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A SIMULATION MODEL FOR WIND ENERGY STORAGE SYSTEMS

MASTER

Volume II: Operation Manual

A. W. Warren, R. W. Edsinger, J.D. Burroughs
ENERGY TECHNOLOGY APPLICATIONS DIVISION
BOEING COMPUTER SERVICES COMPANY
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FOREWARD

This report presents results of work conducted by Boeing Computer Services Company under NASA Contract NAS3-20385, "Wind Energy Storage Model Development." This program was conducted under the sponsorship of the Advanced Physical Methods Branch, Office of Conservation, ERDA, under the direction of Dr. G. C. Chang, and was administered by the NASA-Lewis Research Center Thermal and Mechanical Storage Section with Mr. L. H. Gordon as Project Manager. This report is in three volumes.

- I. Technical Report
- II. Operation Manual
- III. Program Descriptions

The Boeing Program Manager for this work was R. W. Edsinger, and A. W. Warren was the principal investigator.

For completeness, the summary sections 1.1 and 1.2 of Volume I have been repeated in the Operation Manual, Volume II.

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1.0 INTRODUCTION

Energy storage systems for the utilization of intermittent power sources have received increased study over the past few years. However, the type and degree of storage required for optimal utilization of wind energy and the total costs and utility of the resulting wind turbine/generator/storage system have not been thoroughly analyzed. The purpose of the SIMWEST (Simulation Model for Wind Energy Storage) program described in this document is to provide a tool for performing this needed analysis. It is a tool to aid in the design of an optimal wind energy system for a given application and to allow the resulting system to be evaluated and verified through realistic simulation.

SIMWEST consists of a library of system components and a precompiler program which allows these components to be put together in building block form. The present library contains components for five types of energy storage systems. They are pumped hydro, battery, thermal, flywheel, and pneumatic. The SIMWEST program, as described here runs on the UNIVAC 1100 series of computers.

Other computer programs exist for the simulation of wind systems and various forms of energy storage. However SIMWEST is the only program capable of simulating total wind systems containing any one or combination of the above types of storage and at the same time having the flexibility and depth required to perform thorough and meaningful parameter studies.

1.1 GENERAL APPROACH

The structure and much of the software for the SIMWEST program is based on a computer program called EASY, which was previously developed by Boeing Computer Services, Inc. (BCS). SIMWEST consists of two basic programs, and a library of system, environmental, and load components. The first program, the Model Generation Program, is a precompiler which generates computer models (in FORTRAN) of complex wind energy generator/storage/application systems, from user specifications using SIMWEST library components. The second program exercises the resulting computer model to perform cost and potential utiliza-

tion analysis. It handles input, output, integration of system dynamics, and iterates to obtain convergence of variables involved in implicit loops. The combination of these two programs provides a powerful tool for analyzing alternate storage system designs.

Figure 1-1 shows the general organization of the SIMWEST program. In addition to the two programs described above, there is a third which performs file maintenance. It is used to incorporate user supplied data for new subsystem models. Although the program is shown to be made up of a number of subprograms, it can be executed as a single batch program by supplying the model description control cards and the control cards describing the desired analysis to be performed and the desired tabular and/or plotted output.

1.2 SIMWEST LIBRARY

1.2.1 Overview

The SIMWEST library is listed in Table 1-1. It is made up of five types of components: physical, environmental, load, logical, and utility.

Physical components encompass such things as motors, generators, transmissions, flywheels, etc. These components model actual physical hardware which might be used in a wind energy system. The selection of the particular SIMWEST library set of physical components was based on the requirement that it be capable of modeling five types of energy storage systems mentioned previously: thermal, flywheel, battery, pumped hydro and pneumatic.

The degree of detail in the component models is based upon two design criteria. First, all models should contain sufficient detail to simulate all physical characteristics and constraints having significant impact on the systems overall cost effectiveness. Second, the models should be designed to minimize computer time and required user specification. It is assumed that a typical SIMWEST simulation might cover a time span of one year. Thus

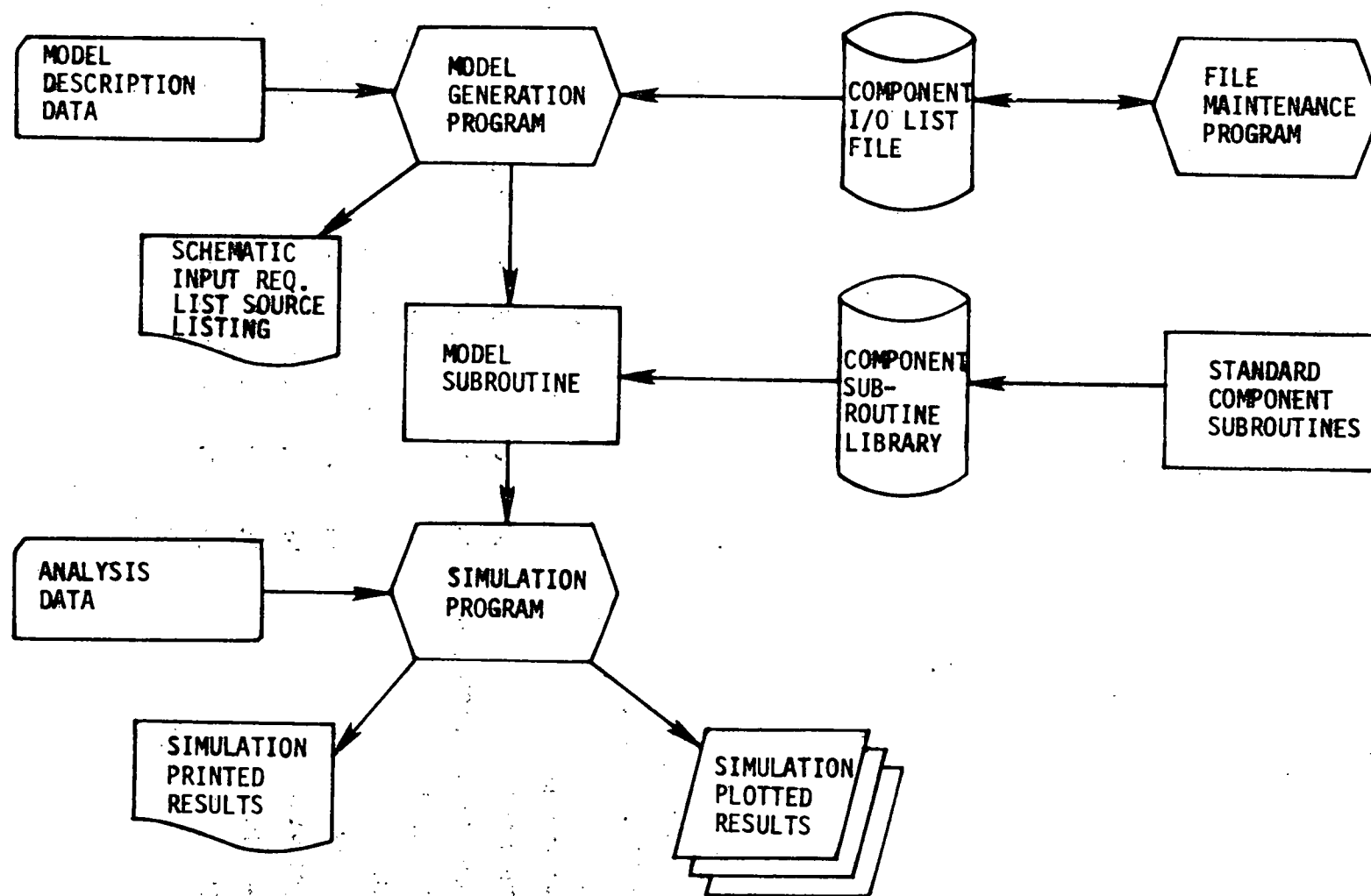


FIGURE 1-1 SIMWEST PROGRAM ORGANIZATION

TABLE 1-1 SIMWEST LIBRARY COMPONENTS

<u>PHYSICAL</u>		<u>ENVIRONMENTAL</u>	
WIND TURBINE	WT	WIND	WD
TURBINE/GENERATOR	WP	AMBIENT TEMP	TP
AC INDUCTION GEN.	GE		
FIXED RATIO TRANSMISSION	GR	<u>LOAD</u>	
RECTIFIER	RE	ELECTRICAL LOAD	LO
BATTERY	BA	THERMAL LOAD	TL
INVERTER	IV		
ADMITTANCE	AD	<u>LOGIC</u>	
COMPRESSOR (PNEUMATIC)	CO	POWER DIVIDER	PD
ADIABATIC HEAT EXCHANGER (INPUT CYCLE)	HX	POWER ACCUMULATOR	PA
ADIABATIC HEAT EXCHANGER (OUTPUT CYCLE)	HY	PRIORITY INTERRUPT	PI
		SWITCH	SW, SX, SY, SZ
PNEUMATIC STORAGE VESSEL	CS	<u>UTILITY</u>	
BURNER	BN	COST MONITOR	CM
TURBINE (PNEUMATIC)	TU	SATURATION	SA
INDUCTION MOTOR	MO	RANDOM NUMBER GENERATOR	RN
VARIABLE RATIO TRANSMISSION	TR	TEST FUNCTIONS	AF
FLYWHEEL/CLUTCH	FL	TABLE LOOKUP	FU, FV
PUMP (HYDRO)	PU	TRANSFER FUNCTION	IT, LA, LL, TF
TURBINE (HYDRO)	HT	ARITHMETIC ELEMENT	MA, MB, MC
HYDRO STORAGE	HS	HISTOGRAM	HG
THERMAL STORAGE	TS	TAPE READ	TA
UTILITY	UT	TIME CONVERSION	TI

from a computer run time and economic impact point of view a simulation step size of between 15 minutes and one hour seemed reasonable.

As a result of the above two design criteria many physical components, such as the electrical components, were modeled mainly in terms of power flow and steady state response. This lack of detail is consistent with the 15 minute time step and with the concept that the important transients are on the time scale of demand curves or weather patterns, i.e. an hour or more, rather than on the time scale of electric motor transients of a few seconds. If short electric transients were to be modeled, much detail would need to be added to the component models which would greatly increase the user's task of specifying the model. Further, the simulation time step would have to be reduced to a fraction of a second so the model would not only be much larger but computer runs would be much costlier.

Environmental components are those which simulate environmental conditions. In the present SIMWEST library these conditions are wind speed and ambient temperature. These variables are generally used as inputs to physical components. Environmental component output can either be computed from measurement data provided by the user on a data tape, or from randomly generated data, based on user furnished profiles.

The load components in the SIMWEST library are used to simulate various types of power demand. They also monitor how well the system meets the simulated demand and compute the value of the energy delivered by the wind energy system to the load. Like the environmental components these components may be computed from actual measurement data or from randomly generated data based on user furnished load profiles.

The library's logical components are the power dividers, power accumulators, switches and priority interrupts. Although physical hardware could generally be built to serve the function of the logical components, they are not meant to represent any particular piece of existing hardware. Instead, they are

idealized components that allow the user the flexibility of modeling the wide variety of control logic which a wind energy storage system would require. In practice, the control function might be performed by a control room operator using a predefined control strategy or by use of a minicomputer.

Finally, the utility components include such things as the tape read, the histogram and the cost monitor. These components serve only to help the user run the simulation and analyze its results.

1.2.2 Storage Subsystems

Figures 1-2 through 1-6 give example configurations of the five types of storage subsystems which can be modeled with the present SIMWEST library. For illustrative purposes the number of variables shown passed between components is limited. A description of the variables being passed is given in Table 1-2.

A total wind energy system will generally be made up of elements from a number of different subsystems (see Figure 1-8). In addition, the SIMWEST program can be used for models which include networks of storage subsystems of the same type or a network of wind generators.

1.2.3 Logic Components

The capability for modeling complex system control logic is provided by the power divider, power accumulator and priority interrupt components. Both the divider and accumulator operate on a priority basis. The priority interrupt is used by other system components to change the priority setting of the divider and accumulator.

The power divider has one input power port and four output power ports (not all output ports need be used for a given simulation). The divider also has

TABLE 1-2 PARTIAL LIST OF COMPONENT INPUTS AND OUTPUTS

SYMBOLS

P	POWER
RE	POWER REQUEST
MP	MAXIMUM POWER
RS	ROTOR SPEED
T	TEMPERATURE
TA	AMBIENT TEMPERATURE
M	MASS FLOW RATE
H	RESERVOIR HEIGHT
LD	THERMAL LOAD DELIVERED
WV	WIND VELOCITY
GR	GEAR RATIO
EF	EFFICIENCY
INT	INTERRUPT FLAG
TSO	MINIMUM AIR TEMPERATURE
PR	PRESSURE
PS	PRIORITY SEQUENCE
WY	WEEK OF YEAR
DW	DAY OF WEEK
TD	TIME OF DAY
SP	SURPLUS POWER
VAR	FILE READ VARIABLE

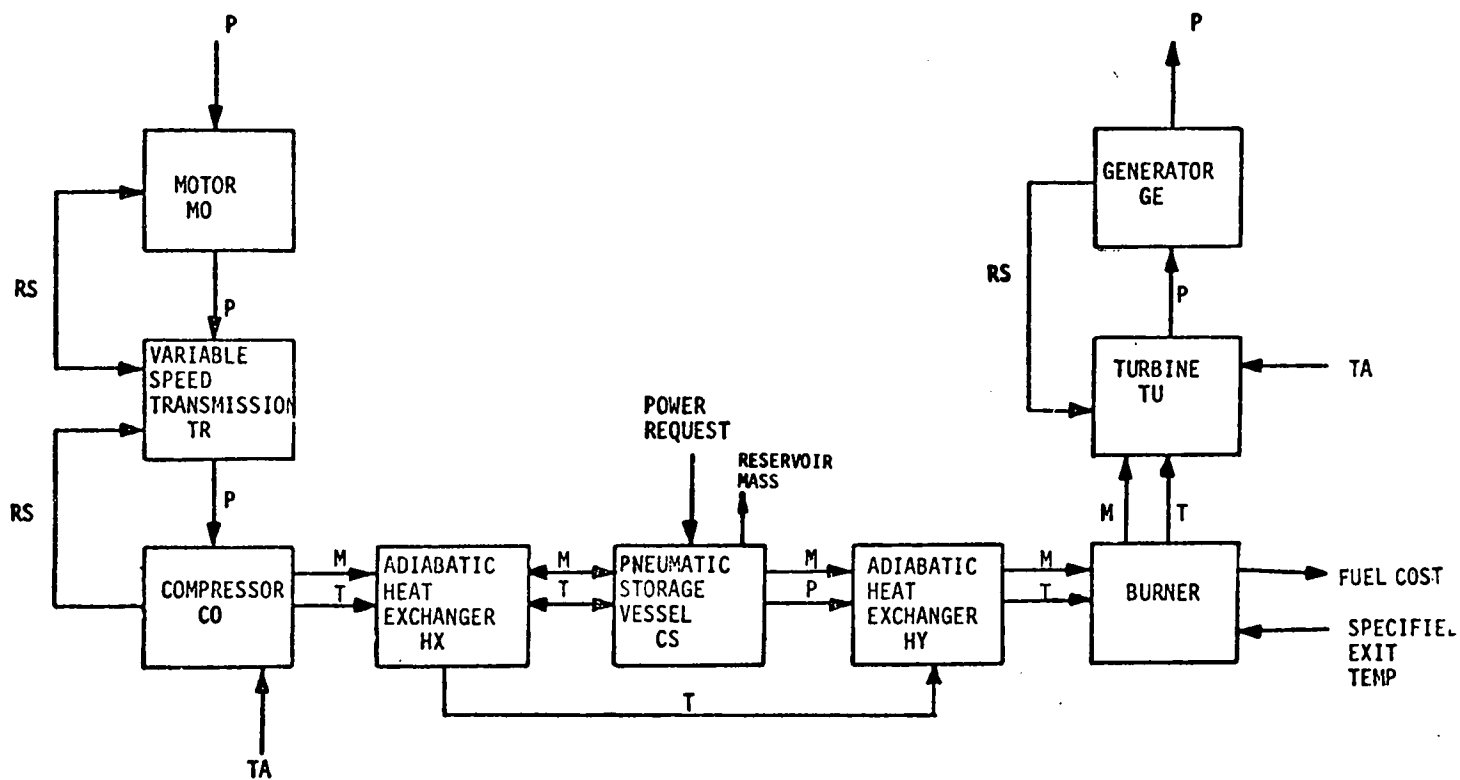


FIGURE 1-2 PNEUMATIC STORAGE SUBSYSTEM

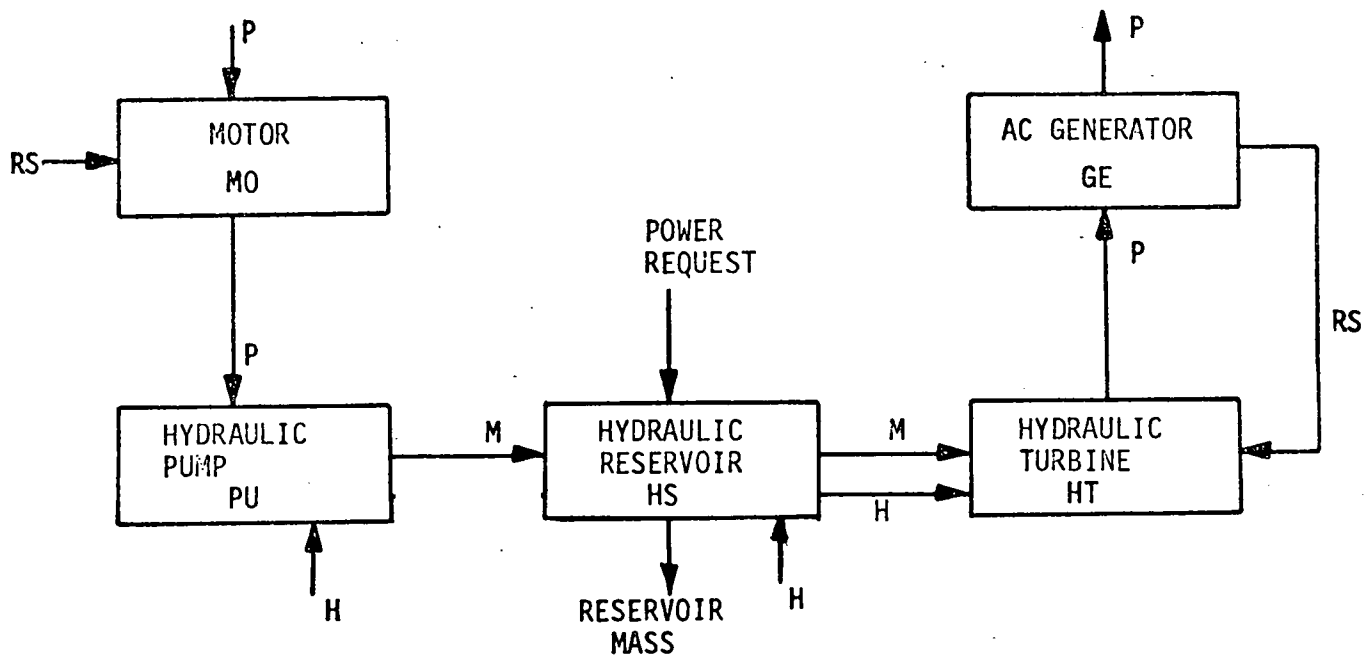


FIGURE 1-3 PUMPED HYDRO STORAGE SUBSYSTEM

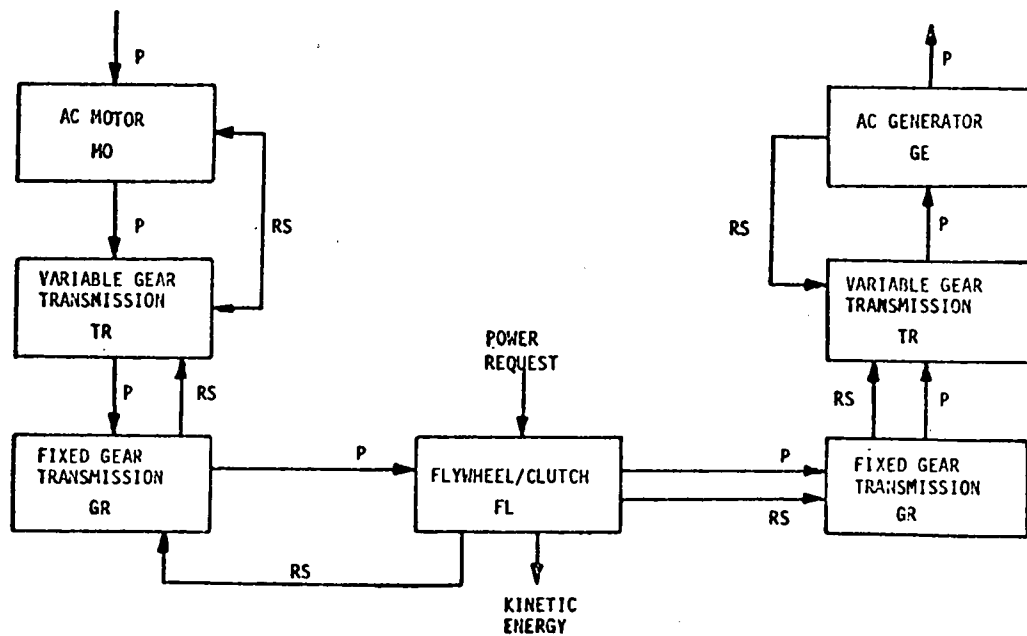


FIGURE 1-4 FLYWHEEL STORAGE

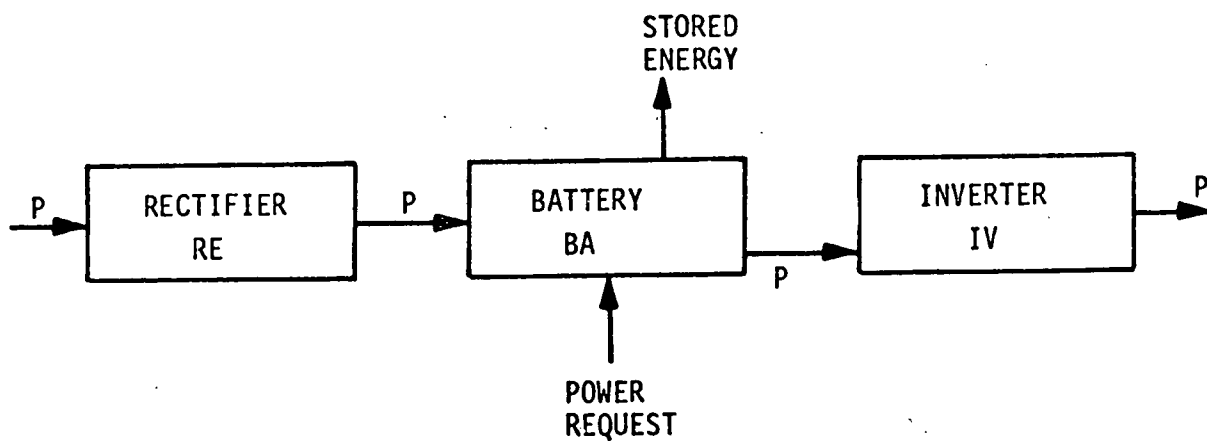
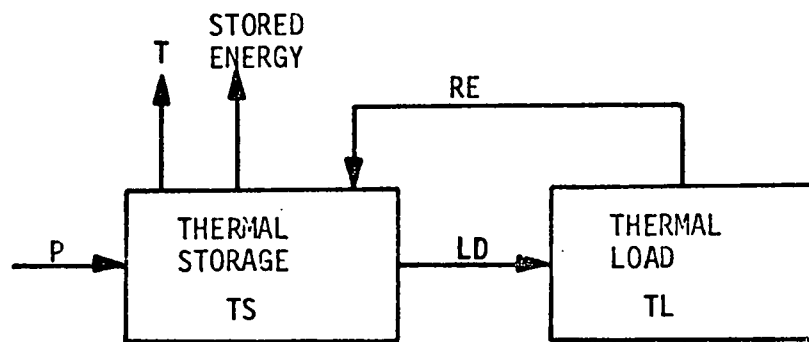


FIGURE 1-5 BATTERY STORAGE



LD = LOAD DELIVERED

FIGURE 1-6 THERMAL STORAGE

an input request associated with each of its output power ports. These power requests generally come from a component with which the output power port is directly or indirectly connected. The user specifies priorities of either 0,1,2,3, or 4 to be associated with each of the output ports. If the input power to the power divider exceeds that requested of the port with highest priority (priority 1) then the excess power goes to the port with the next lower priority. This process continues until either all power is distributed or all requests of non-zero priority ports are met. A port with zero (0) priority will never receive power. Such ports are included so that the port may be connected to a component but transmit power only in critical situations, say, when a battery has been in discharge state for a critical amount of time. In these situations, the connected component would have to change the zero priority setting of the power divider by use of a priority interrupt.

Two or more ports may be assigned the same priority in which case the user may specify weights to be associated with each port. Then if there is not enough power available to satisfy all requests of equal priority the power is divided between them in proportion to the user specified weights.

The power accumulator is similar to the divider except that instead of distributing power from a single input port between four output ports, it accumulates power from four input ports and sends it out through a single output port. The power accumulator also accepts output power requests from the component connected to its single output power port and it outputs requests for each of its input ports in order to service the output power request.

In addition to the actual power delivered to each input port, the power accumulator also accepts information as to the maximum power that can be delivered to that port. These values are used by the accumulator to determine how to distribute its power request between its four input ports. If the input power request exceeds the maximum deliverable power for the port of highest priority, then the remainder is shifted to the port with the next lower priority. This process continues until either the power request has been completely distributed between the highest priority input ports or all input

ports have requests equal to their maximum deliverable power. An example illustrative of the use of power dividers and power accumulators is given in Figure 1-7.

Here the wind turbine distributes power first to satisfy the request from load 1. If there is power left over, it then tries to satisfy the request from the battery. Finally, if the battery is full or if its charging rate is met, then the excess power goes to the flywheel. The battery is connected to the wind turbine and also has a priority zero connection to the utility. Thus, if the battery remains in a discharge state for more than a specified amount of time, it can change the utility priority (from 0 to 1) to receive the needed power.

Also in Figure 1-7, we see that load 2 prefers to draw power from the flywheel before turning to the battery. This configuration tends to keep the flywheel as discharged as possible, using it primarily as a means to absorb large influxes of power.

Figure 1-7 is a rather simple configuration used for illustrative purposes. A more complex configuration is shown in Figure 1-8.

1.2.4 SIMWEST Output

There are three basic forms of SIMWEST output to facilitate the analysis of wind energy storage systems; line printer plots, histograms of system variables and time sequenced output of variable values. To enhance the usefulness of these outputs each SIMWEST library component is associated with a number of output variables. Prior to simulating a given system the user specifies which of these variables he wants plotted. For plotted output he may select to have the independent variable be the plot time or any of the other variables. For example he may want to plot the energy of pneumatic storage as a function of time and/or as a function of storage versus temperature. If the user wants a time sequenced listing of all variable values

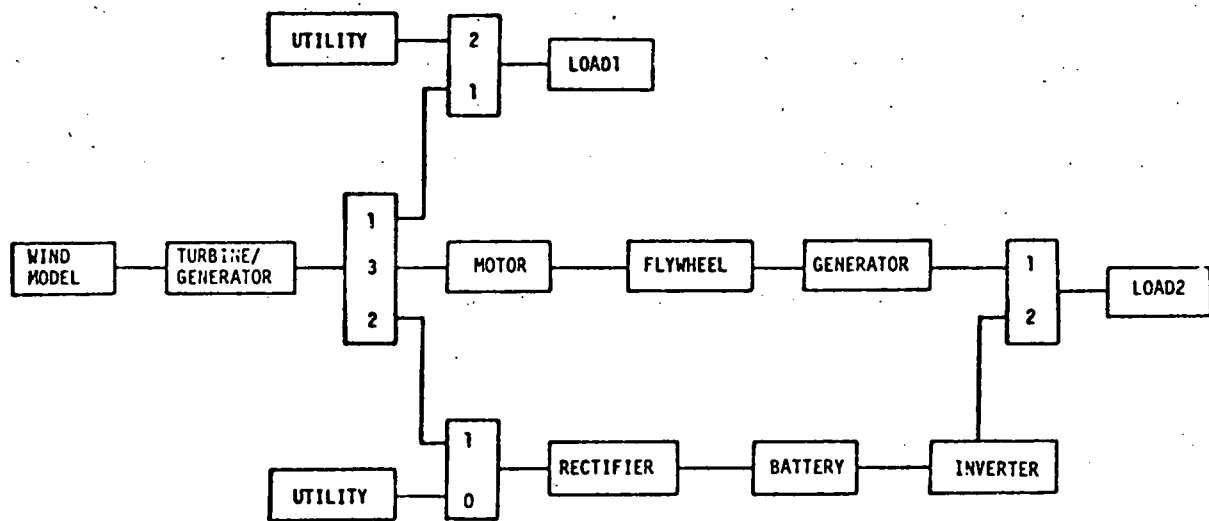


FIGURE 1-7 EXAMPLE OF POWER DIVIDER & ACCUMULATOR USE

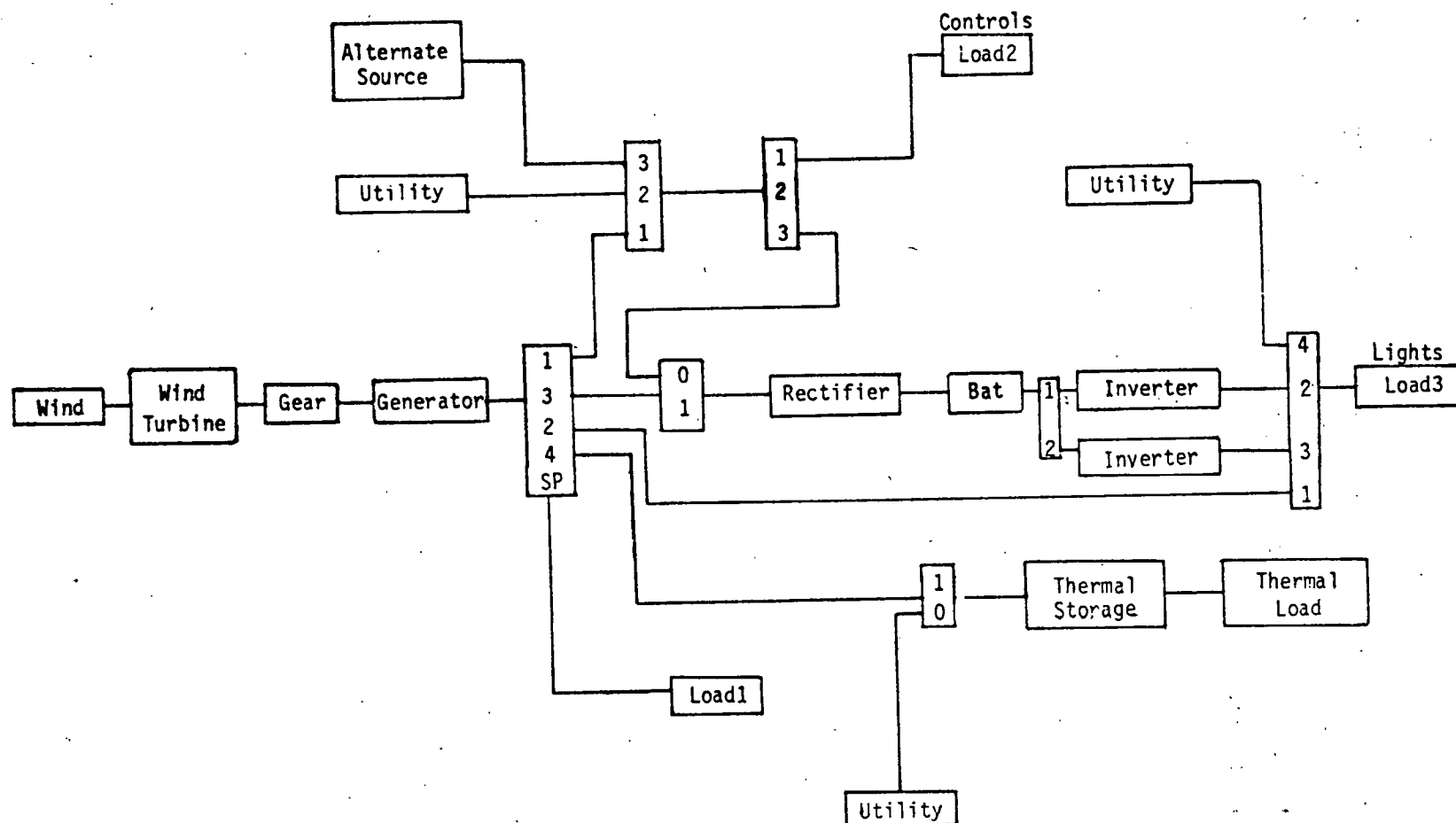


FIGURE 1-8 PLUMBROOK CONFIGURATION FOR PARAMETER STUDY

he just specifies the time step between printouts. The listing of all variables has proven to be a useful tool in understanding the performance of the storage system under consideration and a valuable aid in validating the system design.

2.0 MODEL GENERATION

The Model Generation program design is based on the assumption that the system analyst will begin by constructing a schematic diagram of the system he wishes to analyze. This schematic will be comprised primarily of standard SIMWEST library components. Standard library components include wind turbine, wind models, AC induction motors, inverters, rectifiers, etc. If a particular system cannot be modeled with existing standard components, the analyst may construct the model by including appropriate FORTRAN statements in his system description.

All interconnections between standard components are accomplished by the Model Generation program. The analyst merely specifies each standard component in the schematic diagram and all of the components that provide inputs to that component. The Model Generation program then generates names and the proper interconnections between the specified components. This is accomplished by matching the input quantities required by each standard component to the output quantities of the specified input components.

After processing the complete system model description, the Model Generation program generates a schematic diagram of the model showing the interconnections between standard components and the quantities such as power, pressure, temperature, mass flow rates, etc., that pass through each interconnection. This schematic is produced on the lineprinter to provide a rapid graphic check on the program's interpretation of the model description.

In addition, the program produces a list of input data that will be required by each component to complete the model description. Both the scalar parameters and tabular data required for the analysis are included in this list. The program assumes that any quantity not supplied by another component will be supplied as a fixed parameter by the analyst. Thus requests for non-parameter items in the input data list will reveal any connection that was omitted from the system model description.

2.1 MODEL DESCRIPTION

The Model Generation program is a precompiler program which accepts model description instructions and from these instructions generates a FORTRAN model of a system. These instructions, referred to as "program commands," are made up of one or more words. In addition, the system model description contains numeric values, standard component names, and standard input and output quantity names.

The Model Generation commands may be best introduced with a simple example of their use to describe a wind turbine system. Figure 2.1-1 shows an analyst's schematic of a wind turbine model that has been constructed using standard components on a SIMWEST schematic form. The standard component names used in this sample are:

- WD - Wind Model
- WT - Wind Turbine
- TI - Time Conversion
- HG - Histogram Generator
- GR - Fixed Ratio Transmission
- LO - Electrical Load
- GE - AC Induction Generator

The SIMWEST description of this model would be as follows:

Example 2.1

LIST STANDARD COMPONENTS

MODEL DESCRIPTION	WIND TURBINE TEST CASE	
LOCATION=15	TI	
LOCATION=11	WD	INPUTS=TI
LOCATION=31	WT	INPUTS=WD

SIMWEST SCHEMATIC FORM

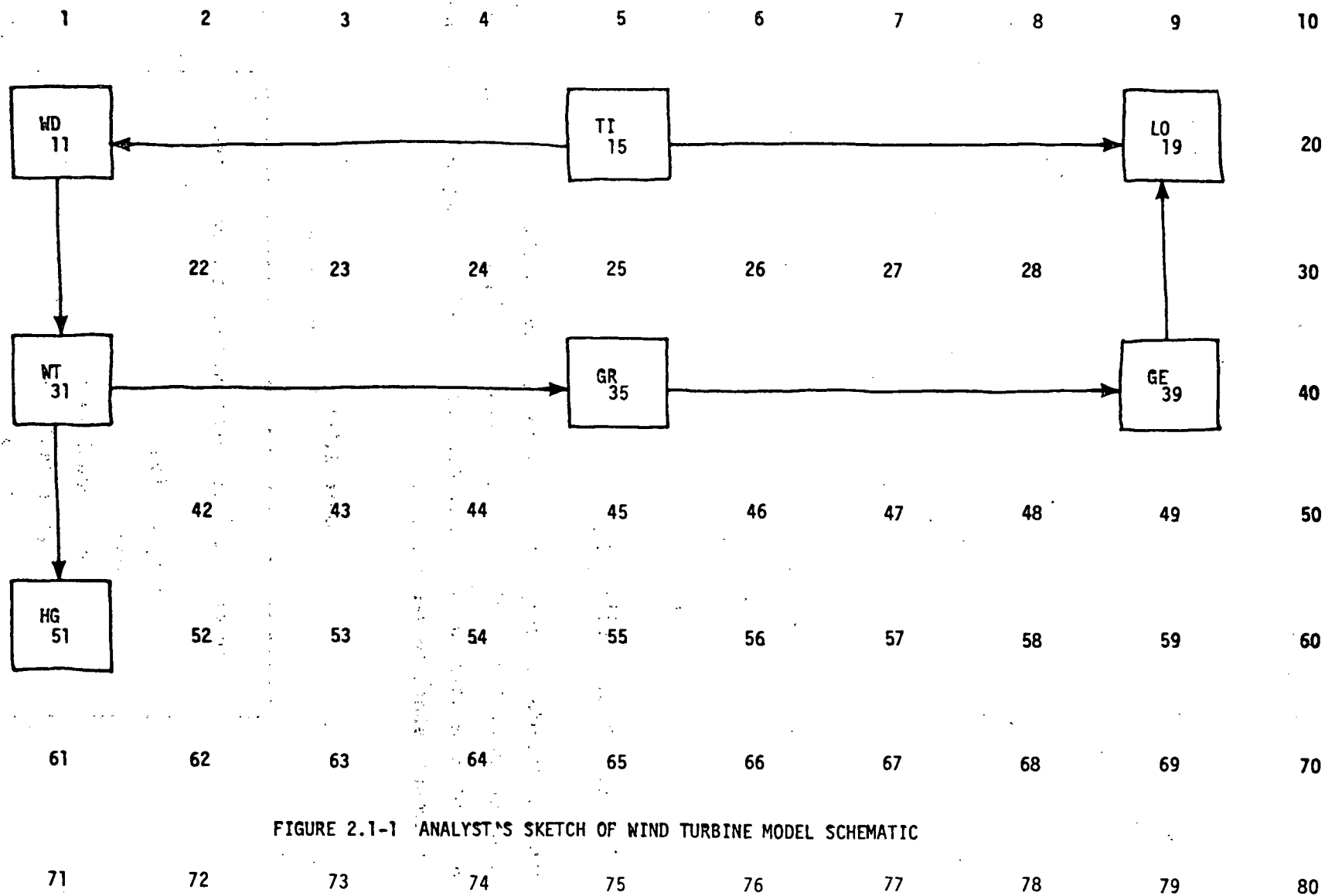


FIGURE 2.1-1 ANALYST'S SKETCH OF WIND TURBINE MODEL SCHEMATIC

Example 2.1 (Cont.)

```
LOCATION=35      GR      INPUTS=WT
LOCATION=51      HG      INPUTS=WT(P =FIN)
LOCATION=39      GE      INPUTS=GR
LOCATION=19      LO      INPUTS=GE,TI
END OF MODEL
PRINT
```

The model description consists of a statement as to the location of each component in the schematic and a list of all components that provide inputs to that component. The location of the component in the schematic is used for a line printer drawn schematic of the model, such as shown in Figure 2.1-2. In the line printer schematic the input and output quantities such as powers (P2 WT, P2 GE, P2 GR) are shown on the various connecting lines.

2.1.1 Phrases and Delimiters

The system model description is interpreted by the Model Generation program as a series of "phrases", which can appear in a free field format in any position on a data card. Phrases must be separated by any one of the delimiter symbols shown in Table 2.1-1.

Table 2.1-1

Model Generation Program Language Delimiters

- = equal sign
- , comma
- (left parenthesis
-) right parenthesis
- three or more blanks

FIGURE 2.1-2 LINEPRINTER-DRAWN WIND TURBINE MODEL SCHEMATIC

2.1.2. Command Phrases

The Model Generation command phrases are described in this section in a logical sequence similar to that in which they appear in system model descriptions.

MODEL DESCRIPTION

The MODEL DESCRIPTION command phrase indicates the start of a new system model. This phrase may be followed, (on the same card), by a title of up to 60 characters. This title will be used to identify various program output schematics, lists and program listings. In Example 2.1, the title was "Wind Turbine Test Case."

LOCATION

The LOCATION command phrase indicates the start of the description of a new component in the system model. This command must be followed by a numeric value phrase that specifies the location of the new component on the model schematic. Thus in the example of Figure 2.1-1, the location number of the wind model WD was 11 and the wind turbine WT was 31, etc. To be a valid component location, the last two digits of this number must comprise a number between 1 and 80. The hundreds column is used to specify additional pages as needed for the schematic. Thus the numbers:

1, 13, 51, 80

would be valid location numbers for components on the first page, (PAGE 0), of a system schematic. These same locations on the second page of the schematic, (PAGE 1), would be:

101, 113, 151, 180

The location number phrase is followed by the name of the component at that location. Component names are discussed in Section 2.2.

A LOCATION statement should be given only once for each component. That is, once a LOCATION statement is started for a component the complete description of all inputs to that component should be given.

INPUTS

The INPUTS command phrase indicates that the following phrases contain the names of the components that provide inputs to the component at the specified location. Thus in the example of Figure 2.1-1, the electric load at location 19 which receives inputs from generator GE and the time source TI was described as:

```
LOCATION=19    LO    INPUTS=GE,TI
```

In this example the command phrase INPUTS is followed by two component names. As many component names as are necessary to specify the inputs to a particular system component may be included in each component description.

For some system components there are multiple input and/or output ports. For example, a power divider has four input power ports. When specifying the connections between such components, it is advisable to specify which ports are to be connected. This is done by adding the port numbers to be connected after the name of the input component. Thus, the wind turbine to transmission connection could have been more explicitly described as:

```
LOCATION=35    GR    INPUTS=WT(2,1)
```

This says that port 2 of the wind turbine (WT) drives port 1 of the transmission (GR). Any quantities which have no port numbers are considered "universal ports" for input connections. Thus, the GR input of GR is connected

up to GR WT, and the RS input of WT is connected up to RSIGR by the above command. If the port designations are omitted, as they were in example 2.1., the connections will be made to the first available input port starting with the minimum port number. Once a connection has been made to an input port, those input quantities that are connected are unavailable for further connections. An exception is made when the physical quantities of both input and output are specified. This method of specifying connections is described in the following paragraphs.

For certain components, such as control elements, the inputs to the component can be any physical quantity in the model. For these components, the input component names must be supplemented by the name of the particular output quantity that is to provide the input.

As an example, consider a component that represents a linear first order lag transfer function. If the transfer function component's input, FIN, was to be the rotor speed of the wind turbine WT in example 2.1, then the statement:

```
LOCATION=53      LA      INPUTS=WT(RS=FIN)
```

would indicate to the program that of the outputs of the wind turbine, the output rotor speed, RS, was to be used as the input, FIN, to the transfer function, LA.

To summarize, there are three levels of connection specification:

1. Default (only component names are specified)

Connections are made between all unconnected inputs and outputs for the first ports for which a match of physical quantity names occurs.

2. Ports Specified

Connections are made between matching physical quantities for all unconnected inputs and outputs of the specified ports.

3. Physical Quantities Specified

Connections are made between only those quantities specified. Previous connections can be over-ridden, providing the three character physical quantity name of the previously connected variable is used. For example, the phrase

```
LOCATION=19      LO      INPUTS=GE,GE(P,2=MP2),TI
```

will replace the input parameter MP1LO by MP26E and then override the connection MP2GE and substitute P2 GE as the LO input.

END OF MODEL

The END OF MODEL command phrase indicates that model description has been completed and that the Model Generation program should proceed with the generation of the model subroutines.

PRINT

The PRINT command phrase causes the program to: (1) draw a schematic of the system model, as shown in Figure 2.1-2; (2) print a list of input requirements for the model; and (3) print a source listing of the FORTRAN subroutines that were generated for the model. The Model Generation program then terminates.

PUNCH

The PUNCH command phrase has the same effect as the PRINT command, but in addition a FORTRAN source deck of the system model is produced.

FORTRAN STATEMENTS

The FORTRAN STATEMENTS command phrase allows the system analyst to supplement the library components with FORTRAN statements. Using this feature, the analyst can introduce his own program logic, DO loops, etc., as necessary to model any system feature not obtainable with standard library components.

One of the common uses of the FORTRAN STATEMENTS command is to input large tables into the model. Two function subprograms TBLU1 and TBLU2 are provided for this use. They perform linear interpolation from one and two dimension tables, respectively. TBLU1 is in general called in the form

$$F = \text{TBLU1}(X, \text{TAB}(4), \text{TAB}(4+N), I, \pm N),$$

where F is the interpolated value at the desired point X, TAB is a one dimension table with dimension N, TAB(4) is the independent variable and TAB(4+N) is the dependent variable list, I = 0 for equal spaced data, I = 1 for unequal spaced data, and the dimension N is specified as the last variable if linear extrapolation is desired, and -N is specified if truncation is desired outside the table limits. Similarly, TBLU2 is in general called using the form

$$F = \text{TBLU2}(X, Y, \text{TAB}(4+M), \text{TAB}(4), \text{TAB}(4+M+N), IX, IY, \pm N, \pm M, N, M),$$

where X and Y are the values of the primary and secondary independent variables, N and M are the dimensions of the primary and secondary variable arrays, IX and IY are indicators for equal spaced or unequal spaced data as above, and the sign convention on N and M is positive for extrapolation, negative for truncation.

The FORTRAN STATEMENTS command would normally be used only when some portion of the system cannot be modeled with library components. Then using this feature of the program, the analyst must perform many of the detail connections

and naming of variables, that are normally accomplished by the Model Generation program. In return for these added tasks, the analyst gains a great deal of additional freedom and flexibility in forming details of his system model. Non-executable code such as common blocks must precede the first component definition and executable code should come after a component has been defined for the iteration logic to work properly.

ADD STATES
ADD VARIABLES
ADD PARAMETERS
ADD TABLES

The ADD commands may be used in conjunction with the FORTRAN STATEMENTS to add states, variables, parameters, and tables that occur within the FORTRAN statements, to the system model. Quantities that are not specified by one of these commands cannot be accessed or manipulated by the Analysis Program.

Before discussing these commands, a few definitions of terms are in order.

States:

States are those quantities in the system model that are described by first order differential equations. The state variables are the result of integrating the set of first order differential equations that comprise the dynamic system model. The number of states equals the order of the system model. The states are dynamic, time varying quantities during most simulation studies. The initial values, (initial conditions), of the states must be input as part of the system model description.

Variables: Variables are all other dynamic time varying quantities in the system model that are not states. In general, variables are related to states by algebraic relationships.

Parameters: Parameters are constant scalar quantities in the system model. Parameters can be manipulated by the analyst to alter the system model. All parameter values* should be input as part of the system model description.

Tables: Tables are constant nonscalar quantities in the system model. Tables are used to represent algebraic functional relationships with one or two independent variables. All table values must be input as part of the system model description.

The format for the ADD commands is that the command is followed by one or more phrases that contain the names of the states, variables, parameters, or tables. In addition to each table name, a number, specifying the amount of storage to be allocated for that table must be given. This number is positive if the table is two dimensional and negative if one dimensional, with absolute value determined by the formula:

$$N = 3 + I + J + D$$

N = the total storage required by the table,
in words.

* For certain components, default values are provided for some parameters.

I = the number of data points in the primary independent variable table.

J = the number of data points in the secondary independent variable table. (J=0 if there is only one independent variable.)

D = the number of data points in the dependent variable table. (D=1 if there is only one independent variable. D=I*J if there are two independent variables.

The following example illustrates the use of FORTRAN STATEMENTS in the parameter study model:

Example 2.2

MODEL DESCRIPTION	PARAMETER STUDY
-------------------	-----------------

.	
.	
.	

ADD TABLES = WIND,802	
-----------------------	--

LOCATION = 41 TI	
------------------	--

FORTRAN STATEMENTS	
--------------------	--

C READ WIND VELOCITY DATA	
---------------------------	--

WVIWD = TBLU2(TD TI,DY TI,WIND(35),WIND(4),	
---	--

1 WIND(59),0,0,24,-31,24,31)	
------------------------------	--

LOCATION = 71 WD INPUTS = TI	
------------------------------	--

.	
.	
.	

In this model, Fortran is used to input wind velocity data. The wind table, denoted WIND, consists of up to 31 days of hourly wind speeds. Hence, as described previously, the total storage required is $3+24+31+24*31=802$. The Fortran is inserted after time of day and day of the year are computed in T1. In this case, $N=24$, $M=31$, the data is equal spaced, and extrapolation is used to provide velocity data over each 24 hour period. The variable WIND is the name at the wind input to WD generated by the precompiler. Fortran insertion in the model ends when the LOCATION=71 ... command is read and a call to the subroutine WD is then generated.

LIST STANDARD COMPONENTS

The LIST STANDARD COMPONENTS command phrase causes the program to print a list of all standard components. For each standard component, lists of inputs, outputs, and tables for that component are provided. For each input, the physical quantity name and port number is given. For each output, the physical quantity name, port number, and the letter S, if the quantity is a state is given. For each table, the table name, the number of independent variables and the maximum amount of storage allowed is provided. This command is usually given as the first command of a model description and will result in a list of all standard component information as the first output from the Model Generation program.

2.2 NAMING CONVENTION

All standard components are given names consisting of two characters, the first of which is alphabetical. Thus we have WT for wind turbine, GE for generator, WD for wind model, etc. Where multiple components of the same type are required, the second character is used to distinguish between the different models of the same basic component type. A specific component in a model can be distinguished from other components of the same type by adding one

more character to the standard component name. This character is usually numeric but can also be alphabetical or blank. Thus a given model can contain up to 37 different components of the same standard component type. For example, a model with ten different wind turbines might have these components designated as:

WT1,WT2,WT3,.....,WT8,WT9,WT10

2.2.1 Variable, Parameter, and Table Naming Conventions

All of the input, output, and tabular quantities required by each component in a system model must have unique FORTRAN names. These quantities are given names consisting of up to three characters that describe the physical quantity they represent.

Since a single component may have several inputs or outputs of the same physical quantity, the program adds the port number to the second or third character of the physical quantity name to prevent such a duplication.

The physical quantities that are outputs of a given component are identified by adding the three character name of that component to the three character name of the physical quantity. In this way, unique six character FORTRAN names are generated for all output quantities of the system model components.

Input quantities to a component that are driven by another component carry the names of the component that drives them. Any inputs that are not driven by other model components are assumed to be parameters and are assigned the name of the component for which they are an input.

If a component should require tabular data as an input, unique table names are generated just as scalar input quantity names by adding the component

name to the table name. A pictorial representation of the character assignment in component, variable, and table names is given in Figure 2.2-1.

2.3 MODEL SCHEMATIC

The Model Generation program produces a schematic diagram of the system being modeled. This schematic is crude but is inexpensive and does not have the flow time delays associated with more elaborate plotting methods. Its purpose is to provide a means of rapidly locating errors in the model description.

In order to construct a schematic diagram in an efficient manner with a reasonable size program, it was necessary to establish some simple rules for symbol generation, component connection paths, and labeling. If these rules are kept in mind when laying-out a schematic for the system, the SIMWEST produced schematic will match that developed by the analyst. If the rules are violated by the analyst's schematic, the SIMWEST schematic should still be correct, but may contain some unusual component connection paths and some labeling information may be overwritten.

2.3.1 Standard Schematic Form

The SIMWEST schematic diagrams are produced on a standard 11" by 14" line-printer page with 80 component locations per page. A standard form containing only the location numbers can be obtained by executing the Model Generation program with the single program command, PRINT. This form can then be reproduced and the copies used as forms for drawing system model schematics.

2.3.2 Input Quantity Labeling

The names of the physical quantities that are input to one component from another component are listed adjacent to the downstream component symbol.

INPUT/OUTPUT OR TABLE NAMES

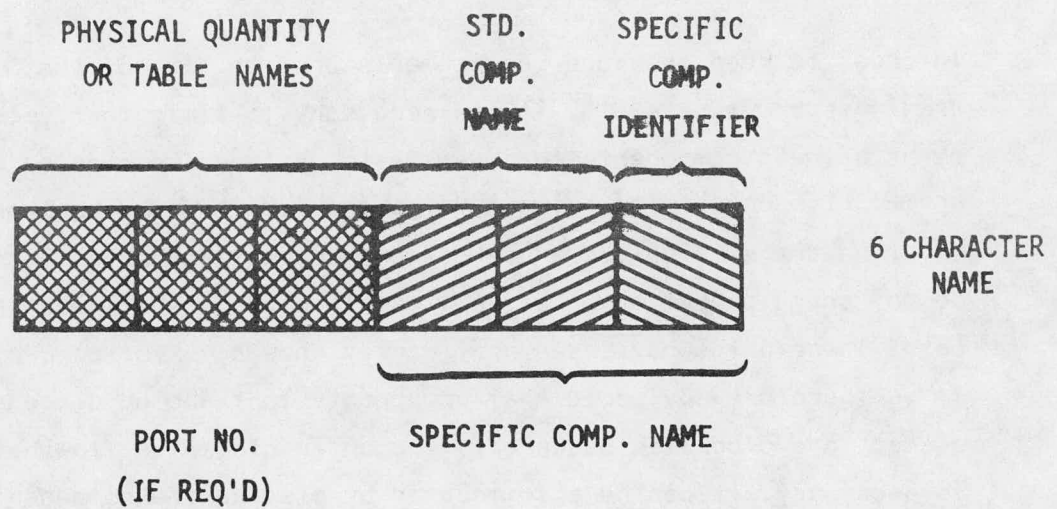


FIGURE 2.2-1 CHARACTER ASSIGNMENT INPUT/OUTPUT OR TABLE NAME

These labels are placed near the connecting line that joins the two components. Since these names are composed of the physical quantity name and the name of the component that generates the information, the source of the input is evident from the name itself. Parameter and tabular inputs to a component are not shown on the schematic. These constant inputs are described in the Input Requirements List.

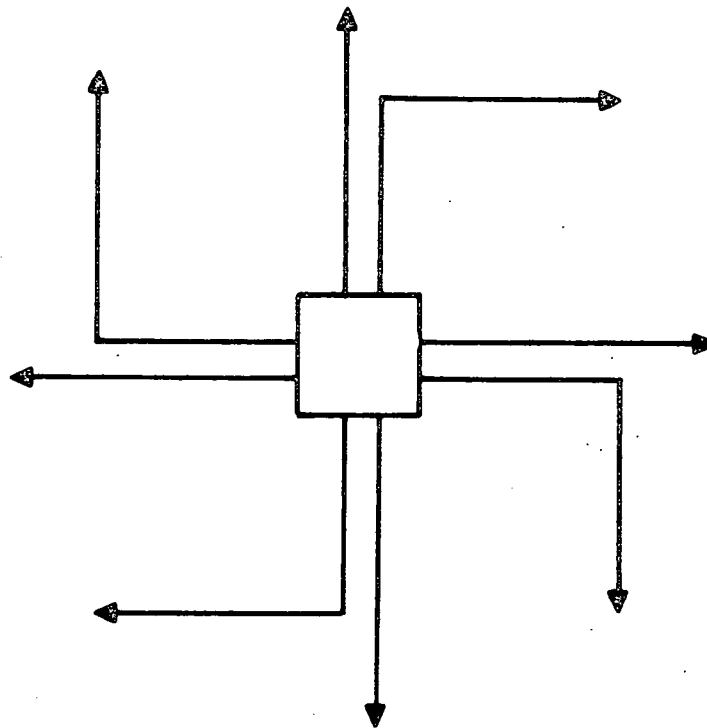
2.3.3 Component Connection Paths

In order to keep the core requirements and run time of the SIMWEST schematic drawing subroutine small, it was necessary to limit the types of connecting paths between components to a few basic routes. These paths are shown in Figure 2.3-1. Connections between components on the same horizontal or vertical line are straightforward. However, connections between components that do not share a horizontal or vertical line require at least a two segment path. These paths have been arbitrarily chosen to follow a clockwise route. It is therefore advisable that components that are on diagonal locations be placed in a clockwise sequence. If counter-clockwise flow between components is necessary, it can be accommodated by placing the components on the same horizontal or vertical lines.

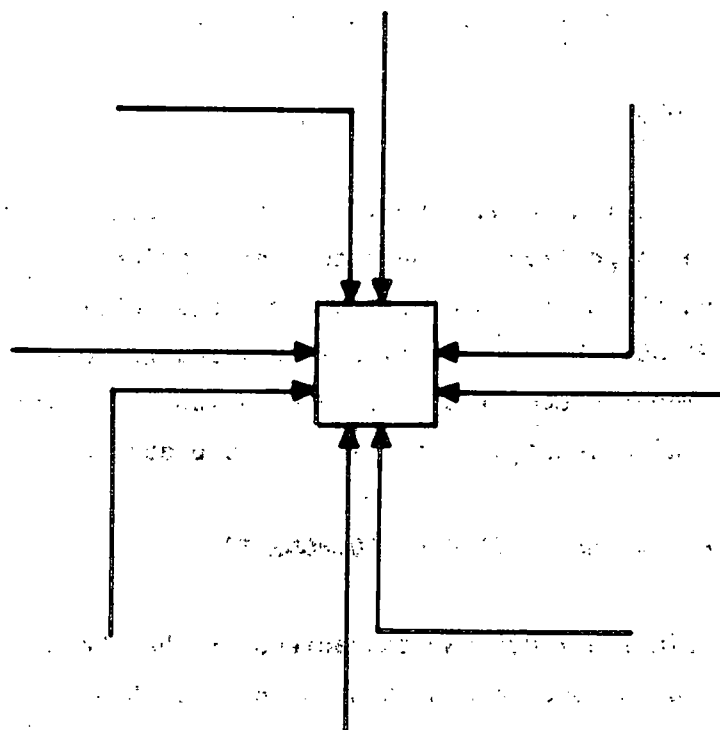
The SIMWEST schematic drawing subroutine makes no attempt to go around components that get in the way of a connection path. Such components are "run-over" by the connecting line.

2.3.4 Additional Pages

The SIMWEST schematic diagram may be broken down into as many pages as are necessary. No attempt is made to draw connecting paths between components located on different pages. It is therefore advisable to minimize the number of connecting paths between pages. This can usually be done by grouping



POSSIBLE OUTPUT PATHS



POSSIBLE INPUT PATHS

FIGURE 2.3-1 COMPONENT CONNECTION PATHS

components with many interconnections on the same page and placing page boundaries between such groups of components.

2.3.5 Guidelines for Schematic Layout

The following guidelines may help in creating schematic layouts that can be duplicated by the SIMWEST program.

1. Try to place connected components on the same horizontal or vertical line.
2. Avoid placing components on adjacent location points.
3. Place diagonal components so that flow is clockwise.
4. Group components to minimize flow paths between pages.

2.4 WARNING MESSAGES

One or more of the following warning messages will occur if the program is unable to interpret a portion of the model description or encounters problems in assembling the system model. These messages will be preceded by: *** WARNING *** or *** NOTICE ***. The symbols xxx and zzz are used to indicate phrases from the model description that are included as part of the warning message. The following messages are listed in alphabetical order:

1. CAN'T IDENTIFY xxx AS A STANDARD COMPONENT

xxx will contain the first two characters of the phrase which cannot be identified as a command or standard component. This message will often follow other warning messages as the program makes successive attempts to interpret the given phrase.

2. CAN'T IDENTIFY xxx AS A VALID INPUT COMPONENT TO zzz

The component xxx cannot be found in the list of components for the current system model.

3. CAN'T LOCATE xxx AS AN INPUT COMPONENT TO LOCATION n

This message indicates that the component xxx, which provides inputs to location n in the schematic, has not been assigned a location number. Check for a missing LOCATION statement or misspelling of the component name.

4. COMPONENT xxx DEFINITION WASN'T COMPLETED BEFORE STARTING THE DEFINITION OF COMPONENT zzz

The command INPUTS was not given between the component names xxx and zzz. Check for proper spelling of INPUTS and a valid delimiter after the phrase xxx.

5. COMPONENT xxx HAS ALREADY BEEN DEFINED

The component xxx was defined in a previous LOCATION statement.

6. LOCATION NO. xxx FOR COMPONENT zzz HAS LAST TWO DIGITS OUTSIDE THE ALLOWABLE RANGE 1 TO 80. NO SYMBOL WILL BE PLACED IN SCHEMATIC FOR THIS COMPONENT

This message will occur at the end of the model description for a component zzz which has an invalid location number. The system model may still be valid but the schematic will not contain this component.

7. NO xxx OUTPUTS MATCH UNSATISFIED zzz INPUTS

Check that it was intended to drive component zzz with component xxx or that the inputs to zzz have been previously satisfied by other component connections.

8. TABLE NAME xxx MUST BE FOLLOWED BY A NUMERIC DIMENSION RATHER THAN zzz

When using the ADD TABLES command, it is necessary to provide the maximum amount of storage to be allocated for the table as well as the table name. This storage value must be a numeric quantity.

9. xxx IS NOT A VALID INPUT QUANTITY OR PORT DESIGNATION FOR COMPONENT zzz

The phrase xxx cannot be located as one of the input quantities or input ports of the component zzz. No connections will occur. Check the list of standard components for the proper spelling or port designations for this component.

10. xxx IS NOT A VALID LOCATION NUMBER

The LOCATION command must be followed by a numeric location number.

11. xxx IS NOT A VALID PORT DESIGNATION FOR INPUT COMPONENT zzz. ERRONEOUS CONNECTIONS MAY OCCUR.

The phrase xxx cannot be located as a valid input port for the component zzz. Connections will be attempted using the upstream output port that was identified.

2.5 MODEL GENERATION LIMITATIONS

Certain limitations exist in the Model Generation program due to array dimensions within the program. For most applications these limits should not be encountered. However, if they should be encountered they can usually be extended at the expense of larger core requirements to execute the program. The following table describes these limitations:

<u>Limitation Description</u>	<u>Maximum Value</u>
Standard components in library	150
Components per model	200
Inputs per any standard component	50
Outputs per any standard component	50
Tables per any standard component	15
Tables per model	100
Table dimension (words)	960

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3.0 SIMULATION PROGRAM

Once a model has been generated as described in Section 2, the user must describe the simulation he wishes to perform. This involves specifying the various parameters detailing the model components and setting the models initial conditions. It involves defining input data tables and the type and quantities of printed output, both tabular and plotted. The user must also specify the number of iterations he wishes to perform at each time step and the maximum number of component diagnostics. This section describes in detail the commands for specifying the simulation and gives some example output.

3.1 MODEL INPUT DATA

A dynamic system model requires that the values of numerous model parameters, tables and initial conditions, be provided to complete the model description. Sections 3.1.1, 3.1.2 and 3.2 describe the methods used to specify parameter values, tables, and initial conditions.

3.1.1 Scalar Data

PARAMETER VALUES (Default values = .99999)

This program command allows the numeric values of parameters to be loaded into the system model. The PARAMETER VALUES command is followed by one or more parameter names followed by a numeric value. Each name and its value are separated by one of the standard delimiter symbols. This command is used to specify the values of all system model parameters at the beginning of an analysis. It may also be used at any point between analyses to modify the value of one or more model parameters. A default value of .99999 is provided by the Model Generation program for all parameters not so specified.

Example 3.1-1

PARAMETER VALUES = CYCLES = 6.01, TO TI = 0, EC WP = .2,
CR CM = 15, LE CM = 30, MDEHS = 4.E5,

3.1.2 Tabular Data

If tabular data is required by the system model, it should be loaded before any of the simulation commands described in Section 3.4 are issued. Tables may be modified between analyses by loading new values. The tables required by a SIMWEST generated model are specified in the Input Requirements List. These tables may have either one or two independent variables. All data items are in a free field format with each item separated by one of the standard delimiters: comma [,], equal sign [=], left or right parenthesis () , or three or more consecutive blank spaces. The data items required for each table are placed on cards as follows:

Card 1	TABLE	table name	NX	NZ
Card 2*	Z table values			
Card 3*	X table values			
Card 4*	Y table values			

where: Table Name - The six character table name generated by the Model Generation program.

NX - The number of points in the primary independent variable table.

NZ** - The number of points in the secondary independent variable table.

Z table ** - Table of NZ secondary independent variable values.

X table - Table of NX independent table values.

Y table - 1 or NZ tables of NX dependent variable values.

* As many cards as required may be used. Each table must start with a new card and NZ, NX, and NX*NZ points must be given per table.

** These items are omitted for tables with one independent variable.

A copy of all tabular input data is printed as it is interpreted from data cards. The following example shows the data cards for a one and a two independent variable table.

Example 3.1-2

Card 1	TABLE, TABONE, 10
Card 2	1, 2, 3, 4, 5, 6, 7, 8, 9, 10
Card 3	11, 12, 13, 14, 15, 16, 17, 18, 19, 110
Card 4	TABLE, TABTWO, 5, 4
Card 5	10.3, 20.4, 30.5, 40.6
Card 6	1, 2, 3, 4, 5
Card 7	11, 12, 13, 14, 15
Card 8	21, 22, 23, 24, 25
Card 9	31, 32, 33, 34, 35
Card 10	41, 42, 43, 44, 45

The printout of these tables would be:

TABLE TABONE									
PRIMARY INDEPENDENT VARIABLE TABLE									
1.000	2.000	3.000	4.000	5.000	6.000	7.000	8.000	9.000	10.00
DEPENDENT VARIABLE TABLE									
11.00	12.00	13.00	14.00	15.00	16.00	17.00	18.00	19.00	110.00
TABLE TABTWO									
SECONDARY INDEPENDENT VARIABLE TABLE									
10.30	20.40	30.50	40.60						
PRIMARY INDEPENDENT VARIABLE TABLE									
1.000	2.000	3.000	4.000	5.000					
DEPENDENT VARIABLE TABLE									
11.00	12.00	13.00	14.00	15.00					
21.00	22.00	23.00	24.00	25.00					
31.00	32.00	33.00	34.00	35.00					
41.00	42.00	43.00	44.00	45.00					

3.2 INITIAL CONDITION AND INTEGRATION CONTROLS

INITIAL CONDITIONS (Default value = 0)

INT CONTROLS (Default value = 1.0)

These program commands may be used to specify initial condition values and the integrator status, (either active (=1) or frozen (=0)). Default values of 0. for initial conditions and 1 for integration controls are furnished by the simulation program. However, it is strongly recommended that values appropriate to the particular system model be furnished for the initial conditions.

Each of these commands is followed by phrases of the form of a state name followed by a numeric value.

Example 3.2-1:

INITIAL CONDITIONS = MA HS = 1.6E6, E TS = 600, VDELO = 0,

INT CONTROLS = MA HS = 0, E TS = 1, VDELO = 1,

ALL STATES (Default Condition)

NO STATES

These program commands may be used to activate or freeze all system integrators. These commands are normally used together with the INT CONTROLS command to specify the desired integrator configuration.

3.3 INITIAL CONDITION STORAGE COMMANDS

XIC-X
XIC-XIC1
XIC-XIC2
XIC-XIC3
XIC1-XIC
XIC2-XIC
XIC3-XIC

These program commands are used to transfer data from the current state vector, X, to the initial condition vector, XIC, and between the XIC vector and three auxiliary initial condition vectors XIC1, XIC2, XIC3.

Example 3.3-1

XIC1-XIC, XIC-X, XIC2-XIC

The three program commands shown above would take the current operating point (initial condition vector) and store it in vector XIC1; then transfer the current state, X, into XIC; and then store that value of XIC in XIC2.

3.4 SIMULATION COMMANDS

SIMULATE

This program command initiates simulation operation. Associated with this command are the program values:

<u>Default Values:</u>		
TINC	= time increment, hours	0.1
TMAX	= duration of the simulation run hours	1.0
OUTRATE	= output rate	1
PRATE	= print rate	1
PRINT CONTROL	= print control variable	0

These program commands specify the integration time increment, duration of simulation run, the simulation output rate, the printing rate, and the quantity of printing, at each point in time. These quantities should be specified before the first issuance of the SIMULATE command.

The Time increment, TINC, provides the integrator time step size, in hours, for the integrator. TINC also provides the report interval for which data will be available for printing or plotting. The default value for TINC is 0.1.

The duration of a simulation calculation in hours, is specified by the TMAX parameter. The default value of TMAX is 1.

The output rate parameter, OUTRATE, determines the sampling rate at which simulation data is added to plots. Thus, if OUTRATE is set equal to 10, data will be plotted every 10th time increment, TINC. The default value of OUTRATE is 1. OUTRATE should only be set to positive integer values.

The number of data samples plotted for a simulation analysis is thus given by:

$$\text{No. of Plotted Samples} = \frac{\text{TMAX}}{\text{TINC} * \text{OUTRATE}} + 1$$

For most simulation operation, the plotted output specified by the DISPLAY commands is the primary output and no line printer output is used. However, for diagnosing problems in a simulation, the line printer options provided by the PRINT CONTROL parameter allow large amounts of detailed information about the simulated system to be obtained.

The value of the PRINT CONTROL parameter controls the quantity of data printed at each print report interval as shown in Table 3.4-1. Options 1 through 4 give "snap-shots" of all states, rates, variables, and parameters of the system model at a particular point in time. Option 5 provides tabular lists

of up to 10 specified quantities.* The default value for PRINT CONTROL is 0.

TABLE 3.4-1

Print Control Values	
PRINT CONTROL	Resultant Lineprinter Output.
0	None (Default Condition)
1	All states, rates, and time
2	All states, rates, variables, and time
3	All states, rates, variables, and parameters at time = 0
4	All states, rates, variables, and parameters
5	Time and the quantities specified via PRINT VARIABLES command.

The PRATE parameter determines the sampling rate at which the simulation data specified by the PRINT CONTROL parameter is presented on the line-printer. Thus, if PRATE is set equal to 5, data will be printed on the line printer every 5th time it is added to the output plots. The rate of output to the lineprinter can never be greater than that to the plots. The default value of PRATE is 1. PRATE should only be set to positive integer values.

The number of data samples printed for a simulation analysis is thus given by:

$$\text{No. of Printed Samples} = \frac{\text{TMAX}}{\text{TINC} * \text{OUTRATE} * \text{PRATE}} + 1$$

*See the PRINT VARIABLES command description below.

Example 3.4-1:

```
PRINT CONTROL = 2, TINC = .01, TMAX = 10.,  
OUTRATE = 10, PRATE = 10, SIMULATE
```

In the example, the simulation would run for 10 hours. Plotted output would occur every .1 hour, (10* .01), and printed output would occur every 1. hour (10* 10* .01).

PRINT VARIABLES

This program command allows up to ten variables to be specified for printing under option 5 of the PRINT CONTROL. This command is followed by from one to ten state, rate, or variable names separated by delimiters. This command wipes out all previously stored PRINT VARIABLES names.

Example 3.4-2:

```
PRINT VARIABLES = MA HS, E TS, VDELO
```

3.5 PLOT DESIGNATION COMMANDS

```
DISPLAY1  
DISPLAY2  
DISPLAY3  
DISPLAY4  
DISPLAY5  
DISPLAY6
```

These program commands may be used to define the quantities to be displayed by lineprinter plots for simulation calculations. These commands must be issued before the simulation analysis is requested. From one to five plots may be specified per display. Each plot is specified by stating the dependent variable and the independent variable separated by the letters VS. If

desired, the independent and dependent axis scale ranges can also be specified. The independent scale range is specified by the word **XRANGE** followed by the minimum and maximum values for this scale. The dependent scale similarly is specified by the word **YRANGE**. If scale ranges are not specified, values will be used that span the given data.

SI MANUAL SCALES

SI AUTO SCALES (Default Condition)

The **SI MANUAL SCALES** command allows the plotted output requested by the **DISPLAY** commands to be plotted on manual scales specified by the **YRANGE** and **XRANGE** commands. The **SI AUTO SCALES** command can be used to return plotting to the automatic scaling mode. Auto scales are selected so that they span each plotted quantity. The auto scale option is the default used until manual scales are requested. The **PRINTER PLOTS** command is also required to obtain plots.

Example 3.5-1:

```
SI MANUAL SCALES, PRINTER PLOTS
DISPLAY1
WV2WD, VS, TIME, YRANGE = 10,40
P1 PD, VS, TIME, YRANGE = 0,1000
P2 PD, VS, TIME, YRANGE = 0,1000
DISPLAY2
P2 IV, VS, TIME
RE2BA, VS, TIME
RE1LO, VS, TIME
DISPLAY3
P1 PD, VS, P2 PD, YRANGE = 0,1000, XRANGE = 0,1000
```

TITLE

The TITLE command allows a title to be placed on all plotted output. Up to 74 characters may follow the delimiter that follows the TITLE command. The TITLE command may be changed before each analysis. Once defined, the title remains in effect until a new title is entered.

Example 3.5-2:

```
TITLE = BATTERY TEST MODEL
```

3.6 ITERATION AND DIAGNOSTIC CONTROL

There are three built-in parameters in any SIMWEST model : CYCLES, DLINEs and RESET. These parameters are specified similar to component parameters using the PARAMETER VALUES command.

CYCLES controls the number of iterations through the model to obtain steady state. If $CYCLES \leq 0$, then only one pass is made through the model. If CYCLES is a positive integer then the number of iterations through the model is equal to $CYCLES + 1$. If cycles is positive, but not an integer, then the number of iterations is equal to the smallest integer value exceeding cycles. A maximum of 20 iterations are permitted per time step. Most of the simple models of Section 8 require between four and six iterations per time step to attain steady state. A complex model with cascaded logic components may require more.

The task of finding the correct value for CYCLES is facilitated by the program printing at each time step all variables which have a greater than 5% change in value in the last iteration.

Since output statistics are only updated the last iteration, many of the variables printed indicating nonconvergence are just statistics, and as such should be ignored.

DLINES controls the amount of convergence related printout to be controlled as well as the amount of diagnostic printout put out by the library components. If DLINES >0 then the total number of diagnostic printouts is no greater than DLINES. Figure 3.6 shows a typical section of diagnostic printout using DLINES >0. If DLINES <0 then only library component diagnostics are printed with no greater than - DLINES of output. Typically, DLINES = 100 is sufficient to catch most simulation errors per run.

PC3PA	NONCONVERGENCE, OLD VALUE=	4.209	NEW VALUE=	6.109
SR UT	NONCONVERGENCE, OLD VALUE=	177.720	NEW VALUE=	264.359
PC3PA	NONCONVERGENCE, OLD VALUE=	6.109	NEW VALUE=	7.054
SR UT	NONCONVERGENCE, OLD VALUE=	264.359	NEW VALUE=	312.718
FLYWHEEL KINETIC ENERGY	39.875 FALLS BELOW MINIMUM REQUIREMENT			40.000
FLYWHEEL CLUTCH LOSS	1.217 EXCEEDS DELIVERABLE POWER			.400
SP MO	NONCONVERGENCE, OLD VALUE=	553.569	NEW VALUE=	601.994
SPCFL	NONCONVERGENCE, OLD VALUE=	543.583	NEW VALUE=	590.798
PC3PA	NONCONVERGENCE, OLD VALUE=	7.054	NEW VALUE=	8.152
SR UT	NONCONVERGENCE, OLD VALUE=	312.718	NEW VALUE=	370.217

FIGURE 3.6 TYPICAL DIAGNOSTIC OUTPUT

RESET controls the initialization value for the random number generators if several simulations are run back to back. If RESET >0 (Default) then the same random numbers are used for each simulation. If RESET ≤ 0 then the random numbers at the start of each simulation are obtained from the last value at the end of the previous simulation.

3.7 DEFINE COMMANDS

DEFINE STATES
 DEFINE RATES
 DEFINE PARAMETERS
 DEFINE VARIABLES

These program commands may be used to define the alphanumeric names that will be used to refer to states, rates, parameters, and variables. All system models formed by the Model Generation program have model related names generated for all states, variables, and parameters in the model. State variable derivatives, (Rates), are generated as R1, R2,... for all models. R1, R2, ... refer to the rates of the first, second,... states respectively. If it is desired to replace these machine generated names with other names, the DEFINE command may be used to substitute any eight character name of the analyst's choosing. These names are associated with the corresponding numeric quantities located in the labeled commons /CX/, /CXDOT/, /CP/, and /CV/. The appropriate location for each quantity is printed out along with the quantity name prior to each simulation. Each of these commands is followed by phrases containing the location numeric followed by an alphanumeric name with one to eight characters the first of which must be alphabetic.

Example 3.7:

```
DEFINE STATES
```

```
1 = PRESSURE, 2 = STROKE, 5 = VELOCITY, 7 = ANGLE
```

```
DEFINE PARAMETERS
```

```
5 = MASS, 35 = DCT AREA
```

```
DEFINE VARIABLES, 1 = T OUTLET, 2 = LIQ H2O
```

Note that the program commands, numeric values and alphanumeric names must be separated by delimiters which are: comma [,], equals [=], left parentheses [(], right parenthesis [)], or three or more consecutive spaces.

3.8 EXAMPLE OUTPUT

Figure 3.8 shows a sample of the output print format generated using PRINT CONTROL = 3. This sample is taken from the Wind Turbine and File Read run

ANALYSIS AND PLUTTER EXECUTION

DATE 072677

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TIME = .0000		STATES	
1 VDELU	.00000		
RATES		RATES	
1 M1	5.0009		
VARIABLES			
1 I TI	.00000	2 TO TI	.00000
6 MY TI	1.0000	7 MY TI	1.0000
11 M TAW	.25000	12 MVZMO	18.477
16 IIMND	-1.0000	17 P2 WT	241.84
21 MAPMT	795.36	22 MT WT	72080.
26 IO GH	895.48	27 PL GH	12.184
31 SAMHG	1.0000	32 AV HG	241.84
36 MS GE	1805.2	37 PL GE	12.224
41 SP GE	27.179	42 VANTAL	572.02
46 MEILU	636.24	47 LOZLU	572.02
51 TIMLU	1.0000	52 CN LU	-1.9575
3 TM TI	.00000	4 DM TI	1.0000
8 VANTAM	18.477	9 N TAW	446.00
13 MV WD	18.477	14 AV WD	20.354
18 TO WT	72080.	19 CO WT	12500
23 MPUNT	241.84	24 SP WT	30.230
28 EFZGR	.94961	29 MPZGR	.10000+11
33 SO HG	58485.	34 P2 GE	217.43
38 EFZGE	.89906	39 MP2GE	750.00
43 N TAL	446.00	44 TO TAL	.00000
48 SRELU	71.502	49 SDELU	27.179
5 DY TI	1.0000	10 TO TAW	.00000
15 M WD	58.846	20 GR WT	76.391
25 P2 GR	229.65	30 HS1GR	23.631
35 EE GE	.97710	40 MPNGE	.28991
45 M TAL	.25000	50 PC LU	38.011
PARAMETERS			
1 TO TI	.00000	2 NSTTAM	.00000
6 MSGMT	1800.0	7 BR WT	80.000
11 CPMT	.41000	12 CP WT	.99999
16 MP1GR	.10000+11	17 CC GH	1000.0
21 F3 HG	.00000	22 F4 HG	1.0000
26 F8 HG	.00000	27 F9 HG	.00000
31 F13HG	.00000	32 F14HG	.00000
36 FUPHG	1000.0	37 FLUNG	50.000
41 DA GE	.20000	42 SR GE	.50000-02
46 NSTTAL	.00000	47 ITFTAL	2.0000
51 STDLU	6.0000	52 VE LU	.25000-01
3 ITFTAM	1.0000	4 VO WT	21.000
8 EC WT	1.0000	9 AD WT	.23000-02
13 CC WT	16000.	14 CM WT	2000.0
18 CM GH	200.00	19 F1 HG	.00000
23 FS HG	.00000	24 F6 HG	.00000
28 F10HG	.00000	29 F11HG	.00000
33 F13HG	.00000	34 F16HG	.00000
38 MAPGE	750.00	39 KSYGE	1800.0
43 VU GE	400.00	44 CC GE	1000.0
48 NC LO	.57400-02	49 CT LO	4.0000
53 CYCLES	2.0100	54 DLINES	.99999
5 VR WT	28.350	10 LAMWT	9.4000
15 EF1GR	.99999	20 F2 HG	.00000
25 F7 HG	.00000	30 F12HG	.00000
35 PA HG	67.857	40 RASGE	.10000-01
45 CM GE	200.00	50 MN LO	.00000
55 RESET	.99999		
TIME = 12.00		STATES	
1 VDELU	97.264		
RATES		RATES	
1 M1	.63123		
VARIABLES			
1 I TI	12.000	2 TO TI	12.000
6 MY TI	1.0000	7 MY TI	1.0000
11 M TAW	.25000	12 MVZMO	13.444
16 IIMND	-1.0000	17 P2 WT	36.664
21 MAPMT	795.36	22 MT WT	.23555+06
26 IO GH	157.67	27 PL GH	1.4660
31 SAMHG	47.000	32 AV HG	38884.
36 MS GE	1800.7	37 PL GE	7.7533
41 SP GE	4256.0	42 VANTAL	1024.2
46 MEILU	1002.0	47 LOZLU	1024.2
51 TIMLU	1.0000	52 CN LU	-1.9575
3 TM TI	12.000	4 DM TI	1.0000
8 VANTAM	13.444	9 N TAW	446.00
13 MV WD	39.006	14 AV WD	20.354
18 TO WT	10456.	19 CO WT	12.125
23 MPUNT	795.36	24 SP WT	4861.1
28 EFZGR	.95999	29 MPZGR	.10000+11
33 SO HG	.24279+08	34 P2 GE	27.445
38 EFZGE	.74853	39 MP2GE	750.00
43 N TAL	446.00	44 TO TAL	.00000
48 SRELU	8481.5	49 SDELU	4256.0
5 DY TI	1.0000	10 TO TAW	.00000
15 M WD	58.846	20 GR WT	76.391
25 P2 GR	35.198	30 HS1GR	23.572
35 EE GE	.97710	40 MPNGE	.93304
45 M TAL	.25000	50 PC LO	50.180
TIME = 24.00		STATES	
1 VDELU	239.65		

FIGURE 3.8. SAMPLE PRINTER OUTPUT

described in Section 8.1, which is a very simple model. At each print time the output quantities are indexed by number and component name as they occur in the model. For example, first all the variables for component TI are printed, then all variables for component TAW, etc. The parameter values at time = 0 show both the input values and the default parameters. After T = 0 only the states, rates, and output variables are printed. Since all the model connection variables and output variables are printed, this mode is especially valuable for program debugging and analysis at a fixed time. The printer plots, samples of which are shown in Section 8, are useful for monitoring the time behavior of critical parameters such as energy in storage and percent of load delivered by storage.

4.0 JOB CONTROL PROCEDURES

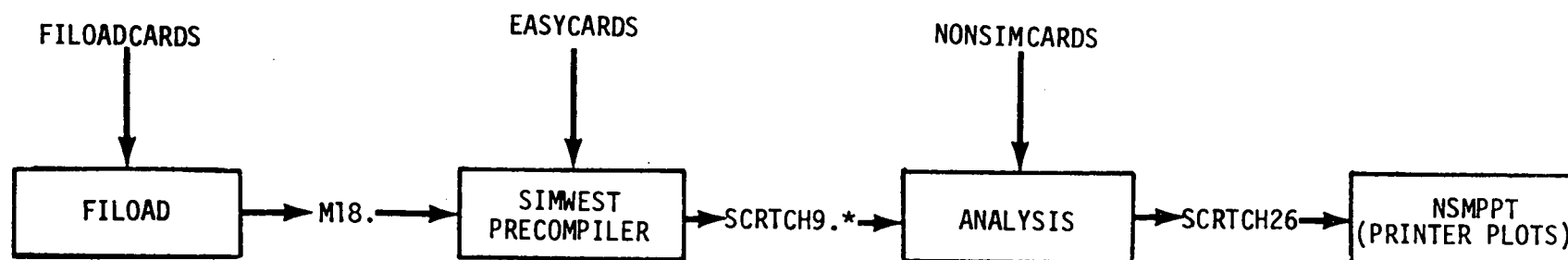
In this section, we describe job control procedures for running and maintaining the SIMWEST programs. For the convenience of the user, a number of procedure files have been set up which simplify the user control cards required. In Section 4.1, we describe the control cards for executing the model generation and analysis programs. Section 4.2 describes the procedures to maintain the programs and update the component library.

4.1 MODEL GENERATION AND ANALYSIS EXECUTION

Figure 4.1-1 shows an overview of the program structure to execute a simulation run. The program FILOAD is only executed when the component library is updated, and is thus described in the next section. The user input data for the model generation program is put on a file called EASYCARDS. A procedure file called XQTEASY is then used to generate the model Fortran and compile this model. Similarly, the user input data for the analysis program is put on a file called NONSIMCARDS, and a file called XQTANALYSIS maps the relocatable elements into absolute file elements, and executes both the simulation and printer plot programs.

A job control stream to execute these programs in a batch environment is given by:

```
@RUN ...  
@DELETE,C EASYCARDS.  
@ASG,UP EASYCARDS.  
@DATA,IL EASYCARDS.  
.  
.  
.  
INPUT DATA DECK  
FOR MODEL  
.  
.  
.  
@END  
@ASG,A XQTEASY.
```



*SCRTCH9 IS FORTRAN SOURCE CODE OUTPUT

FIGURE 4.1-1 SIMWEST PROGRAM EXECUTION STRUCTURE

```

@ADD,PL XQTEASY.
@DELETE,C NONSIMCARDS.
@ASG,UP NONSIMCARDS.
@DATA,IL NONSIMCARDS.
.
.
.
INPUT DATA DECK
FOR ANALYSIS
.
.
.
@END
@ASG,A XQTANALYSIS.
@ADD,PL XQTANALYSIS.
@FIN

```

The job control procedures XQTEASY and XQTANALYSIS are shown in Figures 4.1-2 and 4.1-3. If a user is creating data inputs from a terminal, then it may be somewhat simpler to create new job control procedures similar to XQTEASY and XQTANALYSIS, but substituting his data input file names for EASYCARDS and NONSIMCARDS, respectively. If the same model is used for a series of runs, then only the analysis program is required for execution. However, it is safer and also relatively inexpensive to execute both programs when using the above job stream. Whenever the file read component is desired, the user must either substitute his file for F1 or F2, or add the following job cards to XQTANALYSIS:

```

@ASG,A MYFILE.
@USE M, MYFILE.

```

where MYFILE is the user time history file and M is a unit number between 13 and 18. (See 7.38 for a discussion of the tape/file read component.)

4.2 PROGRAM MAINTENANCE AND LIBRARY UPDATES

Whenever the component library is updated, the user must compile the Fortran code and run the FILOAD program to furnish the model generation program com-

```

@HDG SIMWEST MODEL GENERATION
@ASG,AX MGABS.
@ASG,A M18.
@USE 18,M18.
@ASG,T M7.
@USE 7,M7.
@ASG,T SCRTCH8.
@USE 8,SCRTCH8.
@DELETE,C SCRTCH9.
@ASG,UP SCRTCH9.
@USE 9,SCRTCH9.
@ASG,T SCRTCH10.
@USE 10,SCRTCH10.
@ASG,T SCRTCH11.
@USE 11,SCRTCH11.
@ASG,T SCRTCH12.
@USE 12,SCRTCH12.
@ASG,A EASYCARDS.
@USE 5,EASYCARDS.
@XQT MGABS.EASY
@ASG,AX ASRO.
@ASG,AX ASSI.
@ADD,PL 9.
@FREE 18.,7.,8.,9.,10.,11.,12.

```

FIGURE 4.1-2 XQTEASY JOB CONTROL FILE

```

@HDG SIMWEST ANALYSIS
@ASG,AX MAPANALYSIS.
@ADD,PL MAPANALYSIS.
@ASG,AX ASABS.
@ASG,AX F1.
@USE 11,F1.
@ASG,AX F2.
@USE 12,F2.
@ASG,T SCRTCH25.
@USE 25,SCRTCH25.
@DELETE,C SCRTCH26.
@ASG,UP SCRTCH26.
@USE 26,SCRTCH26.
@ASG,AX NONSIMCARDS.
@USE 5,NONSIMCARDS.
@XQT ASABS.NONSIM
@XQT ASABS.NSMPPT
@FREE 11.,12.,25.,26.

```

FIGURE 4.1-3 XQTANALYSIS JOB CONTROL FILE

ponent input and output name lists. A job control stream to compile a new component denoted DC and add it to the component library is given by:

```

@ASG,T SOURCE.
@DATA,IL SOURCE.
@FOR,IS COSI.DC,CORO.DC
.
.
.
USER FORTRAN SUBROUTINE DC
.
.
.
@END
@ASG,A COSI.
@ASG,A CORO.
@ADD,PL SOURCE.
@ASG,A CMPLCO.
@ED,U CMPLCO.
ADD SOURCE.
EXIT

```

If an old component is to be updated, then one can edit the source code on CMPLCO and recompile entirely, or copy the edited subroutine including the @FOR,IS control card onto a new file and recompile. A job stream to execute the FILOAD program is given by:

```

@DELETE,C FILOADCARDS.
@ASG,UP FILOADCARDS.
@DATA,IL FILOADCARDS.
.
.
.
USER INPUT DATA
FOR FILOAD
.
.
.
@END
@ASG,A XQTFILOAD.
@ADD,PL XQTFILOAD.

```


The procedure file XQTFILOAD is shown in Figure 4.2-1. If a mistake is made in the input cards, it is possible that the output file M18 will be destroyed. As a backup, M18 is copied onto M18X before FILOAD is run.

```
@HDG FILOAD EXECUTION
@ASG,AX FILOAD4.
@DELETE,C M19.,M18X.
@ASG,UP M19.,F/O/TRK/1000/      . FILOAD DATA FILE
@ASG,UP M18X.,F/O/TRK/1000/
@ASG,AX DUMPF9.
@ASG,AX M18.
@COPY M18.,M18X.
@USE 18,M18.
@USE 19,M19.
@USE 9,DUMPF9.
@ASG,AX FILOADCARDS.
@USE 3,FILOADCARDS.
@XQT FILOAD4.
@COPY 19.,18.
@FREE 18.,19.,9.
```

FIGURE 4.2-1 XQTFILOAD JOB CONTROL FILE

It may be necessary to modify the Fortran code for one or more of the SIMWEST programs from time to time. In this case, the procedure is to edit the source file, recompile the file, and remap the relocatables to obtain absolute file elements. Table 4.2 gives the file names for using this procedure.

