

CONF-970335--42
ANL/ET/CP--90989
**IMMOBILIZATION OF FISSION PRODUCTS IN LOW-TEMPERATURE
CERAMIC WASTE FORMS***

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January 1997

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For publication in Proceedings of Waste Management '97 Conference, Tucson AZ, March 2-6, 1997.

*Work supported by the U.S. Department of Energy, Office of Technology Development (EM-50), as part of the Efficient Separations and Processing Crosscutting Program, under Contract W-31-109-Eng-38.

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IMMOBILIZATION OF FISSION PRODUCTS IN LOW-TEMPERATURE CERAMIC WASTE FORMS

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ABSTRACT

Over the last few years, Argonne National Laboratory has been developing room-temperature-setting chemically bonded phosphate ceramics (CBPCs) for use in solidifying and stabilizing low-level mixed wastes. The focus of this work is development of CBPCs for use with fission-product wastes generated from high-level waste (HLW) tank cleaning or other decontamination and decommissioning activities. The volatile fission products such as Tc, Cs, and Sr removed from HLW need to be disposed of in a low-temperature immobilization system. Specifically, this paper reports on the solidification and stabilization of separated ^{99}Tc from Los Alamos National Laboratory's complexation-elution process. Using rhenium as a surrogate for technetium, we fabricated CBPC waste forms by acid-base reactions. Dense and hard ceramic waste forms are produced in this process. The principal advantage of this technology is that the contaminants are immobilized by both chemical stabilization and subsequent microencapsulation of the reaction products. This paper reports the results of durability studies conducted on waste forms made with 35 wt.% waste loading. Standard leaching tests such as ANS 16.1 and PCT were

conducted on the final waste forms. In addition, stability of the waste forms in aqueous environments was evaluated by long-term water-immersion tests.

INTRODUCTION

The current volume of high-level waste (HLW) across the Department of Energy (DOE) complex is several hundred thousand cubic meters. The presence of fission products such as ^{99}Tc in the HLW poses myriad problems; this radionuclide, for example, is highly volatile and may escape into offgas during HLW vitrification, thus generating a secondary waste stream that requires additional stabilization/solidification (S/S). Technetium is readily oxidized to a highly soluble pertechnetate form that is extremely difficult to immobilize. Technetium and cesium (^{135}Cs) have extremely long half-lives ($\approx 10^6$ years) and require a durable immobilization system.

The approach that is being considered is to remove fission products from HLW and dispose of them separately. Removing fission products from the HLW reduces the overall waste volume and radioactivity levels of HLW, thus simplifying waste-handling operations. In this regard, several separation technologies are being developed as part of DOE's Efficient Separations and Processing Crosscutting Program. These separation technologies, along with other decontamination activities, result in waste streams that are rich in fission products and, if not returned to the bulk HLW stream, require S/S for safe disposal in compliance with federal regulations. Currently, no robust and reliable low-temperature technologies are available to immobilize these fission-product wastes. A low-temperature stabilization and immobilization technology could produce durable waste forms for long-term storage and disposal of the fission products and/or the "loaded" separating agents used to remove fission

products from the HLW streams. To this end, we are developing and demonstrating a low-temperature treatment and stabilization technology based on chemically bonded phosphate ceramics (CBPC).

CBPCs are dense and hard materials that can be processed at low temperatures [1,2]. Phosphates exhibit high solid-solution capacity for incorporating heavy metals, actinides, and rare-earth contaminants [3]. Also, the very low solubilities of phosphates of heavy metals, actinides, and rare earths [4] indicate that phosphate-bonded ceramics should be effective in stabilizing these contaminants. In addition, the durable natural-analog monazite and apatite minerals [5] suggest that phosphates are good hosts for radionuclides. The present developmental program on phosphate waste forms is being conducted to utilize their attractive properties in S/S of fission products, especially ^{99}Tc , because fabrication can be achieved at room temperature or slightly elevated temperatures to minimize off-gassing.

The goal of this work is to incorporate simulated wastes of partitioned ^{99}Tc generated by the Los Alamos National Laboratory (LANL) complexation-elution process in magnesium-phosphate-based ceramic systems, and to conduct assessments of the resulting waste forms to establish their performance. In addition, physical and microstructural characteristics of the final waste forms are being determined to gain insight into the stabilization mechanisms of the phosphate ceramics and the durability of the final waste forms. Results to date show that phosphate ceramics are a viable S/S technology for treating ^{99}Tc -containing waste streams.

