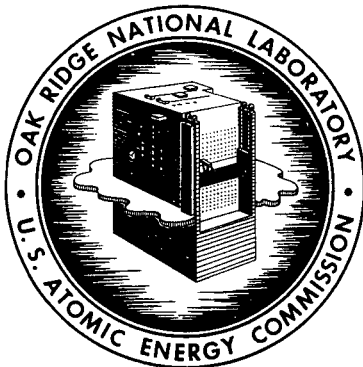


CENTRAL RESEARCH LIBRARY
DOCUMENT COLLECTION

OAK RIDGE NATIONAL LABORATORY
provided by
UNION CARBIDE CORPORATION
for the
U.S. ATOMIC ENERGY COMMISSION



ORNL - TM - 384

COPY NO. - 84

DATE - Sept. 26, 1962

U-Th RECOVERY FROM PYROLYTIC CARBON-COATED CARBIDE FUEL PARTICLES BY ELECTROLYSIS IN NITRIC ACID

A. H. Kibbey
L. M. Ferris

ABSTRACT

Electrodissolver experiments were conducted with pyrolytic carbon-coated UC_2-ThC_2 fuel particles in both a direct contact anode dissolver and a U-shaped "series" dissolver. Under the conditions investigated (HNO_3 concentration, 4-10 M; current density, 1-10 amp/cm²; temperature 25-80°C), uranium and thorium recoveries were less than 0.2%. The results of these experiments indicated that electrolytic methods are not adaptable to the processing of graphite-base reactor fuels containing carbon-coated particles.

CENTRAL RESEARCH LIBRARY
DOCUMENT COLLECTION
LIBRARY LOAN COPY
DO NOT TRANSFER TO ANOTHER PERSON
If you wish someone else to see this
document, send in name with document
and the library will arrange a loan

NOTICE

This document contains information of a preliminary nature and was prepared primarily for internal use at the Oak Ridge National Laboratory. It is subject to revision or correction and therefore does not represent a final report. The information is not to be abstracted, reprinted or otherwise given public dissemination without the approval of the ORNL patent branch, Legal and Information Control Department.

LEGAL NOTICE

This report was prepared as an account of Government sponsored work. Neither the United States, nor the Commission, nor any person acting on behalf of the Commission:

- A. Makes any warranty or representation, expressed or implied, with respect to the accuracy, completeness, or usefulness of the information contained in this report, or that the use of any information, apparatus, method, or process disclosed in this report may not infringe privately owned rights; or
- B. Assumes any liabilities with respect to the use of, or for damages resulting from the use of any information, apparatus, method, or process disclosed in this report.

As used in the above, "person acting on behalf of the Commission" includes any employee or contractor of the Commission, or employee of such contractor, to the extent that such employee or contractor of the Commission, or employee of such contractor prepares, disseminates, or provides access to, any information pursuant to his employment or contract with the Commission, or his employment with such contractor.

1.0 INTRODUCTION

The purpose of this memo is to summarize laboratory electrolytic experiments relating to the recovery of uranium and thorium from graphite-base reactor fuel elements which contain carbon-coated fuel particles. Prior work on the direct contact anodic disintegration in nitric acid of fuels which did not contain coated fuel particles resulted in nearly quantitative uranium recovery.¹⁻³ However, in preliminary experiments at ORNL with fuel specimens containing carbon-coated particles, it was shown that although the graphite matrix readily disintegrated when the fuel was made an anode in a nitric acid electrolyte the coated particles were virtually unaffected and the uranium and thorium recoveries were less than 5% (ref. 4). Similar results were obtained at BMI with irradiated coated particle fuels.⁵ To avoid the problems of direct contact of the anode with the fuel piece, "series" or "liquid contact" dissolvers were used at ICPP⁶ and SRL^{7,8} for the dissolution of metallic fuel elements. In this type of dissolver, the fuel pieces are not in contact with either electrode but become separate electrolytic cells under the influence of the overall potential gradient.

Two series of experiments, reported below, were conducted to determine cursorily the influence of nitric acid concentration, current density, and temperature on the recovery of uranium and thorium from a batch of carbon-coated fuel particles. It was hoped that conditions for penetrating the particle coatings could be discovered despite the prior evidence to the contrary. It was assumed that these conditions, if found, would also be satisfactory for recovering uranium and thorium from graphite-base coated particle fuels.

