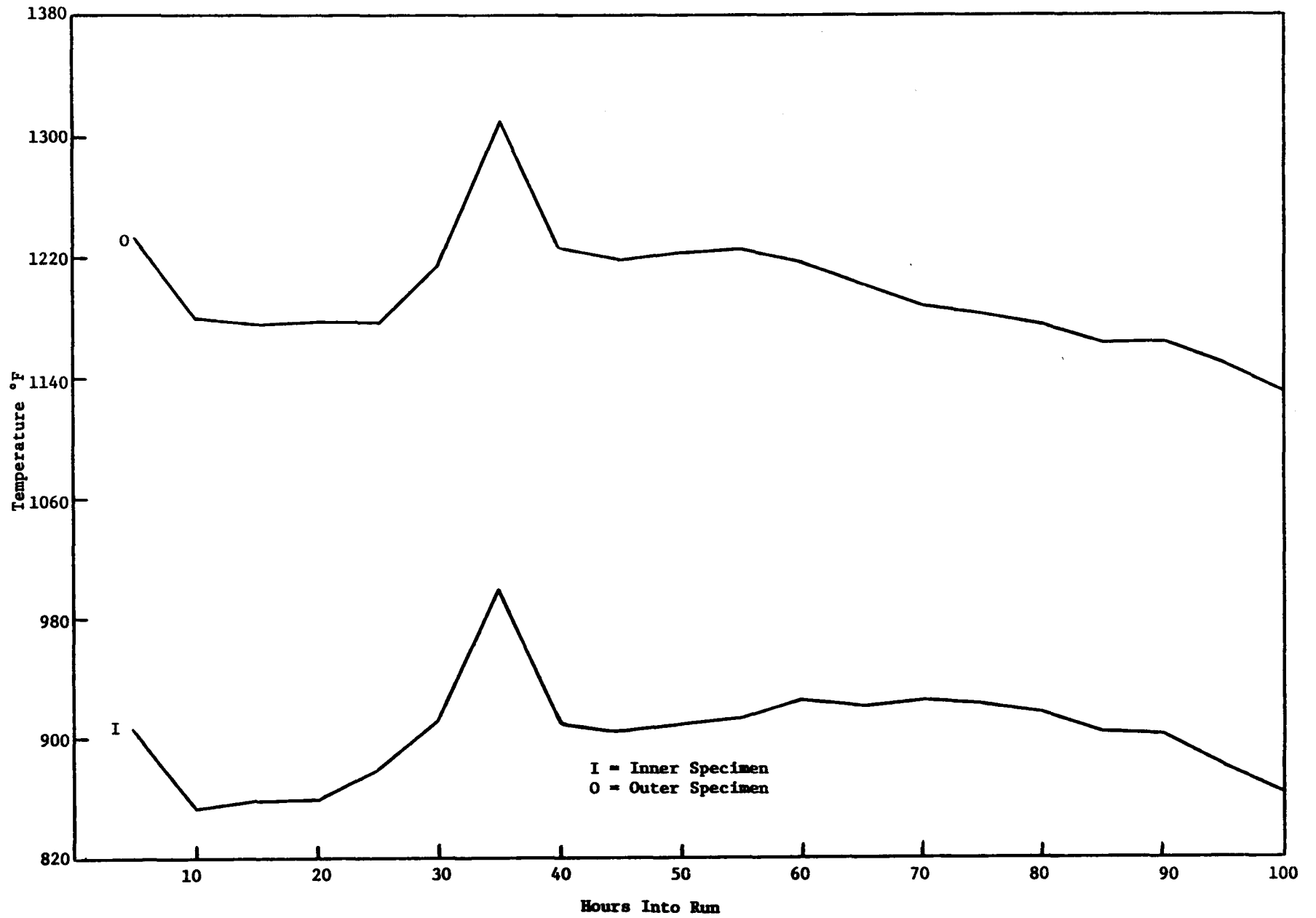


Figure A-11

Probe #8 1050°F In Bed (Shakedown Run 67)

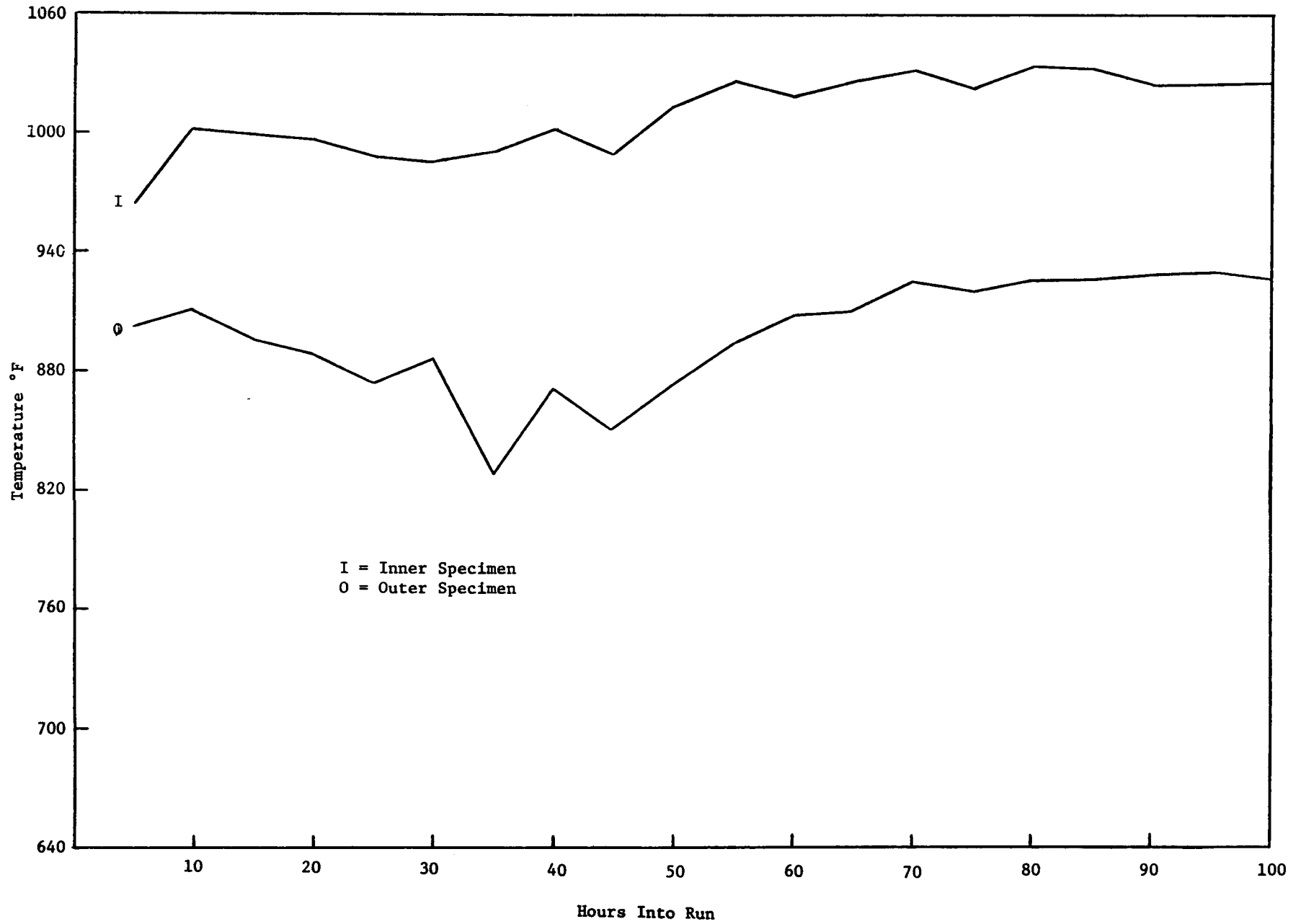


Figure A-12

1600°F In-Bed Probe (Top Side View)

After Shakedown

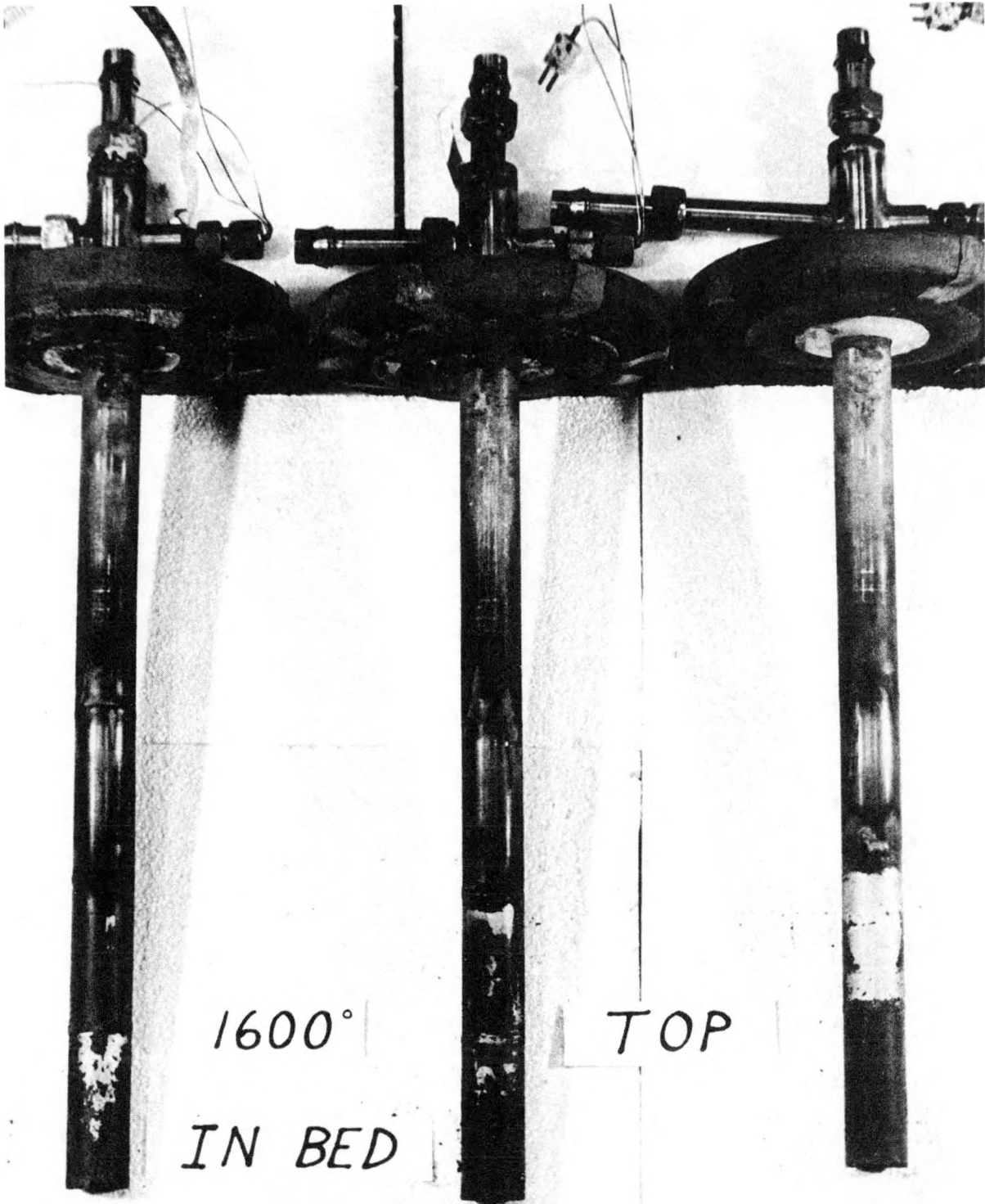


Figure A-13

1600°F Above-Bed Probe (Top Side View)

After Shakedown

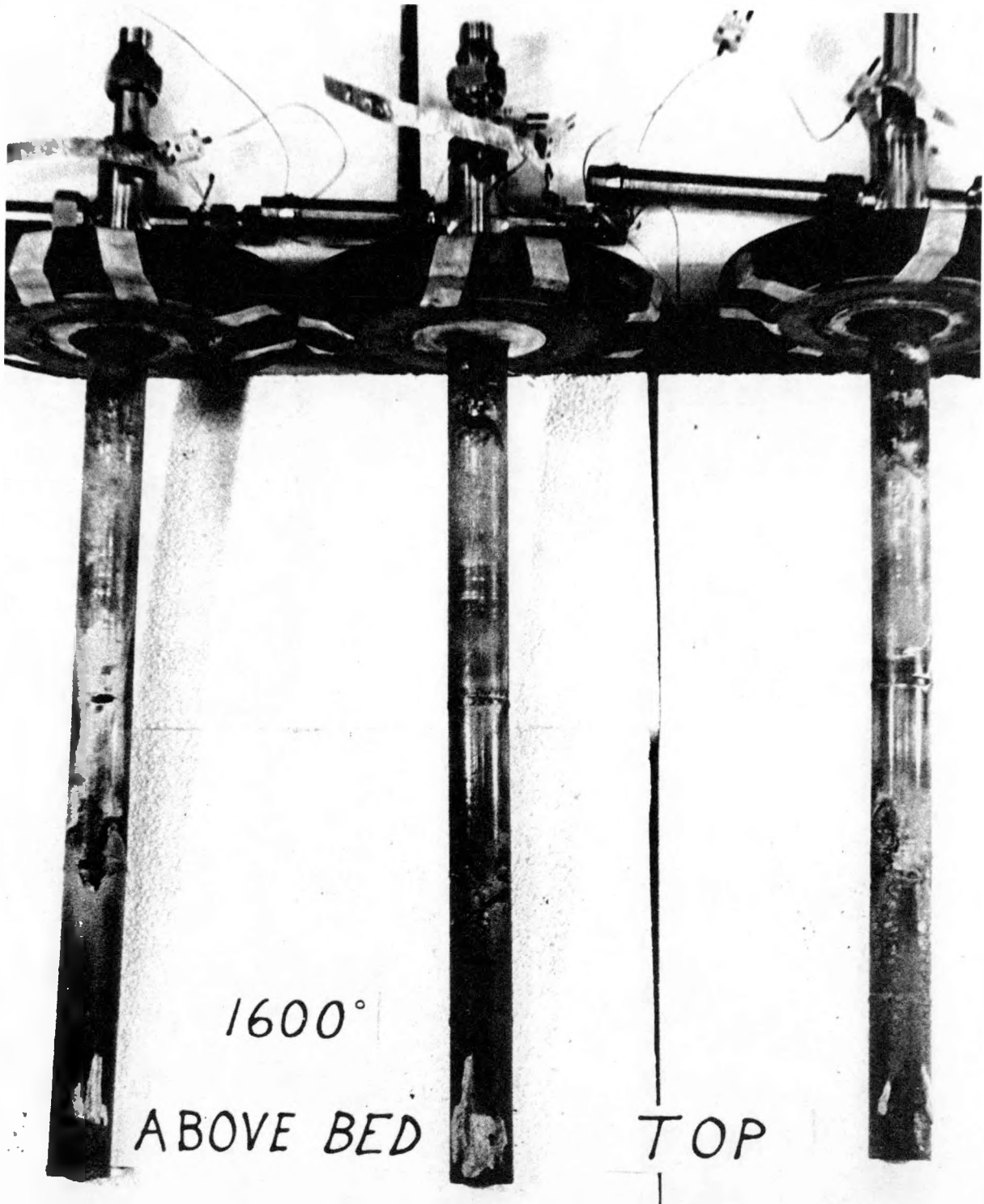


Figure A-14

1400°F In-Bed Probe (Bottom Side View)

After Shakedown

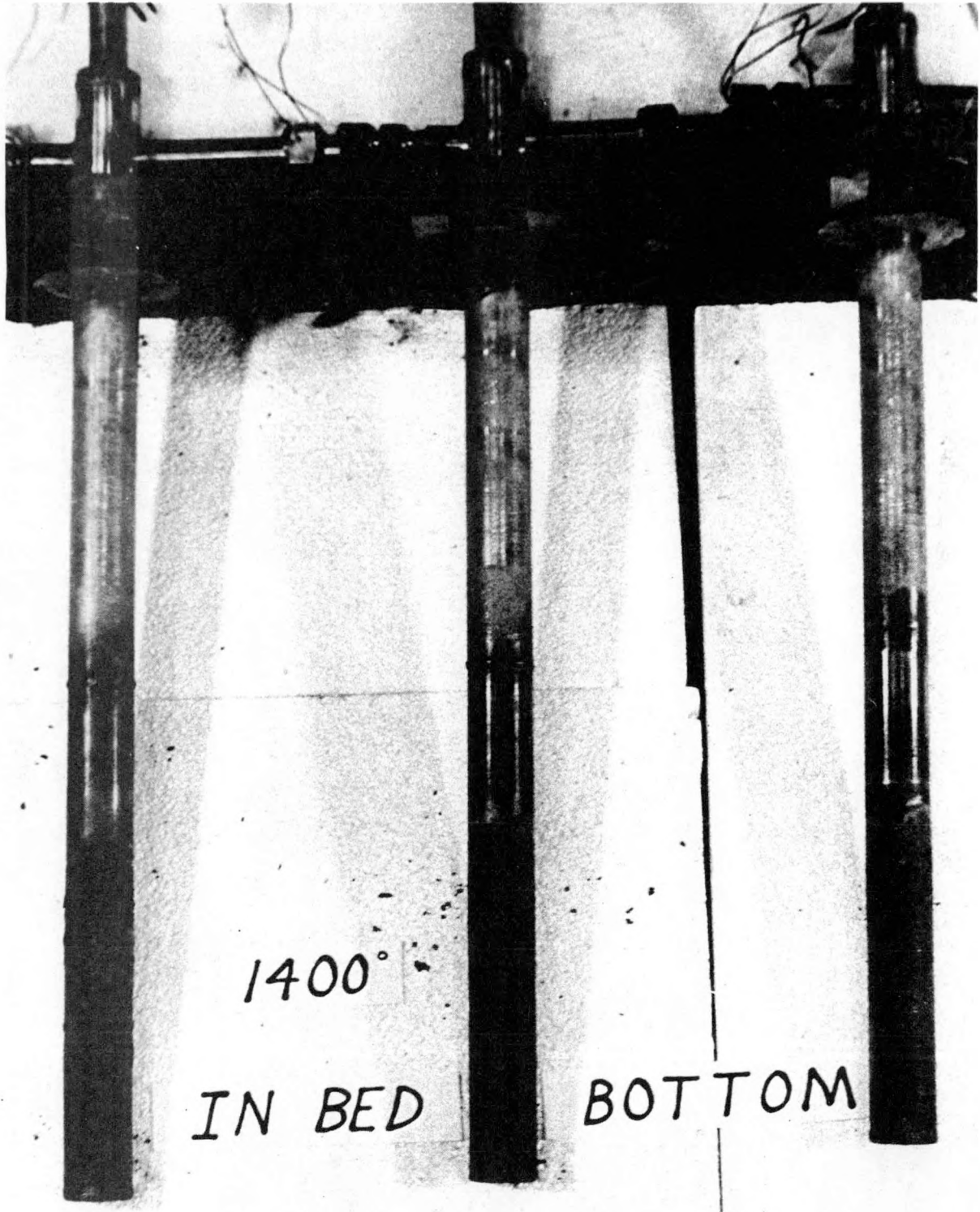


Figure A-15

1400°F Above Bed Probe (Top Side View)

After Shakedown

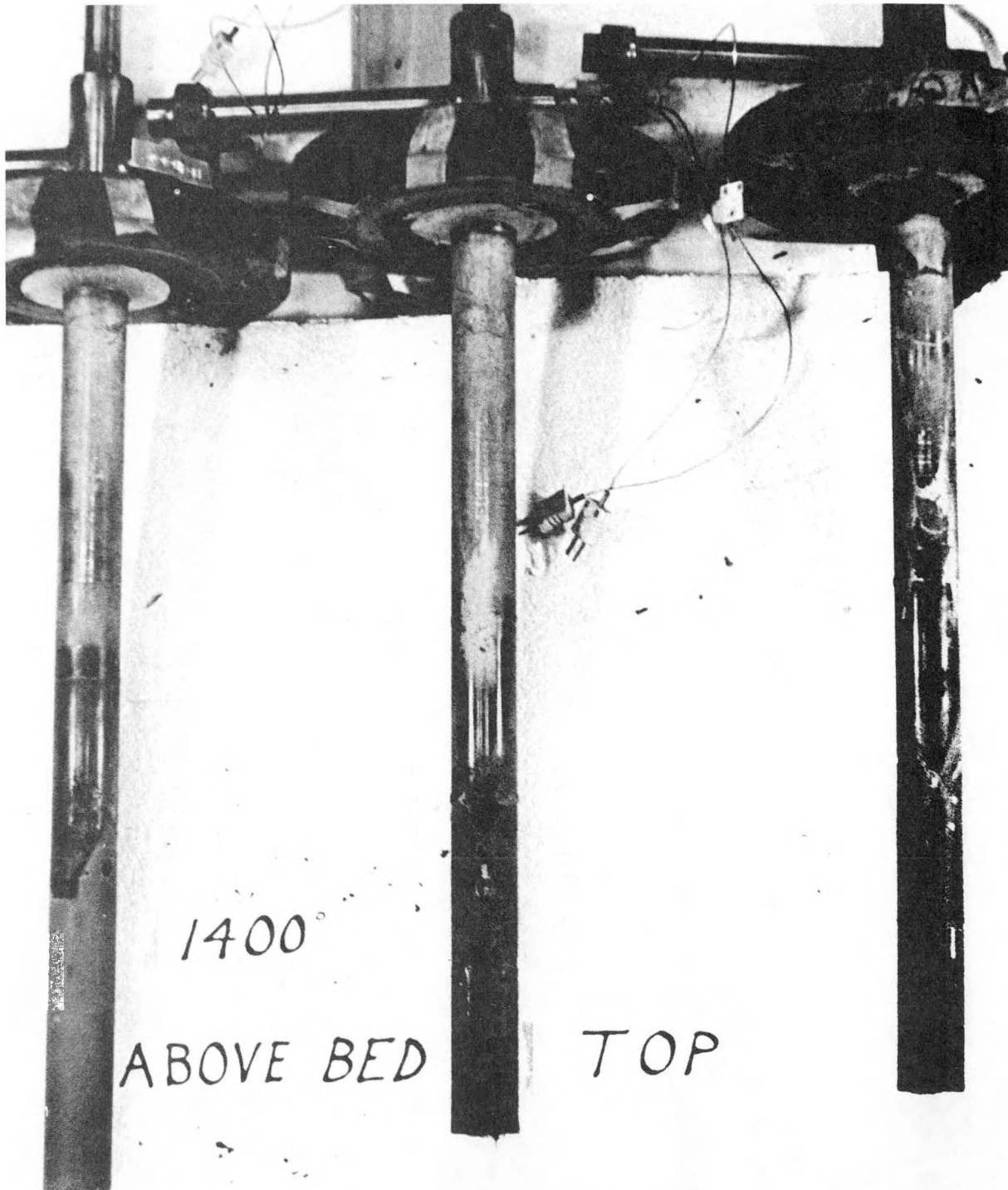


Figure A-16

1200°F In-Bed Probe (Bottom Side View)

After Shakedown

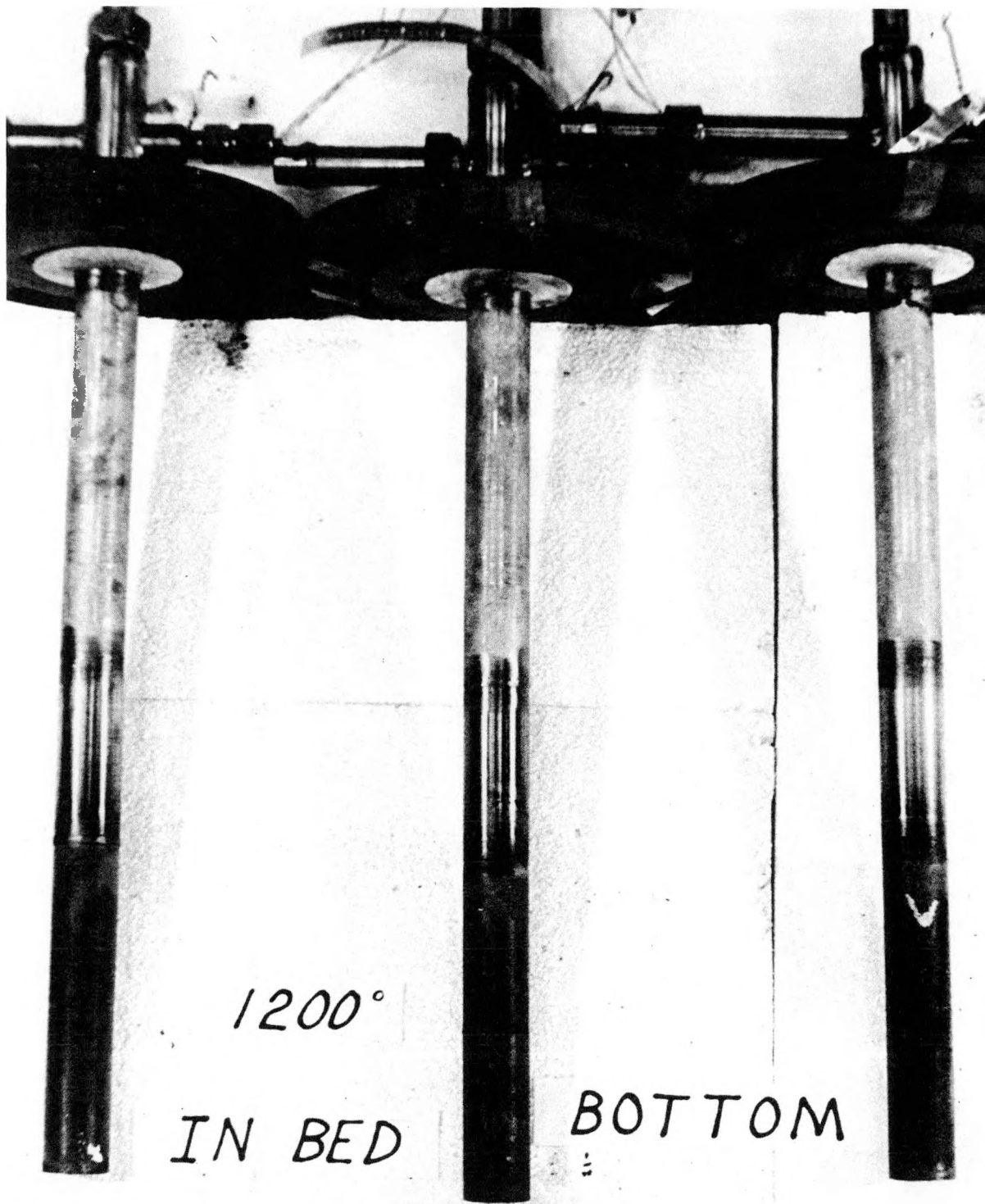


Figure A-17

1200°F Above-Bed Probe (Bottom Side View)

