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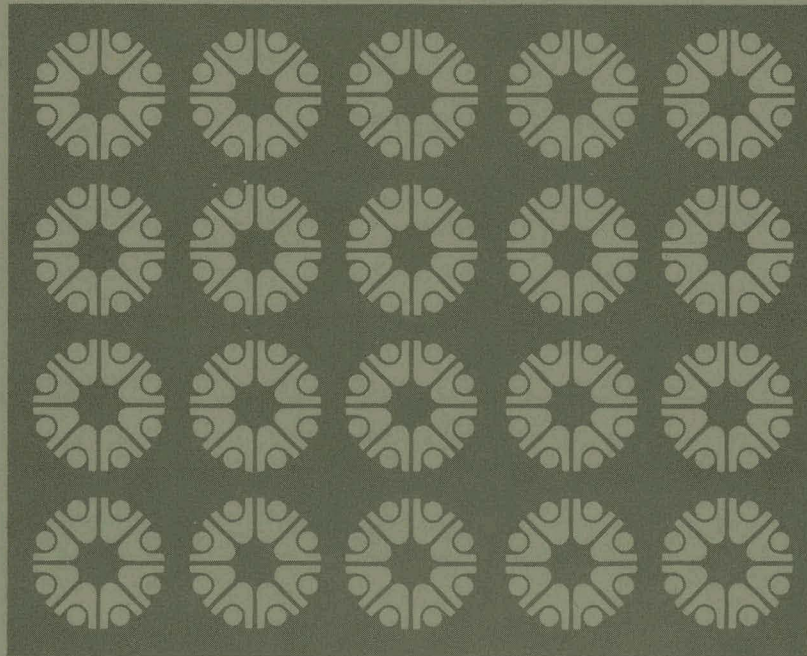
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DESTRUCTION OF NITROUS ACID  
AND HYDRAZOIC ACID  
IN PUREX SYSTEMS

AUGUST 1971



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By

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August 1971

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## DESTRUCTION OF NITROUS ACID AND HYDRAZOIC ACID IN PUREX SYSTEMS

J. L. Swanson

### INTRODUCTION

In the Purex process for the recovery and purification of uranium and plutonium, separation of the plutonium from the uranium is generally accomplished by reducing plutonium(IV) to plutonium(III), which is virtually inextractable. This reduction step is performed in the presence of a "holding reductant" which is added to react with nitrous acid and thus prevent reoxidation of the plutonium. Sulfamic acid has proven to be a very successful holding reductant but the fact that it is converted to sulfuric acid is detrimental. Because hydrazine also reacts rapidly with nitrous acid and does not form corrosive reaction products, it has seen increasing use as a holding reductant.

The reaction of hydrazine with nitrous acid is known to produce hydrazoic acid under certain conditions. Although hydrazoic acid can form explosive compounds or mixtures under appropriate conditions, the probability of this occurring in the Hanford plant as normally operated is extremely minute. However, means of minimizing its formation and/or safely destroying that which does form were desired as a precautionary measure. An additional goal was to accomplish this by methods suitable for use in existing equipment and which would add little or no salts to the waste stream.

### SUMMARY

Most of the hydrazoic acid formed in the Purex process will be present in the organic phase until it is removed as azide ion by the carbonate wash in the organic recovery process. The destruction of the azide ion in the carbonate solution can be accomplished by platinum-



catalyzed hydrazine reduction. Azide destruction can be accomplished in several ways in acid solution; the most promising method for use at Hanford is the reaction with permanganate following acidification of the mixed permanganate-carbonate solvent wash solution.

Elimination of nitrous acid from the organic stream fed to the partition column (the 1BXF solution) would markedly reduce if not eliminate hydrazoic acid formation in the 1BX column. Several ways of accomplishing this were demonstrated; the most promising method for plant application is the reaction with hydroxylamine before the organic stream is fed to the column.

