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Bulk and Mechanical Properties of the Paintbrush Tuff Recovered from Boreholes UE25 NRG-4 and -5: Data Report

P. J. Boyd, R. H. Price, J. S. Noel, R. J. Martin

Prepared by
Sandia National Laboratories
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**BULK AND MECHANICAL PROPERTIES OF THE PAINTBRUSH TUFF
RECOVERED FROM BOREHOLES UE25 NRG-4 AND -5:
DATA REPORT**

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ABSTRACT

Experimental results are presented for bulk and mechanical properties measurements on specimens of the Paintbrush tuff recovered from boreholes UE25 NRG-4 and -5, at Yucca Mountain, Nevada. Measurements have been performed on three thermal/mechanical units, PTn, TSw1, and TSw2. On each specimen the following bulk properties have been reported: dry bulk density, saturated bulk density, average grain density, and porosity. Unconfined compression to failure, confined compression to failure, and indirect tensile strength tests were performed on selected specimens recovered from the boreholes. In addition, compressional and shear wave velocities were measured on specimens designated for unconfined compression and confined compression experiments. Measurements were conducted at room temperature on nominally water-saturated specimens. The nominal strain rate for the fracture experiments was 10^5 s^{-1} .

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This report was prepared for the Yucca Mountain Site Characterization Project. The scientific investigation discussed in this report is covered under the description of work for WBS number 1.2.3.2.7.1.3, QA Grading Report # 1.2.3.2.7.1.3, Revision 00. The planning documents that guided this work activity are site characterization Plan Section 8.3.1.15.1.3; Study Plan SP-8.3.1.15.1.3, Revision 0; and Work Agreement WA-0090. The information and data documented in this report were collected under a fully qualified QA Program and may be used in the licensing process.

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1.0 INTRODUCTION

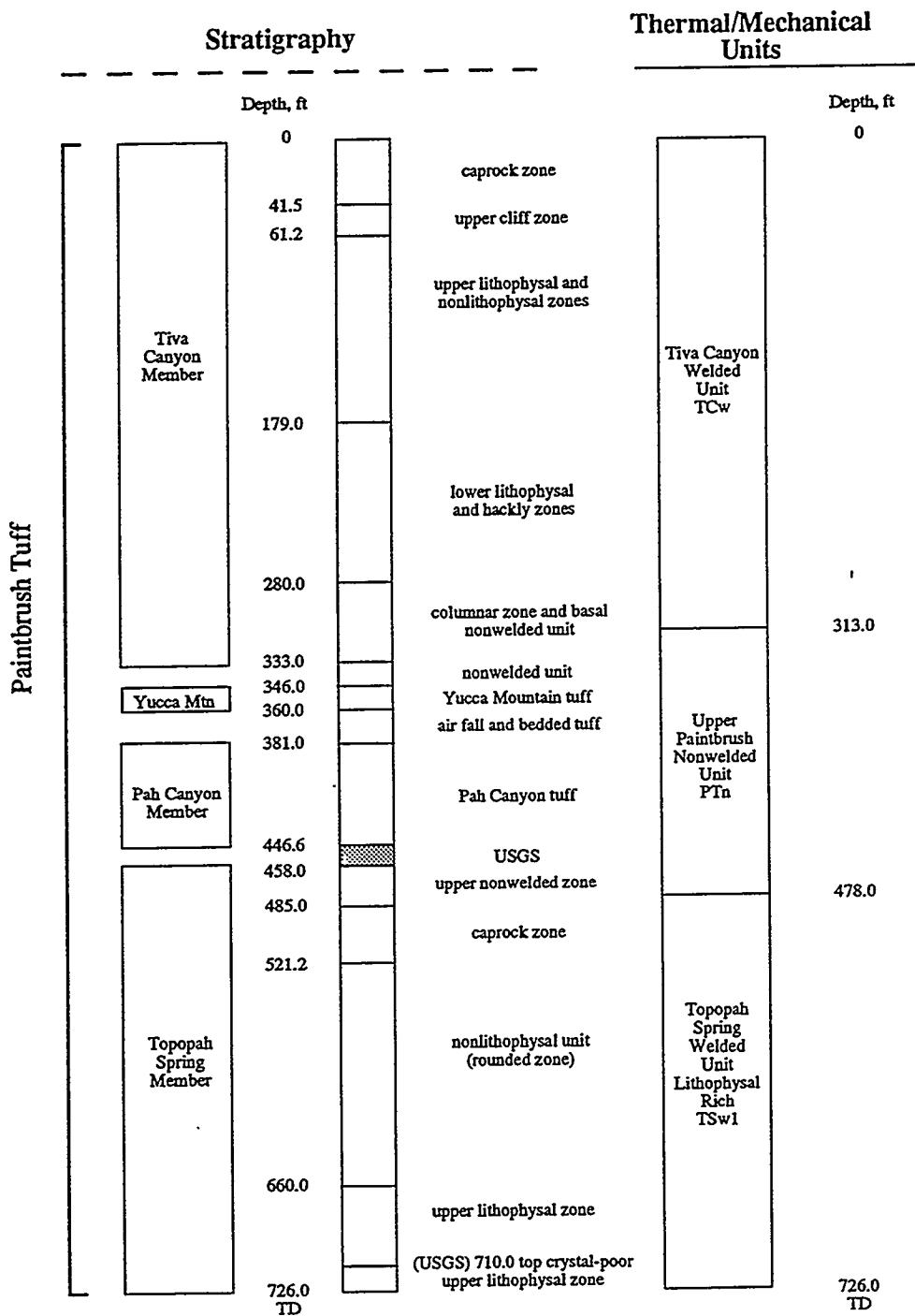
An integral part of the licensing procedure for the potential nuclear waste repository at Yucca Mountain, Nevada, involves characterization of the *in situ* rheology for the design and construction of the facility and the emplacement of canisters containing radioactive waste. The data used to model the thermal and mechanical behavior of the repository and surrounding lithologies include dry and saturated bulk densities, average grain density, porosity, compressional and shear wave velocities, elastic moduli, and compressional and tensional fracture strengths. In this study, a suite of experiments was performed on cores recovered from boreholes UE25 NRG-4 and -5 drilled in support of the Exploratory Studies Facility (ESF) at Yucca Mountain. The holes penetrated as many as four thermal/mechanical units of the Paintbrush tuff. The thermal/mechanical stratigraphy was defined by Ortiz et al. (1985) to group rock horizons of similar properties for the purpose of simplifying modeling efforts. The relationship between the geologic stratigraphy and the thermal/mechanical stratigraphy for each borehole is presented in Figures 1 and 2. The tuff samples studied have a wide range of welding characteristics (usually reflected in sample porosity), and a smaller range of mineralogic and petrologic characteristics. Generally, the samples are silicic, ash-fall tuffs that exhibit large variability in their elastic and strength properties (see Price and Bauer, 1985).

Sixty-eight cores from UE25 NRG-4 and -5 were sent to New England Research, Inc., for bulk and baseline mechanical property measurements. A breakdown of the samples according to tests performed is given below:

Type of Test	Number of Samples Tested
Average Grain Density	68
Unconfined Compression	36
Confined Compression	7
Indirect Tensile Strength	35

On twenty-three cores there was insufficient material, or the material was of such poor quality that mechanical tests could not be performed. On these cores, only the average grain density and porosity were determined.

UE25 NRG-4 Stratigraphic and Thermal/Mechanical Units Summary

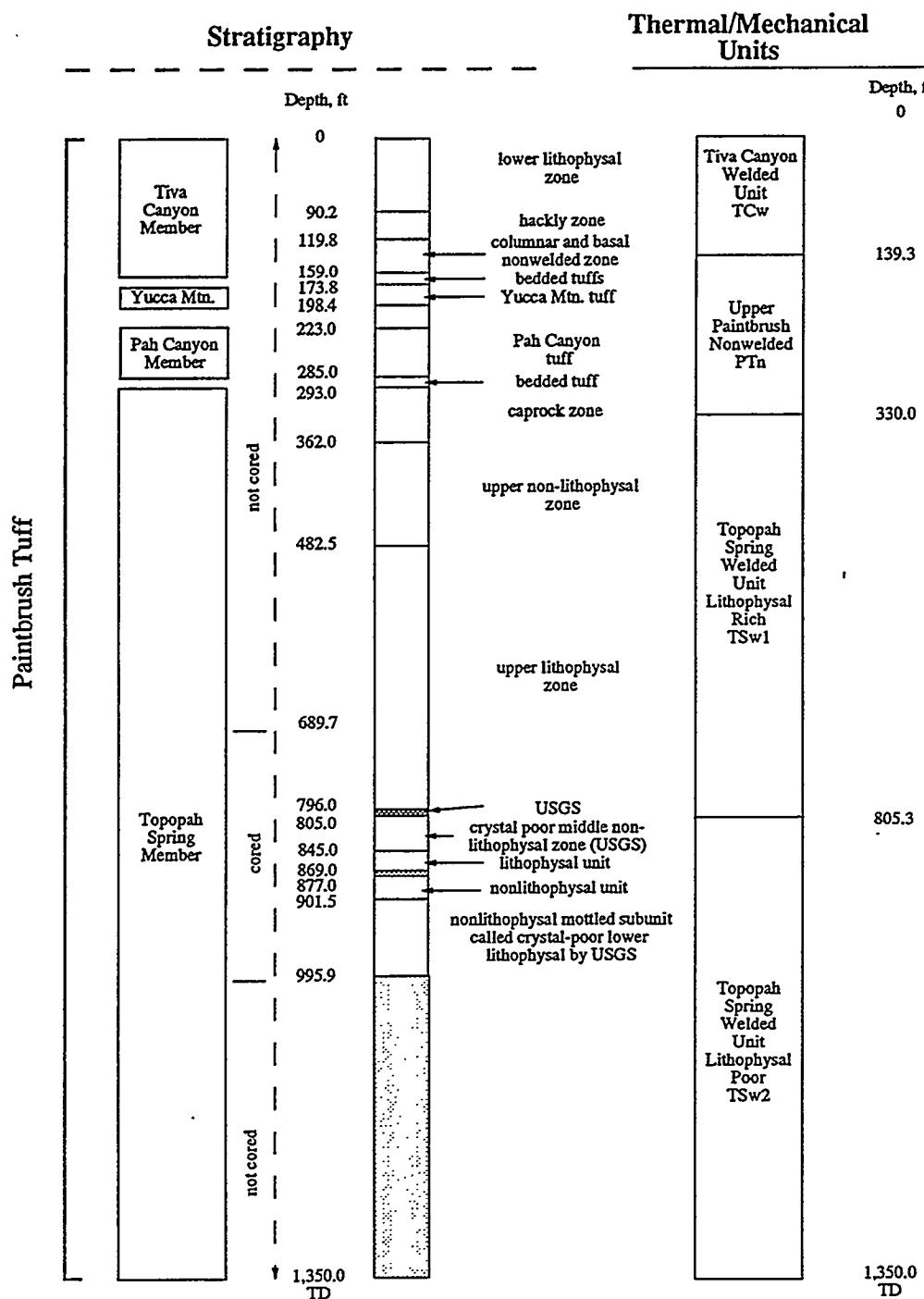


 Unresolved contact, criteria being developed by the USGS.

Note: Stratigraphy between 0 and 375 feet based on drilling cuttings.

Figure 1: The correlation between the stratigraphic and thermal/mechanical units for borehole UE25 NRG-4 at Yucca Mountain, Nevada (per preliminary stratigraphy by J.F.T. Agapito and Associates, Inc., 11/10/93).

UE25 NRG-5
Stratigraphic and Thermal/Mechanical Units Summary



 Unresolved contact, criteria being developed by the USGS.

Stratigraphy between 0 and 689.7 feet based on examination of drill cuttings

Figure 2: The correlation between the stratigraphic and thermal/mechanical units for borehole UE25 NRG-5 at Yucca Mountain, Nevada (per preliminary stratigraphy by J.F.T. Agapito and Associates, Inc., 11/15/93).

2.0 EXPERIMENTAL PROCEDURE

Measurements were performed on 68 specimens prepared from core recovered from boreholes UE25 NRG-4 and -5. When the core was received, it was examined to determine the best utilization of the rock material to obtain the maximum mechanical data. The size of the specimen for each type of measurement was a major part of the selection criteria. The nominal dimensions of the cylindrical rock specimens for each of the mechanical tests are given below:

Test	Length (mm)	Diameter (mm)
Indirect Tensile Strength	38.1	50.8
Unconfined Compression	101.6	50.8
Confined Compression	50.8	25.4

The length and diameter have a tolerance of ± 0.125 mm. The ends of the cylinders were parallel to within 0.025 mm.

Dry and saturated bulk densities were measured on each of the specimens prepared for unconfined compression, confined compression, and indirect tensile strength tests. Average grain density was determined with the water pycnometry technique using pieces remaining from the subcoring attendant to the preparation of the test specimens.

2.1 Sample Preparation

All specimens prepared for unconfined compression, confined compression, and indirect tensile strength testing were ground, right circular cylinders with dimensions listed above. The dimensions of the specimens were checked and verified according to the Sandia National Laboratories (SNL) Technical Procedure (TP) 51 entitled "Preparing Cylindrical Samples, Including Inspection of Dimensional and Shape Tolerances."

In some cases, more than one specimen was obtained from a core. This was particularly true for the confined compression tests. This approach was adopted on a limited basis for several reasons. The tuff is very heterogeneous. Testing a limited number of specimens at confining pressures of 5 or 10 MPa may not reflect the singular effect of pressure on fracture strength and elastic constants. The determination of the influence of

pressure is further complicated by limited sample availability. Standard test methods suggest that measurements should be carried out on specimens greater than 47 mm in diameter, but they allow for smaller specimens, as long as the decision is documented. If the latter approach is adopted, the influence of the smaller specimen volume must be incorporated into the engineering analysis of the data. By preparing a statistically significant number of 25.4 mm diameter specimens from raw core, the effect of pressure can be more clearly distinguished without the complicating effects of variable porosity and pore geometry. A core of the TSw1 thermal/mechanical unit, recovered from a depth of 527.0 feet from borehole UE25 NRG-4 was of sufficient quality and homogeneity to machine 9 specimens for confined compression experiments. Subdivisions of these cores were treated as new specimens and a Chain-of-Custody form was prepared for each piece of material generated in the subdivision process (per SNL QAIP 20-03, "Sample Control"). The prepared specimens were labeled and stored in containers until the measurement sequence was initiated.

The general measurement sequence for each specimen is given below:

- Dimensions measurement
- Specimen description
- CT Scan (unconfined compression specimens only)
- Drying specimen to a constant weight
- Dry bulk density measurement
- Compressional and shear wave velocities for the dry condition (all unconfined and representative confined compression specimens)
- Saturating specimen to a constant weight with water
- Saturated bulk density measurement
- Compressional and shear wave velocities for the saturated state (all unconfined and representative confined compression specimens)
- Mechanical testing (unconfined compression, confined compression, or indirect tensile strength tests)
- Description of post failure condition of the specimen
- Post-test photograph taken

Average grain density measurements were performed concurrently with the other activities.

2.2 CT Scans of Each Specimen Tested in Unconfined Compression

Prior to testing, a computerized tomography (CT) scan was performed on each specimen designated for testing in unconfined compression. Because CT scans are sensitive to variations in density, this visual representation permits an initial qualitative examination of the distribution of pores and low density zones throughout the rock specimen and provides data for more quantitative analyses, if desired. Given the presence of lithophysae and vapor-phase altered zones within the tuff, the CT scan is a particularly useful technique for evaluating the effects these features may have on the mechanical properties of the tuff at the laboratory scale.

2.3 Drying, Saturation, Bulk Density, Average Grain Density, and Porosity

The dry and saturated bulk densities, average grain density, and porosity were determined for each specimen prepared for a mechanical test. The procedures were developed in accordance with ASTM D 854 "Standard Test Method for Specific Gravity of Soils" and ASTM C 135 "Standard Test Method for True Specific Gravity of Refractory Materials by Water Immersion."

2.3.1 Procedure for Drying a Specimen

The specimen was dried to a constant weight and its dry bulk density determined. Drying was carried out at 110 ± 5 °C according to SNL TP-65, "Drying Geologic Specimens to a Constant Weight." Once the mass change for successive drying cycles had stabilized to within $\pm 0.05\%$, the dry bulk density, ρ_{db} , was computed. Previous studies have shown that drying at 110 °C produces no noticeable damage (microcracks) in welded tuff. This was demonstrated by measuring compressional and shear wave velocities before and after heating a TSw2 specimen to 110 °C. Thermal cycling produced no reduction in the velocities suggesting no thermally induced microcracking. If microcracks develop due to differential thermal expansion, the velocities will decrease.

Each specimen is dried in an oven controlled to an accuracy of ± 5 °C. The procedure for drying is outlined below.

1. Place the specimen in the oven. Increase the temperature in the oven to 110 ± 5 °C at a rate less than or equal to 2 °C min $^{-1}$.
2. Maintain the specimen at 110 ± 5 °C for 120 to 128 hours. Reduce the temperature in the oven at a rate of less than or equal to 2 °C min $^{-1}$ until the oven temperature is between ambient and 40 °C.
3. Remove the specimen from the drying oven and weigh it three times. The specimen should be weighed within 15 seconds of removal from the oven. Calculate the mean dry mass of the specimen for the three measurements.
4. Repeat steps 1 through 3.
5. Calculate the mass change of the specimen for the successive drying cycles. If the change in mass for successive drying cycles is less than or equal to 0.05%, the process has met the specification and oven drying of the specimen is terminated. If the mass change is greater than 0.05%, steps 1 through 3 must be repeated until the specification is met.
6. Compute the dry bulk density by dividing the dry mass by the specimen volume.

2.3.2 Procedure for Water Saturation

The mechanical tests were performed on nominally water-saturated specimens. Saturation of the specimens was achieved in a two-stage process. First, the specimen was pressure saturated at 10 MPa for a minimum of 1 hour. Next, a minimum of two vacuum saturation cycles were performed, according to SNL TP-64, “Procedure for Vacuum Saturation of Geologic Core Samples.” Once the mass change for successive saturation cycles had stabilized to within $\pm 0.05\%$, the saturated bulk density, ρ_{Sb} , was computed. The specimens were stored in distilled water following saturation and prior to testing.

A brief synopsis of the procedure for saturation follows:

1. Place the specimen in a pressure vessel filled with distilled water.

2. Pressurize the vessel to 10 MPa and hold constant for at least one hour.
3. Remove the specimen from the pressure vessel, blot it with a damp lint free paper towel.
4. Weigh the specimen within 15 seconds of blotting. Record the mass of the specimen in the laboratory notebook.
5. Place the specimen in a container filled with distilled water.
6. Place the water-filled container with the specimen in a vacuum chamber.
7. Apply a vacuum to the vacuum chamber.
8. Vacuum saturate the specimen for at least 30 hours.
9. Turn off the vacuum pump, open the valve on the vacuum chamber and allow the pressure to equilibrate with atmospheric conditions.
10. Keep the specimen submerged in water at ambient pressure for at least 16 hours.
11. Remove the specimen from the container and blot it with a damp lint free paper towel.
12. Weigh the specimen within 15 seconds of blotting. Record the mass of the specimen on the vacuum saturation data sheet.
13. Return the specimen to the water-filled container and repeat steps 11 and 12. Calculate the mean saturated mass of the specimen for the two measurements.
14. Return the specimen to the water-filled container and repeat the vacuum saturation procedure in steps 6 through 13. Calculate the mass change for each successive vacuum saturation cycle. If the mass change for successive vacuum

saturation cycles is less than or equal to 0.05%, the process has met the specification and the saturation procedure is terminated. If the mass change is greater than 0.05%, steps 6 through 13 must be repeated until the specification is met.

15. Store the specimen in distilled water at ambient pressure and temperature until it is ready for mechanical testing.
16. Compute the saturated bulk density by dividing the saturated mass by the specimen volume.

2.3.3 Average Grain Density Measurement Using Water Pycnometry

The average grain density of each core received from boreholes UE25 NRG-4 and -5 was measured using the water pycnometry method. The technique employs a two-stage measurement. First, the mass of a dry, powdered specimen is measured. Next, the volume of the powder is determined. These two measurements are combined to compute the average grain density.

Pieces of core with a mass of approximately 20 to 50 grams are ground to a powder with a particle size of 1.5 mm or less. The powder is dried according to SNL TP-65 (without any cooling cycles).

The powdered specimen of tuff is added to a dry, calibrated water pycnometer with a nominal volume of 100 ml. The step-by-step procedure presented below produces measurements of the dry mass of the powdered specimen and the corresponding volume of the specimen. The technique has been verified using quartz powders with a well characterized density.

1. Pulverize approximately 20 to 50 g of the specimen to a particle size of 1.5 mm or less. The powder is dried in an aluminum drying pan according to SNL TP-65, except cooling is not allowed at any time in order to minimize rehydration.
2. Add the dried sample to a calibrated, clean, dry and numbered pycnometer by pouring it through a clean, dry transfer funnel.
3. Weigh the pycnometer with the dry sample immediately (do not allow it to cool).

4. Add 50 to 60 ml of distilled water to the pycnometer and swirl it to moisten all of the sample powder.
5. Place the pycnometer, with the sample, in an active vacuum for a minimum of 16 hours. For the first one or two hours, watch the pycnometer to ensure that the boiling action does not displace any of the sample from the pycnometer. The vacuum should be regulated depending on the observed phenomena.
6. Remove the pycnometer from the vacuum chamber and pour additional deaired water into the pycnometer until the water level is just below the scribe line. Note that pouring water down the neck reduces the likelihood of entrapping air in the water as it is added to the pycnometer.
7. Use a pipette to add water until the bottom of the meniscus is at the height of the scribe line. It may be necessary to raise the water level higher than the scribe line to wet the sides of the pycnometer for a suitable meniscus. In this case, water is removed to obtain the correct reading.
8. Use a cotton swab to dry the inside of the neck of the pycnometer.
9. Use a lint-free wipe to clean and dry the exterior of the pycnometer.
10. Weigh the pycnometer and its contents.
11. Measure the water temperature in the pycnometer to the nearest 0.2 ° C.
12. Calculate the average grain density (ρ_g) of the specimen using the water pycnometer grain density measurement sheet (Figure 3).
13. Pour the sample and water into a clean container to allow the water to evaporate.
14. Store the sample powder in a container to maintain it in its original condition.

