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MICROSTRUCTURAL DEVELOPMENT IN Ag-CLAD Bi-2223
COMPOSITE CONDUCTORS***

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EFFECT OF LEAD CONTENT ON PHASE EVOLUTION AND MICROSTRUCTURAL DEVELOPMENT IN Ag-CLAD Bi-2223 COMPOSITE CONDUCTORS*

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Abstract

A two powder process was used to prepare silver-sheathed monofilamentary $\text{Bi}_{1.8}\text{Pb}_x\text{Sr}_{1.98}\text{Ca}_{1.97}\text{Cu}_{3.08}\text{O}_y$ (Bi-2223) tapes with varying lead contents, x , from 0.2 to 0.5. The resulting tapes were subjected to thermomechanical processing and then characterized by x-ray diffraction (XRD), scanning electron microscopy (SEM), and energy dispersive x-ray analysis (EDX). Layered phase texture was accessed using image analysis software on scanned SEM micrographs. Transport currents were measured at 77 K and zero field by the four-probe method. It was found that tapes with low lead content ($x=0.2$ and 0.25) showed incomplete conversion to Bi-2223, had small grain size and poor c-axis texture. Tapes having higher lead content ($x=0.4$ and 0.5) also showed incomplete conversion and the presence of lead-rich secondary phases. Tapes with lead content $x=0.3$ and 0.35 showed complete conversion to Bi-2223, and had the least amount of secondary phases, the best c-axis texture, and the highest transport currents (J_c). The carbon content of the precursor powder also had a strong influence on secondary-phase chemistry.

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Introduction

Since the discovery of the 110 K superconducting phase $\text{Bi}_2\text{Sr}_2\text{Ca}_2\text{Cu}_3\text{O}_y$ (Bi-2223) in 1988 [1,2], a great deal of research has been focused on optimization of its phase purity and microstructure [3-6]. Lead addition to the Bi-Sr-Ca-Cu-O system was shown to stabilize the Bi-2223 phase and also accelerate the phase formation kinetics [7-9]. Other related studies revealed that the lead content is a critical variable in fabricating tapes by the two-powder process [10,11].

Earlier studies by Dorris et al. [11-13] revealed that the optimum lead content in $\text{Bi}_{1.8}\text{Pb}_x\text{Sr}_2\text{Ca}_2\text{Cu}_3\text{O}_y$ is near $x=0.4$ and that the mode of lead addition (whether in $\text{Bi}_2\text{Sr}_2\text{CaCu}_2\text{O}_8$ (Bi-2212) or in the secondary phases) is an important factor. However, no systematic work has been done to study the effect of lead content on the microstructure and superconducting properties of Ag-clad Bi-2223 composite conductors.

In this paper, we extend the prior work of Dorris et al. [11-13] to an investigation of microstructural evolution in two-powder Ag/Bi-2223 composite conductors containing $\text{Bi}_{1.8}\text{Pb}_x\text{Sr}_2\text{CaCu}_2\text{O}_8$ with various lead contents in the range from $x=0.2$ to 0.5.

Experimental Procedure

Lead-doped $\text{Bi}_{1.8}\text{Pb}_x\text{Sr}_2\text{Ca}_{1.0}\text{Cu}_2\text{O}_8$ (Bi-2212) powders were prepared with x values of 0.2, 0.25, 0.3, 0.35, 0.4, and 0.5. The six powder mixtures with appropriate amounts of Bi_2O_3 , PbO , SrCO_3 , CaCO_3 , and CuO were calcined first at a reduced total pressure of ~ 3 torr O_2 ($20^\circ\text{C}/\text{h}$ to 750°C , followed by 6 h at 750°C) to ensure complete decomposition of the carbonates. After calcining at reduced pressure, the Bi-2212 phase was formed by further calcining for 24 h at 840°C in CO_2 -free air at ambient pressure. The powders were then ball milled in isopropyl alcohol for 12-16 h and calcined again for 24 h at 840°C in CO_2 -free air at ambient pressure. This sequence of calcinations in air followed by intermediate ball milling was repeated until near-single-phase materials were obtained. The powders were then calcined in argon to remove any Ca_2PbO_4 that may have formed and to ensure that all the lead was incorporated in the Bi-2212 phase [14]. The Bi-2223 precursors were prepared by mixing each of the six lead-doped Bi-2212 batches with an equimolar amount of CaCuO_2 , then ball milling in isopropyl alcohol for 12-16 h and calcining at ~ 3 torr ($60^\circ\text{C}/\text{h}$ to 720°C , followed by 3 h at 720°C) to eliminate carbon introduced during milling. Two separate batches of powder with lead content $x=0.4$ and 0.5 were not given this low temperature anneal (LTA) in order to study the effect of high residual carbon. Powder-in-tube (PIT) tapes were prepared from the Bi-2223 precursor powders by a thermomechanical procedure described elsewhere [15].

