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THE CRYSTAL STRUCTURE DETERMINATIONS OF trans-DICYANO
TRIEN COBALT(III) PERCHLORATE AND POTASSIUM ANTIMONY(III)
PENTACHLORIDE AND TWO PHASE DETERMINATION
TECHNIQUES BASED ON PATTERSON
DECONVOLUTION

Ph.D. Thesis Submitted to Iowa State University,
November, 1972

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Date of Manuscript: November, 1972

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The crystal structure determinations of
trans-dicyano trien cobalt(III) perchlorate
and potassium antimony(III) pentachloride
and
two phase determination techniques
based on Patterson deconvolution

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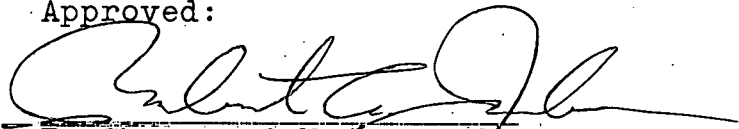
Robert Kingsley Wismer

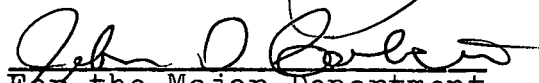
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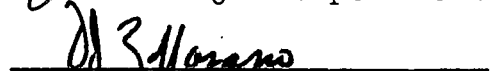
Department: Chemistry

Major: Physical Chemistry

Approved:


In Charge of Major Work


For the Major Department


For the Graduate College

Iowa State University
Of Science and Technology
Ames, Iowa

1972

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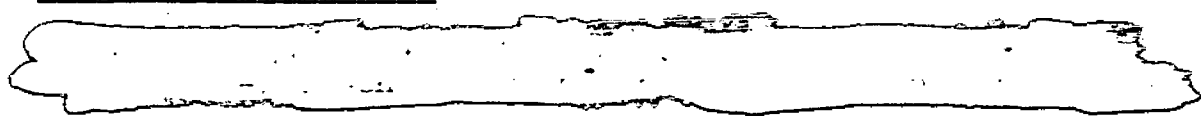
two phase determination techniques
 based on Patterson deconvolution*

Robert Kingsley Wismer

Under the supervision of R. A. Jacobson
 From the Department of Chemistry
 Iowa State University of Science and Technology

The crystal structure of trans-dicyano triethylene-
 tetramine cobalt(III) perchlorate (monoclinic, $P2_1/n$,
 $a = 9.85$, $b = 22.35$, $c = 6.68$ A, $\beta = 100.9^\circ$, $Z = 4$,
 $MoK\alpha$ radiation) has been determined by three-dimensional
 X-ray analysis. The structure was solved by conventional
 Patterson and Fourier techniques and refined by full
 matrix least squares to a final discrepancy factor of
 0.123 for the 3314 observed reflections. The complex
 has a distorted octahedral configuration with the trien
 ligand equatorially coordinated. The bonding mode of
 the cyanide group is clearly through carbon.

The crystal structure of potassium antimony(III)



pentachloride (K_2SbCl_5 , monoclinic, $P2_1/c$, $a = 8.87$, $b = 12.46$, $c = 8.93$ Å, $\beta = 110.5^\circ$, $Z = 4$, MoK α radiation) has been determined by three-dimensional X-ray analysis. The structure was solved by conventional Patterson and Fourier techniques and refined by full matrix least squares to a final conventional discrepancy factor of 0.054 for the 1543 observed reflections. The $SbCl_5$ exhibits a distorted square pyramidal configuration in which the axial antimony - chloride bond (2.39 Å) is shorter than the mean basal antimony - chloride bond and two of the basal bonds are distorted by interionic and packing forces.

The superposition technique has been programmed for semi-automatic use in solving heavy atom and pseudo heavy atom problems. From a list of peaks, obtained by program analysis of a Patterson map, a heavy atom peak is chosen. This is then used as the origin for an in-core superposition. By utilizing the symmetry of the structure being solved, the program then determines the amount by which the origin of the resultant superposition map is shifted from the origin in electron density space, and computes the location of atoms in the unit cell. The program is written to handle inversion, mirror, glide, two-fold, and two-fold screw symmetry.

A method of phase determination which utilizes

both the Σ_2 relation and Patterson superposition techniques has been developed. Reflections input into the initial Σ_2 relation are used to compute a map upon which the Patterson is superimposed. The Fourier transform of the resultant map, with negative regions set equal to zero, yields reliable phases for the larger $|E|$ values. These are then extended and refined by usual direct method techniques. Application of this method to both a centric and an acentric structure is presented. Further refinements and extensions of the method are also discussed.

INTRODUCTION

This thesis describes the crystal structures of two compounds and details two methods for the determination of the phases of structure factors. The crystal structures were undertaken to extend the currently available knowledge of cobalt and antimony complexes.

The cobalt compound was believed by its discoverers to be cis- $\alpha(\text{NC})_2$ trien cobalt(III) perchlorate. Thus, it would have been the sole known mononuclear cobalt complex in which the cyanide group was coordinated to cobalt through the nitrogen atom. The structure that was determined is actually trans-(CN) $_2$ trien cobalt(III) perchlorate and is one of the few examples in which a quadridentate ligand, not restricted by its own structure to be planar, is equatorially coordinated to cobalt.

The second structure described is that of K_2SbCl_5 . The structure of the SbCl_5^- anion has only been determined once previously, in the compound $(\text{NH}_4)_2\text{SbCl}_5$. In that instance, the disagreement between observed and calculated structure factors was such that the uncertainty in bond distances was 0.5 Å. Structures of antimony halides are known to be very sensitive to the cation present.

The first of the phase determining methods applies the techniques of pseudo heavy atom superposition and then uses space group symmetry to determine atomic

locations in electron density space. All of these operations are performed by a computer program with a minimum of human intervention.

The second phase determining method also uses superposition techniques, to enhance the phase determining properties of a pseudo electron density map which has been computed from origin-defining reflections. The coefficients of the Fourier transform of this modified map are then used to phase those reflections with the largest normalized unitary structure factors. This method greatly simplifies one of the major problems of direct methods, the expansion of the origin-defining set.

THE CRYSTAL AND MOLECULAR STRUCTURE OF TRANS-DICYANO
TRIETHYLENETETRAMINE COBALT(III) PERCHLORATE

Introduction

The bonding mode of cyanide to cobalt has been the subject of considerable controversy in recent years. The energy difference between the cyano and isocyano coordinations is small enough to permit either to occur.¹ However, neutron diffraction studies of cyano-cobalt complexes^{2,3,4} have regularly shown that the cyanide group bonds through carbon. Since it is oftentimes difficult to distinguish between atoms which differ by but one electron by X-ray diffraction, bonding via the carbon has sometimes been assumed.⁵

Kuroda and Gentile⁶ recently have prepared what they characterize as an isocyano cobalt complex, cis- α -isocyano-triethylenetetramine cobalt(III) perchlorate. Their assignment of the isocyano coordination is based on visible and ultraviolet spectroscopy. Because there is some doubt as to the correctness of this assignment,⁷ it was decided to carry out an X-ray structure determination of this compound.

Experimental

A sample of the compound, prepared by the method of Kuroda and Gentile,⁶ was kindly supplied by Dr. James H.

Espenson. Amber-colored crystals were obtained by recrystallization from an aqueous solution. High resolution infrared spectra of the initial sample and of the recrystallized material, both in KBr pellets, were virtually identical, indicating that isomerization had not occurred during solution or recrystallization. Microscopic examination revealed that the crystals have sharply defined faces and are needle-like in appearance with a distorted hexagonal cross section in which alternate sides are of unequal lengths.

Crystals were selected and mounted on a glass fiber with Duco cement thinned with amyl acetate. Preliminary Weissenberg and precession photographs exhibited $2/m$ Laue symmetry, indicating a monoclinic space group. The following systematic absences were observed: $h0\ell$ when $h + \ell = 2n + 1$, and $0k0$ when $k = 2n + 1$. These absences are only consistent with the space group $P2_1/n$. The unit cell parameters at 25°C are $a = 9.8544 \pm 0.0015$, $b = 22.3529 \pm 0.0045$, $c = 6.6766 \pm 0.0020 \text{ \AA}$, and $\beta = 100.85 \pm 0.03^\circ$. These parameters and their standard deviations were obtained by a least squares fit⁸ to the two-theta values of twelve independent reflections whose centers were determined by top-bottom, left-right beam splitting on a previously aligned Hilger-Watts four-circle diffractometer (MoK α radiation, $\lambda = 0.71069 \text{ \AA}$). Any

error in the instrumental zero was eliminated by centering the reflection at both plus two-theta and minus two-theta. A calculated density of 1.62 g/cc for four molecules per unit cell agrees quite well with an observed density of 1.65 ± 0.01 g/cc, which was determined by flotation techniques.

For data collection, a crystal was selected having approximate dimensions 0.1 x 0.1 x 0.9 mm along the a, b, and c crystal axes, respectively, and was mounted such that the c axis coincided with the ϕ axis of the diffractometer. Data were collected at room temperature using a Hilger-Watts four-circle diffractometer interfaced to an SDS 910 computer in a real time mode, equipped with a scintillation counter, and using Zr-filtered $\text{MoK}\alpha$ radiation. Within a two-theta sphere of 60° ($\sin\theta/\lambda = 0.704 \text{ \AA}^{-1}$) all data in the hk^l and $\bar{h}k^l$ octants were recorded using the θ - 2θ scan technique with a take-off angle of 5.5° . Symmetric scan ranges of 1.2° in 2θ at low two-theta values to 2.0° at large two-theta values were used. Stationary-crystal, stationary-counter background counts of half the scan time were taken at the beginning and end of each scan. A counting rate of 0.4096 seconds per step of 0.01° in θ was employed. A total of 5081 reflections were measured in this way.

As a general check on electronic and crystal stability, the intensities of three standard reflections were remeasured periodically during the data collection period. These reflections did not vary to any significant degree during the entire period of data collection.

Based on a linear absorption coefficient of $\mu = 14.982 \text{ cm}^{-1}$, the maximum and minimum transmission factors⁹ were 87.86% and 85.96% respectively, and no absorption correction was deemed necessary.

The intensity data were corrected for Lorentz-polarization effects. The estimated error in each intensity was calculated by

$$\sigma_I^2 = C_T + C_B + (0.03 C_T)^2 + (0.03 C_B)^2$$

where C_T and C_B are the total count and the background count, respectively. The factor 0.03 represents an estimate of non-statistical errors. The estimated deviations in the structure factors were calculated by the finite difference method.¹⁰ Of the 4678 independent reflections, 3314 were considered observed ($> 3\sigma_F$).

Solution and Refinement

The positions of the cobalt and chlorine atoms were obtained from analysis of a sharpened Patterson function.¹¹ The remaining non-hydrogen atoms were found by successive structure factor¹² and electron density map calcula-

tions.^{13,14} These atomic positions were then refined by a full matrix least squares procedure,¹² minimizing the function $\sum w (|F_o| - |F_c|)^2$, where $w = 1/\sigma_F^2$, to a conventional discrepancy factor of $R = \sum ||F_o| - |F_c|| / \sum |F_o| = 0.170$. The scattering factors used were those of Hanson *et al.*¹⁵ with the cobalt and chlorine scattering factors modified for the real and imaginary parts of anomalous dispersion.¹⁶

An electron density difference map verified that all the non-hydrogen atoms had been accounted for, but indicated that some anisotropic motion, particularly of the cobalt and chlorine atoms, was present. Accordingly, anisotropic refinement was begun and after six cycles of refinement, values of R and $R (= \sum w (|F_o| - |F_c|)^2 / \sum w |F_o|^2)^{1/2}$ of 0.154 and 0.169, respectively, were obtained. The positions of the hydrogens bonded to carbons in the triethylenetetramine ligand were calculated with an H-C-C angle of 109.5° and a C-H distance of $1.07 \text{ \AA}$. The hydrogen atoms were assigned isotropic thermal parameters of $3.0 \text{ \AA}^2$. Two cycles of refinement with anisotropic thermal parameters for all non-hydrogen atoms, varying only the positional and thermal parameters of the non-hydrogen atoms and the overall scale factor, followed by a recalculation of the hydrogen atom positions and two further cycles of least squares refinement, yielded values for R and wR of 0.123.

and 0.156, respectively.

A final electron density difference map showed no peaks greater than $1.2 \text{ e}/\text{\AA}^3$. A final statistical analysis of the F_o and F_c values as a function of the scattering angle and magnitude of F_o revealed no unusual trends and suggests that the relative weighting scheme used is a reasonable one.

The bonding orientation of the two cyanide groups was determined after the final least squares refinement. The atom multipliers of the two cyanide group atoms were allowed to vary under two sets of conditions. In the first of these, carbon scattering factors were assigned to C(7) and C(8) and nitrogen scattering factors were assigned to N(5) and N(6). In the second instance, the scattering factor assignments were reversed. All four atom multipliers were initially set at a value of 1.00. The results of these refinements are shown in Table I and clearly indicate the correct assignments.

The final positional and thermal parameters for the non-hydrogen atoms are listed in Table II. The standard deviations were calculated from the inverse matrix of the final least squares refinement cycle. The calculated hydrogen atom positions are listed in Table III. Bond

Table I. Determination of the bonding mode of cyanide in
trans-(CN)₂ trien Co^{III}ClO₄

Atom	Assigned Scattering Factor Table	Atom Actual	Multiplier Theoretical		R	ωR
			Co-C-N	Co-N-C		
C(7)	Carbon	1.033	1.0	1.17		
C(8)	Carbon	1.034	1.0	1.17		
N(5)	Nitrogen	1.026	1.0	0.86		
N(6)	Nitrogen	1.046	1.0	0.86	12.4	15.8
C(7)	Nitrogen	0.823	0.86	1.0		
C(8)	Nitrogen	0.825	0.86	1.0		
N(5)	Carbon	1.293	1.17	1.0		
N(6)	Carbon	1.314	1.17	1.0	12.4	15.8

Table II

Final positional and anisotropic thermal parameters of non-hydrogen atoms in trans-(NC)₂-trien Co^{III}ClO₄^{a, b}

Atom	x	y	z	10 ⁴ β ₁₁	10 ⁴ β ₂₂	10 ⁴ β ₃₃	10 ⁴ β ₁₂	10 ⁴ β ₁₃	10 ⁴ β ₂₃
Co	0.6629(1)	0.3488(1)	0.6552(2)	55.9(1.4)	9.2(0.2)	169.9(3.6)	1.1(0.5)	13.9(1.6)	0.7(0.9)
Cl	0.6616(3)	0.1285(1)	0.6466(6)	79.7(3.0)	15.6(0.6)	306.3(9.7)	3.6(1.1)	12.7(4.3)	6.1(2.2)
O(1)	0.6601(9)	0.0863(4)	0.4868(15)	139(12)	21(2)	360(32)	10(4)	-26(15)	11(7)
O(2)	0.5498(9)	0.1700(4)	0.5928(16)	121(12)	30(2)	486(39)	32(4)	-79(17)	43(8)
O(3)	0.7893(8)	0.1635(4)	0.6748(15)	92(10)	26(2)	386(32)	-5(4)	-7(14)	13(7)
O(4)	0.6586(11)	0.0988(5)	0.8283(16)	204(17)	34(3)	333(33)	-2(5.6)	90(19)	-3(9)
N(1)	0.4727(8)	0.3159(4)	0.5898(14)	69(9)	14(2)	198(24)	-9(3)	2(12)	10(6)
N(2)	0.5927(8)	0.4122(3)	0.8075(12)	77(9)	11(2)	148(21)	3(3)	11(11)	4(5)
N(3)	0.8378(8)	0.3891(4)	0.7368(15)	66(9)	14(2)	224(26)	-4(3)	23(13)	-9(6)
N(4)	0.7579(9)	0.2898(4)	0.5051(13)	97(11)	14(2)	197(25)	8(4)	39(13)	7(6)
C(7)	0.6226(10)	0.3942(5)	0.4078(18)	68(11)	12(2)	205(30)	3(4)	17(15)	-8(6.7)
C(8)	0.6997(10)	0.3013(4)	0.8952(18)	63(11)	9(2)	250(33)	-7(3.5)	31(15)	-7(7)
C(1)	0.3914(11)	0.3494(6)	0.7122(20)	77(12)	22(3)	274(36)	-7(5)	15(17)	-5(9)
C(2)	0.4392(11)	0.4144(5)	0.7393(20)	62(11)	20(3)	313(39)	10(4)	39(17)	15(9)
C(3)	0.6694(12)	0.4679(5)	0.7878(19)	93(13)	12(2)	280(37)	-4(4)	3(17)	-11(8)
C(4)	0.8173(13)	0.4545(5)	0.7531(24)	118(17)	16(3)	388(47)	-7(5)	11(22)	-19(9)
C(5)	0.9274(12)	0.3720(5)	0.6003(21)	81(13)	26(3)	289(40)	-5(5)	42(19)	-15(10)
C(6)	0.9102(13)	0.3045(5)	0.5589(23)	105(16)	26(3)	407(50)	18(6)	96(23)	14(11)
N(5)	0.6027(11)	0.4174(5)	0.2488(19)	116(13)	19(2)	349(38)	3(4)	27(16)	9(8)
N(6)	0.7204(10)	0.2762(4)	1.0540(15)	115(12)	16(2)	230(28)	3(4)	28(15)	5(7)

^a In this and subsequent tables, numbers in parentheses represent standard deviations in the least significant digits.^b Anisotropic thermal parameters are defined by: $T = \exp[-(h^2\beta_{11} + k^2\beta_{22} + l^2\beta_{33} + 2hk\beta_{12} + 2kl\beta_{23} + 2hl\beta_{13})]$.

Table III. Calculated hydrogen atomic positions in trans-
 $(\text{CN})_2$ trien $\text{Co}^{\text{III}}\text{ClO}_4$

Atom	x	y	z
H(AC1)	0.4041	0.3289	0.8624
H(BC1)	0.2834	0.3479	0.6404
H(AC2)	0.3934	0.4374	0.8519
H(BC2)	0.4113	0.4386	0.5960
H(AC3)	0.6762	0.4947	0.9921
H(BC3)	0.6135	0.4932	0.6569
H(AC4)	0.8303	0.4765	0.6143
H(BC4)	0.8906	0.4724	0.8798
H(AC5)	1.0339	0.3827	0.6673
H(BC5)	0.8990	0.3961	0.4566
H(AC6)	0.9606	0.2912	0.4366
H(BC6)	0.9593	0.2799	0.6960

lengths and bond angles, and significant non-bonded distances are listed in Tables IV and V, respectively, along with their standard deviations.¹⁷ The final values of the observed and calculated structure factors are listed in Table VI.

Shortly after the data had been collected and the crystal removed from the diffractometer, the instrument was found to be slightly misaligned. Thus, the data are somewhat poorer than might be expected. However, since all the stereochemical features of interest were well determined and the electron density difference map was rather featureless, the data were not retaken.

Description of the Structure

The results clearly indicate that the bonding of cyanide to the cobalt is through the carbon and not the nitrogen, and that these groups are trans and not cis to one another, contrary to the predictions of Kuroda and Gentile.⁶ Hence, the compound is trans-dicyanotriethylene-tetramine cobalt(III) perchlorate, and is illustrated in Figure 1.¹⁸ This configuration has been anticipated by Konya, Nishikawa, and Shibita⁷ on the basis of spectroscopic examination of similar compounds. The trans configuration is also consistent with an exceedingly sharp band for the C-N stretching frequency at 2145 cm^{-1} , with no evidence of splitting.

Table IV. Selected bond distances and angles in angstroms and degrees for cis-(CN)_2 trien $\text{Co}^{\text{III}}\text{ClO}_4$

Cl-O(1)	1.427(9)	C(8)-N(6)	1.180(13)
Cl-O(2)	1.424(8)	N(1)-C(1)	1.462(15)
Cl-O(3)	1.456(9)	N(2)-C(2)	1.488(12)
Cl-O(4)	1.392(10)	N(2)-C(3)	1.476(13)
Co-N(1)	1.978(8)	N(3)-C(4)	1.484(14)
Co-N(2)	1.951(8)	N(3)-C(5)	1.444(15)
Co-N(3)	1.922(8)	N(4)-C(6)	1.506(15)
Co-N(4)	2.001(8)	C(1)-C(2)	1.527(16)
Co-C(7)	1.909(12)	C(3)-C(4)	1.551(17)
Co-C(8)	1.894(12)	C(5)-C(6)	1.536(18)
C(7)-N(5)	1.161(14)		
O(1)-Cl-O(2)	110.7(6)	N(4)-Co-C(8)	91.5(4)
O(1)-Cl-O(3)	109.1(6)	C(7)-Co-C(8)	177.9(4)
O(1)-Cl-O(4)	109.3(6)	Co-N(1)-C(1)	106.7(6)
O(2)-Cl-O(3)	107.1(6)	Co-N(2)-C(2)	108.1(7)
O(2)-Cl-O(4)	112.3(7)	Co-N(2)-C(3)	108.9(7)
O(3)-Cl-O(4)	108.4(6)	Co-N(3)-C(4)	110.8(7)
N(1)-Co-N(2)	88.0(4)	Co-N(3)-C(5)	109.0(7)
N(1)-Co-N(3)	172.5(4)	Co-N(4)-C(6)	106.3(7)
N(1)-Co-N(4)	99.4(4)	Co-C(7)-N(5)	173.7(10)
N(1)-Co-C(7)	89.2(4)	Co-C(8)-N(6)	174.1(9)

Table IV (Continued)

N(1)-Co-C(8)	89.2(4)	N(1)-C(1)-C(2)	111.3(9)
N(2)-Co-N(3)	84.5(4)	N(2)-C(2)-C(1)	105.9(8)
N(2)-Co-N(4)	172.6(4)	N(2)-C(3)-C(4)	111.4(8)
N(2)-Co-C(7)	91.8(4)	N(3)-C(4)-C(3)	110.2(9)
N(2)-Co-C(8)	89.6(4)	N(3)-C(5)-C(6)	108.3(10)
N(3)-Co-N(4)	88.1(4)	N(4)-C(6)-C(5)	109.1(9)
N(3)-Co-C(7)	90.7(4)	C(2)-N(2)-C(3)	116.8(8)
N(3)-Co-C(8)	91.0(4)	C(4)-N(3)-C(5)	114.5(10)
N(4)-Co-C(7)	87.3(4)		

Table V. Significant non-bonded distances in trans-(CN)₂
trien Co^{III}ClO₄^a

C(7)-H(BC3)	2.870(10)
C(7)-H(AC4)	2.884(10)
C(8)-O(2)	2.694(13)
C(8)-O(3)	3.601(13)
N(4)-O(3)	3.034(12)
O(1)-H(AC5)'	2.34(1)
O(4)-H(BC1)'	2.49(1)

^a Primed atoms indicate atoms in another molecule.

Table VI. Observed and calculated structure factors

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80																				

Table VI. (Continued)

[illegible]

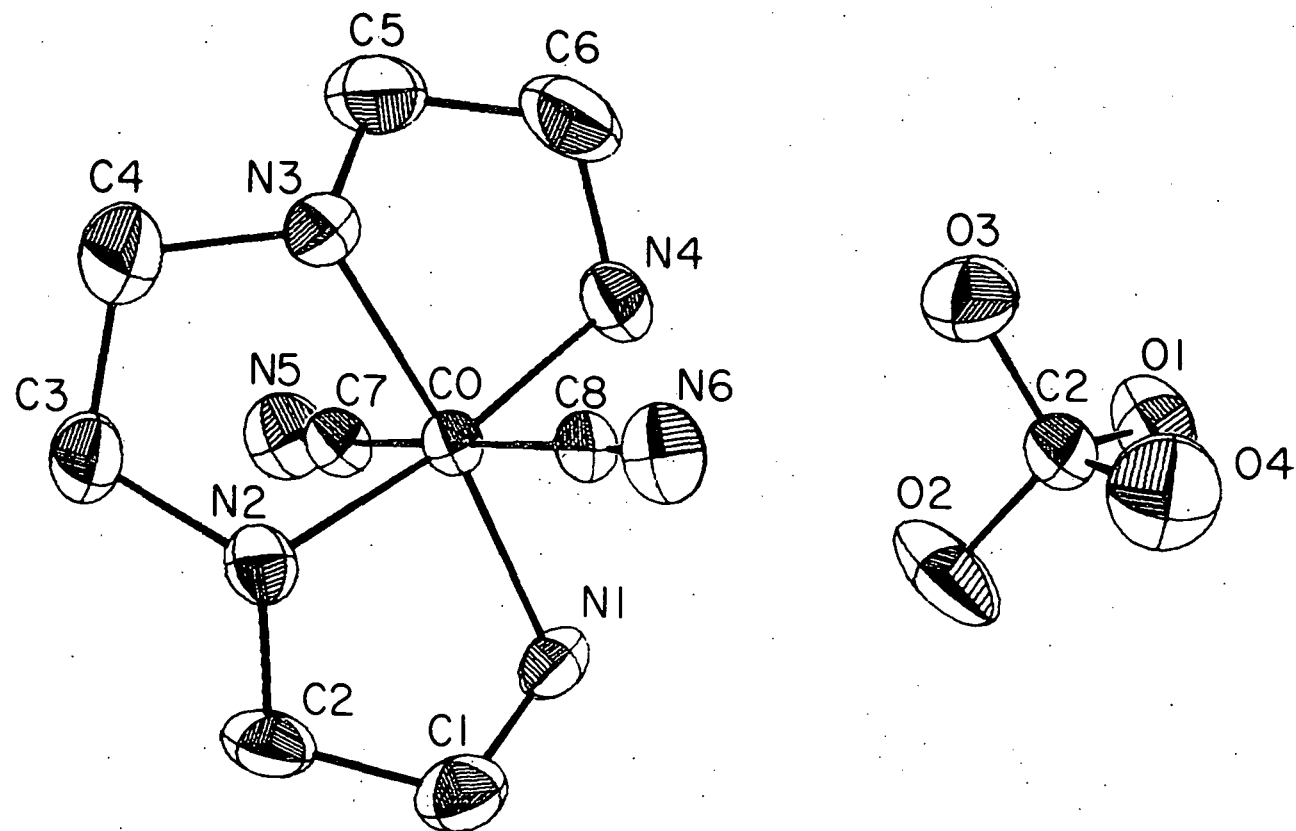


Figure 1. A formula unit of trans-cyano triethylenetetramine cobalt(III) perchlorate

The cyanide groups are within a degree of being perpendicular to the nitrogens of the trien ligand (Table IV), and the variations from an ideal octahedral configuration displayed by the N-Co-N angles appear to simply reflect the restrictions imposed by the quadridentate ligand (Figure 2). This trien ligand coordinated to cobalt in a cis configuration has been investigated by Freeman and Maxwell,¹⁹ and Dwyler and Maxwell;²⁰ their results have been used as the basis of many of the comparisons which follow.

The N(1)-Co-N(2) and N(3)-Co-N(4) angles of 88.0 and 88.1° are reasonable and consistent with similar results obtained in other investigations of the trien ligand. A slight compression of the Co-N(2)-C(3)-C(4)-N(3) ring due to the equatorial coordination of the ligand adequately explains the somewhat small value of 84.5° for the N(2)-Co-N(3) angle. Hydrogen-hydrogen repulsions would be expected to produce an increase in the N(1)-Co-N(4) angle compared to the nominal 90°, and the 99° angle found is quite reasonable. A similar result was obtained during the investigation of a cobalt compound containing a homologous ligand.²¹ The bond angles within the trien ligand, with the exception of the C-N-C angles, do not differ from the expected tetrahedral angles by more than three standard deviations. In addition, they fall within two standard deviations of the range of values of 108.4°

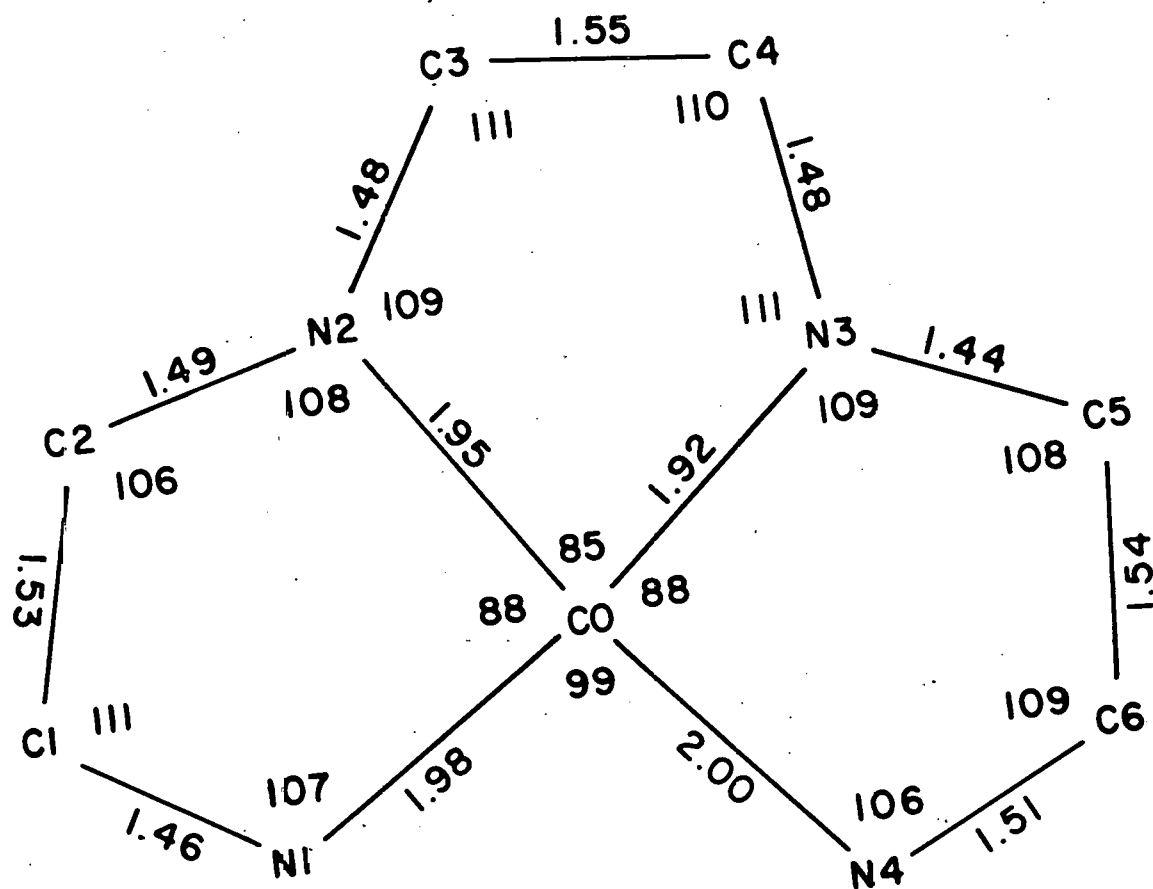


Figure 2. Bond distances and angles within the trien ligand

to 112.3° for Co-N-C bonds, and of 105.2° to 111.4° for N-C-C bonds reported by other investigators of this ligand. The C-N-C bond angles of 116.8° and 114.6° are also reasonable in view of the fact that the Co-N-C angles are, on the average, somewhat less than tetrahedral. These C-N-C angles also agree within three standard deviations with other results obtained in investigations of this ligand.

The bond distances within the trien ligand range from 1.92 to 2.00 Å for Co-N bonds, from 1.44 to 1.51 Å for N-C bonds, and from 1.53 to 1.55 Å for C-C bonds, with average values of 1.96, 1.48, and 1.54 Å, respectively. These distances in no instance differ significantly from previously reported values for other compounds involving the trien ligand coordinated to cobalt.

The four trien nitrogens and the cobalt atom all fall within 0.01 Å of the least squares plane. The three five-membered rings formed by the quadridentate ligand and the cobalt atom are not planar, however, as the carbon atoms are located above and below the N-Co-N planes. Nonetheless, all of the atoms in the trien ligand fall within 0.37 Å of a least squares plane.