2.0 RESULTS

2.1 Disintegration of Graphite Fuel

Preliminary runs in the U-tube "series" dissolver (Sect. 3.0) using graphite fuel containing about 9% uranium as uncoated UO_2 particles, 10 M HNO_3 at 24°C, and an anode current density of about 1 amp/cm² indicated that under these conditions (which are probably not optimum) matrix disintegration does occur slowly with gas evolution at the anode end of the fuel piece. Reversing the polarity of the dissolver electrodes reversed the end of the specimen at which the gas was evolved. The electro-disintegration rate was much lower than the disintegration rate obtained with the same fuel in 90% HNO_3 (ref. 9). In 3- to 4-hr tests at 25°C, complete disintegration was achieved in 90% HNO_3 but only about 10% of the sample disintegrated in the "series" dissolver.

2.2 Experiments with Carbon-Coated UC₂-ThC₂ Particles

Two series of 7-hr experiments, one each in the direct contact anode and "series" dissolvers (Sect. 3.0), were conducted with Batch OR-1 carbon-coated UC₂-ThC₂

OAK RIDGE NATIONAL LABORATORY LIBRARIES



3 4456 0548955 7

particles to evaluate the effects of nitric acid concentration, current density, and temperature on the recovery of uranium and thorium. The UC_2 - ThC_2 particles were 147-417 microns in diameter and were coated with 55 to 60 microns of pyrolytic carbon. Only 0.006 and 0.025% of the uranium and thorium, respectively, was lost when a sample of the particles was leached for 5 hr in boiling 90% HNO_3 . This test indicated that the integrity of the particle coatings was sufficient for the electro-dissolver experiments.

Uranium and thorium recoveries, less than 0.04 and 0.2%, respectively, irrespective of the type of dissolver used (Table 1), were unacceptable for a fuel recovery process. These recoveries were essentially the same as those obtained by leaching the particles with nitric acid alone. Temperature had little effect on the recoveries; but, if a trend is indicated, the recoveries tend to decrease with increasing temperature (Table 1). At constant temperature and electrolyte concentration, an increase in current density from 1 to 10 amp/cm² increased recoveries by a factor of 2 to 3. Recoveries were 2- to 4-times higher in the direct contact anode dissolver than in the "series" dissolver, other pertinent conditions being the same.

The extreme conditions of (1) very high acid concentration at a high enough voltage to produce adequate current density and (2) low acid concentrations at high current density near the freezing points of the solutions were not scouted. The effects of additives to the nitric acid electrolyte, other electrolytes, and prolonged soaking of the particles prior to electrolysis were also not studied. Future work should probably be directed along these lines in addition to more experiments with pieces of coated particle fuels. However, the poor results obtained show that nitric acid electrolysis techniques do not warrant further major development effort. As time permits, additional scouting studies will be performed.

3.0 EXPERIMENTAL

The direct contact anode dissolver was a basket-type dissolver whose anode was fashioned from a small platinum crucible (about 0.7 cm² on the bottom) welded to a platinum wire. The cathode was a round disc of heavy platinum foil, about 2.5 cm in diameter, welded vertically onto a platinum wire electrode.

The "series" dissolver was a U-shaped, water-jacketed, tube similar to that described by Bomar⁶:

