

DOE/PC/93219--T12

Novel Carbon-Ion Fuel Cells

Quarterly Technical Report

APRIL - JUNE 1996

Performance Period ~~9/1/93 - 03/31/96~~ (Quarter #11)

Submitted to the
U.S. Department of Energy

Grant Number DE-FG22-93PC93219

Grant Period 10/1/93 to 9/30/96

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I. TASK DESCRIPTION

This report presents research to develop an entirely new, fundamentally different class of fuel cell using a solid electrolyte that transports carbon ions. This new class of fuel cell would use solid carbon dissolved in molten metal as a fuel reservoir and anode. Expensive gaseous or liquid fuel would not be required.

A high temperature fuel cell based on a carbon ion membrane/electrolyte would operate in a manner reminiscent of yttria-doped zirconia solid oxide fuel cells. Unlike zirconia, which transports oxygen ions from the atmosphere to the gas to be oxidized, however, the carbon ion electrolyte fuel cell would transport the carbon in ionic form from a fuel source to the oxygen gas present in the atmosphere. Such carbon-ion fuel cells, operating at temperatures above 1000 C, would produce an exhaust gas that could be fed directly into existing boilers, and could thus act as "topping cycles" to existing power plant steam cycles.

Fuel cell technology has progressed from laboratory study in England during the period 1804-1960 to space applications in the USA from 1957-1975. With current technology, four classes of cells predominate: hydrogen ion electrolyte cells, phosphoric acid electrolyte cells, molten carbonate electrolyte cells, and solid oxide electrolyte cells. Hydrogen ion cells have advanced to the point that they are the best power technology for many space applications. The other three classes of cells are at the age when demonstration plants of up to 5 megawatt are being built.¹ All four fuel cell types use gaseous fuels: hydrogen, carbon monoxide or H₂ and CO derived from methane. No fuel cell that uses a solid fuel has advanced beyond laboratory study, despite the fact that the majority of the world's fossil fuel reserves are solid carbon in the form of coal.

After identification by Japan's Ministry of International Trade and Industry (MITI) as a technology in which to strive for international industrial superiority, the Japanese are currently the world's largest supporters of fuel cell research, and have committed Japan to establishing 2000

megawatts of fuel cell capacity by the year 2000 at an estimated cost of 3 billion US dollars.² By the year 2010 Japan intends to have 8300 megawatts installed.²

Fuel cell development is being funded in the USA at one seventh the Japanese rate and in Europe at one tenth the Japanese rate.^{1,3,4} A World Fuel Cell Council was launched in September 1991 to coordinate fuel cell technology.² These commitments indicate that these four classes of fuel cells are near commercial viability after decades of research funding.

Thermodynamic factors favor a carbon-ion fuel cell over other fuel cell designs. A combination of enthalpy, entropy and Gibbs free energy values makes the reaction of solid carbon and oxygen one of remarkable high efficiency. The entropy change in the reaction allows this efficiency to slightly increase at high temperatures, unlike gas-fed fuel cell designs that decrease in efficiency with temperature.⁵ In addition to its potential for high efficiency in a single step of energy to electricity conversion inside the fuel cell, the high temperature exhaust of the carbon-ion fuel cell could make the cell useful as a "topping cycle," to be followed by conventional steam turbine systems. This two step system could be economically viable at cell efficiencies as low as 15%.⁶

High temperature operation can be seen to have dual advantages. First, solid electrolytes inherently reach higher levels of ionic conductivity as the temperature increases to just below their melting point. Second, elevated operation allows the exhaust gas of the carbon-ion fuel cell to exit with enough temperature to feed a "bottoming Carnot cycle" placed downstream of the fuel cell so that total combined efficiency of the fuel cell/turbine combination is increased. Only highly refractory materials like the rare-earth carbides have melting temperatures that allow operation at these elevated levels.