As has been described above, the coordination of the cyanide groups to the cobalt is clearly through the carbon. The Co-C average bond distance of 1.90 Å is in good

agreement with previously published values. The average C-N distance of 1.17 Å also agrees quite well with the range of previously reported values, 1.15 to 1.18 Å.^{2,22-24} The fact that no part of the chain N(6)-C(8)-Co-C(7)-N(5) is linear, with bond angles of N(6)-C(8)-Co, C(8)-Co-C(7), and Co-C(7)-N(5) of 174.1, 177.9, and 173.7°, respectively, is somewhat unusual but not surprising. Curry and Runciman² have already observed such a phenomenon. Much of this can be attributed to steric effects both inside the moiety and between moieties (Figure 3). Significant non-bonded distances are given in Table V.

The Cl-O bond distances in the perchlorate group average 1.42 Å and the angles average 109.5°. The relatively large thermal parameters, possibly due to spatial as well as temporal disorder probably account for the large individual deviations from the average values. However, these average values agree reasonably well with previously published values for this anion.²¹ A weak hydrogen bond is possible between N(4) and O(3), which are 3.03 Å apart. Such a hydrogen bond would help stabilize the perchlorate group.

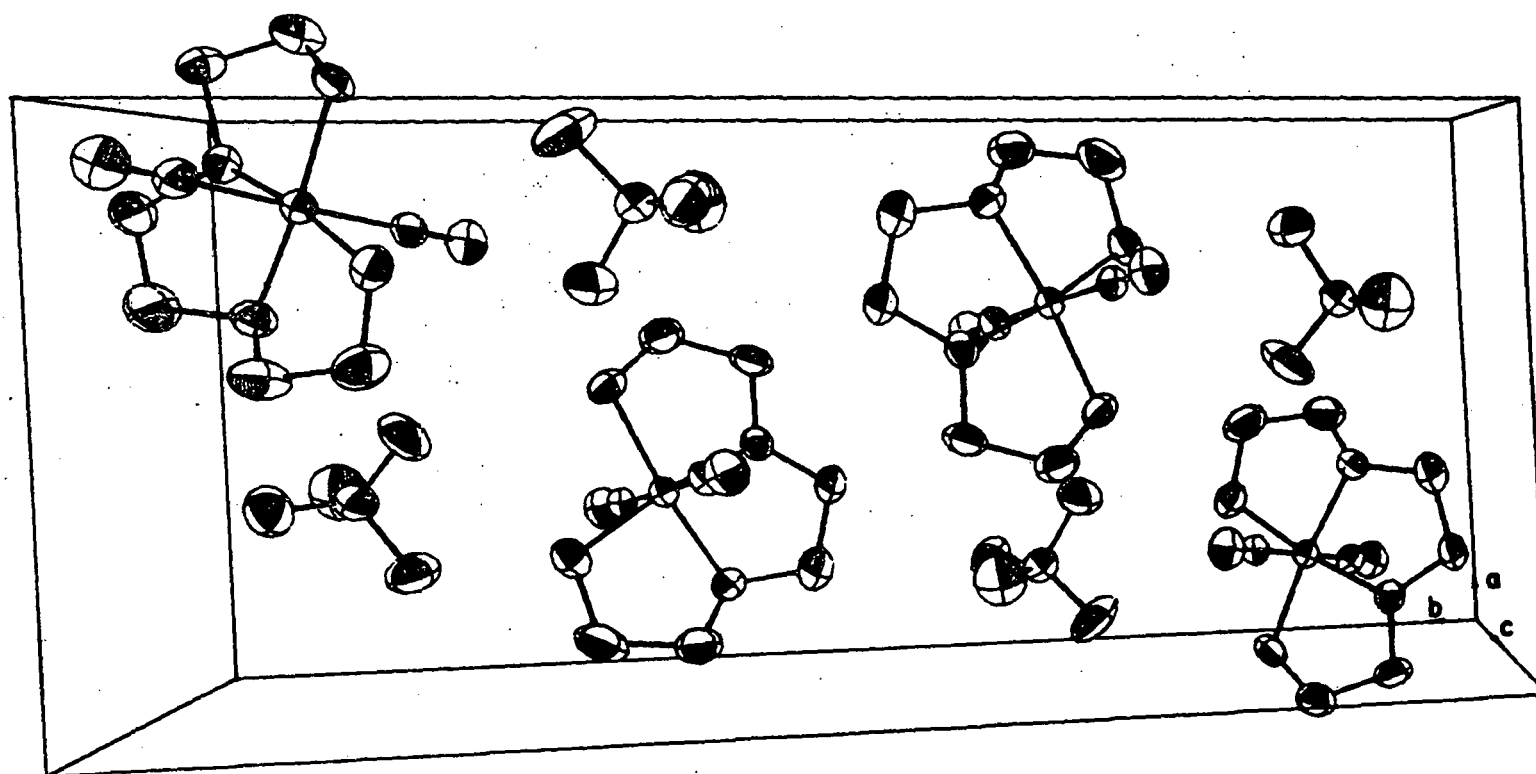


Figure 3. Unit cell showing packing of trans-cyano triethylenetetramine cobalt(III) perchlorate

THE STRUCTURE OF POTASSIUM
ANTIMONY(III) PENTACHLORIDE

Introduction

Structural investigations of antimony halide complexes have been actively pursued in this laboratory during recent years, beginning with the work of Lawton and Jacobson.²⁵ The structures of species containing antimony(III) are of particular interest because of questions concerning the stereochemical role of the lone pair of electrons.

Only a very few antimony(III) chloride structures have been reported in the literature. SbCl_3 exhibits a trigonal pyramid structure with antimony at the apex,²⁶ while in $(\text{NH}_4)_2\text{SbCl}_5$ the chlorine atoms are arranged in a square pyramidal coordination geometry around the antimony.²⁷ In $[\text{C}_5\text{H}_5\text{NH}][\text{Sb}^{\text{III}}\text{Cl}_4]$, the halogen configuration around the antimony can be described as tetragonally distorted octahedral with two of the equatorial atoms removed,²⁸ and SbCl_6^{3-} forms perfect octahedra in $\text{Co}(\text{NH}_3)_6\text{SbCl}_6$.²⁹

Because of the relatively poor determination ($R = 0.24$) of the structure of $(\text{NH}_4)_2\text{SbCl}_5$ and because of the seeming variety of structural geometries possible for antimony(III), it was decided to undertake a structure determination of K_2SbCl_5 .

Experimental

A sample of K_2SbCl_5 was kindly supplied by Dr. Donald Macalady, who prepared the compound in the following manner: Two solutions, one of $SbCl_3$ in 3N HCl and one of KCl in 3N HCl, were combined so that the molar ratio of potassium to antimony in the resulting solution was 5:7. This solution was allowed to stand, and crystals formed by slow evaporation. Microscopic examination revealed many different crystal morphologies. Thin plates appeared to be the basic unit of all these morphologies, however.

A crystal was cut from one of these plates and mounted on the end of a glass fiber with Duco cement thinned with amyl acetate. Preliminary Weissenberg and precession photographs exhibited 2/m Laue symmetry, indicating a monoclinic space group. The following systematic absences were observed: $h0\ell$ when $\ell = 2n + 1$, and $0k0$ when $k = 2n + 1$. These absences are only consistent with the space group $P2_1/c$. The unit cell parameters at 25°C are $a = 8.8686 \pm 0.0007$, $b = 12.4577 \pm 0.0013$, $c = 8.9280 \pm 0.0013$ Å and $\beta = 110.512 \pm 0.011^\circ$. These parameters and their standard deviations were obtained by a least squares fit⁸ to the 2θ values of sixteen independent reflections whose centers were determined by left-right, top-bottom beam splitting on a previously aligned four-circle diffractometer (MoK α radiation, $\lambda = 0.71069$ Å). A calculated

density of 2.711 g/cc for four molecules per unit cell agrees quite well with an observed density of 2.72 ± 0.01 g/cc, determined by flotation techniques.

For data collection the crystal described above, measuring approximately 0.2 mm along each of the crystal axes, was mounted so that the c axis coincided with the ϕ axis of the diffractometer. Data were collected at room temperature using an automated four-circle diffractometer designed and built in the Ames Laboratory. The upper full circle was purchased from STOE and is equipped with encoders (Baldwin Optical) and drive motors. The design of the base allows the encoders to be directly connected to the main θ and 2θ shafts, using solid and hollow shaft encoders, respectively. The diffractometer is interfaced to a PDP-15 computer in a real time mode and is equipped with a scintillation counter. Zirconium-filtered MoK α radiation was used for the data collection. A scan rate of 0.1 second per step of 0.01° in θ was employed with a variable scan range of 35 steps plus 1 step per degree theta. Stationary-crystal, stationary-counter background counts of a quarter of the scan time were taken at the beginning and end of each scan. Before the scan was made a peak height measurement was used to determine if the reflection was observed. To be scanned, the reflection had to exceed the background by

more than six counts. If the reflection met this criterion, the ω setting was then adjusted slightly, if necessary, to maximize the peak height. Within a two-theta sphere of 50° ($\sin\theta/\lambda = 0.595 \text{ \AA}^{-1}$), all data in the hkl and $\bar{h}k\bar{l}$ octants were measured in this manner, using a take-off angle of 4.5° . Of the 1750 reflections examined, 1614 met the peak height criterion and were scanned.

As a general check on electronic and crystal stability, the intensities of three standard reflections were remeasured every twenty-five reflections. These reflections did not vary to any significant degree during the entire period of data collection.

The intensity data were corrected for Lorentz-polarization effects and for effects due to absorption. An absorption correction was made using the Tompa-Alcock absorption correction program^{30,31} using a linear absorption coefficient of $\mu = 52.28 \text{ cm}^{-1}$. The maximum and minimum transmission factors were 43.95% and 35.98%, respectively. The estimated error in each intensity was calculated by

$$\sigma_I^2 = C_T + 2C_B + (0.03 C_T)^2 + (0.03 C_B)^2 + (0.03 C_I)^2 T_a^2,$$

where C_T , C_B , C_I , and T_a are the total count, the

background count, the net count, and the transmission factor, respectively, and the factor 0.03 represents an estimate of non-statistical errors. The estimated deviations in the structure factors were calculated by the finite difference method.¹⁰ Of the 1614 independent reflections, 1543 were considered observed ($> 2.0\sigma_F$).

Solution and Refinement

The position of the antimony atom was obtained from analysis of a sharpened three-dimensional Patterson function.¹¹ The remaining atoms were found by successive structure factor¹² and electron density map calculations.¹⁴ These atomic positions were refined by a full matrix least squares procedure,¹² minimizing the function $\sum w(|F_o| - |F_c|)^2$, where $w = 1/\sigma_F^2$, to a conventional discrepancy factor of $R = 0.169$. The scattering factors used were those of Hanson *et al.*,¹⁵ modified for the real and imaginary parts of anomalous dispersion.¹⁶

An electron density difference map verified that all the atoms had been accounted for, but indicated that some anisotropic motion, particularly of the antimony, was present. Accordingly, anisotropic refinement was begun and after four cycles of refinement, values of R and wR of 0.054 and 0.078, respectively, were obtained.

A final electron density difference map showed no peaks greater than $0.9 \text{ e}/\text{\AA}^3$. A final statistical analysis of $\overline{w\Delta^2}$, where $\Delta = (|F_o| - |F_c|)$, as a function of the scattering angle and magnitude of F_o revealed no unusual trends and suggests that the relative weighting scheme used is a reasonable one.

The final positional and thermal parameters are listed in Table VII. The standard deviations were calculated from the inverse matrix of the final least squares cycle. Bond lengths, bond angles, and significant non-bonded distances¹⁷ are listed in Table VIII. The final values of the observed and calculated structure factors are listed in Table IX.

Description and Discussion

The configuration of SbCl_5^- in K_2SbCl_5 is essentially that of a square pyramid which has been distorted by interionic and packing forces. The inversion-related anions are packed approximately base to base, as depicted in Figure 4.¹⁸ The axial antimony-chlorine bond length is $2.385 \text{ \AA}$, in good agreement with the axial distance in $(\text{NH}_4)_2\text{SbCl}_5$ ($2.36 \text{ \AA}$),²⁷ the shorter distance ($2.38 \text{ \AA}$) in $[\text{C}_5\text{H}_5\text{NH}][\text{Sb}^{\text{III}}\text{Cl}_4]$,²⁸ and only slightly longer than the distance ($2.32 \text{ \AA}$) in SbCl_3 .²⁶

Table VII. Final atomic coordinates and thermal parameters ($\times 10^4$) for K_2SbCl_5 ^a

Atom	x	y	z	β_{11}	β_{22}	β_{33}	β_{12}	β_{13}	β_{23}
Sb	0.1835(1)	-0.0068(1)	0.2025(1)	75(1)	42(1)	80(1)	-2(.4)	20(.8)	-3(.4)
Cl(1)	0.2414(3)	0.0959(2)	0.0510(3)	141(4)	55(2)	98(3)	-3(2)	47(3)	3(2)
Cl(2)	-0.0097(3)	0.1519(2)	0.2070(3)	90(3)	51(2)	160(4)	6(2)	47(3)	2(2)
Cl(3)	0.4157(3)	-0.1400(2)	0.2121(3)	143(4)	68(2)	115(4)	35(2)	41(3)	.8(2)
Cl(4)	0.3885(3)	0.1137(2)	0.3563(3)	89(3)	61(2)	99(3)	-17(2)	26(3)	-9(2)
Cl(5)	0.1706(3)	-0.0770(2)	0.4511(3)	118(4)	67(2)	100(3)	-11(2)	40(3)	16(2)
K(1)	0.1853(3)	0.1746(2)	0.5939(3)	135(3)	56(1)	112(3)	2(2)	52(3)	-1(2)
K(2)	0.3742(3)	-0.1285(2)	0.8452(3)	106(3)	94(2)	129(4)	5(2)	43(3)	-24(2)

^a Anisotropic thermal parameters are defined by:

$$T = \exp \left(-h^2 \beta_{11} + k^2 \beta_{22} + l^2 \beta_{33} + hk \beta_{12} + hl \beta_{13} + kl \beta_{23} \right) .$$

Table VIII. Bond lengths, bond angles, and significant non-bonded distances in $K_2SbCl_5^a$

Sb-Cl(1)	2.799(2)	Sb-Cl(2)	2.625(2)
Sb-Cl(3)	2.622(2)	Sb-Cl(4)	2.385(2)
Sb-Cl(5)	2.509(2)		
Cl(4)-Sb-Cl(1)	81.92(7)	Cl(4)-Sb-Cl(2)	83.54(8)
Cl(4)-Sb-Cl(3)	87.06(8)	Cl(4)-Sb-Cl(5)	87.77(8)
Cl(1)-Sb-Cl(2)	88.50(7)	Cl(2)-Sb-Cl(5)	90.43(8)
Cl(5)-Sb-Cl(3)	92.19(3)	Cl(3)-Sb-Cl(1)	87.22(8)
Cl(1)-Sb-Cl(5)	169.69(8)	Cl(2)-Sb-Cl(3)	170.13(8)
Sb-Sb'	3.932(1)	Sb-Cl(2)'	3.881(3)
Cl(1)-Sb'	3.701(2)	Cl(1)-Cl(2)'	3.699(3)
Cl(2)-Cl(5) _i	3.768(3)	Cl(1)-Cl(3) _{ii}	3.832(4)
Cl(1)-K(1) _{iii}	3.187(3)	Cl(1)-K(2) _{iii}	3.290(3)
Cl(2)-K(2) _{iii}	3.168(3)	Cl(1)-K(1) _{iv}	3.247(3)
Cl(2)-K(1) _{iv}	3.147(3)	Cl(3)-K(2) _v	3.190(4)
Cl(2)-K(1)	3.289(3)	Cl(4)-K(1)	3.317(3)

^a Primed atoms are those related by the center of inversion, as in Figure 4. Other symmetry operations referred to are: (i) $-x, \frac{1}{2}+y, -z$; (ii) $x, y, z-1$; (iii) $x, \frac{1}{2}-y, z-1$; (iv) $x, -\frac{1}{2}-y, z-1$; (v) $1-x, -y, -z$.

Table IX. Observed and calculated structure factors

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80																				

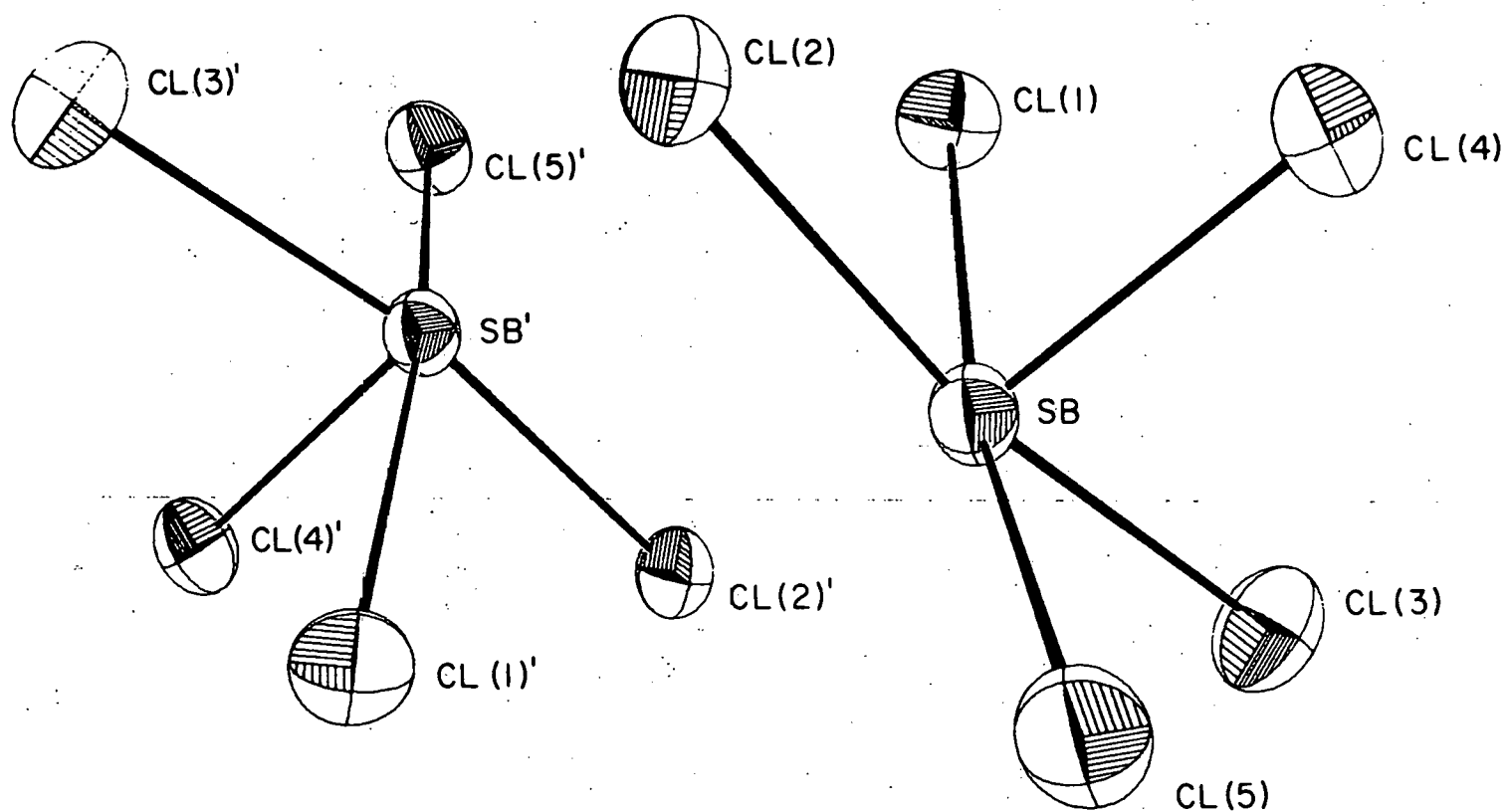


Figure 4. Two inversion-related SbCl_5^- anions

The antimony-chlorine bond distances in the base are all considerably longer than the axial distance. Two of these distances are almost identical (2.622, 2.625 Å) and involve chlorines trans to each other. The other pair of chlorines form bonds of 2.799 and 2.509 Å length, with an average of 2.654 Å. In $(\text{NH}_4)_2\text{SbCl}_5$ all basal antimony-chlorine bonds were found to be essentially of equal length (2.62 Å average) while in $[\text{C}_5\text{H}_5\text{NH}][\text{SbCl}_4]$ the corresponding bond length for chlorines trans to one another is 2.63 Å.

In the present study, the lengthening of the Sb-Cl(1) distance to 2.799 Å appears to be due to electrostatic repulsions and packing effects, as it is this chlorine that is involved in the closest non-bonded contacts; significant non-bonded distances are given in Table VIII. An antimony atom is only 3.701 Å from Cl(1), whereas the sum of the van der Waal's radii is 4.0 Å. Also, the shortest chlorine-chlorine distance found, 3.699 Å, is between this chlorine and Cl(2)'. Both these distances would become significantly shorter if the Sb-Cl(1) bond were shortened. Thus, it can be inferred that this bond can be readily distorted if more efficient packing of the ions results. The shortening of the Sb-Cl(5) bond appears to be a trans effect in response to the lengthening of the Sb-Cl(1) bond.

The observed bond lengths of the basal antimony-chlorine bonds described above are consistent with characterizing the antimony bonding orbitals as being composed primarily of p-orbitals as in the three-center four-electron bonding scheme described by Porter and Jacobson.³² The lone pair appears to have a comparatively small stereochemical effect. This is supported by the relatively short antimony-antimony distance of 3.932 Å, where localized lone pairs, if present, would have to be directed toward one another. Distortions of the Cl-Sb-Cl bond angles from the expected 90° (cf. Table VIII) can be explained by interionic repulsions between inversion-related complexes.

The arrangement of the SbCl_5^- complexes in the unit cell is such that the chlorine atoms approximate a closest packed arrangement in the bc plane, as is evident in Figure 5, with the shortest chlorine-chlorine distances approximating the sum of the van der Waal's radii. None of the potassium ions lie between these planes, but rather are located among the SbCl_5^- ions in the planes. The shortest potassium-chlorine distance is 3.147 Å.

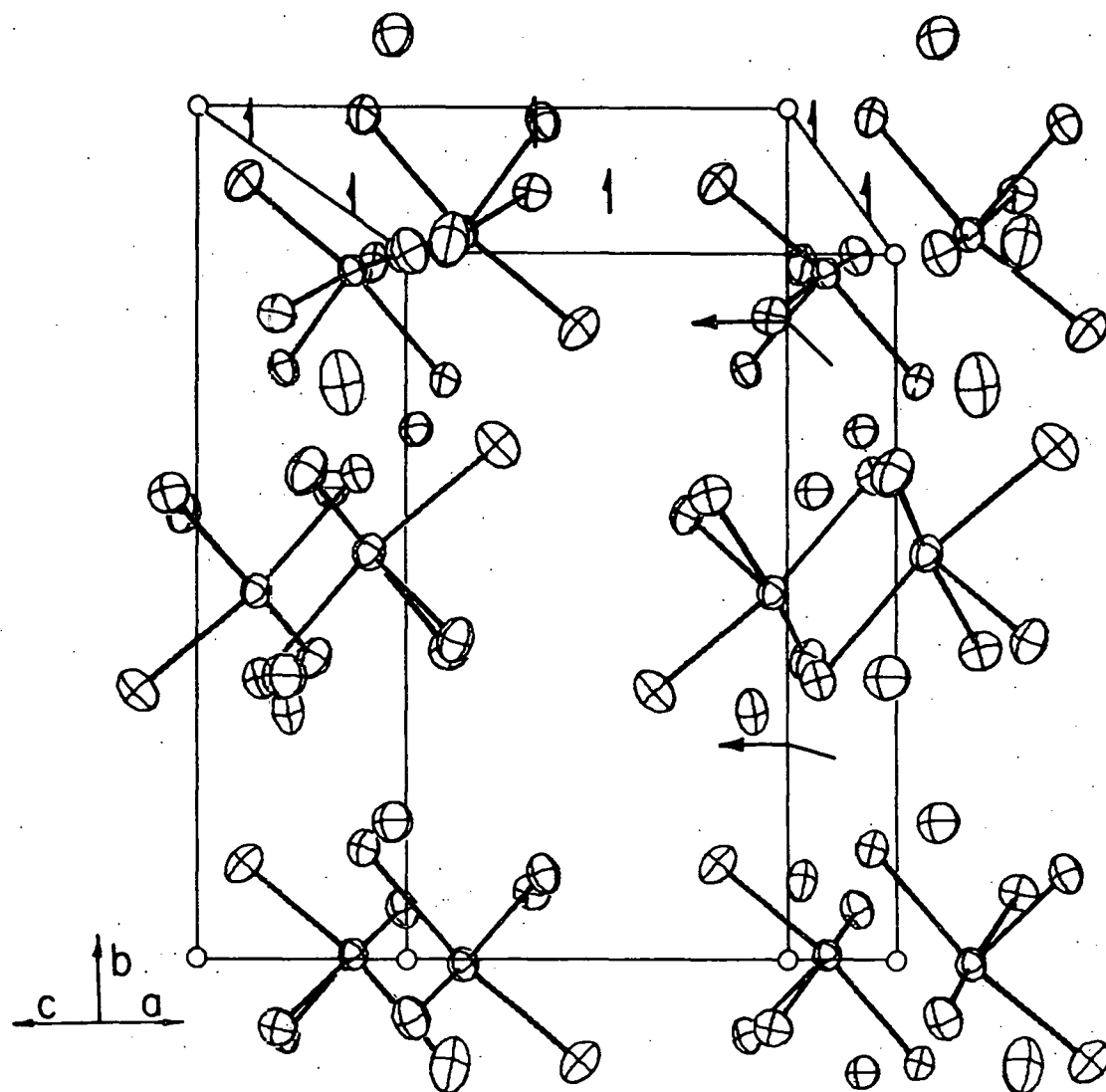


Figure 5. Packing diagram of K_2SbCl_5

ALOP: A PROGRAMMED, SEMI-AUTOMATIC VERSION
OF THE PSEUDO HEAVY ATOM TECHNIQUE

Introduction

The increasing availability of high speed digital computers has enabled the crystallographer to make much more frequent use of mathematical techniques which previously were extremely time consuming. This fact has greatly enhanced the development and usage of direct methods, which recently have evolved to such an extent as to permit semi-automatic solution of crystal structures. In contrast, such indirect methods as Patterson superposition techniques have been employed more and more infrequently in recent times. Despite their great power, these latter methods require a great deal of human intervention and are somewhat tedious to perform. Clearly, what is required is a series of programs which would enable one to solve a structure using superposition techniques but requiring a minimum of human intervention.

This series of programs probably would have greatest applicability to, and thus should be specifically designed to solve, the pseudo heavy atom problem, in which the "heavy" atom does not contribute enough to the phasing to make heavy atom methods feasible. This problem occurs with compounds in which there are many light atoms and but

few heavy atoms, such as transition metal complexes or heavy atom derivatives of organic compounds.

In what follows, the essential features of this series of programs are detailed. The techniques employed naturally divide into two categories: (1) preparation of a Patterson map suitable for evaluation, and (2) utilization of this map to solve the structure.

Map Preparation

A sharpened Patterson map¹¹ is created on either tape or disk by the program ALFF¹⁴ or any other similar Fourier series program. However, in this form the map is somewhat cumbersome to analyze. Hence, the program ALPP (Ames Laboratory Peak Picker) finds and outputs the heights and positions of all the peaks above a certain limit on the Patterson map. ALPP is divided into four subprocedures, the function of which is described below, and a main procedure, which controls the order of execution of the subprocedures. The program listing for ALPP is given in Appendix A.

Input to the first subprocedure, SETUP, consists of the size of the map and the minimum height of a peak which should be recognized. This subprocedure then reads and rewrites the map by layers, setting all points less than the minimum limit equal to zero.

The second subprocedure, LAYERS, reads these map layers and outputs layers with all non-peak grid points negated. The essence of this subprocedure is the subroutine PICKER, which is flowcharted in Figure 6. PICKER analyzes a line of the map point by point. The absolute value of each point is compared with that of the point before it. The lesser of the two is negated. LAYERS calls PICKER for each row and each column of the layer, and then compares points located diagonally to each point, negating those with smaller absolute values.

The next subprocedure, NTRLAY, compares the absolute value of a peak with those of the nine peaks adjacent to it in the next layer, again negating the smaller values. The only positive grid points which now remain are those of peaks. Next, these peak locations and heights are output and the modified map is printed, if desired for debugging purposes.

The final subprocedure, PKSORT, is a modified PL/I translation of QSTSRIT. PKSORT sorts the peaks in order of decreasing height and outputs the ordered peaks.

The entire program runs in less core and requires somewhat less execution time than does ALFF. Thus, it is feasible to run the two programs back to back as one job.

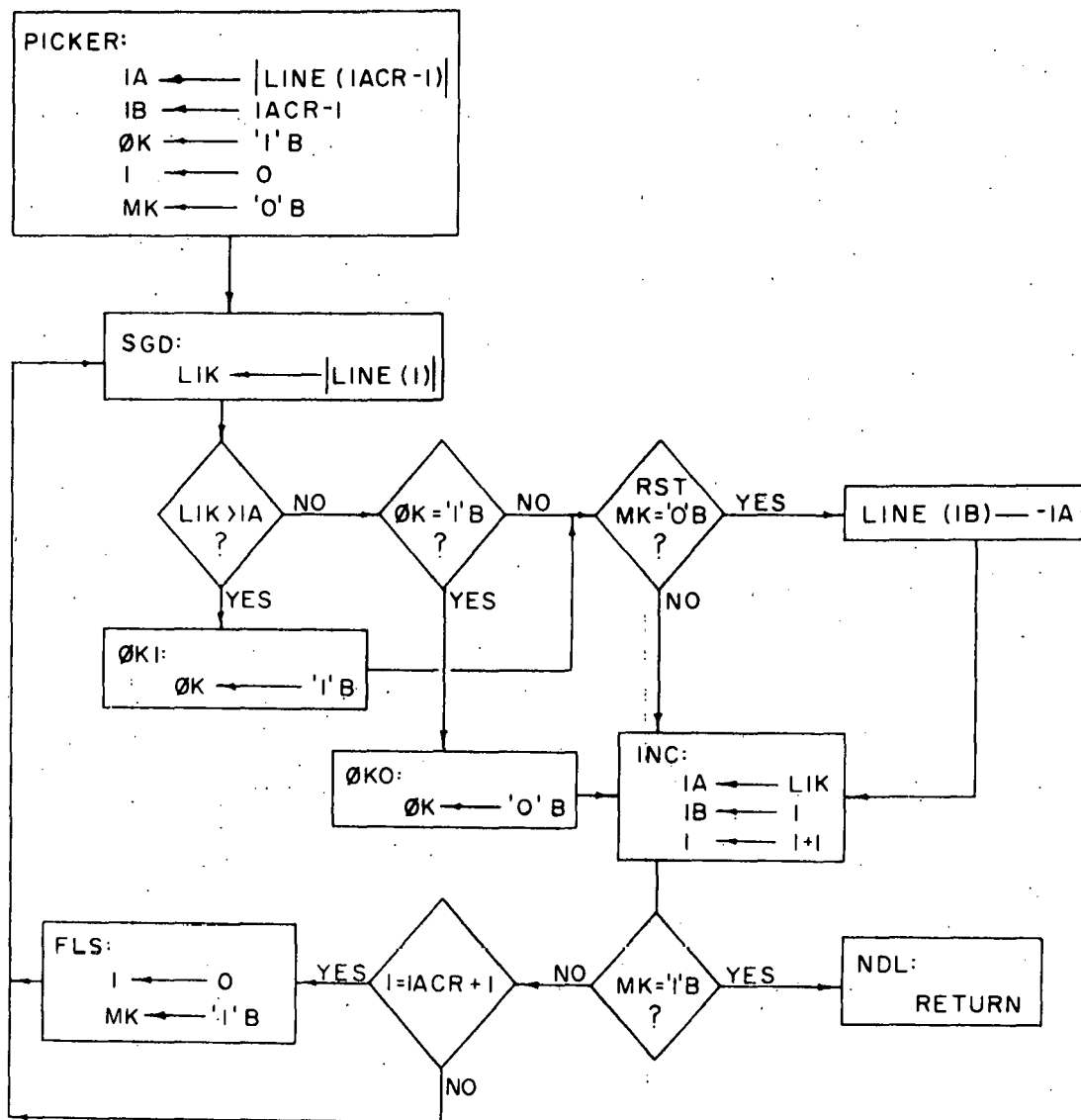


Figure 6. Flowchart of subroutine PICKER

Solution of the Structure

The main program of the series is ALOP (Ames Laboratory Origin Picker), and the program listing is given in Appendix B. ALOP is divided into a main procedure and seven subprocedures.