2.3.4 Dry Bulk Density, Saturated Bulk Density, and Porosity

The dry bulk density, ρ_{db} , is obtained by computing the volume of a test specimen from its external dimensions and dividing it into the mass measured in a dry condition. The density corresponding to the measurement in the saturated condition is the saturated bulk density, ρ_{sb} . Preferably, porosity, ϕ , is computed using the following relation:

Bulk Properties
Yucca Mountain Project
WATER PYCNOMETER GRAIN DENSITY MEASUREMENT
per TP- 229 Rev. 0

SAMPLE ID: _____

WATER PYCNOMETER ID: _____

Date of latest calibration: _____ Nominal Pycnometer Volume: _____

DATA:

Dry Pyc. Wt.: _____ g (A) Dry Pyc. + Dry Sample Wt.: _____ g (B)

Dry Sample Wt.: _____ g (C) = B-A

Wt. Pyc. + Sample + Water: _____ g (D)

Water Temperature: _____ °C (E) Water Density at (E) (See Below): _____ g/cc (F)

Wt. Water Only: _____ g (G) = D-B

Volume Water: _____ cc (H) = G/F

Volume Pyc. at (E) from Calibration: _____ cc (I)

Volume Sample: _____ cc (J) = I-H

Sample Grain Density: _____ g/cc (K) = C/J

Absolute Density of Water

(From Lange's Handbook of Chemistry, edited by J. Dean, 11th Edition, Sect. 10-127)

Temp °C	Density						
18.0	0.998595	20.8	0.998035	23.6	0.997394	26.4	0.996676
18.2	0.998553	21.0	0.997992	23.8	0.997345	26.6	0.996621
18.4	0.998520	21.2	0.997948	24.0	0.997296	26.8	0.996567
18.6	0.998482	21.4	0.997904	24.2	0.997246	27.0	0.996512
18.8	0.998444	21.6	0.997850	24.4	0.997196	27.2	0.996457
19.0	0.998405	21.8	0.997815	24.6	0.997146	27.4	0.996401
19.2	0.998365	22.0	0.997770	24.8	0.997095	27.6	0.996345
19.4	0.998325	22.2	0.997724	25.0	0.997044	27.8	0.996289
19.6	0.998285	22.4	0.997678	25.2	0.996992	28.0	0.996232
19.8	0.998244	22.6	0.997632	25.4	0.996941	28.2	0.996175
20.0	0.998203	22.8	0.997585	25.6	0.996888	28.4	0.996118
20.2	0.998162	23.0	0.997535	25.8	0.996835	28.6	0.996060
20.4	0.998120	23.2	0.997490	26.0	0.996783	28.8	0.996002
20.6	0.998078	23.4	0.997442	26.2	0.996729	29.0	0.995944

Operator: Print/Sign: _____ Date/Time: _____

Figure 3: Bulk properties worksheet used to record measurements and reduce data for the computation of average grain density.

$$\phi = \frac{\rho_g - \rho_{db}}{\rho_g} \times 100\%.$$

Alternatively, the porosity can be calculated from the dry bulk density and saturated bulk density according to:

$$\phi = \frac{\rho_{sb} - \rho_{db}}{\rho_w} \times 100\%$$

where ρ_w is the density of water.

2.4 Compressional and Shear Wave Velocity Measurements

Compressional and shear wave velocities were measured on right circular cylinders with a nominal length-to-diameter ratio of 2:1. The velocities were measured for both dry and water-saturated conditions at ambient temperature in a benchtop apparatus. Specimens were dried at 110 °C according to SNL TP-65 (as in Section 2.3.1). Earlier investigations have shown that heating specimens of Topopah Spring Member tuff to 110 °C does not damage them by the formation of microcracks.

The compressional and shear wave velocity measurements are used for two main purposes. First, a measure of the specimen anisotropy can be directly obtained by comparing the compressional and shear wave velocities measured both parallel and normal to the core axis. Second, compressional and shear wave velocity data, combined with the density of the specimen, are used to compute Young's modulus and Poisson's ratio. These elastic moduli will be referred to as dynamic moduli in subsequent discussions. The dynamic moduli can then be compared with the moduli computed for the data on the unconfined compression tests conducted at a strain rate of 10^{-5} s^{-1} . The elastic constants computed from stress and strain measurements in a deformational experiment are often referred to as static. For porous rocks, the dynamic moduli are greater than the static moduli measured during the constant strain rate experiments, and therefore serve as an upper bound on the static moduli (Simmons and Brace, 1965; Cheng and Johnston, 1981; Haupt et al., 1992).

A self-contained ultrasonic measuring system is used to perform the velocity measurements. A tuff specimen is placed between a matched set of ultrasonic transducers. One transducer serves as the source; the second as the receiver (Figure 4). The travel time through the rock is divided by the sample length to compute the velocity.

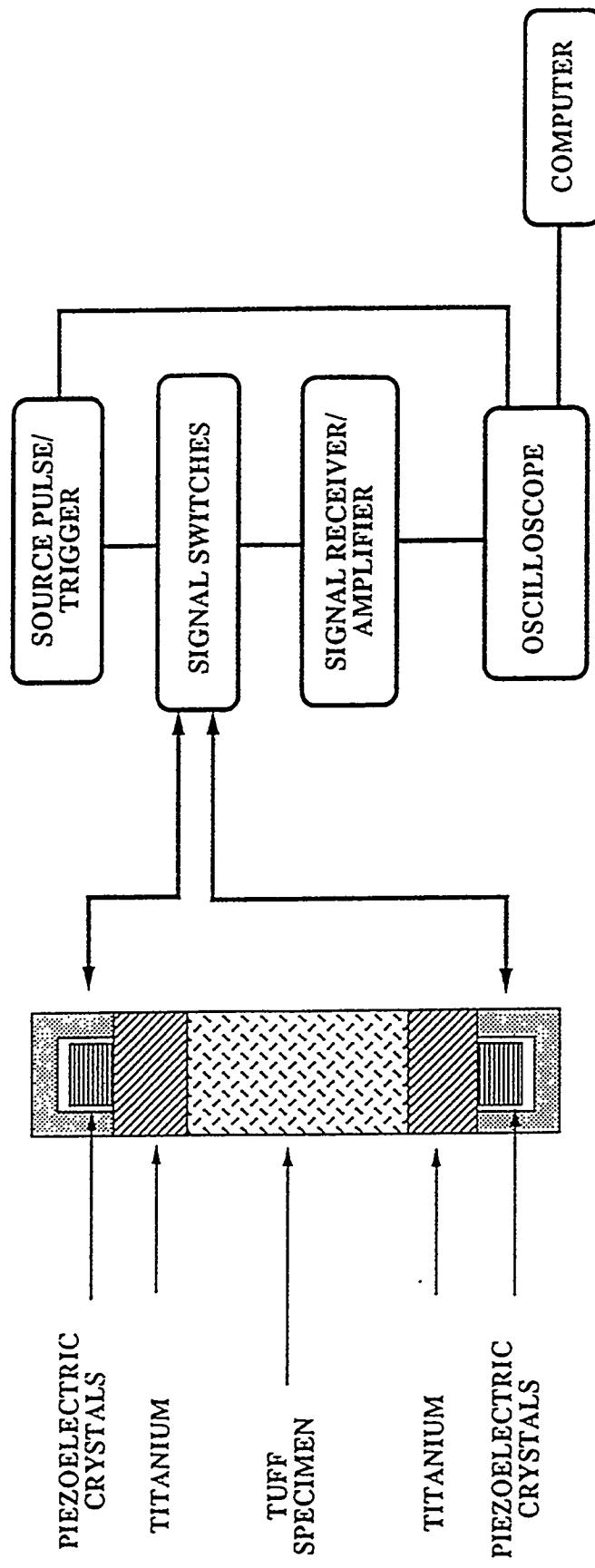


Figure 4: Schematic diagram of the geometry used to measure compressional and shear wave velocities in tuff. The diagram shows the setup for the measurement of velocities parallel to the core axis.

Each ultrasonic transducer contains one compressional and one or two polarized shear wave elements. For the measurements parallel to the core axis, one compressional and two orthogonally polarized shear waves are propagated. For measurements normal to the core axis, one compressional and one polarized shear wave velocity are measured. The polarization direction of the shear wave propagating normal to the core axis is parallel to the axis of the core.

The transducers are constructed using piezoelectric crystals with a resonant frequency of 1 MHz. The multicomponent piezoelectric crystals are bonded to a titanium substrate. Titanium has been selected because it has a good acoustical impedance match both to the rock and to the piezoelectric crystals. The source crystal is excited with a fast rise time pulse generator. The crystal produces a broad band ultrasonic pulse propagated through the adjacent titanium substrate, the rock, the titanium at the opposite end of the core, and into the receiver crystal. The received electrical signal is then amplified and filtered through the receiving section of the pulser-receiver and displayed on a digital storage oscilloscope. The signals are amplified, and high pass filtered above 0.3 MHz. The time series displayed on the oscilloscope is then digitized and transferred to a computer for subsequent analysis including picking the first arrival of the compressional and shear wave energy to compute the compressional and shear wave velocities. The accuracy of the travel time is ± 0.02 microseconds.

A diagram of the system is shown in Figure 5. Pneumatic actuators couple the transducer assemblies in both the axial and radial directions. The stress across the interface for both the matched transducer pairs is identical; this is accomplished by adjusting the loading areas in the pneumatic actuators. The titanium pieces for the radial transducers are concave to mate with the rock surface. Because of the geometry of the interface, only polarizations parallel to the core axis are propagated for shear waves in the radial direction.

2.4.1 Detailed Procedure for Compressional and Shear Wave Velocity Measurements

The detailed procedure for measuring compressional and shear wave velocities on dry and water-saturated tuff specimens is presented below.

1. The tuff sample is a ground, right-circular cylinder with a nominal length-to-diameter ratio of 2:1. The sample is machined to meet or exceed the tolerances specified in SNL TP-51.

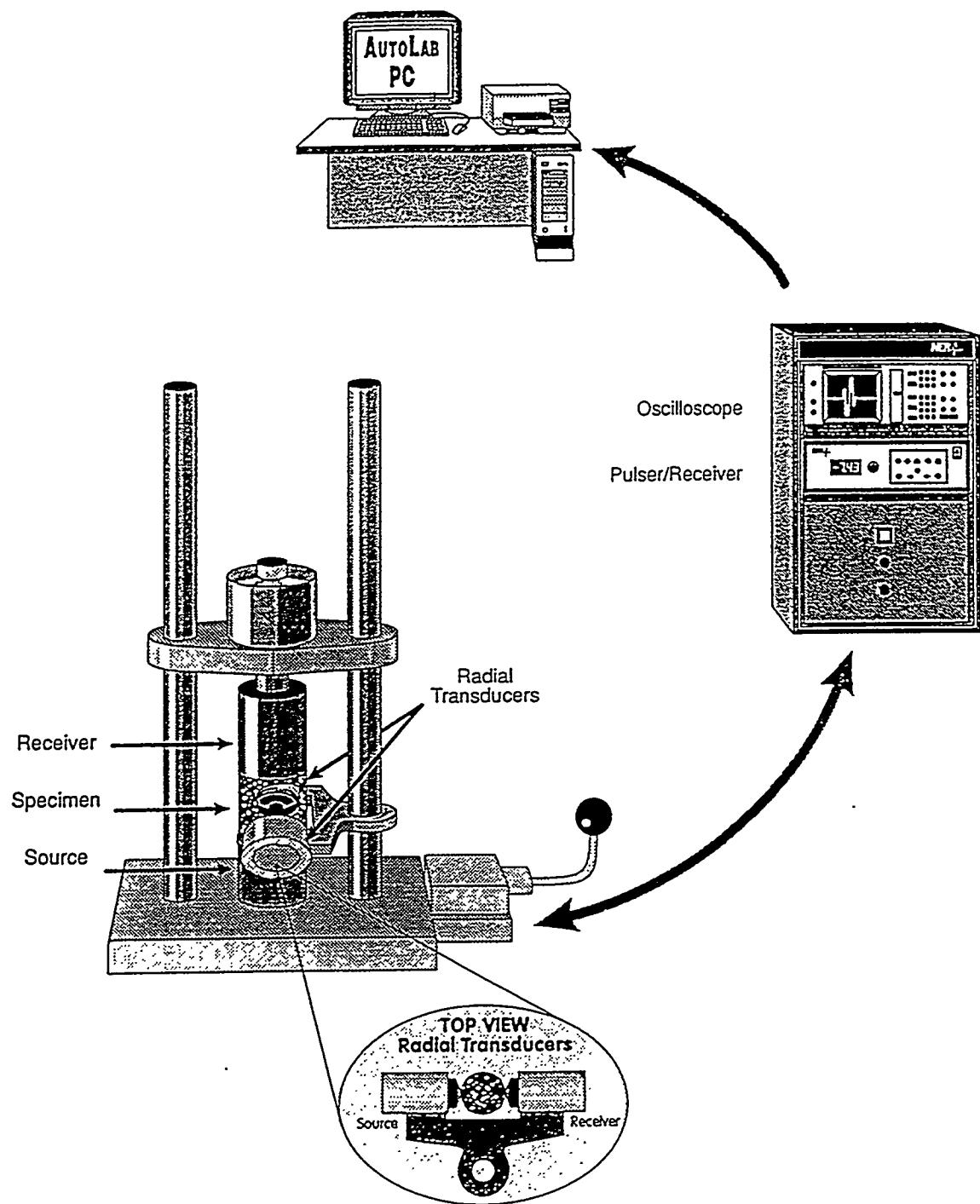


Figure 5: Schematic of the apparatus used to measure ultrasonic velocities parallel and normal to the core axis under ambient conditions prior to testing in unconfined compression.

2. Coat the ends of the specimen with a shear wave couplant. Shear wave couplant is a viscous substance that facilitates the propagation of shear waves across the specimen-titanium interface. Shear wave couplant is also applied at the midpoint of the specimen where the velocities normal to the specimen axis are measured.
3. Position the specimen in the ultrasonic velocity measuring apparatus. Ensure that the specimen is lined up with the transducers in the axial direction.
4. Increase the pressure in the pneumatic actuators to load the axial and radial transducer assemblies to the specimen. Ensure that the specimen has not shifted during this procedure and that the specimen is well coupled to the transducer assembly.
5. Turn on the data acquisition system. First, set the signal selection switch for a compressional (P) wave along the axis of the specimen. Observe the received signal on the digital oscilloscope. Adjust the pulse excitation signal gain and/or attenuation to obtain a well-defined signal.
6. Initiate the data acquisition software to store the waveform; capture and store the waveform.
7. Capture the two shear (S1 and S2) wave polarizations with a propagation direction parallel to the core axis, and the compressional and shear wave signals for the propagation direction normal to the core axis, following the same procedure used for the compressional wave in steps 5 and 6.
8. Compute the compressional and shear wave velocities by determining the travel time through the specimen and dividing it into the sample length. The travel time is determined by picking the time of the first arrival of the compressional or shear wave energy. The measured travel times are reduced by the travel time through the titanium substrates. The corrected travel time is then divided into the sample length to determine the velocity.
9. Print the stored waveforms, along with the computed compressional and shear

wave velocities, and place the data in the scientific notebook.

10. Compute the dynamic Young's modulus (E) and Poisson's ratio (v) from the velocity data collected parallel to the core axis and the bulk density of the specimen for the measurement condition. The dynamic elastic moduli are computed as follows:

$$E = [\rho V_s^2 (3V_p^2 - 4V_s^2) / (V_p^2 - V_s^2)]$$

$$v = (V_p^2 - 2V_s^2) / [2(V_p^2 - V_s^2)]$$

where

V_p = compressional wave velocity, km s^{-1}

V_s = average shear wave velocity, km s^{-1}

ρ = bulk density for the measurement conditions, g cm^{-3} .

2.5 Unconfined Compression to Failure

The unconfined compression experiments were performed on saturated right-circular cylinders of tuff with a nominal length to diameter ratio of 2:1, at a constant axial strain rate of 10^{-5} s^{-1} at room temperature. System checks of the entire test system were conducted during this experimental series to establish the performance of the system using an aluminum specimen with the same nominal dimensions as the tuff test specimens.

A description of the equipment and an overview of the test procedures places the step-by-step procedures in the proper context. All the compression tests were carried out in a servo-controlled hydraulic loading frame with a capacity of $1.1 \times 10^6 \text{ N}$. The servo-controller is a self-contained digital unit, which operates in either force or displacement feedback. The rate at which the reference signal is updated can be varied from 10^{-5} to 10^3 times per second. The loading rate or displacement rate depends on the range of the feedback transducers and the time between steps. The feedback transducers are conditioned with amplifiers in the servo-control unit and balanced so that the full-scale output of the transducer corresponds to the maximum range of the reference signal generator. The full-scale output (10 V) is divided into 2^{12} discrete steps.

Figure 6 is a schematic diagram of an instrumented specimen. The test assembly consists of the specimen positioned between hardened steel end caps. The specimen is jacketed in a flexible membrane to maintain its moisture level.

For this experimental series, five outputs from a variety of transducers were monitored. The output from each device is conditioned, amplified, converted to digital format, and recorded as a function of time. The outputs from the devices were recorded with a microcomputer acquisition system. Each channel is sampled at a frequency of 4 Hz.

For constant strain rate tests, the loading frame is operated in displacement feedback. The displacement can be controlled to within $\pm 10^{-3}$ mm when the system is in the displacement mode. The accuracy and the reproducibility of the strain rate in this system is $\pm 0.5\%$.

During each test, the axial and radial displacements of the specimen were measured with Linear Variable Differential Transformers (LVDTs). A schematic of their arrangement is shown in Figure 6. Two LVDTs monitor the axial displacement. The LVDT barrels are secured in a ring which is attached to one specimen radius from the upper end of the specimen. The cores for the displacement transducers are on extended rods which attach to a second ring separated from the first by one specimen diameter. The second ring is mounted approximately one specimen radius from the lower end of the specimen.

The most direct way to measure radial strain is with the radial displacement gage developed by Holcomb and McNamee (1984). This gage consists of an LVDT mounted in a ring which is spring loaded against the surface of the specimen (Figure 6). The core of the LVDT is connected to the spring. As the specimen diameter changes, the spring deflects, changing the position of the core within the barrel of the LVDT in direct proportion to the radial displacement.

The force on the test column is measured with a load cell. The accuracy of the load cell is better than 0.5% of its full-scale output; the combined linearity and hysteresis are better than 1.0%. The position of the hydraulic piston is observed with a displacement transducer. This transducer provides feedback control in constant strain rate tests and is continuously monitored along with all the transducer outputs. The hydraulic piston advances at a constant rate; this is equivalent to deforming the specimen at a constant strain rate only in the linear portion of the stress-strain curve.

Checks of the entire test system are made using a sample of 6061-T6511 aluminum with the same nominal dimensions as the test specimens. One check is performed before the experiments on a suite of tuff samples, and then after each group of ten tuff samples.

Axial and Radial Deformation Instrumentation

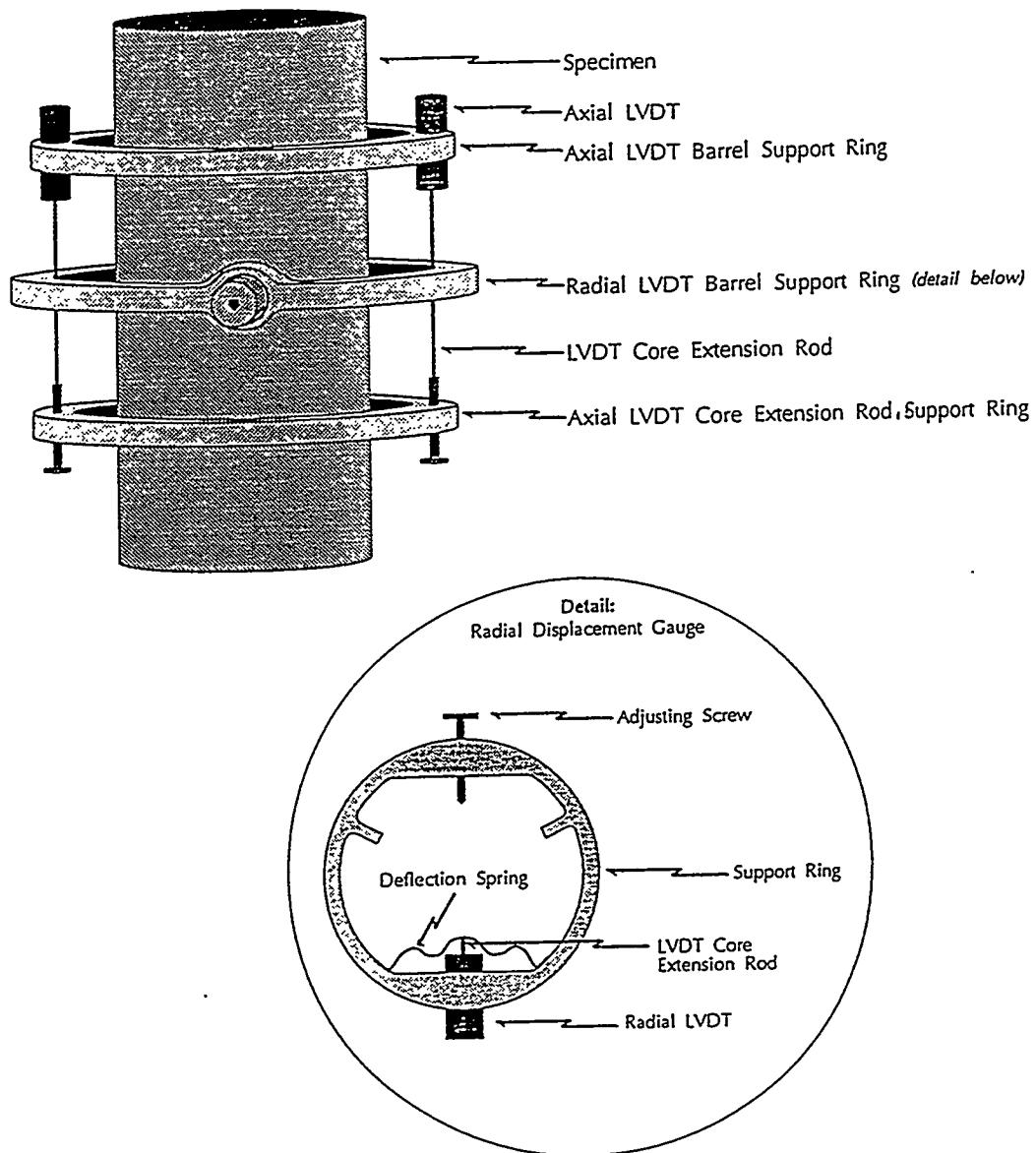


Figure 6: Schematic of the transducer configuration used to measure the axial and radial displacement of specimens during unconfined and confined compression tests.

Each check was performed at the same conditions as the experiments on the tuff specimens: a nominal strain rate of 10^{-5} s $^{-1}$, at ambient temperature.

2.5.1 Experimental Procedures for Unconfined Compression Tests

Specimens of tuff were tested to failure at a constant strain rate of 10^{-5} s $^{-1}$, under ambient temperature and pressure conditions. The following sections include the step-by-step procedures for the mechanical experiments based on SNL TP 219 “Unconfined Compression Experiments at 22 °C and a Strain Rate of 10^{-5} s $^{-1}$.” The test procedure relies on ASTM Standard Method D 3148 “Standard Test Method for Elastic Moduli of Intact Rock Core Specimens in Uniaxial Compression” and ISRM procedure “Suggested Methods for Determining the Uniaxial Compressive Strength and Deformability of Rock Materials.”

1. Each tuff specimen is machined according to SNL TP-51, dried according to SNL TP-65, and saturated according to SNL TP-64. Velocity measurements are performed after the drying and saturation procedures.
2. List all transducers used for each experiment. The information includes the serial numbers of the device, signal conditioning amplifier number, the computer channel on which the output is recorded, and the scaling factor for the amplified output.
3. Visually inspect the test specimen and note any surface irregularities and imperfections.
4. Jacket the saturated specimen in a thin, flexible membrane. The membrane is extended 12 mm beyond each end of the specimen. Hardened steel-end caps are then positioned at each end of the specimen.
5. Position the ring supporting the two axial LVDT barrels approximately one specimen radius from the upper end of the specimen. Carefully center the ring so that it is concentric with the specimen.
6. Position the LVDT ring used to measure the radial displacement at the midpoint of the specimen. The supporting ring for the LVDT (with a range of ± 1.25 mm) is positioned in such a way to ensure that the line between the adjusting screw on the ring and the axis of the core barrel of the LVDT passes through the axis of

the specimen and is perpendicular to the axis of the specimen.