Short samples (~ 3 cm long) were cut from the as-rolled tapes and heat treated in 8% O_2 at 820°C . The samples were annealed for 50 h, then uniaxially cold pressed at ~ 2 GPa. Following pressing, the tapes were annealed for an additional 100 h at 820°C . The process of annealing and pressing was repeated until cumulative heat-treatment times of 250 h had been reached. The fully-processed samples typically were 100 to 120 μm thick. Ramp rates from ambient temperature to processing

temperature and cool down to ambient temperature were 60°C/h. The J_c of each tape was measured at 77 K and zero field by the four-probe method, using the 1 $\mu\text{V}/\text{cm}$ criterion. X-ray diffraction (XRD) was performed on peeled sections of fully processed tape samples using a Philips Diffractometer. The conversion of Bi-2212 to Bi-2223 was computed on the basis of x-ray intensity ratios of the (0010)₂₂₂₃ and (008)₂₂₁₂ diffraction lines. Scanning electron microscopy (SEM) and energy dispersive x-ray (EDX) analysis were done with a JEOL 6400 SEM unit coupled to a Noran EDX unit. Texture analysis was carried out on scanned SEM images using Agfa Arcus II scanner along with Adobe Photoshop and NIH Image software [16].

Results and Discussion

Compositions and Conversion Kinetics

Table I shows the compositions of the six precursor powders as determined by inductively coupled plasma/atomic emission spectroscopy (ICP/AES). The lead content in all the powders is very close to the desired stoichiometry. Copper exhibits the greatest deviation from the desired value but the maximum deviation is less than 3 percent. Figure 1 shows a bar plot of percent conversion to Bi-2223 versus lead content, x , for the eight tapes used in this study. These tapes were processed for 250 h in 8% O₂ at 820°C. From the plot it is clear that the LTA tapes with lead contents in the range 0.3 to 0.4 are nearly 100% Bi-2223. Tapes with lower lead content (0.2 and 0.25) show incomplete conversion to Bi-2223, presumably due to inadequate liquid phase formation because of lead deficiency. Compositions that have the highest lead content (0.5) or high carbon contents (no LTA), also show incomplete conversion. This may be due to accelerated secondary phase growth in these samples during the early stages of conversion.

Microstructure and Texture Studies

Figure 2 presents SEM micrographs of longitudinal sections (after etching) of the LTA tapes with lead contents $x=0.2$, 0.3, 0.4 and 0.5. It can be seen from the micrographs that the sample with $x=0.2$ has very poor texture, small grains and no platy structure. This is consistent with the fact that the $x=0.2$ tape is expected to have the least amount of liquid phase formed due to lead deficiency. In the microstructure for $x=0.3$, the Bi-2223 layered phase has large grains with good texture. The microstructures with $x=0.4$ and 0.5, has disrupted grains with a platy

Table I. Stoichiometric compositions of Bi-2223 precursor powders determined by ICP-AES.

Sample No.	Bi	Pb	Sr	Ca	Cu
1	1.82	0.20	1.98	1.95	3.05
2	1.81	0.25	1.97	1.97	3.06
3	1.80	0.29	1.96	1.98	3.07
4	1.80	0.35	1.98	1.98	3.07
5	1.77	0.39	1.98	1.97	3.09
6	1.79	0.49	1.97	1.96	3.09