The main procedure reads in the size of the map, the number of peaks produced by ALPP, and the symmetry operations of the space group under consideration. These are in the form: $p_x x + q_x$, $p_y y + q_y$, $p_z z + q_z$, where p_x , p_y , $p_z = 1$ or -1 and q_x , q_y , $q_z = 0$ or $\frac{1}{2}$. Thus one can represent an equivalent position produced by: an inversion, a two-fold axis, a two-fold screw axis, a mirror plane in one of the three crystal directions or an a-, b-, or c-glide plane. Any of the triclinic, monoclinic, or orthorhombic space groups can be represented by these five symmetry operations (except $Fdd2$ or $Fddd$). In addition, any of the other 230 crystallographic space groups can be converted into a space group which only uses these operations, although some loss of symmetry generally occurs.

The first subprocedure, PART1, searches the peaks produced by ALPP for a suitable heavy atom peak. This peak must be among the largest 20% of the peaks. In addition, if any of its coordinates, u , v , w , is equal to 0 or $\frac{1}{2}$ of the unit cell, then it must be at least twice as large as the largest peak which has no one of u , v , w

equal to 0 or $\frac{1}{2}$. These criteria assure that the heavy atom peak chosen is not solely a Harker vector, but allow the choice of a heavy atom which has 0 or $\frac{1}{2}$ as one of its three coordinates, such as the antimony atom in K_2SbCl_5 .

When PART1 finds a suitable heavy atom peak, it prints its coordinates, u_H , v_H , w_H , and uses it as the shift vector of an in-core algebraic superposition. For a peak u , v , w , to be retained, there must also be a peak at $u' = u + u_H$, $v' = v + v_H$, $w' = w + w_H$ in the list of peaks produced by ALPP. In practice, since ALPP only determines the maximum grid point, and not the center, of each peak, these requirements are somewhat too stringent and thus u' , v' , w' is permitted to be off by one grid point in each direction. The values of u' , v' , w' thus found are output for subsequent use.

PART2 assumes that the peaks produced by PART1 represent an electron density map of the compound, with its origin shifted to t_x , t_y , t_z , i.e., the following relations hold: $u_i = x_i + t_x$, $v_i = y_i + t_y$, $w_i = z_i + t_z$, where x_i , y_i , z_i are the coordinates of the peak in electron density space. When the symmetry operations defined above are applied to a peak at x , y , z they produce an equivalent peak at $p_x x + q_x$, $p_y y + q_y$, $p_z z + q_z$. Thus for every peak at $u = x + t_x$, $v = y + t_y$, $w = z + t_z$ there is an equivalent peak at $u' = p_x x + t_x + q_x$, $v' = p_y y + t_y$

+ q_y , $w' = p_z z + t_z + q_z$. In Table X the results of subtracting and adding u, v, w and u', v', w' are given for all permutations of p_x, p_y, p_z . The asterisked (*) sums determine values of t_x, t_y , and t_z . PART2 and PART3 accumulate all possible values of t_x, t_y , and t_z for the symmetry operations, as shown in Table XI. PART3 and PART4 write these values, along with the frequency of occurrence of each, on file SORTIN for future use. If any one of t_x, t_y, t_z is not determined, as is the case with all but inversion symmetry, it is set equal to -1. In addition to writing out the exact values of t_x, t_y , and t_z , those which are as much as one grid point off in each direction are also written out. Tables X and XI also demonstrate that values of t_x, t_y, t_z determined by two-folds, screws, mirrors, and glides have to meet criteria before they are acceptable, whereas inversions do not. Therefore, a greater weight is placed on these former values.

At this point, the following items may be present on file SORTIN: t_x, t_y, t_z triples; t_x, t_y ; t_y, t_z ; or t_x, t_z doubles; or t_x, t_y , or t_z singles. These are sorted by the IBM procedure IHESRTA within their different types in order of decreasing frequency of occurrence. PART5 reads and stores 1/64 of the triples, 1/16 of the doubles, and 1/4 of the singles, all of which have the largest frequencies. These singles, doubles, and triples

Table X. Relationships used in determining t_x , t_y , t_z

Quantity	u	v	w
U	$A = x + t_x$	$B = y + t_y$	$C = z + t_z$
U_0	$A + q_x$	$B + q_y$	$C + q_z$
$U_0 + U$	$2A + q_x$	$2B + q_y$	$2C + q_z$
$U_0 - U$	q_x	q_y	q_z
U_1	$-x + t_x + q_x$	$B + q_y$	$C + q_z$
$U_1 + U$	* $2t_x + q_x$	$2B + q_y$	$2C + q_z$
$U_1 - U$	$-2x + q_x$	q_y	q_z
U_2	$A + q_x$	$-y + t_y + q_y$	$C + q_z$
$U_2 + U$	$2A + q_x$	* $2t_y + q_y$	$2C + q_z$
$U_2 - U$	q_x	$-2y + q_y$	q_z
U_3	$-x + t_x + q_x$	$-y + t_y + q_y$	$C + q_z$
$U_3 + U$	* $2t_x + q_x$	* $2t_y + q_y$	$2C + q_z$
$U_3 - U$	$-2x + q_x$	$-2y + q_y$	q_z
U_4	$A + q_x$	$B + q_y$	$-z + t_z + q_z$
$U_4 + U$	$2A + q_x$	$2B + q_y$	* $2t_z + q_z$
$U_4 - U$	q_x	q_y	$-2z + q_z$
U_5	$-x + t_x + q_x$	$B + q_y$	$-z + t_z + q_z$
$U_5 + U$	* $2t_x + q_x$	$2B + q_y$	* $2t_z + q_z$
$U_5 - U$	$-2x + q_x$	q_y	$-2z + q_z$

Table X. (Continued)

Quantity	u	v	w
U_6	$A + q_x$	$-y + t_y + q_y$	$-z + t_z + q_z$
$U_6 + U$	$2A + q_x$	* $2t_y + q_y$	* $2t_z + q_z$
$U_6 - U$	q_x	$2y + q_y$	$2z + q_z$
U_7	$-x + t_x + q_x$	$-y + t_y + q_y$	$-z + t_z + q_z$
$U_7 + U$	* $2t_x + q_x$	* $2t_y + q_y$	* $2t_z + q_z$
$U_7 - U$	$2x + q_x$	$2y + q_y$	$2z + t_z$

Table XI. Restrictions placed on the determination of t_x , t_y , t_z by the type of symmetry element

Type of symmetry element	Determines	Restrictions
Plane perpendicular to x	t_x	$v_1 - v = q_y, w_1 - w = q_z$
Plane perpendicular to y	t_y	$u_2 - u = q_x, w_2 - w = q_z$
Plane perpendicular to z	t_z	$u_4 - u = q_x, v_4 - v = q_y$
Axis in x	t_y, t_z	$u_6 - u = q_x$
Axis in y	t_x, t_z	$v_5 - v = q_y$
Axis in z	t_x, t_y	$w_3 - w = q_z$
Inversion	t_x, t_y, t_z	None

are then merged with each other as described in Table XII, with a latitude of one grid point allowed in each direction. Thus, if a single in t_x equals the t_x of a t_x, t_y double or is off by one grid point, then the frequency of the t_x, t_y double is increased by the frequency of the single. A record is kept of each such merge.

This record is used in PART6, where all of the possible mergings for each symmetry element present are computed. Consider, as an example, the space group $P2_1/c$ which has an inversion producing a triple t_x, t_y, t_z , a two-fold screw axis producing a double in t_x, t_z and a c -glide producing a single in t_y . PART5 should have merged a single in t_y and a double in t_x, t_z with each triple and left a record of having done so. The values of the triples which were not suitably merged are eliminated, and the triple remaining with the highest frequency of occurrence is then output for use in PART7.

Sometimes, however, a space group may not have an inversion. If it has three two-fold or screw axes, these will produce three doubles: $t_{x1} t_{y1}, t_{x2} t_{z2}, t_{y3} t_{z3}$. In the cases where $t_{x1} = t_{x2}, t_{y1} = t_{y3}$, and $t_{z2} = t_{z3}$, a triple is created with a frequency equal to the sum of the frequencies of the three doubles. The highest such triple is then taken as the origin. If any one of t_x, t_y , or t_z is not determined by the above procedures, it

Table XII. Merging of singles and doubles into doubles and triples

Single or double	Double or triple merged into
t_x	$t_x t_y, t_x t_z, t_x t_y t_z$
t_y	$t_x t_y, t_y t_z, t_x t_y t_z$
t_z	$t_x t_z, t_y t_z, t_x t_y t_z$
$t_x t_y$	$t_x t_z, t_y t_z, t_x t_y t_z$
$t_x t_z$	$t_x t_y, t_y t_z, t_x t_y t_z$
$t_y t_z$	$t_x t_y, t_x t_z, t_x t_y t_z$

is set to zero, as the origin may have any value in that direction.

PART7 computes the electron density space coordinates of all the peaks found in PART1 by using the equations: $x_i = u_i - t_x$, $y_i = v_i - t_y$, $z_i = w_i - t_z$. For each peak, this procedure then attempts to find the symmetry equivalent peaks. If at least half of the equivalent peaks are present, a peak is output with the appropriate fractional coordinates.

ALOP uses less than 32K words of main core storage and runs in less than five minutes of CPU time for a 32 x 32 x 32 map with less than 500 peaks input from ALPP.

Results

The programs ALPP and ALOP were tried on two different problems and the technique was successful in both cases. In the first case, the structure of D-(1,5)-glucono lactone (space group $P2_12_12_1$)³³ was "chlorinated" by substituting chlorines for two of the hydrogens, yielding a molecule with two chlorines, six oxygens, and six carbons. The heavy atom ratio for this compound was $\Sigma Z_{\text{heavy}}^2 / \Sigma (Z_{\text{light}})^2 = 0.963$. All of the non-hydrogen atoms were used in a structure factor calculation and a sharpened Patterson map was computed from these structure factors. ALPP found 502 off-origin peaks in this map with heights rang-

ing from 13 to 234. A heavy atom peak, which proved to be an oxygen-chlorine vector, was found at $u = 30$, $v = 26$, $w = 3$ with a height of 99 on the $32 \times 32 \times 32$ map. In-core superposition retained 187 peaks with a minimum height of 23. This is a good demonstration of how the superposition process tends to eliminate spurious peaks. Multiple merging produced eleven possible origins, of which the one with the highest frequency of occurrence was $t_x = 14$, $t_y = 13$, $t_z = 12$. When this value was used as an origin, 33 symmetry independent peaks were retained. Subsequent least square refinement of the positional parameters and atom multipliers of these 33 positions through twelve least squares cycles resulted in a conventional discrepancy factor of $R = 0.206$. The scattering factor curve for this and the subsequent test case is defined by:

$$\hat{f}_i = \frac{\sum_{j=1}^N f_{ij}}{\sum_{j=1}^N Z_j},$$

where f_{ij} is the normal scattering factor for the j^{th} atom over a range of $\sin\theta/\lambda$,¹⁵ Z_j is the atomic number of the j^{th} atom, and the sum is over all the atoms in the unit cell.

The second test case was that of $K_2\text{SbCl}_5$ which crystallizes in space group $P2_1/c$ with four eight-atom moieties per unit cell. The heavy atom ratio for this compound is 1.200. ALPP found 258 off-origin peaks on the sharpened

Patterson map, ranging in height from 17 to 508. A heavy atom peak, which was produced by an antimony-antimony vector, was found at $u = 20$, $v = 16$, $w = 3$ with a height of 282 on the $32 \times 32 \times 32$ map. In-core superposition retained 112 peaks. The origin with the highest frequency of occurrence was at $t_x = 10$, $t_y = 0$, $t_z = 9$, and its use yielded 20 symmetry independent peaks. Sixteen cycles of full matrix least squares refinement of the positional parameters and atom multipliers of these positions led to the removal of eleven of them as their atom multipliers dropped to less than 0.40. The remaining nine positions refined to yield a conventional discrepancy factor of $R = 0.240$.

2

PSST: A COMBINATION OF PATTERSON SUPERPOSITION
AND SIGMA-2 TECHNIQUES FOR PHASE DETERMINATION

Introduction

At present there are two methods commonly used for solving structures of moderate complexity. Direct methods, such as those using the Σ_2 relation,³⁴ are primarily reciprocal space methods, while methods based on the deconvolution of the Patterson function (for a detailed bibliography see Buerger³⁵) are primarily real space methods.

There is a certain parallelism between these two methods and both have their advantages and disadvantages. Both involve some initial choices which can greatly influence the success of the method. The Σ_2 relation can be readily programmed and many automatic or semi-automatic procedures have been developed based on this relation. However, it is usually difficult to make use of known structural information in this approach. Furthermore, if no reasonable structure is produced, the investigator has little recourse but to modify his choice of origin-determining reflections or to closely examine those phases selected at the early and most critical part of this phase determination procedure. With Patterson methods, on the other hand, there are usually a greater number of options initially available corresponding to differing modes of

selection of peaks for superposition. Also, known structural information can be more readily introduced, since a real space representation is being employed. For complex structures, however, large numbers of superpositions are generally required and severe degradation of the structural image can result due to the accumulation of errors in the atom position selections.

The advent of the fast Fourier transform technique and its application to crystallography³⁶ allows rapid real space - reciprocal space conversions. Thus, it is appropriate to consider whether a hybrid direct method - Patterson method approach having greater power than either method alone can be developed. It is just such a hybrid that is described here.

Theoretical Basis of the Method

In direct methods employing the Σ_2 relation, one starts with E's of large magnitude so that phases will be determined with reasonably high probabilities. Due to the fact that the initial contributors are few in number, erroneous phase indications may still result which then propagate in the phase determination procedure. Consider the map produced by a Fourier transform using as non-zero coefficients only those reflections input into the Σ_2 relation (henceforth this map will be referred to as the Σ_2 map). For the phase determination procedure to be successful, it

is necessary that the square of this Σ_2 -map better resemble the true electron density function than does the Σ_2 -map itself. If so, the phases of the transformed coefficients with larger magnitudes should be good approximations to the phases of the corresponding large $|E|$'s.

Since the initial set of E 's is very small in number, possibly only the three origin-determining reflections, it is the characteristics of the Σ_2 -map which should be closely examined. First, if large $|E|$'s are used, there is a high probability that atoms will lie on, or at least near, some of the maxima occurring on this map. Second, there will be a large number of extraneous maxima on the square of the Σ_2 -map -- a number far exceeding the number of atoms in the cell. The first is an asset and the second a liability for successful phase determination. These extraneous peaks come from either maxima or minima on the Σ_2 -map. It is the presence of these extra peaks that greatly inhibits the production of additional phase information.

One would like to modify the square of the Σ_2 -map so that it better resembles the electron density function. An obvious such modification is to eliminate all negative regions (or possibly regions less than a certain lower bound) by setting these regions equal to zero before squaring. Indeed, this technique has been applied by Barrett

and Zwick³⁷ to some extent in the extension and refinement of crystallographic protein phases.

In the initial application of the Σ_2 relation, there are so few phased E's that even with the modification described above, there are large positive regions in many areas of the map which do not correspond to atomic locations. However, the Patterson function contains images of the structure with each atom in turn at the origin. Therefore, if an atomic position can be selected on the Σ_2 -map, a superposition of the appropriately scaled Patterson map on this position should produce a map with considerably fewer extraneous peaks and with much better resemblance to the electron density function. If such a map is then squared to emphasize the higher peaks and transformed, better and more extensive phase information will result. Once a sufficiently large set of phased E's has been obtained, the remaining $|E|$'s can be efficiently phased by normal application of phase extension and refinement techniques of the Σ_2 type.

Application of the Method

Centric case

The compound β -picoline-N-oxide fumaric acid adduct³⁸ was chosen as a centrosymmetric test case. We felt this would be a good test case as the structure had previously been solved only with difficulty by use of a roving model --

vector verification technique after usual superposition and symbolic addition procedures had not proved successful.

This adduct crystallizes in the space group $P2_1/c$ with $a = 3.888$, $b = 14.194$, $c = 14.666$ Å and $\beta = 98.85^\circ$. There are two adducts of formula $C_{16}H_{18}N_2O_{12}$ per unit cell, i.e., the adduct has a center of symmetry. Values of $|E|$ were computed in the ordinary way and there were 270 $|E|$'s greater than 1.0. The three selected origin-determining reflections are given in Table XIII. These three, along with the symmetry-related reflections, were used in a Σ_2 -map calculation ($32 \times 32 \times 32$ grid points). Some typical sections of this map are shown in Figure 7.

The positions of the five highest peaks on this map were noted and in each case checked by examining the Patterson for the presence of vectors between symmetry-related atoms. In each case, such vectors were found and indeed these peaks fell approximately (within 0.5 Å) at the positions of four carbons and a nitrogen in the structure.

All of the negative regions in the Σ_2 -map were then set equal to zero and five independent superpositions were carried out by placing the origin of the Patterson at each of the five peak positions and the symmetry-related points. A sharpened Patterson function was used and the minimum procedure employed.³⁹ The scale of the Patterson was

Table XIII. Origin-determining reflections for the centric test case (β -picoline-N-oxide fumaric acid adduct)

h	k	l	E	Sign
1	0	2	4.17	+
3	1	3	2.53	-
1	14	-5	2.14	+

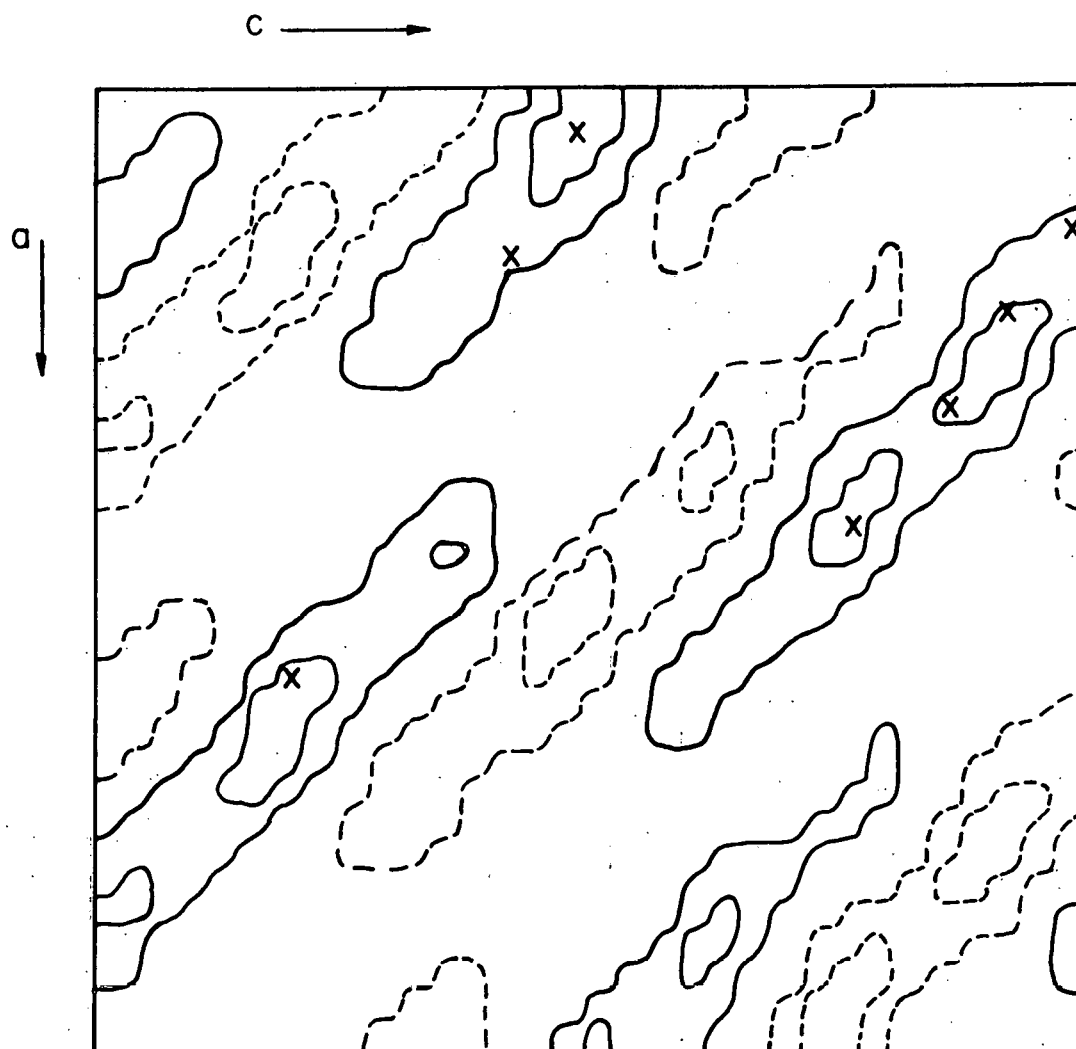


Figure 7a. Composite of layers 3,4,5 of a Σ_2 -map for β -picoline-N-oxide fumaric acid adduct.
— contoured at 40 and 80. ---- contoured at -40 and -80. Atom positions indicated by X.

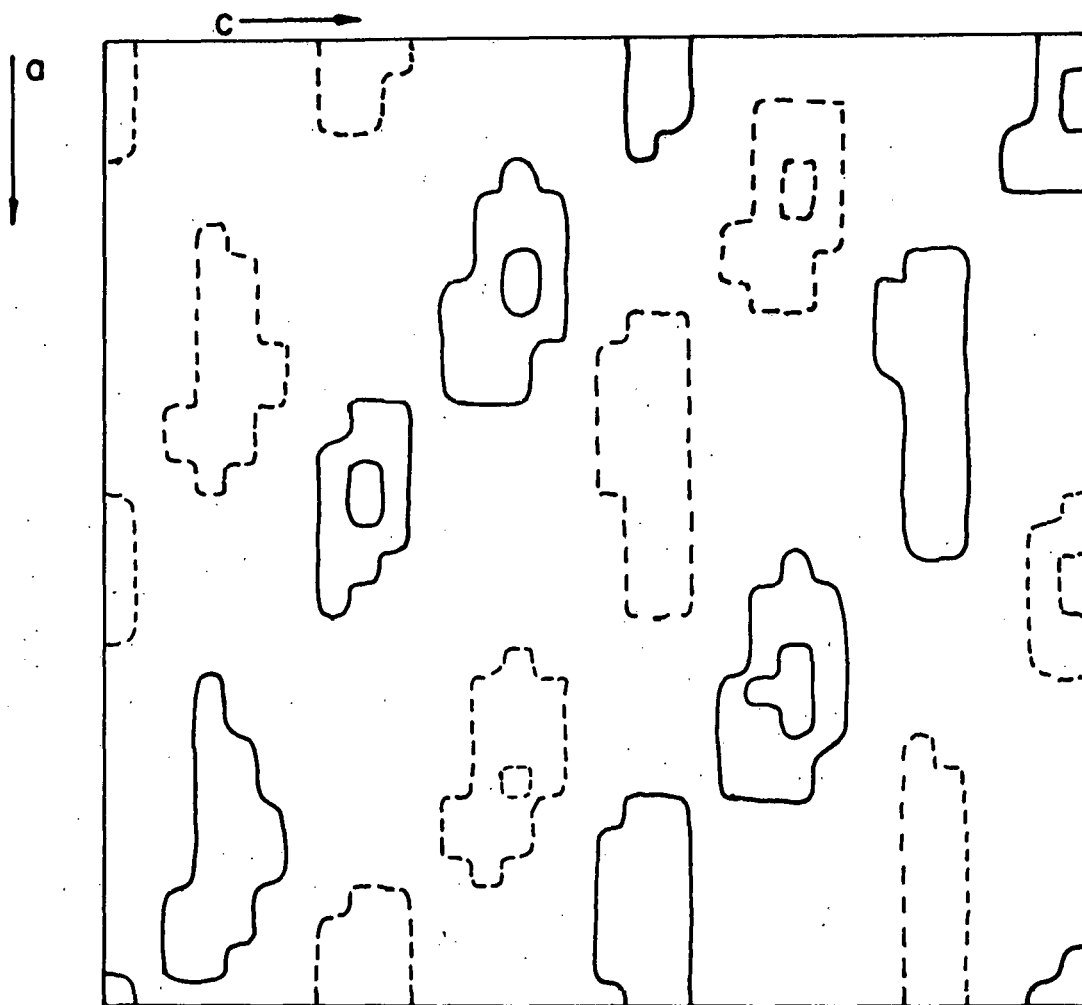


Figure 7b. Layer 9 of a Σ_2 -map for β -picoline-N-oxide fumaric acid adduct. — contoured at 15 and 25. ---- contoured at -15 and -25. No atoms in or near this section.

adjusted so that the value of the highest off-origin peak on the Patterson map was approximately equal to the value of the highest off-origin peak on the Σ_2 -map. Figure 8 shows some typical results using the peak corresponding to the nitrogen atom position as the superposition point.

Each of the five maps was then squared and the resulting transform coefficients (G_{hkl}) calculated using a fast Fourier algorithm.¹⁴ Only the 50 reflections with the largest values of the product $|E^*G|$ and with $|E| > 1.50$ were kept. Some typical results are shown in Table XIV. The signs determined for each hkl were then averaged. (In some cases more than 80% of the 50 largest $|E|$'s were signed correctly in the individual sets.) These signed reflections were then used to compute a new Σ_2 -type map, and negative regions were set equal to zero. The transform of the square of this map was used to obtain signs (92% of which were correct) for input at the 90% confidence level into a phase extending program.⁴⁰ The resulting complete set of 270 phases was used to compute a map from which the positions of all the non-hydrogen atoms in the structure were readily determined. There were no significant spurious peaks on this map. This method has recently been used to solve the structure of diisopropyl-(2,3,4,5-tetraphenyl-cyclopenta-2,4-diene)-phosphate, which crystallizes in space group $P2_1/c$ with 160 non-

Table XIV. Representative results^a obtained for a centric test case (β -picoline-N-oxide fumaric acid adduct)

h	k	l	E	Calculated signs					Known sign
				1	2	3	4	5	
-2	10	4	3.25	-	+	+	+	+	+
-1	11	7	3.13	-	+	+		+	+
0	11	9	3.00	-		+			+
0	12	4	2.94				+		-
-1	10	12	2.80	-	-	-	-	-	-
1	10	8	2.73	+	-	-		-	-
-2	4	12	2.63				+		+
1	11	7	2.55	+	-			-	-

^a The absence of a calculated sign indicates that the value of $|E^*G|$ for that reflection was smaller than the limit used.

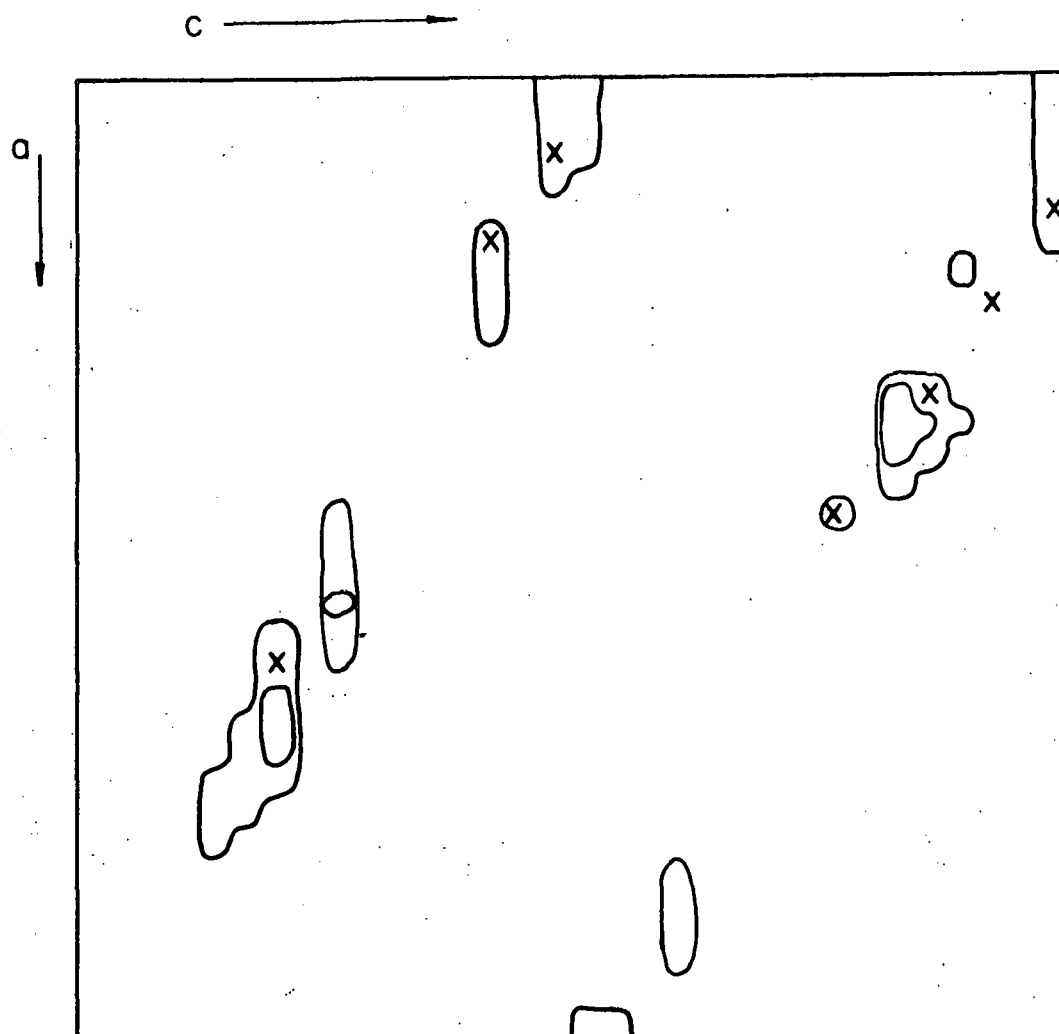


Figure 8a. Results of Patterson map superimposed on the Σ_2 -map of Figure 7, at the four nitrogen equivalent positions. Composite of layers 3,4,5. — contoured at 9 and 18. Atom positions indicated by X.