7. Position the lower support ring for the axial LVDT concentrically about the specimen approximately one specimen diameter from the upper ring. This ring supports the stainless steel extension rods for the LVDT cores. Ensure that the axes of the LVDT core barrels are aligned parallel with the axis of the specimen. The extension rods are supported with adjusting screws that are secured with locking nuts.
8. Measure the center-to-center separation of the axial LVDT support rings with a caliper-micrometer. Record this value in the scientific notebook.
9. Place the specimen assembly on the base plug of the load frame.
10. Connect the two axial LVDTs and the radial LVDT to the electrical leads in the base plug.
11. Advance the loading piston, in displacement control, until a small load is exerted on the specimen column (just enough to hold the specimen securely in position).
12. Make the final mechanical adjustments on the LVDTs. Each LVDT is adjusted so that its initial amplified output is approximately 0.10 V. Note that all the LVDTs are wired so that increasing the specimen diameter and shortening the specimen assembly results in an increasing positive output voltage.
13. Retract the hydraulic piston until there is no force on the loading column.
14. Initiate data acquisition. The amplified outputs from five transducers are monitored and recorded using a microprocessor-based data acquisition system. The transducers that are monitored include the three LVDTs, the feedback displacement transducer, and the force cell. All the channels are sampled every 0.25 seconds. Data are stored when the output of one channel deviates from the previous value by a preselected threshold. The threshold for each channel is independently set prior to the experiment.
15. Adjust the setting on the displacement rate controller to the displacement rate that corresponds to a nominal strain rate of 10^{-5} s^{-1} . After a final check of all the

transducer values, start loading the specimen.

16. Load the specimen to failure.
17. Remove the specimen from the press and examine the manner in which it failed. Record the observations in the scientific notebook. Photograph the specimen. Ensure that the field of view of the photograph includes the specimen identification, TP (Technical Procedure) identification, scale, date, type of test performed, and NER (New England Research, Inc.) identification.
18. Return the specimen to its original container and return it to storage.
19. Reduce the data. The following elastic constants are computed:
 - (a) Young's modulus, E
 $E = \Delta \text{ (axial stress)} / \Delta \text{ (axial strain)}$
 - (b) Poisson's ratio, ν
 $\nu = \Delta \text{ (radial strain)} / \Delta \text{ (axial strain)}$.

The elastic constants are computed by performing a least-squares linear fit to the data collected between 10 and 50% of the fracture strength. Axial stress is computed by dividing the axial force by the initial cross-sectional area of the specimen. Stress is reported in MPa. Axial strain is obtained by dividing the average axial displacement of the axial LVDT support rings by the original ring separation distance. Radial strain is computed by dividing the change in radial displacement observed by the radial LVDT by the initial specimen diameter. All strains are reported in millistrain.

2.6 Confined Compression to Failure

Confined compression tests were carried out on specimens from cores with sufficient uniform material that numerous specimens could be obtained. The specimens had a length-to-diameter ratio of 2:1 with a diameter of 25.4 mm and were tested in a saturated condition. The general procedure for testing these specimens was the same as that described for the unconfined compression tests except that the specimens were jacketed

in copper and deformed in a pressure vessel at a fixed confining pressure. The procedure was based on TP-219 and conforms to ISRM "Suggested Methods for Determining the Strength of Rock Materials in Triaxial Compression" and ASTM D 2664 "Triaxial Compressive Strength of Undrained Rock Core Specimens Without Pore Pressure Measurements." The series of tests was designed so that at least three specimens were tested for each confining pressure. Specimens were tested at confining pressures of 5, and 10 MPa.

Each specimen was jacketed in dead soft copper 0.13 mm thick. The jacket was seated to the rock specimen by subjecting it to a hydrostatic pressure of 10 MPa. Once the jacket was seated, it was visually inspected to ensure that there were no holes that would permit leakage of the confining medium into the rock core during the test. Next, the specimen was instrumented using the same arrangement utilized for the unconfined compression tests (Figure 6).

The instrumented specimen was mounted on the base plug of a 50 MPa capacity pressure vessel. The LVDTs were adjusted. Once the LVDTs were on scale and functioning properly, the base plug of the pressure vessel containing the instrumented specimen assembly was inserted into the pressure vessel. Next, the confining pressure was exerted on the specimen using a servo-controlled hydraulic intensifier. The confining medium was argon gas. The confining pressure was allowed to stabilize. The confining pressure was held constant during the remainder of the experiment to within ± 0.1 MPa.

Once the confining pressure reached thermal equilibrium, the specimen was monotonically loaded to failure at a strain rate of 10^{-5} s⁻¹. After the specimen failed, the confining pressure was released and the specimen was removed and inspected. The data were reduced to determine Young's modulus, Poisson's ratio, and fracture strength. Young's modulus and Poisson's ratio are computed in the same manner as for the unconfined compression tests, between 10 and 50% of the stress difference at failure.

2.7 Indirect Tensile Strength Tests

Indirect tensile strength tests, commonly referred to as Brazil tests, were carried out using a procedure adhering to ASTM D-3967 "Splitting Tensile Strength of Intact Rock Core Specimens." The test is quite simple in principle. A load is applied to a cylindrical specimen with its axis normal to the loading direction. A tensile stress develops in the center of the cylinder. The specimen fails by an extension fracture along the diametral loading plane. The force is increased until the specimen fails. The strength is computed

from the force at failure.

The tests were performed in the servo-controlled load frame used for the unconfined and confined compression tests. For these measurements the only transducer was a load cell with a capacity of 4.5×10^4 N. A schematic diagram of the setup is shown in Figure 7.

The specimens were right-circular cylinders, ground to the dimensions and tolerances listed in Section 2.0. The dry bulk density and saturated bulk density were measured prior to testing. The specimens were tested in a water-saturated condition.

To obtain reproducible and accurate data, it is important that the loading axis of the test frame passes through the axis of the specimen. As an aid in the alignment of the specimen in the loading column, diametral lines are scribed on the bearing surfaces.

2.7.1 Experimental Procedures for Indirect Tensile Strength Tests

The detailed procedure developed according to ASTM D-3967 is presented below.

1. Each tuff specimen was machined according to SNL TP-51, dried according to SNL TP-65, and saturated according to SNL TP-64. All initial conditions were documented.
2. Mark diametral lines on the ends of the specimen.
3. Cut 2.5-cm-wide by 4.0-cm-long (slightly longer than the specimens) pieces of notepad-backing cardboard approximately 0.89 mm thick for bearing strips.
4. Place one bearing strip onto the bottom bearing platen with its length parallel to the diametral line scribed onto the platen.
5. Place the specimen onto the bearing strip making certain its full length is supported by the bearing strip. Align the axis of the specimen parallel to the line scribed onto the platen (lines on both ends of the specimen line up with the line scribed on the platen).
6. Place the second bearing strip onto the top of the specimen making certain it will support the full length of the specimen.

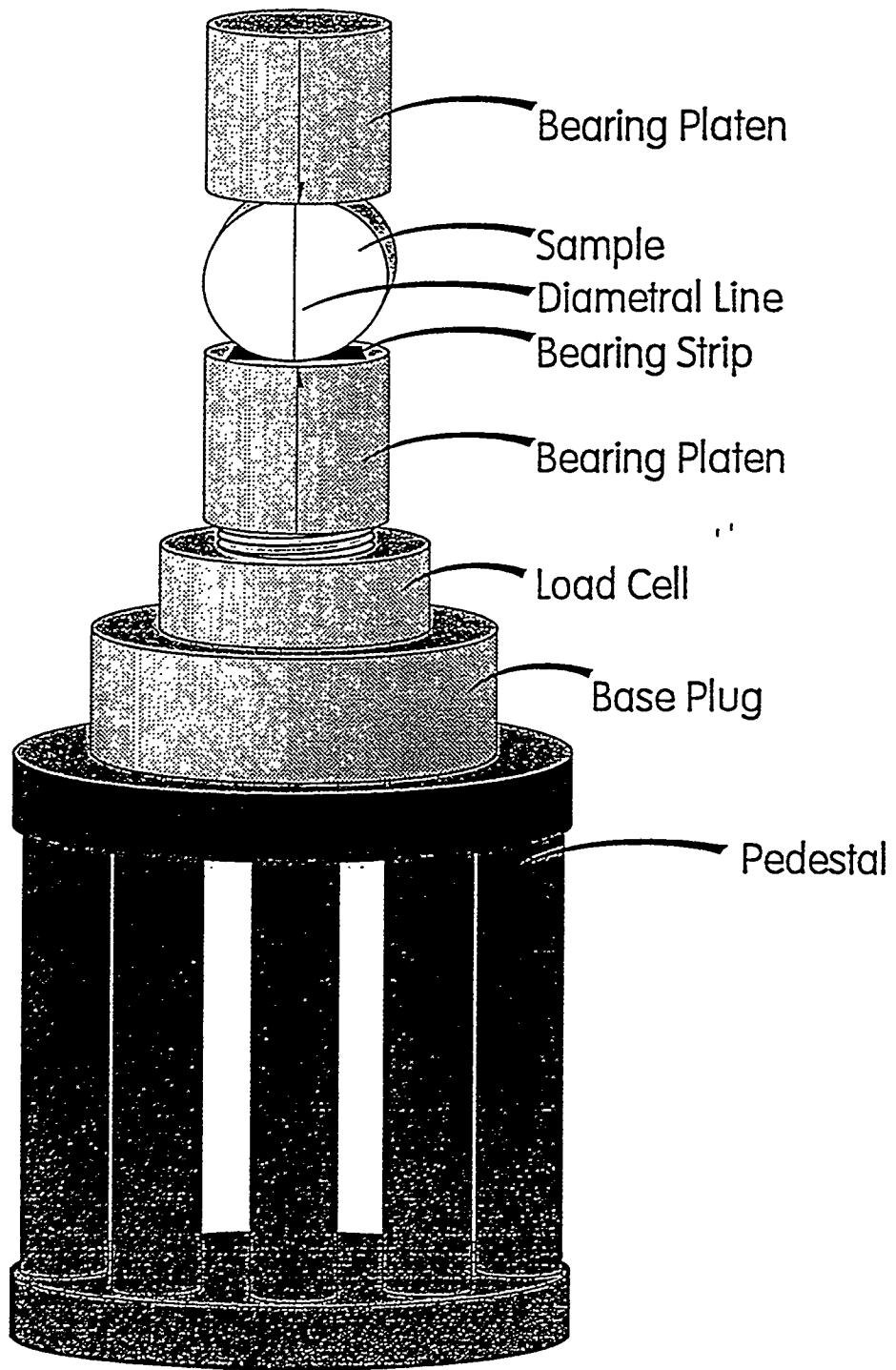


Figure 7: Schematic of the loading arrangement and sample geometry used for the indirect tensile strength tests.

7. Advance the loading piston, in displacement control, until a small load is applied (just enough to hold the specimen and the bearing strips in place while positioning them).
8. Make final adjustments to the specimen's position to ensure the diametral plane of the two lines marked onto the specimen line up with the center of thrust (lines scribed onto the top and bottom bearing planes), and its midpoint along its length is also lined up to within ± 0.025 mm of the center of the bearing platens. The midpoint is centered by repeatedly measuring the distance from the specimen ends to the edge of the bearing platens and adjusting its position until they are equal.
9. Initiate the data acquisition system.
10. Load the specimen monotonically to failure in displacement control at the same rate used for the unconfined compression tests. Once the specimen fails, data acquisition is terminated and any remaining load is removed. The specimen is removed from the loading column, described, and photographed.
11. Calculate the indirect tensile strength using the formula:

$$\sigma_t = 2F/\pi L D$$

where

F = applied force
 L = specimen length
 D = specimen diameter.

The indirect tensile strength is reported in MPa.

3.0 RESULTS

The results of the bulk properties measurements and the mechanical tests are presented in Tables 1, 2, 3, and 4. Table 1 presents the data associated with the unconfined compression tests. The data include dry bulk density, saturated bulk density, average grain density, porosity, compressional and shear wave velocities for the dry and saturated conditions both parallel [axial] and normal [radial] to the core axis, static Young's modulus, static Poisson's ratio, axial stress at failure, and axial strain at failure. These data

Table 1

SUMMARY DATA SHEET: NRG-4 BOREHOLE
Unconfined Compression Tests

Sample IDs are shortened from the "NRG-4-Depth-SNL-Subdivision" Format
 Test Conditions: Saturated samples, ambient pressure and temperature, and a nominal strain rate of 10E-5 sE-1.

Depth, ft:	416.6	422.3	428.4	433.2	456.0	458.7	466.8	469.0	508.4	515.5
T/M Unit:	PTn	PTn	PTn	PTn	PTn	PTn	PTn	PTn	PTn	TSw1
Date Tested:	1/5/94	1/5/94	1/5/94	1/11/94	1/5/94	1/11/94	1/5/94	1/5/94	1/6/94	1/6/94
Dry Bulk Density (g/cc):	1.175	1.066	1.114	1.179	1.390	1.488	1.485	1.278	2.266	2.262
Saturated Bulk Density (g/cc):	1.647	1.579	1.622	1.661	1.759	1.864	1.872	1.747	2.364	2.360
Average Grain Density (g/cc):	2.350	2.321	2.352	2.358	2.420	2.472	2.433	2.527	2.566	2.563
Porosity via Grain Density (%):	53.1	54.1	52.7	50.0	42.6	39.8	39.0	49.4	11.7	11.7
Dry P Velocity (km/s):									4.344	4.348
Dry S1 Velocity (km/s):										2.617
Dry S2 Velocity (km/s):										2.630
Dry Radial P Velocity (km/s):										
Dry Radial S Velocity (km/s):										
Sat. P Velocity (km/s):									4.419	4.470
Sat. S1 Velocity (km/s):										2.726
Sat. S2 Velocity (km/s):										
Saturated Radial P Velocity (km/s):									4.499	4.447
Saturated Radial S Velocity (km/s):										3.197
Static Young's modulus (GPa):	1.9	0.7	1.2	0.8	2.1	0.8	1.7	0.2	32.3	31.6
Static Poisson's ratio:	0.28	0.53	0.18	0.36	0.09	0.15	0.14	0.19	0.22	0.22
Ultimate Axial Stress (MPa):	4.9	1.8	3.5	3.3	9.4	5.2	6.4	2.0	102.6	98.5
Ax. Strn at Ult. Ax. Sis. (milstr):	3.00	2.79	2.97	3.82	4.90	6.66	4.11	6.04	3.43	3.17

P is the compressional wave, S1 and S2 are the two orthogonally polarized shear waves.

Elastic properties are calculated between 10 and 50% of the ultimate axial stress.

Table 1 (continued)

SUMMARY DATA SHEET: NRG-4 BOREHOLE
Unconfined Compression Tests

Sample IDs are shortened from the "NRG-4 Depth-SNL-Subdivision" Format
Test Conditions: Saturated samples, ambient pressure and temperature, and a nominal strain rate of 10E-5 sE-1.

Depth, ft:	525.0	530.4	535.3	541.0	546.0	550.0	582.4	591.7	597.0	602.9
T/M Unit:	TSw1									
Date Tested:	1/6/94	1/6/94	1/6/94	1/6/94	1/6/94	1/7/94	1/7/94	1/7/94	1/7/94	1/7/94
Dry Bulk Density (g/cc):	2.151	2.082	2.072	2.017	2.109	2.115	2.151	2.111	2.133	2.152
Saturated Bulk Density (g/cc):	2.264	2.231	2.230	2.220	2.283	2.284	2.303	2.284	2.298	2.307
Average Grain Density (g/cc):	2.536	2.539	2.541	2.588	2.591	2.595	2.582	2.577	2.575	2.572
Porosity via Grain Density (%):	15.2	18.0	18.5	22.1	18.6	18.5	16.7	18.1	17.2	16.3
Dry P Velocity (km/s):	4.162	3.981	3.873	3.427	3.557	3.712	3.238			3.155
Dry S1 Velocity (km/s):		2.435	2.391				2.048			
Dry S2 Velocity (km/s):		2.465	2.388				2.036			
Dry Radial P Velocity (km/s):	4.247	4.099	3.996				3.677			
Dry Radial S Velocity (km/s):	2.553		2.478							
Sat. P Velocity (km/s):	4.209	4.054	3.920		3.885	3.938				
Sat. S1 Velocity (km/s):										
Sat. S2 Velocity (km/s):										
Saturated Radial P Velocity (km/s):	4.306	4.240	4.082							
Saturated Radial S Velocity (km/s):										
Static Young's modulus (GPa):	27.3	21.6	22.3	14.6	19.2	20.8	13.2	9.2	15.6	13.6
Static Poisson's ratio:	0.21	0.20	0.22	0.34	0.26	0.22	0.28	0.26	0.29	0.27
Ultimate Axial Stress (MPa):	97.9	67.1	55.4	33.2	56.8	61.9	26.2	31.8	33.3	34.1
Ax. Strn at Ult. Ax. Sts. (milstr):	3.96	3.37	2.50	2.50	3.40	3.46	2.27	4.50	2.41	3.41

P is the compressional wave, S1 and S2 are the two orthogonally polarized shear waves.

Elastic properties are calculated between 10 and 50% of the ultimate axial stress.

Table 1 (continued)

SUMMARY DATA SHEET: NRG-4 BOREHOLE
Unconfined Compression Tests

Sample IDs are shortened from the "NRG-4-Depth-SNL-Subdivision" Format
Test Conditions: Saturated samples, ambient pressure and temperature, and a nominal strain rate of 10E-5 sE-1.

Depth, ft:	607.6	612.5	623.8	627.7	655.8	664.4	667.8	695.8
T/M Unit:	TSw1	TSw1	TSw1	TSw1	TSw1	TSw1	TSw1	TSw1
Date Tested:	1/7/94	1/10/94	1/10/94	1/10/94	1/10/94	1/10/94	1/10/94	1/11/94
Dry Bulk Density (g/cc):	2.114	2.158	2.201	2.198	2.185	2.099	2.066	2.008
Saturated Bulk Density (g/cc):	2.283	2.309	2.331	2.317	2.320	2.243	2.224	2.191
Average Grain Density (g/cc):	2.574	2.569	2.569	2.552	2.561	2.536	2.540	2.544
Porosity via Grain Density (%):	17.9	16.0	14.3	13.9	14.7	17.2	18.7	21.1
Dry P Velocity (km/s):	3.040	3.234	3.540	3.730	3.491	3.626		
Dry S1 Velocity (km/s):			2.197					
Dry S2 Velocity (km/s):			2.179					
Dry Radial P Velocity (km/s):	3.014	3.237	3.491	3.883		3.589		
Dry Radial S Velocity (km/s):	1.742							
Sat. P Velocity (km/s):			3.877	4.236				
Sat. S1 Velocity (km/s):								
Sat. S2 Velocity (km/s):								
Saturated Radial P Velocity (km/s):	3.315		4.085		4.043			
Saturated Radial S Velocity (km/s):								
Static Young's modulus (GPa):	11.4	17.2	14.9	11.2	14.5	10.7	6.4	10.3
Static Poisson's ratio:	0.27	0.32	0.27	0.20	0.41	0.60	0.31	0.28
Ultimate Axial Stress (MPa):	43.7	47.9	43.4	32.0	31.1	26.9	17.4	35.9
Ax. Strn at Ult. Ax. Sts. (milstr):	5.07	3.03	4.57	3.34	2.90	3.23	3.21	4.12

P is the compressional wave, S1 and S2 are the two orthogonally polarized shear waves.

Elastic properties are calculated between 10 and 50% of the ultimate axial stress.

Table 1 (continued)

SUMMARY DATA SHEET: NRG-5 BOREHOLE
Unconfined Compression Tests

Sample IDs are shortened from the "NRG-5-Depth-SNL-Subdivision" Format
Test Conditions: Saturated samples, ambient pressure and temperature, and a nominal strain rate of 10E-5 sE-1.

Depth, ft:	847.2	849.4	861.2	873.4	887.2	888.8	891.9	896.5
T/M Unit:	TSw2							
Date Tested:	10/26/93	10/26/93	10/26/93	10/27/93	10/28/93	10/28/93	10/28/93	10/28/93
Dry Bulk Density (g/cc):	2.294	2.310	2.177	2.181	2.280	2.287	2.282	2.284
Saturated Bulk Density (g/cc):	2.378	2.392	2.320	2.313	2.372	2.375	2.374	2.373
Average Grain Density (g/cc):	2.547	2.535	2.568	2.565	2.537	2.521	2.533	2.527
Porosity via Grain Density (%):	9.9	8.9	15.2	15.0	10.1	9.3	9.9	9.6
Dry P Velocity (km/s):	4.709	4.486	4.386	4.663	4.641	4.610	4.608	
Dry S1 Velocity (km/s):	2.962	2.860	2.913	2.918	2.868	2.871		
Dry S2 Velocity (km/s):	2.962	2.889	2.918	2.921	2.878	2.884		
Dry Radial P Velocity (km/s):	4.598	4.651	4.074	4.449	4.668	4.622	4.578	4.651
Dry Radial S Velocity (km/s):	2.887	2.822	2.509	2.764	2.944	2.908	2.885	2.919
Sat. P Velocity (km/s):	4.704	4.575	4.412	4.636	4.608	4.531	4.549	
Sat. S1 Velocity (km/s):								
Sat. S2 Velocity (km/s):								
Saturated Radial P Velocity (km/s):	4.646	4.668	4.497	4.396	4.585	4.556	4.522	4.626
Saturated Radial S Velocity (km/s):								
Static Young's modulus (GPa):	35.2	37.0	17.1	13.4	40.5	39.4	38.3	39.1
Static Poisson's ratio:	0.21	0.19	0.23	0.30	0.20	0.19	0.15	0.10
Ultimate Axial Stress (MPa):	84.2	240.8	55.3	38.4	240.9	288.9	253.5	184.7
Ax. Strn at Ult. Ax. Str. (mils/in):	2.58	7.46	3.38	4.64	6.37	8.11	7.30	4.24(+)*

P is the compressional wave, S1 and S2 are the two orthogonally polarized shear waves.

Elastic properties are calculated between 10 and 50% of the ultimate axial stress.

*: Early spalling caused axial LVDTs to go off scale at 166 MPa.

Table 2

SUMMARY DATA SHEET: NRG-4 BOREHOLE
Confined Compression Tests

Sample IDs are shortened from the "NRG-4-Depth-SNL-Subdivision" Format
Test Conditions: Saturated samples, ambient temperature, and a nominal strain rate of 10E-5 sE-1.

Depth, ft:	527.0-A	527.0-B	527.0-D	527.0-E	527.0-G	527.0-F	527.0-H	527.0-I
T/M Unit:	TSw1							
Date Tested:	1/25/94	1/21/94	1/24/94	1/24/94	1/21/94	1/24/94	1/25/94	1/25/94
Dry Bulk Density (g/cc):	2.078	2.112	2.103	2.079	2.043	2.143	2.121	2.114
Saturated Bulk Density (g/cc):	2.224	2.245	2.231	2.217	2.161	2.264	2.249	2.242
Average Grain Density (g/cc):	2.528	2.528	2.528	2.528	2.528	2.528	2.528	2.528
Porosity via Grain Density (%):	17.8	16.5	16.8	17.8	19.2	15.2	16.1	16.4
Sat. P Velocity at 10 MPa (km/s):	4.237	4.268	4.248	4.254	4.220	4.301	4.213	4.252
Sat. S1 Velocity at 10 MPa (km/s):	2.468	2.470	2.442	2.421	2.420	2.469	2.410	2.428
Sat. S2 Velocity at 10 MPa (km/s):	2.446	2.444	2.444	2.494	2.428	2.462	2.434	2.429
Confining Pressure (MPa):	5	5	5	5	5	10	10	10
Static Young's modulus (GPa):	21.1	22.6	23.4	19.7	14.7	25.5	25.8	23.0
Static Poisson's ratio:	0.19	0.23	0.16	0.17	0.13	0.18	0.19	0.20
Ultimate Diff. Axial Stress (MPa):	71.5	103.9	108.6	85.0	62.5	150.8	132.1	121.4
Ax. Strn at Ult. Ax. Str. (milstrn):	4.02	6.81	4.95	7.51	5.43	6.82	5.74	6.02
								6.57

P is the compressional wave, S1 and S2 are the two orthogonally polarized shear waves.