Carbon ions are known to exist in select compounds. Wells, in his classic text Structural Inorganic Chemistry, divides the nature of carbides into Classes 1,2,3, and 4.⁷ Class 1 are the carbides of the more electropositive elements that have many of the properties associated with ionic crystals: such as colorless transparent crystals and electronic insulation. Wells further sub-divides Class 1 carbides into Group A and Group B. Group A, Class 1 carbides yield methane upon

hydrolysis with water.⁸ Beryllium carbide and aluminum carbides are in this group and class. Group B, Class 1 carbides yield acetylene upon hydrolysis with water, and contain the well known calcium carbide along with SrC_2 and BaC_2 . Group B Class 1 carbides are thought to contain C-C^{-2} ions that are cigar like in shape.⁹

Class 2 carbides are those from the elements from La to Lu. Class 2 carbides form three types of crystal structures, some of which are similar to those of Class 1, but Class 2 carbides have mixed and varying characteristics that are temperature dependent.¹⁰ For example, room temperature hydrolysis with water of LaC_2 or CeC_2 yield a mixture of acetylene, methane and other hydrocarbons, but when the temperature is increased to 200 Centigrade, no acetylene is produced and the product is primarily methane.

The crystal structures of many carbides may be favorable for good ionic conduction. Compounds with atomic crystal structures analogous to the known ionic conductor calcium fluorite exist in the carbides but have not been studied as electrolytes, probably due to a traditional assumption that carbon forms only covalent bonds without any exceptions.^{12,13,14}

The economic consequences of a carbon-ion fuel cell would be extremely valuable, particularly in the USA with its large reserves of coal. A carbon-ion fuel cell could be fueled directly from either solid un-gasified coal, coke, or petroleum coke.

The environmental benefits of a carbon-ion fuel cell would be substantial. With the electrolyte in the cell inherently designed for passing only carbon-ions, emissions from the cell of SO_2 , NO_x and particulates would be near zero. Conventional solid oxide fuel cells pass oxygen ions and can form these unwanted pollutants. As the anode of a carbon-ion fuel cell would consist of a molten metal such as iron, impurities in the solid fuel fed to the cell could be trapped in slag formed in the molten metal in a manner similar to those employed in steel furnaces. This slagging prior to reaction is a feature unique to the carbon-ion fuel cell design and is somewhat analogous to the advantage fluidized bed combustion with limestone has over conventional combustion.

With this overview, we now discuss the thermodynamics of such carbon-ion fuel cells.

A Review of Carbon-Ion Fuel Cell Thermodynamic Efficiency

It has long been recognized that producing electricity chemically in fuel cells has thermodynamic advantages over producing electricity with the cycles traditionally used that rely on combustion-working fluid-turbine-generator combinations. To contrast the fuel cell to these cycle combinations, the first step is the familiar Carnot equation which limits conventional power cycles to a maximum permitted efficiency of $(T_2 - T_1)/T_2$, where T_1 is the low temperature reservoir (air or water outside the plant) into which the plant exhausts it's heat, and T_2 the high temperature reservoir (a working fluid heated by fuel combustion) from which the turbine obtains energy. In the best modern power plants T_1 is typically 311 Kelvin (100 Fahrenheit) and T_2 is 922 K (1200 Fahrenheit).⁴ The maximum theoretical efficiency is therefore about 66%. In reality, heat losses, friction and pollution controls reduce this maximum permitted efficiency to an actual efficiency of approximately 39% in today's best coal fired plants. Incremental improvements may increase this to 45% in a decade.¹⁵

The theoretical maximum efficiency of a fuel cell is given by $\Delta G/\Delta H$, where ΔG is the change in Gibbs free energy of the chemical reaction in the cell, and ΔH is the change in enthalpy of the chemical reaction in the cell.⁴ Table 1 is a compilation of chemical reactions listing the appropriate values of ΔH and ΔG for Standard Conditions of 298 degrees Kelvin and one atmosphere of pressure, plus the maximum efficiencies of fuel cell operation at 298, 600 and 1000 K.⁴