FABRICATION OF CBPC WASTE FORMS

Phosphate-bonded ceramics can be classified as acid-base cements because they are fabricated by chemical reactions between an oxide powder and an acid solution. A magnesium phosphate ceramic was prepared by reacting calcined magnesium oxide powder with an acid solution [6]. Particle size of the starting magnesium oxide powder was $\approx 8 \mu\text{m}$. The powder was continuously added to the acid solution, and the mixture was vigorously mixed to a desired consistency and then transferred to a mold and allowed to set. The mix hardened in ≈ 2 h to form hard and dense monoliths. After complete curing for >7 days, the monoliths were removed from the molds for physical and chemical evaluation.

Specific CBPCs are being developed for S/S of ^{99}Tc partitioned from HLW by LANL's sorption process. Surrogate formulations of the separated Tc waste stream based on LANL's complexation-elution process have been prepared and the waste subsequently incorporated in the phosphate ceramic. However, in this work, Re was used as a surrogate for Tc. The composition of the waste stream used was 1 M NaOH, 1 M ethylenediamine, and 0.005 M Sn(II) and 0.00005 M Re [7]. Loading of the waste stream in the final waste form was $\approx 35\text{-}40$ wt.%. The final waste forms were fabricated by mixing the liquid waste with the acid solution in desired weight percentages. Rhenium was added so that in the final waste forms its content was 3 ppm. In addition, CBPC waste forms were fabricated in which Re was directly added as $\text{ReO}_2 \cdot 2\text{H}_2\text{O}$. The net Re content in these waste forms was maintained at either 5 or 50 ppm, which is the expected range of ^{99}Tc in the actual waste. Subsequently, the powders were added at a slow rate and thoroughly mixed. The slurry was then poured

into a mold and allowed to set. After complete setting, all of the specimens formed hard ceramics that were used for further evaluation.

RESULTS AND DISCUSSION

Physical properties

Density of the magnesium phosphate-LANL waste forms with 35 wt.% loading was 1.8 g/cm^3 . The corresponding porosity was 4%. Such low porosity values are highly desirable for minimizing water intrusion in the final waste form.

Phase analysis

Figure 1 shows an X-ray diffraction (XRD) pattern of the CBPC-36 wt.% eluted waste form. The major phase is of magnesium phosphate system, a highly insoluble phase. In addition, there is some unreacted magnesium oxide. Using XRD on the final waste forms, we determined that both crystalline and noncrystalline phases of magnesium phosphate are present as the binding

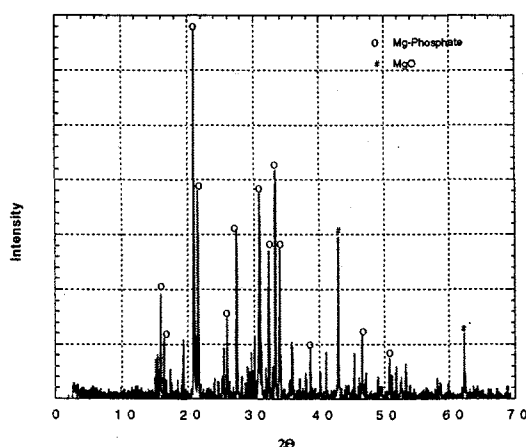


Fig. 1.
XRD Pattern of CBPC-35 wt.%
Eluted Waste Form.

phases. Analysis of noncrystalline phases, which is much more complex and requires a combination of techniques, is currently the focus of our work.

Microstructural analysis

Figure 2 is a photomicrograph of the fracture surface of CBPC-35 wt.% eluted waste form. As seen in this figure, the fabricated ceramic is extremely dense. Needlelike crystals of the magnesium phosphate phase are evident. Scanning electron microscopy (SEM) was also used to map the distribution of the metal contaminants in the magnesium phosphate final waste form. Rhenium was found to be well distributed and physically microencapsulated by the phosphate matrix, and we believe that this phenomenon, along with chemical stabilization, leads to excellent performance of the phosphate systems in preventing leaching of the Re during the tests discussed below. It is expected that Tc will behave similarly.

Compression strength

Compression strength of fully cured waste form samples was measured with an Instron machine on samples of 0.5 in. diameter and 1-2 in. length. For monolithic magnesium phosphate specimens, the average compression strength was 4320 ± 954 psi. This value is higher than those of other room-temperature-setting materials such as portland cement.

