

Validation of the SEPHIS Program for the Modeling of the HM Process

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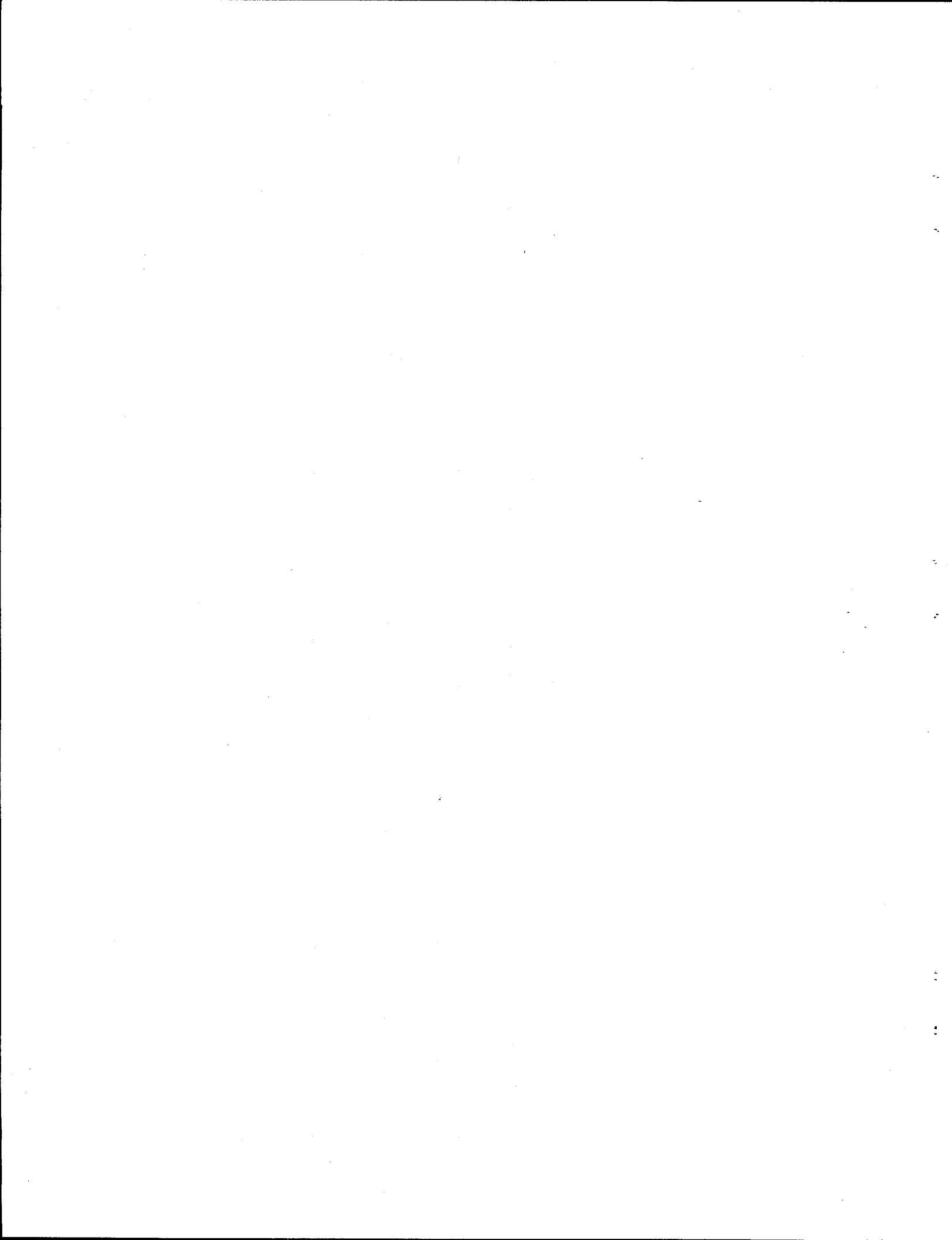


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Acronyms and Definitions:

ANN, Al – Aluminum nitrate nonahydrate, source of aluminum used to complex fluoride. Aluminum is also present as cladding on SRS reactor fuel and targets.

$D_{o/a}$ – Distribution Coefficient, ratio of concentration in organic phase divided by concentration in aqueous phase

DBP – DiButyl Phosphate, Degradation product from TriButyl Phosphate resulting from the loss of a butyl group and replacement by an acid group. Forms a sodium salt in sodium carbonate solution and is stripped from the solvent.

FS - Ferrous Sulfamate is the primary reducing agent used to adjust Pu and Np valence states in the Purex process.

GTM - Generalized Truex Model, Argonne National Laboratory developed software and models used to develop solvent extraction flowsheets. SASSE was a calculational component developed to aid design of such processes.

HLW - High Level Waste, liquid waste containing actinides that will be transferred to the tank farm

SASSE - Excel spreadsheet based macros developed by Argonne National Laboratory for the solution of material balances of countercurrent solvent extraction processes.

SEPHIS - Fortran computer code developed by Oak Ridge National Laboratory in 1975-9 for the solution of material balances of countercurrent solvent extraction processes. This code includes algorithms for the prediction of distribution coefficients for Pu and U based on TBP concentration , extractable and inextractable nitrate concentrations and Pu and U metal ion concentrations.

SOLVEX - Fortran computer code developed by SRS in 1975 for the solution of material balances of countercurrent solvent extraction process.

Strip - The removal of an extracted component (i.e. Pu) via contact with weak acid, reducing agent or complexant

TBP - TriButyl Phosphate is the extractant used in the Purex solvent extraction process. SRS uses a mixture of straight chain hydrocarbons called normal paraffin hydrocarbon (NPH) with an average carbon chain length of 12 to 14 as a diluent for its TBP processes.

TRUEX - TRansUranium EXtraction, General description given to various processes proposed for the separation of many component waste streams containing actinides via countercurrent flow solvent extraction.

Ua - Aqueous concentration of U (g/l), assumed to be pure U235 for purposes of conversion between molar units and g/l units.

Uo – Organic concentration of U (g/l).

Ha - Aqueous concentration of nitric acid, M.

Ho – Organic concentration of nitric acid, M.

Summary

The SEPHIS computer program is currently being used to evaluate the effect of all process variables on the criticality safety of the HM 1st Uranium Cycle process in H Canyon. The objective of its use has three main purposes. 1) To provide a better technical basis for those process variables that do not have any realistic effect on the criticality safety of the process. 2) To qualitatively study those conditions that have been previously recognized to affect the nuclear safety of the process or additional conditions that modeling has indicated may pose a criticality safety issue. 3) To judge the adequacy of existing or future neutron monitors locations in the detection of the initial stages of reflux for specific scenarios.

Although SEPHIS generally over-predicts the distribution of uranium to the organic phase, it is a capable simulation tool as long as the user recognizes its biases and takes special care when using the program for scenarios where the prediction bias is non-conservative. The temperature coefficient used by SEPHIS is poor at predicting effect of temperature on uranium extraction for the 7.5 % TBP used in the HM process. Therefore, SEPHIS should not be used to study temperature related scenarios. However, within normal operating temperatures when other process variables are being studied, it may be used. Care must be given to understanding the prediction bias and its effect on any conclusion for the particular scenario that is under consideration. Uranium extraction with aluminum nitrate is over-predicted worse than for nitric acid systems. However, the extraction section of the 1A bank has sufficient excess capability that these errors, while relatively large, still allow SEPHIS to be used to develop reasonable qualitative assessments for reflux scenarios. However, high losses to the 1AW stream cannot be modeled by SEPHIS.

Background

Historical HM Process in H-Canyon:

Typical HM feed consists of fuel tubes with a uranium-aluminum core⁵. Mercuric nitrate acts as a catalyst to the nitric acid dissolution process to dissolve the aluminum. Initial nitric acid concentrations of 4 to 8M HNO₃ are used in the dissolver. The solution acidity is depleted during the dissolution to less than 1M HNO₃ (due to oxidation reactions with generation of NO_x and H₂O). The solution containing the dissolved Al, U, Np and Pu is then transferred through head-end in batches. Head-end treatment of the solution consists of combinations of gelatin/MnO₂ strike(s) to remove silica and reduce the Zr and Nb content. The MnO₂ strike is not currently required as the fuel available for dissolution is sufficiently aged that the Zr and Nb has already decayed to minimal levels. A centrifugation step is used to remove gelatin, MnO₂ and any other solids. The U solution is then adjusted to make it suitable for 1st Uranium Cycle processing.

1st Uranium Cycle feed is ~4 g U/l, >0.5 M HNO₃, <2M aluminum nitrate with small amounts Np(IV), Pu (IV), and fission products. The U and Np(IV) are extracted into the 7.5% TBP solvent in the 1A bank. Pu is reduced by the FS in the 1AS stream to Pu(III) and exits the process in the 1AW stream. Aluminum nitrate in the extraction section increases the U, Np and HNO₃ distribution coefficient (D_{0/a}) in the extraction section due to "salting". The solvent retains the U and Np(IV) and both are transported to the 1B bank where Np(IV) is stripped out of the solvent by the 1BX. The 1BX contains an intermediate HNO₃ concentration such that

Figure 1. Current Flowsheet for HM 1st Uranium Cycle Process.