After Shakedown

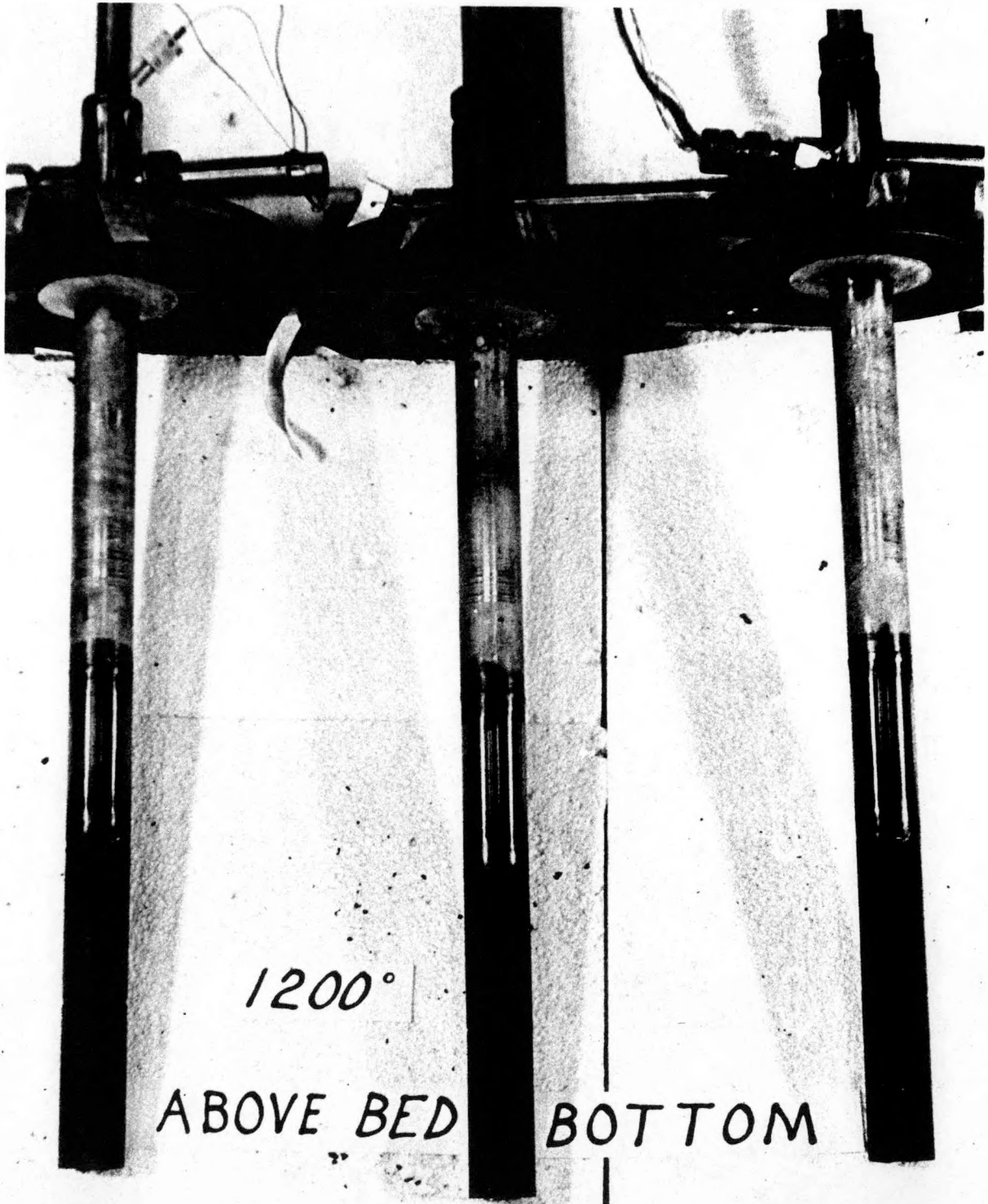


Figure A-18

1050°F In-Bed Probe (Bottom Side View)

After Shakedown

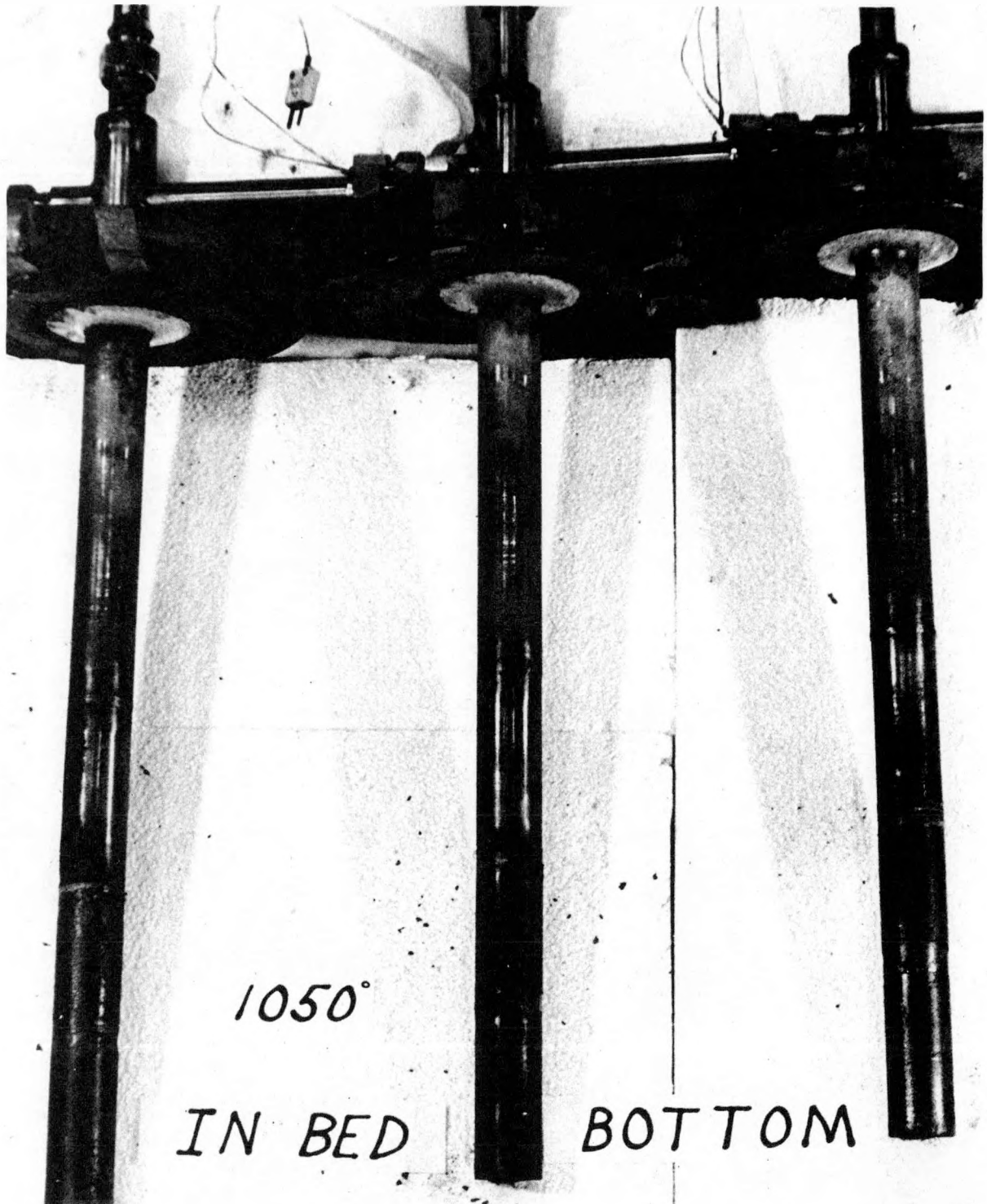


Table A-1

Heat Exchanger Probes Temperature History (Shakedown)

Control Temperature: 1600°F		1400°F												1200°F						1050°F																					
Combusitor Location:		In Bed				Above Bed				In Bed				Above Bed				In Bed			Above Bed			In Bed																	
Port Number	Specimen	1	3	5	13	15	17	2	4	6	14	16	18	7	9	11	19	20	22	8	10	12																			
Hours Into Run	X	H	H	X	H	X	X	H	X	H	X	H	X	X	H	X	H	X	H	X	H	X	X	H	X	H	X	H	X	H	X	H	X	H	X	H	X	H	X	H	X
5 Hour																																									
Avg. Temp. °F	1541	1575	1510	1568	1528	1575	1588	1543	1585	1531	1578	1518	1247	1383	1183	1386	1211	1353	1330	1368	1290	1413	1238	1436	1029	1162	1119	1057	1068	1138	954	1211	906	1233	855	1199	963	903	952	708	1045
Std. Dev.	54	44	58	39	55	32	12	13	13	13	14	12	22	15	21	22	20	59	35	22	14	8	39	29	38	42	75	81	73	49	18	21	49	24	28	26	11	18	7	13	14
Hi Temp. °F	1597	1609	1579	1598	1588	1601	1607	1560	1606	1552	1598	1538	1275	1405	1217	1393	1245	1410	1385	1395	1315	1428	1290	1473	1096	1225	1226	1165	1168	1205	978	1238	971	1263	945	1258	981	941	938	737	1075
Lo Temp. °F	1430	1496	1407	1502	1433	1522	1556	1508	1562	1499	1541	1499	1195	1353	1133	1326	1161	1241	1291	1340	1268	1402	1191	1395	966	1078	1010	956	986	1058	931	1179	849	1194	817	1147	927	848	965	680	1031
10 Hour																																									
Avg. Temp. °F	1581	1605	1551	1591	1574	1593	1576	1522	1569	1511	1561	1494	1269	1397	1194	1385	1229	1384	1368	1381	1294	1401	1195	1396	1086	1192	1195	1131	1162	1187	951	1164	853	1181	876	1112	1002	911	951	720	1032
Std. Dev.	11	3	16	5	13	3	11	10	10	10	10	10	12	5	19	5	19	14	11	4	11	4	4	6	14	28	15	13	19	8	8	7	7	6	6	11	22	34	7	11	5
Hi Temp. °F	1605	1613	1590	1607	1600	1599	1601	1547	1593	1536	1584	1518	1289	1407	1225	1395	1283	1407	1386	1383	1314	1407	1206	1409	1107	1229	1221	1159	1199	1201	970	1181	867	1197	886	1146	1090	996	970	745	1039
Lo Temp. °F	1565	1594	1519	1583	1551	1588	1555	1505	1550	1496	1543	1478	1253	1387	1154	1378	1193	1366	1345	1375	1272	1395	1188	1384	1057	1149	1163	1114	1123	1175	943	1151	840	1174	858	1100	979	872	942	697	1023
15 Hour																																									
Avg. Temp. °F	1588	1604	1557	1589	1576	1591	1573	1518	1566	1506	1558	1489	1274	1398	1198	1385	1235	1377	1367	1371	1298	1396	1193	1387	1092	1167	1200	1133	1163	1187	967	1151	859	1178	876	1105	999	896	953	726	1031
Std. Dev.	11	4	19	4	12	3	8	7	8	7	7	6	11	6	16	5	18	5	13	2	10	3	4	3	15	9	18	9	20	8	7	3	4	2	4	4	12	12	6	15	6
Hi Temp. °F	1607	1610	1599	1596	1606	1596	1590	1533	1582	1523	1573	1503	1301	1407	1227	1395	1288	1388	1384	1374	1313	1401	1203	1393	1120	1182	1219	1151	1202	1202	978	1156	865	1181	884	1119	1024	921	966	758	1043
Lo Temp. °F	1560	1587	1528	1576	1549	1587	1558	1505	1552	1494	1544	1477	1260	1387	1171	1375	1211	1367	1351	1366	1283	1392	1188	1381	1056	1150	1165	1120	1133	1173	955	1145	852	1173	869	1099	985	868	940	698	1020
20 Hour																																									
Avg. Temp. °F	1589	1597	1565	1591	1579	1590	1579	1528	1571	1515	1563	1497	1273	1398	1200	1385	1230	1377	1359	1385	1286	1395	1193	1387	1097	1172	1192	1138	1173	1190	959	1150	859	1178	878	1113	996	889	952	726	1032
Std. Dev.	9	3	15	3	10	3	7	7	7	7	7	6	10	6	15	17	17	4	12	9	10	2	4	3	11	10	15	9	16	8	7	3	6	4	19	5	14	11	7	11	7
Hi Temp. °F	1602	1601	1598	1598	1604	1594	1597	1541	1589	1528	1580	1510	1292	1409	1229	1395	1258	1383	1376	1400	1304	1401	1201	1391	1114	1192	1219	1154	1197	1208	976	1155	870	1181	975	1130	1024	907	969	742	1048
Lo Temp. °F	1573	1590	1536	1586	1560	1584	1565	1512	1557	1500	1550	1483	1254	1389	1174	1378	1205	1371	1351	1373	1270	1392	1183	1382	1079	1157	1156	1122	1144	1174	947	1144	849	1167	869	1105	976	862	941	697	1017
25 Hour																																									
Avg. Temp. °F	1588	1597	1555	1589	1578	1590	1585	1540	1577	1527	1568	1509	1272	1399	1206	1388	1238	1375	1357	1401	1278	1395	1194	1381	1095	1190	1204	1148	1171	1188	969	1169	880	1179	904	1135	988	874	954	726	1031
Std. Dev.	7	2	13	3	10	3	6	6	6	6	6	7	9	5	12	5	13	5	8	3	11	3	4	4	13	10	16	13	15	7	24	18	18	13	34	26	17	12	7	11	6
Hi Temp. °F	1598	1600	1576	1595	1592	1598	1598	1554	1590	1541	1581	1523	1286	1409	1226	1396	1259	1384	1370	1407	1195	1400	1201	1390	1117	1213	1233	1172	1195	1202	1014	1203	913	1204	968	1186	1022	900	966	742	1043
Lo Temp. °F	1576	1591	1529	1584	1552	1584	1575	1529	1567	1514	1558	1496	1256	1388	1188	1378	1207	1364	1341	1395	1250	1389	1188	1373	1066	1172	1168	1120	1139	1174	946	1147	864	1166	872	1112	960	855	940	697	1020
30 Hour																																									
Avg. Temp. °F	1587	1592	1561	1588	1583	1593	1568	1558	1577	1550	1565	1533	1272	1392	1201	1390	1250	1382	1341	1391	1235	1409	1198	1397	1085	1174	1179	1128	1143	1169	1000	1213	913	1215	967	1221	985	886	951	732	1028
Std. Dev.	10	8	19	4	18	6	45	25	11	31	17	34	17	12	29	5	24	10	31	22	37	17	15	21	30	58	43	53	67	45	17	36	13	30	20	59	20	21	13	27	19
Hi Temp. °F	1604	1600	1595	1594	1615	1601	1598	1606	1590	1610	1581	1603	1292	1406	1240	1396	1279	1402	1366	1411	1284	1446	1214	1439	1119	1223	1232	1169	1198	1210	1026	1299	950	1283	982	1344	1041	940	972	789	1055
Lo Temp. °F	1576	1578	1522	1583	1554	1582	1443	1535	1547	1524	1523	1506	1228	1357	1147	1378	1207	1366	1274	1352	1160	1392	1166	1376	1033	1050	1103	1023	1016	1086	954	1190	898	1195	923	1186	958	860	929	682	994
36 Hour																																									
Avg. Temp. °F	1583	1590	1543	1590	1564	1593	1528	1604	1578	1605	1549	1603	1189	1371	1162	1384	1235	1380	1303	1364	1197	1437	1164	1425	1042	1094	1149	1049	1049	1107	1075	1321	997	1312	1013	1371	990	829	934	688	1054
Std. Dev.	5	5	15	4	13	8	20	4	13	7	17	8	29	27	14	6	10	3	13	11	16	9	15	5	11	48	21	37	23	18	67	53	57	44	50	42	18	39	14	10	14
Hi Temp. °F	1593	1597	1565	1596	1582	1604	1564	1613	1599	1618	1577	1613	1235	1409	1186	1395	1260	1384	1327	1389	1221	1454	1190	1432	1074	1168	1183	1110	1076	1138	1173	1391	1084	1367	1093	1428	1033	906	956	709	1072
Lo Temp. °F	1576	1583	1521	1581	1546	1574	1505	1597	1555	1592	1518	1586	1136	1330	1144	1376	1224	1374	1279	1351	1164	1422	1143	1417	1031	1002	1116	994	1010	1080	957	1228	906	1237	948	1295	963	781	913	673	1030
40 Hour																																									
Avg. Temp. °F	1585	1599	1546	1595	1573	1603	1581	1595	1607	1589	1585	1578	1124	1339	1194	1396	1245	1383	1335	1406	1237	1416	1204	1398	1079	1192	1154	1105	1089	1144	972	1236	910	1227	933	1252	1003	872	957	714	1033
Std. Dev.	7	2	13	3	8	2	16	3	6	6	6	4	96	63	24	6	10	4	4	8	6	3	7	10	12	18	13	12	17	7	7	6	6	19	24	14	10	7	8	5	
Hi Temp. °F	1595	1603	1566	1600	1586	1608	1604	1598	1619	1597	1597	1585	1273	1418	1394	1405	1259	1389	1344	1416	1247	1422	1219	1418	1103	1226	1178	1125	1112	1158	982	1245	918	1236	963	1283	1026	888	969	726	1040
Lo Temp. °F	1575	1596	1520	1590	1559	1599	1543	1587	1599	1576	1576	1571	1013	1254	1166	1383	1232	1375	1330	1394	1229	1411	1196	1387	1064	1167	1135	1084	1060	1135	957	1225	899	1219	911	1221	973	851	946	700	1023

Table A-1 (Cont'd)

Heat Exchanger Probes Temperature History (Shakedown)

Control Temperature: 1600°F		1400°F												1200°F						1050°F																						
Combusator Location:		In Bed			Above Bed						In Bed			Above Bed			In Bed			Above Bed			In Bed																			
Port Number	Specimen	1	3	5	13	15	17	2	4	6	14	16	18	7	9	11	19	20	22	8	10	12																				
Hours Into Run		X	H	H	X	H	X	X	H	X	X	H	X	X	H	X	X	H	X	X	H	X																				
45 Hour	Avg. Temp. °F	1587	1599	1545	1596	1575	1604	1580	1597	1606	1592	1586	1580	1101	1330	1195	1392	1233	1381	1336	1417	1234	1417	1199	1386	1077	1194	1162	1111	1100	1147	972	1218	905	1219	909	1225	989	852	957	714	1033
	Std. Dev.	8	1	11	2	8	3	22	3	5	5	6	5	13	12	20	7	8	5	3	6	8	5	4	2	8	18	24	14	23	21	7	15	6	4	14	12	18	11	6	6	5
	Hi Temp. °F	1599	1602	1566	1599	1587	1610	1602	1601	1615	1598	1597	1586	1124	1346	1232	1407	1246	1391	1340	1429	1249	1423	1210	1392	1089	1218	1193	1132	1144	1182	985	1244	914	1226	924	1246	1018	870	968	725	1045
	Lo Temp. °F	1566	1597	1523	1590	1563	1600	1539	1591	1597	1581	1577	1568	1082	1304	1160	1382	1221	1373	1329	1408	1218	1407	1192	1382	1066	1149	1127	1092	1068	1134	961	1193	892	1214	883	1210	958	829	949	699	1026
50 Hour	Avg. Temp. °F	1580	1600	1542	1597	1573	1605	1569	1597	1607	1594	1598	1582	1195	1391	1203	1395	1254	1391	1330	1415	1232	1418	1207	1392	1122	1211	1204	1148	1173	1209	969	1208	909	1223	890	1216	1014	874	991	717	1030
	Std. Dev.	7	2	12	3	8	2	22	3	6	4	7	5	118	114	17	9	16	7	7	5	8	4	6	4	35	25	21	17	34	22	4	4	5	5	6	12	17	14	24	11	4
	Hi Temp. °F	1593	1603	1565	1603	1585	1608	1599	1602	1620	1600	1613	1590	1248	1435	1223	1408	1282	1400	1341	1425	1245	1425	1216	1400	1157	1245	1237	1167	1221	1234	977	1214	916	1230	899	1233	1040	892	1015	742	1036
	Lo Temp. °F	1570	1596	1520	1593	1558	1601	1523	1592	1598	1588	1586	1574	785	996	1173	1379	1223	1377	1322	1404	1218	1412	1193	1386	1051	1150	1157	1112	1101	1156	963	1202	899	1215	882	1197	978	851	945	704	1022
55 Hour	Avg. Temp. °F	1582	1600	1543	1596	1572	1604	1571	1597	1607	1592	1592	1579	1228	1419	1208	1398	1266	1396	1326	1416	1229	1420	1197	1391	1136	1229	1213	1152	1189	1223	975	1186	913	1226	890	1225	1026	895	1006	720	1032
	Std. Dev.	6	2	15	2	10	2	27	4	9	8	25	9	5	5	15	3	14	6	5	4	10	4	7	3	12	12	17	11	20	7	8	13	8	5	11	14	17	12	7	12	5
	Hi Temp. °F	1594	1603	1567	1601	1586	1608	1609	1602	1622	1602	1615	1591	1239	1430	1234	1403	1296	1407	1331	1421	1244	1427	1213	1400	1159	1250	1232	1176	1222	1237	986	1217	923	1242	919	1257	1063	917	1015	740	1042
	Lo Temp. °F	1574	1597	1522	1593	1557	1601	1528	1586	1590	1572	1582	1557	1218	1480	1188	1390	1247	1389	1315	1407	1208	1415	1188	1386	1117	1199	1173	1138	1161	1214	956	1173	897	1219	875	1203	1002	872	991	694	1022
60 Hour	Avg. Temp. °F	1585	1598	1555	1598	1581	1603	1592	1581	1601	1569	1593	1555	1236	1413	1230	1401	1281	1395	1330	1413	1243	1412	1208	1386	1141	1238	1214	1165	1205	1226	986	1176	924	1218	895	1204	1019	909	1006	719	1026
	Std. Dev.	8	3	12	3	11	2	20	14	9	18	9	19	10	5	22	4	16	4	10	7	9	8	5	25	12	12	20	14	20	8	5	6	7	11	10	33	10	10	6	13	5
	Hi Temp. °F	1600	1601	1576	1603	1603	1607	1609	1599	1617	1595	1610	1583	1254	1420	1258	1407	1305	1400	1342	1424	1252	1426	1217	1397	1174	1255	1241	1187	1240	1239	995	1186	932	1244	916	1277	1063	924	1016	748	1036
	Lo Temp. °F	1574	1592	1535	1593	1568	1600	1544	1558	1586	1544	1577	1529	1226	1404	1181	1395	1258	1388	1322	1401	1229	1402	1193	1378	1119	1212	1186	1143	1172	1212	975	1168	909	1201	883	1174	1002	891	995	700	1018
65 Hour	Avg. Temp. °F	1593	1589	1567	1594	1593	1599	1579	1541	1572	1527	1563	1512	1245	1407	1243	1392	1289	1390	1341	1401	1256	1394	1223	1384	1161	1240	1213	1166	1219	1227	1000	1160	921	1202	897	1164	1026	912	1005	726	1019
	Std. Dev.	7	10	19	7	7	8	18	18	17	19	17	18	6	5	19	6	15	4	9	4	13	7	11	2	18	12	20	11	22	7	11	6	8	7	4	8	16	11	6	11	5
	Hi Temp. °F	1602	1597	1600	1603	1606	1605	1597	1563	1590	1547	1581	1532	1254	1417	1281	1403	1314	1396	1367	1407	1284	1403	1248	1387	1184	1255	1244	1183	1262	1238	1031	1172	933	1212	908	1175	1048	928	1015	741	1028
	Lo Temp. °F	1579	1556	1526	1571	1582	1574	1531	1493	1525	1478	1516	1465	1231	1399	1221	1382	1270	1382	1330	1394	1240	1379	1210	1380	1135	1221	1187	1147	1184	1215	988	1151	913	1186	891	1147	1000	893	992	703	1012
70 Hour	Avg. Temp. °F	1604	1576	1583	1583	1603	1588	1548	1505	1540	1487	1521	1475	1254	1407	1261	1392	1303	1388	1355	1395	1286	1381	1238	1385	1156	1243	1218	1175	1227	1220	1022	1140	924	1189	905	1145	1032	926	1008	729	1023
	Std. Dev.	6	7	9	6	7	4	8	8	8	9	8	8	8	4	22	5	25	5	10	3	11	4	6	2	16	11	19	9	20	10	9	6	4	4	4	6	20	11	7	12	6
	Hi Temp. °F	1614	1587	1597	1588	1611	1595	1558	1518	1551	1500	1542	1487	1270	1411	1297	1398	1344	1395	1381	1399	1299	1389	1247	1388	1180	1261	1242	1187	1263	1234	1038	1150	932	1198	916	1157	1060	939	1018	744	1035
	Lo Temp. °F	1593	1559	1564	1567	1586	1574	1531	1488	1524	1470	1516	1458	1243	1399	1221	1380	1269	1381	1342	1391	1255	1374	1230	1380	1122	1227	1191	1154	1193	1205	1003	1130	919	1183	901	1137	992	904	994	703	1016
75 Hour	Avg. Temp. °F	1607	1571	1580	1578	1605	1585	1540	1495	1533	1476	1524	1464	1255	1407	1258	1390	1303	1388	1364	1392	1295	1377	1239	1384	1145	1239	1221	1170	1209	1209	1034	1133	922	1183	911	1134	1023	922	1009	731	1024
	Std. Dev.	6	5	18	4	7	4	5	4	5	5	5	4	6	4	13	4	16	6	7	2	8	2	5	2	13	12	19	11	16	8	11	3	2	4	4	3	13	11	6	10	7
	Hi Temp. °F	1620	1581	1600	1585	1616	1590	1551	1503	1544	1485	1535	1473	1263	1415	1274	1397	1337	1399	1376	1397	1305	1379	1248	1387	1166	1255	1256	1186	1234	1220	1047	1139	927	1190	918	1142	1041	940	1021	751	1035
	Lo Temp. °F	1599	1564	1541	1574	1592	1579	1532	1487	1524	1467	1515	1456	1245	1400	1239	1384	1276	1378	1355	1387	1281	1374	1233	1380	1125	1215	1199	1155	1187	1199	1017	1128	919	1179	905	1131	986	897	999	716	1012
80 Hour	Avg. Temp. °F	1609	1568	1586	1575	1608	1582	1537	1494	1530	1475	1520	1463	1258	1407	1263	1391	1304	1389	1365	1394	1294	1377	1244	1382	1154	1242	1213	1169	1215	1211	1032	1135	916	1175	915	1141	1034	927	1014	731	1029
	Std. Dev.	7	6	15	6	6	7	6	6	6	6	6	6	4	4	13	3	18	3	6	3	7	2	7	3	13	9	18	8	17	6	13	3	11	9	5	4	17	14	7	9	7
	Hi Temp. °F	1621	1579	1604	1582	1617	1592	1543	1501	1536	1482	1526	1468	1268	1414	1284	1397	1334	1393	1399	1376	1312	1382	1253	1386	1176	1257	1242	1185	1239	1223	1053	1141	932	1184	922	1151	1058	942	1024	750	1040
	Lo Temp. °F	1595	1557	1555	1563	1592	1569	1524	1480	1518	1462	1509	1449	1232	1401</																											

