

CHARACTERISTICS OF MULTIWIRE PROPORTIONAL COUNTERS WITH  
DELAY LINE READOUT FOR MINIMUM IONIZING PARTICLES

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ABSTRACT

We have investigated the effect of gas mixture and chamber thickness on the gain and pulse shape of a multiwire proportional counter with delay line readout. We were primarily concerned with optimizing the position accuracy for high-energy particle physics applications. Our best results, both from the point of view of chamber gain and the risetime and uniformity of the delay line pulses were obtained with a 4 mm gap chamber run on a mixture of 30% carbon dioxide and 70% Argon. We have found it necessary to bias the outer grids negative with respect to ground to prevent electrons in the drift regions from migrating into the multiplication region and spoiling the delay-line pulse shape.

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## I. Introduction

We present here some measurements on the gain of the chamber and the shape of the delay line pulses that are relevant to particle physics applications in which an energetic, charged particle traverses the chamber with small energy loss; the shape and amplitude of the proportional signal vary substantially from event to event, and the chamber parameters must be optimized carefully to maintain the spatial resolution. This is a more difficult case than other applications in which low energy gamma rays convert in the chamber producing a small region of ionization and uniform, easily localizable pulses.<sup>1</sup>

We have studied chamber performance as a function of three parameters: (1) voltage gradient, (2) gas mixture, and (3) gap spacing. In addition, we have experimented with "drift regions" located between the outer grids and the grounded aluminum windows, which constitute the gas envelope of the chamber. Our criteria for satisfactory chamber performance are (1) the signal from the chamber should be as large as possible to overwhelm the noise inherent in the input stage of the delay line amplifiers.<sup>2</sup> (2) The gain should be stable without leakage, breakdown, or "regenerative feedback" leading to uncontrolled amplification of the signals. (3) The delay line signals should be fast, narrow, symmetric, and vary in shape as little as possible from pulse to pulse.

Each of these items is discussed in turn in Section III.

## II. Chamber Description.

These tests were made with two different multiwire proportional counters, which are essentially identical except for the gap spacing,

9.5 mm between anode and cathode in the thick chamber and 4.1 mm in the thin chamber. The construction is shown schematically in fig. 1. The chambers are double gapped with the central plane at positive high voltage and the two outside grids near ground potential. A "prompt" signal is extracted from the anode, and the delay lines are coupled to the two cathode planes, which give an X and Y readout. The mechanical parameters of the chambers are summarized in Table I. The construction of the delay lines is described in references 3 and 4.

Table I - Chamber Construction

Plane Spacing	9.5 mm or 4.1 mm
Central Plane	20 $\mu$ stainless wound 5/cm.
Ground Plane	80 $\mu$ stainless wound 10/cm.
Chamber Area	50 $\times$ 25 $\text{cm}^2$
Windows	0.5 mil mylar, 0.5 mil aluminum
Delay Lines	40 cm and 60 cm long impedance 1.3 K ohms 6.5 nSec/mm propagation time
Spacing between ground planes and windows	8 mm

These chambers were designed for a series of cyclotron and Bevatron experiments involving high energy protons and alpha particles. They were the final elements of a magnet spectrometer system, consequently spatial resolution was at a premium. No attempt was made, however, to use  $dE/dx$  or pulse height information from the chambers, and the start time signal

was obtained from a system of scintillators and fast logic. Hence we are not concerned with the properties of the signal from the central plane but only from the delay lines. It is often convenient to use the central plane signal to start the digitizing electronics, but no loss of positioning accuracy is involved in using a start time signal generated independently of the chamber so long as the pulses from both ends of the delay lines are digitized and the position obtained by subtracting the two delays.<sup>2</sup>

### III. Results

The gain of the chambers was measured as a function of voltage by observing the pulse height on the central plane due to 22 keV gamma rays from Cd<sup>109</sup> converting in the chamber. A scope picture of these pulses is shown in fig. 2. The gain curves are plotted for four different gas mixtures in fig. 3. These graphs were made with the thin chamber. Comparable curves could be made with the thick chamber but poor chamber insulation and excessive leakage prevented us from extending the voltage over 5800 volts.

The four gain curves in fig. 3 extend from the voltage at which the signal was just large enough to distinguish clearly from the amplifier noise to what we regard as the maximum usable gain. It is an important point that this limitation on the maximum gain comes about differently for different gas mixtures:

- a) 7% CH<sub>4</sub>, 93% Ar. Above 2600 volts the pulse begins to widen and develop subsidiary peaks. As the voltage is increased an orderly succession of "saw-teeth" spread out from the initial pulse.