### RESULTS AND DISCUSSION

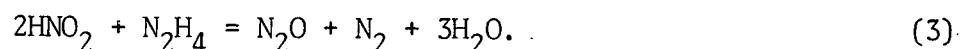
Nitrous acid reacts with hydrazine to form hydrazoic acid



Nitrous acid also reacts with hydrazoic acid



so that the overall reaction with an excess of nitrous acid is



With a sufficient excess of hydrazine, however, reaction (2) is unimportant and essentially quantitative conversion of nitrous acid into hydrazoic acid occurs.<sup>(1)</sup> Quantitative conversion of nitrous acid into hydrazoic acid is also aided by the presence of a tributyl phosphate (TBP) phase, which extracts hydrazoic acid and thus decreases the possibility of reaction (2) occurring.

The use of hydrazine as a holding reductant in a Purex process partition column (1BX column) thus presents an ideal situation for quantitative conversion of nitrous acid into hydrazoic acid in that there is both an excess of hydrazine and an organic phase to extract the hydrazoic acid as it forms. A reduction in the amount of nitrous acid fed to the 1BX column would result in a corresponding reduction in the amount of hydrazoic acid formed in this column.



### DESTRUCTION OF NITROUS ACID IN 1BXF SOLUTION

The organic feed solution to the 1BX column in the Hanford Purex plant contains not only the organic product from the first extraction column but also organic streams recycled from several other process steps. This solution, called 1BXF, contains nitrous acid from three sources; that present in the feed to the first extraction column (the HA column), that added to the HA column to improve neptunium recovery, and that added to the feed to the third plutonium cycle in excess of the amount required to react with the plutonium(III) and reductants present in the product of the second plutonium cycle. Destruction of the  $\text{HNO}_2$  present in this solution before it is fed to the 1BX column would markedly reduce (if not eliminate) the formation of hydrazoic acid.

One way of destroying the nitrous acid present in the 1BXF before it is fed to the 1BX column is to contact the 1BXF with an aqueous phase containing a material which reacts with nitrous acid. With the present equipment, aqueous solutions added to the 1BXF tank accompany the organic solution into the 1BX column; the volume of aqueous phase must therefore be kept small.

With hydrazine as the reactant, rapid reaction occurred but hydrazoic acid was formed unless the quantity of hydrazine was limited to one-half mole per mole  $\text{HNO}_2$  or less. With less than one-half mole hydrazine per mole  $\text{HNO}_2$ , complete reaction of the  $\text{HNO}_2$  cannot be accomplished. Thus for complete reaction of the  $\text{HNO}_2$  without hydrazoic acid formation, the precise stoichiometric amount of hydrazine must be used. Data showing yields of hydrazoic acid at various hydrazine to  $\text{HNO}_2$  ratios are given in Table 1.

With hydroxylamine as the reactant, slower reaction of the  $\text{HNO}_2$  was observed. In an experiment similar to those in Table 1, only 68% of the  $\text{HNO}_2$  reacted in five minutes when an organic phase was contacted with 0.02 volumes of 0.2M hydroxylamine (giving a hydroxylamine to  $\text{HNO}_2$  mole ratio of 3.5). Other evidence that hydroxylamine reacts more slowly with  $\text{HNO}_2$  than does hydrazine was obtained by contacting simulated 1BXF with an aqueous phase containing equal concentrations of hydrazine and

hydroxylamine. Nearly all of the  $\text{HNO}_2$  was converted to  $\text{HN}_3$ , demonstrating that the  $\text{HNO}_2$  reacted with the hydrazine in preference to the hydroxylamine. While the hydroxylamine reaction is considerably slower than the hydrazine reaction, it should still be sufficiently rapid to react with all the  $\text{HNO}_2$  in the LBXF (the temperature of the solution in the LBXF tank is about 50 °C and the average residence time is about one hour).