TABLE 4.2 SIMWEST MAINTENANCE FILE DIRECTORY

	<u>LIBRARY UPDATE</u>	<u>MODEL GENERATION</u>	<u>ANALYSIS</u>	<u>PRINTER PLOTS</u>
FORTRAN SOURCE FILES - SDF	UTIL FILOAD	CMPLMG CMPLMG2	CMPLAS CMPLAS2	NSMPPT
FORTRAN SOURCE FILES - ELT	FSSI	MGSI	ASSI	ASSI
RELOCATABLE FILES	FSRO	MGRO	ASRO	ASRO
COLLECTION PROCEDURES	MAPFILOAD	MAPEASY	MAPANALYSIS	MAPNSMPPT

The collection procedures are shown in Figures 4.2-2 to 4.2-5. As an example, the jobstream to edit, recompile and remap a subroutine in CMPLMG is given by:

```

@ASG,A CMPLMG.
@ED,U CMPLMG.
.
.
.
FORTRAN EDITING
.
.
.
@ASG,A MGSI.
@ASG,A MGRO.
@ADD,PL CMPLMG.
@ASG,A MAPEASY.
@ADD,PL MAPEASY.

```

```

@ASG,AX FSRO.
@PREP FSRO.
@ASG,AX MAPFSSI.
@ASG,AX FILOAD4.
@MAP,I MAPFSSI.FILOAD,FILOAD4.
  IN FSRO.FILOAD
  LIB:FSRO.
END

```

FIGURE 4.2-2 MAPFILOAD PROCEDURE FILE

```

@ASG,AX MGRO.
@PREP MGRO.
@ASG,AX MAPMGSI.
@ASG,AX MGABS.
@ASG,AX FSRO.
@PREP FSRO.
@MAP,I MAPMGSI.EASY,MGABS.EASY
  IN MGRO.EASY
  LIB FSRO.,MGRO.,FSRO.
END

```

FIGURE 4.2-3 MAPEASY PROCEDURE FILE

```

@ASG,AX FSRO.
@ASG,AX ASRO.
@ASG,AX CORO.
@PREP CORO.
@PREP FSRO.
@PREP ASRO.
@ASG,AX MAPASSI.
@ASG,AX ASABS.
@MAP,I MAPASSI.NONSIM,ASABS.NONSIM
  IN ASRO.NONSIM
  IN ASRO.BLOCKDA
  IN ASRO.MODEL
  LIB FSRO.,ASRO.,FSRO.,CORO.
END

```

FIGURE 4.2-4 MAPANALYSIS PROCEDURE FILE

```
@ASG,AX FSRO.  
@ASG,AX ASRO.  
@PREP FSRO.  
@PREP ASRO.  
@ASG,AX MAPASSI.  
@ASG,AX ASABS.  
@MAP,I MAPASSI,NSMPPT,ASABS.NSMPPT  
  IN ASRO.NSMPPT  
  LIB FSRO.,ASRO.,FSRO.  
END
```

FIGURE 4.2-5 MAPNSMPPT PROCEDURE FILE

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5.0 DIAGNOSTICS

Diagnostic messages are printed by both the model generation and the simulation program. In addition, individual library components generally have diagnostic printout associated with them. The diagnostics associated with the model generation program are discussed in Section 2. Section 5 describes the diagnostics associated with the simulation program and the library components.

5.1 WARNING MESSAGES

One or more of the following warning messages will occur if the program encounters difficulty in interpreting analysis instructions or performing an analysis. These messages will be preceded by the flag:

*** WARNING ***

Message symbols xxx, zzz, or nnn are used to indicate phrases from the analysis description that are included as part of the warning message. The following messages are listed in alphabetical order:

1. A VALID PARAMETER NAME MUST PRECEDE THE NUMERIC VALUE nnn

This message indicates that a valid parameter name was not identified preceding the numeric value nnn. Check for missing delimiters or misspelled parameter name.

2. xxx CAN'T BE SET EQUAL TO zzz. VALUE MUST BE NUMERIC

Check for missing numeric value or delimiters.

3. CAN'T IDENTIFY xxx AS A VALID PRINT VARIABLE

Check spelling of xxx or for missing delimiters.

4. CAN'T IDENTIFY xxx VALUE WILL BE IGNORED.

This will result in not setting the quantity intended by xxx to its new value. Check for spelling of xxx or for missing delimiters.

5. CAN'T INTERPRET xxx

The phrase xxx cannot be recognized as a valid program command, program name, or program value. Check spelling of xxx or for missing delimiters.

6. nnn EXCEEDS THE ALLOWABLE INDEX RANGE FOR xxx THIS QUANTITY WILL NOT BE DEFINED

The number nnn was outside the allowable range of states, rates, variables, or parameters. Therefore, the name xxx cannot be assigned as a name for the nnnth state, rate, variable or parameter.

7. NON-ALPHA NAME ON THIS CARD --- xxx. WILL IGNORE THIS CARD.

The table inputs routine expected an alphanumeric table name but encountered a numeric value on the data card printed. Check the sequence and number of tabular data cards to assure that they match those required by the model's tables and table input formats. See Section 3.1.2 for correct formats.

8. NON-NUMERIC DATA ON THIS CARD --- xxx. WILL READ NEXT TABLE

The table input routine expected a numeric value but encountered an alphanumeric name on the data card printed. Check that the sequence and number of tabular data cards matches the model's tables and table input formats. See Section 3.1.2 for correct formats.

9. nnn PRIMARY and xxx SECONDARY INDEPENDENT VARIABLE POINTS EXCEEDS THE
zzz WORD STORAGE LIMIT FOR THE FOLLOWING TABLE. SOME DATA WILL BE LOST.

The maximum amount of data allowed for each table is given in the Input Requirements List produced by the Model Generation program. Check that given data falls within this limit or for data card errors.

5.2 DIAGNOSTIC MESSAGES FOR LIBRARY COMPONENTS

A diagnostic message associated to a component is printed when a variable gets out of bounds during analysis. Adjustment of component parameters may be necessary.

In component alphabetical order, these diagnostic messages are:

AD: INPUT POWER xxxx TOO HIGH RELATIVE TO ADMITTANCE xxxx AND RATED VOLTAGE
xxx
ADMITTANCE POWER LOSS xxxx EXCEEDS INPUT POWER xxxx

BA: POWER REQUEST xxxx EXCEEDS BATTERY CAPABILITY. CHECK VC, VO, AND RT.

BN: BN INLET AIR MASS FLOW RATE xxxx GREATER THAN MAXIMUM ALLOWABLE xxxx

CO: MAX ITERATIONS FOR COMPRESSOR EFFICIENCY. NP, XNP, RS = xxxx, xxxx,
xxxx

CS: CS STORAGE TEMPERATURE xxxx GREATER THAN ALLOWABLE xxxx
CS MASS OF AIR IN STORAGE xxxx BELOW MINIMUM ALLOWABLE xxxx
CS MASS OF AIR IN STORAGE xxxx EXCEEDS MAXIMUM ALLOWABLE xxxx

FL: FLYWHEEL POWER LOSS xxxx EXCEEDS CHARGING POWER xxxx
FLYWHEEL LOSS xxxx EXCEEDS DISCHARGING POWER xxxx
FLYWHEEL CLUTCH LOSS xxxx EXCEEDS MAXIMUM INPUT POWER xxxx
FLYWHEEL CLUTCH LOSS xxxx EXCEEDS DELIVERABLE POWER xxxx

FLYWHEEL KINETIC ENERGY xxxx EXCEEDS CAPACITY xxxx
FLYWHEEL KINETIC ENERGY xxxx FALLS BELOW MINIMUM REQUIREMENT xxxx

GE: GENERATOR OUTPUT EXCEEDS RATED POWER

HS: HS INLET MASS FLOW RATE xxxx OR OUTLET MASS FLOW RATE xxxx IS GREATER
THAN MAXIMUM xxxx
HS RESERVOIR VOLUME xxxx EXCEEDED MAXIMUM ALLOWABLE xxxx
HS RESERVOIR VOLUME xxxx DROPPED BELOW MINIMUM xxxx

HT: HT TURBINE CHARACTERISTIC PARAMETER OUT OF RANGE
HT INLET MASS FLOW RATE xxxx GREATER THAN MAXIMUM DESIGN VALUE

HX: HX EXIT TEMPERATURE xxxx GREATER THAN MAXIMUM ALLOWABLE xxxx

IV: IV POWER LOSS xxxx EXCEEDS INPUT POWER xxxx CHECK RATED DC VOLTAGE VDC

MB: WARNING-DIVISOR IN MB EQUALS 0., HAS BEEN SET = 1.

MO: MOTOR INPUT POWER xxxx .GT. RATED INPUT POWER xxxx
MOTOR SLIP xxxx EXCEEDS RATED POWER SLIP xxxx
STATOR RESISTANCE xxxx OR DAMPING xxxx TOO HIGH FOR MOTOR

RE: RE POWER LOSS xxxx EXCEEDS INPUT POWER xxxx
RE, AC INPUT POWER xxxx TOO LARGE IN RELATION TO TRANSFORMER REACTANCE
xxxx AND RATED AC VOLTAGE xxxx

TA: FILE DATA OUT OF RANGE. INITIAL VALUE = xxxx ON UNIT xx
TIME POINT PAST TABLE RANGE. LAST VALUE = xxxx ON UNIT xx
READ ERROR OR END OF FILE ON UNIT xx

TR: TRANSMISSION POWER LOSS xxxx EXCEEDS INPUT xxxx

TRANSMISSION POWER LOSS xxxx EXCEEDS MAXIMUM INPUT POWER

TS: TS WORKING FLUID FLOW RATE xxxx GREATER THAN MAXIMUM ALLOWED xxxx

TS INPUT POWER xxxx GREATER THAN MAXIMUM ALLOWED CHARGE RATE xxxx

TS STORAGE TEMPERATURE xxxx OUTSIDE MINIMUM xxxx OR MAXIMUM xxxx

TU: TURBINE BACK PRESSURE xxxx GREATER THAN STORAGE VESSEL PRESSURE xxxx

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6.0 CREATION OF NEW LIBRARY COMPONENTS

The addition of new standard components to the SIMWEST library involves two steps. The first is the design of the component. This design must conform to certain design conventions if the new component is to be compatible with existing components. Section 6.1 discusses these design conventions and the addition of the component subroutine to the SIMWEST library. The second step involves the addition of the new component's input and output description to the SIMWEST file M18. File M18 is used by the precompiler to generate subroutine calling sequences for the library components. Section 6.2 discusses the use of the FILOAD program to accomplish this task.

6.1 LIBRARY COMPONENT CODING

6.1.1 Component Call Sequence

The items in the component subroutine call sequence must be arranged in the following order:

1. Tables
2. Output Quantities
3. Input Quantities

Tables or inputs may not be present in the subroutine call sequence. However those items that are present must follow the sequence given above.

Dummy argument names for the call sequence quantities that are used within each subroutine should be chosen to match the physical quantity names placed in the input, output, and table name lists. Exceptions to this policy may be made when integer names (names starting with I through N) must be avoided or when additional letters will clarify the name.

The subroutine name must contain only two characters and must not duplicate the name of an existing standard component.

Tables

The table arrays must be dimensioned within the component subroutine. They must be dimensioned with only one subscript; e.g. `DIMENSION TABLE (1)`. When table data is passed to the component subroutine, the first word in the array contains the name of the table. The second word contains the number of values given for the primary independent variable. The third word contains the number of values given for the secondary independent variable. Both of these numbers are stored as REAL quantities and must be converted to INTEGER before they can be used as a subscript. This can be done by a statement such as:

```
NX = TABLE (2) - number of primary independent variables
NZ = TABLE (3) - number of secondary independent variables
```

If there is a secondary independent variable, the secondary independent variable array will begin with the fourth word in the array. Thus if this array is designated as `z(1), z(2), ...,` then:

```
z(1) = TABLE (4)
z(2) = TABLE (5)
z(3) = TABLE (6)
.      .
.      .
.      .
```

The primary independent variable array begins with word `NZ + 4`. Thus if this array is designated as `X (1), X(2), ... ,` then:

```
X(1) = TABLE (NZ + 4)
X(2) = TABLE (NZ + 5)
.      .
.      .
.      .
```

The dependent variable array begins with word $NX + 4$ if there is no secondary independent variable. Thus if this array is designated as $Y(1), Y(2), \dots$, then:

$Y(1) = \text{TABLE } (NX + 4)$

$Y(2) = \text{TABLE } (NX + 5)$

• •
• •
• •

If there is a secondary independent variable array and this array was designated $Y(I, J)$, with $1 \leq I \leq NX$ and $1 \leq J \leq NZ$, then $Y(I, J)$ would be related to the table array as:

$Y(I, J) = \text{TABLE } (NX + NZ + 3 + I + (J - 1) * NX)$

Normally the individual elements in the table are not used directly but are passed to a table look-up routine. In this case the starting address of the X , Y , and Z tables would be referred to as:

$Z(1) = \text{TABLE } (4)$ secondary independent variable table

$X(1) = \text{TABLE } (NZ + 4)$ primary independent variable table

$Y(1, 1) = \text{TABLE } (NX + NZ + 4)$ dependent variable table

If more than one table is used by a component subroutine, the table names must appear in the same sequence in the table name list stored in M18 file as in the subroutine call sequence.

Example 6.1: Given a component, HA, that requires the tables TPH and TPC as an inputs. The call sequence of this subroutine would appear as:

SUBROUTINE HA(TPH, TPC, ...

Output Quantities

The term "output quantity" refers to information that is calculated and then "output" by a particular component subroutine. This is not to be confused with the "outlet quantities" of the component. The outlet quantities are associated with a particular component port as a result of assigning a positive direction of power or information flow through the component. Some outlet quantities may be calculated by the component subroutine and thus become output quantities of that component. While other outlet quantities may be furnished to the component subroutine and thus become input quantities to that subroutine.

The output quantities should be grouped together by port. That is, all outlet, (port two quantities), then all inlet, (port one quantities), etc. If a component has multiple outlet ports, the output quantities associated with each outlet port should be grouped together and listed before any inlet port output quantities.

Certain output quantities may be internal to the component and not associated with any port. In other cases the same output quantity may be associated with several ports. In such cases, no port designation is assigned to the output quantity. Such quantities are referred to as "universal port" quantities. As such, they are allowed to connect to any other similar physical quantity regardless of the input quantities port number. This is not the case for quantities with specified port numbers. Once a connection has been made between an input and output quantity with given port numbers, only connections of matching physical quantities with those port numbers occur. Manual override of this provision can be made by specifying particular physical quantity connections.

Three quantities are required for each state variable output. The first is the state variable, the second is the state variable derivative, (rate),

and the third is an integer quantity, the integrator control variable.

Example: Given a component, HA, with the following outputs:

Physical Quantity	Port No.	
T	3	} Outlet Ports
T	4	
P	1 (State Variable)	} Inlet Ports
P	2 (State Variable)	

The call sequence arguments for these outputs would be:

SUBROUTINE HA(TPH,TPC,T3,T4,P1,P1DOT,IP1,P2,P2DOT,IP2,...

Input Quantities

The term "input quantity" refers to information that is provided to a particular component subroutine. This is not to be confused with the "inlet quantities" of the component. The inlet quantities are associated with a particular component port as a result of assigning a positive direction of power or information, through the component. Some inlet quantities may be calculated by the component subroutine and thus become output quantities of that component, while other inlet quantities may be furnished to the component subroutine and thus become input quantities to that subroutine.

The input quantities should be grouped together by port. That is, all inlet, (port one quantities), then all outlet, (port two quantities), etc. Port designations for two port components which have the same physical quantity on both inlet and outlet will be: port 1 for upstream or inlet port and port 2 for downstream or outlet port. It is important that the inlet port quantities be listed before any outlet port quantities. If a component has multiple inlet ports, the input quantities associated with each inlet port should be grouped together and listed before any outlet port quantities.

Certain input quantities may be internal to the component and not associated with any port. In other cases the same input quantity may be associated with several ports. In such cases, no port designation is assigned to the input quantity. Such quantities are referred to as "universal port" quantities. As such, they are allowed to connect to any other similar physical quantity regardless of the output quantities port number. This is not the case for quantities with specified port numbers. Once a connection has been made between an input and output quantity with given port numbers, only connections of matching physical quantities with those port numbers occur. Manual override of this provision can be made by specifying particular physical quantity connections.

Example: Given the component HA described in the above example, with the following inputs:

Physical Quantity	Port No.	
T	1	} Inlet Ports
T	2	
P	3	} Outlet Ports
P	4	
AKH	(universal port quantity)	

The call sequence for these inputs would follow the output arguments, giving the complete call sequence:

```
SUBROUTINE HA(TPH,TPC,T3,T4,P1,P1DOT,IP1,P2,P2DOT,IP2,T1,T2,P3,P4,AKH)
```

The call sequence for standard component subroutines should follow the order shown in Table 6.1-1.

6.1.2 Additions and Modifications to Component Library

Section 4.2 describes the job control procedures to add a new component to the component library, compile the source code that describes the new component and add the relocatable binaries to the component library CORO.

TABLE 6.1-1

COMPONENT SUBROUTINE
CALL SEQUENCE ORDER

1. Tables
2. Output Quantities
 - 2.1 All Outlet Port Quantities*
 - 2.2 All Inlet Port Quantities* (feedback variables)
 - 2.3 All Other Output Quantities
3. Input Quantities
 - 3.1 All Inlet Port Quantities*
 - 3.2 All Outlet Port Quantities* (feedback variables)
 - 3.3 All Other Input Quantities

* Group quantities with the same port number together. If multiple inlet or outlet ports exist, arrange port quantities in order of increasing port numbers.

6.1.3 Coding Conventions

There are several coding rules which apply to any component coded. First of all, the calling sequence must be ordered so that it agrees with that constructed from the Fiload program. Hence the calling sequence begins with table arrays, is followed by output variables, and then by input parameters. State variables require three sequential parameters in the calling sequence: the state variable, the state derivative, and an integer valued integration control. With the exception of the latter, all parameters in the calling sequence are real valued. In general one cannot use any local variables or arrays to store information from call to call since there may be several components in the model which call a given subroutine. In other words, local variables can only be used for scratch calculations, unless the computed information is based on COMMON block inputs.

Most of the coding conventions and techniques used are illustrated in Figures 6.1-1 and 6.1-2. Figure 6.1-1 shows the code for the simple power curve component WP. Following the call sequence are a number of comment cards including the component purpose and calling sequence. The table PW is treated as a single dimension Fortran array. Power output is obtained from the table interpolation subroutine TBLU1. (Use of the table interpolation routines TBLU1 and TBLU2 is explained in Section 2.1). The rest of the code shows the conventions used to compute output statistics and add costs for the cost summary. IMPL is an integer variable which indicates the iteration control status:

IMPL = 0 the first time in a simulation that the model (EQMO) is
called
= 1 if more iterations and hence subroutine calls are expected at a given time step
>1 the final iteration through the model.

Hence when IMPL = 0, subroutine variables are initialized, default values are assigned, etc. The statistics are only updated at the final iteration

```

00100 1* CWP
00101 2* SUBROUTINE WP ( PW,BI,PO,AMI,AMP,SP,CO,VO,WVO,WV1,WV,CCI,CHI,EC)
00101 3* C
00101 4* C PURPOSE MODEL THE WIND TURBINE AND GENERATOR USING A POWER CURVE
00101 5* C
00101 6* C WRITTEN BY A.W. WARREN VERSION 1, MARCH 3 1977
00101 7* C
00101 8* C CALL SEQUENCE
00101 9* C TABLES
00101 10* C PW = WIND GENERATION POWER IN KW VERSUS WIND VELOCITY IN MPH
00101 11* C
00101 12* C OUTPUTS
00101 13* C BI = OUTPUT BUS CURRENT, AMPS
00101 14* C PO = POWER OUTPUT, KW
00101 15* C AMI = MAX. OBSERVED CURRENT, AMPS
00101 16* C AMP = MAX. OBSERVED POWER, KW
00101 17* C SP = TOTAL OUTPUT ENERGY, KWH
00101 18* C CU = OPERATING COST, $
00101 19* C
00101 20* C INPUTS
00101 21* C VO = RATED BUS VOLTAGE, VOLTS
00101 22* C WVO = POWER CUTIN VELOCITY, MPH
00101 23* C WV1 = POWER CUTOFF VELOCITY, MPH
00101 24* C WV = WIND VELOCITY, MPH
00101 25* C CCI = CAPITOL COST / YEAR, $
00101 26* C CHI = MAINTENANCE COST / YEAR, $
00101 27* C EC = CONTROL ENERGY RATE, $/HR
00101 28* C
00103 29* DIMENSION PW(1)
00104 30* COMMON / CIMPL / IMPL
00105 31* COMMON/COST/ CC,CM,COP /CTIME/ TIME /CSIMUL/ DUM(6),TINC,TMAX
00105 32* C
00105 33* C POWER OUTPUT CALCULATIONS
00105 34* C
00106 35* PO = 0.
00107 36* IF(WV.LT.WVO .OR. WV.GT.WV1) GO TO 10
00111 37* N = PW(2)
00112 38* PO = TBLU1(WV,PW(4),PW(4+N),1,-N)
00113 39* 10 BI = PO*1000/VO
00113 40* C STATISTICS
00113 41* C
00114 42* IF(IMPL.GT.0) GO TO 20
00116 43* CO = 0.
00117 44* AMI = 0.
00120 45* AMP = 0.
00121 46* SP = 0.
00122 47* TMAX1=TMAX*.99999
00123 48* 20 IF(IMPL.LE.1) RETURN
00125 49* AMI = AMAX1(AMI,BI)
00126 50* AMP = AMAX1(AMP,PO)
00127 51* SP = SP + PO*.5*TINC
00130 52* CO = CO + EC*.5*TINC
00130 53* C COST SUMMATION
00131 54* IF( TIME.LT.TMAX1) RETURN
00133 55* CC = CC + CCI
00134 56* CM = CM + CHI
00135 57* COP = COP + CO
00136 58* RETURN
00137 59* END
) FOR

```

FIGURE 6.1-1 SAMPLE COMPONENT CODE

```

00100      10      CGR      SUBROUTINE GE(P2,EE,RS,PL,EF2,P2,PMN,SP,P1,RAP,RSY,RAS,DA,SW,VN,
00101      20      1 (EF1,PM1,CCI,CMI)
00101      30      C
00101      40      C PURPOSE      MODEL AC INDUCTION GENERATOR
00101      50      C
00101      60      C METHOD      MECHANICAL AND ELECTRICAL EFFICIENCIES ARE USED TO COMPUTE
00101      70      C      OUTPUT POWER. ROTOR SPEED IS COMPUTED ASSUMING POWER IS
00101      80      C      PROPORTIONAL TO SLIP.
00101      90      C
00101     100      C      WRITTEN BY A.H. HARNEN                                VERSION 1, MARCH 16 1977
00101     110      C
00101     120      C CALL SEQUENCE
00101     130      C      OUTPUTS
00101     140      C      P2 = OUTPUT POWER, KW
00101     150      C      EE = ELECTRICAL EFFICIENCY
00101     160      C      RS = ROTOR SPEED, RPM
00101     170      C      PL = POWER LOSS, KW
00101     180      C      EF2 = OUTPUT PRODUCT EFFICIENCY
00101     190      C      PM2 = MAXIMUM OUTPUT POWER, KW
00101     200      C      PMN = MAX. (OBSERVED) OUTPUT POWER / RATED POWER
00101     210      C      SP = TOTAL OUTPUT ENERGY, KWH
00101     220      C
00101     230      C      INPUTS
00101     240      C      P1 = INPUT POWER, KW
00101     250      C      RAP = RATED OUTPUT POWER, KW
00101     260      C      RSY = SYNCHRONOUS ROTOR SPEED, RPMN
00101     270      C      RAS = RATED POWER SLIP (DEFAULT = .05)
00101     280      C      DA = MECHANICAL DAMPING, JOULE-SEC
00101     290      C      SR = STATOR RESISTANCE, OHMS
00101     300      C      VO = RATED RMS VOLTAGE, VOLTS
00101     310      C      EF1 = INPUT PRODUCT EFFICIENCY
00101     320      C      PM1 = MAXIMUM INPUT POWER, KW
00101     330      C      CCI = CAPITAL COST/YEAR, $
00101     340      C      CMI = MAINTENANCE COST/YEAR, $
00101     350      C
00101     360      C
00101     370      C      COMMON /CINPL/ INPL,ICNT /CTIME/ TIME
00101     380      C      COMMON /COST/ CC,CH,CO,CV /CSIMUL/ DUM(6),TINC,TMAX
00101     390      C      INITIALIZATION
00101     400      C
00101     410      C      IF (INPL.GT.0) GO TO 10
00101     420      C      EFF = 1.
00101     430      C      TMAX1 = TMAX*.99999
00101     440      C      IF (RSY.EQ..99999) RSY = 1800.
00101     450      C      IF (RAS.EQ..99999) RAS = .05
00101     460      C      IF (DA.EQ..99999) DA = 0.
00101     470      C      IF (SR.EQ..99999) SR = 6.0/RAP
00101     480      C      IF (VO.EQ..99999) VO = 400.
00101     490      C      IF (PM1.EQ..99999) PM1 = 1.E10
00101     500      C      PMN = 0.0
00101     510      C      SP = 0.0
00101     520      C      RAT1 = RAP*1000./VO
00101     530      C      EE = RAP/(RAP + SR*.001*RAT1**2)
00101     540      C
00101     550      C      COMPUTE ROTOR SPEED AND OUTPUT POWER
00101     560      C
00101     570      C      10 IF (P1.GT.0.) GO TO 20
00101     580      C      P2 = 0.0
00101     590      C      PL = 0.0
00101     600      C      RS = RSY
00101     610      C      GO TO 30
00101     620      C
00101     630      C      20 A = RAP/(EE+RAS)
00101     640      C      B = RSY/(1 + RSY**2*DA*1.0966E-5)
00101     650      C      RS = MAX(A + P1)
00101     660      C      P2 = RAP*(RS/RSY - 1)/RAS
00101     670      C      IF (P2.GT.RAP.AND.(INPL.EQ.2)) WRITE(6,100)
00101     680      C      100 FORMAT(1H0, 40X,37HGENERATOR OUTPUT EXCEEDS RATED POWER /)
00101     690      C
00101     700      C      IF (P2.GT.RAP .AND. INPL.EQ.2) ICNT=ICNT+1
00101     710      C      PL = P1 - P2
00101     720      C      EFF = P2/P1
00101     730      C      30 EF2 = EF1*EFF
00101     740      C      PM2 = AMIN1(RAP, PM1*EFF)
00101     750      C
00101     760      C      STATISTICS
00101     770      C      IF (INPL.LE.1) RETURN
00101     780      C      PMN = AMAX1(PMN, P2/RAP)
00101     790      C      SP = SP + P2*.5*TINC
00101     800      C
00101     810      C      COST SUMMATION
00101     820      C      IF (TIME.LT.TMAX1) RETURN
00101     830      C      CC = CC + CCI
00101     840      C      CH = CH + CMI
00101     850      C
00101     860      C      RETURN
00101     870      C      END
END FOR

```

FIGURE 6.1-2 SAMPLE COMPONENT CODE

when the model has presumably attained steady state values. Finally, the costs are added up when the simulation has reached the maximum time point. Capital costs, maintenance costs, and operating costs are stored in the first three locations of common block COST.

Figure 6.1-2 shows the code for the generator component GE. The program automatically assigns default parameters = .99999. Hence, when IMPL = 0 component dependent default values are assigned whenever the .99999 default is assumed. The code near Format statement 100 shows a typical diagnostic printout. The diagnostic is only printed if IMPL = 2 since we need only diagnose errors at the final iteration. Note that a counter ICNT is updated each time a diagnostic is printed. It is stored in the second location of common block CIMPL and is monitored to see if diagnostic print lines exceeds DLINEs. If so, IMPL is set to 3 the final iteration, so that no further diagnostics are printed. The last convention observed here concerns the use of the maximum power and product efficiency variables denoted PM1, EF1, PM2, EF2. These variables are used to communicate information to the logic components PD and PA. The efficiency variable EFF is defined as the ratio of output power to input power except when P1 = 0. In this case the old EFF value is used, but in any case EFF = 0 must be avoided since this would communicate a zero efficiency to a logic device which would then generate an infinite request. It is seen that EF2 and PM2 represent the joint efficiency and maximum power at the output port as a consequence of the rated generator power and computed input/output efficiency.

Storage devices have in addition to the above, certain conventions to communicate with the logic components. An input parameter RE1 for port 1 request is used to initiate power discharge from storage. An output variable RE2 for port 2 request is used to communicate a maximum charge rate request and is usually computed by

$$RE2 = \text{MIN} (MP1, RAP) / EF1$$

where MP1 and EF1 are the input maximum power and input product efficiency,

and RAP denotes the maximum storage charging rate. A priority interrupt INT should also be defined so that $INT = 1$. when storage is empty or at a minimum, $INT = 0$. if no interrupt is required, and $INT = -1$. at full storage capacity. The state of storage is normally a state variable so that the code computes the state derivative at each time point and lets the integrator update the state at each time point.

6.2 FILOAD PROGRAM

In addition to placing the subroutine representing the new standard component in the component library, descriptions of the inputs, outputs, and tables required by the new component must be added to the permanent file, M18. These lists are used by the Model Generation program to direct the connection of component inputs and outputs. The program FILOAD is provided to perform any of the following tasks:

1. Add new input, output, or table name lists.
2. Replace existing input, output or table name lists.
3. Remove all name lists for specified components.
4. Dump contents of M18 file onto Tape 9 in input format.

6.2.1 FILOAD Program Commands

The FILOAD program will recognize the following commands.

LIST STANDARD COMPONENTS

The LIST COMPONENTS command causes the program to print the input, output, and table lists for all components modified or added to the M18 file. If this command is not given the program will merely give a message stating the name of the new components being added to the file.

PURGE

The PURGE command can be used to remove a component from the M18 file. The PURGE command is followed by the names of the components to be purged. The command and the component names must be separated by one of the standard delimiters; i.e. [] three or more blanks, [,] comma, [=] equal sign, [()] left or right parentheses.

Example 6.3: PURGE = CM, TB, OB

This command would remove all lists for the CM, TB, and OB components from the name list file.

SYMBOL

The SYMBOL command may be used to designate the type of symbol that is to appear for each standard component in the lineprinter drawn model schematic diagram. The SYMBOL command is followed by the names of the components each followed by a symbol number. The symbol numbers and their associated symbols are shown in Figure 6.2-1. The SYMBOL command, component names, and symbol numbers are separated by standard delimiters.

Example: SYMBOL, CO = 100, SH = 200, TU = 300, OC = 400

If a symbol number is not specified for a component the default symbol of a square box will be used.

DUMP FILE

The DUMP FILE command causes the FILOAD program to dump the contents of the M18 file onto DUMPF9, in the input format of the FILOAD program. Thus for each standard component, a list of inputs, outputs, and tables will be produced. This data will be preceded by the command NEW FILE described below. This file may be edited to modify the input, output or tables description of any existing standard component or to derive a new standard component

STANDARD SCHEMATIC SYMBOLS

4	5	6	7	8
14	<pre> ** * * * * * * * * * CO * * 15 * * * * * * * ** ** SYMBOL = 100 </pre>	16	<pre> 00000000 0 0 0 OC 0 0 17 0 0 0 00000000 </pre>	18
24	25	26	27	28
34	<pre> ***** * * * SH * * 35 * * * ***** SYMBOL = 200 </pre>	36	<pre> ***** * * * ME * * 37 * * * ***** SYMBOL = ANY OTHER NUMBER </pre>	38
44	45	46	47	48
54	<pre> ** * * * * * * * * TU * * 55 * * * * * * ** </pre>	56	57	58
64	65	66	67	68
		SYMBOL = 300		

FIGURE 6.2-1 LIST OF STANDARD COMPONENT SYMBOLS

description from an existing one. The results of such an editing would then serve as input data to a subsequent run of the FILOAD program. Unless it is intended to purge the M18 file and start anew, the NEW FILE command at the beginning of DUMPF9 should be removed before the subsequent run of the FILOAD program.

NEW FILE

The NEW FILE command instructs the FILOAD program to construct a new M18 file. This command must occur as the first card in a set of data describing a completely new M18 file. Any previous components that may have existed on the M18 file are purged by this command. It is therefore only used when installing a complete new M18 file.

FILE NAME

This command is used to load the file name to be associated with the M18 file. The current M18 file name is WINDENERGY. This command is used as:

FILE NAME = WINDENERGY

6.2.2 Input Name Lists

Input name lists are identified by the letters INPT following the component name. Thus, the input name list for a component DC would be introduced with the phrase, DCINPT. This must be followed by a phrase that contains the number of names in the input name list.

The input names are contained on the following data cards, 8 names per card. The names must be left adjusted in fields, 10 characters wide. The names are placed in Columns 1 through 3 of each field. Column 9 of each field can be used to indicate a port number which can be attached to the name to distinguish it from other quantities of the same name that occur with the given

component. Thus, to indicate that temperature, T, is an input to port 1, the input name list would be:

Column:	1	2	3	4	5	6	7	8	9	10
Item:	T									1

This quantity would then be referred to as T1.

Example 6.4:

```
SWINPT = 3
IN.....1.IN.....2.CNT
```

(The dots are used here to indicate blank spaces and would not be included in an actual data card).

These two data cards would indicate that the component SW had 3 input quantity names. A quantity IN appears at port 1, and is to be referred to as IN1. A quantity IN appears at port 2, and is to be referred to as IN2. A third input quantity CNT has no port designation. Note that if a port number is to be attached to a quantity name, that name should contain no more than 2 characters.

The sequence of names in the input name list must match the sequence of input arguments in the component call sequence.

6.2.3 Output Name Lists

Output name lists are identified by the letters OUTP following the component name. Thus, the output name list for a component DC would be introduced with the phrase, DCOUTP. This must be followed by a phrase that contains the number of names in the output name list.

The output names are contained on the following data cards, 8 names per card. The names must be left adjusted in fields 10 characters wide. The names are placed in Columns 1 through 3 of each field. Column 9 of each field can be used to introduce a port number which can be attached to the name to distinguish it from other quantities of the same name that occur with the given component. If the output quantity is a state variable, this must be indicated by placing S in Column 10 of the field. Thus, if power P is a state variable output quantity at port 2, the output name list would be:

Column:	1	2	3	4	5	6	7	8	9	10
Item:	P								2	S

This quantity would then be referred to as P2.

Example 6.5:

```
TZOUTP = 3
X.....1SX.....2SOUT
```

(The dots are used here to indicate blank spaces, and would not be included on an actual data card).

These two data cards would indicate that the component TZ had 3 output quantity names. A quantity X appears at port 1. This is a state variable, and will be referred to as X1. A quantity X is also a state variable that appears at port 2. It will be referred to as X2. The quantity OUT is an output variable, not a state variable, and does not have a port number associated with it. Note, that if a port number is to be attached to a quantity name that name should contain no more than 2 characters. These two characters plus the port number will reach the maximum number of 3 characters in a quantity name.

The sequence of names in the output name list must match the sequence of output arguments in the component call sequence. However, whereas three argu-

ments are provided for each state in the subroutine call sequence, only one name is included in the output name list.

6.2.4 Table Name Lists

Table name lists are identified by the letters TABS, following the component name. Thus, the table name list for a component CM would be introduced with the phrase CMTABS. This must be followed by a phrase containing the number of names in the table name list. The table names are contained in the following cards, one table name per card. The name is located in the first 3 columns of the card. It must be accompanied by the maximum dimension that is to be provided for this table. This number must be given in columns 4 through 10 and should have a decimal point given. For single independent variable tables this number must be negative. For tables with two independent variables, this number must be positive.

Example:

```
CMTABS = 3
TAM      53.
TAB      43.
TCM     -27.
```

These four data cards would indicate that the component CM had 3 tables. The first two tables TAM and TAB have two independent variables each, as indicated by the positive dimension numbers. The table TCM has only one independent variable, as indicated by the negative dimension number. 53, 43, and 27 words of storage are to be provided for tables TAM, TAB, and TCM respectively. The maximum storage is related to the maximum number of primary, NX, and secondary, NZ, independent variables by:

```
MAX = 3 + NX+NZ+NX*NZ for tables with two independent variables
MAX = 3 + 2*NX for tables with one independent variable
```

7.0 LIBRARY COMPONENT DESCRIPTIONS

This section describes the mathematical algorithms and input/output structure of the SIMWEST library components. Each component writeup contains a brief textual description of the algorithms, a mathematical expression summarizing its function, a list of input and output variables, and a description of the calculation sequence and logic used in the model. A figure is provided which shows the nominal input and output connections, and the state variables of each component.

There are a number of features and conventions in the component descriptions which require some elaboration. These are briefly summarized below.

7a. INPUT/OUTPUT NAME LISTS

A potentially confusing factor is the way port numbers on input parameters and output variables are designated. On the model generation input cards the name of the physical quantity and the port number is separated by a comma. For example, the power variable with port designation 1 is denoted P,1. In defining input to the simulation program, this same variable would be denoted P1. To emphasize the distinction between the physical quantities and port numbers, they are listed separately in the name lists of the component writeups. For example, P 1 in the name list denotes the power variable (or parameter) with port designation 1 even though in other parts of the text it may simply be denoted P1.

Another convention in the name lists is that the alphabetic symbol 'O' is shown as Ø to distinguish this symbol from a zero. Elsewhere in the text symbols such as VØ may be referred to as V0.

7b. INPUT PARAMETER SPECIFICATION

All input parameters are associated with default values. Many of the parameters have default values denoted in the parameter description by the letter D. For example in the Battery component the default value for terminal resistance, RT, is $D = .001$ ohms. All input parameters for which a default value is not so specified has a default value of .99999. Default values are intended to enable users to put models together quickly by specifying a minimum of input data. Users need only specify detailed parameter values for those components of current interest. One must be careful using this approach since the operating characteristics and efficiency of a 10kw rated device may for example be quite different than for a 100kw device.

Any user specified input parameter can be driven by one or two dimension table lookups using the FU and FV components. This enables the user to build more detailed models using time or other output variables to drive the tables. For example, if one needs to specify cost of peak load generation to the utility component as a function of peak load request, then one adds FU as an input to UT and specifies load request as an input connection to FU. The desired function table is then input to FU.

It may be noted that not all of the components have maintenance or operating cost inputs. Thus, whenever these costs are important, one can aggregate such costs and input lumped costs to the model. For example, the maintenance cost of the hydro storage system may include maintenance costs for the pump and turbine.

7c. COMPONENT LOGIC

In constructing SIMWEST components, we have adopted several conventions to aid communication with the logic components. All physical components distributing power are given two input parameters EF and MP (port 1) and two output

variables EF and MP (port 2). The output EF is the product efficiency of all components in the distribution subsystem up to and including the given component, and MP is the maximum power deliverable at the output of the component. Each storage component has in addition a power request input denoted RE (port 1), a power request output denoted RE (port 2), and a priority interrupt flag denoted INT.

Figure 7.0 shows the logic and physical variable connections for power flow in and out of a hydro reservoir. Power flows from the power divider to the pump at a rate not to exceed the request RE from HS. The HS request is computed by dividing the input maximum power by the input (or pump) efficiency EF. Hence, the maximum power flowing to HS cannot exceed $RE * EF = MP$. Similarly, the input request to HS is computed by the PA component so as not to exceed the maximum input power MP divided by EF (turbine efficiency). Hence, the power that flows to PA cannot exceed $RE * EF = \text{input maximum power}$.

When the hydro reservoir is empty, the interrupt flag is turned on and the priority sequence is changed to 1 so that the reservoir is given access to power flowing into the divider.

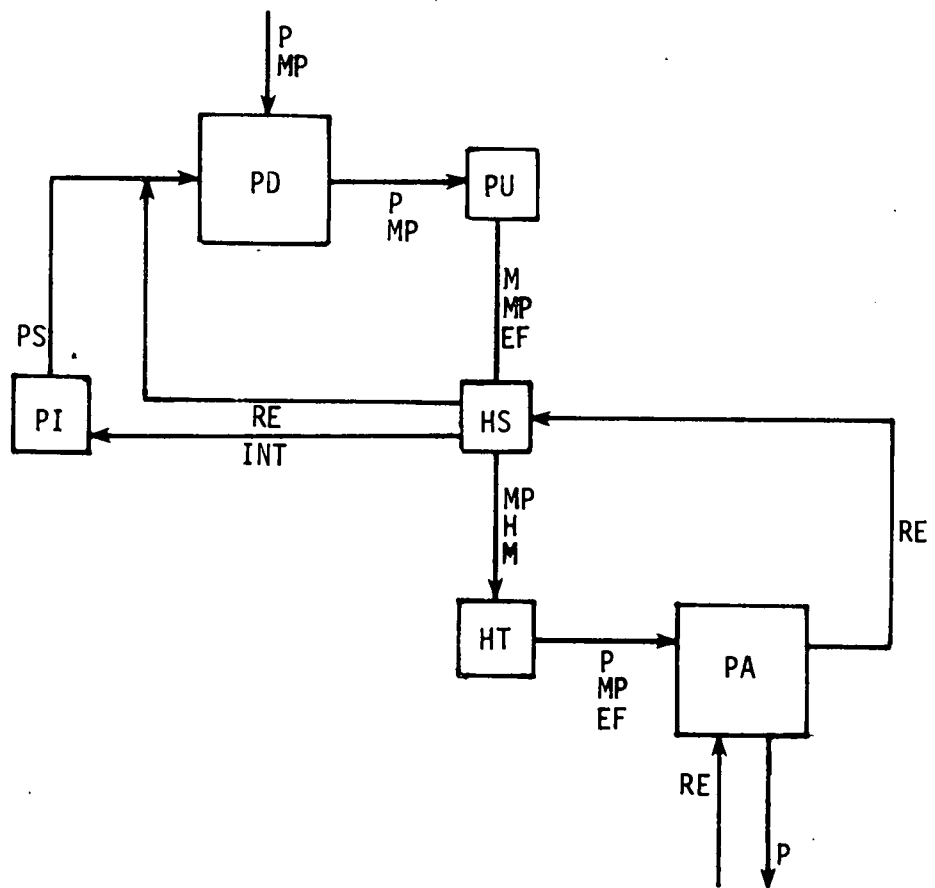
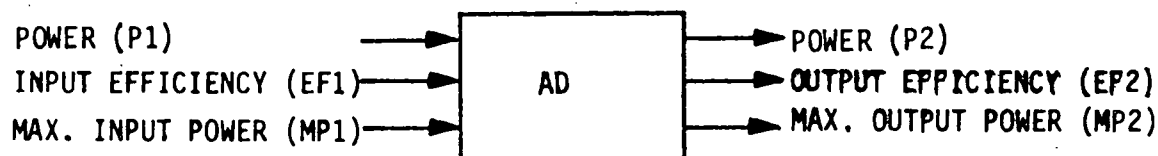


FIGURE 7.0 SAMPLE CONNECTIONS FOR LOGIC COMPONENTS

7.1 ADMITTANCE



The admittance model can be used to model transmission lines, transformers, capacitors or impedance power flows. A primary assumption is that the reactive parameters dominate the real parameters so that power transfer angle is solely based on reactive values, and power losses are based on the real admittance parameters and on power angle. The equation for power loss is based upon the following model:

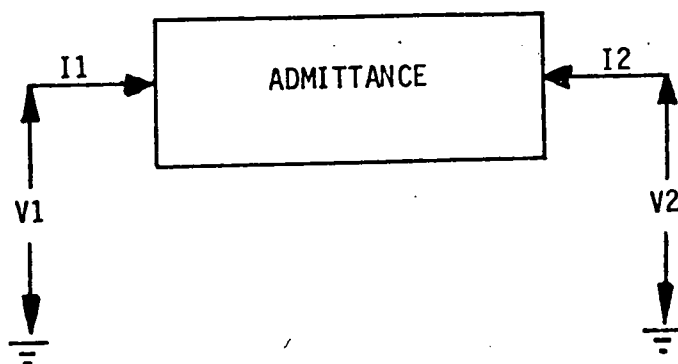


FIGURE 7.1 ADMITTANCE NETWORK MODEL

$$\begin{pmatrix} I_1 \\ I_2 \end{pmatrix} = \begin{pmatrix} G_1 + jB_1 & G_M + jB_M \\ G_M + jB_M & G_2 + jB_2 \end{pmatrix} \begin{pmatrix} V_1 \\ V_2 \end{pmatrix}$$

Where the reactive parameters B_1 and B_2 do not enter into the power loss calculations.

Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
G1,GM,G2	Real admittance parameters *	mho
BM	Reactive admittance parameter * (≠0)	mho
V0	Rated voltage magnitude	volts
P 1	Input power	kw
EF 1	Input product efficiency	-
MP 1	Maximum input power	kw
CC	Capital cost/year	\$

Outputs

<u>Variable/Port</u>			
P 2	Output power		kw
PL	Power loss		kw
PA	Power angle		deg
EF 2	Output product efficiency		-
MP 2	Maximum output power		kw

* - See next page for User Input to Model Transmission lines, Transformers and Impedances.

Transmission Line Input:

$$G1 = G2 = g * \ell$$

$$GM = -g * \ell$$

$$BM = 1 / (\omega * L * \ell)$$

where g = line conductance per unit length

ℓ = length of line

ω = frequency in radians/sec = 120π

L = line inductance per unit length

Transformer Input:

$$G1 = G2 = GM = 0$$

$$BM = 1 / X * h$$

where X = reactance in ohms

h = turns ratio

(No power loss modeled with a transformer)

Impedance Input: (Includes capacitors and inductors)

$$G1 = G2 = -GM = R / (R^2 + X^2)$$

$$BM = X / (R^2 + X^2)$$

where R = resistance in ohms

X = reactance in ohms

$$= \begin{pmatrix} \omega L & \text{for an inductance } L \\ -\frac{1}{\omega C} & \text{for a capacitance } C \end{pmatrix}$$

Calculation Sequence

If $P_1 \leq 0$ $P_2 = P_L = P_A = 0$ and Return

1) Compute power angle

If $P_1 * 1000 > B_M * V_0^2$, $\cos \theta = 0$ and write DIAGNOSTIC

$$\theta = -\sin^{-1}(P_1 * 1000 / B_M * V_0^2)$$

$$P_A = \theta * 180 / \pi$$

$$\cos \theta = \sqrt{1 - (P_1 * 1000 / B_M * V_0^2)^2}$$

2) Compute power loss and output power

$$P_L = V_0^2 * (G_1 + G_2 + 2 * G_M * \cos \theta) / 1000$$

$$P_2 = P_1 - P_L$$

$$EFF = P_2 / P_1$$

If $P_2 > 0$ go to 3)

write DIAGNOSTIC

$$EFF = 1.$$

3) Efficiency and maximum output power

$$EF_2 = EF_1 * EFF$$

$$MP_2 = \min(MP_1, |B_M| * V_0^2 / 1000) * EFF$$

4) Compute costs

ENTRY POINT 000212

COMMON BLOCKS

EXTERNAL REFERENCES (BLOCK, NAME)

0007	NWDUS
0010	H102S
0011	ASIN
0012	SQPT
0013	NEPR3S

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

3001	000017	10L	0001	000060	100L	0000	000006	108F	0001	000076	200L	0001	000140	300L
3002	000027	308F	0001	000162	400L	0006	R 000000	CCI	0005	000000	DUM	0000	R 000005	EFF
3003	I 000001	1CNT	0003	I 000000	IMPL	0000	000054	INJPS	0000	R 000001	RR	0000	R 000003	RPC
0000	R 000002	RR2	0000	R 000004	THETA	0004	R 000000	TIME	0005	R 000007	THAX	0000	R 000000	THAX1

```

00100      1*      CAD
00101      2*      SUBROUTINE ADIP2,PL,PA,EF2,MP2,  61,GM,62,BM,VO,P1,EF1,MP1,CC)
00101      3*      C
00101      4*      C      PURPOSE      MODEL OF TRANSMISSION LINES,TRANSFORMERS,
00101      5*      C      CAPACITORS, OR IMPEDANCE POWER LOSS
00101      6*      C
00101      7*      C      METHOD      OUTPUT POWER AND POWER LOSS COMPUTED FROM
00101      8*      C      INPUT POWER
00101      9*      C
00101     10*      C      WRITTEN BY Y.K.CHAN      VERSION 1, JULY,1977
00101     11*      C
00101     12*      C      CALL SEQUENCE
00101     13*      C      OUTPUTS
00101     14*      C      P2  -OUTPUT POWER,KW
00101     15*      C      PL  -POWER LOSS,KW
00101     16*      C      PA  -POWER ANGLE,DEG
00101     17*      C      EF2 -OUTPUT PRODUCT EFFICIENCY
00101     18*      C      MP2 -MAXIMUM OUTPUT POWER,KW
00101     19*      C      INPUTS
00101     20*      C      G1,6M,62  -REAL ADMITTANCE PARAMETERS,MHO
00101     21*      C      PM  -REACTIVE ADMITTANCE PARAMETERS (-NE.O.),MHO

```

[illegible]

AD

00101	22*	C	VO -RATED VOLTAGE MAGNITUDE,VOLTS	000000
00101	23*	C	P1 -INPUT POWER,KW	000000
00101	24*	C	EF1 -INPUT PRODUCT EFFICIENCY	000000
00101	25*	C	MP1 -MAXIMUM INPUT POWER,KW	000000
00101	26*	C	CC -CAPITAL COST/YEAR,\$	000000
00101	27*	C		000000
00103	28*		COMMON /CIMPL/IMPL,ICNT/CTIME/TIME/CSIMUL/DUM(7),TMAX	000000
00103	29*	X	/COST/CCI	000000
00104	30*		REAL MP2,MP1	000000
00104	31*	C		000000
00105	32*		P2=0.	000000
00106	33*			000000
00106	34*		TMAX1=TMAX*.99999	000000
00107	35*		IF(P1.GT.C.)GO TO 10	000003
00111	36*		P2=0.	000006
00112	37*		PL=C.	000007
00113	38*		PA=C.	000010
00114	39*		MP2=MP1	000011
00115	40*		EF2=EF1	000013
00116	41*		GO TO 400	000015
00116	42*	C		000015
00116	43*	C	COMPUTE POWER ANGLE	000015
00116	44*	C		000015
00117	45*		10 RR=P1*1000./(BM*VO*VO)	000017
00120	46*		RR2=RR*RR	000025
00121	47*		IF(RR2.LE.1.)GO TO 100	000027
00123	48*		PA=-90.	000032
00124	49*		RFC=0.	000034
00125	50*		IF(IMPL.EQ.2)WRITE(6,108)P1,BM,VO	000035
00133	51*		108 FORMAT(1HC,13H INPUT POWER ,F12.3,33H TOO HIGH RELATIVE TO ADMITTA	000050
00133	52*		XNCE ,F12.3,19H AND RATED VOLTAGE ,F12.3)	000050
00134	53*		IF(IMPL.EQ.2)ICNT=ICNT+1	000050
00136	54*		GO TO 200	000056
00137	55*		100 THETA=-ASIN(RR)	000060
00140	56*		PA=THETA*180./3.14159	000063
00141	57*		RRC=SQRT(1.-RR2)	000066
00141	58*	C		000066
00141	59*	C	COMPUTE POWER LOSS AND OUTPUT POWER	000066
00141	60*	C		000066
00142	61*		200 PL=VO*VO*(G1+G2+2.*GM*RRC)/1000.	000076
00143	62*		P2=P1-PL	000110
00144	63*		EFF= P2/P1	000112
00145	64*		IF(P2.GE.0.)GO TO 300	000114
00147	65*		P2=0.	000117
00150	66*		EFF=1.	000120
00151	67*		IF(IMPL.NE.2)GO TO 300	000122
00153	68*		WRITE(6,308)PL,P1	000125
00157	69*		308 FORMAT(1HC,24H ADMITTANCE POWER LOSS ,F12.3,21H EXCEEDS INPUT POWE	000134
00157	70*		XR ,F12.3)	000134
00160	71*		ICNT=ICNT+1	000134
00160	72*	C		000134
00161	73*		300 EF2=EF1	000140
00162	74*		IF(P2.GT.0.)EF2=EF1*EFF	000141
00164	75*		MP2=AMIN1(MP1,ABS(BM)*VO*VO/1000.)*EFF	000147
00164	76*	C		000147
00165	77*		400 IF(IMPL.LE.1)RETURN	000162
00167	78*		IF(TIME.LT.TMAX1)RETURN	000170

AJ

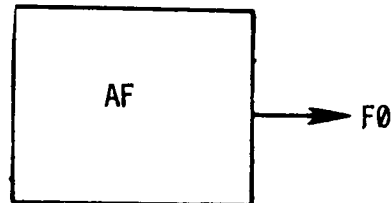
00171 79*
00171 80*
00172 81*
00173 82*

C

CCI=CCI+CC
RETURN
END

000177
000177
000202
000263

7.2 TEST FUNCTION GENERATOR



Inputs

Parameter/Port

Description

C0D	Specifies which analytic function is calculated. (See equations below for use of these inputs)
C1	
C2	
C3	
C4	
C5	

Outputs

Variable/Port

F0	Output variable
----	-----------------

Calculation Sequence

```

C0D = 1   F0 = C1 + C2*SIN(C3*T + C4)
          2   F0 = C1 + C2*COS(C3*T + C4)
          3   F0 = C1 + exp(-C5*T) * SIN(C3*T + C4)
          4   F0 = C1 + exp(-C5*T) * COS(C3*T + C4)
          5   F0 = C1 + C2*T
          6   F0 = C1 + C2*exp(-C3*T)
              where: T = TIME
  
```

SUBROUTINE AF ENTRY POINT 000143

STORAGE USED CODE(1) 000166; DATA(0) 000014; BLANK COMMON(2) 000600

COMMON BLOCKS

0003 CTIME 000001

EXTERNAL REFERENCES (BLOCK, NAME)

0004 NERR25
0005 SIN
0006 COS
0007 EXP
0010 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

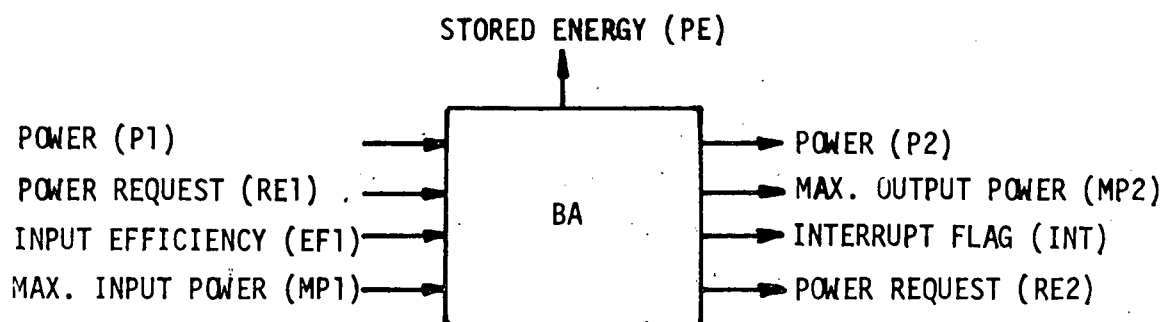
0001	000022	10L	0001	00013R	100L	0001	000035	20L	0001	000050	30L	0001	000073	40L
0001	000116	50L	0001	000123	60L	0000	000001	INJPS	0000	I	000000	NCODE	0003	R 000000 TIME

00100	1*	CAF												000000
00101	2*		SUBROUTINE AF(F0,COD,C1,C2,C3,C4,C5)											000000
00101	3*	C												000000
00101	4*	C	PURPOSE - TO SIMULATE ANALYTICAL FUNCTIONS											000000
00101	5*	C												000000
00101	6*	C												000000
00101	7*	C	METHOD - SEE CODING											000000
00101	8*	C												000000
00101	9*	C												000000
00101	10*	C	WRITTEN BY - ADAM LLOYD			LATEST REVISION		FEB 76						000000
00101	11*	C												000000
00101	12*	C												000000
00101	13*	C	LIMITATIONS - NONE											000000
00101	14*	C												000000
00101	15*	C												000000
00101	16*	C	INPUT/OUTPUT LIST											000000
00101	17*	C												000000
00101	18*	C	F0	OUTPUT VARIABLE		ANY	OUTPUT VAR							000000
00101	19*	C	COD	CODE IDENTIFYING ANALYTICAL FUNCTION	---		INPUT PARAM							000000
00101	20*	C		CODE= F0=										000000
00101	21*	C		1 C1+C2*SIN(C3*TIME+C4)										000000
00101	22*	C		2 C1+C2*COS(C3*TIME+C4)										000000
00101	23*	C		3 C1+C2*EXP(-C5*TIME)*SIN(C3*TIME+C4)										000000
00101	24*	C		4 C1+C2*EXP(-C5*TIME)*COS(C3*TIME+C4)										000000
00101	25*	C		5 C1+C2*TIME										000000
00101	26*	C		6 C1+C2*EXP(-C5*TIME)										000000

AF

00101	27*	C	C1	CONSTANT INPUTS FOR ABOVE EQNS	---	INPUT	PARAM	000000
00101	28*	C	C2	CONSTANT INPUTS FOR ABOVE EQNS	---	INPUT	PARAM	000000
00101	29*	C	C3	CONSTANT INPUTS FOR ABOVE EQNS	---	INPUT	PARAM	000000
00101	30*	C	C4	CONSTANT INPUTS FOR ABOVE EQNS	---	INPUT	PARAM	000000
00101	31*	C	C5	CONSTANT INPUTS FOR ABOVE EQNS	---	INPUT	PARAM	000000
00103	32*			COMMON/CTIME/TIME				000000
00104	33*			NCODE=000				000000
00105	34*			GO TO (10,20,30,40,50,60),NCODE				000006
00106	35*	10		F0=C1+C2*SIN(C3*TIME+C4)				000022
00107	36*			GO TO 100				000033
00110	37*	20		F0=C1+C2*COS(C3*TIME+C4)				000035
00111	38*			GO TO 100				000046
00112	39*	30		F0=C1+C2*EXP(-C5*TIME)*SIN(C3*TIME+C4)				000050
00113	40*			GO TO 100				000071
00114	41*	40		F0=C1+C2*EXP(-C5*TIME)*COS(C3*TIME+C4)				000073
00115	42*			GO TO 100				000114
00116	43*	50		F0=C1+C2*TIME				000116
00117	44*			GO TO 100				000121
00120	45*	60		F0=C1+C2*EXP(-C5*TIME)				000123
00121	46*	100		RETURN				000134
00122	47*			END				000165

7.3 BATTERY



The battery model is based on the circuit diagram shown below. Current flow is determined by the output power request minus input power. Battery leakage is proportional to stored energy. Priority interrupt logic is activated when a minimum or maximum capacity level is attained.

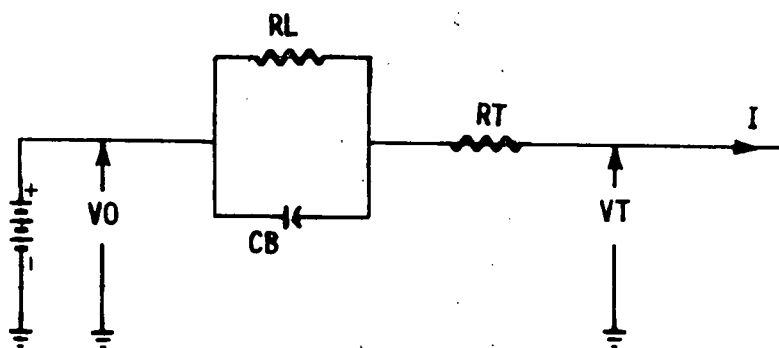


FIGURE 7.3 BATTERY CIRCUIT DIAGRAM

Basic Equations

The output power P2, stored energy PE, terminal current I, and capacitor voltage VC is computed using the following equations:

$$P2 = RE1$$

$$PE = (VC^2 + 2*V0*VC)*CB/7.2 \times 10^6$$

$$(P2 - P1) * 1000 = (V0 + VC)I - I^2 * RT$$

$$\dot{PE} = -(I + VC/RL)(VC + V0)/1000$$

Inputs

<u>Parameter/Port</u>		<u>Description</u>	<u>Units</u>
P	1	Input power	kw
V0		Internal voltage	volts
RT		Terminal resistance (D = 0.001)	ohms
CB ¹		Battery capacitance (D = 2.88×10^8)	farads
RL ¹		Leakage resistance (D = 0.05)	ohms
RAP		Rated input power	kw
EF	1	Input product efficiency	-
MP	1	Maximum input power	kw
E1		Maximum energy storage	kwh
RE	1	Power request	kw
EDE		Energy deadband for priority resequencing	kwh
DT		Down time for priority resequencing	h
CC		Capital cost/year	\$
CM		Maintenance cost/year	\$

Outputs

<u>Variable/Port</u>			
P	2	Output power (=RE1)	kw
PE		Stored energy (state of charge)	kwh
I		Terminal current (+ = out, - = in)	amps
VC		Capacitor voltage	volts
VT		Terminal voltage	volts
PL		Power loss	kw
T0		Time when battery was discharged	h
MP	2	Maximum output power	kw
INT		Priority interrupt flag	-
RE	2	Maximum charging rate request	kw

D - Default values supplied

1 - Battery leakage time constant in hours = $CB * RL / 3600$

Statistics

<u>Variable/Port</u>	<u>Description</u>	<u>Units</u>
MPE	Maximum stored energy	kwh
SPC	Sum of charging energy	kwh
SPD	Sum of discharging energy	kwh

Calculation Sequence

1) Compute VC

$$VC = \sqrt{7.2 \times 10^6 * PE / CB + V0^2} - V0$$

2) Solve for terminal current I

If $(P2 - P1) * 1000 \geq (VC + V0)^2 / 4 * RT$, GO TO 2'

$$I = \frac{(VC + V0) - \sqrt{(VC + V0)^2 - 4 * RT * (P2 - P1) * 1000}}{2 * RT}$$

Go to 3)

2)' $I = (VC + V0) / 2 * RT$ and write DIAGNOSTIC

3) Compute VT

$$VT = VC + V0 - I * RT$$

4) Potential energy balance and power loss

$$PE = -(I + VC / RL) (VC + V0) / 1000.$$

$$PL = (I^2 * RT + VC^2 / RL) / 1000.$$

5) Maximum charging and discharging rates

$$RE2 = \min(MP1, RAP, (E1 - PE) / TINC) / EF1$$

$$MP2 = \min(RAP, (VC + V0)^2 / (4000 * RT), (PE - EDE) / TINC)$$

where TINC = integration step size

Calculation Sequence Cont.

6) Priority interrupt logic

If $PE \leq EDE$ and $T0 = 10^6$, $T0 = TIME$

If $PE \leq EDE$ and $TIME - T0 \geq DT$, $INT = 1$ and go to 7)

$T0 = 10^6$

If $PE > 2 \times EDE$ and $INT = 1$, $INT = 0$

If $PE \geq E1$, $INT = -1$

If $PE < E1 - EDE$ and $INT = -1$, $INT = 0$

7) Compute Statistics and Costs

ENTRY POINT 000372

COMMON BLOCKS

EXTERNAL REFERENCES (BLOCK, NAME)

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

00100          1*      CRA
00101          2*      SUBROUTINE BA(P2,PE,PED,IPE,I,VC,VT,PL,TO,MP2,INT,RE2,MPE,SPC,SPD,
00101          3*      1      P1,VO,RT,CB,RL,RAP,CF1,MP1,E1,RE1,EDE,DT,CC,CM)
00101          4*      C
00101          5*      C      PURPOSE      BATTERY MODEL
00101          6*      C
00101          7*      C      METHOD      COMPUTE STORED ENERGY AND POWER OUTPUT AS
00101          8*      C      FUNCTIONS OF POWER INPUT AND POWER REQUEST.
00101          9*      C      A RESISTOR/CAPACITOR NETWORK IS USED TO
00101         10*      C      MODEL BATTERY STORAGE.
00101         11*      C
00101         12*      C      WRITTEN BY Y.K.CHAN      VERSION 1, JUNE 3,1977
00101         13*      C
00101         14*      C      CALL SEQUENCE
00101         15*      C      OUTPUTS
00101         16*      C      P2      -OUTPUT POWER, KW
00101         17*      C      PE      -STORED ENERGY (STATE),KWH
00101         18*      C      PED     -STORED ENERGY DERIVATIVE
00101         19*      C      IPE    -INTEGRATOR CONTROL
00101         20*      C      I      -TERMINAL CURRENT (+=OUT,-=IN),AMPS

```

[illegible]**BA**


```

00101 21* C VC -CAPACITOR VOLTAGE, VOLTS 000000
00101 22* C VT -TERMINAL VOLTAGE, VOLTS 000000
00101 23* C PL -POWER LOSS, KW 000000
00101 24* C TO TIME WHEN BATTERY WAS DISCHARGED, HR 000000
00101 25* C MP2 -MAXIMUM OUTPUT POWER, KW 000000
00101 26* C INT -PRIORITY INTERRUPT FLAG 000000
00101 27* C RE2 -MAXIMUM CHARGING RATE REQUEST, KW 000000
00101 28* C STATISTICS 000000
00101 29* C SPC -SUM OF CHARGING ENERGY, KWH 000000
00101 30* C MPE -MAXIMUM STORED ENERGY, KWH 000000
00101 31* C SPD -SUM OF DISCHARGING ENERGY, KWH 000000
00101 32* C INPUTS 000000
00101 33* C P1 -INPUT POWER, KW 000000
00101 34* C V0 -INTERNAL VOLTAGE, VOLTS 000000
00101 35* C PT -TERMINAL RESISTANCE, OHMS 000000
00101 36* C CB -BATTERY CAPACITANCE, FARADS 000000
00101 37* C RL -LEAKAGE RESISTANCE, OHMS 000000
00101 38* C RAP -RATED INPUT POWER, KW 000000
00101 39* C EF1 -INPUT PRODUCT EFFICIENCY 000000
00101 40* C MP1 -MAXIMUM INPUT POWER, KW 000000
00101 41* C E1 -MAXIMUM ENERGY STORAGE, KWH 000000
00101 42* C RE1 -POWER REQUEST, KW 000000
00101 43* C EDE -ENERGY DEADPAND FOR PRIORITY RESEQUENCING, KWH 000000
00101 44* C DT -DOWNTIME FOR PRIORITY RESEQUENCING, HR 000000
00101 45* C CC -CAPITAL COST/YEAR, $ 000000
00101 46* C CM -MAINTENANCE COST/YEAR, $ 000000
00101 47* C
00103 48* COMMON /CIMPL/IMPL,ICNT/CTIME/TIME/CSIMUL/DUM(7),TMAX/COST/CCI,CHI 000000
00104 49* REAL I,MP2,MPE,MP1,INT 000000
00105 50* DOUBLE PRECISION AA,B,B2 000000
00106 51* TJNC1=DUM(7)*.5 000000
00106 52* C 000000
00107 53* IF(IMPL.GT.0) GO TO 100 000002
00111 54* IF(RT.EQ..99999)RT=.001 000005
00113 55* IF(CB.EQ..99999)CB=2.88E8 000012
00115 56* IF(PL.EQ..99999)RL=.05 000017
00117 57* TO=1000000. 000024
00120 58* INT=0 000026
00121 59* TMAX1=TMAX*.99999 000027
00122 60* 000032
00122 61* MPE=0. 000032
00123 62* SPC=0. 000033
00124 63* SPD=0. 000034
00124 64* C 000034
00124 65* C CAPACITOR VOLTAGE 000034
00124 66* C 000034
00125 67* 100 VC=SQRT((7.2E6)*PE/CB + V0**2) -V0 000034
00125 68* C 000036
00125 69* C TERMINAL CURRENT. 000036
00125 70* C 000036
00126 71* P2=RE1 000051
00127 72* AA=(P2-P1)*4000.*RT 000053
00130 73* B=VC+V0 000062
00131 74* B2=B*B 000066
001 75* IF(AA.GT.B2) GO TO 200 000070
001 76* I= B-DSQRT(B2-AA) 000073
001 77* I=I/(2.*RT) 000103

```

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00136 78*      60 TO 300
00136 79*      C
00137 80*      200 I=B/(2.*RT)
00140 81*      IF (IMPL.EQ.2)WRITE(6,208)P2
00144 82*      208 FORMAT(1H0,15H POWER REQUEST ,F12.3,50H EXCEEDS BATTERY CAPABILITY
00144 83*      1. CHECK VC,V0, AND RT. )
00145 84*      IF (IMPL.EQ.2)ICNT=ICNT+1
00145 85*      C
00145 86*      C      TERMINAL VOLTAGE
00145 87*      C
00147 88*      300 VT=VC+V0-I*RT
00147 89*      C
00147 90*      C      POTENTIAL ENERGY BALANCE AND ENERGY LOSS
00147 91*      C
00150 92*      IF (IPE.NE.0)PED=(-I-VC/RL)*(VC+V0)/1000.
00152 93*      PL=(I+I*RT+VC+VC/RL)/1000.
00152 94*      C
00152 95*      C      MAXIMUM CHARGING AND DISCHARGING RATES
00152 96*      C
00153 97*      AP1=AMAX1(0.,(E1-PE)/DUM(7))
00154 98*      RE2=AMIN1(MP1,RAP,AP1)
00155 99*      RE2=RE2/EF1
00156 100*      AP2=AMAX1(0.,(PE-EDE)/DUM(7))
00157 101*      MP2=AMIN1(RAP,82/(4000.*RT),AP2)
00157 102*      C
00157 103*      C      PRIORITY INTERRUPT
00157 104*      C
00160 105*      C=E1-EDE
00161 106*      ED2=EDE+EDE
00162 107*      IF (PE.GT.ED2)GO TO 401
00164 108*      IF (TO.GT.999999.)TO=TIME
00166 109*      WAIT=TIME-TO
00167 110*      IF (WAIT.GT.DT)INT=1
00171 111*      60 TO 400
00172 112*      401 TO=1000000
00173 113*      IF (PE.LE.ED2)GO TO 400
00175 114*      IF (PE.GT.E1)GO TO 403
00177 115*      IF (PE.GT.C)GO TO 400
00201 116*      INT=0
00202 117*      60 TO 400
00203 118*      403 INT=-1
00204 119*      400 CONTINUE
00204 120*      C
00205 121*      IF (IMPL.LE.1)RETURN
00205 122*      C
00205 123*      C      STATISTICS
00205 124*      C
00207 125*      MPE=AMAX1(MPE,PE)
00210 126*      SPC=SPC+TINC1*P1
00211 127*      SPD=SPD+TINC1*P2
00211 128*      C
00212 129*      IF (TIME.LT.TMAX1)RETURN
00214 130*      CCI=CCI+CC
00215 131*      CMI=CMI+CM
00215 132*      C
00216 133*      RETURN
00217 134*      END

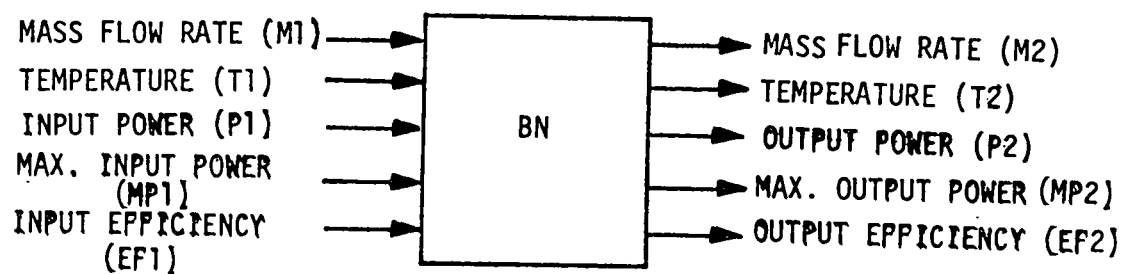
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7.4 BURNER



The burner model computes the amount of fuel required to be burned in the inlet airstream to raise the air temperature from the given inlet temperature to the specified outlet temperature. The fuel mass flow rate when integrated over time allows calculation of the cost of burner fuel.

Basic Equation

The mass of fuel consumed, F , is computed from the equation:

$$\dot{F} = \frac{M1 * CP * (T2 - T1)}{NU * HF}$$

Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
M 1	Inlet air mass flow rate	lb/h
CP	Air heat capacity ($D = 72 \times 10^{-6}$)	kwh/lb-°F
T 1	Inlet air temperature	°F
T 3	Outlet air temperature (specified)	°F
NU	Combustor efficiency ($D = 0.98$)	-
HF	Fuel heating value ($D = 5.56$)	kwh/lb
CF	Specific fuel cost ($D = 0.094$)	\$/lb
FDM	Maximum allowable fuel mass flow rate ($D=17800$)	lb/h
CB	Burner cost coefficient ($D = 1.683$)	\$/lb/h
LE	Burner life expectancy	years
MDM	Maximum allowable air mass flow rate ($D=27000$)	lb/h
EF 1	Input product efficiency	-
MP 1	Maximum input power	kw
P 1	Input power	kw

Outputs

Variable/Port

F	Fuel mass consumed (state)	lb
EF 2	Output product efficiency	-
MP 2	Maximum output power	kw
T 2	Outlet air temperature	°F
FD	Fuel mass flow rate	lb/h
CC0	Burner capital cost/year	\$
C0	Fuel cost	\$
M 2	Outlet mass flow rate (= M1)	lb/h
P 2	Output power	kw

Statistics

FDU	Maximum fuel mass flow rate	lb/h
-----	-----------------------------	------

D - Default values supplied

The calculation sequence and default values are based on a burner sized using first principles to maintain the outlet temperature at 600°F assuming an inlet temperature of 120°F and a mass flowrate of 2.7×10^4 lb/h. These conditions represent the extreme conditions expected and should satisfy all burner requirements. No. 6 fuel oil is assumed to be the fuel type. Cost and heating values were obtained from References 1 and 2. Cost estimates for the burner were estimated from the results of Reference 1.

Calculation Sequence

1) Capital Cost

$$CC0 = CB * MDM / LE$$

2) Maximum air mass flow rate allowed

If $M_1 = 0$ set $EFF = 1$, $MP2 = MP1$ and go to 3)

$$M_{1M} = \min \left\{ \frac{NU * HF * FDM}{CP * (T_3 - T_1)}, MDM \right\}$$

If $T_1 > T_3$, $M_{1M} = MDM$

3) Efficiency and maximum discharge power

$$EFF = 1 + M_1 * CP * (T_2 - T_1) / P_1 \quad (\text{if } P_1 > 0)$$

$$EF2 = EF1 * EFF$$

$$MP2 = \min \{ MP1 * EFF, P_1 * M_{1M} / M_1 \} \quad (\text{if } M_1 > 0)$$

$$P2 = P1 * EFF$$

-
1. "Preliminary Feasibility Evaluation of Compressed Air Storage Power Systems," United Technologies AER 74-00242, December 1976.
 2. Steam, Its Generation and Use, Babcock and Wilcox, New York, NY, 1972.

Calculation Sequence Cont.

4) Fuel mass flow rate

$$F = \frac{M1 * CP * (T2 - T1)}{NU * HF}$$

$$T2 = \text{MAX}(T1, T3)$$

If $M1 > M1M$ write DIAGNOSTIC

5) Compute Statistics and Costs

$$C0 = CF * F$$

ENTRY POINT 000270

COMMON BLOCKS

```
0003      CIMPL      000002
0004      CTIME      000001
0005      CSIMUL      000010
0006      COST        000003
```

0007	NW00S
0010	NI02S
0011	NE03S

```

0001 000056 100L      0001 000237 1000L      0000 000003 1010F      0001 000121 200L      0001 000107 300L
0006 R 000030 CCI      0006 000031 CMI      0006 R 000002 COP      0005 000000 DUM      0000 R 000002 EFF
0003 I 000001 ICNT      0003 I 000000 IMPL      0000 000034 INJPS      0000 R 000000 MIM      0004 R 000000 TIME
0005 R 000007 THAX      0000 R 000001 THAX1

```

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00100      1*      CBN
00101      2*      SUBROUTINE RN(F,DF,IF,EF2,MP2,T3,FD,CC,CO,M2,P2,F0U,M1,CP,T1,T2
00101      3*      1      ,NU,HF,CF,F0M,CB,LE,MDM,EF1,MP1,P1)
00101      4*      C
00101      5*      C PURPOSE      COMPUTE FUEL REQUIRED TO RAISE THE AIRSTREAM
00101      6*      C
00101      7*      C TEMPERATURE A GIVEN INCREMENT.
00101      8*      C
00101      9*      C METHOD      INTEGRATE THE FUEL MASS FLOW RATE OVER TIME
00101     10*      C
00101     11*      C WRITTEN BY F.O. MAHONY      VERSION 1, MARCH 22 1977
00101     12*      C
00101     13*      C CALL SEQUENCE
00101     14*      C
00101     15*      C      OUTPUTS
00101     16*      C      F - FUEL MASS CONSUMED SINCE TIME=0 (STATE), LB
00101     17*      C      DF - FUEL MASS DERIVATIVE
00101     18*      C      IF - STATUS INDICATOR
00101     19*      C      EF2 - OUTPUT PRODUCT EFFICIENCY
00101     20*      C      MP2 - MAXIMUM OUTPUT POWER, KW
00101     21*      C      T3 - OUTLET AIR TEMPERATURE, DEG F
00101     22*      C      FD - FUEL MASS FLOW RATE, LB/HR
00101     23*      C      CC - BURNER CAPITAL COST/YEAR, $

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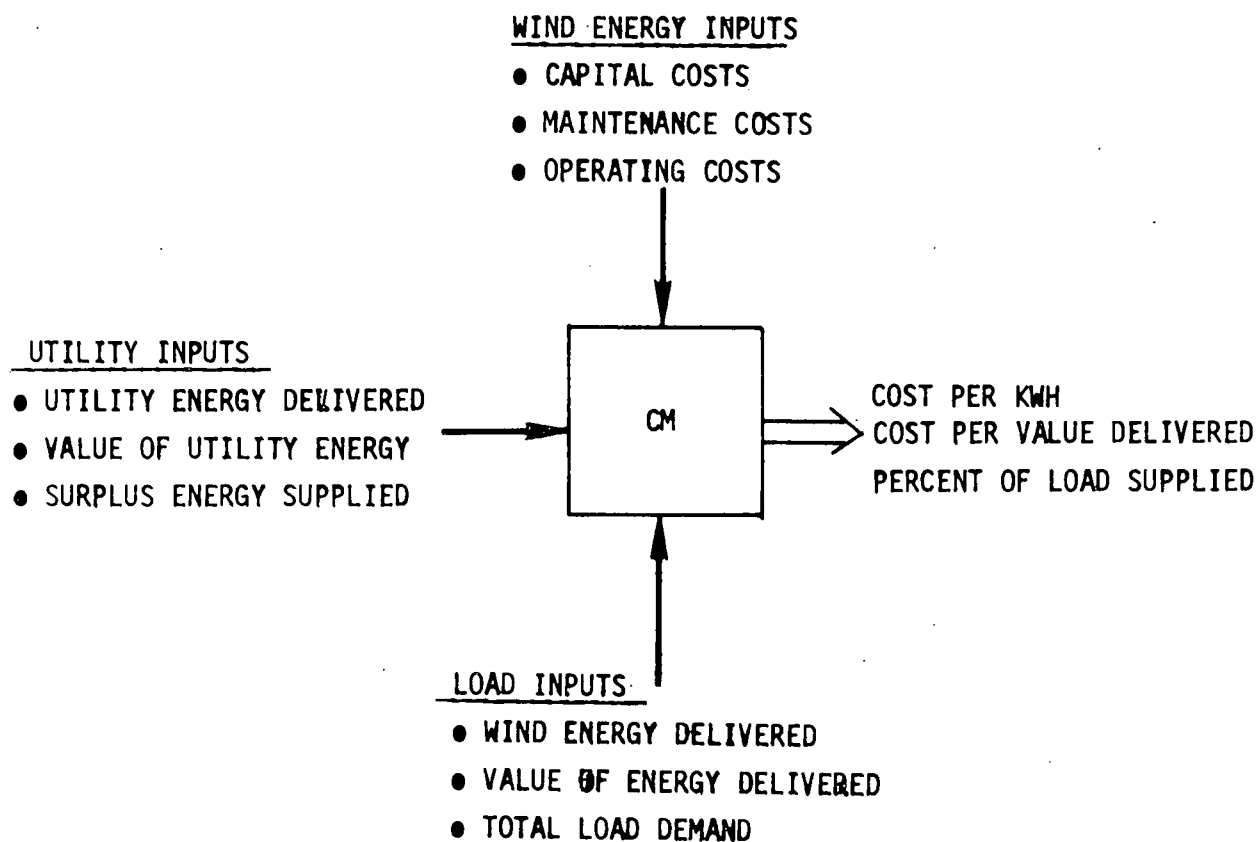
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50C000
6CLCG0
U00000
OC09C0
C0C0C0
C0C000





00150	81*		IF(M1.GT.0.) MP2=AMIN1(MP1*EFF,P1*M1M/M1)	000125
00152	82*		P2=P1*EFF	000142
00152	83*	C		000142
00152	84*	C	FUEL FLOW RATE	000142
00152	85*	C		000142
00153	86*		IF(IF.NE.0) DF= M1*CP*(T2-T1)/NU/HF	000145
00155	87*		IF(T1.GT.T2) DF=0.0	000157
00157	88*		FD=DF	000164
00157	89*	C		000164
00157	90*	C	COSTS	000164
00160	91*		CO = CF*F	000166
00161	92*		T3= AMAX1(T1,T2)	000171
00162	93*		M2=M1	000177
00162	94*	C		000177
00162	95*	C	STATISTICS	000177
00163	96*		IF(IMPL.LE.1) RETURN	000201
00163	97*	C		000201
00165	98*		FDU = AMAX1(FD,FDU)	000210
00165	99*	C		000210
00166	100*		IF(TIME.LT.TMAX1) RETURN	000216
00170	101*		CCI= CCI + CC	000225
00171	102*		COP= COP + CO	000230
00172	103*		RETURN	000233
00172	104*	C		000233
00173	105*		1000 IF(IMPL.EQ.2)WRITE(6,1010) M1,M1M	000237
00200	106*		1010 FORMAT(1H0,20HBN INLET AIR MASS FLOW RATE ,F12.3,	000250
00200	107*		1 36H GREATER THAN MAXIMUM ALLOWABLE ,F12.3)	000250
00201	108*		IF(IMPL.EQ.2)ICNT=ICNT+1	000250
00203	109*		GO TO 300	000256
00204	110*		END	000410

7.5 COST MONITOR¹



This component sums the capital, operating and maintenance costs of all system components. The total yearly cost TC is then computed using a fixed charge rate factor which represents depreciation, cost of money, insurance and taxes.

¹ This component must be placed last in the model generation input file, i.e., just prior to the END OF MODEL command.

The total wind energy delivered to the loads plus surplus energy is then summed and yearly energy delivered TED computed. Cost of operation in mills is then given by

$$\text{Wind system cost/kwh} = \text{TC} * 1000. / \text{TED}$$

Similarly, the value of energy delivered to the loads is summed minus the utility energy value and including the value of surplus energy, and factored to give yearly energy value delivered VED. Energy value in mills is given by

$$\text{Load value/kwh} = \text{VED} * 1000. / \text{TED}.$$

Cost per value delivered is the ratio of the above two equations.

In addition to the above cost calculations, percent of total load supplied by wind storage PCW, percent of load supplied by utilities PCU and, percent of wind energy surplused to the utilities PCS is computed. The total cost in mills to meet the load is then given by

$$\text{Load cost/kwh} = (\text{wind system cost/kwh} * \text{PCW} + \text{utility cost/kwh} * \text{PCU}) / 100.,$$

where

$$\text{Utility cost/kwh} = \text{value of utility energy} * 1000. / \text{utility energy delivered}.$$

Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
CR	Capital charge rate	%/year
LE	System life expectancy	years

Common Block Inputs

CC	Total yearly capital costs	\$
CM	Total yearly maintenance costs	\$
CO	Operating and fuel costs over TMAX	\$
TMAX	Simulation time interval	hr
VDE	Value of energy delivered (including surplus)	\$
TDE	Wind energy delivered (including surplus)	kwh
TLD	Total load demand	kwh
UTV	Value of utility energy	\$
UTD	Utility energy delivered	kwh
SPD	Surplus wind energy supplied	kwh

Outputs ¹

Total yearly costs (TC)	\$
Yearly energy delivered (TED)	kwh
Cost of energy per kwh	mills
Yearly value delivered (VED)	\$
Cost per value delivered	-
Percent of load supplied by	
Wind Storage (PCW)	-
Utility (PCU)	-
Surplus energy load factor (PCS)	-
Total load cost per kwh	mills

¹ Printout only occurs when simulation is completed. Thus no output variable symbol is required.

SUBROUTINE CM ENTRY POINT 000213

STORAGE USED CODE(1) 000226; DATA(0) 000330; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 COST 000011
0004 CIMPL 000001
0005 CTIME 000001
0006 CSIMUL 000010

EXTERNAL REFERENCES (BLOCK, NAME)

0007 NWDUS
0010 NI024
0011 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000020 100L	0000 000016 200F	0000 000034 300F	0000 000105 400F	0000 000210 500F
0003 R 000000 CC	0000 R 000003 CCY	0003 R 000001 CMA	0003 R 000002 CO	0000 R 000002 COY
0000 R 000015 CPKWH	0000 R 000011 CPV	0006 000000 DUM	0000 R 000005 EDE	0004 I 000000 IMPL
0000 000013 INJPS	0000 I 000006 IVDE	0000 I 000001 LLE	0000 R 000012 PCD	0000 R 000014 PCS
0000 R 000013 PCU	0003 R 000010 SPD	0003 R 000004 TDE	0005 R 000000 TIME	0003 R 000005 TLD
0006 R 000007 TMAX	0000 R 000000 TMAX1	0000 R 000004 TOY	0000 R 000007 TOYN	0003 R 000007 UTD
0003 R 000006 UTV	0003 R 000003 VDE	0000 R 000010 VDEN		

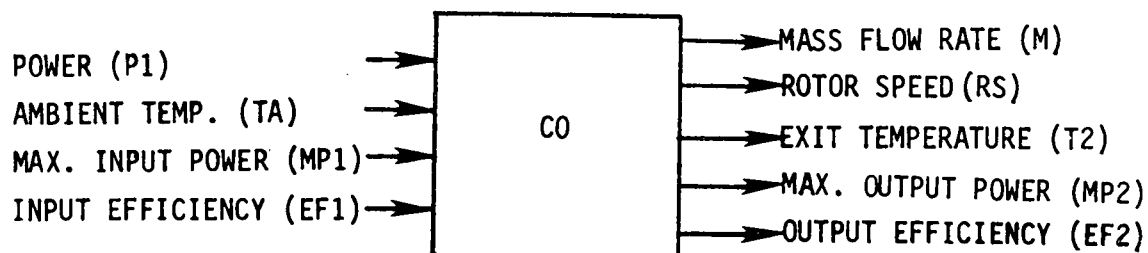
00100	1*	COST		000000
00101	2*	SUBROUTINE CM(DUMM,FCR,LE)		000000
00101	3*	C		000000
00101	4*	C	PURPOSE SUMMARIZE WIND ENERGY STORAGE COSTS AND LEVELIZED	000000
00101	5*	C	ENERGY COSTS PER KWH.	000000
00101	6*	C		000000
00101	7*	C	WRITTEN BY A.W. WARREN	000000
00101	8*	C	VERSION 1, MAY 1977	000000
00101	9*	C	INPUT PARAMETERS	000000
00101	10*	C		000000
00101	11*	C	FCR - FIXED CHARGE RATE FACTOR INCLUDING DEPRECIATION,	000000
00101	12*	C	MONEY COST, INSURANCE, AND TAXES, PER YEAR	000000
00101	13*	C	LE - SYSTEM LIFE EXPECTANCY, YEARS	000000
00101	14*	C	TMAX - SIMULATION TIME, HR	000000
00101	15*	C	CC - TOTAL YEARLY CAPITAL COSTS, \$	000000
00101	16*	C	CM - TOTAL YEARLY MAINTENANCE COSTS, \$	000000
00101	17*	C	CO - TOTAL OPERATING AND FUEL COSTS OVER TMAX, \$	000000
001	18*	C	VDE - VALUE OF ENERGY DELIVERED OVER TMAX, \$	000000
001	19*	C	TDE - TOTAL ENERGY DELIVERED OVER TMAX, KWH	000000
001	20*	C	TLD - TOTAL LOAD DEMAND OVER TMAX, KWH	000000

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00162	78*	6 2X,F6.2)	000144
00162	79*	C	000144
00163	81*	PCD= (TDE-SPD)*100./TLD	000144
00164	81*	PCU= UTD*100./TLD	000150
00165	82*	PCS= SPD*100./TLD	000154
00166	83*	CPKWH= (TOYH*(TDE-SPD) + UTV*1000.)/TLD	000160
00167	84*	WRITE(6,500)PCD ,PCU,PCS,CPKWH	000167
00175	85*	5CD FORMAT(//// 30X,31H0 LOAD FACTOR / 1H+,29X,	000200
00175	86*	1 1H+ / 1H-,42X,	000200
00175	87*	1 26HPERCENT OF LOAD SUPPLIED , F6.1, 2H / 1H ,42X,22HBY TOTAL WIN	000200
00175	88*	2ND SYSTEM / 1H0,42X,24HPERCENT OF LOAD SUPPLIED,2X,F6.1 /	000200
00175	89*	2 1H ,41X,11H BY UTILITY /	000200
00175	90*	3 1H0,42X,26HPERCENT OF WIND ENERGY , F6.1 /	000200
00175	91*	3 1H ,42X,9HSURPLUSED /	000200
00175	92*	4 1H0,42X,23HCOST TO MEET LOAD , 3X,F6.1,6H MILLS/	000200
00175	93*	5 1H ,42X,27H(WIND + UTILITY) / 1H1)	000200
00175	94*	C	000200
00176	95*	RETURN	000200
00177	96*	END	000225

7.6 COMPRESSOR (PNEUMATIC)



The compressor model represents the off-design performance of a typical axial flow compressor. The compressor is assumed designed for a specified set of design operating conditions and performance requirements. The mass flow rate is assumed directly proportional to angular velocity and independent of the pressure ratio across the compressor. This is expected to hold for $\pm 15\%$ of the design mass flow rate. The polytropic efficiency of the compressor is assumed to be a weak function of the angular velocity. Initial calculations are made with the design polytropic efficiency, and refinements made after the off-design parameters are calculated.

Basic Equations

The expression for the angular velocity is

$$RS = P1 * \frac{RSD}{MD} \frac{EFF}{CP * (TA + 460) * [(PR2/PA)^A - 1]}$$

where:

$$EFF = ((PR2/PA)^{(A*NP)} - 1.) / ((PR2/PA)^A - 1.)$$

$$A = (GAM - 1) / GAM * NP$$

Inputs

<u>Parameter/Port</u>		<u>Description</u>	<u>Units</u>
P	1	Input power	kw
RSD		Design angular velocity (D = 3600)	rpm
MD		Design mass flow rate (D = 3000)	lb/h
CP		Heat capacity of air (D = 7.2×10^{-5})	kwh/lb ^o F
TA		Inlet air temperature (ambient) (D = 70)	^o F
PR	2	Exit pressure (D = 147)	psi
PA		Inlet pressure (ambient) (D = 14.7)	psi
GAM		Heat capacity ratio (D = 1.4)	-
EF	1	Input product efficiency	-
MP	1	Maximum input power	kw
NPD		Design polytropic efficiency (D = 0.88)	-
PID		Design inlet pressure (ambient) (D = 14.7)	psi
P OD		Design outlet pressure (D = 147)	psi
TID		Design inlet air temp (ambient) (D = 70)	^o F
CK		Compressor capacity cost coefficient ¹ (D = 1.0)	-
F O		Compressor exponent for cost calculations (D = 0.75)	-

Outputs

<u>Variable/Port</u>			
NP		Polytropic efficiency	-
EF	2	Output product efficiency	-
MP	2	Maximum output power	kw
T O		Torque	ft-lb
M		Mass flow rate	lb/h
T	2	Exit temperature	^o F
RS		Angular velocity	rpm
CC O		Cost of compressor/year	\$

¹ CK = capital cost (known unit)/(design point mass flow rate)^{F~~O~~} *
LN (outlet/inlet pressure ratio)*(life expectancy of unit)
D - Default values supplied

<u>Statistics</u>	<u>Description</u>	<u>Units</u>
MT	Maximum temperature	°F
MF	Maximum mass flow rate	lb/h

The calculation sequence and the default values are based on the assumption of an axial flow compressor, nominally rated at 125kw, and a pressure ratio of 10. The equations used relate first order effects among the various physical quantities and were derived from first principles originally to support the research work of Reference 1. Cost scaling was also developed in that reference based on cost estimates obtained from turbomachinery manufacturers.

Calculation Sequence

1) Costs (First pass only)

$$CC0 = CK * (MD) ** F0 * LN \left(\frac{P0D}{PID} \right)$$

If P1 > 0 go to 2)

$$A = (GAM - 1) / (GAM * NPD)$$

$$RAT = (P0D / PID) ** A$$

$$EFF = 1, RS = 0, \text{ go to 3)}$$

-
1. "Closed Cycle High Temperature Central Receiver Concept for Solar Electric Power," BEC/EPRI RP 377-1, June 1976.

Calculation Sequence Cont.

2) Angular velocity iteration

$$A = (GAM-1)/(GAM*NP) \quad (\text{Initially } NP = NPD)$$

$$RAT = (PR2/PA)**A$$

$$EFF = (RAT**NP-1)/(RAT-1)$$

$$\frac{RS}{RSD} = \frac{P1}{MD \cdot CP \cdot (TA+460)} \cdot \frac{EFF}{(RAT-1)}$$

Polytropic efficiency

$$NP = 1 - (1 - NPD) * [2.0 - \left(\frac{PID * (TA+460) * RSD}{PA \cdot (TID+460) \cdot RS} \right) ** 0.2]$$

Iterate until NP and RS are consistent

(If iteration doesn't converge, then write DIAGNOSTIC and exit)

3) Mass flow rate

$$M = MD * RS / RSD$$

4) Exit temperature

$$T2 = (TA+460)*RAT - 460$$

5) Torque

If $P1 \leq 0$, set $T0 = 0$ and go to 6)

$$T0 = P1 * 737.6 / (RS * 2\pi / 60)$$

6) Efficiency and maximum power

$$EF2 = EF1 * EFF$$

$$MP2 = \text{MIN}(MP1 * EFF, 1.5 * MD * CP * (T2 - TA))$$

7) Compute Statistics and Costs

SUBROUTINE CO

ENTRY POINT 000420

STORAGE USED CODE(1) 000613; DATA(0) 000066; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000001
 0004 CTIME 000001
 0005 CSTMUL 000010
 0006 COST 000001

EXTERNAL REFERENCES (BLOCK, NAME)

0007 XPRR
 0010 ALOG
 0011 NWDUS
 0012 N1023
 0013 NSTOPS
 0014 NERR33

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000136	100L	0001	000375	1000L	0000	000010	1010F	0001	000166	200L	0001	000271	300L					
0001	000315	400L	0000	R	000005	A	0006	R	000000	CC1	0005	000000	DUM	0000	R	000003	EFF		
0003	I	000000	IMPL	0000	000052	INJPS	0000	I	000002	ISP	0000	R	000000	PI	0000	R	000004	RAT	
0000	R	000006	RSNO	0004	R	000000	TIME	0005	R	000007	TMAX	0000	R	000001	TMAX1	0000	R	000007	XNP

00100	1*	CCO																000000
00101	2*		SUBROUTINE CO(INP,EF2,MP2,TO,H,T2,RS,CC,MT,MF,P1,RSD,MD,CP,TA,PR2,															000000
00101	3*		1	PR1,GAM,EF1,MP1,NPD,PID,POD,TID,CK,FO)														000000
00101	4*	C																000000
00101	5*	C	PURPOSE	PERFORMANCE MODEL OF AXIAL FLOW COMPRESSOR														000000
00101	6*	C																000000
00101	7*	C	METHOD	COMPRESSOR IS SIZED FROM INPUT OPERATING REQUIREMENTS.														000000
00101	8*	C																000000
00101	9*	C		MASS FLOW IS ASSUMED PROPORTIONAL TO ANGULAR VELOCITY														000000
00101	10*	C																000000
00101	11*	C		AND INDEPENDENT OF PRESSURE RATIO.														000000
00101	12*	C																000000
00101	13*	C	WRITTEN BY F.O. MAHONY															000000
00101	14*	C		VERSION 1, MARCH 22 1977														000000
00101	15*	C	CALL SEQUENCE															000000
00101	16*	C	OUTPUTS															000000
00101	17*	C		NP - POLYTROPIC EFFICIENCY														000000
00101	18*	C		EF2 - OUTPUT PRODUCT EFFICIENCY														000000
00101	19*	C		MP2 - MAXIMUM OUTPUT POWER, KW														000000
00101	20*	C		TO - TORQUE, FT-LB														000000