- b) 30%  $\text{CH}_4$ , 70% Ar. At maximum gain the chamber begins to spark. Even with a 22  $\text{M}\Omega$  protection resistor in series with the high voltage one can hear distinct sparks as the chamber capacitance is discharged.
- c) 7%  $\text{CO}_2$ , 93% Ar. The gain is limited by a regenerative feedback mechanism, which causes the pulses to grow erratically in amplitude and length. At slightly higher voltage the discharges become self sustaining.
- d) 30%  $\text{CO}_2$ , 70% Ar. As the gain is increased the chamber loses pulse height resolution and the well-defined band of pulses from gamma conversion disappears entirely.

An important advantage of the  $\text{CO}_2$  mixtures is that the discharges in the chamber are self limiting; i.e., they draw sufficient current through the protection resistor to reduce the chamber voltage and thus prevent sparks. We have no evidence that the sparks that occur in methane mixtures do any real damage, but in the case of larger chambers with more capacity or accidental overvoltage the sparks could easily damage the thin central wires.

Of the gas mixtures tested the 30%  $\text{CO}_2$  clearly provides the highest gain for both the thin and thick chambers. Gain curves for a number of intermediate  $\text{CO}_2$  concentrations and similar chambers are presented in ref. 5. These curves suggest that the optimum concentration of  $\text{CO}_2$  is at least 25% for 4 mm gap spacing and about 20% for 8 mm spacing, i.e. the thinner the gap the more  $\text{CO}_2$  needed to achieve optimum gain. The maximum attainable gain remains roughly constant as the  $\text{CO}_2$  concentration is increased but the voltage necessary to reach it continues to rise.

One eventually exceeds the limitations of the chamber insulation. For example, we were unable to run our thick chamber over 5.8 kV because of excessive leakage, but at this voltage the 30%  $\text{CO}_2$  gain curve had not reached its maximum.

In addition to the gain, the pulse shape from the delay lines is extremely important in maintaining adequate resolution. The pulse width, after all, is at least 200 ns or about 4 cm in spatial extent. So to match the spatial resolution inherent in the chamber, the discriminator must find the center of the delay line pulse accurately to within a few percent of the pulse width. To mitigate this task we try to optimize the chamber to produce pulses that are as narrow and symmetric as possible.

The pulse shape measurements reported here were all made with a cosmic ray counter telescope, which insured that a minimum ionizing particle traversed the chamber within a small area ( $\sim 5 \times 5 \text{ cm}^2$ ) and within a small cone of angles ( $\sim \pm 20^\circ$ ) to the perpendicular.

One mechanism that seriously deteriorates pulse shape is the diffusion of electrons from outside the gap, through the cathode grids and into the multiplication region. Even (especially) when there is no potential difference between the grounded aluminum windows and the cathode many electrons produced in this "drift region" find their way into the central gap. This process is slow enough that the latecomers spoil the trailing edge of the delay line pulse producing multiple peaks. We have been able to eliminate this effect by biasing the outer planes negative with respect to the grounded windows, 300 volts in the

case of the thin chamber and 600 volts for the thick chamber. We had originally intended to collect the electrons from these drift regions by biasing the cathode grids positive with respect to ground, thus accelerating the electrons into the multiplication region and increasing the effective thickness of the chamber. Even with very large biasing voltage, however, the pulses produced in this way were unacceptably broad and irregular. The situation is quite different when low energy gamma rays convert in the drift region. Because the recoil photo-electrons have such a short range in the gas the ionization electrons drift "in step" with each other into the multiplication region and produce a standard pulse shape. Thus the drift regions, which seem useless for high-energy work, are very practical in x-ray imaging applications.

Another parameter that affects the delay line pulse shape is the thickness of the central gaps. Quite reasonably, the thicker the gap the broader the pulse, not only because of the increased electron collection time but also because of the spreading of the field lines going from anode to the cathode. We observe about 30% to 50% increase in pulse width depending on gas mixture between the thick and thin chambers. This increase comes about without appreciable deterioration of rise time, rather the pulses become broader and flatter on top. These trapezoid-like pulses are especially undesirable for use with zero-cross discriminators because the cross-over point of the differentiated pulse is not very well defined.<sup>6</sup> For this reason we have tried to keep the pulses as short and triangular as possible, and from this

point of view the thinner chamber is definitely preferable.

Finally we have investigated the effect of gas mixture on the chamber pulses. From our measurements we can make the following observations:

1. Both the amplitude and the shape of the pulses vary substantially from event to event. The amplitude fluctuations have a full width at half maximum of about 50% and are consistent with the expected Landau fluctuations in  $dE/dx$  in the chamber gas.

The variations in pulse shape affect the risetime and the pulse width. They are presumably due to statistical fluctuations in ionization density along the track and are exacerbated by the differentiation in the chamber-delay line coupling. These fluctuations contribute to the error in pulse timing. They can be minimized by optimum choice of chamber thickness and gas mixture.