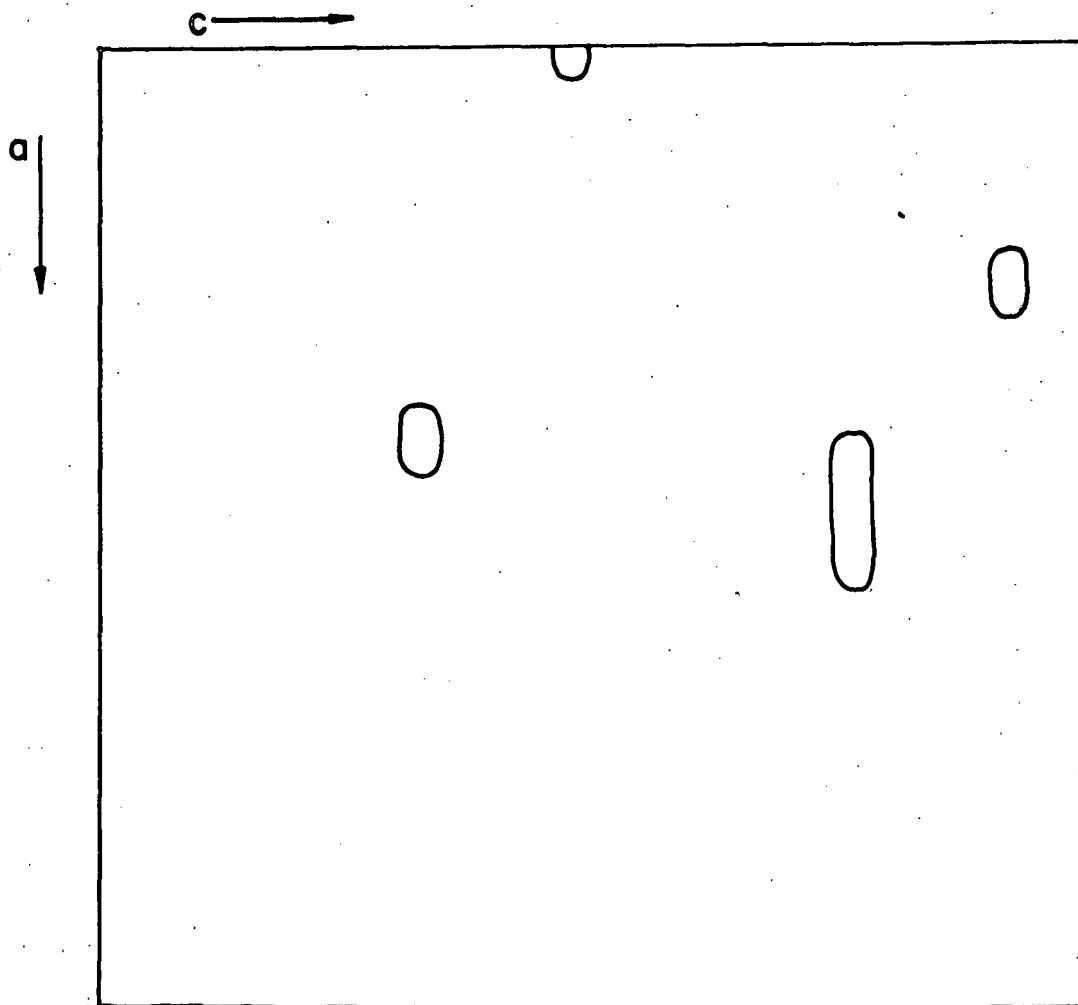


Figure 8b. Results of Patterson map superimposed on the Σ_2 -map of Figure 7 at the four nitrogen equivalent positions. Layer 9. — contoured at 5. No atoms in or near this section.

hydrogen atoms per cell.⁴¹

Acentric case

The compound chosen as a test for the acentric case was D-(1,5)-glucono lactone,³³ which crystallizes in the space group $P2_12_12_1$ with axial lengths $a = 7.838$, $b = 12.322$, $c = 7.544$ Å. Of the 1259 unique observed reflections, 435 have $|E|$ greater than 1.0. Three origin-determining reflections were selected ($|E| = 2.39, 2.51, 2.04$), two of which were non-zonal reflections. To make the test a reasonably severe one, no enantiomorph-selecting reflection was included; the enantiomorph was chosen as part of the superposition procedure.

The Σ_2 -map produced from these and their symmetry-related reflections showed more than 25 large peaks, all of which had relative heights between 120 and 185. The relative height of the other peaks on this map was less than 90. However, only eight of these 25 peaks generated appropriate Harker vectors on the Patterson. Of these eight, four were clearly in one enantiomorph, since they remained when the superposition point was a member of the set.

Using these four peaks and proceeding in a manner similar to the centric case above, the average phases of the 30 largest $|E^*G|$'s with $|E| > 1.40$ were obtained. Some typical results for this acentric structure are given in

Table XV. The transform of the square of the expanded Σ_2 -map yielded initial phases for the 50 largest $|E^*G|$'s with $|E| > 1.40$. These phased E's were then input into a phase-extending program at the 90% confidence level. In the resulting set of 410 phased E's, 390 were within 40° of the published phases and their transform readily revealed all the non-hydrogen atomic positions. As in the centric case, there were no significant spurious peaks on this final map.

Extensions of the Method

Since a reasonably severe test of the method was desired, only three origin-determining reflections were used for the initial Σ_2 -map calculation in each case. Other reflections, phased by either Σ_2 or Σ_1 relations (and perhaps with appropriate weights), can also be included to produce peaks of greater reliability. In the centric case, those Σ_1 reflections which were determined with greater than 90% probability were included in the calculation of the Σ_2 -map. Their addition improved the phase agreement to a small extent. The frequency check procedure⁴² can also be applied to the Σ_2 -map.

It is also possible to include an additional strong reflection in the origin-determining reflections, thus producing two Σ_2 -maps in the centric case, for example. The resulting two sets of averaged phases could then be

Table XV. Representative results^a obtained for an acentric test case (D-(1,5)-glucono lactone)

h	k	l	E	Calculated phases (°)				Known phase
				1	2	3	4	
0	3	6	3.48	270	270	270	270	270
0	4	3	2.67	0	180	180	180	180
0	7	9	2.58		90	90	90	90
0	11	2	2.36	89				90
2	2	6	2.22		277		256	296
1	7	5	2.19			276	284	293
4	-9	-1	2.04	230	243	220	256	252
0	4	0	1.95	179				0
3	-3	-7	1.77	179	171	182	177	197
3	4	2	1.64		261		278	316
1	-3	-2	1.59		83		90	81
0	2	3	1.58	179	0		0	180
2	4	6	1.56	84	88		91	114

^a The absence of a calculated phase indicates that the value of $|E^*G|$ for that reflection was smaller than the limit used.

handled in a similar way as in those direct methods programs which produce multiple solutions.

Lower bounds different from zero can be used for modification of the resultant superposition map. Indeed, some calculations for the centric example have shown that use of a lower bound of 10% of the maximum peak height results in somewhat improved agreement.

From Tables XIV and XV, it is obvious that a straight average is a poor procedure compared to a more judicious method of averaging. Preliminary computations indicate that in the centric case a requirement of a net of two like signs produces a significant improvement in the percentage of correct signs selected.

The phases are also somewhat sensitive to grid point resolution of the maps. In the centric structure, calculations were run using a grid of $0.12 \times 0.45 \times 0.45$ Å resolution. Results improve if a resolution of approximately 0.25 Å is used in all three directions.

Squaring the resultant superposition map appears to give the best phases compared with other powers which could be employed. All exponents from 0.2 to 6.6 in steps of 0.2 were examined for a typical run, with 2.0 appearing the most satisfactory.

RESEARCH PROPOSALS

The proposals for research given below suggested themselves during the course of the research described in this thesis. No claim of an exhaustive literature search for these ideas is implied, although it is the author's belief that they are not presently under investigation.

Due to the fact that more investigators without formal training are employing crystallography as a research tool, there is a desperate need for the development of computer programs which can make many of the routine decisions now requiring human intervention. ALPP eliminates, or at least makes much less tedious, the contouring of a map, and is an example of this type of program. Such a program should be developed to implement the PSSST method. One could write a program to implement the heavy atom technique, which would work in conjunction with ALOP, by cycling structure factor and Fourier series calculations, at the same time deciding whether or not possible atomic positions should be retained. As well as being easy for the initiate to use, the above programs should also permit enough intervention so that the course of their execution can be altered by the more experienced user.

The prime difficulties in implementing direct methods are in choosing between various sets of phases

produced and in discriminating spurious from real atomic peaks. The first problem is being extensively researched and such methods as the comparison of absolute figures of merit and the psi zero test of MULTAN,⁴⁰ the absolute value of rho test reported by W. Ozborn,⁴³ and a plot of psi zero vs. the absolute figure of merit as described by Cochran and Douglas⁴⁴ are all examples of possible solutions. A promising approach to the problem of peak discrimination should be the superposition of the Patterson on a likely atomic position, similar to the technique used in the PSST method. Another approach would be the development of a program which makes use of known interatomic vectors, such as those within a benzene ring, to choose peaks of chemical sense. A third would be the development of a more exact and easily used technique for producing three-dimensional models. A model constructed of wooden spheres suspended by fine lines from a perforated plate would satisfy these requirements.

The relative ease in determining the bonding mode of cyanide in trans-(CN)₂ trien cobalt (III) perchlorate indicates that X-ray diffraction data may be sensitive enough to distinguish between carbon and nitrogen. A more intensive effort on the part of investigators on this problem and perhaps even a reexamination of published data could be initiated.

The number of antimony (III) structures which have been determined is exceedingly small. The investigation of a number of different compounds of formula $M_2Sb^{III}X_5$ ($M = Na, K, Rb, Cs$; $X = Cl, Br, I$) would be of interest in determining the influence of the M^+ and the X^- on the configuration of the SbX_5^- complex.

The Σ_2 -map has a much wider applicability than is described in the PSST method. In combination with the discriminator function⁴⁵ to test possible atomic positions, it should have great power. In addition, using the expanded starting set of phased E's to produce a map which then would be used in place of the Σ_2 -map, is an extension which has promise.

APPENDIX A

PROGRAM LISTING OF ALPP

SORT PEAKS INTO DESCENDING ORDER BY HEIGHT AND OUTPUT

CALL PKSORT(#PEAK);
PUT EDIT ('NORMAL PROGRAM TERMINATION')(PAGE,A);
END CONTOUR;

ALPP0460
*/ ALPP0470
ALPP0480
ALPP0490
ALPP0500

```

* PROCESS('ATR,XREF,NOSTMT,OPT=02');
/* READ IN THE CONTROL CARDS AND INITIALIZE THE MAP
SETUP:  PROCEDURE (IACR,IDWN,ILAY,IPRT,LMT,FW,SP,IACS,PMIN,PMAX);
        DECLARE (IACR, IDWN, ILAY, IPRT, LMT, FW, SP, IACS, PMIN,
                PMAX, ISTEP) FIXED BINARY (15);
        DECLARE LNALFF (0:IACR-1) CONTROLLED FLOAT BINARY,
                (LNFOUR(0:IACR), LAYER (0:IACR,0:IDWN))
        DECLARE PGM CHARACTER (4);
        DECLARE XLM FLOAT BINARY;
        DECLARE TITLE CHARACTER (80);
        DECLARE MPOUT FILE ENVIRONMENT (REGIONAL(1)) KEYED;
        DECLARE STAMP CHARACTER (54) EXTERNAL;
        CALL TM_DT;

/* READ AND INTERPRET THE CONTROL CARDS
GET EDIT (TITLE,PGM,IACR,IDWN,ILAY,IPRT,LMT,FW,SP,IMUD)
        (A(80),A(4),7 F(4),X(44),F(4));
CLOSE FILE (SYSIN);
PUT EDIT (TITLE, STAMP,
        'NUMBER OF GRIDS ACROSS A FULL LINE =',IACR,
        'NUMBER OF LINES DOWN A FULL LAYER = ',IDWN,
        'NUMBER OF LAYERS IN A FULL MAP =',ILAY,
        'LOWER LIMIT OF A RECOGNIZABLE PEAK = ',LMT)
        (A(80),SKIP(2),X(20),A(54),4 (SKIP(2),X(25),A,
        COL(65),F(4)));
PUT EDIT ('THE GENERATING PROGRAM WAS "',PGM,"".')
        (SKIP(2),X(20),A,A(4),A);
IACS = 0;
IF (IPRT=1) THEN PRTR: DO;
        PUT EDIT ('THE MAP WILL BE PRINTED')(SKIP(2),X(25),A);
PUT EDIT ('FIELD WIDTH =',FW,'SPACES BETWEEN LINES =',SP)
        (2 (SKIP(2),X(25),A,F(4)));
CALL PRSETUP (IACS,IACR,FW,SP,PMIN,PMAX,ISTEP);
IF (ISTEP=1) THEN GO TO ABND; ELSE;
        END PRTR; ELSE PUT EDIT ('THE MAP WILL NOT BE PRINTED')
        (SKIP(2),X(25),A);
IF (PGM='ALFF') THEN ALLOCATE LNALFF; ELSE;
ALLOCATE LNFOUR, LAYER;
PUT PAGE;

```

STUP0010
*/ STUP0020
STUP0030
STUP0040
STUP0050
STUP0060
STUP0070
STUP0080
STUP0090
STUP0100
STUP0110
STUP0120
STUP0130
STUP0140
STUP0150
STUP0160
*/ STUP0170
STUP0180
STUP0190
STUP0200
STUP0210
STUP0220
STUP0230
STUP0240
STUP0250
STUP0260
STUP0270
STUP0280
STUP0290
STUP0300
STUP0310
STUP0320
STUP0330
STUP0340
STUP0350
STUP0360
STUP0370
STUP0380
STUP0390
STUP0400
STUP0410

```

OPEN FILE (MAPIN) INPUT RECORD SEQUENTIAL,
FILE (MPOUT) OUTPUT RECORD SEQUENTIAL;
/*
READ MAP LINES, ZERO POINTS LESS THAN LMT, & WRITE MAP LAYERS */
IF (PGM='ALFF') THEN DO;      XLM = LMT;
    NLAY = ILAY-1;      NDWN = IDWN-1;      END;
    ELSE DO;
        NLAY = ILAY - 1;      NDWN = IDWN;      END;
LYLUP: DO L = 0 TO NLAY BY 1;
LNLUP: DO K = 0 TO NDWN BY 1;
    IF (PGM='ALFF') THEN AL: DO;
        READ FILE (MAPIN) INTO (LNALFF);
        DO J = 0 TO IACR-1 BY 1;
            IF (LNALFF(J)<=XLM) THEN LAYER (J,K) = 0;
            ELSE LAYER (J,K) = LNALFF(J);
        END GDLUP;
        LAYER(IACR,K) = LAYER(0,K);
        END AL;
    ELSE FR: DO;
        READ FILE (MAPIN) INTO (LNFOUR);
        DO J = 0 TO IACR BY 1;
            IF (LNFOUR(J)<=LMT) THEN LAYER (J,K) = 0;
            ELSE LAYER (J,K) = LNFOUR (J);
        END PTLUP;
        END FR;
    END LNLUP;
    LAYER(*,IACR) = LAYER(*,0);
    WRITE FILE (MPOUT) FROM (LAYER) KEYFROM(L);
    PUT EDIT ('LAYER NUMBER ',L,' WRITTEN OUT.')
        (SKIP,A,F(3),A);
    END LYLUP;
    FREE LNALFF, LNFOUR, LAYER;
    CLOSE FILE (MAPIN), FILE (MPOUT);
    RETURN;
ABND: END SETUP;

```

```

STUP0420
STUP0430
STUP0440
STUP0450
STUP0460
STUP0470
STUP0480
STUP0490
STUP0500
STUP0510
STUP0520
STUP0530
STUP0540
STUP0550
STUP0560
STUP0570
STUP0580
STUP0590
STUP0600
STUP0610
STUP0620
STUP0630
STUP0640
STUP0650
STUP0660
STUP0670
STUP0680
STUP0690
STUP0700
STUP0710
STUP0720
STUP0730
STUP0740
STUP0750
STUP0760
STUP0770

```

```

* PROCESS('ATR,XREF,NOSTMT,OPT=02');
/* CREATES A TIME - DATE STAMP FOR FUTURE USE
(SUBRG,STRG): TM DT: PROCEDURE;
DECLARE STAMP CHARACTER(54) EXTERNAL, AMPM CHARACTER(4);
DECLARE MOS(12) CHARACTER(9) VARYING INITIAL ('JANUARY','FEBRUARY',
'MARCH','APRIL','MAY','JUNE','JULY','AUGUST','SEPTEMBER',
'OCTOBER','NOVEMBER','DECEMBER');
DECLARE TM CHARACTER(9), TMS(2) CHARACTER(2) DEFINED TM; TM = TIME;
DECLARE DT CHARACTER(6), DS (3) CHARACTER(2) DEFINED DT; DT = DATE;
IF (TMS(1) > 11) THEN AMPM = 'P.M.'; ELSE AMPM = 'A.M.';

```

```

TMDT0010
TMDT0020
TMDT0030
TMDT0040
TMDT0050
TMDT0060
TMDT0070
TMDT0080
TMDT0090
TMDT0100

```

```

STAMP = 'RUN ON ' || MOS(DS(2)) || ' ' || DS(3) || ' ' || 19 || DS(1) || TMDT0110
      ' , AT ' || TMS(1) || ' HOURS ' || TMS(2) || ' MINUTES ' || AMPM; TMDT0120
END TM_DT; TMDT0130

```

```

* PROCESS('ATR,XREF,NOSTMT,OPT=02');
/* A PROCEDURE TO CHECK THE PRINT PARAMETERS AND SET UP PRINTING */ PRSU0010
PRSETUP: PROCEDURE (ACRS,ACRE,FW,SP,PMIN,PMAX,ISTP); PRSU0020
  DECLARE (ACRS,ACRE, /* INITIAL & FINAL ACROSS GRIDS */ PRSU0030
           FW,SP, /* FIELD WIDTH, SPACES BTWN LINES */ PRSU0040
           PMIN,PMAX, /* MINIMUM AND MAXIMUM PEAK HEIGHT */ PRSU0050
           ISTD,PMN,PMX) FIXED BINARY (15); PRSU0060
  DECLARE XXX CHARACTER (9); PRSU0070
  DECLARE MN(2) FIXED BIN INIT (-9,-99); PRSU0080
  DECLARE MX(2) FIXED BIN INIT (99,999); PRSU0090
  DECLARE NUMS(*) CHAR(*) EXTERNAL CONTROLLED, PRSU0100
  HEAD CHAR (132) STATIC EXTERNAL; PRSU0110
  IF (FW*(ACRE-ACRS+1)>128) THEN DO; PRSU0120
    PUT EDIT ('***** FW IS TOO LARGE FOR THE NUMBER OF GRID', PRSU0130
             ' POINTS ACROSS THE PAGE * TERMINATING *****') PRSU0140
    (SKIP(4),COL(20),A,A); PRSU0150
    GO TO TERM; PRSU0160
  IF (FW=2) THEN I=1; PRSU0170
  ELSE I=2; PRSU0180
  PMIN = MN(I); PRSU0190
  PMAX = MX(I); PRSU0200
  IF ((PMIN<MN(I)) | (PMAX>MX(I))) THEN DO; PRSU0210
    PUT EDIT ('***** PMIN OR PMAX OUT OF RANGE * DEFAULTS ', PRSU0220
             ' ASSUMED *****') PRSU0230
    (SKIP(4),COL(20),A,A); PRSU0240
    IF (PMIN<MN(I)) THEN PMIN = MN(I); PRSU0250
    IF (PMAX>MX(I)) THEN PMAX = MX(I); PRSU0260
  IF (PMIN>0) THEN PMIN=0; PRSU0270
  ALLOCATE NUMS (PMIN-1:PMAX+1) CHAR(FW); PRSU0280
/* NUMS ARRAY CONTAINS CHAR REPRESENTATION OF ALL NUMBERS FROM PRSU0290
   PMIN TO PMAX. HEAD IS THE HEADING FOR EACH LAYER */ PRSU0300
BL: DO J = 1 TO 132 BY 1; PRSU0310
    SUBSTR(HEAD,J,1) = ' '; PRSU0320
    END BL; PRSU0330
NM: DO I = PMIN TO PMAX; PRSU0340
    XXX = I; PRSU0350
    NUMS(I) = SUBSTR(XXX,10-FW,FW); PRSU0360
    PMN = PMIN - 1; PRSU0370
    PMX = PMAX + 1; PRSU0380
    NUMS(PMN) = SUBSTR(' ',6-FW,FW); PRSU0390
    NUMS(PMX) = SUBSTR('*****',6-FW,FW); PRSU0400
    J = 5 - FW; PRSU0410
    HD: DO I = ACRS TO ACRE; PRSU0420
        PRSU0430

```

```

J = J + FW;
SUBSTR(HEAD,J,FW) = NUMS(I);
ISTP = 0;
RTN: RETURN;
TERM: ISTP = 1;
GO TO RTN;
END PRSETUP;
END HD;
PRSU0440
PRSU0450
PRSU0460
PRSU0470
PRSU0480
PRSU0490
PRSU0500

```

```

/* PICK PEAKS FROM EACH LAYER AND WRITE OUT THE REVISED LAYERS */
LAYERS: PROCEDURE (IACR,IDWN,ILAY,FW,SP,IACS,PMIN,PMAX);
DECLARE (IACR,IDWN,ILAY,FW,SP,IACS,PMIN,PMAX)
FIXED BINARY (15);
DECLARE MPOUT FILE ENVIRONMENT (REGIONAL(1)) KEYED;
DECLARE (LNACR(0:IACR), LNDWN(0:IDWN), LAYER(0:IACR,0:IDWN))
CONTROLLED FIXED BINARY;
OPEN FILE (MPOUT) UPDATE RECORD DIRECT;
ALLOCATE LAYER, LNDWN, LNACR;
PUT PAGE;

/*
FIND THE PEAKS LAYER BY LAYER
LAYLP: DO L = 0 TO ILAY-1 BY 1;
READ FILE (MPOUT) INTO (LAYER) KEY (L);
/*
GO THROUGH THE LAYERS ROW BY ROW
LINLP: DO K = 0 TO IDWN BY 1;
LNACR(*) = LAYER (*,K);
CALL PICKER (LNACR,IACR);
LAYER(*,K) = LNACR;
END LINLP;
/*
GO THROUGH THE LAYERS COLUMN BY COLUMN
COLUP: DO J = 0 TO IACR BY 1;
LNDWN = LAYER (J,*);
CALL PICKER (LNDWN,IDWN);
LAYER(J,*) = LNDWN;
END COLUP;
/*
CHECK DIAGONAL ELEMENTS
KLUP: DO K = 0 TO IDWN BY 1;
IF (K=0) THEN IDM = IDWN - 1;
ELSE IDM = K - 1;
IF (K=IDWN) THEN IDP = 1;
*/
LYRS0010
LYRS0020
LYRS0030
LYRS0040
LYRS0050
LYRS0060
LYRS0070
LYRS0080
LYRS0090
LYRS0100
LYRS0110
LYRS0120
LYRS0130
LYRS0140
LYRS0150
LYRS0160
LYRS0170
LYRS0180
LYRS0190
LYRS0200
LYRS0210
LYRS0220
LYRS0230
LYRS0240
LYRS0250
LYRS0260
LYRS0270
LYRS0280
LYRS0290
LYRS0300
LYRS0310
LYRS0320
LYRS0330
LYRS0340
LYRS0350
LYRS0360
LYRS0370
LYRS0380
LYRS0390

```

```

JLUP:      DO J = 0 TO IACR BY 1;
            ELSE IDP = K + 1;
            IF (LAYER(J,K) = 0) THEN GO TO NDJL;
            IF (J=0) THEN IAM = IACR - 1;
                ELSE IAM = J - 1;
            IF (J=IACR) THEN IAP = 1;
                ELSE IAP = J + 1;
            LJK = LAYER(J,K);
            LAJK = ABS(LAYER(J,K));
            IF (ABS(LAYER(IAP,IDP)) > LAJK) THEN LJK = -LAJK;
                ELSE LAYER(IAP,IDP) = -ABS(LAYER(IAP,IDP));
            IF (ABS(LAYER(IAP,IDM)) > LAJK) THEN LJK = -LAJK;
                ELSE LAYER(IAP,IDM) = -ABS(LAYER(IAP,IDM));
            IF (ABS(LAYER(IAM,IDP)) > LAJK) THEN LJK = -LAJK;
                ELSE LAYER(IAM,IDP) = -ABS(LAYER(IAM,IDP));
            IF (ABS(LAYER(IAM,IDM)) > LAJK) THEN LJK = -LAJK;
                ELSE LAYER(IAM,IDM) = -ABS(LAYER(IAM,IDM));
            LAYER(J,K) = LJK;
NDJL:      END JLUP;
            END KLUP;
/*
            OUTPUT THE CONTOURED MAP LAYER

            REWRITE FILE (MPOUT) FROM (LAYER) KEY (L);
            PUT EDIT ('PEAK-PICKED LAYER ',L,' HAS BEEN REWRITTEN.')
                (SKIP,A,F(3),A);
            END LAYLP;
            RETURN;
            END LAYERS;

```

ELSE;

*/

* PROCESS('ATR,XREF,NOSTMT,OPT=02');

/* PROCEDURE TO CONTOUR A LINE

PICKER: PROCEDURE (LINE,IACR);

DECLARE LINE (*);

DECLARE (IACR,IA,IB,I,LIK)

DECLARE (OK, MK)

IA = ABS (LINE(IACR-1));

IB = IACR - 1;

OK = '1'B;

I = 0;

MK = '0'B;

SGD: LIK = ABS (LINE(I));

IF (LIK > IA) THEN GO TO OK1;

IF (OK) THEN GO TO OK0;

OK0: OK = '0'B;

GO TO INC;

OK1: OK = '1'B;

FIXED BINARY (15);

FIXED BINARY (15);

BIT (1);

ELSE GO TO RST;

ELSE

LYRS0400
LYRS0410
LYRS0420
LYRS0430
LYRS0440
LYRS0450
LYRS0460
LYRS0470
LYRS0480
LYRS0490
LYRS0500
LYRS0510
LYRS0520
LYRS0530
LYRS0540
LYRS0550
LYRS0560
LYRS0570
LYRS0580
LYRS0590
LYRS0600
LYRS0610
LYRS0620
LYRS0630
LYRS0640
LYRS0650
LYRS0660
LYRS0670
LYRS0680

PIKR0010
PIKR0020
PIKR0030
PIKR0040
PIKR0050
PIKR0060
PIKR0070
PIKR0080
PIKR0090
PIKR0100
PIKR0110
PIKR0120
PIKR0130
PIKR0140
PIKR0150
PIKR0160
PIKR0170

RST:	IF (-MK) THEN LINE(IB) = -IA;	ELSE:	PIKR0180
INC:	IA = LIK;		PIKR0190
	IB = I;		PIKR0200
	I = I + 1;		PIKR0210
	IF (MK) THEN GO TO NDL;	ELSE:	PIKR0220
FLS:	IF (I = IACR+1) THEN GO TO FLS;	ELSE GO TO SGD;	PIKR0230
	I = 0;		PIKR0240
	MK = '1'B;		PIKR0250
	GO TO SGD;		PIKR0260
NDL:	RETURN;		PIKR0270
	END PICKER;		PIKR0280

* PROCESS('ATR,XREF,NOSTMT,OPT=02');		NRLY0010
/* PICK PEAKS BETWEEN LAYERS AND OUTPUT THEIR POSITION AND HEIGHT */		NRLY0020
NTRLAY: PROCEDURE (IACR,IDWN,ILAY,FW,SP,IACS,PMIN,PMAX,#PEAK,IPRT);		NRLY0030
DECLARE (IACR,IDWN,ILAY,FW,SP,IACS,PMIN,PMAX,#PEAK,IPRT)		NRLY0040
	FIXED BINARY (15);	NRLY0050
DECLARE (LAYER(0:IACR,0:IDWN), LYRB4(0:IACR,0:IDWN))		NRLY0060
	CONTROLLED FIXED BINARY (15);	NRLY0070
DECLARE HEAD		NRLY0080
DECLARE 1 PEAK,		NRLY0090
	2 (U,V,W,VALU)	NRLY0100
DECLARE MPOUT	FILE ENVIRONMENT(REGIONAL(1)) KEYED,	NRLY0110
PEAKS	FILE RECORD SEQUENTIAL;	NRLY0120
DECLARE LNACR(0:IACR)	CONTROLLED FIXED BINARY(15);	NRLY0130
ALLOCATE LNACR;		NRLY0140
#PEAK = 0;		NRLY0150
PUT PAGE;		NRLY0160
OPEN FILE (MPOUT) UPDATE RECORD DIRECT;		NRLY0170
ALLOCATE LAYER, LYRB4;		NRLY0180
READ FILE (MPOUT) INTO (LYRB4) KEY (ILAY-1);		NRLY0190
/*		NRLY0200
GO THROUGH THE MAP LAYER BY LAYER		NRLY0210
		NRLY0220
LAYLUP: DO L = 0 TO ILAY-1 BY 1;		NRLY0230
READ FILE (MPOUT) INTO (LAYER) KEY(L);		NRLY0240
IF (L=0) THEN LB4 = ILAY - 1;		NRLY0250
ELSE LB4 = L - 1;		NRLY0260
/*		NRLY0270
GO THROUGH EACH LAYER LINE BY LINE		NRLY0280
		NRLY0290
DOWNLUP: DO K = 0 TO IDWN BY 1;		NRLY0300
IF (K=0) THEN IDM = IDWN - 1;		NRLY0310
ELSE IDM = K - 1;		NRLY0320
IF (K=IDWN) THEN IDP = 1;		NRLY0330
ELSE IDP = K + 1;		NRLY0340
/*		NRLY0350

```

GO THROUGH EACH LINE POINT BY POINT

ACRLUP: DO J = 0 TO IACR BY 1;
        IF (LAYER(J,K) = 0) THEN GO TO NDAL;
        IF (J=0) THEN IAM = IACR - 1;
            ELSE IAM = J - 1;
        IF (J=IACR) THEN IAP = 1;
            ELSE IAP = J + 1;
        LJK = LAYER(J,K);
        LAJK = ABS(LAYER(J,K));

/*
DETERMINE IF THE PEAK SHOULD BE KEPT

        IF (ABS(LYRB4(IAP,IDP)) > LAJK) THEN LJK = -LAJK;
            ELSE LYRB4(IAP,IDP) = -ABS(LYRB4(IAP,IDP));
        IF (ABS(LYRB4(IAP,K)) > LAJK) THEN LJK = -LAJK;
            ELSE LYRB4(IAP,K) = -ABS(LYRB4(IAP,K));
        IF (ABS(LYRB4(IAP,IDM)) > LAJK) THEN LJK = -LAJK;
            ELSE LYRB4(IAP,IDM) = -ABS(LYRB4(IAP,IDM));
        IF (ABS(LYRB4(J,IDP)) > LAJK) THEN LJK = -LAJK;
            ELSE LYRB4(J,IDP) = -ABS(LYRB4(J,IDP));
        IF (ABS(LYRB4(J,K)) > LAJK) THEN LJK = -LAJK;
            ELSE LYRB4(J,K) = -ABS(LYRB4(J,K));
        IF (ABS(LYRB4(J,IDM)) > LAJK) THEN LJK = -LAJK;
            ELSE LYRB4(J,IDM) = -ABS(LYRB4(J,IDM));
        IF (ABS(LYRB4(IAM,IDP)) > LAJK) THEN LJK = -LAJK;
            ELSE LYRB4(IAM,IDP) = -ABS(LYRB4(IAM,IDP));
        IF (ABS(LYRB4(IAM,K)) > LAJK) THEN LJK = -LAJK;
            ELSE LYRB4(IAM,K) = -ABS(LYRB4(IAM,K));
        IF (ABS(LYRB4(IAM,IDM)) > LAJK) THEN LJK = -LAJK;
            ELSE LYRB4(IAM,IDM) = -ABS(LYRB4(IAM,IDM));
        LAYER(J,K) = LJK;
NDAL:   END ACRLUP;
        END DWNLUP;
        REWRITE FILE (MPOUT) FROM (LYRB4) KEY (LB4);
        IF (IPRT=1) THEN CALL OUTP;
        PUT EDIT ('MAP LAYER ',L,' HAS BEEN REWRITTEN')
            (SKIP,A,F(3),A);
        LYRB4 = LAYER;
        END LAYLUP;
        REWRITE FILE (MPOUT) FROM (LAYER) KEY (ILAY-1);
        FREE LYRB4;
        PUT PAGE;
        OPEN FILE (PEAKS) OUTPUT;

/*
FIND AND WRITE OUT ALL THE PEAKS

LUPLAY: DO L = 0 TO ILAY-1 BY 1;
        READ FILE (MPOUT) INTO (LAYER) KEY (L);
        W = L;