ANS 16.1 test

Leaching studies on the fabricated waste forms were conducted according to the standard American Nuclear Society's ANS 16.1 test and the Product Consistency Test (PCT) [8,9]. The ANS 16.1 test was followed to evaluate the

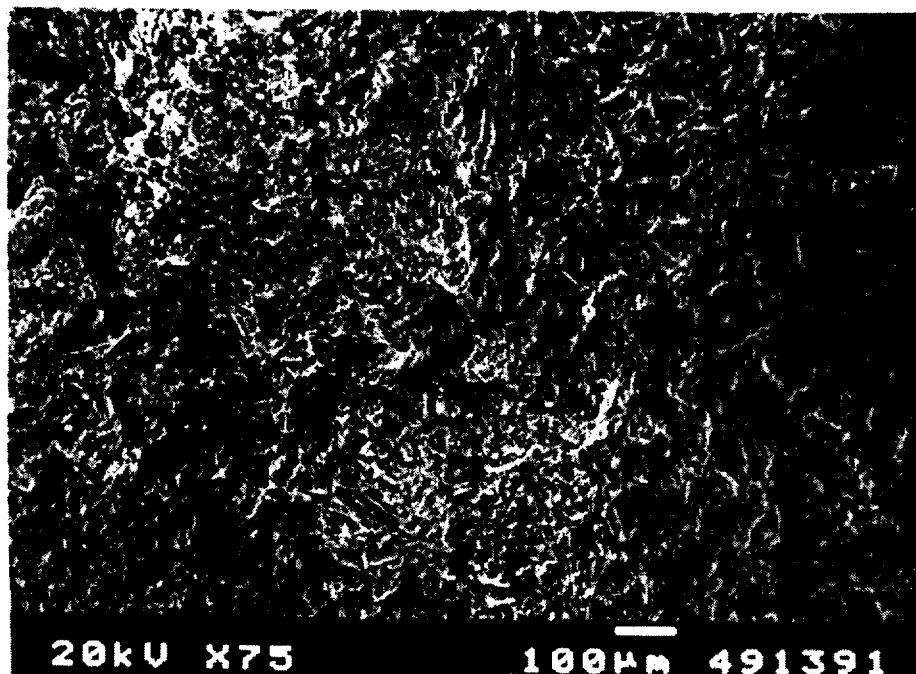


Fig. 2. SEM Photomicrograph of Fracture Surface of CBPC-35 wt.% Eluted Re Final Waste Form.

diffusion constants and the leachability indexes for Re; results are presented in Table 1. As expected, diffusivity of the contaminants is extremely low, indicating excellent stabilization of Re in the phosphate matrix system. The determined leachability indexes range from 10 for 3 ppm loading to as high as 12 for 50 ppm Re loading, significantly higher than Nuclear Regulatory Commission's passing criterion of 6. (A higher leachability index indicates better retention of the contaminant in the final waste form.) These results are further evidence of the superior containment characteristics of the CBPC final waste forms. The reason for this superior immobilization is chemical stabilization of the contaminants in the matrix due to reaction between the contaminant and the acid solution, followed by physical encapsulation within the dense phosphate matrix. Also, physical encapsulation immobilizes the contaminants in the matrix, thus forming an excellent final waste form.

Table 1. Diffusion Constants and Leachability Indices for Re in CBPC-Eluted Re Waste Forms

Waste Form	Re Contaminant Loading (ppm)	Diffusion Constant (cm ² /s)	Leachability Index
CBPC + 36 wt.% LANL eluted waste	3	1×10^{-10}	11.3
CBPC + ReO ₂ .2H ₂ O	5	6×10^{-9}	10.4
CBPC + ReO ₂ .2H ₂ O	50	9×10^{-13}	12.4

Product Consistency Test

Product Consistency Test (PCT) was conducted on CBPC-bonded 35 wt.% LANL eluted waste, and also on CBPC waste forms in which Re was directly added as ReO₂.2H₂O to concentrations of 5 and 50 ppm of Re in the final waste form. PCT tests were carried out at 90°C for 7 days in Teflon containers holding 1 g of 100-200 mesh waste form particles in 10 mL of deionized water. Table 2 summarizes the leaching rates observed for each type of waste form sample; leaching of Re is extremely low for all three samples. These values are significantly lower than those reported for ⁹⁹Tc release from borosilicate glass (≈ 0.12 g/m²) [10]. Moreover, no significant change was observed in the leaching rate of Re with an increase in concentration of Re in the waste form. It is clear that Re cannot act completely as a surrogate for ⁹⁹Tc, but based on redox chemistry, it is more prone to becoming oxidized to the perrhennate form that is ⁹⁹Tc to the pertechnetate form. Hence, Re is more susceptible to leaching out than ⁹⁹Tc.