```

00101 21* C M - MASS FLOW RATE, LB/HR 000000
00101 22* C T2 - EXIT TEMPERATURE, DEG F 000000
00101 23* C RS - ANGULAR VELOCITY, RPM 000000
00101 24* C CC - COST OF COMPRESSOR PER YEAR, $/YEAR 000000
00101 25* C MT - MAXIMUM TEMPERATURE OBSERVED, DEG F 000000
00101 26* C MF - MAXIMUM MASS FLOW RATE, LB/HR 000000
00101 27* C
00101 28* C
00101 29* C INPUTS 000000
00101 30* C P1 - INPUT POWER, KW 000000
00101 31* C RSD - DESIGN ANGULAR VELOCITY, RPM 000000
00101 32* C MD - DESIGN MASS FLOW RATE, LB/HR 000000
00101 33* C CP - HEAT CAPACITY OF AIR, KWH/LB-DEG F 000000
00101 34* C TA - INLET AIR TEMPERATURE (AMBIENT), DEG F 000000
00101 35* C PR2 - EXIT PRESSURE, PSI 000000
00101 36* C PR1 - INLET PRESSURE (AMBIENT), PSI 000000
00101 37* C GAM - HEAT CAPACITY RATIO 000000
00101 38* C EF1 - INPUT PRODUCT EFFICIENCY 000000
00101 39* C MPI - INPUT MAXIMUM DISCHARGE POWER, KW 000000
00101 40* C NPD - DESIGN POLYTROPIC EFFICIENCY 000000
00101 41* C PID - DESIGN INLET PRESSURE (AMBIENT), PSI 000000
00101 42* C POD - DESIGN OUTLET PRESSURE (AMBIENT), PSI 000000
00101 43* C TID - DESIGN INLET TEMPERATURE (AMBIENT), DEG F 000000
00101 44* C CK - COMPRESSOR CAPACITY COST COEFFICIENT 000000
00101 45* C FO - COMPRESSOR EXPONENT FOR COST CALCULATION 000000
00103 46* COMMON /CIMPL/ IMPL /CTIME/ TIME /CSIMUL/DUM(7),TMAX /COST/CCI 000000
00104 47* REAL MD,MPI,NPD,NP,MP2,M,MT,MF 000000
00105 48* DATA PI /3.14159/ 000000
00105 49* C INITIALIZATION 000000
00107 50* C
00107 51* IF (IMPL.GT.0) GO TO 100 000000
00111 52* MT = 0.0 000000
00112 53* MF = 0.0 000000
00112 54* C 000000
00113 55* C 000000
00115 56* IF (RSD.EQ. .99999) RSD = 3600.0 000000
00117 57* IF (MD.EQ. .99999) MD = 3.0E3 000000
00121 58* IF (MPI.EQ. .99999) MPI = 1.E8 000000
00123 59* IF (CP.EQ. .99999) CP = 72.0E-6 000000
00125 60* IF (TA.EQ. .99999) TA = 70.0 000000
00127 61* IF (PR2.EQ. .99999) PR2 = 147.0 000000
00131 62* IF (PR1.EQ. .99999) PR1 = 14.7 000000
00133 63* IF (GAM.EQ. .99999) GAM = 1.4 000000
00135 64* IF (NPD.EQ. .99999) NPD = 0.88 000000
00137 65* IF (PID.EQ. .99999) PID = 14.7 000000
00141 66* IF (POD.EQ. .99999) POD = 147.0 000000
00143 67* IF (TID.EQ. .99999) TID = 70.0 000000
00145 68* IF (CK.EQ. .99999) CK = 1.0 000000
00147 69* IF (FO.EQ. .99999) FO = 0.75 000000
00147 70* NP = NPD 000000
00147 71* C 000000
00147 72* C COST 000000
00150 73* CC = CK*MD**FO+ALOG(POD/PID) 000000
00151 74* TMAX1 = TMAX*.99999 000000
00152 75* 100 CONTINUE 000000
00 76* C 000000
00 77* C SOLVE FOR POLYTROPIC EFFICIENCY 000000

```

```

                                AND ANGULAR VELOCITY
00152  78*  C
00152  79*  C
00153  80*  ISP = 0
00153  81*  C
00154  82*  EFF=1.0
00155  83*  IF(P1.GT.0.0)GO TO 200
00155  84*  C
00157  85*  RAT= (POD/PID)**((GAM-1.0)/(GAM+NP))
00160  86*  TO =0.0
00161  87*  RS=0.0
00162  88*  NP=NP0
00163  89*  GO TO 300
00163  90*  C
00164  91*  200 A = (GAM-1.0)/(GAM+NP)
00165  92*  RAT= (PR2/PP1)**A
00166  93*  EFF=(RAT**NP - 1.)/(RAT - 1.)
00166  94*  C
00167  95*  RSNO = EFF*P1/MD*1.0/CP/(TA+460.0)/(RAT-1.0)
00167  96*  C
00170  97*  XNP = NP
00170  98*  C
00171  99*  NP = 1.0-(1.0-NPD)*(2.0-(PID/PR1*(TA+460.0)/(TID+460.0)/RSNO)
00171 100*  1 **0.2)
00171 101*  C
00172 102*  IF(ISP.GT.10), GO TO 1000
00172 103*  C
00174 104*  ISP = ISP+1
00174 105*  C
00175 106*  IF(ABS((NP-XNP)/NP).GT.0.001) GO TO 200
00177 107*  RS= RSD*RSNO
00177 108*  C
00177 109*  C
00177 110*  C
00200 111*  300 M = MD*RS/RS0
00203 112*  C
00203 113*  C
00203 114*  C
00201 115*  T2 = (TA+460.0)*RAT-460.0
00202 116*  IF(P1.LE.0.0)GO TO 400
00202 117*  C
00202 118*  C
00202 119*  C
00204 120*  TO = P1*737.6/(RS*2.0*PI/60.0)
00204 121*  C
00204 122*  C
00204 123*  C
00204 124*  C
00204 125*  C
00205 126*  400 EF2 = EF1*EFF
00205 127*  C
00206 128*  MP2 = AMIN1(MP1*EFF,1.5*MD*CP*(T2-TA))
00206 129*  C
00206 130*  C
00207 131*  C
00211 132*  IF (IMPL.LE.1) RETURN
00211 133*  MT = AMAX1(MT, T2)
00212 134*  MF = AMAX1(MF, M)
00213 135*  IF (TIME.LT.TMAX1) RETURN

```

```

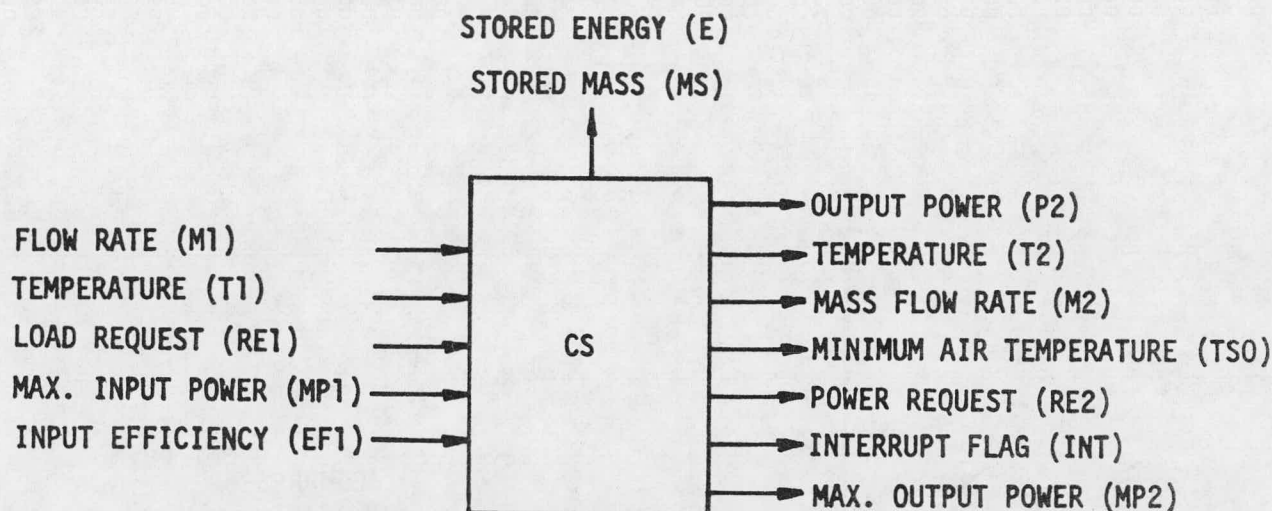
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```

```
00215 135*      CCI = CCI + CC
00215 136*      C
00216 137*      RETURN
00216 138*      C
00217 139*      1000 WRITE (6,1010) NP,XNP,RS
00224 140*      1010 FORMAT (1H0,40HMAX ITERATIONS FOR COMPRESSOR EFFICIENCY,
00224 141*      1      15H - NP,XNP,RS = ,3F12.6)
00225 142*      STOP
00226 143*      END
```

```
000366
000366
000371
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000375
000404
000404
000404
000404
000612
```

7.7 PNEUMATIC STORAGE VESSEL (CONSTANT PRESSURE)



The pneumatic storage vessel is based on a constant pressure underground cavern design as represented in Figure 7.7. A surface pressure-compensation pond via a water shaft is assumed to maintain the vessel pressure at a constant value. This model is assumed to be used in conjunction with a heat exchanger. The energy is calculated as a function of the stored gas mass, the inlet/storage air temperature, and a leakage function proportional to the stored energy.

Basic Equation

The rate of energy storage is computed from the equation

$$\dot{E} = M1 * CP * (T1 - T0) - NU * E, \text{ charging}$$

$$\dot{E} = -M2 * CP * (T2 - T0) - NU * E, \text{ discharging}$$

where $M1$ = mass flow rate during charge

$M2$ = mass flow rate during discharge

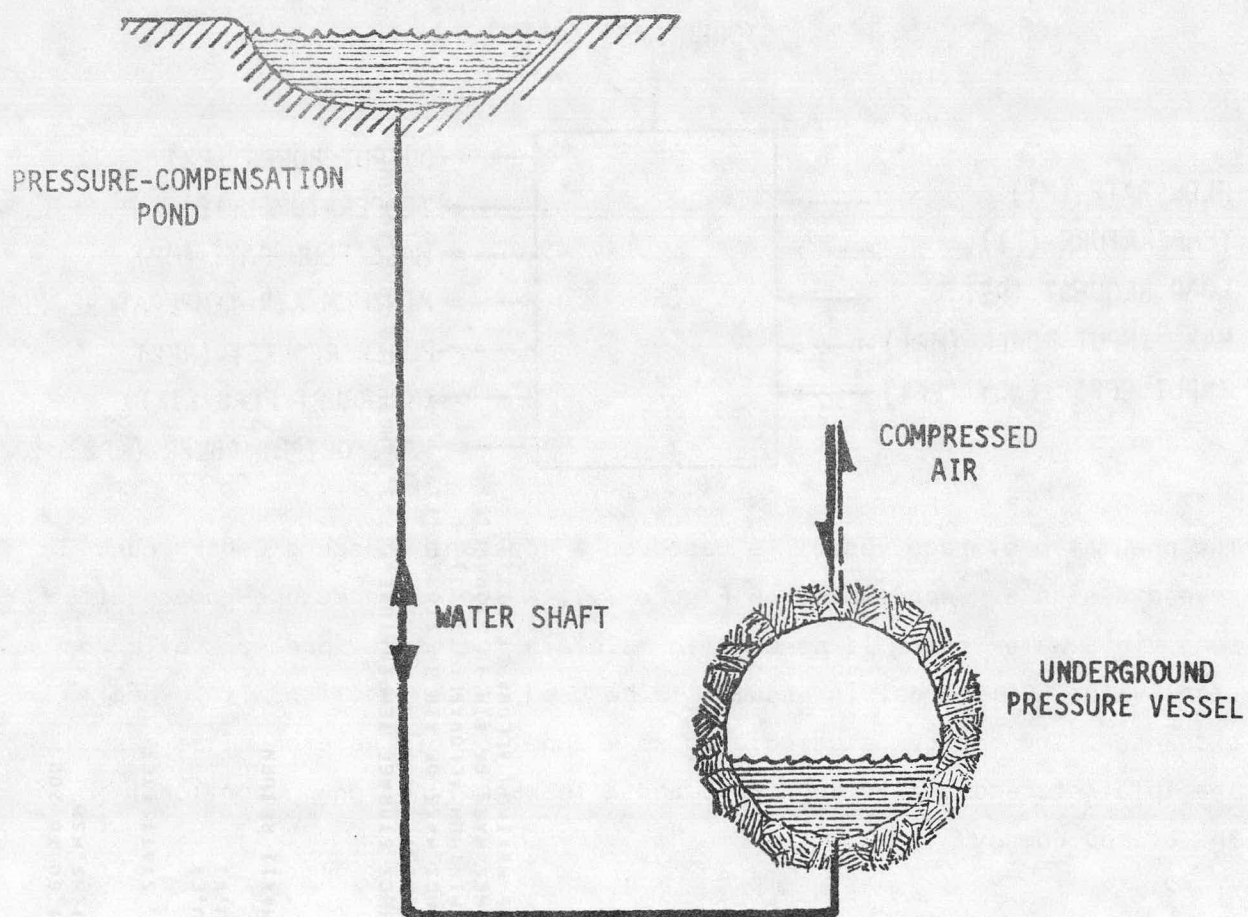


FIGURE 7.7 CONSTANT PRESSURE AIR STORAGE

Inputs

<u>Parameter/Port</u>		<u>Description</u>	<u>Units</u>
M	1	Inlet air mass flow rate	lb/h
CP		Air heat capacity ($D = 7.2 \times 10^{-5}$)	kwh/lb ^o F
T	1	Inlet air temperature	^o F
T0		Minimum air temperature ($D = 60$)	^o F
NU		Leakage coefficient ($D = 0.0008$)	h ⁻¹
R		Gas constant ($D = 2.009 \times 10^{-5}$)	kwh/lb
VM		Maximum storage capacity ($D = 1.2 \times 10^6$)	ft ³
PR	1	Vessel pressure ($D = 147$)	psi
LE		Life expectancy of vessel	years
CV		Vessel capacity cost ($D = 0.22$)	\$/ft ³
RE	1	Load request	kw
EF	1	Input product efficiency	-
MP	1	Input maximum power	kw
MDE		Mass threshold for priority resequencing	lb
MD		Maximum charge or discharge mass flow rate	lb
TM		Maximum allowable air temperature ($D = 120$)	^o F
TEM		Maximum allowable inlet temperature	^o F
CM		Maintenance cost/year	\$

Outputs

<u>Variable/Port</u>			
E		Stored energy (state)	kwh
M	2	Outlet mass flowrate	lb/hr
T	2	Storage temperature	^o F
V		Storage volume	ft ³
CC0		Cost of vessel/year	\$
MS		Mass of air in storage (state)	lb
MP	2	Maximum output power	kw
RE	2	Maximum charging rate	kw
INT		Interrupt priority flag	-
TS0		Minimum air temperature (=T0)	^o F

D - Default values supplied

Outputs Cont.Variable/Port

PR	2	Vessel pressure (=PR1)	psi
P	2	Output power (discharge)	kw
MDM		Maximum allowable mass flow rate (=MD)	

Statistics

EU		Maximum stored energy	kwh
VU		Maximum storage volume	ft ³

The pneumatic storage vessel calculation sequence and default values assume a 10atm cavern approximately 340 ft. below ground and sized for storage of 120kw for 24 hours. A maximum cavern wall temperature of 120°F is assumed. Cost estimates for the vessel were estimated from the results of Reference 1, with cost scaling by .05 to account for plant size differences.

-
1. "Preliminary Feasibility Evaluation of Compressed Air Storage Power Systems," United Technologies AER 74-00242, December 1976.

Calculation Sequence

TINC = integration step size, hr

C1 = conversion constant = 5.43×10^{-5}

$\frac{\text{kwh/ft}^3}{\text{psi}}$

- 1) Vessel Cost

$$CC0 = CV * VM / LE$$

- 2) Storage temperature

$$T2 = \frac{E}{CP * MS} + T0$$

- 3) Storage volume

$$V = MS * \frac{R * (T2 + 460)}{PR1 * C1}$$

- 4) Maximum Mass and charging rate

$$MSM = VM * \frac{(PR1 * C1)}{R * (T2 + 460)}$$

$$MD1 = \text{MIN}(MDM, (MSM - MS) / TINC)$$

$$RE2 = \min \left\{ MP1, MD1 * CP * (TEM - T0) \right\} / EF1$$

- 5) Mass flow out (discharge mode)

$$M2 = \frac{RE1}{CP * (T2 - T0)}$$

$$P2 = RE1$$

- 6) Maximum discharge rate

$$MD = \text{MIN}(MDM, (MS - MDE) / TINC)$$

$$MP2 = CP * (T2 - T0) * MD$$

Calculation Sequence Cont.

- 7) Stored energy rate

$$\dot{E} = CP*(T1-T0)*M1 - NU*E - RE1$$

- 8) Stored mass rate

$$\dot{M}S = M1 - M2$$

- 9) Priority interrupt

If $MS \leq MDE$, $INT = 1$

If $MS > 2*MDE$ and $INT = 1$, $INT = 0$

If $MS \geq MSM$, $INT = -1$

If $MS < MSM - MDE$ and $INT = -1$, $INT = 0$

If $T2 > TM$ write diagnostic and set $INT = -1$

If $MS < MDE$ or $MS > MSM$ write diagnostic

- 10) Compute Statistics and Costs

ENTRY POINT 000427

COMMON BLOCKS

```
0003      C1MPL      000002
0004      C1ME       000001
0005      CSTMUL      000010
0006      COST        000002
```

EXTERNAL REFERENCES (BLOCK, NAME)

0007	NW008
0010	NI028
0011	NERP38

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000326	10L	0001	000074	100L	0000	000004	10C0F	0000	000021	1010F	0000	000036	1020F
0001	000344	20L	0001	000362	200L	0006	R 000000	CCY	0006	R 000001	CHI	0000	R 000003	CI
0005	R 000000	DUM	0003	I 000001	ICNY	0003	I 000000	IMPL	0000	000072	INJP%	0000	R 000001	MDI
0000	R 000000	MSH	0004	R 000000	TIME	0005	R 000007	THAX	0000	R 000002	THAX1			

00100	1*	CCS		000000
00101	2*		SUBROUTINE CS(E,DE,IE,MS,DMS,IMS,M2,T2,V,CC,MP2,RE2,INT,T50,PR2	000000
00101	3*		1 ,P,MDM,EU,VU,M1,CP,T,TO,R,VN,PR1,LE,NU,CV,RE1,EF1,MP1,MDE,HD,TM	000000
00101	4*		2 ,TEM,CM)	000000
00101	5*	C		000000
00101	6*	C	PURPOSE PERFORMANCE MODEL OF CONSTANT PRESSURE STORAGE VESSEL	000000
00101	7*	C		000000
00101	8*	C	METHOD ENERGY IN STORAGE COMPUTED AS A FUNCTION MASS AND	000000
00101	9*	C		000000
00101	10*	C	INLET TEMPERATURE.	000000
00101	11*	C		000000
00101	12*	C	WRITTEN BY F.O. MAHONY	000000
00101	13*	C	VERSION 1, MARCH 23 1977	000000
00101	14*	C	CALL SEQUENCE	000000
00101	15*	C		000000
00101	16*	C	OUTPUTS	000000
00101	17*	C	E - STORED ENERGY (STATE VARIABLE), KWH	000000
00101	18*	C	DE - STORED ENERGY DERIVATIVE, KW	000000
00101	19*	C	IE - STATUS INDICATOR FOR E	000000
00101	20*	C	MS - MASS OF AIR IN STORAGE (STATE VARIABLE), LB	000000
00101	21*	C	DMS - AIR FLOW RATE, LB/HR	000000
00101	22*	C	IMS - STATUS INDICATOR FOR MS	000000
00101	23*	C	M2 - OUTLET MASS FLOWRATE, LB/HR	000000



00101	24*	C	T2 - STORAGE TEMPERATURE, DEG F	00000C
00101	25*	C	V - STORAGE VOLUME, FT**3	000000
00101	26*	C	CC - COST OF VESSEL/YEAR, \$	000000
00101	27*	C	MP2 - MAXIMUM OUTPUT POWER, KW	000000
00101	28*	C	RE2 - MAXIMUM CHARGING RATE, KW	000000
00101	29*	C	INT - INTERRUPT PRIORITY FLAG	000000
00101	30*	C	TSO - MINIMUM AIR TEMPERATURE, DEG F	000000
00101	31*	C	PR2 - VESSEL PRESSURE, PSI	000000
00101	32*	C	P - OUTPUT POWER (DISCHARGE), KW	000000
00101	33*	C	MDM - MAXIMUM ALLOWABLE MASS FLOW RATE, LB/HR	000000
00101	34*	C	EU - MAXIMUM STORED ENERGY, KWH	000000
00101	35*	C	VU - MAXIMUM STORAGE VOLUME, FT**3	000000
00101	36*	C		000000
00101	37*	C	INPUTS	000000
00101	38*	C	M1 - INLET AIR MASS FLOW RATE, LB/HR	000000
00101	39*	C	CP - AIR HEAT CAPACITY, KWH/LB-DEG F	000000
00101	40*	C	T - INLET AIR TEMPERATURE, DEG F	000000
00101	41*	C	TO - MINIMUM AIR TEMPERATURE, DEG F	000000
00101	42*	C	R - GAS CONSTANT, KWH/LB-DEG R	000000
00101	43*	C	VM - MAXIMUM STORAGE CAPACITY, FT**3	000000
00101	44*	C	PR1 - VESSEL PRESSURE, PSI	000000
00101	45*	C	LE - LIFE EXPECTANCY OF VESSEL, YEARS	000000
00101	46*	C	NU - LEAKAGE COEFFICIENT, 1/HR	000000
00101	47*	C	CV - VESSEL CAPACITY COST, \$/FT**3	000000
00101	48*	C	RE1 - LOAD REQUEST, KW	000000
00101	49*	C	EF1 - INPUT PRODUCT EFFICIENCY	000000
00101	50*	C	MP1 - INPUT MAXIMUM POWER, KW	000000
00101	51*	C	MDE - RESERVOIR THRESHOLD MASS FOR PRIORITY	000000
00101	52*	C	RESEQUENCING, LB	000000
00101	53*	C	MD - MAXIMUM CHARGE / DISCHARGE MASS FLOW RATE, LB/HR	000000
00101	54*	C	TM - MAXIMUM ALLOWABLE STORAGE TEMPERATURE, DEG F	000000
00101	55*	C	TEM - MAXIMUM ALLOWABLE INLET TEMPERATURE, DEG F	000000
00101	56*	C	CM - MAINTENANCE COST / YEAR, \$	000000
00101	57*	C		000000
00101	58*	C		000000
00103	59*		COMMON /CIMPL/IMPL,ICNT/CTIME/ TIME /CSIMUL/DUM(7),TMAX	000000
00104	60*		COMMON /COST/ CCI,CMI	000000
00105	61*		REAL NU,MS,MP2,INT,MDM,M1,LE,MP1,MDE,MD,M2,MSH,MD1	000000
00105	62*	C		000000
00105	63*	C		000000
00106	64*		IF(IMPL.GT.0) GO TO 100	000000
00106	65*	C		000000
00110	66*		IF(CP.EQ..99999) CP = 72.0E-6	000002
00112	67*		IF(TM.EQ..99999) TM= 120.0	000007
00114	68*		IF(TO.EQ..99999) TO = 60.0	000014
00116	69*		IF(NU.EQ..99999) NU = 0.0008	000021
00120	70*		IF(R.EQ..99999) R = 2.009E-5	000026
00122	71*		IF(VM.EQ..99999) VM = 1.2E+6	000033
00124	72*		IF(PR1.EQ..99999) PR1 = 147.0	000040
00126	73*		IF(CV.EQ..99999) CV = 0.22	000045
00130	74*		RE1=0.0	000052
00130	75*	C		000053
00131	76*		TMAX1 = TMAX*0.99999	000056
00132	77*		TSO=TO	000056
00132	78*	C		000060
00133	79*		CC = CV*VM/LE	000060
00134	80*		C1 = 5.43E-5	000064



```

00134      81*      C      INT = 0.
00135      82*      PR2=PR1
00136      83*      EU= 0.
00137      84*      VU= 0.
00140      85*      100 CONTINUE
00141      86*
00141      87*      C
00141      88*      C
00141      89*      C
00141      90*      C      STORAGE TEMPERATURE
00141      91*      C
00142      92*      T2 = E/CP/MS+T0
00142      93*      C
00142      94*      C      STORAGE VOLUME
00142      95*      C
00143      96*      V = MS*R*(T2+460.0)/PR1/C1
00143      97*      C
00143      98*      C      MAXIMUM MASS AND CHARGING RATE
00143      99*      C
00144      100*      MSM = VM*PR1*C1/R/(T2+460.0)
00145      101*      MDM=MD
00146      102*      MD1= AMIN1(MDM,AMAX1(0.,(MSH-MS)/DUM(7)))
00147      103*      RE2 = AMIN1(MP1,MD1*CP*(TEM-T0))/EF1
00147      104*      C
00147      105*      C      MASS FLOW OUT (DISCHARGE)
00147      106*      C
00150      107*      M2 = RE1/CP/(T2-T0)
00151      108*      P = RE1
00151      109*      C
00151      110*      C      MAXIMUM DISCHARGE RATE
00151      111*      C
00152      112*      MDM= AMIN1(MDM,AMAX1(0.,(MS-MDE)/DUM(7)))
00153      113*      MP2 = CP*(T2-T0)*MDM
00153      114*      C
00153      115*      C      STORED ENERGY RATE
00153      116*      C
00154      117*      IF(IE.NE.0) DE=CP*(T-T0)*M1 - NU*E -RE1
00154      118*      C
00154      119*      C      STORED MASS RATE
00154      120*      C
00156      121*      IF(IMS.NE.0) DMS=M1-M2
00156      122*      C
00156      123*      C      PRIORITY INTERRUPT LOGIC
00160      124*      IF(MS.LE. MDE) INT=1.
00162      125*      IF(MS.GT. 2.*MDE .AND. INT.EQ.1.) INT=0.
00164      126*      IF(MS.GE.MSH) INT = -1.
00166      127*      IF(MS.LT. MSM-MDE .AND. INT.EQ.-1.) INT=0.
00170      128*      IF(T2.GT. TM) INT= -1.
00170      129*      C
00172      130*      IF(IMPL.LE.1) RETURN
00174      131*      IF(IMPL.GT.2)GO TO 200
00176      132*      IF(T2.LT.TM) GO TO 10
00200      133*      WRITE(6,1000) T2,TM
00204      134*      ICNT=ICNT+1
00205      135*      10 IF(MS.GT.MDE) GO TO 20
00207      136*      WRITE(6,1010)MS,MDE
00213      137*      ICNT=ICNT+1

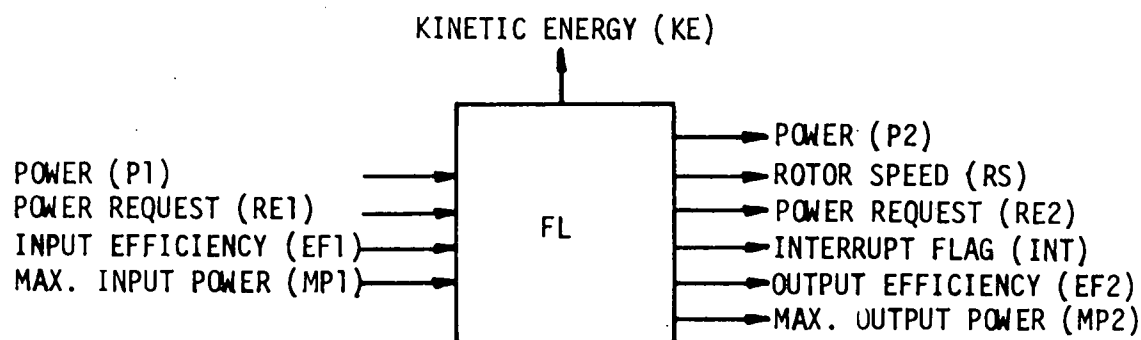
```

C00C64
 000066
 000C67
 000C71
 C00072
 C00074
 C00C74
 C00C74
 C00C74
 000074
 000C74
 000074
 000C74
 C00C74
 000100
 000100
 000100
 000110
 C00116
 C00120
 000133
 000133
 000133
 C00133
 000145
 C00153
 000153
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 C00153
 000155
 000171
 C00171
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 C00174
 C00174
 C00207
 000207
 000207
 C00214
 C00222
 C00241
 C00247
 C00266
 000266
 000274
 000303
 C00307
 C00313
 000322
 000326
 000331
 000340



00214	138*	20	IF(MS.LT.MSH) GO TO 200	000344
00216	139*		WRITE(6,1020) MS,MSH	000347
00222	140*		ICNT=ICNT+1	000356
00222	141*	C		000356
00222	142*	C	STATISTICS	000356
00222	143*	C		000356
00223	144*	200	EU = AMAX1(EU,E)	000362
00224	145*		VU = AMAX1(VU,V)	000367
00224	146*	C		000367
00225	147*		IF(TIME.LT.TMAX1) RETURN	000375
00227	148*		CCI = CCI+CC	000404
00230	149*		CHI=CHI+CM	000407
00230	150*	C		000407
00231	151*		RETURN	000412
00232	152*	1000	FORMAT(1H0,23HCS STORAGE TEMPERATURE,F12.3,18HGREATER THAN ALLOW,	000636
00232	153*	1	SHABLE , F12.3)	000636
00233	154*	1010	FORMAT(1H0,25HCS MASS OF AIR IN STORAGE,F12.3,	000636
00233	155*	1	26H BELOW MINIMUM ALLOWABLE,F12.3)	000636
00234	156*	1020	FORMAT(1H0,25HCS MASS OF AIR IN STORAGE,F12.3,	000636
00234	157*	1	28H EXCEEDS MAXIMUM ALLOWABLE,F12.3)	000636
00235	158*		END	000636

7.8 FLYWHEEL/CLUTCH



The flywheel model is a first order differential equation for kinetic energy which is driven by input power when charging and by a load request when discharging. Power losses include clutch losses versus shaft speed and torque, windage losses, and friction losses due to bearing and seals. Shaft speed is determined analytically from kinetic energy. Priority interrupt logic is activated if minimum or maximum capacity levels are reached.

Basic Equations

$$KE = k * \omega^2$$

$$\dot{KE} = P_{IN} - P_{OUT} - C_1 * \omega - C_2 * \omega^{2.8},$$

where k, C_1, C_2 are flywheel constants

ω = rotor speed in rad/sec

P_{IN} = input power - clutch losses

P_{OUT} = output load request

<u>Tables</u>	<u>Description</u>	<u>Units</u>
CL0	Clutch losses versus rotor speed (rpm) and torque (ft-lb), when engaged (Table dimension = 90)	kw
CL1	Clutch losses versus rotor speed (rpm) when disengaged (Table dimension = 17)	kw

Inputs

Parameter/Port

PR		Pressure in vacuum housing	psi
HM		Moment of inertia ¹	slug-ft ²
RF		Radius of flywheel	ft
SR		Shaft radius	ft
WT		Flywheel weight	lb
KF		Coefficient of friction	-
ZE		Width of flywheel at tip	ft
C2		Windage loss coefficient (analytic default)	-
P	1	Input power	kw
EF	1	Input product efficiency	-
MP	1	Input maximum charging rate	kw
RAP		Rated power, charge or discharge	kw
RE	1	Discharge load request	kw
E0		Minimum allowable storage capacity	kwh
E1		Maximum allowable storage capacity	kwh
EDE		Energy deadband for priority resequencing	kwh
CM		Maintenance cost/year	\$
CC		Capital cost/year	\$

Outputs

Variable/Port

RS		Rotor speed	rpm
KE		Kinetic energy (state)	kwh

¹ Includes physical drive system.

Outputs Cont.

<u>Variable/Port</u>	<u>Description</u>	<u>Units</u>
T0	Input torque (charging)	ft-lb
T1	Output torque (discharging)	ft-lb
P 2	Output power	kw
PL0	Clutch losses (charging)	kw
PL1	Clutch losses (discharging)	kw
EF 2	Output efficiency	-
MP 2	Maximum output power	kw
INT	Priority interrupt flag	-
RE 2	Maximum charging power request	kw

Statistics

ME	Maximum stored energy	kwh
MPC	Maximum charge rate	kw
MPD	Maximum discharge rate	kw
SPC	Sum of charging energy	kwh
SPD	Sum of discharging energy	kwh

Calculation Sequence

- 1) Compute flywheel constants

$$k = \frac{1}{2} * HM * 3.76616 * 10^{-7}$$

$$C_1 = KF * WT * SR * 1.3558 * 10^{-3}$$

$$C_2 = C_o * PR^{0.8} * RF^{4.6} * (1 + 2.3 * ZE / RF) \quad (\text{DEFAULT})$$

$$C_o = 1.0946 * 10^{-7}$$

If $KE < E0$ or $KE > E1$ write diagnostic

- 2) Compute rotor speed

$$\omega = \sqrt{KE/k}$$

$$RS = \omega * (60 / 2\pi)$$

$$P_{IN} = 0$$

- 3) Compute power losses and net power when charging

If $P1 = 0$, set $T0 = PL0 = P_{IN} = 0$ and go to 4)

$$T0 = P1 * 737.6 / \omega$$

$$PLO = CL0(RS, T0)$$

$$P_{IN} = P1 - PLO$$

If $P_{IN} < 0$, write diagnostic

- 4) Compute power losses and output power when discharging

If $RE1 = 0$, set $T1 = PL1 = P2 = P_{OUT} = 0$ and go to 5)

$$T1 = RE1 * 737.6 / \omega$$

$$PL1 = CL0(RS, -T1)$$

Calculation Sequence

4) Cont.

$$P2 = RE1 - PL1$$

$$P_{OUT} = RE1$$

If $P2 < 0$, set $P2 = 0$. and write diagnostic

5) Compute power losses when disengaged

If $P1 > 0$ or $RE1 > 0$, go to 6)

$$P_{OUT} = CL1(RS)$$

6) Flywheel kinetic energy rate

$$\dot{KE} = P_{IN} - P_{OUT} - C_1 * \omega - C_2 * \omega^{2.8}$$

7) Maximum Input (charging power)

$$TM = MP1 * 737.6 / \omega$$

$$MP0 = MP1 - CL0(RS, TM)$$

If $MP0 \leq 0$, write diagnostic and go to 8)

$$EF0 = EF1 * MP0 / MP1$$

$$RE2 = \min(MP0, RAP), (E1 - KE) / TINC / EF0$$

8) Output efficiency and maximum power

$$RAP1 = \min(RAP, (KE - E0) / TINC), TINC = \text{integration step}$$

$$TM = RAP1 * 737.6 / \omega$$

$$MP2 = RAP1 - CL0(RS, -TM)$$

Calculation Sequence

8) Cont.

If $MP2 < 0$ write diagnostic

$$EF2 = MP2/RAP1$$

If $RE1 > 0$, $EF2 = P2/RE1$

9) Priority interrupt logic

If $KE \leq E0$, $INT = 1$

If $KE > E0 + EDE$ and $INT=1$, $INT=0$

If $KE \geq E1$, $INT = -1$

If $KE < E1 - EDE$ and $INT= -1$, $INT=0$

10) Compute Statistics and Costs

SUBROUTINE FL ENTRY POINT 001125

STORAGE USED CODE(1) 001333; DATA(0) 000231; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 C1MPL 000002
 0004 CTIME 000001
 0005 CSIMUL 000010
 0006 COST 000002

EXTERNAL REFERENCES (BLOCK, NAME)

0007 TBLU2
 0010 TBLU1
 0011 XPRR
 0012 NWDS
 0013 NI025
 0014 SQRT
 0015 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000060 10L	0000 000042 108F	0000 000026 109F	0001 000147 20L	0001 000315 200L
0000 000060 208F	0001 000412 300L	0000 000074 308F	0001 000440 400L	0001 000544 500L
0000 000110 508F	0001 000574 600L	0001 000705 700L	0000 000125 708F	0000 R 000005 AK
0000 R 000022 APC	0006 R 000000 CCI	0006 R 000001 CHI	0000 R 000006 C1	0005 R 000000 DUM
0000 R 000025 ECO	0000 R 000024 EC1	0000 R 000021 EFO	0003 I 000001 ICNT	0003 I 000000 IMPL
0000 000166 INJPS	0000 I 000012 MN4	0000 R 000001 MPA	0000 R 000002 MPB	0000 R 000000 MPO
0000 I 000011 M4	0000 I 000013 NNNRS	0000 I 000014 NNNRS4	0000 I 000007 NNRS	0000 I 000013 NNT
0000 R 000015 OMEGA	0000 R 000016 PIN	0000 R 000017 POUT	0000 R 000023 RAPT	0010 R 000000 TBLU1
0007 R 000000 TPLU2	0004 R 000000 TIME	0000 R 000003 TINC	0000 R 000020 TM	0005 R 000007 TMAX
0000 R 000004 TMAX1				

00100 1* CFL
 00101 2*
 00101 3* SUBROUTINE FLICLO,CL1,RS,KE,KED,IKE,TO,T1,P2,PL0,PL1,EF2,MP2,INT,
 00101 4* 1 RE2,ME,MPC,MPD,SPC,SPD, PR,HM,RF,SR,WT,KF,ZE,C2,P1,EF1,MP1,RAP
 00101 5* 2 ,RE1,E0,E1,EDE,CM,CC)
 00101 6* C
 00101 7* C PURPOSE MODEL OF FLYWHEEL CAPABLE OF ABSORBING POWER
 00101 8* C AND OF DELIVERING POWER ON REQUEST
 00101 9* C METHOD OUTPUT POWER AND KINETIC ENERGY COMPUTED FROM
 00103 10* C
 00103 11* C POWER REQUEST AND INPUT POWER
 00103 12* C
 00103 13* C

000007
 000007
 000007
 000007
 000007
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 000007



00114	71*	C		000046
00115	72*		MF=0.	000051
00116	73*		RE1=0.	000052
00117	74*		MPC=0.	000053
00120	75*		MPD=0.	000054
00121	76*		SPC=0.	000055
00122	77*		SPD=0.	000056
00123	78*	10	CONTINUE	000060
00124	79*		AK=.5*HM*3.76616E-7	000060
00125	80*		C1=KF*WT*SR*1.3558E-3	000063
00126	81*		IF(((KE.GT.E0).AND.(KE.LT.E1)).OR.(IMPL.NE.2))GO TO 20	000070
00130	82*		IF(KE.LE.E0)WRITE(6,108)KE,E0	000115
00135	83*		IF(KE.GE.E1)WRITE(6,109)KE,E1	000130
00142	84*	109	FORMAT(1H0,26H FLYWHEEL KINETIC ENERGY ,F12.3,	000143
00142	85*		X 18H EXCEEDS CAPACITY ,F12.3)	000143
00143	86*	108	FORMAT(1H0,24H FLYWHEEL KINETIC ENERGY,F12.3,	000143
00143	87*		X 33H FALLS BELOW MINIMUM REQUIREMENT ,F12.3)	000143
00144	88*		ICNT=ICNT+1	000143
00145	89*	20	CONTINUE	000147
00146	90*		NNRS=CLO(2)	000147
00147	91*		NNT=CLO(3)	000155
00150	92*		M4=NNT+4	000164
00151	93*		MN4=M4+NNRS	000166
00152	94*		NNNRS=CL1(2)	000170
00153	95*		NNNRS4=NNNRS+4	000177
00154	96*		T0=0.	000201
00155	97*		T1=0.	000202
00156	98*		P2=0.	000203
00157	99*		PL0=0.	000204
00160	100*		PL1=0.	000205
00161	101*		RE2=0.	000206
00161	102*	C		000206
00161	103*	C	COMPUTE ROTOR SPEED	000206
00161	104*	C		000206
00162	105*	100	OMEGA=1.E-6	000207
00163	106*		IF(KE.GT.C.)OMEGA=SQRT(KE/AK)	000211
00165	107*		RS= OMEGA*30./73.14159	000223
00166	108*		PIN=0.	000227
00166	109*	C		000227
00166	110*	C	COMPUTE POWER LOSSES AND NET POWER WHEN CHARGING	000227
00166	111*	C		000227
00167	112*		IF(P1.EQ.0.)GO TO 200	000230
00171	113*		T0=P1*737.6/OMEGA	000236
00172	114*		PL0=TBLU2(RS,T0,CLO(M4),CLO(4),CLO(MN4),1,1,-NNRS,-NNT,NNRS,NNT)	000242
00173	115*		PIN=P1-PL0	000272
00174	116*		POUT=0.	000274
00174	117*	C		000274
00175	118*		IF(PIN.GE.0.)GO TO 200	000275
00177	119*		IF(IMPL.NE.2)GO TO 200	000277
00201	120*		WRITE(6,208)PL0,P1	000302
00205	121*	208	FORMAT(1H0,21H FLYWHEEL POWER LOSS ,F12.3,	000311
00205	122*		X24H EXCEEDS CHARGING POWER ,F12.3)	000311
00206	123*		ICNT=ICNT+1	000311
00206	124*	C		000311
00206	125*	C	COMPUTE POWER LOSSES AND OUTPUT POWER WHEN DISCHARGING	000311
00206	126*	C		000311
00207	127*	200	IF(RE1.EQ.0.)GO TO 300	000315



```

00211 128*      T1=RE1*737.6/OMEGA
00212 129*      PL1=TPLU2(RS,-T1,CLO(M4),CLO(4),CLO(MN4),1,1,-NNRS,-NNT,NNRS,NNT)
00213 130*      P2=RE1-PL1
00214 131*      POUT=RE1
00215 132*      IF(P2.GT.0..OR.IMPL.NE.2)GO TO 300
00217 133*      WRITE(6,308)PL1,RE1
00223 134*      308 FORMAT(1H0,16H FLYWHEEL LOSS ,F12.3,
00223 135*      X27H EXCEEDS DISCHARGING POWER ,F12.3)
00224 136*      ICNT=ICNT+1
00225 137*      P2=0.
00225 138*      C
00225 139*      C      COMPUTE POWER LOSSES WHEN DISENGAGED
00225 140*      C
00226 141*
00226 142*
00226 143*      300 IF(P1.GT.0.)GO TO 400
00230 144*      IF(RE1.GT.0.)GO TO 400
00232 145*      POUT=TBLU1(RS,CL1(4),CL1(MNRS4),1,-NNRS)
00232 146*      C
00232 147*      C      FLYWHEEL KINETIC ENERGY BALANCE
00232 148*      C
00233 149*      400 IF((KE.NE.0)KED=PIN-POUT-C1*OMEGA-C2*(OMEGA**2.8)
00233 150*      C
00233 151*      C      MAXIMUM CHARGING POWER REQUEST
00233 152*      C
00235 153*      TM=MP1*737.6/OMEGA
00236 154*      MPA=TBLU2(RS,TM,CLO(M4),CLO(4),CLO(MN4),1,1,-NNRS,-NNT,
00236 155*      X NNRS,NNT)
00237 156*      MPO=MP1-MPA
00240 157*      IF(MPO.GT.0.)GO TO 500
00242 158*      IF(IMPL.EQ.2)WRITE(6,508)MPA,MP1
00247 159*      508 FORMAT(1H0,22H FLYWHEEL CLUTCH LOSS ,F12.3,
00247 160*      X 31H EXCEEDS MAXIMUM INPUT POWER ,F12.3)
00250 161*      IF(IMPL.EQ.2)ICNT=ICNT+1
00252 162*      GO TO 600
00253 163*      500 EFO=EF1*MPO/MP1
00254 164*      APC=AMAX1(0.,(E1-KE)/DUM(7))
00255 165*      RE2=AMIN1(MPO,RAP,APC)
00256 166*      RE2=RE2/EFO
00256 167*      C
00256 168*      C      OUTPUT EFFICIENCY AND MAXIMUM POWER
00256 169*      C
00257 170*      600 RAPT=(KE-E0)/(TINC*2.)
00260 171*      RAPT=AMIN1(RAPT,RAP)
00261 172*      RAPT=AMAX1(RAPT,RAP/1000.)
00262 173*      TM=RAPT*737.6/OMEGA
00263 174*      MPB=TBLU2(RS,-TM,CLO(M4),CLO(4),CLO(MN4),1,1,-NNRS,-NNT,
00263 175*      X NNRS,NNT)
00264 176*      MP2=RAPT-MPB
00265 177*      IF(MP2.GT.0..OR.IMPL.NE.2)GO TO 700
00267 178*      708 FORMAT(1H0,22H FLYWHEEL CLUTCH LOSS ,F12.3,
00267 179*      X27H EXCEEDS DELIVERABLE POWER ,F12.3)
00270 180*      WRITE(6,708)MPB,RAPT
00274 181*      ICNT=ICNT+1
00275 182*      700 MP2=AMAX1(MP2,RAP/1000.)
00276 183*      EF2=MP2/RAPT
00276 184*      IF(RE1.GT.0..AND.P2.GT.0.)EF2=P2/RE1

```

```

000316
000322
000357
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000606
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000620
000655
000657
000672
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000672
000701
000705
000713
000715

```

00277	185*	C	
00277	186*	C	
00277	187*	C	
00301	188*		
00302	189*		
00303	190*		
00305	191*		
00307	192*		
00307	193*		
00311	194*		
00313	195*		
00315	196*		
00315	197*	C	
00315	198*	C	
00315	199*	C	
00317	200*		
00320	201*		
00321	202*		
00322	203*		
00323	204*		
00323	205*	C	
00324	206*		
00326	207*		
00327	208*		
00327	209*	C	
00330	210*		
00330	211*		
00331	212*		

PRIORITY INTERRUPT

```

EC1=E1-EDE
ECO=E0+EDE
IF((KE.GT.ECO).AND.(INT.E0.1.))INT=0.
IF((KE.LT.EC1).AND.(INT.E0.-1.))INT=0.

IF(KE.LE.E0)INT=1.
IF(KE.GT.E1)INT=-1.
IF((KF.GT.ECO).AND.(KE.LT.EC1))INT=0.
IF(IMPL.LE.1)RETURN

```

STATISTICS

```

ME=AMAX1(ME,KE)
MPC=AMAX1(MPC,KED)
MPD=AMAX1(MPD,-KED)
SPC=SPC+TINC*P1
SPD=SPD+TINC*P2

IF(TIME.LT.TMAX)RETURN
CCI=CCI+CC
CHI=CHI+CM

```

```

RETURN
END

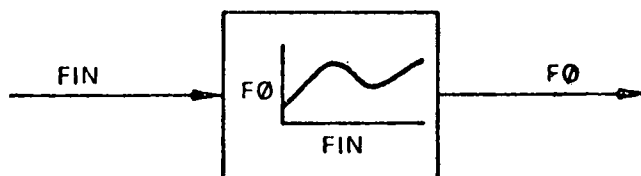
```

```

000715
000715
000715
000734
000737
000742
000760
000776
000776
001004
001012
001031
001031
001031
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001031
001046
001054
001062
001066
001066
001072
001101
001104
001104
001107
001107
001332

```

7.9 ONE DIMENSION TABLE LOOKUP



Tables

FTA

Description

Tabular values of function

Inputs

Parameter/Port

FIN

Input quantity

AN

$ABS(AN) \leq 0.5$ for equispaced interpolation
($AN < 0$ prevents extrapolation)

Outputs

Variable/Port

F0

Output quantity

Calculation Sequence

$$F0 = FTA(FIN)$$

NOTE: A maximum of 18 points is allowed in the table.

SUBROUTINE FU

ENTRY POINT 000065

STORAGE USED CODE(1) 000075; DATA(0) 000014; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 TBLU1
0004 NERR35

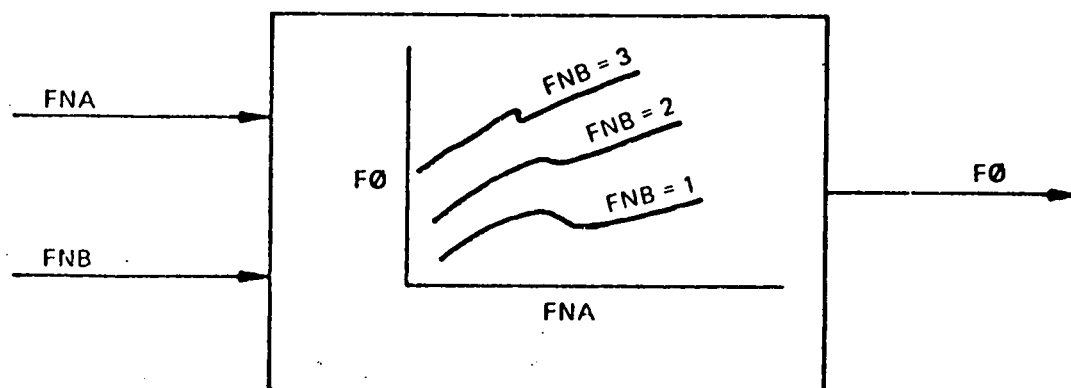
STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 000005 INJPS 0000 I 000002 N 0000 I 000000 NA 0000 I 000001 NB 0003 R 000000 TBLU1

00100	1*	CFU				000003
00101	2*		SUBROUTINE FU(FTA,FO,FIN,AN)			000003
00101	3*	C				000003
00101	4*	C	PURPOSE - TO CALCULATE OUTPUT FO AS AN ARBITRARY FUNCTION OF			000003
00101	5*	C	INPUT FIN USING TABULAR INPUT FTA GIVING FO=F(FIN)			000003
00101	6*	C				000003
00101	7*	C	METHOD - SELF EXPLANATORY			000003
00101	8*	C				000003
00101	9*	C				000003
00101	10*	C	LIMITATIONS - MAXIMUM ARRAY SIZE IS 18			000003
00101	11*	C				000003
00101	12*	C				000003
00101	13*	C	WRITTEN BY - ADAM LLOYD	LATEST REVISION	APRIL 77	000003
00101	14*	C				000003
00101	15*	C				000003
00101	16*	C	INPUT/OUTPUT LIST			000003
00101	17*	C				000003
00101	18*	C	FTA TABULAR INPUT FO=F(FIN)	ANY	INPUT TABLE	000003
00101	19*	C	FO OUTPUT	ANY	OUTPUT VAR	000003
00101	20*	C	FIN INPUT	ANY	INPUT VAR	000003
00101	21*	C	AN SET ABS(AN).GT.0.5 FOR UNEQUAL SPACED TABLE DATA---INPUT			000003
00101	22*	C	SET ABS(AN).LE.0.5 FOR EQUI-SPACED TABLE DATA			000003
00101	23*	C	A NEGATIVE VALUE OF AN WILL			000003
00101	24*	C	PREVENT EXTRAPOLATION BEYOND			000003
00101	25*	C	TABLE LIMITS			000003
00101	26*	C				000003
00103	27*		DIMENSION FTA(1)			000003
00104	28*		NA= SIGNIFTA(2),AN)			000003
00105	29*		NP=FTA(2)+4			000015
00106	30*		N=1			000026
00107	31*		IF(ABS(AN).LE.0.5) N=0			000030
00111	32*		FO=TBLU1IFIN,FTA(4),FTA(NB),N,NA)			000035
00112	33*		RETURN			000053
00113	34*		END			000074

FU

7.10 TWO DIMENSION TABLE LOOKUP



Tables

FTA

Description

Table of functional relationships (maximum number of table values = 144)

Inputs

Parameter/Port

FNA	Input quantity (primary)
FNB	Input quantity (secondary)
AN	$ABS(AN) \leq 0.5$ for equal spaced FNA data*
BN	$ABS(BN) \leq 0.5$ for equal spaced FNB data*

Outputs

Variable/Port

F0	Output quantity
----	-----------------

Calculation Sequence

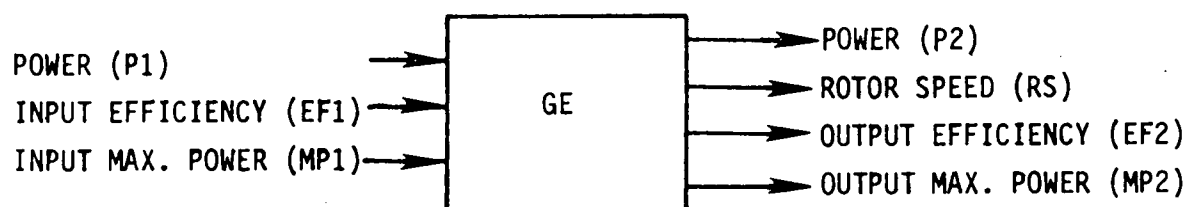
$$F0 = FTA(FNA, FNB)$$

* A negative value for AN or BN prevents extrapolation beyond the table boundaries.



00107	34*	N4=FTA(3)	000035
00110	35*	N5= SIGN(FTA(2),AN)	000044
00111	36*	N6= SIGN(FTA(3),BN)	000056
00112	37*	NAN=1	000070
00113	38*	IF (ABS(AN).LE.0.5) NAN=0	000072
00115	39*	NPN=1	000077
00116	40*	IF (ABS(BN).LE.0.5) NBN=0	000101
00120	41*	FO=TBLU2(FNA,FNB,FTA(N1),FTA(4),FTA(N2),NAN,NBN,N5,N6,N3,N4)	000114
00121	42*	RETURN	000142
00122	43*	END	000203

7.11 AC INDUCTION GENERATOR



The induction generator produces electrical power proportional to rotor slip, i.e. difference between rotor speed and synchronous speed. This relationship is used to compute rotor speed given input power and the generator parameters. Two power losses are modeled: a constant multiplicative term due to resistive heating and an additive term due to mechanical friction. Default parameters are based on a conventional squirrel-cage induction motor/generator machine. This component can also be used as a synchronous generator with $RAS \leq .01$.

Basic Equations

Output power P2 and rotor speed RS are computed from the following equations:

$$P2 = EE * (P1 - C * RS^2)$$

$$\frac{P2}{RAP} = \frac{(RS/RSY - 1)}{RAS} \quad (\text{Power is proportional to slip})$$

where EE = electrical efficiency

C = constant of conversion

Inputs

<u>Parameter/Port</u>		<u>Description</u>	<u>Units</u>
P	1	Input power	kw
RAP		Rated output power	kw
RSY		Synchronous rotor speed (D = 1800)	rpm
RAS		Rated power slip (D = 0.05)	-
DA		Mechanical damping (D = 0.0)	joule-sec
SR		Internal stator resistance (D = 6.4/RAP)	ohms
V0		Rated bus voltage (D = 400)	volts
EF	1	Input product efficiency	-
MP	1	Maximum input discharge rate (D = 1×10^8)	kw
CC		Capital cost/year	\$
CM		Maintenance cost/year	\$

Outputs

<u>Variable/Port</u>			
P	2	Output power	kw
EE		Electrical efficiency	-
RS		Rotor speed	rpm
PL		Power loss	kw
EF	2	Output product efficiency	-
MP	2	Maximum output discharge rate	kw

Statistics

MPN	Maximum output power/rated power	kw
SP	Total output energy	kwh

D - Default values supplied.

Calculation Sequence

- 1) First pass only

$$EFF = 1$$

$$I_{RAT} = RAP * 1000 / V_0$$

$$EE = \frac{RAP}{RAP + SR * I_{RAT}^2 / 1000}$$

- 2) If $P_1 = 0$ set $P_2 = 0$, $RS = RSY$ and go to 4)

Compute rotor speed ω in rad/sec using

$$\frac{EE(P_1 * 1000 - \omega^2 * DA)}{RAP * 1000} = \frac{(\omega / \omega_0 - 1)}{RAS}$$

$$\text{with } \omega_0 = RSY * (2\pi / 60)$$

- 3) Compute RS and output power

$$RS = \omega * (60 / 2\pi)$$

$$P_2 = RAP(RS / RSY - 1) / RAS$$

$$P_2 > RAP \Rightarrow \text{DIAGNOSTIC}$$

$$EFF = P_2 / P_1$$

- 4) Compute loss, efficiency terms

$$PL = P_1 - P_2$$

$$EF2 = EF1 * EFF$$

- 5) Compute maximum output rate

$$MP2 = \text{MIN}(RAP, MP1 * EFF)$$

- 6) Compute Statistics and Costs

SUBROUTINE GE ENTRY POINT 000253

STORAGE USED CODE(1) 000363; DATA(0) 000043; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000002
0004 CTIME 000001
0005 COST 000004
0006 CSIMUL 000010

EXTERNAL REFERENCES (BLOCK, NAME)

0007 NWDUS
0010 NI029
0011 NERR39

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000064 10L	0000 000005 100F	0001 000074 20L	0001 000172 30L	0000 R 000003 A
0000 R 000004 B	0005 R 000000 CC	0005 P 000001 CM	0005 000003 CV	0005 CC0002 CO
0006 000000 DUM	0000 R 000000 EFF	0003 I 000001 ICNT	0003 I 000000 IMPL	0000 000032 INJPS
0000 R 000002 RATI	0004 R 000000 TIME	0006 R 000006 TINC	0006 R 000007 TMAX	0000 R 000001 TMAX1

00100	1*	C6E		000000
00101	2*		SUBROUTINE GE(P2,EE,RS,PL,EF2,PM2,PMN,SP,P1,RAP,RSY,RAS,DA,SR,VO,	000000
00101	3*		1 EF1,PM1,CCI,CHI)	000000
00101	4*	C		000000
00101	5*	C	PURPOSE MODEL AC INDUCTION GENERATOR	000000
00101	6*	C		000000
00101	7*	C	METHOD MECHANICAL AND ELECTRICAL EFFICIENCIES ARE USED TO COMPUTE	000000
00101	8*	C	OUTPUT POWER. ROTOR SPEED IS COMPUTED ASSUMING POWER IS	000000
00101	9*	C	PROPORTIONAL TO SLIP.	000000
00101	10*	C		000000
00101	11*	C	WRITTEN BY A.W. WARREN	000000
00101	12*	C		000000
00101	13*	C	CALL SEQUENCE	000000
00101	14*	C	OUTPUTS	000000
00101	15*	C	P2 - OUTPUT POWER, KW	000000
00101	16*	C	EE - ELECTRICAL EFFICIENCY	000000
00101	17*	C	RS - ROTOR SPEED, RPM	000000
00101	18*	C	PL - POWER LOSS, KW	000000
00101	19*	C	EF2 - OUTPUT PRODUCT EFFICIENCY	000000
00101	20*	C	PM2 - MAXIMUM OUTPUT POWER, KW	000000
00101	21*	C	PMN - MAX. OBSERVED OUTPUT POWER / RATED POWER	000000
00101	22*	C	SP - TOTAL OUTPUT ENERGY, KWH	000000
00101	23*	C		000000

VERSION 1, MARCH 16 1977

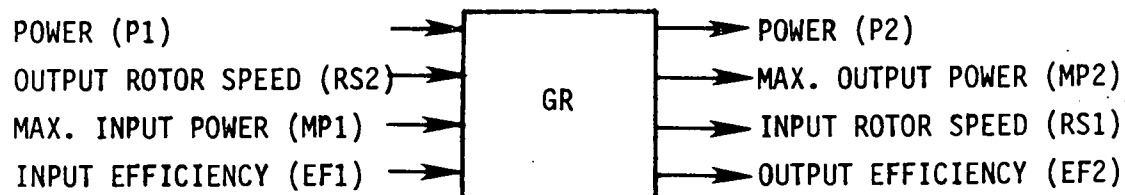
GF

[illegible]

CO160	81*	C		COST SUMMATION
00161	82*		IF(TIME.LT.TMAX1) RETURN	
CO163	83*		CC = CC + CCI	
00164	84*		CM = CM + CHI	
00164	85*	C		
SD165	86*		RETURN	
00166	87*		END	

000221
000226
000235
000240
000240
000243
000362

7.12 FIXED RATIO TRANSMISSION



This component models a fixed gear ratio transmission. Power losses are modeled by a table lookup depending on input power. Rotor input speed is used as a feedback variable.

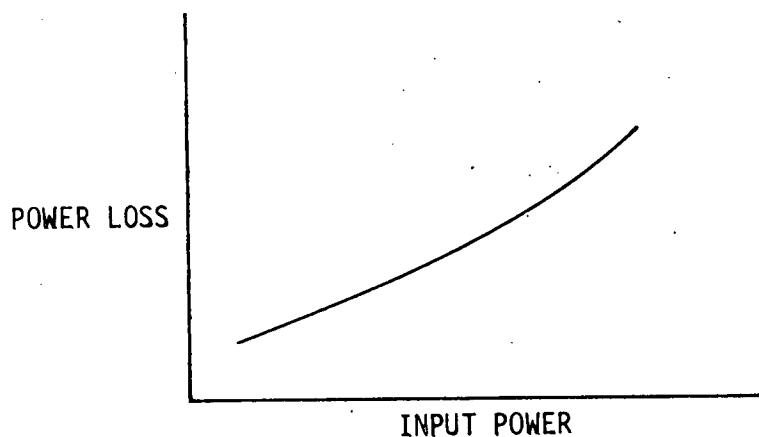


FIGURE 7.12: FIXED GEAR POWER LOSS

<u>Tables</u>	<u>Description</u>	<u>Units</u>
PLØ	Power loss versus input power	kw

Inputs

Parameter/Port

GR		Gear ratio	-
RS	2	Output rotor speed	rpm
P	1	Input power	kw
EF	1	Input product efficiency	-
MP	1	Maximum input power (Default = 1×10^8)	kw
CC		Capital cost/year	\$
CM		Maintenance cost/year	\$

Outputs

Variable/Port

P	2	Output power	kw
TØ		Output torque	ft-lb
PL		Power loss	kw
EF	2	Output product efficiency	-
MP	2	Maximum output power	kw
RS	1	Input rotor speed	rpm

Calculation Sequence

1) $MP2 = MP1 - PL0(MP1)$ (First Pass Only)

If $P1 \leq 0$, set $PL = P2 = 0$ and go to 2)

$$PL = PL0(P1)$$

$$P2 = P1 - PL$$

$$RS1 = RS2/GR$$

$$EF2 = EF1 * P2 / P1$$

2) $T0 = P2 * 737.6 / (RS2 * 2 \pi / 60)$

3) Compute Costs

SUBROUTINE GR ENTRY POINT 00G157

STORAGE USED CODE(1) 000237; DATA(0) 000023; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000001
0004 CTIME 000001
0005 COST 000004
0006 CSIMUL 000010

EXTERNAL REFERENCES (BLOCK, NAME)

0007 TBLU1
0010 NEPR3s

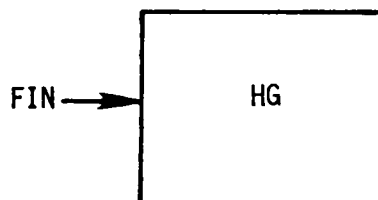
STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000057	10L	0001	000113	20L	0005 R	000000	CC	0005 R	000001	CM	0005	000002	CO
0005	000003	CV	0006	000000	DUM	0003 I	000000	IMPL	0000	000007	INJPS	0000	I	000000
0007 R	000000	TBLU1	0004 R	000000	TIME	0006 R	000007	THAX	0000 R	000001	THAX1			

00100	1*	CGR		000000
00101	2*		SUBROUTINE GR(PLO,P2,TO,PL,EF2,PM2,RS1,GRA,RS2,P1,EF1,PH1,CCI,CHI)	000000
00101	3*	C		000000
00101	4*	C	PURPOSE MODEL A FIXED GEAR RATIO TRANSMISSION	000000
00101	5*	C		000000
00101	6*	C	METHOD POWER LOSSES ARE INPUT AS A FUNCTION OF INPUT POWER P1.	000000
00101	7*	C		000000
00101	8*	C	WRITTEN BY A.W. WARREN	000000
00101	9*	C	VERSION 1, MARCH 16 1977	000000
00101	10*	C	CALL SEQUENCE	000000
00101	11*	C	TABLES	000000
00101	12*	C	PLO - POWER LOSS IN KW VERSUS INPUT POWER IN KW	000000
00101	13*	C		000000
00101	14*	C	OUTPUTS	000000
00101	15*	C	P2 - OUTPUT POWER, KW	000000
00101	16*	C	TO - OUTPUT TORQUE, FT-LB	000000
00101	17*	C	PL - POWER LOSS, KW	000000
00101	18*	C	EF2 - OUTPUT PRODUCT EFFICIENCY	000000
00101	19*	C	PM2 - MAXIMUM OUTPUT POWER, KW	000000
00101	20*	C	RS1 - INPUT ROTOR SPEED, RPM	000000
00101	21*	C		000000
00101	22*	C	INPUTS	000000
00101	23*	C	GRA - GEAR RATIO	000000
00101	24*	C	RS2 - OUTPUT ROTOR SPEED, RPM	000000
00101	25*	C	P1 - INPUT POWER, KW	000000

00101	26*	C	EF1 - INPUT PRODUCT EFFICIENCY	000000
00101	27*	C	PM1 - MAXIMUM INPUT POWER, KW	000000
00101	28*	C	CCI - CAPITAL COST / YEAR, \$	000000
00101	29*	C	CMI - MAINTENANCE COST / YEAR, \$	000000
00101	30*	C		000000
00103	31*		DIMENSION PLO(1)	000000
00104	32*		COMMON /CIMPL/IMPL /CTIME/ TIME	000000
00105	33*		COMMON /COST/CC,CM,CO,CV /CSIMUL/ DUM(7),TMAX	000000
00105	34*	C		000000
00105	35*	C	INITIALIZATION	000000
00105	36*	C		000000
00106	37*		NP = PLO(2)	000000
00107	38*		IF(IMPL.GT.0) GO TO 10	000000
00111	39*		EF2= 1.	000007
00112	40*		TMAX1 = .99999*TMAX	000012
00113	41*		RS2=1.	000014
00114	42*		IF(PM1.EQ. .99999) PM1=1.E10	000021
00116	43*		PM2 = PM1	000023
00117	44*		IF(PM1.LE. PLO(3+NP)) PM2 = PM1-TBLU1(PM1,PLO(4),PLO(4+NP),1,-NP)	000030
00117	45*	C		000032
00117	46*	C	POWER LOSS AND ROTOR SPEED CALCULATIONS	000032
00121	47*		10 PL=0.	000057
00122	48*		P2=0.	000057
00123	49*		IF(P1 .EQ. 0.) GO TO 20	000060
00125	50*		PL = TBLU1(P1,PLO(4),PLO(4+NP),1,-NP)	000062
00126	51*		P2 = P1 - PL	000102
00127	52*		EF2 = EF1*P2/ P1	000104
00130	53*		RS1 = RS2/6PA	000107
00131	54*		20 IF(RS2 .GT. 0.) TO = P2*7043./RS2	000113
00131	55*	C		000113
00131	56*	C	COST SUMMATION	000113
00133	57*		IF(IMPL.LE.1) RETURN	000121
00135	58*		IF(TIME.LE.TMAX1) RETURN	000130
00137	59*		CC = CC + CCI	000137
00140	60*		CM = CM + CMI	000142
00141	61*		RETURN	000145
00142	62*		END	000236

7.13 HISTOGRAM



The input quantity is monitored during a SIMULATE analysis. When time reaches TMAX a plotted histogram is produced with 16 intervals that span the range from FLO to FUP.

Inputs

<u>Variable/Port</u>	<u>Description</u>
FIN	Input quantity to be monitored
FUP	Upper limit for histogram
FLO	Lower limit for histogram
F1,...F16 ¹	Array containing histogram data
FA ¹	Measurement interval

Outputs

<u>Variable/Port</u>	
AV	Mean value (running sum during simulation)
SD	Standard deviation (running sum squared)
SAM	Number of samples

¹ These quantities do not require data input values.

SUBROUTINE HG

ENTRY POINT 000430

STORAGE USED CODE(1) 000506; DATA(0) 000166; BLANK COMMON(2) 012174

COMMON BLOCKS

0003 CTIME 000001
 0004 CSIMUL 000010
 0005 COVRLY 000004
 0006 CIMPL 000001

EXTERNAL REFERENCES (BLOCK, NAME)

0007 SORT
 0010 NMDUS
 0011 NI035
 0012 NI025
 0013 NI015
 0014 NLRR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000023	100L	0000	000052	100CF	0000	000056	1100F	0001	000012	120G	0000	000062	1200F
0000	000067	1300F	0001	000034	134G	0000	000073	140CF	0001	000111	154G	0001	000154	166G
0001	000175	177G	0001	000203	205G	0001	000211	213G	0001	000216	220G	0001	000223	225G
0001	000224	230G	0001	000234	236G	0001	000257	242G	0001	000272	246G	0001	000306	255G
0001	000314	262G	0001	000053	300L	0001	000364	303G	0001	000364	305G	0000	000047	900F
0000 R	000010	AX1	0000 R	000030	BLANK	0005	000003	CPUSEC	0004	000000	DUM	0005	000000	DUMH
0000 R	000036	FAX	0002 R	000000	GRAPH	0000 R	000032	HORIZ	0000 R	000041	HX	0000 I	000034	I
0000 I	000043	IC	0006 I	000000	IMPL	0000	000135	INJP5	0000 I	000037	ISAMP	0000 I	000042	J
0000 I	000044	J1	0000 I	000045	J2	0000 I	000046	J3	0000 I	000035	L	0000 R	000033	POINT
0000 R	000000	T01	0003 R	000000	TIME	0004 R	000007	TMAX	0000 R	000031	VERT	0000 R	000040	XMAX

00100 1* CHG
 00101 2* SUBROUTINE HG(SAMP,AV,SD,F1,F2,F3,F4,F5,F6,F7,F8,F9,F10,F11,
 00101 3* 1 F12,F13,F14,F15,F16,FA,FIN,FUP,FLO)
 00101 4* C VERSION 2. REVISED MARCH 1977
 00101 5* C PURPOSE - DEVELOP A RUNNING HISTOGRAM OF AN INPUT SEQUENCE
 00101 6* C CALL SEQUENCE
 00101 7* C SAMP- OUTPUT NUMBER OF SAMPLES
 00101 8* C AV - OUTPUT AVERAGE (RUNNING SUM)
 00101 9* C SD - OUTPUT STANDARD DEVIATION (RUNNING SUM SQUARED)
 00101 10* C F1-F16 - ARRAY WITH NUMBER OF OCCURENCES IN EACH INTERVAL
 00101 11* C FA - OUTPUT CONTAINING MEASUREMENT INTERVAL
 00101 12* C FUP - INPUT SPECIFYING UPPER MEASUREMENT LIMIT
 00101 13* C FLO - INPUT SPECIFYING LOWER MEASUREMENT LIMIT
 00101 14* C FIN - INPUT MEASUREMENT

000003
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HG

00103	15*	DIMENSION F1(16),TD1(8),AX1(16)	000003
00104	16*	DIMENSION GRAPH(114,46)	000003
00105	17*	COMMON GRAPH	000003
00106	18*	COMMON/CTIME/TIME/CSIMUL/DUM(7),TMAX	000003
00107	19*	COMMON/COVRLY/DUM(13),CPUSEC /CIMPL/IMPL	000003
00110	20*	DATA PLANK,VERT,HORIZ,POINT/1H ,1H1,1H-,1H*/	000003
00115	21*	IF(IMPL.GT.0) GO TO 100	000003
00117	22*	DO 50 I=1,16	000012
00122	23*	50 F1(I)=0.	000012
00124	24*	FA=(FUP-FLO)/14.	000013
00125	25*	SD=0.	000017
00126	26*	AV =0.0	000020
00127	27*	SAMP=0.0	000021
00130	28*	100 CONTINUE	000023
00131	29*	IF(IMPL.LT.2) RETURN	000023
00133	30*	DO 200 I=1,16	000034
00136	31*	L=1	000034
00137	32*	FAX=FLO+(I-1)*FA	000036
00140	33*	IF(FIN.LE.FAX) GO TO 300	000045
00142	34*	200 CONTINUE	000053
00144	35*	300 F1(L)=F1(L)+1.	000057
00145	36*	SAMP=SAMP+1.	000062
00146	37*	AV=AV+FIN	000065
00147	38*	SD=SD+FIN*FIN	000071
00150	39*	IF(TIME.LT.TMAX+.99999)RETURN	000104
00152	40*	SAMP=0.	000111
00153	41*	DO 350 I=1,16	000111
00156	42*	350 SAMP=SAMP+F1(I)	000114
00160	43*	ISAMP=SAMP	000123
00161	44*	ISAMP=MAX(1,ISAMP)	000130
00162	45*	AV=AV/ISAMP	000135
00163	46*	SD=SD/ISAMP	000147
00164	47*	SD=SD/ISAMP-AV*AV	000154
00165	48*	XMAX=F1(1)	000154
00170	49*	DO 360 I=1,16	000163
00173	50*	360 IF(F1(I).GE.XMAX) XMAX=F1(I)	000175
00175	51*	IF(XMAX.EQ.0.) XMAX=10.	000175
00176	52*	HX=XMAX/44.	000176
00201	53*	DO 370 I=1,46	000203
00202	54*	GRAPH(I,1)=VERT	000204
00204	55*	370 GRAPH(114,I)=VERT	000211
00207	56*	DO 380 I=2,113	000211
00210	57*	GRAPH(I,1)=HORIZ	000216
00212	58*	380 GRAPH(I,46)=HORIZ	000216
00215	59*	DO 400 I=5,103,14	000224
00217	60*	400 GRAPH(I,46)=VERT	000224
00222	61*	DO 450 I=8,106,7	000224
00224	62*	450 GRAPH(I,1)=VERT	000234
00227	63*	DO 500 I=2,45	000240
00232	64*	DO 500 J=2,113	000252
00235	65*	500 GRAPH(J,I)=PLANK	000257
00240	66*	DO 600 IC=1,16	000263
00241	67*	J=IFIX(45.5-F1(IC)/HX)	000272
00244	68*	DO 600 J1=1,7	000272
00245	69*	J2=(IC-1)*7+J1+1	
00250	70*	DO 600 J3=J,45	
00250	71*	600 GRAPH(J2,J3)=POINT	

HC

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00254      72*      DO 700 I=1,16
00257      73*
00257      74*      700 AX1(I)=F1(I)/ISAMP
00261      75*      DO 800 I=1,8
00264      76*
00264      77*      800 TD1(I)=FLO+(I-1)*2.*FA-FA/2.
00266      78*
00266      79*      WRITE(6,900)(GRAPH(I,1),I=1,114)
00271      80*      900 FORMAT(1H1,9X,114A1/)
00272      81*      WRITE(6,1000)(AX1(I),I=1,16)
00275      82*      1000 FORMAT(1H+,9X,1H1,16F7.5,1H1/)
00276      83*      WRITE(6,1100)
00300      84*      1100 FORMAT(1H+,9X,1H1,112X,1H1/)
00301      85*      WRITE(6,1200)((GRAPH(I,J),I=1,114),J=2,46)
00312      86*      1200 FORMAT(1H+,9X,114A1/45(10X,114A1/))
00313      87*      WRITE(6,1300)(TD1(I),I=1,8)
00316      88*      1300 FORMAT(1H+,9X,8(F13.5,1X)///)
00317      89*      WRITE(6,1400) ISAMP,AV,SD
00324      90*      1400 FORMAT(1H+,10X,14HHISTOGRAM FOR ,I7,8H SAMPLES,
00324      91*      19H MEAN= ,F13.5,18H STANDARD DEV.= ,F13.5/)
00325      92*      RETURN
00326      93*      END

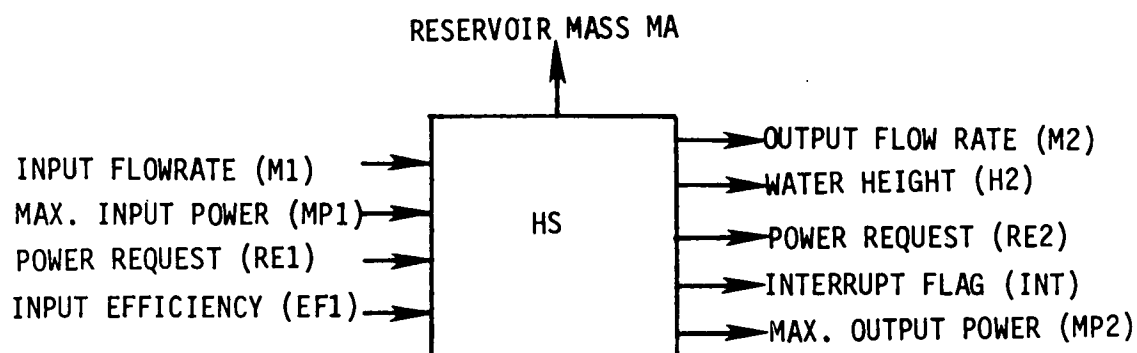
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7.14 HYDRO STORAGE VESSEL



The hydro storage vessel is modeled as an above ground reservoir with a large and constant surface area. The change in reservoir height between maximum and minimum levels is assumed small in comparison to the height of the water above the turbine. Hence, reservoir height is assumed constant. The reservoir has specified evaporation and leakage rates. Average input flow gained by rainfall is also specified. Energy storage is calculated based on the potential energy of the water in the reservoir relative to the turbine inlet.

Basic Equation

$$MA = M1 - M2 - NE*AS - NL + MDR*AS/14052$$

Inputs

<u>Parameter/Port</u>		<u>Description</u>	<u>Units</u>
M	1	Input water mass flow rate	gal/h
NE		Evaporation coefficient (D = 0.03)	gal/ft ² -h
AS		Reservoir surface area	ft ²
NL		Leakage coefficient (D = 8.0)	gal/h
MDR		Rainfall rate	inches/year
MDM		Maximum allowable mass flow rate (D = 4X10 ⁵)	gal/h
MM		Maximum allowable reservoir capacity (D=5X10 ⁶)	gal
M0		Minimum allowable reservoir capacity	gal
H	1	Reservoir height above turbine	ft
MDE		Reservoir deadband for priority resequence	gal
RE	1	Power request (discharge)	kw
CR		Reservoir cost coefficient (D = 0.025)	\$/gal
EF	1	Input product efficiency	-
MP	1	Maximum input charging rate	kw
LE		Reservoir life expectancy	years
CM		Maintenance cost/year	\$

Outputs

<u>Variable/Port</u>			
M	2	Outlet water mass flow rate	gal/hr
E		Energy stored	kwh
H	2	Reservoir height above turbine (=H1)	ft
MA		Reservoir mass (state)	gal
CC0		Reservoir cost/year	\$
MP	2	Maximum discharge rate allowable	kw
INT		Priority interrupt flag	-
RE	2	Maximum charging rate request	kw

D - Default values supplied

<u>Statistics</u>	<u>Description</u>	<u>Units</u>
MDU	Maximum mass flow rate	gal/hr
MU	Maximum reservoir mass	gal
ML	Minimum reservoir mass	gal

The calculation sequence and default values assume a pond sized for 120kw storage for 24 hours (5×10^6 gallons of water 200 ft. above turbine inlet). The evaporation coefficient NE assures the pond drops $\frac{1}{2}$ " in height per 10 hours. To obtain a more accurate value for this parameter requires knowledge of local conditions. The leakage coefficient NL is based on the assumption of a loss of 0.1% of the maximum reservoir capacity in the rated storage time of 24 hours. The reservoir cost estimates are based on the compensation reservoir given in Reference 1.

-
1. "Preliminary Feasibility Evaluation of Compressed Air Storage Power Systems," United Technologies AER 74-00242, December 1976.

Calculation Sequence

$$C1 = \text{conversion constant} = 0.377 \times 10^{-6} \frac{\text{kwh}}{\text{ft-lb}}$$

$$C2 = \text{conversion constant} = 8.3398 \text{ lb/gal}$$

$$A = C1 * C2 * H1$$

1) Reservoir cost

$$CC = CR * MM / LE$$

2) Volume of water discharged

$$M2 = RE1 / A$$

3) Reservoir water volume

$$MA = M1 - M2 - NE * AS - NL + (MDR * AS / 14052.)$$

4) Energy stored

$$E = A * M$$

5) Checks

$$M1 > MDM \text{ or } M2 > MDM \Rightarrow \text{DIAGNOSTIC}$$

$$M > MM, \Rightarrow \text{DIAGNOSTIC}$$

$$M < M0 \Rightarrow \text{DIAGNOSTIC}$$

6) Priority interrupt

$$\text{If } M \leq M0, \text{ INT} = 1$$

$$\text{IF } M > M0 + MDE \text{ and } \text{INT} = 1, \text{ INT} = 0$$

$$\text{If } M \geq MM, \text{ INT} = -1$$

$$\text{If } M < MM - DME \text{ and } \text{INT} = -1, \text{ INT} = 0$$

Calculation Sequence Cont.