```

```

NRLY0360
*/ NRLY0370
NRLY0380
ELSE; NRLY0390
NRLY0400
NRLY0410
NRLY0420
NRLY0430
NRLY0440
NRLY0450
NRLY0460
NRLY0470
*/ NRLY0480
NRLY0490
NRLY0500
NRLY0510
NRLY0520
NRLY0530
NRLY0540
NRLY0550
NRLY0560
NRLY0570
NRLY0580
NRLY0590
NRLY0600
NRLY0610
NRLY0620
NRLY0630
NRLY0640
NRLY0650
NRLY0660
NRLY0670
NRLY0680
NRLY0690
NRLY0700
ELSE; NRLY0710
NRLY0720
NRLY0730
NRLY0740
NRLY0750
NRLY0760
NRLY0770
NRLY0780
NRLY0790
NRLY0800
NRLY0810
*/ NRLY0820
NRLY0830
NRLY0840
NRLY0850

```


A SORT IN ASCENDING ORDER IS ACCOMPLISHED BY REVERSING THE COMPARISONS ON THE SEVEN CARDS INVOLVING LOGICAL COMPARISONS WITH THE EG ELEMENT IN THE B STRUCTURAL ARRAY. THESE COMPARISONS ARE THE STATEMENTS LABELED: REV1, REV2, REV3, REV4, REV5, REV6, REV7. THEY ARE REVERSED IN THE FOLLOWING MANNER: >= --> <= AND <= --> >= .

```

* * * * *
DECLARE (IU(16), IL(16))      FIXED BINARY;
DECLARE #PEAK                 FIXED BINARY (15);
DECLARE 1 PEAK,
      2 (U,V,W,VALU)          FIXED BINARY (31);
DECLARE PEAKS                 FILE RECORD SEQUENTIAL;
DECLARE 1 T,
      2 (U,V,W,EG)            FIXED BINARY (15);
DECLARE 1 B (#PEAK)           CONTROLLED,
      2 (U,V,W,EG)            FIXED BINARY (15);
DECLARE 1 TT LIKE T;
ALLOCATE B;
OPEN FILE (PEAKS);

/*
  READ IN THE PEAKS PICKED FROM THE MAP
ILUP:  DO I = 1 TO #PEAK BY 1;
      READ FILE (PEAKS) INTO (PEAK);
      B.U(I) = PEAK.U;
      B.V(I) = PEAK.V;
      B.W(I) = PEAK.W;
      B.EG(I) = PEAK.VALU;
      END ILUP;
      CLOSE FILE (PEAKS);

/*
  DO THE ACTUAL SORT
M = 1;
II, I = 1;
J = #PEAK;
L05:  IF (I >= J) THEN          GO TO L70;
L10:  K = I;
      IJ = (J+I)/2;
      T = B(IJ);
REV1:  IF (B.EG(I) >= T.EG) THEN GO TO L20;
      B(IJ) = B(I);
      B(I) = T;
      T = B(IJ);
L20:  L=J;
REV2:  IF (B.EG(J) <= T.EG) THEN GO TO L40;
      B(IJ) = B(J);
      B(J) = T;

```

PKST0120
 PKST0130
 PKST0140
 PKST0150
 PKST0160
 PKST0170
 PKST0180
 PKST0190
 PKST0200
 PKST0210
 PKST0220
 PKST0230
 PKST0240
 PKST0250
 PKST0260
 PKST0270
 PKST0280
 PKST0290
 PKST0300
 PKST0310
 PKST0320
 PKST0330
 PKST0340
 PKST0350
 PKST0360
 PKST0370
 PKST0380
 PKST0390
 PKST0400
 PKST0410
 PKST0420
 PKST0430
 PKST0440
 PKST0450
 PKST0460
 PKST0470
 PKST0480
 PKST0490
 PKST0500
 PKST0510
 PKST0520
 PKST0530
 PKST0540
 PKST0550
 PKST0560
 PKST0570
 PKST0580
 PKST0590
 PKST0600
 PKST0610

```

REV3:  T = B(IJ);
        IF (B.EG(I) >= T.EG) THEN      GO TO L40;      ELSE;
        B(IJ) = B(I);
        B(I) = T;
        T = B(IJ);
        GO TO L40;
L30:   B(L) = B(K);
        B(K) = TT;
L40:   L = L-1;
REV4:  IF (B.EG(L) < T.EG) THEN      GO TO L40;      ELSE;
        TT = B(L);
L50:   K = K+1;
REV5:  IF (B.EG(K) > T.EG) THEN      GO TO L50;
        IF (K <= L) THEN              GO TO L30;
        IF (L-I <= J-K) THEN          GO TO L60;
        IL(M) = I;
        IU(M) = L;
        I = K;
        M = M+1;
        GO TO L80;
L60:   IL(M) = K;
        IU(M) = J;
        J = L;
0.615661 M = M+1;
        GO TO L80;
L70:   M = M-1;
        IF (M = 0) THEN GO TO NDSRT;
        I = IL(M);
        J = IU(M);
L80:   IF (J-I >= II) THEN      GO TO L10;
        IF (I = II) THEN      GO TO L05;
        I = I-1;
L90:   I = I+1;
        IF (I = J) THEN      GO TO L70;
        T = B(I+1);
REV6:  IF (B.EG(I) >= T.EG) THEN      GO TO L90;
        K = I;
L95:   B(K+1) = B(K);
        K = K-1;
REV7:  IF (T.EG > B.EG(K)) THEN      GO TO L95;
        B(K+1) = T;              GO TO L90;
/*
WRITE OUT THE SORTED PEAKS
NDSRT: PUT EDIT ('LIST OF SORTED PEAKS',
              :
              :          IU          IV          IW          IHEIGHT
              :          IU          IV          IW          IHEIGHT
              :          IU          IV          IW          IHEIGHT
              (PAGE,A,SKIP,3 A);
              PUT SKIP;
              OPEN FILE (PEAKS) OUTPUT;
              DO I = 1 TO #PEAK BY 1;
              PEAK.U = B.U(I);

```

```

PKST0620
PKST0630
PKST0640
PKST0650
PKST0660
PKST0670
PKST0680
PKST0690
PKST0700
PKST0710
PKST0720
PKST0730
PKST0740
PKST0750
PKST0760
PKST0770
PKST0780
PKST0790
PKST0800
PKST0810
PKST0820
PKST0830
PKST0840
PKST0850
PKST0860
PKST0870
PKST0880
PKST0890
PKST0900
PKST0910
PKST0920
PKST0930
PKST0940
PKST0950
PKST0960
PKST0970
PKST0980
PKST0990
PKST1000
PKST1010
PKST1020
PKST1030
PKST1040
PKST1050
PKST1060
PKST1070
PKST1080
PKST1090
PKST1100
PKST1110

```

```

PEAK.V = B.V(I);
PEAK.W = B.W(I);
PEAK.VALU = B.EG(I);
WRITE FILE (PEAKS) FROM (PEAK);
PUT EDIT (PEAK, ' ') (4 F(10), X(3), A);
PUT FILE (PUNCH) EDIT (PEAK) (4 F(5));
END LUPI;
CLOSE FILE (PEAKS);
FREE B;
PUT EDIT ('THE SORTED PEAKS HAVE BEEN WRITTEN OUT')
      (SKIP(4), A);
RETURN;
END PKSORT;

```

```

PKST1120
PKST1130
PKST1140
PKST1150
PKST1160
PKST1170
PKST1180
PKST1190
PKST1200
PKST1210
PKST1220
PKST1230
PKST1240

```

```

* PROCESS('ATR,XREF');
/* PROCEDURE TO PRINT A LINE OF THE MAP
(SUBRG,STRG):
PLINE:  PROCEDURE (FW, SP, PMN, PMX, LN, ACRS, ACRE, LIN);
        DECLARE
            NUMS(*)      CHAR(*) EXTERNAL CONTROLLED,
            HEAD          CHAR (132) STATIC EXTERNAL,
            LINE          CHAR (132) STATIC,
            LIN(*)        CONTROLLED FIXED BINARY,
            (FW, SP, PMN, PMX, LN, ACRS, ACRE, LL)
                        FIXED BINARY;

        LINE = HEAD;
        SUBSTR(LINE,1,2) = SUBSTR(NUMS(LN),FW-1,2);
        J = 5 - FW;
LOOP:   DO I = ACRS TO ACRE;
        J = J + FW;
        LL = LIN(I);
        IF (LL < PMN) THEN LL = PMN - 1;
        IF (LL > PMX) THEN LL = PMX + 1;
        SUBSTR(LINE,J,FW) = NUMS(LL);
        J = J + FW + 2;
        IF (J > 130) THEN GO TO PRINT;
        SUBSTR(LINE,J,2) = SUBSTR(NUMS(LN),FW-1,2);
PRINT:  PUT SKIP(SP+1) EDIT (LINE) (A(132));
        RETURN;
END PLINE;

```

```

*/
PLIN0010
PLIN0020
PLIN0030
PLIN0040
PLIN0050
PLIN0060
PLIN0070
PLIN0080
PLIN0090
PLIN0200
PLIN0210
PLIN0220
PLIN0230
PLIN0240
PLIN0250
PLIN0260
PLIN0270
PLIN0280
PLIN0290
PLIN0300
PLIN0310
PLIN0320
PLIN0330
PLIN0340
PLIN0350

```

END LOOP;

```

//LKED.SYSLMOD DD DSN=PROG.CRYST,
// UNIT=DISK, VOLUME=SER=PROGPK, DISP=(OLD,KEEP)
//LKED.SYSIN DD *
OVERLAY ALPHA

```

```

JCL-0060
JCL-0070
JCL-0080
OVL00010

```

INSERT SETUP
OVERLAY BETA
INSERT TM_DT
OVERLAY BETA
INSERT PRSETUP
OVERLAY ALPHA
INSERT LAYERS
INSERT PICKER
OVERLAY ALPHA
INSERT NTRLAY
INSERT PLINE
OVERLAY ALPHA
INSERT PKSORT
NAME ALPP(R)

OVLY0020
OVLY0030
OVLY0040
OVLY0050
OVLY0060
OVLY0070
OVLY0080
OVLY0090
OVLY0100
OVLY0110
OVLY0120
OVLY0130
OVLY0140
JCL-0090

APPENDIX B

PROGRAM LISTING OF ALOP


```

DECLARE STAMP CHARACTER (54) EXTERNAL; ALPO0460
DECLARE 1 SYMMPQ (#SYMM) CONTROLLED EXTERNAL, ALPO0470
2 (PX,QX,PY,QY,PZ,QZ) FIXED BINARY (15); ALPO0480
DECLARE (#PEAKS,#SYMM,#RTND,IACR,IDWN,ILAY) ALPO0490
FIXED BINARY (15); ALPO0500
DECLARE (SGNL, NCNT) BIT (1) EXTERNAL; ALPO0510
ALPO0520
/*
SGNL='1'B IF THERE IS A SYMMETRY ELEMENT WITH PX=PY=PZ=-1. ALPO0530
NCNT='1'B IF THERE ARE SYMMETRY ELEMENTS WITH ONLY: PX=-1, ALPO0540
PY=-1, PZ=-1, PX=PY=-1, PY=PZ=-1, PZ=PX=-1. ALPO0550
*/ ALPO0560
DECLARE (ITXYZ,LNG,IERR) FIXED BINARY (31); ALPO0570
DECLARE IHESRTA ENTRY (CHAR(53), CHAR(39), ALPO0580
FIXED BIN(31), FIXED BIN(31)); ALPO0590
DECLARE SFLD CHARACTER (53); ALPO0600
RFLD CHARACTER (39); ALPO0610
DECLARE SORTIN FILE RECORD SEQUENTIAL; ALPO0620
DECLARE SDBG CHARACTER (100) VARYING; ALPO0630
DECLARE DBG EXTERNAL BIT (1); ALPO0640
DECLARE DNV BIT (1) EXTERNAL; ALPO0650
IF (LENGTH(SDBG) > 1) THEN DNV = '1'B; ELSE DNV = '0'B; ALPO0660
IF (LENGTH(SDBG) = 0) THEN DBG = '0'B; ELSE DBG = '1'B; ALPO0670
CALL TM_DT; ALPO0680
LNG = 24000; ALPO0690
RFLD=' RECORD TYPE=V,LENGTH=(24,24,24,24,24) ';; ALPO0700
ON SUBSCRIPTRANGE SNAP BEGIN; PUT DATA (I); EXIT; END; ALPO0710
/* ALPO0720
READ AND INTERPRET THE CONTROL CARDS ALPO0730
IF (DBG) THEN PUT EDIT ('DEBUGGING OUTPUT WILL BE PRINTED.') /* ALPO0740
(SKIP(4),A); ELSE; ALPO0750
ALPO0760
GET EDIT (TITLE,#PEAKS,IACR,IDWN,ILAY,#SYMM) ALPO0770
(A(80),5 F(4)); ALPO0780
PUT EDIT (TITLE, STAMP, ALPO0790
'NUMBER OF POINTS ACROSS A FULL LINE =',IACR, ALPO0800
'NUMBER OF LINES DOWN A FULL LAYER =',IDWN, ALPO0810
'NUMBER OF LAYERS IN A FULL MAP =',ILAY, ALPO0820
'NUMBER OF PEAKS IN INPUT DATA SET =',#PEAKS, ALPO0830
'NUMBER OF SYMMETRY CARDS TO BE READ =',#SYMM) ALPO0840
(A(80),SKIP(3),A(54),5 (SKIP(3),X(20),A,F(4))); ALPO0850
ALPO0860
SLUP: ALLOCATE SYMMPQ; ALPO0870
DO I = 1 TO #SYMM BY 1; ALPO0880
GET EDIT (PX(I),QX(I),PY(I),QY(I),PZ(I),QZ(I)) ALPO0890
(SKIP,6 F(4)); ALPO0900
PUT EDIT ('SYMMETRY OPERATION',I,PX(I),'*X +',QX(I),' /2', ALPO0910
PY(I),'*Y +',QY(I),' /2',PZ(I),'*Z +',QZ(I),' /2') ALPO0920
(SKIP(2),X(25),A,F(3),3 (F(7),A,F(2),A)); ALPO0930
END SLUP; ALPO0940
GET SKIP; ALPO0950
/*

```

```

CLOSE FILE (SYSIN);
PICK AN APPROPRIATE HEAVY-ATOM PEAK & TEST ALL OTHER PEAKS
/* CALL PART1 (#PEAKS,IACR,IDWN,ILAY,#RTND);
USING SYMMETRY, FIND ALL POSSIBLE VALUES OF TX, TY, TZ
/* CALL PART2 (#RTND,IACR,IDWN,ILAY,#SYMM);
IF (-SGNL) THEN GO TO PT4;
ELSE;
/*
/* GROUP ALL TX, TY, TZ AND OUTPUT THOSE WITH FREQUENCY > 5
PT3: OPEN FILE (SORTIN) OUTPUT;
CALL PART3 (IACR,IDWN,ILAY,#RTND);
IF (-NCNT) THEN GO TO SRT;
ELSE;
/* PICK ALL NON-INVERSION TX,TY,TZ > 5 IN # AND OUTPUT W/ SYM#
PT4: CALL PART4 (IACR, IDWN, ILAY);
/* SORT THE FILE OF TX,TY,TZ BY TX, TY, TZ & SYM#
SRT: CLOSE FILE (SORTIN);
SFLD=' SORT FIELDS=(11,02,FI,D,21,4,FL,D),SIZE=E7000
CALL IHESRTA (SFLD,RFLD,LNG,IERR);
IF (IERR=0) THEN GO TO PT5;
PUT EDIT ('THE SECOND SORT WAS UNSUCCESSFUL — RETRY')
      (SKIP(2),A);
EXIT;
/* MAP THE SYMMETRY ELEMENTS INTO EACH OTHER
PT5: CALL PART5 (IACR, IDWN, ILAY);
/* CHOOSE THE MOST FREQUENT VALUE OF TX, TY, AND TZ
/* CALL PART6 (IACR, IDWN, ILAY);
/* DETERMINE WHICH PEAKS ARE TO BE KEPT
CALL PART7 (IACR, IDWN, ILAY, #RTND, #SYMM);
END ALOP;
* PROCESS('ATR,XREF,NOSTMT,OPT=02');
/* CREATES A TIME - DATE STAMP FOR FUTURE USE
(SUBRG,STRG): TM_DT: PROCEDURE;

```

```

DECLARE STAMP CHARACTER(54) EXTERNAL, AMPM CHARACTER(4);
DECLARE MOS(12) CHARACTER(9) VARYING INITIAL ('JANUARY', 'FEBRUARY',
'MARCH', 'APRIL', 'MAY', 'JUNE', 'JULY', 'AUGUST', 'SEPTEMBER',
'OCTOBER', 'NOVEMBER', 'DECEMBER');
DECLARE TM CHARACTER(9), TMS(2) CHARACTER(2) DEFINED TM; TM = TIME;
DECLARE DT CHARACTER(6), DS(3) CHARACTER(2) DEFINED DT; DT = DATE;
IF (TMS(1) > 11) THEN AMPM = 'P.M.'; ELSE AMPM = 'A.M.';
STAMP = 'RUN ON ' || MOS(DS(2)) || ' ' || DS(3) || ' ' || DS(1) ||
', AT ' || TMS(1) || ' HOURS ' || TMS(2) || ' MINUTES ' || AMPM;
END TM_DT;

```

```

TMDT0040
TMDT0050
TMDT0060
TMDT0070
TMDT0080
TMDT0090
TMDT0100
TMDT0110
TMDT0120
TMDT0130

```

```

* PROCESS('ATR,XREF,NOSTMT,OPT=02');
/* PICK AN APPROPRIATE HEAVY-ATOM PEAK & TEST ALL OTHER PEAKS */
/* IN-CORE HEAVY-ATOM SINGLE SUPERPOSITION */
PART1: PROCEDURE (#PEAKS,IACR,IDWN,ILAY,#RTND);
DECLARE (#PEAKS,IACR,IDWN,ILAY,#RTND) FIXED BINARY (15);
DECLARE 1 PEAKS (#PEAKS) CONTROLLED;
      2 (U,V,W,VALU,MEAN) FIXED BINARY (15);
DECLARE PKFILE FILE RECORD INPUT SEQUENTIAL;
DECLARE RETAIN FILE RECORD SEQUENTIAL;
DECLARE 1 PEAKR,
      2 (RU,RV,RW,VAL,AVG) FIXED BINARY (31);
DECLARE 1 SPEAK,
      2 (SU,SV,SW,VLU) FIXED BINARY (31);
DECLARE DIF LABEL;
DECLARE (BU,BV,BW) BIT (1);
DECLARE (DELU,DELV,DELW) FIXED BINARY (15);
DECLARE (P1,P2,P3) FLOAT BINARY;
DECLARE (IDU,IDV,IDW) FIXED BINARY (15);
DECLARE DBG EXTERNAL BIT (1);
/* ON SUBSCRIPTRANGE SNAP BEGIN; PUT DATA (I,J,K,L); EXIT; END; */

SET UP CONSTANTS FOR CHECKING
/*
IA2 = IACR / 2;
ID2 = IDWN / 2;
IL2 = ILAY / 2;
P1 = 0.800;
P2 = 0.650;
P3 = 0.500;
/*
READ IN THE PEAKS PICKED FROM THE MAP BY ALPPKR
/*
PLUP: ALLOCATE PEAKS;
DO I = 1 TO #PEAKS BY 1;
GET EDIT (SPEAK) (4 F(5));
U(I) = SU;

```

```

-P1-0010
-P1-0020
-P1-0030
-P1-0040
-P1-0050
-P1-0060
-P1-0070
-P1-0080
-P1-0090
-P1-0100
-P1-0110
-P1-0120
-P1-0130
-P1-0140
-P1-0150
-P1-0160
-P1-0170
-P1-0180
-P1-0190
-P1-0200
-P1-0210
-P1-0220
-P1-0230
-P1-0240
-P1-0250
-P1-0260
-P1-0270
-P1-0280
-P1-0290
-P1-0300
-P1-0310
-P1-0320
-P1-0330
-P1-0340
-P1-0350
-P1-0360

```

```

V(I) = SV;
W(I) = SW;
VALU(I) = VLU;
MEAN(I) = 0;
END PLUP;
/*
FIND THE LIKELY HEAVY ATOM PEAK FROM THE FIRST 20%
IF (#PEAKS<100) THEN ITOP = MIN(20,#PEAKS);
ELSE ITOP = #PEAKS / 5;
IA2 = IACR / 2;
ID2 = IDWN / 2;
IL2 = ILAY / 2;
DIF = HARD;
ITIME = 1;
JTIME = 0;
TLUP: DO I = 1 TO ITOP BY 1;
IU = U(I);
IV = V(I);
IW = W(I);
KVAL = VALU(I);
GO TO DIF;
/*
LARGEST PEAK ACCEPTED AS HEAVY ATOM WHICH HASN'T U,V,W=0,1/2
HARD: IF ((IU=0)|(IU=IACR)|(IU=IA2)|(IV=0)|(IV=IDWN)|(IV=ID2)|
(IW=0)|(IW=ILAY)|(IW=IL2)) THEN GO TO NOPE;
ELSE GO TO YEP;
/*
LARGEST ACCEPTED AS HEAVY ATOM HAVING ONLY ONE OF U,V,W=0,1/2
MEDM: BU = ~((IU=0)|(IU=IACR)|(IU=IA2));
BV = ~((IV=0)|(IV=IDWN)|(IV=ID2));
BW = ~((IW=0)|(IW=ILAY)|(IW=IL2));
IF ((BU&BV) | (BU&BW) | (BV&BW)) THEN GO TO YEP;
ELSE GO TO NOPE;
/*
LARGEST ACCEPTED AS HEAVY ATOM HAVING TWO ONLY OF U,V,W=0,1/2
EASY: BU = ~((IU=0)|(IU=IACR)|(IU=IA2));
BV = ~((IV=0)|(IV=IDWN)|(IV=ID2));
BW = ~((IW=0)|(IW=ILAY)|(IW=IL2));
IF (BU | BV | BW) THEN GO TO YEP;
ELSE GO TO NOPE;
NOPE: END TLUP;
IF (ITIME=1) THEN GO TO FIRST;
ELSE IF (ITIME=2) THEN GO TO SCND;
ELSE GO TO FAIL;
FIRST: DIF = MEDM;
ITIME = 2;

```

```

-P1-0370
-P1-0380
-P1-0390
-P1-0400
-P1-0410
-P1-0420
-P1-0430
*/ -P1-0440
-P1-0450
-P1-0460
-P1-0470
-P1-0480
-P1-0490
-P1-0500
-P1-0510
-P1-0520
-P1-0530
-P1-0540
-P1-0550
-P1-0560
-P1-0570
-P1-0580
-P1-0590
-P1-0600
*/ -P1-0610
-P1-0620
-P1-0630
-P1-0640
-P1-0650
-P1-0660
*/ -P1-0670
-P1-0680
-P1-0690
-P1-0700
-P1-0710
-P1-0720
-P1-0730
-P1-0740
*/ -P1-0750
-P1-0760
-P1-0770
-P1-0780
-P1-0790
-P1-0800
-P1-0810
-P1-0820
-P1-0830
-P1-0840
-P1-0850
-P1-0860

```

```

SCND:  GO TO TLUP;
      DIF = EASY;
      ITIME = 3;
      GO TO TLUP;
/*
      UNABLE TO FIND A SUITABLE HEAVY ATOM
FAIL:  PUT EDIT ('***** UNABLE TO PICK A HEAVY-ATOM PEAK *****')
      (SKIP(4),A);
      EXIT;
/*
      SUITABLE HEAVY ATOM PEAK FOUND
YEP:   KU = IU;
      KV = IV;
      KW = IW;
      KP = I;
      PUT EDIT ('HEAVY ATOM PEAK FOUND AT U =',KU,'V =',KV,'W =',
      KW,'VALUE =',KVAL)
      (SKIP(3),X(20),4 (A,F(4),X(3)));
/*
      DECIDE ON WHETHER TO USE A HARKER OR A GENERAL PEAK
      IF ((ITIME=1) & (JTIME=0)) THEN GO TO TAGN;
      IF ((ITIME=1) & (JTIME=1)) THEN GO TO COMPR;
      ELSE;
      ELSE;
TAGN:  GKP = KP;          GKVL = KVAL;          JTIME = 1;
      GKU = KU;          GKV = KV;          GKW = KW;
      GO TO FIRST;
COMPR: GNRL = FLOAT (GKVL);
      HRKR = FLOAT (KVAL) / 2.2000;
      IF (HRKR > GNRL) THEN GO TO TYPE;
      ELSE;
      KW = GKW;
      KU = GKU;          KV = GKV;          KVAL = GKVL;
      KP = GKP;
TYPE:  PUT EDIT ('##### PEAK FINALLY CHOSEN AT: #####',
      'U =',KU,'V =',KV,'W =',KW,'VALUE =',KVAL,
      'INDEX =',KP) (SKIP(2),X(10),A,SKIP,3 (X(20),A,F(5)),
      SKIP,2 (X(20),A,F(5)));
/*
      USING THIS PEAK, DETERMINE WHICH PEAKS TO RETAIN
RSTR:  PUT EDIT ('PEAKS FOUND, USING HEAVY-ATOM PEAK',
      '      U      V      W      HEIGHT      MEAN',
      '      U      V      W      HEIGHT      MEAN',
      '      U      V      W      HEIGHT      MEAN',
      '      U      V      W      HEIGHT      MEAN',
      (PAGE,A,SKIP,A,A,A,SKIP,A));
      PUT SKIP;
ILUP:  DO I = 1 TO #PEAKS BY 1;
/*

```

```

-P1-0870
-P1-0880
-P1-0890
-P1-0900
-P1-0910
-P1-0920
-P1-0930
-P1-0940
-P1-0950
-P1-0960
-P1-0970
-P1-0980
-P1-0990
-P1-1000
-P1-1010
-P1-1020
-P1-1030
-P1-1040
-P1-1050
-P1-1060
-P1-1070
-P1-1080
-P1-1090
-P1-1100
-P1-1110
-P1-1120
-P1-1130
-P1-1140
-P1-1150
-P1-1160
-P1-1170
-P1-1180
-P1-1190
-P1-1200
-P1-1210
-P1-1220
-P1-1230
-P1-1240
-P1-1250
-P1-1260
-P1-1270
-P1-1280
-P1-1290
-P1-1300
-P1-1310
-P1-1320
-P1-1330
-P1-1340
-P1-1350
-P1-1360

```

CALCULATE THE PEAK POSITION TO LOOK FOR

```

K = I;
IDU = KU + U(I);
IDV = KV + V(I);
IDW = KW + W(I);
IF (IDU<0) THEN IDU = IDU + IACR;
ELSE IF (IDU>IACR) THEN IDU = IDU - IACR; ELSE;
IF (IDU<0) THEN IDU = IDU + IACR;
ELSE IF (IDU>IACR) THEN IDU = IDU - IACR; ELSE;
IF (IDV<0) THEN IDV = IDV + IDWN;
ELSE IF (IDV>IDWN) THEN IDV = IDV - IDWN; ELSE;
IF (IDV<0) THEN IDV = IDV + IDWN;
ELSE IF (IDV>IDWN) THEN IDV = IDV - IDWN; ELSE;
IF (IDW<0) THEN IDW = IDW + ILAY;
ELSE IF (IDW>ILAY) THEN IDW = IDW - ILAY; ELSE;
IF (IDW<0) THEN IDW = IDW + ILAY;
ELSE IF (IDW>ILAY) THEN IDW = IDW - ILAY; ELSE;

```

/*

DETERMINE IF ANY OF THE OTHER PEAKS FITS EXACTLY
TO THIS CALCULATED POSITION, OR IF IT IS OFF ONLY SLIGHTLY

JLUP:

```

DO J = 1 TO #PEAKS BY 1;
L = J;
DELU = U(J) - IDU;
DELV = V(J) - IDV;
DELW = W(J) - IDW;
IF (DELU > IA2) THEN DELU = DELU - IACR; ELSE;
IF (DELU > IA2) THEN DELU = DELU - IACR; ELSE;
IF (DELU < -IA2) THEN DELU = DELU + IACR; ELSE;
IF (DELU < -IA2) THEN DELU = DELU + IACR; ELSE;
IF (DELV > ID2) THEN DELV = DELV - IDWN; ELSE;
IF (DELV > ID2) THEN DELV = DELV - IDWN; ELSE;
IF (DELV < -ID2) THEN DELV = DELV + IDWN; ELSE;
IF (DELV < -ID2) THEN DELV = DELV + IDWN; ELSE;
IF (DELW > IL2) THEN DELW = DELW - ILAY; ELSE;
IF (DELW > IL2) THEN DELW = DELW - ILAY; ELSE;
IF (DELW < -IL2) THEN DELW = DELW + ILAY; ELSE;
IF (DELW < -IL2) THEN DELW = DELW + ILAY; ELSE;
IF ((DELU=0) & (DELV=0) & (DELW=0)) THEN GO TO OFF0; ELSE;
DELU = ABS (DELU);
DELV = ABS (DELV);
DELW = ABS (DELW);
IF ((DELU=1) & (DELV=0) & (DELW=0)) |
((DELU=0) & (DELV=1) & (DELW=0)) |
((DELU=0) & (DELV=0) & (DELW=1))) THEN GO TO OFF1; ELSE;
IF ((DELU=1) & (DELV=1) & (DELW=0)) |
((DELU=0) & (DELV=1) & (DELW=1)) |
((DELU=1) & (DELV=0) & (DELW=1))) THEN GO TO OFF2; ELSE;
IF ((DELU=1) & (DELV=1) & (DELW=1)) THEN GO TO OFF3; ELSE;

```

```

END JLUP;
GO TC NDI;
/*
PEAK IS RIGHT ON
OFF0: MEAN(J) = SQRT (FLOAT (VALU(I) * VALU(J)));
PUT EDIT (U(J),V(J),W(J),VALU(J),MEAN(J)) (3 F(5),2 F(9));
GO TO NDI;
/*
PEAK IS OFF 1 GRID IN ONE DIRECTION
OFF1: MEAN(J) = P1 * SQRT (FLOAT (VALU(I) * VALU(J)));
PUT EDIT (U(J),V(J),W(J),VALU(J),MEAN(J)) (3 F(5),2 F(9));
GO TO NDI;
/*
THE PEAK IS OFF 1 GRID POINT IN EACH OF TWO DIRECTIONS
OFF2: MEAN(J) = P2 * SQRT (FLOAT (VALU(I) * VALU(J)));
PUT EDIT (U(J),V(J),W(J),VALU(J),MEAN(J)) (3 F(5),2 F(9));
GO TO NDI;
/*
THE PEAK IS OFF 1 GRID POINT IN ALL THREE DIRECTIONS
OFF3: MEAN(J) = P3 * SQRT (FLOAT (VALU(I) * VALU(J)));
PUT EDIT (U(J),V(J),W(J),VALU(J),MEAN(J)) (3 F(5),2 F(9));
NDI: END ILUP;
/*
WRITE OUT THE PEAKS WHICH WERE FOUND
OPEN FILE (RETAIN) OUTPUT;
#RTND = 0;
LUPI: DO I = 1 TO #PEAKS BY 1;
IF (MEAN(I)=C) THEN GO TO FNLI;
RU = U(I);
RV = V(I);
RW = W(I);
VAL = VALU(I);
AVG = MEAN(I);
#RTND = #RTND + 1;
WRITE FILE (RETAIN) FROM (PEAKR);
FNLI: END LUPI;
CLOSE FILE (RETAIN);
FREE PEAKS;
RETURN;
END PART1;