Table A-1 (Cont'd)

Heat Exchanger Probes Temperature History (Shakedown)

Control Temperature: 1600°F		1400°F												1200°F						1050°F																															
Combusitor Location:		In Bed				Above Bed				In Bed				Above Bed				In Bed			Above Bed			In Bed																											
Port Number	Specimen	1	3	5	13	15	17	2	4	6	14	16	18	7	9	11	19	20	22	8	10	12																													
Hours Into Run		X	M	N	X	N	X	X	N	X	X	N	X	N	X	X	N	X	N	X	N	X																													
85 Hour																																																			
Avg. Temp. °F		1608	1568	1588	1573	1604	1580	1534	1489	1527	1470	1518	1457	1256	1406	1265	1389	1302	1309	1367	1392	1301	1376	1242	1381	1150	1239	1216	1174	1227	1215	1038	1134	902	1164	921	1135	1037	928	1014				731	1025						
Std. Dev.		8	7	12	6	6	6	4	8	4	5	4	4	4	4	15	3	13	5	6	3	8	2	5	2	13	11	18	8	21	11	9	3	7	6	3	10	17	13	7				8	5						
Hi Temp. °F		1622	1578	1600	1582	1615	1589	1545	1502	1538	1483	1528	1468	1261	1414	1284	1399	1328	1395	1375	1396	1311	1380	1249	1384	1173	1252	1248	1190	1248	1229	1083	1140	913	1175	926	1153	1059	945	1029				740	1033						
Lo Temp. °F		1592	1554	1561	1561	1593	1569	1528	1483	1522	1463	1513	1452	1249	1402	1239	1384	1286	1381	1355	1388	1284	1373	1231	1378	1129	1222	1192	1163	1189	1195	1023	1130	890	1155	915	1131	1005	896	1002				712	1015						
90 Hour																																																			
Avg. Temp. °F		1607	1564	1592	1571	1605	1578	1533	1492	1527	1474	1517	1461	1257	1406	1259	1390	1305	1390	1367	1397	1297	1377	1243	1382	1152	1240	1218	1173	1209	1214	1037	1139	902	1165	919	1150	1025	930	1018				734	1029						
Std. Dev.		6	5	15	4	6	6	6	5	6	5	5	5	5	4	14	5	16	5	6	3	9	2	10	3	17	7	12	10	17	8	11	4	9	7	5	5	12	9	4				15	5						
Hi Temp. °F		1620	1571	1604	1576	1614	1587	1544	1500	1536	1481	1526	1469	1267	1396	1283	1403	1328	1398	1377	1402	1315	1381	1253	1386	1174	1249	1239	1193	1246	1228	1059	1149	917	1174	929	1158	1044	949	1026				759	1040						
Lo Temp. °F		1596	1554	1552	1560	1592	1565	1524	1483	1518	1466	1508	1453	1246	1412	1230	1382	1280	1381	1358	1392	1281	1374	1234	1378	1121	1222	1195	1161	1187	1202	1020	1134	881	1150	910	1141	1004	916	1011				699	1019						
95 Hour																																																			
Avg. Temp. °F		1607	1563	1588	1568	1606	1578	1529	1488	1522	1469	1512	1457	1258	1407	1263	1393	1305	1391	1371	1399	1298	1377	1250	1382	1151	1240	1226	1169	1222	1220	1035	1141	881	1150	923	1147	1025	931	1019				728	1033						
Std. Dev.		9	8	18	6	8	6	4	4	4	4	4	4	7	3	16	4	16	6	5	2	8	2	5	2	4	7	16	7	17	7	10	4	12	9	5	5	13	7	5				14	8						
Hi Temp. °F		1627	1576	1608	1576	1619	1588	1534	1494	1527	1475	1518	1463	1270	1413	1285	1400	1336	1401	1379	1405	1311	1382	1257	1386	1171	1253	1248	1182	1244	1230	1052	1146	903	1166	929	1153	1051	940	1031				747	1050						
Lo Temp. °F		1594	1549	1543	1559	1589	1568	1522	1481	1515	1463	1506	1451	1243	1403	1234	1384	1286	1380	1356	1396	1282	1373	1240	1377	1128	1228	1206	1159	1192	1211	1020	1132	862	1137	912	1140	1005	915	1012				704	1015						
100 Hour																																																			
Avg. Temp. °F		1604	1559	1596	1565	1604	1571	1522	1480	1516	1462	1507	1449	1262	1408	1259	1388	1305	1388	1373	1396	1298	1375	1253	1382	1157	1240	1219	1168	1215	1216	1040	1142	863	1132	921	1147	1026	928	1016				738	1035						
Std. Dev.		6	6	7	5	4	5	7	6	7	5	7	5	13	7	17	4	15	3	6	1	6	2	5	2	11	7	18	9	18	8	12	3	8	10	7	5	18	11	4				11	5						
Hi Temp. °F		1614	1568	1605	1571	1610	1577	1530	1486	1526	1469	1516	1454	1285	1421	1280	1397	1325	1395	1385	1398	1307	1379	1264	1386	1179	1252	1250	1180	1244	1225	1061	1146	882	1144	933	1155	1049	952	1023				755	1042						
Lo Temp. °F		1596	1548	1582	1556	1598	1557	1507	1467	1501	1450	1492	1438	1243	1391	1231	1380	1276	1385	1365	1394	1287	1373	1247	1380	1143	1228	1186	1150	1195	1195	1025	1138	854	1124	912	1136	996	911	1008				714	1028						

APPENDIX B
PARTICULATE CAPTURE DATA

Table B-1
Second Cyclone Capture
Size Distribution

<u>Run/Dump No.</u>	<u>Vol. % Finer Than</u>						
	<u>5%</u>	<u>10%</u>	<u>25%</u>	<u>50%</u>	<u>75%</u>	<u>90%</u>	<u>95%</u>
79 130	4.4	6.0	9.6	15.5	32.5	68.0	94.0
79 18	7.4	10.0	15.0	28.0	55.0	92.0	120.2
80 64	5.9	8.1	13.0	24.0	47.0	92.0	120.0
81 15	5.8	8.0	14.5	33.0	92.0	--	--
81 74	5.4	8.0	15.0	36.0	100.0	--	--
106.1 2	5.0	6.6	10.5	18.0	38.0	83.0	140.0
106.1 11	7.0	14.0	34.0	84.0	165.0	310.0	430.0
106.2 23	4.2	6.0	11.5	23.0	52.0	105.0	160.0
106.3 57	4.8	6.4	11.5	23.0	52.0	105.0	160.0

Table B-2

Third Cyclone Captured Material
Size Distribution

<u>Run/Sample</u>		<u>Vol. % Finer Than</u>						
		<u>5%</u>	<u>10%</u>	<u>25%</u>	<u>50%</u>	<u>75%</u>	<u>90%</u>	<u>95%</u>
78	31	1.4	1.75	2.5	3.55	5.2	8.4	11.0
78	52	1.8	2.3	3.5	5.1	7.6	10.0	12.5
78	85	2.1	2.5	3.4	4.8	6.6	8.8	10.0
78	120	1.65	2.2	3.1	4.5	6.6	10.0	13.0
79	1	1.75	2.15	2.7	3.4	4.5	8.0	11.8
79	18	1.6	2.1	2.9	4.4	6.4	9.6	10.25
79	42	2.4	2.9	4.2	5.9	8.9	12.5	16.0
79	50	2.2	2.9	4.3	6.1	8.8	11.5	12.0
80	64	1.35	1.70	2.5	3.90	6.0	8.6	9.8
81	15	1.2	1.4	1.95	3.35	6.20	10.0	12.7
81	74	1.8	2.2	3.1	4.80	7.80	12.0	14.3

Table B-3

Flue Gas Particulates Entering Turbine Test
Section (Exiting 3rd Cyclone) Size Distribution and Concentration

Run/Sample	Particulate Concentration (gr/SCF)	Vol. % Finer Than							
		5%	10%	25%	50%	75%	90%	95%	
78BB 2	0.033	0.48	0.56	0.74	1.0	1.4	5.0	8.7	
78BA 3	0.034	0.60	0.75	1.10	2.0	4.8	8.5	9.8	
78BA 4	0.028	0.62	0.78	1.10	3.1	5.8	10.8	12.5	
78BB 5	0.039	0.46	0.54	0.74	1.1	2.9	6.1	8.4	
78BA 6	N/A	0.48	0.55	0.79	2.1	5.9	12.0	14.0	
78BA 7	0.042	0.48	0.58	0.74	1.0	1.5	3.1	5.0	
78BA 8	0.056	0.79	1.0	1.49	2.5	5.5	9.2	11.5	
78BA 9	0.045	0.74	0.97	1.47	2.5	5.7	9.6	11.5	
78BA 10	0.056	0.60	0.76	1.3	3.0	5.7	8.8	11.0	
78BA 11	0.054	0.79	1.1	1.75	2.5	3.7	5.7	8.0	
Avg. of Test 2-11		0.58	0.66	0.98	1.9	4.6	8.5	11.0	
79BA 1	0.012	0.54	0.68	1.0	1.8	3.7	6.4	8.8	
79BA 2	0.009	0.47	0.53	0.69	1.0	2.4	8.8	13.5	
79BA 3	0.034	0.47	0.56	0.75	1.1	1.8	2.2	8.0	
80BB 1	0.014	0.52	0.60	0.69	0.9	1.2	1.8	2.3	
80BA 2	0.023	0.55	0.61	0.76	1.0	1.9	6.0	9.0	
80BA 3	0.026	0.54	0.61	0.78	1.1	2.0	4.9	9.0	
80BB 4	0.021	0.53	0.59	0.70	0.9	1.3	1.8	2.5	
80BA 5	0.023	0.56	0.64	0.91	1.3	2.0	3.4	4.9	
80BB 6	0.021	0.46	0.53	0.70	1.0	1.4	2.2	5.0	
80BA 7	0.028	0.58	0.71	1.05	1.5	2.4	4.5	6.4	
80BB 8	0.015	0.47	0.54	0.73	1.1	1.6	2.5	4.0	
80BA 9	0.024	0.96	1.18	1.45	1.9	2.9	4.7	6.0	
80BB 10	0.023	0.47	0.56	0.76	1.1	1.6	2.5	5.0	

Table B-3 (Cont'd)

Flue Gas Particulates Entering Turbine Test
Section (Exiting 3rd Cyclone) Size Distribution and Concentration

<u>Run/Sample</u>		<u>Particulate Concentration (gr/SCF)</u>	<u>Vol. % Finer Than</u>						
			<u>5%</u>	<u>10%</u>	<u>25%</u>	<u>50%</u>	<u>75%</u>	<u>90%</u>	<u>95%</u>
81BA	4	0.063	0.50	0.60	0.79	1.2	2.8	7.5	11.5
81BA	10	0.031	0.56	0.60	0.76	1.1	1.7	6.35	13.0
81BB	11	0.037	0.63	0.80	1.2	1.7	3.4	6.0	8.0
81BA	13	0.037	0.56	0.62	0.77	1.25	3.2	9.0	14.0
81BA	16	0.039	0.58	0.70	1.0	1.45	3.1	9.4	16.0
81BB	18	0.021	0.52	0.59	0.72	1.6	5.8	11.5	16.0
81BB	20	0.018	0.58	0.63	0.80	1.25	2.9	5.8	8.0
106BA	1	0.083	0.79	1.05	1.45	2.1	3.3	5.6	7.4
106BA	3	0.029	0.74	0.93	1.25	1.7	2.4	4.6	7.0
106BA	5	0.049	0.64	0.84	1.15	1.7	2.8	5.0	8.0
106BA	6	0.037	0.79	1.05	1.45	2.0	2.8	4.0	5.0
106BA	7	0.460	1.10	1.40	2.20	3.5	5.6	7.8	9.8
106BA	8	0.048	1.70	2.20	3.10	4.9	6.9	9.2	10.0
106BA	9	0.094	0.79	1.15	1.65	3.1	4.5	6.3	8.0
106BA	13	0.089	0.79	1.10	1.70	2.8	4.3	6.3	9.2
106BA	17	0.055	0.56	0.62	0.80	1.2	2.4	4.9	8.0
106BA	20	0.063	0.64	0.79	1.20	1.7	2.7	4.9	7.2
106BA	24	0.054	0.56	0.65	0.90	1.3	2.7	5.5	8.0
106BA	28	0.047	0.58	0.65	0.85	1.2	1.9	4.6	8.0
106BA	32	0.043	0.59	0.68	0.90	1.3	2.1	4.6	7.0
106BA	34	0.043	0.60	0.70	1.00	1.4	2.1	3.8	6.35

N/A = Data Not Available

APPENDIX C

HEAT EXCHANGER PROBE HISTORY

Enclosed is temperature history data for the heat exchanger probes for runs 78 thru 81 and run 106. Also, included are photographs of the probes after 1117 hours and 682 hours of operation.

Table C-1

Heat Exchanger Probes Temperature History (Run 78)

Control Temperature: 1600°F

		1400°F												1200°F						1050°F																				
Combusitor Location:		In Bed				Above Bed				In Bed				Above Bed				In Bed			Above Bed			In Bed																
Port Number	Specimen	1	3	5	13	15	17	2	4	6	14	16	18	7	9	11	19	20	22	8	12	10																		
Route Into Run		X	H	H	X	H	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X																		
5 Hour																																								
Avg. Temp. °F		1584	1555	1476	1531	1540	1575	1577	1593	1573	1589	1563	1159	1373	1142	1300	1185	1186	1383	1302	1337	1357	1291	1333	1034	1160	1043	1046	997	1089	1166	1168	1100	1283	724	1295	628	745	687	687
Std. Dev.		2	7	13	4	4	10	2	2	3	3	4	66	56	101	45	67	66	55	54	83	38	57	53	7	19	12	12	51	14	34	33	116	75	156	76	25	55	8	7
Hi Temp. °F		1587	1561	1487	1536	1545	1583	1576	1595	1578	1594	1569	1205	1410	1235	1337	1265	1240	1465	1355	1442	1394	1343	1379	1043	1171	1063	1060	1077	1104	1226	1227	1224	1365	893	1366	665	835	698	696
Lo Temp. °F		1581	1544	1454	1526	1535	1563	1580	1590	1572	1587	1560	1045	1274	975	1221	1079	1071	1304	1215	1214	1300	1200	1254	1023	1139	1032	1026	937	1073	1146	1147	911	1162	586	1168	597	698	676	678
10 Hour																																								
Avg. Temp. °F		1584	1555	1518	1570	1573	1595	1573	1590	1565	1588	1557	1226	1401	1289	1376	1342	1337	1304	1404	1297	1440	1283	1425	1036	1180	1060	1064	957	1120	1124	1124	972	972	542	542	802	889	836	835
Std. Dev.		4.51	5	17	6	3	12	17	11	19	17	21	11	4	18	4	46	48	5	4	15	11	11	4	12	15	11	6	12	31	14	15	23	23	8	8	88	90	57	60
Hi Temp. °F		1592	1563	1547	1576	1579	1613	1598	1613	1593	1613	1587	1244	1406	1333	1387	1393	1396	1318	1410	1318	1452	1299	1461	1055	1194	1072	1071	966	1148	1134	1133	1008	1006	550	550	893	978	887	889
Lo Temp. °F		1579	1551	1451	1531	1537	1581	1564	1576	1546	1570	1534	1218	1395	1266	1371	1274	1278	1297	1395	1281	1426	1264	1402	1023	1162	1046	1056	938	1066	1099	1097	942	942	530	530	672	762	768	764
15 Hour																																								
Avg. Temp. °F		1581	1552	1517	1568	1571	1591	1565	1587	1557	1581	1549	1230	1399	1302	1376	1378	1371	1308	1401	1305	1432	1292	1418	1029	1177	1054	1070	963	1125	1140	1140	929	929	541	541	821	925	886	887
Std. Dev.		4	2	14	3	2	8	6	7	6	6	6	11	2	17	6	18	17	2	8	14	3	8	4	11	13	8	6	10	9	7	7	27	27	4	5	28	35	5	7
Hi Temp. °F		1586	1561	1549	1575	1574	1612	1585	1608	1576	1602	1572	1240	1404	1324	1386	1407	1402	1311	1405	1324	1436	1309	1430	1046	1188	1063	1077	972	1133	1151	1151	958	960	546	547	866	984	895	897
Lo Temp. °F		1576	1549	1499	1561	1566	1584	1561	1579	1548	1572	1537	1215	1391	1280	1368	1364	1358	1302	1388	1281	1420	1284	1413	1020	1155	1044	1063	952	1109	1133	1134	886	886	536	535	800	895	881	878
20 Hour																																								
Avg. Temp. °F		1522	1515	1495	1512	1522	1539	1511	1538	1504	1532	1500	1256	1389	1312	1368	1382	1380	1309	1375	1303	1400	1290	1381	1062	1186	1063	1065	978	1115	1171	1171	870	869	577	577	831	958	913	913
Std. Dev.		130	97	82	122	113	130	136	131	133	129	131	64	22	44	15	10	8	2	6	12	70	9	77	46	11	23	12	54	9	74	74	140	137	45	45	50	47	36	36
Hi Temp. °F		1587	1567	1549	1576	1574	1610	1588	1615	1589	1618	1582	1370	1412	1377	1389	1410	1407	1311	1408	1308	1446	1308	1423	1138	1202	1098	1081	1074	1124	1302	1303	950	950	656	656	919	1025	976	977
Lo Temp. °F		972	946	954	978	967	1153	1163	1158	1161	1165	1164	940	955	940	953	946	946	1138	1148	1151	1142	1149	1145	1019	1175	1042	1050	951	1104	1129	1128	626	626	552	551	802	920	891	892
25 Hour																																								
Avg. Temp. °F		1585	1552	1513	1563	1574	1607	1590	1613	1584	1608	1574	1213	1403	1267	1360	1358	1358	1303	1392	1274	1438	1294	1411	1027	1143	1052	1022	937	1087	1131	1130	965	965	551	551	790	924	892	895
Std. Dev.		2	5	11	2	1	12	3	4	5	5	4	7	2	20	7	9	11	2	4	18	2	2	2	16	23	21	12	8	7	8	8	14	15	3	3	41	34	15	15
Hi Temp. °F		1590	1559	1542	1566	1577	1616	1595	1618	1592	1618	1583	1221	1406	1295	1368	1369	1376	1306	1397	1297	1441	1295	1414	1050	1164	1077	1041	945	1095	1140	1140	988	989	555	555	861	982	908	914
Lo Temp. °F		1583	1540	1495	1559	1511	1582	1573	1605	1577	1602	1569	1203	1393	1247	1351	1348	1346	1301	1387	1254	1435	1291	1410	1010	1107	1034	1011	927	1080	1122	1122	951	950	546	546	759	893	874	876
30 Hour																																								
Avg. Temp. °F		1579	1553	1510	1557	1571	1586	1587	1595	1581	1593	1573	1199	1396	1274	1354	1363	1365	1295	1382	1262	1437	1289	1411	1027	1120	1057	1020	933	1071	1109	1108	964	963	543	543	748	913	909	908
Std. Dev.		6	4	7	2	3	26	15	10	19	7	22	15	7	23	4	17	20	7	6	24	9	8	3	12	41	22	16	13	10	8	8	18	18	3	3	14	21	18	18
Hi Temp. °F		1584	1558	1513	1559	1575	1609	1602	1605	1603	1599	1597	1222	1402	1305	1358	1383	1389	1304	1389	1302	1449	1298	1415	1036	1152	1084	1035	947	1087	1122	1121	984	983	547	547	767	944	932	929
Lo Temp. °F		1570	1547	1501	1555	1568	1546	1566	1585	1557	1581	1546	1195	1388	1241	1347	1346	1338	1286	1376	1244	1425	1279	1407	1007	1050	1031	998	915	1062	1103	1102	936	936	540	539	732	892	887	885
35 Hour																																								
Avg. Temp. °F		1582	1551	1521	1561	1574	1602	1567	1598	1559	1591	1550	1203	1396	1267	1357	1367	1369	1300	1376	1268	1426	1299	1420	1080	1177	1097	1072	1002	1127	1174	1174	912	912	658	658	825	996	983	984
Std. Dev.		4	7	15	4	3	23	23	23	22	22	21	8	3	27	2	17	13	4	5	7	7	11	6	46	34	54	63	60	47	45	45	48	48	107	106	57	83	97	97
Hi Temp. °F		1586	1560	1539	1565	1577	1615	1582	1611	1569	1604	1563	1211	1399	1306	1365	1381	1387	1304	1384	1281	1435	1318	1428	1043	1216	1148	1125	1069	1163	1212	1213	966	966	765	764	890	1075	1069	1069
Lo Temp. °F		1575	1541	1504	1555	1569	1561	1527	1558	1521	1552	1515	1194	1393	1243	1346	1342	1350	1294	137	1264	1415	1288	1411	1107	1142	1029	1001	937	1071	1118	1118	848	848	543	543	750	888	865	864
40 Hour																																								
Avg. Temp. °F		1584	1546	1511	1558	1573	1589	1596	1603	1592	1604	1585	1192	1396	1273	1354	1365	1365	1296	1387	1254	1441	1280	1406	1087	1190	1140	1105	1025	1160	1005	1246	962	1241	546	1295	853	1017	1013	1013
Std. Dev.		4	8	18	4	2	22	8	11	10	11	15	4	5	10	5	11	16	7	15	12	7	10	8	16	23	11	16	9	7	29	32	43	46	10	51	36	47	34	32
Hi Temp. °F		1589	1554	1528	1564	1576	1614	1605	1616	1605	1614	1603	1197	1400	1285	1361	1377	1384	1304	1405	1263	1444	1293	1415	1101	1211	1153	1123	1038	1167	1050	1291	1010	1298	557	1361	909	1098	1057	1052
Lo Temp. °F		1578	1533	1491	1553	1571	1565	1589	1587	1583	1587	1573	1187	1389	1259	1350	1351	1345	1289	1371	1232	1434	1269	1398	1069	1159	1123	1079	1017	1149	981	1221	914	1193	536	1246	808	975	983	985

Table C-1 (Cont'd)

Heat Exchanger Probes Temperature History (Run 78)

Control Temperature: 1600°F

1400°F

1200°F

1050°F

Combusitor Location:		In Bed					Above Bed					In Bed					Above Bed					In Bed					Above Bed					In Bed											
Port Number	Specimen	1	3	5			13	15	17			2	4	6			14	16	18			7	9	11			19	20	22			8	10	12									
Hours Into Run		X	H	H	X	H	X	X	H	H	X	H	X	X	H	X	H	X	X	H	X	H	X	X	H	X	H	X	X	H	X	H	X	X	H	X	H	X					
45 Hour																																											
Avg. Temp. °F		1578	1547	1513	1554	1570		1563	1603	1594	1605	1591	1601	1196	1395	1250	1354	1358	1360	1293	1394	1248	1448	1268	1404	1073	1175	1157	1103	1027	1168	1032	1267	989	1275	554	1331	784	972	997		994	
Std. Dev.		2	2	13	6	3		18	2	4	2	4	4	11	4	26	7	8	10	9	10	5	5	15	6	20	13	12	8	8	7	50	24	35	32	11	35	3	12	9		10	
Hi Temp. °F		1580	1549	1525	1560	1575		1583	1606	1598	1608	1596	1606	1213	1399	1281	1362	1368	1368	1307	1404	1254	1456	1290	1410	1102	1189	1169	1113	1037	1175	1107	1299	1043	1321	571	1371	787	984	1005		1005	
Lo Temp. °F		1576	1545	1492	1546	1567		1539	1601	1590	1603	1587	1596	1186	1388	1226	1348	1348	1346	1284	1378	1241	1442	1249	1396	1050	1158	1140	1094	1019	1158	972	1232	946	1232	541	1284						
50 Hour																																											
Avg. Temp. °F		1578	1551	1510	1552	1569		1561	1597	1594	1598	1600	1590	1185	1393	1268	1353	1354	1352	1287	1371	1239	1440	1282	1422	1072	1127	1159	1098	1019	1153	972	1233	957	1234	538	1276	788	977	994		997	
Std. Dev.		1	5	18	3	4		15	3	6	4	13	6	6	3	17	6	10	6	3	7	4	3	5	7	7	26	14	19	5	11	16	8	5	7	3	5	21	12	16		17	
Hi Temp. °F		1579	1557	1525	1556	1574		1573	1600	1602	1602	1619	1597	1193	1395	1278	1359	1365	1359	1291	1382	1244	1443	1288	1431	1077	1160	1174	1125	1025	1167	983	1239	963	1245	541	1282	819	995	1016		1019	
Lo Temp. °F		1576	1546	1486	1550	1564		1543	1593	1588	1593	1489	1583	1178	1388	1242	1346	1343	1344	1285	1367	1234	1437	1278	1413	1062	1097	1140	1082	1014	1142	948	1222	952	1230	535	1272	775	969	978		984	
55 Hour																																											
Avg. Temp. °F		1576	1549	1509	1551	1569		1598	1585	1611	1581	1610	1568	1189	1388	1274	1346	1370	1368	1293	1370	1254	1433	1281	1426	1091	1163	1145	1093	1042	1146	972	1222	915	1199	545	1254	780	999	1020		1024	
Std. Dev.		3	10	21	3	1		9	6	3	9	8	8	3	9	35	7	19	15	7	3	11	3	3	3	17	28	21	13	13	11	5	5	17	14	9	14	14	15	20		17	
Hi Temp. °F		1578	1558	1537	1554	1569		1610	1590	1614	1586	1615	1574	1192	1398	1297	1355	1390	1385	1297	1371	1261	1436	1284	1429	1096	1186	1175	1106	1055	1155	978	1226	934	1212	542	1270	818	1019	1032		1035	
Lo Temp. °F		1572	1540	1485	1547	1566		1589	1517	1607	1568	1599	1556	1185	1377	1222	1338	1348	1354	1282	1366	1239	1429	1278	1421	1106	1122	1128	1078	1029	1131	968	1215	893	1180	525	1237	785	986	990		998	
60 Hour																																											
Avg. Temp. °F		1578	1551	1512	1553	1569		1589	1587	1611	1584	1611	1572	1183	1390	1274	1341	1356	1361	1297	1374	1239	1430	1279	1431	1073	1151	1166	1124	1072	1176	976	1226	909	1192	524	1238	799	993	1014		1016	
Std. Dev.		4	5	14	3	3		17	2	7	5	3	5	6	6	29	8	9	9	2	1	7	2	9	2	8	14	16	11	14	8	5	1	8	6	1	3	21	29	17		16	
Hi Temp. °F		1582	1554	1535	1558	1572		1610	1590	1620	1589	1615	1578	1189	1397	1301	1352	1366	1370	1298	1375	1247	1432	1292	1434	1081	1171	1185	1139	1086	1187	984	1227	916	1200	524	1241	817	1018	1042		1041	
Lo Temp. °F		1574	1544	1495	1549	1564		1565	1584	1603	1577	1606	1565	1174	1382	1231	1332	1346	1351	1294	1375	1229	1428	1269	1430	1063	1133	1149	1112	1053	1166	972	1224	896	1186	523	1234	769	948	999		1002	
65 Hour																																											
Avg. Temp. °F		577	1546	1503	1552	1568		1585	1587	1611	1584	1611	1711	1185	1391	1239	1338	1370	1371	1297	1374	1231	1428	1286	1435	1072	1149	1174	1116	1062	1180	978	1229	915	1199	529	1243	799	997	1018		1019	
Std. Dev.		3	4	7	3	3		14	3	7	6	3	7	5	4	12	4	11	12	3	1	2	3	6	4	11	20	18	14	26	8	4	6	8	7	4	5	19	23	23		27	
Hi Temp. °F		581	1551	1510	1556	1511		1599	1591	1619	1591	1615	1578	1191	1396	1257	1340	1384	1381	1300	1376	1234	1432	1291	1439	1083	1174	1195	1133	1093	1187	983	1237	924	1207	534	1250	828	1023	1048		1056	
Lo Temp. °F		574	1541	1495	1547	1564		1562	1583	1603	1576	1609	1563	1178	1384	1225	1333	1358	1352	1293	1372	1228	1424	1279	1428	1057	1124	1149	1098	1028	1168	972	1221	902	1188	524	1236	785	972	999		998	
70 Hour																																											
Avg. Temp. °F		576	1552	1494	1545	1566		1565	1599	1590	1601	1593	1592	1185	1388	1258	1345	1360	1356	1291	1372	1225	1432	1278	1425	1071	1160	1170	1109	1052	1174	972	1235	949	1230	522	1262	790	1001	1008		1009	
Std. Dev.		4	5	5	4	2		16	2	3	2	3	2	2	6	25	6	11	12	5	5	7	1	3	3	13	9	14	14	18	8	6	6	7	4	8	13	9	19	29		28	
Hi Temp. °F		580	1560	1503	1550	1568		1582	1600	1595	1602	1598	1594	1188	1397	1287	1353	1373	1372	1295	1379	1234	1433	1282	1428	1085	1167	1188	1132	1067	1181	982	1244	957	1236	533	1273	798	1024	1043		1044	
Lo Temp. °F		570	1547	1491	1539	1563		1547	1596	1587	1598	1589	1589	1182	1382	1229	1337	1344	1340	1285	1368	1216	1430	1274	1421	1057	1149	1157	1096	1023	1163	967	1229	942	1225	511	1242	780	982	977		979	
75 Hour																																											
Avg. Temp. °F		572	1555	1504	1547	1565		1562	1597	1596	1599	1596	1590	1187	1387	1248	1341	1355	1356	1295	1374	1228	1432	1277	1426	1075	1156	1152	1102	1049	1154	978	1240	954	1233	522	1270	789	1010	1013		1010	
Std. Dev.		5	6	10	8	2		17	4	6	5	7	6	2	3	31	7	17	17	4	1	3	3	5	1	20	24	9	11	19	49	17	18	14	12	10	21	12	15	16		17	
Hi Temp. °F		579	1566	1511	1558	1569		1585	1604	1604	1608	1606	1600	1189	1392	1291	1353	1370	1379	1300	1375	1231	1437	1285	1428	1106	1188	1162	1117	1074	1190	1005	1269	976	1253	541	1306	805	1029	1032		1036	
Lo Temp. °F		567	1550	1487	1539	1563		1542	1592	1589	1593	1586	1582	1183	1383	1217	1334	1329	1337	1291	1373	1225	1429	1271	1425	1054	1130	1142	1088	1023	1069	959	1223	938	1219	516	1252	776	990	977		996	
80 Hour																																											
Avg. Temp. °F		572	1545	1506	1547	1563		1573	1583	1593	1583	1590	1571	1191	1388	1259	13																										