7) Maximum charging rate request

$$MD1 = \text{MIN} (MDM, (MM-M)/TINC)$$

$$RE2 = \text{MIN} (MP1, MD1*A)/EF1$$

Maximum discharge rate

$$MP2 = A * \text{MIN} (MDM, (M-MD)/TINC)$$

where TINC = integration step size in hrs

8) Compute Statistics and Costs

ENTRY POINT 000405

COMMON BLOCKS

```
0003      CEMPL      000002
0004      CTIME      000001
0005      CSIMUL      000010
0006      COST        000002
```

0007	WINDUS
0010	N1025
0011	NEBR35

0001	G0C055	100L	0000	000005	1010F	0000	000030	1020F	0000	000045	1030F	0001	000144	200L
0001	C0C171	300L	0001	000215	403L	0000 R	000004	A	0006 R	000000	CCI	0006 R	000001	CM1
0000 R	G0C003	C1	0005 R	000000	DUM	0003 I	000001	ICNT	0003 I	000000	IMPL	0000	000076	INJPs
0000 R	000001	MDM1	0000 R	000000	MD1	0004 R	000000	TIME	0005 R	000007	THAX	0000 R	000002	THAX1

```

C0100      1*      CHS
C0101      2*      SUBROUTINE HS(M,DM,IM,M2,E,H2,CC,MP2,INT,RE2,MDU,MU,HL,M1,NE
C0101      3*      1      ,AS,NL,MDR,MDM,MH,MO,M1,MDE,RE1,CR,EF1,MP1,LE,CH)
C0101      4*      C
C0101      5*      C      PURPOSE      PERFORMANCE OF A LARGE RESERVOIR AS AN ENERGY STORAGE
C0101      6*      C
C0101      7*      C      DEVICE.
C0101      8*      C
C0101      9*      C      METHOD      ENERGY IN STORAGE IS CALCULATED FROM THE POTENTIAL
C0101     10*      C
C0101     11*      C      BETWEEN THE RESERVOIR AND THE TURBINE INLET.
C0101     12*      C
C0101     13*      C      WRITTEN BY F. O. MAHONY      VERSION 1, MARCH 30 1977
C0101     14*      C
C0101     15*      C      CALL SEQUENCE
C0101     16*      C      OUTPUTS
C0101     17*      C      M      - RESERVOIR MASS (STATE VARIABLE), GAL
C0101     18*      C      DM     - RESERVOIR MASS FLOWRATE, GAL/HR
C0101     19*      C      IM     - STATUS INDICATOR
C0101     20*      C      M2     - OUTLET WATER MASS FLOW RATE, GAL/HR
C0101     21*      C      E      - ENERGY STORED, KWH
C0101     22*      C      H2     - RESERVOIR HEIGHT ABOVE TURBINE (=H1), FT
C0101     23*      C      CC     - RESERVOIR COST/YEAR, $

```

[illegible]

00101	24*	C	MP2 - MAXIMUM DISCHARGE RATE ALLOWABLE, KW	000000
00101	25*	C	INT - PRIORITY INTERRUPT FLAG	000000
00101	26*	C	RE2 - MAXIMUM CHARGING RATE REQUEST, KW	000000
00101	27*	C	MDU - MAXIMUM MASS FLOW RATE, GAL/HR	000000
00101	28*	C	MU - MAXIMUM RESERVOIR MASS, GAL	000000
00101	29*	C	ML - MINIMUM RESERVOIR MASS, GAL	000000
00101	30*	C		000000
00101	31*	C	INPUTS	000000
00101	32*	C	M1 - INPUT WATER MASS FLOW RATE, GAL/HR	000000
00101	33*	C	NE - EVAPORATION COEFFICIENT, GAL/FT**2-HR	000000
00101	34*	C	AS - RESERVOIR SURFACE AREA, FT**2	000000
00101	35*	C	NL - LEAKAGE COEFFICIENT	000000
00101	36*	C	MDR - RAINFALL RATE, INCHES/YEAR	000000
00101	37*	C	MDM - MAXIMUM ALLOWABLE MASS FLOW RATE, GAL/HR	000000
00101	38*	C	MM - MAXIMUM ALLOWABLE RESERVOIR CAPACITY, GAL	000000
00101	39*	C	MO - MINIMUM ALLOWABLE RESERVOIR CAPACITY, GAL	000000
00101	40*	C	H1 - RESERVOIR HEIGHT ABOVE TURBINE, FT	000000
00101	41*	C	MDE - RESERVOIR DEADEND FOR PRIORITY RESEQUENCE, GAL	000000
00101	42*	C	RE1 - POWER REQUEST (DISCHARGE), KW	000000
00101	43*	C	CR - RESERVOIR COST COEFFICIENT	000000
00101	44*	C	EF1 - INPUT PRODUCT EFFICIENCY	000000
00101	45*	C	MP1 - MAXIMUM INPUT CHARGING RATE, KW	000000
00101	46*	C	LE - RESERVOIR LIFE EXPECTANCY, YEARS	000000
00101	47*	C	CM - MAINTENANCE COST/YEAR, \$	000000
00101	48*	C		000000
00103	49*		COMMON/CIMPL/INPL,ICNT/CTIME/TIME/CSIMUL/DUM(7),TMAX	000000
00104	50*		COMMON/COST/CCI,CHI	000000
00105	51*		REAL M2,MP2,MDU,MU,ML,M1,NE,NL,MDR,MDM,MM,MO,MDE,MP1,LE,INT,M	000000
00106	52*		REAL MD1,MDM1	000000
00106	53*	C		000000
00107	54*		IF(IMPL.GT.C)GO TO 100	000000
00107	55*	C		000000
00111	56*		RF1=0.0	000000
00112	57*		M2=M1	000000
00113	58*		TMAX1=TMAX*0.999999	000000
00114	59*		C1 = 3.1441E-6	000010
00114	60*	C		000010
00115	61*		INT=0.0	000012
00116	62*		MDU=0.0	000013
00117	63*		MU =0.0	000014
00120	64*		ML =1.0E10	000015
00121	65*		IF(NE .EQ. .99999)NE =0.03	000017
00123	66*		IF(NL .EQ. .99999)NL =8.0	000024
00125	67*		IF(MDM.EQ. .99999)MDM=4.0E5	000031
00127	68*		IF(MM .EQ. .99999)MM =5.0E6	000036
00131	69*		IF(CR .EQ. .99999)CR =0.025	000043
00131	70*	C		000043
00131	71*	C		000043
00131	72*	C	RESERVOIR COST	000043
00131	73*	C		000043
00133	74*		CC =CR*MM/LE	000050
00133	75*	C		000050
00133	76*	C	VOLUME OF WATER DISCHARGED	000050
00133	77*	C		000050
00134	78*		100 A=C1*M1	000055
0013	79*		M2 =RE1/A	000057
0013	80*	C		000057

H₂

```

00135      81*      C      RESERVOIR MASS FLOW RATE      G00057
00135      82*      C      IF (IM.NE.O) DM=M1-M2-NE*AS-NL+MDR*AS/14052.0      G00057
00136      83*      C      IF (IM.NE.O) DM=M1-M2-NE*AS-NL+MDR*AS/14052.0      G00062
00136      84*      C      ENERGY STORED      G00062
00136      85*      C      E =A*M      G00062
00136      86*      C      MDM1=MDM/.9999      G00077
00140      87*      C      IF (M1.LT.MDM1.AND.      G00077
00140      88*      C      1 M2.LT.MDM1) GO TO 200      G00102
00141      89*      C      IF (IMPL.EQ.2) WRITE (6,1010) M1,M2,MDM      G00105
00142      90*      C      IF (IMPL.EQ.2) ICNT=ICNT+1      G00105
00142      91*      C      200 IF (M .LT. MM+MDE) GO TO 300      G00105
00142      92*      C      IF (IMPL.EQ.2) WRITE (6,1020) M,MM      G00122
00144      93*      C      IF (IMPL.EQ.2) ICNT=ICNT+1      G00135
00152      94*      C      300 IF (M .GT. MO) GO TO 400      G00135
00152      95*      C      IF (IMPL.EQ.2) WRITE (6,1030) M,MO      G00144
00154      96*      C      IF (IMPL.EQ.2) ICNT=ICNT+1      G00144
00154      97*      C      400 IF (M .LE. MO) INT=1.0      G00150
00156      98*      C      IF (M .GT. (MO+MDE).AND.      G00162
00163      99*      C      1 INT.EQ.1.0) INT=0.0      G00162
00163      100*      C      IF (M .GT. MM) INT=-1.0      G00171
00165      101*      C      IF (M .LT. (MM-MDE).AND.      G00171
00165      102*      C      1 INT.EQ.-1.0) INT=0.0      G00174
00167      103*      C      PRIORITY INTERRUPT      G00206
00174      104*      C      400 IF (M .LE. MO) INT=1.0      G00206
00174      105*      C      IF (M .GT. (MO+MDE).AND.      G00206
00174      106*      C      1 INT.EQ.1.0) INT=0.0      G00206
00174      107*      C      IF (M .GT. MM) INT=-1.0      G00206
00176      108*      C      1 INT.EQ.-1.0) INT=0.0      G00215
00176      109*      C      MAXIMUM CHARGE RATE REQUEST AND DISCHARGE RATE      G00222
00200      110*      C      MD1=AMIN1(MDM,AMAX1(0.,(MM-M)/DUM(7)))      G00222
00200      111*      C      RE2=AMIN1(MP1,MD1*A)/EF1      G00241
00202      112*      C      MP2=AMIN1(MDM,AMAX1(0.,(M-MO)/DUM(7))) *A      G00247
00204      113*      C      IF (IMPL.LE.1) RETURN      G00247
00204      114*      C      STATISTICS      G00247
00204      115*      C      MDU=AMAX1(DM,MDU)      G00266
00204      116*      C      MU =AMAX1(M ,MU )      G00302
00206      117*      C      ML =AMIN1(M ,ML )      G00311
00207      118*      C      IF (IMPL.LE.1) RETURN      G00311
00210      119*      C      STATISTICS      G00326
00211      120*      C      MDU=AMAX1(DM,MDU)      G00326
00211      121*      C      MU =AMAX1(M ,MU )      G00335
00211      122*      C      ML =AMIN1(M ,ML )      G00343
00213      123*      C      IF (TIME.LT.TMAX1) RETURN      G00351
00216      124*      C      CCI=CCI+CC      G00351
00216      125*      C      CMI=CMI+CM      G00357
00220      126*      C      RETURN      G00366
00220      127*      C      1010 FORMAT(1H0,23HHS INLET MASS FLOW RATE,F12.3, 5H OR ,      G00371
00221      128*      C      1 21HOUTLET MASS FLOW RATE,F12.3,      G00371
00221      129*      C      G00374
00222      130*      C      G00374
00222      131*      C      G00550
00223      132*      C      G00550
00223      133*      C      G00550
00223      134*      C      G00550
00223      135*      C      G00550
00223      136*      C      G00550
00223      137*      C      G00550

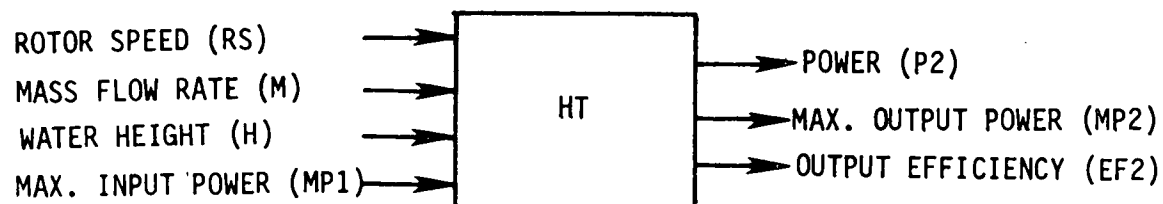
```

HS


```
00223 138*      2      26H  IS GREATER THAN MAXIMUM,F12.3)
00224 139*    1020 FORMAT(1H0,19HMS RESERVOIR VOLUME,F12.3,
00224 140*      1      30H  EXCEEDED MAXIMUM ALLOWABLE,F12.3)
00225 141*    1030 FORMAT(1H0,19HMS RESERVOIR VOLUME,F12.3,
00225 142*      1      24H  DROPEO BELOW MINIMUM,F12.3)
00225 143*  C
00226 144*      END
```

```
000550
C00550
000550
000550
000550
C00550
C00550
```

7.15 HYDRAULIC TURBINE



The hydraulic turbine model is based on a constant speed design and is typical of a reaction/Francis type turbine. The turbine is assumed to be designed to a specified operating point and output power.

For off design performance the pump efficiency is assumed to be functionally related to the first power of the mass flow rate. The equations are assumed to be valid over a specified range of values for the turbine parameter.

Basic Equations

$$P = \text{EFF} * M * C1 * C2 * H$$

$$\text{EFF} = 1 - (1 - \text{EFD}) * \text{WD} / M$$

where C1, C2 are conversion constants.

Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
M	Inlet mass flow rate	gal/h
H	Height of reservoir above turbine inlet	ft
EFD	Design pt. turbine efficiency (D = 0.90)	-
MD	Design pt. mass flow rate (D = 2×10^5)	gal/h
MM	Maximum mass flow rate (D = 3×10^5)	gal/h
EF	1 Input product efficiency	-
MP	1 Input maximum discharge rate	kw
CK	Turbine capacity cost coefficient ¹ (D = 0.011)	-
F0	Turbine exponent for cost calculations (D = 0.5)	-
RS	Angular velocity	rpm
X	Turbine head exponent for cost calculations (D = 0.25)	-

Outputs

<u>Variable/Port</u>		
CC0	Turbine cost/year	\$
EFF	Turbine efficiency	-
P	2 Output power	kw
EF	2 Output product efficiency	-
MP	2 Output maximum discharge rate	kw
CP	Turbine characteristic parameter	-

Statistics

CPU	Maximum CP	-
CPL	Minimum CP	-
PU	Maximum output power	kw

D - Default values

¹CK = Capital cost (known unit)/((MD*481.2)**FO*H**X*life expectancy)

The calculation sequence and default values assume a constant speed reaction type hydraulic turbine nominally rated for 120kw and located 200 ft. below the reservoir. The equations relating the various physical parameters are assumed to be valid for the indicated range of the characteristic turbine parameter, CP. The equations and cost estimates are based on the data given in Reference 1, and the cost estimates on data from Reference 2.

Calculation Sequence

$$C1 = 0.377 \times 10^{-6} \frac{\text{kwh}}{\text{ft-lb}}$$

$$C2 = 8.3398 \text{ lb/gal}$$

$$A = C1 * C2 * H$$

1) Costs

$$CC0 = CK * (MD * 481.2) * F0 * H * X$$

2) Efficiency

If $M \leq 0$ set $EFF = 1$ and go to 3)

$$EFF = 1 - (1 - EFD) * MD / M$$

$$EFF = \text{MAX}(EFF, 0.6)$$

-
1. L. Marks and T. Baumeister, "Mechanical Engineers Handbook", McGraw Hill, N.Y., 1958, Section 9, p. 207.
 2. Carson and Fogleman, "Comparison of Methods for Converting Existing Power Plants to Pumped Storage Facilities", International Engineering Company, Inc., 1974.

Calculation Sequence Cont.

3) Output Power

$$P2 = EFF * A * M$$

4) Product Efficiency

$$EF2 = EF1 * EFF$$

$$EFM = MM - (1 - EFD) * MD$$

5) Maximum Discharge Rate

$$MP2 = \text{Min} \{ MP1 * EFD, EFM * A \}$$

6) Turbine Characteristic Parameter

(If $P2 \leq 0$ go to 7)

$$CP = RS * \text{SQRT} (P2 * 0.746) / H^{**1.25}$$

If $CP > 100$ write DIAGNOSTIC

If $M > MM$ write DIAGNOSTIC

7) Compute Statistics and Costs

SUBROUTINE HT

ENTRY POINT 000305

STORAGE USED CODE(1) 000430; DATA(0) 000075; BLANK COMMON(2) 000000

COMMON BLOCKS

```

0003 CIMPL 000002
0004 CTIME 000001
0005 CSIMUL 000010
0006 COST 000001

```

EXTERNAL REFERENCES (BLOCK, NAME)

```

0007 XPRR
0010 SCRT
0011 NWDUS
0012 N1024
0013 NERR35

```

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

0001 000073 100L 0000 000003 1010F 0000 000016 1020F 0001 000205 200L 0001 000231 300L
0001 000113 400L 0006 R 000000 CCI 0000 R 000001 C1 0005 000000 DUM 0000 R 000002 EFM
0003 I 000001 ICNT 0003 I 000000 IMPL 0000 000057 INJPS 0004 R 000000 TIME 0005 R 000007 TMAX
0000 R 000000 TMAX1

```

```

00100 1* CHT 000000
00101 2* SUBROUTINE HT(C,C,EFF,P,EF2,MP2,CP,CPU,CPL,PU,H,H,EFD,MD,MH 000000
00101 3* 1 ,EF1,MP1,CK,FO,RS,X) 000000
00101 4* C 000000
00101 5* C PURPOSE PERFORMANCE OF A HYDRAULIC TURBINE 000000
00101 6* C 000000
00101 7* C METHOD OFF DESIGN PERFORMANCE IS ASSUMED PROPORTIONAL TO 000000
00101 8* C 000000
00101 9* C MASS FLOW RATE 000000
00101 10* C 000000
00101 11* C WRITTEN BY F. O. MAHONY VERSION 1, MARCH 30 1977 000000
00101 12* C 000000
00101 13* C CALL SEQUENCE 000000
00101 14* C OUTPUTS 000000
00101 15* C CC - TURBINE COST/YEAR, $ 000000
00101 16* C EFF - TURBINE EFFICIENCY 000000
00101 17* C P - OUTPUT POWER, KW 000000
00101 18* C EF2 - OUTPUT PRODUCT EFFICIENCY 000000
00101 19* C MP2 - OUTPUT MAXIMUM DISCHARGE RATE, KW 000000
00101 20* C CP - TURBINE CHARACTERISTIC PARAMETER 000000
00101 21* C CPU - MAXIMUM CP 000000

```

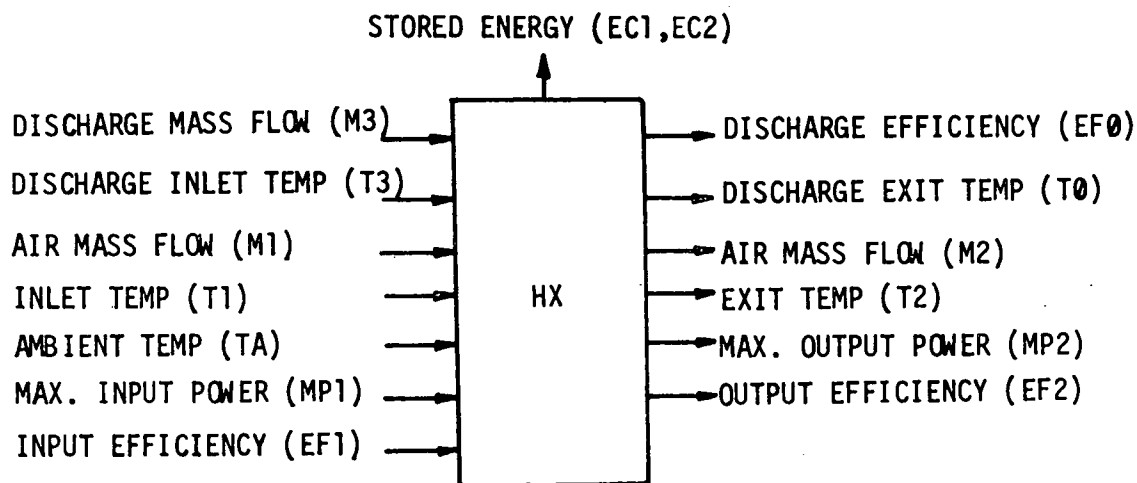
HT

00101	22*	C	CPL - MINIMUM CP	000000
00101	23*	C	PU - MAXIMUM OUTPUT POWER, KW	000000
00101	24*	C		000000
00101	25*	C	INPUTS	000000
00101	26*	C	M - INLET MASS FLOW RATE, GAL/HR	000000
00101	27*	C	H - HEIGHT OF RESERVOIR ABOVE TURBINE INLET, FT	000000
00101	28*	C	EFD - DESIGN POINT TURBINE EFFICIENCY	000000
00101	29*	C	MD - DESIGN POINT MASS FLOW RATE, GAL/HR	000000
00101	30*	C	MM - MAXIMUM MASS FLOW RATE, GAL/HR	000000
00101	31*	C	EF1 - INPUT PRODUCT EFFICIENCY	000000
00101	32*	C	MP1 - INPUT MAXIMUM DISCHARGE RATE	000000
00101	33*	C	CK - TURBINE CAPACITY COST COEFFICIENT	000000
00101	34*	C	FO - TURBINE EXPONENT FOR COST CALCULATIONS	000000
00101	35*	C	RS - ANGULAR VELOCITY, RPM	000000
00101	36*	C	X - TURBINE HEAD EXPONENT FOR COST CALCULATIONS	000000
00101	37*	C		000000
00103	38*		COMMON/CIMPL/IMPL,ICNT/CTIME/TIME /CSIMUL/DUM(7),TMAX /COST/ CCI	000000
00104	39*		REAL MP2,M,MD,MM,MP1	000000
00104	40*	C		000000
00105	41*		IF(IMPL.GT.0)GO TO 100	000000
00105	42*	C		000000
00107	43*		TMAX1=TMAX*0.99999	000002
00110	44*		RS =3600.0	000005
00110	45*	C		000005
00111	46*		IF(EFD.EQ. .99999)EFD=0.9	000007
00113	47*		IF(MD .EQ. .99999)MD =2.0E5	000014
00115	48*		IF(MM .EQ. .99999)MM =3.0E5	000021
00117	49*		IF(CK .EQ. .99999)CK =0.011	000026
00121	50*		IF(FO .EQ. .99999)FO =0.5	000033
00123	51*		IF(X .EQ. .99999)X =0.25	000040
00123	52*	C		000040
00125	53*		CPL=1.0E10	000045
00126	54*		CPU=0.0	000047
00127	55*		PU =0.0	000050
00127	56*	C		000050
00130	57*		C1 = 3.1441E-6	000051
00131	58*		CC =CK*(MD*481.2)**FO*M**X	000053
00131	59*	C		000053
00131	60*	C	EFFICIENCY	000053
00132	61*		100 EFF =1.0	000073
00132	62*	C		000073
00133	63*		IF(M.LE.0.0)GO TO 400	000074
00133	64*	C		000074
00135	65*		EFF=1.0-(1.0-EFD)*MD/M	000077
00136	66*		IF(EFF.LT.0.6) EFF=0.6	000104
00136	67*	C		000104
00136	68*	C	OUTPUT POWER	000104
00136	69*	C		000104
00140	70*		400 P =EFF*M*H*C1	000113
00140	71*	C		000113
00140	72*	C	PRODUCT EFFICIENCY	000113
00140	73*	C		000113
00141	74*		EF2=EF1*EFF	000117
00141	75*	C		000117
00141	76*	C	MAXIMUM DISCHARGE RATE	000117
00141	77*	C		000117
00141	78*		EFM =MM*.9999-(1.0-EFD)*MD	000122

HT

00142	79*	C		000122
00143	80*		MP2=AMIN1(MP1*EFD,EFH*H+C1)	000131
00143	81*	C		000131
00143	82*	C	TURBINE CHARACTERISTIC PARAMETER	000131
00143	83*	C		000131
00144	84*		IF(P .LE. 0.0) GO TO 300	000142
00146	85*		CP =RS*SQRT(P*0.746)/H**1.25	000144
00146	86*	C		000144
00147	87*		IF(CP.LT.100.0)GO TO 200	000162
00147	88*	C		000162
00151	89*		IF(IMPL.E0.2)WRITE(6,1010)CP	000165
00155	90*		IF(IMPL.E0.2) ICNT=ICNT+1	000176
00155	91*	C		000176
00157	92*		200 IF(M.LT.MM)GO TO 300	000205
00157	93*	C		000205
00161	94*		IF(IMPL.E0.2)WRITE(6,1020)M,MM	000210
00166	95*		IF(IMPL.E0.2) ICNT=ICNT+1	000222
00166	96*	C		000222
00170	97*		300 IF(IMPL.LE.1)RETURN	000231
00170	98*	C		000231
00170	99*	C	STATISTICS	000231
00170	100*	C		000231
00172	101*		CPU=AMAX1(CPU,CP)	000237
00173	102*		CPL=AMIN1(CPL,CP)	000245
00174	103*		PU =AMAX1(PU ,P)	000253
00174	104*	C		000253
00175	105*		IF(TIME.LT.TMAX1)RETURN	000261
00175	106*	C		000261
00175	107*	C	COST	000261
00175	108*	C		000261
00177	109*		CCI=CCI+CC	000270
00177	110*	C		000270
00200	111*		RETURN	000273
00200	112*	C		000273
00201	113*		1010 FORMAT(1H0,48HHT TURBINE CHARACTERISTIC PARAMETER OUT OF RANGE	000427
00201	114*		1 F12.3)	000427
00202	115*		1020 FORMAT(1H0,23HHT INLET MASS FLOW RATE,F12.3	000427
00202	116*		1 ,37H GREATER THAN MAXIMUM DESIGN VALUE,F12.3)	000427
00202	117*	C		000427
00203	118*		END	000427

7.16 ADIABATIC HEAT EXCHANGER



The purpose of the adiabatic heat exchanger is to recover a portion of the heat of compression from the high pressure, high temperature air exiting from the compressor. Figure 7.16-1 shows an adiabatic heat exchanger used in an underground, constant pressure compressed air energy storage system. The adiabatic heat exchanger operates in a manner similar to the high temperature thermal energy storage systems currently conceived for solar thermal power plants¹. In the storage charging mode, high pressure, high temperature air enters the top of the heat exchanger and deposits a portion of its thermal energy in the storage media as either sensible heat or latent heat of fusion. The exiting high pressure air is stored in an appropriate vessel, e.g., underground cavern. In the discharge cycle (HY), high pressure, low temperature air enters the bottom of the heat exchanger, recovers thermal energy from the storage media and exits to the turbine.

The adiabatic heat exchanger model is based on a two cell storage model. Given the stored energy in both cells, a linear temperature profile is computed

¹ BEC/EPRI RP 788-1, "Advanced Thermal Energy Storage Systems," November 1976.

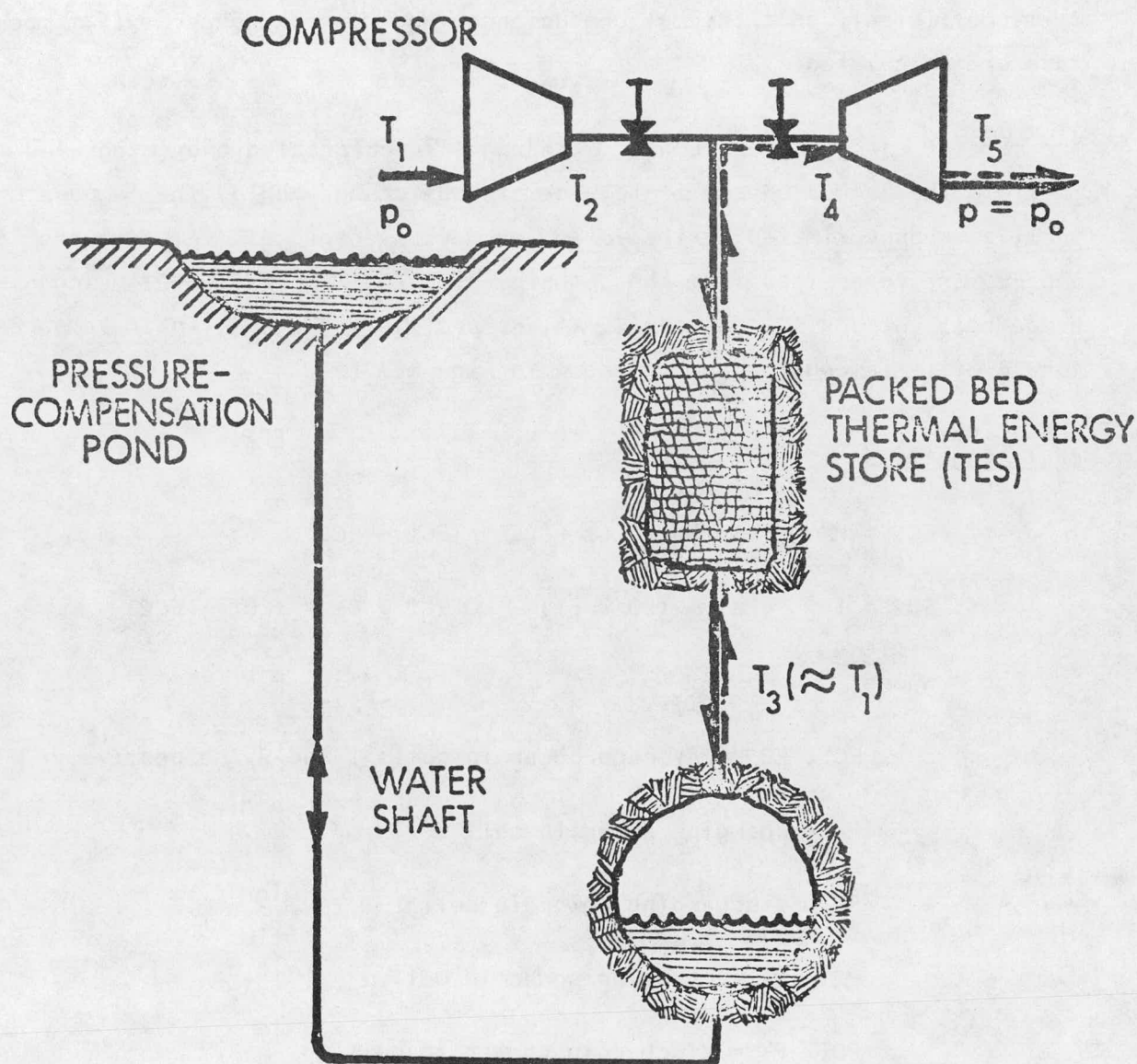


FIGURE 7.16-1 KOUTZ-GLENDENNING ADIABATIC COMPRESSED AIR STORAGE SCHEME (SINGLE-STAGE HEAT-OF-COMPRESSION STORAGE)

for the media mass. Based on a given inlet mass flow rate, the convective film coefficient, unit thermal conductance, and heat exchanger exit temperature are calculated.

The rate of energy deposited (or withdrawn) is calculated and integrated to yield the stored energy state. For a phase change media, the temperature profile is approximated in the following way: Average cell temperatures TS1 and TS2 are determined from the enthalpy diagram (Figure 7.16-2) using average cell entropy EC1/MA and EC2/MA, respectively. Then a linear temperature profile is constructed as shown in Figure 7.16-3.

Basic Equations

$$\dot{EC}_1 = PX - PY - NU * EC_1 - BE * (EC_1 - EC_2)$$

$$\dot{EC}_2 = (P_2 - PX) - (P_0 - PY) - NU * EC_2 + BE * (EC_1 - EC_2)$$

where

EC1, EC2 = storage power in cells 1 and 2, respectively

PX = charging power in cell 1

PY = discharging power in cell 1

P2 - PX = charging power in cell 2

P0 - PY = discharging power in cell 2

NU = storage media leakage constant

BE = storage media mixing constant

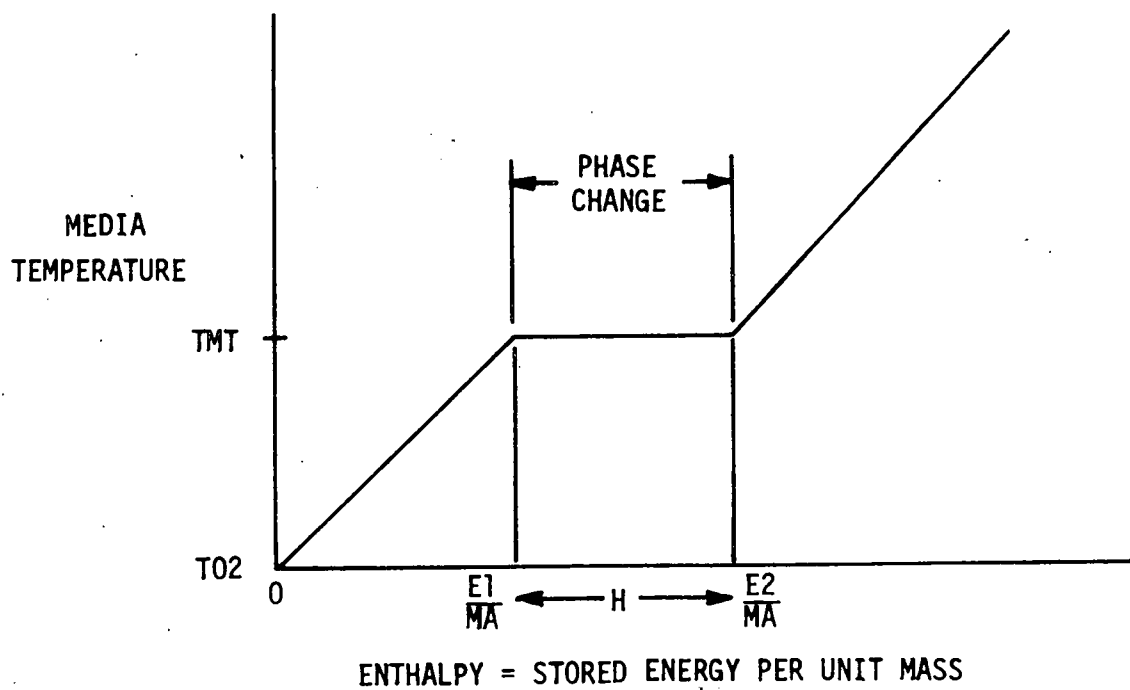


FIGURE 7.16-2: ENTHALPY-TEMPERATURE DIAGRAM FOR HX

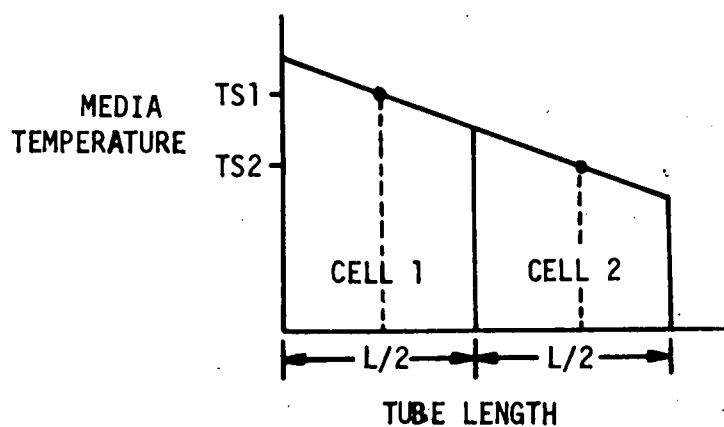


FIGURE 7.16-3: STORAGE TEMPERATURE VERSUS TUBE LENGTH

Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
NU	Storage energy loss coefficient (D = 0.002)	(h) ⁻¹
ST	Rated storage time ¹	h
BE	Storage energy mixing coefficient (D = 0.0)	h ⁻¹
T01	Minimum allowable storage temperature (D = 60)	°F
DTD	Media temperature swing ¹ (D = 400)	°F
PD	Rated storage thermal power	kw
TEM	Maximum allowable exit temperature (D = 240)	°F
XD	Design point fraction of molten media mass (D = 0.8)	-
EF	1 Input product efficiency	-
MP	1 Maximum input charging rate	kw
CP1	Storage media heat capacity (D = 2.93X10 ⁻⁴)	kwh/lb °F
H	Storage media heat of fusion ² (D = 0.0219)	kwh/lb
TMT	Storage media melt temperature ² (D = 147)	°F
CPF	Air heat capacity (D = 7.6X10 ⁻⁵)	kwh/lb °F
KF	Air thermal conductivity (D = 1.03X10 ⁻⁴)	kw/ft °F
MU	Air viscosity (D = 0.055)	lb/ft-h
NT	Number of tubes (D = 200)	-
D	Tube diameter (D = 0.03)	ft
L	Tube length (D = 4)	ft
DEL	Tube half spacing (D = 0.085)	ft
K	Storage media thermal conductivity (D = 0.0078)	kw/ft-°F
T	1 Inlet air temperature	°F
M	1 Inlet mass flow rate	lb/h
CM	Storage device yearly maintenance cost (D = 0.6)	\$/kw
CSA	Storage device capacity cost (D = 50)	\$/kw
CSB	Storage device energy cost (D = 15.6)	\$/kwh
LE	Unit life expectancy	years

D - Default values specified

1 - Design point conditions

2 - Used for phase change media, H = 0 for sensible heat

Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
M 3	Discharge cycle mass flow rate from storage	lb/hr
T 3	Discharge cycle temperature from storage	°F
TA	Ambient temperature	°F
TS0	Storage vessel minimum temperature	°F

Outputs

<u>Variable/Port</u>	<u>Description</u>	<u>Units</u>
EC1	Stored energy (state) for cell 1 (hot side)	kwh
EC2	Stored energy (state) for cell 2 (cold side)	kwh
M 2	Outlet mass flow rate (=M1)	lb/hr
MP 2	Maximum discharge rate	kw
TS1,TS2	Average temperatures for cells 1 and 2	°F
T 2	Air exit temperature	°F
MA	Required storage media mass	lb
CC0	Storage device capital cost/year	\$
HF	Convective heat transfer coefficient	kwh/ft ² -°F
U	Unit thermal conductance	kwh/ft ² -°F
P 2	Charge rate into heat exchanger	kw
E1,E2	Energy stored at start and end of melt	kwh
PM	Maximum allowable charge rate	kw
EF 2	Output product efficiency	-
RT	Thermal resistance	°F/kw
P0	Discharge power taken from heat exchanger	kw
T0	Discharge cycle output temperature	°F
EF0	Discharge cycle efficiency	-

Statistics

TSU	Maximum storage temperature	°F
TSL	Minimum storage temperature	°F
ME	Maximum stored energy	kwh
MT	Maximum exit temperature	°F

The default values assume use of paraffin wax as the phase change storage medium. (In reality, paraffin wax may not be applicable to temperatures as high as 600°F. The selection of a phase change medium involves careful consideration of a number of factors [see Reference 1]). The heat exchanger geometric parameters, i.e., tube number, diameter, etc., and heat exchanger cost estimates are based on the baseline phase change storage device developed in Reference 1, but scaled down to reflect expected mass flow rates and required media mass. Although these data were developed for a different application (50 MWe, 6 hour storage, average temperature = 786°C), they can be considered representative until detail design data is available.

1. "Advanced Thermal Energy Storage," BEC/EPRI RP 788-1, July 1976.

Calculation Sequence

1) Initial Calculations

$$MA = \frac{PD \cdot ST \cdot 0.5}{XD \cdot H + CP1 \cdot DTD}$$

$$CC0 = (CSA + CSB \cdot ST) \cdot PD / LE$$

$$E1 = MA \cdot CP1 \cdot (TMT - T01)$$

$$E2 = MA \cdot [H + CP1 \cdot (TMT - T01)]$$

$$T3 = TS0 = TA$$

$$A = (D \cdot DEL + DEL \cdot \Delta^2) / 5.$$

$$RB(1) = D/2, \quad RB(i+1) = \sqrt{RB(i)^2 + A} \quad i=1,5$$

$$RN(i) = \sqrt{(RB(i+1)^2 + RB(i)^2) / 2}$$

$$RT = \frac{D}{2 \cdot k} \sum_{i=1}^4 \ln \left(\frac{RN(i+1)}{RN(i)} \right)$$

2) Storage Temperature (see Figure 7.16-2)

$$TS = \begin{cases} T01 + \frac{E}{MA \cdot CP1} & \text{if } E < E_1 \\ TMT & \text{if } E_1 \leq E \leq E_2 \\ T01 + \frac{\left(\frac{E}{MA} - H \right)}{CP1} & \text{if } E > E_2 \end{cases}$$

where $TS = TS1$ and $E = EC1$ for storage cell 1 and similarly for cell 2.

3) HX Exit Temperature Calculations

$$M2 = M1$$

$$P2 = 0$$

$$PX = 0$$

3) Cont.

$$T2 = TS2 - (TS1 - TS2)/2$$

$$\Delta T = TS1 - TS2$$

If $M1 = 0$, GO TO 7)

4) Convective Heat Transfer Coefficient¹

$$HF = \frac{KF}{D} \left[0.0215 * \left(\frac{M1}{NT} * \frac{4}{MU * PI * D} \right)^{0.8} * \left(\frac{CPF * MU}{KF} \right)^{0.6} \right]$$

5) Thermal Conductance

$$U = \left\{ \frac{1}{HF} + RT \right\}^{-1}$$

$$UA = U * PI * D * L * NT / (CPF * M1 * 2)$$

6) Exit Temperature and Charge Rate (See Equation A2. in Appendix)

$$TX = T1 - \Delta T - (1. - \exp(-UA)) * (T1 - TS1 - \Delta T/2 - \Delta T/UA)$$

$$T2 = TX - \Delta T - (1. - \exp(-UA)) * (TX - (TS1 + TS2)/2 - \Delta T/UA)$$

$$P2 = M1 * CPF * (T1 - T2)$$

$$PX = M1 * CPF * (T1 - TX)$$

7) HY Exit Temperature Calculations

$$T0 = TS1 + \Delta T/2$$

$$P0 = 0.$$

$$PY = 0.$$

If $M3 = 0$ GO TO 11)

¹ Kays, W. M., Convective Heat and Mass Transfer, McGraw Hill, N.Y., 1966, p. 173.

8) Convective Heat Transfer Coefficient

$$HF0 = \frac{KF}{D} \left(.0215 * \left(\frac{M3}{NT} * \frac{4}{MU * PI * D} \right)^{0.8} * \left(\frac{CPF * MU}{KF} \right)^{0.6} \right)$$

9) Thermal Conductance

$$U0 = \left(\frac{1}{HF0} + RT \right)^{-1}$$

$$UA = U0 * PI * D * L * NT / (CPF * M3 * 2)$$

10) Exit Temperature and Discharge Rate (See Equation A3. in Appendix)

$$TY = T3 + \Delta T - (1. - EXP(-UA)) * (T3 - TS2 + \Delta T / 2 + \Delta T / UA)$$

$$T0 = TY + \Delta T - (1. - EXP(-UA)) * (TY - (TS1 + TS2) / 2 + \Delta T / UA)$$

$$P0 = M3 * CPF * (T0 - T3)$$

$$PY = M3 * CPF * (T0 - TY)$$

11) Energy Deposited

$$\dot{EC1} = PX - NU * EC1 - PY - BE * (EC1 - EC2)$$

$$\dot{EC2} = (P2 - PX) - NU * EC2 - (P0 - PY) + BE * (EC1 - EC2)$$

If $T2 \geq TEM$, WRITE DIAGNOSTIC

12) Maximum Allowable Mass Flow Rate

$$MDM = PD / (CPF * DTD)$$

13) Maximum Allowable Charge Rate

$$PM = MDM * CPF * (T1 - TA)$$

14) Charging and Discharging Efficiency

$$EFF = 1$$

$$\text{If } T2 > TS0 \quad EFF = \frac{T2 - TS0}{T1 - TA}$$

$$EF0 = 1$$

$$\text{If } T3 > TS0 \quad EF0 = \frac{T0 - TA}{T3 - TS0}$$

$$MP2 = \text{MIN } (MP1, PM) * EFF$$

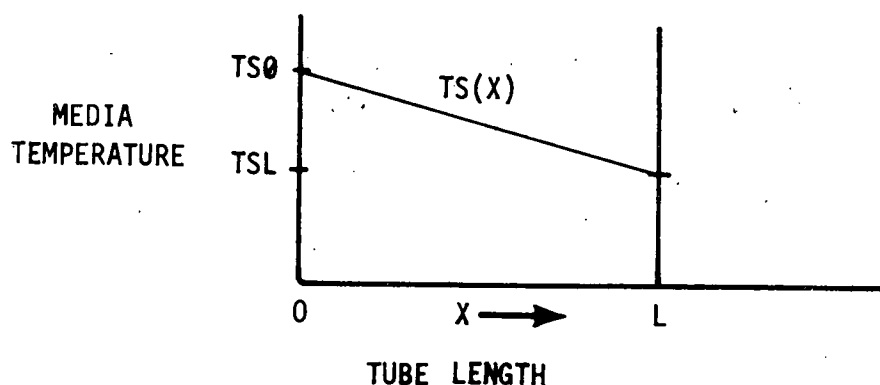
$$EF2 = EF1 * EFF$$

15) Compute Statistics and Cost Summation

Appendix: Temperature Equations for a Media with Constant Gradient

Assumptions

- 1) Constant Gradient Media Temperature:



- 2) Working Fluid Differential Equation:

$$A1. \quad \frac{\partial T_f}{\partial X} = \frac{UA}{L} (TS - T_f) \quad 0 < x < L$$

Main Results: Exit temperature in the charging and discharging cycles are given by

$$A2. \quad T_f(L) = T_f(0) + \Delta TS - (1 - \exp(-UA)) * \left(T_f(0) - TS0 + \frac{\Delta TS}{UA} \right)$$

$$A3. \quad T_f(0) = T_f(L) - \Delta TS - (1 - \exp(-UA)) * \left(T_f(L) - TSL - \frac{\Delta TS}{UA} \right)$$

where $\Delta TS = TSL - TS0$.

Proof: Multiplying A1. by $\exp(UA \cdot X/L)$ and recombining terms yields:

$$A4. \quad \frac{\partial}{\partial X} \left(\exp(UA \cdot X/L) * T_f \right) = \frac{UA}{L} * \exp(UA \cdot X/L) * TS(X).$$

Integrating A4. and substituting $TS(X) = TS0 + \frac{\Delta TS}{L} * X$ yields

$$\begin{aligned}
 \text{A5.} \quad T_f(X) &= \exp(-UA \cdot X/L) \cdot T_f(0) + \frac{UA}{L} \int_0^X \exp(-UA(x-y)/L) \cdot TS(y) dy \\
 &= \exp(-UA \cdot X/L) T_f(0) + (1 - \exp(-UA \cdot X/L)) \cdot (TS_0 - \Delta TS/UA) \\
 &\quad + \frac{\Delta TS}{L} \cdot X
 \end{aligned}$$

Recombining terms in A5. and letting $X=L$ yields A2. Equation A3. follows from A2. by symmetry, i.e., substitute in A2:

$T_f(0)$ for $T_f(L)$

$T_f(L)$ for $T_f(0)$

TSL for TS_0

TS_0 for TSL .

SUBROUTINE HX ENTRY POINT 001065

STORAGE USED CODE(1) 001517; DATA(0) 000143; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000002
0004 CTIME 000001
0005 CSTMUL 000010
0006 COST 000002

EXTERNAL REFERENCES (BLOCK, NAME)

0007 SORT
0010 ALOG
0011 XPRR
0012 EXP
0013 NWDCS
0014 N1024
0015 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000301	100L	0000	000034	1010F	0001	000514	200L	0001	000236	205G	0001	000264	214G
0001	000637	300L	0001	000714	500L	0000 R	000016	A	0006 R	000000	CCI	0006 R	000001	CHI
0000 R	000020	DELT	0005	000000	DUM	0000 R	000033	EFF	0000 R	000030	HFO	0000 I	000017	I
0003 I	000001	ICNT	0003 I	000000	IMPL	0000	000107	INJP5	0000 R	000000	MDM	0000 R	000014	PI
0000 R	000023	PX	0000 R	000027	PY	0000 R	000001	RB	0000 R	000007	RN	0000 R	000025	TEMP
0004 R	000000	TIME	0005 R	000007	TMAX	0000 R	000015	TMAX1	0000 R	000022	TSC	0000 R	000021	TSH
0000 R	000026	TX	0000 R	000032	TY	0000 R	000024	UA	0000 R	000031	UO			

00100	1*	CHX	
00101	2*		SUBROUTINE HX(IE1,DE1,IE1,EC2,DE2,IE2,M2,MP2,TS1,TS2,T2,MA,
00101	3*		1CC,HF,U,P,E1,E2,PH,EF2,PO,TO,EFO,R,TSU,TSL,ME,MT,NU,ST,BE,T01,DT0
00101	4*		2 ,PD,TEM,XD,EF1,MP1,CP1,H,TMT,CPF,KF,MU,NT,D,L,DEL,K,T1
00101	5*		3 ,M1,CH,CSA,CSB,LE,M3,T3,TA,TS0)
00101	6*	C	
00101	7*	C	PURPOSE PERFORMANCE OF ADIABATIC HEAT EXCHANGER DURING CHARGE
00101	8*	C	
00101	9*	C	CYCLE
00101	10*	C	
00101	11*	C	METHOD HEAT STORAGE MEDIA ASSUMED TO CONTAIN NO TEMPERATURE
00101	12*	C	
00101	13*	C	GRADIENTS. ENERGY DEPOSITED IS A FUNCTION OF TEMPERATURE
00101	14*	C	
00101	15*	C	AND THERMAL CONDUCTANCE
00101	16*	C	

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HX

00101	17*	C
00101	18*	C
00101	19*	C
00101	20*	C
00101	21*	C
00101	22*	C
00101	23*	C
00101	24*	C
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00101	63*	C
00101	64*	C
00101	65*	C
00101	66*	C
00101	67*	C
00101	68*	C
00101	69*	C
00101	70*	C
00101	71*	C
00101	72*	C
00101	73*	C

WRITTEN BY F. D. MAHONY

VERSION 2, JUNE 1977

CALL SEQUENCE OUTPUTS

```

EC1 - STORED ENERGY (STATE ) FOR STORAGE CELL 1, KWH
DE1 - ENERGY RATE FOR EC1, KW
IE1 - STATUS INDICATOR FOR EC1
EC2 - STORED ENERGY STATE FOR STORAGE CELL 2, KWH
DE2 - ENERGY RATE FOR EC2, KW
IE2 - STATUS INDICATOR FOR EC2
M2 - OUTLET MASS FLOW RATE, LB/HR
MP2 - MAXIMUM DISCHARGE RATE ALLOWABLE, KW
TS1 - STORAGE TEMPERATURE IN CELL 1, DEG F
TS2 - STORAGE TEMPERATURE IN CELL 2, DEG F
T2 - AIR EXIT TEMPERATURE, DEG F
MA - REQUIRED STORAGE MEDIA MASS LB
CC - STORAGE DEVICE CAPITAL COST/YEAR, $
HF - CONVECTIVE HEAT TRANSFER COEFFICIENT, KWH/FT2-F
U - UNIT THERMAL CONDUCTANCE, KWH/FT2-F
P - CHARGE RATE OF HEAT EXCHANGER
E1 - ENERGY STORED AT STAPT OF MELT PHASE, KWH
E2 - ENERGY STORED AT END OF MELT PHASE, KWH
PM - MAXIMUM ALLOWABLE CHARGE RATE, KW
EF2 - OUTPUT PRODUCT EFFICIENCY
PO - DISCHARGE POWER TAKEN FROM HEAT EXCHANGER, KW
TO - DISCHARGE CYCLE OUTPUT TEMPERATURE, DEG F
EFO - DISCHARGE CYCLE EFFICIENCY
R - THERMAL RESISTANCE, DEG F/KW

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STATISTICS

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TSU - MAXIMUM STORAGE TEMPERATURE, DEG F
TSL - MINIMUM STORAGE TEMPERATURE, DEG F
ME - MAXIMUM STORED ENERGY, KWH
MT - MAXIMUM EXIT TEMPERATURE, DEG F

```

INPUTS

- NU - STORAGE ENERGY LOSS COEFFICIENT
- ST - RATED STORAGE TIME, HR
- BE - STORAGE ENERGY MIXING COEFFICIENT, 1/HR
- TO1 - MINIMUM ALLOWABLE STORAGE TEMPERATURE, DEG F
- DTD - MEDIA TEMPERATURE SWING, DEG F
- PD - RATED THERMAL STORAGE POWER, KW
- TEM - MAXIMUM ALLOWABLE EXIT TEMPERATURE, DEG F
- XD - DESIGN POINT FRACTION OF MOLTEN MEDIA MASS
- EF1 - INPUT PRODUCT EFFICIENCY
- MP1 - MAXIMUM INPUT CHARGING RATE
- CP1 - STORAGE MEDIA HEAT CAPACITY, KWH/LB-F
- H - STORAGE MEDIA HEAT OF FUSION, KWH/LB
- TMT - STORAGE MEDIA MELT TEMPERATURE, DEG F
- CPF - AIR HEAT CAPACITY, KWH/LB-F
- KF - AIR THERMAL CONDUCTIVITY, KWH/FT-F
- MU - AIR VISCOSITY, LB/FT-HR
- NT - NUMBER OF H/X TUBES
- D - TUBE DIAMETER, FT
- L - TUBE LENGTH, FT
- DEL - TUBE HALF SPACING, FT
- K - STORAGE MEDIA THERMAL CONDUCTIVITY

[illegible]

工




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00202 131* C COMPUTE THERMAL RESISTANCE OF MEDIA
00202 132* C
00203 133* RB(1)=D/2.0
00203 134* C
00204 135* DO 20 I=1,5
00207 136* RB(I+1)=SQRT(RB(I)**2+A)
00210 137* 20 RN(I)=SQRT((RB(I+1)**2+RB(I)**2)/2.0)
00210 138* C
00212 139* R=0.0
00212 140* C
00213 141* DO 30 I=1,4
00216 142* 30 R=R+ALOG(RN(I+1)/RN(I))
00216 143* C
00220 144* R=R*D/2.C/K
00220 145* C
00220 146* C STORAGE TEMPERATURES
00220 147* C
00221 148* 100 TS1=TMT
00221 149* C
00222 150* IF(EC1.LT.E1) TS1= T01+ EC1/(HA*CP1)
00224 151* IF(EC1.GT.E2) TS1= T01+ (EC1/HA - H)/CP1
00226 152* TS2=TMT
00227 153* IF(EC2.LT.E1) TS2= T01+ EC2/(HA*CP1)
00231 154* IF(EC2.GT.E2) TS2= T01+ (EC2/HA - H)/CP1
00231 155* C
00233 156* DELT= TS1 - TS2
00234 157* TSH= TS1+ .5*DELT
00235 158* TSC= TS2 - .5*DELT
00235 159* C
00236 160* T2= TSC
00237 161* M2=M1
00240 162* P =0.0
00241 163* PX=0.0
00242 164* U=1.0/R
00242 165* C
00243 166* IF(M1.LT.0.001)60 TO 200
00243 167* C
00243 168* C CONVECTIVE HEAT TRANSFER COEFFICIENT
00243 169* C
00245 170* HF =KF/D*(0.0215*(M1/NT*4.0/HU/PI/D)**0.8*(CPF*HU/KF)**0.6)
00245 171* C
00245 172* C UNIT THERMAL CONDUCTANCE
00245 173* C
00246 174* U = 1.0/(1.0/HF+R)
00247 175* UA= U*PI*D*L*NT/(M1*CPF*2.)
00250 176* TEMP= DELT/UA
00251 177* UA= 1. - EXP(-UA)
00251 178* C
00251 179* C EXIT TEMPERATURE
00251 180* C
00252 181* TX= T1 - DELT - UA*(T1-TSH-TEMP)
00253 182* T2= TX- DELT - UA*(TX-(TS1+TS2)*.5-TEMP)
00253 183* C
00253 184* C CHARGE RATE
00253 185* C
00255 186* P =M1*CPF*(T1-T2)
00255 187* PX = M1*CPF*(T1-TX)

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000221
000221
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000302
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000432
000440
000452
000455
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000463
000473
000473
000473
000473
000504
000507

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HY

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00255 188* C
00255 189* C
00255 190* C
00256 191* 200 TO = TSH
00257 192* PO = 0.0
00260 193* PY = 0.0
00261 194* IF (M3.LT. .001) GO TO 300
00261 195* C
00261 196* C
00261 197* C
00263 198* CONVECTIVE HEAT TRANSFER COEFFICIENT
00263 199* C
00263 200* C
00263 201* C
00264 202* MFO = KF/D*(0.0215*(M3/NT+4.0/MU/PI/D)**0.8*(CPF+MU/KF)**0.6)
00265 203* UNIT THERMAL CONDUCTANCE
00266 204* C
00267 205* C
00267 206* C
00267 207* C
00267 208* C
00270 209* UO = 1.0/(1.0/MFO+R)
00271 210* UA = UO*PI*D*L*NT/(M3*CPF*2.)
00272 211* TEMP = DELT/UA
00273 212* UA = EXP(-UA) - 1.
00273 213* C
00273 214* C
00273 215* C
00273 216* C
00274 217* EXIT TEMPERATURE AND DISCHARGE RATE
00276 218* TY = T3 + DELT + UA*(T3-TSC+TEMP)
00276 219* TO = TY + DELT + UA*(TY-(TS1+TS2)*.5+TEMP)
00300 220* PO = M3*CPF*(TO-T3)
00300 221* PY = M3*CPF*(TO-TY)
00302 222* C
00302 223* C
00302 224* C
00302 225* C
00302 226* C
00307 227* ENERGY DEPOSITED
00307 228* C
00307 229* C
00307 230* C
00311 231* 300 IF (IE1.NE.0) DE1 = PX - PY - NU*EC1 - BE*(EC1-EC2)
00311 232* IF (IE2.NE.0) DE2 = P-PX - (PO-PY) - NU*EC2 + BE*(EC1-EC2)
00312 233* IF (T2.LT.TEM) GO TO 500
00312 234* C
00312 235* C
00312 236* C
00312 237* C
00312 238* C
00312 239* IF (IMPL.EQ.2) WRITE(6,1010) T2,TEM
00312 240* IF (IMPL.EQ.2) ICNT = ICNT+1
00313 241* C
00313 242* C
00313 243* C
00313 244* C
00314 245* MAXIMUM ALLOWABLE CHARGE AND FLOW RATES
00314 246* C
00314 247* C
00314 248* C
00314 249* C
00314 250* 500 MDM = PO/(CPF*DTD)
00315 251* PM = MDM*CPF*(T1-TA)
00316 252* C
00316 253* C
00316 254* C
00316 255* C
00316 256* CHARGING AND DISCHARGING EFFICIENCY
00316 257* C
00316 258* C
00316 259* C
00316 260* C
00316 261* EFF = 1.0
00316 262* C
00316 263* C
00316 264* C
00316 265* IF (T2.GE.TS0) EFF = (T2-TS0)/(T1-TA)
00316 266* C
00316 267* C
00316 268* C
00316 269* C
00316 270* EFO = 1.0
00316 271* C
00316 272* C
00316 273* C
00316 274* C
00316 275* IF (T3.GT.TS0) EFO = (TO-TA)/(T3-TS0)
00316 276* C
00316 277* C
00316 278* C
00316 279* C
00316 280* MP2 = AMIN1(MP1,PM)*EFF
00316 281* C
00316 282* C
00316 283* C
00316 284* C
00316 285* EF2 = EF1*EFF
00316 286* C

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```

FX

```

00322 245* C
00322 246* C
00322 247* C
00323 248* IF(IMPL.LE.1)RETURN
00323 249* C
00325 250* TSU =AMAX1(TSU,TS1)
00326 251* TSL =AMIN1(TSL,TS2)
00327 252* ME = AMAX1(ME, EC1*EC2)
00330 253* MT =AMAX1(MT ,T2)
00330 254* C
00331 255* IF(TIME.LT.TMAX1)RETURN
00331 256* C
00333 257* CCI =CCI+CC
00334 258* CMI=CMJ+CM
00335 259* CM= CM/PD
00335 260* C
00336 261* RETURN
00336 262* C
00337 263* 1010 FORMAT(1H0,22HXX EXIT TEMPERATURE ,F12.3
00337 264* 1 ,35H GREATER THAN MAXIMUM ALLOWABLE ,F12.3)
00337 265* C
00340 266* END

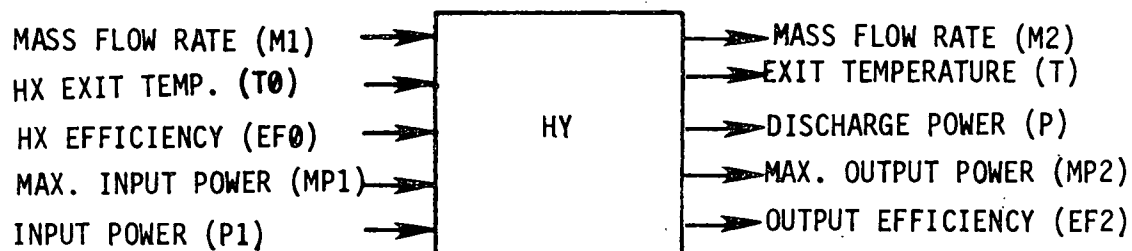
```

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```

7.17 ADIABATIC HEAT EXCHANGER - DISCHARGING CYCLE



HY is the discharge cycle complement to HX. All the calculations to obtain the exit temperature and heat exchange power deposited or withdrawn are done in HX. The results are then passed to HY for summary.

Inputs

<u>Parameter/Port</u>		<u>Description</u>	<u>Units</u>
M	1	Air mass flow rate from storage	lb/hr
T0		Exit temperature from HX	°F
P	1	Discharge power from storage	kw
EF0		Discharge cycle efficiency from HX	-
MP	1	Maximum power from storage	kw

Outputs

<u>Variable/Port</u>			
M	2	Exit air mass flow rate (=M1)	lb/hr
T		Exit temperature (=T0)	°F
P	2	Discharge power	kw
MP	2	Maximum discharge power	kw
EF	2	Output product efficiency	-

Statistics

TL	Minimum exit temperature	°F
TU	Maximum exit temperature	°F
SP	Total energy discharged	kwh

Calculation Sequence

1) $M2 = M1$

$T = T0$

$MP2 = MP1 * EF0$

$EF2 = EF0$

$P2 = P1 * EF0$

2) Compute Statistics

SUBROUTINE HY

ENTRY POINT 000064

STORAGE USED CODE(1) 000135; DATA(0) 000017; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000001

0004 CSIMUL 000007

EXTERNAL REFERENCES (BLOCK, NAME)

0005 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

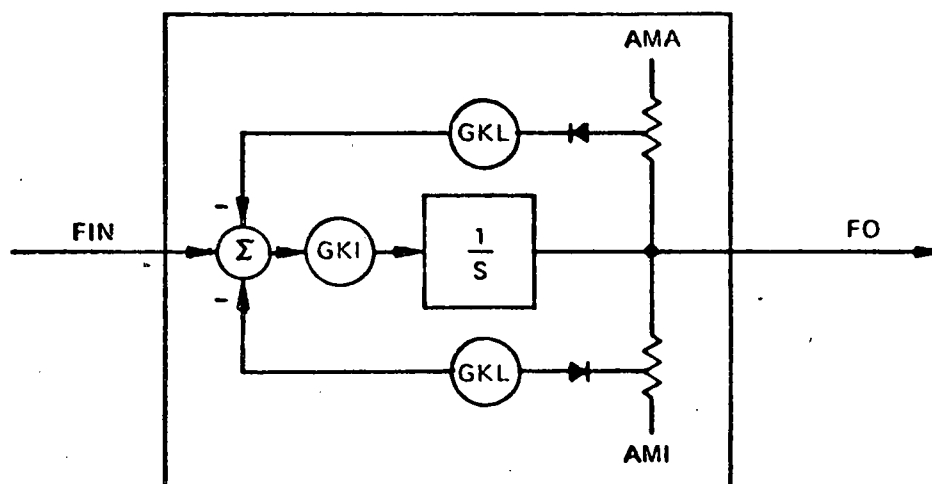
0001 000007 100L 0004 000000 DUM 0003 1.000000 IMPL 0000 000002 INJPS 0004 R 000006 TINC

00100	1*	CHY		000000
00101	2*		SUBROUTINE HY(M2,T,P2,MP2,EF2,TL,TU,SP,H1,TO,P1,EFO,MP1)	000000
00101	3*	C		000000
00101	4*	C	PURPOSE PERFORMANCE OF ADIABATIC HEAT EXCHANGER DURING DISCHARGE	000000
00101	5*	C		000000
00101	6*	C	CYCLE	000000
00101	7*	C		000000
00101	8*	C	METHOD COMPUTE EXIT CONDITIONS USING HEAT EXCHANGER STATE	000000
00101	9*	C		000000
00101	10*	C	DETERMINED IN HX	000000
00101	11*	C		000000
00101	12*	C	WRITTEN BY F. O. MAHONY VERSION 1, MARCH 27 1977	000000
00101	13*	C		000000
00101	14*	C	CALL SEQUENCE	000000
00101	15*	C	OUTPUTS	000000
00101	16*	C	M2 - EXIT AIR MASS FLOW RATE (=M1), LB/HR	000000
00101	17*	C	T - EXIT TEMPERATURE (=TO), DEG F	000000
00101	18*	C	P2 - TOTAL DISCHARGE POWER, KW	000000
00101	19*	C	MP2 - MAXIMUM DISCHARGE POWER, KW	000000
00101	20*	C	EF2 - OUTPUT PRODUCT EFFICIENCY	000000
00101	21*	C		000000
00101	22*	C	STATISTICS	000000
00101	23*	C	TL - MINIMUM EXIT TEMPERATURE, DEG F	000000
00101	24*	C	TU - MAXIMUM EXIT TEMPERATURE, DEG F	000000
00101	25*	C	SP - TOTAL ENERGY DISCHARGED, KWH	000000
00101	26*	C		000000
00101	27*	C	INPUTS	000000
00101	28*	C	M1 - AIR MASS FLOW RATE FROM STORAGE, LB/HR	000000
00101	29*	C	TO - EXIT TEMPERATURE FROM HX, DEG F	000000
00101	30*	C	P1 - DISCHARGE POWER FROM STORAGE, KW	000000

HY

00101	31*	C	EFO - DISCHARGE CYCLE EFFICIENCY	000000
00101	32*	C	MP1 - MAXIMUM POWER FROM STORAGE, KW	000000
00101	33*	C		000000
00103	34*		COMMON /CIMPL/IMPL /CSIMUL/DUM(6),TINC	000000
00103	35*	C		000000
00104	36*		REAL M2,MP2,M1,MP1	000000
00104	37*	C		000000
00105	38*		IF(IMPL.GT.0)GO TO 100	000000
00105	39*	C		000000
00107	40*		TU =0.0	000002
00110	41*		SP =0.0	000003
00110	42*	C		000003
00111	43*		TL =1.0E10	000004
00112	44*	100	M2 =M1	000007
00113	45*		T =T0	000010
00114	46*		P2 =P1*EFO	000012
00115	47*		MP2=MP1*EFO	000015
00116	48*		EF2=EFO	000020
00116	49*	C		000020
00117	50*		IF(IMPL.LE.1)RETURN	000022
00117	51*	C		000022
00121	52*		TL =AMIN1(TL ,T)	000031
00122	53*		TU =AMAX1(TU ,T)	000037
00122	54*	C		000037
00123	55*		SP =SP +P2*TINC/2.0	000045
00123	56*	C		000045
00124	57*		RETURN	000052
00125	58*		END	000134

7.18 INTEGRATOR WITH SATURATION

InputsParameter/PortDescription

FIN	Input
GKI	Integration gain
GKL	Saturation limiter gain
AMA	Upper limit of output (Default = 10^{36})
AMI	Lower limit of output (Default = -10^{36})

OutputsVariable/Port

F0	Output (state)
----	----------------

Calculation Sequence

$F0 = GKl * [FIN - GKl * (F0 - AMA)]$	if $F0 > AMA$
$F0 = GKl * FIN$	if $AMI \leq F0 \leq AMA$
$F0 = GKl * [FIN - GKl * (F0 - AMI)]$	if $F0 < AMI$

SUBROUTINE IT ENTRY POINT 000051

STORAGE USED CODE(1) 000067; DATA(0) 000007; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 NEPR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 R 000000 EPS 0000 000003 INJPS

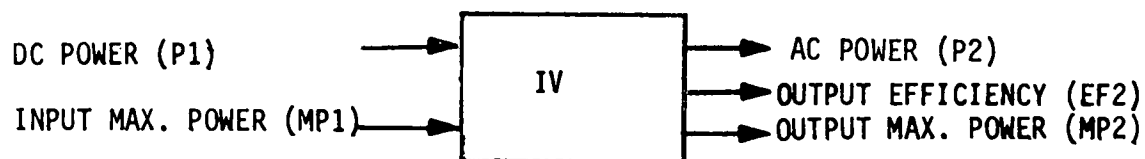
00100	1*	CIT				000000
00101	2*		SUBROUTINE IT(FO,FODOT,IFO,FIN,GKI,GKL,AMA,AHI)			000000
00101	3*	C	VERSION 2.	REVISED OCT 8 1976		000000
00101	4*	C				000000
00101	5*	C	PURPOSE - SIMULATION OF AN INTEGRATOR WITH SATURATION			000000
00101	6*	C				000000
00101	7*	C				000000
00101	8*	C	METHOD - SEE CODING			000000
00101	9*	C				000000
00101	10*	C				000000
00101	11*	C	LIMITATIONS - EXCESSIVELY HIGH VALUES OF GKL MAY RESULT IN POOR			000000
00101	12*	C	STEADY STATE CONVERGENCE			000000
00101	13*	C				000000
00101	14*	C				000000
00101	15*	C	WRITTEN BY - ADAM LLOYD	LATEST REVISION - NOV 75		000000
00101	16*	C				000000
00101	17*	C				000000
00101	18*	C	INPUT/OUTPUT LIST			000000
00101	19*	C				000000
00101	20*	C	FO INTEGRATOR OUTPUT	ANY	OUTPUT STATE	000000
00101	21*	C	FODOT OUTPUT DERIVATIVE	ANY	OUTPUT DERIV	000000
00101	22*	C	IFO INTEGRATOR CONTROL	---	PROGRAM VAR	000000
00101	23*	C	FIN FUNCTION INPUT	ANY	INPUT VAR	000000
00101	24*	C	GKI INTEGRATOR GAIN	ANY	INPUT PARAM	000000
00101	25*	C	GKL DERIVATIVE LIMITER GAIN	ANY	INPUT PARAM	000000
00101	26*	C	AMA UPPER LIMIT OF OUTPUT	ANY	INPUT PARAM	000000
00101	27*	C	WHERE DERIV. LIMITER STARTS			000000
00101	28*	C	AHI LOWER LIMIT OF OUTPUT	ANY	INPUT PARAM	000000
00101	29*	C	WHERE DERIV. LIMITER STARTS			000000
00103	30*		EPS=FIN			000000
00103	31*	C	----- PROVIDE DEFAULTS THAT ELLIMINATE SATURATION			000000
00104	32*		IF(AMA.E0..99999)AMA=1.E36			000001
00104	33*		IF(AHI.E0..99999)AHI=-1.E36			000006
00104	34*		IF(FO.GT.AMA)EPS = FIN - GKL*(FO-AMA)			000013
00104	35*		IF(FO.LT.AHI)EPS = FIN - GKL*(FO-AHI)			000024

00114	36*
00116	37*
00117	38*

IF(IFO.NE.O)FODOT=GKI+EPS
RETURN
END

000035
000042
000066

7.19 DC-AC INVERTER



This component models a solid state inverter/transformer. Power losses due to resistive heating and contact potential loss are modeled. A step-up transformer may also be needed to boost output voltage up to that of the bus. Default parameter values are based on rated power = 200 kw.

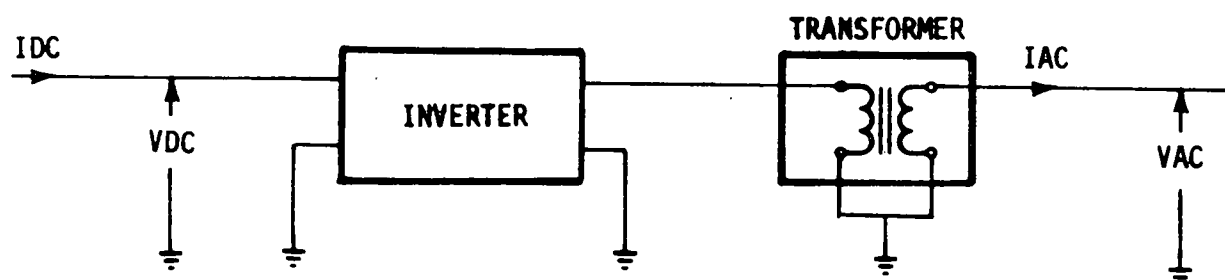


FIGURE 7.19 INVERTER FUNCTIONAL DIAGRAM

Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
P 1	DC input power	kw
RT	Transformer resistance (D = 0)	ohms
VDC	Rated DC voltage (D = 100)	volts
DI	Inverter contact potential (D = 0)	volts
RI	Inverter resistance (D = 0.005)	ohms
RAP	Rated input power	kw
EF 1	Input product efficiency	-
MP 1	Maximum input power	kw
CC	Inverter cost/year	\$

Outputs

<u>Variable/Port</u>			
P 2	AC output power		kw
IDC	DC input current		amps
PL	Power loss		kw
EF 2	Output product efficiency		-
MP 2	Maximum output power		kw

D - Default values supplied.

Calculation Sequence

If $P_1 \leq 0$, $P_2 = IDC = PL = 0$, $EFF = 1$ and go to 3)

- 1) Input and output current

$$IDC = P_1 * 1000 / VDC$$

$$IAC = \sqrt{6} * IDC / \pi$$

- 2) Power loss and output power

$$PL = (IDC * (DI + RI * IDC) + \sqrt{3} * RT * IAC^2) / 1000$$

$$P_2 = P_1 - PL$$

$$EFF = P_2 / P_1$$

$$P_2 \leq 0 \Rightarrow \text{Diagnostic, } EFF = 1$$

- 3) Efficiency and maximum power

$$EF2 = EF1 * EFF$$

$$MP2 = \text{MIN}(MP1, RAP) * EFF$$

- 4) Compute Costs

ENTRY POINT 000175

STORAGE USED CODE(1) 000261; DATA(0) 000046; BLANK COMMON(2) 000000

COMMON BLOCKS

```
0003      CIMPL      000002
0004      CTIME      000001
0005      CSIMUL      000010
0006      COST        000001
```

EXTERNAL REFERENCES (BLOCK, NAME)

0007	SOBT
0010	P.WDUS
0011	N1028
0012	NERR38

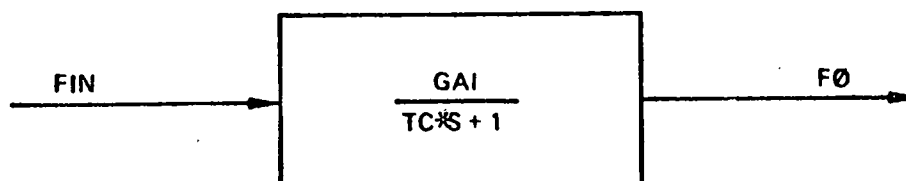
STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	00003G	100L	0001	000047	200L	0000	000004	208F	0001	000145	400L	0006	R	000000	CCI			
0005	000000	DUM	0000	R	000003	EFF	0000	R	000000	IAC	0003	I	000001	ICNT	0003	I	000000	IMPL
0000	000034	INJPS	0000	R	000001	PI	0004	R	000000	TIME	0005	R	000007	TMAX	0000	R	000002	TMAX1

ADDRESS	HEX	ASCII	DATA
00100	1*	CTV	000000
00101	2*	SUBROUTINE IV(P2,IDC,PL,EF2,MP2,P1,RT,VDC,DI,RI,RAP,EF1,MP1,CC)	000000
00101	3*	C	000000
00101	4*	C	000000
00101	5*	C	000000
00101	6*	C	000000
00101	7*	C	000000
00101	8*	C	000000
00101	9*	C	000000
00101	10*	C	000000
00101	11*	C	000000
00101	12*	C	000000
00101	13*	C	000000
00101	14*	C	000000
00101	15*	C	000000
00101	16*	C	000000
00101	17*	C	000000
00101	18*	C	000000
00101	19*	C	000000
00101	20*	C	000000
00101	21*	C	000000
00101	22*	C	000000
00101	23*	C	000000

G0101	24*	C	RAP -RATED OUTPUT POWER, KW	000000
G0101	25*	C	EF1 -INPUT PRODUCT EFFICIENCY	000000
G0101	26*	C	MP1 -MAXIMUM INPUT POWER, KW	000000
G0101	27*	C	CC -INVERTER COST/YEAR	000000
G0101	28*	C		000000
G0103	29*		COMMON /CIMPL/IMPL,ICNT/CTIME/TIME/CSIMUL/DUM(7),THAX/COST/CCI	000000
G0104	30*		REAL IDC,MP2,MP1,IAC	000000
G0105	31*		DATA PI/3.14159/	000000
G0105	32*	C		000000
G0107	33*		IF(IMPL.GT.0) GO TO 100	000000
G0111	34*		IF(RT.EQ..99999)RT=0.	000002
G0113	35*		IF(VDC.EQ..99999)VDC=100.	000006
G0115	36*		IF(DI.EQ..99999)DI=0.	000013
G0117	37*		IF(RI.EQ..99999)RI=.005	000017
G0121	38*		THAX1=THAX*.99999	000024
G0121	39*	C		000024
G0121	40*	C	COMPUTE INPUT AND OUTPUT CURRENT	000024
G0121	41*	C		000024
G0122	42*		100 IF(P1.GT.0.)GO TO 200	000030
G0124	43*		P2=0.	000032
G0125	44*		IDC=0.	000033
G0126	45*		PL=0.	000034
G0127	46*		EF2=EF1	000035
G0130	47*		MP2=AMIN1(MP1,RAP)	000037
G0131	48*		GO TO 400	000045
G0132	49*		200 IDC=P1*1000./VDC	000047
G0133	50*		IAC=SQRT(6.)*IDC/PI	000052
G0133	51*	C		000052
G0133	52*	C	POWER LOSS AND OUTPUT POWER	000052
G0133	53*	C		000052
G0134	54*		PL=(IDC*(DI+RI+IDC)+SQRT(3.)*RT*IAC*IAC)/1000.	000060
G0135	55*		P2=P1-PL	000075
G0136	56*		EFF=P2/P1	000077
G0136	57*	C		000077
G0136	58*	C	EFFICIENCY AND MAXIMUM POWER	000077
G0136	59*	C		000077
G0137	60*		EF2=EF1*EFF	000101
G0140	61*		MP2=AMIN1(MP1,RAP)	000103
G0141	62*		MP2=MP2*EFF	000111
G0142	63*		IF(P2.GT.0.)GO TO 400	000114
G0142	64*	C		000114
G0144	65*		EF2=EF1	000117
G0145	66*		MP2=AMIN1(MP1,RAP)	000121
G0146	67*		IF(IMPL.EQ.2)WRITE(6,208)PL,P1	000123
G0153	68*		208 FORMAT(1H0,14HIV POWER LOSS ,F12.3,21H EXCEEDS INPUT POWER ,F12.3,	000135
G0153	69*		128H CHECK RATED DC VOLTAGE VDC)	000135
G0154	70*		IF(IMPL.EQ.2)ICNT=ICNT+1	000135
G0156	71*		P2=0.	000143
G0156	72*	C		000143
G0157	73*		400 IF(IMPL.LE.1)RETURN	000145
G0161	74*		IF(TIME.LT.THAX1)RETURN	000153
G0163	75*		CCI=CCI+CC	000162
G0164	76*		RETURN	000165
G0165	77*		END	000260

7.20 FIRST ORDER LAG



Inputs

<u>Parameter/Port</u>	<u>Description</u>
FIN	Input quantity
GAI	Gain
TC	Time constant ¹ (hours)
F0	Output variable (state)

Calculation Sequence

$$\dot{F0} = (GAI * FIN - F0) / TC$$

NOTE: d.c. gain = GAI; time constant = TC

infinite frequency gain = 0

pole location = $\frac{1}{TC}$ rad/sec.

¹ If TC = 0, then F0 = FIN * GAI

SUBROUTINE LA ENTRY POINT 000026

STORAGE USED CODE(1) 000045; DATA(0) 000010; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIO 000003

EXTERNAL REFERENCES (BLOCK, NAME)

0004 NERR35

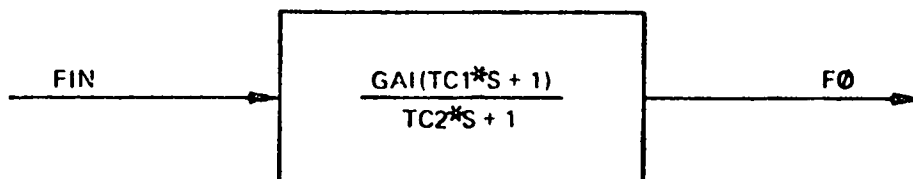
STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000010 10L 0003 000002 IDIAG 0000 000000 INJPS 0003 000000 IREAD 0003 000001 IWRITE

00100	1*	CLA				000000
00101	2*		SUBROUTINE LA(F0,FODOT,IFO,FIN,GAI,TC)			000000
00101	3*	C				000000
00101	4*	C	PURPOSE - TO SIMULATE FIRST ORDER LAG	F0	GAI	000000
00101	5*	C		----	-----	000000
00101	6*	C		FIN	(1.+TC*S)	000000
00101	7*	C				000000
00101	8*	C				000000
00101	9*	C	METHOD - SEE CODING			000000
00101	10*	C				000000
00101	11*	C				000000
00101	12*	C	WRITTEN BY - ADAM LLOYD	LATEST REVISION	NOV 75	000000
00101	13*	C				000000
00101	14*	C				000000
00101	15*	C	INPUT/OUTPUT LIST			000000
00101	16*	C				000000
00101	17*	C	F0	TRANSFER FUNCTION OUTPUT	ANY	OUTPUT STATE
00101	18*	C	FODOT	TRANSFER FUNCTION OUTPUT DERIV.	ANY	OUTPUT STATE
00101	19*	C	IFO	INTEGERATOR CONTROL	---	PROGRAM VAR
00101	20*	C	FIN	TRANSFER FUNCTION INPUT	ANY	INPUT VAR
00101	21*	C	GAI	TRANSFER FUNCTION GAIN	---	INPUT PARAM
00101	22*	C	TC	TIME CONSTANT	SECS	INPUT PARAM
00103	23*		COMMON/CIO/IREAD,IWRITE,IDIAG			000000
00104	24*		IF(TC.NE.C.) GO TO 10			000000
00106	25*		F0= GAI*FIN			000001
00107	26*		RETURN			000004
00110	27*		10 IF(IFO.NE.0) FODOT=(GAI*FIN-F0)/TC			000010
00112	28*		RETURN			000016
00113	29*		END			000044



7.21 LEAD LAG

Inputs

<u>Parameter/Port</u>	<u>Description</u>
FIN	Input quantity
TC1	Numerator time constant (hours)
TC2	Denominator time constant (hours)
GAI	Gain

Outputs

<u>Variable/Port</u>	
X1	Intermediate quantity (state)
F0	Output quantity (variable)

Calculation Sequence

$$F0 = (X1 + FIN*TC1*GAI)/TC2$$

$$\dot{X1} = GAI*FIN - F0$$

NOTE: d.c. gain = GAI

$$\text{infinite gain} = \frac{GAI*TC1}{TC2}$$

$$\text{zero location} = -\frac{1}{TC1}, \text{ rad/sec}$$

$$\text{pole location} = -\frac{1}{TC2}, \text{ rad/sec}$$

SUBROUTINE LL ENTRY POINT 000022

STORAGE USED CODE(1) 000031; DATA(0) 000004; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIO 000003

EXTERNAL REFERENCES (BLOCK, NAME)

0004 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0003 000002 IDIAG 0000 000000 INJPS 0003 000000 IREAD 0003 000001 IWRITE

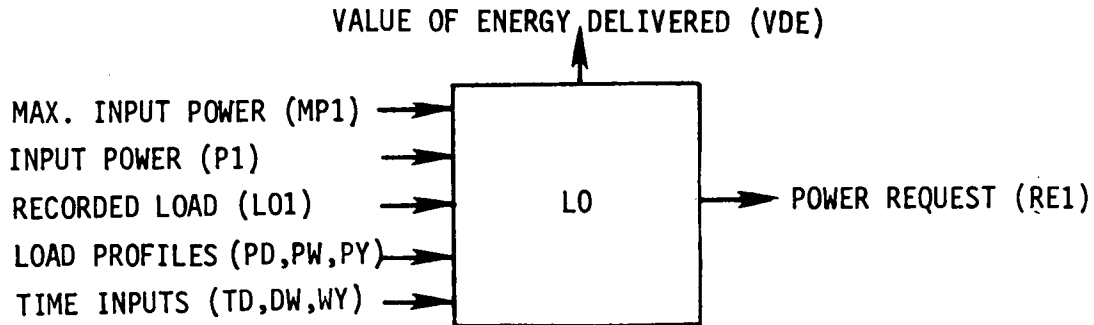
00100	1*	CLL				000000
00101	2*		SUBROUTINE LL(X1,X1DOT,IX1,FO,FIN,TC1,TC2,GAI)			000000
00101	3*	C				000000
00101	4*	C	PURPOSE - TO SIMULATE LEAD LAG TRANSFER FUNCTION			000000
00101	5*	C				000000
00101	6*	C	FO = GAI*(1.+TC1*S)			000000
00101	7*	C	----- = -----			000000
00101	8*	C	FIN (1.+TC2*S)			000000
00101	9*	C				000000
00101	10*	C				000000
00101	11*	C	METHOD - SELF EXPLANATORY			000000
00101	12*	C				000000
00101	13*	C				000000
00101	14*	C	LIMITATIONS - NONE			000000
00101	15*	C				000000
00101	16*	C				000000
00101	17*	C	WRITTEN BY - ADAM LLOYD LATEST REVISION NOV 75			000000
00101	18*	C				000000
00101	19*	C				000000
00101	20*	C	INPUT/OUTPUT LIST			000000
00101	21*	C				000000
00101	22*	C	X1 STATE VARIABLE	ANY	OUTPUT STATE	000000
00101	23*	C	X1DOT STATE VARIABLE DERIVATIVE	ANY	OUTPUT STATE	000000
00101	24*	C	IX1 INTEGRATOR CONTROL	---	PROGRAM VAR	000000
00101	25*	C	FO TRANSFER FUNCTION OUTPUT	ANY	OUTPUT VAR	000000
00101	26*	C	FIN TRANSFER FUNCTION INPUT	ANY	INPUT VAR	000000
00101	27*	C	TC1 TIME CONSTANT (NUMERATOR)	SECS	INPUT PARAM	000000
00101	28*	C	TC2 TIME CONSTANT (DENOMINATOR)	SECS	INPUT PARAM	000000
00101	29*	C	GAI TRANSFER FUNCTION GAIN	---	INPUT PARAM	000000
0010	30*		COMMON/CIO/IREAD,IWRITE,IDIAG			000000
0010	31*		FO=(X1*FIN*TC1*GAI)/TC2			000000

CO105	32*
CO107	33*
CO110	34*

IF(IX1.NE.0)X1DOT= GAI+FIN-FO
RETURN
END

000005
C0C013
C0C030

7.22 ELECTRICAL LOAD



This component represents electrical load either by a user-specified data file time history or by a set of random numbers with user-specified daily, weekly, and yearly average profiles and user-specified random variation. It also computes the value of the power delivered to the load by the system. This value delivered is determined from a user-specified value per kwh. This value may be input in tabular form as a function of time of day, time of year, or any other system parameter.

If the user selects to have the electrical load represented by random numbers, then the load (L02) is generated from the following equation:

Basic Equation

$$L02 = \left[PD(TD) + CN(t) \right] * PW(DW) * PY(WY) * NC$$

where

PD, PW, PY are the daily, weekly, and yearly profiles, respectively, and TD, DW, WY are the time of day, day of the week, and week of the year, respectively. NC is a normalizing constant.

CN is a colored noise term with user-specified correlation time, standard deviation and mean.

<u>Tables</u>	<u>Description</u>	<u>Units</u>
PD	Daily profile (tabular with TD)	kw
PW	Weekly profile (tabular with DW)	arbitrary
PY	Yearly profile (tabular with WY)	arbitrary

Inputs

Parameter/Port

P	1	Power delivered	kw
MP	1	Maximum Input Power deliverable ($D = 1 \times 10^{10}$)	kw
NC		Normalizing constant	
VE		Value of Electrical Energy	\$/kwh
LØ	1	Electrical load data file input	kw
TD		Time of day	-
DW		Day of week	-
WY		Week of year	-
CT		Correlation time of random noise	hr
MN,STD		Mean ($D = 0$) and std. deviation of random noise	kw
EF	1	Input Power Efficiency	-

Outputs

Variable/Port

RE	1	Power request	kw
VDE		Value of energy delivered (state)	\$
LØ	2	Electrical load	kw
TIM		Last time a random sample was used	hr
CN		Colored noise sample	kw

Statistics

SRE	Total energy requested	kwh
SDE	Total energy delivered	kwh
PC	Percentage of load met	-

D - Default values supplied

Calculation Sequence

1) Initialize CN(0) (first pass)

2) Check for data file input

 If L01 = .99999 go to 3)

 L02 = L01 and go to 5)

3) Generate colored noise CN

 If TIM = TIME go to 5)

$$A = \begin{cases} \exp(-\Delta/CT), & CT > 0, \Delta = \text{integration step size, hr} \\ 0, & CT = 0 \end{cases}$$

$$CN = A*CN + W,$$

Where W is white noise generated by RN with

$$\text{Mean} = MN * (1-A) \text{ and standard deviation} = \text{STD} * \sqrt{1-A^2}$$

4) Compute L02

$$L02 = (PD(TD) + CN) * PW(DW) * PY(WY) * NC$$

$$TIM = TIME$$

5) Power request and value delivered

$$RE = \text{MIN}(MP, L02) / EF1$$

6) Statistics

$$VDE = P1 * VE$$

$$SRE = SRE + L02 * \Delta / 2$$

$$SDE = SDE + P1 * \Delta / 2$$

$$PC = 100. * SDE / SRE$$

ENTRY POINT 000344

COMMON BLOCKS

EXTERNAL REFERENCES (BLOCK, NAME)

0007	RN
0010	TBLU1
0011	EXP
0012	SQRT
0013	NCRR3S

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0301	CC0062	10L	0001	000070	100L	0001	000233	150L	0000 R	000005	A	0C00 R	000000	AX
0006	0C0200	CC	0006 R	000004	COE	0006	000001	CM	0006	000002	CO	0006 R	000005	CRE
0006 R	000003	CV	0000	000011	DLO	0000	000000	DUM	0003 I	000000	IMPL	0000	000022	INJPS
0000 I	000001	ND	0000 I	000002	NW	0000 I	000003	NY	0010 R	000000	TBLU1	0005 R	000000	TIME
0004 R	000006	TINC	0004 R	000007	TMAX	0000 R	000004	TMAX1	0000 R	000010	W	0000 R	000012	WLO
0000 R	000006	WMN	0000 R	000007	WSD	0000 R	000013	YLO						

```

00100      1*      CLO
00101      2*      SUBROUTINE LO (PD,PW,PY,VDE,DVD,IVD,RE,LOZ,SRE,SDE,PC,TIMO,XN,
00101      3*      1 TD,DW,WY,XNC,CT,XMN,STD,VE,LO1,PHAX,PO,EF)
00101      4*      C
00101      5*      C PURPOSE GENERATE ELECTRICAL LOAD FROM DAILY, WEEKLY, YEARLY AND
00101      6*      C RANDOM PROFILE DATA AND EVALUATE PERFORMANCE STATISTICS
00101      7*      C
00101      8*      C METHOD COLORED NOISE IS ADDED TO A MEAN DAILY PROFILE AND MULTIPLIED
00101      9*      C BY WEEKLY AND YEARLY WEIGHTING FCNS. POWER REQUESTED IS EITHER
00101     10*      C THE GENERATED LOAD OR THE MAX. POWER DELIVERABLE.
00101     11*      C
00101     12*      C WRITTEN BY A.W.WARREN
00101     13*      C
00101     14*      C CALL SEQUENCE
00101     15*      C TABLES
00101     16*      C PD - MEAN DAILY PROFILE, KW
00101     17*      C PW - MEAN WEEKLY PROFILE, -
00101     18*      C PY - MEAN YEARLY PROFILE, -
00101     19*      C