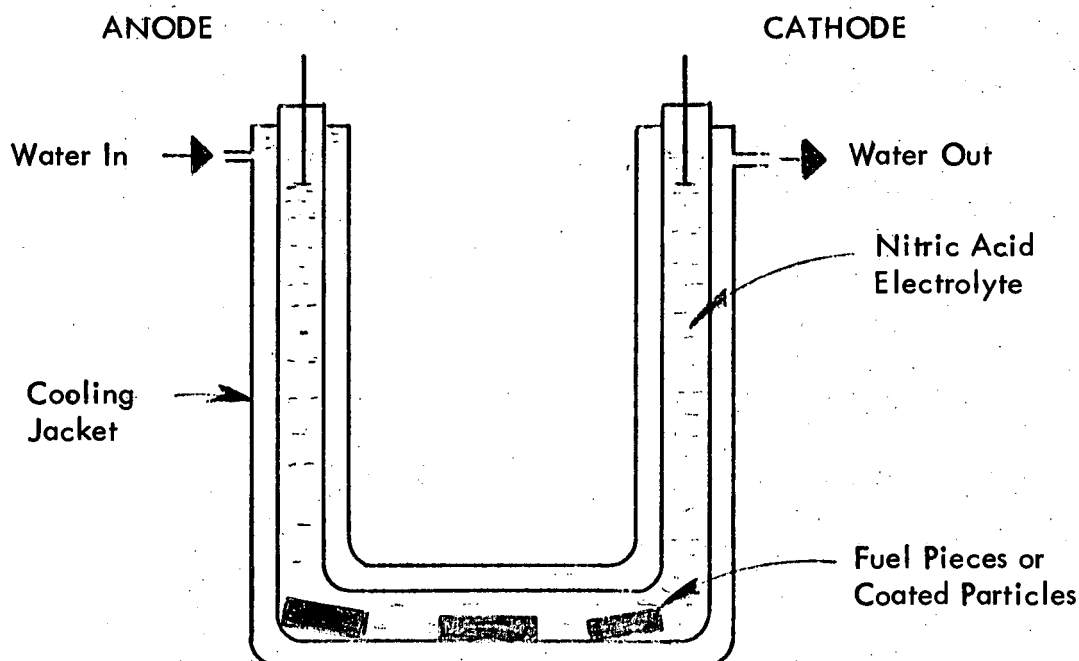
Table 1. Electrodissolver Experiments with Batch OR-1 Carbon-Coated UC₂-ThC₂ Fuel Particles

Conditions: Electrolysis time: 7 hr
Effective electrode areas: 0.7 cm²

Run No., OR-1-	Type of Dissolver	Fuel Comp., %		Temp., °C	Current Density amp/cm ²	HNO ₃ Conc., M	Recoveries, %	
		U	Th				U	Th
1B	None ^a	18.2	43.3	25	0	10	0.013	0.011
9	DA ^b	18.9	42.8	25	1.0	4	0.006	0.050
2	DA	15.0	33.8	30	1.0	10	0.020	0.16
11	DA	18.4	41.8	66	10	4	0.015	0.020
10	DA	18.1	42.3	67	10	10	0.030	0.050
8	Series	12.4	28.5	25	1.0	4	0.020	0.050
1	Series	17.1	37.4	25	1.0	10	0.015	0.014
3	Series	18.	41.	37	1.0	10	0.007	0.030
4	Series	19.2	42.6	52	1.0	10	0.014	0.035
5	Series	19.0	43.5	75-80	1.0	10	0.005	0.012
6	Series	18.7	43.6	32-45	10	10	0.008	0.009
7	Series	19.0	43.1	42	10	10	0.020	0.010

^aNo potential applied.

^bDA = direct contact anode dissolver.



The electrodes (area of each, 0.7 cm^2) are inserted into the open ends at the top of the vertical U-tube. Current, which passes through the electrolyte, causes formation of a separate electrolytic cell in each piece of fuel or particle.

Temperature was difficult to control in both dissolvers, but was especially so in the direct contact anode equipment which was essentially an open beaker with no condenser or cooling jacket. The "series" dissolver could be immersed in a constant temperature bath and was equipped with condensers on the off-gas vents, but the temperature gradient between the electrode and fuel specimen was often as much as 15°C , since there was no provision for circulation of the electrolyte.

Nitric acid concentrations above 13 molar were found to be poor electrolytes (Fig. 1). The investigation, therefore, was limited to acid concentrations in the range of 4 to 10 molar since current densities of 1 to 10 amps/cm^2 were desired. Higher current densities required higher voltages, and the amount of heat generated rendered the modest cooling system ineffective for preventing boiling of the electrolyte. In addition, at current densities greater than 10 amps/cm^2 , excessive foaming occurred which was attributable to increased electrochemical decomposition of the electrolyte at the higher voltage and elevated temperatures which resulted in rapid evolution of gaseous products.