Elastic properties are calculated between 10 and 50% of the ultimate differential axial stress.

Table 3

SUMMARY DATA SHEET: NRG-4 BOREHOLE
Indirect Tensile Strength (Brazil) Tests

Sample IDs are shortened from the "NRG-4-Depth-SNL-Subdivision" Format
 Test Conditions: Saturated samples, ambient pressure and temperature.

Depth, ft:	382.9	428.4	433.2	439.4	456.0	458.7	469.0	489.4	504.5	504.5
T/M Unit:	PTn	TSw1	TSw1							
Date Tested:	1/11/94	1/11/94	1/11/94	1/11/94	1/11/94	1/11/94	1/11/94	1/11/94	1/11/94	1/11/94
Dry Bulk Density (g/cc):	1.132	1.053	1.155	1.084	1.322	1.558	1.363	2.401	2.208	2.228
Saturated Bulk Density (g/cc):	1.614	1.578	1.628	1.564	1.753	1.911	1.823	2.460	2.325	2.340
Average Grain Density (g/cc):	2.269	2.352	2.358	2.357	2.420	2.472	2.527	2.576	2.572	2.572
Porosity via Grain Density (%):	50.1	55.2	51.0	54.0	45.4	37.0	46.1	6.8	14.2	13.4
Ultimate Tensile Stress (MPa):	0.1	0.2	0.2	0.2	0.7	0.8	0.1	7.7	9.0	9.3

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Depth, ft:	515.5	525.0	530.4	535.3	541.0	546.0	550.0	587.4	587.4	591.7
T/M Unit:	TSw1									
Date Tested:	1/12/94	1/12/94	1/12/94	1/12/94	1/12/94	1/12/94	1/12/94	1/12/94	1/12/94	1/12/94
Dry Bulk Density (g/cc):	2.235	2.159	2.113	2.079	1.998	2.099	2.086	2.128	2.155	2.072
Saturated Bulk Density (g/cc):	2.340	2.277	2.253	2.238	2.205	2.275	2.266	2.284	2.299	2.252
Average Grain Density (g/cc):	2.563	2.536	2.539	2.541	2.588	2.591	2.595	2.586	2.586	2.577
Porosity via Grain Density (%):	12.8	14.9	16.8	18.2	22.8	19.0	19.6	17.7	16.7	19.6
Ultimate Tensile Stress (MPa):	6.7	8.6	8.2	7.5	2.8	4.8	5.8	3.0	4.2	2.3

Depth, ft:	597.0	602.9	607.6	612.5	617.4	617.4	617.4	691.8	691.8
T/M Unit:	TSw1								
Date Tested:	1/12/94	1/14/94	1/14/94	1/14/94	1/14/94	1/14/94	1/14/94	1/14/94	1/14/94
Dry Bulk Density (g/cc):	2.147	2.172	2.109	2.180	2.177	2.184	2.222	2.030	1.978
Saturated Bulk Density (g/cc):	2.306	2.316	2.276	2.317	2.315	2.317	2.346	2.199	2.173
Average Grain Density (g/cc):	2.575	2.572	2.574	2.569	2.566	2.566	2.542	2.542	2.542
Porosity via Grain Density (%):	16.6	15.6	18.1	15.1	15.2	14.9	13.4	20.1	22.2
Ultimate Tensile Stress (MPa):	2.7	3.4	2.8	4.3	3.6	4.0	3.6	3.7	3.7

Table 3 (continued)

SUMMARY DATA SHEET: NRG-5 BOREHOLE

Indirect Tensile Strength (Brazil) Tests

Sample IDs are shortened from the "NRG-5-Depth-SNL-Subdivision" Format
Test Conditions: Saturated samples, ambient pressure and temperature.

Depth, ft:	788.6	832.9	847.2	887.2	888.8	891.9
T/M Unit:	TSw1	TSw2	TSw2	TSw2	TSw2	TSw2
Date Tested:	10/26/93	10/26/93	10/26/93	10/26/93	10/26/93	10/26/93
Dry Bulk Density (g/cc):	2.042	2.253	2.210	2.286	2.293	2.267
Saturated Bulk Density (g/cc):	2.228	2.360	2.331	2.376	2.381	2.374
Average Grain Density (g/cc):	2.526	2.545	2.547	2.537	2.521	2.533
Porosity via Grain Density (%):	19.2	11.5	13.2	9.9	9.0	10.5
Ultimate Tensile Stress (MPa):	4.3	7.7	5.7	16.8	15.9	12.9

Table 4
SUMMARY DATA SHEET: NRG-4 BOREHOLE
Porosity Values for Untestable Sample Intervals

Sample IDs are shortened from the "NRG-4-Depth-SNL-Subdivision" Format

Depth, ft:	422.3	439.4	469.0	477.5	483.0	483.0
T/M Unit:	PTn	PTn	PTn	TSw1	TSw1	TSw1
Date Tested:	1/26/94	12/30/93	1/26/94	1/26/94	1/26/94	1/26/94
Dry bulk Density, (g/cc):	0.950	1.085	1.286	1.364	1.769	1.688
Average Grain Density (g/cc):	2.321	2.357	2.527	2.438	2.395	2.395
Porosity via Grain Density (%):	59.1	54.0	49.1	44.1	26.1	29.5

SUMMARY DATA SHEET: NRG-5 BOREHOLE

Table 4 (continued)

Porosity Values for Untestable Sample Intervals

Sample IDs are shortened from the "NRG-5-Depth-SNL-Subdivision" Format

Depth, ft:	781.0	790.3	798.0	800.2	802.7	807.0	812.4	817.7	823.3	838.5
T/M Unit:	TSw1	TSw1	TSw1	TSw1	TSw1	TSw2	TSw2	TSw2	TSw2	TSw2
Date Tested:	11/2/93	11/3/93	11/4/93	11/4/93	11/2/93	11/4/93	11/2/93	11/4/93	11/4/93	11/4/93
Dry bulk Density, (g/cc):	2.196	2.148	2.149	1.864	2.285	2.135	2.293	2.301	2.281	2.316
Average Grain Density (g/cc):	2.527	2.539	2.550	2.553	2.534	2.543	2.541	2.540	2.546	2.547
Porosity via Grain Density (%):	13.1	15.4	15.7	27.0	9.8	16.0	9.8	9.4	10.4	9.1
Depth, ft:	857.1	869.2	877.6	924.9	972.3	976.7	991.9			
T/M Unit:	TSw2									
Date Tested:	11/2/93	11/2/93	11/2/93	11/4/93	11/4/93	11/4/93	11/3/93			
Dry bulk Density, (g/cc):	2.139	2.241	2.274	2.310	2.349	2.233	2.315			
Average Grain Density (g/cc):	2.558	2.564	2.536	2.607	2.574	2.575	2.588			
Porosity via Grain Density (%):	16.4	12.6	10.3	11.4	8.7	13.3	10.6			

have been grouped according to depth. The thermal/mechanical unit is indicated for each specimen. For some specimens, reliable compressional and shear wave velocities were not obtained due to poor signal quality. The absence of the data is reflected in Table 1.

The porosity reported in Tables 1, 2, 3 and 4 is the total porosity including occluded porosity. The value is computed from the grain density and dry bulk density. The total porosity is most applicable when elastic constants and strength characteristics are measured. The porosity computed from the dry and saturated bulk densities is typically lower than the total porosity and reflects the interconnected porosity. The latter value is applicable when considering fluid transport properties.

Table 2 presents the data for the confined compression tests for a core from UE25 NRG-4. The dry bulk density, saturated bulk density, average grain density, porosity, compressional and shear wave velocities for propagation parallel to the specimen axis at one confining pressure, confining pressure at which the sample was tested, static Young's modulus, static Poisson's ratio, axial stress difference at failure, and axial strain difference at failure are presented for confined compression tests performed on core recovered from a depth of 527.0 feet.

Table 3 presents the results of the indirect tensile strength tests. The data are presented as a function of depth and include dry bulk density, saturated bulk density, average grain density, porosity, and indirect tensile strength. The thermal/mechanical unit for each specimen is also indicated. No compressional or shear wave velocities were measured on these specimens.

Table 4 lists the specimens for which only average grain density, dry bulk density, and porosity were measured. The thermal/mechanical unit for each of these specimens is indicated.

All specimens tested in this study were ideally water saturated. However, the saturation is not 100%. Porosities computed using the saturated bulk density and dry bulk density yield consistently lower values than those computed using the average grain density and dry bulk density. In part, the differences can be attributed to an under-estimation of the saturated bulk density due to water loss on the surface of the specimen. However, these errors are small and cannot account for the total discrepancy. The major contribution to the differences is occluded porosity (isolated pores that are not filled during saturation). As a result, the specimens are not 100% saturated prior to mechanical testing; the saturations range between 80 and 95%.

3.1 Computerized Tomographic X-ray Images

Prior to testing, computerized tomographic X-ray (CT) imaging was performed on each of the specimens tested in unconfined compression. A single image was obtained through the center of the specimen parallel to the core axis. These data serve as a qualitative measure of the shape and distribution of the pores and density heterogeneity within the specimen. CT images for specimens of TSw2 recovered from depths of 861.2 and 873.4 feet from borehole UE25 NRG-5 are shown in Figures 8 and 9, respectively. These images show the physical characteristics of the lithophysal cavities. Each specimen has a porosity of approximately 15%. The white areas are extremely low density rock and open pores. With increasing density, the image darkens.

Both specimens have a large, nearly elliptical lithophysal cavity with its long axis normal to the axis of the specimen. The specimen from 873.4 feet has the larger, centrally located cavity, which may explain its lower strength. The light gray zones surrounding the open pores are altered zones whose density is lower than that of the welded matrix. Many TSw2 specimens have more than one large open cavity, while others are uniformly welded. It should be noted that not all of the porosity for TSw2 is concentrated in the lithophysae; the majority is contained in pores below the resolution of the CT scan, (i.e., less than 1.5 mm).

3.2 Compressional and Shear Wave Velocity Measurements

Compressional and shear wave velocity measurements were performed parallel and normal to the core axis for both dry and saturated conditions on all specimens tested in unconfined compression. Compressional and shear wave velocities were measured parallel to the core axis only, for the specimens tested in confined compression. In some cases data were not collected due to the inability to transmit the waves through the specimen; the greatest difficulty was encountered measuring shear wave velocities under saturated conditions. Particular difficulty was encountered measuring shear wave velocities under both dry and saturated conditions in the more porous/vuggy specimens (typically the PTn and TSw1 specimens). Velocity data were most often obtainable for specimens of TSw2. An examination of the data shows that both compressional and shear wave velocities increased with decreasing specimen porosity.

Typical time series plots measured on UE25 NRG-5-891.9 are shown in Figures 10 and 11. Figure 10 presents the data for compressional (P) and shear waves (S1 and S2) propagated parallel to the specimen axis. Figure 11 exhibits the measurements for P and S

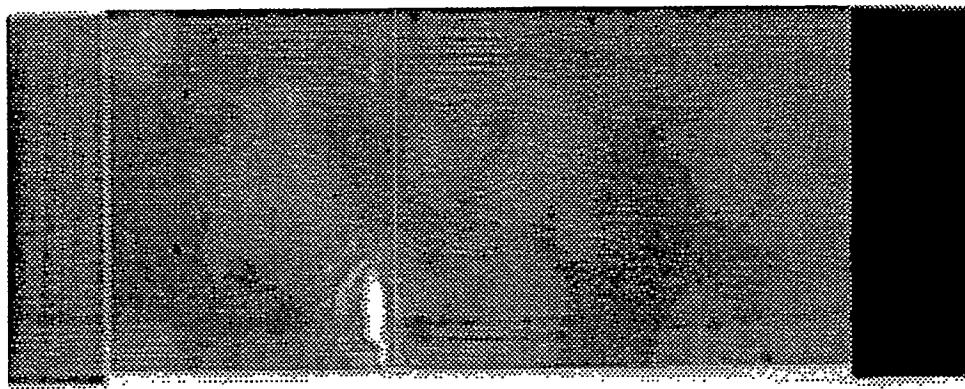


Figure 8: A tomographic image (CT scan) for a specimen of non-lithophysal Topopah Spring member tuff (TSw2) recovered from a depth of 861.2 feet from borehole UE25 NRG-5 at Yucca Mountain, NV.

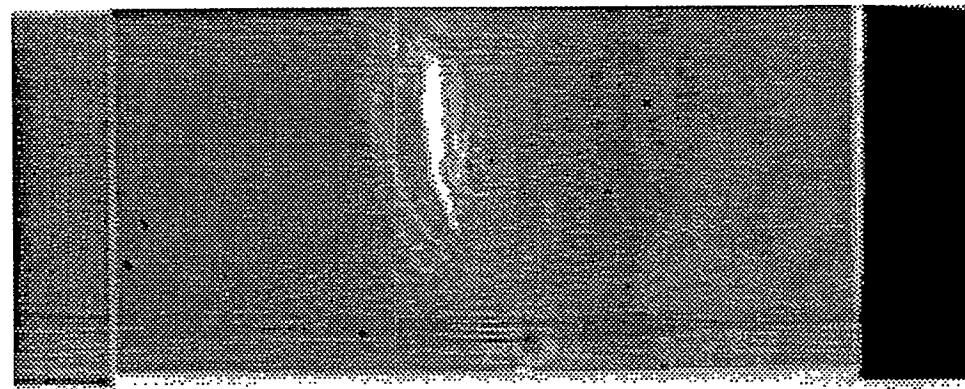


Figure 9: A tomographic image (CT scan) for a specimen of non-lithophysal Topopah Spring member tuff (TSw2) recovered from a depth of 873.4 feet from borehole UE25 NRG-5 at Yucca Mountain, NV.

Well: NRG-5
 Sample: NRG5-891-SNL-A
 Fluid: DRY
 File: N5891ADA

Length: 10.165 cm
 Conf Pr: 0.00 psi
 Pore Pr: 0.00 psi
 10-18-93 13: 41
 Temp: 22.00 C

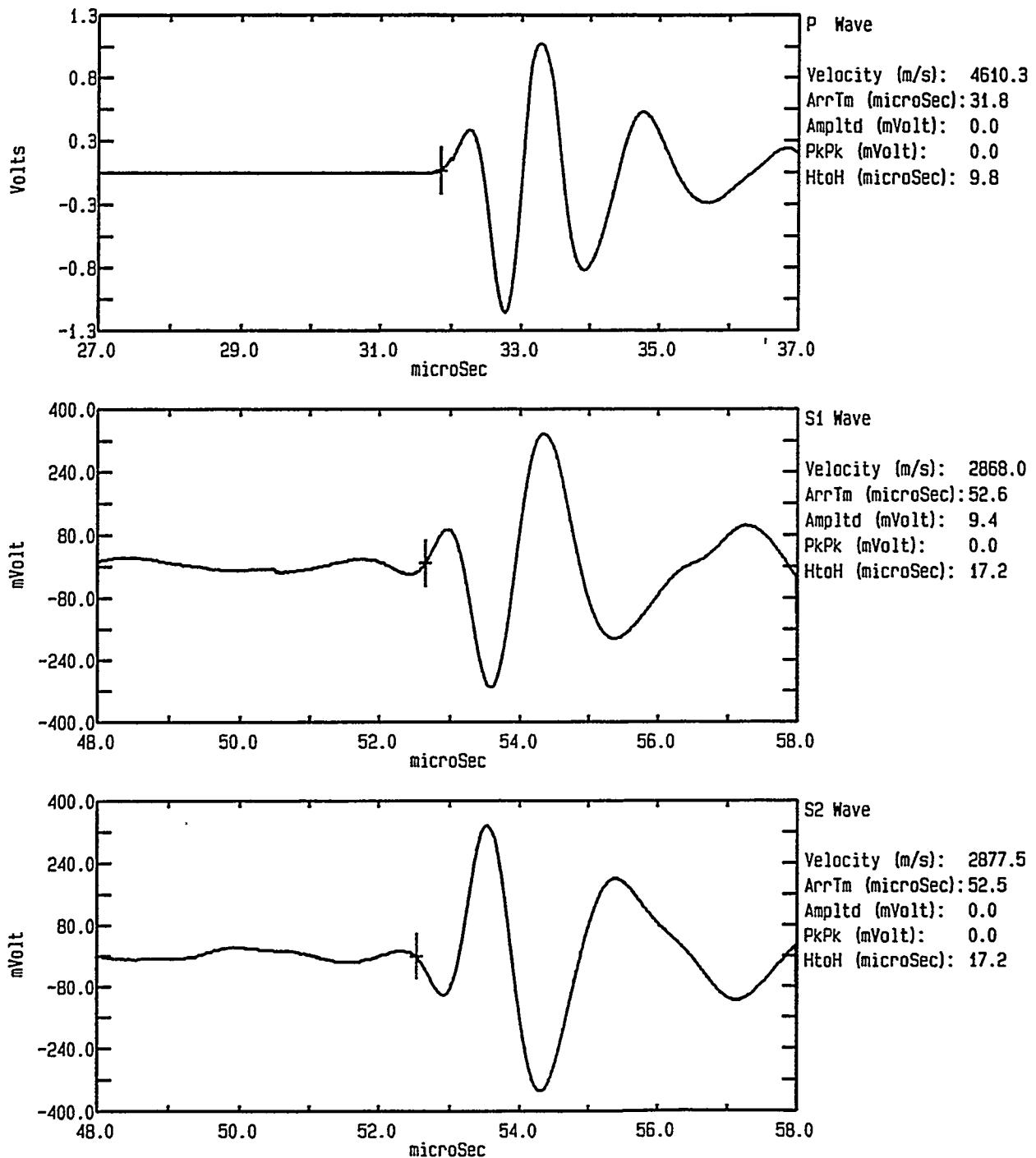


Figure 10: Time series for compressional and shear waves propagated parallel to the axis of a specimen of TSw2 recovered from a depth of 891.9 feet from borehole UE25 NRG-5, Yucca Mountain, NV.

Well: NRG-5
 Sample: NRG5-891-SNL-A Length: 5.077 cm Conf Pr: 0.00 psi
 Fluid: DRY Pore Pr: 0.00 psi
 File: N5891ADR 10-18-93 13:30 Temp: 22.00 C

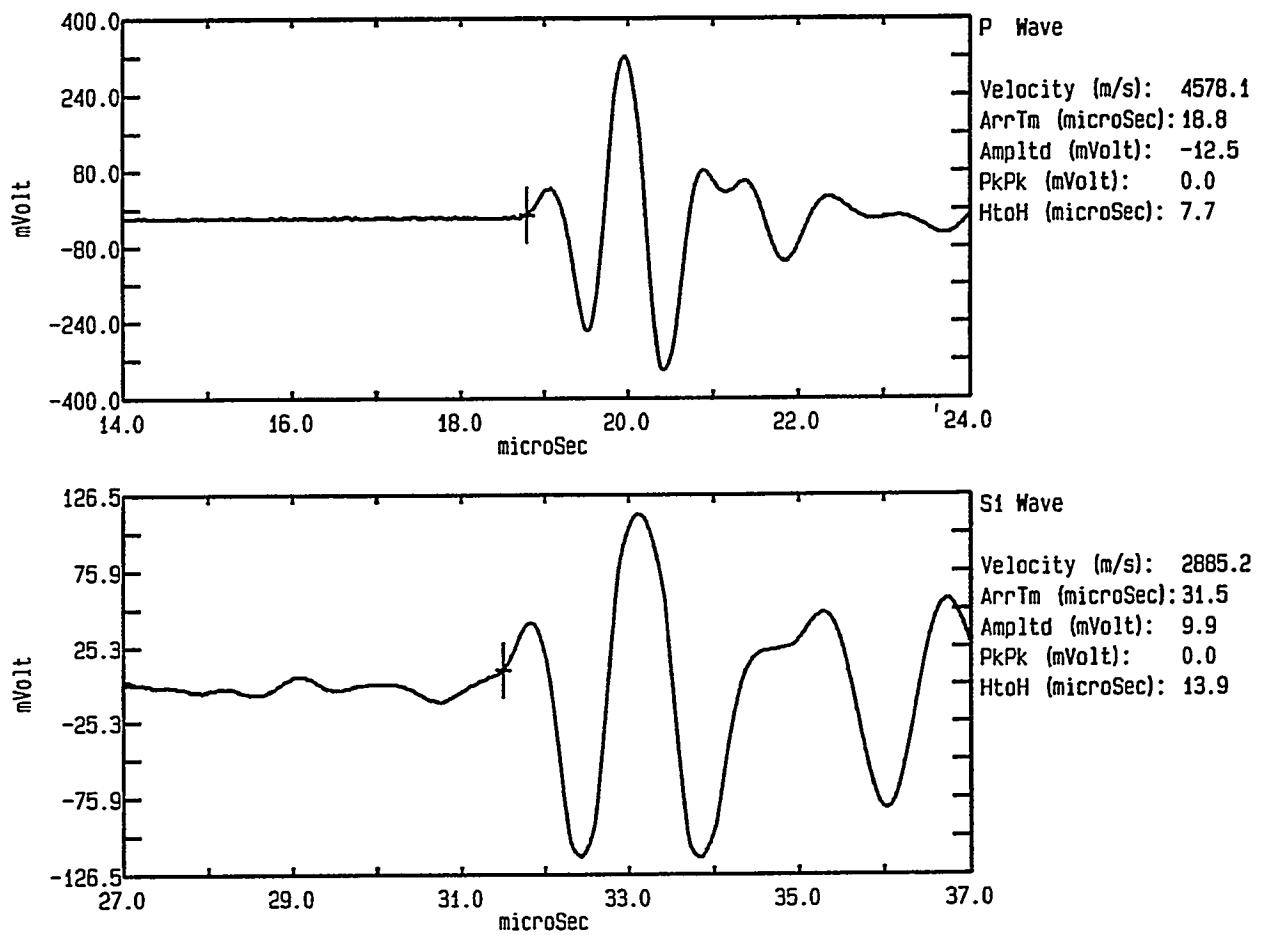


Figure 11: Time series for compressional and shear waves propagated normal to the axis of a specimen of TSw2 recovered from a depth of 891.9 feet from borehole UE25 NRG-5, Yucca Mountain, NV.

waves propagated normal to the core axis. Both figures display the output voltage of the receiver transducer as a function of time in microseconds. The data show that there is no elastic anisotropy in the specimen; the P and S wave velocities are independent of propagation direction, to within the accuracy of the measurement.

3.3 Unconfined Compression Tests

The plots of representative data sets for two specimens tested in unconfined compression are presented in Figures 12 and 13. Figure 12 shows the data for a high porosity (22.1%) saturated specimen of TSw1 recovered from borehole UE25 NRG-4 at a depth of 541.0 feet. Four graphs are presented: axial stress vs axial strain; radial strain vs axial strain; axial strain vs time; and axial stress vs volumetric strain. The Young's modulus and fracture strength computed from these data are 14.6 GPa and 33.2 MPa, respectively. Poisson's ratio is computed from these data over the same stress interval as Young's modulus. Poisson's ratio is 0.34.