TABLE I. Hydrazoic Acid Yields

Conditions: Simulated LBXF solution contacted with aqueous phase for one minute at 23 °C

$\text{HNO}_2$ in organic initially, <u>M</u>	mole $\text{N}_2\text{H}_4$ mole $\text{HNO}_2$	In organic after contact, <u>M</u>		Percentage of $\text{HNO}_2$ converted to $\text{HN}_3$
		$\text{HNO}_2$	$\text{HN}_3$	
0.0012	0.56	N.D. (1)	0.00009	7
0.00044	0.76	N.D.	0.00017	38
0.013	43	N.D.	0.013	100

(1) N.D. indicates none detected.

With urea as the reactant, much slower reaction of the  $\text{HNO}_2$  was observed, as shown in Figure 1. These data were obtained in the absence of light in stainless steel equipment, with stirring just sufficiently vigorous to suspend droplets of the aqueous phase in the organic phase. The urea reaction appears to be too slow to be of much value.

Hydrogen peroxide rapidly oxidizes  $\text{HNO}_2$  to nitric acid. The addition of  $\text{H}_2\text{O}_2$  to LBXF would necessitate strict control, however, since any excess would consume reductant in the LBX column. Since  $\text{H}_2\text{O}_2$  extracts appreciably into 30% TBP-NPH (normal paraffin hydrocarbon), the peroxide could be added to the LBXF tank as an organic solution if desired. Peroxide distribution coefficients of about 0.1 were measured from dilute  $\text{HNO}_3$  solutions.

Nitrous acid is unstable in acid solution, especially when gaseous products are removed to shift the equilibria in the desired direction.

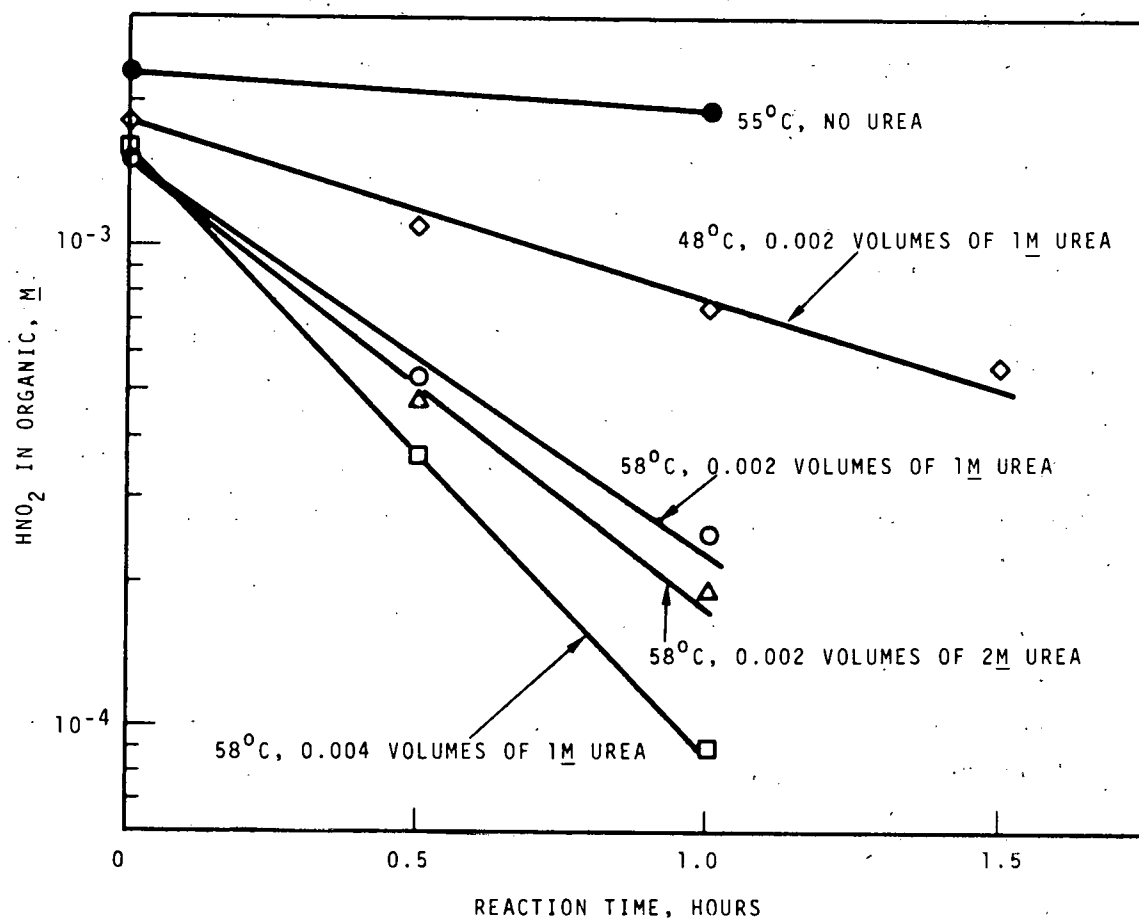
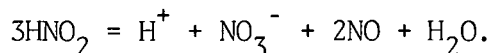
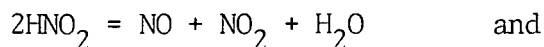