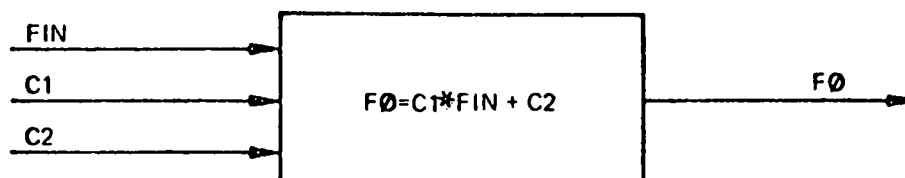
```

[illegible]**10**

00101	20*	C	OUTPUTS	000002
00101	21*	C	VDE - VALUE OF ENERGY DELIVERED (STATE), S	000002
00101	22*	C	DVD - DERIVATIVE OF VDE	000002
00101	23*	C	IVD - INDICATOR FOR VDE	000002
00101	24*	C	RE - POWER REQUEST, KW	000002
00101	25*	C	LO2 - ELECTRICAL LOAD DEMAND, KW	000002
00101	26*	C	SRE - SUM OF ENERGY DESIRED, KWH	000002
00101	27*	C	SDE - SUM OF ENERGY DELIVERED, KWH	000002
00101	28*	C	PC - CUMULATIVE PERCENT OF LOAD DELIVERED, -	000002
00101	29*	C	TIMO - LAST TIME A RANDOM SAMPLE WAS USED, HR	000002
00101	30*	C	XN - COLORED NOISE SAMPLE, KW	000002
00101	31*	C		000002
00101	32*	C	INPUTS	000002
00101	33*	C	TD - TIME OF DAY, HR	000002
00101	34*	C	DW - DAY OF WEEK (1-7)	000002
00101	35*	C	WY - WEEK OF YEAR (1-52)	000002
00101	36*	C	XNC - NORMALIZING CONSTANT, -	000002
00101	37*	C	CT - CORRELATION TIME OF RANDOM NOISE, HR	000002
00101	38*	C	XMN - MEAN OF RANDOM NOISE, KW	000002
00101	39*	C	STD - STANDARD DEVIATION OF RANDOM NOISE, KW	000002
00101	40*	C	VE - VALUE OF ELECTRICAL ENERGY, \$/KWH	000002
00101	41*	C	LO1 - ELECTRICAL LOAD DATA FILE INPUT, XW	000002
00101	42*	C	PHAX - MAX. INPUT POWER DELIVERABLE, KW	000002
00101	43*	C	PO - POWER DELIVERED TO LOAD, KW	000002
00101	44*	C	EF - INPUT POWER EFFICIENCY	000002
00101	45*	C		000002
00103	46*		DIMENSION PD(1),PW(1),PY(1)	000002
00104	47*		REAL LO1,LO2	000002
00105	48*		COMMON /CIMPL/ IMPL /CSIMUL/ DUM(6),TINC,TMAX/CTIME/TIME	000002
00106	49*		COMMON /COST/CC,CH,CO,CV,CDE,CRE	000002
00107	50*		DATA AX/.99999/	000002
00107	51*	C		000002
00107	52*	C	INITIALIZATION	000002
00107	53*	C		000002
00111	54*		ND = PD(2)	000002
00112	55*		NW = PW(2)	000011
00113	56*		NY = PY(2)	000020
00114	57*		IF(IMPL.GT.0) GO TO 10	000027
00116	58*		IF(XMN.EQ. .99999)XMN=0.	000032
00120	59*		TMAX1 = TMAX+.99999	000036
00121	60*		TIMO=-1.	000041
00122	61*		SRE =0.0	000043
00123	62*		SDE =0.0	000044
00124	63*		PC =0.0	000045
00125	64*		CALL RN(XN,AX,STD,XMN)	000046
00126	65*		IF(PHAX.EQ. .99999) PHAX = 1.E10	000054
00126	66*	C		000054
00126	67*	C	CHECK FOR DATA FILE INPUT	000054
00126	68*	C		000054
00130	69*		10 IF(LO1.EQ. .99999) GO TO 100	000062
00132	70*		LO2 = LO1	000064
00133	71*		GO TO 150	000066
00133	72*	C		000066
00133	73*	C	GENERATE COLORED NOISE SAMPLE XN	000066
00133	74*	C		000066
00133	75*		100 IF(TIMO.EQ.TIME) GO TO 150	000070
00133	76*		A=0.	000072

00137	77*	IF(CT.GT.0.) A = EXP(-TINC/CT)	000073
00141	78*	WMN = XMN*(1.-A)	000116
00142	79*	WSD = STD*SORT(1.-A*A)	000122
00143	80*	CALL RN(W,AX,WSD,WMN)	000133
00144	81*	XN = XN*A + W	000141
00144	82*	C COMPUTE ELECTRICAL LOAD DEMAND	000141
00144	83*	C	000141
00145	84*	DLO = TBLUI(TD,PD(4),PD(ND+4),1,-ND)	000145
00146	85*	WLO = TBLUI(DW,PW(4),PW(NW+4),1,-NW)	000164
00147	86*	YLO = TBLUI(WY,PY(4),PY(NY+4),1,-NY)	000203
00150	87*	LO2 = (DLO*XN)*WLO + YLO*XNC	000222
00151	88*	TIME = TIME	000230
00152	89*	150 RE = AMIN1(PMAX,LO2)/EF	000233
00152	90*	C PERFORMANCE STATISTICS	000233
00152	91*	C	000233
00153	92*	IF(IMPL.LE.1) RETURN	000241
00155	93*	IF(IYN.NE.0) DVD = P0*VE	000250
00157	94*	SRE = SRE + LO2*0.5*TINC	000261
00160	95*	SDE = SDE + P0*0.5*TINC	000266
00161	96*	IF(SRE.GT.0.) PC = 100.*SDE/SRE	000271
00161	97*	C	000271
00163	98*	IF(TIME.LT.TMAX1) RETURN	000300
00165	99*	CV = CV + VDE	000307
00166	100*	CDE = CDE + SDE - P0*0.5*TINC	000312
00167	101*	CRE = CRE + SRE - LO2*0.5*TINC	000316
00170	102*	RETURN	000325
00171	103*	END	000470

7.23 MULTIPLY AND ADD



Inputs

<u>Parameter/Port</u>	<u>Description</u>
FIN	Input quantity
C1	Input quantity
C2	Input quantity

Outputs

<u>Variable/Port</u>	
F0	Output quantity

Calculation Sequence

$$F0 = C1 * FIN + C2$$

SUBROUTINE MA

ENTRY POINT 000012

STORAGE USED CODE(1) 000016; DATA(0) 000004; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 NERR35

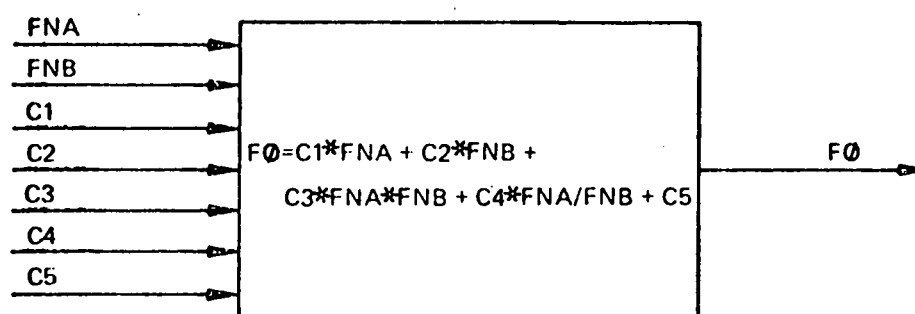
STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 000000 INJPS

00100	1*	CMA				000000
00101	2*		SUBROUTINE MA(F0,FIN,C1,C2)			000000
00101	3*	C				000000
00101	4*	C	PURPOSE - TO SIMULATE THE EQUATION	OUTPUT=C1*INPUT + C2		000000
00101	5*	C				000000
00101	6*	C				000000
00101	7*	C	METHOD - SEE CODING			000000
00101	8*	C				000000
00101	9*	C				000000
00101	10*	C	WRITTEN BY - ADAM LLOYD	LATEST REVISION	NOV 75	000000
00101	11*	C				000000
00101	12*	C				000000
00101	13*	C	LIMITATIONS - NONE			000000
00101	14*	C				000000
00101	15*	C				000000
00101	16*	C	INPUT/OUTPUT LIST			000000
00101	17*	C				000000
00101	18*	C	F0	OUTPUT VARIABLE	ANY	000000
00101	19*	C	FIN	INPUT VARIABLE	ANY	000000
00101	20*	C	C1	CONSTANT MULTIPLIER	---	000000
00101	21*	C	C2	CONSTANT ADDITION	---	000000
00103	22*		F0=C1*FIN + C2			000000
00104	23*		RETURN			000003
00105	24*		END			000015

MA

7.24 MULTIPLY, DIVIDE, AND ADD



Inputs

<u>Parameter/Port</u>	<u>Description</u>
FNA	Input quantity
FNB	Input quantity
C1	Input quantity
C2	Input quantity
C3	Input quantity
C4	Input quantity
C5	Input quantity.

Outputs

<u>Variable/Port</u>	
F0	Output quantity

Calculation Sequence

$$F0 = C1 * FNA + C2 * FNB + C3 * FNA * FNB + C4 * FNA / FNB + C5$$

SUBROUTINE MB ENTRY POINT 000051

STORAGE USED CODE(1) 000064; DATA(0) 000023; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 ERMESS 000002
0004 C10 000003

EXTERNAL REFERENCES (BLOCK, NAME)

0005 NWDUS
0006 N102S
0007 NERR3S

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	C00030	10L	0000	000300	20F	0001	000042	30L	0004	000002	IDTAG	0003	000001	IERR
0003	000000	IFATAL	0000	000015	INJPS	0004	000000	IREAD	0004	I	000001	IWRITE		

00100	1*	CMB												000000
00101	2*		SUBROUTINE MB(F0,FNA,FNB,C1,C2,C3,C4,C5)											000000
00101	3*	C												000000
00101	4*	C	PURPOSE - TO SIMULATE THE EQUATION	$Y=C1*XA+C2*XB+C3*XA*XB+C4*XA/XR+C5$										000000
00101	5*	C												000000
00101	6*	C												000000
00101	7*	C	WRITTEN BY - GEORGE DULEBA		LATEST REVISION	MAY 76								000000
00101	8*	C												000000
00101	9*	C												000000
00101	10*	C	LIMITATIONS - IF FNB=0 DURING DIVISION, FNB IS SET TO E-20.											000000
00101	11*	C	DIAGNOSTIC MESSAGE IS GIVEN.											000000
00101	12*	C												000000
00101	13*	C												000000
00101	14*	C	INPUT/OUTPUT LIST											000000
00101	15*	C												000000
00101	16*	C	F0	OUTPUT VARIABLE	ANY		OUTPUT	VAR						000000
00101	17*	C	FNA	INPUT VARIABLE A	ANY		INPUT	VAR						000000
00101	18*	C	FNB	INPUT VARIABLE B	ANY		INPUT	VA						000000
00101	19*	C	C1	MULTIPLIER 1	ANY		INPUT	VAR						000000
00101	20*	C	C2	MULTIPLIER 2	ANY		INPUT	VAR						000000
00101	21*	C	C3	MULTIPLIER 3	ANY		INPUT	VAR						000000
00101	22*	C	C4	MULTIPLIER 4	ANY		INPUT	VAR						000000
00101	23*	C	C5	ADDITIVE VARIABLE	ANY		INPUT	VAR						000000
00101	24*	C												000000
00101	25*	C												000000
00103	26*		COMMON/ERMESS/IFATAL,IERR											000000
00104	27*		COMMON/C10/IREAD,IWRITE,IDTAG											000000

MB

```

00105      28*      FO= C1*FNA + C2*FNB + C3*FNA*FNB + C5
00106      29*      IF(C4.EQ.0.99999) GO TO 30
00110      30*      IF(FNB.EQ.0.) GO TO 10
00112      31*      FO= FO + C4*FNA/FNB
00113      32*      RETURN
00114      33*      10  WRITE(IWRITE,20)
00116      34*      20  FORMAT(/,30X, 53HWARNING- DIVISOR IN MB EQUALS 0., HAS BEEN SET=1.
00116      35*      2E-20)
00117      36*      FO= FO + C4*FNA*1.E+20
00120      37*      30  RETURN
00121      38*      END

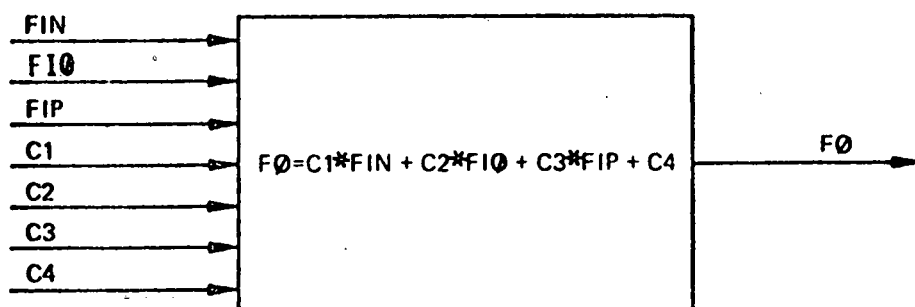
```

```

000000
000012
000015
000017
000024
000030
000034
000034
000034
000042
000063

```

7.25 MULTIPLY AND ADD



Inputs

<u>Parameter/Port</u>	<u>Description</u>
FIN	Input quantity
FI0	Input quantity
FIP	Input quantity
C1	Input quantity
C2	Input quantity
C3	Input quantity
C4	Input quantity

Outputs

<u>Variable/Port</u>	
F0	Output quantity

Calculation Sequence

$$F0 = C1*FIN + C2*FI0 + C3*FIP + C4$$

SUBROUTINE MC ENTRY POINT 000020

STORAGE USED CODE(1) 000024; DATA(0) 000004; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

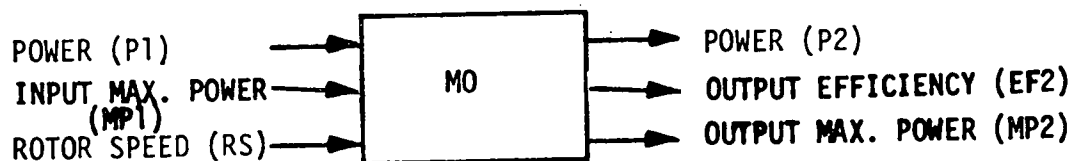
0003 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 000000 INJPS

00100	1*	C	CMC					000000
00101	2*			SUBROUTINE MC(F0,FIN,FIO,FIP,C1,C2,C3,C4)				000000
00101	3*	C						000000
00101	4*	C		PURPOSE - TO SIMULATE THE EQUATION $F0=C1*FIN+C2*FIO+C3*FIP+C4$				000000
00101	5*	C						000000
00101	6*	C						000000
00101	7*	C		METHOD - SEE CODING				000000
00101	8*	C						000000
00101	9*	C						000000
00101	10*	C		WRITTEN BY - ADAM LLOYD	LATEST REVISION	NOV 75		000000
00101	11*	C						000000
00101	12*	C						000000
00101	13*	C		LIMITATIONS - NONE				000000
00101	14*	C						000000
00101	15*	C						000000
00101	16*	C		INPUT/OUTPUT LIST				000000
00101	17*	C						000000
00101	18*	C	F0	OUTPUT VARIABLE	ANY	OUTPUT	VAR	000000
00101	19*	C	FIN	INPUT VARIABLE	ANY	INPUT	VAR	000000
00101	20*	C	FIO	INPUT VARIABLE	ANY	INPUT	VAR	000000
00101	21*	C	FIP	INPUT VARIABLE	ANY	INPUT	VAR	000000
00101	22*	C	C1	CONSTANT MULTIPLIER	---	INPUT	PARAM	000000
00101	23*	C	C2	CONSTANT MULTIPLIER	---	INPUT	PARAM	000000
00101	24*	C	C3	CONSTANT MULTIPLIER	---	INPUT	PARAM	000000
00101	25*	C	C4	CONSTANT ADDITION	---	INPUT	PARAM	000000
00103	26*			$F0=C1*FIN+C2*FIO+C3*FIP+C4$				000000
00104	27*			RETURN				000011
00105	28*			END				000023

7.26 AC INDUCTION MOTOR



The induction motor produces mechanical power and torque proportional to slip speed, i.e. power and torque approach zero as the rotor approaches synchronous speed. Two power losses are modeled: a constant multiplicative term due to resistive heating and an additive term due to mechanical friction. Default parameters are based on a conventional squirrel-cage induction motor/generator machine.

Basic Equations

$$P2 = EE * P1 + DA * RS^2 * C$$

where

$P1, P2$ = input and output power

EE = electrical efficiency

DA = mechanical damping

C = conversion constant

Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
P 1	Input power	kw
DA	Mechanical damping (D = 0)	joule-sec
RS	Rotor speed	rpm
RSY	Synchronous rotor speed (D = 1800)	rpm
SR	Stator resistance (D = 8/RAP)	ohms
V0	Rated input voltage (D = 400)	volts
RAP	Rated input power	kw
RAS	Rated power slip (D = 0.05)	-
EF 1	Input product efficiency	-
MP 1	Maximum input power (D = 1×10^8)	kw
CC	Capital cost/year	\$
CM	Maintenance cost/year	\$

Outputs

<u>Variable/Port</u>		
P 2	Output mechanical power	kw
EE	Electrical efficiency	-
T0	Mechanical torque	ft-lb
PL	Power loss	kw
EF 2	Output product efficiency	-
MP 2	Output maximum power	kw

Statistics

MT	Maximum torque	ft-lb
MPN	Maximum output power/rated power	-
SP	Output energy sum	kwh

D - Default values supplied.

Calculation Sequence

- 1) Compute electrical efficiency (first pass only)

$$I_{RAT} = RAP * 1000 / V_0$$

$$EE = 1 - SR * I_{RAT}^2 / RAP * 1000$$

- 2) Diagnostics

$$P_1 > RAP \Rightarrow \text{DIAGNOSTIC}$$

$$SLIP = 1 - RS / RSY > RAS \Rightarrow \text{DIAGNOSTIC}$$

- 3) Output power and power loss

$$\omega = RS * (2\pi / 60)$$

$$P_2 = EE * P_1 - DA * \omega^2 / 1000$$

$$PL = P_1 - P_2$$

- 4) If $P_2 > 0$ go to 5)

$$P_1 > 0 \Rightarrow \text{DIAGNOSTIC}$$

$$EF_2 = EF_1, MP_2 = \min(MP_1, RAP)$$

Go to 7)

- 5) Compute torque

$$T_0 = P_2 * 1000 / \omega * k$$

$$k = 1.3558 \text{ joules/ft-lb}$$

Calculation Sequence Cont.

6) Efficiency and maximum output power

$$EF2 = EF1 * (P2/P1)$$

$$MP2 = \text{MIN}(MP1, RAP) * (P2/P1)$$

7) Compute Statistics and Costs

ENTRY POINT 000312

STORAGE USED CODE(1) 000434; DATA(0) 000102; BLANK COMMON(2) 000000

COMMON BLOCKS

```
0003      CIMPL      000002
0004      CTIME      000001
0005      CSTIMUL     000010
0006      COST        000010
```

EXTERNAL REFERENCES (BLOCK, NAME)

0007 NMDUS
0010 N102S
0011 NEPR3S

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000062	100L	0001	000106	200L	0000	000004	208F	0001	000135	300L	0000	000017	308F
0001	000213	400L	0009	000032	408F	0001	000201	409L	0001	000235	500L	0006 R	000009	CCY
0006 R	000001	CMI	0006	000002	COP	0005 R	000000	NUM	0003 I	000001	ICNY	0003 I	000000	IMPL
0000	000066	INJPS	0000 R	000003	OMEGA	0000 R	000002	SLIP	0006	000004	TDE	0006 R	000000	TIME
0000 R	000001	TINC	0006	000005	TLD	0005 R	000007	TMAX	0000 R	000000	TMAX1	0006	000007	UTD
0006	000006	UTV	0006	000003	VDE									

```

00100      1*      CMO
00101      2*      SUBROUTINE MO(P2,EE,TO,PL,EF2,MP2,MT,MPN,SP,
00101      3*      1      P1,DA,RS,RSY,SR,VO,RAP,RAS,EF1,MP1,CC,CM)
00101      4*      C
00101      5*      C      PURPOSE      AC INDUCTION MOTOR MODEL
00101      6*      C
00101      7*      C      METHOD      MECHANICAL POWER AND TORQUE CALCULATED
00101      8*      C      FROM INPUT AC POWER AND ROTOR SPEED
00101      9*      C
00101     10*      C      WRITTEN BY Y.K.CHAN      VERSION 1, JUNE 13, 1977
00101     11*      C
00101     12*      C      CALL SEQUENCE
00101     13*      C      OUTPUTS
00101     14*      C      P2      -OUTPUT MECHANICAL POWER,KW
00101     15*      C      EE      -ELECTRICAL EFFICIENCY
00101     16*      C      TO      -MECHANICAL TORQUE,FT-LB
00101     17*      C      PL      -POWER LOSS,KW
00101     18*      C      EF2     -OUTPUT POWER EFFICIENCY
00101     19*      C      MP2     -OUTPUT MAXIMUM POWER,KW
00101     20*      C      STATISTICS
00101     21*      C      MT      -MAXIMUM TORQUE,FT-LB

```

W O

00101	22*	C	MPN -MAXIMUM OUTPUT POWER/RATED POWER	000000
00101	23*	C	SP-OUTPUT POWER SUM	000000
00101	24*	C	INPUTS	000000
00101	25*	C	P1 -INPUT POWER,KW	000000
00101	26*	C	DA -MECHANICAL DAMPING,JOULE-SEC	000000
00101	27*	C	RS -ROTOR SPEED,RPM	000000
00101	28*	C	RSY -SYNCHRONOUS ROTOR SPEED,RPM	000000
00101	29*	C	SR -STATOR RESISTANCE,OHMS	000000
00101	30*	C	VO -RATED INPUT VOLTAGE,VOLTS	000000
00101	31*	C	RAP -RATED INPUT POWER,KW	000000
00101	32*	C	RAS -RATED PWER SLIP	000000
00101	33*	C	EF1 -INPUT PRODUCT EFFICIENCY	000000
00101	34*	C	MP1 -MAXIMUM INPUT POME,KW	000000
00101	35*	C	CC -CAPITAL COST/YEAR,\$	000000
00101	36*	C	CM -MAINTENANCE COST/YEAR,\$	000000
00101	37*	C		000000
00103	38*		COMMON /CIMPL/IMPL,ICNT/CTIME/TIME/CSIMUL/DUM(7),TMAX	000000
00103	39*	X	/COST/CCI,CHI,COP,VDE,TDE,TLO,UTV,UTD	000000
00104	40*		REAL MP2,MT,MPN,MP1	000000
00104	41*	C		000000
00105	42*		IF(IMPL.GT.0)GO TO 100	000000
00107	43*		IF(DA.EQ..99999)DA=0.	000002
00111	44*		IF(RSY.EQ..99999)RSY=1800.	000006
00113	45*		IF(SR.EQ..99999)SR=8./RAP	000013
00115	46*		IF(VO.EQ..99999)VO=400.	000021
00117	47*		IF(MP1.EQ..99999)MP1=1.E8	000026
00121	48*		IF(RAS.EQ..99999)RAS=.05	000033
00123	49*		TMAX1=TMAX*.99999	000040
00124	50*		MT=C.	000043
00125	51*		MPN=0.	000044
00126	52*		SP=0.	000045
00127	53*		TINC=DUM(7)*.5	000046
00127	54*	C		000046
00127	55*	C	COMPUTE ELECTRICAL EFFICIENCY	000046
00127	56*	C		000046
00130	57*		EE=1.-SR*RAP*1000./(VO*VO)	000051
00131	58*	100	IF(P1.LE.RAP)GO TO 200	000062
00133	59*		IF(IMPL.EQ.2)WRITE(6,208)P1,RAP	000065
00140	60*	208	FORMAT(1H0,18H MOTOR INPUT POWER,F12.3,23H .GT.RATED INPUT POWER ,	000077
00140	61*	1	F12.3)	000077
00141	62*		IF(IMPL.EQ.2)ICNT=ICNT+1	000106
00143	63*	200	SLIP=1.-(RS/RSY)	000111
00144	64*		IF(SLIP.LE.PAS)GO TO 300	000114
00146	65*		IF(IMPL.EQ.2)WRITE(6,308)SLIP,RAS	000126
00153	66*	308	FORMAT(1H0,11H MOTOR SLIP,F12.3,25H EXCEEDS RATED POWER SLIP,	000126
00153	67*	1	F12.3)	000126
00154	68*		IF(IMPL.EQ.2)ICNT=ICNT+1	000126
00154	69*	C		000126
00154	70*	C	COMPUTE POWER AND POWER LOSS	000126
00154	71*	C		000126
00156	72*	300	OMEGA=RS*3.14159/30.	000135
00157	73*		P2=EE*P1-DA*OMEGA*OMEGA/1000.	000140
00160	74*		PL=P1-P2	000147
00161	75*		TC=0.	000151
00162	76*		IF(P2.GT.0.)GO TO 400	000152
00164	77*		IF(P1.LE.0.)GO TO 409	000155
00166	78*		IF(IMPL.EQ.2)WRITE(6,408)SR,DA	000160



```

CO173 79* 408 FORMAT(1H0,19H STATOR RESISTANCE ,F12.3,12H OR DAMPING ,
CO173 80* XF12.3,20H TOO HIGH FOR MOTOR )
CO174 81* IF(IMPL.EQ.2)ICNT=ICNT+1
C
C EFFICIENCY AND MAXIMUM OUTPUT POWER
C
409 CONTINUE
P2=0.
EF2=EF1
MP2=AMIN1(MP1,RAP)
GO TO 500
CO200 87*
CO201 88* 400 EF2=EF1*P2/P1
CO202 89* MP2=AMIN1(MP1,RAP)*P2/P1
CO203 90* IF (RS.NE.C.)TO=P2*737.6/OMEGA
CO204 91*
CO205 92* C
CO205 93* 500 IF(IMPL.LE.1)RETURN
CO207 94* C
CO207 95* C STATISTICS
CO207 96* C
CO207 97* C
CO211 98* MT=AMAX1(TO,MT)
CO212 99* MPN=AMAX1(P2/RAP,MPN)
CO213 100* SP=SP+P2*TINC
CO213 101* C
CO214 102* IF (TIME.LT.TMAX1)RETURN
CO216 103* CCI=CCI+CC
CO217 104* CMI=CMI+CM
CO217 105* C
CO220 106* RETURN
CO221 107* END

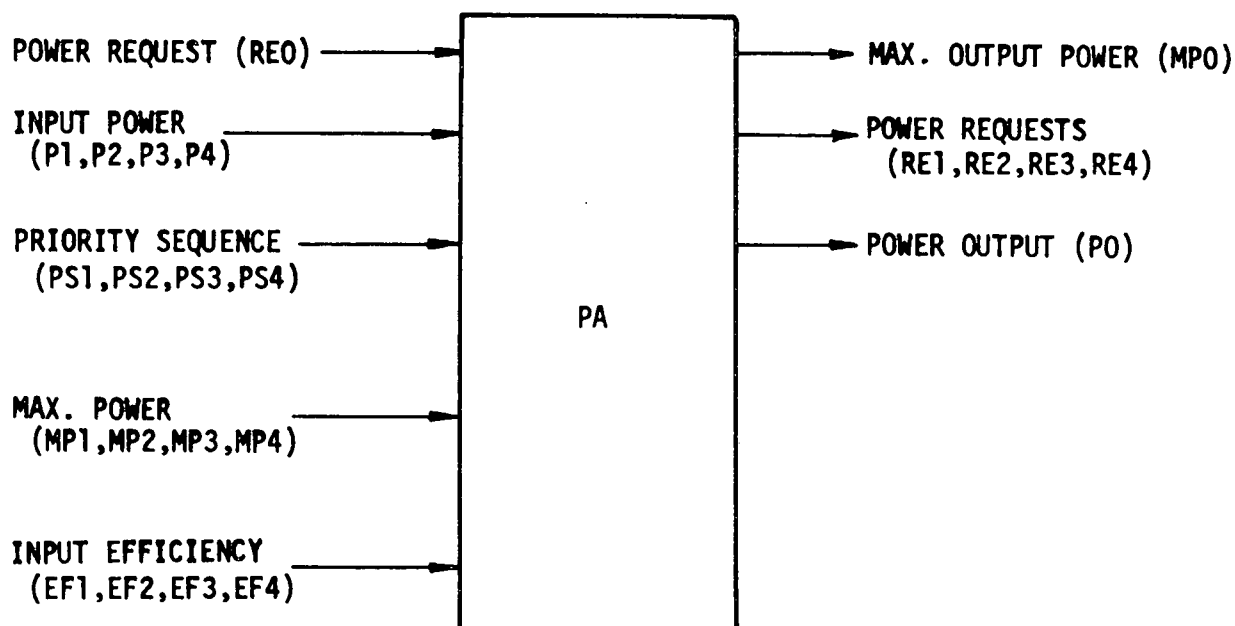
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7.27 POWER ACCUMULATOR



This component sums power from four input ports and allocates power requests to each port's source of power generation. If an input power request (load) exceeds the maximum power that can be delivered by the port of highest priority, then the remaining load is allocated according to weight within priority, and then allocated to the next priority ports. (See 1.2.3 for further discussion.)

Inputs¹

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
RE 0	Load request	kw
EF 1,2,3,4	Input efficiency from port i	-
P 1,2,3,4	Input power from port i (default = 0.)	kw
PS 1,2,3,4	Priority sequence (default=1,2,3,4)	-
F 1,2,3,4	Allocation weight (for equal priorities)	-
MP 1,2,3,4	Maximum power (default = 1×10^8)	kw

Outputs

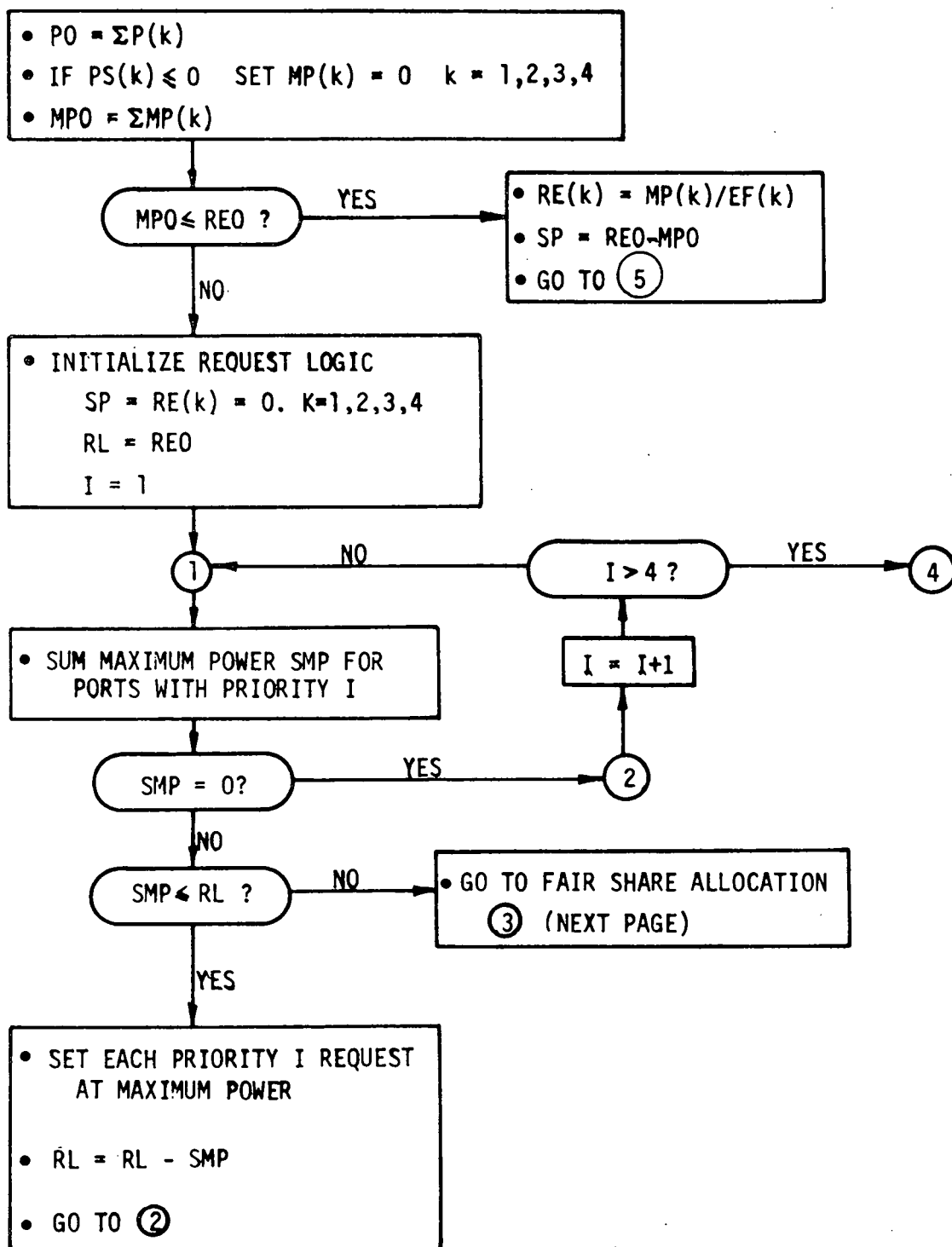
<u>Variable/Port</u>			
MP 0	Maximum deliverable power ($\sum MP(i)$)		kw
RE 1,2,3,4	Power request for port i		kw
P 0	Power output		kw
SP	Supplemental power request to meet load (Power deficit) = $RE_0 - \sum MP_i$		kw

Statistics

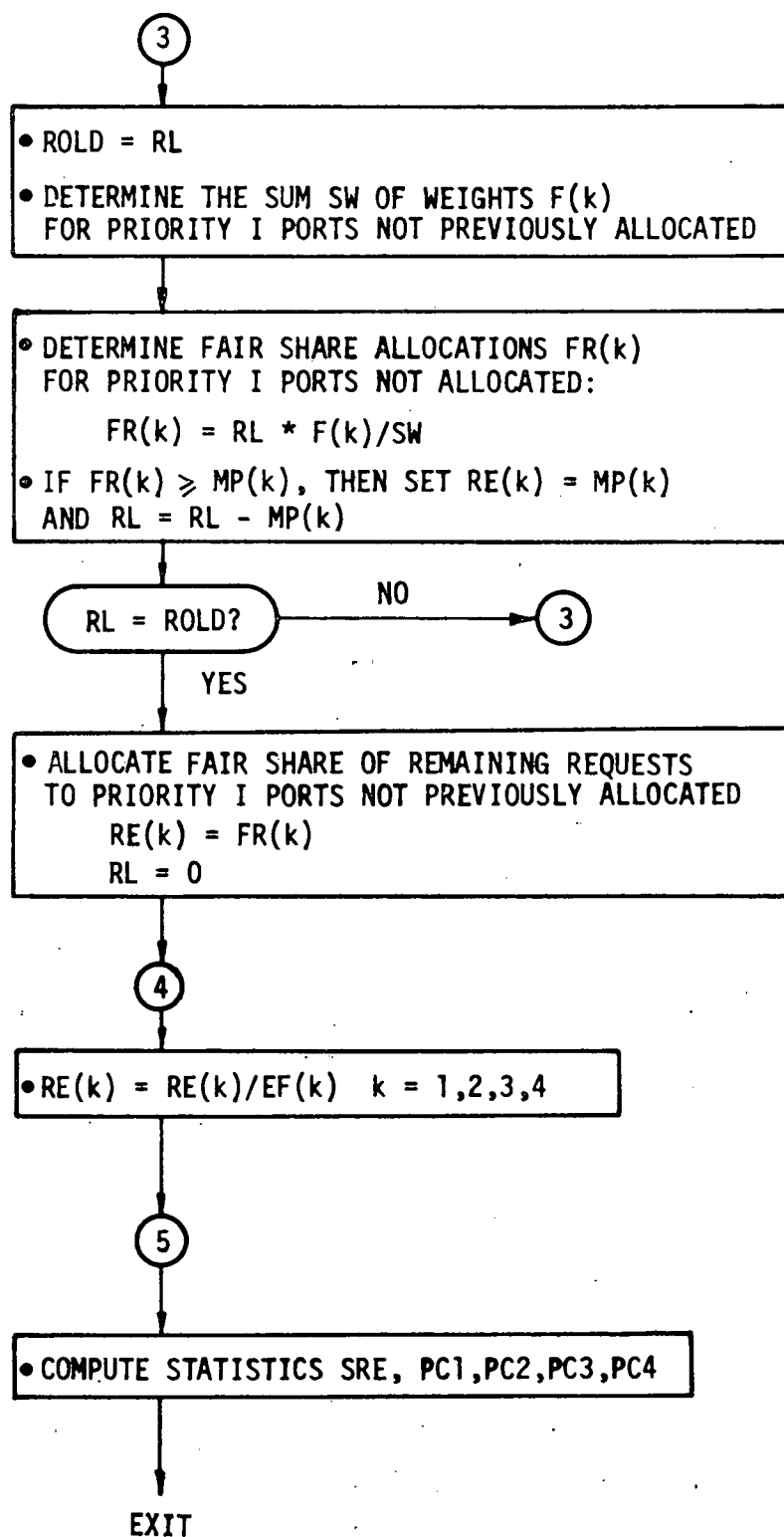
SRE	Sum of energy requested	kwh
PC 1,2,3,4	Percent of cumulative load request delivered by port i	%

¹ No capital costs assigned since this is an allocation component, not a physical device.

CALCULATION LOGIC



PA FAIR SHARE ALLOCATION



SUBROUTINE PA ENTRY POINT 000520

STORAGE USED CODE(1) 000752; DATA(0) 000110; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000001
0004 CSTMUL 000010

EXTERNAL REFERENCES (BLOCK, NAME)

0005 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000376	100CL	0001	000401	200CL	0001	000235	2346	0001	000244	2416	0001	000264	2546
0001	000306	2736	0001	000325	3056	0001	000363	3256	0001	000104	40L	0001	000301	400L
0001	000417	500L	0001	000301	600L	0001	000316	70CL	0001	000161	80L	0001	000353	800L
0001	000372	900L	0004	000000	DUM	0000 R	000030	FR	0000 R	000042	FRU	0000 I	000037	I
0003 I	000000	IMPL	0000	000055	INJP5	0000 I	000041	K	0000 R	000034	LL	0000 R	000035	LOLD
0000 R	000014	MP	0000 R	000004	PR	0000 R	000000	R	0000 R	000024	SMP	0000 R	000044	SRI
0000 R	000043	SRO	0000 R	000020	SW	0004 R	000006	TINC	0000 R	000036	TINC1	0004	000007	TMAX
0000 R	000016	W	0000 R	000040	XI									

00100	1*	CPA												000000
00101	2*													000000
00101	3*		1											000000
00101	4*		2											000000
00101	5*		3											000000
00101	6*		4											000000
00101	7*		4											000000
00101	8*		5											000000
00101	9*		6											000000
00101	10*		7											000000
00101	11*		8											000000
00101	12*	C												000000
00101	13*	C												000000
00101	14*	C												000000
00101	15*	C												000000
00101	16*	C												000000
00101	17*	C												000000
00101	18*	C												000000
00101	19*	C												000000
00101	20*	C												000000
00101	21*	C												000000
00101	22*	C												000000
00101	23*	C												000000

SUBROUTINE PA(MPD,
R1, R2, R3, R4,
PD,SP,
SR,PC1,PC2,PC3,PC4,
RO,
EF1, EF2, EF3, EF4,
P1, P2, P3, P4,
PR1, PR2, PR3, PR4,
W1, W2, W3, W4,
MP1, MP2, MP3, MP4)

PURPOSE. MODEL POWER ACCUMULATOR

METHOD. PRIMARY REQUEST ALLOCATION RESULTING FROM PRIORITY ASSIGNMENTS. SECONDARY REQUEST ALLOCATION RESULTING FROM WEIGHT ASSIGNMENTS.

THAT IS, REQUESTS ARE ALLOCATED ACCORDING TO

- * PORT PRIORITY (HIGHEST PRIORITY = 1)
- * PORT WEIGHTS (IN CASE OF EQUAL PRIORITIES.)

FORMAL ARGUMENT DEFINITION.

R1,..., R4 POWER REQUESTS IN KW (OUTPUTS)

```

00101 24* C MPO TOTAL MAXIMUM POWER (OUTPUT) 000000
00101 25* C SP SURPLUS REQUEST (OUTPUT) 000000
00101 26* C PO TOTAL LOAD IN KW (OUTPUT) 000000
00101 27* C SR SUM OF ENERGY REQUESTED, KWH (OUTPUT) 000000
00101 28* C PC1,...,PC4 PERCENT OF CUM LOAD DELIVERED (OUTPUT) 000000
00101 29* C RO TOTAL POWER REQUESTED,KW (INPUT) 000000
00101 30* C P1,..., P4 INPUT POWER IN KW (INPUTS) 000000
00101 31* C PR1,..., PR4 PORT PRIORITIES (INPUTS) 000000
00101 32* C W1,..., W4 PORT WEIGHTS (INPUTS) 000000
00101 33* C MP1, ..., MP4 MAXIMUM POWERS (INPUTS) 000000
00101 34* C EF1, ..., EF4 EFFICIENCIES (INPUTS) 000000
00101 35* C COMMON STORAGE 000000
00103 36* COMMON/ CIMPL / IMPL 000000
00104 37* COMMON / CSIMUL / DUM(6), TINC, THAX 000000
00105 38* REAL MPO,MP1,MP2,MP3,MP4 000000
00105 39* C 000000
00105 40* C LOCAL VARIABLES 000000
00105 41* C 000000
00105 42* C 000000
00105 43* C R(K) IS THE POWER REQUEST AT PORT K 000000
00106 44* REAL R(4) 000000
00106 45* C 000000
00106 46* C PR(K) IS THE PRIORITY ASSIGNED TO PORT K 000000
00107 47* REAL PR(4) 000000
00107 48* C 000000
00107 49* C W(K) IS THE WEIGHT ASSIGNED TO PORT K 000000
00110 50* REAL W(4) 000000
00110 51* C 000000
00110 52* C MP(K) IS MAXIMUM POWER TO BE ALLOCATED TO PORT K 000000
00111 53* REAL MP(4) 000000
00111 54* C 000000
00111 55* C SW(I) IS THE SUM OF THE WEIGHTS ASSIGNED TO PRIORITY-I PORTS 000000
00112 56* REAL SW(4) 000000
00112 57* C 000000
00112 58* C SMP(I) IS THE SUM OF THE MAXIMUM POWER AT PRIORITY-I PORTS 000000
00113 59* REAL SMP(4) 000000
00113 60* C 000000
00113 61* C FRU IS "FAIR SHARE" UNIT FOR PRIORITY-I PORTS 000000
00113 62* C 000000
00113 63* C FR(K) IS THE COMPUTED "FAIR SHARE" REQUEST FOR PORT K 000000
00114 64* REAL FR(4) 000000
00114 65* C 000000
00114 66* C LL IS THE LOAD LEFT AT EACH POINT IN THE ITERATION 000000
00115 67* REAL LL,LOLD 000000
00115 68* C 000000
00115 69* C IF IMPL IS ZERO, THEN ASSIGN DEFAULT VALUES 000000
00116 70* IF (IMPL .GT. 0) GO TO 40 000000
00120 71* RO = 0.0 000000
00121 72* IF (PR1 .EQ. 0.99999) PR1 = 1.0 000003
00123 73* IF (PR2 .EQ. 0.99999) PR2 = 2.0 000010
00125 74* IF (PR3 .EQ. 0.99999) PR3 = 3.0 000015
00127 75* IF (PR4 .EQ. 0.99999) PP4 = 4.0 000022
00131 76* IF (MP1 .EQ. 0.99999) MP1 = 1.0E8 000027
00133 77* IF (MP2 .EQ. 0.99999) MP2 = 1.0E8 000034
00135 78* IF (MP3 .EQ. 0.99999) MP3 = 1.0E8 000041
00137 79* IF (MP4 .EQ. 0.99999) MP4 = 1.0E8 000046
00141 80* IF (P1 .EQ. .99999) P1=0.0 000053

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00143      81*      IF(P2 .EQ. .99999) P2=0.0
00145      82*      IF(P3 .EQ. .99999) P3= 0.0
00147      83*      IF(P4 .EQ. .99999) P4=0.0
00151      84*      SR=0.
00152      85*      PC1=0.
00153      86*      PC2=0.
00154      87*      PC3=0.
00155      88*      PC4=0.
00156      89*      TINC1= 0.5*YINC
00157      90*      40 CONTINUE
00157      91*      C
00157      92*      C      IF THE TOTAL MAXIMUM POWER IS .LE. TOTAL POWER
00157      93*      C      REQUESTED, THEN SUBMIT REQUESTS AT MAX-POWER, SET REQUEST
00157      94*      C      SURPLUS EQUAL TO THE DIFFERENCE, AND RETURN
00160      95*      PC = P1 + P2 + P3 + P4
00161      96*      IF(PR1.LE.0.0) MP1=0.
00163      97*      IF(PR2.LE.0.0) MP2=0.
00165      98*      IF(PR3.LE.0.0) MP3=0.
00167      99*      IF(PR4.LE.0.0) MP4=0.
00171     100*      MPG = MP1 + MP2 + MP3 + MP4
00172     101*      IF (MPG .GT. R0) 60 TO 80
00174     102*      R1 = MP1/EF1
00175     103*      R2 = MP2/EF2
00176     104*      R3 = MP3/EF3
00177     105*      R4 = MP4/EF4
00200     106*      SP = R0 - MPG
00201     107*      60 TO 500
00202     108*      80 CONTINUE
00202     109*      C
00202     110*      C      PROCEED WITH ALLOCATION ALGORITHM SINCE THE SUM OF
00202     111*      C      ALL MAXIMUM POWER INPUTS EXCEEDS THE TOTAL REQUEST R0
00202     112*      C
00202     113*      C      INITIALIZATION
00203     114*      LL = R0
00204     115*      R1 = 0.0
00205     116*      R2 = 0.0
00206     117*      R3 = 0.0
00207     118*      R4 = 0.0
00210     119*      SP = 0.0
00210     120*      C
00210     121*      C      IF THE TOTAL REQUEST (OR LOAD) IS ZERO, THEN RETURN
00211     122*      IF (R0 .LE. 0.0) 60 TO 500
00213     123*      R(1)=R1
00214     124*      R(2)=R2
00215     125*      R(3)=R3
00216     126*      R(4)=R4
00217     127*      PR(1) = PR1
00220     128*      PR(2) = PR2
00221     129*      PR(3) = PR3
00222     130*      PR(4) = PR4
00223     131*      W(1) = W1
00224     132*      W(2) = W2
00225     133*      W(3) = W3
00226     134*      W(4) = W4
00227     135*      MP(1) = MP1
00228     136*      MP(2) = MP2
00229     137*      MP(3) = MP3

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00232	138*		MP(4) = MP4	000227
00232	139*	C		000227
00232	140*	C		000227
00232	141*	C	ITERATE ON PRIORITY I FOR I = 1, 2, 3, 4	000227
00232	142*	C		000227
00233	143*		DO 1000 I = 1, 4	000235
00233	144*	C		000235
00236	145*		XI = I	000235
00236	146*	C	OBTAIN SUM OF MAXIMUM POWER FOR PORTS WITH PRIORITY I	000235
00237	147*		SMP(I) = 0.0	000240
00240	148*		DO 100 K = 1, 4	000244
00243	149*		IF (PR(K) .EQ. XI) SMP(I) = SMP(I) + MP(K)	000244
00245	150*	100	CONTINUE	000253
00245	151*	C		000253
00245	152*	C	IF NO PRIORITY-I MAXIMUM POWER EXISTS, THEN PROCEED WITH	000253
00245	153*	C	THE NEXT HIGHER PRIORITY	000253
00247	154*		IF (SMP(I) .EQ. 0.0) GO TO 1000	000253
00247	155*	C		000253
00247	156*	C	IF THE SUM OF ALL PRIORITY-I MAXIMUM POWER .GT. LOAD	000253
00247	157*	C	LEFT, THEN GO AROUND	000253
00251	158*		IF (SMP(I) .GT. LL) GO TO 400	000255
00251	159*	C		000255
00251	160*	C	THE SUM OF ALL PRIORITY-I MAXIMUM POWER .LE. LOAD	000255
00251	161*	C	LEFT, SO SUBMIT EACH PRIORITY-I REQUEST	000255
00253	162*		DO 200 K = 1, 4	000264
00256	163*		IF (PR(K) .EQ. XI) R(K) = MP(K)	000264
00260	164*	200	CONTINUE	000272
00260	165*	C		000272
00260	166*	C	UPDATE LOAD LEFT	000272
00262	167*		LL = LL - SMP(I)	000272
00262	168*	C		000272
00262	169*	C	IF THE REMAINING LOAD IS ZERO, THEN EXIT THE ITERATION	000272
00263	170*		IF (LL .LE. 0.0) GO TO 2000	000275
00263	171*	C		000275
00263	172*	C	OTHERWISE, PROCEED WITH NEXT HIGHER PRIORITY	000275
00265	173*		GO TO 1000	000277
00265	174*	C		000277
00266	175*	400	CONTINUE	000301
00266	176*	C		000301
00266	177*	C	THE SUM OF THE PRIORITY-I MAXIMUM POWER EXCEEDS THE	000301
00266	178*	C	LOAD LEFT, SO COMPUTE AND SUBMIT FAIR SHARE REQUESTS	000301
00266	179*	C	TO EACH PRIORITY-I PORT	000301
00266	180*	C		000301
00267	181*	600	CONTINUE	000301
00267	182*	C		000301
00267	183*	C	SAVE LL FOR LATER REFERENCE	000301
00270	184*		LOLD = LL	000301
00270	185*	C		000301
00270	186*	C	DETERMINE FAIR SHARE UNITS FOR ALL PRIORITY-I	000301
00270	187*	C	PORTS TO WHICH NO REQUEST HAS BEEN SUBMITTED	000301
00271	188*		SW(I) = 0.0	000302
00272	189*		DO 700 K = 1, 4	000306
00275	190*		IF (R(K) .NE. 0.0) GO TO 700	000306
00277	191*		IF (PR(K) .EQ. XI) SW(I) = SW(I) + W(K)	000307
00301	192*	700	CONTINUE	000317
00303	193*		FRU = 1.0 / SW(I)	000317
00303	194*	C		000317

PA

00303	195*	C	FIRST, SUBMIT FAIR SHARE REQUESTS TO PORTS FOR WHICH THE	000317
00303	196*	C	FAIR SHARE REQUEST EXCEEDS THE MAXIMUM POWER. CONSIDER ONLY	000317
00303	197*	C	PORTS TO WHICH NO REQUEST HAS BEEN SUBMITTED	000317
00304	198*		DO 800 K = 1, 4	000325
00307	199*		IF (R(K) .NE. 0.0) GO TO 800	000325
00311	200*		IF (PR(K) .NE. XI) GO TO 800	000326
00311	201*	C		000326
00311	202*	C	COMPUTE FAIR SHARE	000326
00313	203*		FR(K) = (W(K) * FRU) * LL	000331
00313	204*	C		000331
00313	205*	C	IF FAIR SHARE EXCEEDS MAXIMUM POWER, THEN SUBMIT REQUEST	000331
00314	206*		IF (FR(K) .GE. MP(K)) R(K) = MP(K)	000335
00314	207*	C	- - - AND REDUCE LOAD LEFT TALLY	000335
00316	208*		IF (FR(K) .GE. MP(K)) LL = LL - MP(K)	000343
00320	209*		800 CONTINUE	000354
00320	210*	C		000354
00320	211*	C	IF LL .NE. LOLD, THEN LL WAS REDUCED DURING THE	000354
00320	212*	C	PROCESSING IN THE "DO 800" LOOP ABOVE. THIS CHANGES	000354
00320	213*	C	THE FAIR SHARE COMPUTATION. IT IS THEREFORE	000354
00320	214*	C	NECESSARY TO GO BACK THROUGH THE "DO 800" LOOP IN	000354
00320	215*	C	ORDER TO RECONSIDER ANY PORT WHICH MAY NOW	000354
00320	216*	C	SATISFY THE REQUIREMENT THAT FR(K) .GE. MP(K). ONLY	000354
00320	217*	C	PRIORITY-1 PORTS TO WHICH NO REQUEST HAS BEEN	000354
00320	218*	C	MADE ARE ELIGIBLE FOR RECONSIDERATION	000354
00322	219*		IF (LL .LT. LOLD) GO TO 600	000354
00322	220*	C		000354
00322	221*	C	FINALLY, SUBMIT REQUESTS TO THOSE PORTS FOR WHICH THE FAIR SHARE	000354
00322	222*	C	.LT. THAN THEIR MAXIMUM POWER. CONSIDER ONLY	000354
00322	223*	C	PRIORITY-1 PORTS TO WHICH NO REQUEST HAS BEEN SUBMITTED	000354
00324	224*		DO 900 K = 1, 4	000363
00327	225*		IF (R(K) .NE. 0.0) GO TO 900	000363
00331	226*		IF (PR(K) .NE. XI) GO TO 900	000364
00333	227*		R(K) = FR(K)	000367
00334	228*		900 CONTINUE	000373
00336	229*		LL=0.0	000373
00337	230*		GO TO 2000	000374
00337	231*	C		000374
00340	232*		1000 CONTINUE	000401
00340	233*	C		000401
00342	234*		2000 CONTINUE	000401
00342	235*	C		000401
00342	236*	C	FINALLY, ASSIGN OUTPUTS TO NON-SUBSCRIPTED FORMAL PARAMETERS.	000401
00342	237*	C	ALSO, MODIFY ALL REQUESTS ACCORDING TO THE INPUT EFFICIENCIES	000401
00343	238*		R1 = R(1) / EF1	000401
00344	239*		R2 = R(2) / EF2	000403
00345	240*		R3 = R(3) / EF3	000406
00346	241*		R4 = R(4) / EF4	000411
00347	242*		SP = LL	000414
00350	243*		500 IF (IMPL.LE.1) RETURN	000417
00352	244*		SPO= SR	000425
00353	245*		SR=SR+ RC*TINCI	000427
00354	246*		IF (SR.LE.0.) RETURN	000433
00356	247*		SRO=SR/SR	000441
00357	248*		SRI= TINCI*100./SR	000444
00360	49*		PC1= PC1+SRO + P1*SRI	000450
00361	50*		PC2= PC2+SRO + P2*SRI	000454
00362	51*		PC3= PC3+SRO + P3*SRI	000462

P.F.

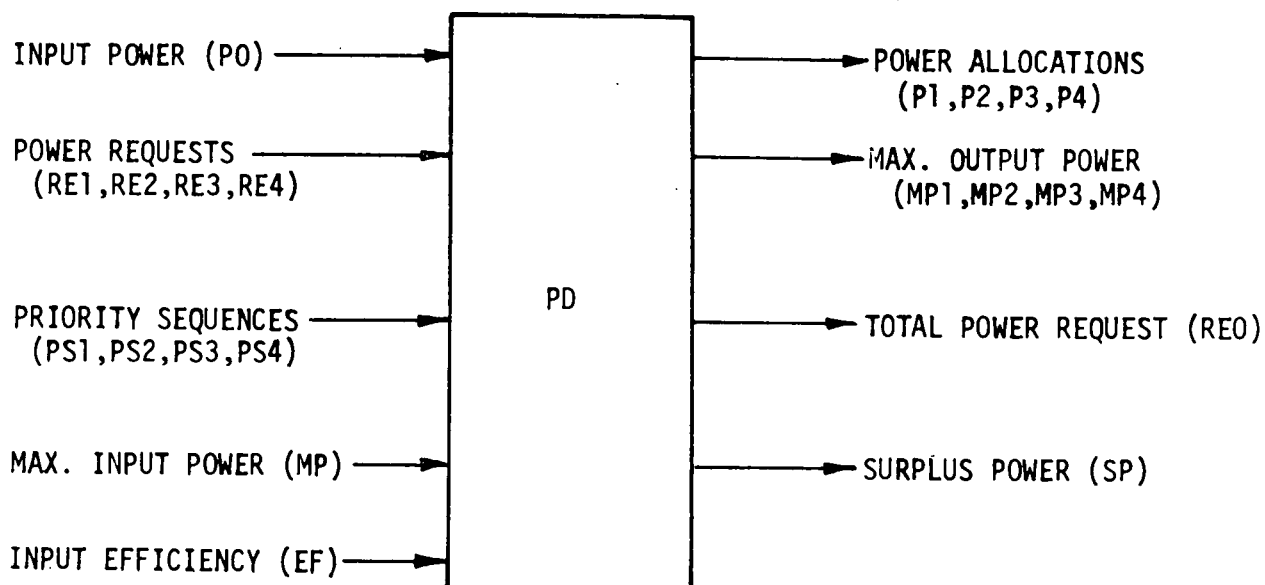
BCS 40180-2

00363	252*
00364	253*
00365	254*

PC4= PC4+SRO + P4+SRI
RETURN
END

C0C470
000476
C0C751

7.28 POWER DIVIDER



This component allocates power to four ports plus surplus based on priority, port requests, and allocation weights for equal priority ports. Each port is assigned a priority sequence from 1 to 4, and a weighting $F_i > 0$, $i=1,2,3,4$ for proportional allocation among equal priority ports. If power available exceeds the power requested for a set of ports of equal priority, then the remaining power is allocated to ports having the next highest priority. If power available is less than the power requested for ports of equal priority then power is allocated between them in proportion to their respective allocation weights.

The total power request is the sum of the port requests divided by input efficiency. The maximum power outputs $MP_1, \dots, MP_4$ are necessary for direct connections to a power accumulator PA. These variables may be used as maximum power inputs to other components, although such connections are not required. (See 1.2.3 for further discussion.)

Inputs¹

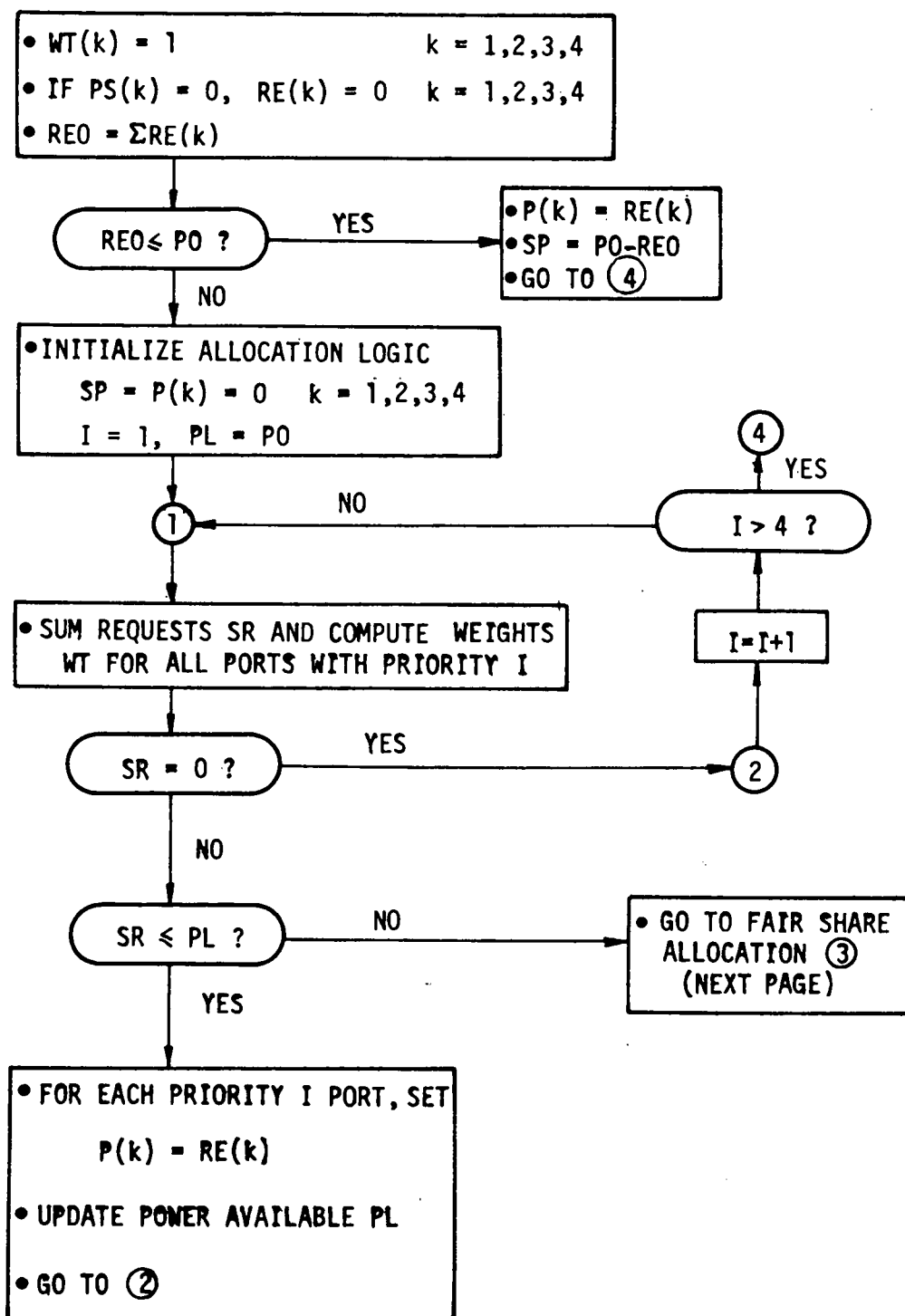
<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
P 0	Input power	kw
RE 1,2,3,4	Power requests of output ports	kw
PS 1,2,3,4	Priority sequence (default = 1,2,3,4)	-
F 1,2,3,4	Allocation weight (for equal priorities)	-
MP	Maximum input power (default = 1×10^8)	kw
EF	Input efficiency	-

Outputs

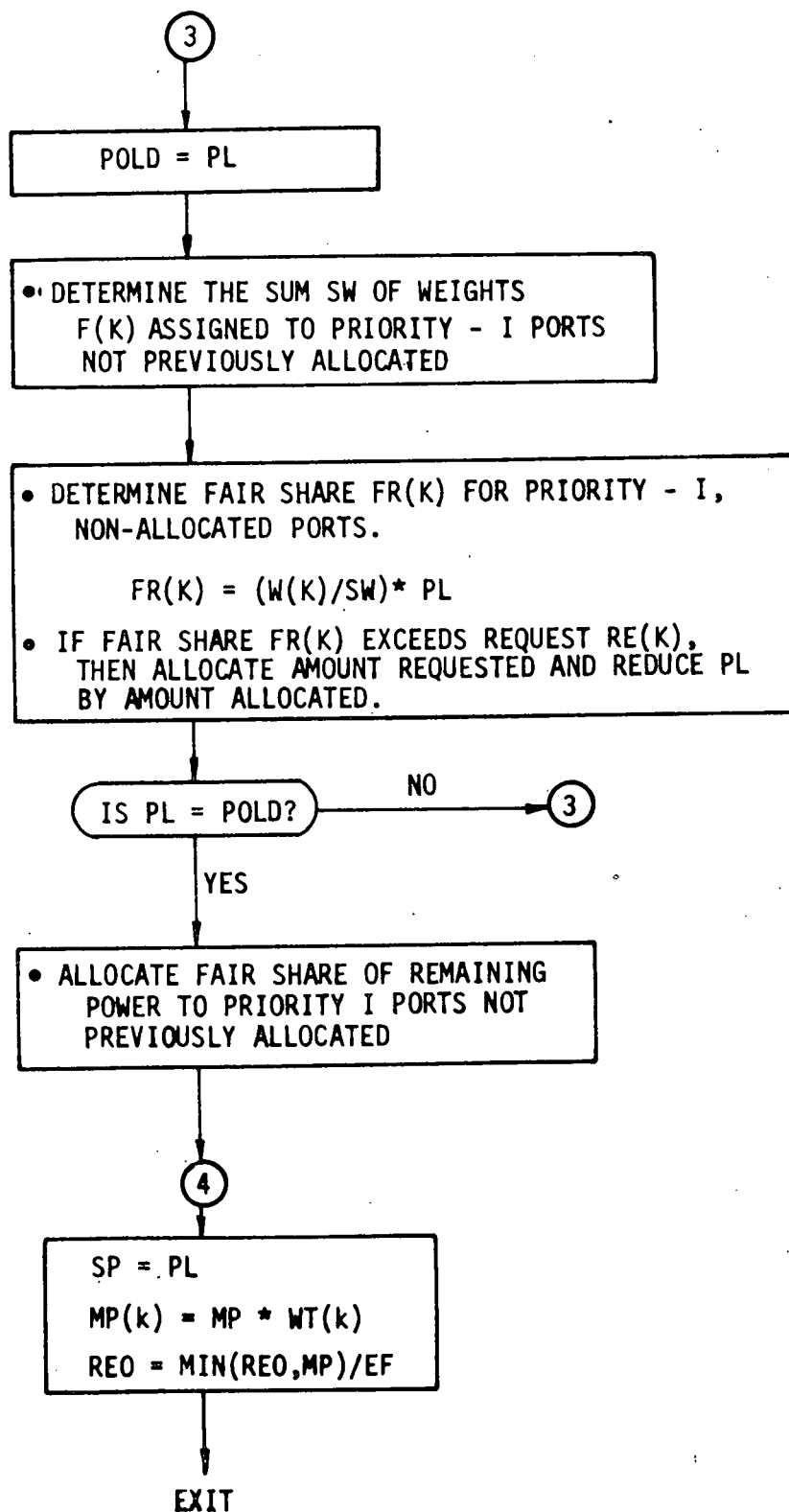
<u>Variable/Port</u>			
P 1,2,3,4	Output power for port i		kw
RE 0	Output power request		kw
SP	Surplus power		kw
MP 1,2,3,4	Output maximum power based on MP		kw

¹ No capital costs assigned since this is an allocation component, not a physical device.

CALCULATION LOGIC



PD FAIR SHARE ALLOCATION



Dr.

```

00101      26*      C      UPDATE POWER AVAILABLE
00101      27*      C      EXIT
00101      28*      C      NO.
00101      29*      C      IS SUM OF ALL PRIORITY-1 REQUESTS .LT. PO
00101      30*      C      YES.
00101      31*      C      FULFILL EACH PRIORITY-1 REQUEST
00101      32*      C      UPDATE POWER AVAILABLE (TO PL)
00101      33*      C      GO ON TO PRIORITY-2 REQUESTS
00101      34*      C      NO.
00101      35*      C      ALLOCATE "FAIR SHARE" TO EACH PRIORITY-1 PORT
00101      36*      C      EXIT.
00101      37*      C      IS SUM OF ALL PRIORITY-2 REQUESTS .LT. PL
00101      38*      C
00101      39*      C      AND SO ON AND SO FORTH
00101      40*      C
00101      41*      C      FORMAL ARGUMENT DEFINITION.
00101      42*      C      P1,..., P4      POWER ALLOCATIONS IN KW      (OUTPUTS)
00101      43*      C      RC      TOTAL POWER REQUESTED      (OUTPUT)
00101      44*      C      SP      SURPLUS POWER      (OUTPUT)
00101      45*      C      PM1,...,PM4      PORT MAXIMUM OUTPUT POWER IN KW      (OUTPUT)
00101      46*      C      PO      TOTAL POWER INPUT IN KW      (INPUT)
00101      47*      C      R1,..., R4      PORT REQUESTS IN KW      (INPUTS)
00101      48*      C      PR1,..., PR4      PORT PRIORITIES      (INPUTS)
00101      49*      C      W1,..., W4      PORT WEIGHTS      (INPUTS)
00101      50*      C      PM      MAXIMUM INPUT POWER IN KW      (INPUT)
00101      51*      C      EF      INPUT EFFICIENCY      (INPUT)
00101      52*      C
00101      53*      C      COMMON STORAGE
00103      54*      C      COMMON/ CIMPL / IMPL
00103      55*      C
00103      56*      C      LOCAL VARIABLES
00103      57*      C
00103      58*      C      P(K) IS THE POWER ALLOCATED TO PORT K
00104      59*      C      REAL P(4)
00104      60*      C
00104      61*      C      R(K) IS THE POWER REQUEST AT PORT K
00105      62*      C      REAL R(4)
00105      63*      C
00105      64*      C      PRI(K) IS THE PRIORITY ASSIGNED TO PORT K
00106      65*      C      REAL PRI(4)
00106      66*      C
00106      67*      C      W(K) IS THE WEIGHT ASSIGNED TO PORT K
00107      68*      C      REAL W(4)
00107      69*      C
00107      70*      C      SW(I) IS THE SUM OF THE WEIGHTS ASSIGNED TO PRIORITY-I PORTS
00110      71*      C      REAL SW(4)
00110      72*      C
00110      73*      C      SR(I) IS THE SUM OF THE REQUESTS AT PRIORITY-I PORTS
00111      74*      C      REAL SR(4)
00111      75*      C
00111      76*      C      FRU IS "FAIR SHARE" UNIT FOR PRIORITY-I PORTS
00111      77*      C
00111      78*      C      FR(K) IS THE COMPUTED "FAIR SHARE" ALLOCATION TO PORT K
00112      79*      C      REAL FR(4)
00112      80*      C
00112      81*      C      PL IS THE POWER LEFT AT EACH POINT IN THE ITERATION
00113      82*      C      REAL PL

```

[illegible]

22

00113	83*	C		000000
00113	84*	C	IF IMPL IS ZERO, THEN ASSIGN DEFAULT VALUES	000000
00114	85*		IF (IMPL .GT. 0) GO TO 40	000000
00116	86*		R1 = 0.0	000002
00117	87*		R2 = 0.0	000003
00120	88*		R3 = 0.0	000004
00121	89*		R4 = 0.0	000005
00122	90*		IF (PM.EQ. .99999) PM=1.E8	000006
00124	91*		IF (PR1 .EQ. 0.99999) PR1 = 1.0	000013
00126	92*		IF (PR2 .EQ. 0.99999) PR2 = 2.0	000020
00130	93*		IF (PR3 .EQ. 0.99999) PR3 = 3.0	000025
00132	94*		IF (PR4 .EQ. 0.99999) PR4 = 4.0	000032
00134	95*		IF (PM .EQ. .99999) PM= 1.E8	000037
00134	96*	C	INITIALIZATION OF F'S	000037
00134	97*	C		000037
00136	98*		40 CONTINUE	000045
00137	99*		F1= 1.	000045
00140	100*		F2= 1.	000046
00141	101*		F3= 1.	000047
00142	102*		F4= 1.	000050
00142	103*	C		000050
00142	104*	C	IF THE TOTAL POWER REQUESTED IS .LE. TOTAL POWER	000050
00142	105*	C	INPUT, THEN SATISFY REQUESTS, SET POWER SURPLUS	000050
00142	106*	C	EQUAL TO THE DIFFERENCE, AND RETURN	000050
00143	107*		IF (PR1.LE.0.0) R1=0.0	000051
00145	108*		IF (PR2.LE.0.0) R2=0.0	000055
00147	109*		IF (PR3.LE.0.0) R3=0.0	000061
00151	110*		IF (PR4.LE.0.0) R4=0.0	000065
00153	111*		RO = R1 + R2 + R3 + R4	000071
00154	112*		IF (RO .GT. PO) GO TO 80	000076
00156	113*		P1 = R1	000101
00157	114*		P2 = R2	000103
00160	115*		P3 = R3	000105
00161	116*		P4 = R4	000107
00162	117*		SP = PO - RO	000111
00163	118*		GO TO 3000	000114
00164	119*		80 CONTINUE	000116
00164	120*	C		000116
00164	121*	C	PROCEED WITH ALLOCATION ALGORITHM SINCE THE SUM OF	000116
00164	122*	C	ALL REQUESTS EXCEEDS THE TOTAL AVAILABLE POWER PO	000116
00164	123*	C		000116
00164	124*	C	INITIALIZATION	000116
00165	125*		PL = PO	000116
00166	126*		P1 = 0.0	000117
00167	127*		P2 = 0.0	000120
00170	128*		P3 = 0.0	000121
00171	129*		P4 = 0.0	000122
00172	130*		SP = 0.0	000123
00172	131*	C		000123
00172	132*	C	IF THE TOTAL POWER IS ZERO, THEN RETURN	000123
00173	133*		IF (PO .EQ. 0.0) GO TO 3000	000124
00175	134*		P(1) = P1	000126
00176	135*		P(2) = P2	000130
00177	136*		P(3) = P3	000132
00200	137*		P(4) = P4	000134
00200	138*		R(1) = R1	000136
00202	139*		R(2) = R2	000140

PL

00203	140*	R(3) = R3	000142
00204	141*	R(4) = R4	000144
00205	142*	PR(1) = PR1	000146
00206	143*	PR(2) = PR2	000150
00207	144*	PR(3) = PR3	000152
00210	145*	PR(4) = PR4	000154
00211	146*	W(1) = W1	000156
00212	147*	W(2) = W2	000163
00213	148*	W(3) = W3	000162
00214	149*	W(4) = W4	000164
00214	150*		000164
00214	151*		000164
00214	152*	ITERATE ON PRIORITY I FOR I = 1, 2, 3, 4	000164
00214	153*		000164
00215	154*	DO 1000 I = 1, 4	000172
00215	155*		000172
00220	156*	XI = I	000172
00220	157*	C OBTAIN SUM OF REQUESTS FROM PORTS WITH PRIORITY I	000172
00221	158*	SR(I) = 0.0	000175
00222	159*	WT=0.0	000176
00223	160*	DO 100 K = 1, 4	000202
00226	161*	IF (PR(K) .EQ. XI) SR(I) = SR(I) + R(K)	000202
00230	162*	IF (PR(K) .EQ. XI) WT= WT+ W(K)	000207
00232	163*	100 CONTINUE	000217
00232	164*		000217
00234	165*	IF (PR1 .EQ. XI) F1= W1/WT	000217
00236	166*	IF (PR2 .EQ. XI) F2 =W2/WT	000225
00240	167*	IF (PR3 .EQ. XI) F3= W3/WT	000233
00242	168*	IF (PR4 .EQ. XI) F4= W4/WT	000241
00244	169*	IF (PL .LE. 0.0) GO TO 1000	000247
00244	170*		000247
00244	171*	C IF NO PRIORITY-I REQUESTS EXIST, THEN PROCEED WITH	000247
00244	172*	C THE NEXT HIGHER PRIORITY	000247
00246	173*	IF (SR(I) .EQ. 0.0) GO TO 1000	000252
00246	174*		000252
00246	175*	C IF THE SUM OF ALL PRIORITY-I REQUESTS .GT. POWER	000252
00246	176*	C AVAILABLE, THEN GO AROUND	000252
00250	177*	IF (SR(I) .GT. PL) GO TO 400	000254
00250	178*		000254
00250	179*	C THE SUM OF ALL PRIORITY-I REQUESTS .LE. POWER	000254
00250	180*	C AVAILABLE, SO FULFILL EACH PRIORITY-I REQUEST	000254
00252	181*	DO 200 K = 1, 4	000263
00255	182*	IF (PR(K) .EQ. XI) P(K) = R(K)	000263
00257	183*	200 CONTINUE	000271
00257	184*		000271
00257	185*	C UPDATE POWER AVAILABLE	000271
00261	186*	PL = PL - SR(I)	000271
00262	187*	GO TO 1000	000274
00262	188*		000274
00263	189*	400 CONTINUE	000276
00263	190*		000276
00263	191*	C THE SUM OF THE PRIORITY-I REQUESTS EXCEEDS THE	000276
00263	192*	C POWER AVAILABLE, SO COMPUTE AND ALLOCATE FAIR	000276
00263	193*	C SHARE TO EACH PRIORITY-I PORT	000276
00263	194*		000276
00264	195*	600 CONTINUE	000276
00264	196*		000276

PD

Address	Instruction	Comment	Address
00269	197*	C	000276
00265	198*	C	000276
00265	199*	C	000276
00265	200*	C	000276
00265	201*	C	000276
00266	202*	C	000276
00267	203*	C	000277
00272	204*	C	000303
00274	205*	C	000303
00276	206*	C	000304
00300	207*	C	000314
00300	208*	C	000314
00300	209*	C	000314
00300	210*	C	000314
00300	211*	C	000314
00300	212*	C	000314
00301	213*	C	000314
00304	214*	C	000322
00306	215*	C	000322
00306	216*	C	000323
00306	217*	C	000323
00310	218*	C	000323
00310	219*	C	000326
00310	220*	C	000326
00311	221*	C	000326
00311	222*	C	000332
00313	223*	C	000332
00315	224*	C	000340
00315	225*	C	000351
00315	226*	C	000351
00315	227*	C	000351
00315	228*	C	000351
00315	229*	C	000351
00315	230*	C	000351
00315	231*	C	000351
00315	232*	C	000351
00315	233*	C	000351
00317	234*	C	000351
00317	235*	C	000351
00317	236*	C	000351
00317	237*	C	000351
00317	238*	C	000351
00321	239*	C	000351
00324	240*	C	000357
00326	241*	C	000357
00330	242*	C	000360
00331	243*	C	000363
00333	244*	C	000367
00333	245*	C	000367
00334	246*	C	000373
00334	247*	C	000373
00334	248*	C	000373
00334	249*	C	000373
0033	250*	C	000373
0033	251*	C	000373
0033	252*	C	000375
00340	253*	C	000377

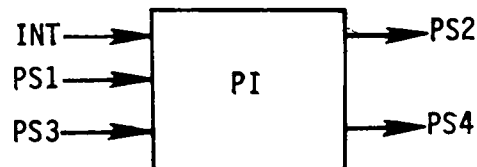
00341 254*
00342 255*
00343 256*
00344 257*
00345 258*
00346 259*
00347 260*
00350 261*
00351 262*

3000 P4 = P(4)
SP = PL
PM1=PM*F1
PM2=PM*F2
PM3=PM*F3
PM4=PM*F4
RO= AMIN1(RO,PM)/EF
RETURN
END

000401
000403
000406
000410
000413
000416
000421
000430
000641

PD

7.29 PRIORITY INTERRUPT



This component is used by the storage components to change priority of the power requests when minimum or maximum capacity is approached.

Inputs

<u>Parameter/Port</u>		<u>Description</u>
PS	1	Input priority for PS4 output
PS	3	Input priority for PS2 output (default=PS1)
INT		Interrupt flag

Outputs

<u>Variable/Port</u>		
PS	2	Output priority for charge cycle
PS	4	Output priority for discharge cycle

Equations

$$\begin{aligned}
 PS2 &= PS1 && \text{if } INT=0 \\
 PS2 &= 1 && \text{if } INT > 0 \\
 PS2 &= 0 && \text{if } INT < 0 \\
 PS4 &= PS3 && \text{if } INT \leq 0 \\
 PS4 &= 0 && \text{if } INT > 0
 \end{aligned}$$

SUBROUTINE PI ENTRY POINT 000040

STORAGE USED CODE(1) 000061; DATA(0) 000010; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000001

EXTERNAL REFERENCES (BLOCK, NAME)

0004 NERR31

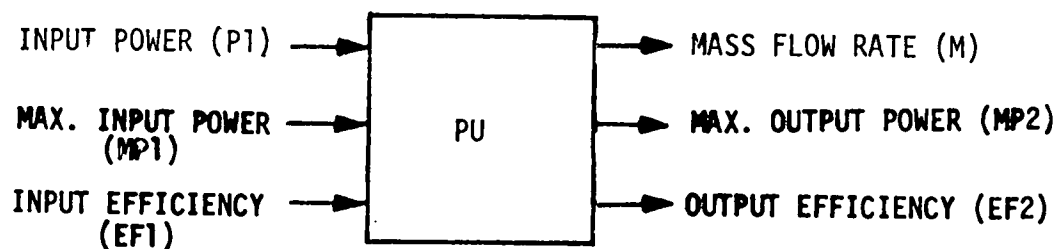
STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000010 10L 0003 I 000000 IMPL 0000 000002 INJPS

00100	1*	CPI		000000
00101	2*		SUBROUTINE PI(PS2,PS4,PS1,PS3,INT)	000000
00101	3*	C		000000
00101	4*	C	PURPOSE CHANGE PRIORITY OF POWER ALLOCATION TO STORAGE COMPONENTS	000000
00101	5*	C		000000
00101	6*	C	WRITTEN BY A.W.WARREN	000000
00101	7*	C	VERSION 1, APRIL 14 1977	000000
00101	8*	C		000000
00101	9*	C	CALL SEQUENCE	000000
00101	10*	C	PS2 - OUTPUT PRIORITY (0 TO 4)	000000
00101	11*	C	PS4 - OUTPUT PRIORITY (COMPLEMENT TO PS2)	000000
00101	12*	C	PS1 - INPUT PRIORITY FOR PS2	000000
00101	13*	C	PS3 - INPUT PRIORITY FOR PS4	000000
00101	14*	C	INT - INTERRUPT FLAG	000000
00101	15*	C	0= NO INTERRUPT	000000
00101	16*	C	1= INCREASE ALLOCATION PRIORITY	000000
00101	17*	C	-1= DECREASE ALLOCATION PRIORITY	000000
00103	18*		REAL INT	000000
00104	19*		COMMON /CIMPL/IMPL	000000
00105	20*		IF(IMPL.GT.0) GO TO 10	000000
00107	21*		IF(PS3.EQ. .99999) PS3=PS1	000002
00107	22*	C		000002
00111	23*		10 PS2=PS1	000010
00112	24*		PS4=PS3	000011
00113	25*		IF(INT.GT.0.) PS2=1.	000013
00115	26*		IF(INT.LT.0.) PS2=0.	000020
00117	27*		IF(INT.GT.0) PS4= 0.	000024
00121	28*		RETURN	000030
00122	29*		END	000060

PI

7.30 HYDRAULIC PUMP



The hydraulic pump model is based on a constant speed design. The pump is assumed to be designed to a nominal operating point and input power. For off-design performance the pump efficiency is assumed to be functionally related to the square root of the mass flow rate.

Basic Equations

The output mass flow rate is based on the equations

$$M = P1 * EFF / (C1 * C2 * H1)$$

$$EFF = 1 - (1 - EFD) * SQRT(MD / M)$$

where C1, C2 are conversion constants

Inputs

<u>Parameter/Port</u>		<u>Description</u>	<u>Units</u>
P	1	Input power	kw
H	1	Height of water above inlet	ft
EFD		Pump efficiency at design pt. (D = 0.90)	-
MD		Mass flow rate at design pt. (D = 2×10^5)	gal/h
EF	1	Input product efficiency	-
MP	1	Input maximum charging rate	kw
MM		Maximum allowable mass flow rate (D = 3×10^5)	gal/h
CK		Pump capacity cost coefficient ¹ (D = 0.011)	-
F0		Pump exponent for cost calculations (D = 0.5)	-
Y		Pumphead exponent for cost calculations (D=0.25)	-

Outputs

Variable/Port

M		Output mass flow rate	gal/h
EFF		Pump efficiency	-
CC0		Pump cost/year	\$
EF	2	Output product efficiency	-
MP	2	Maximum output power	kw

Statistics

M2U		Maximum output mass flow rate	gal/h
-----	--	-------------------------------	-------

D - default values

¹CK = capital cost (known unit)/((MD*481.2)**FO*H1 **Y * expected life time)

The calculation sequence and default values assume a constant speed hydraulic pump nominally rated for 120KW and located 200 ft. below a reservoir. The equations relating the various physical quantities and the cost estimates are based on first principles and the data presented in Reference 1, and the cost estimates on Reference 2.

Calculation Sequence

$$C1 = 0.377 \times 10^{-6} \frac{\text{kwh}}{\text{ft-lb}}$$

$$C2 = 8.3398 \text{ lb/gal}$$

1) Costs (first pass only)

$$CC = CK * (MD * 481.2)^{F0} * H1 * Y$$

-
1. L. Marks and T. Baumeister, "Mechanical Engineers Handbook", McGraw Hill, N.Y., 1958, Section 14, p. 19.
 2. Carson and Fogleman, "Comparison of Methods for Converting Existing Power Plants to Pumped Storage Facilities", International Engineering Company, Inc., 1974.

Calculation Sequence Cont.

2) Mass flow rate and pump efficiency

If $P_1 \leq 0$, set $EFF = 1$, $M = 0$ and go to 3)

Solve the basic equations for M and EFF using:

$$X^3 - XA + B = 0$$

where

$$A = P_1 / (C_1 * C_2 * H_1)$$

$$B = A * (1 - EFD) * \sqrt{MD}$$

$$M = X^2$$

$$EFF = 1 - (1 - EFD) * \sqrt{MD} / X$$

3) Product efficiency and maximum charge rate

$$EF2 = EF1 * EFF$$

$$MP2 = \min(MP1 * EFF, \quad MM * C_1 * C_2 * H_1)$$

4) Compute Statistics and Costs

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00101 24* C H1 - HEIGHT OF WATER ABOVE INLET, FT 000000
00101 25* C EFD - PUMP EFFICIENCY AT DESIGN POINT 000000
00101 26* C MD - MASS FLOW RATE AT DESIGN POINT, GAL/HR 000000
00101 27* C EF1 - INPUT PRODUCT EFFICIENCY 000000
00101 28* C MP1 - INPUT MAXIMUM CHARGING RATE, KW 000000
00101 29* C MM - MAXIMUM ALLOWABLE MASS FLOW RATE, GAL/HR 000000
00101 30* C CK - PUMP CAPACITY COST COEFFICIENT 000500
00101 31* C FO - PUMP EXPONENT FOR COST CALCULATIONS 000000
00101 32* C Y - PUMP HEAD EXPONENT FOR COST CALCULATIONS 000000
00101 33* C 000000
00103 34* COMMON /CIMPL/IMPL /CTIME/TIME/CSIMUL/DUM(7),TMAX /COST/CCI 000000
00103 35* C 000000
00104 36* REAL M,MP2,M2U,MD,MP1,MM 000000
00104 37* C 000000
00105 38* IF(IMPL.GT.0)GO TO 100 000000
00105 39* C 000000
00107 40* TMAX1=TMAX+.99999 000000
00107 41* C 000002
00110 42* C1= 3.1441E-6 000002
00110 43* C 000005
00111 44* IF(EFD.EQ. .99999)EFD=0.9 000005
00113 45* IF(MD.EQ. .99999)MD =2.0E5 000007
00115 46* IF(MP1.EQ. .99999)MP1=1.E8 000014
00117 47* IF(MM.EQ. .99999)MM =3.0E5 000021
00121 48* IF(CK.EQ. .99999)CK =0.011 000026
00123 49* IF(FO.EQ. .99999)FO =0.5 000033
00125 50* IF(Y.EQ. .99999)Y =0.25 000040
00127 51* CC =CK*(MD*.481.21)**FO*H1**Y 000045
00127 52* C 000052
00130 53* M2U =C.0 000052
00131 54* 100 EFF= 1.0 000071
00132 55* M= C.0 000073
00133 56* IF(P1 .LE. 0.0) GO TO 200 000074
00133 57* C 000075
00133 58* C SOLVE CUBIC EQUATION FOR M AND EFF 000075
00133 59* C 000075
00135 60* A3= -P1/(C1*H1) 000075
00136 61* A4 =-A3*(1.0-EFD)*SORT(MD) 000100
00136 62* C 000105
00137 63* CALL CUBIC(A3,A4,ANS) 000105
00140 64* IF(ANS.LE.0.) GO TO 200 000115
00140 65* C 000122
00142 66* M =ANS**2 000122
00143 67* EFF=1.0-(1.0-EFD)*SORT(MD)/ANS 000125
00143 68* C 000130
00143 69* C PRODUCT EFFICIENCY AND CHARGE RATE 000130
00143 70* C 000130
00144 71* 200 EF2=EF1*EFF 000142
00145 72* MP2=AMIN1(MP1*EFF,MM*H1*C1) 000144
00145 73* C 000144
00146 74* IF(IMPL.LE.1)RETURN 000156
00146 75* C 000156
00146 76* C STATISTICS 000156
00146 77* C 000156
00150 78* M2U=AMAX1(M2U,M ) 000165
00150 79* C 000165
00151 80* IF(TIME.LT.TMAX1)RETURN 000173

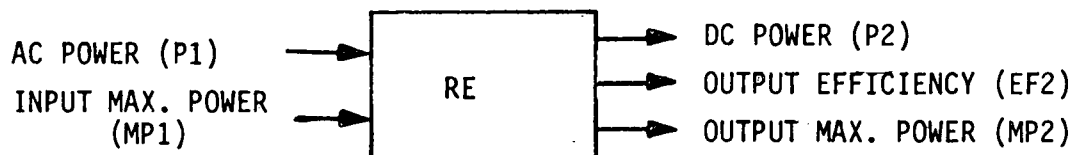
```

PU

00151	81*	C	
00153	82*		CCI=CCI+CC
00153	83*	C	
00154	84*		RETURN
00155	85*		END

000173
000202
000202
000205
000312

7.31 AC-DC RECTIFIER



This component models a solid-state rectifier/transformer. Power losses due to resistive heating and contact potential loss are modeled. Default parameter values determining power losses are based on 200 kw rated power.

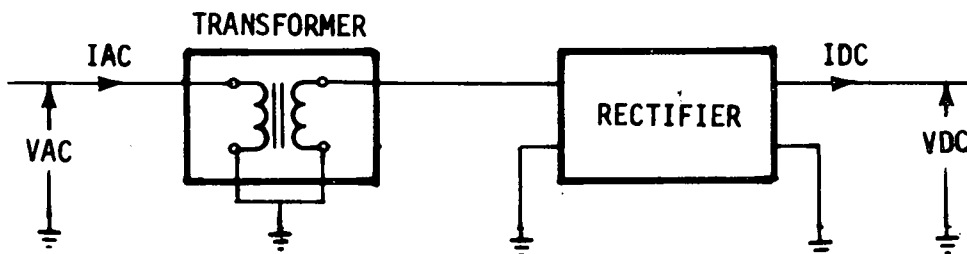


FIGURE 7.31: RECTIFIER FUNCTIONAL DIAGRAM

Inputs

<u>Parameter/Port</u>		<u>Description</u>	<u>Units</u>
P	1	AC input power	kw
RT		Transformer resistance (D = 0)	ohms
XT		Transformer reactance (D = 0.03)	ohms
VAC		Rated AC voltage (D = 440)	volts
DR		Rectifier contact potential (D = 0)	volts
RR		Rectifier resistance (D = 0.02)	ohms
RAP		Rated input power	kw
EF	1	Input product efficiency	-
MP	1	Maximum input power (D = 1×10^8)	kw
CC		Rectifier cost/year	\$

Outputs

<u>Variable/Port</u>			
P	2	DC output power	kw
IAC		AC input current	amps
PL		Power loss	kw
EF	2	Output product efficiency	-
MP	2	Maximum output power	kw

D - Default values supplied.