Table C-1 (Cont'd)

Heat Exchanger Probes Temperature History (Run 78)

Control Temperature: 1600°F

1400°F

1200°F

1050°F

Compressor Location:

Port Number Hours Into Run	In Bed					Above Bed					In Bed					Above Bed					In Bed					Above Bed					In Bed																																																	
	1	3	5	13	15	17	2	4	6	14	16	18	7	9	11	19	20	22	8	12	10	1	3	5	13	15	17	2	4	6	14	16	18	7	9	11	19	20	22	8	12	10																																						
85 Hour																																																																																
Avg. Temp. °F	1575	1549	1509	1548	1565	1565	1598	1593	1601	1590	1591	1190	1390	1270	1342	1358	1358	1319	1392	1219	1400	1275	1423	1077	1146	1185	1096	1047	1160	970	1233	920	1207	515	1243	773	1006	1018	1017																																									
Std. Dev.	4	7	20	2	3	22	3	4	4	5	5	8	4	28	8	14	16	7	3	8	2	6	2	23	31	21	16	11	9	6	5	15	12	8	8	9	6	13	13																																									
Hi Temp. °F	1580	1558	1542	1551	1569	1592	1602	1596	1606	1595	1598	1201	1394	1287	1355	1371	1371	1328	1395	1226	1433	1280	1427	1102	1176	1214	1116	1063	1172	978	1241	938	1223	525	1254	785	1014	1032	1030																																									
Lo Temp. °F	1569	1544	1493	1546	1560	1541	1595	1587	1597	1583	1586	1181	1384	1221	1336	1334	1330	1308	1388	1206	1428	1265	1421	1048	1110	1166	1076	1034	1151	965	1228	904	1197	507	1235	761	1000	999	997																																									
90 Hour																																																																																
Avg. Temp. °F	1568	1549	1503	1541	1552	1555	1602	1588	1605	1583	1599	1183	1375	1266	1347	1363	1358	1305	1376	1220	1432	1271	1425	1060	1121	1181	1093	1033	1167	1093	1255	940	1227	525	1269	779	1020	1027	1021																																									
Std. Dev.	2	9	17	7	12	18	2	8	2	7	3	11	3	40	10	15	15	46	35	5	3	4	4	10	18	20	32	12	2	24	20	19	16	12	17	29	26	8	9																																									
Hi Temp. °F	1570	1557	1520	1547	1561	1579	1603	1598	1607	1591	1601	1198	1379	1297	1353	1385	1381	1373	1429	1224	1437	1275	1430	1071	1143	1209	1125	1046	1169	1016	1271	956	1239	536	1286	816	1057	1036	1039																																									
Lo Temp. °F	1566	1538	1480	1532	1535	1539	1600	1581	1604	1577	1594	1173	1372	1208	1333	1354	1349	1278	1355	1215	1430	1267	1421	1047	1100	1164	1065	1021	1165	962	1227	912	1204	512	1245	746	996	1019	1020																																									
95 Hour																																																																																
Avg. Temp. °F	1564	1550	1512	1542	1560	1545	1602	1585	1606	1581	1600	1186	1385	1244	1341	1352	1355	1283	1361	1213	1430	1265	1420	1071	1113	1162	1089	1045	1161	987	1252	942	1230	525	1269	775	1037	1023	1024																																									
Std. Dev.	6	10	16	6	2	21	1	3	1	3	1	5	5	27	4	14	14	3	3	5	3	3	4	17	14	10	17	12	5	33	3	2	2	12	4	20	23	10	10																																									
Hi Temp. °F	1569	1561	1525	1549	1563	1567	1604	1589	1608	1585	1602	1191	1392	1282	1347	1375	1373	1284	1363	1221	1434	1269	1424	1092	1134	1171	1105	1061	1169	991	1258	945	1232	531	1272	810	1076	1031	1034																																									
Lo Temp. °F	1558	1539	1489	1535	1558	1518	1601	1582	1605	1576	1598	1181	1381	1211	1334	1337	1334	1278	1356	1208	1428	1261	1415	1051	1096	1148	1066	1027	1158	983	1249	940	1227	523	1263	760	1017	1011	1012																																									
100 Hour																																																																																
Avg. Temp. °F	1564	1544	1504	1544	1561	1580	1595	1599	1598	1596	1588	1191	1381	1254	1342	1348	1352	1290	1365	1226	1428	1272	1421	1071	1120	1180	1095	1054	1161	967	1236	922	1205	514	1252	785	1044	1030	1029																																									
Std. Dev.	8	4	20	5	4	7	2	5	3	6	4	4	10	29	6	14	14	7	4	5	2	5	3	18	18	12	19	17	4	9	4	5	7	5	8	13	28	16	16																																									
Hi Temp. °F	1572	1550	1528	1549	1565	1588	1596	1605	1600	1606	1592	1197	1391	1299	1348	1363	1372	1300	1373	1232	1430	1280	1425	1097	1142	1197	1114	1078	1167	982	1241	928	1214	519	1260	800	1073	1047	1050																																									
Lo Temp. °F	1554	1539	1488	1539	1554	1570	1592	1592	1593	1590	1581	1187	1365	1219	1334	1333	1337	1281	1359	1217	1426	1266	1418	1065	1103	1166	1074	1029	1157	959	1231	916	1198	508	1243	772	998	1012	1010																																									
105 Hour																																																																																
Avg. Temp. °F	1567	1550	1506	1537	1561	1548	1601	1591	1605	1585	1597	1183	1378	1244	1341	1354	1357	1281	1361	1210	1430	1262	1421	1076	1139	1174	1083	1034	1162	970	1242	916	1206	494	1254	778	1030	1029	1031																																									
Std. Dev.	4	5	14	4	4	25	3	8	4	9	5	12	3	30	10	15	12	11	4	10	2	6	3	17	16	18	13	8	7	9	6	7	8	4	9	36	28	11	11																																									
Hi Temp. °F	1570	1554	1525	1543	1566	1582	1603	1603	1608	1600	1601	1200	1380	1288	1352	1366	1370	1292	1366	1223	1432	1270	1424	1094	1166	1197	1095	1040	1170	981	1251	922	1216	499	1265	835	1075	1038	1039																																									
Lo Temp. °F	1562	1542	1489	1533	1555	1513	1597	1584	1598	1578	1588	1174	1374	1219	1332	1330	1337	1266	1356	1198	1427	1256	1417	1052	1124	1167	1061	1020	1155	962	1237	904	1193	489	1241	741	1006	1016	1015																																									
110 Hour																																																																																
Avg. Temp. °F	1568	1547	1515	1541	1559	1554	1600	1599	1605	1589	1596	1182	1376	1273	1347	1344	1346	1285	1364	1220	1430	1267	1420	1057	1129	1178	1090	1043	1156	963	1238	918	1204	493	1252	769	1036	1036	1037																																									
Std. Dev.	5	9	13	2	5	26	3	9	4	9	5	7	9	21	7	13	12	5	2	7	3	4	3	5	14	22	10	8	8	13	9	12	14	10	12	11	8	21	19																																									
Hi Temp. °F	1574	1555	1526	1544	1566	1584	1604	1611	1610	1602	1602	1198	1387	1295	1353	1361	1361	1288	1367	1232	1434	1271	1424	1062	1153	1206	1101	1055	1168	975	1247	933	1220	503	1262	783	1049	1053	1057																																									
Lo Temp. °F	1560	1533	1497	1538	1552	1524	1595	1587	1598	1579	1587	1180	1368	1240	1338	1327	1330	1276	1361	1215	1428	1262	1418	1050	1117	1147	1076	1034	1148	941	1223	900	1183	481	1234	758	1029	1011	1013																																									
115 Hour																																																																																
Avg. Temp. °F	1571	1551	1514	1546	1564	1579	1595	1609	1594	1599	1582	1199	1384	1271	1342	1349	1350	1294	1370	1222	1424	1271	1422	1070	1136	1178	1102	1048	1159	968	1236	894	1180	488	1234	794	1030	1022	1024																																									
Std. Dev.	4	8	12	3	3	11	2	6	4	7	5	6	6	26	9	9	9	8	3	8	2	5	3	23	20	10	11	14	4	9	4	4	4	13	8	31	37	16	14																																									
Hi Temp. °F	1575	1558	1528	1551	1568	1592	1597	1615	1598	1608	1587	1204	1391	1292	1351	1364	1361	1306	1373	1230	1426	1278	1428	1096	1166	1190	1114	1059	1162	975	1241	899	1184	510	1242	848	1096	1043	1041																																									
Lo Temp. °F	1566	1540	1499	1543	1560	1566	1593	1600	1590	1591	1577	1191	1375	1238	1329	1341	1340	1287	1367	1213	1420	1266	1420	1045	1117	1164	1090	1023	1154	952	1231	890	1174	476	1223	771	1007	1007	1008																																									
120 Hour																																																																																
Avg. Temp. °F	1577	1561	1532	1556	1564	1554	1605	1590	1611	1575	1603	1189	1382	1249	1340	1344	1347	1277	1358	1213	1433	1266	1422	1080	1147	1177	1087	1048	1167	1002	1264	941	1230	533	1281	759	1034	1056	1061																																									
Std. Dev.	9	14	26	14	6	38	4	13	7	15	10	3	13	13	6	17	18	10	6	11	4	4	4	15	28	15	10	8	12	32	24	24	23	12	36	9	19	33	40																																									
Hi Temp. °F	1586	1573	1565	1568	1573	1595	1610	1603	1621	1596	1616	1192	1390	1263	1346	1364	1363	1293	1367	1228	1439	1270	1428	1090	1185	1197	1096	1056	1181	970	1299	974	1265	553	1331	769	1062	1112	1127																																									
Lo Temp. °F	1567	1540	1502	1539	1559	1493	1601	1568	1604	1550	1593	1186	1360	1230	1334	1319	1317	1267	1347	1199	1429	1261	1417	1061	1114	1162	1074	1036	1150	1054	1238	909	1203	520	1240	754	1013	1035	1034																																									

Table C-1 (Cont'd)

Heat Exchanger Probes Temperature History (Run 78)

Control Temperature: 1600°F

1400°F

1200°F

1050°F

Combustor Location:		In Bed					Above Bed					In Bed					Above Bed					In Bed					Above Bed					In Bed					Above Bed				
Port Number	Specimen	1	3	5			13	15	17			2	4	6			14	16	18			7	9	11			19	20	22			8	12	10							
Hours Into Run		X	H	H	X	H	X	X	H	H	X	H	X	X	H	X	H	X	H	X	X	H	X	H	X	X	H	X	H	X	X	H	X	H	X	X	H	X	H	X	
125 Hour		1576	1564	1551	1564	1575	1510	1610	1564	1620	1551	1618	1174	1377	1252	1349	1329	1329	1269	1349	1191	1439	1255	1416	1096	1191	1180	1096	1040	1177	1065	1305	986	1270	551	1345	783	1059	1038	1040	
Avg. Temp. °F		7	9	9	2	4	15	1	7	2	5	3	4	7	15	6	9	10	15	11	7	2	2	3	9	44	31	12	14	12	9	6	6	6	6	8	9	17	12	13	
Std. Dev.		1583	1579	1562	1566	1579	1522	1611	1580	1622	1569	1620	1179	1386	1278	1357	1338	1337	1287	1364	1202	1441	1257	1420	1104	1253	1227	1109	1059	1190	1074	1311	994	1276	557	1351	792	1074	1050	1053	
Hi Temp. °F		1567	1557	1539	1561	1569	1489	1609	1564	1618	1545	1613	1167	1368	1239	1341	1316	1315	1254	1340	1184	1436	1252	1412	1085	1131	1144	1083	1026	1159	1052	1295	977	1261	544	1331	772	1036	1020	1031	
Lo Temp. °F		1571	1563	1552	1565	1577	1478	1610	1559	1625	1538	1625	1168	1374	1270	1362	1324	1325	1285	1357	1181	1440	1245	1416	1067	1227	1178	1091	1027	1158	1106	1332	1017	1299	557	1371	1023	1023	1088	1029	
Avg. Temp. °F		7	3	14	13	4	15	2	12	3	13	6	11	5	35	8	15	15	6	5	8	3	13	2	20	25	20	14	8	8	31	18	24	20	9	17	36	37	7	7	
Std. Dev.		1580	1566	1572	1580	1584	1491	1612	1570	1629	1551	1632	1179	1380	1304	1367	1341	1337	1292	1362	1191	1443	1259	1419	1121	1264	1200	1111	1034	1168	1150	1355	1049	1325	569	1397	786	1081	1034	1036	
Hi Temp. °F		1563	1558	1538	1553	1574	1455	1608	1546	1621	1521	1618	1166	1368	1230	1349	1300	1298	1278	1350	1173	1436	1229	1413	1076	1206	1146	1079	1014	1148	1069	1313	991	1276	547	1355	701	990	1020	1021	
Lo Temp. °F		1572	1567	1564	1565	1578	1489	1609	1514	1601	1489	1604	1181	1382	1271	1369	1330	1314	1280	1355	1179	1435	1296	1386	1090	1199	1175	1081	1032	1159	1113	1328	1025	1300	561	1375	707	1014	1033	1025	
Avg. Temp. °F		5	10	18	7	8	61	5	36	15	35	16	21	8	26	6	36	16	16	3	13	11	35	25	13	10	12	6	11	12	54	40	47	40	18	38	11	19	18	20	
Std. Dev.		1579	1581	1592	1573	1589	1592	1613	1556	1627	1538	1630	1216	1391	1314	1368	1391	1339	1307	136	1196	1443	1238	1410	1097	1214	1191	1086	1047	1170	1156	1357	1062	1333	579	1406	722	1029	1053	1055	
Hi Temp. °F		1566	1559	1549	1555	1567	1441	1600	1484	1588	1457	1585	1164	1370	1252	1352	1299	1298	1266	1353	1164	1416	1144	1347	1067	1185	1161	1074	1016	1142	1024	1260	949	1235	551	1314	693	984	1024	1023	
Lo Temp. °F		1572	1572	1551	1561	1580	1485	1611	1505	1600	1473	1601	1185	1380	1267	1360	1319	1318	1287	1357	1183	1438	1207	1396	1084	1193	1171	1083	1033	1170	1124	1339	1033	1310	568	1389	719	1027	1049	1050	
Avg. Temp. °F		5	7	14	7	5	29	2	9	2	9	2	13	8	41	8	9	10	9	3	11	5	7	7	9	24	15	9	19	13	16	12	18	11	5	12	10	21	13	13	
Std. Dev.		1577	1580	1568	1573	1585	1534	1613	1521	1602	1488	1604	1195	1393	1318	1370	1331	1332	1299	1360	1194	1441	1212	1404	1100	1215	1192	1097	1057	1183	1144	1354	1053	1322	576	1402	735	1054	1064	1067	
Hi Temp. °F		1567	1562	1531	1555	1571	1460	1609	1497	1598	1465	1598	1167	1375	1229	1350	1306	1305	1274	1353	1169	1433	1195	1386	1078	1153	1151	1067	1013	1148	1103	1320	1005	1292	561	1369	707	998	1036	1034	
Lo Temp. °F		1575	1564	1542	1563	1579	1482	1603	1502	1598	1456	1600	1182	1380	1266	1363	1312	1313	1274	1350	1179	1440	1212	1398	1079	1218	1169	1081	1042	1172	1110	1334	1031	1307	575	1381	710	1015	1047	1047	
Avg. Temp. °F		8	7	10	7	3	8	5	7	2	28	2	6	6	28	13	10	8	11	5	6	2	15	11	8	17	19	13	2	13	17	10	14	10	16	9	7	8	17	16	
Std. Dev.		1586	1571	1549	1569	1582	1489	1613	1508	1600	1478	1603	1189	1388	1298	1377	1326	1324	1289	1358	1184	1442	1220	1408	1088	1244	1192	1097	1045	1182	1132	1342	1050	1317	599	1392	719	1025	1069	1069	
Hi Temp. °F		1566	1556	1524	1557	1574	1469	1607	1492	1595	1462	1597	1175	1372	1242	1346	1302	1304	1262	1345	1172	1438	1186	1380	1069	1195	1146	1065	1039	1151	1088	1321	1016	1297	561	1368	702	1004	1027	1027	
Lo Temp. °F		1573	1575	1553	1567	1578	1477	1610	1520	1606	1456	1602	1194	1378	1272	1355	1314	1313	1283	1352	1184	1441	1219	1403	1100	1195	1178	1082	1034	1160	1109	1331	1027	1309	595	1386	24	25	13	12	
Avg. Temp. °F		4	17	10	5	7	9	1	40	16	28	1	6	7	31	6	15	15	7	6	5	3	9	4	12	44	21	13	11	12	13	8	11	8	4	10	758	1044	1017	1017	
Std. Dev.		1578	1595	1561	1575	1584	1486	1611	1584	1631	1474	1603	1203	1389	1321	1362	1335	1333	1292	1359	1190	1444	1234	1407	1116	1256	1202	1098	1047	1170	1122	1341	1041	1318	599	1399	693	979	985	989	
Hi Temp. °F		1569	1554	1536	1562	1566	1465	1609	1478	1588	1462	1600	1188	1372	1247	1347	1297	1297	1272	1346	1178	1438	1209	1397	1116	1256	1202	1098	1047	1170	1122	1341	1041	1318	599	1399	693	979	985	989	
Lo Temp. °F		1571	1571	1542	1570	1581	1477	1609	1476	1585	1468	1601	1198	1383	1259	1354	1327	1326	1293	1352	1186	1440	1223	1403	1094	1226	1179	1084	1037	1161	1111	1332	1030	1307	585	1385	711	1011	1007	1007	
Avg. Temp. °F		4	8	18	5	4	10	2	6	1	8	2	5	6	24	11	16	14	6	4	8	2	11	5	7	45	15	4	9	6	9	11	12	12	7	15	17	30	38	38	
Std. Dev.		1578	1581	1566	1576	1586	1490	1611	1485	1586	1480	1602	1204	1388	1296	1370	1344	1340	1301	1357	1198	1443	1230	1408	1100	1282	1195	1091	1046	1168	1117	1340	1039	1317	593	1398	738	1052	1065	1064	
Hi Temp. °F		1568	1561	1521	1564	1577	1467	1606	1469	1584	1459	1598	1193	1374	1238	1346	1304	1304	1287	1348	1179	1437	1205	1397	1083	1170	1158	1081	1024	1152	1095	1315	1011	1288	576	1360	694	984	964	961	
Lo Temp. °F		1566	1574	1543	1571	1586	1466	1610	1472	1586	1463	1602	1192	1377	1283	1363	1308	1309	1285	1350	1183	1442	1230	1411	1093	1261	1168	1082	1037	1159	1127	1340	1044	1315	584	1398	716	1016	977	976	
Avg. Temp. °F		2	7	16	7	4	10	2	3	2	4	2	8	7	43	9	6	7	7	4	6	4	7	6	19	26	16	11	9	5	22	10	17	13	7	15	13	20	11	14	
Std. Dev.		1569	1582	1561	1579	1589	1477	1613	1476	1588	1470	1605	1203	1384	1316	1373	1313	1316	1296	1355	1192	1445	1238	1421	1116	1301	1188	1095	1049	1163	1163	1355	1071	1333	594	1415	729	1044	986	988	
Hi Temp. °F		1563	1566	1528	1565	1581	1454	1608	1468	1584	1458	1600	1183	1366	1226	1350	1299	1298	1279	1346	1175	1434	1221	1406	1068	1231	1154	1066	1023	1151	1105	1331	1027	1302	577	1379	698	995	954	953	
Lo Temp. °F																																									

Table C-1 (Cont'd)

Heat Exchanger Probes Temperature History (Run 78)