FIGURE 1. DESTRUCTION OF HNO<sub>2</sub> IN 1BXF WITH UREA

Two such reactions are



The results of experiments in which air was bubbled into or swept over simulated LBXF solutions are presented in Figure 2. The rate of  $\text{HNO}_2$  decomposition increased with increasing air sparge rate but at a reasonable sparge rate decomposition was not very rapid. These data were obtained with the solution being stirred in a stainless steel beaker simulating the LBXF tank; perhaps more rapid decomposition would occur if the gas-liquid contact were more efficient (as in a packed column).

Another possibility for reducing the concentration of  $\text{HNO}_2$  in LBXF is that of photochemical reduction of the  $\text{HNO}_2$ . Nitrous acid was observed to be much more stable in LBXF in the absence of light than on exposure to the normal fluorescent lighting of the laboratory. A few scouting experiments were performed with ultraviolet lamps but no marked effect was observed. One possible complication is that  $\text{HNO}_2$  can be formed by photochemical reduction of nitric acid as well as being destroyed by photochemical reduction.

The  $\text{HNO}_2$  added to the LBXF in the recycle organic stream from the third plutonium cycle (3BW) is normally only a small fraction of the total present. Destruction of the  $\text{HNO}_2$  in the stream would, however, prevent significant increase in the  $\text{HNO}_2$  content of LBXF in the event of an exceptionally large addition of  $\text{NaNO}_2$  to the solution fed to this cycle.

Data on the rate of removal of  $\text{HNO}_2$  from simulated 3BW by contacting with aqueous phases containing various reactants are shown in Figure 3. Very rapid removal of  $\text{HNO}_2$  occurred with hydrogen peroxide or hydrazine; very slow removal occurred with urea or hydroxylamine. Addition of nitric acid gave more rapid reaction with hydroxylamine or peroxide (the only two tested at higher acidities). As before, hydrazoic acid was formed when using hydrazine.