Calculation Sequence

- 1) Compute transformer power angles

$$Y = \sin(\theta) = \sqrt{3} * XT * P1 * 1000 / VAC^2$$

$$ABS(Y) > 1 \Rightarrow \text{DIAGNOSTIC}$$

- 2) Input and output current

If $P1 \leq 0$ set $P2 = IAC = PL = 0.$, $EFF = 1$ and go to 4)

$$IAC = VAC \sqrt{2 - 2\cos(\theta)} / (\sqrt{3} * XT)$$

$$I = VAC \sqrt{2 - 2 * \sqrt{1 - Y^2}} / (\sqrt{3} * XT)$$

$$IDC = \pi * IAC / \sqrt{6}$$

- 3) Power loss and output power

$$PL = (\sqrt{3} * RT * IAC^2 + IDC * (DR + IDC * RR)) / 1000$$

$$P2 = P1 - PL$$

$$EFF = P2 / P1$$

$$P2 \leq 0 \Rightarrow \text{DIAGNOSTIC, } EFF = 1$$

- 4) Efficiency and maximum power

$$EF2 = EF1 * EFF$$

$$MP2 = \min(MP1, RAP) * EFF$$

- 5) Compute Costs

SUBROUTINE RE ENTRY POINT 000257

STORAGE USED CODE(1) 000352; DATA(0) 000073; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000002
0004 CTIME 000001
0005 CSMUL 000010
0006 COST 000001

EXTERNAL REFERENCES (BLOCK, NAME)

0007 NWDUS
0010 NI025
0011 SGR1
0012 NEPR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000042	100L	0000	000007	108F	0001	000100	200L	0001	000117	300L	0000	000034	308F					
0001	000214	400L	0006	R	000000	CCI	0005	000000	DUM	0000	R	000006	EFF	0003	I	000031	ICNT		
0000	R	000000	IDC	0003	I	000000	IMPL	0000	000061	INJP5	0000	R	000001	PI	0000	R	000032	RO0Y3	
0004	R	000000	TIME	0005	R	000007	TMAX	0000	R	000003	TMAX1	0000	R	000004	Y	0000	R	000005	YY

00100	1*	CRE				000000
00101	2*		SUBROUTINE RE(P2,IAC,PL,EF2,MP2,P1,RT,XT,VAC,DR,RR,RAP,EF1,MP1,CC)			000000
00101	3*	C				000000
00101	4*	C	PURPOSE	SOLID STATE RECTIFIER/TRANSFORMER MODEL		000000
00101	5*	C				000000
00101	6*	C	METHOD	COMPUTE OUTPUT DC POWER AS A FUNCTION		000000
00101	7*	C		OF INPUT AC POWER		000000
00101	8*	C				000000
00101	9*	C	WRITTEN BY Y.K.CHAN	VERSION 1, JUNE 1, 1977		000000
00101	10*	C				000000
00101	11*	C	CALL SEQUENCE			000000
00101	12*	C	OUTPUTS			000000
00101	13*	C	P2	-DC OUTPUT POWER, KW		000000
00101	14*	C	IAC	-AC INPUT CURRENT, AMPS		000000
00101	15*	C	PL	-POWER LOSS, KW		000000
00101	16*	C	EF2	-OUTPUT PRODUCT EFFICIENCY		000000
00101	17*	C	MP2	-MAXIMUM OUTPUT POWER, KW		000000
00101	18*	C	INPUTS			000000
00101	19*	C	P1	-AC INPUT POWER, KW		000000
00101	20*	C	RT	-TRANSFORMER RESISTANCE, OHMS		000000
00101	21*	C	XT	-TRANSFORMER REACTANCE, OHMS		000000
00101	22*	C	VAC	-RATED AC VOLTAGE, VOLTS		000000

RL

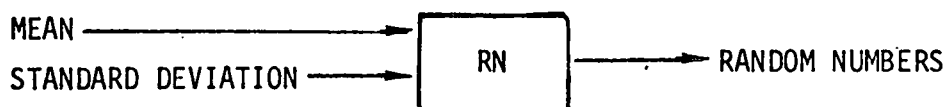
00101	23*	C	DR -RECTIFIER CONTACT POTENTIAL, VOLTS	000000
00101	24*	C	RR -RECTIFIER RESISTANCE, OHMS	000000
00101	25*	C	RAP -RATED INPUT POWER, KW	000000
00101	26*	C	EF1 -INPUT PRODUCT EFFICIENCY	000000
00101	27*	C	MP1 -MAXIMUM INPUT POWER, KW	000000
00101	28*	C	CC -RECTIFIER COST/YEAR, \$	000000
00101	29*	C		000000
00103	30*		COMMON /CIMPL/IMPL,ICNT/CTIME/TIME/CSIMUL/DUM(7),TMAX/COST/CCI	000000
00104	31*		REAL IAC,MP2,MP1,IDC	000000
00105	32*		DATA PI/3.14159/	000000
00107	33*		DATA R0013/1.73205/	000000
00107	34*	C		000000
00111	35*		IF(IMPL.GT.0) GO TO 100	000000
00113	36*		IF(MP1.EQ..999999)MP1=1.E8	000002
00115	37*		IF(RT.EQ..999999) RT=0.	000007
00117	38*		IF(XT.EQ..999999) XT=.03	000013
00121	39*		IF(VAC.EQ..999999) VAC=440.	000020
00123	40*		IF(DR.EQ..999999) DR=0.	000025
00125	41*		IF(RR.EQ..999999) RR=.02	000031
00127	42*		TMAX1=TMAX*.999999	000036
00127	43*	C		000036
00127	44*	C	COMPUTE TRANSFORMER POWER ANGLES	000036
00127	45*	C		000036
00130	46*		100 Y=ROOT3*XT*PI+1000./(VAC+VAC)	000042
00131	47*		YY=Y*Y	000051
00132	48*		IF(YY.LE.1.)GO TO 200	000053
00134	49*		IF(IMPL.EQ.2)WRITE(6,108)PI,XT,VAC	000056
00142	50*		108 FORMAT(1HG,19HRE, AC INPUT POWER ,F12.3,49H 100 LARGE IN RELATION	000071
00142	51*		1TO TRANSFORMER REACTANCE ,F12.3,22H AND RATED AC VOLTAGE ,F12.3)	000071
00143	52*		IF(IMPL.EQ.2)ICNT=ICNT+1	000071
00145	53*		200 YY=AMIN1(1.,YY)	000100
00145	54*	C		000100
00145	55*	C	INPUT AND OUTPUT CURRENT	000100
00145	56*	C		000100
00146	57*		IF(PI.GT.0.)GO TO 300	000105
00150	58*		P2=0.	000110
00151	59*		IAC=0.	000111
00152	60*		PL=0.	000112
00153	61*		EFF=1.	000113
00154	62*		GO TO 400	000115
00154	63*	C		000115
00155	64*		300 IAC=VAC*SQRT(2.-2.*SQRT(1.-YY))/(ROOT3*XT)	000117
00156	65*		IDC=PI*IAC/SQRT(6.)	000140
00156	66*	C		000140
00156	67*	C	POWER LOSS AND OUTPUT POWER	000140
00156	68*	C		000140
00157	69*		PL=(ROOT3*RT*IAC+IAC*IDC*(DR+IDC*RR))/1000.	000147
00160	70*		P2=P1-PL	000161
00161	71*		EFF=P2/PI	000163
00162	72*		IF(P2.GT.0.) GO TO 400	000165
00164	73*		IF(IMPL.EQ.2)WRITE(6,308)PL,P1	000170
00171	74*		308 FORMAT(1H0,14HRE POWER LOSS ,F12.3,21H EXCEEDS INPUT POWER ,F12.3)	000202
00172	75*		IF(IMPL.EQ.2)ICNT=ICNT+1	000202
00174	76*		P2=0.	000210
00175	77*		EFF=1.	000211
00175	78*	C		000211
00175	79*	C	EFFICIENCY AND MAXIMUM POWER	000211

RE

00175	80*	C	
00176	81*		400 EF2=EF1*EFF
00177	82*		MP2=AMIN1(MP1,RAP)
00200	83*		MP2=MP2*EFF
00201	84*		IF(IMPL.LE.1)RETURN
00203	85*		IF(1IME.LT.TMAX1)RETURN
00205	86*		CCI=CCI+CC
00205	87*	C	
00206	88*		RETURN
00207	89*		END

000211
000214
000216
000224
000226
000235
000244
000244
000247
000351

7.32 RANDOM NUMBERS



This component generates an uncorrelated sequence of normally distributed random numbers with a specified mean and standard deviation.

Inputs

Parameter/Port

Description

MN	Mean value of sequence
SIG	Standard deviation of sequence
NST ¹	Start parameter. (Use any odd integer greater than 1). Default supplied.

Outputs

Variable/Port

F0	Random number output
----	----------------------

¹ If RESET parameter > 0 then succeeding simulations use NST to start random sequence.

SUBROUTINE RN ENTRY POINT 000065

STORAGE USED CODE(1) 000105; DATA(0) 000033; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000003

EXTERNAL REFERENCES (BLOCK, NAME)

0004 NEPR35

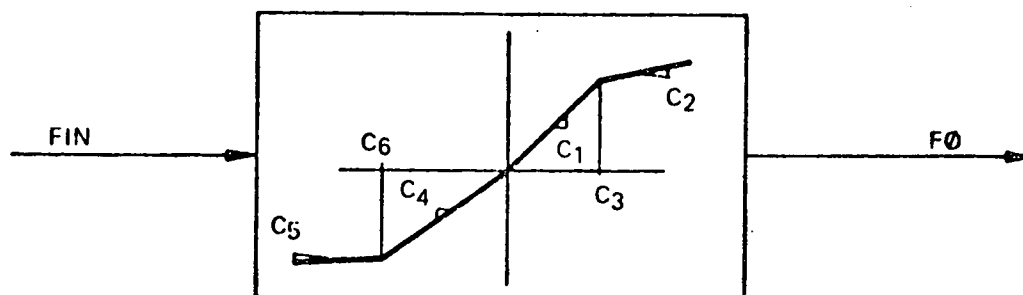
STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000026	1236	0001	000021	SL	0000	R	000006	AX0	0000	I	000007	I	0003	000001	ICNT		
0003	I	000000	IMPL	0000	000024	INJP5	0003	I	000002	ITEST	0000	D	000004	SUM	0000	D	000000	X
0000	D	000002	Y															

00100	1*	CRN				000000
00101	2*		SUBROUTINE RN(U,AX,SIG,AMN)			000000
00101	3*	C	VERSION 2.	REVISED MAY 1977		000000
00101	4*	C	PURPOSE -	GENERATES A NORMALLY DISTRIBUTED RANDOM NUMMER		000000
00101	5*	C	CALL SEQUENCE			000000
00101	6*	C		U - RANDOM NUMBER OUTPUT		000000
00101	7*	C		AX- A START PARAMETER WHICH CONTROLS THE BEGINNING POINT		000000
00101	8*	C		OF THE OUTPUT SEQUENCE. AX SHOULD BE ANY ODD INTEGER		000000
00101	9*	C		GREATER THAN ONE. THE DEFAULT VALUE OF AX IS 431469.		000000
00101	10*	C		AX IS UPDATED FOR NEW CALLS TO THE SUBROUTINE.		000000
00101	11*	C		SIG- THE DESIRED STANDARD DEVIATION OF THE SEQUENCE		000000
00101	12*	C		AMN- THE DESIRED MEAN OF THE SEQUENCE		000000
00101	13*	C				000000
00101	14*	C	DESIGNED BY	ROGER W. CALL	SEPT 1976	000000
00103	15*		COMMON /CIMPL/IMPL,ICNT,ITEST			000000
00104	16*		DOUBLE PRECISION X,Y,SUM			000000
00105	17*		DATA Y /253967.DD/ AX0/D./			000000
00110	18*		IF(IMPL.GT.0)GO TO 5			000000
00112	19*		IF(AX.EQ..999999) AX=431469.			000002
00114	20*		IF(AX0.EQ.0.) AX0= AX			000007
00116	21*		IF(ITEST.EQ.1) AX= AX0			000013
00120	22*	5	X =AX			000021
00121	23*		SUM=0.DD			000022
00122	24*		DO 1 I=1,12			000026
00125	25*		X= DMOD(X*Y,16777216.DD)			000026
00126	26*	1	SUM= SUM+ X/16777215.DD			000036
00130	27*		AX= X			000043
00131	28*		U=(SUM-6.C)*SIG*AMN			000045
00132	29*		RETURN			000054
00133	30*		END			000104

RM

7.33 SATURATION FUNCTION



Inputs

<u>Parameter/Port</u>	<u>Description</u>
FIN	Input quantity
C1	Slope $0 < \text{FIN} < C3$
C2	Slope $\text{FIN} > C3$
C3	Positive saturation intercept
C4	Slope $0 > \text{FIN} > C6$
C5	Slope $\text{FIN} < C6$
C6	Negative saturation intercept

Outputs

<u>Variable/Port</u>	<u>Description</u>
F0	Output quantity

Calculation Sequence

$F0 = C1 * C3 + C2 * (\text{FIN} - C3)$	if $\text{FIN} > C3$
$F0 = C1 * \text{FIN}$	if $0 < \text{FIN} < C3$
$F0 = C4 * \text{FIN}$	if $0 > \text{FIN} > C6$
$F0 = C4 * C6 + C5 * (\text{FIN} - C6)$	if $\text{FIN} < C6$

SUBROUTINE SA ENTRY POINT 000051

STORAGE USED CODE(1) 000076; DATA(3) 000013; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000017 10L 0001 000042 100L 0001 000027 20L 0001 000037 30L 0000 000000 INJPS

00100	1*	CSA				000000
00101	2*		SUBROUTINE SA(F0,FIN,C1,C2,C3,C4,C5,C6)			000000
00101	3*	C				000000
00101	4*	C	PURPOSE - TO SIMULATE SATURATION			000000
00101	5*	C				000000
00101	6*	C				000000
00101	7*	C	METHOD - SEE CODING. C3 AND C6 ARE VALUES OF THE INPUT AT WHICH			000000
00101	8*	C	SATURATION OCCURS. C3 IS GREATER THAN C6. THE ROUTINE			000000
00101	9*	C	CAN SIMULATE A CHANGE OF SLOPE AT THE ORIGIN (C1.NE.C4)			000000
00101	10*	C	PROVIDED C6 IS LESS THAN ZERO. SIMILARLY THE SLOPES			000000
00101	11*	C	IN THE SATURATION REGION (C2 AND C5) CAN DIFFER.			000000
00101	12*	C	THE SLOPES CAN BE POSITIVE OR NEGATIVE			000000
00101	13*	C				000000
00101	14*	C				000000
00101	15*	C	WRITTEN BY - ADAM LLOYD	LATEST REVISION - NOV 75		000000
00101	16*	C				000000
00101	17*	C	LIMITATIONS - USE OF ZERO SLOPES (C2=0 OR C5=0) IN THE SATURATION			000000
00101	18*	C	REGION SHOULD BE AVOIDED. IT IS DESIRABLE THAT THE			000000
00101	19*	C	SLOPE RATIOS C1/C2 AND C4/C5 SHOULD NOT EXCEED 100.			000000
00101	20*	C	EXCESSIVE SLOPE RATIOS MAY RESULT IN VERY SLOW			000000
00101	21*	C	CONVERGENCE			000000
00101	22*	C				000000
00101	23*	C				000000
00101	24*	C	INPUT/OUTPUT LIST			000000
00101	25*	C				000000
00101	26*	C	F0 OUTPUT VARIABLE	ANY	OUTPUT VAR	000000
00101	27*	C	FIN INPUT VARIABLE	ANY	INPUT VAR	000000
00101	28*	C	C1 SLOPE	ANY	INPUT PARAM	000000
00101	29*	C	C2 SATURATION SLOPE	ANY	INPUT PARAM	000000
00101	30*	C	C3 SATURATION INTERCEPT	ANY	INPUT PARAM	000000
00101	31*	C	C4 SLOPE	ANY	INPUT PARAM	000000
00101	32*	C	C5 SATURATION SLOPE	ANY	INPUT PARAM	000000
00101	33*	C	C6 SATURATION INTERCEPT	ANY	INPUT PARAM	000000
00101	34*	C				000000
00101	35*		IF(FIN.GT.C3)GO TO 10			000000

51

```

00105 36*      IF(FIN.LT.C6)GO TO 20
00107 37*      IF(FIN.LT.0.)GO TO 30
00111 38*      FO=C1*FIN
00112 39*      GO TO 100
00112 40*      C   POSITIVE SATURATION
00113 41*      10   FO=C1+C3+C2*(FIN-C3)
00114 42*      GO TO 100
00114 43*      C   NEGATIVE SATURATION
00115 44*      20   FO=C4+C6+C5*(FIN-C6)
00116 45*      GO TO 100
00116 46*      C   NEGATIVE UNSATURATED
00117 47*      30   FO=C4*FIN
00120 48*      100  RETURN
00121 49*      END

```

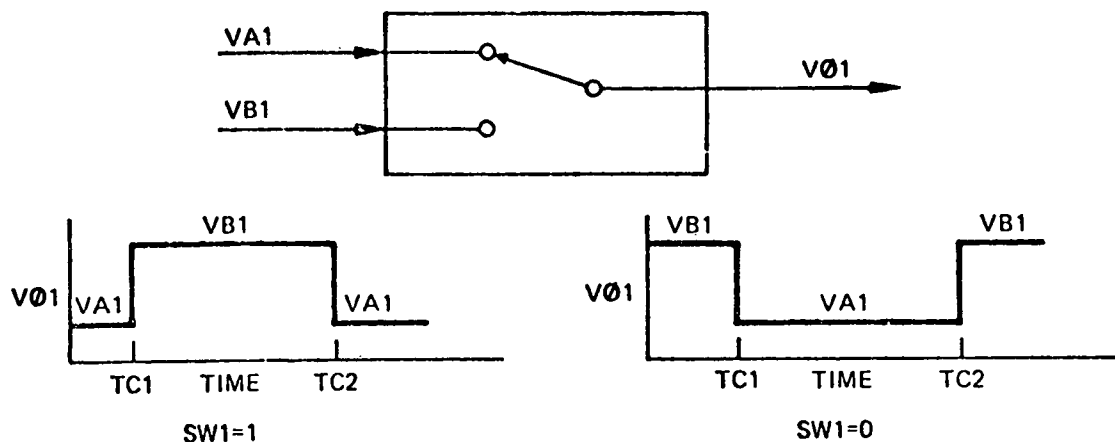
```

000003
000007
000012
000015
000015
000017
000025
000025
000027
000035
000035
000037
000042
000075

```

SA

7.34 SINGLE POLE SWITCH



THE SWITCHING OPERATION MAY BE CONTROLLED BY EITHER TIME OR THE INPUT PARAMETER SW1. THE TIME DEPENDENCE MAY BE ELIMINATED BY SETTING $TC1 = 10^{36}$

Inputs

<u>Parameter/Port</u>	<u>Description</u>
VA1	Input to switch
VB1	Input to switch
SW1	Switch control parameter
TC1	Time for first switching (hours)
TC2	Time for second switching (hours)

Outputs

<u>Variable/Port</u>	
V01	Switch output

Calculation Sequence

If $SW1 = 0$ then

$$V01 = \begin{pmatrix} VA1 & TC1 < TIME < TC2 \\ VB1 & \text{otherwise} \end{pmatrix}$$

If $SW1 = 1$ then

$$V01 = \begin{pmatrix} VB1 & TC1 < TIME < TC2 \\ VA1 & \text{otherwise} \end{pmatrix}$$

SUBROUTINE SW ENTRY POINT 000C42

STORAGE USED CODE(1) 000047; DATA(0) 000007; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CTIME 000001
0004 CIO 000003

EXTERNAL REFERENCES (BLOCK, NAME)

0005 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0004 000002 IDIAG 0000 000003 INJPS 0004 000000 IREAD 0004 000001 IWRITE 0000 R 000000 SX
0003 R 000000 TIME

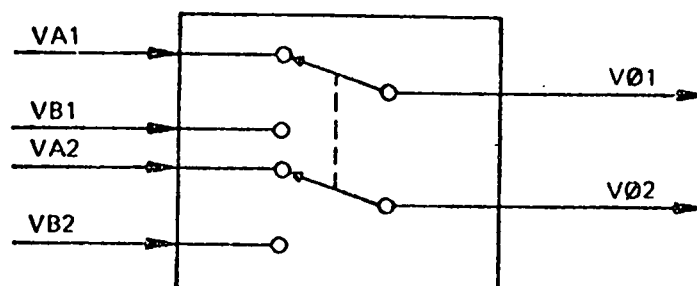
00100	1*	CSW							000000
00101	2*		SUBROUTINE SW(V01,VA1,V01,SW1,TC1,TC2)						000000
00101	3*	C							000000
00101	4*	C	PURPOSE - TO PROVIDE SWITCH CONTROL FOR ONE VARIABLE						000000
00101	5*	C							000000
00101	6*	C							000000
00101	7*	C	METHOD - SEE CODING						000000
00101	8*	C							000000
00101	9*	C							000000
00101	10*	C	WRITTEN BY - ADAM LLOYD	LATEST REVISION	NOV 75				000000
00101	11*	C							000000
00101	12*	C							000000
00101	13*	C	LIMITATIONS - NOT MORE THAN TWO SWITCHINGS AT TIMES TC1 AND TC2						000000
00101	14*	C							000000
00101	15*	C							000000
00101	16*	C	INPUT/OUTPUT LIST						000000
00101	17*	C							000000
00101	18*	C	V01 OUTPUT VARIABLE NO 1	ANY	OUTPUT VAR				000000
00101	19*	C	VA1 INPUT VARIABLE NO A1	ANY	INPUT VAR				000000
00101	20*	C	V01 INPUT VARIABLE NO R1	ANY	INPUT VAR				000000
00101	21*	C	SW1 SWITCH CONTROL INITIAL VALUE	---	INPUT PARAM				000000
00101	22*	C	=1. V0=VR						000000
00101	23*	C	=0. V0=VA						000000
00101	24*	C	TC1 TIME FOR FIRST SWITCH	SECS	INPUT PARAM				000000
00101	25*	C	TC2 TIME FOR SECOND SWITCH	SECS	INPUT PARAM				000000
00101	26*	C	(TC2.GT.TC1)						000000
00103	27*		COMMON/CTIME/TIME						000000
00104	28*		COMMON/CIO/IREAD,IWRITE,IDIAG						000000
00105	29*		SX=SW1						000000

SW

```
00106      30*      IF(TIME.GT.TC1.AND.TIME.LT.TC2)SX=ABS(SW1-1.)
00110      31*      V01=VA1
00111      32*      IF(SX.GT.0.5)V01=VB1
00113      33*      RETURN
00114      34*      END
```

```
000001
000023
000025
000033
000046
```

7.35 TWO POLE SWITCH



SEE SW FOR SWITCH CONTROL LOGIC

Inputs

Parameter/Port

Description

VA1	Input to switch 1
VA2	Input to switch 2
VB1	Input to switch 1
VB2	Input to switch 2
SW1	Switch control parameter
TC1	Time for first switching (hours)
TC2	Time for second switching (hours)

Outputs

Variable/Port

V01	Output from switch 1
V02	Output from switch 2

SUBROUTINE SX ENTRY POINT 000052

STORAGE USED CODE(1) 000062; DATA(0) 000007; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CTIME 000001
0004 CIO 000003

EXTERNAL REFERENCES (BLOCK, NAME)

0005 NERR38

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0004 000002 IDIAG 0000 000003 INJPS 0004 000000 IREAD 0004 000001 IWRITE 0000 R 000000 SW
0003 R 000000 TIME

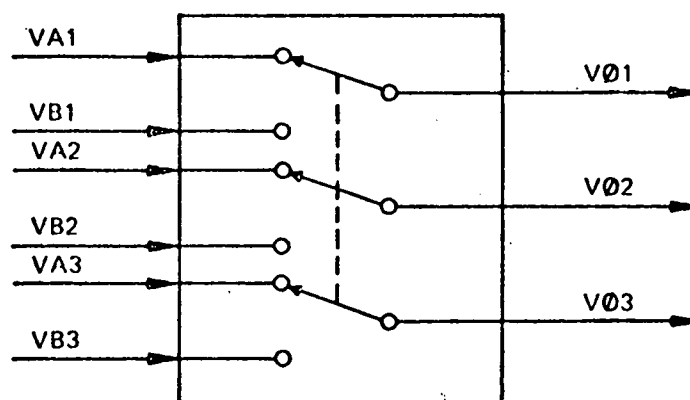
00100	1*	CSX					000000
00101	2*		SUBROUTINE SX(V01,V02,VA1,VA2,VB1,VB2,SW1,TC1,TC2)				000000
00101	3*	C					000000
00101	4*	C	PURPOSE - TO PROVIDE A SWITCH COMPONENT FOR TWO VARIABLES				000000
00101	5*	C					000000
00101	6*	C					000000
00101	7*	C	METHOD - SEE CODING				000000
00101	8*	C					000000
00101	9*	C					000000
00101	10*	C	WRITTEN BY - ADAM LLOYD	LATEST REVISION	NOV 75		000000
00101	11*	C					000000
00101	12*	C					000000
00101	13*	C	LIMITATIONS - NOT MORE THAN TWO SWITCHINGS AT TIMES TC1 AND TC2				000000
00101	14*	C					000000
00101	15*	C					000000
00101	16*	C	INPUT/OUTPUT LIST				000000
00101	17*	C					000000
00101	18*	C	V01	OUTPUT VARIABLE NO 1	ANY	OUTPUT VAR	000000
00101	19*	C	V02	OUTPUT VARIABLE NO 2	ANY	OUTPUT VAR	000000
00101	20*	C	VA1	INPUT VARIABLE NO A1	ANY	INPUT VAR	000000
00101	21*	C	VA2	INPUT VARIABLE NO A2	ANY	INPUT VAR	000000
00101	22*	C	VB1	INPUT VARIABLE NO B1	ANY	INPUT VAR	000000
00101	23*	C	VB2	INPUT VARIABLE NO B2	ANY	INPUT VAR	000000
00101	24*	C	SW1	SWITCH CONTROL INITIAL VALUE	---	INPUT PARAM	000000
00101	25*	C		=1. VO=VB			000000
00101	26*	C		=0. VO=VA			000000
00101	27*	C	TC1	TIME FOR FIRST SWITCH	SECS	INPUT PARAM	000000
00101	28*	C	TC2	TIME FOR SECOND SWITCH	SECS	INPUT PARAM	000000
00101	29*	C		(TC2.GT.TC1)			000000

00103	30*	COMMON/CTIME/TIME
00104	31*	COMMON/CIO/TREAD,TWRITE,IDIAS
00105	32*	SW=SW1
00106	33*	IF (TIME.GT.TC1.AND.TIME.LT.TC2) SW=ABS (SW1-1.)
00110	34*	V01=VA1
00111	35*	V02=VA2
00112	36*	IF (SW.GT.0.5) V01=VB1
00114	37*	IF (SW.GT.0.5) V02=VB2
00116	38*	RETURN
00117	39*	END

C0C000
C00000
C00000
C0C001
C0G023
C00025
C00027
C00035
C0G043
C00061

SX

7.36 THREE POLE SWITCH



SEE SW FOR SWITCH CONTROL LOGIC

Inputs

<u>Parameter/Port</u>	<u>Description</u>
VA1	Input to switch 1
VA2	Input to switch 2
VA3	Input to switch 3
VB1	Input to switch 1
VB2	Input to switch 2
VB3	Input to switch 3
SW1	Switch control parameter
TC1	Time for first switching (hours)
TC2	Time for second switching (hours)

Outputs

<u>Variable/Port</u>	
V01	Output from switch 1
V02	Output from switch 2
V03	Output from switch 3

ENTRY POINT 000063

STORAGE USED CODE(1) 000077; DATA(0) 000011; BLANK COMMON(2) 000000

```
0003      CTIME      000001
0004      CIO        000003
```

0205 · NEAR38

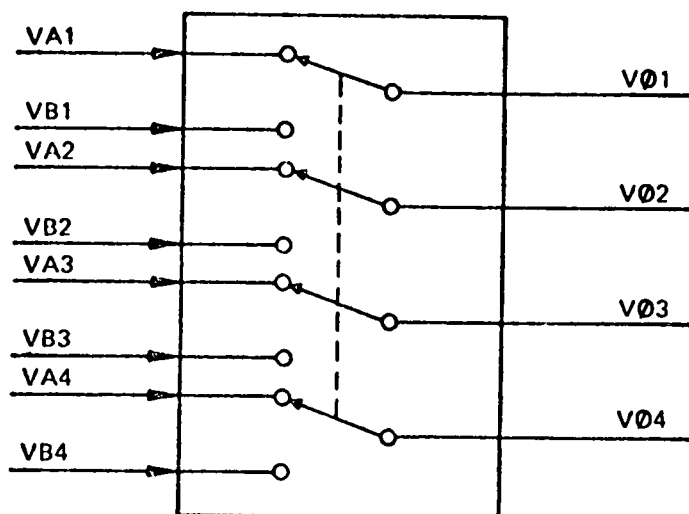
```
0004 000002 IDIAG      0000 000003 INJPS      0004 000000 IREAD      0004 000001 IWRITE      0000 R 000000 SW
0003 R 000000 TIME
```

[illegible]

SYN

00101	30*	C	TC1	TIME FOR FIRST SWITCH	SECS	INPUT	PARAM	000000
00101	31*	C	TC2	TIME FOR SECOND SWITCH	SECS	INPUT	PARAM	000000
00101	32*	C		(TC2.GT.TC1)				000000
00103	33*			COMMON/CTIME/TIME				000000
00104	34*			COMMON/CIO/IREAD,IWRITE,IDIAG				000000
00105	35*			SW=SW1				000000
00106	36*			V01=VA1				000001
00107	37*			V02=VA2				000003
00110	38*			V03=VA3				000005
00111	39*			IF(TIME.GT.TC1.AND.TIME.LT.TC2)SW=ABS(SW1-1.)				000007
00113	40*			IF(SW.GT.0.5)V01=VB1				000031
00115	41*			IF(SW.GT.0.5)V02=VB2				000037
00117	42*			IF(SW.GT.0.5)V03=VB3				000045
00121	43*			RETURN				000053
00122	44*			END				000076

7.37 FOUR POLE SWITCH



SEE SW FOR SWITCH CONTROL LOGIC

Inputs

<u>Parameter/Port</u>	<u>Description</u>
VA1	Input to switch 1
VA2	Input to switch 2
VA3	Input to switch 3
VA4	Input to switch 4
VB1	Input to switch 1
VB2	Input to switch 2
VB3	Input to switch 3
VB4	Input to switch 4
SW1	Switch control parameter
TC1	Time for first switching (hours)
TC2	Time for second switching (hours)

Outputs

<u>Variable/Port</u>	
V01	Output from switch 1
V02	Output from switch 2
V03	Output from switch 3
V04	Output from switch 4

SUPROUTINE SZ ENTRY POINT 000073

STORAGE USED CODE(1) 000112; DATA(0) 000011; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CTIME 000001
0004 CIO 000003

EXTERNAL REFERENCES (BLOCK, NAME)

0005 NERR35

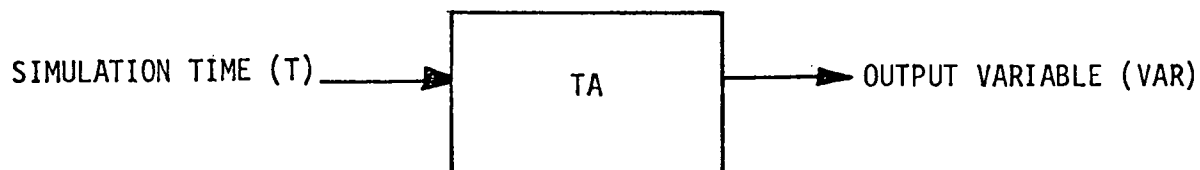
STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0004 000002 INIAG 0000 000003 INJPS 0004 000000 IREAD 0004 000001 IWRITE 0000 R 000000 SW
0003 R 000000 TIME

00100	1*	CSZ				000000
00101	2*		SUBROUTINE SZ (V01,V02,V03,V04,VA1,VA2,VA3,VA4,VB1,VB2,VB3,VB4,			000000
00101	3*		1 SW1,TC1,TC2)			000000
00101	4*	C				000000
00101	5*	C	PURPOSE - TO PROVIDE A SWITCH COMPONENT FOR FOUR VARIABLES			000000
00101	6*	C				000000
00101	7*	C				000000
00101	8*	C	METHOD - SEE CODING			000000
00101	9*	C				000000
00101	10*	C				000000
00101	11*	C	WRITTEN BY - ADAM LLOYD	LATEST REVISION	NOV 75	000000
00101	12*	C				000000
00101	13*	C				000000
00101	14*	C	LIMITATIONS - NOT MORE THAN TWO SWITCHINGS AT TIMES TC1 AND TC2			000000
00101	15*	C				000000
00101	16*	C				000000
00101	17*	C	INPUT/OUTPUT LIST			000000
00101	18*	C				000000
00101	19*	C	V01	OUTPUT VARIABLE NO 1	ANY	OUTPUT VAR
00101	20*	C	V02	OUTPUT VARIABLE NO 2	ANY	OUTPUT VAR
00101	21*	C	V03	OUTPUT VARIABLE NO 3	ANY	OUTPUT VAR
00101	22*	C	V04	OUTPUT VARIABLE NO 4	ANY	OUTPUT VAR
00101	23*	C	VA1	INPUT VARIABLE NO A1	ANY	INPUT VAR
00101	24*	C	VA2	INPUT VARIABLE NO A2	ANY	INPUT VAR
00101	25*	C	VA3	INPUT VARIABLE NO A3	ANY	INPUT VAR
00101	26*	C	VA4	INPUT VARIABLE NO A4	ANY	INPUT VAR
00101	27*	C	VB1	INPUT VARIABLE NO B1	ANY	INPUT VAR
00101	28*	C	VB2	INPUT VARIABLE NO B2	ANY	INPUT VAR
00101	29*	C	VB3	INPUT VARIABLE NO B3	ANY	INPUT VAR

00101	30*	C	VB4	INPUT VARIABLE NO B4	ANY	INPUT	VAR	000000
00101	31*	C	SW1	SWITCH CONTROL INITIAL VALUE	---	INPUT	PARAM	000000
00101	32*	C		=1. V0=VB				000000
00101	33*	C		=0. V0=VA				000000
00101	34*	C	TC1	TIME FOR FIRST SWITCH	SECS	INPUT	PARAM	000000
00101	35*	C	TC2	TIME FOR SECOND SWITCH	SECS	INPUT	PARAM	000000
00101	36*	C		(TC2.GT.TC1)				000000
00103	37*			COMMON/CTIME/TIME				000000
00104	38*			COMMON/CIO/IREAD,IWRITE,IDIAG				000000
00105	39*			SW=SW1				000000
00106	40*			IF(TIME.GT.TC1.AND.TIME.LT.TC2)SW=ABS(SW1-1.)				000001
00110	41*			V01=VA1				000023
00111	42*			V02=VA2				000025
00112	43*			V03=VA3				000027
00113	44*			V04=VA4				000031
00114	45*			IF(SW.GT.0.5)V01=VB1				000033
00116	46*			IF(SW.GT.0.5)V02=VB2				000041
00120	47*			IF(SW.GT.0.5)V03=VB3				000047
00122	48*			IF(SW.GT.0.5)V04=VB4				000055
00124	49*			RETURN				000063
00125	50*			END				000111

7.38 TAPE/FILE READ



This component reads a data file containing a single output variable time history. The file structure is specified below, and assumes equal increment data. Linear interpolation is used to obtain the output value. No more than eight TA components are allowed per model. The component T1 is used to supply the time input T. The data files must be catalogued using the names F1, F2, or the JCL procedure file XQTANALYSIS modified appropriately. If tape data is used, it must be read into permanent storage files in a prior job step.

Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
NST	Number of records to skip at start ¹	
T	Simulation time referenced to start of year	hr
ITF	Indicator function: 0 = no read J = read data into Jth array (J ≤ 8)	

¹ NST = (start time of simulation - start time of file) / (data increment × 446)

Outputs

<u>Variable/Port</u>	<u>Description</u>	<u>Units</u>
VAR	Output variable at time T	
N	Length of file record	
T0	Time of first data value in current record	hr
H	Time increment between data values	hr

Record Structure

1st record = identification header, 28 words

Nth record ($N > 1$): 448 words

first word = time of first data value in hours (T0)

second word = time increment between data values (H)

J+2 word = data value at time = $T0 + (J-1)H$

($J=1, \dots, 446$)

If the useful data ends in the middle of a record, then an end value = .99999 is used to signal end of information.

Calculation Sequence

If ITF = 0 RETURN

1) Initialization. (First Pass Only)

o Read 1st record and write out identification header data and unit number. (Error exit to 6))

o Read past NST data records. Go to 4)

Calculation Sequence Cont.

2) File location incorrect; use initial value

```
o If  $T \geq T_0$  GO TO 3)
  Write diagnostic
  VAR = A(1,J)    (J=1TF)
  Return
```

3) Table Interpolation for Output

```
o If  $T \geq T_0 + N * H$  GO TO 4)
  XT(1) =  $T_0$ 
  XT(2) =  $T_0 + H$ 
  VAR = TBLU1(T,XT,A(1,J),0,N)
  Return
```

4) Read Next Data Record

```
If end has been encountered previously go to 5)
Read next record into array A(*,J). If end encountered, set
N = last value. (Error exit to 6))
   $T_0 = A(1,J)$ 
   $H = A(2,J)$ 
  GO TO 3)
```

5) End of File. Use last value.

```
VAR = A(N,J)
Write Diagnostic
Return
```

6) Read Error Encountered

```
Write Diagnostic and STOP
```

SUBROUTINE TA ENTRY POINT 000343

STORAGE USED CODE(1) 000403; DATA(3) 007132; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CEMPL 000002
0004 DATARD 000700

EXTERNAL REFERENCES (BLOCK, NAME)

0005 NTRAN
0006 TBLU1
0007 NWDUS
0010 IIO3S
0011 NI02S
0012 NSTOPS
0013 NERR3S

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000321 10L	0001 000102 100L	0001 000231 1676	0000 007035 20F	0001 000135 200L
0000 007046 30F	0001 000176 300L	0001 000262 400L	0001 000244 60L	0000 007062 80F
0000 007076 90F	0000 R 000000 A	0000 R 006760 B	0000 I 007034 I	0003 I 000001 ICNT
0003 I 000000 IMPL	0000 I 007014 IND	0000 007121 INJPS	0000 I 007030 IUM	0000 I 007027 J
0000 I 007031 LI	0000 I 007033 N	0000 I 007032 NO	0006 R 000000 TBLU1	0004 R 000000 TEMP
0000 R 007026 X	0000 R 007024 XT			

00100	1*	CTAPE		000000
00101	2*		SUBROUTINE TA(VAR,NOUT,TD,H,NST,T,ITF)	000000
00101	3*	C		000000
00101	4*	C	PURPOSE READ TIME HISTORY DATA ON STORAGE DEVICE	000000
00101	5*	C		000000
00101	6*	C		000000
00101	7*	C	METHOD USE NTRAN SEQUENTIAL BLOCK READ FROM MASS STORAGE	000000
00101	8*	C	INTO CORE. LINEAR INTERPOLATION IS USED TO OBTAIN	000000
00101	9*	C	VALUE AT SPECIFIED TIME T.	000000
00101	10*	C		000000
00101	11*	C	WRITTEN BY A.W. WARREN	000000
00101	12*	C		000000
00101	13*	C	CALL SEQUENCE	000000
00101	14*	C	OUTPUTS	000000
00101	15*	C	VAR - OUTPUT VARIABLE AT TIME T	000000
00101	16*	C	NOUT - LENGTH OF DATA BLOCK LAST READ	000000
00101	17*	C	TD - TIME OF FIRST DATA VALUE IN CORE, HR	000000
00101	18*	C	H - TIME INCREMENT BETWEEN DATA VALUES, HR	000000
00101	19*	C	INPUTS	000000

TA

00101	20*	C	NST - NUMBER OF BLOCKS TO SKIP AT START	000000
00101	21*	C	T - SIMULATION TIME REFERENCED TO START OF YEAR, HR	000000
00101	22*	C	ITF - INDICATOR FOR LOGICAL UNIT TO READ	000000
00101	23*	C	= 0 NO READ	000000
00101	24*	C	= 1,...8 FOR LOGICAL UNITS 11,...18, RESP.	000000
00101	25*	C		000000
00103	26*		DIMENSION A(446,8),B(28),IND(8),XT(2)	000000
00104	27*		COMMON /CIMPL/ IMPL,ICNT /DATARD/ TEMP(448)	000000
00105	28*		REAL NST,NOUT,ITF	000000
00106	29*		DATA X/.999999/	000000
00106	30*	C		000000
00106	31*	C	INITIALIZE AND POSITION THE FILE	000000
00106	32*	C		000000
00110	33*		VAR=X	000000
00111	34*		J=ITF+.001	000001
00112	35*		IF(J.EQ.0) RETURN	000012
00114	36*		IUN= J+10	000017
00115	37*		IF(IMPL.67.0) GO TO 100	000022
00115	38*	C		000022
00117	39*		CALL NTRAN(IUN,10)	000026
00120	40*		CALL NTRAN(IUN,2,28,B,L1,22)	000032
00121	41*		IF(L1.LT.0)GO TO 10	000042
00123	42*		WRITE(6,20) IUN,B	000045
00127	43*	20	FORMAT(1H0,30HIDENTIFICATION HEADER FOR UNIT,13/(1H ,10A6))	000056
00130	44*		NO= NST*16.+.001	000056
00131	45*		CALL NTRAN(IUN,6,NO,22)	000070
00132	46*		IND(J)= L1	000076
00133	47*		GO TO 300	000100
00133	48*	C		000100
00133	49*	C	TOO MANY BLOCKS READ	000100
00133	50*	C		000100
00134	51*	100	IF(T.GE.TO) GO TO 200	000102
00136	52*		VAR= A(1,J)	000105
00137	53*		IF(IMPL.EQ.2) WRITE(6,30) VAR,IUN	000111
00144	54*	30	FORMAT(1H0,39HFILE DATA OUT OF RANGE. INITIAL VALUE= ,	000123
00144	55*	1	F12.5,9H ON UNIT,14)	000123
00145	56*		IF(IMPL.EQ.2)ICNT=ICNT+1	000131
00147	57*		RETURN	000131
00147	58*	C		000131
00147	59*	C	TABLE INTERPOLATION FOR OUTPUT	000131
00147	60*	C		000131
00150	61*	200	IF(T.GE.TO+NOUT*H) GO TO 300	000135
00152	62*		XT(1)= TO	000142
00153	63*		XT(2)= TO+H	000144
00154	64*		N=NOUT	000146
00155	65*		VAR = TBLU1(T,XT,A(1,J),0,N)	000155
00156	66*		RETURN	000172
00156	67*	C		000172
00156	68*	C	READ NEXT DATA BLOCK	000172
00156	69*	C		000172
00157	70*	300	IF(IND(J).EQ.0)GO TO 400	000176
00161	71*		CALL NTRAN(IUN,2,448,TEMP,IND(J),22)	000200
00162	72*		IF(IND(J).LT.0)GO TO 10	000212
00164	73*		TO= TEMP(1)	000220
00	74*		H= TEMP(2)	000222
00	75*	C		000222
00166	76*		DO 50 I=1,446	000231

TA

```

00171 77*      IF(TEMP(I+2).EQ.X)GO TO 60
00173 78*      50 A(I,J)= TEMP(I+2)
00175 79*      I=I+1
00176 80*      60 NCUT= I-1
00177 81*      IF(I.LT.447)INO(J)=0
00201 82*      60 TO 200
00201 83*      C
00201 84*      C      END OF USEFUL DATA REACHED
00201 85*      C      (.99999 DATA VALUE ENCOUNTERED.)
00201 86*      C
00202 87*      400 N= NCUT
00203 88*      VAR=A(N,J)
00204 89*      IF(IMPL.EQ.2)WRITE(6,80)VAR,IUN
00211 90*      80 FORMAT(1H0,41HTIME POINT PAST TABLE RANGE. LAST VALUE= ,
00211 91*      1 F12.5,9H ON UNIT,I4)
00212 92*      IF(IMPL.EQ.2)ICNT=ICNT+1
00214 93*      RETURN
00214 94*      C
00214 95*      C      READ ERROR OR END OF FILE REACHED
00214 96*      C
00215 97*      10 WRITE(6,90)IUN
00220 98*      90 FORMAT(1H0,33HREAD ERROR OR END OF FILE ON UNIT,I4)
00221 99*      STOP
00222 100*     END 2 SUBROUTINE TA

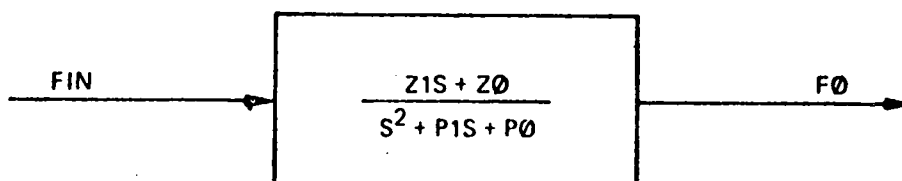
```

```

000231
000234
000240
000244
000250
000260
000260
000260
000260
000260
000262
000270
000275
000307
000307
000307
000315
000315
000315
000315
000321
000326
000326
000402

```

7.39 SECOND ORDER TRANSFER FUNCTION



Inputs

<u>Parameter/Port</u>	<u>Description</u>
FIN	Input quantity
Z0	Numerator coefficient
Z1	Numerator coefficient
P0	Denominator coefficient
P1	Denominator coefficient

Outputs

Variable/Port

X1	Intermediate state
F0	Output quantity (state)

Calculation Sequence

$$\begin{aligned} \dot{X1} &= Z0*FIN - P0*F0 \\ \dot{F0} &= X1 + Z1*FIN - P1*F0 \end{aligned}$$

NOTE: d.c. gain = $\frac{Z0}{P0}$; infinite frequency gain = 0.

SUBROUTINE TF

ENTRY POINT 000027

STORAGE USED CODE(1) 000035; DATA(0) 000004; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 C10 000003

EXTERNAL REFERENCES (BLOCK, NAME)

0004 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

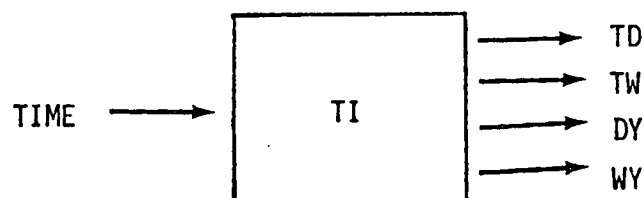
0003 000002 IDIAG 0000 000000 INJPS DC03 000000 IREAD 0003 000001 IWRITE

00100	1*	CTF				000000
00101	2*		SUBROUTINE TF(X1,X1DOT,IX1,F0,F0DOT,IFO,FIN,Z0,Z1,PO,P1)			000000
00101	3*	C				000000
00101	4*	C	PURPOSE - TO SIMULATE A SECOND ORDER TRANSFER FUNCTION WITH			000000
00101	5*	C	FIRST ORDER NUMERATOR			000000
00101	6*	C				000000
00101	7*	C	F0	Z1*S + Z0		000000
00101	8*	C	$\frac{\text{F0}}{\text{FIN}} = \frac{\text{Z1*S} + \text{Z0}}{\text{S} + \text{P1*S} + \text{PO}}$			000000
00101	9*	C	FIN	2		000000
00101	10*	C		S + P1*S+PO		000000
00101	11*	C				000000
00101	12*	C	METHOD - SELF EXPLANATORY			000000
00101	13*	C				000000
00101	14*	C				000000
00101	15*	C	LIMITATIONS - NONE			000000
00101	16*	C				000000
00101	17*	C				000000
00101	18*	C	WRITTEN BY	ADAM LLOYD	LATEST REVISION NOV 75	000000
00101	19*	C				000000
00101	20*	C				000000
00101	21*	C	INPUT/OUTPUT LIST			000000
00101	22*	C				000000
00101	23*	C	X1	INTERMEDIATE STATE VARIABLE	ANY	OUTPUT STATE
00101	24*	C	X1DOT	STATE VARIABLE DERIVATIVE	ANY	OUTPUT STATE
00101	25*	C	IX1	INTEGRATOR CONTROL	---	PROGRAM VAR
00101	26*	C	F0	TRANSFER FUNCTION OUTPUT	ANY	OUTPUT STATE
00101	27*	C	F0DOT	TRANSFER FUNCTION OUTPUT DERIV.	ANY	OUTPUT STATE
00101	28*	C	IFO	INTEGRATOR CONTROL	---	PROGRAM VAR
00101	29*	C	FIN	TRANSFER FUNCTION INPUT	ANY	INPUT VAR
00101	30*	C	Z0	NUMERATOR COEFFICIENT	ANY	INPUT VAR
00101	31*	C	Z1	NUMERATOR COEFFICIENT	ANY	INPUT VAR



00101	32*	C	P0	DENOMINATOR COEFFICIENT	1/SEC2	INPUT	VAR	000000
00101	33*	C	P1	DENOMINATOR COEFFICIENT	1/SEC	INPUT	VAR	000000
00103	34*			COMMON/C10/IREAD,IWRITE,IOIAS				000000
00104	35*			IF(IX1.NE.0)X1DOT=20*FIN-P0*F0				000000
00106	36*			IF(IFO.NE.0)F0DOT=X1+21*FIN-P1*F0				000007
00110	37*			RETURN				000020
00111	38*			END				000034

7.40 TIME CONVERSION



Converts simulation running time in hours to time referenced to start of day and start of week, and computes number of days and weeks elapsed since start of year.

Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
TO	Initial time of simulation from start of year	hrs
TIME	Running time (input via common/CTIME)	hrs

Outputs

<u>Variable/Port</u>		
TW	Time since start of week	hrs
TD	Time since start of day	hrs
WY	Number of weeks	-
DY	Number of days	-
MY	Number of months (approx.)	-
T	Running time from start of year	hrs
DW	Day of week	-

Calculation Sequence

$T = \text{AMOD}(TO + \text{TIME}, 8760)$	$TW = \text{AMOD}(T, 168)$
$WY = T / 168 + 1$	$TD = \text{AMOD}(T, 24)$
$DY = T / 24 + 1$	$DW = TW / 24 + 1$
$MY = T / 730 + 1$	

SUBROUTINE TI ENTRY POINT 000122

STORAGE USED CODE(1) 000155; DATA(0) 000031; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CTIME 000001

EXTERNAL REFERENCES (BLOCK, NAME)

0004 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 000013 INJPS 0000 I 000002 MY 0000 I 000000 ND 0000 I 000001 NW 0003 R 000000 TIME

00100	1*	CTI		000000
00101	2*		SUBROUTINE TI(T,TD,TW,DW,DY,WY,MY,TO)	000000
00101	3*	C		000000
00101	4*	C	PURPOSE CONVERT SIMULATION TIME TO DAILY, WEEKLY, MONTHLY UNITS	000000
00101	5*	C		000000
00101	6*	C	WRITTEN BY A.W. WARREN	000000
00101	7*	C	VERSION 1, MARCH 3 1977	000000
00101	8*	C	CALL SEQUENCE	000000
00101	9*	C	T - SIMULATION TIME FROM START OF YEAR, HR	000000
00101	10*	C	TD - TIME OF DAY, HR	000000
00101	11*	C	TW - TIME SINCE START OF WEEK, HR	000000
00101	12*	C	DW - DAY OF WEEK	000000
00101	13*	C	DY - DAY OF YEAR	000000
00101	14*	C	WY - WEEK OF YEAR	000000
00101	15*	C	MY - MONTH OF YEAR (APPROX.)	000000
00101	16*	C	TO - SIMULATION INITIAL TIME FROM START OF YEAR, HR	000000
00101	17*	C		000000
00103	18*		COMMON / CTIME / TIME	000000
00104	19*		T = AMOD(TO + TIME, 8760.)	000000
00105	20*		TD = AMOD(T, 24.)	000000
00106	21*		TW = AMOD(T, 168.)	000000
00107	22*		ND = TW/24.+1.001	000000
00110	23*		DW = ND	000000
00111	24*		ND = T/24.+1.001	000000
00112	25*		DY = ND	000000
00113	26*		NW = T/168.+1.001	000000
00114	27*		WY = NW	000000
00115	28*		MY = T/730.+1.001	000000
00116	29*		AMY = MY	000000
00116	30*	C		000000
001	31*		RETURN	000000

11

00120

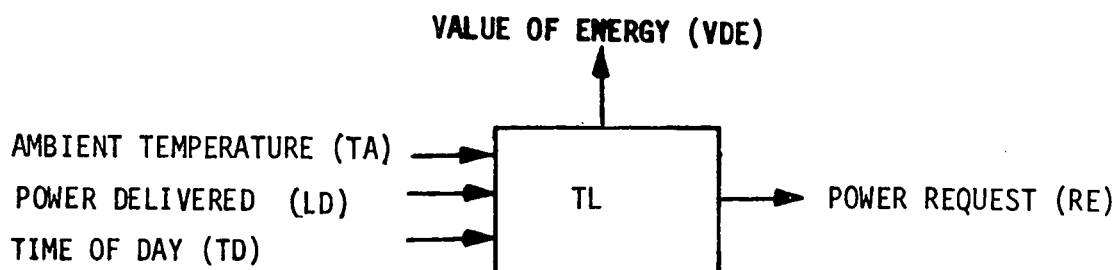
32*

END

000154



7.41 THERMAL LOAD



Thermal load is computed as a user specified function of ambient temperature and time of day. The actual load delivered is either the load requested or the maximum discharge rate of the thermal storage chamber. The value of the thermal energy delivered and % of total load actually delivered are also computed.

Basic Equation

$$RE = TL\theta(TA) * TWT(TD) * NC$$

where

$TL\theta$ = Thermal load versus temperature table

TWT = Daily profile weighting function

NC = Normalizing constant

<u>Tables</u>	<u>Description</u>	<u>Units</u>
TL0	Thermal load versus ambient temperature	kw
TWT	Daily profile weighting function (tabular with time of day)	

<u>Inputs</u>		
<u>Parameter/Port</u>		
TA	Ambient temperature	°F
LD	Power delivered	kw
TD	Time of day (0-24)	h
VE	Value of thermal energy	\$/kwh
NC	Normalizing constant	

<u>Outputs</u>		
<u>Variable/Port</u>		
RE	Load request	kw
VDE	Total value of energy delivered (state)	\$

<u>Statistics</u>		
PC	Cumulative percent of load delivered	-
SLD	Total energy delivered	kwh
SRE	Total energy requested	kwh

Calculation Sequence

- 1) Compute load request

$$RE = TL0(TA)*TWT(TD)*NC$$

- 2) Value of energy dynamics

$$\dot{VDE} = LD*VE$$

- 3) Statistics

$$SLD = SLD + LD * \Delta / 2$$

$$SRE = SRE + RE * \Delta / 2$$

$$PC = 100. * SLD / SRE$$

where Δ = integration step size

ENTRY POINT 000173

COMMON BLOCKS

```
0003      CIMPL      C00001
0004      CSIMUL     000010
0005      CTIME      000001
0006      COST       000006
```

0007 TBLUI
0010 NERR3S

0001	C00034	100L	0006	030000	CC	0006	R	000004	CLD	0006	000001	CM	0006	000002	CO	
0006	R	000005	CRE	0006	R	000003	CV	0004	R	000000	DUM	0003	I	000000	IMPL	
0000	I	000000	ITL	0000	I	000001	ITW	0007	R	000000	TBLU1	0005	R	000000	TIME	
0000	R	000003	TINC1	0000	R	000004	TLD	0004	R	000007	TMAX	0000	R	000002	TMAX1	
													0004	R	000006	TINC
													0000	R	000005	TW

```

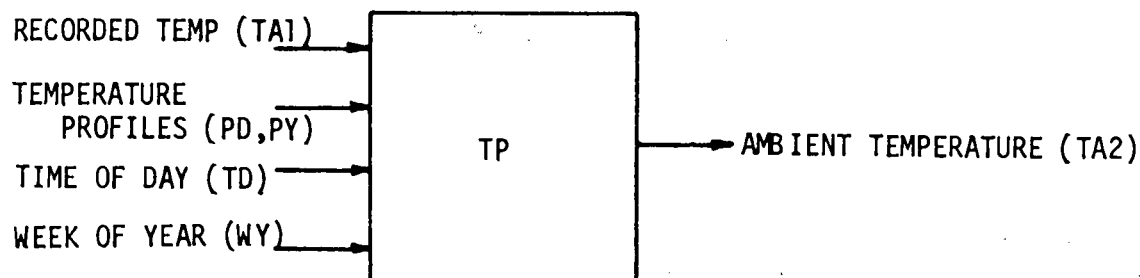
00100      1*      CTL
00101      2*      SUBROUTINE TL(TLO,TWT,VDE,DVD,IVD,RE,PC,SLO,SRE,TA,LD,TD,VE,NC)
00101      3*      C
00101      4*      C    PURPOSE      COMPUTE ENERGY RESPONSE FROM A THERMAL LOAD REQUEST
00101      5*      C
00101      6*      C    METHOD        ENERGY DELIVERED IS EQUAL TO THE LOAD REQUESTED OR
00101      7*      C
00101      8*      C              THE MAXIMUM DISCHARGE RATE.
00101      9*      C
00101     10*      C    WRITTEN BY F. O. MAHONY                                VERSION 1, APRIL 1 1977
00101     11*      C
00101     12*      C    CALL SEQUENCE
00101     13*      C          TABLES
00101     14*      C          TLO - THERMAL LOAD AS FUNCTION OF AMBIENT TEMPERATURE
00101     15*      C          TWT - DAILY PROFILE WEIGHTING FUNCTION VS TIME OF DAY
00101     16*      C
00101     17*      C          OUTPUTS
00101     18*      C          VDE - VALUE OF ENERGY DELIVERED (STATE), %
00101     19*      C          DVD - DERIVATIVE OF VDE
00101     20*      C          IVD - INDICATOR FOR VDE
00101     21*      C          RE - LOAD REQUEST, KW
00101     22*      C          PC - CUMULATIVE PERCENT OF LOAD DELIVERED
00101     23*      C          SLO - TOTAL ENERGY DELIVERED, KWH
00101     24*      C          SRE - TOTAL ENERGY REQUESTED, KWH

```

[illegible]

00101	25*	C		000001
00101	26*	C	INPUTS	000001
00101	27*	C	TA - AMBIENT TEMPERATURE, DEG F	000001
00101	28*	C	LD - POWER DELIVERED, KW	000001
00101	29*	C	TD - TIME OF DAY, HR	000001
00101	30*	C	VE - VALUE OF THERMAL ENERGY, S/KWH	000001
00101	31*	C	NC - NORMALIZING CONSTANT FOR LOAD REQUEST	000001
00101	32*	C		000001
00103	33*		DIMENSION TLO(3),TWT(5)	000001
00104	34*		COMMON/CIMPL/IMPL /CSIMUL/ DUM(6),TINC,THAX/CTIME/TIME	000001
00105	35*		COMMON/COST /CC,CM,CO,CV,CLD,CRE	000001
00106	36*		REAL LD,NC	000001
00106	37*	C		000001
00107	38*		ITL=TLO(2)	000001
00110	39*		ITW=TWT(2)	000010
00111	40*		IF(IMPL.GT.0)GO TO 100	000017
00111	41*	C		000017
00111	42*	C		000017
00113	43*		THAX1=THAX*0.99999	000022
00114	44*		TINC1=TINC*.5	000025
00114	45*	C		000025
00115	46*		PC=0.0	000030
00116	47*		SLD=0.0	000031
00117	48*		SRE=0.0	000032
00117	49*	C		000032
00117	50*	C		000032
00117	51*	C	COMPUTE LOAD REQUEST	000032
00117	52*	C		000032
00120	53*		100 TLD=TLU1(TA,TLO(4),TLO(ITL+4),1,-ITL)	000034
00121	54*		TW=TLU1(TD,TWT(4),TWT(ITW+4),1,-ITW)	000053
00121	55*	C		000053
00122	56*		RE=TLD*TW*NC	000073
00122	57*	C		000073
00122	58*	C	VALUE OF ENERGY	000073
00122	59*	C		000073
00123	60*		IF(IVD.NE.C)DVD=LD*VE	000076
00123	61*	C		000076
00125	62*		IF(IMPL.LE.1)RETURN	000103
00125	63*	C		000103
00125	64*	C	PERFORMANCE STATISTICS	000103
00125	65*	C		000103
00127	66*		SLD=SLD+LD*TINC1	000115
00130	67*		SRE=SRE+RE*TINC1	000120
00130	68*	C		000120
00131	69*		IF(SRE.GT.0.0)PC=100.0*SLD/SRE	000124
00131	70*	C		000124
00133	71*		IF(TIME.LT.THAX1)RETURN	000133
00133	72*	C		000133
00135	73*		CV=CV+VDE	000142
00136	74*		CLD=CLD+SLD-LD*TINC1	000145
00137	75*		CRE= CRE+ SRE-RE*TINC1	000151
00137	76*	C		000151
00137	77*		RETURN	000157
001	78*		END	000250

7.42 AMBIENT TEMPERATURE



This component is very similar to the wind component. Ambient temperature is output either from user supplied time histories on storage files or by generating a set of random numbers with user specified random variations. If user supplied profiles are available, then the temperatures are generated from the following equation:

$$TA2 = [PD(TD) + CN(t)] * PY(WY) / M0$$

where PD and PY are the user supplied daily and weekly profiles, TD and WY are the time of the day and week of the year, CN is a colored noise term and M0 is the average value of PY:

$$M0 = \frac{1}{J} \sum_{j=1}^J PY(j)$$

<u>Tables</u>	<u>Description</u>	<u>Units</u>
PD	Daily profile versus TD	$^{\circ}\text{F}$
PY	Yearly profile versus WY	arbitrary

Inputs

<u>Parameter/Port</u>			
TA	1	Ambient temperature data file	$^{\circ}\text{F}$
TD		Time of day	hr
WY		Week of the year	-
CT		Correlation time of colored noise	hr
MN		Mean temperature of colored noise	$^{\circ}\text{F}$
STD		Standard deviation of colored noise	$^{\circ}\text{F}$

Outputs

<u>Variable/Port</u>			
CN		Colored noise sample	$^{\circ}\text{F}$
TA	2	Ambient temperature	$^{\circ}\text{F}$
AV		Mean of daily temperature	$^{\circ}\text{F}$
MO		Mean of yearly profile	
TIM		Last time a random sample was generated	hr

Calculation Sequence

1) Initialization (first pass only)

Compute AV, MO, and initial CN

$$AV = MN + \frac{1}{N} \sum_{j=1}^N PD(j)$$

2) Check for data file input

If TA1 = .99999 go to 3)

TA2 = TA1

Return

3) Generate colored noise sample CN

If TIME = TIM RETURN

$$A = \begin{cases} \text{EXP}(-TINC/CT) & CT > 0 \\ 0. & CT = 0 \end{cases}$$

where TINC = integration step size

CN = CN * A + W

Where W is white noise with mean = MN*(1-A) and

standard deviation = STD* $\sqrt{1-A^2}$

TIM = TIME

4) Compute Temperature

TA2 = (PD(TD) + CN) * PY (WY) / MO

ENTRY POINT 000265

COMMON BLOCKS

```
0003      CIMPL      000001
0004      CSTMUL      000007
0005      CTIME       000001
```

EXTERNAL REFERENCES (BLOCK, NAME)

```
0006      RN
0007      TBLUI
0010      EXP
0011      SQRT
0012      NERR3$
```

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000121	10L	0001	000127	100L	0001	000057	1176	0001	000102	1276	0001	000247	150L	
0000	R	C00G05	A	0000	R	000000	AX	0000	R	000011	0TP	0004	000000	DUM	
0003	I	00C000	IMPL	0000	000016	INJPS		0000	I	000004	L	0000	I	000001	ND
0007	R	000000	TRLU1	0005	R	000000	TIME	0004	R	000006	TI NC	0000	R	000010	W
0003	R	000007	WSD	0000	R	000012	YTP								

```

00100      1*      CTP
00101      2*      SUBROUTINE TP (PD,PY,TAO,AV,XM,TIMO,XN, TAI, TD,WY,CT,XMN,STD)
00101      3*      C
00101      4*      C PURPOSE      GENERATE AMBIENT TEMPERATURE FROM DAILY, YEARLY AND RANDOM DATA
00101      5*      C
00101      6*      C METHOD      COLORED NOISE WITH SPECIFIED PARMS IS ADDED TO A MEAN DAILY
00101      7*      C PROFILE AND MULTIPLIED BY A YEARLY PROFILE.
00101      8*      C
00101      9*      C WRITTEN BY  A.W. WARREN                                VERSION 1, MARCH 7 1977
00101     10*      C
00101     11*      C CALL SEQUENCE
00101     12*      C TABLES
00101     13*      C PD - MEAN DAILY PROFILE, DEG.F
00101     14*      C PY - MEAN YEARLY PROFILE, DEG.F
00101     15*      C OUTPUTS
00101     16*      C TAO - AMBIENT TEMPERATURE OUTPUT, DEG.F
00101     17*      C AV - MEAN DAILY TEMPERATURE, DEG.F
00101     18*      C XM - MEAN YEARLY TEMPERATURE,DEG.F
00101     19*      C TIMO- LAST TIME COLORED NOISE WAS USED, HR
00101     20*      C XN - COLORED NOISE SAMPLE, DEG.F
00101     21*      C

```

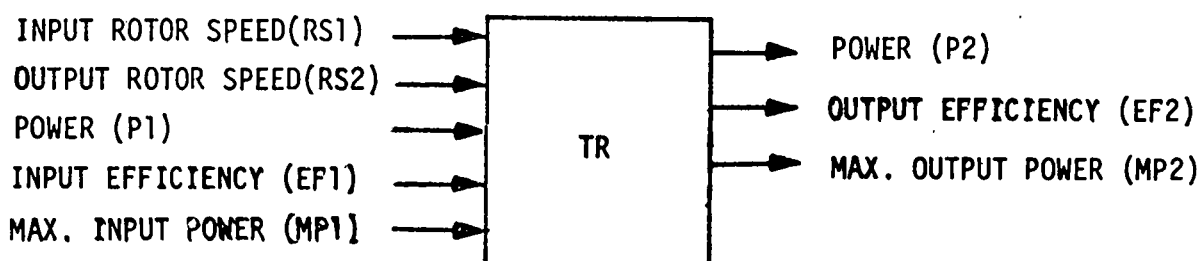
000007
C0C007
G00007
C0C007
000007
U00007
C0C007
C0C007
C0C007
000007
C0C007
C0C007
C0C007
000007
G00007
C0C007
C0C007
C0C007
C0C007
C0C007
C0C007
C0C007

16

Line	Code	Statement	Line
00101	22*	C	000007
00101	23*	C	000007
00101	24*	C	000007
00101	25*	C	000007
00101	26*	C	000007
00101	27*	C	000007
00101	28*	C	000007
00101	29*	C	000007
00103	30*	C	000007
00104	31*	C	000007
00105	32*	C	000007
00105	33*	C	000007
00105	34*	C	000007
00107	35*	C	000007
00110	36*	C	000016
00111	37*	C	000025
00113	38*	C	000030
00114	39*	C	000032
00114	40*	C	000032
00115	41*	C	000040
00116	42*	C	000057
00121	43*	C	000057
00122	44*	C	000062
00124	45*	C	000071
00124	46*	C	000071
00125	47*	C	000076
00126	48*	C	000102
00131	49*	C	000102
00132	50*	C	000107
00134	51*	C	000114
00134	52*	C	000114
00134	53*	C	000114
00135	54*	C	000121
00137	55*	C	000123
00140	56*	C	000125
00140	57*	C	000125
00140	58*	C	000125
00141	59*	C	000127
00143	60*	C	000131
00144	61*	C	000132
00146	62*	C	000152
00147	63*	C	000156
00150	64*	C	000167
00151	65*	C	000175
00151	66*	C	000175
00151	67*	C	000175
00152	68*	C	000201
00153	69*	C	000220
00154	70*	C	000237
00155	71*	C	000244
00155	72*	C	000244
00156	73*	C	000247
00157	74*	C	000347

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7.43 VARIABLE RATIO TRANSMISSION



This component models a transmission which couples a fixed speed rotor input (or output) to a variable speed rotor output (or input) component. Power losses are modeled as a table lookup depending on gear ratio and input power.

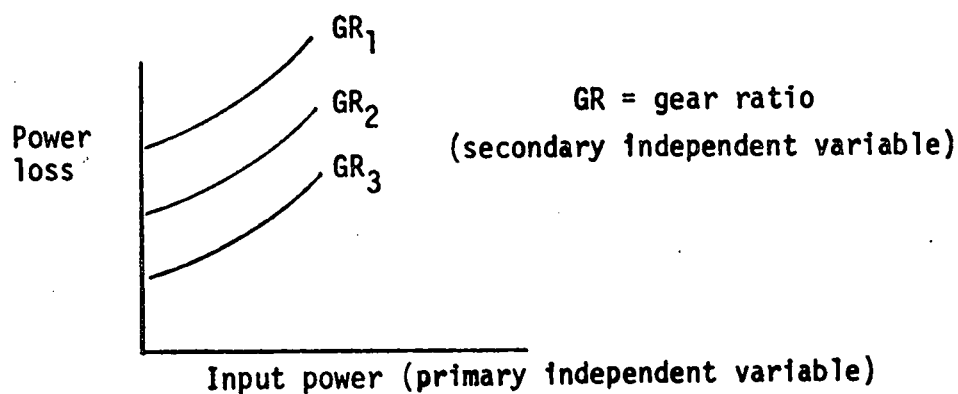


FIGURE 7.43 TRANSMISSION MODEL - LOOKUP TABLE

<u>Tables</u>		<u>Description</u>	<u>Units</u>
PLØ		Power loss versus input power and gear ratio (TABLE DIMENSION = 66)	kw
<u>Inputs</u>			
<u>Parameter/Port</u>			
RS	1	Input rotor speed	rpm
RS	2	Output rotor speed	rpm
P	1	Input power	kw
EF	1	Input product efficiency	-
MP	1	Maximum input power	kw
CC		Capital cost/year	\$
CM		Maintenance cost/year	\$
<u>Outputs</u>			
<u>Variable/Port</u>			
P	2	Output power	kw
TØ		Output torque	ft-lb
PL		Power loss	kw
EF	2	Output product efficiency	-
MP	2	Maximum power output	kw

Calculation Sequence

If $P_1 \leq 0$ or $RS_1 \leq 0$ set $P_2 = T_0 = PL = 0$ and go to 4)

- 1) Determine gear ratio and power terms

$$GR = RS_2/RS_1$$

$$PL = PL_0(P_1, GR)$$

$$P_2 = P_1 - PL$$

- 2) Determine output torque

$$T_0 = P_2 * 737.6 / (RS_2 * (2 \pi / 60))$$

- 3) Efficiency and maximum power

$$EF_2 = EF_1 * (P_2 / P_1)$$

If $P_2 \leq 0$, set $EF_2 = EF_1$ and write Diagnostic

$$MP_2 = MP_1 - PL_0(MP_1, GR)$$

$$MP_2 \leq 0 \Rightarrow \text{DIAGNOSTIC}$$

- 4) Compute Costs

ENTRY POINT 000307

COMMON BLOCKS

```
0003      CIMPL      000002
0004      CTIME      000001
0005      CSIMUL      000010
0006      COST        000002
```

EXTERNAL REFERENCES (BLOCK, NAME)

0007	TBLU2
0010	NWDUS
0011	NIO29
0012	NERR39

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

[illegible]

```

00100      1*      CTR
00101      2*      SUBROUTINE TR(PLO,P2,TO,PL,EF2,MP2,RS2,P1,EF1,MP1,CC,CH)
00101      3*      C
00101      4*      C      PURPOSE      TRANSMISSION MODEL
00101      5*      C
00101      6*      C      METHOD      OUTPUT POWER AND TORQUE COMPUTED FROM
00101      7*      C      INPUT AND OUTPUT ROTOR SPEEDS. POWER
00101      8*      C      LOSS MODELED BY TABLE LOOKUP DEPENDING
00101      9*      C      ON GEAR RATIO AND INPUT POWER
00101     10*      C
00101     11*      C      WRITTEN BY Y.K.CHAN      VERSION 1,JUNE 17,1977
00101     12*      C
00101     13*      C      CALL SEQUENCE
00101     14*      C      TABLES
00101     15*      C      PLO -POWER LOSS VERSUS INPUT POWER AND GEAR RATIO ,KW
00101     16*      C      OUTPUTS
00101     17*      C      P2  -OUTPUT POWER,KW
00101     18*      C      TO  -OUTPUT TORQUE,FT-LB
00101     19*      C      PL  -POWER LOSS,KW
00101     20*      C      EF2 -OUTPUT PRODUCT EFFICIENCY
00101     21*      C      MP2 -MAXIMUM POWER OUTPUT,KW

```

[illegible]

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00101	22*	C	INPUTS	C00003
00101	23*	C	RS1 -INPUT ROTOR SPEED,RPM	C00003
00101	24*	C	RS2 -OUTPUT ROTOR SPEED,RPM	C00003
00101	25*	C	P1 -INPUT POWER,KW	C00003
00101	26*	C	EF1 -INPUT PRODUCT EFFICIENCY	C00003
00101	27*	C	MP1 -MAXIMUM INPUT POWER,KW	C00003
00101	28*	C	CC -CAPITOL COST/YEAR,\$	C00003
00101	29*	C	CM -MAINTENANCE COST/YEAR,\$	C00003
00101	30*	C		C00003
00103	31*		COMMON/CIMPL/IMPL,ICNT/CTIME/TIME/CSIMUL/DUM(7),TMAX	C00003
00103	32*	X	/COST/CCI,CM1	C00003
00104	33*		REAL MP2,MP1	C00003
00105	34*		DIMENSION PLO(1)	C00003
00105	35*	C		C00003
00106	36*		IF(IMPL.GT.0)GO TO 10	C00003
00110	37*		TMAX1=TMAX*.99999	C00006
00111	38*		RS2=RS1	C00011
00112	39*	10	CONTINUE	C00014
00113	40*		NNGR=PLO(3)	C00014
00114	41*		NNP1=PLO(2)	C00022
00115	42*		M4=NNGR*4	C00031
00116	43*		MN4=NNP1*M4	C00033
00116	44*	C		C00033
00116	45*	C	COMPUTE GEAR RATIO AND POWER TERMS	C00033
00116	46*	C		C00033
00117	47*		P2=0.	C00035
00120	48*		T0=0.	C00036
00121	49*		PL=0.	C00037
00122	50*		EF2=EF1	C00040
00123	51*		MP2=MP1	C00042
00124	52*	100	IF(1(RS1.LE.0.).OR.(P1.LE.0.))GO TO 400	C00044
00126	53*		P2=P1	C00060
00127	54*	200	IF(RS2.LE.0)GO TO 400	C00062
00131	55*	300	GR=RS2/RS1	C00071
00132	56*		PL=TBLU2(P1,GR,PLO(M4),PLO(4),PLO(MN4),1,1,-NNP1,-NNGR,NNP1,NNGR)	C00074
00133	57*		P2=P1-PL	C00124
00133	58*	C		C00124
00133	59*	C	OUTPUT TORQUE	C00124
00133	60*	C		C00124
00134	61*		T0=P2*737.6*30./(RS2*3.14159)	C00126
00134	62*	C		C00126
00134	63*	C	EFFICIENCY AND MAXIMUM POWER	C00126
00134	64*	C		C00126
00135	65*		EF2=EF1*P2/P1	C00134
00136	66*		IF(EF2.GT.0.)GO TO 409	C00140
00140	67*		EF2=EF1	C00142
00141	68*		IF(IMPL.EQ.2)WRITE(6,408)PL,P1	C00144
00146	69*	408	FORMAT(1H0,75H TRANSMISSION POWER LOSS ,F12.3,	C00156
00146	70*	X	21H EXCEEDS INPUT POWER ,F12.3)	C00156
00147	71*		IF(IMPL.EQ.2)ICNT=ICNT+1	C00156
00151	72*	409	CONTINUE	C00165
00152	73*		AMP2=TBLU2(MP1,GR,PLO(M4),PLO(4),PLO(MN4),1,1,-NNP1,-NNGR,	C00165
00152	74*		XNNP1,NNGR)	C00165
00153	75*			C00220
00153	76*		MP2=MP1-AMP2	C00220
00154	77*		IF(MP2.GT.0.)GO TO 400	C00222
00154	78*		IF(IMPL.EQ.2)WRITE(6,508)AMP2,MP1	C00224

```

00163 79*      508 FORMAT(1H0,25H TRANSMISSION POWER LOSS ,F12.3,
00163 80*      X 29H EXCEEDS MAXIMUM INPUT POWER ,F12.3)
00164 81*      IF(IMPL.EQ.2)ICNT=ICNT+1
00164 82*      C
00166 83*      400 IF(IMPL.LE.1)RETURN
00170 84*      IF(TIME.LT.TMAX1)RETURN
00172 85*      CCI=CCI+CC
00173 86*      CMI=CMI+CM
00173 87*      C
00174 88*      RETURN
00175 89*      END

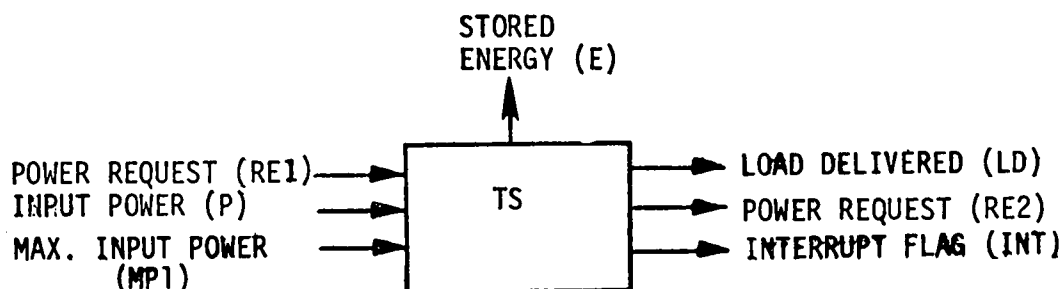
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```

000236
000236
000236
000236
000245
000253
000262
000265
000265
000270
000373

```


7.44 THERMAL STORAGE CHAMBER



The thermal storage chamber is modeled by a "lumped" parameter approach. The entire storage media mass is characterized by a single temperature (no temperature gradient). The storage media is either a sensible heat or a phase change media. Energy is input via electrical resistance heaters and withdrawn by a heat exchanger. Energy is deposited in the media at a rate equal to the available electrical power up to a maximum charging power. The discharge heat exchanger fluid mass flow rate is adjusted to provide the desired heat load demand. The maximum mass flow rate condition determines the maximum thermal load. The maximum energy limit represents the point where the maximum media temperature is reached.

The model initially calculates the required storage media mass to provide the rated thermal energy storage (design point). Cost calculations are also made on the design point conditions. Initial checks on charge and discharge power and initial stored energy level are made. The storage temperature is determined based on the energy level.

Basic Equation

$$E = P - LD - NU * E$$

<u>Tables</u>		<u>Description</u>	<u>Units</u>
HT		Media temperature versus enthalpy in KWH/LB ¹	°F
<u>Inputs</u>			
<u>Parameter/Port</u>			
P		Input power	kw
RE	1	Demand thermal load	kw
NU		Stored energy loss coefficient (D = 0.02)	(h) ⁻¹
TS		Rated storage time ²	h
V0		Rated input voltage ²	V
TM1		Maximum allowable storage temperature (D = 212)	°F
T01		Minimum allowable storage temperature (D = 60)	°F
DH		Design point enthalpy	kwh/lb
PD		Rated storage thermal power ²	kw
PM		Maximum charge rate (D = 2*PD)	kw
MFM		Maximum working fluid mass flow rate (D = 9000)	lb/h
TDE		Temperature deadband for priority resequence (D = 4)	°F
EF	1	Input product efficiency	-
MP	1	Maximum input charging rate (D = 1.X10 ⁸)	kw
CP2		Working fluid heat capacity (D = 2.93X10 ⁻⁴)	kwh/lb-°F
T02		Working fluid return temperature (D = 40)	°F
TM2		Maximum allowable working fluid temperature (D = 212)	°F
R		Effective heat exchanger thermal resistance (D = 3.08X10 ⁻⁴)	°F/kw
CM		Storage device yearly maintenance cost (D = 0.6)	\$/kw
CSA		Storage device capacity cost (D = 50)	\$/kw
CSB		Storage device energy cost (D = 15.2)	\$/kwh
LE		Unit life expectancy	years

D - Default values specified

1 - See Figure 7.44

2 - Design point conditions

Outputs

<u>Variable/Port</u>	<u>Description</u>	<u>Units</u>
E	Stored energy (state)	kwh
I	Input current	amps
MP 2	Maximum discharge rate allowable	kw
INT	Priority interrupt flag	-
T	Storage temperature	°F
M	Required storage media mass	lb
CCØ	Storage device capital cost/year	\$
RE 2	Maximum charging rate request	kw
MF	Working fluid mass flow rate	lb/h
LD	Power Delivered	kw

Statistics

TSU	Maximum storage temperature	°F
TSL	Minimum storage temperature	°F
ME	Maximum stored energy	kwh
MFU	Maximum working fluid mass flow rate	lb/h

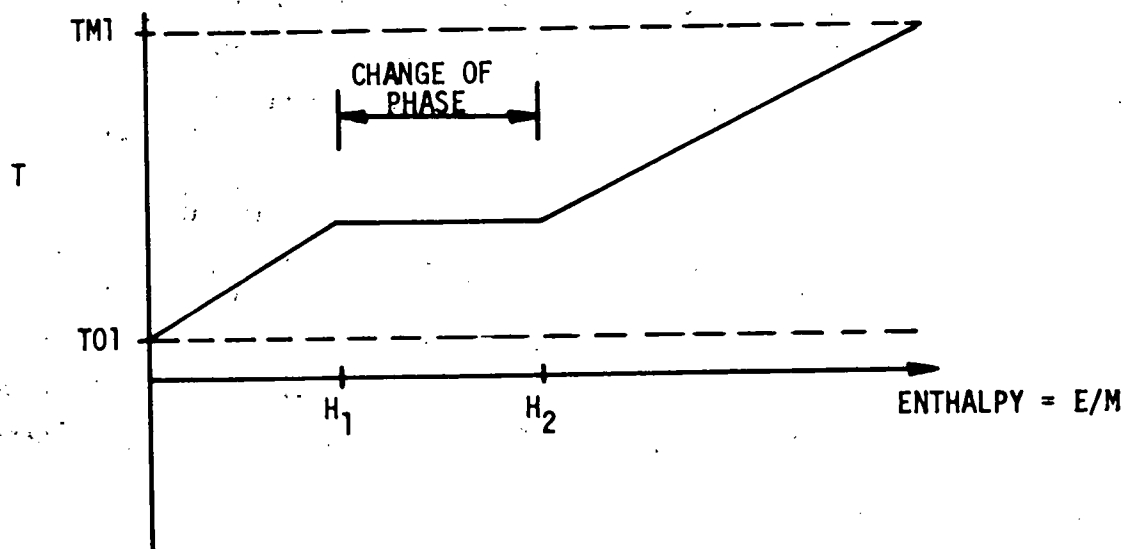


FIGURE 7.44: TEMPERATURE - ENTHALPY DIAGRAM

The calculation sequence and default values assume a thermal storage device sized to provide 10kw for 24 hours. A paraffin wax phase change storage medium is assumed. Water is assumed as the thermal transport fluid. Costs are assumed to be given by data for the phase change storage device given in Reference 1. The thermal resistance value, R, is assumed equal to that determined for the device of Reference 1. The value for the maximum charging rate, PM, reflects the acceptance of twice the design charge rate. The actual numbers which should be used will depend on specific design and performance requirements obtained from a desired application.

Calculation Sequence

- 1) Media mass, capital cost, maintenance cost (first pass)

$$M = \frac{PD \cdot TS}{DH}$$

$$CC = (CSA + CSB \cdot TS) \cdot PD / LE$$

$$CM = CM \cdot PD$$

- 2) Storage Temperature and Working Fluid Temperature

$$T = HT(E/M)$$

$$TF = \min\{TM2, \max[T02, T - RE1 \cdot R]\}$$

$$E2 = M \cdot HT^{-1}(TM1)$$

1. "Advanced Thermal Energy Storage," BEC/EPRI RP 788-1, July 1976.

Calculation Sequence Cont.

3) Discharge Rate and Thermal Load

$$\begin{aligned} E1 &= M*HT^{-1}(T01) \\ MP2 &= MFM*CP2*(TF-T02) \\ LD &= \min(RE1, MP2, (E-E1)/TINC) \\ MF &= LD/(CP2*(TF-T02)) \end{aligned}$$

4) Diagnostic Checks

$$\begin{aligned} MF &\leq MFM \\ P &\leq PM \\ T01 &\leq T \leq TM1 \end{aligned}$$

5) Current calculations

$$I = \frac{P*1000}{V0}$$

6) Energy dynamics

$$\dot{E} = P - LD - NU*E$$

7) Maximum Charging Rates

$$RE2 = \min(PM, MP1, (E2-E)/TINC)/EF1$$

where TINC = integration step size

Calculation Sequence Cont.

8) Priority resequencing

```

    if  $T \leq T01$ ,  $INT = 1$ 
    if  $T \geq T01 + TDE$  and  $INT=1$ ,  $INT=0$ 
    if  $T \geq TM1$ ,  $INT=-1$ 
    if  $T < TM1 - TDE$  and  $INT=-1$ ,  $INT=0$ 

```

9) Compute Statistics and Costs

ENTRY POINT 000612

COMMON BLOCKS

```
0003      CIMPL      000002
0004      CTIME      000001
0005      CSIMUL      000010
0006      COST        000002
```

0007	T6LU1
0010	NWDUS
0011	NI02S
0012	NERR3S

[illegible]

```

00100      1*      CTS
00101      2*      SUBROUTINE TS(HT,F,DE,IE,I,MP2,INT,T,M,CCO,RE,MF,LD
00101      3*      1      ,TSU,TSL,ME,MFU,P,RE1,NU,TSO,V0,TM1,TO1,DH,PD,PH,
00101      4*      2      MFM,TDE,EF1,MP1,CP2,T02,TM2,R,CM,CSA,CSB,LE)
00101      5*      C
00101      6*      C PURPOSE      COMPUTE ENERGY CONTAINED IN A THERMAL STORAGE MEDIA
00101      7*      C
00101      8*      C METHOD      A PHASE CHANGE OR SENSIBLE HEAT MEDIA IS MODELED AS
00101      9*      C
00101     10*      C      A SINGLE TEMPERATURE MASS WITH NO GRADIENTS.
00101     11*      C
00101     12*      C WRITTEN BY F. O. MAHONY      VERSION 2, JULY 1977
00101     13*      C
00101     14*      C CALL SEQUENCE
00101     15*      C
00101     16*      C      TABLES
00101     17*      C      HT - MEDIA TEMPERATURE VERSUS ENTHALPY IN KWH/LB, DEG F
00101     18*      C      OUTPUTS
00101     19*      C      E - STORED ENERGY (STATE VARIABLE), KWH
00101     20*      C      DE - POWER INTO STORAGE, KW
00101     21*      C      IE - STATUS INDICATOR

```

[illegible]

00101	22*	C	I - INPUT ELECTRIC CURRENT, KW	000000
00101	23*	C	MP2 - MAXIMUM DISCHARGE RATE ALLOWABLE, KW	000000
00101	24*	C	INT - PRIORITY FLAG INTERRUPT	000000
00101	25*	C	T - STORAGE TEMPERATURE, DEG F	000000
00101	26*	C	M - REQUIRED STORAGE MEDIA MASS, LB	000000
00101	27*	C	CCO - STORAGE DEVICE CAPITAL COST/YEAR, \$	000000
00101	28*	C	RE - MAXIMUM CHARGING RATE REQUEST, KW	000000
00101	29*	C	MF - WORKING FLUID MASS FLOW RATE, LB/HR	000000
00101	30*	C	LD - THERMAL LOAD DELIVERED, KW	000000
00101	31*	C	TSU - MAXIMUM STORAGE TEMPERATURE, DEG F	000000
00101	32*	C	TSL - MINIMUM STORAGE TEMPERATURE, DEG F	000000
00101	33*	C	ME - MAXIMUM STORED ENERGY, KWH	000000
00101	34*	C	MFU - MAXIMUM WORKING FLUID MASS FLOW RATE, LB/HR	000000
00101	35*	C	INPUTS	000000
00101	36*	C	P - INPUT POWER, KW	000000
00101	37*	C	RE1 - THERMAL DISCHARGE REQUEST, KW	000000
00101	38*	C	NU - STORAGE ENERGY LOSS COEFFICIENT, 1/HR	000000
00101	39*	C	TSO - RATED STORAGE TIME, HR	000000
00101	40*	C	VO - RATED INPUT VOLTAGE, VOLTS	000000
00101	41*	C	TM1 - MAXIMUM ALLOWABLE STORAGE TEMPERATURE, DEG F	000000
00101	42*	C	T01 - MINIMUM ALLOWABLE STORAGE TEMPERATURE, DEG F	000000
00101	43*	C	DH - DESIGN POINT ENTHALPY, KWH/LB	000000
00101	44*	C	PD - RATED STORAGE THERMAL POWER, KW	000000
00101	45*	C	PM - MAXIMUM CHARGE RATE, KW	000000
00101	46*	C	MFH - MAXIMUM WORKING FLUID MASS FLOW RATE, LB/HR	000000
00101	47*	C	TDE - TEMPERATURE DEADBAND FOR PRIORITY RESEQUENCE, DEG F	000000
00101	48*	C	EF1 - INPUT PRODUCT EFFICIENCY	000000
00101	49*	C	MP1 - MAXIMUM INPUT CHARGING RATE, KW	000000
00101	50*	C	CP2 - WORKING FLUID HEAT CAPACITY, KWH/LB-F	000000
00101	51*	C	T02 - WORKING FLUID RETURN TEMPERATURE, DEG F	000000
00101	52*	C	TM2 - MAXIMUM ALLOWABLE WORKING FLUID TEMPERATURE, DEG F	000000
00101	53*	C	R - EFFECTIVE HEAT EXCHANGER THERMAL RESISTANCE, F/KW	000000
00101	54*	C	CM - STORAGE DEVICE YEARLY MAINTENANCE COST, \$/KW	000000
00101	55*	C	CSA - STORAGE DEVICE CAPACITY COST, \$/KW	000000
00101	56*	C	CSB - STORAGE DEVICE ENERGY COST, \$/KWH	000000
00101	57*	C	LE - UNIT/LIFE FILE EXPECTANCY, YEARS	000000
00101	58*	C		000000
00103	59*		COMMON/CIMPL/IMPL,ICN/CTIME/TIME /CSIMUL/DUM(1),TMAX /COST/CCI,CHI	000000
00104	60*		REAL NU,I,MP2,INT,MF,LD,ME,MFU,MFM,MP1,LE,M	000000
00105	61*		DIMENSION HT(1)	000000
00105	62*	C		000000
00106	63*		IF(IMPL.GT.0)GO TO 100	000000
00110	64*		TMAX1=TMAX*.99999	000003
00111	65*		TINC= DUM(7)	000006
00111	66*	C		000006
00111	67*	C		000006
00112	68*		IF(NU.EQ. .99999)NU=0.02	000010
00114	69*		IF(TM1.EQ. .99999)TM1=212.0	000015
00116	70*		IF(T01.EQ. .99999)T01=60.0	000022
00120	71*		IF(PH.EQ. .99999) PH=2.0*PD	000027
00122	72*		IF(MFM.EQ. .99999)MFM=9000.0	000035
00124	73*		IF(TDE.EQ. .99999)TDE=4.0	000042
00126	74*		IF(CP2.EQ. .99999)CP2=2.93E-4	000047
00130	75*		IF(T02.EQ. .99999)T02=40.0	000054
00132	76*		IF(TM2.EQ. .99999)TM2=212.0	000061
00134	77*		IF(R.EQ. .99999)R =3.08E-4	000066
00134	78*		IF(CM.EQ. .99999)CM =0.6	000073

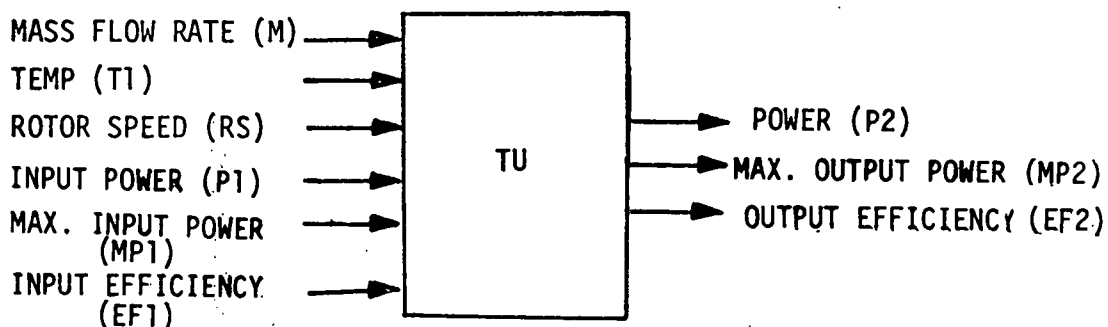
TS

00140	79*		IF(CSA.EQ. .99999)CSA=50.0	000100
00142	80*		IF(CSB.EQ. .99999)CSB=15.2	000105
00144	81*		IF(MP1.EQ. .99999) MP1= 1.0E8	000112
00144	82*	C		000112
00146	83*		INT=0.0	000117
00147	84*		RE1=0.0	000120
00147	85*	C		000120
00150	86*		TSU=0.0	000121
00151	87*		ME =0.0	000122
00152	88*		MFU=0.0	000123
00153	89*		TSL=1.0E8	000124
00154	90*		CM= CM*PD	000126
00154	91*	C		000126
00155	92*		M =PD*TSO/DH	000131
00156	93*		CCO=(CSA+CSR*TSO)*PD/LE	000135
00156	94*	C		000135
00156	95*	C	COMPUTE STORAGE TEMPERATURE	000135
00156	96*	C		000135
00157	97*		100 NH= HT(2)	000144
00160	98*		T= TBLU1(E/M,HT(4),HT(4+NH),1,NH)	000152
00161	99*		E1= M*TBLU1(TM1,HT(4+NH),HT(4),1,NH)	000173
00161	100*	C		000173
00161	101*	C		000173
00161	102*	C	WORKING FLUID TEMPERATURE	000173
00161	103*	C		000173
00162	104*		TF =AMIN1(TM2,AMAX1(TO2,T-RE1*R))	000212
00162	105*	C		000212
00162	106*	C	MAXIMUM DISCHARGE RATE AND THERMAL LOAD	000212
00162	107*	C		000212
00163	108*		MP2=MFH*CP2*(TF-TO2)	000226
00164	109*		IF(INT.EQ.1.)MP2=0.	000234
00166	110*		LD =AMIN1(RE1,MP2)	000240
00166	111*	C		000240
00166	112*	C	WORKING FLUID MASS FLOW RATE	000240
00166	113*	C		000240
00167	114*		IF(LD.GT.0.0) MF =LD/CP2*(TF-TO2)	000246
00167	115*	C		000246
00171	116*		IF(IMPL.LE.1)60 TO 200	000255
00173	117*		IF(IMPL.GT.2) 60 TO 200	000261
00175	118*		PM1= PM/.9999	000265
00175	119*	C		000265
00176	120*		IF(MF .GT.MFH)WRITE(6,1010)MF,MFH	000270
00203	121*		IF(P .GT.PM1)WRITE(6,1020)P ,PM	000303
00210	122*		IF(MF.GT.MFH .OR. P.GT.PM1)ICN=ICN+1	000316
00212	123*		IF(T .LT.TO1.OR.	000337
00212	124*		1 T .GT.TM1)WRITE(6,1030)T,TO1,TM1	000337
00220	125*		IF(T.LT.TO1 .OR. T.GT.TM1) ICN=ICN+1	000365
00220	126*	C		000365
00220	127*	C	CURRENT CALCULATION	000365
00220	128*	C		000365
00222	129*		200 I =P*1000.0/V0	000407
00222	130*	C		000407
00222	131*	C	ENERGY STATE	000407
002	132*	C		000407
002	133*	C		000407
002	134*		IF(IE.NE.0)DE=P-LD-NU*E	000412
00223	135*	C		000412

TSO

00223	136*	C	MAXIMUM CHARGING RATE REQUEST.	000412
00223	137*	C		000412
00223	138*	C		000412
00225	139*		A= AMAX1(E1-E,0.)/TINC	000422
00226	140*		RE =AMIN1(PM,MP1,A)/EF1	000432
00226	141*	C		000432
00226	142*	C		000432
00226	143*	C	PRIORITY RESEQUENCING	000432
00226	144*	C		000432
00227	145*		IF(T.LE.T01)INT=1.0	000445
00227	146*	C		000445
00231	147*		IF(T.GE.(T01+TDE).AND.	000453
00231	148*		1 INT.EQ.1.)INT=0.0	000453
00231	149*	C		000453
00233	150*		IF(T.GE.TM1)INT=-1.0	000472
00233	151*	C		000472
00235	152*		IF(T.LT.(TM1-TDE).AND.	000500
00235	153*		1 INT.EQ.-1.)INT=0.0	000500
00235	154*	C		000500
00237	155*		IF(IMPL.LE.1)RETURN	000517
00237	156*	C		000517
00241	157*		TSU=AMAX1(TSU,T)	000526
00242	158*		TSL=AMIN1(TSL,T)	000534
00243	159*		MC =AMAX1(MC ,E)	000542
00244	160*		MFU=AMAX1(MFU,MF)	000550
00245	161*		IF(TIME.LT.TMAX)RETURN	000556
00245	162*	C		000556
00245	163*	C	COST	000556
00245	164*	C		000556
00247	165*		CHI=CHI+CM	000565
00250	166*		CCI=CCI+CCO	000570
00251	167*		CM = CM/PD	000570
00251	168*	C		000570
00252	169*		RETURN	000576
00253	170*		1010 FORMAT(1H0,26HTS WORKING FLUID FLOW RATE,F12.3	001070
00253	171*		1 ,32H GREATER THAN MAXIMUM ALLOWED,F12.3)	001070
00254	172*		1020 FORMAT(1H0,14HTS INPUT POWER,F12.3	001070
00254	173*		1 ,44H GREATER THAN MAXIMUM ALLOWED CHARGE RATE,F12.3)	001070
00255	174*		1030 FORMAT(1H0, 23HTS STORAGE TEMPERATURE ,F12.3	001070
00255	175*		1 ,20H OUTSIDE MINIMUM ,F12.3	001070
00255	176*		2 ,15H AND MAXIMUM,F12.3)	001070
00255	177*	C		001070
00256	178*		END	001070

7.45 TURBINE (PNEUMATIC)



The turbine model is based on a high pressure ratio, constant angular velocity design. The turbine is assumed to be designed to a set of of operating conditions defined in terms of user specified parameters. The polytropic efficiency is only weakly related to angular velocity. Initial calculations are made with the design polytropic efficiency, and refinements are then computed after off-design parameters are calculated.