Figure 13 shows stress-strain data collected on a specimen of TSw2 recovered from UE25 NRG-5 from a depth of 891.9 feet. The data are in the same format as Figure 12. The Young's modulus and fracture strength computed from these data are 38.3 GPa and 253.5 MPa, respectively. Poisson's ratio, also computed between 10 and 50% of the fracture strength, is 0.15. It is important to note that the differences between the specimens is not the petrography but the porosity. Specimen NRG-4-541.0 has a porosity of 22.1%, whereas that of NRG-5-891.9 is 9.9%.

3.4 Confined Compression Tests

The results of confined compression tests on small-diameter specimens obtained from a core recovered from a depth of 527.0 feet in borehole UE25 NRG-4 are presented in Table 2. Specimens were tested at confining pressures of 5 and 10 MPa. The specimens have moderate porosity (15.2-19.2%) and are from the TSw1 thermal/mechanical unit. The differential stress at failure increased with increasing confining pressure.

3.5 Indirect Tensile Strength Tests

Thirty-five indirect tensile strength tests were performed on the cores recovered from boreholes UE25 NRG-4 and -5. The tensile strengths ranged between 0.1 (PTn) and 16.8 (TSw2) MPa. The weakest specimens were the nonwelded, high porosity units; the strongest were the low porosity, welded units.

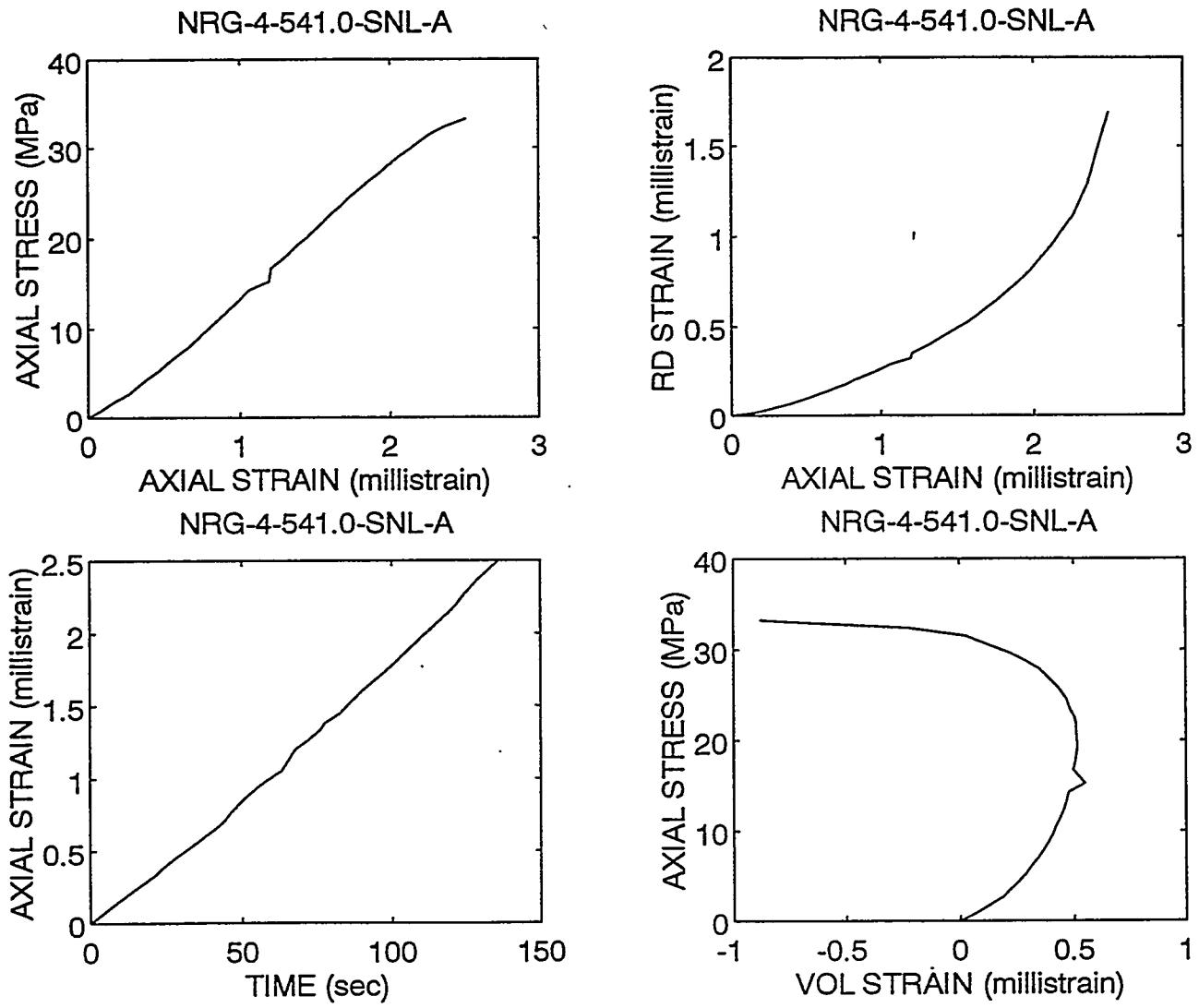


Figure 12: Axial stress and radial strain are plotted as a function of axial strain, axial strain as a function of time, and axial stress as a function of volumetric strain for a specimen of TSw1 tested in unconfined compression. The specimen was recovered from a depth of 541.0 feet from borehole UE25 NRG-4, Yucca Mountain, NV.

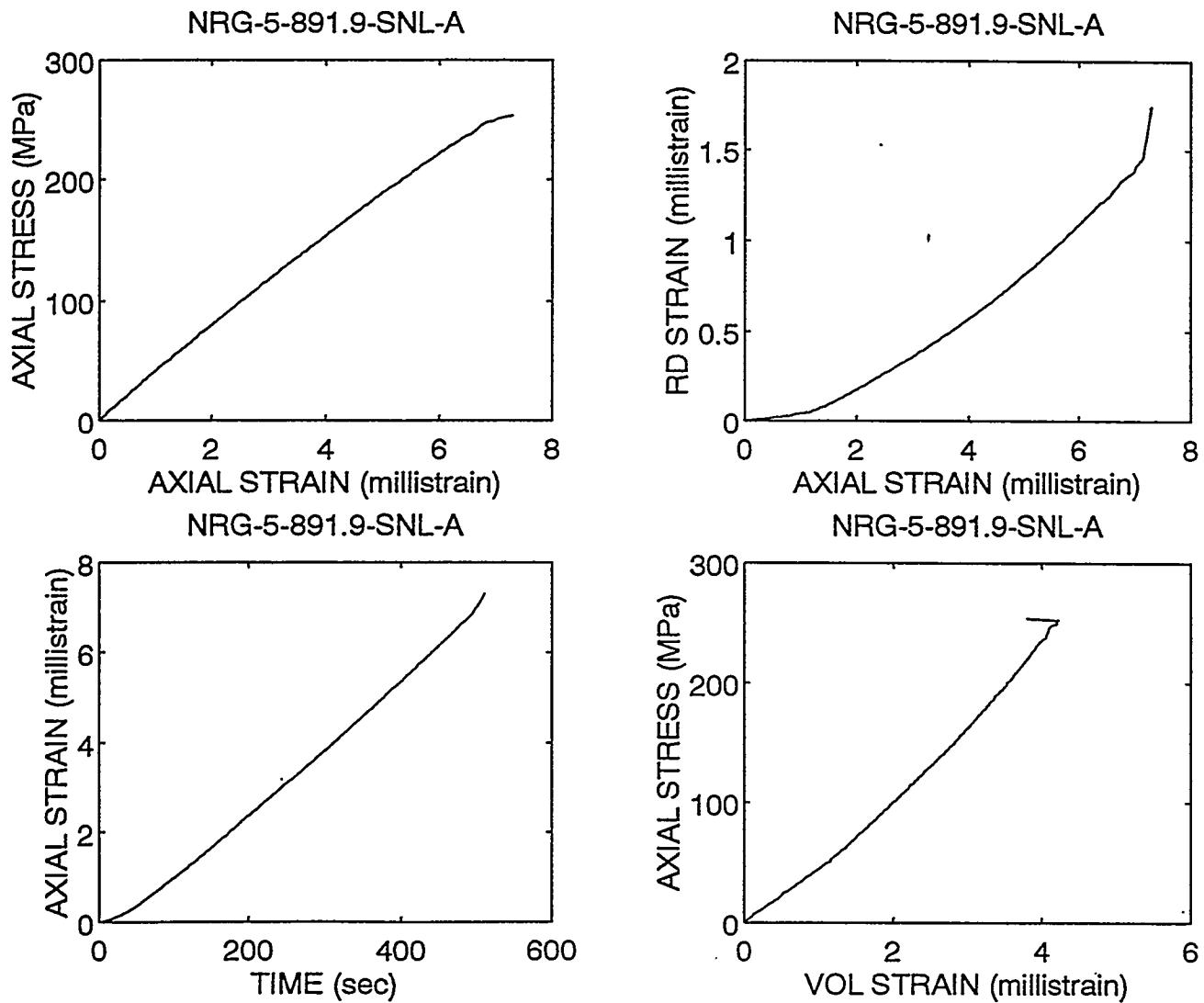


Figure 13. Axial stress and radial strain are plotted as a function of axial strain, axial strain as a function of time, and axial stress as a function of volumetric strain for a specimen of TSw2. The specimen was recovered from a depth of 891.9 feet from borehole UE25 NRG-5, Yucca Mountain, NV.

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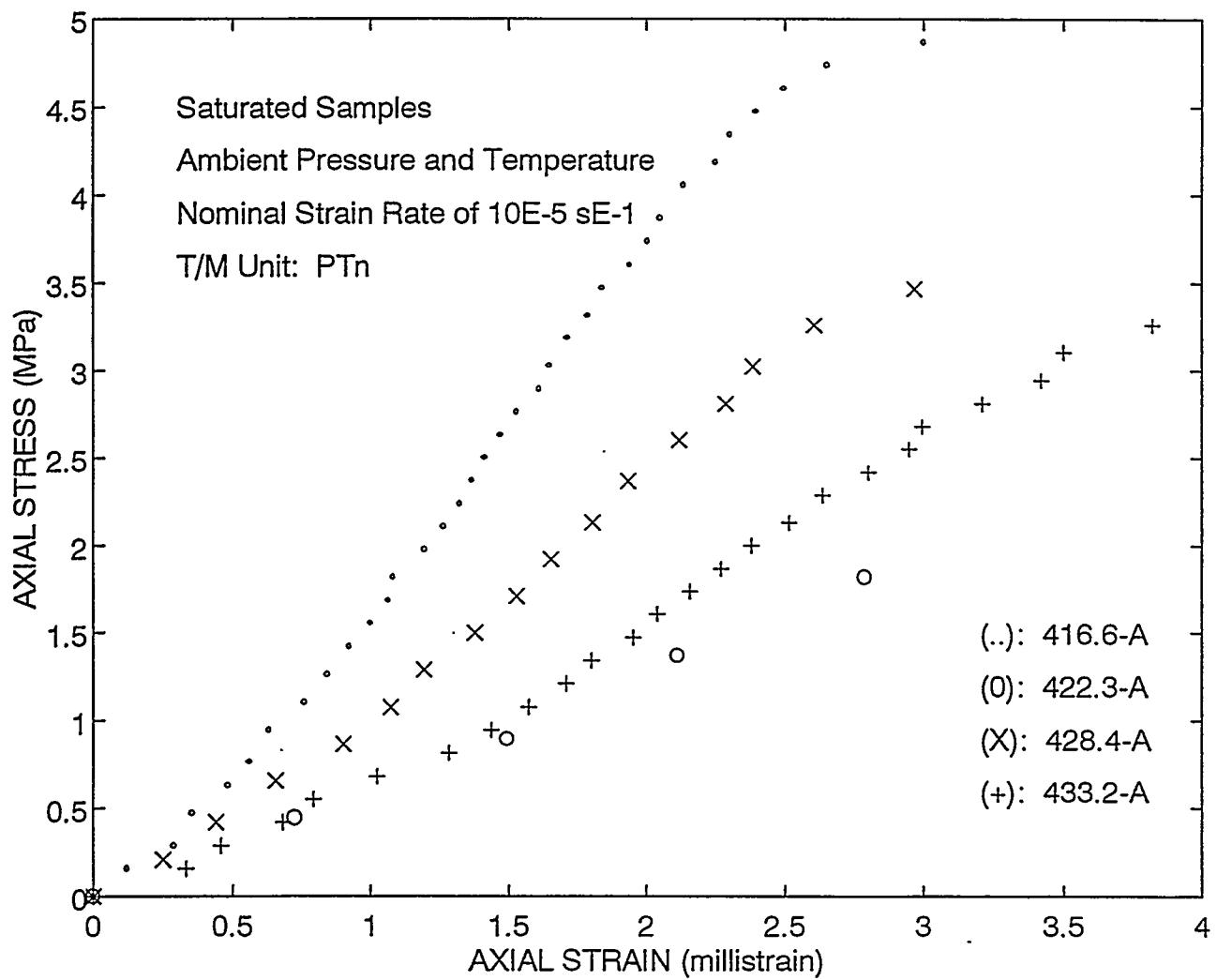
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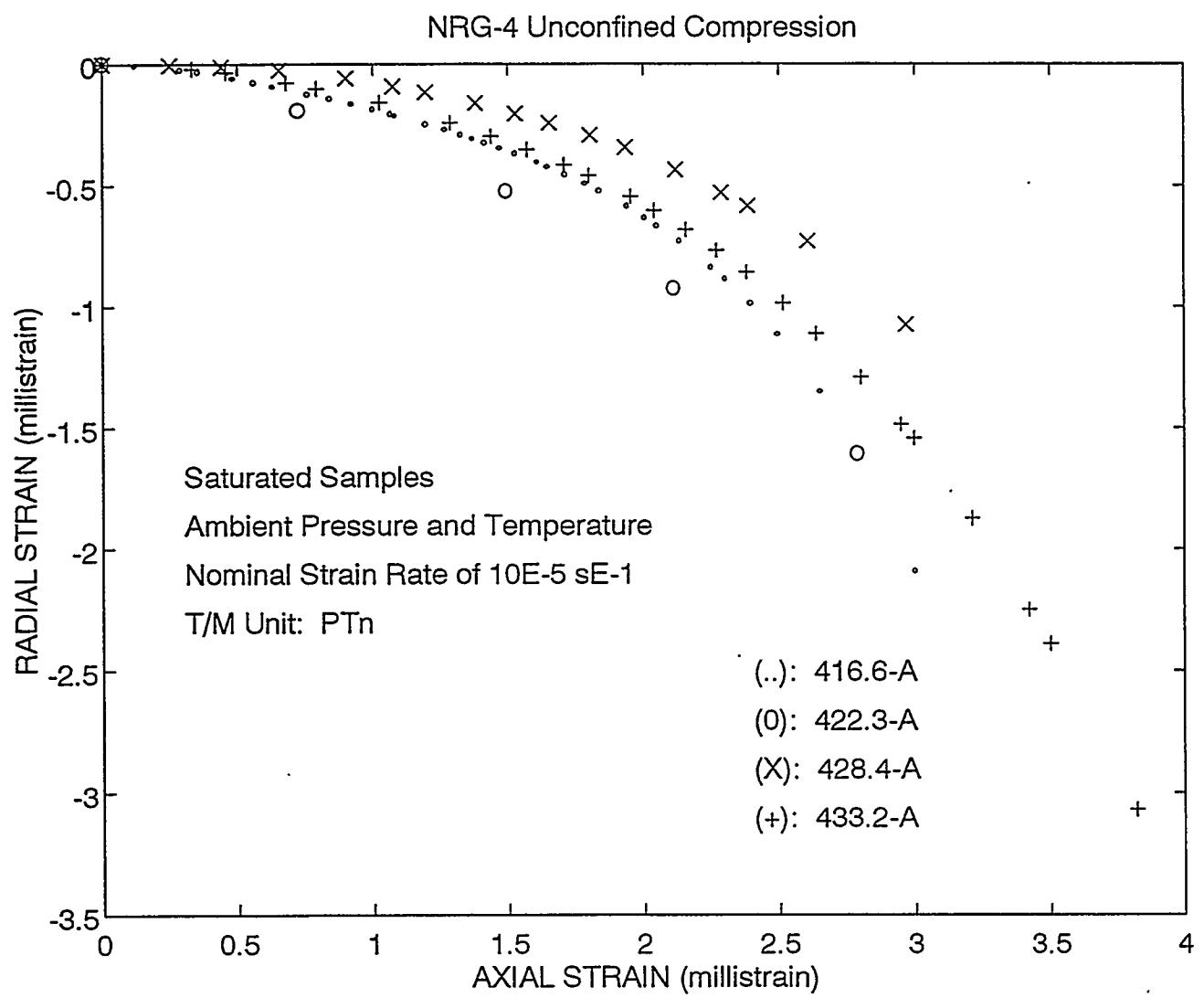
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APPENDIX I

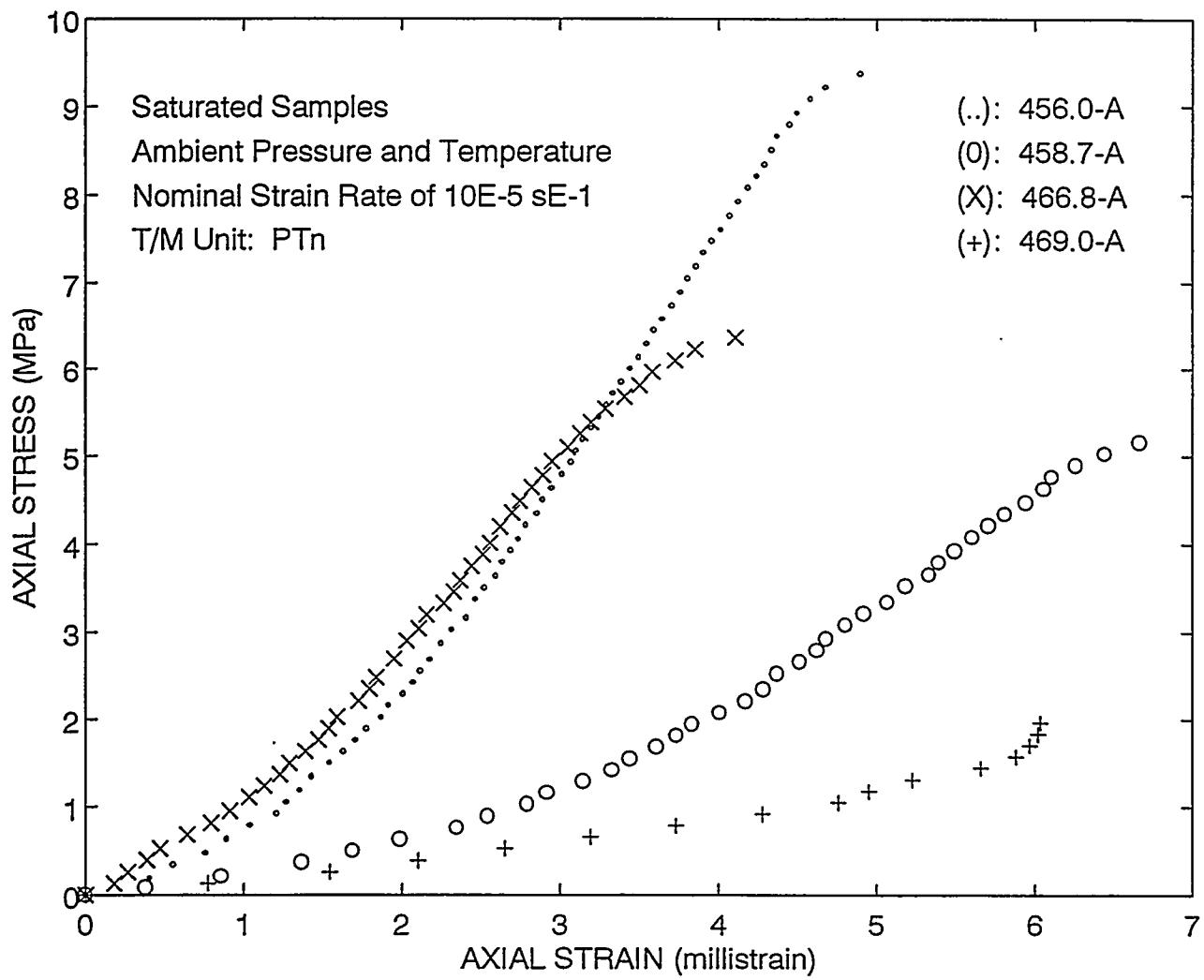
Stress vs Axial Strain and Radial Strain vs Axial Strain Plots for Unconfined Compression Experiments