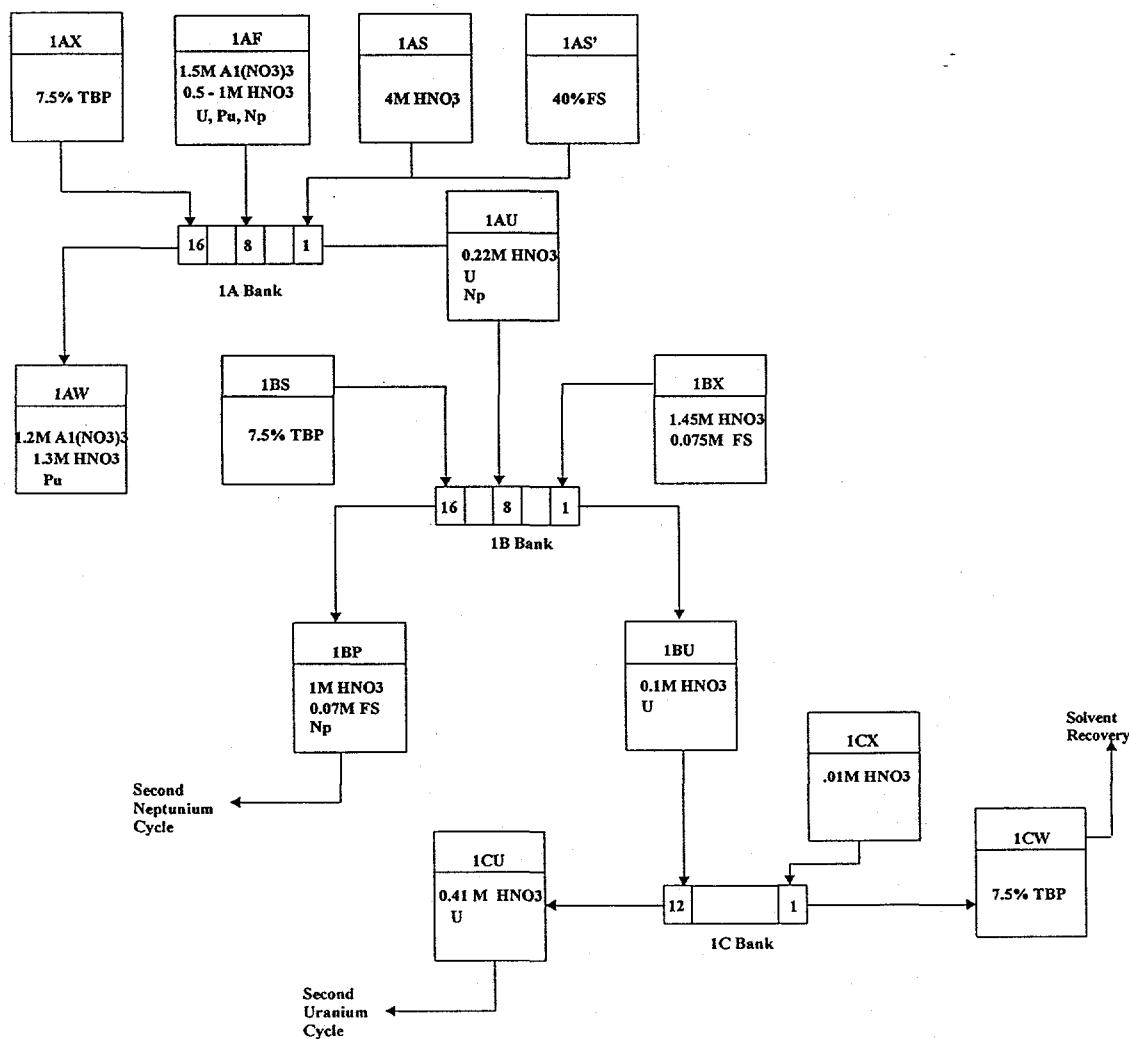


Table I. Operating Conditions, Limits and Assumptions for Modeling the HM 1st Uranium Cycle Process.⁵

IAF	Flow Rate, l/min			Temperature, C			Concentration, g/l, M or Volume %		
	Minimum	Nominal	Maximum	Minimum	Nominal	Maximum	Minimum	Nominal	Maximum
1AF	7.5	8.3	9.2	25	30	37	0.5	8.4	g/l U235
							~1	1.2	M, HNO ₃
1AX	13.7	14.6	15.3	35	40	44	7	7.5	M, ANN
1AS-A	1.60	1.80	2.00				4		Vol % TBP
1AS-FS	0.13	0.11	0.16				0.12		M, HNO ₃
1AS (total)	1.73	1.91	2.16	34	38	44	3.8		M, FS
1BS	24.4	26.3	28.1	35	39	44	7	7.5	M, HNO ₃
1BX	8.2	8.7	9.3	32	35	44	1.45	8.5	Vol % TBP
							0.075	1.6	M, FS
1CX	9.7	10.4	11.1	50	60	65	0.005	0.01	M, HNO ₃

HM Assumptions:

- Organic Phase Flows from stage to stage by Gravity Only
- Aqueous is Pumped from stage to stage by mixer impellers
- Phase ratios in mixer stages are proportional to flow rate ratios
- Phase ratios in settler stages are controlled by interface height in exiting stage at 2/3 organic 1/3 aqueous
- Sephis adequately calculates temperatures of mixed streams
 - S. Heat of organic = $0.321 + 0.078 * \text{volume frac TBP, cal/g/C}$ 0.3269
 - S. Heat of aqueous=1 cal/g/C

		liters/stage	Aqueous	Organic
A, B, & D Bank	Mixer Volume, liters	2.36	2.36	0
		9.439	9.439 * A/(O+A)	9.439 * O/(O+A)
	total	11.8		
C & E Bank	Settler Volume, liters	21.1	21.1	0
		42.1	0	42.1
	total	63.2		
	Mixer Volume, liters	6.637	6.637	0
		25.22	25.22 * A/(O+A)	25.22 * O/(O+A)
	total	31.857		
	Settler Volume, liters	84.93	84.93	0
	total	169.83	0	169.83
		254.8		

Np(IV) is stripped from the solvent, but U is retained until it is stripped in the 1C bank. FS is present in the 1BX to prevent oxidation of Np(IV) to Np(VI) which has a significantly higher $D_{o/a}$. The 1BS stream is a solvent stream that scrubs the U from the 1BP (Np) product. If the quantity of Np recovered is small, the 1BP stream will be neutralized and discarded to the tank farm along with the 1AW stream. U is stripped out of the solvent by the 1CX stream (0.01 M HNO₃) which is purified further in the 2nd Uranium cycle. Residual U remaining in the solvent in the 1CW stream is removed in the carbonate washers. A HM 1st Uranium Cycle process flowchart is shown in Figure 1 and current operating limits are listed in Table I.

All 1st cycle input streams (except the 1AF) are heated to between 32 and 65°C by steam powered heat exchangers. The 1AF stream is capable of being cooled (to remove radioactive decay heat) and is nominally at 30°C. Inter-bank streams such as the 1AU and 1BU are not heated or cooled as they are transferred between banks (except for heat transfer through the piping). The inlet process streams are the only source of heat for the solvent extraction equipment.

During normal operation of the process, the solvent flow has sufficient capacity to extract all U that is fed and transport it from the 1A bank, though the 1B bank until it is stripped in the 1C bank at a concentration no greater than the feed concentration. If process conditions exist in a portion of the bank that are less favorable to extraction, then the stage concentrations and inventories will be increased. Under extreme upset conditions, the process cannot remove the all the uranium fed to the bank and a build-up of inventory occurs. A solvent extraction process that is operating under conditions that result in a U buildup within the bank is commonly

referred to as being in "reflux". Countercurrent flow processes naturally tend to reflux. When the uranium concentration profile reaches a maximum at any stage other than the feed or product stage, the bank may be said to be refluxing uranium. However, this would only represent a potential nuclear safety problem if that maximum U concentration were greater than the feed stream concentration¹⁴. Improper flowrate ratios alone can result in U concentrations in the exit streams of any bank and while this does not represent a reflux condition, such operation can pose a nuclear safety problem if the resulting U concentration is greater than 10.8 g U₂₃₅ equivalent/l¹⁴.

Process Modeling:

Starting in the 1960's, a number of computer programs were written to simulate solvent extraction processes. SOLVEX and SEPHIS are Fortran programs developed in the 1970's that built on the earlier work. Both the SOLVEX¹¹ and SEPHIS^{4,7} programs solve the material balance equations for both unsteady and steady state solvent extraction processes, but take different approaches in how the D_{o/a} are provided to the code. SOLVEX was an advancement at the time it was developed in that it added the ability to input D_{o/a} data in tabular form (for interpolation) rather than use of polynomial type equations. SEPHIS attempted to utilize thermodynamically consistent equations to correlate D_{o/a} data that not only accounted for the effects of nitrate salting and uranium concentration, but also TBP concentration and temperature. This made it a useful tool for studying a wide variety of effects. However, since its D_{o/a} data entirely incorporated into Fortran code, it is not readily modifiable. Also the data utilized to correlate the D_{o/a} data relied heavily on 20 to 30% TBP data at relatively high uranium concentrations. For this reason, Bendixsen² developed a low TBP specific program based on SEPHIS called ICPSEF to model the pulse columns used in the ICPP. These issues highlight accuracy problems with SEPHIS when dealing with the low uranium and TBP concentrations necessarily used with an enriched uranium process.

As part of the development of the GTM for the TRUEX process, Argonne National Laboratory has developed a program that runs in an Excel environment as a macro^{6,18}. This program is called SASSE and allows the calculation of steady-state material balances for counter-current flow solvent-extraction processes with user input of appropriate values of D_{o/a} and flowrates. While this program cannot perform unsteady state simulations, it is very easy to use when appropriate values of D_{o/a} are available for input. It also allows ready incorporation of any equations that are convenient for prediction of D_{o/a} based on component concentrations on individual stages.

Both SOLVEX and SEPHIS are written in Fortran and were developed with the intention of the programs being run on mainframe computers. In 1989, SEPHIS was ported to run in Microsoft Fortran on a PC in DOS by SRTC. This involved updating many of the input-output statements from statements that were no longer supported by the compiler. No calculation related changes were made at that time.

The most critical use of any of these programs is the recognition of operating conditions that in the actual process will cause reflux and a potentially unsafe condition. Process variables can be varied in the computer run and the calculated process inventory will rise and fall. By running these programs over a wide range of conditions, inventory trends are studied. The approach of reflux conditions results in convergence difficulties for the steady state solution of the material balances. None of these programs will converge to a steady state concentration profile when severe reflux conditions are specified as input parameters. Under **mild reflux conditions, these programs may reach the limit of iteration (time or number of iterations) with little or no indication that a steady state material balance was not converged.** With such a simulation, it is necessary for the operator to take steps to recognize when results are not steady state results.

Distribution Data:

Validation of any solvent extraction simulation program for the HM process requires a good set of uranium extraction data to compare the program against. Experimental U extraction data for the original HM process was developed in the 1950's^{1,8,12}. Additional data was taken by Thompson when the 1st Cycle process was changed to 7.5% TBP^{13,14,15,16,17}. DP-1500 was compiled in the later 1970's and documented both the process and equipment details along with extraction data⁵. These provide the three main authoritative sources of D_{o/a} information that are applicable to the HM process today. A larger body of data exists at the higher TBP concentrations typically used in the PUREX process, but this is not particularly useful for modeling the HM process^{3,9}. DP-1384 contains extensive uranium extraction data for 7.5 volume percent TBP over a wide range of nitric acid and uranium concentrations for 23, 45, and 60°C. It also has a limited amount of data for aluminum nitrate/HNO₃ salted extraction at the same temperatures. DP-53 contains some uranium extraction data for 2 to 10 volume percent TBP for the temperature range of 25 to 45.9°C. For this effort, DP-1384 was

the primary source of $D_{o/a}$ acid salted data, supplemented by DP-53. DP-1500 and DP-1384 were relied on for aluminum nitrate salted data.

Calculational Methodology:

Use of a PC rather than a mainframe computer has the advantage that retrieval of output is quick and simple and output can be readily transferred to other desktop applications for analysis and study. During this work SEPHIS output was directly imported as text into Word and tables within the output were then converted to actual tables using the "Convert text to table" option of Word. This allowed data transfer to either Excel or SigmaPlot for preparation of graphs to visualize the results simulated by SEPHIS. A standard Excel spreadsheet was set up that allowed for the output of a series of SEPHIS cases to be imported into a spreadsheet separating cells using the delimiter ";" used in SEPHIS to separate columnar data. Other sheets of the spreadsheet then read the values of the cells from the first sheet for each case in sequence. Standard graphs compared the different cases contained in the run. This allowed rapid preparation of a graphical presentation of the results of the study of a variable.