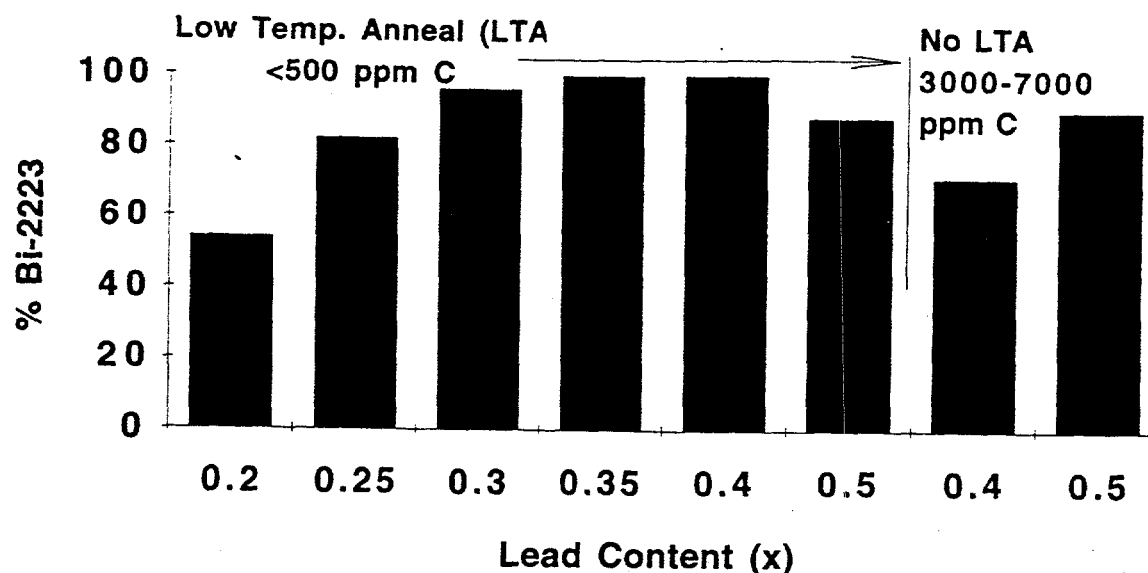


Figure 1. Effect of lead content and low temperature anneal on conversion kinetics in Ag-clad Bi-2223 composite conductors.

appearance.

Figure 3 depicts the average grain orientation (with respect to the silver interface) in various tapes versus lead content. The average grain orientation was obtained by using image analysis software on scanned SEM micrographs of longitudinal sections of samples, such as those in Figure 2. It can be seen that layered phase grains in the composite with $x=0.3$ have the lowest average angle with respect to the silver interface. This tape thus exhibits the best Bi-2223 grain texture. The orientation of the layered phase grain improves from $x=0.2$ to $x=0.3$ but does not change significantly for the LTA samples with $x>0.3$. The samples with $x=0.4$ and $x=0.5$ that did not receive the LTA show poorer texture than their counterparts that did receive the LTA.

Figure 4 shows SEM micrographs taken in the backscatter mode on transverse sections of the fully processed tapes with the higher lead contents (0.4 and 0.5) that were not subjected to LTA and, consequently, had carbon contents in the 3000 to 7000 ppm range. It can be seen that the sample with $x=0.4$ contains large secondary phases, mostly of the $(\text{Ca,Sr})_{14}\text{Cu}_{24}\text{O}_{41}$ type. The sample with $x=0.5$ shows a large number of Sr-rich phases (black) apart from the white streaky phases that are the lead-rich phases (3221 and plumbates). It is our belief that the Sr-rich regions are created during heat treatment of the high-carbon composites, initially as SrCO_3 that eventually decomposes to SrO agglomerates, which persist throughout the processing but eventually become carbonates again when the core is exposed to air during specimen mounting. The presence of (Bi/Pb)-rich and Sr-