Control Temperature: 1600°F		1400°F												1200°F						1050°F																								
Combusator Location:		In Bed			Above Bed						In Bed			Above Bed						In Bed			Above Bed			In Bed																		
Port Number		1	3	5	13	15	17	2	4	6	14	16	18	7	9	11	19	20	22	8	12	10																						
Hours Into Run	Specimen	X	H	H	X	H	X	X	H	H	X	H	X	X	H	H	X	H	H	X	H	H	X	X	H	H	X	H	H	X	X	H	H	X	H	H	X	X	H	H	X	H	H	X
165 Hour		1569	1571	1543	1568	1583	1473	1608	1475	1585	1456	1602	1194	1375	1255	1366	1317	1321	1285	1353	1180	1442	1220	1406	1086	1249	1180	1084	1032	1154	1115	1339	1034	1311	581	1393	710	993	973	972				
Std. Dev.		3	14	22	8	3	28	2	7	2	29	3	6	10	46	6	17	15	10	7	15	3	18	13	20	20	12	5	13	10	23	19	26	21	11	20	15	22	11	10				
Hi Temp. °F		1572	1582	1575	1577	1585	1502	1610	1482	1587	1475	1605	1200	1386	1307	1374	1347	1344	1297	1361	1205	1447	1237	1416	1120	1267	1200	1090	1043	1163	1137	1359	1060	1336	593	1423	725	1017	986	982				
Lo Temp. °F		1566	1547	1522	1558	1579	1442	1606	1466	1583	1455	1598	1184	1362	1237	1358	1301	1508	1272	1343	1169	1439	1190	1383	1072	1221	1170	1077	1011	1143	1080	1314	1001	1283	566	1383	694	972	960	959				
170 Hour		1524	1549	1557	1531	1548	1525	1559	1511	1542	1505	1544	1229	1372	1297	1354	1360	1359	1328	1367	1251	1417	1129	1323	1138	1212	1189	1106	1064	1152	1033	1257	899	1185	578	1327	747	1024	1041	1040				
Std. Dev.		54	48	48	53	50	57	58	37	53	38	63	46	11	67	9	45	44	56	21	62	24	84	79	29	36	11	25	44	9	59	62	119	112	10	48	68	50	100	102				
Hi Temp. °F		1565	1594	1613	1563	1584	1607	1608	1552	1586	1544	1601	1310	1382	1389	1368	1416	1415	1413	1388	1334	1441	1217	1411	1171	1258	1204	1143	1140	1161	1103	1336	1025	1308	592	1391	865	1112	1213	1217				
Lo Temp. °F		1441	1468	1480	1447	1465	1454	1475	1470	1464	1458	1454	1201	1353	1237	1343	1314	1313	1278	1346	1170	1386	1013	1220	1100	1165	1180	1082	1033	1141	959	1206	730	1037	566	1271	692	1001	969	969				
175 Hour		1568	1567	1557	1572	1572	1461	1608	1473	1582	1466	1603	1196	1386	1266	1356	1339	1337	1293	1359	1190	1444	1212	1399	1093	1164	1175	1091	1024	1151	1105	1331	1021	1302	580	1383	703	1001	973	974				
Std. Dev.		3	13	8	5	5	9	2	2	1	4	1	4	9	35	9	25	24	9	4	10	4	7	3	13	15	12	11	13	8	10	6	11	7	5	6	15	19	26	28				
Hi Temp. °F		1572	1578	1564	1575	1576	1471	1610	1475	1588	1470	1604	1199	1394	1312	1367	1368	1369	1303	1365	1203	1447	1218	1403	1113	1185	1187	1105	1043	1161	1120	1338	1035	1312	587	1390	727	1031	1005	1012				
Lo Temp. °F		1565	1548	1543	1564	1563	1448	1606	1470	1586	1461	1603	1191	1372	1226	1344	1301	1303	1285	1355	1177	1438	1201	1396	1079	1151	1155	1076	1011	1142	1092	1322	1006	1294	574	1375	689	978	934	935				
180 Hour		1567	1557	1542	1571	1574	1450	1610	1468	1582	1460	1604	1196	1386	1264	1352	1347	1344	1289	1359	1191	1446	1209	1405	1092	1139	1171	1084	1029	1154	1117	1340	1031	1037	585	1391	729	1025	964	965				
Std. Dev.		2	8	11	7	7	7	1	1	4	2	1	8	7	29	9	12	13	8	4	12	4	3	1	16	16	15	10	8	7	9	3	8	6	2	6	26	30	14	16				
Hi Temp. °F		1570	1570	1553	1580	1577	1460	1611	1470	1590	1462	1605	1209	1393	1300	1363	1362	1361	1297	1364	1202	1450	1213	1406	1117	1157	1186	1098	1040	1163	1129	1345	1042	1317	587	1401	760	1063	982	988				
Lo Temp. °F		1565	1547	1527	1563	1561	1443	1608	1467	1585	1457	1602	1189	1375	1230	1340	1328	1325	1276	1354	1175	1440	1204	1404	1074	1114	1152	1072	1018	1144	1106	1337	1023	1303	583	1387	708	990	947	946				
185 Hour		1560	1567	1551	1566	1573	1510	1594	1499	1574	1492	1583	1209	1385	1285	1356	1361	1359	1298	1361	1215	1437	1154	1360	1110	1183	1186	1094	1047	1152	1058	1292	969	1251	575	1357	718	1008	998	997				
Std. Dev.		15	15	28	11	3	47	28	42	23	41	33	25	5	22	8	21	25	14	16	19	18	70	62	29	34	18	10	14	8	41	42	77	75	11	33	29	19	18	20				
Hi Temp. °F		1568	1589	1598	1575	1575	1572	1610	1572	1588	1562	1604	1251	1391	1302	1365	1396	1402	1324	1388	1249	1451	1206	1408	1155	1234	1203	1106	1066	1159	1104	1331	1025	1304	589	1384	765	1036	1028	1030				
Lo Temp. °F		1533	1550	1528	1549	1567	1460	1544	1470	1533	1460	1525	1190	1378	1249	1346	1345	1342	1291	1345	1203	1407	1037	1254	1080	1147	1165	1079	1028	1141	994	1226	835	1120	560	1301	692	987	980	983				
190 Hour		1564	1562	1534	1571	1580	1500	1608	1484	1586	1477	1600	1195	1378	1272	1356	1368	1368	1304	1364	1200	1442	1176	1379	1104	1190	1168	1094	1028	1153	1064	1292	996	1280	570	1357	707	1009	1005	1008				
Std. Dev.		2	10	27	5	7	8	2	2	2	5	2	6	5	37	9	20	20	12	13	10	3	12	5	19	17	22	5	13	15	14	17	9	8	8	13	4	14	24	21				
Hi Temp. °F		1567	1580	1572	1576	1586	1514	1610	1486	1588	1483	1604	1203	1384	1313	1362	1396	1392	1319	1380	1217	1446	1190	1385	1126	1218	1199	1100	1048	1169	1081	1307	1006	1289	579	1371	713	1029	1023	1022				
Lo Temp. °F		1562	1555	1518	1563	1570	1494	1606	1482	1584	1470	1598	1189	1372	1228	1340	1341	1337	1291	1352	1190	1439	1167	1374	1081	1174	1146	1086	1015	1134	1047	1265	988	1273	561	1343	702	995	964	971				
195 Hour		1565	1563	1522	1572	1569	1462	1610	1472	1589	1463	1604	1193	1380	1283	1372	1359	1361	1312	1376	1188	1446	1180	1391	1088	1163	1176	1072	1048	1160	1093	1320	1025	1302	577	1388	708	1020	998	999				
Std. Dev.		3	18	15	15	7	38	3	12	3	13	5	11	78	36	11	17	19	10	6	17	6	15	17	15	39	9	16	12	7	38	29	40	34	16	31	15	16	10	11				
Hi Temp. °F		1568	1582	1546	1592	1578	1510	1614	1484	1593	1473	1611	1207	1391	1329	1384	1385	1393	1323	1384	1209	1454	1205	1417	1107	1226	1190	1096	1056	1166	1150	1366	1084	1354	601	1438	725	1038	1006	1008				
Lo Temp. °F		1561	1542	1509	1555	1559	1415	1608	1457	1587	1447	1600	1178	1372	1238	1358	1343	1344	1301	1371	1163	1439	1163	1371	1068	1126	1168	1058	1027	1148	1058	1298	984	1268	560	1366	694	1001	982	980				
200 Hour		1563	1565	1524	1579	1571	1491	1609	1470	1587	1473	1601	1199	1375	1296	1372	1379	1375	1320	1379	1201	1444	1171	1377	1101	1141	1187	1086	1030	1157	1155	1293	989	1277	558	1361	703	1010	991	991				
Std. Dev.		2	14	10	20	6	9	1	1	3	2	2	8	9	32	6	8	7	8	5	6	2	6	3	19	25	18	24	7	5	2	4	6	4	5	7	21	26	15	12				
Hi Temp. °F		1565	1579	1533	1603	1579	1500	1610	1480	1590	1475	1603	1210	1388	1336	1381	1390	1384	1333	1386	1209	1447	1176	1380	1114	1173	1206	1111	1037	1165	1057	1299	994	1282	564	1373	2727	1039	1008	1007				
Lo Temp. °F		1561	1543	1511	1560	1564	1479	1608	1477	1583	1470	1598	1191	1366	1258	1364	1368	1364	1313	1374	1195	1442	1162	1372	1068	1111	1166	1055	1022	1151	1053	1288	982	1271	551	1353	677	984	974	980				

Table C-1 (Cont'd)

Heat Exchanger Probes Temperature History (Run 78)

Control Temperature: 1600°F		1400°F												1200°F						1050°F																				
Combusitor Location:		In Bed					Above Bed					In Bed			Above Bed			In Bed			Above Bed			In Bed																
Port Number	Specimen	1	3	5			13	15	17				2	4	6	14	16	18	7	9	11	19	20	22	8	12	10													
Hours Into Run	Specimen	X	H	H	X	H	X	X	H	H	X	H	X	B	X	X	B	X	B	X	B	B	X	3	8	8	3	8	3	8	3	3	8	8	3	2	9	9	9	
205 Hour		1562	1562	1527	1578	1577	1461	1610	1472	1586	1463	1603	1204	1383	1305	1375	1377	1376	1311	1376	1198	1452	1191	1392	1096	1189	1179	1086	1039	1160	1093	1316	1024	1302	568	1381	709	1014	998	998
Std. Dev.		1	14	22	14	6	14	2	3	1	5	32	8	8	28	11	8	11	13	6	12	2	10	10	8	20	30	13	15	7	19	13	15	12	9	6	9	17	16	16
Hi Temp. °F		1563	1578	1559	1596	1584	1478	1613	1475	1587	1470	1606	1215	1391	1332	1386	1390	1390	1327	1386	1214	1455	1207	1408	1107	1217	1212	1105	1054	1168	1118	1335	1041	1318	582	1387	721	1004	1013	1034
Lo Temp. °F		1560	1543	1505	1567	1567	1444	1608	1464	1584	1457	1602	1193	1371	1261	1359	1370	1366	1297	1369	1184	1450	1181	1383	1088	1163	1138	1074	1019	1154	1075	1300	1003	1284	558	1373	698	1001	973	973
210 Hour		1565	1560	1534	1566	1582	1460	1610	1468	1587	1460	1605	1198	1377	1312	1369	1372	1372	1301	1368	1186	1450	1190	1396	1109	1221	1190	1085	1034	1154	1106	1325	1032	1311	545	1391	719	1010	1017	1017
Std. Dev.		2	11	14	6	5	17	2	5	3	4	3	9	5	11	5	9	7	6	3	7	2	7	4	18	22	14	7	9	5	16	10	11	8	15	9	16	16	31	24
Hi Temp. °F		1566	1579	1555	1573	1590	1473	1612	1473	1591	1463	1608	1211	1383	1323	1376	1382	1382	1310	1371	1194	1453	1196	1400	1124	1249	1206	1091	1044	1160	1123	1336	1041	1320	566	1400	738	1034	1067	1055
Lo Temp. °F		1562	1554	1520	1557	1578	1431	1606	1462	1584	1453	1602	1189	1371	1301	1364	1360	1364	1293	1364	1178	1449	1181	1392	1079	1194	1173	1073	1025	1147	1087	1312	1013	1303	525	1380	696	996	984	990
215 Hour		1563	1560	1532	1565	1581	1448	1609	1465	1587	1459	1605	1199	1382	1287	1370	1375	1377	1300	1372	1182	1452	1186	1397	1096	1223	1196	1091	1049	1157	1096	1328	1024	1307	528	1386	718	1019	1011	1014
Std. Dev.		4	12	17	6	7	24	2	8	2	5	3	7	8	24	8	17	14	3	4	6	2	12	6	9	27	13	6	10	5	17	12	21	11	9	13	9	4	8	9
Hi Temp. °F		1567	1573	1560	1574	1591	1484	1612	1476	1588	1467	1609	1207	1388	1318	1379	1389	1391	1303	1377	1191	1455	1200	1404	1107	1256	1214	1097	1058	1162	1117	1344	1056	1323	538	1405	725	1024	1023	1027
Lo Temp. °F		1558	1545	1517	1558	1571	1422	1608	1456	1584	1454	1600	1189	1370	1254	1361	1347	1353	1297	1368	1175	1450	1169	1388	1081	1182	1182	1082	1037	1149	1074	131	1003	1293	520	1373	711	1014	1002	1003
220 Hour		1571	1569	1560	1591	1585	1465	1608	1477	1591	1467	1604	1207	1392	1292	1405	1370	1369	1324	1387	1164	1431	1175	1386	1110	1180	1188	1078	1060	1167	1084	131	1014	1294	533	1376	724	1038	1024	1024
Std. Dev.		4	20	25	9	11	26	1	9	4	7	4	10	10	31	30	15	15	12	8	28	9	15	13	19	26	19	9	7	13	30	25	31	22	18	23	777	1075	1048	1043
Hi Temp. °F		1577	1590	1580	1601	1595	1490	1610	1488	1596	1475	1611	1217	1402	1347	1432	1385	1382	1339	1396	1207	1455	1191	1399	1133	1209	1211	1092	1069	1186	1127	134	1062	132	560	1410	713	1016	990	989
Lo Temp. °F		1566	1542	1527	1578	1569	1423	1607	1466	1585	1453	1600	1194	1378	1270	1361	1346	1346	1310	1375	1141	1422	1154	1366	1087	1155	1164	1070	1052	1152	1044	128	979	126	513	1349				
225 Hour		1570	1576	1555	1585	1597	1470	1609	1478	1591	1463	1603	1206	1380	1267	1416	1391	1392	1322	1388	1140	1423	1175	1385	1116	1225	1193	1091	1063	1182	1082	1305	1002	1288	536	1373	740	1051	1037	1030
Std. Dev.		2	12	14	4	4	10	1	4	1	5	1	12	6	8	7	13	12	8	5	5	2	6	5	13	40	17	11	14	5	6	5	8	5	7	7	19	28	38	38
Hi Temp. °F		1572	1588	1579	1591	1603	1481	1611	1484	1591	1469	1604	1223	1387	1278	1425	1405	1407	1330	1395	1146	1426	1184	1393	1134	1269	1219	1105	1076	1186	1090	1310	1013	1292	545	1382	764	1070	1092	1093
Lo Temp. °F		1568	1555	1544	1582	1593	1458	1608	1475	1590	1457	1602	1194	1371	1258	1409	1374	1377	1313	1382	1132	1420	1169	1381	1101	1177	1173	1079	1043	1174	1075	1298	993	1281	528	1364	713	1003	988	999
230 Hour		1570	1575	1559	1584	1593	1447	1608	1473	1590	1458	1605	1208	1385	1274	1416	1382	1377	1323	1382	1138	1426	1181	1390	1120	1201	1188	1080	1065	1180	1086	312	1014	1296	529	1376	722	1033	1021	1021
Std. Dev.		4	18	12	10	1	24	1	6	1	6	3	3	5	8	5	16	15	7	4	9	3	12	8	14	29	19	15	8	4	11	10	7	8	13	13	18	17	13	17
Hi Temp. °F		1573	1595	1572	1597	1594	1471	1609	1478	1591	1453	1602	1210	1390	1281	1423	1398	1391	1330	1387	1147	1428	1194	1400	1137	1235	1218	1094	1073	1186	1103	1323	1021	1306	545	1393	755	1051	1033	1036
Lo Temp. °F		1566	1553	1541	1572	1592	1415	1607	1464	1589	1453	1602	1203	1378	1261	1411	1364	1360	1315	1377	1127	1422	1168	1382	1105	1168	1170	1063	1053	1176	1076	1301	1006	1287	517	1359	712	1007	1006	1003
235 Hour		1569	1571	1555	1588	1594	1454	1608	1476	1592	1460	1605	1207	1387	1264	1417	1373	1376	1322	1383	1153	1432	1182	1391	1115	1218	1191	1075	1053	1174	1078	1309	1017	1294	542	1374	715	1025	1018	1016
Std. Dev.		2	11	17	3	8	9	2	3	2	3	2	6	5	7	4	6	9	7	2	6	3	4	2	4	20	17	16	7	9	11	4	5	4	5	4	19	23	12	11
Hi Temp. °F		1571	1579	1581	1592	1598	1462	1611	1480	1594	1465	1607	1216	1393	1270	1420	1381	1390	1330	1386	1159	1436	1185	1394	1120	1235	1205	1098	1060	1183	1090	1313	1023	1299	550	1380	746	1059	1031	1030
Lo Temp. °F		1568	1552	1540	1585	1579	1441	1607	1473	1590	1457	1603	1200	1380	1253	1411	1365	1368	1313	1381	1144	1427	1178	1388	1110	1195	1165	1057	1043	1161	1065	1304	1010	1288	536	1370	694	1003	1000	1000
240 Hour		1569	1571	1563	1591	1590	1459	1608	1475	1592	1460	1605	1202	1380	1258	1414	1384	1383	1326	1387	1147	1430	1178	1388	1118	1205	1195	1077	1064	1176	1085	1311	1012	1293	537	1375	717	1031	1024	1028
Std. Dev.		4	20	13	7	7	23	2	7	1	7	2	8	6	11	6	12	12	5	2	11	6	16	11	16	25	17	11	10	8	20	16	22	16	17	12	23	16	20	
Hi Temp. °F		1575	1592	1574	1598	1598	1478	1610	1481	1593	1467	1608	1212	1391	1271	1422	1397	1394	1331	1391	1165	1437	1199	1405	1134	1242	1216	1088	1074	1185	1117	1335	1047	1317	556	1400	730	1058	1044	1049
Lo Temp. °F		1565	1539	1544	1580	1582	1422	1606	1467	1591	1451	1603	1191	1378	1243	1407	1366	1362	1318	1385	1137	1422	1163	1378	1094	1181	1178	1064	1053	1164	1068	1299	990	1281	513	1354	701	998	1006	1002

Table C-1 (Cont'd)

Heat Exchanger Probes Temperature History (Run 78)

Control Temperature: 1600°F		1400°F												1200°F						1050°F																				
Combusitor Location:		In Bed			Above Bed						In Bed			Above Bed			In Bed			Above Bed			In Bed																	
Port Number	Specimen	1	3	5	13	15	17	2	4	6	14	16	18	7	9	11	19	20	22	8	12	10																		
Hours Into Run		X	H	H	X	H	X	X	H	H	X	H	X	X	H	X	X	H	X	X	H	X	X	H	X															
245 Hour																																								
Avg. Temp. °F		1569	1572	1557	1586	1596	1451	1608	1473	1592	1458	1605	1200	1380	1265	1415	1377	1380	1322	1384	1150	1430	1184	1394	1126	1179	1179	1082	1066	1175	1084	1316	1127	1302	553	1381	730	1045	1031	1033
Std. Dev.		2	15	17	8	2	23	1	8	2	7	2	10	16	11	2	16	15	3	3	8	5	11	10	6	7	18	14	10	6	27	19	25	20	10	19	17	20	9	9
Hi Temp. °F		1571	1585	1577	1594	1599	1465	1604	1481	1594	1466	1608	1214	1396	1282	1418	1393	1396	1326	1387	1158	1438	1203	1411	1133	1187	1202	1100	1077	1183	1123	1348	1071	1337	570	1414	746	1065	1041	1043
Lo Temp. °F		1566	1547	1538	1575	1593	1411	1607	1459	1590	1448	1603	1188	1362	1257	1413	1353	1363	1319	1380	1140	1424	1178	1387	1118	1168	1157	1061	1055	1166	1067	1299	1011	1289	544	1369	701	1024	1016	1022
250 Hour																																								
Avg. Temp. °F		1558	1572	1556	1577	1582	1514	1590	1508	1574	1495	1581	1220	1388	1295	1418	1406	1403	1348	1398	1176	1414	1124	1357	1134	1192	1189	1090	1068	1164	1021	1259	947	1224	539	1324	738	1055	1058	1058
Std. Dev.		26	9	26	29	17	61	33	39	30	40	39	16	5	25	5	41	41	34	17	32	21	74	66	13	13	18	22	15	8	64	57	83	84	7	36	37	20	44	43
Hi Temp. °F		1571	1584	1584	1597	1595	1597	1609	1557	1592	1549	1607	1241	1392	1329	1426	1465	1458	1402	1425	1221	1430	1191	1398	1152	1206	1215	1117	1086	1173	1076	1308	1013	1291	547	1374	781	1080	1121	1123
Lo Temp. °F		1512	1561	1521	1528	1553	1459	1532	1477	1522	1463	1515	1208	1380	1271	1413	1376	1371	1322	1384	1142	1381	1014	1241	1117	1187	1164	1064	1051	1155	950	1187	822	1098	528	1291	707	1032	1016	1017
255 Hour																																								
Avg. Temp. °F		1568	1580	1561	1586	1596	1436	1609	1466	1593	1451	1605	1204	1376	1266	1414	1379	1382	1310	1376	1139	1436	1176	1393	1121	1193	1178	1084	1071	1182	1090	1322	1024	1305	536	1387	715	1036	1048	1046
Std. Dev.		2	14	16	8	6	9	1	4	1	5	3	6	13	2	2	13	15	5	3	6	2	7	5	8	34	15	12	11	7	21	11	8	9	12	11	13	21	10	8
Hi Temp. °F		1570	1593	1574	1600	1602	1444	1611	1473	1594	1468	1603	1210	1394	1268	1417	1391	1397	1318	1379	1147	1432	1186	1398	1132	1232	1204	1102	1077	1188	1110	1331	1030	1313	545	1398	727	1068	1055	1054
Lo Temp. °F		1512	1561	1521	1528	1553	1444	1611	1473	1594	1468	1603	1198	1369	1264	1412	1361	1358	1305	1373	1133	1428	1169	1386	1112	1138	1165	1074	1052	1171	1066	1308	1015	1295	517	1373	693	1006	1026	1033

Table C-2

Heat Exchanger Probes Temperature History (Run 79)

Control Temperature: 1600

1400

1200

1050

Combustor Location:

		In Bed						Above Bed						In Bed						Above Bed						In Bed						Above Bed						In Bed					
Port Number	Specimen	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42
5 Hour																																											
Avg. Temp. °F		1443	1487	1417	1501	1287	1507	1293	1489	1357	1502	1267	1506	1055	1299	754	1410	1317	1325	1163	1288	915	1325	979	1262	971	1032	1076	1103	915	1071	826	1140	803	1092	739	1133	594	807	893	933	940	
Std. Dev.		73	56	92	69	101	58	87	75	80	71	77	55	78	62	14	54	64	65	84	72	79	56	41	32	75	81	66	74	65	67	104	92	95	87	96	112	67	85	67	115	103	
Hi Temp. °F		1537	1567	1549	1590	1425	1588	1426	1586	1476	1595	1391	1582	1158	1384	774	1485	1411	1419	1279	1383	1028	1399	1018	1291	1067	1134	1155	1201	1006	1174	994	1273	963	993	911	1300	682	903	998	1115	1098	
Lo Temp. °F		1360	1433	1315	1419	1185	1448	1207	1417	1283	1428	1183	1430	964	1230	742	1354	1234	1244	1075	1206	836	1263	920	1210	889	920	1012	1025	841	1008	712	1018	712	1231	711	990	522	714	824	801	814	
10 Hour																																											
Avg. Temp. °F		1022	1045	1015	1043	988	1038	1043	1097	1052	1095	1015	1092	849	959	553	994	947	950	976	1015	884	1013	591	783	774	823	817	850	753	892	629	796	719	880	757	951	553	649	715	722	704	
Std. Dev.		674	664	667	665	641	673	545	545	557	549	524	549	517	590	365	621	603	606	489	460	425	480	417	517	451	474	490	499	435	487	408	502	384	445	303	415	218	343	401	381	391	
Hi Temp. °F		1567	1594	1548	1596	1528	1588	1468	1466	1496	1588	1411	1581	1311	1391	858	1478	1415	1416	1345	1394	1328	1395	989	1255	1142	1227	1190	1230	1145	1196	984	1243	1050	1216	934	1288	711	922	1069	1009	995	
Lo Temp. °F		152	172	152	171	156	164	257	257	253	336	252	328	157	168	105	171	156	156	252	347	249	315	115	155	157	164	155	167	174	174	133	177	179	240	256	332	191	154	155	173	154	
15 Hour																																											
Avg. Temp. °F		1553	1580	1532	1589	1468	1590	1446	1588	1489	1593	1397	1584	1160	1384	909	1476	1371	1373	1296	1395	1078	1397	999	1263	1070	1104	1176	1190	1019	1174	966	1242	954	1221	926	1290	657	876	945	967	976	
Std. Dev.		16	3	15	3	40	2	9	2	2	1	4	1	5	4	7	5	18	27	5	2	4	1	3	4	19	17	15	14	10	6	8	5	1	5	3	3	34	37	21	8	11	
Hi Temp. °F		1568	1582	1538	1593	1514	1593	1451	1585	1492	1595	1402	1585	1167	1388	191	1483	1388	1396	1301	1396	1083	1396	1005	1268	1094	1134	1191	1207	1028	1179	980	1251	956	1226	929	1294	708	925	974	979	993	
Lo Temp. °F		1530	1575	1515	1586	1425	1588	1436	1585	1487	1592	1393	1583	1155	1377	902	1469	1345	1339	1287	1393	1074	1396	996	1257	1051	1090	1156	1171	1005	1165	959	1237	952	1216	920	1286	616	827	921	959	961	
20 Hour																																											
Avg. Temp. °F		1544	1574	1539	1590	1470	1588	1461	1585	1493	1592	1403	1582	1171	1377	910	1472	1396	1399	1298	1394	1072	1395	1001	1267	1077	1095	1154	1181	1020	1172	964	1242	952	1225	931	1289	659	896	947	959	979	
Std. Dev.		10	7	19	5	31	6	14	2	9	4	11	2	10	5	6	5	31	26	8	6	10	3	16	15	5	12	22	10	18	9	4	6	4	5	3	6	31	40	13	14	9	
Hi Temp. °F		1558	1579	1569	1598	1413	1592	1478	1590	1505	1596	1417	1585	1180	1382	916	1475	1425	1429	1309	1403	1086	1395	1015	1283	1084	1107	1188	1191	1044	1180	970	1249	956	1230	936	1297	691	928	963	974	987	
Lo Temp. °F		1532	1562	1522	1587	1431	1578	1439	1586	1481	1585	1388	1579	1158	1369	902	1464	1357	1364	1288	1386	1061	1392	977	1244	1071	1081	1134	1164	1002	1163	960	1234	945	1217	927	1280	617	834	928	946	964	
25 Hour																																											
Avg. Temp. °F		1555	1575	1539	1586	1462	1591	1438	1591	1482	1597	1389	1585	1165	1376	902	1470	1371	1379	1295	1391	1063	1396	1169	1378	1074	1097	1142	1170	1021	1170	955	1242	949	1227	928	1298	653	893	955	962	984	
Std. Dev.		12	7	8	4	18	2	14	1	6	2	8	2	10	7	4	7	20	21	3	3	3	2	135	85	13	14	17	13	8	4	3	6	2	2	3	5	35	34	11	9	11	
Hi Temp. °F		1571	1581	1549	1589	1483	1594	1453	1592	1490	1600	1399	1587	1175	1384	908	1477	1402	1411	1299	1395	1067	1398	1276	1445	1091	1120	1166	1188	1032	1175	958	1251	952	1229	931	1304	692	937	967	971	1001	
Lo Temp. °F		1539	1565	1530	1579	1441	1589	1421	1590	1476	1595	1379	1584	1149	1367	898	1458	1352	1360	1291	1387	1059	1394	1013	1278	1062	1083	1125	1152	1015	1165	951	1235	947	1225	924	1292	616	862	939	949	974	
30 Hour																																											
Avg. Temp. °F		1576	1599	1568	1610	1466	1609	1472	1609	1508	1615	1416	1604	1189	1393	908	1469	1349	1347	1320	1417	1096	1415	1158	1372	1099	1116	1185	1192	1050	1188	958	1246	948	1227	926	1295	699	938	975	980	996	
Std. Dev.		16	7	17	4	15	3	20	1	7	3	9	3	6	5	5	3	11	9	7	4	6	2	66	43	8	7	21	7	17	9	4	3	3	2	4	4	37	36	11	7	21	
Hi Temp. °F		1596	1611	1588	1615	1483	1615	1492	1610	1514	1619	1424	1609	1195	1398	913	1474	1359	1355	1329	1423	1100	1417	1201	1399	1109	1125	1214	1199	1062	1198	963	1248	953	1229	932	1300	746	980	993	987	1031	
Lo Temp. °F		1558	1594	1544	1603	1445	1606	1439	1608	1497	1612	1400	1601	1179	1384	903	1467	1333	1332	1310	1413	1087	1414	1041	1295	1089	1109	1167	1181	1021	1176	954	1241	946	1224	920	1291	665	900	965	969	980	
35 Hour																																											
Avg. Temp. °F		1569	1596	1559	1608	1498	1611	1467	1608	1506	1615	1414	1603	1192	1394	911	1467	1350	1351	1325	1420	1100	1413	1184	1387	1086	1108	1184	1198	1042	1185	962	1243	945	1227	923	1288	679	910	970	985	993	
Std. Dev.		14	3	16	4	18	1	16	1	5	1	5	2	5	6	4	6	12	12	6	3	6	1	6	4	16	11	34	15	11	6	7	5	2	1	4	2	18	14	12	5	17	
Hi Temp. °F		1593	1599	1577	1614	1513	1613	1479	1609	1511	1616	1420	1606	1197	1399	915	1475	1367	1365	1331	1424	1110	1415	1194	1393	1106	1122	1215	1212	1054	1192	968	1248	947	1229	926	1292	704	922	986	989	1019	
Lo Temp. °F		1559	1592	1545	1605	1471	1610	1441	1607	1499	1614	1406	1601	1184	1385	907	1459	1336	1340	1316	1418	1094	1412	1178	1384	1064	1092	1133	1181	1026	1178	951	1235	942	1226	917	1287	656	887	957	977	973	
40 Hour																																											
Avg. Temp. °F		1575	1588	1565	1600	1477	1610	1450	1609	1501	1615	1402	1604	1188	1395	917	1473	1336	1334	1316	1405	1075	1408	1193	1406	1106	1115	1183	1185	1053	1186	949	1251	937	1235	918	1311	665	929	979	969	984	
Std. Dev.		16	7	14	7	16	3	7	1	5	1	6	1	7	6	6	10	12	11	7	9	17	3	13	14	18	12	27	14	12	6	13	8	1	7	1	15	38	30	21	16	17	
Hi Temp. °F		1592	1597	1516	1606	1501	1614	1461	1611	1505	1616	1412	1605	1195	1405	924	1483	1351	1346	1327	1419	1095	1412	1210	1423	1130	1136	1226	1206	1072	1195	968	1259	939	1245	919	1331	707	969	1011	989	1009	
Lo Temp. °F		1553	1580	1546	1588	1455	160																																				