The punched profile output was also used in a similar manner. This file contains profiles for concentrations and temperature for both the aqueous and organic phases for each stage. This punch file was directly imported into Excel and $D_{o/a}$ calculated. This technique was also used to produce predictions for $D_{o/a}$ to

compare with literature data. Table II lists the assumptions and setup that was used to predict a single data point using a single isothermal stage. By inputting a data set that contains a similar case for each data point to be predicted by SEPHIS, a file containing 2 lines of output for each point was produced. Once a standard Excel file was created, copies of that file were created and new data pasted into the punched output sheet. This greatly reduced the effort to analyze the results and minimized the potential for transcription errors.

Operation of SASSE was fairly straightforward. The "sasse_generator" macro

Table II. Method for Calculation of $D_{o/a}$ Using SEPHIS.

Inputs:

- 10 lpm Aqueous Flow (T, U_a , $HNO_{3,a}$)
- 0.0001 lpm Organic Flow (T, TBP)
- Single Isothermal Stage (All streams at same T)

Calculated Outputs:

- 10 lpm Aqueous (T, U_a , $HNO_{3,a}$)
- 0.0001 lpm Organic Flow (T, TBP, U_o , $HNO_{3,o}$)
- $D_{o/a}$ for $U = U_o/U_a$

Since Aqueous Flow >> Organic Flow, the extraction of U and HNO_3 is insignificant to the material balance

was loaded into Excel and the macro run to setup a new process simulation spreadsheet¹⁸. After input of the number of sections, stages and components, a new spreadsheet for the process was created. Input flowrates and concentrations had to be entered as well as entering values or equations for $D_{o/a}$. It is necessary to activate the "Iteration" feature of the "Calculation" tab of the "Options" tab of the Tools command. This is how SASSE solves the material balances for the counter-current-flow solvent extraction equations. Since some versions of Excel have reported a recalculation "bug", special attention was given to forcing a "Ctrl-Alt-F9" recalculation after any changes were made to a SASSE spreadsheet. Once the HM process was set up in SASSE, the spreadsheet was then copied so that different conditions could be simulated without recreating the overall spreadsheet.

One significant difference in nomenclature is that SASSE adopts a stage numbering convention that is opposite that which has always been used at SRS. Whereas SRS numbers stages such that the organic flow travels from high stage numbers to low, SASSE numbers stages such that organic flows from low to high. This requires a translation of stage designation to be made to compare the results of the two programs and care has to be taken to place the feed stage to a bank on the correct stage.

Results and Discussion:**SEPHIS Predictions with Aluminum Nitrate Present**

Material Balance Checks: The extraction section of the 1A bank contains significant amounts of aluminum nitrate. This is accounted for in SEPHIS as non-extractable nitrate and is input as 3 times the aluminum molarity. The correlation used in SEPHIS to calculate aqueous density significantly over-predicts the density of solutions containing significant amounts of aluminum nitrate. Since SEPHIS constantly converts units between moles/liter and moles/kg, the aqueous density errors could significantly affect the material balance. This potential problem was investigated by running SEPHIS with both 1.2M and 2M Al and extracting the $U_{D_{0a}}$ that SEPHIS calculated. The same input conditions and D_{0a} values were then copied into SASSE and the U profiles between the two programs were compared. Table III shows edited results of the 2M Al

Table III. SEPHIS versus SASSE Material Balance Comparison.

(U_a Difference is calculated as $(U_a \text{ SEPHIS} - U_a \text{ SASSE})/U_a \text{ SEPHIS} *100\%.$)

STAGE NO.	NITRIC ACID (MOL/L)	URANIUM (G/L)	NITRATE ION (MOL/L)	DENSITY (G/ML)	MIXER FLOW (L/MIN)	TEMPERATURE (CENTIGRADE)	SASSE	
							URANIUM (G/L)	U _a Difference
1	3.80	0.754	0.00	1.14	1.93	45.0	0.758	-0.6%
2	3.80	0.781	0.00	1.14	1.93	45.0	0.780	0.1%
3	3.80	0.782	0.00	1.14	1.93	45.0	0.781	0.1%
4	3.80	0.782	0.00	1.14	1.93	45.0	0.781	0.1%
5	3.80	0.781	0.00	1.14	1.93	45.0	0.781	0.1%
6	3.82	0.780	0.00	1.14	1.93	45.0	0.781	-0.1%
7	3.90	0.775	0.000	1.14	1.94	45.0	0.781	-0.7%
8	1.18	0.049	4.87	2.13	10.23	45.0	0.049	-1.4%
9	1.18	0.0004	4.87	2.13	10.23	45.0	0.0004	-2.5%
10	1.18	3.0E-06	4.87	2.13	10.23	45.0	3.1E-06	-3.8%
11	1.18	2.4E-08	4.87	2.13	10.23	45.0	2.5E-08	-5.2%
12	1.18	1.8E-10	4.87	2.13	10.23	45.0	2.0E-10	-6.5%
13	1.18	1.4E-12	4.87	2.13	10.23	45.0	1.6E-12	-8.8%
14	1.18	1.1E-14	4.87	2.13	10.23	45.0	1.2E-14	-11.4%
15	1.15	0.0E+00	4.87	2.13	10.22	45.0	1.1E-16	
16	0.86	0.0E+00	4.92	2.12	10.13	45.0	1.2E-17	
	PRODUCT STREAM				10.13			

ORGANIC PHASE

STAGE NO.	NITRIC ACID (MOL/L)	URANIUM (G/L)	U EXTRACTION FACTOR	HNO ₃ EXTRACT FACTOR	DENSITY (G/ML)	MIXER FLOW (L/MIN)	SASSE	
							URANIUM (G/L)	U _o Difference
1	PRODUCT STREAM				14.73			
1	0.19	3.380	34.2	0.38	0.827	14.73	3.411	-0.9%
2	0.19	3.479	34.0	0.38	0.827	14.73	3.510	-0.9%
3	0.19	3.482	34.0	0.38	0.827	14.73	3.512	-0.9%
4	0.19	3.483	34.0	0.38	0.827	14.73	3.513	-0.8%
5	0.19	3.483	34.0	0.38	0.827	14.73	3.513	-0.8%
6	0.19	3.482	34.1	0.38	0.827	14.73	3.513	-0.9%
7	0.19	3.482	34.2	0.38	0.827	14.74	3.513	-0.9%
8	0.21	3.480	102.8	0.25	0.828	14.74	3.513	-0.9%
9	0.23	0.034	127.3	0.28	0.824	14.74	0.035	-2.0%
10	0.23	0.0003	127.6	0.28	0.824	14.74	2.7E-04	-3.2%
11	0.23	2.1E-06	127.6	0.28	0.824	14.74	2.2E-06	-4.5%
12	0.23	1.6E-08	127.6	0.28	0.824	14.74	1.7E-08	-5.8%
13	0.23	1.3E-10	127.6	0.28	0.824	14.74	1.4E-10	-8.0%
14	0.23	9.9E-13	127.8	0.28	0.824	14.74	1.1E-12	-10.4%
15	0.23	0.0E+00		0.29	0.824	14.74	9.7E-15	
16	0.21	0.0E+00		0.36	0.823	14.73	1.1E-15	

comparison for 1A bank (both extraction and scrub sections). The scrub section shows differences in U concentration of up to 1% and the extraction section shows differences of 2 to 10%. The differences in the extraction section are differences between small concentrations of U which don't appear to be a significant problem. The differences in the scrub section are not large enough to be of serious concern and although not investigated in depth, may be due to rounding differences in the calculations or the difference between the use of an iterative solution method in one program and a 4th order Runge Kutta numerical integration method in the other. Overall, the relatively small differences in the U material balance indicate that the large differences in aqueous density do not seriously affect the U stage to stage profiles. The good agreement between the two independent programs validates the overall material balance and stage to stage profiles with the assumption that good values of D_{oa} are being provided.

D_{oa} Prediction: SEPHIS calculates the D_{oa} based on a pseudo mass-action equilibrium constant^{4,7} that is dependent on a term that equates to the total nitrate in the aqueous phase. DP-1500⁵ contains a graph of D_{oa} for U from 1.6M ANN/0.5M HNO₃ into 7.5 volume % TBP as U_a is varied for both 23 and 45°C. This graph has been digitally reproduced and SEPHIS predictions for both 23 and 45°C have been added and are included as Figure 2. Inspection of this graph shows that SEPHIS significantly over-predicts the D_{oa} for both temperatures. A numerical comparison showed that for less than 2 g/l U_a, SEPHIS over-predicted the DP-1500 curves by 25-300% for 23°C and by 40-350% for 45°C. These comparisons agree with the past observations that SEPHIS tends to under-predict losses to the AW stream. Due to the small U inventories involved on stages where aluminum nitrate is present and the relatively large D_{oa} 's that experimentally exist when >1M aluminum nitrate is present, it does not appear these prediction errors pose a serious problem. The errors could be reduced by artificially lowering the amount of aluminum used in the input to SEPHIS or by using SASSE with more realistic values for D_{oa} .

Figure 2. SEPHIS Predictions as a Function of U_a for DP-1500 Aluminum Nitrate System.