TABLE 1
Fuel Cell Thermodynamic Values and
Maximum Permitted Efficiencies⁴

Reaction	ΔH_{298}	ΔG_{298}	%E@298K	%E@600K	%E@1000K
$H_2 + 1/2 O_2 = H_2O (liq)$	286.0	237.3	82.97	n.a.	n.a.
$H_2 + 1/2 O_2 = H_2O (g)$	253	237.3	94.01	87.93	79.90
$CO + 1/2 O_2 = CO_2 (g)$	283.1	257.2	90.86	81.60	69.33
$C + O_2 = CO_2 (g)$	393.7	394.6	100.22	100.44	100.73

Note that the oxidation of solid carbon has the surprising efficiency of 100.22% at 298 Kelvin (77 Fahrenheit) and 100.73% at 1000 Kelvin (1340 Fahrenheit). This is not a misprint, but is also NOT a violation of the First or Second Law of Thermodynamics. As explained by Appleby in Fuel Cell Handbook, "It is interesting to note that for combustion reactions which proceed with an increase in entropy, energy conversion efficiencies in excess of 100% are theoretically possible. In addition to converting the chemical energy contained in the reactants to free energy in the form of electricity, such reactions theoretically would absorb additional heat from the surroundings and convert this heat to additional electrical energy so long as the heat could be supplied." ⁴

In other words, the small amount of efficiency over 100% is not coming directly from inside the fuel cell but is the result of heat transferred from the environment that surrounds the fuel cell system. This heat transfer is due to entropy change between reactants and products in solid carbon oxidation.

One should not dwell upon this high numerical value as extraordinary, except to point out that a carbon-ion fuel cell that was only "utilizing" 33% of its theoretical maximum potential at a practical operating temperature of 1000 Kelvin would still be 33% efficient, whereas a hydrogen / oxygen fuel cell operating at 1000 Kelvin would only be $.33 \times 79.9\% = 26\%$ efficient. (refer back to Table 1, column of values @ 1000K) Even more disadvantaged would be a carbon monoxide/oxygen fuel cell where the efficiency would drop to $.33 \times 69.33\% = 23\%$.

If one were given a supply of carbon as a base stock to run a fuel cell, it is today possible to react the carbon with steam in the "water gas" reaction and run an "off the shelf" fuel cell on the resultant hydrogen and carbon monoxide. However, the above numbers indicate that it would be far more thermodynamically efficient to have a carbon-ion fuel cell to directly consume the solid carbon.

Mathematically, this relationship between entropy and thermodynamic efficiency can be expressed as follows:

$$\text{Maximum Efficiency} = [\Delta G / \Delta H] \times 100\%$$

Substitute in the above equation:

$\Delta G = \Delta H - T\Delta S$ where ΔS is the change in entropy

and T is Temperature in Kelvin.

Maximum Efficiency = $(\Delta H - T\Delta S) / \Delta H \times 100\%$

Rearranging the above terms:

$$= [1 - (T\Delta S/\Delta H)] \times 100\%$$

If the number $(T\Delta S/\Delta H)$ is a negative number, then the maximum efficiency can be greater than 100% because the environment around the fuel cell is transferring energy into the fuel cell in an amount equal to $T\Delta S$.

A carbon-ion fuel cell would operate at a temperature above the melting point of the metal used as the anode of the cell. At a temperature of 1500 Celsius (2732 Fahrenheit) the nominal melting point of iron, the maximum efficiency of the reaction of carbon and oxygen is theoretically 101.31%.

If it would be desirable to operate a carbon-ion fuel cell at a lower temperature, several lower melting point metals for use as the cell anode are available. Aluminum, Calcium and Lithium are potential candidates with melting temperatures ranging from 839 to 181 Celsius. Carbon/Lithium electrochemical cells might have great potential as primary or secondary batteries due to the energy density that is theoretically possible. By selecting different metals, the carbon-ion fuel cell concept can be designed to operate over a wide temperature range, but high temperatures are preferred for efficiency reasons.