NRG-4 Unconfined Compression

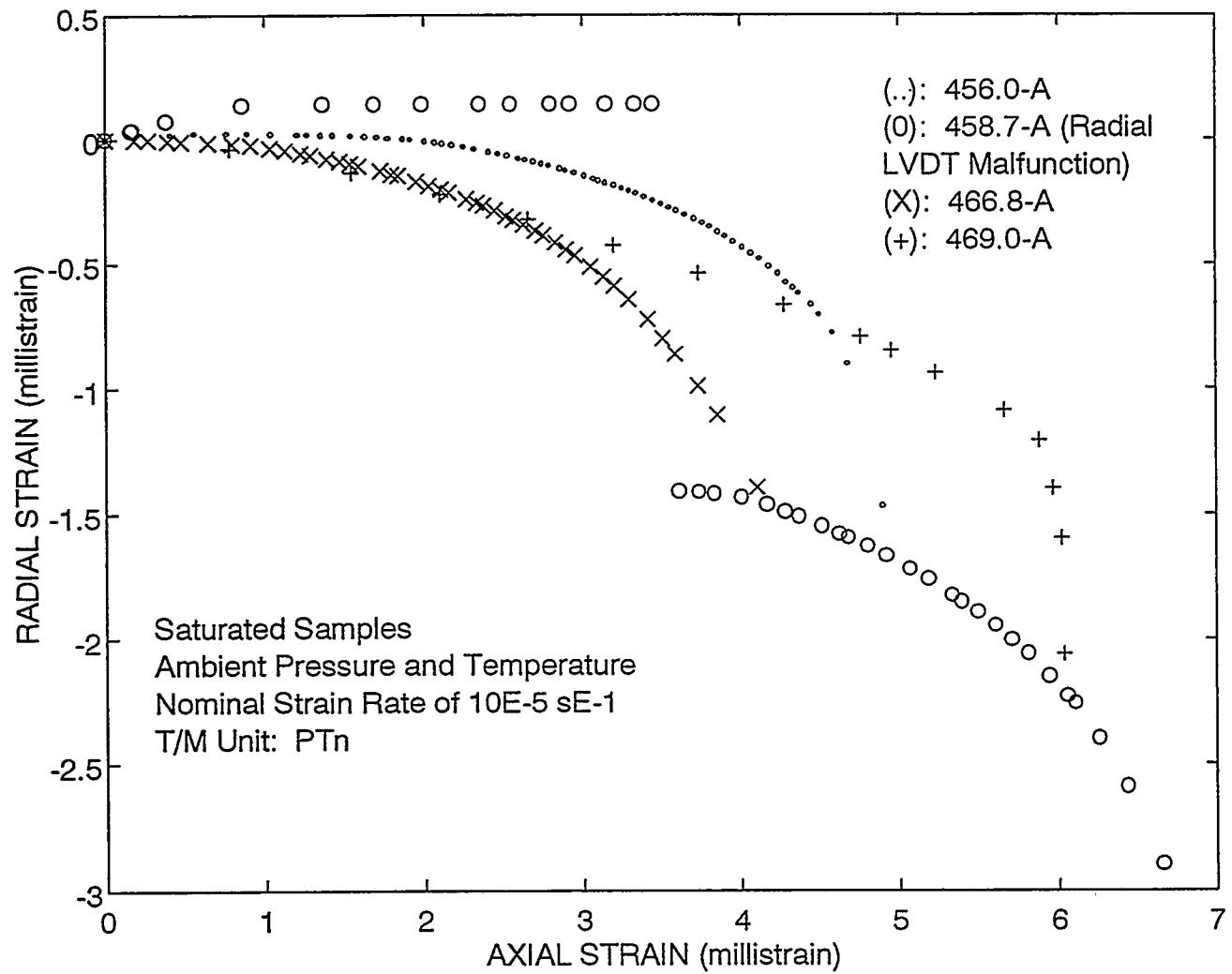




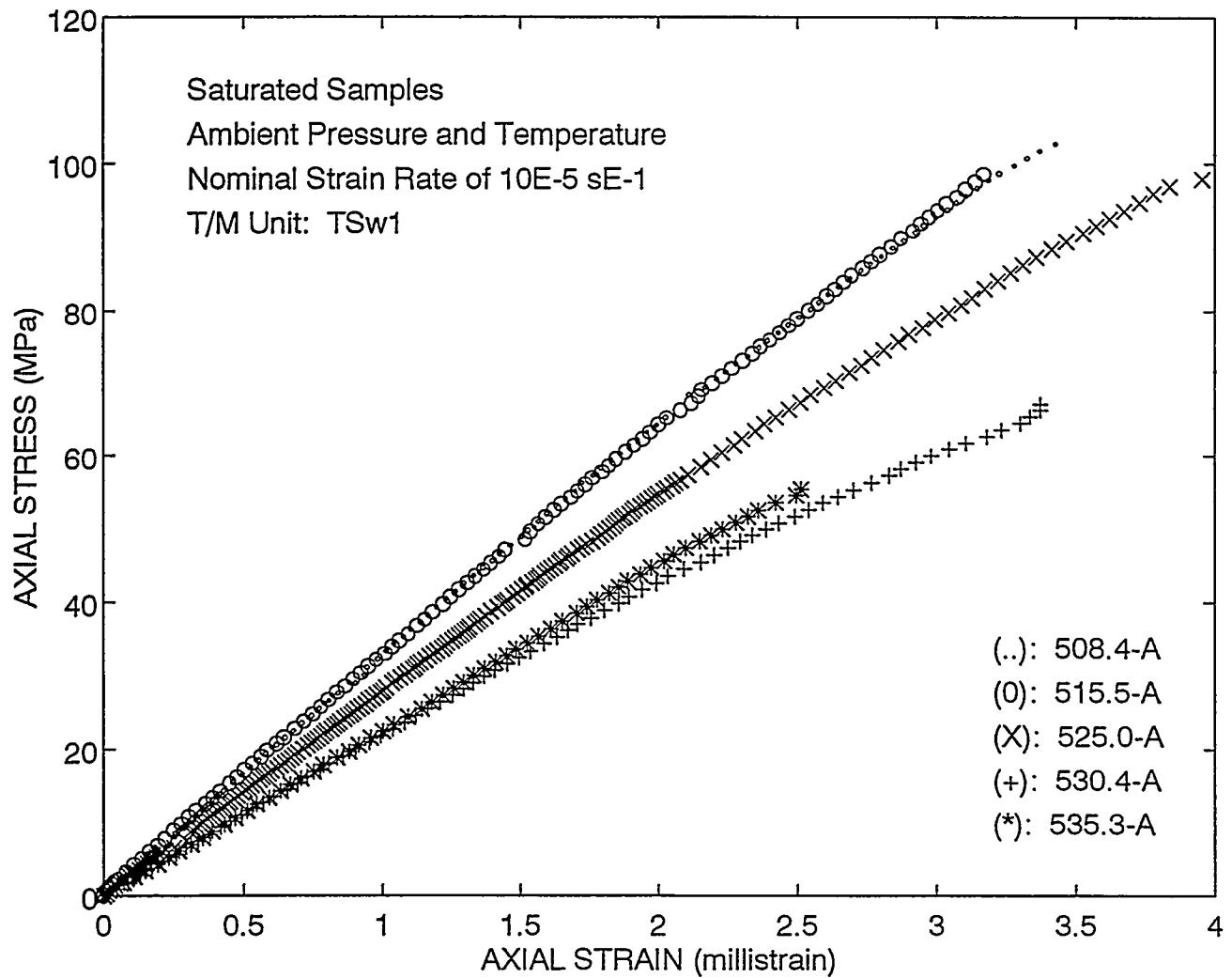
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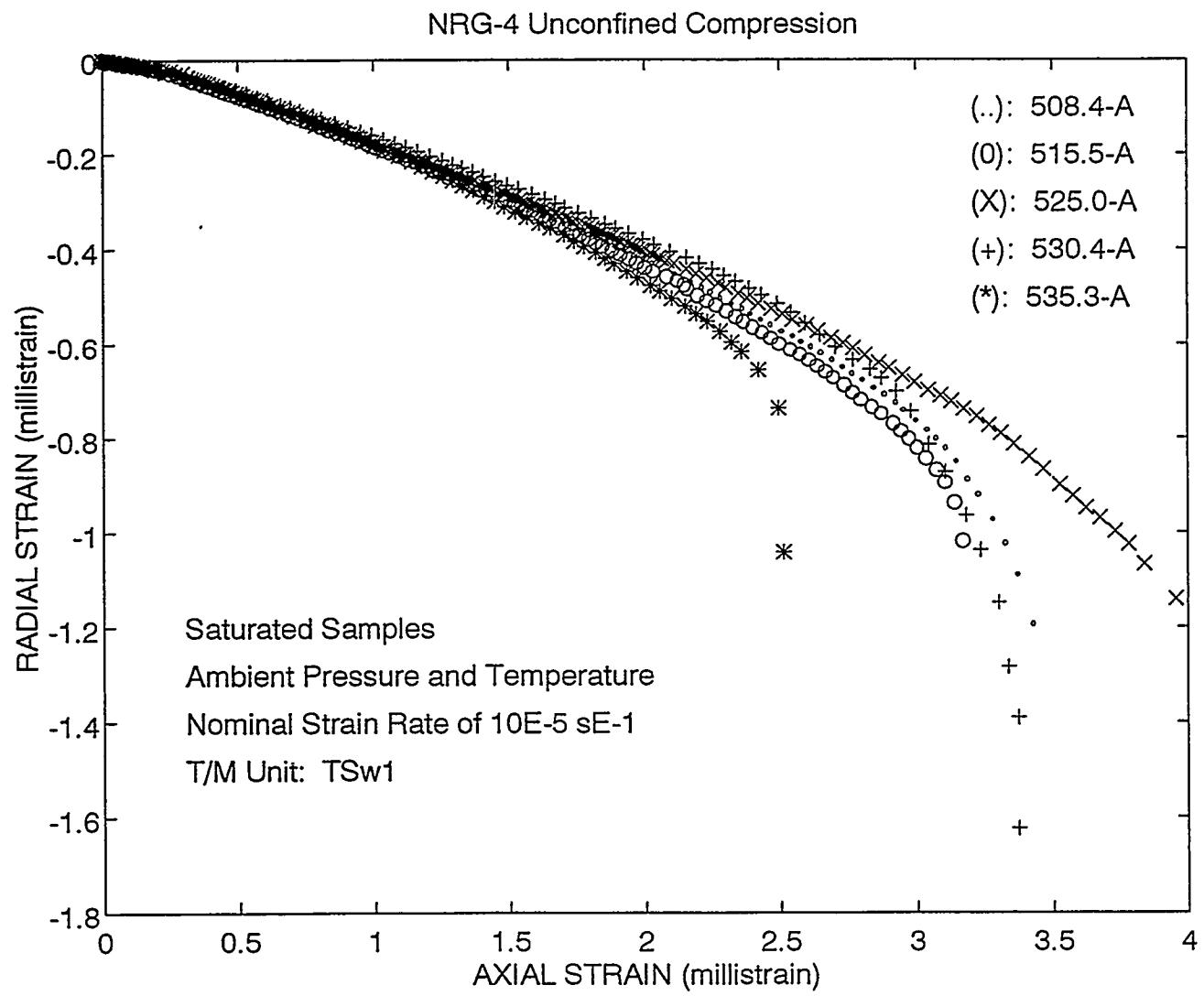


NRG-4 Unconfined Compression

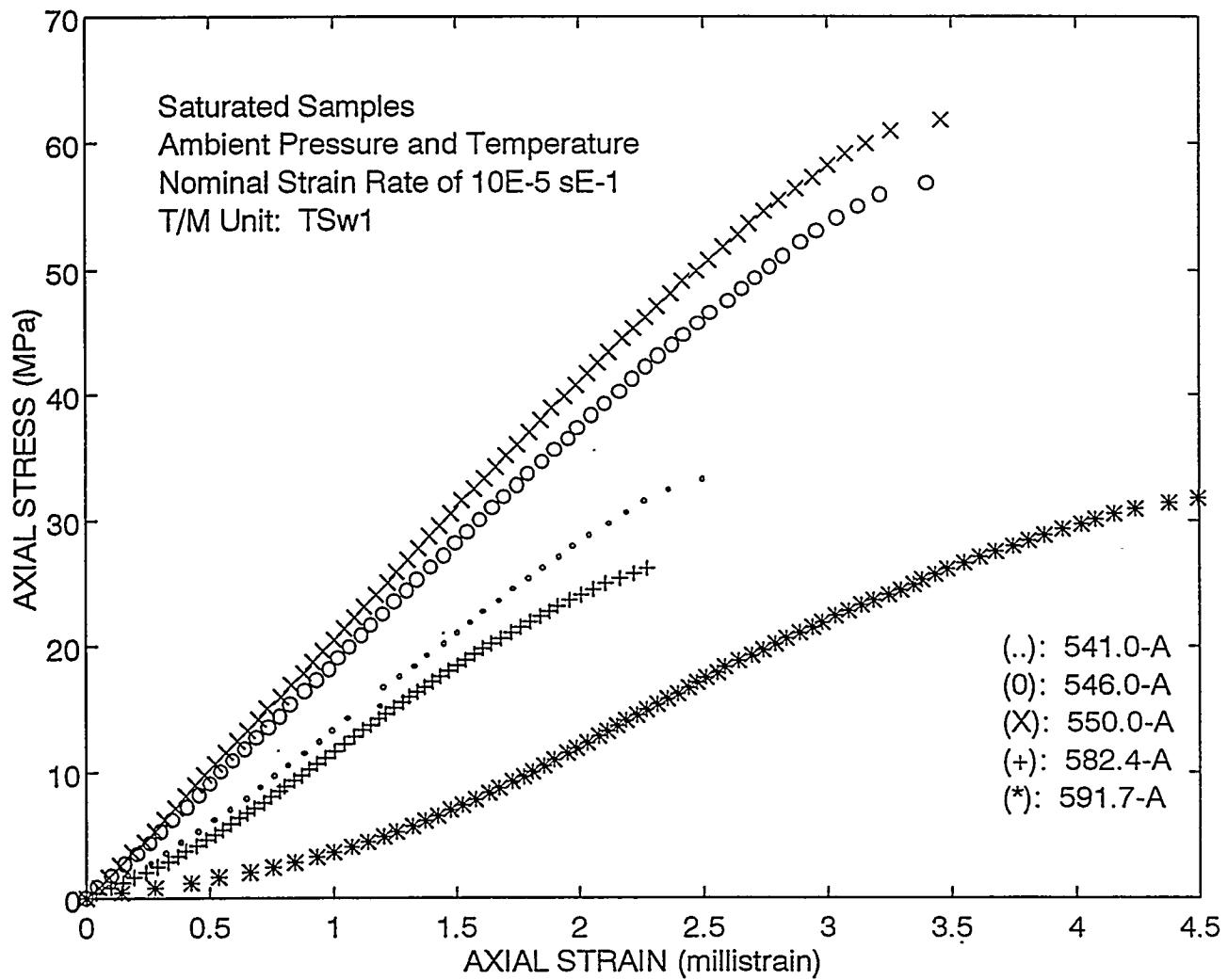


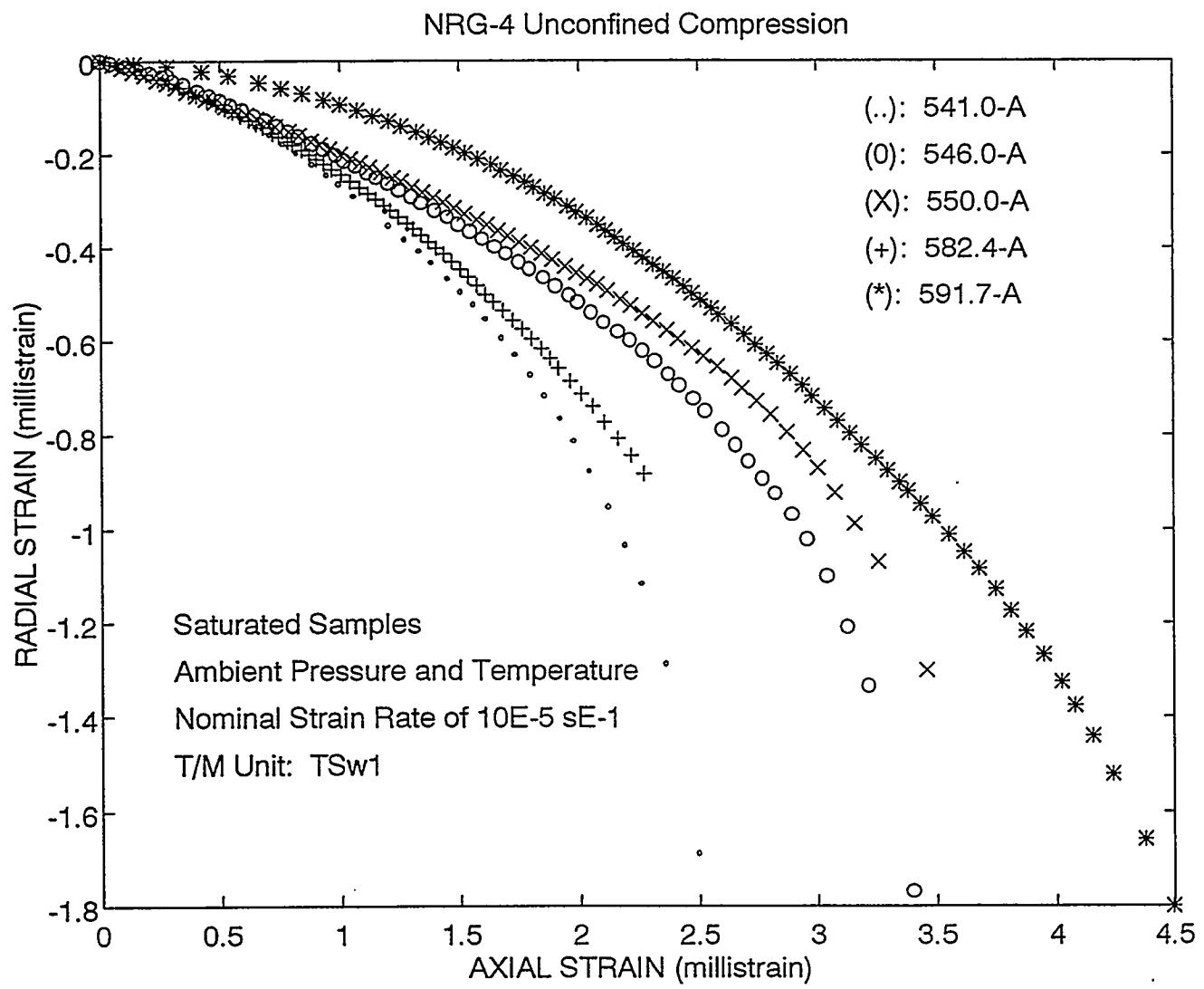
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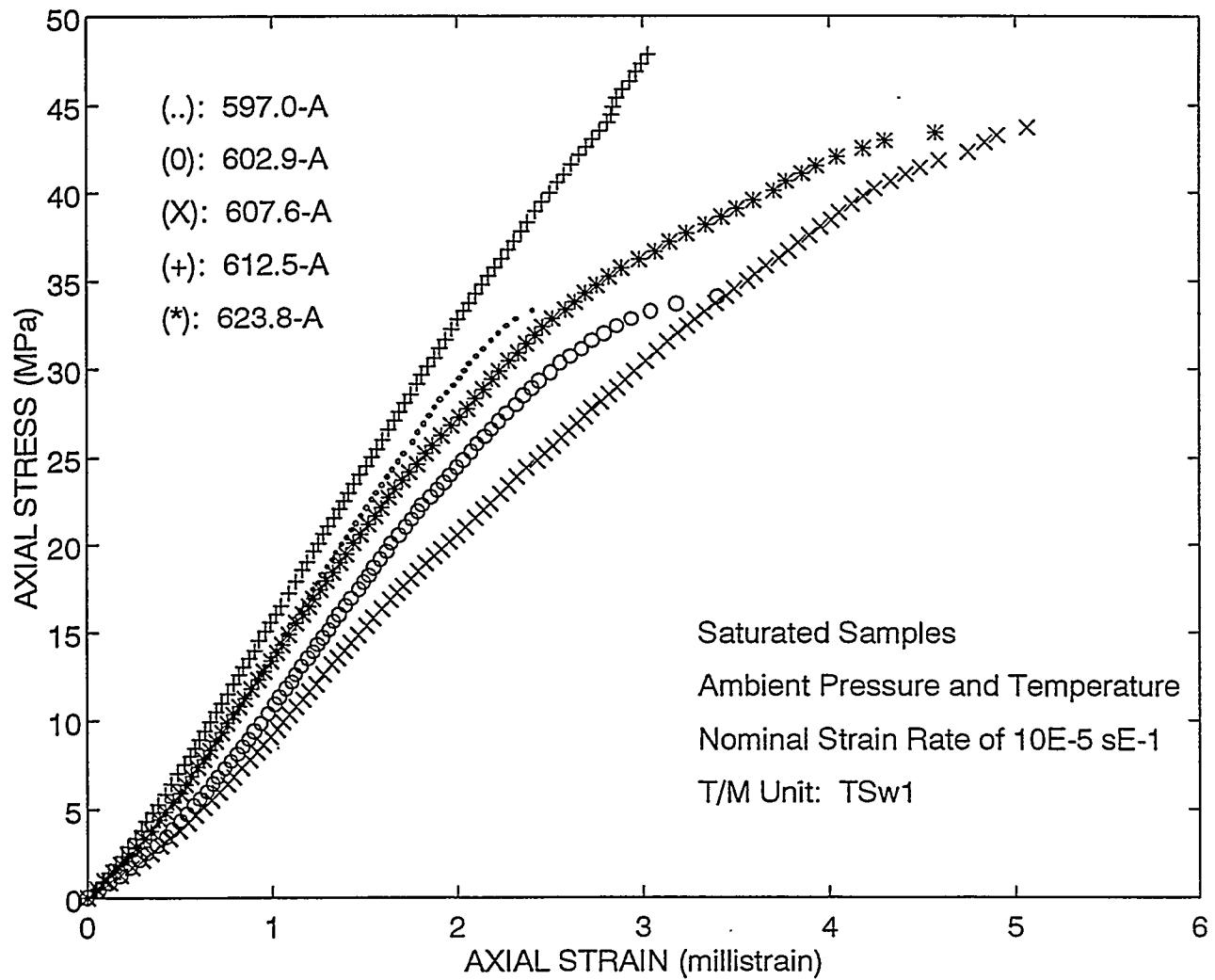