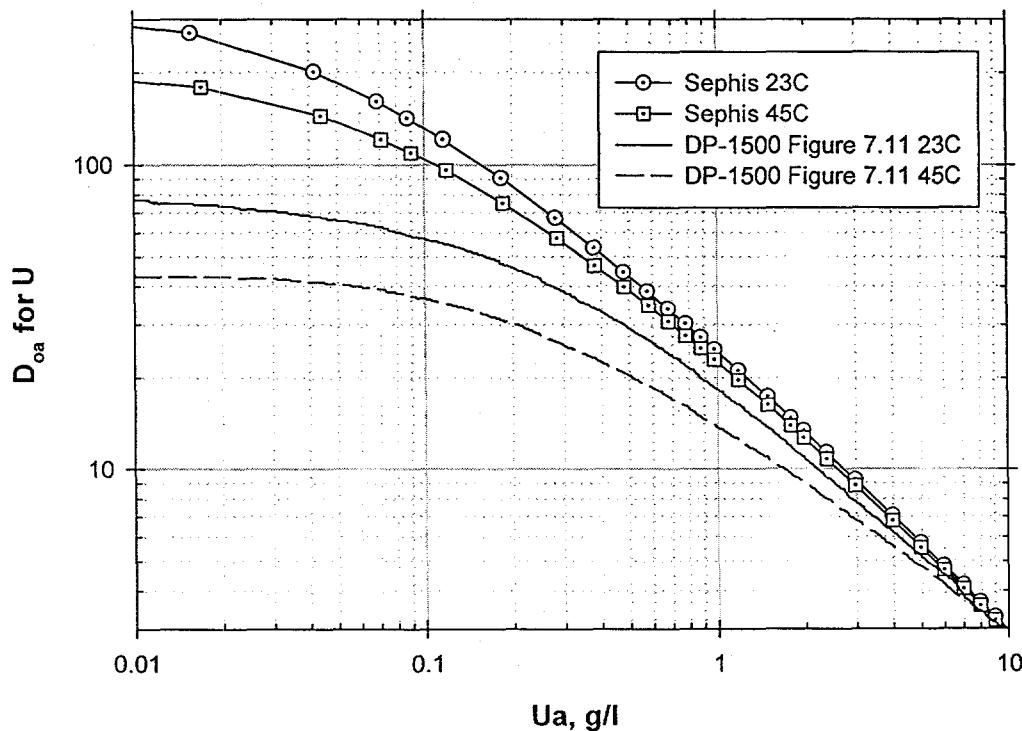
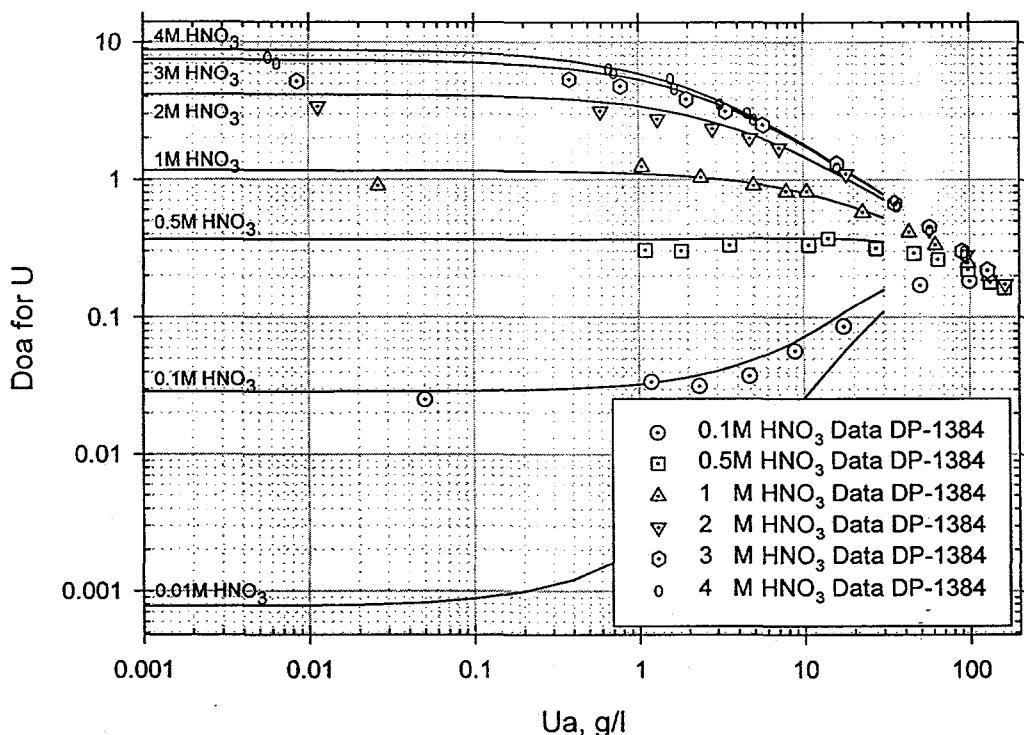


Figure 3. SEPHIS Predictions of $U D_{0/a}$ for DP-1384 HNO₃ Systems 23°C.

SEPHIS Predictions with Nitric Acid Salting Only

$D_{0/a}$ Prediction: When nitric acid is the only salting agent present SEPHIS still calculates the $D_{0/a}$ based on the same pseudo mass-action equilibrium constant with dependence on total nitrate in the aqueous phase. DP-53¹² and DP-1384¹⁶ provide data on the $D_{0/a}$ for U from HNO₃ solution into 7.5% TBP at temperatures between 23 and 60°C. Figures 3, 4 and 5 show a comparison of $D_{0/a}$ for U between SEPHIS predictions and the data of DP-1384. Isotherms of 23, 45 and 60°C are shown as functions of both U_a and HNO₃. The data are also included as tables V, VI, and VII in the appendix.

Figure 6 shows the error of SEPHIS in predicting $D_{0/a}$ for U as a function of U_a for the data from DP-53 and DP-1384. It shows a wide scatter but SEPHIS generally over-predicts the data by 20%. There appears to be a trend toward improved prediction at higher U_a concentrations. Figure 7 contains the same data, but plotted as a function of the volume percent TBP. The trends of better fit at either higher TBP or higher U_a concentrations was expected due to the sources of data used in the SEPHIS correlation. Figure 8 also contains the same data, but plotted as a function of temperature. It appears clear from this graph that SEPHIS does not accurately account for the effect of temperature for the 2.5 to 10% TBP data referenced in this work. It appears that SEPHIS increasingly over-predicts the $D_{0/a}$ at higher temperatures. Figure 9 is still the same data, but this time plotted as a function of aqueous acid concentration. There is not an obvious trend in looking at this plot.

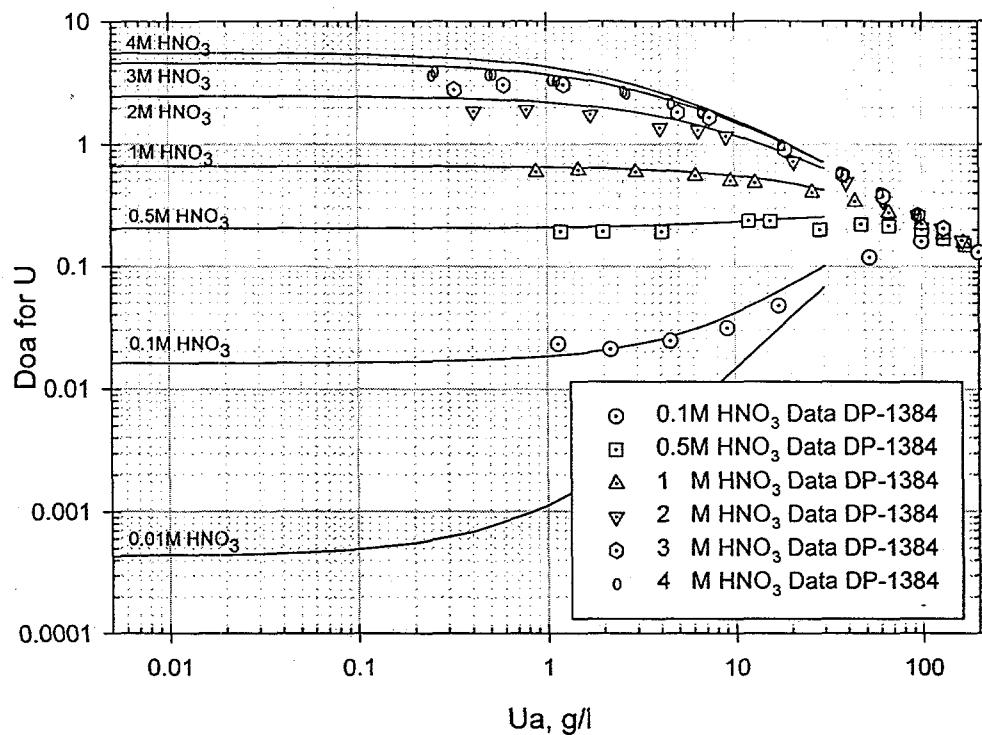
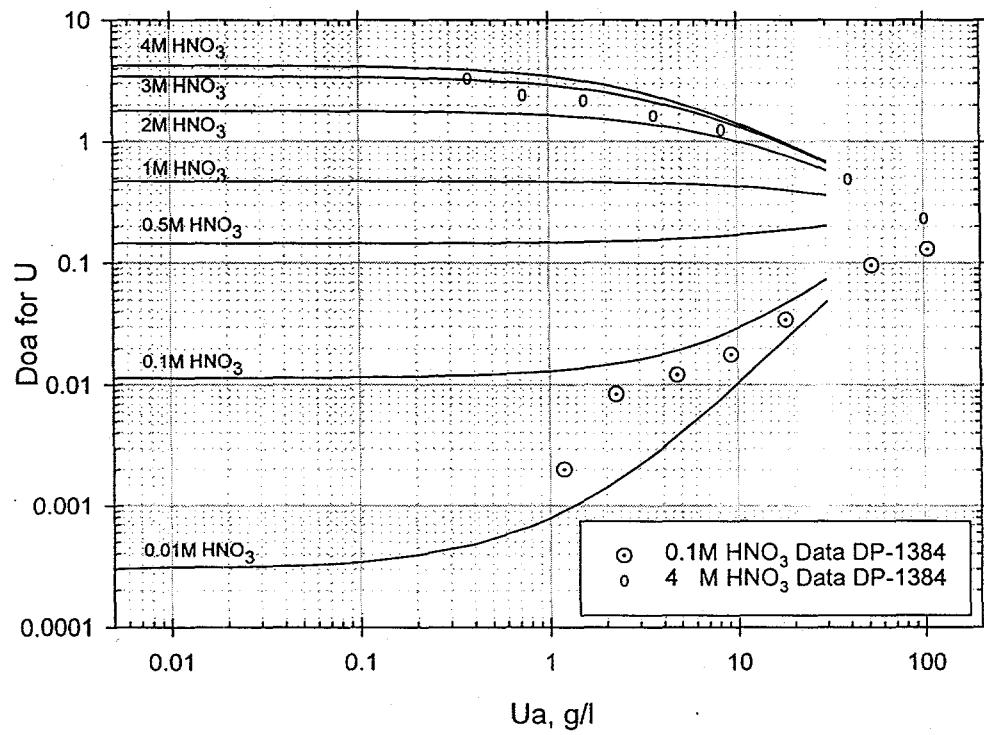
Figure 4. SEPHIS Predictions of $U D_{0/a}$ for DP-1384 HNO₃ Systems 45°C.Figure 5. SEPHIS Predictions of $U D_{0/a}$ for DP-1384 HNO₃ Systems 60°C.

Figure 6. SEPHIS Error as a Function of U_a Concentration.