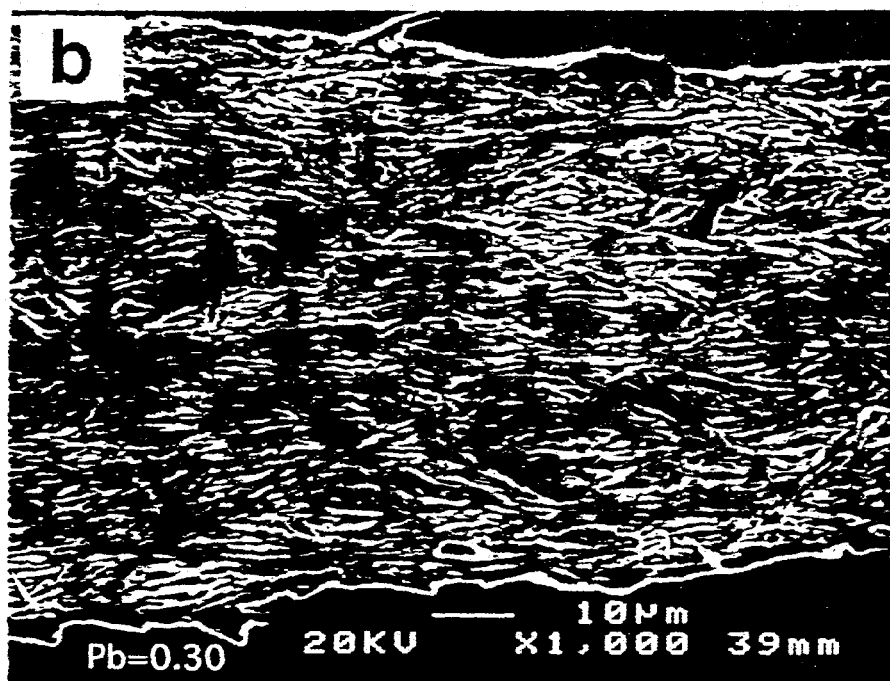
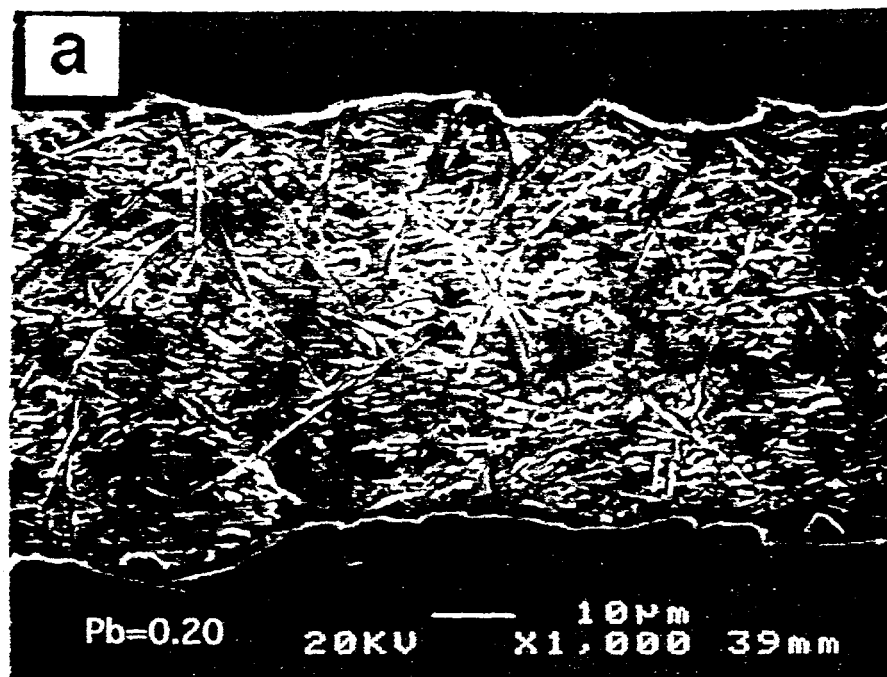


Figure 2. SEM images of longitudinal sections of fully processed tapes after etching: the lead contents were (a) Pb = 0.2, (b) Pb = 0.3, (c) Pb = 0.4, and (d) Pb = 0.5. (The powder in each of these tapes received the low temperature anneal.)