```

```

-P1-1870
-P1-1880
-P1-1890
-P1-1900
*/ -P1-1910
-P1-1920
-P1-1930
-P1-1940
-P1-1950
-P1-1960
*/ -P1-1970
-P1-1980
-P1-1990
-P1-2000
-P1-2010
-P1-2020
*/ -P1-2030
-P1-2040
-P1-2050
-P1-2060
-P1-2070
-P1-2080
*/ -P1-2090
-P1-2100
-P1-2110
-P1-2120
-P1-2130
-P1-2140
*/ -P1-2150
-P1-2160
-P1-2170
-P1-2180
ELSE; -P1-2190
-P1-2200
-P1-2210
-P1-2220
-P1-2230
-P1-2240
-P1-2250
-P1-2260
-P1-2270
-P1-2280
-P1-2290
-P1-2300
-P1-2310

```

* PROCESS('ATR,XREF,NOSTMT,OPT=02');

-P2-0010

```

/* USING SYMMETRY, FIND ALL THE VALUES OF TX, TY, TZ          */
/* FROM THE PEAKS OBTAINED FROM THE SUPERPOSITION OF PART 1    */
PART2:  PROCEDURE (#RTND,IACR,IDWN,ILAY,#SYMM);                */
/*

```

```

THIS SECTION COMPUTES ALL OF THE POSSIBLE VALUES OF TX, TY, &
TZ FROM THE PEAKS LEFT BY THE SUPERPOSITION AS FOLLOWS:
LET U,V,W & U',V',W' REPRESENT THE TWO PEAKS. IF THESE PEAKS
ARE SYMMETRY RELATED BUT THE SUPERPOSITION ORIGIN IS OFF
BY TX, TY, TZ, THEN U = X+TX, V = Y+TY, AND W = Z+TZ. DEPENDING
ON THE VALUES OF PX, PY, PZ THERE ARE THEN 18 DIFFERENT COMBINA-
TIONS OF THE TWO PEAKS (DESIGNATED AS P1 AND P2):

```

QUANTITY	U OF QUANTITY	V OF QUANTITY	W OF QUANTITY	
P1	X + TX	Y + TY	Z + TZ	
P2(0) ---	QX + X + TX	QY + Y + TY	QZ + Z + TZ	
P2(0)+P1	QX + 2X + 2TX	QY + 2Y + 2TY	QZ + 2Z + 2TZ	
P2(0)-P1	QX	QY	QZ	
P2(1) ---	QX - X + TX	QY + Y + TY	QZ + Z + TZ	
P2(1)+P1 *	QX + 2TX	QY + 2Y + 2TY	QZ + 2Z + 2TZ	
P2(1)-P1	QX - 2X	# QY	# QZ	
P2(2) ---	QX + X + TX	QY - Y + TY	QZ + Z + TZ	
P2(2)+P1	QX + 2X + 2TX	* QY + 2TY	QZ + 2Z + 2TZ	
P2(2)-P1 #	QX	QY - 2Y	# QZ	
P2(3) ---	QX - X + TX	QY - Y + TY	QZ + Z + TZ	
P2(3)+P1 *	QX + 2TX	* QY + 2TY	QZ + 2Z + 2TZ	
P2(3)-P1	QX - 2X	QY - 2Y	# QZ	
P2(4) ---	QX + X + TX	QY + Y + TY	QZ - Z + TZ	
P2(4)+P1	QX + 2X + 2TX	QY + 2Y + 2TY	* QZ + 2TZ	
P2(4)-P1 #	QX	# QY	QZ - 2Z	
P2(5) ---	QX - X + TX	QY + Y + TY	QZ - Z + TZ	
P2(5)+P1 *	QX + 2TX	QY + 2Y + 2TY	* QZ + 2TZ	
P2(5)-P1	QX - 2X	# QY	QZ - 2Z	
P2(6) ---	QX + X + TX	QY - Y + TY	QZ - Z + TZ	
P2(6)+P1	QX + 2X + 2TX	* QY + 2TY	* QZ + 2TZ	
P2(6)-P1 #	QX	QY - 2Y	QZ - 2Z	
P2(7) ---	QX - X + TX	QY - Y + TY	QZ - Z + TZ	
P2(7)+P1 *	QX + 2TX	* QY + 2TY	* QZ + 2TZ	
P2(7)-P1	QX - 2X	QY - 2Y	QZ - 2Z	

```

AS QX,QY,QZ ARE EITHER 0 OR 1/2 FOR ANY SYMMETRY ELEMENT AND
ARE KNOWN, VALUES OF TX; TY; TX, TY; TZ; TX, TZ; TY, TZ OR
TX, TY, TZ ARE THEN COMPUTED. FOR ALL BUT THE INVERSION, THE
FREQUENCY OF OCCURRENCE OF THESE VALUES IS STORED IN CORE.
FOR THE INVERSION, THE TX, TY, TZ TRIPLES ARE WRITTEN OUT,
SORTED INTO ORDER, AND THEN GROUPED TOGETHER ON REAPING IN
PART 3. A LATITUDE OF ONE GRID POINT IN EACH DIRECTION IS
ALLOWED FOR THE VALUES OF TX, TY, TZ AND APPROPRIATE WEIGHTS
ASSIGNED. THE ASTERISKED (*) RELATIONS ABOVE GIVE VALUES
OF TX, TY, TZ, PROVIDED THE NUMBERED (#) RELATIONS ARE OBEYED.

```

```

DECLARE (#RTND,IACR,IDWN,ILAY,#SYMM)    FIXED BINARY (15);          */ -P2-0520
DECLARE IS (#SYMM)                        FIXED BINARY (15) CONTROLLED; -P2-0530
DECLARE 1 PEAKS (#RTND)                   CONTROLLED EXTERNAL,      -P2-0540
      2 (U,V,W,VALU,MEAN) FIXED BINARY (15);                      -P2-0550
DECLARE 1 SYMMPQ (#SYMM)                  CONTROLLED EXTERNAL,      -P2-0560
      2 (PX,QX,PY,QY,PZ,QZ) FIXED BINARY (15);                    -P2-0570
DECLARE RETAIN                            FILE RECORD SEQUENTIAL;   -P2-0580
DECLARE 1 PEAKR,                           -P2-0590
      2 (RU,RV,RW,VAL,AVG)    FIXED BINARY (31);                  -P2-0600
DECLARE 1 TXYZ,                           -P2-0610
      2 (TX, TY, TZ, KS)     FIXED BINARY (15),                   -P2-0620
      2 (VIJ, MIJ, FREQ)     FLOAT BINARY;                        -P2-0630
DECLARE SYM(7)                          LABEL;                     -P2-0640
DECLARE ITXYZ                            FIXED BINARY (31);        -P2-0650
DECLARE (XLINE#(0:IACR), YLINE#(0:IDWN), ZLINE#(0:ILAY),          -P2-0660
      XYLAY#(0:IA,0:ID), YZLAY#(0:ID,0:IL), ZXLAY#(0:IL,0:IA)) -P2-0670
      EXTERNAL CONTROLLED FLOAT BINARY;                           -P2-0680
/* THE SEVEN-MEMBERED BIT(1) ARRAY "ION" SHOWS THE TYPE OF SYMMETRY -P2-0690
   ELEMENTS BEING USED. THE BIT IS SET IF THE SYMMETRY ELEMENT IS -P2-0700
   PRESENT.                                                         -P2-0710
ELEMENT      NO      PX      PY      PZ      DETERMINE TX,TY,TZ? -P2-0720
PLANE PERP. TO X      1      -1      1      1      TX              -P2-0730
PLANE PERP. TO Y      2      1      -1      1      TY              -P2-0740
AXIS IN Z              3      -1      -1      1      TX, TY        -P2-0750
PLANE PERP. TO Z      4      1      1      -1      TZ              -P2-0760
AXIS IN Y              5      -1      1      -1      TX, TZ        -P2-0770
AXIS IN X              6      1      -1      -1      TY, TZ        -P2-0780
INVERSION              7      -1      -1      -1      TX, TY, TZ    -P2-0790
SGNL='1'B IF THERE IS AN INVERSION; NCNT='1'B IF THERE ARE OTHERS -P2-0800
                                                         */ -P2-0810
DECLARE (ION(7),SGNL,NCNT) BIT (1) EXTERNAL;                       -P2-0820
DECLARE AL(7)              LABEL;                                   -P2-0830
DECLARE DBG                EXTERNAL BIT (1);                       -P2-0840
DECLARE (IA2,ID2,IL2,I4A,I4D,I4L,JPIU,JPIV,JPIW,JMIU,JMIV,      -P2-0850
      JMIW,JMIUP,JMIVP,JMIWP,JMIUM,JMIVM,JMIWM)                -P2-0860
      FIXED BINARY (15);                                          -P2-0870
DECLARE LAY# (0:ILAY)      EXTERNAL CTL BIT(1);                   -P2-0880
DECLARE (XQ, YQ, ZQ)       EXTERNAL FIXED BIN;                   -P2-0890
IA2 = IACR / 2;            -P2-0900
ID2 = IDWN / 2;            -P2-0910
IL2 = ILAY / 2;            -P2-0920
I4A = IACR * 4;            -P2-0930
I4D = IDWN * 4;            -P2-0940
I4L = ILAY * 4;            -P2-0950
/*                                                                    -P2-0960
I1 : MIRRORS AND PLANES RIGHT ON (TX|TY|TZ).                        -P2-0970
I2 : TWO-FOLDS OR SCREWS RIGHT ON (TX,TY|TY,TZ|TX,TZ).           -P2-0980
I3 : MIRRORS AND PLANES OFF ONE GRID POINT.                       -P2-0990
I4 : TWO-FOLDS OR SCREWS OFF ONE IN ONE DIRECTION.                -P2-1000

```

```

I6 : TWO-FOLDS OR SCREWS OFF ONE IN BOTH DIRECTIONS.
DECLARE (I1,I2,I3,I4,I5,I6,TH)          FLOAT BINARY;
DECLARE (J1,J2,J3,J4,J5,J6,MEANI,J)     FLOAT BINARY;
TH = 10.000;                             J1 = 18;
J2 = 10;                                 J3 = 9;
J4 = 6;                                 J5 = 4;
J6 = 2;
ON SUBSCRIPTRANGE SNAP BEGIN; PUT DATA
    (I,KS,J,K,TX,TY,TZ);                EXIT;
/*
READ IN THE PEAKS, SORTED BY LAYER
OPEN FILE (RETAIN) INPUT;
ALLOCATE PEAKS, IS;
ILUP: DO I = 1 TO #RTND BY 1;
READ FILE (RETAIN) INTO (PEAKR);
U(I) = RU;
V(I) = RV;
W(I) = RW;
VALU(I) = VAL;
MEAN(I) = AVG;
END ILUP;
CLOSE FILE (RETAIN);
ION = '0'B;
NCNT = '0'B;
IA = IACR;
ID = IDWN;
IL = ILAY;
/*
TRANSFORM THE SYMMETRY ELEMENTS INTO MORE USEABLE FORM
SLUP: DO I = 1 TO #SYMM BY 1;
IS(I) = 0;
IF (PX(I) = -1) THEN IS(I) = IS(I) + 1;
IF (PY(I) = -1) THEN IS(I) = IS(I) + 2;
IF (PZ(I) = -1) THEN IS(I) = IS(I) + 4;
IF (QX(I) = 1) THEN QX(I) = IACR / 2;
IF (QY(I) = 1) THEN QY(I) = IDWN / 2;
IF (QZ(I) = 1) THEN QZ(I) = ILAY / 2;
KS = IS(I);
IF (KS = 7) THEN DO;
XQ = QX(I);
YQ = QY(I);
ZQ = QZ(I);
ION(KS) = '1'B;
END SLUP;
PUT EDIT (#RTND,' PEAKS WERE RETAINED') (SKIP(2),F(5),A);
IF (DBG) THEN PUT EDIT('ION =',ION) (SKIP,A,7 (B(1),X(1)));
ELSE;

```

```

- P2-1020
*/ - P2-1030
- P2-1040
- P2-1050
- P2-1060
- P2-1070
- P2-1080
- P2-1090
- P2-1100
- P2-1110
- P2-1120
- P2-1130
*/ - P2-1140
- P2-1150
- P2-1160
- P2-1170
- P2-1180
- P2-1190
- P2-1200
- P2-1210
- P2-1220
- P2-1230
- P2-1240
- P2-1250
- P2-1260
- P2-1270
- P2-1280
- P2-1290
- P2-1300
- P2-1310
- P2-1320
*/ - P2-1330
- P2-1340
- P2-1350
ELSE; - P2-1360
ELSE; - P2-1370
ELSE; - P2-1380
ELSE; - P2-1390
ELSE; - P2-1400
ELSE; - P2-1410
- P2-1420
- P2-1430
- P2-1440
- P2-1450
ELSE; - P2-1460
- P2-1470
- P2-1480
- P2-1490
- P2-1500
- P2-1510

```

```

/*      IF (DBG) THEN PUT PAGE;                                ELSE; -P2-1520
      ALLOCATE ARRAYS FOR MIRRORS, GLIDES, TWO-FOLDS, AND SCREWS -P2-1530
                                                                */ -P2-1540
ALLOC: DO I = 1 TO 7;                                          -P2-1550
      IF (ION(I)) THEN GO TO AL(I);                            ELSE GO TO NDA; -P2-1560
AL(1): ALLOCATE XLINE#;                                       -P2-1570
      XLINE# = 0.000;                                         -P2-1580
      NCNT = '1'B;                                           -P2-1590
      GO TO NDA;                                             -P2-1600
AL(2): ALLOCATE YLINE#;                                       -P2-1610
      YLINE# = 0.000;                                         -P2-1620
      NCNT = '1'B;                                           -P2-1630
      GO TO NDA;                                             -P2-1640
AL(3): ALLOCATE XYLAY#;                                       -P2-1650
      XYLAY# = 0.000;                                         -P2-1660
      NCNT = '1'B;                                           -P2-1670
      GO TO NDA;                                             -P2-1680
AL(4): ALLOCATE ZLINE#;                                       -P2-1690
      ZLINE# = 0.000;                                         -P2-1700
      NCNT = '1'B;                                           -P2-1710
      GO TO NDA;                                             -P2-1720
AL(5): ALLOCATE ZXLAY#;                                       -P2-1730
      ZXLAY# = 0.000;                                         -P2-1740
      NCNT = '1'B;                                           -P2-1750
      GO TO NDA;                                             -P2-1760
AL(6): ALLOCATE YZLAY#;                                       -P2-1770
      YZLAY# = 0.000;                                         -P2-1780
      NCNT = '1'B;                                           -P2-1790
      GO TO NDA;                                             -P2-1800
AL(7): ALLOCATE LAY#;                                         -P2-1810
      LAY# = '0'B;                                           -P2-1820
NDA:   END ALLOC;                                             -P2-1830
      SGNL = ION(7);                                         -P2-1840
/*                                                                -P2-1850
      SEARCH THROUGH ALL PEAKS                                -P2-1860
                                                                */ -P2-1870
OUTER: DO J = 1 TO #RTND BY 1;                                -P2-1880
      JU = U(J);                                              -P2-1890
      JV = V(J);                                              -P2-1900
      JW = W(J);                                              -P2-1910
      MEANJ = MEAN(J);                                         -P2-1920
INNER: DO I = J TO #RTND BY 1;                                -P2-1930
      IU = U(I);      I1 = J1 * MEANIJ;      I2 = J2 * MEANIJ; -P2-1940
      IV = V(I);      I3 = J3 * MEANIJ;      I4 = J4 * MEANIJ; -P2-1950
      IW = W(I);      I5 = J5 * MEANIJ;      I6 = J6 * MEANIJ; -P2-1960
/*                                                                -P2-1970
      COMPUTE THE SUM (P) AND THE DIFFERENCE (M) BETWEEN PEAKS -P2-1980
      JU, JV, JW AND IU, IV, IW ALLOWING ONE GRID POINT POSITIVE (P) -P2-1990
      AND NEGATIVE (M) ERROR                                  -P2-2000
                                                                */ -P2-2010

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```

JPIU = JU + IU;
JPIV = JV + IV;
JPIW = JW + IW;
JMIU = MOD (JU - IU + I4A, IACR);
JMIV = MOD (JV - IV + I4D, IDWN);
JMIW = MOD (JW - IW + I4L, ILAY);
JMIUP = MOD (JMIU + 1 + I4A, IACR);
JMIUM = MOD (JMIU - 1 + I4A, IACR);
JMIVP = MOD (JMIV + 1 + I4D, IDWN);
JMIVM = MOD (JMIV - 1 + I4D, IDWN);
JMIWP = MOD (JMIW + 1 + I4L, ILAY);
JMIWM = MOD (JMIW - 1 + I4L, ILAY);
/*
  LOOP THROUGH ALL SYMMETRY ELEMENTS
SYML: DO K = 1 TO #SYMM BY 1;
      KS = IS (K);
      GO TO SYM(KS);
/*
  MIRROR OR GLIDE PLANE PERPENDICULAR TO X; DETERMINE TX
  NOTE P2(1) ABOVE THAT V2-V1 = QY+/-1 AND W2-W1 = QZ+/-1
  BEFORE U2+U1 = QX+2TX HOLDS.
SYM(1): IF ((JMIVP = QY(K)) & (JMIV = QY(K)) & (JMIWM = QY(K)))
        THEN GO TO NDSY;
        ELSE;
        IF ((JMIWP = QZ(K)) & (JMIW = QZ(K)) & (JMIWM = QZ(K)))
        THEN GO TO NDSY;
        ELSE;
        TX = MOD (((JPIU - QX(K)) / 2) + I4A, IACR);
        XLINE#(TX) = XLINE#(TX) + I1;
        TX = MOD (TX + 1, IACR);
        XLINE#(TX) = XLINE#(TX) + I3;
        TX = MOD (TX - 2 + IACR, IACR);
        XLINE#(TX) = XLINE#(TX) + I3;
        GO TO NDSY;
/*
  MIRROR OR GLIDE PLANE PERPENDICULAR TO Y; DETERMINE TY
  NOTE P2(2) ABOVE THAT U2-U1 = QX+/-1 AND W2-W1 = QZ+/-1
  BEFORE V2+V1 = QY+2TY HOLDS.
SYM(2): IF ((JMIUP = QX(K)) & (JMIU = QX(K)) & (JMIUM = QX(K)))
        THEN GO TO NDSY;
        ELSE;
        IF ((JMIWP = QZ(K)) & (JMIW = QZ(K)) & (JMIWM = QZ(K)))
        THEN GO TO NDSY;
        ELSE;
        TY = MOD (((JPIV - QY(K)) / 2) + I4D, IDWN);
        YLINE#(TY) = YLINE#(TY) + I1;
        TY = MOD (TY + 1, IDWN);
        YLINE#(TY) = YLINE#(TY) + I3;
        TY = MOD (TY - 2 + IDWN, IDWN);
        YLINE#(TY) = YLINE#(TY) + I3;
        GO TO NDSY;

```

```

-P2-2020
-P2-2030
-P2-2040
-P2-2050
-P2-2060
-P2-2070
-P2-2080
-P2-2090
-P2-2100
-P2-2110
-P2-2120
-P2-2130
-P2-2140
-P2-2150
-P2-2160
-P2-2170
-P2-2180
-P2-2190
-P2-2200
-P2-2210
-P2-2220
-P2-2230
-P2-2240
-P2-2250
-P2-2260
-P2-2270
-P2-2280
-P2-2290
-P2-2300
-P2-2310
-P2-2320
-P2-2330
-P2-2340
-P2-2350
-P2-2360
-P2-2370
-P2-2380
-P2-2390
-P2-2400
-P2-2410
-P2-2420
-P2-2430
-P2-2440
-P2-2450
-P2-2460
-P2-2470
-P2-2480
-P2-2490
-P2-2500
-P2-2510

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/*
TWO-FOLD OR TWO-FOLD SCREW AXIS IN Z; DETERMINE TX & TY
NOTE P2(3) ABOVE THAT W2-W1 = QZ+/-1 BEFORE U2+U1 = QX+2TX
AND V2+V1 = QY+2TY HOLDS.
SYM(3): IF ((JMIWP = QZ(K)) & (JMIW = QZ(K)) & (JMIWM = QZ(K)))
      THEN GO TO NDSY;
      ELSE;
      TX = MOD (((JPIU - QX(K)) / 2) + I4A, IACR);
      TY = MOD (((JPIV - QY(K)) / 2) + I4D, IDWN);
      XYLAY#(TX,TY) = XYLAY#(TX,TY) + I2;
      TXP = MOD (TX + 1, IACR);
      TYP = MOD (TY + 1, IDWN);
      TXM = MOD (TX - 1 + IACR, IACR);
      TYM = MOD (TY - 1 + IDWN, IDWN);
      XYLAY#(TX,TYP) = XYLAY#(TX,TYP) + I4;
      XYLAY#(TX,TYM) = XYLAY#(TX,TYM) + I4;
      XYLAY#(TXP,TY) = XYLAY#(TXP,TY) + I4;
      XYLAY#(TXM,TY) = XYLAY#(TXM,TY) + I4;
      XYLAY#(TXM,TYP) = XYLAY#(TXM,TYP) + I6;
      XYLAY#(TXM,TYM) = XYLAY#(TXM,TYM) + I6;
      XYLAY#(TXP,TYM) = XYLAY#(TXP,TYM) + I6;
      XYLAY#(TXP,TYP) = XYLAY#(TXP,TYP) + I6;
      GO TO NDSY;
/*
MIRROR OR GLIDE PLANE PERPENDICULAR TO Z; DETERMINE TZ
NOTE P2(4) ABOVE THAT U2-U1 = QX+/-1 AND V2-V1 = QY+/-1
BEFORE W2+W1 = QZ+2TZ HOLDS
SYM(4): IF ((JMIUP = QX(K)) & (JMIU = QX(K)) & (JMIUM = QX(K)))
      THEN GO TO NDSY;
      ELSE;
      IF ((JMIVP = QY(K)) & (JMIV = QY(K)) & (JMIVM = QY(K)))
      THEN GO TO NDSY;
      ELSE;
      TZ = MOD (((JPIW - QZ(K)) / 2) + I4L, ILAY);
      ZLINE#(TZ) = ZLINE#(TZ) + I1;
      TZ = MOD (TZ + 1, ILAY);
      ZLINE#(TZ) = ZLINE#(TZ) + I3;
      TZ = MOD (TZ - 2 + ILAY, ILAY);
      ZLINE#(TZ) = ZLINE#(TZ) + I3;
      GO TO NDSY;
/*
TWO-FOLD OR TWO-FOLD SCREW AXIS IN Y; DETERMINE TX & TZ
NOTE P2(5) ABOVE THAT V2-V1 = QY+/-1 BEFORE U2+U1 = QX+2TX
AND W2+W1 = QZ+2TZ HOLDS.
SYM(5): IF ((JMIVP = QY(K)) & (JMIV = QY(K)) & (JMIVM = QY(K)))
      THEN GO TO NDSY;
      ELSE;
      TX = MOD (((JPIU - QX(K)) / 2) + I4A, IACR);
      TZ = MOD (((JPIW - QZ(K)) / 2) + I4L, ILAY);
      ZXLAY#(TZ,TX) = ZXLAY#(TZ,TX) + I2;
      TZP = MOD (TZ + 1, ILAY);

```

```

TXP = MOD (TX + 1, IACR);
TZM = MOD (TZ - 1 + ILAY, ILAY);
TXM = MOD (TX - 1 + IACR, IACR);
ZXLAY#(TZ,TXP) = ZXLAY#(TZ,TXP) + I4;
ZXLAY#(TZ,TXM) = ZXLAY#(TZ,TXM) + I4;
ZXLAY#(TZP,TX) = ZXLAY#(TZP,TX) + I4;
ZXLAY#(TZM,TX) = ZXLAY#(TZM,TX) + I4;
ZXLAY#(TZM,TXP) = ZXLAY#(TZM,TXP) + I6;
ZXLAY#(TZM,TXM) = ZXLAY#(TZM,TXM) + I6;
ZXLAY#(TZP,TXM) = ZXLAY#(TZP,TXM) + I6;
ZXLAY#(TZP,TXP) = ZXLAY#(TZP,TXP) + I6;
GO TO NDSY;

/*
TWO-FOLD OR TWO-FOLD SCREW AXIS IN X; DETERMINE TY & TZ
NOTE P2(6) ABOVE THAT U2-U1 = QX+/-1 BEFORE V2+V1 = QY+2TY
AND W2+W1 = QZ+2TZ

SYM(6): IF ((JMIUP /= QX(K)) & (JMIU /= QX(K)) & (JMIUM /= QX(K)))
      THEN GO TO NDSY;
      ELSE;
      TZ = MOD (((JPIW - QZ(K)) / 2) + I4L, ILAY);
      TY = MOD (((JPIV - QY(K)) / 2) + I4D, IDWN);
      YZLAY#(TY,TZ) = YZLAY#(TY,TZ) + I2;
      TYP = MOD (TY + 1, IDWN);
      TZP = MOD (TZ + 1, ILAY);
      TYM = MOD (TY - 1 + IDWN, IDWN);
      TZM = MOD (TZ - 1 + ILAY, ILAY);
      YZLAY#(TY,TZP) = YZLAY#(TY,TZP) + I4;
      YZLAY#(TY,TZM) = YZLAY#(TY,TZM) + I4;
      YZLAY#(TYP,TZ) = YZLAY#(TYP,TZ) + I4;
      YZLAY#(TYM,TZ) = YZLAY#(TYM,TZ) + I4;
      YZLAY#(TYM,TZP) = YZLAY#(TYM,TZP) + I6;
      YZLAY#(TYM,TZM) = YZLAY#(TYM,TZM) + I6;
      YZLAY#(TYP,TZM) = YZLAY#(TYP,TZM) + I6;
      YZLAY#(TYP,TZP) = YZLAY#(TYP,TZP) + I6;
      GO TO NDSY;

/*
CENTER OF INVERSION; DETERMINE TX, TY, & TZ

SYM(7): TZ = MOD (((JPIW - ZQ) / 2) + I4L, ILAY);
/*
DETERMINE THE LAYERS WITH TX, TY, TZ

OUTP: DO IZ = -1 TO 1 BY 1;
      JZ = MOD (TZ + IZ + ILAY, ILAY);
      LAY#(JZ) = '1'B;
      END OUTP;
NDSY: END SYML;
      END INNER;
      IF (DBG) THEN PUT EDIT (' PEAK# =',J) (A,F(4));
      END CUTER;
      ELSE;

```

RETURN;
END PART2;

-P2-3520
-P2-3530

```
* PROCESS('ATR,XREF,NOSTMT,OPT=02');
/* OUTPUT ALL VALUES OF TX.TY.TZ WITH FREQUENCY > 5 TO BE SORTED */
PART3:  PROCEDURE (IACR,IDWN,ILAY,#RTND);
/*
    IN PART2, ALL OF THE POSSIBLE VALUES OF TZ WERE FLAGGED AS
    TO WHETHER OR NOT THEY OCCURRED. IN THIS SUBROUTINE, A LAYER OF
    TX.TY IS FILLED FOR EACH VALUE OF TZ, WITH THE FREQUENCY OF
    OCCURRENCE OF EACH VALUE OF TX.TY.TZ. AFTER THE LAYER HAS BEEN
    CREATED, ALL OF THE TX.TY.TZ TRIPLES WITH FREQUENCY > 5 ARE OUTPUT
    */
    DECLARE    LAYER (0:IACR,0:IDWN)    FLOAT BIN CTL;
    DECLARE    LAY#(0:ILAY)              EXTERNAL BIT(1) CTL;
    DECLARE    (IACR,IDWN,ILAY,#RTND)    FIXED BINARY (15);
    DECLARE    SORTIN                     FILE RECORD SEQUENTIAL;
    DECLARE    (DBG, DNV)                 EXTERNAL BIT (1);
    DECLARE 1  PEAKS (#RTND)              CONTROLLED EXTERNAL,
    2 (U,V,W,VALU,MEAN)                   FIXED BINARY (15);
    DECLARE 1  SXYZ,
    2 (SX, SY, SZ, SK)                    FIXED BINARY (15),
    2 (VAL, AVG, FREQ)                    FLCAT BINARY;
    DECLARE    (02,03,04,05,M1,M2,M3,TH)  FLOAT BINARY;
    DECLARE    (XQ, YQ, ZQ)               EXTERNAL FIXED BIN;
    DECLARE    #INV                       FIXED BIN;
    #INV = 0;                             TH = 50.000;
    02 = 2.00;
    03 = 3.00;
    04 = 4.00;
    05 = 5.00;
    X5 = 05 * 5.0000;
    VAL, AVG = 0.0000;
    SK = 7;
    I4A = IACR * 4;
    I4D = IDWN * 4;
    I4L = ILAY * 4;
    ON ERROR SNAP EXIT;
    IF (DBG) THEN PUT EDIT ('XQ =',XQ,'YQ =',YQ,'ZQ =',ZQ)
    (SKIP(4),3 (A,F(5),X(2))); ELSE;
    IF (CBG) THEN PUT EDIT ('LAY# =',LAY#)
    (SKIP(2),A,(ILAY+1) (X(2),B(1))); ELSE;
    IF (DNV) THEN DO;
    PUT EDIT ('THE TX, TY, TZ PAIRS THAT HAVE MORE THAN 5',
    ' TX TY TZ SY  VALU  MEAN  FREQ',
    ' TX TY TZ SY  VALU  MEAN  FREQ',
    ' TX TY TZ SY  VALU  MEAN  FREQ',
```

-P3-0010
-P3-0020
-P3-0030
-P3-0040
-P3-0050
-P3-0060
-P3-0070
-P3-0080
-P3-0090
-P3-0100
-P3-0110
-P3-0120
-P3-0130
-P3-0140
-P3-0150
-P3-0160
-P3-0170
-P3-0180
-P3-0190
-P3-0200
-P3-0210
-P3-0220
-P3-0230
-P3-0240
-P3-0250
-P3-0260
-P3-0270
-P3-0280
-P3-0290
-P3-0300
-P3-0310
-P3-0320
-P3-0330
-P3-0340
-P3-0350
-P3-0360
-P3-0370
-P3-0380
-P3-0390
-P3-0400
-P3-0410
-P3-0420
-P3-0430
-P3-0440

```

      TX TY TZ SY VALU MEAN FREQ')
      (PAGE,A,SKIP,A,A,A,A); PUT SKIP; END; ELSE;
OPEN FILE (SORTIN) OUTPUT;
ALLOCATE LAYER;
/*
  LOOP THROUGH THE LAYERS, ONE AT A TIME
  IF (-LAY#( LAY)) THEN GO TO NDLAY;
LAYLUP: DO LAY = 0 TO ILAY BY 1;
/*
  OUTER LOOP THROUGH ALL THE PEAKS
GUTER: DO J = 1 TO #RTND BY 1;      MEANJ = MEAN(J);
      K = J + 1;
      IF (K > #RTND) THEN GO TO NDOTR;
      JU = U(J);
      JV = V(J);
      JW = W(J);
/*
  INNER LOOP THROUGH THE REMAINDER OF THE PEAKS
INNER: DO I = K TO #RTND BY 1;      MEANIJ=FLOAT(MEANJ+MEAN(I))/TH;
      JPIW = MOD (((JW + W(I) - ZQ) / 2) + I4L, ILAY);
      JPIWP = MOD (JPIW + 1, ILAY);
      JPIWM = MOD (JPIW - 1 + ILAY, ILAY);
      IF (JPIW = LAY) THEN GO TO RTON;
      IF ((JPIWP = LAY)|(JPIWM = LAY)) THEN GO TO ZOFF1;
      ELSE GO TO NDINR;
/*
  THE VALUE OF ILAY = TZ
RTON: M1 = 05 * MEANIJ;
      M2 = 04 * MEANIJ;
      M3 = 03 * MEANIJ;
      GO TO OK;
/*
  THE VALUE OF ILAY = TZ+1 OR TZ-1
ZOFF1: M1 = 04 * MEANIJ;
      M2 = 03 * MEANIJ;
      M3 = 02 * MEANIJ;
/*
  SET UP THE VALUES OF TX AND TY OFF ONE GRID POINT
OK: JPIU = MOD (((JU + U(I) - XQ) / 2) + I4A, IACR);
      JPIV = MOD (((JV + V(I) - YQ) / 2) + I4D, IDWN);
      JPIUP = MOD (JPIU + 1, IACR);
      JPIVP = MOD (JPIV + 1, IDWN);
      JPIUM = MOD (JPIU - 1 + IACR, IACR);