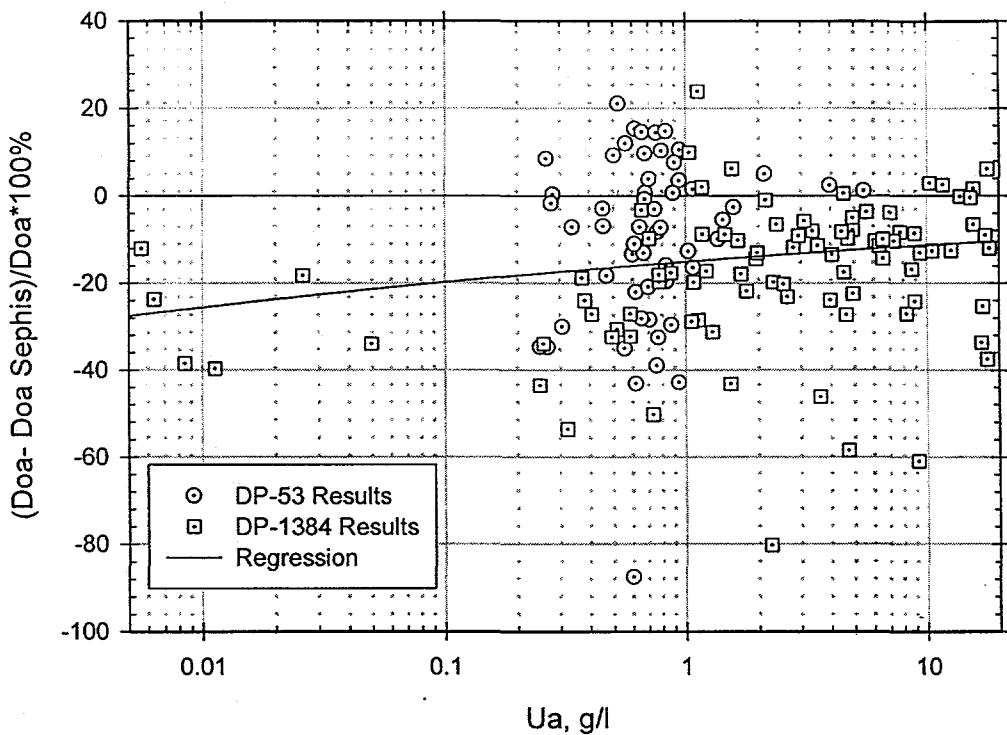


Figure 7. SEPHIS Error as a Function of Volume Percent TBP.

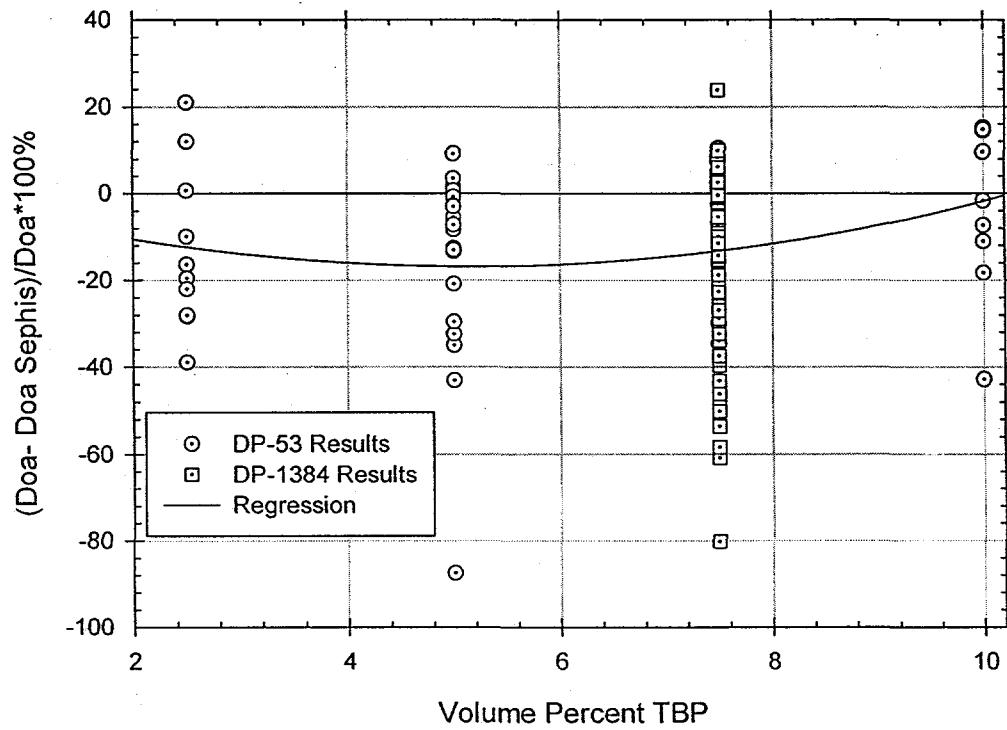
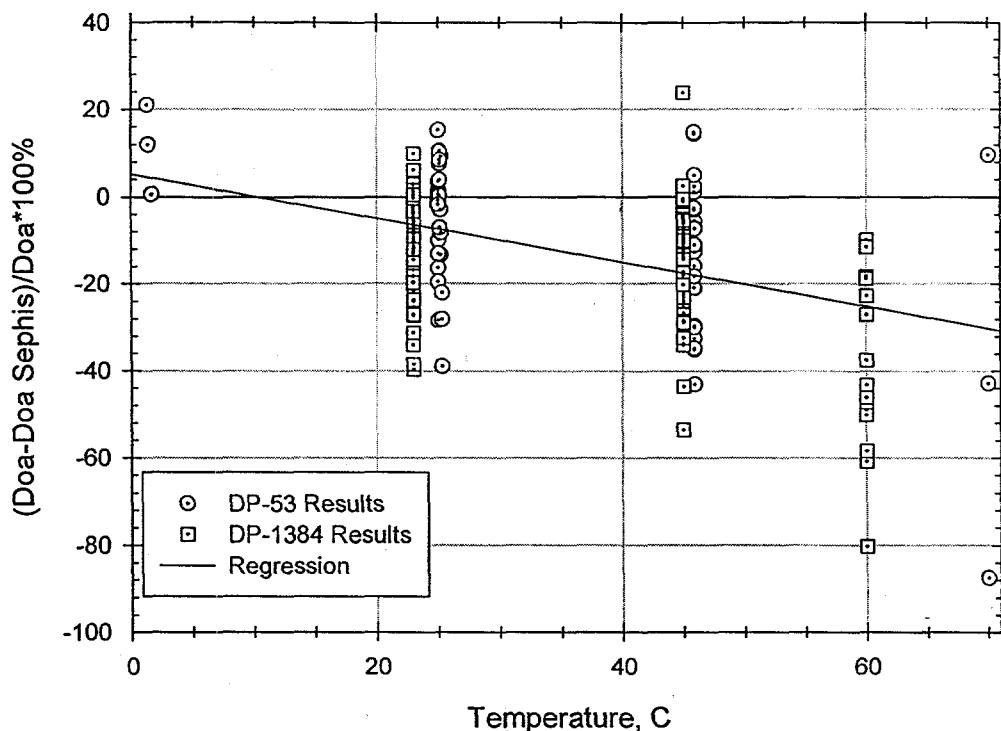
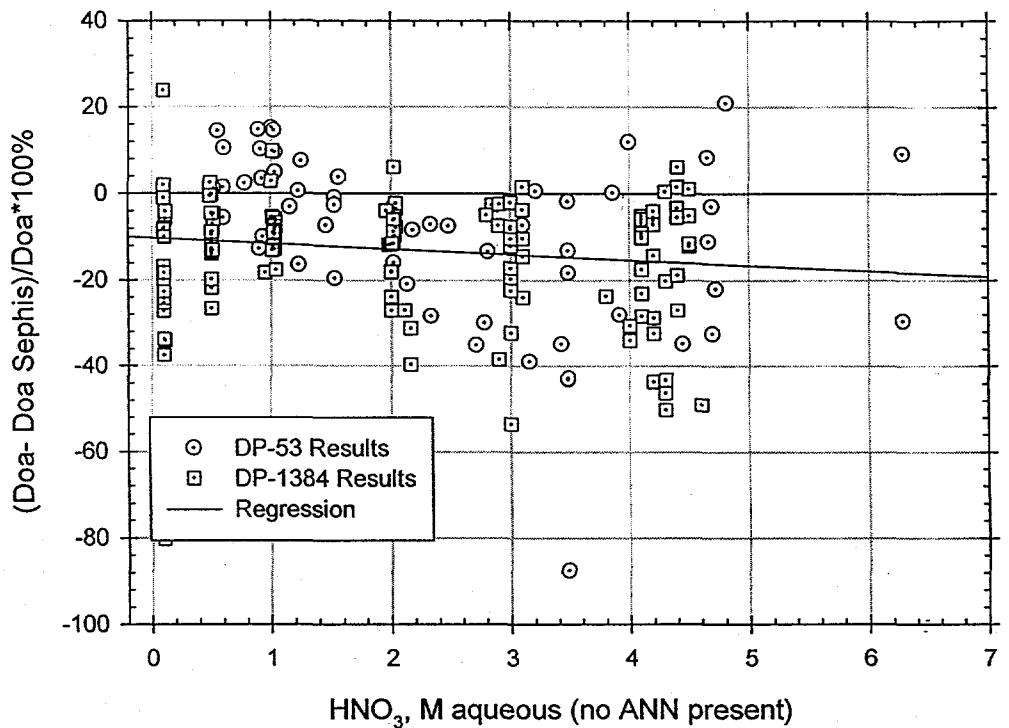
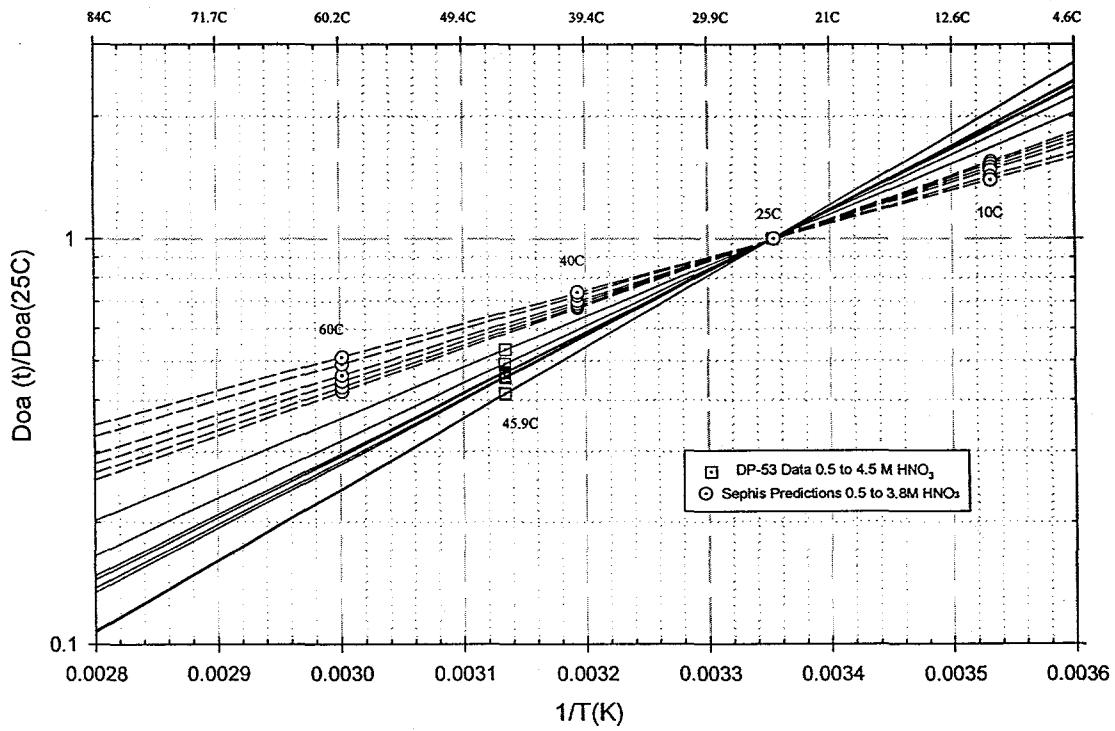


Figure 8. SEPHIS Error as a Function of Temperature.