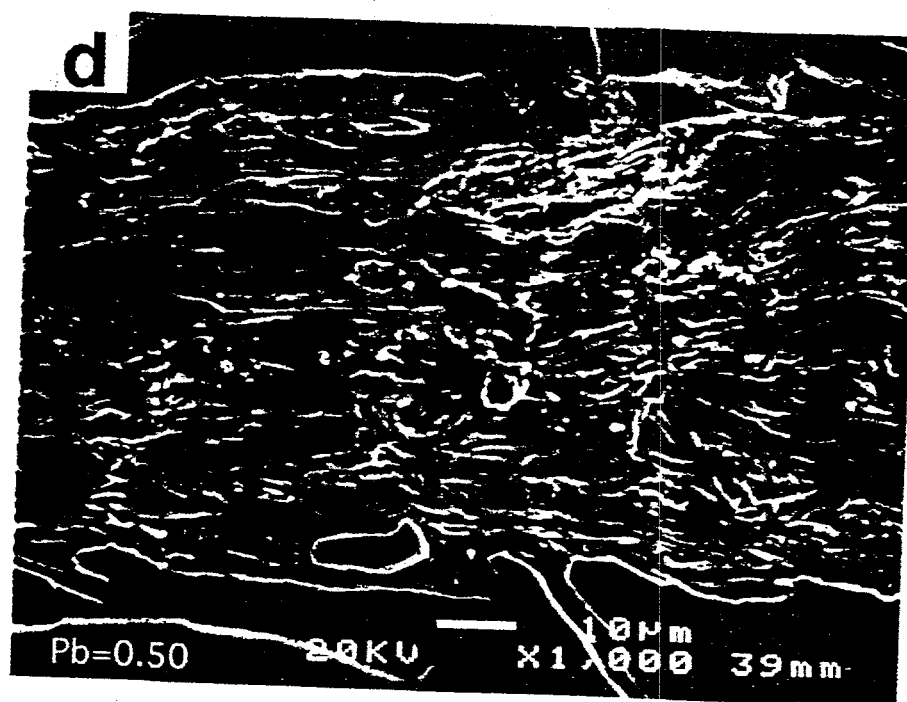
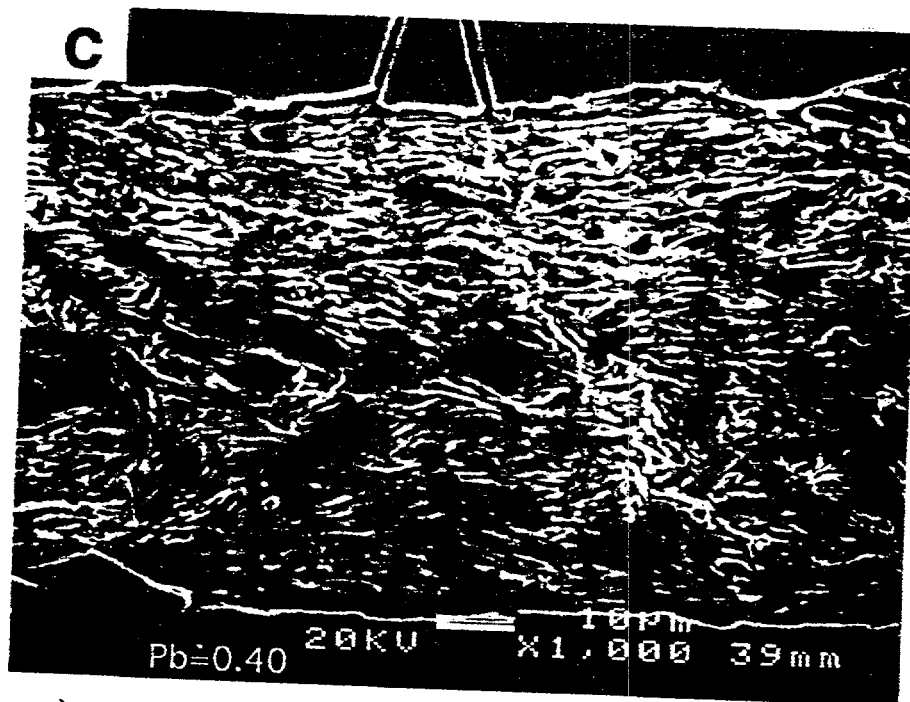


Figure 2 (Continued)

rich phases has been independently confirmed by Luo et al. [17] using Raman microspectroscopy. SEM studies on samples with lead content 0.2 and 0.25 revealed presence of many secondary phases that were mostly $(\text{Ca,Sr})_2\text{CuO}_3$ and $(\text{Ca,Sr})_{14}\text{Cu}_{24}\text{O}_{41}$ type. The extent of conversion to Bi-2223 in these samples was only 60-80%. The appearance of Bi/Pb-rich phases for $x > 0.3$ and the increase in their concentration with Pb content indicate that the solubility limit for lead in Bi-2223 lies between $x = 0.2$ and $x = 0.5$. This limit probably is in the vicinity of $x = 0.3$, judging from the minimal secondary phase content in samples with this lead content.