```

```

-P3-0450
-P3-0460
-P3-0470
-P3-0480
-P3-0490
-P3-0500
-P3-0510
-P3-0520
-P3-0530
-P3-0540
-P3-0550
-P3-0560
-P3-0570
-P3-0580
-P3-0590
-P3-0600
-P3-0610
-P3-0620
-P3-0630
-P3-0640
-P3-0650
-P3-0660
-P3-0670
-P3-0680
-P3-0690
-P3-0700
-P3-0710
-P3-0720
-P3-0730
-P3-0740
-P3-0750
-P3-0760
-P3-0770
-P3-0780
-P3-0790
-P3-0800
-P3-0810
-P3-0820
-P3-0830
-P3-0840
-P3-0850
-P3-0860
-P3-0870
-P3-0880
-P3-0890
-P3-0900
-P3-0910
-P3-0920
-P3-0930
-P3-0940

```

```

/*      JPIVM = MOD (JPIV - 1 + IDWN, IDWN);                                -P3-0950
/*      FILL THE ARRAY WITH THE FREQUENCIES                                -P3-0960
/*      */ -P3-0970
FILL:   LAYER (JPIU ,JPIV ) = LAYER (JPIU ,JPIV ) + M1;                    -P3-0980
        LAYER (JPIU ,JPIVP) = LAYER (JPIU ,JPIVP) + M2;                    -P3-0990
        LAYER (JPIU ,JPIVM) = LAYER (JPIU ,JPIVM) + M2;                    -P3-1000
        LAYER (JPIUP,JPIV ) = LAYER (JPIUP,JPIV ) + M2;                    -P3-1010
        LAYER (JPIUP,JPIVP) = LAYER (JPIUP,JPIVP) + M3;                    -P3-1020
        LAYER (JPIUP,JPIVM) = LAYER (JPIUP,JPIVM) + M3;                    -P3-1030
        LAYER (JPIUM,JPIV ) = LAYER (JPIUM,JPIV ) + M2;                    -P3-1040
        LAYER (JPIUM,JPIVP) = LAYER (JPIUM,JPIVP) + M3;                    -P3-1050
        LAYER (JPIUM,JPIVM) = LAYER (JPIUM,JPIVM) + M3;                    -P3-1060
NDINR:  END INNER;                                                         -P3-1070
NDOTR:  END OUTER;                                                         -P3-1080
/*      */ -P3-1090
        WRITE OUT THE TX.TY.TZ TRIPLES FROM THE LAYER                      -P3-1100
/*      */ -P3-1110
        SZ = LAY;                                                           -P3-1120
SYLP:   DO SY = 0 TO IDWN BY 1;                                           -P3-1130
SXLP:   DO SX = 0 TO IACR BY 1;                                           -P3-1140
        FREQ = LAYER (SX,SY);                                              -P3-1150
        IF (FREQ > X5) THEN GO TO OUTP;                                ELSE GO TO NDSX; -P3-1160
OUTP:   WRITE FILE (SORTIN) FROM (SXYZ);                                  -P3-1170
        #INV = #INV + 1;                                                  -P3-1180
        IF (CNV) THEN PUT EDIT (SXYZ) (4 F(3),3 F(7));                ELSE; -P3-1190
NDSX:   END SXLP;                                                         -P3-1200
        END SYLP;                                                         -P3-1210
        END LAYLUP;                                                       -P3-1220
NDLAY:  FREE LAYER, LAY#, PEAKS;                                          -P3-1230
        PUT EDIT('THERE ARE',#INV,'TX.TY.TZ TRIPLES FROM INVERSIONS.') -P3-1240
        (SKIP(2),A,F(10),X(1),A);                                         -P3-1250
        PUT EDIT ('***** ALL INVERSIONS HAVE BEEN OUTPUT *****') -P3-1260
        (SKIP(2),A);                                                       -P3-1270
        RETURN;                                                           -P3-1280
        END PART3;                                                         -P3-1290
/*      */ -P3-1300

* PROCESS('ATR,XREF,NOSTMT,OPT=02');                                     -P4-0010
/*      OUTPUT TX, TY, TZ, TX.TY, TY.TZ, TZ.TX WITH FREQUENCY > 10      */ -P4-0020
PART4:  PROCEDURE (IACR, IDWN, ILAY);                                     -P4-0030
/*      */ -P4-0040
        IN PART2 THE TX, TY, TZ, TX.TY, TY.TZ, TX.TZ GROUP(S) ARE PRODUCED -P4-0050
        FROM THE NON-INVERSION SYMMETRY ELEMENTS. THESE VALUES OF        -P4-0060
        THE TRANSLATIONS ARE STORED IN THE EXTERNAL ARRAYS XLINE#,        -P4-0070
        YLINE#, ZLINE#, XYLAY#, YZLAY#, ZXLAY#. THESE VALUES ARE          -P4-0080
        WRITTEN OUT ON THE FILE "SORTIN", WITH THE UNDETERMINED VALUES -P4-0090
        SET EQUAL TO -1.                                                  -P4-0100

```

```

DECLARE (IACR,IA,IDWN,ID,ILAY,IL) FIXED BINARY (15);          */ -P4-0110
DECLARE ION(7) BIT (1) EXTERNAL;                               -P4-0120
DECLARE SORTIN FILE RECORD SEQUENTIAL;                         -P4-0130
DECLARE SLB(6) LABEL;                                          -P4-0140
DECLARE (XLINE#(0:IACR), YLINE#(0:IDWN), ZLINE#(0:ILAY),      -P4-0150
        XYLAY#(0:IA,0:ID), YZLAY#(0:ID,0:IL), ZXLAY#(0:IL,0:IA)) -P4-0160
        EXTERNAL CONTROLLED FLOAT BINARY;                     -P4-0170
DECLARE 1 SXYZ,                                                -P4-0180
        2 (SX, SY, SZ, SK) FIXED BINARY (15),                -P4-0190
        2 (VALU,MEAN,FREQ) FLOAT BINARY;                      -P4-0200
DECLARE TEN                                                    -P4-0210
DECLARE DBG                                                    -P4-0220
TEN = 10.000;                                                  -P4-0230
IA = IACR;                                                      -P4-0240
ID = IDWN;                                                       -P4-0250
IL = ILAY;                                                       -P4-0260
VALU, MEAN = 1.000;                                             -P4-0270
ON SUBSCRIPT RANGE SNAP BEGIN; PUT DATA                      -P4-0280
    (SK,SX,SY,SZ);                                             -P4-0290
    IF (DBG) THEN DO;                                          -P4-0300
    PUT EDIT ('PEAKS FROM MIRRORS, GLIDES, TWO-FOLDS, & SCREWS', -P4-0310
        ' SX SY SZ TY VALUE MEAN FREQ',                      -P4-0320
        ' SX SY SZ TY VALUE MEAN FREQ',                      -P4-0330
        ' SX SY SZ TY VALUE MEAN FREQ',                      -P4-0340
        ' SX SY SZ TY VALUE MEAN FREQ',                      -P4-0350
        (PAGE,A,SKIP,A,A,A,A));                               -P4-0360
    PUT SKIP;                                                  -P4-0370
    ELSE;                                                       -P4-0380
    GO THROUGH ALL OF THE SIX NON-INVERSION SYMMETRY TYPES    -P4-0390
    STYP: DO SK = 1 TO 6 BY 1;                                  */ -P4-0400
    IF (ION(SK)) THEN GO TO SLB(SK);                           -P4-0410
    ELSE GO TO NDS;                                             -P4-0420
    OUTPUT ALL TX WITH # > 10 FOR A PLANE NORMAL TO X          -P4-0430
    SLB(1): SY, SZ = -1;                                        */ -P4-0440
    XLUP: DO SX = 0 TO IACR BY 1;                               -P4-0450
    IF (XLINE#(SX) < TEN) THEN GO TO NDX;                     -P4-0460
    FREQ = XLINE#(SX);                                          -P4-0470
    IF (DBG) THEN PUT EDIT (SXYZ) (4 F(3),3 F(7,0));          -P4-0480
    WRITE FILE (SORTIN) FROM (SXYZ);                            ELSE; -P4-0490
    ELSE;                                                       -P4-0500
    NDX: END XLUP;                                              -P4-0510
    FREE XLINE#;                                                -P4-0520
    GO TO NDS;                                                  -P4-0530
    OUTPUT ALL TY WITH # > 10 FOR A PLANE NORMAL TO Y          -P4-0540
    SLB(2): SX, SZ = -1;                                        */ -P4-0550
    YLUP: DO SY = 0 TO IDWN BY 1;                               -P4-0560
    ELSE;                                                       -P4-0570
    ELSE;                                                       -P4-0580
    ELSE;                                                       -P4-0590
    ELSE;                                                       -P4-0600

```

	IF (YLINE#(SY) < TEN) THEN GO TO NDY;	ELSE;	-P4-0610
	FREQ = YLINE#(SY);		-P4-0620
	IF (DBG) THEN PUT EDIT (SXYZ) (4 F(3),3 F(7,0));	ELSE;	-P4-0630
	WRITE FILE (SORTIN) FROM (SXYZ);		-P4-0640
NDY:	END YLUP;		-P4-0650
	FREE YLINE#;		-P4-0660
	GO TO NDS;		-P4-0670
/*	OUTPUT ALL TX.TY WITH # > 10 FOR AN AXIS IN Z		-P4-0680
		*/	-P4-0690
SLB(3):	SZ = -1;		-P4-0700
XLXY:	DO SX = 0 TO IACR BY 1;		-P4-0710
YLXY:	DO SY = 0 TO IDWN BY 1;		-P4-0720
	IF (XYLAY#(SX,SY) < TEN) THEN GO TO NDXY;	ELSE;	-P4-0730
	FREQ = XYLAY#(SX,SY);		-P4-0740
	IF (DBG) THEN PUT EDIT (SXYZ) (4 F(3),3 F(7,0));	ELSE;	-P4-0750
	WRITE FILE (SORTIN) FROM (SXYZ);		-P4-0760
NDXY:	END YLXY;		-P4-0770
	END XLXY;		-P4-0780
	FREE XYLAY#;		-P4-0790
	GO TO NDS;		-P4-0800
/*	OUTPUT ALL TZ WITH # > 10 FOR A PLANE NORMAL TO Z		-P4-0810
		*/	-P4-0820
SLB(4):	SX, SY = -1;		-P4-0830
ZLUP:	DO SZ = 0 TO ILAY BY 1;		-P4-0840
	IF (ZLINE#(SZ) < TEN) THEN GO TO NDZ;	ELSE;	-P4-0850
	FREQ = ZLINE#(SZ);		-P4-0860
	IF (DBG) THEN PUT EDIT (SXYZ) (4 F(3),3 F(7,0));	ELSE;	-P4-0870
	WRITE FILE (SORTIN) FROM (SXYZ);		-P4-0880
NDZ:	END ZLUP;	ELSE;	-P4-0890
	FREE ZLINE#;		-P4-0900
	GO TO NDS;		-P4-0910
/*	OUTPUT ALL TZ.TX WITH # > 10 FOR AN AXIS IN Y		-P4-0920
		*/	-P4-0930
SLB(5):	SY = -1;		-P4-0940
ZLZX:	DO SZ = 0 TO ILAY BY 1;		-P4-0950
XLZX:	DO SX = 0 TO IACR BY 1;		-P4-0960
	IF (ZXLAY#(SZ,SX) < TEN) THEN GO TO NDZX;	ELSE;	-P4-0970
	FREQ = ZXLAY#(SZ,SX);		-P4-0980
	IF (DBG) THEN PUT EDIT (SXYZ) (4 F(3),3 F(7,0));	ELSE;	-P4-0990
	WRITE FILE (SORTIN) FROM (SXYZ);		-P4-1000
NDZX:	END XLZX;	ELSE;	-P4-1010
	END ZLZX;		-P4-1020
	FREE ZXLAY#;		-P4-1030
	GO TO NDS;		-P4-1040
/*	OUTPUT ALL TY.TZ WITH # > 10 FOR AN AXIS IN X		-P4-1050
		*/	-P4-1060
			-P4-1070
			-P4-1080
			-P4-1090
			-P4-1100

```

SLB(6):  SX = -1;
YLYZ:    DO SY = 0 TO IDWN BY 1;
ZLYZ:    DO SZ = 0 TO ILAY BY 1;
          IF (YZLAY#(SY,SZ) < TEN) THEN GO TO NDYZ;
          FREQ = YZLAY#(SY,SZ);
          IF (DBG) THEN PUT EDIT (SXYZ) (4 F(3),3 F(7,0));
          WRITE FILE (SORTIN) FROM (SXYZ);
NDYZ:    END ZLYZ;
          END YLYZ;
          FREE YZLAY#;
NDS:     END STYP;
          RETURN;
          END PART4;

```

```

-P4-1110
-P4-1120
-P4-1130
ELSE: -P4-1140
-P4-1150
ELSE: -P4-1160
-P4-1170
-P4-1180
-P4-1190
-P4-1200
-P4-1210
-P4-1220
-P4-1230

```

```

* PROCESS('ATR,XREF,NOSTMT,OPT=02');
/* MAP THE SYMMETRY ELEMENTS INTO EACH OTHER
PART5: PROCEDURE (IACR, IDWN, ILAY);
/*

```

```

-P5-0010
*/ -P5-0020
-P5-0030
-P5-0040

```

BEFORE THIS PART, THE VALUE OF TX, TY, TZ, TX.TY, TX.TZ, TY.TZ. & TX.TY.TZ WRITTEN OUT BY PART3 AND PART4, WERE SORTED BY DECREASING FREQUENCY (SO THAT THE MOST FREQUENT ARE FIRST) & BY DECREASING SYMMETRY (SO THAT THE INVERSIONS ARE FIRST). A NUMBER OF EACH OF THESE, PROPORTIONAL TO THE SIZE OF THE MAP AND TO THE TOTAL NUMBER OF EACH SYMMETRY ELEMENT POSSIBLE, IS NOW READ AND STORED. AT THIS POINT, THE SYMMETRY ELEMENTS ARE MAPPED INTO EACH OTHER, AS SHOWN BELOW, WITH A LATITUDE OF ONE GRID POINT ALLOWED IN EACH DIRECTION:

SYMMETRY ELEMENT	SYMMETRY ELEMENT MAPPED INTO
TX	TX.TY, TX.TZ, TX.TY.TZ
TY	TX.TY, TY.TZ, TX.TY.TZ
TZ	TX.TZ, TY.TZ, TX.TY.TZ
TX.TY	TY.TZ, TX.TZ, TX.TY.TZ
TX.TZ	TX.TY, TY.TZ, TX.TY.TZ
TY.TZ	TX.TY, TX.TZ, TX.TY.TZ

```

-P5-0050
-P5-0060
-P5-0070
-P5-0080
-P5-0090
-P5-0100
-P5-0110
-P5-0120
-P5-0130
-P5-0140
-P5-0150
-P5-0160
-P5-0170
-P5-0180
-P5-0190
-P5-0200
-P5-0210
-P5-0220
-P5-0230
-P5-0240
-P5-0250

```

A RECORD IS KEPT AS EACH MAPPING IS DONE. ALSO, THE SUMS OF THE FREQUENCIES ENCOUNTERED BY EACH MAPPING ARE COMPUTED AND STORED.

```

DECLARE (IACR, IDWN, ILAY) FIXED BINARY (15);
DECLARE (IA8, ID8, IL8, #XYZ) FIXED BINARY (15) EXTERNAL;
DECLARE 1 TXYZ,
2 (TX, TY, TZ, SK) FIXED BINARY (15),
2 (VALU, MEAN, FRQ) FLOAT BINARY;
DECLARE SORTOUT FILE RECORD SEQUENTIAL;
DECLARE (ION(7), SGNL, NCNT) BIT (1) EXTERNAL;

```

```

*/ -P5-0260
-P5-0270
-P5-0280
-P5-0290
-P5-0300
-P5-0310
-P5-0320
-P5-0330

```

```

DECLARE 1 STORE (#XYZ)          CONTROLLED,          -P5-0340
      2 (SX, SY, SZ, KS)      FIXED BINARY (15),      -P5-0350
      2 FREQ                  FLOAT BINARY;          -P5-0360
DECLARE (CST(7), TST(7))        FIXED BINARY (15);    -P5-0370
DECLARE 1 RESULT (#XYZ)        CONTROLLED EXTERNAL,   -P5-0380
      2 (RX, RY, RZ, RS)      FIXED BINARY (15);     -P5-0390
      2 (BX, BY, BXY, BZ, BXZ, BYZ) BIT (1);         -P5-0400
      2 OK                    FLOAT BINARY;          -P5-0410
DECLARE (FREQI, P1, P2, P0)     FLOAT BINARY;        -P5-0420
DECLARE CK(7)                  LABEL;                -P5-0430
DECLARE DBG                    EXTERNAL BIT (1);     -P5-0440
ON SUBSCRIPTRANGE SNAP BEGIN;  PUT DATA            -P5-0450
      (SK,I,J, KSI,IS,KSJ);      EXIT;              -P5-0460
/*                                END;                -P5-0470
P0: RIGHT ON                    -P5-0480
P1: OFF ONE GRID POINT IN ONE DIRECTION -P5-0490
P2: OFF ONE GRID POINT IN EACH OF TWO DIRECTIONS -P5-0500
/*                                */ -P5-0510
P1 = 0.8500;                    -P5-0520
P2 = 0.7000;                    -P5-0530
P0 = 1.0000;                    -P5-0540
/*                                */ -P5-0550
ALLOCATE ARRAY TO HOLD THE LARGEST TX, TY, TZ / SYMM TYPE -P5-0560
/*                                */ -P5-0570
IA8 = IACR / 4;                  -P5-0580
ID8 = IDWN / 4;                  -P5-0590
IL8 = ILAY / 4;                  -P5-0600
TST(1) = ION(1) * IA8 * 2;       -P5-0610
TST(2) = ION(2) * ID8 * 2;       -P5-0620
TST(4) = ION(4) * IL8 * 2;       -P5-0630
TST(3) = ION(3) * IA8 * ID8 * 2; -P5-0640
TST(5) = ION(5) * IL8 * IA8 * 2; -P5-0650
TST(6) = ION(6) * ID8 * IL8 * 2; -P5-0660
TST(7) = ION(7) * IA8 * ID8 * IL8 * 2; -P5-0670
#XYZ = TST(1)+TST(2)+TST(3)+TST(4)+TST(5)+TST(6)+TST(7); -P5-0680
IF (IDBG) THEN PUT EDIT ('TST =',TST,'ION =',ION) -P5-0690
      (SKIP,A,7 F(4),X(5),A,7 B(1)); ELSE; -P5-0700
ALLOCATE STORE;                  -P5-0710
FREQ = 0.000;                    -P5-0720
CST = 0;                          -P5-0730
/*                                */ -P5-0740
READ IN THE HIGHEST VALUES OF TX, TY, TZ -P5-0750
/*                                */ -P5-0760
ON ENDFILE (SORTOUT) GO TO FIND; -P5-0770
I = 0;                            -P5-0780
RRD: READ FILE (SORTOUT) INTO (TXYZ); -P5-0790
      IF (CST(SK) >= TST(SK)) THEN GO TO RRD; ELSE; -P5-0800
      CST(SK) = CST(SK) + 1;      -P5-0810
      I = I + 1;                  -P5-0820
      SX(I) = TX;                 -P5-0830

```

```

SY(I) = TY;
SZ(I) = TZ;
KS(I) = SK;
FREQ(I) = FREQ(I) + FRQ;
IF (I < #XYZ) THEN GO TO RRD;
/*
MERGE THE LOWER SYMMETRY ELEMENTS INTO THE HIGHER
FIND: CLOSE FILE (SORTOUT);
ALLOCATE RESULT;
BX, BY, BXY, BZ, BXZ, BYZ = '0'B;
RX = SX;
RY = SY;
RZ = SZ;
RS = KS;
OK = 0.000;
IF (DBG) THEN DO;
PUT EDIT ('SAVED TX, TY, TZ — BEFORE MAPPING')(PAGE,A);
PUT EDIT (' TX TY TZ SY FREQ TX TY TZ SY FREQ',
          ' TX TY TZ SY FREQ TX TY TZ SY FREQ',
          ' TX TY TZ SY FREQ TX TY TZ SY FREQ');
PUT EDIT ((SKIP(2),A,A,A); PUT SKIP(2);
END;
PUT EDIT ((STORE (I) DO I = 1 TO #XYZ)) (4 F(3),E(10,3,4));
ELSE;
ILUP: DO I = 1 TO #XYZ BY 1;
IS = KS(I);
ISX = SX(I);
ISY = SY(I);
ISZ = SZ(I);
FREQI = FREQ(I);
JLUP: DO J = 1 TO #XYZ BY 1;
KSJ = KS(J);
GO TO CK(KSJ);
/*
MERGE MIRRORS AND GLIDES WITH SCREWS, TWO-FOLDS AND INVERSIONS
MERGE TX WITH TX.TY, TX.TZ, OR TX.TY.TZ
CK(1): IF ((IS=1)|(IS=2)|(IS=4)|(IS=6)) THEN GO TO NDJ; ELSE;
IDX = ABS (ISX - SX(J));
IF (IDX < 2) THEN BX(I),BX(J) = '1'B; ELSE;
CMPX: IF (IDX=0) THEN OK(I) = OK(I) + (FREQI * FREQ(J)); ELSE;
IF (IDX=1) THEN OK(I) = OK(I) + (P1 * FREQI * FREQ(J)); ELSE;
GO TO NDJ;
/*
MERGE TY WITH TX.TY, TY.TZ OR TX.TY.TZ
CK(2): IF ((IS=1)|(IS=2)|(IS=4)|(IS=5)) THEN GO TO NDJ; ELSE;
IDY = ABS (ISY - SY(J));
IF (IDY < 2) THEN BY(I),BY(J) = '1'B; ELSE;
CMPY: IF (IDY=0) THEN OK(I) = OK(I) + (FREQI * FREQ(J)); ELSE;

```

```

IF (IDY=1) THEN OK(I) = OK(I) + (P1 * FREQI*FREQ(J)); ELSE; -P5-1340
GO TO NDJ; -P5-1350
/* -P5-1360
MERGE TZ WITH TX.TZ, TY.TZ OR TX.TY.TZ -P5-1370
*/ -P5-1380
CK(4): IF ((IS=1)|(IS=2)|(IS=3)|(IS=4)) THEN GO TO NDJ; ELSE; -P5-1390
IDZ = ABS (ISZ - SZ(J)); -P5-1400
IF (IDZ < 2) THEN BZ(I),BZ(J) = '1'B; ELSE; -P5-1410
CMPZ: IF (IDZ=0) THEN OK(I) = OK(I) + (FREQI * FREQ(J)); ELSE; -P5-1420
IF (IDZ=1) THEN OK(I) = OK(I) + (P1 * FREQI*FREQ(J)); ELSE; -P5-1430
GO TO NDJ; -P5-1440
/* -P5-1450
MAP MIRRORS & GLIDES INTO INVERSIONS & OTHER MIRRORS & GLIDES -P5-1460
MERGE TX.TY WITH TX.TZ, TY.TZ OR TX.TY.TZ -P5-1470
*/ -P5-1480
CK(3): IF ((IS=1)|(IS=2)|(IS=3)|(IS=4)) THEN GO TO NDJ; ELSE; -P5-1490
IDX = ABS (ISX - SX(J)); -P5-1500
IDY = ABS (ISY - SY(J)); -P5-1510
IF ((IDX<2) & (IDY<2)) THEN BXY(I),BXY(J)='1'B; ELSE; -P5-1520
ID1 = IDX; -P5-1530
ID2 = IDY; -P5-1540
IF (IS=5) THEN IF (IDX>1) THEN GO TO NDJ; -P5-1550
ELSE DO; BXY(I) = '1'B; -P5-1560
BXY(J)='1'B; GO TO CMPX; END; ELSE; -P5-1570
IF (IS=6) THEN IF (IDY>1) THEN GO TO NDJ; -P5-1580
ELSE DO; BXY(I) = '1'B; -P5-1590
BXY(J)='1'B; GO TO CMPY; END; ELSE; -P5-1600
IF ((IS=7)&(IDY<2)&(IDX<2)) THEN GO TO CMPXYZ; -P5-1610
ELSE GO TO NDJ; -P5-1620
/* -P5-1630
MERGE TX.TZ WITH TX.TY, TY.TZ OR TX.TY.TZ -P5-1640
*/ -P5-1650
CK(5): IF ((IS=1)|(IS=2)|(IS=4)|(IS=5)) THEN GO TO NDJ; ELSE; -P5-1660
IDZ = ABS (ISZ - SZ(J)); -P5-1670
IDX = ABS (ISX - SX(J)); -P5-1680
IF ((IDX<2) & (IDZ<2)) THEN BXZ(I),BXZ(J)='1'B; ELSE; -P5-1690
ID1 = IDZ; -P5-1700
ID2 = IDX; -P5-1710
IF (IS=3) THEN IF (IDX>1) THEN GO TO NDJ; -P5-1720
ELSE DO; BXZ(I) = '1'B; -P5-1730
BXZ(J)='1'B; GO TO CMPX; END; ELSE; -P5-1740
IF (IS=6) THEN IF (IDZ>1) THEN GO TO NDJ; -P5-1750
ELSE DO; BXZ(I) = '1'B; -P5-1760
BXZ(J)='1'B; GO TO CMPZ; END; ELSE; -P5-1770
IF ((IS=7)&(IDX<2)&(IDZ<2)) THEN GO TO CMPXYZ; -P5-1780
ELSE GO TO NDJ; -P5-1790
/* -P5-1800
MERGE TY.TZ WITH TX.TY, TX.TZ OR TX.TY.TZ -P5-1810
*/ -P5-1820
CK(6): IF ((IS=1)|(IS=2)|(IS=4)|(IS=6)) THEN GO TO NDJ; ELSE; -P5-1830

```

```

IDY = ABS (ISY - SY(J));
IDZ = ABS (ISZ - SZ(J));
IF ((IDY<2) & (IDZ<2)) THEN BYZ(I),BYZ(J)='1'B; ELSE;
ID1 = IDY;
ID2 = IDZ;
IF (IS=3) THEN IF (IDY>1) THEN GO TO NDJ;
ELSE DO; BYZ(I) = '1'B;
BYZ(J)='1'B; GO TO CMPY; END; ELSE;
IF (IS=5) THEN IF (IDZ>1) THEN GO TO NDJ;
ELSE DO; BYZ(I) = '1'B;
BYZ(J)='1'; GO TO CMPZ; END; ELSE;
IF ((IS=7)&(IDY<2)&(IDZ<2)) THEN GO TO CMPXYZ;
ELSE GO TO NDJ;
CMPXYZ: IF (ID1=0) THEN IF (ID2=0) THEN P = P0;
ELSE P = P1;
ELSE IF (ID2=0) THEN P = P1;
ELSE P = P2;
OK(J) = OK(J) + (P * FREQI * FREQ(J));
CK(7): NDJ: END JLUP;
END ILUP;
OK = OK * ((1000.000 * FLOAT(#XYZ)) / SUM(OK));
IF (DBG) THEN DO;
PUT EDIT ('SAVED TX, TY, TZ -- AFTER MAPPING')(SKIP(3),A);
PUT EDIT (' TX TY TZ SY FREQ TX TY TZ SY FREQ',
' TX TY TZ SY FREQ TX TY TZ SY FREQ',
' TX TY TZ SY FREQ TX TY TZ SY FREQ')
(SKIP(2),A,A,A); PUT SKIP(2);
PUT EDIT ((RESULT(I) DO I = 1 TO #XYZ))(4 F(3),6 B(1),F(4,0));
END; ELSE;
FREE STORE;
RETURN;
END PART5;

```

```

* PROCESS('ATR,XREF,NOSTMT,OPT=02');
/* CHOOSE THE MOST FREQUENT VALUE OF TX, TY, AND TZ */
PART6: PROCEDURE (IACR, IDWN, ILAY);
/*
THIS SUBROUTINE CHECKS THROUGH ALL OF THE PEAKS MAPPED INTO EACH
OTHER TO FIND THE HIGHEST SYMMETRY ELEMENT INTO WHICH ALL THE
LOWER SYMMETRY ELEMENTS HAVE BEEN MAPPED, WHICH HIGHER SYMMETRY
ELEMENT ALSO HAS THE HIGHEST FREQUENCY. IF THIS SYMMETRY ELEMENT
IS SUCH THAT ALL OF THE OTHER SYMMETRY ELEMENT TYPES HAVE BEEN
MAPPED INTO IT, THE PROGRAM SETS THE APPROPRIATE VALUES OF TX, TY,
& TZ AND EXITS. IF THIS LEAVES ANY ONE OF TX, TY, OR TZ UNDETER-
MINED, IT IS SET TO ZERO, AS THE ORIGIN IN THAT DIRECTION MAY BE
SET TO ANY VALUE. IF THE SYMMETRY ELEMENTS DETERMINE ALL THREE
OF TX, TY, TZ BUT DO NOT OVERLAP, SUCH AS TX.TZ AND TY, THE HIGHEST

```

FREQUENCY OF EACH IS USED TO DETERMINE THE POSITION OF THE ORIGIN. -P6-0150
 IF THE SYMMETRY ELEMENTS OVERLAP, SUCH AS TX.TY, TY.TZ, AND TX.TZ, -P6-0160
 THEN THE DIFFERENT SYMMETRY TYPES ARE SEPARATED INTO THREE ARRAYS, -P6-0170
 ONE FOR TX.TY, ONE FOR TY.TZ, AND ONE FOR TX.TZ, SORTED BY DECREA- -P6-0180
 SING FREQUENCY. THE THREE ARRAYS ARE THEN MERGED, IN THE FOLLOW- -P6-0190
 ING MANNER: LET TX1.TY1, TY2.TZ2, & TX3.TZ3 BE THE THREE DOUBLES. -P6-0200
 THEN, IF TX1=TX3 & TY1=TY2 & TZ2=TZ3, THE TRIPLE TX1.TY2.TZ3 IS -P6-0210
 THEN SAVED WITH THE SUM OF THE THREE FREQUENCIES. THE TRIPLE -P6-0220
 WITH THE HIGHEST FREQUENCY SUM IS THEN USED AS THE ORIGIN. -P6-0230

```

DECLARE      DBG                                EXTERNAL BIT (1);
DECLARE      (ION(7),SGNL,NCNT)                BIT (1) EXTERNAL;
DECLARE      (IA8,ID8,IL8,#XYZ)                FIXED BINARY (15) EXTERNAL;
DECLARE 1    RESULT (#XYZ)                     CONTROLLED EXTERNAL,
          2    (RX,RY,RZ,RS)                   FIXED BINARY (15),
          2    (BX,BY,BXY,BZ,BXZ,BYZ)         BIT (1),
          2    OK                               FLOAT BINARY;
DECLARE      (CKR (7), CKDB)                   BIT (6);
DECLARE      CKOK (7)                          FLOAT BINARY;
DECLARE      JOK (7)                          FIXED BINARY (15);
DECLARE 1    S2XY3 (IAD8)                     CONTROLLED,
          2    (X3,Y3)                         FIXED BINARY (15),
          2    OK3                             FLOAT BINARY;
DECLARE 1    S2XZ5 (IAL8)                     CONTROLLED,
          2    (X5,Z5)                         FIXED BINARY (15),
          2    OK5                             FLOAT BINARY;
DECLARE 1    S2YZ6 (IDL8)                     CONTROLLED,
          2    (Y6,Z6)                         FIXED BINARY (15),
          2    OK6                             FLOAT BINARY;
DECLARE      (J3,K3,L5,J5,K6,L6)              FIXED BINARY (15);
DECLARE      CHR                               CHARACTER (1);
DECLARE      (IFX,IFY,IFZ)                    FIXED BINARY (15) EXTERNAL;
DECLARE      FOK                               FLOAT BINARY;
DECLARE 1    FXYZ (#OK)                       CONTROLLED EXTERNAL,
          2    (XR,YR,ZR,SR)                   FIXED BINARY (15),
          2    BSTRG                           BIT (6),
          2    GOK                             FLOAT BINARY;
DECLARE      #OK                              FIXED BINARY EXTERNAL;
ON SUBSCRIPTRANGE SNAP BEGIN; PUT DATA
(#OK,INDX,II,J,JRS,IRS,JFNL,I3,I3,I6,J3,J5,J6,I,L,K,I356);
EXIT;
  