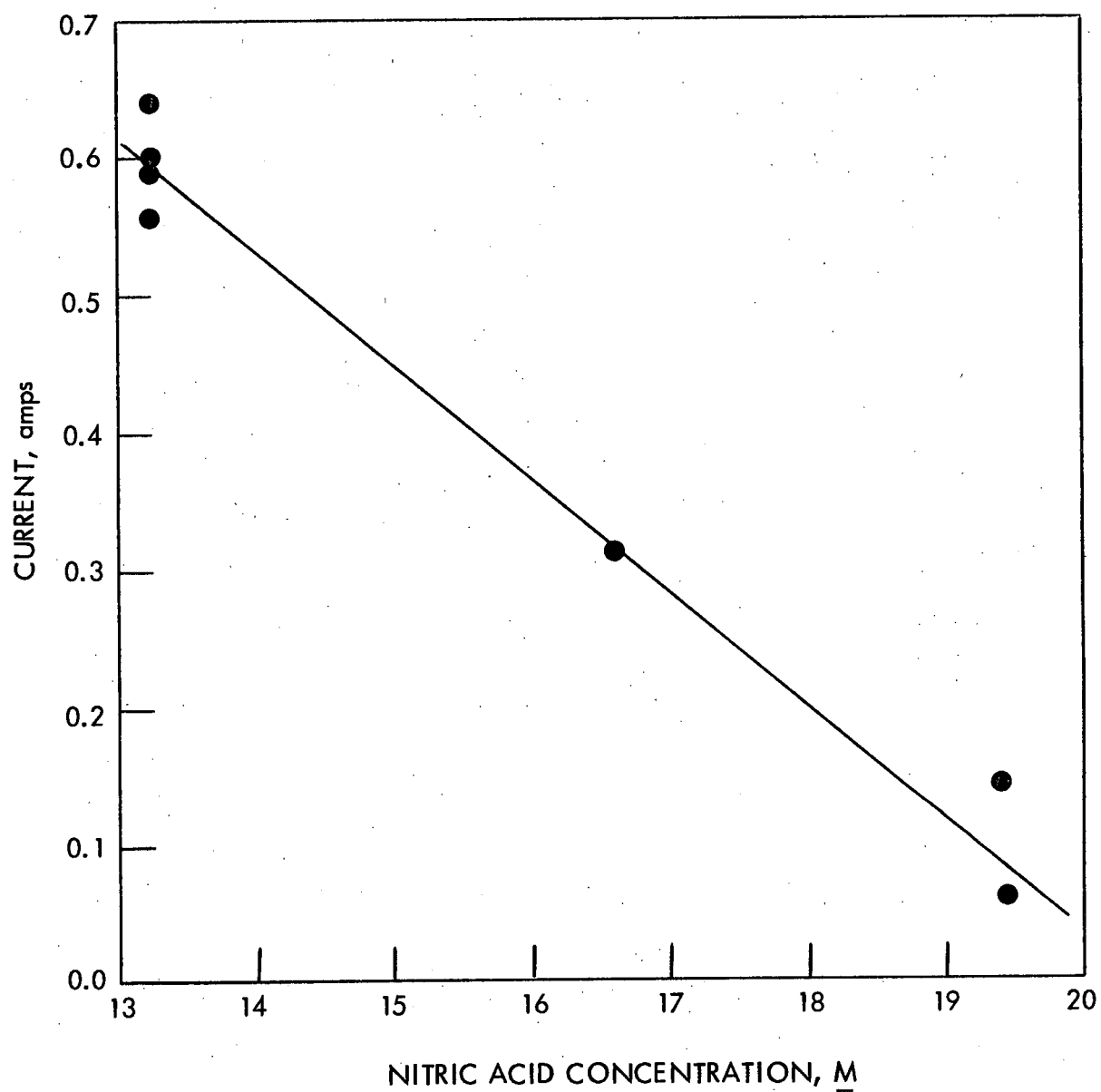


Fig. 1. Effect of nitric acid concentration on current density at constant voltage (18 volts) in the U-shaped "Series" Dissolver. Temperature, 25°C. Electrode area, 0.7 cm².