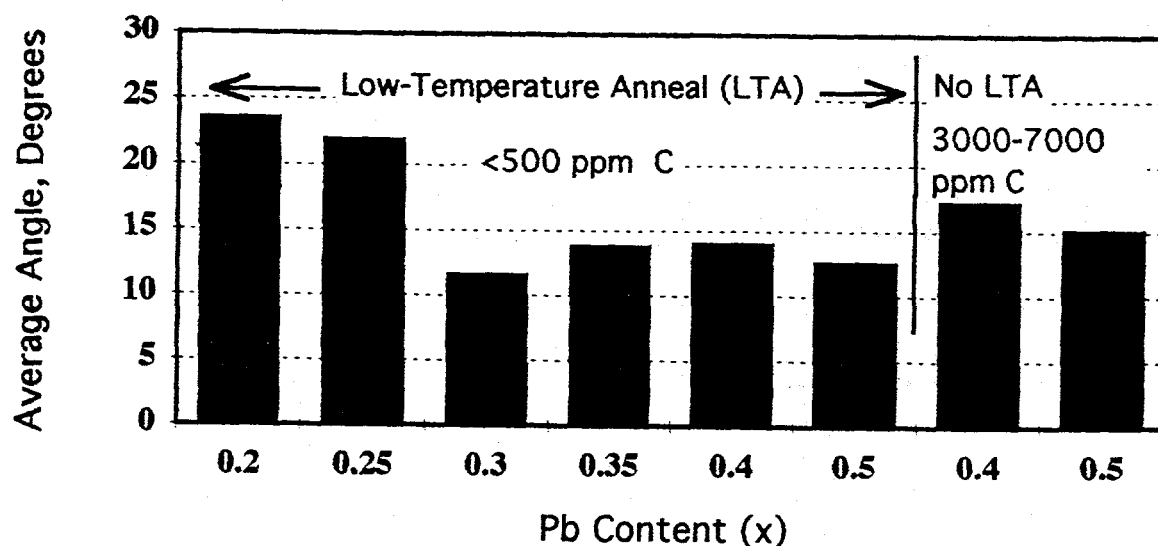


Figure 3. Plot of average layered-phase grain orientation with respect to the silver interface versus lead content.

Superconducting Properties

Figure 5 presents a plot of critical current (I_c) versus lead content for the fully processed tapes after 50, 100, and 250 h of anneal in 8% O_2 at 820°C . The I_c data are in good agreement with the SEM studies and the texture analysis. The I_c increases

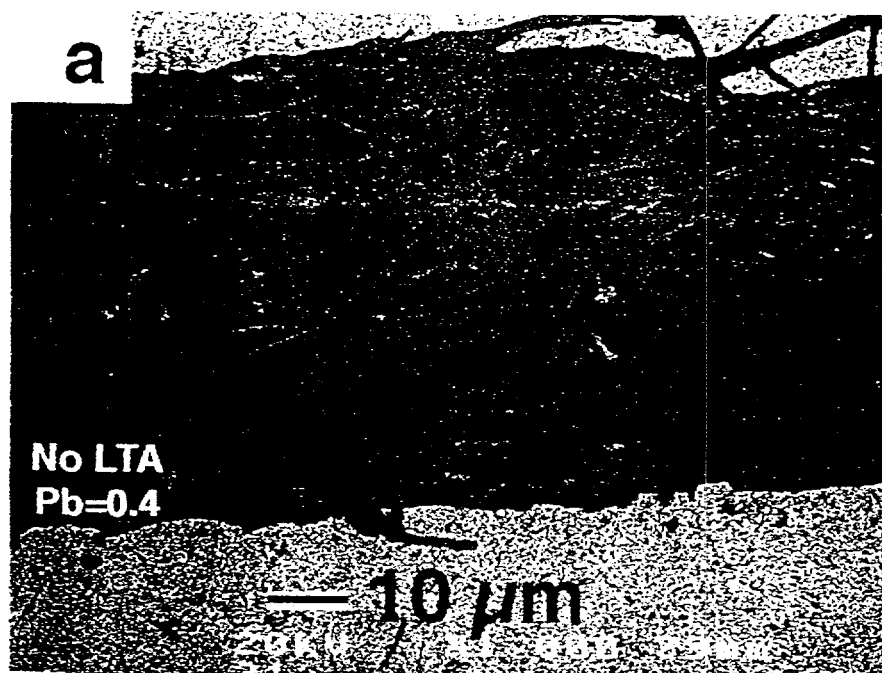


Figure 4. SEM images (in backscatter mode) of transverse sections of tapes with (a) Pb = 0.4 and (b) Pb = 0.5 that were not subjected to low temperature anneal.