#### DESTRUCTION OF HYDRAZOIC ACID

Since hydrazoic acid is quite highly extractable,<sup>(2)</sup> most of that

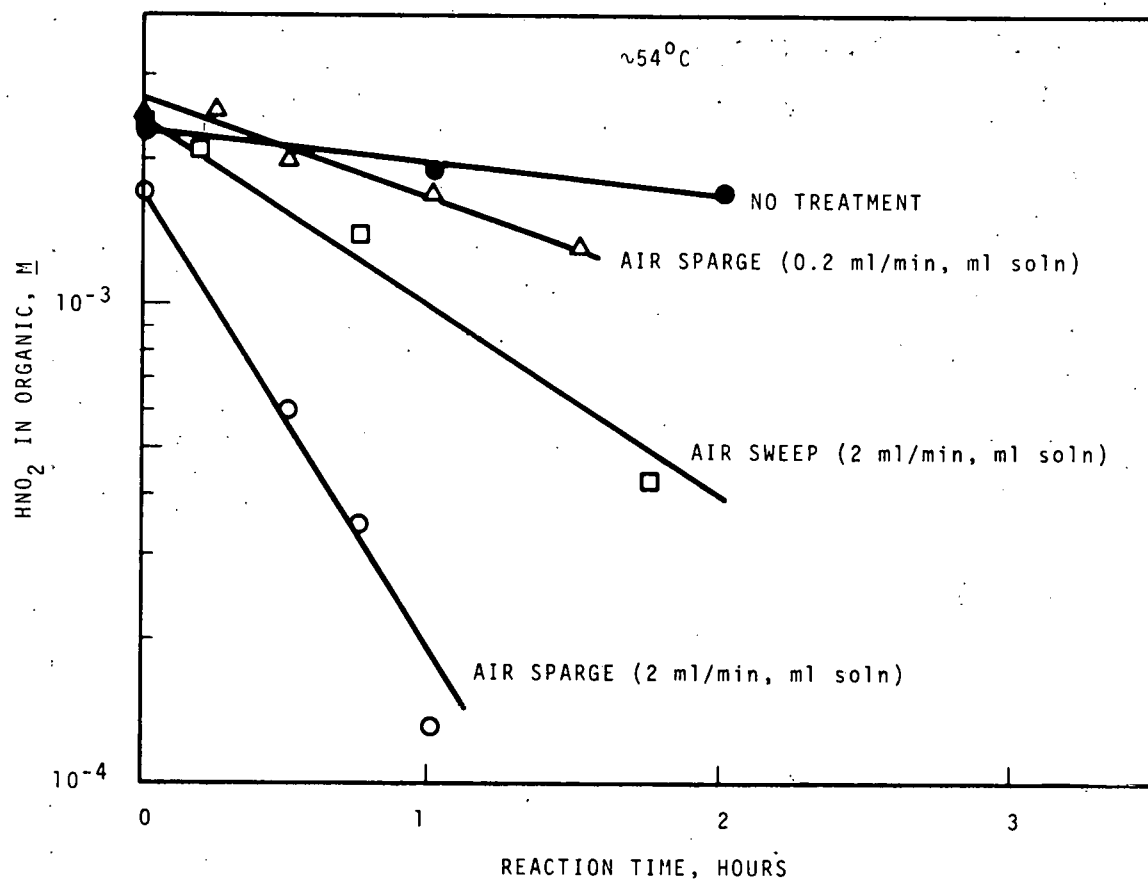


FIGURE 2. EFFECT OF AIR ON  $\text{HNO}_2$  DECOMPOSITION

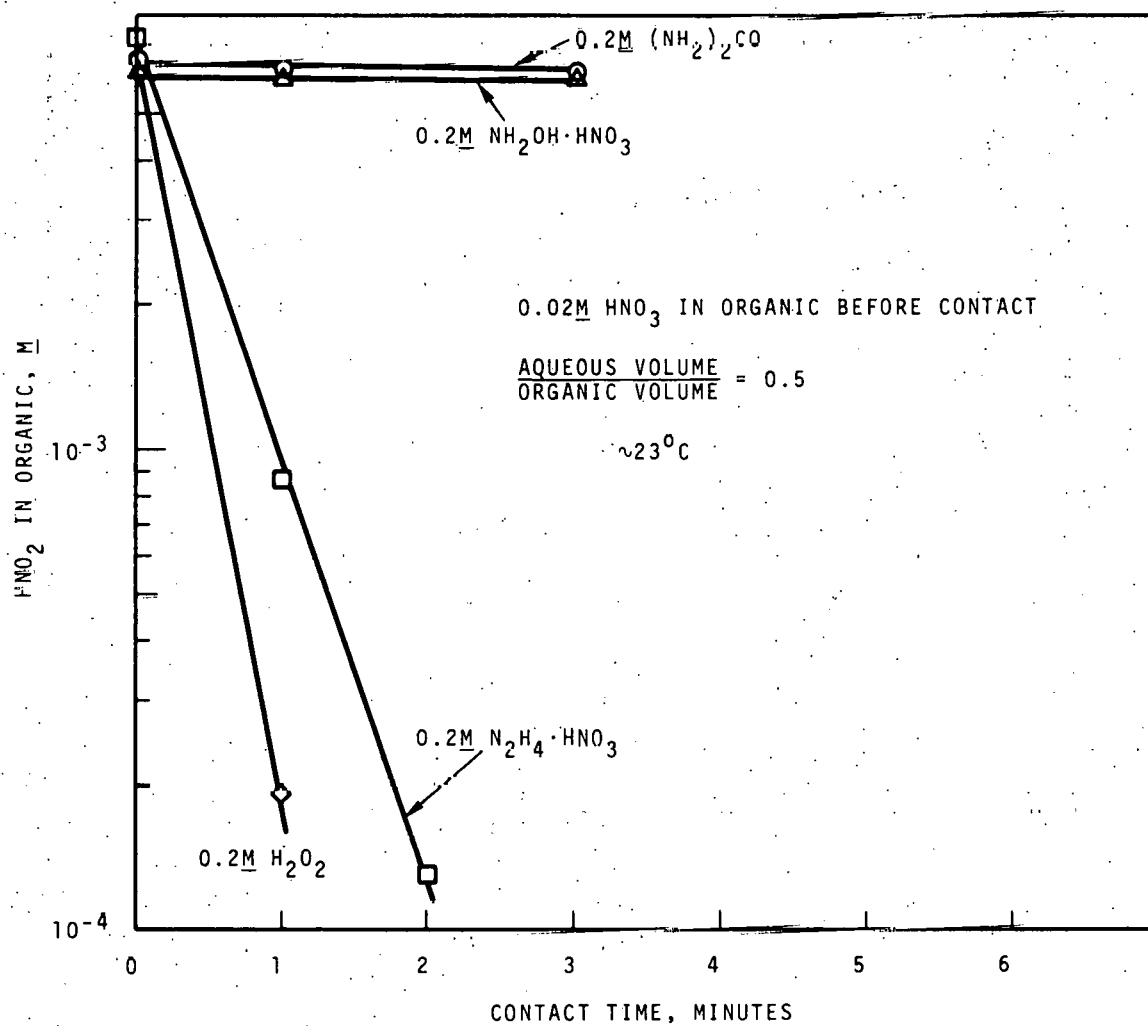
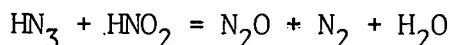


FIGURE 3. DESTRUCTION OF  $\text{HNO}_2$  IN SIMULATED 3BW

formed in the 1BX column will leave the column in the organic phase and remain in the organic when the uranium is stripped out in the 1C column. The hydrazoic acid will be neutralized and stripped from the organic phase during the carbonate wash portion of the organic recovery process. Means of treating this solution to destroy the azide were investigated.

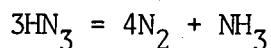
When the carbonate solution used to wash the solvent contains permanganate and manganese dioxide, as it does at Hanford, the azide can be destroyed by simply acidifying the solution. While reaction of permanganate or  $\text{MnO}_2$  with azide ion occurs slowly if at all in carbonate solution, it occurs relatively rapidly in acid solution. No azide was found after one minute (at  $\sim 23^\circ\text{C}$ ) in a  $0.1\text{M}$   $\text{HNO}_3$  solution initially containing  $0.015\text{M}$   $\text{KMnO}_4$  and  $0.04\text{M}$   $\text{NaN}_3$ . Reaction of hydrazoic acid with freshly prepared  $\text{MnO}_2$  was found to be slower than the reaction with permanganate. When solutions initially  $0.01\text{M}$  in  $\text{HN}_3$  were stirred with  $0.75$  mole  $\text{MnO}_2$ /mole  $\text{HN}_3$  at  $\sim 23^\circ\text{C}$  for five minutes,  $60\%$  of the  $\text{HN}_3$  was destroyed when the  $\text{HNO}_3$  concentration was  $0.1\text{M}$ ,  $90\%$  was destroyed in  $0.3\text{M}$   $\text{HNO}_3$ , and  $100\%$  was destroyed in  $1\text{M}$   $\text{HNO}_3$ .