Table C-3

Heat Exchanger Probes Temperature History (Run 80)

LOCATION PORT NO. SPEC. MAT. SPEC. LOC. DATA LOG NO.	IN BED					ABOVE BED					IN BED					ABOVE BED					IN BED					ABOVE BED																
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40		
DEGREES FAHRENHEIT																																										
5 HOUR																																										
AVG. TEMP.	1582	1576	1566	1598	1510	1586	1572	1590	1602	1585	1498	1574	1193	1373	959	1580	1391	1389	1345	1396	1171	1393	1249	1445	1164	1190	1096	1189	1080	1282	919	1149	981	1222	941	1261	876	905	0	1183	995	991
STD. DEV.	22	8	15	5	24	3	27	4	22	8	17	5	6	5	7	99	20	24	7	8	8	4	4	3	11	17	24	19	14	6	9	4	5	2	8	9	8	48	0	48	14	13
HI TEMP.	1648	1594	1590	1687	1542	1591	1615	1596	1642	1595	1531	1581	1261	1381	970	1856	1425	1430	1357	1488	1193	1468	1281	1458	1126	1219	1157	1218	1108	1214	943	1294	989	1225	923	1285	878	909	0	1284	1014	1088
LO TEMP.	1557	1561	1543	1548	1443	1581	1537	1582	1570	1567	1479	1564	1180	1365	948	1465	1367	1363	1334	1386	1157	1387	1264	1441	1098	1165	1068	1146	1059	1187	989	1175	973	1217	892	1252	864	894	0	1152	966	981
10 HOUR																																										
AVG. TEMP.	1585	1578	1563	1604	1517	1587	1607	1572	1593	1562	1559	1557	1206	1378	947	1480	1393	1392	1357	1404	1184	1389	1277	1447	1180	1214	1082	1212	1094	1226	923	1191	986	1219	898	1244	868	893	0	1148	1028	985
STD. DEV.	15	4	17	8	27	5	15	7	9	7	9	33	8	17	10	11	7	23	18	10	3	13	5	2	11	8	14	16	23	14	33	22	5	2	21	7	8	48	0	48	14	13
HI TEMP.	1604	1587	1580	1629	1555	1595	1617	1582	1603	1572	1603	1565	1221	1394	959	1493	1427	1422	1379	1489	1268	1396	1296	1451	1165	1221	1118	1237	1139	1242	968	1254	996	1222	945	1257	893	909	0	1164	1032	1086
LO TEMP.	1558	1572	1535	1593	1462	1581	1595	1556	1579	1564	1519	1541	1184	1366	927	1468	1365	1367	1337	1395	1168	1395	1278	1443	1098	1165	1068	1146	1059	1187	989	1175	973	1217	892	1252	864	894	0	1152	966	981
15 HOUR																																										
AVG. TEMP.	1589	1582	1554	1592	1513	1593	1600	1563	1596	1553	1598	1548	1222	1389	934	1476	1485	1466	1355	1404	1195	1393	1281	1450	1098	1216	1082	1221	1116	1229	973	1213	998	1218	934	1251	868	893	0	1148	1028	985
STD. DEV.	14	3	16	12	27	2	13	7	7	7	7	6	4	3	8	4	25	26	9	3	7	2	7	3	11	4	11	9	28	7	9	6	5	3	15	7	8	48	0	48	14	13
HI TEMP.	1611	1588	1577	1626	1553	1596	1613	1574	1602	1566	1613	1581	1229	1396	944	1483	1435	1438	1379	1489	1214	1397	1298	1455	1118	1227	1181	1222	1145	1264	966	1223	999	1223	958	1264	892	909	0	1164	1032	1086
LO TEMP.	1564	1577	1529	1568	1444	1589	1558	1550	1574	1539	1585	1536	1215	1385	912	1467	1369	1363	1342	1396	1183	1391	1279	1447	1082	1212	1085	1284	1098	1218	954	1282	982	1212	988	1239	868	893	0	1148	1028	985
20 HOUR																																										
AVG. TEMP.	1589	1583	1560	1580	1529	1591	1591	1587	1566	1579	1586	1578	1216	1387	951	1461	1482	1484	1344	1396	1183	1395	1270	1445	1186	1292	1096	1281	1095	1211	946	1214	983	1222	925	1262	889	899	0	1097	1004	997
STD. DEV.	15	4	17	8	27	5	17	7	7	7	10	10	5	8	10	17	22	22	6	3	6	3	8	4	11	8	13	7	27	18	8	6	5	2	14	8	8	48	0	48	14	13
HI TEMP.	1611	1589	1581	1586	1570	1593	1615	1592	1591	1595	1609	1588	1225	1392	988	1470	1428	1435	1353	1404	1190	1401	1285	1452	1119	1217	1119	1212	1165	1233	944	1255	993	1225	952	1273	892	909	0	1164	1032	1086
LO TEMP.	1567	1579	1540	1574	1483	1588	1548	1571	1548	1563	1587	1555	1207	1381	936	1446	1379	1372	1334	1398	1170	1391	1264	1439	1085	1187	1074	1187	1078	1195	944	1283	975	1218	925	1253	878	899	0	1098	998	981
25 HOUR																																										
AVG. TEMP.	1591	1586	1558	1574	1514	1592	1575	1594	1569	1585	1561	1588	1215	1388	964	1468	1395	1393	1339	1389	1174	1398	1269	1448	1184	1203	1097	1284	1089	1215	955	1211	988	1225	928	1265	887	899	0	1183	1007	1088
STD. DEV.	16	2	14	8	27	2	15	3	8	3	11	13	10	5	9	3	28	27	5	7	4	7	2	3	11	6	13	8	16	8	9	6	5	2	16	7	8	48	0	48	14	13
HI TEMP.	1614	1587	1582	1584	1567	1595	1595	1597	1570	1588	1587	1592	1229	1398	976	1475	1425	1427	1351	1396	1185	1483	1272	1451	1115	1217	1181	1219	1142	1232	971	1224	989	1227	969	1275	895	909	0	1164	1032	1086
LO TEMP.	1564	1579	1535	1563	1479	1589	1544	1586	1539	1577	1567	1579	1199	1380	944	1457	1370	1374	1328	1384	1163	1395	1264	1444	1091	1187	1077	1191	1074	1284	942	1195	974	1222	962	1254	877	899	0	1098	998	981
30 HOUR																																										
AVG. TEMP.	1593	1586	1559	1565	1495	1596	1562	1595	1546	1584	1563	1590	1211	1383	964	1463	1413	1418	1342	1392	1179	1408	1267	1445	1116	1196	1089	1199	1188	1211	964	1215	977	1226	926	1267	889	899	0	1184	997	988
STD. DEV.	13	3	6	4	17	1	28	4	14	2	16	4	10	5	8	3	28	27	5	7	3	1	2	3	11	6	13	8	16	8	9	6	5	2	16	7	8	48	0	48	14	13
HI TEMP.	1602	1588	1563	1567	1587	1596	1582	1597	1556	1587	1574	1592	1212	1389	969	1463	1428	1421	1344	1393	1182	1401	1248	1445	1120	1210	1198	1208	1139	1221	964	1216	988	1226	933	1268	893	909	0	1184	1007	1088
LO TEMP.	1583	1584	1555	1562	1483	1595	1542	1592	1536	1584	1551	1587	1210	1376	958	1462	1406	1415	1340	1391	1175	1398	1265	1444	1111	1193	1047	1198	1076	1288	964	1213	974	1225	918	1266	892	899	0	1182	991	993
35 HOUR																																										
AVG. TEMP.	1599	1585	1545	1569	1544	1594	1577	1594	1543	1587	1556	1591	1219	1386	971	1465	1411	1398	1348	1391	1175	1408	1268	1445	1184	1199	1183	1282	1118	1214	956	1214	981	1227	925	1264	892	899	0	1184	997	988
STD. DEV.	12	3	18	6	12	1	10	1	7	1	8	2	10	5	8	4	16	17	4	9	5	3	2	4	11	6	13	8	16	8	9	6	5	2	16	7	8	48	0	48	14	13
HI TEMP.	1613	1589	1587	1575	1564	1595	1591	1597	1552	1584	1566	1593	1224	1392	985	1470	1417	1425	1344	1397	1179	1463	1274	1443	1115	1211	1189	1284	1137	1225	962	1219	989	1229	952	1272	895	909	0	1184	1007	1088
LO TEMP.	1589	1582	1538	1559	1532	1592	1562	1595	1536	1586	1549	1589	1209	1386	967	1459	1375	1371	1327	1386	1172	1397	1265	1442	1097	1189	1098	1198	1094	1295	947	1289	975	1226	911	1262	898	899	0	1182	994	996
40 HOUR																																										
AVG. TEMP.	1592	1584	1571	1567	1529	1594	1567	1597	1543	1587	1559	1591	1215	1387	972	1469	1398	1392	1343	1391	1174	1398	1266	1444	1187	1197	1098	1201	1136	1222	955	1215	988	1227	925	1268	889	899	0	1184	997	988
STD. DEV.	22	4	17	3	20	2	15	9	3	28	27	5	10	5	9	3	28	27	5	7	3	1	2	3	11	6	13	8	16	8	9	6	5	2	16	7	8	48	0	48	14	13
HI TEMP.	1614	1589	1583	1572	1545	1595	1596	1600	1552	1590	1571	1596	1227	1395	981	1474	1438	1437	1346	1396	1188	1402	1269	1444	1106	1193	1093	1201	1195	1232	958	1219	947	1224	929	1272	895	909	0	1184	1007	1088
LO TEMP.	1569	1581	1541	1565	1499	1592	1536	1592	1530	1584	1541	1587	1202	1380	961	1466	1367	1364	1335	1388	1163	1395	1264	1441	1096	1193	1081	1194	1105	1216	958	1211										

Table C-3 (Cont'd)

Heat Exchanger Probes Temperature History (Run 80)

LOCATION PORT NO. SPEC. MAT. SPEC. LOC. DATA LOG NO.	IN BED										ABOVE BED										IN BED										ABOVE BED										IN BED										ABOVE BED									
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50										
	DEGREES FAHRENHEIT																																																											
75 HOUR																																																												
AVG. TEMP.	1281	1278	1269	1286	1249	1292	1328	1339	1297	1327	1318	1331	1068	1169	906	1231	1170	1174	1198	1204	1061	1209	1153	1242	1609	1662	967	1661	1025	1101	835	1031	756	976	819	1089	0	876	0	997	951	937																		
STD. DEV.	443	425	395	403	362	396	325	355	300	348	323	335	247	326	223	359	292	297	208	244	107	251	181	295	149	204	130	200	165	233	150	241	295	358	137	251	0	71	0	155	118	98																		
HI TEMP.	1612	1547	1572	1584	1529	1584	1578	1596	1514	1578	1559	1591	1239	1411	992	1500	1394	1402	1351	1390	1176	1397	1290	1452	1111	1232	1093	1206	1141	1284	952	1216	973	1235	924	1282	0	926	0	1108	1041	1014																		
LO TEMP.	657	715	727	781	759	797	885	862	865	858	885	859	677	707	473	743	753	753	891	856	686	861	843	857	767	772	770	775	771	785	684	751	380	515	664	812	0	752	0	772	758	766																		
80 HOUR																																																												
AVG. TEMP.	1581	1582	1555	1579	1537	1583	1558	1599	1511	1580	1552	1592	1220	1398	948	1495	1481	1481	1342	1384	1156	1388	1269	1442	1107	1196	1056	1218	1171	1281	952	1215	979	1235	925	1272	0	920	0	1169	1034	979																		
STD. DEV.	13	3	14	7	23	3	18	1	5	1	10	2	5	5	9	7	22	22	2	2	11	5	3	2	8	4	5	6	10	6	7	7	3	2	10	2	0	10	0	5	2	15																		
HI TEMP.	1604	1585	1570	1587	1554	1586	1585	1600	1515	1582	1564	1595	1234	1403	962	1505	1417	1416	1344	1346	1168	1393	1273	1440	1118	1202	1062	1225	1187	1289	965	1221	982	1238	936	1274	0	931	0	1115	1037	995																		
LO TEMP.	1569	1579	1538	1571	1497	1579	1541	1596	1502	1579	1537	1590	1220	1392	940	1486	1362	1363	1340	1381	1141	1381	1266	1440	1099	1193	1049	1216	1164	1272	947	1203	975	1232	914	1269	0	907	0	1103	1031	962																		
85 HOUR																																																												
AVG. TEMP.	1573	1582	1562	1578	1494	1583	1543	1598	1507	1580	1540	1591	1222	1396	948	1472	1376	1377	1334	1343	1158	1390	1275	1446	1104	1189	1058	1232	1148	1284	951	1208	980	1236	924	1272	0	925	0	1106	1041	974																		
STD. DEV.	20	2	5	4	19	1	47	2	11	3	27	5	5	5	9	7	22	22	2	2	11	5	3	2	13	6	2	10	29	14	10	13	7	2	12	2	0	11	0	6	1	9																		
HI TEMP.	1595	1584	1568	1581	1520	1584	1585	1599	1514	1583	1556	1597	1230	1400	950	1476	1409	1397	1338	1388	1166	1391	1280	1452	1117	1198	1046	1240	1182	1299	958	1223	985	1237	933	1274	0	933	0	1110	1042	984																		
LO TEMP.	1595	1580	1559	1574	1487	1582	1492	1596	1494	1578	1508	1587	1218	1392	944	1467	1353	1362	1328	1378	1158	1390	1271	1442	1091	1184	1056	1221	1130	1273	939	1198	972	1234	911	1270	0	913	0	1100	1041	966																		
90 HOUR																																																												
AVG. TEMP.	1590	1585	1560	1577	1518	1584	1562	1596	1519	1578	1562	1580	1224	1393	940	1464	1392	1394	1345	1385	1168	1387	1271	1442	1104	1191	1057	1217	1099	1243	950	1204	982	1234	887	1249	0	991	0	1084	1040	979																		
STD. DEV.	15	2	12	4	17	1	17	1	10	2	17	3	6	4	7	4	16	16	12	8	2	5	2	6	3	10	6	18	12	43	31	11	10	3	2	12	10	0	31	0	149	2	14																	
HI TEMP.	1612	1588	1573	1582	1563	1585	1587	1596	1527	1580	1579	1592	1227	1397	947	1468	1410	1417	1356	1388	1178	1390	1277	1440	1120	1198	1075	1227	1173	1296	961	1217	986	1237	908	1265	0	1008	0	1078	1042	995																		
LO TEMP.	1576	1582	1544	1571	1495	1583	1541	1594	1503	1576	1537	1585	1214	1386	929	1460	1369	1366	1333	1383	1162	1384	1264	1439	1095	1182	1050	1199	1067	1228	934	1194	979	1232	878	1241	0	936	0	1023	1036	959																		
95 HOUR																																																												
AVG. TEMP.	1606	1584	1556	1580	1518	1584	1569	1595	1519	1578	1567	1587	1225	1394	956	1467	1403	1400	1346	1386	1167	1388	1271	1440	1105	1188	1076	1217	1059	1204	951	1206	976	1232	894	1245	0	1010	0	1054	1037	994																		
STD. DEV.	8	1	12	7	17	3	14	2	5	2	12	3	3	4	4	13	13	17	2	4	5	2	3	1	9	1	10	3	44	35	6	5	3	3	5	2	6	0	3	0	5	2	6																	
HI TEMP.	1612	1584	1572	1590	1567	1588	1584	1596	1527	1580	1586	1592	1221	1396	967	1471	1412	1413	1346	1391	1173	1390	1275	1442	1115	1190	1093	1221	1115	1241	956	1212	980	1235	894	1257	0	1015	0	1060	1039	1042																		
LO TEMP.	1593	1582	1539	1573	1501	1581	1582	1593	1512	1576	1555	1583	1221	1389	933	1463	1380	1372	1343	1382	1162	1384	1267	1439	1091	1187	1067	1214	1012	1163	943	1200	973	1227	878	1240	0	1007	0	1050	1034	986																		
100 HOUR																																																												
AVG. TEMP.	1603	1586	1561	1578	1530	1580	1578	1588	1531	1573	1573	1579	1220	1387	970	1459	1405	1408	1346	1400	1191	1400	1273	1445	1114	1183	1103	1212	1087	1146	954	1208	981	1228	891	1234	0	1037	0	1051	1015	1010																		
STD. DEV.	14	2	10	11	34	5	21	10	25	9	19	14	11	4	16	8	26	23	11	12	9	7	7	3	10	6	17	10	6	12	12	9	10	5	17	11	0	23	0	7	2	9	14																	
HI TEMP.	1613	1589	1578	1596	1567	1587	1604	1584	1573	1579	1597	1587	1209	1379	947	1447	1376	1384	1339	1382	1176	1390	1267	1443	1101	1176	1090	1198	999	1131	934	1196	971	1221	879	1224	0	1019	0	1041	1006	980																		
LO TEMP.	1580	1584	1555	1569	1490	1575	1558	1576	1515	1558	1556	1555	1234	1388	991	1449	1400	1400	1354	1403	1200	1400	1287	1444	1125	1187	1095	1198	1018	1141	957	1202	981	1223	898	1226	0	1072	0	1049	1010	1014																		
105 HOUR																																																												
AVG. TEMP.	1592	1574	1561	1561	1531	1568	1548	1575	1521	1561	1556	1564	1234	1398	967	1471	1412	1413	1346	1391	1173	1390	1275	1442	1115	1190	1093	1221	1115	1241	956	1212	980	1235	894	1257	0	1015	0	1060	1039	1042																		
STD. DEV.	21	30	18	29	27	22	14	38	6	34	19	40	19	9	17	19	31	34	14	6	7	7	4	30	10	19	13	25	12	14	10	4	3	16	9	17	0	62	0	149	11	25																		
HI TEMP.	1611	1569	1584	1576	1546	1586	1563	1593	1530	1570	1577	1590	1263	1401	1000	1460	1452	1455	1418	1417	1270	1404	1330	1453	1105	1174	1074	1176	1002	1123	946	1186	977	1195	878	1197	0	1037	0	1015	997	981																		
LO TEMP.	1561	1521	1541	1510	1511	1529	1531	1504	1510	1501	1524	1495	1216	1377	967	1416	1374	1369	1337	1398	1172	1391	1273	1422	1105	1174	1074	1176	1002	1123	946	1186	977	1195	878	1197	0	1037	0	1015	997	981																		
110 HOUR																																																												
AVG. TEMP.	1525	1515	1506	1502	1479	1509	1522	1541	1480	1528	1514	1534	1227	1361	934	1415	1364	1363	1339	1377	1215	1386	1285	1420	1115	1193	1120	1194	1036	1146	976	1205	941	1191	893	1215	0	1069	0	996	1025	1025																		
STD. DEV.	157	155	146	151	132	149	105	122	77	116	97	120	12	65	57	98	71	67	8	37	70	41	32	57	47	11	58	14	71	10	41	18	76	86	19	45	0	74	0	43	27	32																		
HI TEMP.	1607	1587	1580	1573	1568	1580	1594	1598	1527	1581	1578	1593	1246	1393	963	1462	1427	1418	1351	1404	1241	1407	1284	1449	1126	1209	1224	1216	1163	1154	1050	1216	979	1234	926	1237	0	1198	0	1021	1072	1086																		
LO TEMP.	1245	1239	1246	1232	1246	1243	1341	1323	1343	1321	1342	1319	1218	1245	832	1242	1252	1252	1328	1312	1191	1341	1267	1318	1102	1186	1069	1178	995	1131	952	1173	809	1036	877	1135	0	1026																						

Table C-3 (Cont'd)

Heat Exchanger Probes Temperature History (Run 80)

LOCATION	IN BED										ABOVE BED										IN BED	ABOVE BED										IN BED	ABOVE BED									
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20		21	22	23	24	25	26	27	28	29	30		31	32	33	34	35	36	37	38	39	40
PORT NO.																																										
SPEC. MAT.																																										
SPEC. LOC.																																										
DATA LOG NO.																																										
DEGREES FAHRENHEIT																																										
145 HOUR																																										
AVG. TEMP.	1594	1578	1552	1570	1529	1586	1534	1600	1502	1582	1536	1594	1221	1392	945	1465	1398	1398	1332	1381	1169	1394	1269	1441	1108	1136	1077	1217	1075	1216	968	1223	969	1234	877	1247	0	1022	0	1028	1023	993
STD. DEV.	11	2	18	4	27	2	31	5	17	4	28	8	7	5	18	8	30	25	6	4	14	5	3	4	12	8	10	11	35	10	13	8	3	4	12	4	0	17	0	5	3	8
HI TEMP.	1605	1581	1572	1575	1571	1588	1586	1604	1532	1585	1585	1600	1231	1397	956	1478	1427	1425	1343	1393	1186	1403	1272	1446	1119	1208	1091	1232	1137	1229	989	1232	973	1238	899	1251	0	1037	0	1032	1027	1006
LO TEMP.	1581	1577	1530	1566	1506	1583	1505	1592	1449	1575	1515	1580	1214	1345	934	1458	1359	1369	1328	1370	1152	1390	1265	1435	1094	1197	1068	1205	1053	1203	958	1210	964	1228	870	1241	0	994	0	1021	1020	985
150 HOUR																																										
AVG. TEMP.	1570	1575	1566	1560	1544	1582	1519	1602	1495	1594	1522	1600	1215	1387	944	1461	1392	1387	1330	1376	1166	1390	1272	1443	1111	1189	1087	1209	1059	1206	968	1222	972	1237	880	1249	0	1015	0	1028	1008	999
STD. DEV.	21	2	16	7	11	3	27	2	10	3	23	5	9	4	13	5	20	24	5	2	24	4	5	5	11	10	11	10	10	7	5	6	7	3	4	6	0	4	0	8	10	9
HI TEMP.	1599	1579	1573	1569	1563	1585	1592	1604	1510	1598	1558	1605	1222	1390	959	1467	1409	1415	1335	1378	1175	1405	1276	1450	1103	1199	1109	1221	1067	1215	973	1229	978	1240	886	1259	0	1019	0	1041	1019	1003
LO TEMP.	1550	1573	1533	1551	1535	1579	1490	1600	1486	1581	1495	1593	1290	1381	925	1457	1361	1361	1322	1372	1157	1395	1267	1437	1100	1186	1070	1197	1046	1196	962	1213	962	1232	876	1246	0	1099	0	1020	994	981
155 HOUR																																										
AVG. TEMP.	1575	1568	1548	1562	1523	1586	1486	1603	1486	1587	1501	1603	1217	1388	951	1468	1382	1381	1295	1344	1164	1399	1275	1448	1102	1184	1080	1214	1074	1212	968	1226	965	1239	886	1255	0	1006	0	1019	1024	1002
STD. DEV.	20	5	23	6	19	3	16	3	7	4	14	5	7	2	12	6	24	29	7	6	9	4	7	3	9	4	15	11	15	16	13	8	4	3	10	8	0	6	0	6	12	20
HI TEMP.	1599	1576	1575	1571	1567	1590	1502	1608	1494	1593	1516	1610	1226	1392	967	1479	1405	1408	1302	1351	1174	1404	1286	1452	1113	1191	1098	1224	1100	1239	987	1236	965	1242	901	1269	0	1016	0	1026	1035	1033
LO TEMP.	1558	1564	1520	1551	1496	1583	1461	1600	1476	1583	1481	1597	1218	1386	935	1460	1355	1347	1288	1337	1154	1396	1268	1444	1091	1180	1060	1199	1064	1198	951	1215	958	1235	877	1249	0	1000	0	1012	1008	980
160 HOUR																																										
AVG. TEMP.	1577	1569	1556	1571	1528	1583	1521	1602	1497	1584	1525	1598	1221	1387	970	1462	1372	1377	1306	1355	1172	1397	1271	1442	1113	1184	1096	1217	1109	1235	967	1222	966	1236	881	1237	0	1032	0	1012	1021	998
STD. DEV.	15	6	23	10	31	3	29	2	6	1	12	4	2	5	2	7	24	25	10	7	24	4	4	4	11	4	17	7	52	31	4	2	3	3	7	7	0	6	0	5	12	17
HI TEMP.	1600	1575	1582	1600	1572	1586	1559	1604	1503	1585	1538	1602	1223	1392	973	1469	1413	1420	1318	1362	1187	1400	1276	1447	1129	1189	1116	1227	1173	1271	972	1225	969	1239	885	1245	0	1025	0	1009	1028	998
LO TEMP.	1561	1559	1532	1555	1500	1580	1490	1600	1491	1583	1515	1594	1219	1382	947	1455	1356	1358	1296	1356	1165	1395	1267	1439	1100	1180	1078	1208	1061	1211	962	1219	963	1232	878	1248	0	1025	0	1007	1011	979
165 HOUR																																										
AVG. TEMP.	1589	1573	1556	1569	1559	1584	1534	1588	1524	1572	1550	1579	1229	1383	996	1458	1405	1397	1327	1367	1184	1402	1272	1447	1113	1174	1104	1207	1122	1249	975	1225	965	1230	880	1225	0	1047	0	1004	1011	993
STD. DEV.	16	2	12	8	27	5	38	22	46	19	33	27	4	4	25	9	42	43	27	13	12	4	4	4	8	11	21	7	22	12	4	4	3	1	3	4	0	43	0	4	13	15
HI TEMP.	1601	1575	1571	1575	1578	1590	1590	1601	1577	1583	1588	1596	1233	1386	1002	1467	1446	1434	1359	1381	1202	1406	1276	1450	1118	1190	1129	1216	1151	1257	983	1230	968	1231	883	1230	0	1123	0	1008	1026	1014
LO TEMP.	1566	1570	1541	1557	1528	1578	1510	1583	1495	1550	1530	1548	1225	1379	978	1449	1362	1350	1310	1356	1176	1394	1267	1441	1102	1164	1085	1202	1094	1231	963	1221	962	1229	876	1221	0	1018	0	998	996	980
170 HOUR																																										
AVG. TEMP.	1586	1571	1550	1578	1541	1582	1556	1596	1517	1578	1559	1585	1230	1391	982	1460	1375	1379	1313	1364	1184	1402	1274	1446	1107	1188	1100	1218	1172	1270	977	1222	970	1152	884	1220	0	1045	0	1001	1023	995
STD. DEV.	11	3	11	13	31	3	25	2	17	2	19	4	2	4	2	13	9	14	15	15	6	2	4	6	13	5	18	6	29	19	5	6	92	74	2	3	0	5	0	5	1	2
HI TEMP.	1603	1574	1560	1596	1558	1587	1590	1596	1543	1581	1593	1589	1236	1393	998	1466	1391	1399	1326	1373	1187	1406	1278	1450	1124	1196	1122	1222	1208	1257	980	1232	976	1233	886	1223	0	1051	0	1005	1024	996
LO TEMP.	1579	1568	1534	1568	1495	1578	1539	1592	1507	1577	1547	1579	1224	1388	964	1445	1359	1364	1295	1357	1180	1395	1270	1435	1089	1183	1078	1207	1147	1243	969	1217	964	1229	881	1218	0	1041	0	996	1023	993
175 HOUR																																										
AVG. TEMP.	1584	1570	1545	1569	1547	1583	1566	1593	1518	1577	1567	1581	1222	1385	982	1456	1396	1393	1315	1364	1186	1404	1274	1448	1109	1189	1096	1207	1043	1188	973	1216	969	1224	885	1214	0	1040	0	999	1015	1001
STD. DEV.	13	4	13	12	22	1	21	4	7	4	12	7	6	1	9	6	22	24	6	5	3	2	3	4	15	4	11	8	10	9	11	7	3	2	10	4	0	18	0	4	4	7
HI TEMP.	1602	1574	1557	1586	1568	1585	1597	1598	1527	1581	1581	1590	1228	1386	994	1461	1414	1422	1323	1370	1200	1407	1280	1452	1114	1194	1111	1215	1055	1196	984	1225	976	1227	894	1216	0	1055	0	1004	1023	1014
LO TEMP.	1569	1563	1523	1556	1518	1581	1550	1589	1508	1571	1549	1571	1215	1384	974	1448	1359	1362	1309	1358	1180	1397	1269	1443	1101	1183	1082	1195	1029	1174	958	1207	965	1221	878	1210	0	1013	0	994	998	993
180 HOUR																																										
AVG. TEMP.	1587	1570	1547	1568	1532	1583	1527	1597	1505	1581	1545	1589	1227	1389	990	1464	1362	1361	1322	1375	1179	1404	1275	1447	1112	1189	1102	1215	1051	1187	970	1216	963	1224	885	1215	0	1040	0	999	1019	1003
STD. DEV.	17	3	19	5	23	2	13	2	3	2	5	2	12	1	5	7	7	3	8	5	6	2	2	3	12	6	14	9	8	12	10	7	3	2	10	4	0	16	0	4	4	7
HI TEMP.	1601	1573	1570	1575	1544	1595	1590	1600	1510	1583	1595	1592	1236	1391	998	1475	1375	1365	1329	1378	1190	1407	1280	1449	1126	1191	1113	1226	1045	1203	983	1221	968	1227	892	1217	0	1046	0	1004	1023	1021
LO TEMP.	1560	1566	1526	1568	1490	1581	1514	1596	1500	1579	1533	1586	1231	1388	986</																											