Basic Equation

The equation for output power P2 is

$$P2 = M * CP * (T1 - TA)$$

Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
M	Inlet mass flow rate	lb/h
CP	Air heat capacity ($D = 7.2 \times 10^{-5}$)	kwh/lb/°F
T 1	Input air temperature	°F
TA	Ambient air temperature	°F
MD	Design mass flow rate ($D = 4800$)	lb/h
TID	Design inlet air temperature ($D = 600$)	°F
PID	Design inlet pressure ($D = 117.6$)	psi
P2D	Design exit pressure (ambient) ($D = 14.7$)	psi
T2D	Design exit temperature (ambient) ($D = 70$)	°F
PS	Storage vessel pressure	psi
RS	Angular velocity	rpm
EF 1	Input product efficiency	-
MP 1	Maximum input power	kw
P 1	Input power	kw
CK	Capacity cost coefficient ¹ ($D = 0.015$)	
F0	Turbine mass flow exponent for capital cost ($D = 0.75$)	-
G	Turbine temperature exponent for capital cost ($D = 0.5$)	-
NPD	Design Polytropic Efficiency ($D = 0.88$)	

Outputs

<u>Variable/Port</u>			
P 2	Output power		kw
CC0	Turbine cost/year		\$
PR	Back pressure		psi
T0	Torque		ft-lb

D - Default values supplied

¹ CK = Capital cost (known unit)/[(design point mass flow rate)^{F0} *
(design point temperature + 460)^G * LN (inlet/outlet pressure ratio)*LE],
where LE = life expectancy in years.

Outputs Cont.

<u>Variable/Port</u>		<u>Description</u>	<u>Units</u>
EF	2	Output product efficiency	-
MP	2	Maximum discharge power	kw

Statistics

MØP		Maximum power observed	kw
-----	--	------------------------	----

The calculation sequence and the default values are based on the assumption of a high pressure ratio, constant angular velocity turbine, rated at 150 kw and a pressure ratio of 8. The equations used relate first order effects among the various physical quantities and were derived from first principles originally in support of the research work of Reference 1. Cost scaling was also developed in that reference based on cost estimates from turbomachinery manufacturers.

-
1. "Closed Cycle High Temperature Control Receiver Concept for Solar Electric Power," BEC/EPRI RP377-1, June 1976.

Calculation Sequence

1) Costs

$$CC = CK*(MD)**F0*(TID+460)**G*LN(PID/P2D)$$

2) Back Pressure PR determined by

$$PR = (M/MD)*PID* \sqrt{(T1+460)/(TID+460)}$$

If PR > PS write DIAGNOSTIC

3) Efficiency

$$RAT = (PID/P2D)**(2/7)$$

$$EFF = (RAT-1.)/(RAT**(1/NPD)-1)$$

4) Power Out

$$P2 = M*CP*(T1-TA)*EFF$$

5) Torque

If RS = 0, set T0 = 0 and go to 6)

$$T0 = P2*(737.6)/(RS*2\pi/60)$$

6) Efficiency and maximum power

$$EF2 = EF1*EFF$$

$$MP2 = \min(MP1*EFF, MD*CP*(T1-TA))$$

7) Compute Statistics and Costs

ENTRY POINT 000335

COMMON BLOCKS

```
0003      CTIME  000002
0004      CTIME  000001
0005      CTIME  000010
0006      COST   000001
```

EXTERNAL REFERENCES (BLOCK, NAME)

```
0007      XPRR
0010      ALOG
0011      SQRT
0012      AMOVS
0013      NI025
0014      NERR35
```

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

0001 000137 100L      0001 000304 1000L      0000 000004 1010F      0001 000204 200L      0001 000233 300L
J006 R J00000 CCI      0005 000000 DUM      0000 R 000003 EFF      0003 I 000001 ICNT      0003 I 000000 IMPL
0000 000047 INJPS      0000 R 000000 PI      0000 R 000002 RA T      0004 R 000000 TIME      0005 R 000007 TMAX
0000 R 000001 TMAX1

```

```

00100      1*      CTU
00101      2*      SUBROUTINE TU(P2,CC,PR,TO,EF2,MP2,MOP,M,CP,T1,TA,MD,TID,PID,P2D,
00101      3*      1      T2D,PS,RS,EF1,MP1,P1,CK,F,6,NPD)
00101      4*      C
00101      5*      C PURPOSE      TURBINE PERFORMANCE MODEL
00101      6*      C
00101      7*      C METHOD      COMPUTE TURBINE POWER OUTPUT FROM INPUT DESIGN
00101      8*      C
00101      9*      C      CONDITIONS AS A FUNCTION OF INLET TEMPERATURE
00101     10*      C
00101     11*      C      AND MASS FLOW RATE
00101     12*      C
00101     13*      C      WRITTEN BY F.O. MAHONY      VERSION 1, MARCH 22 1977
00101     14*      C
00101     15*      C CALL SEQUENCE
00101     16*      C      OUTPUTS
00101     17*      C      P2 - OUTPUT POWER, KW
00101     18*      C      CC - TURBINE COST PER YEAR, $
00101     19*      C      PR - BACK PRESSURE, PSI
00101     20*      C      TO - TORQUE, FT-LB

```

[illegible]

```

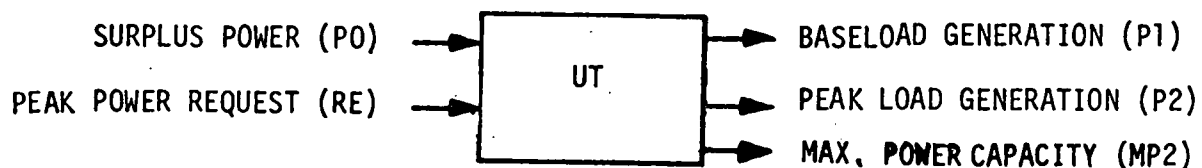
00101 21* C EF2 - OUTPUT PRODUCT EFFICIENCY 000000
00101 22* C MP2 - MAXIMUM DISCHARGE POWER, KW 000000
00101 23* C MOP - MAXIMUM POWER OBSERVED, KW 000000
00101 24* C INPUTS 000000
00101 25* C M - INLET MASS FLOW RATE, LB/HR 000000
00101 26* C CP - AIR HEAT CAPACITY, KWH/LB/DEG F 000000
00101 27* C T1 - INPUT AIR TEMPERATURE, DEG F 000000
00101 28* C TA - AMBIENT AIR TEMPERATURE, DEG F 000000
00101 29* C MD - DESIGN MASS FLOW RATE, LB/HR 000000
00101 30* C TID - DESIGN INLET AIR TEMPERATURE, DEG F 000000
00101 31* C PID - DESIGN INLET PRESSURE, PSI 000000
00101 32* C P2D - DESIGN EXIT PRESSURE (AMBIENT), PSI 000000
00101 33* C T2D - DESIGN EXIT TEMPERATURE (AMBIENT), PSI 000000
00101 34* C PS - STORAGE VESSEL PRESSURE, PSI 000000
00101 35* C RS - ANGULAR VELOCITY, RPM 000000
00101 36* C EF1 - INPUT PRODUCT EFFICIENCY 000000
00101 37* C MP1 - MAXIMUM INPUT POWER, KW 000000
00101 38* C P1 - INPUT POWER, KW 000000
00101 39* C CK - CAPACITY COST COEFFICIENT 000000
00101 40* C F - TURBINE MASS FLOW EXPONENT FOR CAPITAL COST 000000
00101 41* C G - TURBINE TEMPERATURE EXPONENT FOR CAPITAL COST 000000
00101 42* C NPD - DESIGN POLYTROPIC EFFICIENCY 000000
00101 43* C
00103 44* COMMON /CIMPL/IMPL,ICNT/CTIME/ TIME /CSIMUL/DUM(7),THAX /COST/CCI
00104 45* REAL MP2,MOP, M,MD, MP1,NPD 000000
00105 46* DATA PI /3.14159/ 000000
00105 47* C 000000
00107 48* IF(IMPL.GT.0) GO TO 100 000000
00111 49* IF(CP.EQ..99999) CP = 72.0E-6 000002
00113 50* IF(TA.EQ..99999) TA = 70.0 000007
00115 51* IF(MD.EQ..99999) MD = 4800. 000014
00117 52* IF(TID.EQ..99999) TID=600.0 000021
00121 53* IF(PID.EQ..99999) PID=117.6 000026
00123 54* IF(P2D.EQ..99999) P2D=14.7 000033
00125 55* IF(T2D.EQ..99999) T2D=70.0 000040
00127 56* IF(CK.EQ..99999) CK =0.015 000045
00131 57* IF(F.EQ..99999) F =0.75 000052
00133 58* IF(G.EQ..99999) G =0.5 000057
00135 59* IF(NPD.EQ..99999)NPD= .88 000064
00137 60* MOP = 0. 000071
00140 61* RS= AMAX1(0.0,AMIN1(RS, 4000.)) 000072
00141 62* THAX1=.99999*THAX 000104
00142 63* CC = CK*MD**F*(TID+460.0)**G*ALOG(PID/P2D) 000107
00142 64* C DETERMINE BACK PRESSURE 000107
00142 65* C 000107
00143 66* 100 RAT= (PID/P2D)**.2857 000137
00144 67* EFF= (RAT-1.0)/(RAT**(.1/NPD) - 1.0) 000146
00145 68* PR = M/MD*PID*SQRT((T1 + 460.0)/(TID+460.0)) 000162
00145 69* C 000162
00146 70* IF(PR.GT.PS) GO TO 1000 000200
00146 71* C 000200
00146 72* C POWER OUTPUT 000200
00146 73* C 000200
00146 74* C 000200
00150 75* 200 P2= M*CP*(T1-TA)*EFF 000204
00151 76* T0 = 0. 000212
00152 77* IF(RS.EQ.0. .OR. P1.EQ. 0.) GO TO 300 000213

```

TU

00152	78*	C	TORQUE	000213
00154	79*		TO = P2*737.6/(RS*2.0*PI/60.0)	000223
00154	80*	C		000223
00154	81*	C	EFFICIENCY AND MAXIMUM POWER	000223
00154	82*	C		000223
00155	83*		300 EF2 = EF1*EFF	000233
00156	84*		MP2 = AMIN1(MP1*EFF ,MD*CP*(T1-TA))	000235
00157	85*		IF(IMPL.LE. 1) RETURN	000251
00161	86*		MOP = AMAX1(MOP,P2)	000260
00162	87*		IF(TIME.LT.TMAX1) RETURN	000266
00164	88*		CCI = CCI + CC	000275
00164	89*	C		000275
00165	90*		RETURN	000300
00165	91*	C		000300
00166	92*		1000 IF(IMPL.EQ.2)WRITE(6,1010) PR,PS	000304
00173	93*		1010 FORMAT (1H0,21HTURBINE BACK PRESSURE ,F12.3,	000315
00173	94*		1 39H GREATER THAN STORAGE VESSEL PRESSURE ,F12.3)	000315
00174	95*		IF(IMPL.EQ.2)ICNT=ICNT+1	000315
00174	96*	C		000315
00176	97*		GO TO 200	000323
00176	98*	C		000323
00177	99*		END	000470

7.46 UTILITY



The utility model has two power outputs corresponding to baseload and peak generation, with corresponding generation cost inputs. A surplus power input is also provided with cost credit depending on whether baseload or peak power is reduced. Total energy cost, total output power and total peak load requests are monitored.

Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
BS	Baseload generation (default = 0.)	kw
CB	Cost of baseload generation/kwh	\$
MP 1	Maximum power capacity (default = 1×10^8)	kw
P 0	Surplus power returned to utility	kw
RE	Peak generation request	kw
CP	Cost of peak load generation/kwh	\$
CC	Capital cost/year	\$
CM	Maintenance cost/year	\$

Outputs

<u>Variable/Port</u>			
P	1	Baseload generation (= BS)	kw
MP	2	Maximum power capacity (= MP1)	kw
P	2	Peak load generation	kw
C0		Cost of energy used (state)	\$

Statistics

SR	Sum of requested peak generation	kwh
SP0	Sum of output energy	kwh
SP	Sum of surplus energy	kwh
VSP	Value of surplus energy	\$

Calculation Sequence

1) Power outputs

If BS > MP1, write diagnostic

$$P1 = BS, MP2 = MP1$$

$$P2 = \text{MIN} (MP1-BS, RE)$$

2) Energy cost dynamics

$$C0 = BS*CB + (P2-P0)*CX$$

$$CX = \begin{cases} CP & \text{if } P2-P0 > 0 \\ 0 & \text{if } P2-P0 < 0 \end{cases}$$

3) Statistics

$$SR = SR + RE * TINC$$

$$DEL = \begin{cases} 0 & \text{if } P2 > P0 \\ (P0-P2)*TINC & \text{if } P0 > P2 \end{cases}$$

$$SP0 = SP0 + (P1+P2-P0)*TINC + DEL$$

$$SP = SP + DEL$$

$$VSP = VSP + DEL * CB$$

Where TINC = integration step size/2

4) Compute Costs

SUBROUTINE UT ENTRY POINT 000217

STORAGE USED CODE(1) 000341; DATA(0) 000045; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000002
0004 CTIME 000001
0005 CSIMUL 000010
0006 COST 000011

EXTERNAL REFERENCES (BLOCK, NAME)

0007 NWDUS
0010 NI02\$
0011 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000053 100L	0001 000146 200L	0000 000004 208F	0006 R 000000 CCI	0006 R 000001 CMI
0006 000002 COP	0000 R 000002 CX	0005 R 000000 DUM	0003 I 000001 ICNT	0003 I 000000 IMPL
0000 000023 INJP\$	0006 R 000010 SPD	0006 R 000004 TDE	0000 R 000003 TERM	0004 R 000000 TIME
0000 R 000001 TINC1	0006 000005 TLD	0005 R 000007 THAX	0000 R 000000 THAX1	0006 R 000007 UTD
0006 R 000006 UTV	0006 R 000003 VDE			

00100	1*	CUT		000000
00101	2*		SUBROUTINE UT(P1,MP2,P2,CO,COD,ICO,SR,SPO,SP,VSP	000000
00101	3*	1	,BS,CB,MP1,PQ,RE,CP,CC,CH)	000000
00101	4*	C		000000
00101	5*	C	PURPOSE MODEL OF UTILITY CAPABLE OF PRODUCING	000000
00101	6*	C	BASELOAD AND PEAKLOAD POWER, AND OF	000000
00101	7*	C	ABSORBING SURPLUS POWER	000000
00101	8*	C		000000
00101	9*	C	METHOD COMPUTE PEAKLOAD GENERATION AND ENERGY COST	000000
00101	10*	C		000000
00101	11*	C	WRITTEN BY Y.K.CHAN VERSION 1,JUNE 8,1977	000000
00101	12*	C		000000
00101	13*	C	CALL SEQUENCE	000000
00101	14*	C	OUTPUT	000000
00101	15*	C	P1 -BASELOAD GENERATION,KW	000000
00101	16*	C	MP2 -MAXIMUM POWER CAPACITY,KW	000000
00101	17*	C	P2 -PEAKLOAD GENERATION,KW	000000
00101	18*	C	CO -COST OF ENERGY USED (STATE), \$	000000
00101	19*	C	COD -ENERGY COST RATE, \$/HR	000000
00101	20*	C	ICO -INTEGRATOR CONTROL FOR CO	000000
00101	21*	C	STATISTICS	000000
00101	22*	C	SR -SUM OF REQUESTED PEAK GENERATION,KW	000000

UT

00101	23*	C	SPO -SUM OF OUTPUT ENERGY, KWH	000000
00101	24*	C	SP -SUM OF SURPLUS ENERGY, KWH	000000
00101	25*	C	VSP -VALUE OF SURPLUS ENERGY, \$	000000
00101	26*	C	INPUTS	000000
00101	27*	C	BS -BASELOAD GENERATION (DEFAULT=0.),KW	000000
00101	28*	C	CB -COST OF BASELOAD GENERATION/KWH, \$	000000
00101	29*	C	MP1 -MAXIMUM POWER CAPACITY,KW	000000
00101	30*	C	PO -SURPLUS POWER RETURNED TO UTILITY,KW	000000
00101	31*	C	RE -PEAK GENERATION REQUEST, KW	000000
00101	32*	C	CP -COST OF PEAKLOAD GENERATION/KWH, \$	000000
00101	33*	C	CC -CAPITAL COST/YEAR, \$	000000
00101	34*	C	CM -MAINTENANCE COST/YEAR, \$	000000
00101	35*	C		000000
00103	36*		COMMON /CIMPL/IMPL,ICNT/CTIME/TIME/CSIMUL/DUM(7),TMAX	000000
00103	37*		X /COST/CCI,CHI,COP,VDE,TDE,TLO,UTV,UTD,SPD	000000
00104	38*		REAL MP2,MP1	000000
00104	39*	C		000000
00105	40*		IF(IMPL.GT.0)GO TO 100	000000
00107	41*		IF(BS.EQ..99999)BS=0.	000002
00111	42*		IF(MP1.EQ..99999)MP1=1.E8	000006
00113	43*		TMAX1=TMAX+.99999	000013
00114	44*		SR=0.	000016
00115	45*		SP=0.	000017
00116	46*		SPO=0.	000020
00117	47*		VSP=0.	000021
00120	48*		RE=0.	000022
00121	49*		PO=0.	000023
00121	50*	C		000023
00121	51*	C	COMPUTE POWER OUTPUTS	000023
00121	52*	C		000023
00122	53*		TINC1=DUM(7)*.5	000024
00123	54*		IF(BS.LE.MP1)GO TO 100	000027
00125	55*		WRITE(6,208)BS,MP1	000033
00131	56*	208	FORMAT(1H0,10H BASELOAD ,F12.3,32H EXCEEDS MAXIMUM POWER CAPACITY,	000042
00131	57*	1	F12.3)	000042
00132	58*		IF(IMPL.EQ.2)ICNT=ICNT+1	000050
00134	59*		BS=MP1	000050
00134	60*	C		000053
00135	61*	100	P1=BS	000054
00136	62*		MP2=MP1	000056
00137	63*		P2=AMIN1(MP1-BS,RE)	000056
00137	64*	C		000056
00137	65*	C	COMPUTE ENERGY COST	000056
00137	66*	C		000056
00140	67*		CX=0.	000064
00141	68*		IF(P2.GT.PO)CX=CP	000065
00143	69*		IF(ICO.NE.0)ICOD=BS*CB+(P2-PO)*CX	000073
00145	70*		IF(IMPL.LE.1)RETURN	000104
00145	71*	C		000104
00145	72*	C	STATISTICS	000104
00145	73*	C		000113
00147	74*		SR=SR+RE*TINC1	000117
00150	75*		SPO=SPO+ (P1+P2-PO)*TINC1	000125
00151	76*		IF(P2.GT.PO) GO TO 200	000131
00153	77*		TERM=(PO-P2)*TINC1	000135
00154	78*		SPO= SPO+TERM	000137
00155	79*		SP= SP+ TERM	

UT

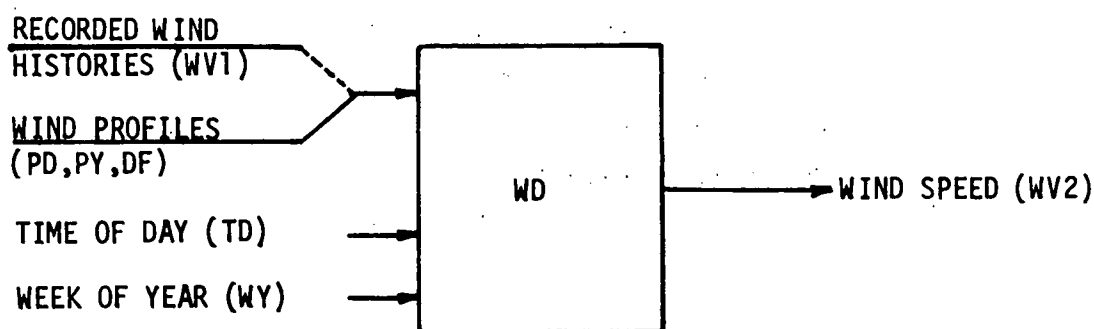
00156 80*
 00157 81*
 00157 82*
 00157 83*
 00161 84*
 00162 85*
 00163 86*
 00164 87*
 00165 88*
 00166 89*
 00167 90*
 00170 91*
 00171 92*

VSP= VSP+ CB*TERM

C 200 IF (TIME.LT.TMAX) RETURN
 CCI=CCI+CC
 CHI=CHI+CM
 VDE=VDE-CO+VSP
 TDE=TDE-SP0+SP
 UTV=UTV+CO
 UTD=UTD+SP0
 SPD= SPD+SP
 RETURN
 END

000141
 000146
 000146
 000146
 000154
 000157
 000162
 000166
 000172
 000175
 000200
 000203
 000340

7.47 WIND



This model computes wind speed either from user supplied time histories (data tape) or by generating a set of random numbers with user supplied daily and yearly average profiles and user specified random variation. If user supplied profiles are available then the wind speeds are generated from the following equation:

Basic Equation

$$WV = [PD(TD) + N(T)] * PY(WY) / M$$

where

- PD is the user supplied daily mean profile
- TD is the time of the day
- PY is the user supplied yearly profile
- WY is the week of the year
- N is white noise with user specified probability distribution

$$M = \frac{1}{J} \sum_{i=1}^J PY(i)$$

<u>Tables</u>	<u>Description</u>	<u>Units</u>
PD	Daily profile versus TD (default = 0)	miles/hr
PY	Yearly profile versus WY	arbitrary
DF	Density function for white noise terms (tabular with speed WV)	arbitrary

Inputs

Parameter/Port

WV	1	Wind speed data file input	miles/hr
TD		Time of day	hr
WY		Week of the year	-

Outputs

Variable/Port

WV	2	Wind speed	miles/hr
M		Mean of yearly profile	
TIM		Last time a random sample was generated	hr

Statistics

MV	Maximum speed	miles/hr
AV	Average speed (expected daily wind)	miles/hr

Calculation Sequence

- 1) Compute distribution function and mean M (first pass only)

$$F(W) = \frac{(\sum DF(V_i) : V_i \leq W)}{\sum DF(V_i)}$$

- 2) Check for data file input

If W1 = .99999 go to 3)

W2 = W1

Go to 5)

- 3) Generate white noise input N

If TIME = TIM go to 5)

U = random noise sample, uniformly distributed [0,1]

Interpolate to find $N = F^{-1}(U)$

TIM = TIME

- 4) Compute wind speed

$W2 = [PD(TD) + N] * PY(WY)/M$

- 5) Compute Statistics

ENTRY POINT 000412

COMMON BLOCKS

```

0003      CIMPL      000001
0004      CTIME      000001

```

EXTERNAL REFERENCES (BLOCK, NAME)

```
0005      UNTF
0006      TDLU1
0007      NERR3$
```

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

[illegible]

```

00100 1* CWD
00101 2* SUBROUTINE WD (PD,PY,WF,WVO,AMV,AV,XM,TIMO ,WVI,YD,WY)
00101 3* C
00101 4* C PURPOSE GENERATE WIND SPEED FROM DAILY, YEARLY, AND RANDOM PROFILE DATA
00101 5* C
00101 6* C METHOD RANDOM NOISE WITH SPECIFIED DIST. IS ADDED TO MEAN DAILY PROFILE
00101 7* C AND MULTIPLIED BY A YEARLY PROFILE. INITIALLY THE DENSITY TABLE
00101 8* C WF IS CONVERTED TO A DIST. FUNCTION.
00101 9* C
00101 10* C WRITTEN BY A.W. WARREN VERSION 1, MARCH 4 1977
00101 11* C
00101 12* C CALL SEQUENCE
00101 13* C TABLES
00101 14* C PD - MEAN DAILY WIND PROFILE, MPH
00101 15* C PY - MEAN YEARLY WIND PROFILE
00101 16* C WF - WIND FREQUENCY FUNCTION (NON-GUST, RANDOM COMPONENT), HR
00101 17* C
00101 18* C OUTPUTS
00101 19* C WVO - WIND VELOCITY OUTPUT, MPH
00101 20* C AMV - MAX. OBSERVED WIND SPEED, MPH
00101 21* C AV - MEAN DAILY WIND SPEED, MPH
00101 22* C XM - MEAN YEARLY WIND, -
00101 23* C TIMO- LAST TIME A RANDOM SAMPLE WAS USED, HR

```

[illegible]

WD

```

00101 29* C
00101 25* C INPUTS
00101 26* C WVI - WIND VELOCITY INPUT FROM DATA FILE, MPH
00101 27* C TD - TIME OF DAY, HR
00101 28* C WY - WEEK OF YEAR (1-52)
00101 29* C
00101 30* C
00101 31* C
00103 32* DIMENSION PD(1),PY(1),WF(1)
00104 33* COMMON/CI MPL/IMPL /CTIME/TIME
00105 34* DATA IX/1/
00105 35* C INITIALIZATION
00105 36* C COMPUTE MEAN DAILY WIND SPEED AND DIST. FCN
00107 37* C
00110 38* NP=WF(2)
00111 39* ND=PD(2)
00112 40* NY=PY(2)
00114 41* IF(IMPL.GT.0) 60 TO 10
00115 42* SUM=0.0
00116 43* AMN=0.0
00117 44* TIMO=-1.
00121 45* IF(WF(4+2*NP).EQ. 1.) 60 TO 40
00124 46* DO 20 I=1,NP
00125 47* WF(I+2) = WF(I+3)
00126 48* L = 3*NP+I
00127 49* A=WF(L)
00130 50* WF(L)=SUM
00131 51* SUM=SUM+ A
00133 52* 20 AMN = AMN + A*WF(2+I)
00134 53* AMN = AMN/SUM
00135 54* WF(3+NP)= WF(NP+2)*2. - WF(NP+1)
00136 55* WF(L+1)= 1.
00141 56* C
00142 57* DO 30 I=1,NP
00144 58* L=3+NP+I
00144 59* 30 WF(L) = WF(L)/SUM
00144 60* 40 CONTINUE
00144 61* C
00145 62* C
00147 63* IF(PD(2).EQ. 1.99999) PD(4)=0.
00151 64* IF(PD(2).EQ. 1.99999) PD(5)=0.
00151 65* IF(PD(2).EQ. 1.99999) PD(2)=1.
00153 66* C
00154 67* AV = 0.
00157 68* DO 25 I=1,ND
00160 69* L = 3*ND+I
00162 70* 25 AV = AV+PD(L)
00162 71* AV = AV/ND + AMN
00163 72* C
00164 73* XM=0.
00167 74* DO 15 I=1,NY
00170 75* L=3+NY+I
00172 76* 15 XM=XM+PY(L)
00173 77* XM=XM/NY
00173 78* AMV =0.
00173 79* C
00174 80* C CHECK FOR DATA FILE INPUT
00174 80* 10 IF( WVI.EQ. .99999) GO TO 100

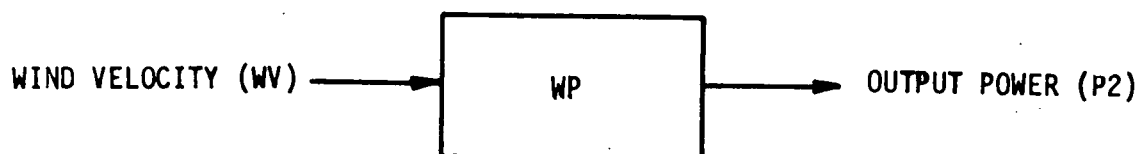
```

[illegible]

WD

00176	81*	WVO = WVI	000247
00177	82*	GO TO 150	000251
00177	83*	C	000251
00177	84*	C	000251
00200	85*	100 IF(TIME.EQ.TIME) GO TO 150	000253
00202	86*	CALL UNIF(U,IX)	000255
00203	87*	NP1=NP+1	000261
00204	88*	WN = TBLU1(U,WF(4+NP),WF(3),1,-NP1)	000264
00204	89*	C	000264
00204	90*	C	000264
00205	91*	GENERATE WIND SPEED USING DAILY AND YEARLY PROFILES	000303
00206	92*	DWV = TBLU1(TD,PD(4),PD(4+ND),1,-ND)	000323
00207	93*	YWV = TBLU1(WY,PY(4),PY(4+NY),1,-NY)	000343
00210	94*	WVO = (DWV + WN)* YWV / XM	000350
00210	95*	TIME=TIME	000350
00210	96*	C	000353
00211	97*	C	000361
00213	98*	MAX. OBSERVED WIND SPEED	000367
00214	99*	150 IF(IMPL.LE.1) RETURN	000472
00215	100*	AMV = AMAX1(AMV,WVO)	
		RETURN	
		END	

7.48 TURBINE/GENERATOR



This component uses a power curve relationship with wind velocity to model the wind turbine and generator. It may be used in place of the more detailed wind turbine-transmission-generator components where a simplified analysis is desirable, or where a nonstandard wind generator model is desired. The model may be used for either A.C. or D.C. power generation.

Basic Equations

$$P_2 = I = 0 \quad \left(\begin{array}{l} WV < WVO \\ WV > WV1 \end{array} \right)$$

$$P_2 = V * I / 1000 \quad WVO \leq WV \leq WV1$$

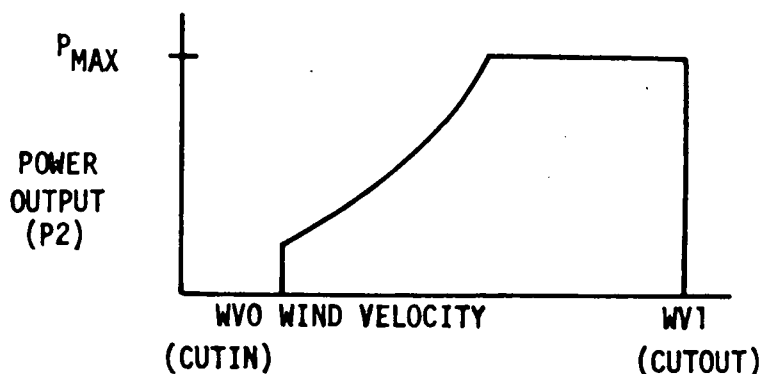


FIGURE 7.48: OUTPUT POWER VERSUS WIND VELOCITY

Tables

PW

Description

Wind generation power versus wind velocity ¹

Units

kw

Inputs

Parameter/Port

V	Bus voltage (Rated).	volts
WV0	Power cutin velocity	mph
WV1	Power cutout velocity	mph
WV	Wind velocity	mph
CC	Capital cost/year	\$
CM	Maintenance cost/year	\$
EC	Control Energy Rate	\$/hr

Outputs

Variable/Port

I	Bus current	amps
P	2 Real power output	kw

Statistics

MI	Maximum current	amps
MP0	Maximum power	kw
SP	Total output energy	kwh
C0	Total operating costs	\$

¹

Output power including mechanical and electrical efficiencies

Calculation Sequence

1) Initialize statistics

2) Compute P2 and I

$$P2 = \begin{pmatrix} PW(WV) & W0 \leq WV \leq WV1 \\ 0 & \text{otherwise} \end{pmatrix}$$

$$I = P2 * 1000 / V$$

3) Compute Statistics and Costs

SUBROUTINE WP ENTRY POINT 000153

STORAGE USED CODE(1) 000232; DATA(0) 000024; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 CIMPL 000001
0004 COST 000003
0005 CTIME 000001
0006 CSIMUL 000010

EXTERNAL REFERENCES (BLOCK, NAME)

0007 TBLU1
0010 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000046 10L	0001 000064 20L	0004 R 000000 CC	0004 R 000001 CM	0004 R 000002 COP
0006 000000 DUM	0003 I 000000 IMPL	0000 000006 INJPS	0000 I 000000 N	0007 R 000000 TBLU1
0005 R 000000 TIME	0006 R 000006 TINC	0006 R 000007 TMAX	0000 R 000001 TMAX1	

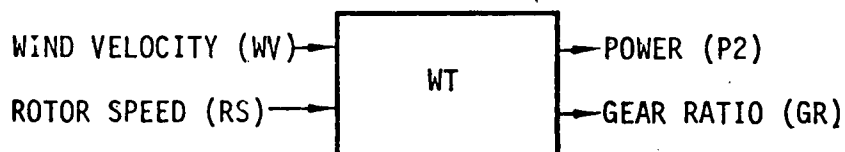
00100	1*	CMP		000000
00101	2*		SUBROUTINE WP (PW,BI,PO,AMI,AMP,SP,CO,VO,WVC,WV1,WV,CCI,CHI,EC)	000000
00101	3*	C		000000
00101	4*	C	PURPOSE MODEL THE WIND TURBINE AND GENERATOR USING A POWER CURVE	000000
00101	5*	C		000000
00101	6*	C	WRITTEN BY A.W. WARREN	000000
00101	7*	C	VERSION 1, MARCH 3 1977	000000
00101	8*	C	CALL SEQUENCE	000000
00101	9*	C	TABLES	000000
00101	10*	C	PW - WIND GENERATION POWER IN KW VERSUS WIND VELOCITY IN MPH	000000
00101	11*	C		000000
00101	12*	C	OUTPUTS	000000
00101	13*	C	BI - OUTPUT BUS CURRENT, AMPS	000000
00101	14*	C	PO - POWER OUTPUT, KW	000000
00101	15*	C	AMI - MAX. OBSERVED CURRENT, AMPS	000000
00101	16*	C	AMP - MAX. OBSERVED POWER, KW	000000
00101	17*	C	SP - TOTAL OUTPUT ENERGY, KWH	000000
00101	18*	C	CO - OPERATING COST, \$	000000
00101	19*	C		000000
00101	20*	C	INPUTS	000000
00101	21*	C	VO - RATED BUS VOLTAGE, VOLTS	000000
00101	22*	C	WVO - POWER CUTIN VELOCITY, MPH	000000
00	23*	C	WV1 - POWER CUTOFF VELOCITY, MPH	000000
00	24*	C	WV - WIND VELOCITY, MPH	000000
00	25*	C	CCI - CAPITOL COST / YEAR, \$	000000

W/P

00101	26*	C	CHI - MAINTENANCE COST / YEAR, \$	000000
00101	27*	C	EC - CONTROL ENERGY RATE, \$/HR	000000
00101	28*	C		000000
00103	29*		DIMENSION PW(1)	000000
00104	30*		COMMON / CIMPL / INPL	000000
00105	31*		COMMON/COST/ CC,CH,COP /CTIME/ TIME /CSIMUL/ DUM(6),TINC,TMAX	000000
00105	32*	C		000000
00105	33*	C	POWER OUTPUT CALCULATIONS	000000
00105	34*	C		000000
00106	35*		PO = C.	000000
00107	36*		IF(MV.LT.WVO .OR. MV.GT.WV1) GO TO 10	000001
00111	37*		N = PW(2)	000017
00112	38*		PO = TBLU1(MV,PW(4),PW(4+N),1,-N)	000026
00113	39*		10 BI = PO*1000/VO	000046
00113	40*	C	STATISTICS	000046
00113	41*	C		000046
00114	42*		IF(IMPL.GT.0) GO TO 20	000051
00116	43*		CO= 0.	000054
00117	44*		AMI = 0.	000055
00120	45*		AMP = 0.	000056
00121	46*		SP = 0.	000057
00122	47*		TMAX1=TMAX*.99999	000060
00123	48*	20	IF(IMPL.LE.1) RETURN	000064
00125	49*		AMI = AMAX1(AMI,BI)	000072
00126	50*		AMP = AMAX1(AMP,PO)	000100
00127	51*		SP = SP + PO*.5*TINC	000106
00130	52*		CO= CO + EC*.5*TINC	000113
00130	53*	C	COST SUMMATION	000113
00131	54*		IF(TIME.LT.TMAX1) RETURN	000120
00133	55*		CC = CC + CCI	000127
00134	56*		CH = CH + CHI	000132
00135	57*		COP= COP + CO	000135
00136	58*		RETURN	000140
00137	59*		END	000231

W/P

7.49 WIND TURBINE



This component models the wind turbine in terms of physical properties such as blade radius, power coefficient, and design tip speed ratio.¹ The step-up gear ratio is computed based on design rotor speed.

Basic Equations

Output power is given by

$$P2 = CP * 1/2 * AD * A * (WV * C)^3 * k$$

where:

CP = effective power coefficient (tabular with WV)

A = $\pi * (BR)^2$

C = 1.4667 (mph to ft/sec. conversion)

k = 1.3558×10^{-3} (ft-lb to kw-sec. conversion)

¹ NASA CR 134937 "Design Study of Wind Turbines - 50kw to 3000 kw - For Electric Utility Applications", Kaman Aerospace Corporation, February 1976.

Inputs

<u>Parameter/Port</u>	<u>Description</u>	<u>Units</u>
WV	Wind speed	mph
V0	Mean wind speed (yearly)	mph
VR	Rated wind speed (default = $1.35 \times V0$)	mph
RS	Rotor speed	rpm
RSG	Generator shaft speed (design)(default = 1800)	rpm
BR	Blade radius	ft
EC	Cost to operate controls	\$/h
AD	Air density (default = 0.0023)	slugs/ft ³
LAM ¹	Design tip speed ratio (default = 9.4)	-
CPM ²	Maximum power coefficient at V0 (default = 0.4)	-
CP	Effective power coefficient (default table versus V0/WV)	-
CC	Capital cost/year	\$
CM	Maintenance cost/year	\$

Outputs

<u>Variable/Port</u>			
P	2	Output mechanical power	kw
T0		Mechanical torque	ft-lb
C0		Total operating cost	\$
GR		Step-up gear ratio	-
RAP		Rated output power	kw

Statistics

MT	Maximum torque	ft-lb
MP0	Maximum power	kw
SP	Total energy delivered	kwh

¹ LAM may be computed using the design equation:

$$LAM = \sqrt{8 / (3 * \text{solidity constant} * \text{design lift coefficient})}$$

² If default CP table not used then set CPM = CP(rated wind speed)

Calculation Sequence

- 1) First pass - Compute Gear Ratio and Rated Power

$$RS = (LAM*V0*C/BR)*(60/2\pi)$$

$$GR = RSG/RS$$

$$RAP = .5*CP1*AD*A*(VR*C)^3$$

where

$$CP1 = \begin{cases} CPM*F(V0/VR) & \text{if CP default used} \\ CPM & \text{otherwise} \end{cases}$$

- 2) Compute power coefficient CP

If $W = 0$ set $P2=T0=0$ and go to 4)

If CP default used, then

$$CP = CPM*F(V0/W)$$

where F is shown in Figure 7.49

- 3) Power and torque

$$A = \pi*BR^2$$

$$P = .5*CP*AD*A*(WV*C)^3$$

$$(C = 1.4667)$$

$$T0 = P/(RS*2\pi/60)$$

$$P2 = P*k$$

$$(k = 1.3558 \times 10^{-3})$$

- 4) Compute Statistics and Costs

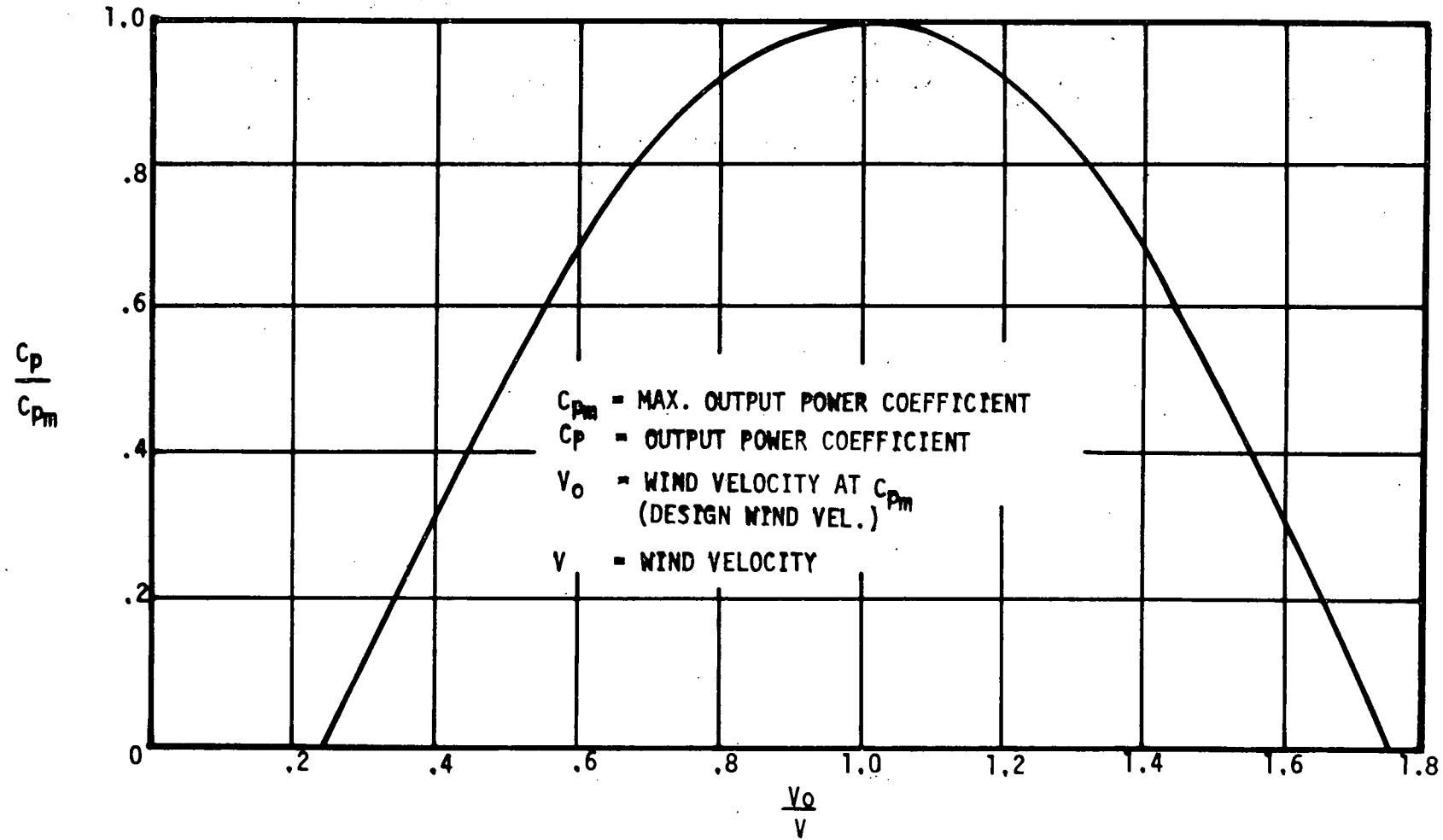


FIGURE 7.49 GENERALIZED MACHINE POWER OUTPUT PERFORMANCE

WT

SUBROUTINE WT ENTRY POINT 000274

STORAGE USED CODE(1) 000413; DATA(0) 000070; BLANK COMMON(2) 000000

COMMON BLOCKS

0003 C1MPL 000001
0004 CTIME 000001
0005 CSIMUL 000010
0006 COST 000003

EXTERNAL REFERENCES (BLOCK, NAME)

0007 TELU1
0010 NERR3s

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000122 100L	0001 000211 200L	0000 R 000034 A	0006 R 000000 CCI	0006 R 000001 CMI
0006 R 000002 C01	0000 R 000033 CP1	0000 R 000026 C1	0000 R 000027 C2	0005 000000 DUM
0000 R 000000 F	0003 I 000000 INPL	0000 000051 INJP5	0000 R 000035 P	0000 R 000030 PJ
0007 R 000000 TPLU1	0004 R 000000 TYNE	0005 R 000006 TINC	0000 R 000032 TINC2	0005 R 000007 TMAX
0000 R 000031 TMAX1				

00100	1*	CMT1		000000
00101	2*		SUBROUTINE WT (P2,TO,CO,GR,RAP,MT,MPO,SP,WV,VO,VR,RS, RSG,BR,EC,	000000
00101	3*	1	AD,LAN,CPM, CP,CC,CH)	000000
00101	4*	C		000000
00101	5*	C	PURPOSE MODEL WIND TURBINE POWER OUTPUT	000000
00101	6*	C		000000
00101	7*	C	METHOD COMPUTE POWER COEFFICIENT AND ROTOR SPEED FROM PHYSICAL	000000
00101	8*	C	DESIGN PARAMETERS. RATED POWER COEFF. IS 3/4 OF CPM.	000000
00101	9*	C		000000
00101	10*	C	WRITTEN BY A. W. WARREN	000000
00101	11*	C	VERSION 2, APRIL 6 1977	000000
00101	12*	C	CALL SEQUENCE	000000
00101	13*	C	OUTPUTS	000000
00101	14*	C	P2 - OUTPUT MECHANICAL POWER, KW	000000
00101	15*	C	TO - OUTPUT MECHANICAL TORQUE, FT-LB	000000
00101	16*	C	CO - OPERATING COST SUM, \$	000000
00101	17*	C	GR - TURBINE/GENERATOR GEAR RATIO	000000
00101	18*	C	RAP - RATED OUTPUT POWER, KW	000000
00101	19*	C	MT - MAXIMUM TORQUE STATISTIC, FT-LB	000000
00101	20*	C	MPO - MAXIMUM POWER STATISTIC, KW	000000
00101	21*	C	SP - TOTAL OUTPUT ENERGY DELIVERED, KWH	000000
00101	22*	C		000000
00101	23*	C	INPUTS	000000

WT

00101	24*	C	WV - WIND SPEED MPH	000000
00101	25*	C	VO - MEAN WIND SPEED (YEARLY), MPH	000000
00101	26*	C	VR - RATED WIND SPEED, MPH	000000
00101	27*	C	RS - ROTOR SPEED, RPM	000000
00101	28*	C	RSG - GENERATOR SHAFT SPEED, RPM	000000
00101	29*	C	BR - BLADE RADIUS, FT	000000
00101	30*	C	EC - CONTROL ENERGY RATE, \$/HR	000000
00101	31*	C	AD - AIR DENSITY, SLUGS/FT**3	000000
00101	32*	C	LAM - DESIGN TIP SPEED RATIO	000000
00101	33*	C	CPM - MAXIMUM POWER COEFFICIENT AT VO	000000
00101	34*	C	CP - EFFECTIVE POWER COEFFICIENT AT WV	000000
00101	35*	C	CC - CAPITAL COST PER YEAR	000000
00101	36*	C	CM - MAINTENANCE COST PER YEAR	000000
00101	37*	C		000000
00103	38*		COMMON /CIMPL/IMPL /CTIME/ TIME /CSIMUL/ DUM(6),TINC,TMAX	000000
00104	39*		COMMON /COST/ CCI,CHI,COI	000000
00105	40*		REAL MT,MPO,LAM	000000
00106	41*		DIMENSION F(22)	000000
00107	42*		DATA F/.24,.4,.6,.68,.8,1.,1.2,1.31,1.4,1.6,1.74,0.,.31,.68,.8,	000000
00107	43*		1 .92,1.,.92,.8,.68,.3,0. /,C1,C2,PI/1.4667,.0013558,3.14159	000000
00107	44*	C		000000
00107	45*	C	INITIALIZATION	000000
00107	46*	C		000000
00114	47*		IF(IMPL.GT.0) GO TO 100	000000
00116	48*		TMAX1 = TMAX*.99999	000000
00117	49*		TINC2 = .5* TINC	000000
00117	50*	C		000000
00120	51*		IF(VR .EQ. .99999) VR = 1.35* VO	000000
00122	52*		IF(RSG .EQ. .99999) RSG= 1800.	000000
00124	53*		IF(AD .EQ. .99999) AD = .0023	000000
00126	54*		IF(LAM .EQ. .99999) LAM= 9.4	000000
00130	55*		IF(CPM .EQ. .99999) CPM= 0.4	000000
00130	56*	C		000000
00132	57*		RS = C1*LAM*VO/BR*(30./PI)	000000
00133	58*		GR = RSG /RS	000000
00134	59*		CP1= CPM	000000
00135	60*		IF(CP.EQ. .99999) CP1= CPM*TBLU1(VO/VR,F(1),F(12),1,-11)	000000
00137	61*		RAP= .5*CP1*AD*PI*BR*BR*(VR*C1)**3*C2	000000
00140	62*		CO = 0.0	000000
00141	63*		SP = 0.0	000000
00142	64*		MPO= 0.0	000000
00143	65*		MT = 0.0	000000
00143	66*	C		000000
00143	67*	C	POWER COEFFICIENT CALCULATION	000000
00143	68*	C		000000
00144	69*		100 P2 = 0.0	000000
00145	70*		TO = 0.0	000000
00146	71*		IF(WV.EQ. 0.) GO TO 200	000000
00150	72*		CP1 = CP	000000
00151	73*		IF(CP1.EQ. .99999) CP1 = CPM*TBLU1(VO/WV,F(1),F(12),1,-11)	000000
00153	74*		IF(CP1.EQ. 0.) GO TO 200	000000
00153	75*	C		000000
00153	76*	C	OUTPUT POWER AND TORQUE	000000
00153	77*	C		000000
00155	78*		A = PI*BR**2	000000
00156	79*		P = .5*CP1*AD*A*(WV*C1)**3	000000
00157	80*		IF(WV.GT.VR)P= RAP/C2	000000

WT


```

00161 81*      T0=P/(RS*PI/30.)
00162 82*      P2 = P*C2
00162 83*      C
00162 84*      C      STATISTICS AND COSTS
00162 85*      C
00163 86*      200 IF(IMPL.LE.1) RETURN
00163 87*      C
00165 88*      CO = CO + EC*TINC2
00166 89*      MT = AMAX1( MT,T0)
00167 90*      MPO= AMAX1(MPO,P2)
00170 91*      SP = SP + P2*TINC2
00170 92*      C
00171 93*      IF(TIME.LT.TMAX1)RETURN
00173 94*      CCI = CCI + CC
00174 95*      CHI = CHI + CM
00175 96*      COI = COI + CO
00175 97*      C
00176 98*      RETURN
00177 99*      END

```

```

000177
000205
000205
000205
000205
000211
000211
000217
000223
000231
000237
000237
000243
000252
000255
000260
000260
000263
000412

```

8.0 EXAMPLES

This section gives five simple example simulations using the SIMWEST program. These examples exercise all physical components of the SIMWEST library and many of the model features such as Fortran code insertion and the file read capability. Each example contains the input data for model generation and analysis, selected printer output generated by the programs and a discussion of the results obtained. It is recommended that a user work through and understand the model connections for these examples before attempting to build more complex models such as that of Figure 1-7.

8.1 WIND TURBINE AND FILE READ MODEL

Figure 8.1-1 shows a simplified schematic of the wind turbine and file read model. In this example a wind turbine is used to feed power directly to a load. Wind and load time histories are read from a mass storage file and then used to drive the simulation. A histogram for power output is also included. Figure 8.1-2 shows the input data to build the model and print out some of the load file data. The order of the component definitions is such that information passes down the list, i.e. no component is defined before components in the INPUTS list. This assures that the component subroutines in the Fortran model will be called in the right order. The first Fortran statement is inserted in the model prior to the Fortran which sets up the iteration loop, while the second set of Fortran statements is within the loop and writes out the load file data from array TEMP the first pass through the model. Figure 8.1-3 shows the model schematic generated. In addition to showing the component connections, the names of the input connections are printed out. Notice that information passes not only from WT to GR but also vice-versa. The input RSIGR to WT is a feedback variable and so is the input RS GE to GR. It is the presence of the feedback variables which require several iterations to attain steady state.

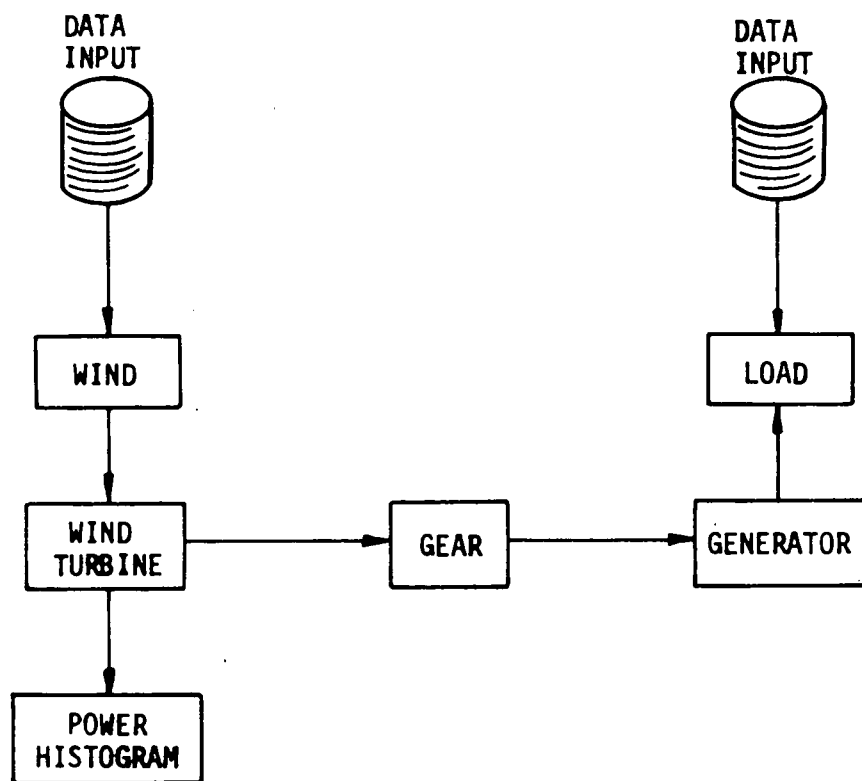


FIGURE 8.1-1: WIND TURBINE AND FILE READ EXAMPLE

```

MODEL DESCRIPTION      TAPE READ TEST
FORTRAN STATEMENTS
COMMON /DATARD/ TEMP(448)
LOCATION=15      TI
LOCATION=3        TAW      INPUTS=TI
LOCATION=11       WD      INPUTS=TI, TAW(VAR=WD)
LOCATION=31       WT      INPUTS=WD
LOCATION=35       GR      INPUTS=WT
LOCATION=51       HG      INPUTS=WT(P =FIN)
LOCATION=39       GE      INPUTS=GR
LOCATION= 7       TAL      INPUTS=TI
LOCATION=19       LO      INPUTS=GE, TI, TAL (VAR=LO)
FORTRAN STATEMENTS
IF(IMPL.GT.0) GO TO 2
WRITE (6,100) (TEMP(I), I=1,448)
100 FORMAT(1H ,12F10.3)
2 CONTINUE
END OF MODEL
LIST STANDARD COMPONENTS
PRINT

```

FIGURE 8.1-2 INPUT DATA FOR FILE READ MODEL

The input data for several simulations using this model is shown in Figure 8.1-4. The component parameter values are first specified, those inputs not specified taking default values. A number of tables are then specified. The WD and LO tables are not really needed here. The wind and load file data was originally generated from an earlier run using these tables. Following the tables are the printer plot input commands, and the simulation values and print commands for a one week run. The parameter values for a second simulation which reads to the end of the file are then given. The last simulation attempts to read past the end of file.

Some of the output for the first simulation are shown in Figures 8.1-5 to 8.1-8. Figure 8.1-5 shows the output resulting from the FORTRAN STATEMENTS code. This data is formatted to output the time of the initial load value (0.0), the data increment step (0.25), and 446 load values at successive time increments. Figure 8.1-6 shows the power output histogram from the wind turbine. Almost 40% of the time the turbine reaches rated power (800 kw). Figure 8.1-7 shows a crossplot of wind turbine output versus wind velocity. The cutin velocity is about 12 mph and rated power is attained at about 28

TAPE READ TEST

PAGE 0

1	2	3	4	5	6	7	8	9	10


```

TITLE= TAPE READ TEST
PARAMETER VALUES
CYCLES=2.01,T0 TI=0,FUPHG=1000,FLOHG=50,NSTTAW=0,ITFTAW=1
UO WT=21,BR WT=80,EC WT=1,CPMWT=.41,CC WT=16000,CM WT=2000
RPSGE=.01,CC GR=1000,CM GR=200,NSTTAL=0,ITFTAL=2
PPAGE=750,RSYGE=1800,DA GE=0.2,SR GE=.005,UO GE=400,CC GE=1000,CM GE=200
NO LO=.00574,CT LO=4,MN LO=0,STDLO=6,VE LO=.023
TABLE,PY WD=13
4.,4.33,8.67,13.,17.33,21.67,26.,30.33,34.67,39.,43.33,47.67,52.
65,67,68,65,61,56,51,49,49,52,56,61,65
TABLE,PD WD=7
0,4,8,12,16,20,24
0,0,0,6,6,6,0
TABLE,DF WD=16
0,3,6,9,12,15,18,21,24,27,30,33,36,39,42,45
5,44,160,380,480,512,440,376,307,270,148,76,40,22,9,3
TABLE,PLOGR =7
0,100,200,300,400,500,600
3,4,9,18,32,50,72
TABLE,PD LO=17
0,1.5,3,4.5,6,7.5,9,10.5,12
13.5,15,16.5,18,19.5,21,22.5,24
450,660,872,930,450,660,810,798,804
690,708,699,702,750,708,570,450
TABLE,PW LO=7
1,2,3,4,5,6,7
1,1,.9,.9,.9,.6,.5
TABLE,PY LO=6
0,10,20,30,40,52
96,194,180,174,194,226
PRINTER PLOTS,DISPLAY1
WEND,US,TIME
P1 WT,US,WUEND
P2 GR,US,P2 WT
LO2LO,US,TIME
PC LO,US,TIME
DISPLAY2,P2 GE,US,TIME
THC=.25,TMAX=168.,PRATE=24,PRINT CONTROL=3,INT MODE=3,OUTRATE=2
SIMULATE
PARAMETER VALUES,T0 TI=4200,NSTTAW=38,NSTTAL=39,TMAX=220
SIMULATE
PARAMETER VALUES,NSTTAL=40,

```

FIGURE 8.1-4 INPUT DATA FOR ANALYSIS PROGRAM

mph. The load-time profile for the simulation is shown in Figure 8.1-8. Daily peaks and troughs are clearly indicated. The lower levels of the last two days reflect week-end load modeling.

PRINT RATE= 24 DISPLAY RATE= 2 MODE= 3 TINC= .25000 TMAX= 168.00

TAPE READ TEST

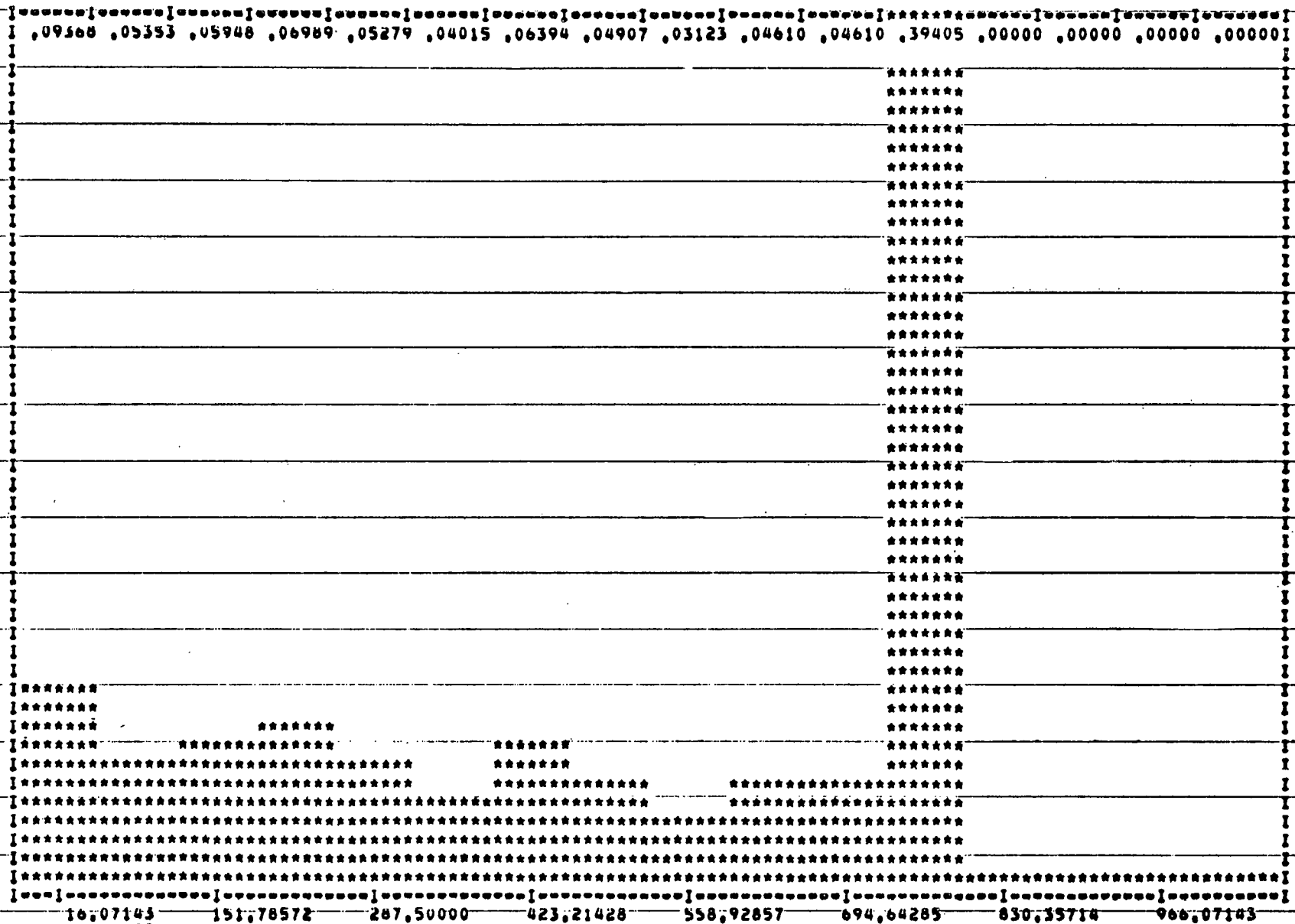
CASE NO. 1

IDENTIFICATION HEADER FOR UNIT 11
NO GENERATED WIND DATA

IDENTIFICATION HEADER FOR UNIT 12
NO GENERATED LOAD DATA

0.000	.250	512.020	576.458	541.273	542.305	504.160	490.027	458.856	465.241	471.429	461.310
472.202	469.504	484.207	478.548	457.784	462.708	428.157	417.025	435.024	424.541	477.498	477.597
524.878	529.235	580.327	574.953	655.125	684.704	751.090	774.545	849.244	842.653	919.063	906.349
976.191	971.344	1035.062	1030.417	1019.400	1025.785	1025.351	1015.678	1029.436	1016.803	1021.731	1030.062
1036.085	1020.695	1024.203	1026.614	982.779	972.742	929.110	935.981	880.547	874.323	888.260	897.320
894.753	914.397	906.599	905.685	896.960	897.141	895.837	899.829	899.173	897.042	908.923	887.126
902.818	898.822	898.457	898.273	910.522	928.584	951.416	932.214	966.968	961.958	927.407	940.644
906.296	909.801	914.014	904.625	848.249	849.443	783.334	799.167	737.316	728.981	668.681	668.212
622.550	633.111	568.890	571.529	529.372	544.840	509.411	501.604	464.107	453.340	459.528	467.007
460.501	477.917	462.686	483.800	462.589	457.579	444.235	439.874	419.515	429.792	483.195	466.143
526.520	528.161	572.035	570.269	660.377	652.042	770.330	756.319	843.668	857.838	896.782	901.220
957.964	976.595	1026.770	1039.277	1021.489	1024.710	1030.602	1024.092	1031.524	1028.826	1013.439	1024.933
1010.194	1036.326	1032.617	1025.094	991.639	974.384	937.970	924.526	874.771	866.031	886.739	888.582
910.831	849.333	847.415	907.327	909.429	902.392	897.479	895.145	901.262	885.588	900.631	888.768
897.689	893.247	886.110	907.132	909.001	926.617	950.342	937.912	958.230	960.438	963.353	935.515
929.145	918.661	845.342	903.105	849.891	844.314	785.423	780.048	725.415	734.232	684.312	683.844
620.583	621.210	527.518	515.674	487.255	479.243	454.255	434.638	413.080	415.578	421.951	409.596
425.091	425.911	429.801	427.555	417.808	404.358	389.100	388.022	376.195	378.948	417.267	427.101
469.653	461.386	516.310	539.500	592.569	600.906	670.397	672.822	764.028	771.088	805.735	828.013
812.988	858.882	932.067	940.076	917.971	932.658	923.327	932.503	929.850	921.327	920.069	942.602
917.149	934.573	925.140	924.464	878.517	881.672	830.214	842.894	801.363	796.343	790.602	795.509
808.635	804.783	818.845	811.978	807.374	814.032	812.055	807.109	803.271	810.696	812.447	801.771
806.953	818.793	749.780	808.956	826.075	820.398	835.254	839.504	854.944	865.872	850.213	837.347
822.271	837.615	832.466	814.272	757.037	770.703	702.264	691.332	654.351	653.748	608.418	607.997
566.499	567.063	522.901	523.648	498.076	490.064	449.639	451.553	411.712	436.143	423.429	408.227
420.876	436.731	431.681	429.435	413.593	408.683	405.614	402.090	378.074	386.922	421.993	438.323
474.379	466.112	568.445	528.789	594.047	596.289	680.816	677.548	750.470	775.412	807.615	820.550
868.372	872.950	942.887	935.459	925.544	915.451	925.206	921.792	913.044	913.864	912.204	922.549
915.379	911.673	926.217	919.446	883.644	883.150	834.940	841.525	791.053	794.974	805.072	799.833
801.172	794.474	811.432	814.259	824.690	812.262	807.840	811.835	801.501	806.079	804.181	800.402
814.525	820.271	800.856	819.777	827.553	837.715	861.511	838.135	850.327	864.102	858.187	844.919
838.785	823.656	812.413	809.656	756.070	757.145	709.836	711.495	659.479	661.320	609.896	615.971
571.225	562.447	518.686	512.937	481.270	488.695	448.270	450.184	410.343	406.747	403.375	418.646
416.260	429.268	417.722	425.220	421.165	413.810	392.056	388.131	376.304	385.152	429.967	427.612
472.609	473.684	513.171	521.326	542.678	592.074	679.849	682.274	761.291	758.607	818.435	812.685
863.755	874.428	935.424	940.586	939.612	929.921	920.590	930.167	914.924	918.590	923.426	908.991
923.353	916.399	928.498	927.420	878.626	885.029	827.477	834.062	804.720	796.452	809.396	801.713
796.556	789.857	809.662	803.548								

FIGURE 8.1-5 TAPE READ FORMATTED LOAD DATA



HISTOGRAM FOR 1345 SAMPLES MEAN 500,779.55 STANDARD DEV. 290,398.80

TIME 168.0
0 1696.7

STATES

FIGURE 8.1-6 WIND TURBINE POWER HISTOGRAM

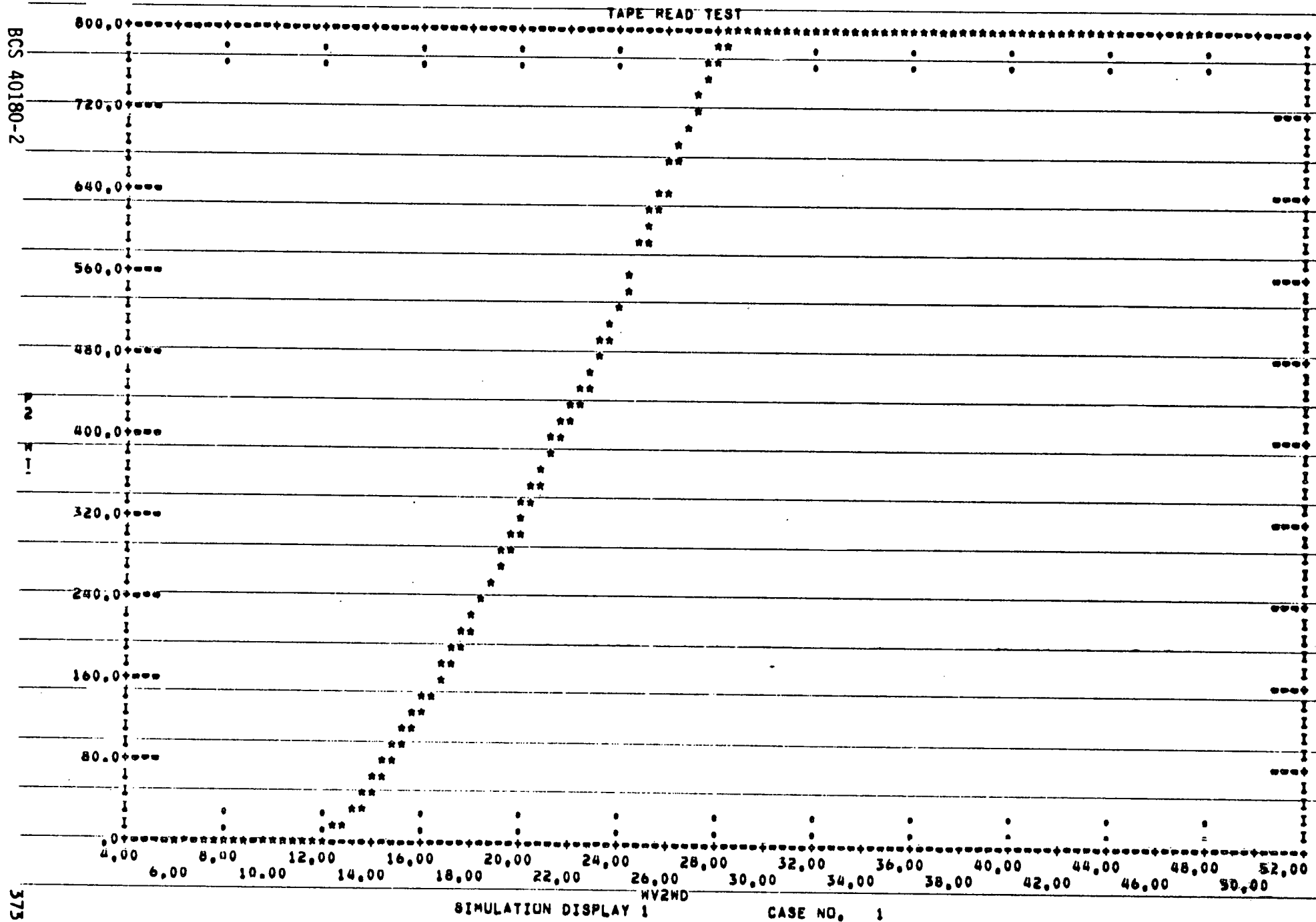


FIGURE 8.1-7 WIND POWER OUTPUT VERSUS WIND VELOCITY

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TAPE READ TEST

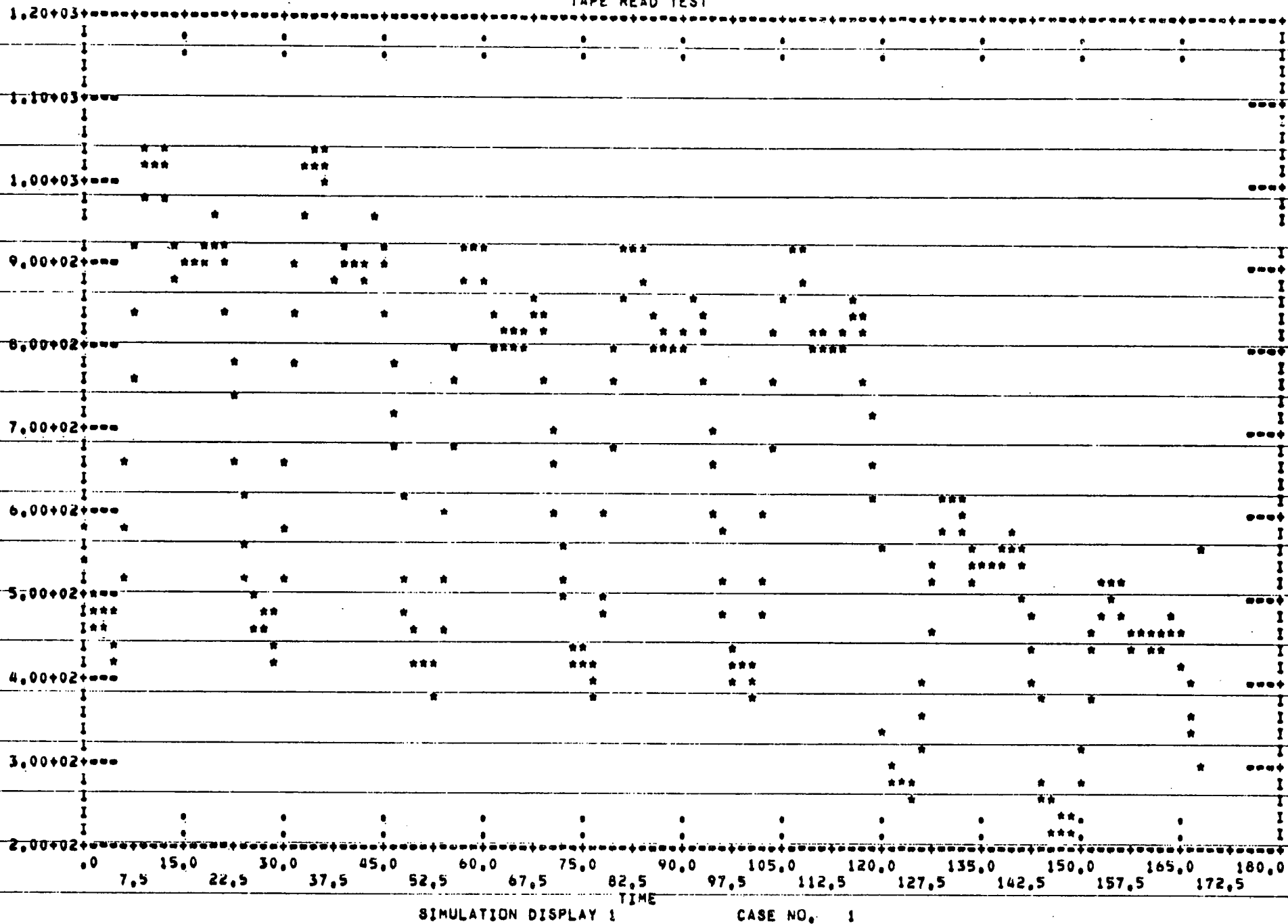
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40180-2

FIGURE 8.1-8 WEEKLY LOAD PROFILE

8.2 BATTERY STORAGE MODEL

A simplified schematic of the battery storage model is shown in Figure 8.2-1. In this model, wind power supplemented by a utility generation source is supplied to a power divider, which delivers power to the load as a first priority, and battery storage as second priority. Similarly, if the load cannot be met from the wind or storage, then the utility is requested to supply peaking power to meet the load. This model exercises the logic components including the priority Interrupt.

Figure 8.2-2 shows the model generation Input data for the model. The components are generally defined in the order of power flow shown in Figure 8.2-1. Ordering the component definition in this way is recommended to avoid convergence problems in the iteration loop. Thus, it would be somewhat better for consistency to define UT after WP rather than after LO in the model. All three types of model connections are illustrated in this example. For example, WP has the general input connection WD, MAB has the specific input connection WP (P,2 = FIN), and PD has the port to port connection PA (1,1). The port connections are especially useful for connecting up the multiport logic components PA and PD. The connection PA (1,1), for example, connects an input request of PD to PA and a power and maximum power input of PA to PD. It may be observed that the utility is connected up to the surplus port of PD. Thus the baseload power sent to MAB in effect is reduced whenever the load and battery cannot absorb all the power generated. The last component defined is the cost monitor CM, which receives cost input data from other components through a common block rather than by model connections. Figure 8.2-3 shows the model schematic generated by the program. Most of the connection inputs are shown but occasionally a model connection will be overprinted. For example, the input RE1PA to PD is not shown in 8.2-3. In cases like this it is necessary to check the Fortran model (EQMO) in order to verify the model connections.

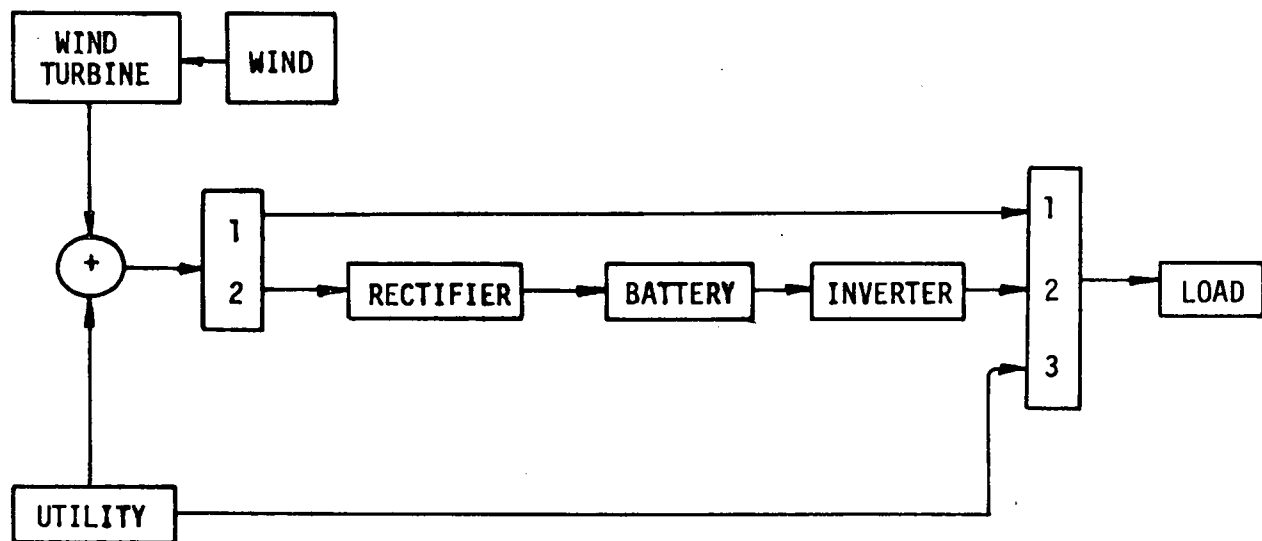


FIGURE 8.2-1: BATTERY STORAGE EXAMPLE

MODEL DESCRIPTION		BATTERY TEST CASE
LOCATION=74	TI	
LOCATION=61	WD	INPUTS=TI
LOCATION=21	WP	INPUTS=WD
LOCATION=42	MAB	INPUTS=WP (P, 2=FIN), UT (P, 1=C2)
LOCATION=33	PD	INPUTS=MAB (FO=P), MAB (FO=WP), PA (1,1), PIB (2,2), BA (RE=RE, 2)
LOCATION=15	RE	INPUTS=PD (2,1)
LOCATION=17	BA	INPUTS=RE, PA (RE, 2=RE)
LOCATION=45	PIB	INPUTS=BA
LOCATION=19	IV	INPUTS=BA
LOCATION=69	PA	INPUTS=IV (2,2), LO (1,0) PIB (4,2), UT (2,3)
LOCATION=76	LO	INPUTS=TI
LOCATION=62	UT	INPUTS=PD (SP=P, 0)
LOCATION=1	CM	
END OF MODEL		
LIST STANDARD COMPONENTS		
PRINT		

FIGURE 8.2-2 BATTERY MODEL INPUT DATA

The input data for two simulations is shown in Figure 8.2-4. In the first simulation the battery is nearly full at time = 0 and the load is chosen larger on the average than the wind and utility power supplied. In the second simulation the reverse is true, i.e. the load is less than that supplied by the wind system, and the battery storage is fairly low. Figures 8.2-5 to 8.2-8 show results from the first simulation. The cost monitor output is shown in Figure 8.2-5. The energy cost of the wind system is low because the wind profile delivers high energy winds during most of the simulation. The average wind velocity in Figure 8.2-6 is about 22 mph. Figure 8.2-7 shows the wind power output supplied directly to the load. The median power output is seen to exceed 450 kw and occasionally output reaches 800 kw or rated power. Figure 8.2-8 shows the usage of battery energy to meet the load during the week, and the increase in storage capacity during the weekends. Since the battery subsystem was limited to 180 kw maximum discharge, the utility was frequently called to meet peak load. Thus about 10% of the load was satisfied by the utility.

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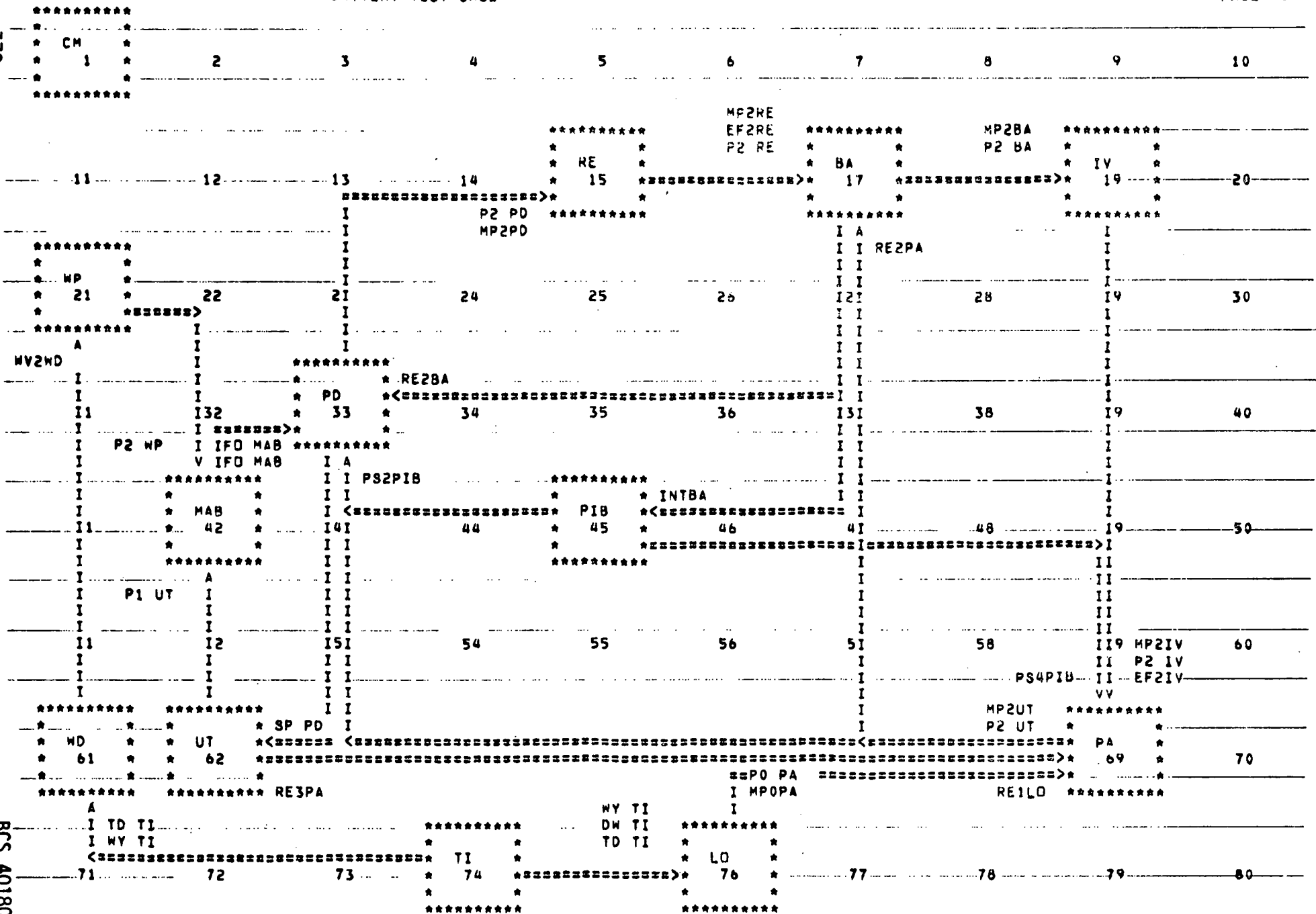


FIGURE 8.2-3 BATTERY MODEL SCHEMATIC