When the solvent wash solution does not contain permanganate, destruction of the azide can be accomplished by adding sodium nitrite and then acidifying. The reaction



is very rapid in aqueous acid solution.

Other ways of destroying hydrazoic acid (in acid solution) and sodium azide (in sodium carbonate solution) were also studied. Hydrazoic acid is thermodynamically unstable with respect to its decomposition into nitrogen and ammonia



and catalysis of the decomposition by platinum has been reported.<sup>(3)</sup> This catalysis was verified but the decomposition was still not very rapid; when  $50\text{ ml}$  of  $0.01\text{M}$   $\text{HN}_3$  in  $0.3\text{M}$   $\text{HNO}_3$  was stirred in contact with  $5\text{ grams}$  of  $0.5\%$  Pt on alumina pellets, the  $\text{HN}_3$  disappeared with a half-time of about  $20\text{ minutes}$  at  $\sim 55^\circ\text{C}$ . Platinum-catalyzed decomposition



of organic-phase hydrazoic acid was also observed but it also was not especially rapid.

The platinum-catalyzed hydrazine reduction of hydrazoic acid in nitric acid solution was found to be more rapid than the platinum-catalyzed decomposition of hydrazoic acid; with the conditions described above the addition of  $0.02M$   $N_2H_5NO_3$  increased the rate of hydrazoic acid disappearance by a factor of about five, giving a half-time of about 4 minutes. Increasing the hydrazine concentration to  $0.2M$  did not further increase the rate, however.

Platinum was also found to catalyze the hydrazine reduction of azide in sodium carbonate solution. The rate in  $0.05M$   $Na_2CO_3$  was about the same as in  $0.3M$   $HNO_3$  and was also independent of hydrazine concentration. This reaction provides a means of destroying azide ion without acidifying the solvent wash solution. Presumably the azide ion is reduced to ammonia in this reaction.

### EXPERIMENTAL

Concentrations of hydrazoic acid were determined spectrophotometrically using the highly colored ferric azide complex.<sup>(4)</sup> Reactant mixtures often had to be treated before analysis to prevent reaction in the analytical solution. For example, organic phases containing both nitrous acid and hydrazoic acid were contacted with sulfamic acid to destroy the nitrous acid before the hydrazoic acid was stripped into carbonate solution and then acidified for analysis. Also, hydrazoic acid-permanganate mixtures were added to stirred mixtures of 30% TBP,  $HNO_3$ , and  $H_2O_2$  to destroy the permanganate and extract the hydrazoic acid, which was then stripped from the organic and analyzed.

Nitrous acid concentrations were also determined spectrophotometrically. Uranium was stripped from the organic samples with 1:1  $H_3PO_4$  to avoid interference.

The simulated 1BXF used here was prepared by contacting three

volumes of 30% TBP-NPH with one volume of 0.72M U in 4M HNO<sub>3</sub>. The resultant organic phase contained about 0.24M U and 0.3M HNO<sub>3</sub>.

ACKNOWLEDGEMENT

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REFERENCES

1. E. K. Dukes and R. M. Wallace. "Formation of Hydrazoic Acid from Hydrazine in Nitric Acid Solutions," DP-728, 1962.
2. C. S. Schlea, et al. "Uranium(IV) as a Reducing Agent for Plutonium(IV) in the Purex Process," DP-808, 1963.
3. W. M. Latimer. Oxidation Potentials, Prentice Hall, 1938, p. 96.
4. E. K. Dukes and R. M. Wallace. "Determination of Hydrazoic Acid and Ferric Ion by Spectrophotometric Measurement of the Ferric Azide Complex," Anal. Chem., vol. 33, no. 2, p. 242, 1961.

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