```

/*

"CKR" HOLDS BIT STRINGS TO BE CHECKED. FOR EXAMPLE IF THERE
 ARE THE FOLLOWING SYMMETRY ELEMENTS TY, TX.TZ, TX.TY.TZ,
 AS IN P21/C, THEN ONE WOULD HAVE ION(1),ION(3),ION(4),ION(6)
 =0 AND ION(2),ION(5),ION(7) = 1. PART5 SHOULD HAVE MAPPED
 TY INTO TX.TY.TZ AND TX.TZ INTO TX.TY.TZ, AND WOULD HAVE LEFT
 A RECORD OF SUCH MAPPING. IF, FOR A PARTICULAR TRIPLE OF
 TX.TY.TZ THERE IS NO INDICATION OF BOTH TY AND TX.TZ BEING
 MAPPED IN, THEN THAT TRIPLE IS ASSUMED TO BE FALSE.

```

/* -P6-0650
CKR(7) = ION(1) || ION(2) || ION(3) || ION(4) || ION(5) || ION(6); -P6-0660
CKR(6) = '0'B || ION(2) || ION(3) || ION(4) || ION(5) || '1'B; -P6-0670
CKR(5) = ION(1) || '0'B || ION(3) || ION(4) || '1'B || ION(6); -P6-0680
CKR(3) = ION(1) || ION(2) || '1'B || '0'B || ION(5) || ION(6); -P6-0690
CKR(4) = '000'B || ION(4) || '00'B; -P6-0700
CKR(2) = '0'B || ION(2) || '0000'B; -P6-0710
CKR(1) = ION(1) || '00000'B; -P6-0720
IF (DBG) THEN PUT EDIT('CKR =',CKR) (SKIP,A,7 (B(7),X(1))); -P6-0730
ELSE; -P6-0740
CKOK = 0.000; -P6-0750
JOK = 0; #OK = 0; -P6-0760
IRS = 0; IDL8 = ID8 * IL8 * 2; -P6-0770
IAD8 = IA8 * ID8 * 2; IAL8 = IA8 * IL8 * 2; -P6-0780
/* -P6-0790
DETERMINE THE HIGHEST SYMMETRY ELEMENT TO BE CONSIDERED -P6-0800
LUPJ: DO J = 1 TO #XYZ BY 1; */ -P6-0810
CKDB = BX(J) || BY(J) || BXY(J) || BZ(J) || BXZ(J) || BYZ(J); -P6-0820
JRS = RS(J); -P6-0830
IF (CKDB = CKR(JRS)) THEN DO; -P6-0840
OK(J) = 0.000; -P6-0850
GO TO NDJL; END; -P6-0860
IF (OK(J) > CKOK(JRS)) THEN DO; ELSE; -P6-0870
CKOK(JRS) = OK(J); -P6-0880
JOK(JRS) = J; END; -P6-0890
IF (JRS = 4) THEN JRS = 3; ELSE; -P6-0900
IF (JRS = 3) THEN JRS = 4; ELSE; -P6-0910
IF (JRS >= IRS) THEN IRS = JRS; ELSE; -P6-0920
IF (OK(J) > 0.0) THEN #OK = #OK + 1; ELSE; -P6-0930
NDJL: END LUPJ; -P6-0940
IF (DBG) THEN DO; -P6-0950
PUT EDIT ('SAVED TX, TY, TZ --- BEFORE MERGING & SORTING') -P6-0960
(PAGE,A); -P6-0970
PUT EDIT (' TX TY TZ SY FREQ TX TY TZ SY FREQ', -P6-0980
' TX TY TZ SY FREQ TX TY TZ SY FREQ', -P6-0990
' TX TY TZ SY FREQ TX TY TZ SY FREQ') -P6-1000
(SKIP(2),A,A,A); PUT SKIP(2); -P6-1010
PUT EDIT ((RESULT(I) DO I = 1 TO #XYZ)) (4 F(3),6 B(1),F(4,0)); -P6-1020
PUT EDIT ('JOK =',JOK,'CKOK =',CKOK) -P6-1030
(SKIP,A,7 F(5),X(10),A,7 F(10,2)); -P6-1040
END; ELSE; -P6-1050
/* -P6-1060
BRANCH, DEPENDING ON THE TYPE OF THE HIGHEST SYMM. ELEMENT -P6-1070
IF (IRS = 3) THEN IRS = 4; ELSE; */ -P6-1080
IF (IRS = 4) THEN IRS = 3; ELSE; -P6-1090
JFNL = JOK(IRS); -P6-1100
IFX = RX(JFNL); -P6-1110
IFY = RY(JFNL); -P6-1120
-P6-1130
-P6-1140

```

```

IFZ = RZ(JFNL);
FOK = OK(JFNL);
IF (IRS=7) THEN GO TO CMP7;
IF ((IRS=6) & (~ION(5)) & (~ION(3))) THEN GO TO CMP6;
IF ((IRS=5) & (~ION(6)) & (~ION(3))) THEN GO TO CMP5;
IF ((IRS=3) & (~ION(6)) & (~ION(5))) THEN GO TO CMP3;
IF ((IRS=4) | (IRS=2) | (IRS=1)) THEN GO TO CMPL;

/*
THERE ARE THREE TWO-FOLD AXES OR TWO-FOLD SCREW AXES

ALLOCATE S2XY3, S2XZ5, S2YZ6;
X3, Y3 = 0;
OK3 = 0.000;
X5, Z5 = 0;
OK5 = 0.000;
Y6, Z6 = 0;
OK6 = 0.000;
I3, I5, I6 = 1;
J3 = JOK(3);
J5 = JOK(5);
J6 = JOK(6);
I356 = 3;
K356, L356 = 0;
OK3, OK5, OK6 = 0.000;
A3: IF (I3 > (IAD8)) THEN GO TO A5;
IF (J3 = 0) THEN GO TO A5;
X3(I3) = RX(J3);
Y3(I3) = RY(J3);
OK3(I3) = OK(J3);
OK(J3) = 0.000;
A5: IF (I5 > (IAL8)) THEN GO TO A6;
IF (J5 = 0) THEN GO TO A6;
X5(I5) = RX(J5);
Z5(I5) = RZ(J5);
OK5(I5) = OK(J5);
OK(J5) = 0.000;
A6: IF (I6 > (IDL8)) THEN GO TO Z356;
IF (J6 = 0) THEN GO TO Z356;
Y6(I6) = RY(J6);
Z6(I6) = RZ(J6);
OK6(I6) = OK(J6);
OK(J6) = 0.000;

/*
PLACE ALL OF THE TWO-FOLDS IN ARRAYS IN DESCENDING ORDER

Z356: K356 = L356;
L356 = I356;
I356 = I3 + I5 + I6;
IF (K356=I356) THEN GO TO PKAL;
IF (DBG) THEN PUT EDIT (I356) (F(6));

```

```

-P6-1150
-P6-1160
ELSE; -P6-1170
ELSE; -P6-1180
ELSE; -P6-1190
ELSE; -P6-1200
ELSE; -P6-1210
-P6-1220
-P6-1230
*/ -P6-1240
-P6-1250
-P6-1260
-P6-1270
-P6-1280
-P6-1290
-P6-1300
-P6-1310
-P6-1320
-P6-1330
-P6-1340
-P6-1350
-P6-1360
-P6-1370
-P6-1380
ELSE; -P6-1390
ELSE; -P6-1400
-P6-1410
-P6-1420
-P6-1430
-P6-1440
ELSE; -P6-1450
ELSE; -P6-1460
-P6-1470
-P6-1480
-P6-1490
-P6-1500
ELSE; -P6-1510
ELSE; -P6-1520
-P6-1530
-P6-1540
-P6-1550
-P6-1560
-P6-1570
-P6-1580
*/ -P6-1590
-P6-1600
-P6-1610
-P6-1620
ELSE; -P6-1630
ELSE; -P6-1640

```

```

J3, J5, J6 = 0;
B3, B5, B6 = 0.001;
IF (I356 > #XYZ) THEN GO TO PKAL;
DLUP: DO I = 1 TO #XYZ BY 1;
      OK356 = OK(I);
      J356 = RS(I);
      IF ((OK356 > B3) & (J356 = 3)) THEN DO;
        B3 = OK356;
        J3 = I;
      ELSE;
      IF ((OK356 > B5) & (J356 = 5)) THEN DO;
        B5 = OK356;
        J5 = I;
      ELSE;
      IF ((OK356 > B6) & (J356 = 6)) THEN DO;
        B6 = OK356;
        J6 = I;
      ELSE;
      END DLUP;
      IF (J3 = 0) THEN I3 = I3 + 1;
      IF (J5 = 0) THEN I5 = I5 + 1;
      IF (J6 = 0) THEN I6 = I6 + 1;
      IF ((I3 > IAD8)) & (I5 > IAL8)) & (I6 > IDL8))
        THEN GO TO PKAL; ELSE GO TO A3;
/*
FIND THE MOST FREQUENT AND CONSISTANT TX.TY.TZ
PKAL: I356 = 0;
      OK = 0.000;
      IF (DBG) THEN DO;
        PUT EDIT ('SORTED TX.TY, TY.TZ, TX.TZ -- PART 6')
          (SKIP(4),A);
        PUT EDIT (' TX TY TZ SY      FREQ TX TY TZ SY      FREQ',
          ' TX TY TZ SY      FREQ TX TY TZ SY      FREQ',
          ' TX TY TZ SY      FREQ TX TY TZ SY      FREQ')
          (SKIP(2),A,A,A); PUT SKIP(2);
        PUT EDIT ((S2XY3(I) DO I = 1 TO IAD8))
          (2 F(3),X(9),F(7,0));
        PUT EDIT ((S2XZ5(I) DO I = 1 TO IAL8))
          (F(3),X(3),F(3),X(6),F(7,0));
        PUT EDIT ((S2YZ6(I) DO I = 1 TO IDL8))
          (X(3),2 F(3),X(6),F(7,0));
      END;
LP6: DO L = 1 TO IDL8 BY 1;
      IF (OK6(L) = 0.000) THEN GO TO FNL2S;
      K6 = Y6(L);
      L6 = Z6(L);
LP5: DO K = 1 TO IAL8 BY 1;
      IF (OK5(K) = 0.000) THEN GO TO NDL5;
      J5 = X5(K);
      L5 = Z5(K);
LP3: DO J = 1 TO IAD8 BY 1;
      IF (OK3(J) = 0.000) THEN GO TO NDL3;

```

```

-P6-1650
-P6-1660
-P6-1670
-P6-1680
-P6-1690
-P6-1700
-P6-1710
-P6-1720
-P6-1730
-P6-1740
-P6-1750
-P6-1760
-P6-1770
-P6-1780
-P6-1790
-P6-1800
-P6-1810
-P6-1820
-P6-1830
-P6-1840
-P6-1850
-P6-1860
-P6-1870
-P6-1880
-P6-1890
-P6-1900
-P6-1910
-P6-1920
-P6-1930
-P6-1940
-P6-1950
-P6-1960
-P6-1970
-P6-1980
-P6-1990
-P6-2000
-P6-2010
-P6-2020
-P6-2030
-P6-2040
-P6-2050
-P6-2060
-P6-2070
-P6-2080
-P6-2090
-P6-2100
-P6-2110
-P6-2120
-P6-2130
-P6-2140

```

```

J3 = X3(J);
K3 = Y3(J);
IF ((J3=J5) & (K3=K6) & (L5=L6)) THEN GOOD: DO;
    I356 = I356 + 1;
    IF (I356 > #XYZ) THEN GO TO FNL2S;
    RX(I356) = J3;
    RY(I356) = K3;
    RZ(I356) = L5;
    RS(I356) = 7;
    OK(I356) = OK6(L) + OK5(K) + OK3(J);
NOL3: END LP3;
NOL5: END LP5;
FNL2S: END LP6;
IF (CBG) THEN DO;
    PUT EDIT ('MERGED TX.TY, TY.TZ, TX.TZ -- PART 6')
    (SKIP(4),A);
    PUT EDIT (' TX TY TZ SY      FREQ TX TY TZ SY      FREQ',
    ' TX TY TZ SY      FREQ TX TY TZ SY      FREQ',
    ' TX TY TZ SY      FREQ TX TY TZ SY      FREQ')
    (SKIP(2),A,A,A);
    PUT EDIT ((RX(I),RY(I),RZ(I),RS(I),OK(I) DO I = 1 TO #XYZ))
    (3 F(3),F(2),F(11,0));
    END;
    ELSE;
    FOK = 0.000;
    DO M = 1 TO #XYZ BY 1;
    IF (OK(M) > FOK) THEN DO;
        MF = M;
        FOK = OK(M);
        END;
    END FLUP;
    IFX = RX(MF);
    IFY = RY(MF);
    IFZ = RZ(MF);
    GO TO WXYZ;
/*
    THERE IS AN INVERSION CENTER
    */
CMP7: PUT EDIT ('THE HIGHEST SYMMETRY ELEMENT IS AN INVERSION.')
    (SKIP(4),A);
    GO TO WXYZ;
/*
    THE HIGHEST SYMMETRY ELEMENT IS A TWO-FOLD OR SCREW
    */
CMP6: CHR = 'X';
    IF (JOK(1) /= 0) THEN DO;
        IFX = RX(JOK(1));
        FOK = FOK + OK(JOK(1));
        GO TO P2G;
        END;
        ELSE;
        IFX = 0;
        GO TO P2B;
    END;
CMP5: CHR = 'Y';

```

```

-P6-2150
-P6-2160
-P6-2170
-P6-2180
-P6-2190
-P6-2200
-P6-2210
-P6-2220
-P6-2230
-P6-2240
-P6-2250
-P6-2260
-P6-2270
-P6-2280
-P6-2290
-P6-2300
-P6-2310
-P6-2320
-P6-2330
-P6-2340
-P6-2350
-P6-2360
-P6-2370
-P6-2380
-P6-2390
-P6-2400
-P6-2410
-P6-2420
-P6-2430
-P6-2440
-P6-2450
-P6-2460
-P6-2470
-P6-2480
-P6-2490
-P6-2500
-P6-2510
-P6-2520
-P6-2530
-P6-2540
-P6-2550
-P6-2560
-P6-2570
-P6-2580
-P6-2590
-P6-2600
-P6-2610
-P6-2620
-P6-2630
-P6-2640

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```

IF (JOK(2) /= 0) THEN DO;
    IFY = RY(JOK(2));
    FCK = FCK + OK(JOK(2));
    GO TO P2G;
END;
ELSE;
    IFY = 0;
    GO TO P2B;
CMP3: CHR = 'Z';
IF (JOK(4) /= 0) THEN DO;
    IFZ = RZ(JOK(4));
    FCK = FCK + OK(JOK(4));
    GO TO P2G;
END;
ELSE;
    IFZ = 0;
P2B: PUT EDIT (' THE HIGHEST SYMMETRY ELEMENT IS AN AXIS IN ',CHR,
    'UNABLE TO DETERMINE T',CHR,'.  THUS, T',CHR,
    'SET EQUAL TO ZERO. ');
    (SKIP(4),X(10),A,A(1),SKIP(1),X(20),3 (A,A(1)));
GO TO WXYZ;
P2G: PUT EDIT (' THE HIGHEST SYMMETRY ELEMENT IS AN AXIS IN ',CHR,
    'HOWEVER, THERE IS A PLANE NORMAL TO ',CHR)
    (SKIP(4),X(10),A,A(1),SKIP(1),X(20),A,A(1));
GO TO WXYZ;
/*
THERE IS ONLY A MIRROR OR GLIDE PLANE NORMAL TO ONE AXIS
CMPL: PUT EDIT ('THERE IS ONLY A PLANE NORMAL TO ONE AXIS.',
    'THE T'S IN THE OTHER DIRECTIONS ARE SET =0.')
    (SKIP(4),X(10),A,SKIP(1),X(20),A);
IFX, IFY, IFZ = 0;
IF (IRS = 4) THEN IFZ = RZ(JFNL);
IF (IRS = 2) THEN IFY = RY(JFNL);
IF (IRS = 1) THEN IFX = RX(JFNL);
WXYZ: PUT EDIT ('***** TX =',IFX,'TY =',IFY,'TZ =',IFZ)
    (SKIP(2),3 (A,F(5),X(5)));
FREE S2YZ6, S2XY3, S2XZ5;
ALLOCATE FXYZ;
INDX = 0;
PUT EDIT ('SAVED TRIPLES, DOUBLES, AND SINGLES') (PAGE,A);
PUT EDIT (' TX TY TZ SY      FREQ TX TY TZ SY      FREQ',
    ' TX TY TZ SY      FREQ TX TY TZ SY      FREQ',
    ' TX TY TZ SY      FREQ TX TY TZ SY      FREQ')
    (SKIP(2),A,A,A);
PUT SKIP(2);
IILP: DO II = 1 TO #XYZ BY 1;
    IF (OK(II) > 1) THEN GO: DO;
    INDX = INDX + 1;
    XR(INDX) = RX(II);
    YR(INDX) = RY(II);
    ZR(INDX) = RZ(II);
    SR(INDX) = RS(II);
    GOK(INDX) = OK(II);
    BSTRG(INDX) = BX(II) || BY(II) || BXY(II) || BZ(II)

```

```

      || BXZ(II) || BYZ(II);
      PUT EDIT (FXYZ(INDX)) (4 F(3),B(6),F(4,0));
END GD;
FREE RESULT;
RETURN;
END PART6;

```

-P6-3150
 -P6-3160
 -P6-3170
 -P6-3180
 -P6-3190
 -P6-3200

```

* PROCESS('ATR,XREF,NOSTMT,OPT=02');
/* DETERMINE WHICH PEAKS ARE TO BE KEPT
PART7: PROCEDURE (IACR, IDWN, ILAY, #RTND, #SYMM);
/*
  THIS SUBROUTINE MAKES USE OF THE ORIGIN TRANSLATION TX.TY.TZ AND
  OF THE SYMMETRY ELEMENTS TO DETERMINE WHICH PEAKS FIT IN E.D.
  SPACE. IF AT LEAST HALF OF THE SYMMETRY-RELATED PEAKS ARE PRESENT
  WHEN THE ENTIRE MAP HAS BEEN SHIFTED BY TX.TY.TZ, THEN THAT SET
  OF PEAKS IS OUTPUT IN THE SHIFTED COORDINATES
  */
  DECLARE (IACR,IDWN,ILAY,#RTND,#SYMM) FIXED BINARY (15);
  DECLARE (IFX,IFY,IFZ) FIXED BINARY (15) EXTERNAL;
  DECLARE 1 SYMMPQ (#SYMM) CONTROLLED EXTERNAL;
  2 (PX,QX,PY,QY,PZ,QZ) FIXED BINARY (15);
  DECLARE #OK FIXED BINARY EXTERNAL;
  DECLARE 1 FXYZ (#OK) CONTROLLED EXTERNAL;
  2 (XR,YR,ZR,SR) FIXED BINARY (15);
  2 BSTRG BIT (6);
  2 GOK FLOAT BINARY;
  DECLARE 1 PEAKS (#RTND) CONTROLLED;
  2 (U,V,W,VLU,X,Y,Z) FIXED BINARY;
  DECLARE 1 PEAKR,
  2 (RU,RV,RW,VAL,AVG) FIXED BINARY (31);
  DECLARE (RETAIN, FINAL) FILE RECORD SEQUENTIAL;
  DECLARE (BX, BY, BZ) BIT (1);
  DECLARE DBG BIT (1) EXTERNAL;
  ON SUBSCRIPTRANGE SNAP BEGIN; PUT DATA (I,J,K); EXIT; END;
  DECLARE JAVG (#SYMM) CONTROLLED FIXED BINARY;
  DECLARE PVALUE (16) FIXED BINARY (15);
  DECLARE (L,M,N) FIXED BINARY (15);
  DECLARE (KX,KY,KZ,NSY,CL(24)) FIXED BINARY (15);
  DECLARE 1 FPEAK,
  2 (HITE,FX,FY,FZ,#) FIXED BINARY (31);
  DECLARE ON= FLOAT BINARY;
  ONE = 1.0000;
  CL(1), CL( 7), CL(13), CL(19) = 40;
  CL(2), CL( 8), CL(14), CL(20) = 56;
  CL(3), CL( 9), CL(15), CL(21) = 72;
  CL(4), CL(10), CL(16), CL(22) = 88;
  CL(5), CL(11), CL(17), CL(23) = 104;

```

-P7-0010
 -P7-0020
 -P7-0030
 -P7-0040
 -P7-0050
 -P7-0060
 -P7-0070
 -P7-0080
 -P7-0090
 -P7-0100
 -P7-0110
 -P7-0120
 -P7-0130
 -P7-0140
 -P7-0150
 -P7-0160
 -P7-0170
 -P7-0180
 -P7-0190
 -P7-0200
 -P7-0210
 -P7-0220
 -P7-0230
 -P7-0240
 -P7-0250
 -P7-0260
 -P7-0270
 -P7-0280
 -P7-0290
 -P7-0300
 -P7-0310
 -P7-0320
 -P7-0330
 -P7-0340
 -P7-0350
 -P7-0360
 -P7-0370
 -P7-0380
 -P7-0390
 -P7-0400

```

CL(6), CL(12), CL(18), CL(24) = 120;
L = ROUND (FLOAT (IACR) / 16.000, 0);
M = ROUND (FLOAT (IDWN) / 16.000, 0);
N = ROUND (FLOAT (ILAY) / 16.000, 0);
ISYM = MAX (#SYMM/2 +1, 1);
IPEAK = 0;
QACR = FLOAT (IACR);
QDWN = FLOAT (IDWN);
QLAY = FLOAT (ILAY);
ALLOCATE PEAKS;
ALLOCATE JAVG;
IF (DBG) THEN PUT EDIT ('$$$$ TX =', IFX, 'TY =', IFY, 'TZ =',
                        IFZ) (SKIP(4), 3 (A, F(5), X(5))); ELSE;
/*
READ AND STORE THE PEAKS, TRANSFORMING THEM TO E.D. COORDS. */
OPEN FILE (RETAIN) INPUT;
RLUP: DO I = 1 TO #RTND BY 1;
      READ FILE (RETAIN) INTO (PEAKR);
      U(I) = RU;
      V(I) = RV;
      W(I) = RW;
      VLU(I) = AVG;
      X(I) = MOD (RU - IFX, IACR);
      Y(I) = MOD (RV - IFY, IDWN);
      Z(I) = MOD (RW - IFZ, ILAY);
      END RLUP;
      CLOSE FILE (RETAIN);
      OPEN FILE (FINAL) OUTPUT;
      NPEAK = 0;
      PUT EDIT ('PEAK BEING CHECKED (PART7) -- #, OR',
                'ORIGINAL (UVW) & TRANSFORMED (XYZ) COORDS., EQUIV. P',
                'POSITIONS (EX,EY,EZ), & # OF MATCHING PEAK (#MP)',
                '  #    U    V    W VALUE    X    Y    Z    ',
                '    EX EY EZ #MP    EX EY EZ #MP    EX EY EZ #MP',
                '    EX EY EZ #MP    EX EY EZ #MP    EX EY EZ #MP')
                (PAGE,A,A,A,SKIP,A,A,A);
      PUT SKIP;
/*
LOOP THROUGH ALL RETAINED PEAKS TO DETERMINE WHICH ONES ARE
ALLOWED BY SYMMETRY AND OUTPUTTING THE ALLOWED PEAKS. */
ILUP: DO I = 1 TO #RTND BY 1;
      IF (VLU(I) < 1.00) THEN GO TO NDIL; ELSE;
      RU = U(I);
      RV = V(I);
      RW = W(I);
      VAL = VLU(I);
      IVAL = VAL;
      AVG = 0;

```

```

RX = X(I);
RY = Y(I);
RZ = Z(I);
PUT EDIT (I, RU, RV, RW, VAL, RX, RY, RZ)
      (SKIP, F(3), 3 F(4), F(6), 3 F(4));
/*
CREATE EQUIVALENT POSITIONS FROM SYMMETRY ELEMENTS
SLUP: DO K = 1 TO #SYMM BY 1;
      KX = MOD ((RX * PX(K)) + QX(K), IACR);
      KY = MOD ((RY * PY(K)) + QY(K), IDWN);
      KZ = MOD ((RZ * PZ(K)) + QZ(K), ILAY);
      KXI = KX + IACR;
      KYI = KY + IDWN;
      KZI = KZ + ILAY;
      NSY = CL(K);
      PUT EDIT (KX, KY, KZ) (COL(NSY), 3 F(3));
/*
LOOP THROUGH ALL PEAKS - LOOKING FOR SYMMETRY RELATED PEAKS
JLUP: DO J = 1 TO #RTND BY 1;
      IF (VLU(J) < 1.00) THEN GO TO NDJL;
      OX = MIN (ABS(KX-X(J)), ABS(KXI-X(J)));
      OY = MIN (ABS(KY-Y(J)), ABS(KYI-Y(J)));
      OZ = MIN (ABS(KZ-Z(J)), ABS(KZI-Z(J)));
      BX = (OX <= L);
      BY = (OY <= M);
      BZ = (OZ <= N);
      IF (BX & BY & BZ) THEN GO TO PNDS;
      NDJL: END JLUP;
      GO TO NDSL;
      PNDS: AVG = AVG + 1;
      JAVG(AVG) = J;
      PUT EDIT (J) (F(4));
      IVAL = IVAL + VLU(J);
      NDSL: END SLUP;
/*
OUTPUT THE GOOD PEAKS
      IF (AVG < ISYM) THEN GO TO NDIL;
      NPEAK = NPEAK + AVG + 1;
      HITE = IVAL / (AVG + 1);
      # = AVG;
      FX = RX;
      FY = RY;
      FZ = RZ;
      VLU(I) = 0;
      WRITE FILE (FINAL) FROM (FPEAK);
      IPEAK = IPEAK + 1;
      LUPJ: DO J = 1 TO AVG BY 1;

```

```

-P7-0910
-P7-0920
-P7-0930
-P7-0940
-P7-0950
-P7-0960
-P7-0970
*/ -P7-0980
-P7-0990
-P7-1000
-P7-1010
-P7-1020
-P7-1030
-P7-1040
-P7-1050
-P7-1060
-P7-1070
-P7-1080
-P7-1090
*/ -P7-1100
-P7-1110
ELSE; -P7-1120
-P7-1130
-P7-1140
-P7-1150
-P7-1160
-P7-1170
-P7-1180
ELSE; -P7-1190
-P7-1200
-P7-1210
-P7-1220
-P7-1230
-P7-1240
-P7-1250
-P7-1260
-P7-1270
-P7-1280
*/ -P7-1290
ELSE; -P7-1300
-P7-1310
-P7-1320
-P7-1330
-P7-1340
-P7-1350
-P7-1360
-P7-1370
-P7-1380
-P7-1390
-P7-1400

```

	JS = JAVG(J);	-P7-1410
	VLU(JS) = 0;	-P7-1420
NDLJ:	END LUPJ;	-P7-1430
NDIL:	END ILUP;	-P7-1440
	PUT EDIT ('# PEAKS RETAINED =',NPEAK) (SKIP(2),A,F(5));	-P7-1450
	CLOSE FILE (FINAL);	-P7-1460
	OPEN FILE (FINAL) INPUT;	-P7-1470
	PUT EDIT ('NUMBER OF INDEPENDENT PEAKS =',IPEAK)	-P7-1480
	(SKIP(2),A,F(5));	-P7-1490
	PUT EDIT ('INDEPENDENT PEAKS AFTER SYMMETRY CHECK',	-P7-1500
	' X Y Z (FOUR.) X Y Z',	-P7-1510
	' (FRACT.) HEIGHT #SYMM', ' ')	-P7-1520
	(PAGE,A,SKIP,A,A,SKIP(2),A);	-P7-1530
/*	OUTPUT PEAKS REMAINING AFTER SYMMETRY CHECK ON "ORFLS" CARDS	-P7-1540
	WRITE OUT FOUND PEAKS AND PUNCH LEAST SQUARES CARDS	-P7-1550
		-P7-1560
		-P7-1570
LUPI:	DO I = 1 TO IPEAK BY 1;	-P7-1580
	READ FILE (FINAL) INTO (FPEAK);	-P7-1590
	XFR = FLOAT (FX) / QACR;	-P7-1600
	YFR = FLOAT (FY) / QDWN;	-P7-1610
	ZFR = FLOAT (FZ) / QLAY;	-P7-1620
	PUT EDIT (FX,FY,FZ,XFR,YFR,ZFR,HITE,#)	-P7-1630
	(SKIP,3 F(5),X(4),3 F(10,5),X(9),2 F(10));	-P7-1640
	PUT FILE (PUNCH) EDIT (HITE,ONE,ONE,XFR,YFR,ZFR)	-P7-1650
	(SKIP,F(5),X(4),5 F(9,5));	-P7-1660
	END LUPI;	-P7-1670
	CLOSE FILE (FINAL), FILE (PUNCH);	-P7-1680
	RETURN;	-P7-1690
	END PART7;	-P7-1700

//LKED.SYSLMOD DD DSN=PROG.CRYST,	JCL-0060
// UNIT=DISK,VOLUME=SER=PROGPK,DISP=(OLD,KEEP)	JCL-0070
//LKED.SYSIN DD *	JCL-0080
OVERLAY ALPHA	OVLY0010
INSERT TM_DT	OVLY0020
OVERLAY ALPHA	OVLY0030
INSERT PART1	OVLY0040
OVERLAY ALPHA	OVLY0050
INSERT PART2	OVLY0060
OVERLAY ALPHA	OVLY0070
INSERT IHESRTA	OVLY0080
OVERLAY ALPHA	OVLY0090
INSERT PART3	OVLY0100
OVERLAY ALPHA	OVLY0110
INSERT PART4	OVLY0120
OVERLAY ALPHA	OVLY0130

INSERT PART5
OVERLAY ALPHA
INSERT PART6
OVERLAY ALPHA
INSERT PART7
NAME ALOP2(R)

OVLY0140
OVLY0150
OVLY0160
OVLY0170
OVLY0180
JCL-0090

60

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ACKNOWLEDGEMENTS

The sources of aid and encouragement received during the course of the research described in this thesis are much too numerous to mention in completeness. However, the author especially would like to express his deep and sincere gratitude to:

Prof. Robert A. Jacobson for his unhesitating willingness to share his experience and extensive theoretical and practical knowledge, his seemingly inexhaustible words of advice and encouragement, and his constantly high expectations of and confidence in the author's abilities;

the State of Iowa and the United States government for financial assistance in the form of teaching and research assistantships;

the faculty and graduate students for their helpful discussions and repeated assistance, and a very special acknowledgement to the members, both past and present, of X-ray Group I;

James Benson for giving so willingly and patiently of his time, knowledge and experience;

Gary Dubois, summer research trainee, and Susan Scott, research helper, for their assistance