2. To some extent the rise time of the delay line pulses is determined by the characteristics of the delay line. But there is still a substantial difference both in risetime and the spread in the fluctuations of the risetime between the worst gas mixture (7%  $CH_4$ ) and the best (30%  $CO_2$ ). These results are summarized in the next table.

Table II. Risetimes of Delay Line Pulses with Various Gas Mixtures

	7%	30%
$CH_4$	$r = 130$ ns	$r = 110$ ns
	$\sigma = 80$ ns	$\sigma = 30$ ns
$CO_2$	$r = 100$ ns	$r = 90$ ns
	$\sigma = 25$ ns	$\sigma = 15$ ns

The risetimes in this table were obtained by observing a series of scope photographs. The  $\sigma$ 's represent the spread between the longest and shortest risetimes observed. The numbers obtained in this way are of course very rough, but they do accurately reflect the significant improvement in the quality of the pulses one obtains with the 30%  $\text{CO}_2$  mixture. (See fig. 4).

3. The risetimes of the signals on the central plane are more indicative of the collection times in the chamber gas because there is no differentiation. These risetimes are given in the next table.

Table III. Risetimes on the Central Plane for Various Gas Mixtures.

	7%	30%
$\text{CH}_4$	180 ns	140 ns
$\text{CO}_2$	125 ns	100 ns

No  $\sigma$  is given because the fluctuations of these signals are substantially less than those on the delay lines. The risetimes of the central plane and delay lines are qualitatively consistent if one takes into account the differentiation characteristics of the delay lines.

4. The total width of the delay lines pulses is strongly dependent on gas mixture. Values for the full width at half maximum are tabulated below along with the spread in this number.

Table IV. Delay Line Pulse Width

	7%	30%
$\text{CH}_4$	260 ns	215 ns
	$\sigma = 80$ ns	$\sigma = 30$ ns
$\text{CO}_2$	220 ns	180 ns
	$\sigma = 60$ ns	$\sigma = 10$ ns

As in all other respects the 30%  $\text{CO}_2$  mixture is clearly superior.

The pulses are almost symmetric with rise time equal to fall time and the timing jitter is minimal. (See fig. 4).

5. The results on pulse shapes are qualitative similar for the thicker chamber if the pulse widths and the  $\sigma$ 's are scaled up by roughly 50%. The import point is that even with the reduced Landau fluctuations in the thick chamber, the timing jitter (discounting possible slewing effects in the discriminators) is less with the thin chamber.

#### Summary

We have investigated the effect of gas mixture and chamber thickness on the gain and pulse shape of a multiwire proportional counter with delay line readout. We were primarily concerned with optimizing the position accuracy for high-energy particle physics applications. Our results can be summarized as follows:

1. Of the two chambers tested, one with a 4.1 mm and the other with a 9.5 mm gap, the thinner chamber produced superior delay line

signals with narrower pulses and less jitter in rise time and pulse width.

2. Four gas mixtures were tried, 7% and 30%  $\text{CO}_2$  or  $\text{CH}_4$  in Argon. The 30%  $\text{CO}_2$  mixture was the best in all respects yielding higher maximum gain and faster pulses with less jitter. It has the additional advantages of being non-flammable and of limiting the electron avalanches in such a way as to prevent sparking in the chamber.

3. The outer chamber grids had to be biased so that free electrons in the drift regions between the cathode and the grounded chamber windows could not be drawn into the multiplication region. Our attempt to increase the effective thickness of the chamber by accelerating electrons from the drift region into the central gap was unsuccessful because of the unacceptably broad and irregular pulses produced.

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Notes and References

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4. R. Grove, I. Ko, B. Leskovar, V. Perez-Mendez, "Phase Compensated Delay Lines for Wire Chamber Readout". Nuclear Instruments and Methods 99, p. 381 (1972).
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6. Discriminators that find the centroid of a pulse by integrating over the area and dividing by two would be quite useful for such pulses.