significantly from $x=0.2$ to $x=0.3$ and then drops down with further lead increase from 0.3 to 0.5. The I_c values of the two tapes prepared with powders that did not receive the LTA were significantly lower than those that had the LTA. This is again consistent with microstructural studies of the same sample. The lead-rich phases tend to coat the superconducting grain boundaries and presumably have a deleterious effect on the current flow.

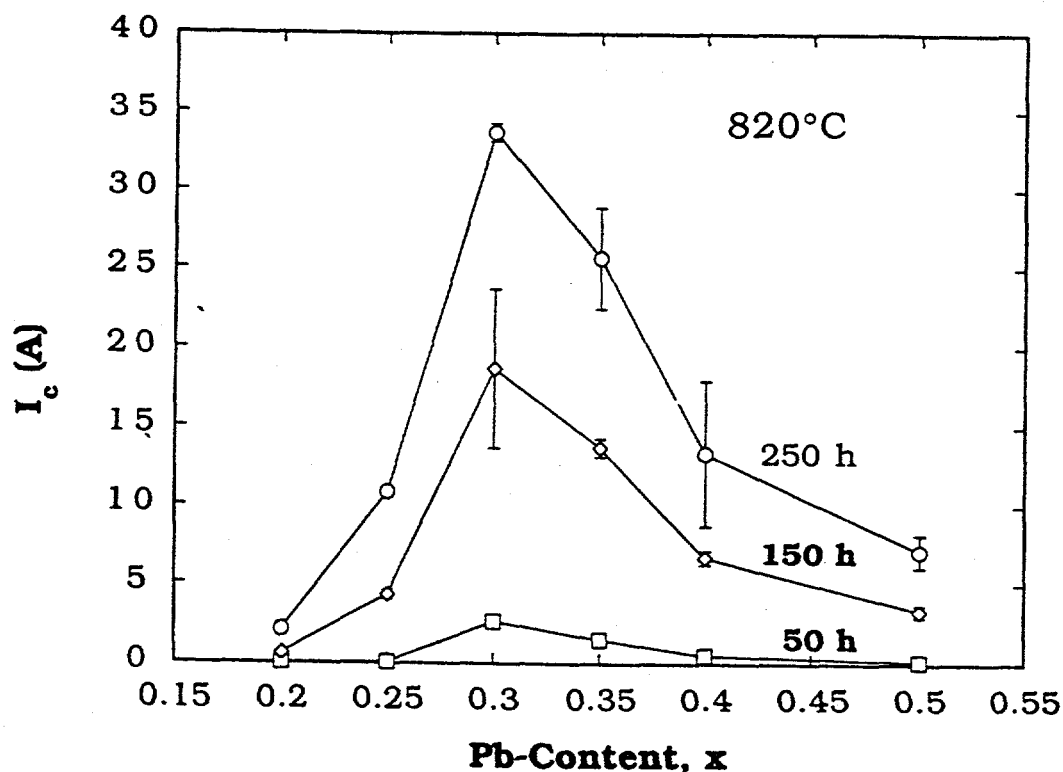


Figure 5. Plot of critical current I_c at 77 K and zero field versus lead content.

Conclusion

In summation, we find that as the lead content x in $\text{Bi}_{1.8}\text{Pb}_x\text{Sr}_{2.0}\text{Ca}_{2.0}\text{Cu}_{3.1}\text{O}_y$ increases from 0.2 to 0.3, (1) layered-phase grain size increases, (2) layered-phase texture improves, and (3) transport I_c increases. As the lead content x is further increased from 0.3 to 0.5, (1) secondary-phase particle size and quantity increase, (2) platy-growth frequency and depth increase, (3) the amount of detectable lead-rich phase increases, and (4) transport I_c decreases. Reducing the carbon content from >3000 ppm to <500 ppm (e.g., by use of the low temperature anneal) (1) reduces the occurrence of Sr-rich phases, (2) reduces the size and quantity of secondary phases, and (3) leads to measurable improvement in texturing and I_c .

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