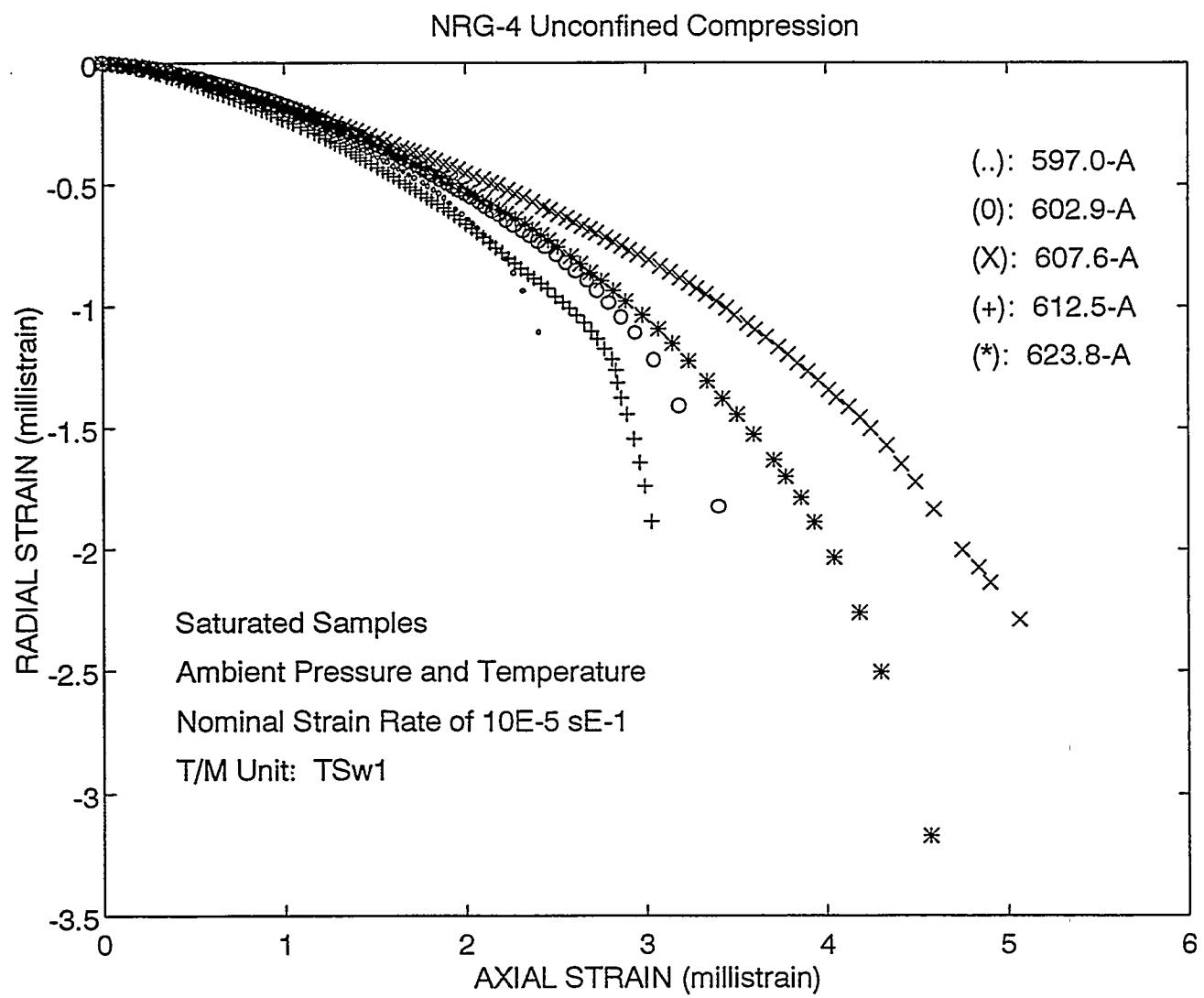
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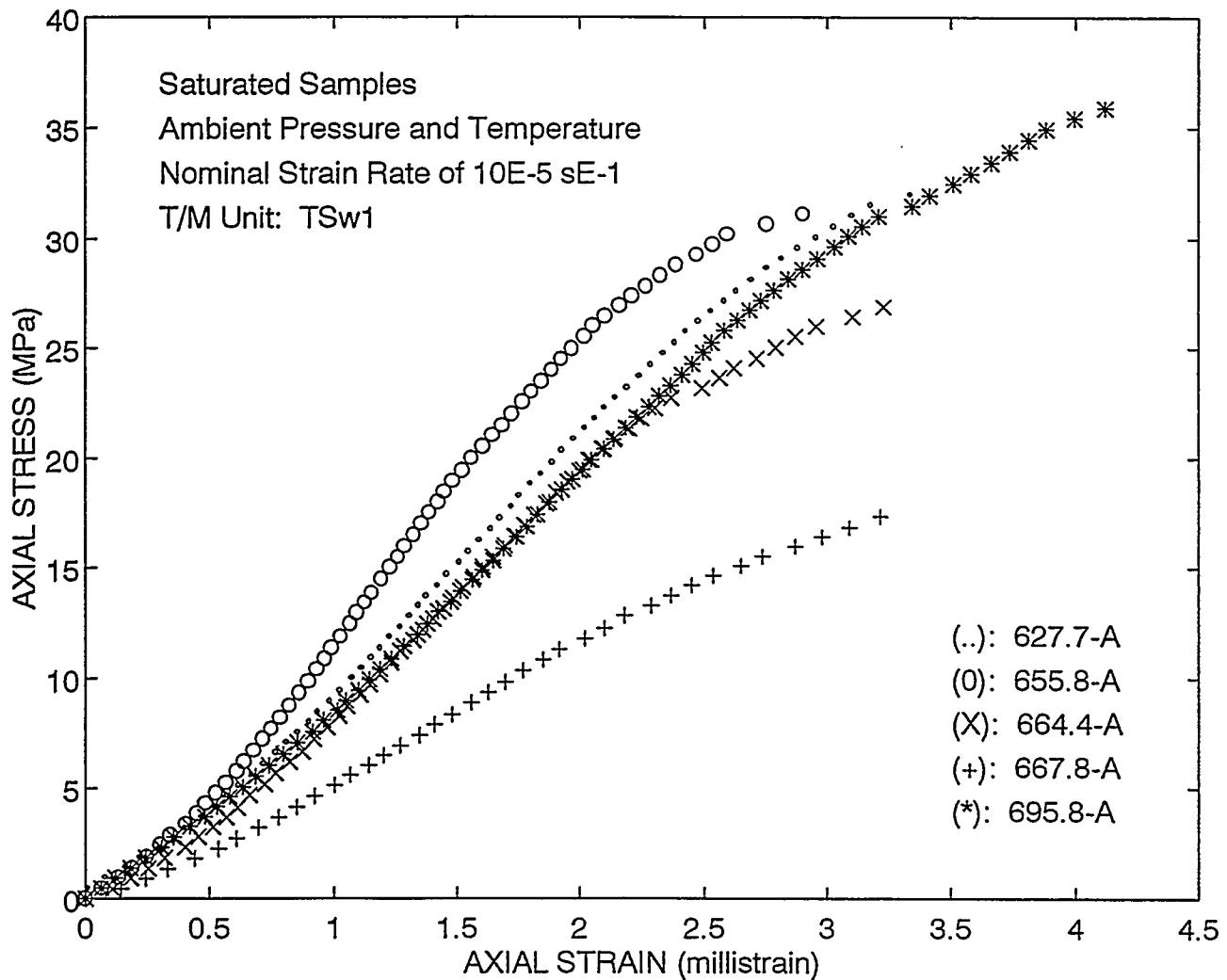


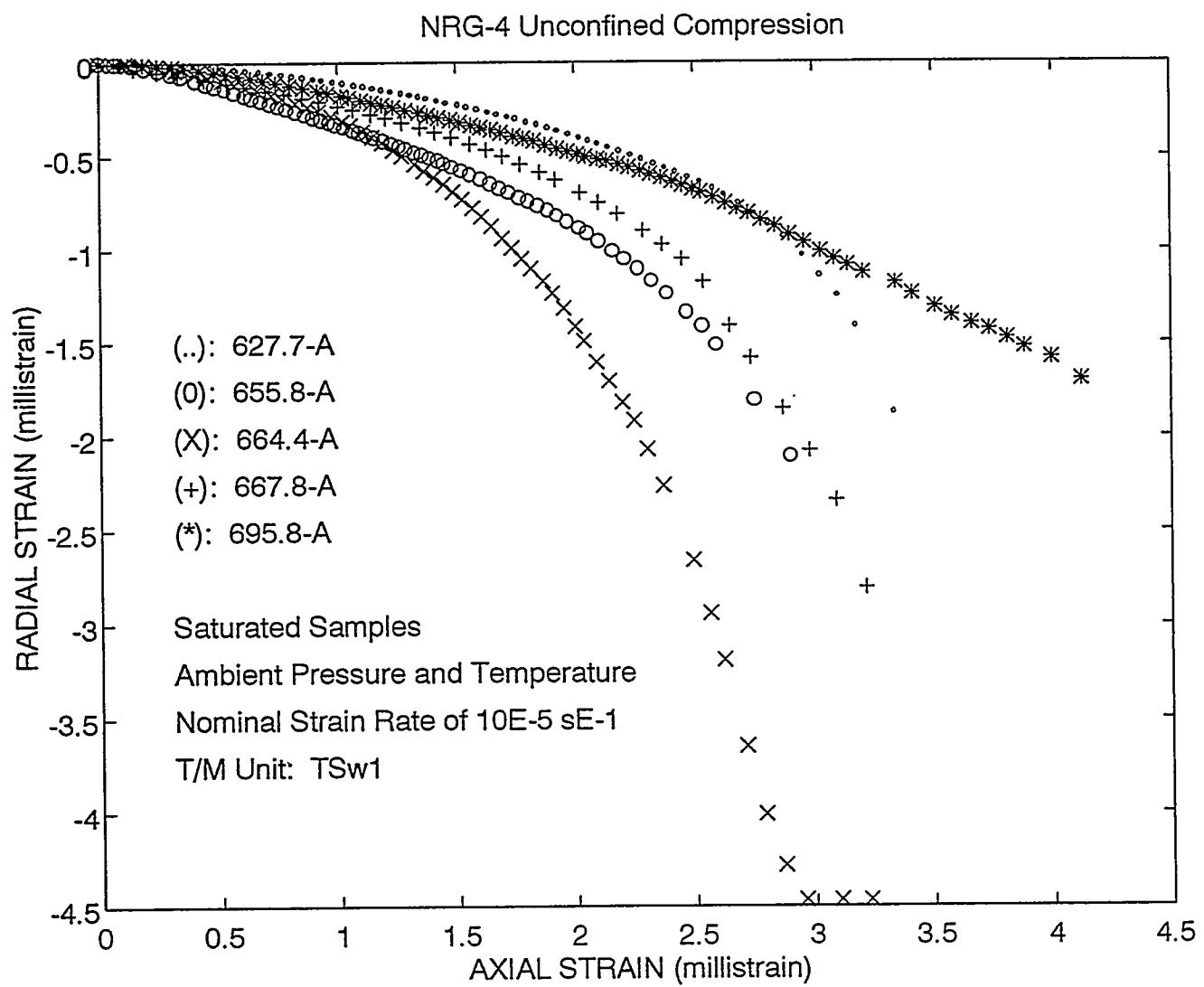
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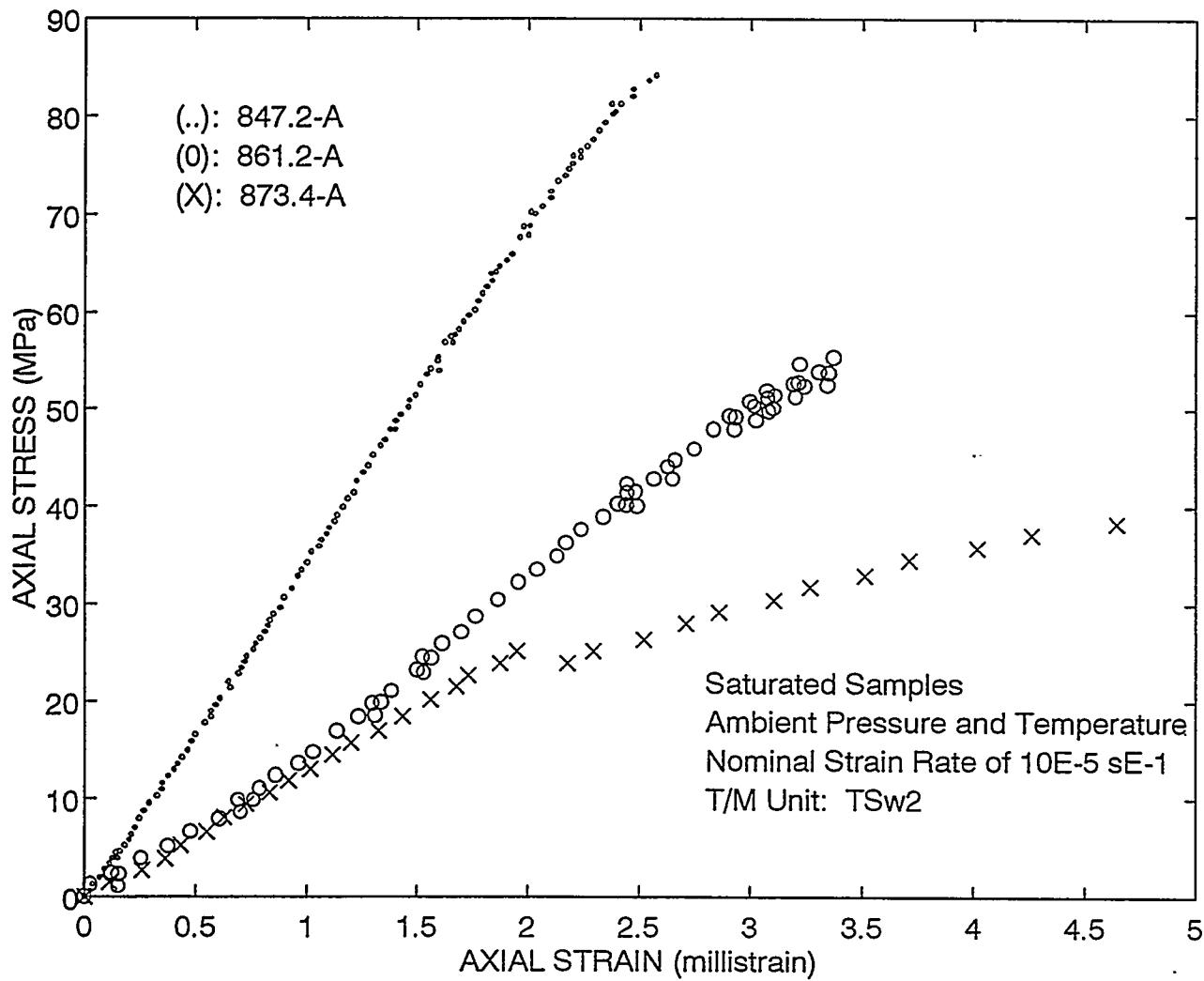


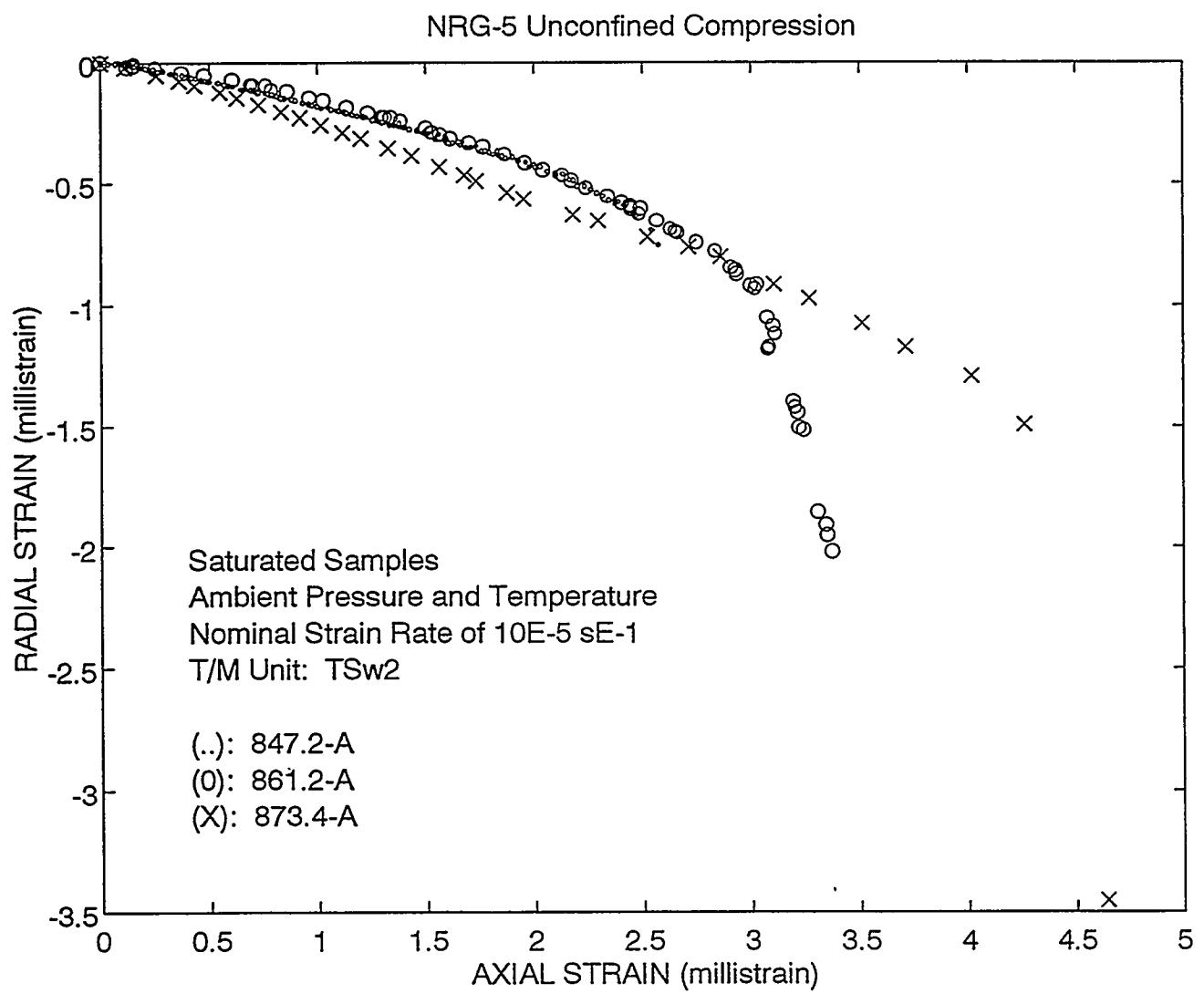
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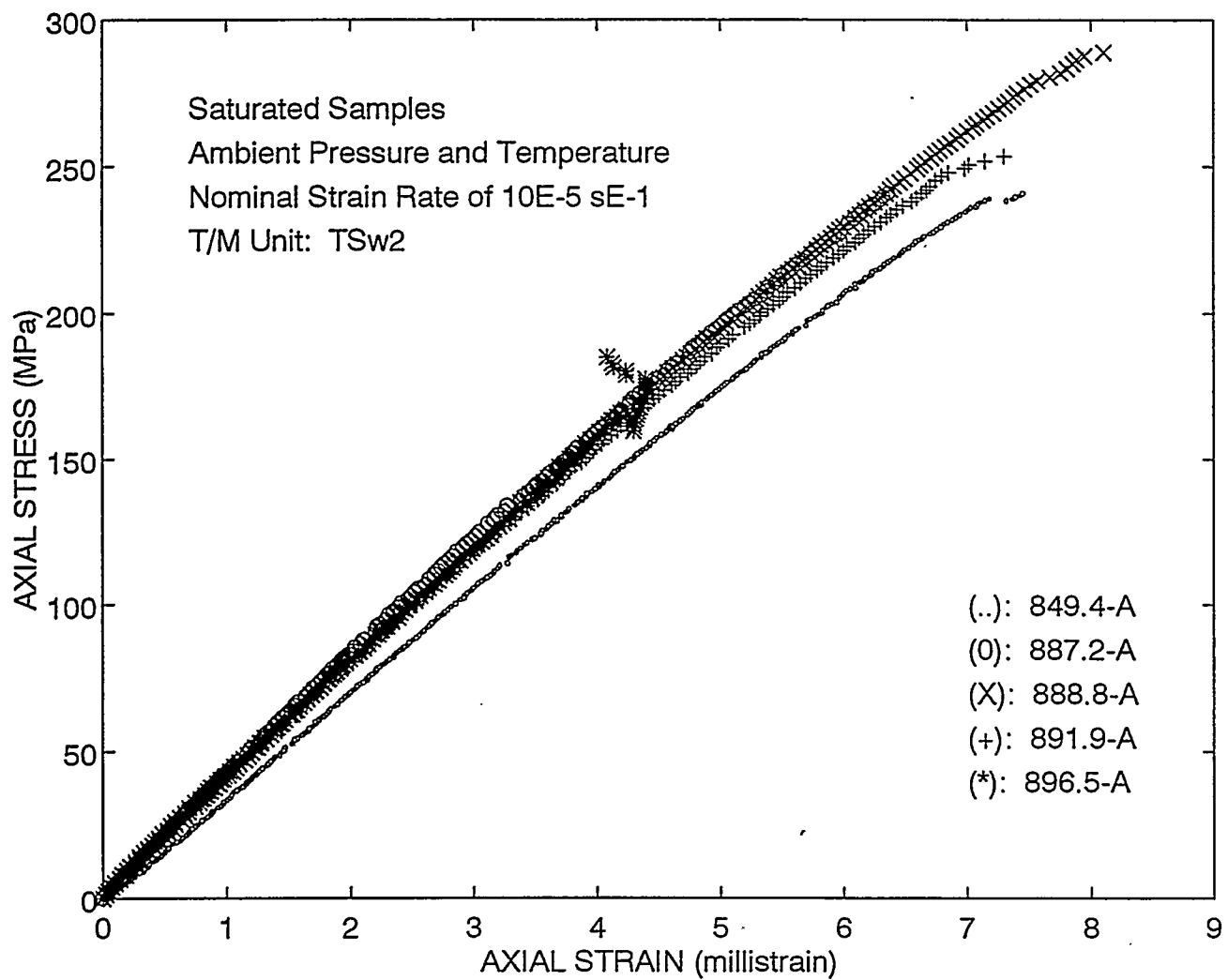