Further investigation of the influence of temperature on SEPHIS prediction of $U D_{o/a}$ has found that SEPHIS has based its temperature correction on an Arrhenius model^{4,13} with a temperature coefficient that apparently under-predicts the response of $D_{o/a}$ to temperature for 7.5% TBP solvent. This results in the tendency of SEPHIS to over-predict the $D_{o/a}$ at higher temperature. Figure 10 shows an Arrhenius plot of $\log\{D_{o/a}(t)/D_{o/a}(t_0)\}$ vs. $1/T$ for DP-53 data at various HNO_3 as well as the corresponding SEPHIS predictions. Inspection of the SEPHIS code indicates the possibility of improving the $D_{o/a}$ predictions by adjusting the single temperature coefficient in the code to a value that better represents U behavior with 7.5% TBP. However, correction of the model and validation of the corrected model was beyond the time constraints of the current report.

SEPHIS does not take into account any effects of heats of mixing or reaction into its temperature calculations. It assumes a constant specific heat for each phase (1 cal/g/C for aqueous phases and 0.321 cal/g/C for pure n-paraffin and 0.399 cal/g/C for pure TBP) and no molecular interaction between any of the species. Since there are interactions between TBP-U-HNO₃-water and even TBP-n-dodecane has volume and enthalpy changes of mixing (indicating non-ideal behavior), these assumptions appear to be somewhat primitive. However the extent of errors in the temperature profile generated by these assumptions are not easy to quantify with the very limited data that is available to compare against.

Figure 9. SEPHIS Error as a Function of HNO_3 Concentration.Figure 10. Comparison of SEPHIS Temperature Coefficient for $U D_{0/a}$ with DP-53 Table VIII Data.

Application of SEPHIS to Analyze for Potential U Reflux Conditions

Since SEPHIS is being used to identify possible operating conditions that could cause unsafe uranium concentrations, it is important to recognize when it might fail to detect potential reflux conditions. Certainly SEPHIS's $D_{o/a}$ models have a limited accuracy when applied to a 7.5% TBP solvent extraction process such as HM and generally over-predict the $D_{o/a}$. When a process variable is being studied for a potential reflux effect, it is recommended that the variable be varied far enough beyond its operating range so that the SEPHIS predictions span the full range of $D_{o/a}$ expected (including the model bias). Analyzing conditions only within the operating limits of the variable may allow a reflux scenario to remain unnoticed if the model bias is non-conservative. The analysis of this report indicates that scenarios involving temperature must be very carefully evaluated as SEPHIS does not have the capability to accurately predict temperature effects on U $D_{o/a}$. Careful modeling of the applicable data in DP-53 and DP-1384 is needed to correct the temperature coefficient of SEPHIS. Even then, a thorough evaluation of the bias of the modified model should be made. Another approach would be to use SASSE to supplement SEPHIS in looking at the steady state solutions for temperature scenarios. This also requires careful modeling of the same data set, but would avoid alteration of the Fortran code.

Uncertainties

There are both experimental and calculational uncertainties throughout this work that can affect the conclusions of this work. The experimental $D_{o/a}$ values from DP-53 and DP-1384 are by far the best data available for evaluating the HM process, but a direct comparison will show discrepancies between these sets of data. No attempt to arbitrate between these data sets was made. The temperature related errors are large enough that they may mask some other prediction error and prevent its identification. The aluminum salting effects on $D_{o/a}$ were not exhaustively analyzed as the reflux issues in the 1A bank were not very sensitive the extraction portion of the process due to the large values of $D_{o/a}$ involved. Large errors involving salting effects here just do not affect the conclusions. The prediction error is generally small enough that errors other than temperature errors are not a serious limitation of the use of this program as long as the general limitations of SEPHIS as a computer model are not forgotten. The heat capacity limitations in SEPHIS will introduce additional uncertainty when extreme values of temperature are involved. Under nominal temperature conditions, the opportunity for significant error caused by specific heat appears to be minimal. Certainly other conditions that can affect the real process (such as low interfacial tension, incomplete phase separation and DBP content of solvent) are far beyond the capability of SEPHIS or any other existing program to identify.

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APPENDIX

Table IV. Uranium Distribution Data from DP-53 Table VIII and Comparison with SEPHIS Results.

TBP Volume %	T C	Ha M	Ua M	Uo M	Doa DP-53	Ua g/l	Doa calc.	Doa Sephis	Error Sephis
2.5	1.7	3.21	0.0029	0.0073	2.51	0.682	2.517	2.494	1%
2.5	1.4	3.99	0.00239	0.0078	3.25	0.562	3.264	2.862	12%
2.5	1.3	4.81	0.00223	0.008	3.57	0.524	3.587	2.821	21%
2.5	25.0	0.93	0.0058	0.00087	0.151	1.363	0.150	0.166	-10%
2.5	25.0	1.23	0.00458	0.00112	0.245	1.076	0.245	0.285	-16%
2.5	25.0	1.53	0.00354	0.00133	0.375	0.832	0.376	0.448	-20%
2.5	25.0	2.33	0.003	0.00239	0.8	0.705	0.797	1.027	-28%
2.5	25.3	3.15	0.00321	0.00349	(1.09)	0.754	1.087	1.515	-39%
2.5	25.3	3.91	0.00278	0.00373	(1.38)	0.653	1.342	1.767	-28%
2.5	25.3	4.72	0.00264	0.00377	(1.45)	0.620	1.428	1.770	-22%
5.0	25.0	0.60	0.00458	0.00112	0.245	1.076	0.245	0.241	1%
5.0	25.0	0.92	0.00401	0.00206	0.513	0.942	0.514	0.495	3%
5.0	25.0	1.23	0.00379	0.0032	0.84	0.891	0.844	0.835	1%
5.0	25.0	1.53	0.00289	0.00365	1.26	0.679	1.263	1.271	-1%
5.0	25.2	2.18	0.00325	0.00693	(2.14)	0.764	2.132	2.319	-8%
5.0	25.2	2.81	0.00256	0.00759	(2.97)	0.602	2.965	3.367	-13%
5.0	25.2	4.69	0.00193	0.0083	(4.14)	0.454	4.301	4.264	-3%
5.0	25.2	6.28	0.00214	0.008	(3.77)	0.503	3.738	3.423	9%
5.0	45.9	0.60	0.00608	0.00082	0.135	1.429	0.135	0.142	-6%
5.0	45.9	0.90	0.00437	0.0011	0.252	1.027	0.252	0.284	-13%
5.0	45.9	1.16	0.00317	0.0014	0.442	0.745	0.442	0.456	-3%
5.0	45.9	1.46	0.00275	0.00186	0.667	0.646	0.676	0.715	-7%
5.0	45.9	2.13	0.00297	0.00361	1.21	0.698	1.215	1.463	-21%
5.0	45.9	2.71	0.00236	0.00381	1.61	0.555	1.614	2.175	-35%
5.0	45.9	4.69	0.00327	0.00691	2.09	0.768	2.113	2.769	-32%
5.0	45.9	6.28	0.0037	0.00648	1.73	0.870	1.751	2.242	-30%
5.0	25.0	3.48	0.00285	0.0099	3.46	0.670	3.474	3.914	-13%
5.0	45.9	3.48	0.00263	0.00505	1.92	0.618	1.920	2.748	-43%
5.0	70.0	3.48	0.00256	0.00254	0.99	0.602	0.992	1.856	-87%
7.5	25.1	0.60	0.00401	0.00206	(0.52)	0.942	0.514	0.461	10%
7.5	25.1	0.91	0.00337	0.00341	(1.01)	0.792	1.012	0.906	10%
7.5	25.1	1.25	0.00382	0.00636	(1.67)	0.898	1.665	1.544	8%
7.5	25.1	1.56	0.003	0.0072	(2.39)	0.705	2.400	2.299	4%
7.5	25.1	2.33	0.00194	0.0082	(4.25)	0.456	4.227	4.548	-7%
7.5	25.1	3.10	0.00144	0.0087	(6.04)	0.338	6.042	6.477	-7%
7.5	25.1	3.86	0.0012	0.009	(7.40)	0.282	7.500	7.385	0%
7.5	25.1	4.65	0.00112	0.0091	(8.00)	0.263	8.125	7.325	8%
7.5	45.9	0.52	0.0234	0.00544	0.232	5.499	0.232	0.229	1%
7.5	45.9	0.78	0.0169	0.0071	0.422	3.972	0.420	0.412	2%
7.5	45.9	1.03	0.009	0.00619	0.69	2.115	0.688	0.656	5%
7.5	45.9	1.53	0.00674	0.0086	1.28	1.584	1.276	1.314	-3%
7.5	45.9	2.02	0.00353	0.00682	1.93	0.830	1.932	2.237	-16%
7.5	45.9	2.78	0.0013	0.00386	2.97	0.306	2.969	3.861	-30%
7.5	45.9	3.42	0.00113	0.00398	3.52	0.266	3.522	4.746	-35%
7.5	45.9	4.44	0.00105	0.00397	3.78	0.247	3.781	5.095	-35%
10.0	25.0	3.48	0.00118	0.0115	9.78	0.277	9.746	9.953	-2%
10.0	45.9	3.48	0.002	0.0107	5.36	0.470	5.350	6.340	-18%
10.0	70.0	3.48	0.00398	0.01165	2.76	0.935	2.927	3.943	-43%
10.0	25.0	1.00	0.00262	0.00505	1.93	0.616	1.927	1.636	15%
10.0	45.9	1.02	0.0028	0.00333	1.19	0.658	1.189	1.017	15%
10.0	70.0	1.03	0.00288	0.00197	0.684	0.677	0.684	0.618	10%
10.0	45.9	0.55	0.0032	0.0014	0.436	0.752	0.438	0.373	14%
10.0	45.9	0.89	0.00352	0.00333	0.946	0.827	0.946	0.807	15%
10.0	45.9	2.48	0.00336	0.0136	4.02	0.790	4.048	4.317	-7%
10.0	45.9	4.66	0.00261	0.0151	5.72	0.613	5.785	6.352	-11%

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Table V. Uranium Distribution Data from DP-1384 Tables 1 & 4 for 23C and Comparison with SEPHIS Results.