```

TITLE= BATTERY MODEL TEST
PARAMETER VALUES
CR CM=15.,LE CM=30.
BS UT=20.,CB UT=.016,CP UT=.03,CC UT=1000.,CM UT=1000.
C1 MAB=1.
CYCLES=4.01,TO TIME=0,V WP=400,WVOWP=8,WV1WP=60,DLINES=100.
CC WP=16000,CM WP=1200,P81PIB=2.
EC WP=.2
NC LO=.005,CT LO=4,MN LO=0,STDLO=6,VE LO=.023
RAPBA=200.,E1 BA=2000.,EDEBA=100.
VO BA=100
DT BA=10.,CC BA=2000.,CM BA=100.
RAPRE=200.,CC RE=200.,RAPIV=200.,CC IV=0.
TABLE,PW WP=10
8,10,12,14,16,18,20,21.53,25,30
25.6,50.1,86.5,137.4,205.1,292.,400.6,500.782.8,800
TABLE,PY WD=13
0.,4.33,8.67,13.,17.33,21.67,26.,30.33,34.67,39.,43.33,47.67,52.
65,67,68,65,61,56,51,49,49,52,56,61,65
TABLE,PD WD=7
0,4,8,12,16,20,24
10,12,14,16,14,12,10
TABLE,DF WD=16
0,1,2,3,4,5,6,7,8,9,10,11,12,13,14,15
5,44,160,380,480,512,440,376,307,270,148,76,40,22,9,3
TABLE,PD LO=17
0,1,5,3,4,5,6,7,5,9,10,5,12
13,5,15,16,5,18,19,5,21,22,5,24
450,360,372,330,450,660,810,798,804
690,708,699,702,750,708,570,450
TABLE,PW LO=7
1,2,3,4,5,6,7
1,1,.9,.9,.9,.6,.5
TABLE,PY LO=6
0,10,20,30,40,52
226,194,180,174,194,226
INITIAL CONDITIONS, PE BA =1990.
PRINTER PLOTS,DISPLAY1
WV2WD,VS,TIME
P1 PD,VS,TIME
P2 PD,VS,TIME
PE BA,VS,TIME
DISPLAY2
P2 IV,VS,TIME
RE2BA,VS,TIME
RE1LO,VS,TIME
TINC=.25,TMAX=336.,PRATE=8,PRINT CONTROL=3,INT MODE=3,OUTRATE=8
SIMULATE
PARAMETER VALUES,BS UT=0.,NC LO=.003
E1 BA=1000.,EDEBA=200.
CC IV=1000.
INITIAL CONDITIONS,PE BA=250.
SIMULATE

```


WIND ENERGY STORAGE COST SUMMARY

30- YEAR LIFE CYCLE

YEARLY SYSTEM COSTS

CAPITAL COST (INCLUDING FIXED CHARGES)	86400. \$
FIXED O + M COST	2300. \$
OPERATING + FUEL COST	1753. \$
TOTAL	90453. \$

• ENERGY DELIVERED

ENERGY DELIVERED 4682165. KWH

★		★
★	ENERGY COST PER KWH	19.3 MILLS ★
★		★

VALUE OF ENERGY DELIVERED	105440. \$
(VALUE OF FUEL SAVED)	

ENERGY VALUE PER KWH 22.5 MILLS

COST PER VALUE DELIVERED .86

• LOAD FACTOR

PERCENT OF LOAD SUPPLIED BY TOTAL WIND SYSTEM	90.4
--	------

PERCENT OF LOAD SUPPLIED BY UTILITY	9.6
--	-----

PERCENT OF WIND ENERGY SURPLUS	4.0
-----------------------------------	-----

COST TO MEET LOAD (WIND + UTILITY)	19.8 MILLS
---------------------------------------	------------

FIGURE 8.2-5 COST MONITOR OUTPUT FOR BATTERY MODEL

BCS 40180-2

M
V
2
H
D

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BATTERY MODEL TEST

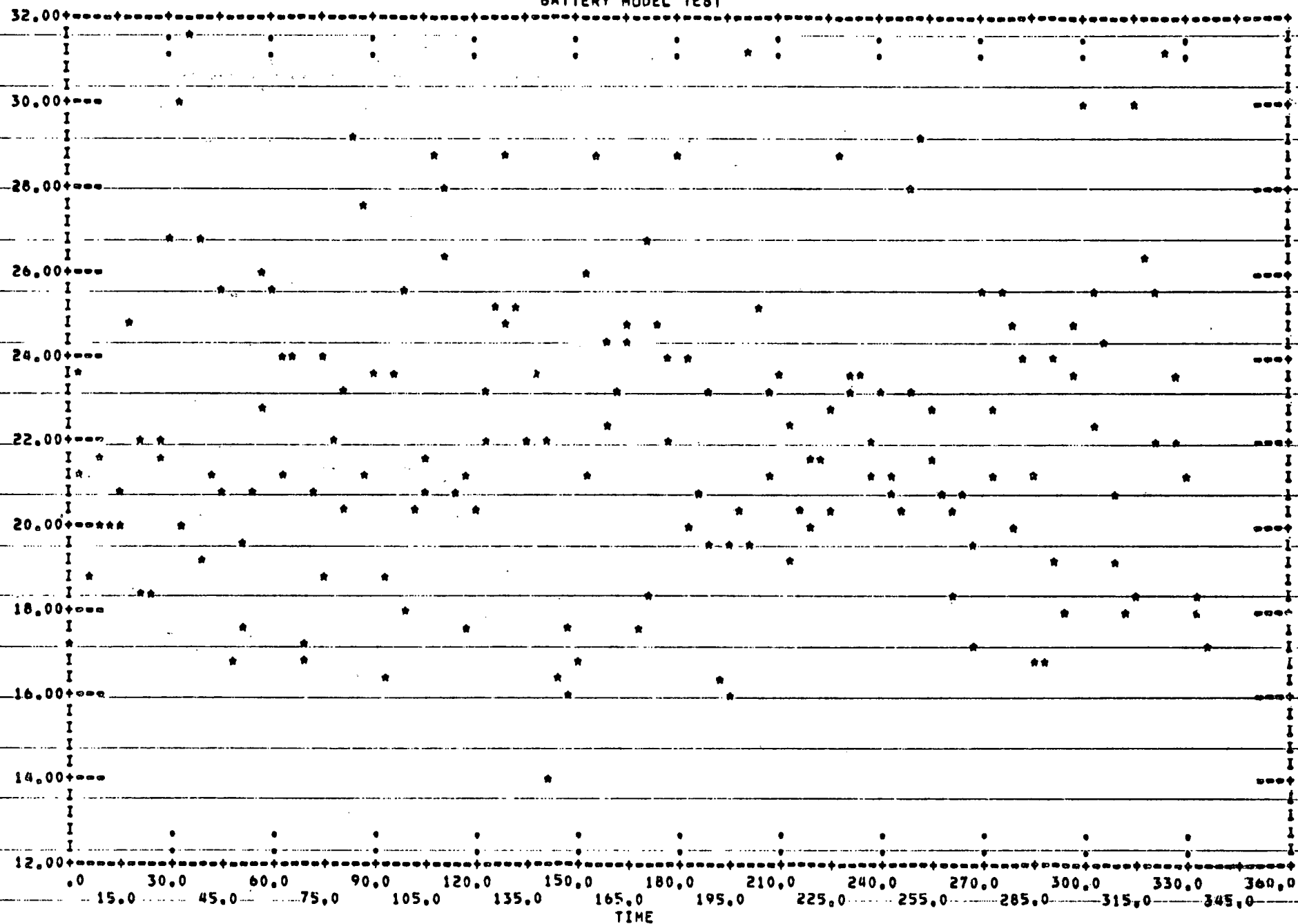


FIGURE 8.2-6 WIND PROFILE FOR BATTERY SIMULATION

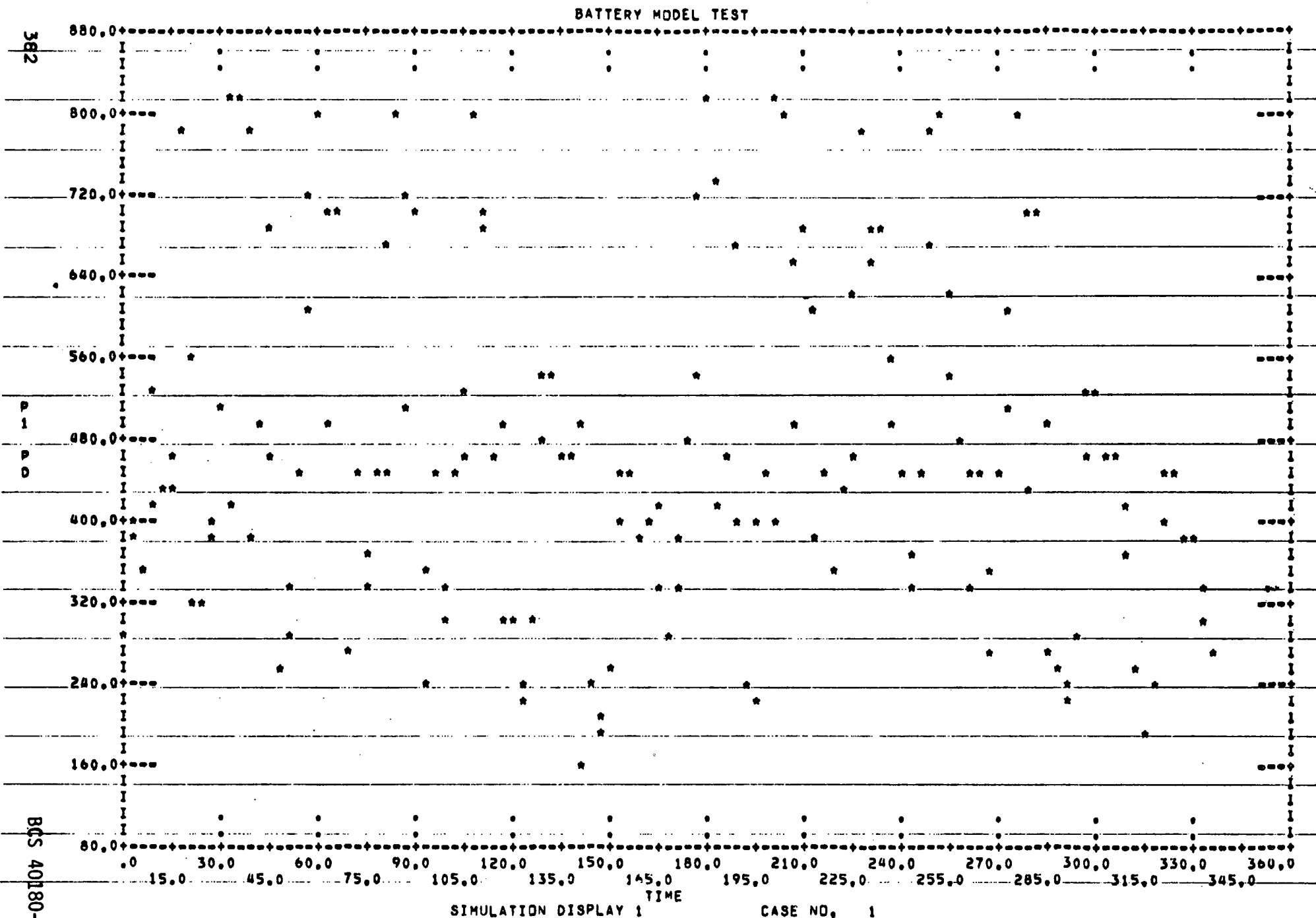


FIGURE 8.2-7 WIND POWER SUPPLIED TO LOAD

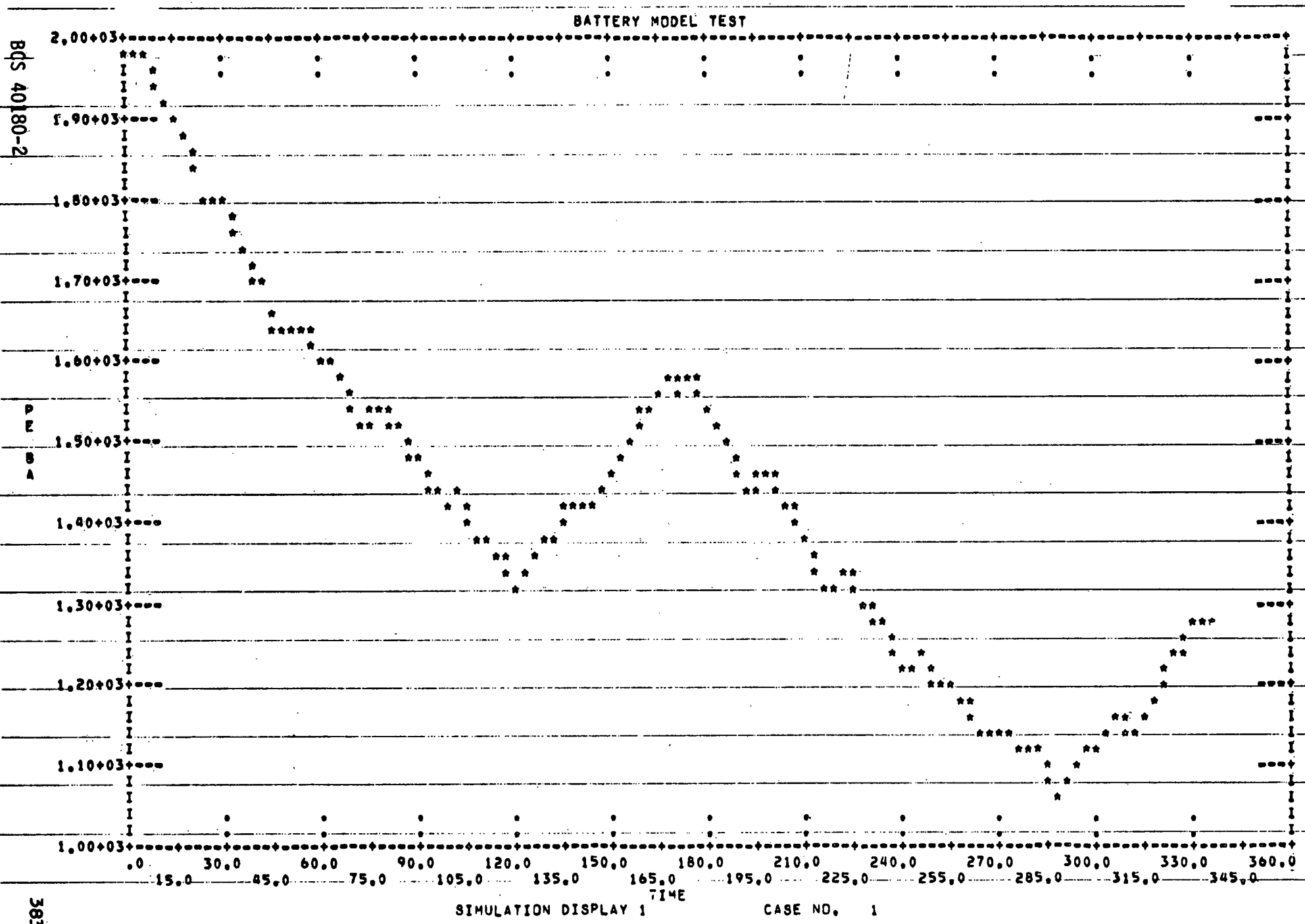


FIGURE 8.2-8 BATTERY POTENTIAL ENERGY STORAGE

8.3 FLYWHEEL STORAGE MODEL

Figure 8.3-1 shows a simplified schematic of the flywheel storage model. This model is very similar to that of 8.2 except that flywheel storage replaces battery storage, and a power line loss is included in the model. The input data for this model is shown in Figure 8.3-2. Observe that the components are defined in the order of information flow shown in 8.3-1. The admittance component AD is used to model transmission line power losses. The model schematic is shown in Figure 8.3-3.

MODEL DESCRIPTION	FLYWHEEL TEST CASE	
LOCATION=74	TI	
LOCATION=61	WD	INPUTS=TI
LOCATION=21	WP	INPUTS=WD
LOCATION=42	MAB	INPUTS=WP(P,2=FIN),UT(P,1=C2)
LOCATION=33	PD	INPUTS=MAB(FO=P,0),MAB(FO=WP),PA(1,1),PIB(2,2) FL(RE=RE,2)
LOCATION=13	MO	INPUTS=PD(2,1)
LOCATION=4	TRI	INPUTS=MO(2,1),FL(RS=RS,2)
LOCATION=6	FL	INPUTS=TRI,PA(2,1)
LOCATION=8	TRO	INPUTS=FL,GE(RS=RS,2)
LOCATION=19	GE	INPUTS=TRO
LOCATION=45	PIB	INPUTS=FL
LOCATION=69	PA	INPUTS=GE(2,2),LO(RE,1=RE,0),PIB(4,2) UT(2,3)
LOCATION=78	AD	INPUTS=PA
LOCATION=76	LO	INPUTS=TI,AD
LOCATION=62	UT	INPUTS=PD(SP=P,0)
LOCATION=1	CM	
END OF MODEL		
LIST STANDARD COMPONENTS		
PRINT		

FIGURE 8.3-2 FLYWHEEL MODEL INPUT DATA

The simulation input data shown in Figure 8.3-4 uses the same wind and load data as Example 8.2. However, the storage component is rated at 400 kw with one hour storage, simulating a system used for temporary storage and discharge during peak power generation and load demand periods. It may be noted that the transmission power loss table is input for both TRI and TRO. Figures 8.3-5 to 8.3-7 show results from the simulation. Charging power to the

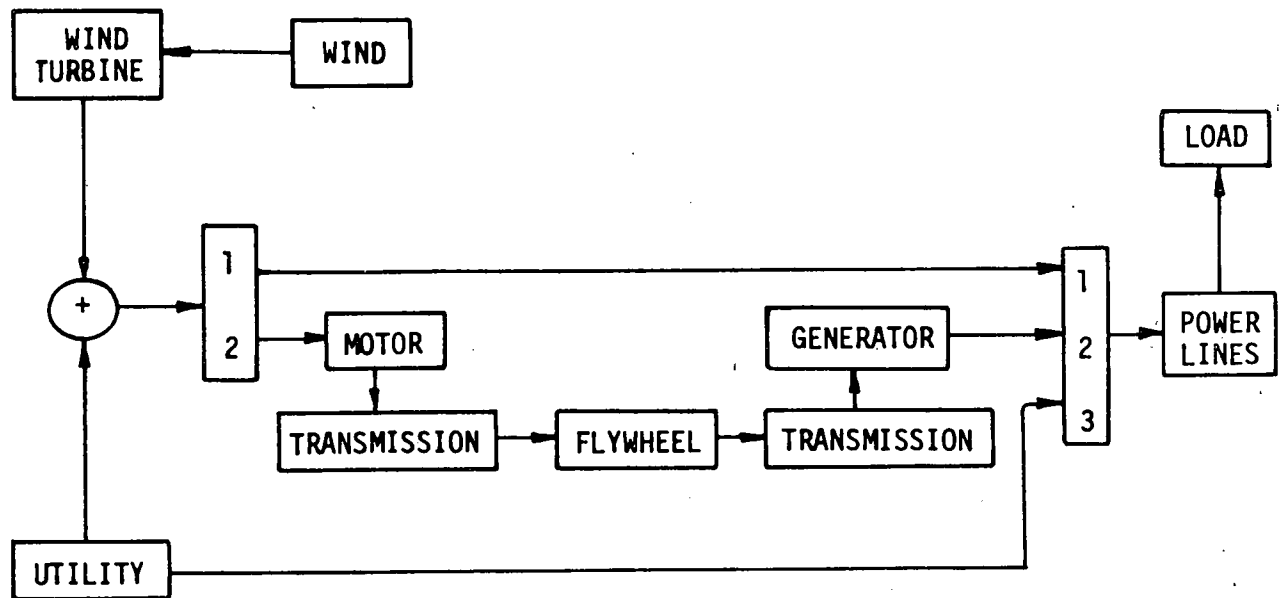


FIGURE 8.3-1: FLYWHEEL STORAGE EXAMPLE



flywheel in excess of that needed for the load is shown in Figure 8.3-5. Even with average load demand exceeding wind generation, the flywheel is charged at rated power fairly often. The kinetic energy stored by the flywheel over a two week period is shown in Figure 8.3-6. During the week energy is frequently withdrawn and storage is generally not much above the dead-band (80 kwh), whereas during the weekend the reverse is true. Output from the cost monitor is shown in Figure 8.3-7. The capital costs are probably low since nominal values were used for component costs. The utility supplied nearly 20% of the load in this case, since flywheel storage capacity is quite low.


```

TITLE= FLYWHEEL MODEL TEST
PARAMETER VALUES
VO AD=100,G1 AD=8,,G2 AD=8,,GM AD=8,,BM AD=200
SR GE=.008,C2 FL=3,E=8
PR FL=.02,MM FL=3372,RF FL=3.5,SR FL=.4,WT FL=24000,KF FL=1,3E=5
ZE FL=.1,RAPFL=400,ED FL=40,E1 FL=400,EDEF=20,CM FL=800,CC FL=300
RS MD=1750,RAPMD=1000,MPIMD=1,E8,CC MD=500,CM MD=0.
RS1TRI=1750,CC TRI=500,CM TRI=0,CC TRD=500,CM TRD=0.
RAPGE=1000,CC GE=1000,CM GE=100.
CR CM=15.,LE CM=30.
BS UT=20.,CB UT=.016,CP UT=.03,CC UT=1000.,CM UT=1000.
C1 MAB=1.
CYCLES=4.01,T0 T1=0,V WP=400,WVOWP=8,WV1WP=60,DLINES=100.
CC WP=16000,CM WP=1200,PS1PIB=2.
EC WP=.2
NC LO=.005,CT LO=4,MN LO=0,STDLO=6,VE LO=.023
TABLE,PLOTRI=5,4
0.5,1,1.5,1.72
0.400,900,1100,1300
0.16,18,18.5,20
0.10,11,11.5,12
0.10,10,10.5,11
0.6,6.5,7,10
TABLE,PLOTRO=5,4
.5,1,1.5,1.72
0.400,900,1100,1300
0.16,18,18.5,20
0.10,11,11.5,12
0.10,10,10.5,11
0.6,6.5,7,10
TABLE,CLOFL=3,3
-1000, 0, 1000
2000,4000,7000
2.8, 7.4, 15
.9, 2.5, 5
2.6, 7.2, 15
TABLE,CL1FL=3
2000,4000,7000
.8, 2.4, 4
TABLE,PW WP=10
8,10,12,14,16,18,20,21.53,25,30
25,5,50,1,86,5,137.4,205.1,292.,400,6,500,782,8,800
TABLE,PY MD=13
0.,4.33,8.67,13.,17.33,21.67,26.,30,33,34,67,39.,43,33,47,67,52.
65,67,68,65,61,56,51,49,49,52,56,61,65
TABLE,PD MD=7
0,4,8,12,16,20,24
10,12,14,16,14,12,10
TABLE,DF MD=16
0,1,2,3,4,5,6,7,8,9,10,11,12,13,14,15
5,44,160,380,480,512,440,376,307,270,148,76,40,22,9,3
TABLE,PD LO=17
0,1,5,3,4,5,6,7,5,9,10,5,12
13.5,15,16.5,18,19.5,21,22.5,24
450,360,372,330,450,660,810,798,804
690,708,699,702,750,708,570,450
TABLE,PW LO=7
1,2,3,4,5,6,7
1,1.,9.,9.,9.,6.,5
TABLE,PY LO=6
0,10,20,30,40,52
226,194,180,174,194,226
INITIAL CONDITIONS, KE FL=300.
PRINTER PLOTS,DISPLAY1
WV2WD,VS,TIME
P1 PD,VS,TIME
P2 PD,VS,TIME
KE FL,VS,TIME
DISPLAY2
P2 GE,VS,TIME
RE2FL,VS,TIME
RE1LO,VS,TIME
TINC=.25,THAX=336.,PRATE=8,PRINT CONTROL=3,INT MODE=3,OUTRATE=8
SIMULATE

```

FIGURE 8.3-4 FLYWHEEL SIMULATION DATA

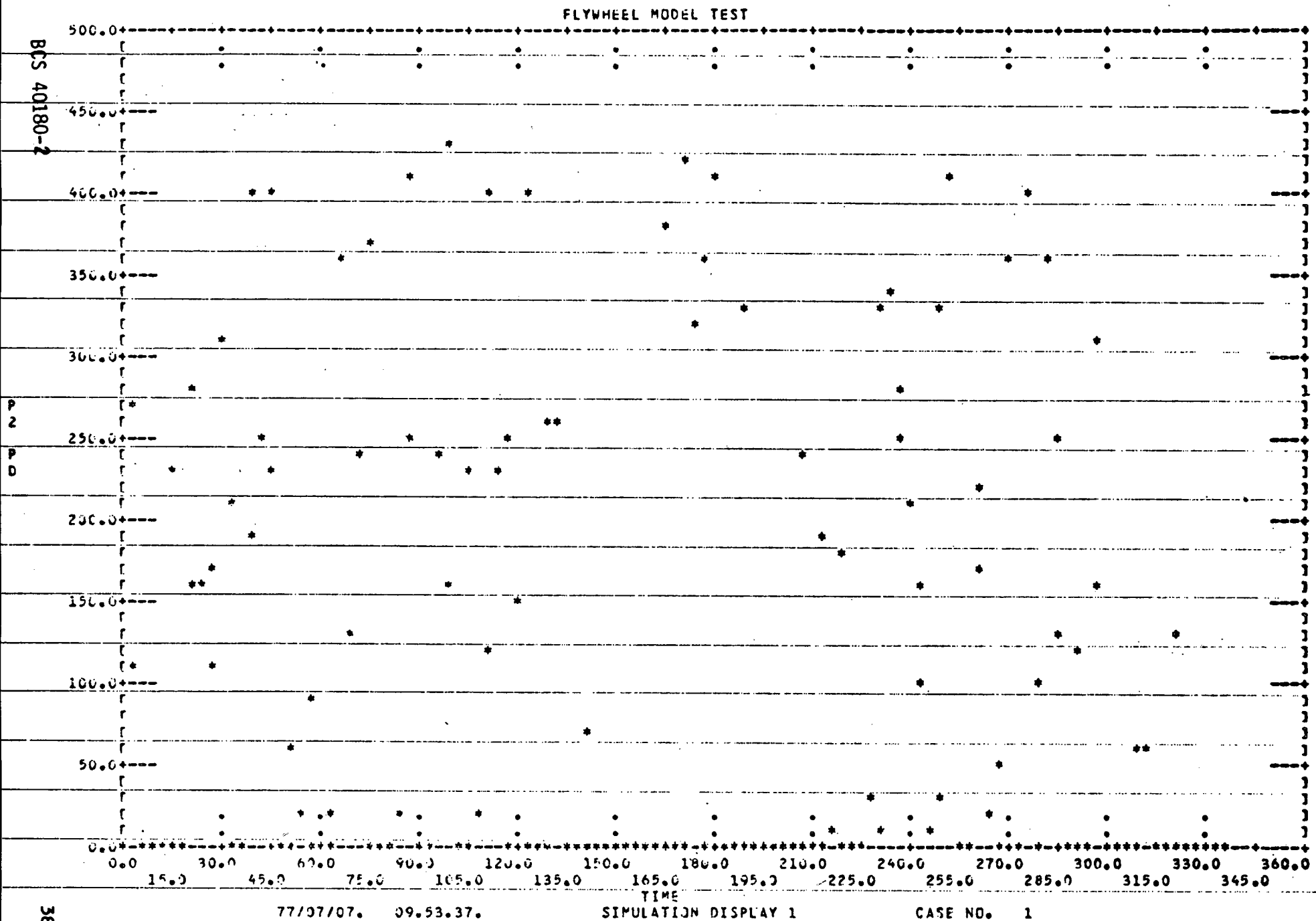


FIGURE 8.3-5 WIND POWER SUPPLIED TO FLYWHEEL STORAGE

FLYWHEEL MODEL TEST

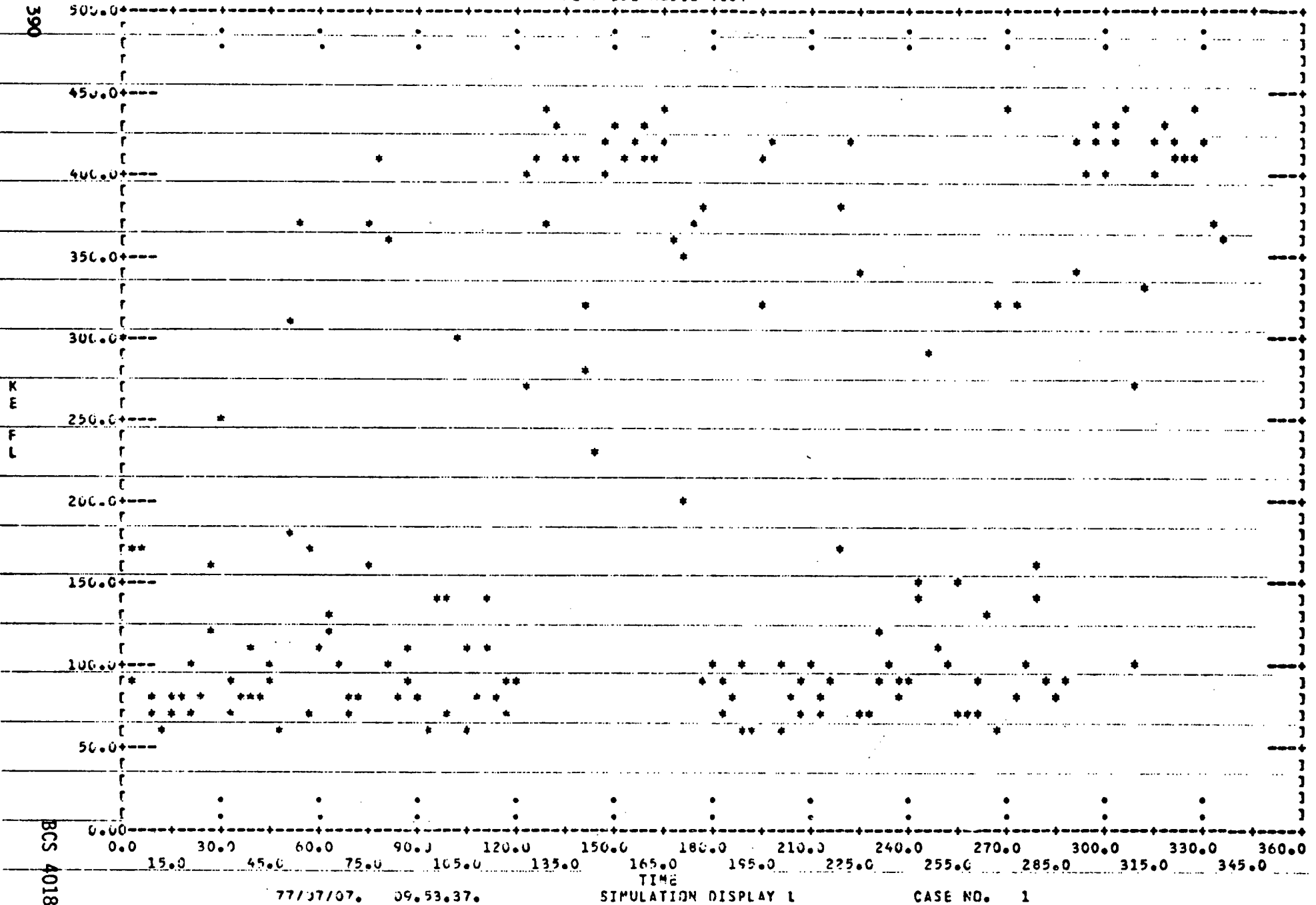


FIGURE 8.3-6 FLYWHEEL KINETIC ENERGY STORAGE

WIND ENERGY STORAGE COST SUMMARY

30 YEAR LIFE CYCLE

YEARLY SYSTEM COSTS

CAPITAL COST (INCLUDING FIXED CHARGES)	89104. \$
FIXED O + M COST	3100. \$
OPERATING + FUEL COST	1753. \$
TOTAL	93957. \$

ENERGY DELIVERED

ENERGY DELIVERED	4440974. KWH
------------------	--------------

↓	↓
ENERGY COST PER KWH	21.2 MILLS
↑	↑

VALUE OF ENERGY DELIVERED (VALUE OF FUEL SAVED)	95217 \$
--	----------

ENERGY VALUE PER KWH	21.4 MILLS
COST PER VALUE DELIVERED	.99

LOAD FACTOR

PERCENT OF LOAD SUPPLIED BY TOTAL WIND SYSTEM	61.3
--	------

PERCENT OF LOAD SUPPLIED BY UTILITY	18.7
--	------

PERCENT OF WIND ENERGY SUPPLUSED	8.3
-------------------------------------	-----

COST TO MEET LOAD (WIND + UTILITY)	22.3 MILLS
---------------------------------------	------------

FIGURE 8.3-7 FLYWHEEL MODEL COST MONITOR OUTPUT

8.4 HYDRO AND THERMAL STORAGE MODEL

Figure 8.4-1 shows the basic model schematic for a model with both thermal and electrical loads. Wind power is supplied first to meet the electrical load, with excess power going into hydro and thermal storage. The thermal load is driven by an ambient temperature component and electrical load energy value is supplied by a time dependent look-up table. Figure 8.4-2 shows the model input data. The components are ordered according to the flow of information in 8.4-1. Observe that the maximum power input of the power divider is connected up to the wind power output P. The model schematic is shown in Figure 8.4-3.

LIST STANDARD COMPONENTS

MODEL DESCRIPTION	HYDRO AND THERMAL TEST CASE
LOCATION=77	TI
LOCATION=51	WD INPUTS=TI
LOCATION=21	WP INPUTS=WD
LOCATION=33	PD INPUTS=WP, WP(P=MP), PA(1,1), PIH(2,2), HS(RE=RE, 2) INPUTS=TS(2,3), PIT(2,3)
LOCATION=13	MO INPUTS=PD(2,1)
LOCATION=15	PU INPUTS=MO
LOCATION=17	HS INPUTS=PU, PA(RE, 2=RE)
LOCATION=45	PIH INPUTS=HS
LOCATION=19	HT INPUTS=HS
LOCATION=40	GE INPUTS=HT
LOCATION=59	PA INPUTS=GE(2,2), LO(1,0), PIH(4,2)
LOCATION=78	FU INPUTS=TI(TD=FIN)
LOCATION=80	LO INPUTS=TI, FU(F0=VE)
LOCATION=63	TS INPUTS=TL
LOCATION=52	PIT INPUTS=TS
LOCATION=67	TP INPUTS=TI
LOCATION=65	TI INPUTS=TI, TP
LOCATION= 1	CM
END OF MODEL	
PRINT	

FIGURE 8.4-2 HYDRO AND THERMAL MODEL INPUT DATA

The input data for a two week simulation with this model is shown in Figure 8.4-4. CYCLES is equal to 6 in this model for sufficient iterations to attain steady state in the hydro storage subsystem. The hydro system has

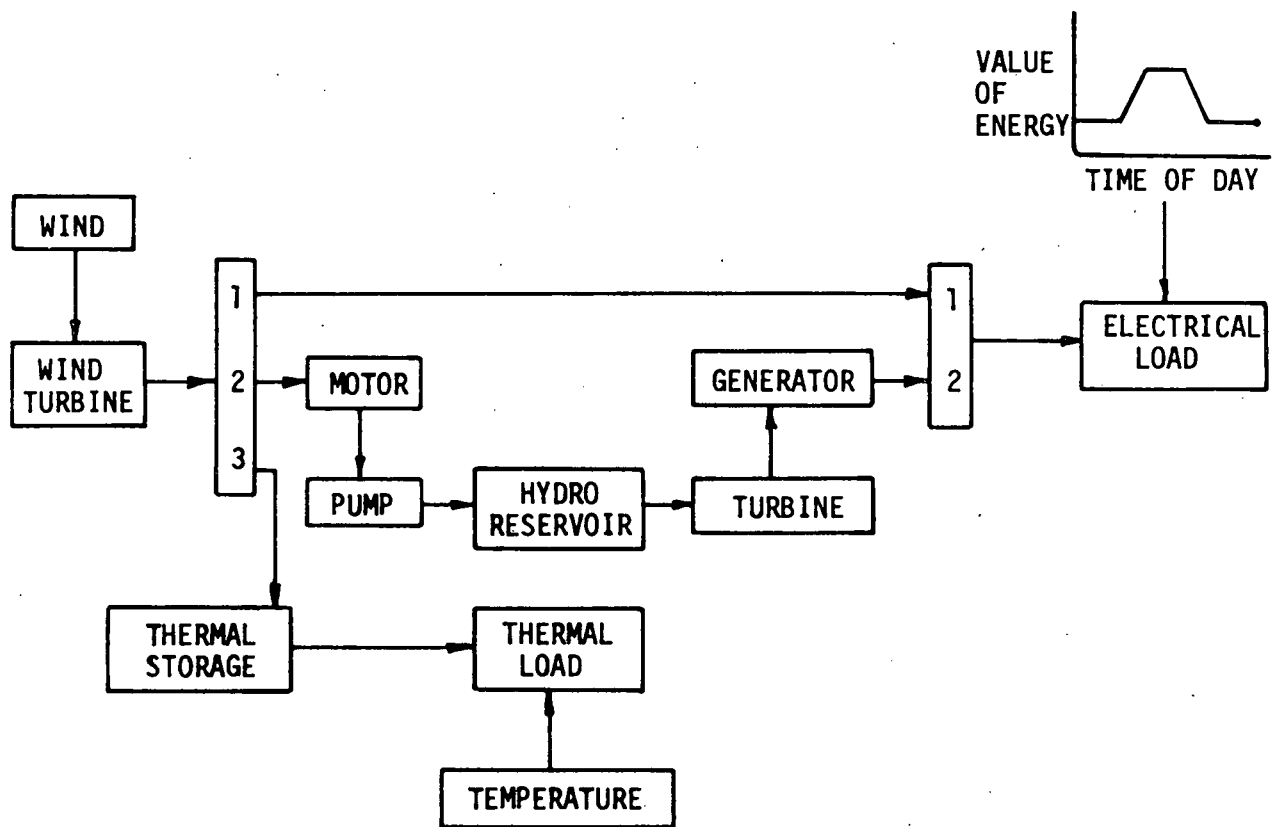
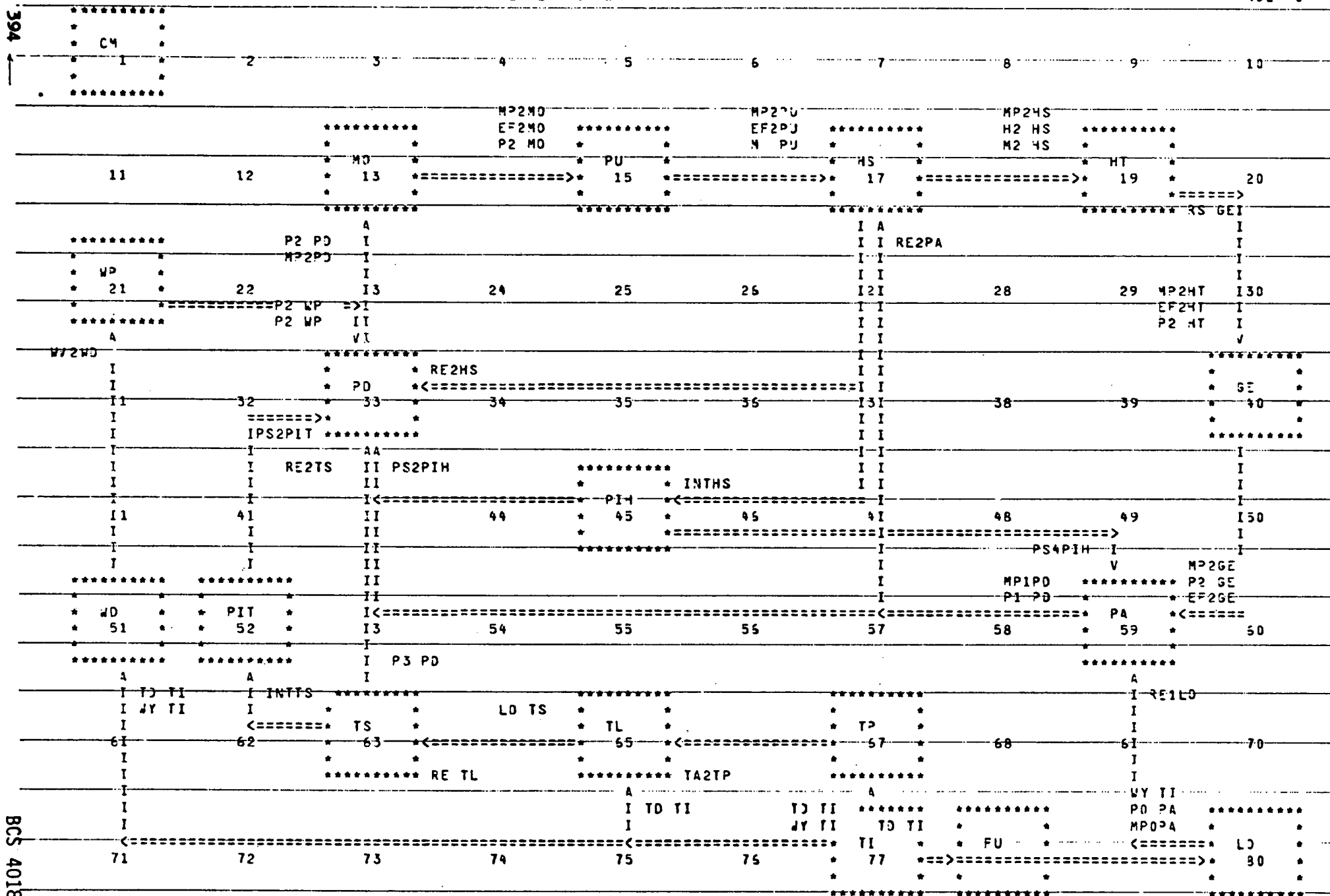


FIGURE 8.4-1: HYDRO AND THERMAL STORAGE EXAMPLE

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PARAMETER VALUES

```

CYCLES=5.01,T0 TI=0,V WP=400,WVOWP=8,WVTP=60,CLINES=100.
CC WP=15000,CM WP=1200,PS1PIH=2.,EC WP=.2,CR CM=15,LE CM=30
41 PU=200,AS HS=3600,MDRHS=80,40 HS=80000,CM HS=1000
41 HS=200,40 HS=400000,LE HS=30,F2 PD=.5,F3 PD=.5
RA GE=200,RSYSE=3600,SR GE=.0333,CC GE=1000,CM GE=120
VC LO=.004,CT LO=4,MN LO=0,STLO=5,AN FU=-1.
PS1PIT=2.,TS=TS=10,V0 TS=110,PD TS=100,LE TS=30,4FMTS=10000.
J4 TS=.01465,TDTS=2,RS MO=1750,RAPO=200,CC MO=500,CM MO=100
VE TL=.023,VC TL=40.,CT TP=12,MN TP=0,STOTP=5.
TABLE,PW WJ=10
3,10,12,14,15,19,20,21.53,25,30
25.6,50.1,85.5,137.4,205.1,292.,400.6,500,782.8,900
TABLE,PY WJ=15
3.,4.33,8.57,13.,17.33,21.67,26.,30.33,34.67,39.,43.33,47.67,52.
53,67,63,53,51,55,51,49,49,52,55,61,65
TABLE,PD WJ=7
3,4,8,12,15,20,24
10,12,14,15,19,12,10
TABLE,DP WJ=15
0,1,2,3,4,5,6,7,8,9,10,11,12,13,14,15
5,14,160,390,480,512,440,376,307,270,148,76,40,22,9,3
TABLE,MT TS=4
.00873,.025131,.047371,.064072
30,147,147,204
TABLE,PD LO=17
0,1.5,3,4.5,5,6,7.5,9,10.5,12
13.5,15,15.5,18,19.5,21,22.5,24
53,360,372,330,450,560,810,798,904
53,709,699,702,750,708,570,430
TABLE,PW LO=7
1,2,3,4,5,6,7
1,1,.9,.9,.9,.6,.5
TABLE,PY LO=5
3,10,20,30,40,52
25,124,180,174,194,226
TABLE, FTA FU = 5
0,5,10,18,22,24
.019,.019,.028,.028,.019,.019
TABLE,TLDTL=4
0,52,50,100
4.,2.,1.5,1.
TABLE,TWTL=4
0,5,18,24
.4,1.,1.,.4
TABLE,PD TP=9
3,5,6,9,12,15,18,21,24
45,45,43,55,52,54,56,48,46
TABLE,PY TP=5
0,13,25,39,52
40,50,75,65,40
INITIAL CONDITIONS, MA HS=1600000,E TS=600
ENTER PLOTTS,DISPLAY1
JW2WD,VS,TIME
P1 PD,VS,TIME
M PU,VS,TIME
DISPLAY2
E HS,VS,TIME

42 HS,VS,TIME
E2HS,VS,TIME
DISPLAY3
PC LO,VS,TIME
P3 PD,VS,TIME
E TS,VS,TIME
E1LO,VS,TIME
DISPLAY4
LO TS,VS,TIME
PC TL,VS,TIME
T42TP,VS,TIME
F3 FU,VS,TD TI
FIVC=.50,TYAK=336.,PRATE=6,PRINT CONTROL=3,INT MODE=3,OUTRATE=4
TITLE = HYDRO AND THERMAL TEST
SIMULATE

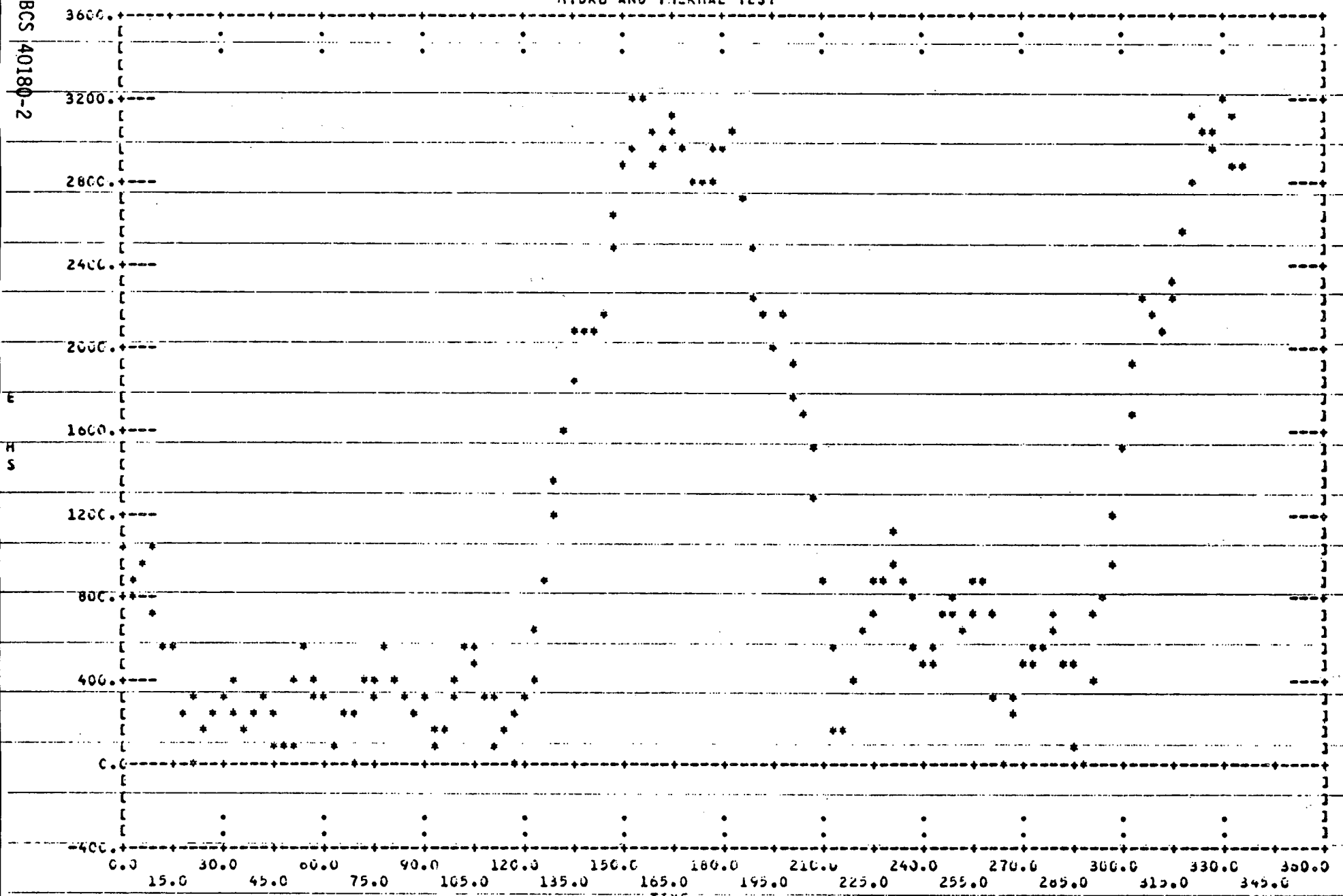
```

FIGURE 8.4-4 HYDRO AND THERMAL SIMULATION DATA

much larger capacity and supplies a bigger load than the thermal system in this run. Figures 8.4-5 to 8.4-9 show results of the simulation. Hydro energy storage is shown in 8.4-5. During the week most of the wind energy goes directly to the load except at night. The reservoir builds up to capacity during the week-ends. The cumulative percent load delivered by wind and hydro storage is shown in 8.4-6, and averages about 91%. Similarly, thermal energy stored and percent thermal load delivered are shown in 8.4-7 and 8.4-8. The ambient temperature profile for a similar, one week simulation is shown in 8.4.9.

BCS 40180-2

HYDRO AND THERMAL TEST



77/06/10. 12.22.50.

SIMULATION DISPLAY 2

CASE NO. 1

FIGURE 8.4-5 HYDRO RESERVOIR ENERGY STORAGE

HYDRO AND THERMAL TEST

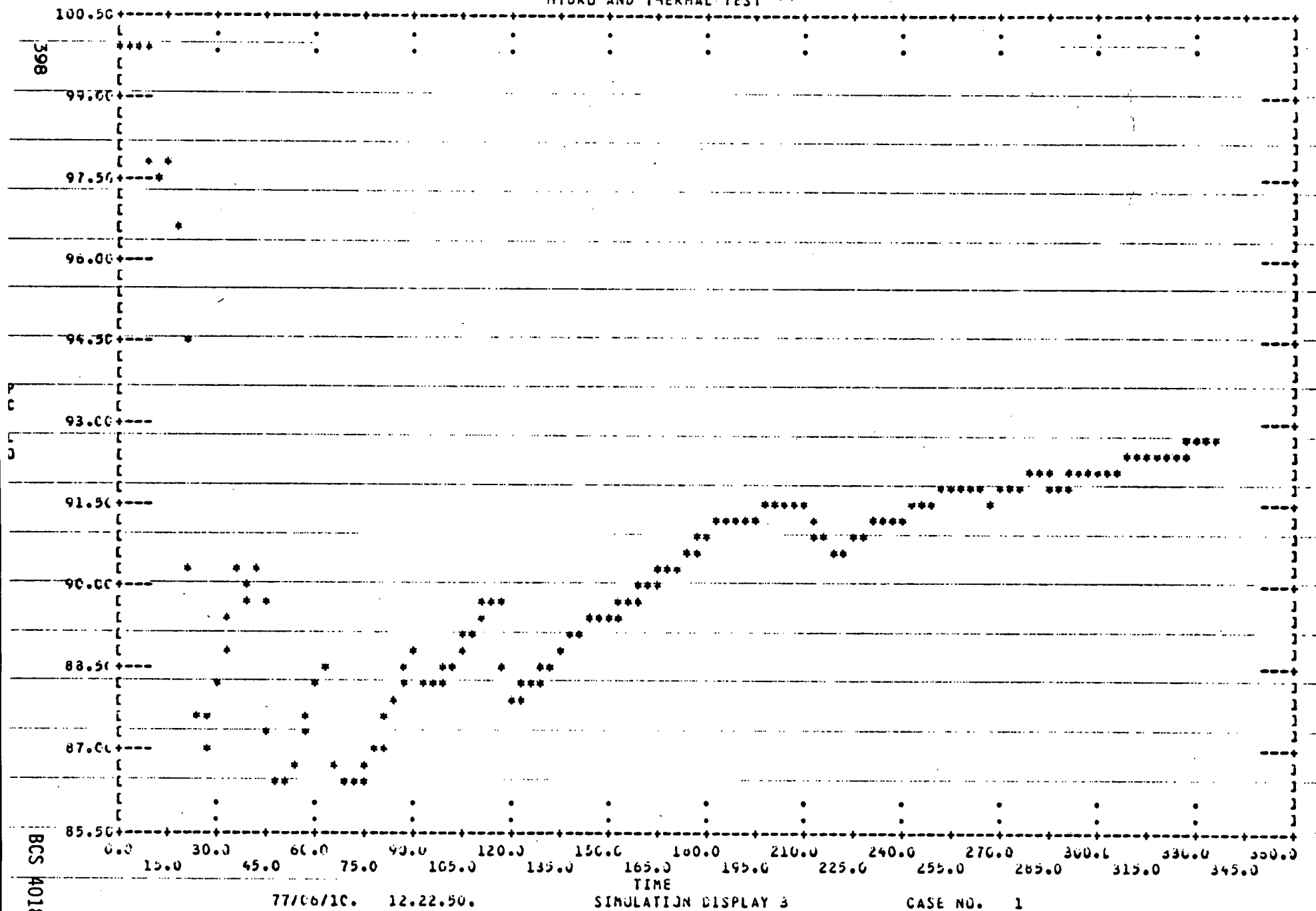
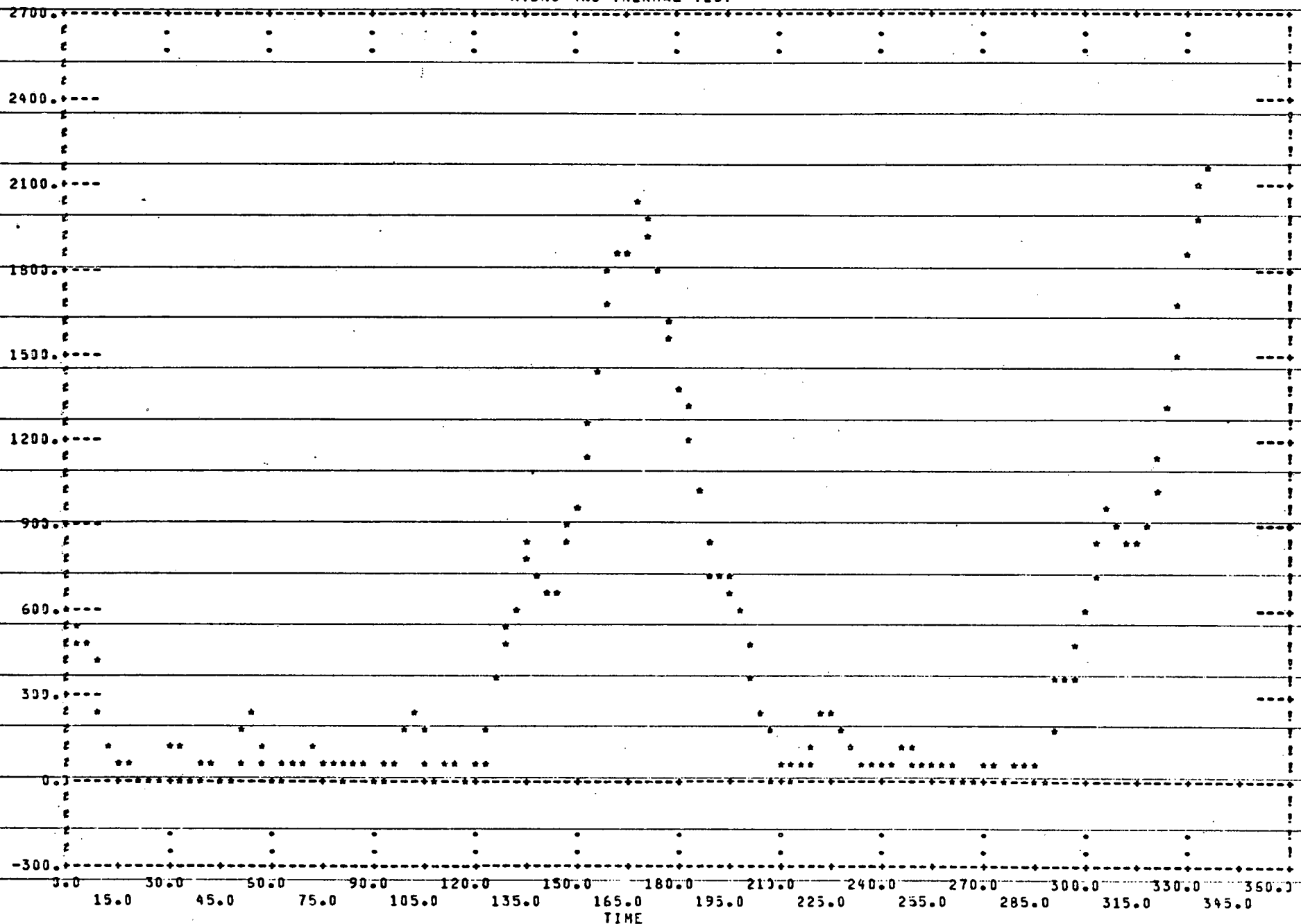


FIGURE 8.4-6 PERCENT CUMULATIVE LOAD DELIVERED

HYDRO AND THERMAL TEST

BCS 40180-2



77/08/04. 11:00:57.

SIMULATION DISPLAY 5

CASE NO. 1

399

FIGURE 8.4-7 THERMAL ENERGY STORAGE

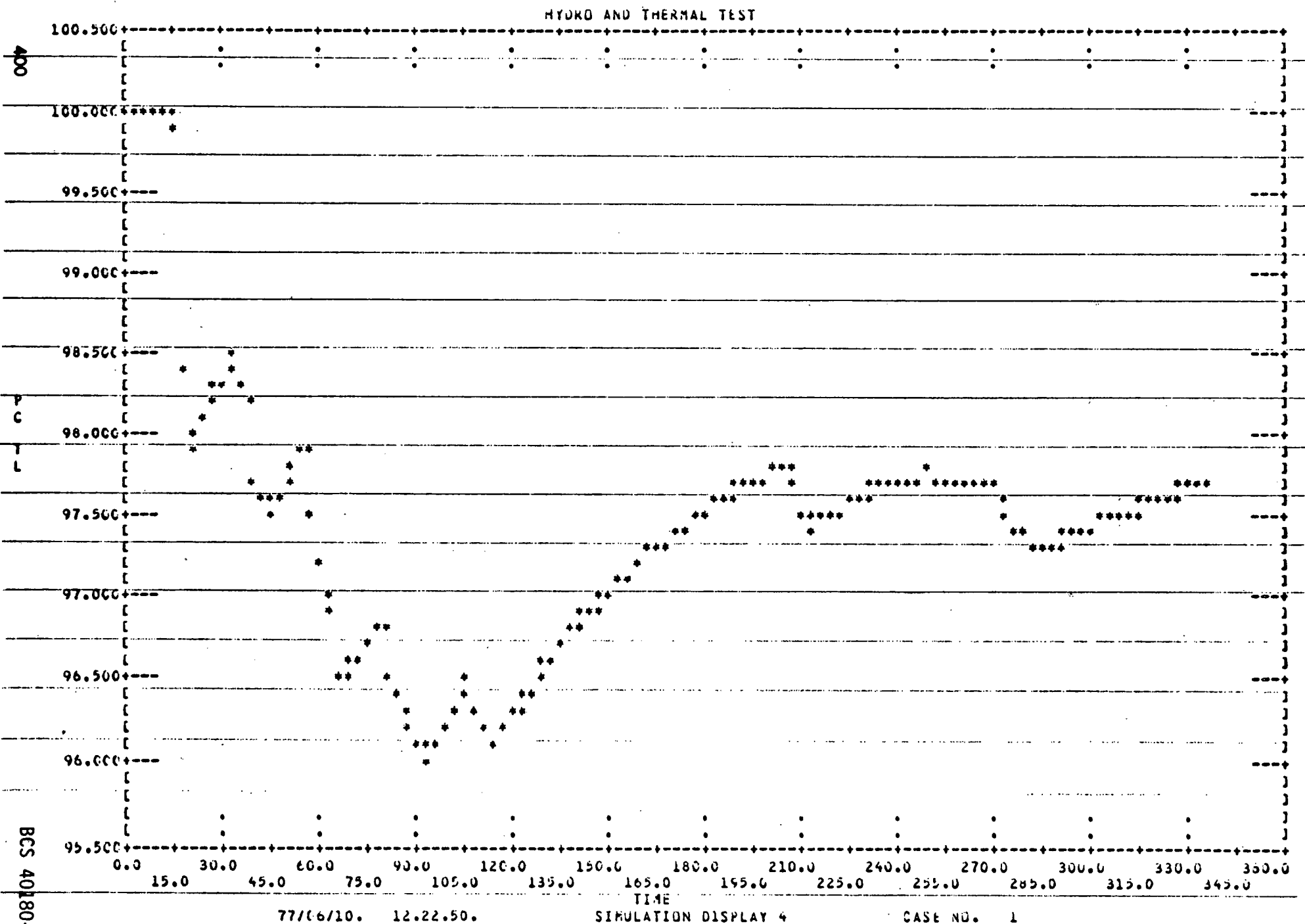


FIGURE 8.4-8 PERCENT CUMULATIVE THERMAL LOAD DELIVERED

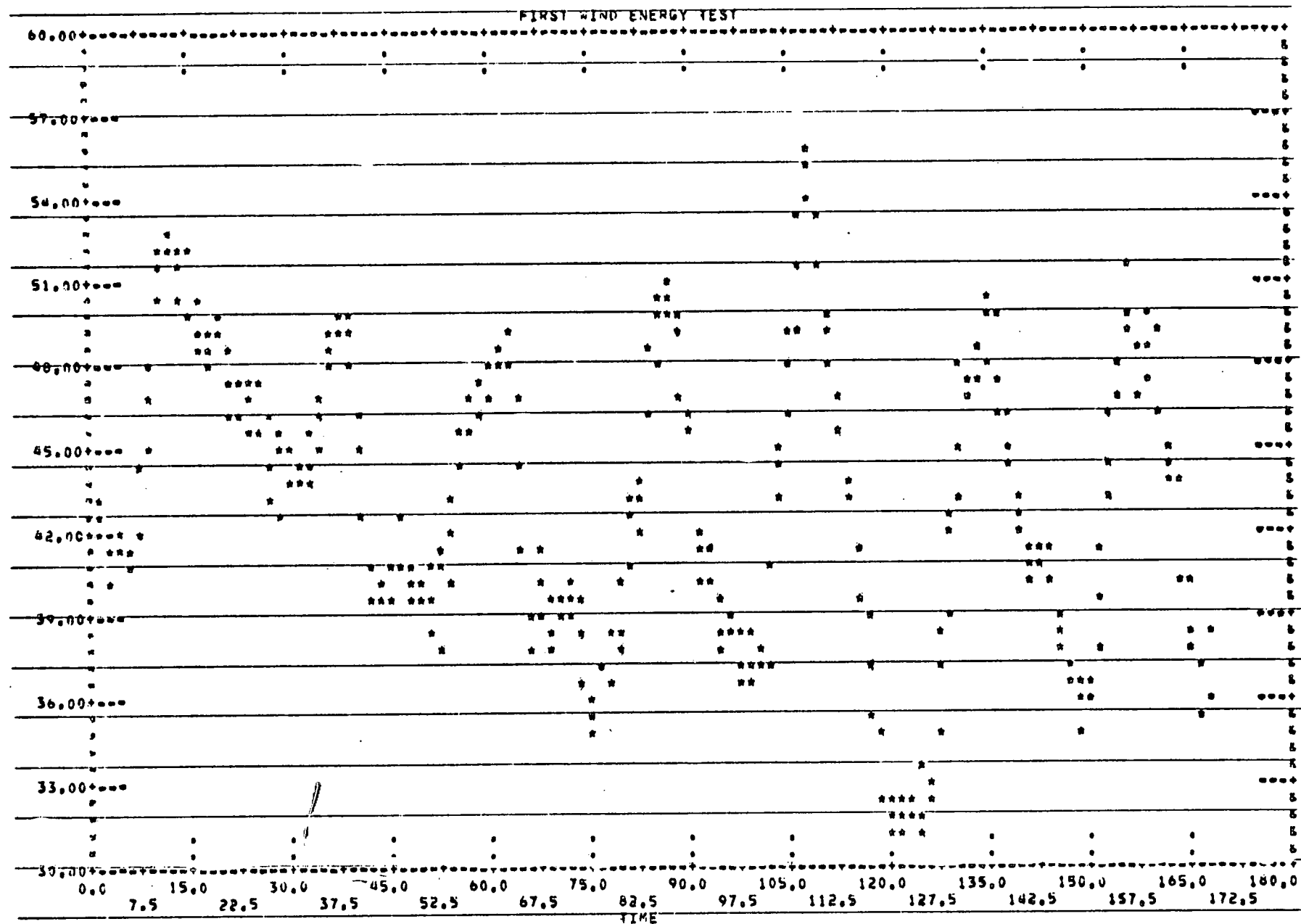


FIGURE 8.4-9 AMBIENT TEMPERATURE SIMULATION OVER ONE WEEK

8.5 PNEUMATIC STORAGE MODEL

Figure 8.5-1 shows the simplified schematic for the pneumatic storage model. For simplicity the motor and generator have been omitted from the pneumatic storage subsystem. A burner is used if needed to heat the exiting air to the turbine. The heat exchanger has a phase change medium. Figure 8.5-2 shows the input data for this model.

MODEL DESCRIPTION		PNEUMATIC STORAGE TEST CASE
LOCATION= 1	TI	
LOCATION=21	WD	INPUTS=TI
LOCATION=51	WP	INPUTS=WD
LOCATION= 5	TP	INPUTS=TI
LOCATION=43	PD	INPUTS=WP, WP (P=WP), PA(1,1), PI(2,2), CS(RE=RE,2)
LOCATION=64	UT	INPUTS=PD(SP=P)
LOCATION=15	CO	INPUTS=PD(2,1), TP
LOCATION=17	HX	INPUTS=CO, TP, CS
LOCATION=47	CS	INPUTS=HX, PA(RE,2=RE)
LOCATION=36	PI	INPUTS=CS
LOCATION=49	HY	INPUTS=CS, HX
LOCATION=59	BN	INPUTS=HY
LOCATION=80	TU	INPUTS=BN, TP, CS(PR=PS)
LOCATION=76	PA	INPUTS=TU(2,2), LO(1,0), PI(4,2), UT(2,3)
LOCATION=72	LO	INPUTS=TI
LOCATION=71	CM	
END OF MODEL		
LIST STANDARD COMPONENTS		
PRINT		

FIGURE 8.5-2 PNEUMATIC STORAGE MODEL INPUT DATA

The input data for a two week simulation is shown in 8.5-3. In order to keep the air entering the storage cavern from overheating, a fairly large leakage coefficient ($NU = 0.01$) is assumed. Hence the storage cavern loses about 2/3 of its heat energy every four days. The load constant NC LO can be adjusted to balance wind energy to the load so that weekly air mass flow in and out of the cavern is balanced. The initial values for the CS and HX states were chosen on the basis of an earlier one week simulation. Figures 8.5-4 to 8.5-8 show results of this simulation. Figure 8.5-4 shows the average temperature of the heat exchanger storage medium for the 'cool' cell. The initial

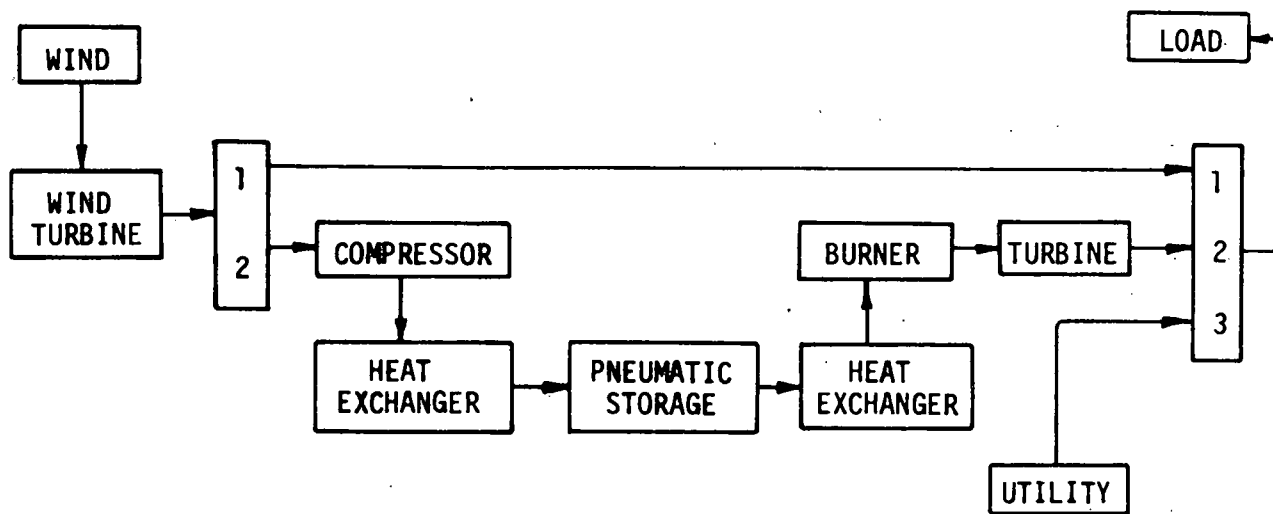


FIGURE 8.5-1: PNEUMATIC STORAGE EXAMPLE


```

TITLE= PNEUMATIC STORAGE TEST CASE2
PARAMETER VALUES
CYCLES=4.01,TO TI=0,CT TP=12,MN TP=0,STDTP=5,DLINES=100
V WP=400,WVOWP=8,WV1WP=60,CC WP=16000,CM WP=1200,PS1PI=2.,EC WP=.2
LE CS=30,MDECS=10000,TEMCS=350,NU CS=.010,TM CS=125,BE HX=.001
MD CM=1500,I3 BN=600,LE BN=30,MDBN=3000
ST HX=24,LE HX=30,PD HX=150,TMTHX=250,TEMHX=350,L HX=8
MD CS=1500,TIDTU=600,RS TU=3600,CR CM=15,LE CM=30,CM CS=400
NC LO=.0043,CT LO=4,MN LO=0,STDLO=6,VE LO=.023
CB UT=.019,MP1UT=1.E8,CP UT=.023,CC UT=0,CM UT=0
TABLE,PW WP=10
8.10.12.14.16.18.20.21.23.24.30
25.6,50.1,86.5,137.4,205.1,292.,400.6,500.,880.,880.
TABLE,PY WD=13
0.,4.33,8.67,13.,17.33,21.67,26.,30.33,34.67,39.,43.33,47.67,52.
65.67,68.65,61.56,51.49,49.52,56.61,65
TABLE,PD WD=7
0,4,8,12,16,20,24
10,12,14,16,14,12,10
TABLE,DF WD=16
0,1,2,3,4,5,6,7,8,9,10,11,12,13,14,15
5,44,160,380,480,512,440,376,307,270,148,76,40,22,9,3
TABLE,PD TP=9
0,3,6,9,12,15,18,21,24
46,45,48,55,62,62,56,48,46
TABLE,PY TP=5
0,13,26,39,52
40,50,75,65,40
TABLE,PD LO=17
0,1,5,3,4,5,6,7,5,9,10,5,12
13,5,15,16,5,18,19,5,21,22,5,24
450,360,372,330,450,660,810,798,804
690,708,699,702,750,708,570,450
TABLE,PW LO=7
1,2,3,4,5,6,7
1,1,.9,.9,.9,.6,.6
TABLE,PY LO=6
0,10,20,30,40,52
226,194,180,174,194,226
INITIAL CONDITIONS,E CS=1250,MS CS=5.E5,EC1HX=1300,EC2HX=800
PRINTER PLOTS,DISPLAY1
M CO,VS,TIME
T2 CO,VS,TIME
T2 HX,VS,TIME
TS1HX,VS,TIME
P2 UT,VS,TIME
DISPLAY2
E CS,VS,TIME
MS CS,VS,TIME
T2 CS,VS,TIME
M2 HY,VS,TIME
T HY,VS,TIME
DISPLAY3,P2 TU,VS,TIME,TS2HX,VS,TIME
TINC=.5,TMAX=336.,PRATE=6,PRINT CONTROL=3,INT MODE=3,OUTRATE=4
SIMULATE

```

FIGURE 8.5-3 PNEUMATIC STORAGE SIMULATION DATA

PNEUMATIC STORAGE TEST CASE2

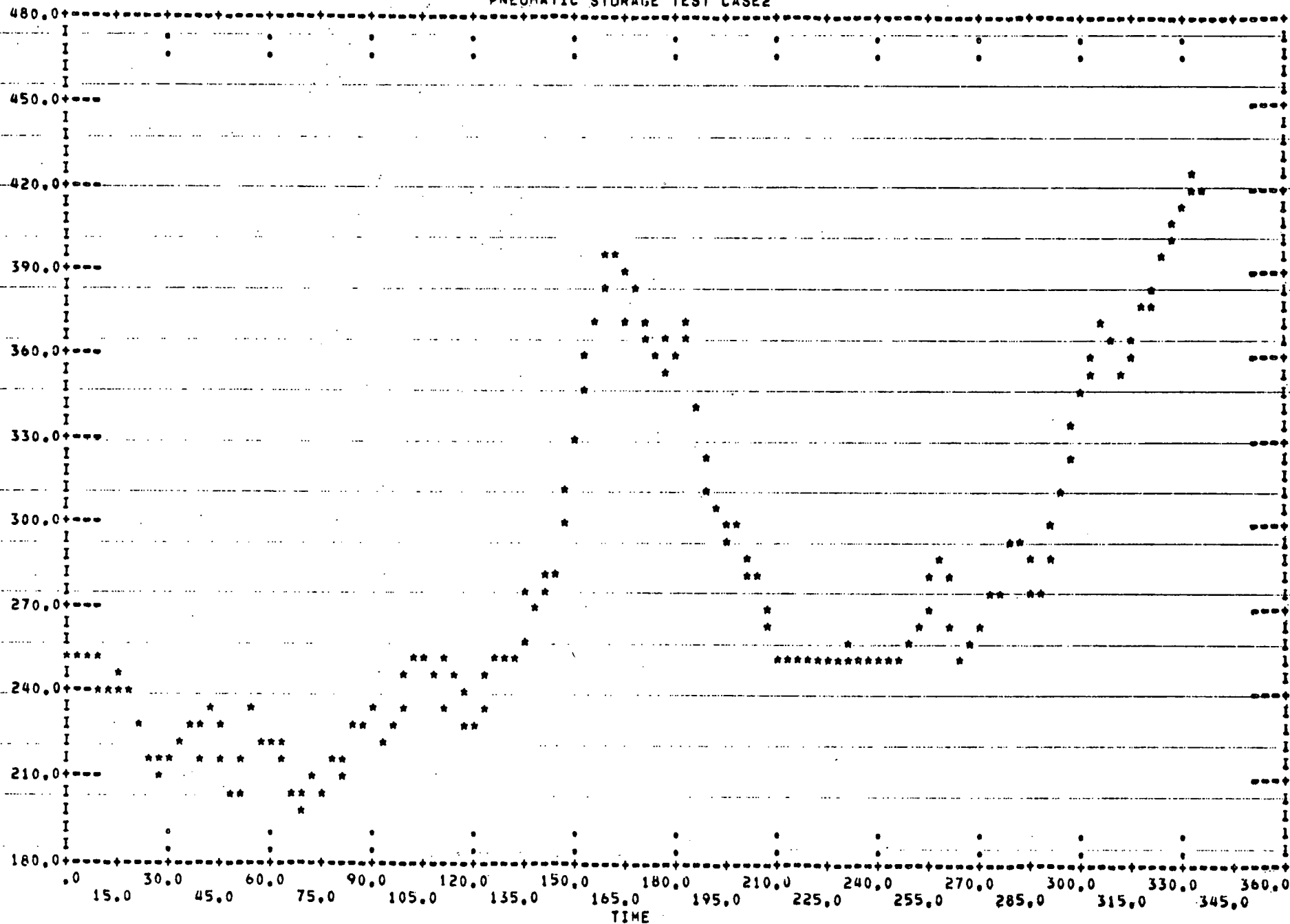


FIGURE 8.5-4 AVERAGE TEMPERATURE IN HEAT EXCHANGER CELL 2

PNEUMATIC STORAGE TEST CASE2

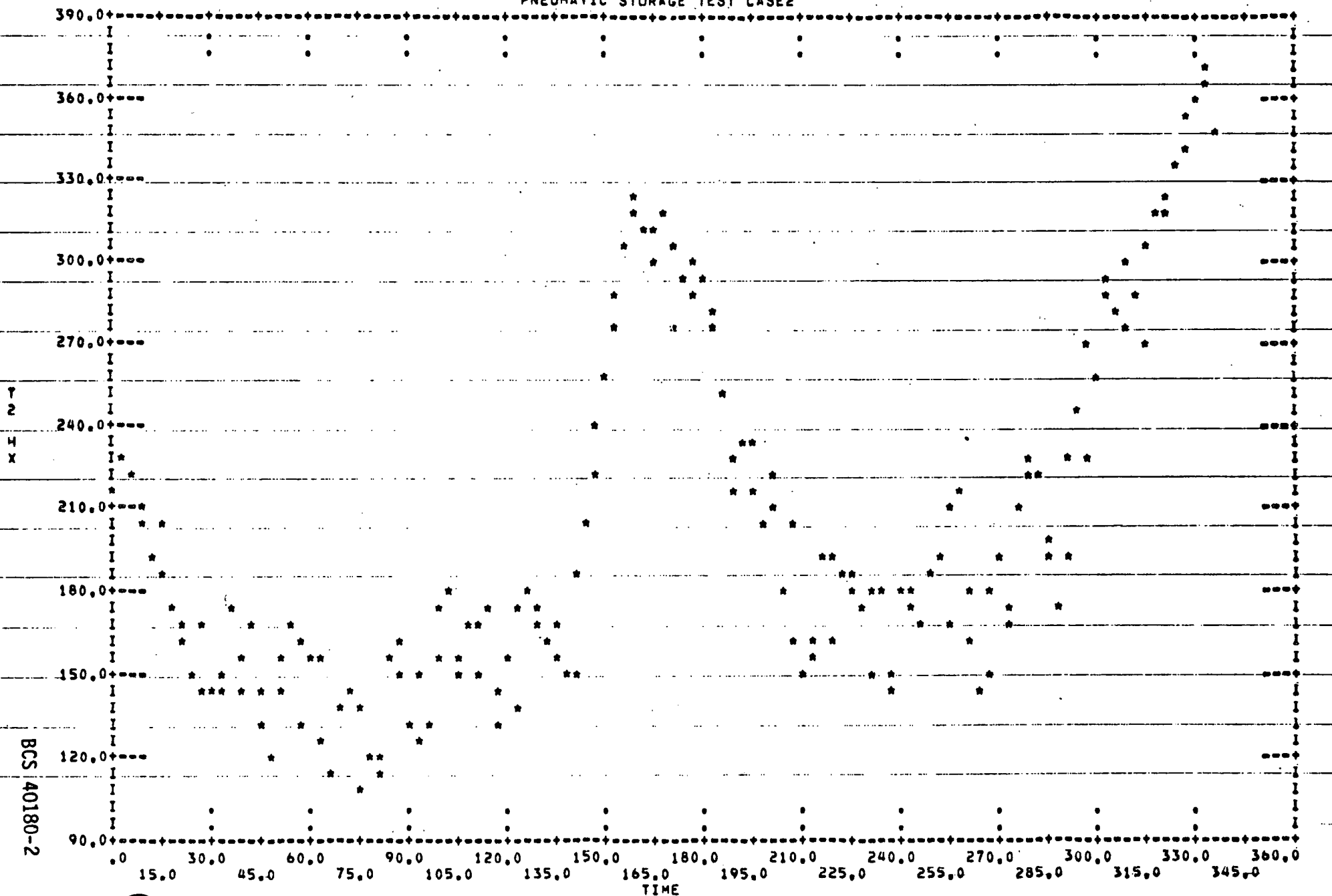


FIGURE 8.5-5 HEAT EXCHANGER OUTLET TEMPERATURE (CHARGING)

BCS 40180-2

PNEUMATIC STORAGE TEST CASE2

M
C
S

407

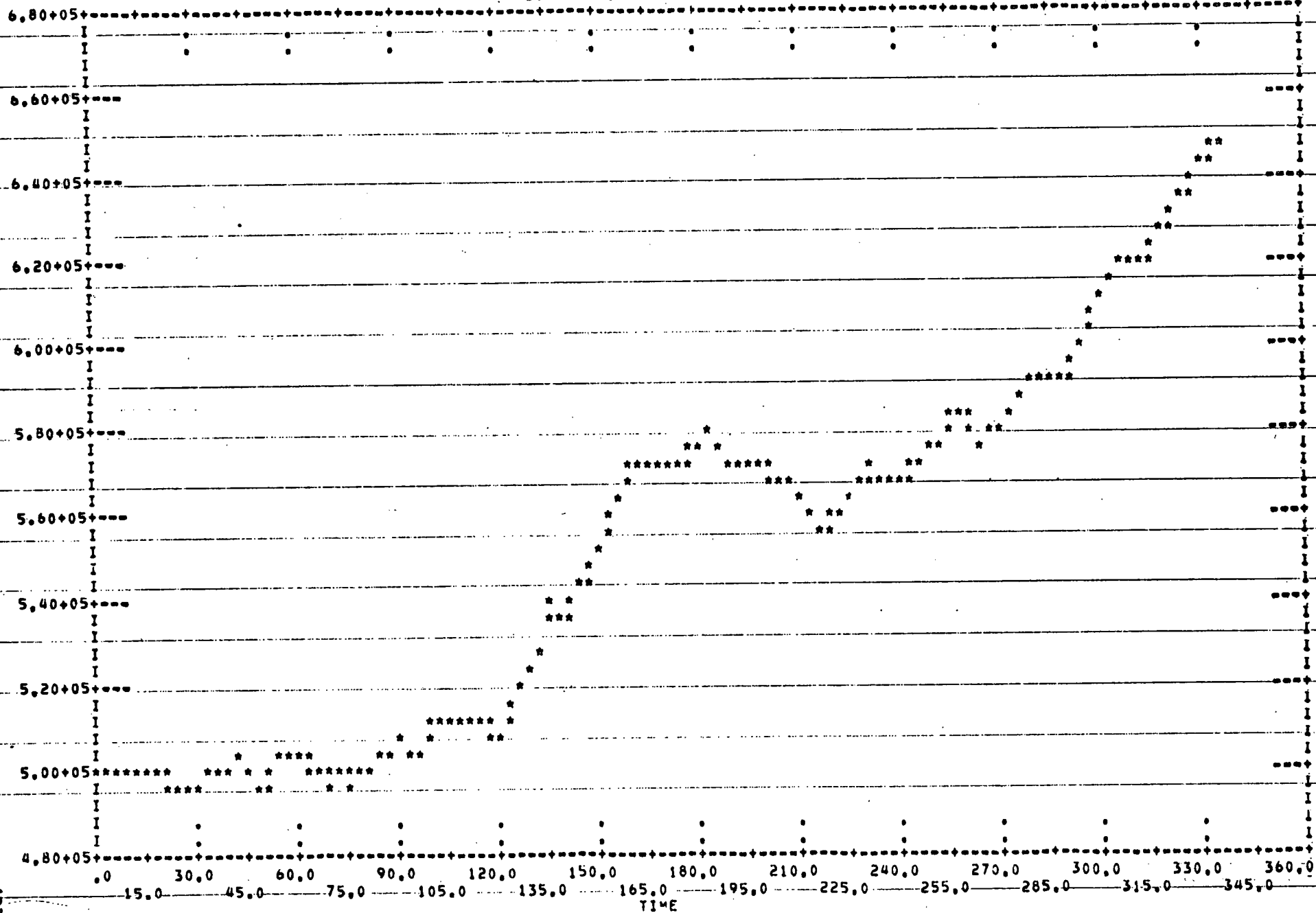


FIGURE 8.5-6 AIR MASS IN PNEUMATIC STORAGE

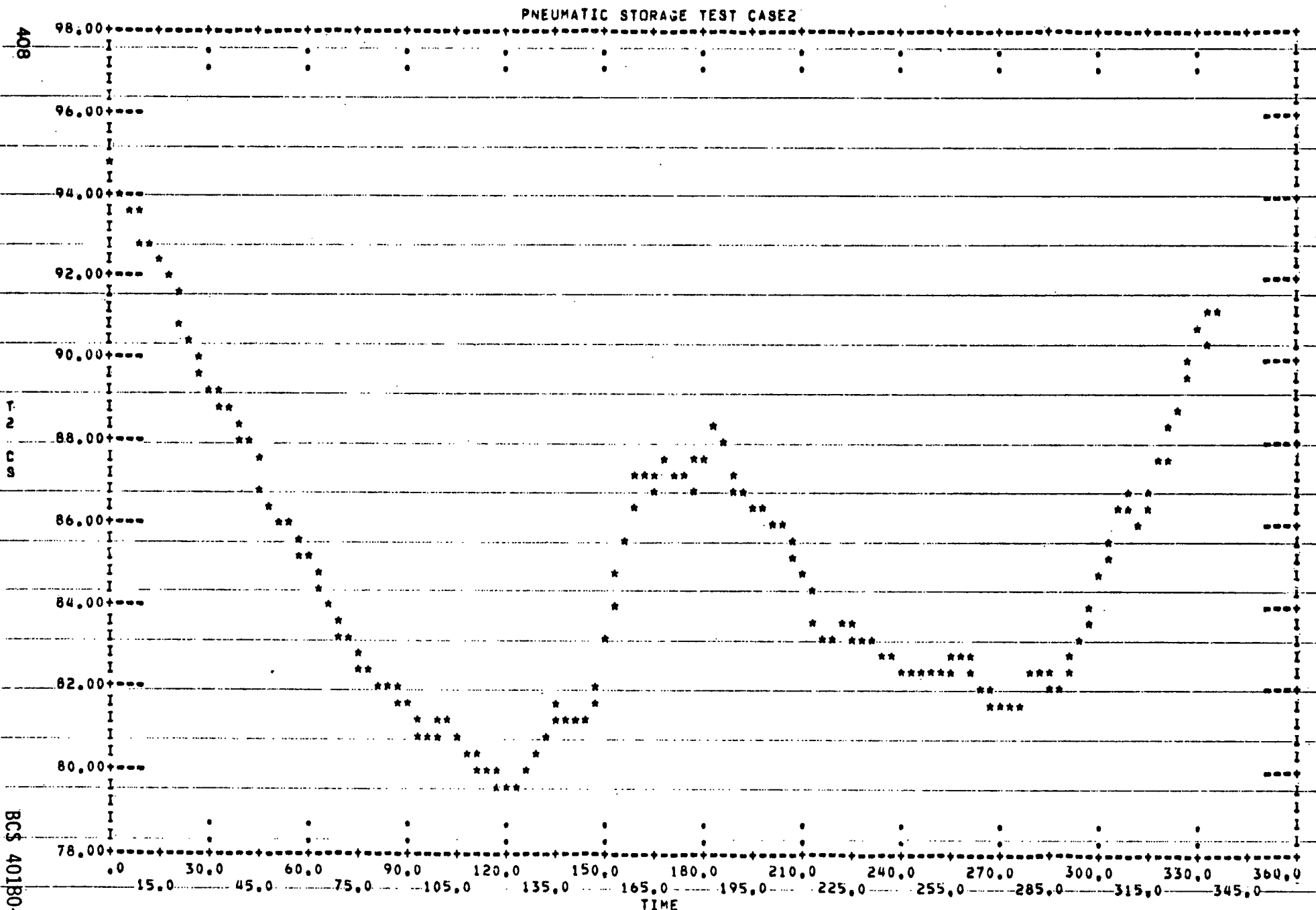


FIGURE 8.5-7 AIR MASS TEMPERATURE IN PNEUMATIC STORAGE VESSEL

BCS 40180-2

PNEUMATIC STORAGE TEST CASE2

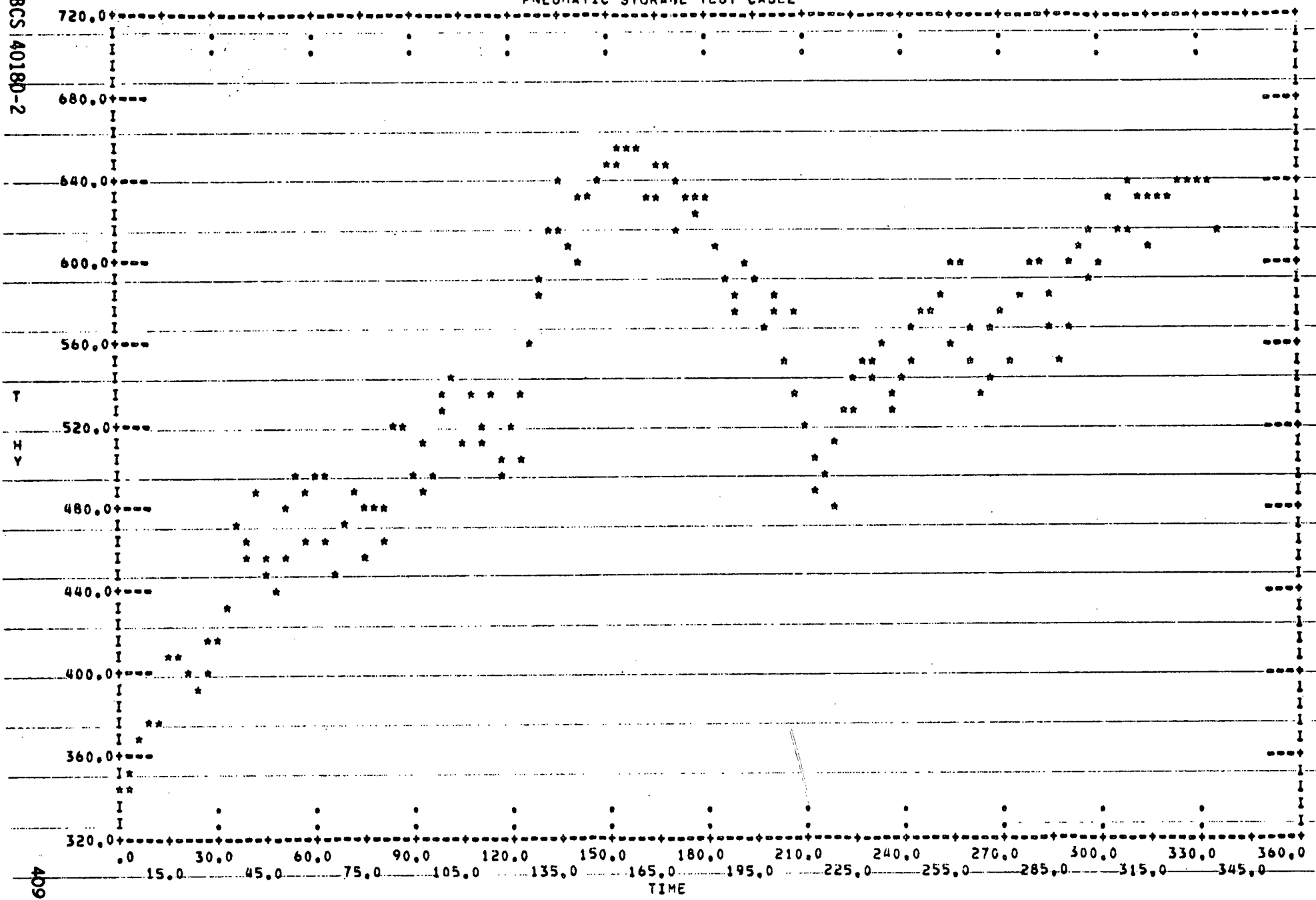


FIGURE 8.5-8 HEAT EXCHANGER OUTLET TEMPERATURE (DISCHARGING)

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temperature at the beginning of the week is a little too cool since the temperature rises to about 400° during the weekends. Phase change in this medium is indicated by the constant temperature intervals at 250° . Figure 8.5-5 shows the air temperature exiting from the heat exchanger into the cavern. During the week this temperature is generally held below 200° but may exceed 350° during the weekend. Figure 8.5-6 shows the air mass stored in the cavern. In this simulation wind power generated exceeded that of the load and thus there is a gradual buildup of air mass in the cavern. The temperature of the stored air mass is shown in Figure 8.5-7. There is about a 10° fluctuation in temperature each week in this case. The last figure, 8.5-8 shows the air temperature exiting from the heat exchanger to the burner. Neglecting the influence of the initial conditions, the average temperature is about 550° and thus a burner is probably not required for this system.

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