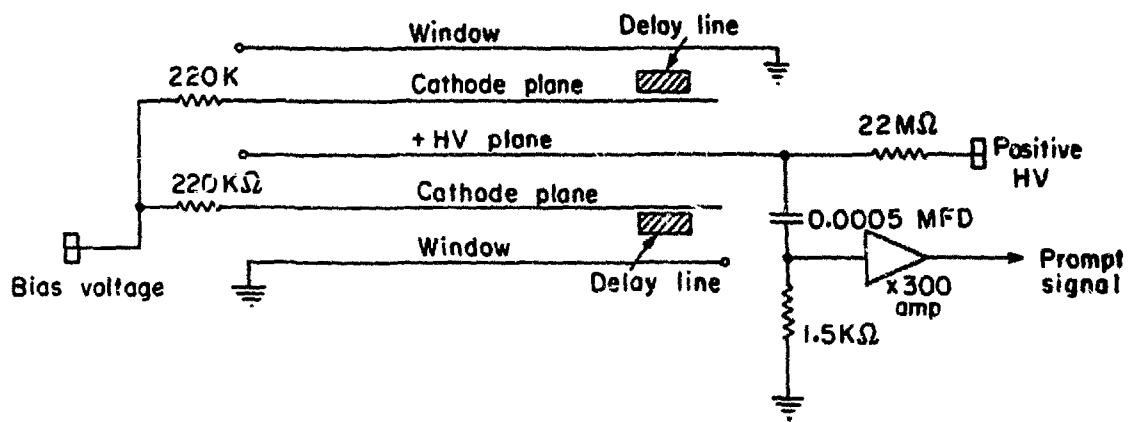
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Fig. 1. Schematic drawing of chamber construction and electronics.

Fig. 2. Oscilloscope picture of pulses observed on the central plane due to gamma rays from  $\text{Cd}^{109}$  converting in the chamber.

Fig. 3. Amplitude of the central plane signals as a function of chamber voltage. The left-hand scale gives the amplitude as observed at the output of a X300 amplifier. The right-hand scale gives the gain (electron multiplication) as inferred from the chamber capacitance.

Fig. 4. a) Delay line pulses with the 7%  $\text{CH}_4$  gas mixture.  
b) Delay line pulses with the 30%  $\text{CO}_2$  gas mixture. The horizontal scale is 50 nSec/cm and the vertical scale is 100 mV/cm.



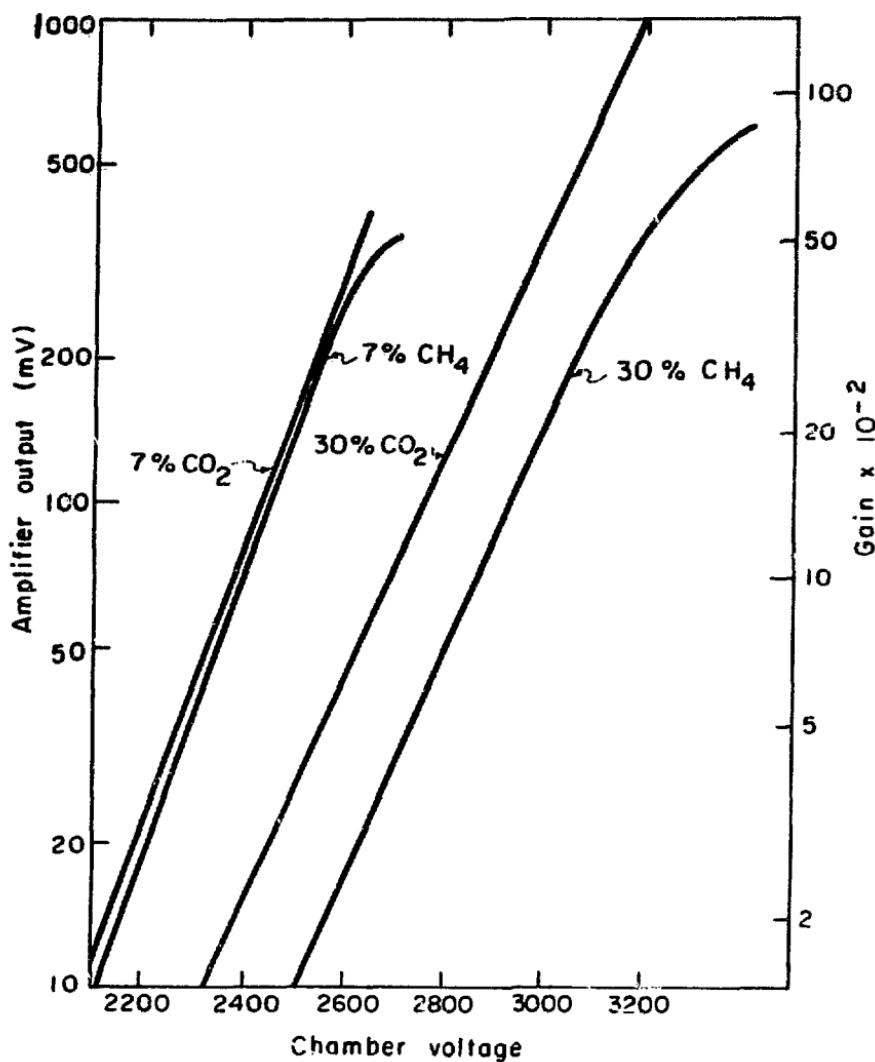
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Fig. 1



XBB 737-4163

Fig. 2



XBL 737 - 3570

Fig. 3



Fig. 4a



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Fig. 4b