HNO3a M	Ua M	rho g/ml	ANN M	HNO3o M	Uo M	Ua g/l	Doa HNO3	Doa U	Sephis Error HNO3	Sephis Error U
0.114	0.9100	1.29	0	0.004	0.115	213.85	0.035	0.126	76%	-6%
0.108	0.4200	1.14	0	0.003	0.077	98.70	0.028	0.183	52%	-10%
0.105	0.2100	1.07	0	0.002	0.036	49.35	0.019	0.171	21%	-18%
0.103	0.0730	1.03	0	0.001	0.0063	17.16	0.010	0.086	-20%	-25%
0.100	0.0370	1.01	0	0.001	0.0021	8.695	0.010	0.057	9%	-17%
0.100	0.0197	1.01	0	(0.001)	0.00074	4.630	(0.010)	0.038	177%	-27%
0.100	0.0098	1.00	0	(0.001)	0.00031	2.303	(0.010)	0.032	168%	-20%
0.100	0.0050	1.00	0	(0.001)	0.00017	1.175	(0.010)	0.034	164%	2%
0.11	0.000211		0	(0.001)	5.3E-06	0.050	(0.009)	0.025	171%	-34%
0.52	0.87	1.30	0	0.006	0.118	204.45	0.012	0.136	30%	-5%
0.51	0.68	1.24	0	0.006	0.111	159.80	0.012	0.163	19%	-5%
0.51	0.56	1.19	0	0.006	0.101	131.60	0.012	0.180	8%	-9%
0.51	0.41	1.15	0	0.007	0.091	96.35	0.014	0.222	6%	-7%
0.50	0.27	1.10	0	0.008	0.071	63.45	0.016	0.263	2%	-9%
0.50	0.192	1.08	0	0.008	0.056	45.12	0.016	0.292	-10%	-10%
0.50	0.114	1.05	0	0.009	0.036	26.79	0.018	0.316	-9%	-13%
0.50	0.059	1.03	0	0.009	0.022	13.87	0.018	0.373	-16%	0%
0.50	0.045	1.03	0	0.009	0.0150	10.58	0.018	0.333	-18%	-13%
0.50	0.0150	1.02	0	0.009	0.0050	3.525	0.018	0.333	-20%	-11%
0.50	0.0076	1.02	0	0.009	0.0023	1.786	0.018	0.303	-20%	-22%
0.50	0.0046	1.02	0	0.009	0.00141	1.081	0.018	0.307	-20%	-20%
1.01	0.55	1.21	0	0.011	0.110	129.25	0.011	0.200	7%	-5%
1.04	0.41	1.16	0	0.012	0.102	96.35	0.012	0.249	-3%	-6%
1.03	0.26	1.12	0	0.014	0.087	61.10	0.014	0.335	-11%	-7%
1.04	0.180	1.09	0	0.017	0.075	42.300	0.016	0.417	-9%	-8%
1.02	0.095	1.06	0	0.020	0.055	22.325	0.020	0.579	-15%	-6%
1.00	0.044	1.05	0	0.023	0.036	10.340	0.023	0.818	-18%	3%
1.03	0.033	1.04	0	0.026	0.027	7.755	0.025	0.818	-15%	-8%
1.03	0.021	1.04	0	0.029	0.0191	4.935	0.028	0.910	-10%	-8%
1.04	0.0101	1.03	0	0.030	0.0105	2.374	0.029	1.040	-16%	-7%
1.01	0.0044	1.03	0	0.032	0.0055	1.034	0.032	1.250	-8%	10%
0.95	0.00011		0	0.03	9.90E-05	0.026	0.032	0.900	-8%	-18%
2.03	0.69	1.28	0	0.015	0.120	162.15	0.007	0.174	-9%	-3%
2.02	0.54	1.24	0	0.018	0.116	126.90	0.009	0.215	-3%	-4%
2	0.40	1.19	0	0.020	0.112	94.00	0.010	0.280	-10%	-3%
2.04	0.24	1.15	0	0.026	0.104	56.40	0.013	0.433	-9%	-2%
2.02	0.076	1.09	0	0.042	0.084	17.86	0.021	1.105	-10%	6%
1.96	0.030	1.08	0	0.058	0.051	7.050	0.030	1.700	-7%	-4%
2.02	0.020	1.07	0	0.064	0.040	4.700	0.032	2.000	-11%	-10%
1.98	0.0119	1.07	0	0.074	0.028	2.797	0.037	2.353	-6%	-12%
2.16	0.0055	1.07	0	0.096	0.0152	1.293	0.044	2.764	-2%	-31%
2.11	0.0025	1.06	0	0.098	0.0079	0.588	0.046	3.160	-5%	-27%
2.16	4.80E-05		0	0.105	1.63E-04	0.011	0.049	3.396	-9%	-40%
2.85	0.54	1.26	0	0.022	0.118	126.90	0.008	0.219	-12%	-3%
2.91	0.38	1.22	0	0.028	0.114	89.30	0.010	0.300	-7%	-2%
3.00	0.24	1.18	0	0.035	0.108	56.40	0.012	0.450	-10%	-2%
3.10	0.148	1.15	0	0.042	0.099	34.78	0.014	0.669	-17%	-3%
3.10	0.067	1.12	0	0.062	0.088	15.75	0.020	1.313	-11%	2%
3.10	0.024	1.12	0	0.092	0.060	5.640	0.030	2.500	-8%	-4%
3.00	0.0143	1.10	0	0.106	0.045	3.361	0.035	3.147	-7%	-8%
3.10	0.0083	1.10	0	0.122	0.032	1.951	0.039	3.855	-8%	-14%
3.00	0.0033	1.10	0	0.142	0.0158	0.776	0.047	4.788	-5%	-20%
3.10	0.00162	1.10	0	0.152	0.0087	0.381	0.049	5.370	-9%	-24%
2.90	3.60E-05		0	0.150	1.87E-04	0.008	0.052	5.194	-11%	-39%

(..) Less than value

Table V. Uranium Distribution Data from DP-1384 Tables 1 & 4 for 23°C and Comparison with SEPHIS Results (continued).

HNO _{3a} M	Ua M	rho g/ml	ANN M	HNO _{3o} M	Uo M	Ua g/l	Doa HNO ₃	Doa U	Sephis Error HNO ₃	Sephis Error U
4.20	0.39	1.26	0	0.032	0.109	91.65	0.008	0.279	-22%	-6%
4.20	0.24	1.21	0	0.040	0.103	56.40	0.010	0.429	-23%	-6%
4.20	0.152	1.18	0	0.050	0.097	35.72	0.012	0.638	-22%	-6%
4.10	0.067	1.16	0	0.072	0.082	15.75	0.018	1.224	-17%	-7%
4.10	0.021	1.14	0	0.110	0.058	4.935	0.027	2.762	-16%	-5%
4.10	0.0132	1.14	0	0.125	0.047	3.102	0.030	3.561	-17%	-6%
4.10	0.0070	1.13	0	0.150	0.032	1.645	0.037	4.571	-13%	-10%
4.10	0.0030	1.13	0	0.170	0.018	0.705	0.041	6.000	-15%	-10%
3.8	2.70E-05		0	0.200	1.90E-04	0.006	0.053	7.037	-7%	-24%
4.50	0.39	1.27	0	0.040	0.116	91.65	0.009	0.297	-3%	1%
4.40	0.147	1.19	0	0.060	0.103	34.55	0.014	0.701	-6%	2%
4.30	0.0193	1.15	0	0.130	0.059	4.536	0.030	3.057	-4%	1%
4.40	0.0066	1.14	0	0.160	0.036	1.551	0.036	5.455	-12%	6%
4.40	0.0028	1.14	0	0.185	0.0180	0.658	0.042	6.429	-11%	-3%
4.5	2.40E-05		0	0.22	1.86E-04	0.006	0.049	7.750	-8%	-12%
5.30	0.100	1.27	0.51	0.08	0.094	23.50	0.015	0.940		
4.30	0.096	1.24	0.56	0.07	0.096	22.56	0.016	1.000		
3.20	0.093	1.21	0.56	0.06	0.099	21.86	0.019	1.065		
2.10	0.093	1.18	0.56	0.04	0.097	21.86	0.019	1.043		
1.08	0.099	1.14	0.54	0.02	0.093	23.27	0.019	0.939		
0.55	0.104	1.13	0.55	0.01	0.088	24.44	0.018	0.846		
3.80	0.094	1.30	1.06	0.07	0.101	22.09	0.018	1.074		
2.70	0.090	1.27	1.05	0.05	0.107	21.15	0.019	1.189		
1.61	0.086	1.24	1.07	0.04	0.110	20.21	0.025	1.279		
0.57	0.087	1.20	1.12	0.02	0.111	20.45	0.035	1.276		
2.20	0.088	1.32	1.62	0.05	0.109	20.68	0.023	1.239		
1.16	0.081	1.29	1.61	0.03	0.114	19.04	0.026	1.407		
0.62	0.078	1.28	1.62	0.02	0.122	18.33	0.032	1.564		
1.01	0.000076	1.26	1.61	0.19	0.0057	0.018	0.188	75.000		
0.97	0.000147	1.26	1.62	0.18	0.0104	0.035	0.186	70.748		
1.04	0.000840	1.27	1.62	0.15	0.039	0.197	0.144	46.429		
1.07	0.00181	1.27	1.61	0.12	0.060	0.425	0.112	33.149		
1.10	0.0044	1.27	1.60	0.09	0.074	1.034	0.082	16.818		
1.13	0.0095	1.27	1.62	0.07	0.091	2.233	0.062	9.579		
1.11	0.038	1.28	1.60	0.04	0.125	8.930	0.036	3.289		
0.64	0.075	1.35	2.10	0.02	0.125	17.63	0.031	1.667		

Table VI. Uranium Distribution Data from DP-1384 Tables 2 & 5 for 45°C and Comparison with SEPHIS Results.