Table C-4

Heat Exchanger Temperature Probes (Run 81)

LOCATION PORT NO. SPEC. MAT. SPEC. LOC. DATA LOG NO.	-----IN RED-----																	-----ABOVE RED-----																	-----IN RED-----																	-----ABOVE RED-----																	-----IN RED-----																	-----ABOVE RED-----																																																										
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18																																				
	DEGREES FAHRENHEIT																																				DEGREES FAHRENHEIT																																				DEGREES FAHRENHEIT																																				DEGREES FAHRENHEIT																																			
5 HOUR	[Temperature Data for 5 Hour]																																				[Temperature Data for 5 Hour]																																				[Temperature Data for 5 Hour]																																				[Temperature Data for 5 Hour]																																			
10 HOUR	[Temperature Data for 10 Hour]																																				[Temperature Data for 10 Hour]																																				[Temperature Data for 10 Hour]																																				[Temperature Data for 10 Hour]																																			
15 HOUR	[Temperature Data for 15 Hour]																																				[Temperature Data for 15 Hour]																																				[Temperature Data for 15 Hour]																																				[Temperature Data for 15 Hour]																																			
20 HOUR	[Temperature Data for 20 Hour]																																				[Temperature Data for 20 Hour]																																				[Temperature Data for 20 Hour]																																				[Temperature Data for 20 Hour]																																			
25 HOUR	[Temperature Data for 25 Hour]																																				[Temperature Data for 25 Hour]																																				[Temperature Data for 25 Hour]																																				[Temperature Data for 25 Hour]																																			
30 HOUR	[Temperature Data for 30 Hour]																																				[Temperature Data for 30 Hour]																																				[Temperature Data for 30 Hour]																																				[Temperature Data for 30 Hour]																																			
35 HOUR	[Temperature Data for 35 Hour]																																				[Temperature Data for 35 Hour]																																				[Temperature Data for 35 Hour]																																				[Temperature Data for 35 Hour]																																			
40 HOUR	[Temperature Data for 40 Hour]																																				[Temperature Data for 40 Hour]																																				[Temperature Data for 40 Hour]																																				[Temperature Data for 40 Hour]																																			
45 HOUR	[Temperature Data for 45 Hour]																																				[Temperature Data for 45 Hour]																																				[Temperature Data for 45 Hour]																																				[Temperature Data for 45 Hour]																																			
50 HOUR	[Temperature Data for 50 Hour]																																				[Temperature Data for 50 Hour]																																				[Temperature Data for 50 Hour]																																				[Temperature Data for 50 Hour]																																			
55 HOUR	[Temperature Data for 55 Hour]																																				[Temperature Data for 55 Hour]																																				[Temperature Data for 55 Hour]																																				[Temperature Data for 55 Hour]																																			
60 HOUR	[Temperature Data for 60 Hour]																																				[Temperature Data for 60 Hour]																																				[Temperature Data for 60 Hour]																																				[Temperature Data for 60 Hour]																																			
65 HOUR	[Temperature Data for 65 Hour]																																				[Temperature Data for 65 Hour]																																				[Temperature Data for 65 Hour]																																				[Temperature Data for 65 Hour]																																			
70 HOUR	[Temperature Data for 70 Hour]																																				[Temperature Data for 70 Hour]																																				[Temperature Data for 70 Hour]																																				[Temperature Data for 70 Hour]																																			

Table C-4 (Cont'd)

Heat Exchanger Probes Temperature History (Run 81)

LOCATION	-----IN RED-----												-----ABOVE RED-----												-----IN RED-----												-----ABOVE RED-----											
	PORT NO.	1	1	3	4	5	13	13	15	15	17	17	2	2	4	4	6	6	14	14	16	16	18	18	7	7	9	9	11	11	19	19	20	20	22	22	8	8	12	12	10	10						
SPEC. MAT.	X	M	M	X	M	X	X	M	M	X	M	X	X	X	X	0	X	8	X	8	X	8	8	X	3	H	A	3	H	3	H	3	3	8	8	3	2	0	1	0	9	2						
SPEC. LOC.	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0						
DATA LOG NO.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42						
	DEGREES FAHRENHEIT												DEGREES FAHRENHEIT												DEGREES FAHRENHEIT												DEGREES FAHRENHEIT											
145 HOUR	AVG. TEMP.	1549	1582	1553	1585	1516	1604	1620	1536	1597	1523	1565	1518	1243	1396	1023	1438	1407	1393	1404	1295	1294	1330	1322	1446	1144	1112	1100	1237	1070	1213	1168	1138	1054	1151	931	1103	0	903	0	1068	1012	975					
	STD. DEV.	12	4	18	6	14	2	3	3	3	4	5	3	2	3	4	5	62	56	10	2	15	5	11	2	13	6	7	5	14	20	6	2	7	3	19	4	0	11	0	3	7	10					
	HI TEMP.	1588	1587	1578	1542	1575	1607	1623	1538	1600	1526	1572	1520	1245	1400	1026	1447	1461	1467	1416	1296	1306	1337	1342	1448	1164	1121	1106	1240	1095	1226	1178	1141	1065	1153	949	1107	0	914	0	1071	1021	992					
	LO TEMP.	1555	1574	1536	1578	1497	1603	1416	1531	1592	1517	1560	1514	1239	1393	1016	1436	1371	1323	1395	1291	1268	1325	1314	1443	1131	1105	1089	1227	1051	1174	1162	1135	1046	1146	903	1096	0	890	0	1064	1005	967					
150 HOUR	AVG. TEMP.	1576	1584	1551	1586	1509	1604	1614	1525	1604	1509	1571	1508	1237	1390	1021	1439	1380	1382	1403	1293	1281	1329	1322	1444	1131	1137	1129	1257	1043	1218	1183	1142	1053	1153	912	1093	0	906	0	1076	995	977					
	STD. DEV.	14	3	20	6	9	2	4	6	4	7	8	5	3	2	6	5	57	64	8	2	16	3	2	3	11	16	22	16	34	7	23	7	27	7	39	7	0	9	0	14	23	11					
	HI TEMP.	1590	1587	1568	1595	1514	1606	1619	1532	1608	1518	1583	1515	1241	1393	1029	1447	1438	1459	1413	1294	1297	1334	1326	1448	1143	1125	1159	1267	1049	1230	1206	1149	1074	1159	948	1099	0	920	0	1095	1014	988					
	LO TEMP.	1553	1580	1518	1578	1494	1602	1608	1518	1598	1502	1562	1502	1234	1387	1014	1433	1325	1289	1393	1290	1262	1325	1321	1439	1121	1096	1094	1229	1043	1211	1144	1130	1006	1141	853	1081	0	895	0	1056	956	960					
155 HOUR	AVG. TEMP.	1571	1582	1565	1544	1514	1602	1613	1524	1606	1507	1572	1505	1241	1394	1021	1439	1325	1360	1401	1291	1288	1327	1321	1442	1127	1119	1103	1242	1041	1223	1200	1149	1070	1166	925	1101	0	907	0	1084	1002	978					
	STD. DEV.	10	3	14	6	25	1	4	4	5	5	11	3	4	4	4	2	39	40	9	2	18	2	8	3	9	6	23	17	14	10	5	2	7	6	20	1	0	12	0	14	1	15					
	HI TEMP.	1582	1584	1579	1590	1551	1604	1616	1527	1611	1513	1584	1509	1247	1397	1026	1441	1385	1418	1413	1295	1306	1330	1331	1444	1135	1129	1140	1272	1102	1213	1205	1151	1078	1174	942	1102	0	919	0	1104	1004	998					
	LO TEMP.	1559	1579	1543	1575	1494	1600	1607	1516	1598	1500	1555	1500	1238	1389	1017	1437	1287	1312	1392	1289	1265	1326	1312	1437	1114	1112	1083	1228	1044	1207	1191	1146	1063	1160	895	1100	0	894	0	1070	1001	966					
160 HOUR	AVG. TEMP.	1580	1584	1554	1585	1521	1604	1616	1527	1602	1515	1564	1511	1244	1393	1021	1441	1369	1379	1400	1291	1278	1328	1319	1445	1126	1117	1102	1274	1042	1220	1198	1144	1071	1177	847	1098	0	915	0	1079	1002	985					
	STD. DEV.	7	3	11	4	13	2	3	2	6	2	4	1	4	3	8	7	49	59	10	1	11	2	2	1	5	4	8	5	24	10	4	3	5	3	19	4	0	5	0	27	4	8					
	HI TEMP.	1584	1587	1564	1588	1533	1604	1619	1529	1611	1517	1572	1512	1248	1397	1035	1450	1413	1440	1412	1292	1293	1329	1322	1446	1132	1129	1113	1242	1120	1229	1206	1152	1080	1191	920	1101	0	920	0	1114	1006	995					
	LO TEMP.	1570	1580	1547	1580	1494	1601	1613	1524	1596	1513	1560	1509	1240	1388	1013	1431	1300	1310	1391	1289	1267	1325	1316	1443	1118	1110	1090	1229	1058	1204	1189	1146	1066	1173	873	1092	0	908	0	1058	996	976					
165 HOUR	AVG. TEMP.	1565	1581	1555	1581	1525	1601	1616	1526	1604	1512	1576	1508	1244	1391	1021	1437	1379	1382	1409	1288	1320	1358	1320	1448	1201	1174	1078	1214	1043	1216	1198	1144	1102	1208	977	1148	0	997	0	1050	1048	1022					
	STD. DEV.	15	3	17	4	17	2	4	3	4	4	9	4	3	3	9	6	64	52	2	1	12	3	8	3	12	4	4	3	4	4	9	2	4	7	25	5	0	6	0	5	8	12					
	HI TEMP.	1583	1584	1574	1586	1551	1603	1619	1528	1609	1516	1588	1512	1247	1393	1032	1446	1460	1440	1410	1289	1338	1362	1327	1449	1220	1142	1086	1218	1047	1225	1208	1152	1113	1220	1021	1155	0	1005	0	1059	1048	1031					
	LO TEMP.	1553	1577	1538	1576	1510	1598	1609	1520	1594	1505	1565	1503	1240	1387	1006	1429	1285	1320	1406	1287	1306	1355	1308	1443	1188	1167	1066	1209	1052	1208	1189	1146	1092	1201	960	1144	0	988	0	1046	1026	1001					
170 HOUR	AVG. TEMP.	1564	1581	1550	1582	1519	1601	1616	1526	1603	1513	1571	1509	1247	1393	1026	1436	1361	1366	1397	1286	1321	1359	1321	1448	1201	1175	1077	1216	1040	1225	1199	1147	1097	1215	979	1153	0	985	0	1054	1039	1022					
	STD. DEV.	9	3	20	4	25	1	4	5	4	5	8	3	3	4	7	7	69	65	10	3	19	2	12	3	4	6	12	6	22	10	5	2	6	4	24	7	0	10	0	9	4	11					
	HI TEMP.	1577	1585	1560	1589	1561	1602	1621	1534	1607	1519	1583	1512	1251	1399	1032	1445	1448	1460	1413	1290	1343	1362	1330	1452	1210	1182	1086	1222	1116	1238	1203	1150	1105	1218	1016	1161	0	997	0	1068	1044	1037					
	LO TEMP.	1556	1578	1534	1579	1494	1600	1609	1519	1598	1505	1561	1505	1242	1390	1015	1427	1293	1299	1388	1283	1303	1356	1302	1445	1189	1164	1056	1207	1042	1212	1191	1144	1092	1210	957	1147	0	972	0	1044	1034	1005					
175 HOUR	AVG. TEMP.	1572	1583	1570	1587	1516	1604	1615	1524	1605	1512	1564	1509	1244	1393	1053	1447	1414	1383	1398	1283	1327	1360	1336	1454	1204	1177	1068	1212	1072	1224	1202	1149	1045	1223	955	1153	0	972	0	1044	1034	1005					
	STD. DEV.	14	3	7	1	15	3	4	4	4	4	3	2	5	2	13	9	44	69	8	2	14	1	9	2	4	4	4	5	10	9	4	2	6	1	16	4	0	10	0	9	4	11					
	HI TEMP.	1590	1585	1579	1588	1534	1607	1618	1527	1610	1515	1567	1511	1248	1395	1064	1450	1454	1471	1409	1285	1345	1360	1344	1456	1211	1182	1079	1218	1079	1241	1210	1151	1102	1224	973	1157	0	997	0	1068	1044	1037					
	LO TEMP.	1558	1578	1561	1587	1501	1601	1610	1519	1600	1506	1559	1506	1237	1390	1041	1430	1373	1324	1390	1281	1312	1359	1325	1452	1199	1174	1058	1206	1057	1221	1193	1147	1089	1222	939	1150	0	972	0	1044	1034	1005					

Table C-5
Heat Exchanger Probes
Temperature History (Run 106)

LOCATION PORT NO. SPEC. MAT. SPEC. LOC.	-----IN RED-----												-----ABOVE BED-----												-----IN RED-----												-----ABOVE BED-----												-----IN RED-----																				
	1	1	3	3	13	13	15	15	2	2	6	14	18	18	7	7	11	11	19	20	20	8	12	1	1	3	3	13	13	15	15	2	2	6	14	18	18	7	7	11	11	19	20	20	8	12	1	1	3	3	13	13	15	15	2	2	6	14	18	18	7	7	11	11	19	20	20	8	12
	DEGREES FAHRENHEIT																								DEGREES FAHRENHEIT																																												
5 HOUR	5/29/79																								5/29/79																																												
AVG. TEMP.	1577	1605	1548	1568	1540	1580	1562	1591	1241	1402	1461	1430	1270	1458	1163	1278	1065	1250	1189	1038	1147	994	0	1577	1605	1548	1568	1540	1580	1562	1591	1241	1402	1461	1430	1270	1458	1163	1278	1065	1250	1189	1038	1147	994	0	1577	1605	1548	1568	1540	1580	1562	1591	1241	1402	1461	1430	1270	1458	1163	1278	1065	1250	1189	1038	1147	994	0
STD. DEV.	13	4	20	8	23	3	6	6	6	4	39	12	8	4	29	14	8	9	24	11	8	12	0	13	4	20	8	23	3	6	6	6	4	39	12	8	4	29	14	8	9	24	11	8	12	0	13	4	20	8	23	3	6	6	6	4	39	12	8	4	29	14	8	9	24	11	8	12	0
MI TEMP.	1598	1611	1574	1582	1573	1583	1571	1598	1253	1410	1573	1454	1288	1464	1194	1295	1079	1262	1222	1058	1160	1013	0	1598	1611	1574	1582	1573	1583	1571	1598	1253	1410	1573	1454	1288	1464	1194	1295	1079	1262	1222	1058	1160	1013	0	1598	1611	1574	1582	1573	1583	1571	1598	1253	1410	1573	1454	1288	1464	1194	1295	1079	1262	1222	1058	1160	1013	0
LO TEMP.	1560	1577	1518	1553	1502	1572	1553	1579	1234	1397	1425	1412	1261	1451	1076	1262	1054	1236	1158	1022	1135	976	0	1560	1577	1518	1553	1502	1572	1553	1579	1234	1397	1425	1412	1261	1451	1076	1262	1054	1236	1158	1022	1135	976	0	1560	1577	1518	1553	1502	1572	1553	1579	1234	1397	1425	1412	1261	1451	1076	1262	1054	1236	1158	1022	1135	976	0
10 HOUR	5/30/79																								5/30/79																																												
AVG. TEMP.	1578	1589	1560	1575	1512	1588	1565	1593	1237	1395	1468	1395	1252	1434	1144	1254	1057	1250	1179	1001	1142	953	0	1578	1589	1560	1575	1512	1588	1565	1593	1237	1395	1468	1395	1252	1434	1144	1254	1057	1250	1179	1001	1142	953	0	1578	1589	1560	1575	1512	1588	1565	1593	1237	1395	1468	1395	1252	1434	1144	1254	1057	1250	1179	1001	1142	953	0
STD. DEV.	15	11	11	10	30	6	10	6	6	9	22	21	19	8	14	21	13	12	20	26	9	36	0	15	11	11	10	30	6	10	6	6	9	22	21	19	8	14	21	13	12	20	26	9	36	0	15	11	11	10	30	6	10	6	6	9	22	21	19	8	14	21	13	12	20	26	9	36	0
MI TEMP.	1603	1611	1575	1595	1577	1594	1592	1603	1246	1410	1497	1439	1288	1451	1169	1297	1074	1270	1215	1059	1155	1028	0	1603	1611	1575	1595	1577	1594	1592	1603	1246	1410	1497	1439	1288	1451	1169	1297	1074	1270	1215	1059	1155	1028	0	1603	1611	1575	1595	1577	1594	1592	1603	1246	1410	1497	1439	1288	1451	1169	1297	1074	1270	1215	1059	1155	1028	0
LO TEMP.	1556	1577	1539	1566	1473	1576	1555	1581	1225	1382	1430	1366	1202	1425	1117	1229	1038	1223	1144	966	1126	907	0	1556	1577	1539	1566	1473	1576	1555	1581	1225	1382	1430	1366	1202	1425	1117	1229	1038	1223	1144	966	1126	907	0	1556	1577	1539	1566	1473	1576	1555	1581	1225	1382	1430	1366	1202	1425	1117	1229	1038	1223	1144	966	1126	907	0
15 HOUR	5/30/79																								5/30/79																																												
AVG. TEMP.	1569	1585	1548	1567	1488	1585	1561	1588	1239	1393	1467	1388	1263	1432	1145	1239	1062	1242	1180	993	1159	948	0	1569	1585	1548	1567	1488	1585	1561	1588	1239	1393	1467	1388	1263	1432	1145	1239	1062	1242	1180	993	1159	948	0	1569	1585	1548	1567	1488	1585	1561	1588	1239	1393	1467	1388	1263	1432	1145	1239	1062	1242	1180	993	1159	948	0
STD. DEV.	12	9	23	5	34	2	4	3	10	7	21	20	26	5	15	17	7	17	19	23	11	26	0	12	9	23	5	34	2	4	3	10	7	21	20	26	5	15	17	7	17	19	23	11	26	0	12	9	23	5	34	2	4	3	10	7	21	20	26	5	15	17	7	17	19	23	11	26	0
MI TEMP.	1587	1603	1581	1576	1543	1588	1566	1593	1259	1406	1501	1430	1286	1439	1166	1268	1073	1271	1217	1036	1179	1002	0	1587	1603	1581	1576	1543	1588	1566	1593	1259	1406	1501	1430	1286	1439	1166	1268	1073	1271	1217	1036	1179	1002	0	1587	1603	1581	1576	1543	1588	1566	1593	1259	1406	1501	1430	1286	1439	1166	1268	1073	1271	1217	1036	1179	1002	0
LO TEMP.	1547	1572	1513	1553	1426	1582	1553	1583	1219	1384	1428	1352	1169	1423	1117	1213	1049	1222	1140	957	1137	908	0	1547	1572	1513	1553	1426	1582	1553	1583	1219	1384	1428	1352	1169	1423	1117	1213	1049	1222	1140	957	1137	908	0	1547	1572	1513	1553	1426	1582	1553	1583	1219	1384	1428	1352	1169	1423	1117	1213	1049	1222	1140	957	1137	908	0
20 HOUR	5/30/79																								5/30/79																																												
AVG. TEMP.	1573	1580	1551	1566	1501	1585	1563	1589	1243	1393	1429	1380	1273	1435	1142	1237	1063	1239	1172	997	1159	949	0	1573	1580	1551	1566	1501	1585	1563	1589	1243	1393	1429	1380	1273	1435	1142	1237	1063	1239	1172	997	1159	949	0	1573	1580	1551	1566	1501	1585	1563	1589	1243	1393	1429	1380	1273	1435	1142	1237	1063	1239	1172	997	1159	949	0
STD. DEV.	15	11	23	5	35	2	7	3	9	8	47	15	4	5	15	21	11	12	19	28	9	36	0	15	11	23	5	35	2	7	3	9	8	47	15	4	5	15	21	11	12	19	28	9	36	0	15	11	23	5	35	2	7	3	9	8	47	15	4	5	15	21	11	12	19	28	9	36	0
MI TEMP.	1616	1605	1590	1574	1547	1589	1572	1593	1256	1406	1486	1407	1283	1446	1161	1283	1078	1257	1214	1053	1173	1037	0	1616	1605	1590	1574	1547	1589	1572	1593	1256	1406	1486	1407	1283	1446	1161	1283	1078	1257	1214	1053	1173	1037	0	1616	1605	1590	1574	1547	1589	1572	1593	1256	1406	1486	1407	1283	1446	1161	1283	1078	1257	1214	1053	1173	1037	0
LO TEMP.	1556	1566	1516	1558	1450	1582	1555	1584	1228	1379	1355	1350	1254	1429	1111	1203	1046	1221	1142	961	1140	904	0	1556	1566	1516	1558	1450	1582	1555	1584	1228	1379	1355	1350	1254	1429	1111	1203	1046	1221	1142	961	1140	904	0	1556	1566	1516	1558	1450	1582	1555	1584	1228	1379	1355	1350	1254	1429	1111	1203	1046	1221	1142	961	1140	904	0
25 HOUR	5/30/79																								5/30/79																																												
AVG. TEMP.	1574	1581	1550	1562	1494	1586	1562	1586	1238	1393	1381	1379	1265	1431	1142	1241	1060	1238	1161	995	1157	943	0	1574	1581	1550	1562	1494	1586	1562	1586	1238	1393	1381	1379	1265	1431	1142	1241	1060	1238	1161	995	1157	943	0	1574	1581	1550	1562	1494	1586	1562	1586	1238	1393	1381	1379	1265	1431	1142	1241	1060	1238	1161	995	1157	943	0
STD. DEV.	13	9	22	5	26	2	11	3	9	8	21	18	9	4	24	20	10	9	21	27	8	32	0	13	9	22	5	26	2	11	3	9	8	21	18	9	4	24	20	10	9	21	27	8	32	0	13	9	22	5	26	2	11	3	9	8	21	18	9	4	24	20	10	9	21	27	8	32	0
MI TEMP.	1594	1598	1584	1571	1545	1588	1594	1592	1253	1406	1415	1399	1278	1439	1183	1286	1072	1257	1184	1066	1170	1026	0	1594	1598	1584	1571	1545	1588	1594	1592	1253	1406	1415	1399	1278	1439	1183	1286	1072	1257	1184	1066	1170	1026	0	1594	1598	1584	1571	1545	1588	1594	1592	1253	1406	1415	1399	1278	1439	1183	1286	1072	1257	1184	1066	1170	1026	0
LO TEMP.	1558	1567	1519	1556	1457	1582	1550	1582	1223	1384	1354	1341	1246	1423	1096																																																						

Table C-5 (Cont'd)

Heat Exchanger Robes

Temperature History (Run 106)