4.0 REFERENCES

1. L. W. Fromm, "Recovery of Uranium from Graphite Shapes by Electrolytic Graphite Disintegration in HNO_3 ," ORNL-238 (February 1949).
2. L. W. Fromm, "Recovery of Valuable Material from Graphite Bodies," U. S. Patent 2,903,402 (Sept. 26, 1951).
3. E. S. Occhipinti, "Reprocessing of Power Reactor Fuels - 12th Quarterly Progress Report, July 1 to Oct. 1, 1960," DP-546 (January 1961).
4. L. M. Ferris, "Chemical Processing of Coated Particle Fuels," ORNL-TM-193 (April 3, 1962).
5. R. A. Ewing, T. S. Elleman, and R. B. Price, Trans. Am. Nuclear Soc., 4 (1):152 (1961).
6. M. R. Bomar, "Series Electrolytic Dissolver for Nuclear Fuels. I. Scoping Studies," IDO-14563 (Nov. 15, 1961).
7. F. G. Rust, et al., "Processing of Power Reactor Fuels - 16th Quarterly Progress Report, July 1 to Oct. 1, 1961," DP-706 (February 1962).
8. V. P. Caracciolo, "Processing of Power Reactor Fuels - 17th Quarterly Progress Report, Oct. 1, 1961 to Jan. 1, 1962," DP-720 (April 1962).
9. L. M. Ferris, M. J. Bradley, and A. H. Kibbey, "Processes for Recovery of Uranium and Thorium from Graphite-Base Fuel Elements. Part II," ORNL-3186 (November 1961).

DISTRIBUTION

1. J. B. Adams
- 2-3. R. E. Blanco
4. J. O. Blomeke
5. W. D. Bond
6. J. C. Bresee
7. K. B. Brown
8. W. E. Clark
9. F. L. Culler
10. W. Davis, Jr.
11. L. M. Ferris
12. D. E. Ferguson
13. J. R. Flanary
14. T. A. Gens
15. H. E. Goeller
16. A. E. Goldman
17. J. M. Googin
18. A. T. Gresky
19. C. E. Guthrie
20. P. A. Haas
21. F. E. Harrington
22. R. F. Hibbs
23. J. M. Holmes
24. R. W. Horton
25. A. R. Irvine
26. W. H. Jordan
27. F. G. Kitts
28. E. Lamb
29. W. H. Lewis
30. R. B. Lindauer
31. A. P. Litman
32. J. T. Long
33. J. P. Nichols
34. E. L. Nicholson
35. R. H. Rainey
36. J. T. Roberts, IAEA, Vienna
37. A. D. Ryon
- 38-40. E. M. Shank
41. M. J. Skinner
42. S. H. Smiley
43. E. G. Struxness
44. J. C. Suddath
45. J. A. Swartout
46. J. W. Ullmann
47. C. D. Watson
48. M. E. Whatley
49. C. E. Winters
50. R. G. Wymer
51. E. L. Anderson, AEC, Washington
52. R. F. Benenati, General Atomics
53. S. Bernstein, Paducah
54. J. A. Buckham, ICPP
55. J. T. Christy, AEC, Hanford
56. F. R. Dowling, AEC, Washington
57. R. A. Ewing, BMI
58. M. K. Harmon, Hanford
59. L. P. Hatch, Brookhaven
60. B. R. Hayward, Atomics Int'l.
61. O. F. Hill, Hanford
62. K. K. Kennedy, ICPP
63. E. M. Kinderman, SRI
64. S. Lawroski, ANL
65. J. A. Lieberman, AEC, Washington
66. J. A. McBride, ICPP
67. R. A. McGuire, ICPP
68. B. Manowitz, BNL
69. J. W. Morris, du Pont, SRL
70. J. Nehls, ORO
71. H. Pearlman, Atomics Int'l.
72. W. H. Reas, Hanford
73. K. L. Rohde, ICPP
74. C. A. Rohrman, Hanford
75. H. Schoen, RAI
76. C. M. Slansky, ICPP
77. J. I. Stevens, ICPP
78. C. E. Stevenson, ANL, Idaho
79. K. G. Steyer, General Atomics
80. V. R. Thayer, du Pont, Wilmington
81. R. E. Tomlinson, Hanford
82. F. M. Warzel, ICPP
83. Document Reference Section
- 84-85. Central Research Library
86. ORNL-RC
- 87-91. Laboratory Records
- 92-106. DTIE
107. Research and Development Div., ORO
108. A. H. Kibbey
109. W. O. Harms