HNO3a M	Ua M	rho g/ml	ANN M	HNO3o M	Uo M	Ua g/l	Doa HNO3	Doa U	Sephis Error HNO3	Sephis Error U
0.116	0.84	1.28	0	0.0030	0.1090	197.40	0.026	0.130	59%	-4%
0.106	0.42	1.14	0	0.0020	0.0670	98.70	0.019	0.160	18%	-8%
0.105	0.22	1.07	0	0.0020	0.0260	51.70	0.019	0.118	15%	-25%
0.104	0.072	1.02	0	0.0010	0.0034	16.92	0.010	0.047	-15%	-34%
0.101	0.038	1.01	0	0.0020	0.001180	8.930	0.020	0.031	56%	-24%
0.100	0.0189	1.01	0		0.000460	4.442	0.000	0.024		-8%
0.101	0.0091	1.00	0		0.000190	2.139	0.000	0.021		-1%
0.096	0.0048	1.00	0		0.000110	1.128	0.000	0.023		24%
0.520	0.71	1.24	0	0.0060	0.1060	166.85	0.012	0.149	2%	-6%
0.500	0.55	1.19	0	0.0080	0.0930	129.25	0.016	0.169	17%	-9%
0.500	0.42	1.15	0	0.0090	0.0840	98.70	0.018	0.200	15%	-5%
0.500	0.28	1.11	0	0.0090	0.0600	65.80	0.018	0.214	1%	-11%
0.500	0.20	1.08	0	0.0090	0.0440	47.00	0.018	0.220	-8%	-14%
0.500	0.12	1.06	0	0.0090	0.0240	28.20	0.018	0.200	-15%	-27%
0.490	0.065	1.03	0	0.0120	0.0153	15.28	0.024	0.235	15%	-1%
0.490	0.050	1.03	0	0.0100	0.0118	11.75	0.020	0.236	-2%	2%
0.500	0.0172	1.02	0	0.0100	0.0033	4.042	0.020	0.192	-2%	-13%
0.510	0.0084	1.02	0	0.0100	0.0016	1.974	0.020	0.193	-5%	-13%
0.500	0.005	1.02	0	0.0090	0.0010	1.175	0.018	0.192	-12%	-9%
1.030	0.70	1.26	0	0.0140	0.1090	164.50	0.014	0.156	22%	-7%
1.030	0.55	1.21	0	0.0160	0.1010	129.25	0.016	0.184	21%	-9%
1.030	0.42	1.17	0	0.0170	0.0930	98.70	0.017	0.221	14%	-8%
1.030	0.28	1.12	0	0.0190	0.0770	65.80	0.018	0.275	6%	-11%
1.030	0.185	1.09	0	0.0200	0.0630	43.48	0.019	0.341	-5%	-9%
1.030	0.11	1.07	0	0.0230	0.0440	25.62	0.022	0.404	-8%	-13%
1.020	0.05	1.05	0	0.0260	0.0260	12.69	0.025	0.481	-9%	-13%
1.010	0.0400	1.04	0	0.0260	0.0200	9.400	0.026	0.500	-12%	-13%
1.02	0.026	1.04	0	0.027	0.0143	6.110	0.026	0.550	-15%	-10%
1.02	0.0125	1.04	0	0.028	0.0074	2.938	0.027	0.592	-16%	-9%
1.02	0.0062	1.03	0	0.03	0.0038	1.457	0.029	0.613	-11%	-9%
1.04	0.0037	1.03	0	0.03	0.0022	0.870	0.029	0.595	-16%	-18%
2.04	0.69	1.29	0	0.023	0.112	162.15	0.011	0.162	13%	-8%
2.03	0.54	1.24	0	0.026	0.11	126.90	0.013	0.204	12%	-6%
2.02	0.40	1.2	0	0.028	0.104	94.00	0.014	0.260	5%	-6%
2.02	0.26	1.15	0	0.036	0.09	61.10	0.018	0.346	9%	-12%
2.03	0.166	1.12	0	0.04	0.081	39.01	0.020	0.488	0%	-10%
2.00	0.087	1.09	0	0.049	0.063	20.45	0.025	0.724	-3%	-12%
2.02	0.038	1.08	0	0.066	0.044	8.930	0.033	1.158	0%	-9%
2.01	0.027	1.07	0	0.073	0.035	6.345	0.036	1.296	2%	-12%
2.00	0.0169	1.07	0	0.078	0.023	3.972	0.039	1.361	0%	-24%
2.00	0.0072	1.06	0	0.086	0.0125	1.692	0.043	1.736	-2%	-18%
2.00	0.0033	1.06	0	0.089	0.0063	0.776	0.045	1.909	-4%	-18%
2.00	0.00173	1.06	0	0.09	0.0032	0.407	0.045	1.850	-6%	-27%
2.8	0.55	1.27	0	0.033	0.112	129.25	0.012	0.204	11%	-5%
2.9	0.40	1.22	0	0.039	0.105	94.00	0.013	0.263	9%	-7%
2.9	0.26	1.18	0	0.048	0.098	61.10	0.017	0.377	9%	-7%
3.0	0.159	1.15	0	0.058	0.089	37.37	0.019	0.560	4%	-8%
3.0	0.078	1.12	0	0.078	0.071	18.33	0.026	0.910	5%	-12%
3.0	0.031	1.11	0	0.098	0.051	7.285	0.033	1.645	-4%	-10%
3.0	0.021	1.1	0	0.118	0.038	4.935	0.039	1.810	4%	-22%
3.0	0.0052	1.1	0	0.143	0.0158	1.222	0.048	3.038	-2%	-17%
3.0	0.0025	1.1	0	0.154	0.0076	0.588	0.051	3.040	-1%	-32%
3.0	0.00137	1.1	0	0.156	0.0038	0.322	0.052	2.774	-3%	-54%

Table VI. Uranium Distribution Data from DP-1384 Tables 2 & 5 for 45°C and Comparison with SEPHIS Results (continued).

HNO _{3a} M	U _a M	rho g/ml	ANN M	HNO _{3o} M	U _o M	U _a g/l	Doa HNO ₃	Doa U	Sephis Error HNO ₃	Sephis Error U
4.2	0.39	1.26	0	0.048	0.105	91.65	0.011	0.269	1%	-5%
4.2	0.25	1.21	0	0.057	0.1	58.75	0.014	0.400	-2%	-4%
4.2	0.162	1.18	0	0.066	0.09	38.07	0.016	0.556	-7%	-7%
4.1	0.075	1.16	0	0.093	0.074	17.63	0.023	0.987	-2%	-9%
4.1	0.028	1.15	0	0.128	0.052	6.580	0.031	1.857	-4%	-10%
4.1	0.0193	1.14	0	0.146	0.041	4.536	0.036	2.124	-1%	-17%
4.1	0.0112	1.13	0	0.164	0.029	2.632	0.040	2.589	-2%	-23%
4.1	0.0048	1.13	0	0.181	0.0156	1.128	0.044	3.250	-6%	-28%
4	0.0022	1.13	0	0.198	0.0081	0.517	0.050	3.682	-3%	-31%
4.0	0.00109	1.13	0	0.2	0.0042	0.256	0.050	3.853	-6%	-34%
4.5	0.40	1.27	0	0.05	0.105	94.00	0.011	0.263	2%	-5%
4.4	0.153	1.19	0	0.08	0.09	35.96	0.018	0.588	7%	-5%
4.2	0.028	1.15	0	0.14	0.05	6.580	0.033	1.786	4%	-14%
4.3	0.0108	1.14	0	0.18	0.029	2.538	0.042	2.685	4%	-20%
4.2	0.0045	1.14	0	0.2	0.0148	1.058	0.048	3.289	2%	-29%
4.2	0.0021	1.14	0	0.2	0.0077	0.494	0.048	3.667	-5%	-32%
4.2	0.00105	1.14	0	0.2	0.0038	0.247	0.048	3.619	-9%	-44%
5.20	0.110	1.28	0.51	0.101	0.080	25.85	0.019	0.727		
4.20	0.106	1.25	0.56	0.088	0.085	24.91	0.021	0.802		
3.20	0.104	1.21	0.56	0.070	0.088	24.44	0.022	0.846		
2.10	0.100	1.18	0.56	0.056	0.086	23.50	0.027	0.860		
1.06	0.107	1.15	0.54	0.029	0.086	25.15	0.027	0.804		
0.52	0.110	1.13	0.55	0.016	0.080	25.85	0.031	0.727		
3.70	0.102	1.30	1.06	0.082	0.090	23.97	0.022	0.882		
2.60	0.099	1.27	1.05	0.064	0.093	23.27	0.025	0.939		
1.66	0.090	1.24	1.07	0.045	0.096	21.15	0.027	1.067		
0.57	0.086	1.20	1.12	0.019	0.102	20.21	0.033	1.186		
2.20	0.091	1.33	1.62	0.058	0.100	21.39	0.026	1.099		
1.16	0.083	1.30	1.61	0.036	0.106	19.51	0.031	1.277		
0.63	0.077	1.28	1.62	0.021	0.109	18.10	0.033	1.416		
0.96	0.00013	1.26	1.61	0.20	0.0052	0.0306	0.208	40.000		
0.98	0.00025	1.26	1.62	0.19	0.0094	0.059	0.194	37.600		
1.05	0.00151	1.27	1.62	0.14	0.037	0.355	0.133	24.503		
1.10	0.0035	1.27	1.61	0.12	0.055	0.823	0.109	15.714		
1.10	0.0073	1.27	1.60	0.09	0.069	1.716	0.082	9.452		
1.14	0.0109	1.27	1.62	0.07	0.078	2.562	0.061	7.156		
1.17	0.043	1.28	1.60	0.04	0.101	10.11	0.034	2.349		
0.66	0.073	1.35	2.10	0.026	0.114	17.16	0.039	1.562		

Table VII. Uranium Distribution Data from DP-1384 Table 3 for 60°C and Comparison with SEPHIS Results.

HNO _{3a} M	U _a M	rho g/ml	ANN M	HNO _{3o} M	U _o M	rho g/ml	U _a g/l	Doa HNO ₃	Doa U	Sephis H	Sephis Error U
0.105	0.87	1.29	0	0.0038	0.101	0.81	204.5	0.036	0.116	67%	-10%
0.105	0.44	1.14	0	0.0021	0.057	0.79	103.4	0.020	0.130	17%	-18%
0.103	0.22	1.07	0	0.0011	0.021	0.78	51.7	0.011	0.095	-56%	-23%
0.103	0.076	1.02	0	0.0005	0.0026	0.77	17.86	0.005	0.034	-134%	-38%
0.104	0.039	1.01	0	0.0004	0.000690	0.77	9.165	0.004	0.018	-104%	-61%
0.100	0.020	1.01	0	0.0005	0.000240	0.77	4.700	0.005	0.012	-27%	-58%
0.102	0.0095	1.00	0	0.0008	0.000080	0.77	2.233	0.008	0.008	22%	-80%
0.100	0.0050	1.00	0	0.0009	0.000010	0.77	1.175	0.009	0.002	34%	-554%
4.600	0.42	1.27	0	0.0710	0.098	0.80	98.70	0.015	0.233	9%	-49%
4.500	0.166	1.20	0	0.0930	0.082	0.80	39.01	0.021	0.494	13%	-11%
4.400	0.0350	1.15	0	0.1560	0.044	0.79	8.225	0.035	1.257	10%	-27%
4.300	0.0153	1.14	0	0.1810	0.025	0.78	3.596	0.042	1.634	6%	-46%
4.300	0.0065	1.14	0	0.2000	0.0143	0.78	1.528	0.047	2.200	2%	-43%
4.300	0.0031	1.14	0	0.2100	0.0075	0.78	0.729	0.049	2.419	0%	-50%
4.400	0.0016	1.14	0	0.2200	0.0052	0.78	0.371	0.050	3.291	-1%	-19%

Distribution

N. M. Askew, 773-A
N. E. Barnett, 707-F
S. E. Booth, 221-H
D. W. Braselman, 221-H
T. G. Campbell, 221-F
M. C. Chandler, 704-2H
D. L. Dolin, 704-2H
J. L. Dunning, 221-H
W. G. Dyer, 704-2H
O. M. Ebra-Lima, 707-F
R.E. Edwards, 704-2H (DOE)
J. S. Evans, 703-F
S. E. Federman, 704-2H
R. A. Frushour, 704-2H
C. R. Goergen, 221-H
A. P. Gouge, 735-11A
F. R. Graham, 773-A
J. H. Gray, 773-A
M.E. Hodges, 773-41A
D. R. Johnson, 704-2H
D.G. Karraker, 773-A
J. C. Knight, 704-2H
J. R. Knight, 773-A
E. A. Kyser, 773-A
C. E. Pickett, 221-H
T. S. Rudisill, 773-A
T.M. Smith, 703-F (DOE)
M. C. Thompson, 773-A
G. J. Winkler, 703-F
C. R. Wolfe, 773-A