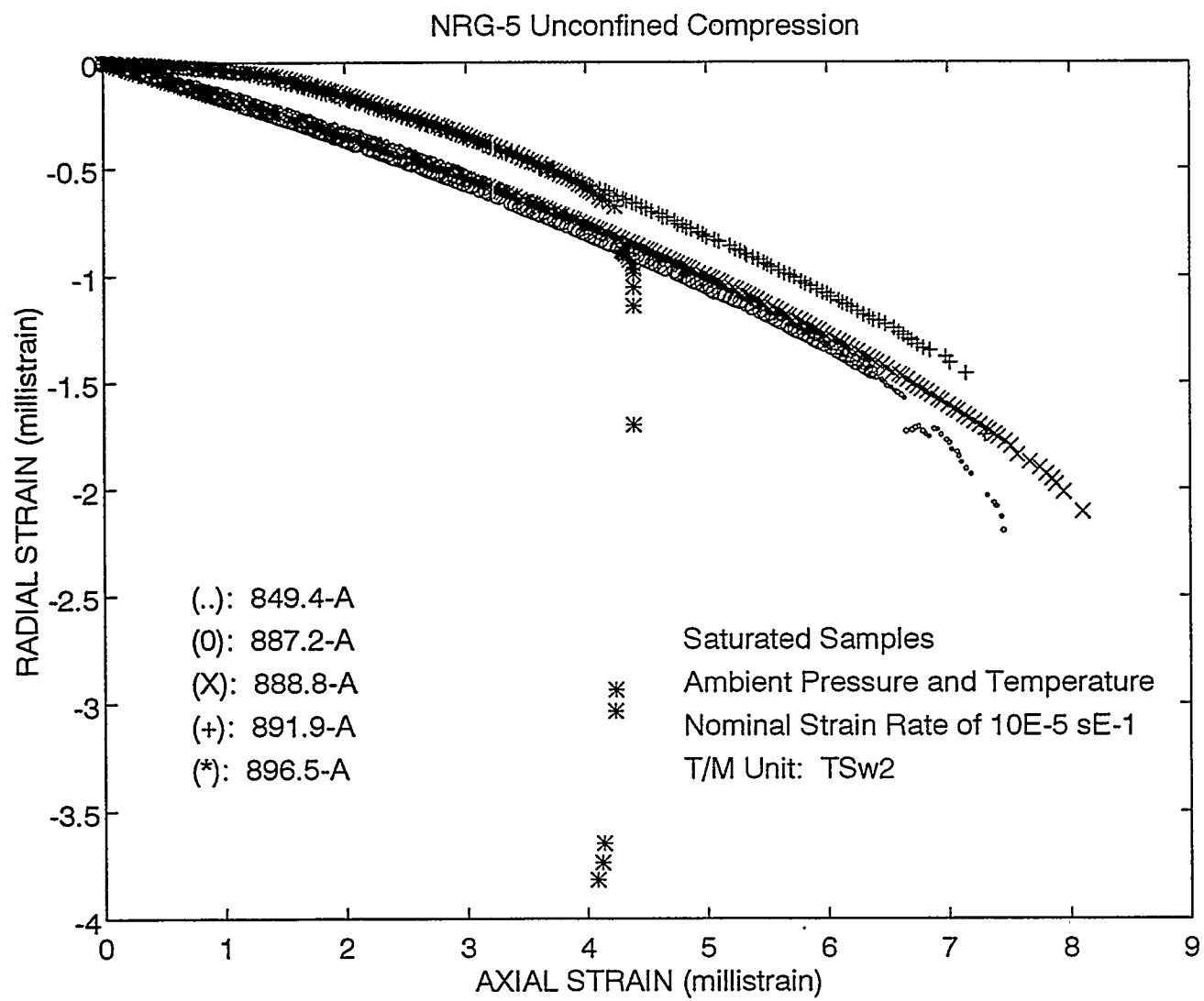
NRG-5 Unconfined Compression





NRG-5 Unconfined Compression

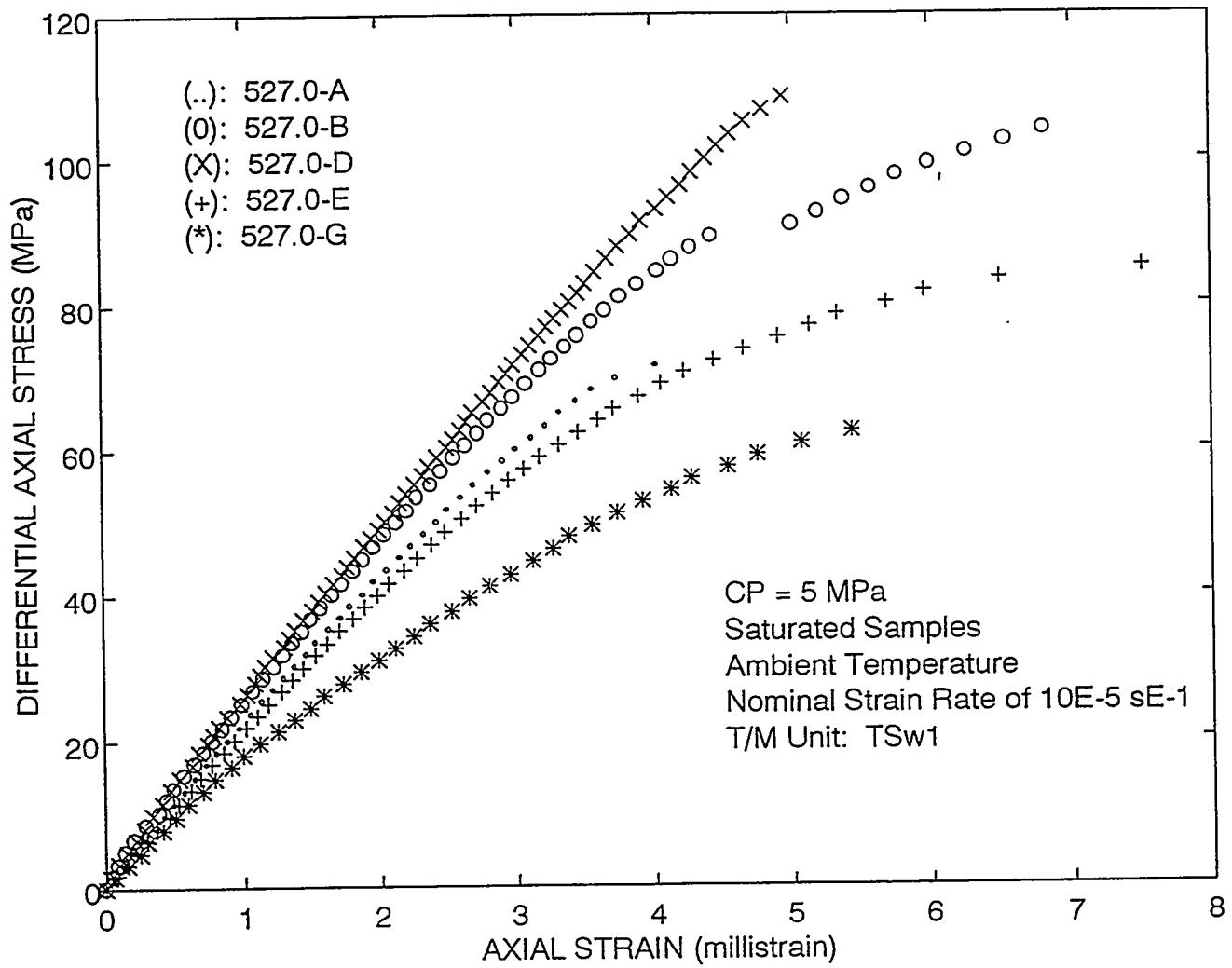




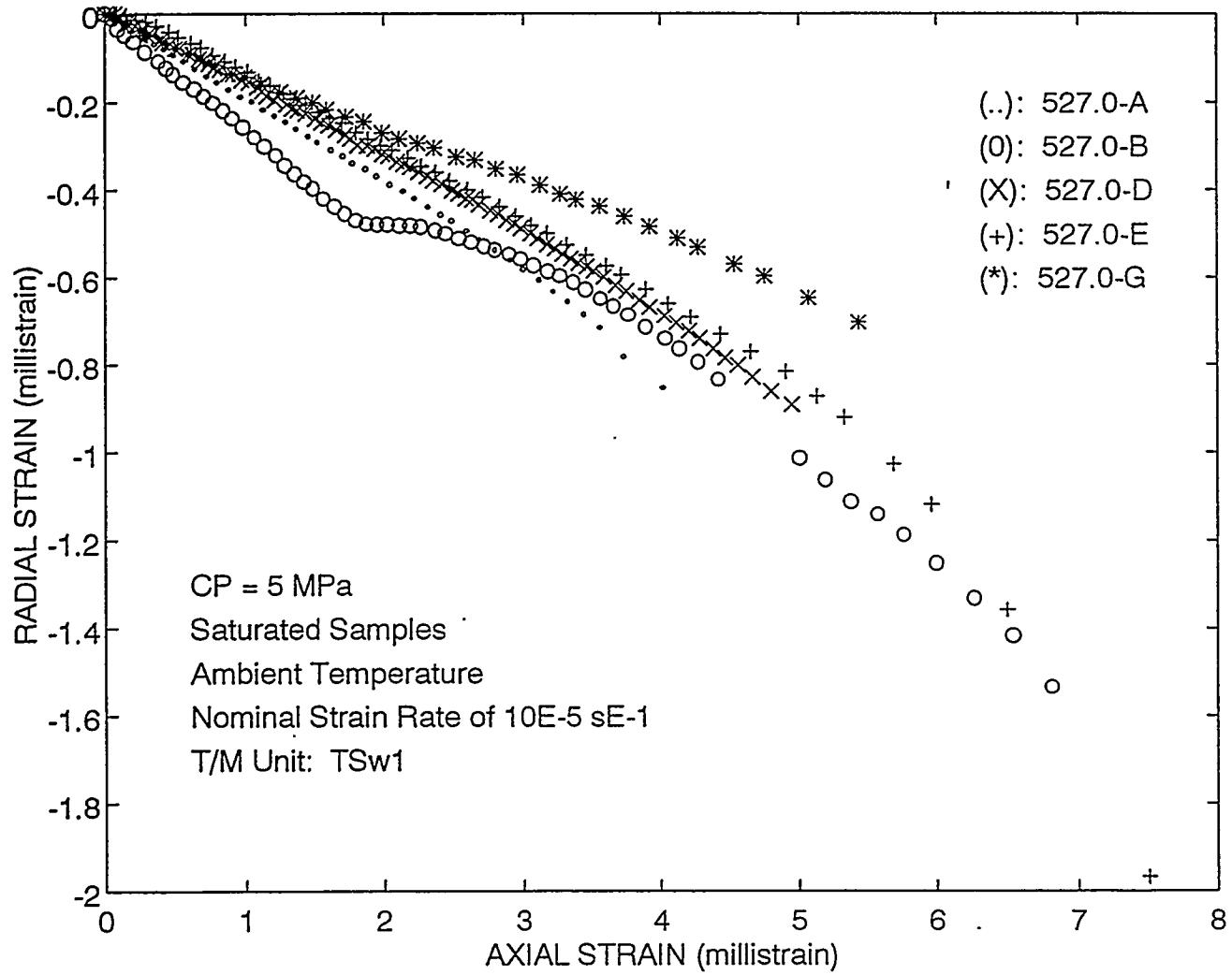
APPENDIX II

Stress vs Axial Strain and Radial Strain vs Axial Strain Plots for Confined Compression Experiments

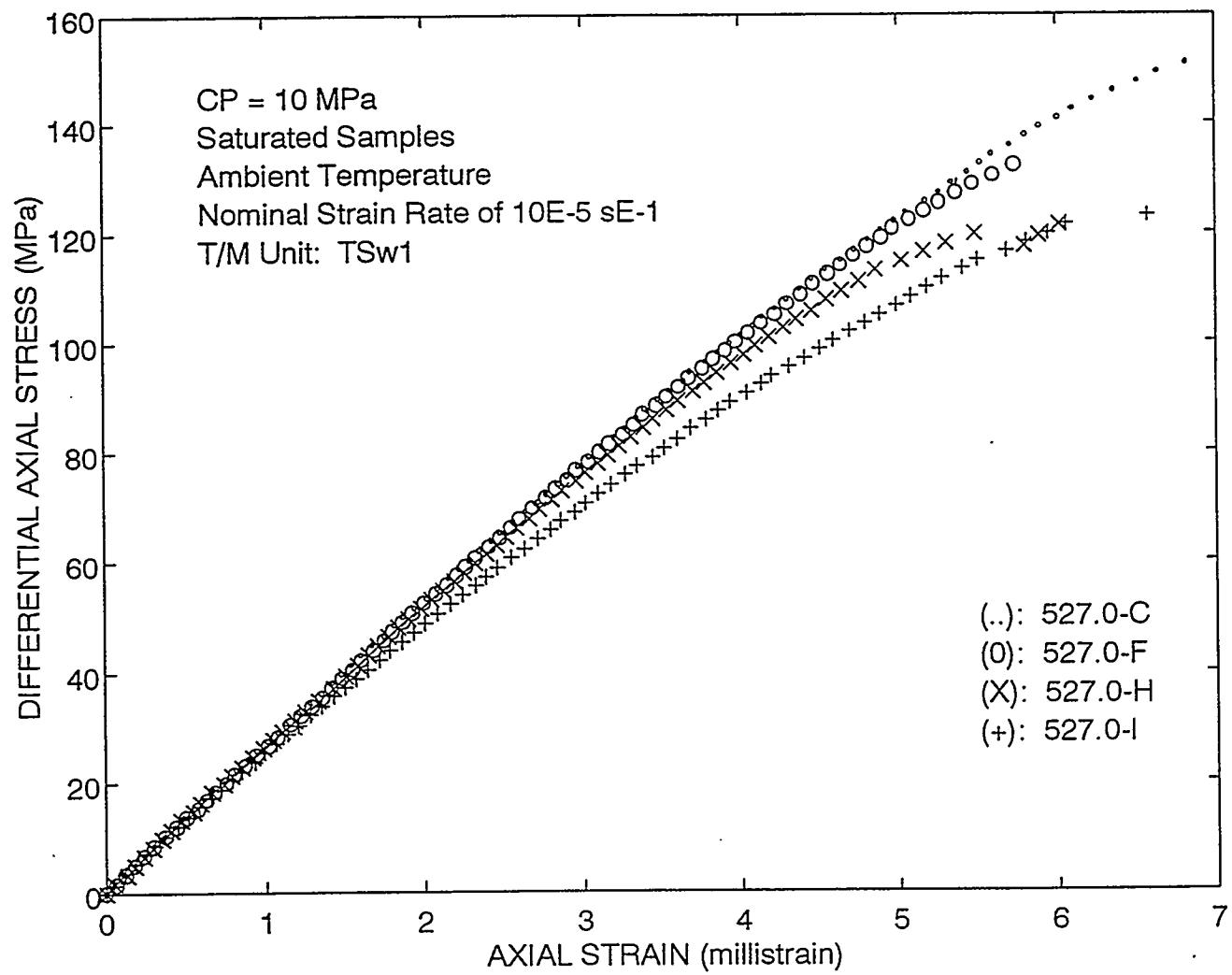
NRG-4 Confined Compression



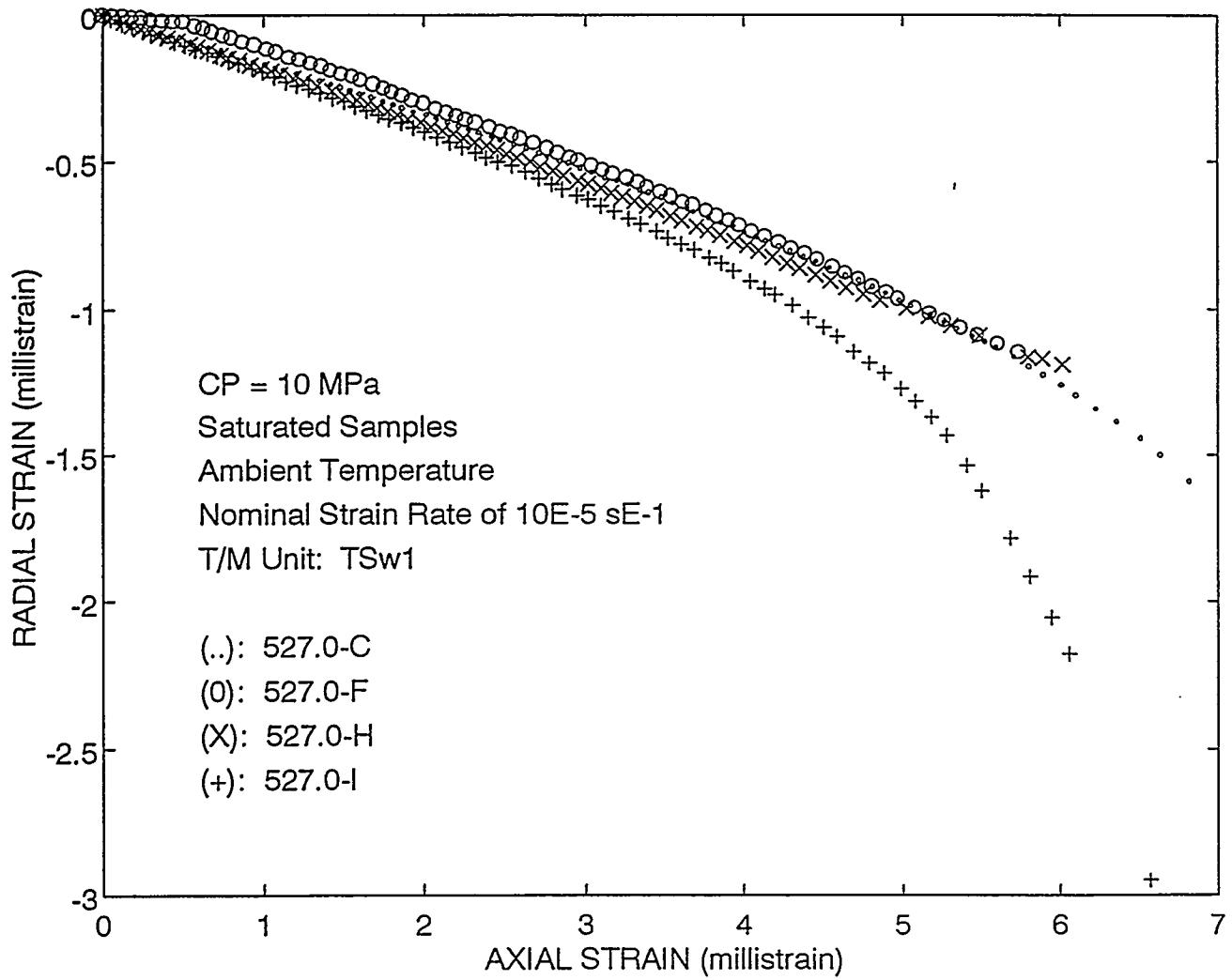
NRG-4 Confined Compression



NRG-4 Confined Compression



NRG-4 Confined Compression



APPENDIX III

System Checks Using an Aluminum Standard Specimen

System Checks Using an Aluminum Standard Specimen

Unconfined compression experiments were performed on a specimen of 6061-T6511 aluminum. The specimen was monotonically loaded at a constant strain rate of 10^{-5} s⁻¹ to 138 MPa, (i.e., approximately one-half of its yield stress). Young's modulus and Poisson's ratio were computed from the stress and strain data. The purpose of the system checks is to ensure that the entire system is performing correctly and that the reported data are accurate.

A system check involves performing the uniaxial compression experiment on aluminum and comparing the observed Young's modulus and Poisson's ratio with the standard values reported for the material. If the measured values deviate by more than ± 5 percent from the published reference values, corrective measures are taken and no further experiments are performed on tuff until the aluminum calibration experiment yields acceptable elastic constants.

Typical results from a calibration experiment are shown in Figure A-1. Axial stress and radial strain are plotted as a function of axial strain for an aluminum specimen with the same nominal dimensions as the tuff. These data were collected using the procedure specified for the unconfined compression experiments. The specimen is cyclically loaded to one-half its yield stress at a strain rate of 10^{-5} s⁻¹; Young's modulus and Poisson's ratio are computed from the data.

A summary of the system checks performed during the course of the study of the specimens from the UE25 NRG-4 and 5 boreholes are presented in Table A-1. The results indicate that the system performed within the specified accuracy during the course of the study.

Compressional and shear wave velocities have been measured on the aluminum standard specimen. These data were used to compute the dynamic Young's modulus and Poisson's ratio. These values are also shown in Table A-1. The fact that these values for both

Young's modulus and Poisson's ratio are larger than those given in the literature, suggests that there are minor variations in the properties of aluminum supplied by the manufacturer. The elastic moduli for nonporous materials are frequently computed from compressional and shear wave velocities. These dynamic values should be used in conjunction with the static measurements. In many cases, the manufacturer's data are obtained for tension experiments and empirically corrected for compression, which can also lead to a discrepancy.

SYSTEM CHECK: September 30, 1993

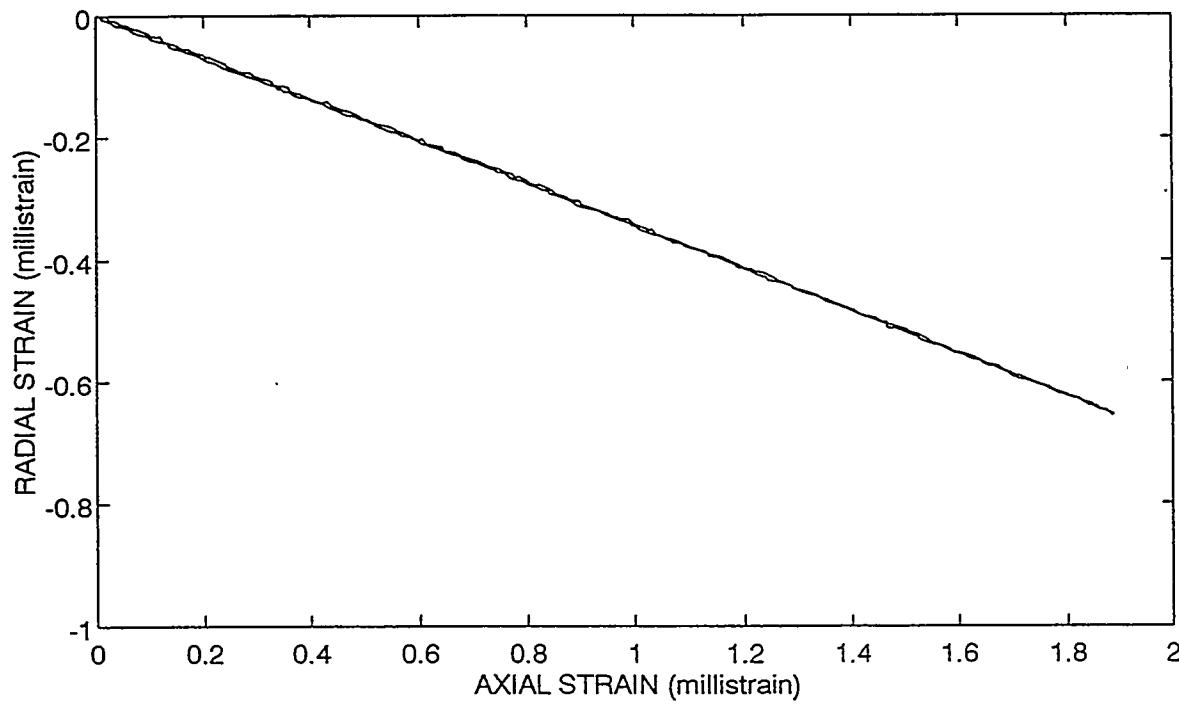
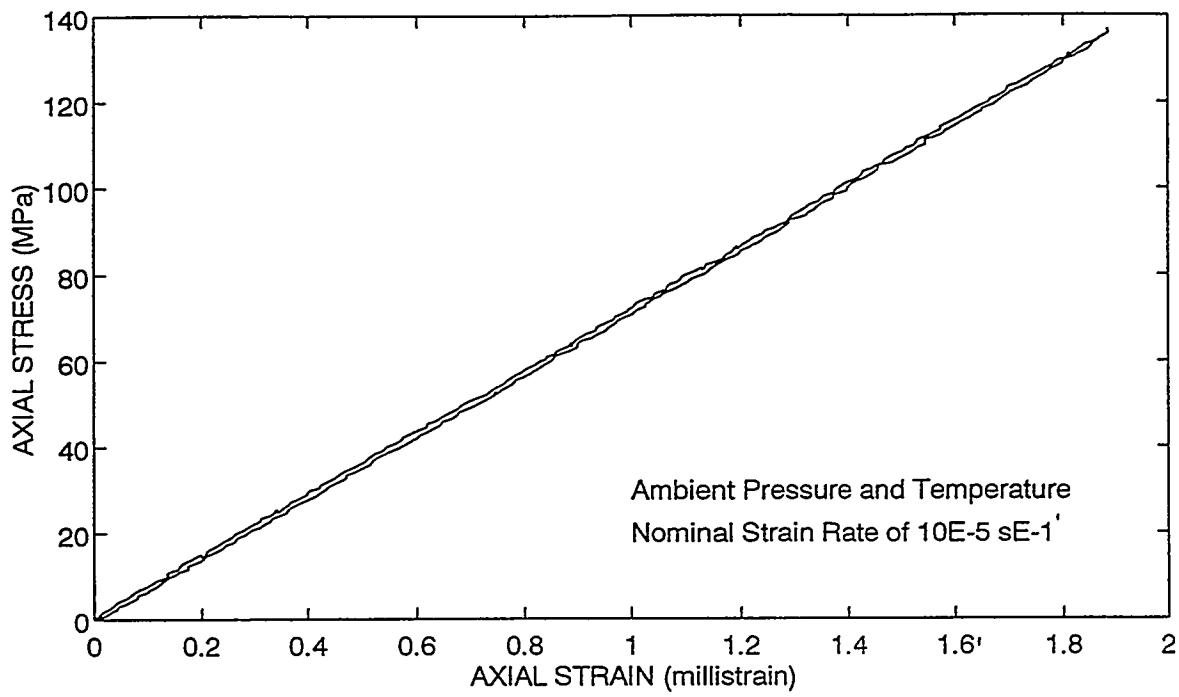


Figure A-1: Axial stress and radial strain are plotted as a function of axial strain for a specimen of 6061-T6511 aluminum cyclically loaded in unconfined compression.

Table A-1
USW NRG-4 and USW NRG-5
System Checks
Aluminum Standard - 6061 T6511

Date	Young's Modulus GPa	Deviation %	Poisson's Ratio	Deviation %
30-Sep-93	72.07	3.3%	0.34	3.0%
27-Oct-93	70.41	1.1%	0.34	3.0%
4-Jan-94	69.87	0.3%	0.34	3.0%
6-Jan-94	69.07	-0.9%	0.33	0.0%
10-Jan-94	70.69	1.5%	0.33	0.0%
Reference	69.66		0.33	
Dynamic	71.02		0.34	

APPENDIX IV

Information from the Reference Information Base Used in this Report

This report contains no information from the Reference Information Base.

Candidate Information for the Reference Information Base

This report contains no information for the Reference Information Base.

Candidate Information for the Geographic Nodal Information Study and Evaluation System

This report contains candidate information for the Geographic Nodal Information Study and Evaluation System (GeNESIS) in Tables 1, 2, 3, and 4. The data have been submitted to the SNL Participant Data Archive (PDA) and are indexed in the Automated Technical Data Tracking system (ATDT). The data packages have the following Data Tracking Numbers (DTN): SNL02030193001.009, SNL02030193001.012, SNL02030193001.014, and SNL02030193001.015.

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