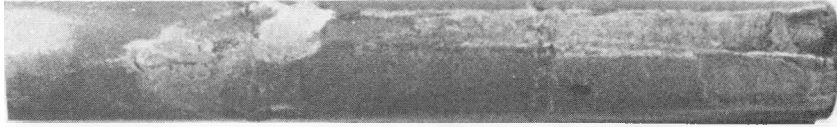
LOCATION PORT NO. SPEC. MAT. SPEC. LOC.	-----IN BED-----										-----ABOVE BED-----										-----IN BED-----										-----ABOVE BED-----										-----IN BED-----										-----ABOVE BED-----										-----IN BED-----										-----ABOVE BED-----																																																																																																																
	1	1	3	3	13	13	15	15	2	2	6	14	1A	1A	7	7	11	11	19	20	20	8	12	1	1	3	3	13	13	15	15	2	2	6	14	1A	1A	7	7	11	11	19	20	20	8	12	1	1	3	3	13	13	15	15	2	2	6	14	1A	1A	7	7	11	11	19	20	20	8	12	1	1	3	3	13	13	15	15	2	2	6	14	1A	1A	7	7	11	11	19	20	20	8	12	1	1	3	3	13	13	15	15	2	2	6	14	1A	1A	7	7	11	11	19	20	20	8	12	1	1	3	3	13	13	15	15	2	2	6	14	1A	1A	7	7	11	11	19	20	20	8	12	1	1	3	3	13	13	15	15	2	2	6	14	1A	1A	7	7	11	11	19	20	20	8	12	1	1	3	3	13	13	15	15	2	2	6	14	1A	1A	7	7	11	11	19	20	20	8
	DEGREES FAHRENHEIT										DEGREES FAHRENHEIT										DEGREES FAHRENHEIT										DEGREES FAHRENHEIT										DEGREES FAHRENHEIT										DEGREES FAHRENHEIT										DEGREES FAHRENHEIT																																																																																																																										
145 HOUR	6/ 6/79										6/ 6/79										6/ 6/79										6/ 6/79										6/ 6/79										6/ 6/79										6/ 6/79																																																																																																																										
AVG. TEMP.	1573	1595	1547	1588	1501	1592	1585	1613	1223	1401	1373	1330	1264	1421	1098	1240	1057	1210	1144	1025	1197	893	981	1573	1595	1547	1588	1501	1592	1585	1613	1223	1401	1373	1330	1264	1421	1098	1240	1057	1210	1144	1025	1197	893	981	1573	1595	1547	1588	1501	1592	1585	1613	1223	1401	1373	1330	1264	1421	1098	1240	1057	1210	1144	1025	1197	893	981	1573	1595	1547	1588	1501	1592	1585	1613	1223	1401	1373	1330	1264	1421	1098	1240	1057	1210	1144	1025	1197	893	981	1573	1595	1547	1588	1501	1592	1585	1613	1223	1401	1373	1330	1264	1421	1098	1240	1057	1210	1144	1025	1197	893	981	1573	1595	1547	1588	1501	1592	1585	1613	1223	1401	1373	1330	1264	1421	1098	1240	1057	1210	1144	1025	1197	893	981																																													
STD. DEV.	10	5	20	7	22	5	4	2	11	5	6	25	7	4	11	21	10	8	19	19	7	11	9	10	5	20	7	22	5	4	2	11	5	6	25	7	4	11	21	10	8	19	19	7	11	9	10	5	20	7	22	5	4	2	11	5	6	25	7	4	11	21	10	8	19	19	7	11	9	10	5	20	7	22	5	4	2	11	5	6	25	7	4	11	21	10	8	19	19	7	11	9	10	5	20	7	22	5	4	2	11	5	6	25	7	4	11	21	10	8	19	19	7	11	9	10	5	20	7	22	5	4	2	11	5	6	25	7	4	11	21	10	8	19	19	7	11	9																																													
HI TEMP.	1596	1603	1577	1598	1530	1609	1591	1617	1242	1413	1380	1368	1272	1429	1119	1266	1072	1226	1182	1058	1207	908	997	1596	1603	1577	1598	1530	1609	1591	1617	1242	1413	1380	1368	1272	1429	1119	1266	1072	1226	1182	1058	1207	908	997	1596	1603	1577	1598	1530	1609	1591	1617	1242	1413	1380	1368	1272	1429	1119	1266	1072	1226	1182	1058	1207	908	997	1596	1603	1577	1598	1530	1609	1591	1617	1242	1413	1380	1368	1272	1429	1119	1266	1072	1226	1182	1058	1207	908	997	1596	1603	1577	1598	1530	1609	1591	1617	1242	1413	1380	1368	1272	1429	1119	1266	1072	1226	1182	1058	1207	908	997	1596	1603	1577	1598	1530	1609	1591	1617	1242	1413	1380	1368	1272	1429	1119	1266	1072	1226	1182	1058	1207	908	997																																													
LO TEMP.	1561	1585	1521	1577	1456	1588	1579	1609	1208	1395	1364	1289	1250	1417	1084	1208	1035	1197	1117	998	1181	873	965	1561	1585	1521	1577	1456	1588	1579	1609	1208	1395	1364	1289	1250	1417	1084	1208	1035	1197	1117	998	1181	873	965	1561	1585	1521	1577	1456	1588	1579	1609	1208	1395	1364	1289	1250	1417	1084	1208	1035	1197	1117	998	1181	873	965	1561	1585	1521	1577	1456	1588	1579	1609	1208	1395	1364	1289	1250	1417	1084	1208	1035	1197	1117	998	1181	873	965	1561	1585	1521	1577	1456	1588	1579	1609	1208	1395	1364	1289	1250	1417	1084	1208	1035	1197	1117	998	1181	873	965	1561	1585	1521	1577	1456	1588	1579	1609	1208	1395	1364	1289	1250	1417	1084	1208	1035	1197	1117	998	1181	873	965																																													
150 HOUR	6/ 6/79										6/ 6/79										6/ 6/79										6/ 6/79										6/ 6/79										6/ 6/79																																																																																																																																				
AVG. TEMP.	1578	1594	1545	1593	1495	1590	1589	1614	1227	1403	1373	1335	1272	1424	1100	1238	1047	1202	1147	1040	1196	888	982	1578	1594	1545	1593	1495	1590	1589	1614	1227	1403	1373	1335	1272	1424	1100	1238	1047	1202	1147	1040	1196	888	982	1578	1594	1545	1593	1495	1590	1589	1614	1227	1403	1373	1335	1272	1424	1100	1238	1047	1202	1147	1040	1196	888	982	1578	1594	1545	1593	1495	1590	1589	1614	1227	1403	1373	1335	1272	1424	1100	1238	1047	1202	1147	1040	1196	888	982	1578	1594	1545	1593	1495	1590	1589	1614	1227	1403	1373	1335	1272	1424	1100	1238	1047	1202	1147	1040	1196	888	982	1578	1594	1545	1593	1495	1590	1589	1614	1227	1403	1373	1335	1272	1424	1100	1238	1047	1202	1147	1040	1196	888	982																																													
STD. DEV.	12	4	24	8	23	1	5	2	7	5	6	20	9	3	10	11	11	8	17	14	6	18	7	12	4	24	8	23	1	5	2	7	5	6	20	9	3	10	11	11	8	17	14	6	18	7	12	4	24	8	23	1	5	2	7	5	6	20	9	3	10	11	11	8	17	14	6	18	7	12	4	24	8	23	1	5	2	7	5	6	20	9	3	10	11	11	8	17	14	6	18	7	12	4	24	8	23	1	5	2	7	5	6	20	9	3	10	11	11	8	17	14	6	18	7	12	4	24	8	23	1	5	2	7	5	6	20	9	3	10	11	11	8	17	14	6	18	7																																													
HI TEMP.	1593	1602	1581	1607	1542	1592	1598	1618	1240	1415	1387	1367	1293	1428	1114	1255	1067	1215	1173	1064	1209	920	993	1593	1602	1581	1607	1542	1592	1598	1618	1240	1415	1387	1367	1293	1428	1114	1255	1067	1215	1173	1064	1209	920	993	1593	1602	1581	1607	1542	1592	1598	1618	1240	1415	1387	1367	1293	1428	1114	1255	1067	1215	1173	1064	1209	920	993	1593	1602	1581	1607	1542	1592	1598	1618	1240	1415	1387	1367	1293	1428	1114	1255	1067	1215	1173	1064	1209	920	993	1593	1602	1581	1607	1542	1592	1598	1618	1240	1415	1387	1367	1293	1428	1114	1255	1067	1215	1173	1064	1209	920	993	1593	1602	1581	1607	1542	1592	1598	1618	1240	1415	1387	1367	1293	1428	1114	1255	1067	1215	1173	1064	1209	920	993																																													
LO TEMP.	1555	1583	1515	1579	1460	1588	1582	1612	1214	1395	1363	1307	1257	1417	1084	1213	1032	1184	1115	1018	1187	851	969	1555	1583	1515	1579	1460	1588	1582	1612	1214	1395	1363	1307	1257	1417	1084	1213	1032	1184	1115	1018	1187	851	969	1555	1583	1515	1579	1460	1588	1582	1612	1214	1395	1363	1307	1257	1417	1084	1213	1032	1184	1115	1018	1187	851	969	1555	1583	1515	1579	1460	1588	1582	1612	1214	1395	1363	1307	1257	1417	1084	1213	1032	1184	1115	1018	1187	851	969	1555	1583	1515	1579	1460	1588	1582	1612	1214	1395	1363	1307	1257	1417	1084	1213	1032	1184	1115	1018	1187	851	969	1555	1583	1515	1579	1460	1588	1582	1612	1214	1395	1363	1307	1257	1417	1084	1213	1032	1184	1115	1018	1187	851	969																																													
155 HOUR	6/ 7/79										6/ 7/79										6/ 7/79										6/ 7/79										6/ 7/79										6/ 7/79																																																																																																																																				
AVG. TEMP.	1579	1595	1534	1588	1500	1591	1594	1619	1222	1401	1373	1335	1249	1422	1103	1240	1048	1204	1136	1028	1194	886	982	1579	1595	1534	1588	1500	1591	1594	1619	1222	1401	1373	1335	1249	1422	1103	1240	1048	1204	1136	1028	1194	886	982	1579	1595	1534	1588	1500	1591	1594	1619	1222	1401	1373	1335	1249	1422	1103	1240	1048	1204	1136	1028	1194	886	982	1579	1595	1534	1588	1500	1591	1594	1619	1222	1401	1373	1335	1249	1422	1103	1240	1048	1204	1136	1028	1194	886	982	1579	1595	1534	1588	1500	1591	1594	1619	1222	1401																																																																																	

Table C-5 (Cont'd)
Heat Exchanger Probes
Temperature History (Run 106)

LOCATION	-----IN RED-----	-----ABOVE RED-----	---IN RED---	---ABOVE RED---	-----IN RED-----	-----ABOVE RED-----	---IN RED---	---ABOVE RED---	-----IN RED-----	-----ABOVE RED-----	---IN RED---	---ABOVE RED---												
POINT NO.	1	1	3	3	13	13	15	15	2	2	6	14	18	18	7	7	11	11	19	20	20	8	12	
SPEC. MAT.	X	M	M	X	M	X	M	X	M	X	M	X	X	M	M	X	M	X	X	M	M	X	M	
SPEC. LOC.	I	O	I	O	I	O	I	O	I	O	I	O	I	O	I	O	I	O	I	O	I	O	I	
	DEGREES FAHRENHEIT												DEGREES FAHRENHEIT											
215 HOUR	6/ 9/79												6/ 9/79											
AVG. TEMP.	1575	1595	1542	1592	1491	1592	1559	1595	1221	1407	1375	1353	1312	1441	1112	1250	1048	1204	1201	1039	1198	837	986	
STD. DEV.	10	8	17	7	23	2	2	2	9	5	3	15	69	19	14	15	13	7	18	11	5	15	6	
HI TEMP.	1594	1609	1570	1614	1529	1595	1563	1596	1235	1414	1380	1380	1441	1500	1129	1286	1067	1215	1231	1058	1205	859	1000	
LO TEMP.	1560	1579	1518	1584	1450	1588	1555	1592	1206	1399	1369	1320	1149	1418	1081	1231	1025	1189	1177	1026	1187	808	978	
220 HOUR	6/ 9/79												6/ 9/79											
AVG. TEMP.	1569	1592	1539	1589	1486	1591	1562	1595	1222	1404	1375	1345	1343	1430	1116	1247	1052	1211	1212	1042	1201	840	986	
STD. DEV.	13	7	22	3	18	3	5	1	7	6	3	19	41	27	13	17	11	5	17	13	10	16	8	
HI TEMP.	1587	1604	1594	1596	1530	1595	1568	1597	1232	1413	1382	1373	1466	1507	1137	1272	1069	1218	1232	1063	1216	863	999	
LO TEMP.	1544	1580	1510	1583	1462	1587	1554	1593	1206	1395	1370	1304	1292	1401	1092	1216	1033	1203	1180	1024	1183	802	969	
225 HOUR	6/ 9/79												6/ 9/79											
AVG. TEMP.	1569	1595	1544	1587	1482	1592	1558	1594	1224	1407	1374	1357	1314	1407	1124	1247	1048	1210	1199	1046	1201	837	995	
STD. DEV.	14	6	18	4	24	4	4	2	9	5	3	17	45	32	9	11	11	10	19	14	7	16	7	
HI TEMP.	1595	1602	1567	1594	1514	1602	1566	1598	1236	1417	1382	1378	1438	1488	1145	1267	1065	1227	1232	1074	1213	869	1007	
LO TEMP.	1544	1580	1515	1580	1455	1587	1553	1591	1210	1400	1370	1318	1259	1359	1111	1232	1030	1188	1173	1026	1190	803	983	
230 HOUR	6/10/79												6/10/79											
AVG. TEMP.	1564	1595	1548	1589	1475	1591	1560	1594	1224	1405	1374	1354	1214	860	1126	1245	1045	1209	1197	1041	1198	837	987	
STD. DEV.	12	4	17	3	24	2	5	2	8	6	3	24	146	211	14	12	12	9	19	16	7	18	6	
HI TEMP.	1587	1601	1569	1595	1516	1593	1568	1598	1235	1415	1380	1388	1312	1426	1161	1258	1069	1226	1230	1063	1210	874	1002	
LO TEMP.	1547	1589	1511	1583	1445	1586	1552	1591	1212	1395	1369	1313	705	383	1105	1223	1035	1196	1178	1019	1187	812	976	
235 HOUR	6/10/79												6/10/79											
AVG. TEMP.	1571	1595	1537	1593	1486	1591	1559	1595	1225	1406	1374	1360	1249	966	1120	1247	1047	1205	1202	1039	1194	834	988	
STD. DEV.	11	7	16	9	25	2	7	3	7	6	3	18	17	120	12	18	10	5	16	18	7	22	8	
HI TEMP.	1588	1605	1561	1613	1520	1596	1576	1599	1240	1416	1382	1386	1264	1150	1146	1216	1066	1212	1239	1066	1208	877	1002	
LO TEMP.	1553	1583	1509	1583	1452	1588	1552	1590	1216	1394	1371	1330	1210	776	1100	1208	1030	1195	1181	1014	1167	797	976	
240 HOUR	6/10/79												6/10/79											
AVG. TEMP.	1564	1593	1515	1614	1480	1591	1559	1594	1224	1406	1374	1339	1211	1066	1117	1246	1049	1204	1207	1041	1192	822	988	
STD. DEV.	11	4	9	4	19	2	4	2	10	5	3	18	56	44	9	14	12	10	13	17	9	18	10	
HI TEMP.	1583	1601	1530	1619	1524	1594	1567	1598	1250	1418	1379	1384	1257	1165	1135	1270	1067	1218	1228	1064	1216	853	1003	
LO TEMP.	1551	1588	1499	1606	1452	1588	1551	1591	1209	1396	1368	1316	1024	986	1105	1216	1029	1185	1187	1017	1178	796	971	
245 HOUR	6/10/79												6/10/79											
AVG. TEMP.	1570	1597	1513	1613	1485	1591	1557	1592	1221	1407	1375	1345	1249	865	1120	1245	1045	1204	1204	1042	1196	822	987	
STD. DEV.	12	3	8	3	24	2	4	2	6	9	3	25	100	93	16	11	10	7	17	17	11	16	5	
HI TEMP.	1590	1602	1528	1617	1528	1596	1563	1596	1231	1431	1382	1378	1267	1056	1163	1266	1062	1213	1236	1070	1220	845	997	
LO TEMP.	1555	1593	1499	1604	1457	1588	1550	1590	1209	1394	1369	1308	879	765	1100	1226	1029	1191	1178	1022	1183	782	976	
250 HOUR	6/10/79												6/10/79											
AVG. TEMP.	1572	1597	1512	1613	1481	1590	1560	1593	1224	1405	1374	1339	1225	805	1119	1247	1049	1206	1218	1038	1192	824	990	
STD. DEV.	9	4	8	4	17	1	3	2	8	5	3	21	21	86	15	13	19	21	4	11	5	11	11	
HI TEMP.	1579	1601	1521	1617	1497	1590	1563	1595	1229	1410	1379	1353	1256	991	1134	1259	1071	1228	1222	1046	1194	838	998	
LO TEMP.	1559	1594	1502	1609	1458	1589	1556	1591	1211	1399	1371	1308	1211	728	1099	1230	1026	1179	1213	1024	1187	813	974	

Figure C-1

Hot Corrosion Heat Exchanger Probes After 1117 Hours
1600°F Above Bed



Top

Port No. 15

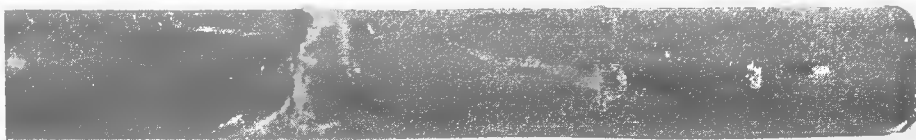


Bottom



Top

Port No. 13



Bottom

Figure C-2

Hot Corrosion Heat Exchanger Probes After 1117 Hours
1400°F Above Bed

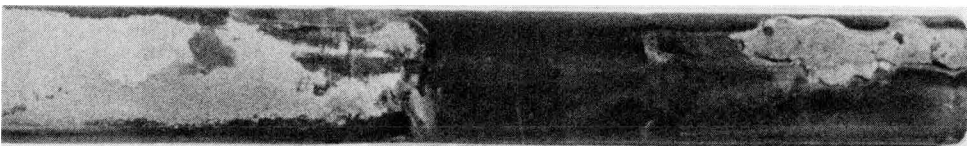


Top

Port No. 18



Bottom



Top

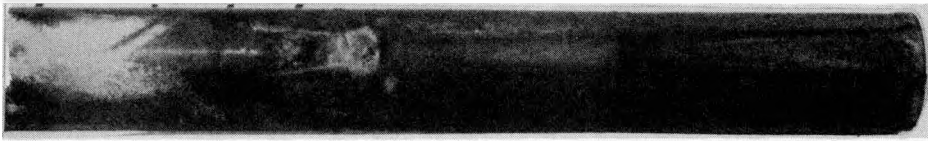
Port No. 14



Bottom

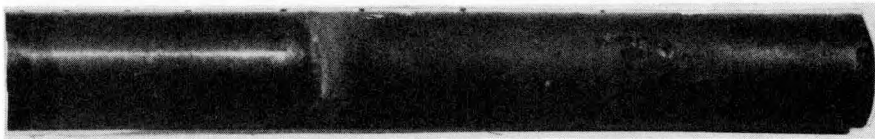
Figure C-3

Hot Corrosion Heat Exchanger Probes After 1117 Hours
1200°F Above Bed



Top

Port No. 20



Bottom



Top

Port No. 19



Bottom

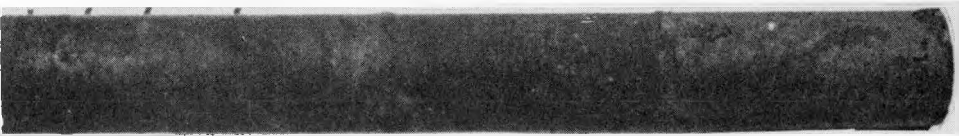
Figure C-4

Hot Corrosion Heat Exchanger Probes After 1117 Hours
1600°F In Bed



Top

Port No. 3

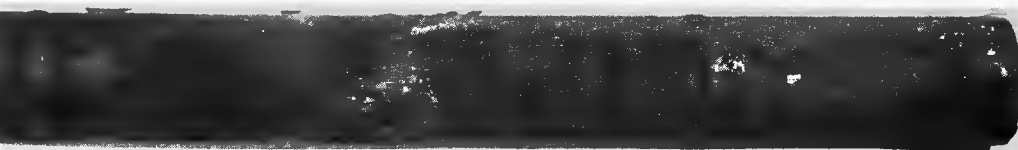


Bottom



Top

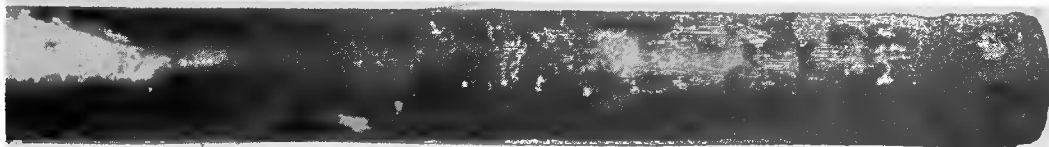
Port No. 1



Bottom

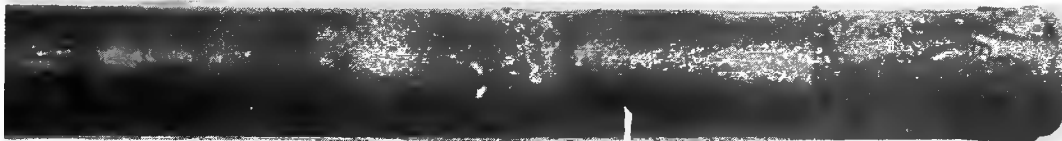
Figure C-5

Hot Corrosion Heat Exchanger Probes After 1117 Hours
1400°F In Bed



Top

Port No. 6

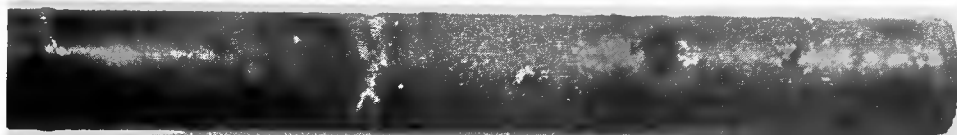


Bottom



Top

Port No. 2



Bottom

Figure C-6

Hot Corrosion Heat Exchanger Probes After 1117 Hours
1200°F In Bed



Top

Probe No. 11



Bottom



Top

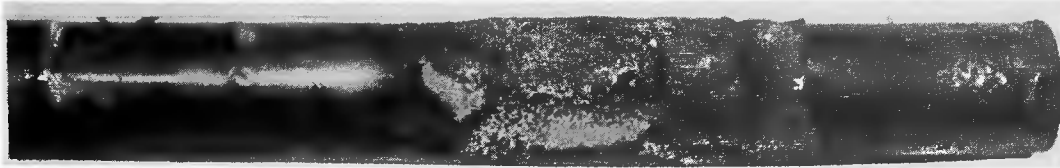
Probe No. 7



Bottom

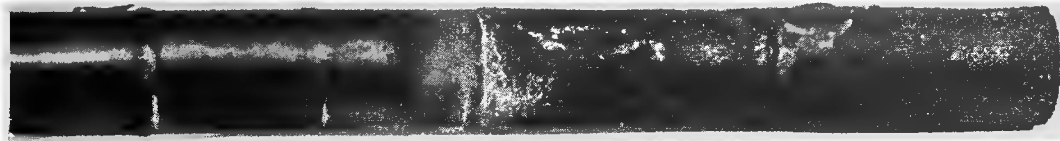
Figure C-7

Hot Corrosion Heat Exchanger Probes After 1117 Hours
1050°F In Bed



Top

Probe No. 12

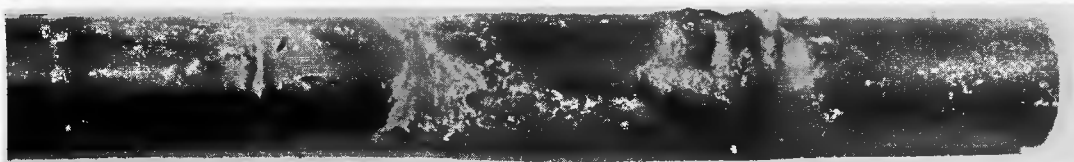


Bottom



Top

Probe No. 8



Bottom

Figure C-8

Hot Corrosion Heat Exchanger Probes After 682 Hours

1200°F Above Bed (Bottom Side View)



Probe No. 19



Probe No. 20



Probe No. 22

Figure C-9

Hot Corrosion Heat Exchanger Probes After 682 Hours

1400°F Above Bed (Top Side View)



Probe No. 14

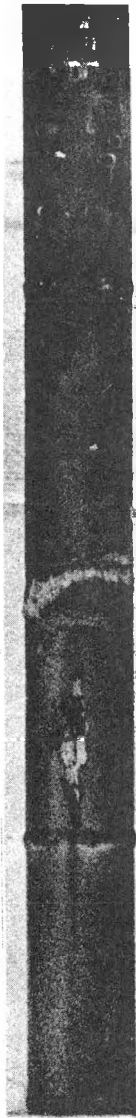
Probe No. 16

Probe No. 18

Figure C-10

Hot Corrosion Heat Exchanger Probes After 682 Hours

1600°F Above Bed (Top Side View)



Probe No. 13

Probe No. 15

Probe No. 17

Figure C-11

Hot Corrosion Heat Exchanger Probes After 682 Hours

1600°F in Bed (Bottom Side View)



Probe No. 1

Probe No. 3

Probe No. 5

Figure C-12

Hot Corrosion Heat Exchanger Probes After 682 Hours

1200°F In Bed (Top Side View)



Probe No. 7

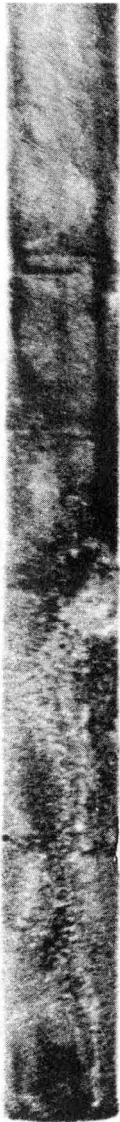
Probe No. 9

Probe No. 11

Figure C-13

Hot Corrosion Heat Exchanger Probes After 682 Hours

1050°F In Bed (Top Side View)



Probe No. 8

Probe No. 12

Probe No. 10

Figure C-14

Hot Corrosion Heat Exchanger Probes After 682 Hours

1400°F In Bed (Top Side View)



Probe No. 2

Probe No. 4

Probe No. 6