Table 2. Results of PCT on Phosphate-Bonded Waste Forms

Waste Form	Re Conc. (ppm)	Leaching Rate (g/m ² -d)
CBPC + 36 wt.% LANL eluted waste	3	9.8×10^{-4}
CBPC + ReO ₂ .2H ₂ O	5	8.5×10^{-4}
CBPC + ReO ₂ .2H ₂ O	50	3.6×10^{-4}

Long-term water immersion study

To study the long-term durability of the final waste forms in an aqueous environment, water immersion studies were initiated. As done for the ANS 16.1 standard, samples were immersed in deionized water (pH \approx 5.5). Samples were removed at regular intervals, dried, and weighed to observe any weight change. Results for CBPC-36 wt.% eluted waste forms are shown in Fig. 3. Initially, an increase in weight was observed. Thereafter, the weight of the sample decreased and held constant. It is not clear why there was an initial weight increase and then a subsequent decrease, but the cause was probably interaction of unreacted MgO and water. After 90 days, only a small decrease (\approx 0.5 wt.%) was seen in the weight of the specimens immersed in the deionized water.

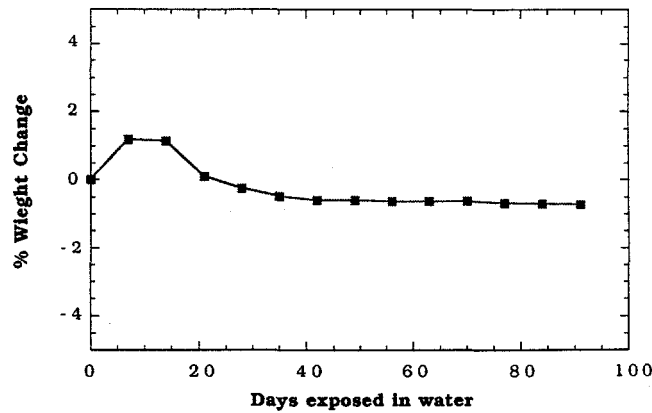


Fig. 3. Variation in Weight of CBPC-35 wt.% LANL Eluted Final Waste Forms Exposed to Deionized Water.

Compression strength before and after water immersion test

Figure 4 compares the average compression strength of the CBPC-35 wt.% eluted waste forms before and after long-term (90-day) water immersion tests. Specimen strength after exposure to deionized water were 1700 ± 372 psi. These values are lower than the average strength of the waste form before the long-term durability test (≈ 4320 psi). The resulting strength of the waste forms is exceptionally good and satisfies the regulatory requirements (>500 psi) after a 90-day exposure to an aqueous environment. The results given here for weight change and compression strength clearly indicate that CBPCs will be durable waste forms.

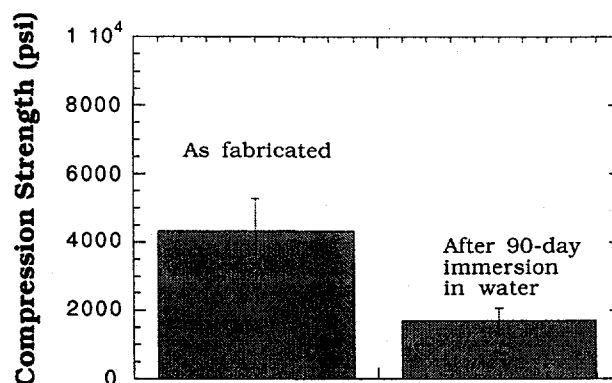


Fig. 4. Compression strengths of CPBC-35 wt.% Eluted Waste Forms in As-Fabricated State and after Exposure to Aqueous Environment.

SUMMARY

This paper reports on the durability of magnesium-phosphate-bonded ceramics for stabilization of eluted Tc wastes from sorption process at low temperatures. Physical and chemical characterization of phosphate materials has shown them to be physically, chemically, and mineralogically stable, with properties superior to those of other room-temperature-setting cements. Surrogate formulations of Tc eluted waste stream have been incorporated and stabilized in CBPCs at loadings of ≈ 35 wt.%. Long-term durability studies using the ANS 16.1 standard test) showed excellent containment of the radioactive surrogates (Re for Tc) in the phosphate matrix when exposed to deionized water. Excellent retainment of contaminants in the CBPC matrix was further confirmed by the PCT test. In addition, CBPC-based final waste forms showed no significant weight changes after exposure to aqueous media for ≈ 90 days, indicating the highly insoluble nature of the phosphate matrix.

ACKNOWLEDGMENT

This work has been supported by the U.S. Department of Energy, Office of Technology Development (EM-50), as part of the Efficient Separations and Processing Crosscutting Program, under Contract W-31-109-Eng-38.

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