The solid carbon reaction increases very slightly in efficiency with an increase in temperature. As can be seen from an examination of Table 1, in the other two oxidation reactions that dominate gas fuel cells, hydrogen or carbon monoxide, efficiency decreases at a significant rate with an increase in temperature. Therefore, the electrochemical oxidation of solid carbon has a theoretical efficiency advantage over the oxidation of either hydrogen or carbon monoxide of approximately 12-31% at realistic operating temperatures.

The above maximum efficiency numbers should be compared to that achieved in cells constructed using today's best techniques. For example, some hydrogen cells in the space

program have achieved efficiencies near 60%, versus their maximum of 94% as shown in the Table 1.⁴ Published designs for a power plant that combines a hydrogen/carbon monoxide cell using a molten carbonate electrolyte with a bottoming cycle steam turbine contain estimates of 48% efficiency for real operating conditions.¹

As shown above, the carbon oxidation reaction is less sensitive to increases in temperature. This has an important beneficial effect on the electrolyte used in the fuel cell. As the ionic conductivity of electrolytes generally increase with temperature, a benefit of this temperature tolerance should be to increase the number and types of materials having usable values of ionic conductivity. Atomic crystal structures that have had too low an ionic conductivity to be recognized as useful ionic conductors between the 100-600 C (221-1112 Fahrenheit), where previous cells have operated, have the potential for operation of a carbon-ion fuel cell at 1500 C.

A further theoretical point concerning carbon is that at a ionic valence of -4, it has a charge carrying advantage over hydrogen whose ionic valence is +1. When passing through a electrolyte, only 1/4 the number of -4 carbon ions need to diffuse across the electrolyte to carry the same current as do +1 hydrogen ions. Compared to carbon monoxide or oxygen ions, only 1/2 the number of carbon ions need to cross the electrolyte as do ions that have a valence of + or - 2.

The efficiency possible with a carbon fuel cell can lead to lower cost electricity. A second environmental point to be made is that this same intrinsic efficiency leads to less production of CO₂ for each kilowatt-hour produced. While the question of CO₂ emissions into the atmosphere and global warming is still very uncertain, it is prudent to investigate methods that make the best use of each molecule of CO₂.

A directly analogous fuel cell could be constructed using a carbon-ion electrolyte rather than a oxygen-ion electrolyte. The carbon-ion electrolyte fuel cell would have the advantage that the carbon dioxide gas product would not be mixing with the super-heated carbon vapor used as fuel in the quartz ionization chamber. With discussion of the thermodynamics of carbon-ion fuel cells, we now review the crystallographic requirements needed by potential carbon-ion electrolyte membranes.

A Review of Electrolyte Crystal Structures

The critical element in an investigation of carbon-ion superionic conductors is clearly first to identify and then improve solid electrolytes in which carbon ions are mobile. Any candidate carbon ion electrolyte must also have low electronic conductivity and must be inert to unwanted chemical reactions involving the other materials that would make up the fuel cell, such as: the molten metal anode, the cathode material and impurities in the fuel.

The ideal material for the transport of carbon ions must exhibit ionic conductivity's greater than approximately $0.1 \text{ ohm}^{-1}\text{centimeter}^{-1}$ and electronic conductivity's less than $10^{-3} \text{ ohm}^{-1}\text{centimeter}^{-1}$.¹⁶ These two characteristics are tied to the crystal structure and bonding in the carbide. While past research on carbides has not explored the ionic conductivity to the extent which compounds containing oxygen, fluorine, or sodium ions have been studied, past carbide research is valuable in pointing out which carbon compounds, such as SiC, are good electronic conductors. SiC is used as a heating element in many furnaces.

Zirconium Oxide (ZrO_2), has a good combination of high ionic conductivity and low electronic conductivity for application with oxygen ions.¹⁷ ZrO_2 has the same crystal structure above 2000C as fluorite (CaF_2) and can be "stabilized" so as to hold this crystal structure at lower temperatures by the process of controlled contamination with another element termed "doping". Figure 1.30, reproduced from Smart and Moore, shows various views of the fluorite crystal structure.

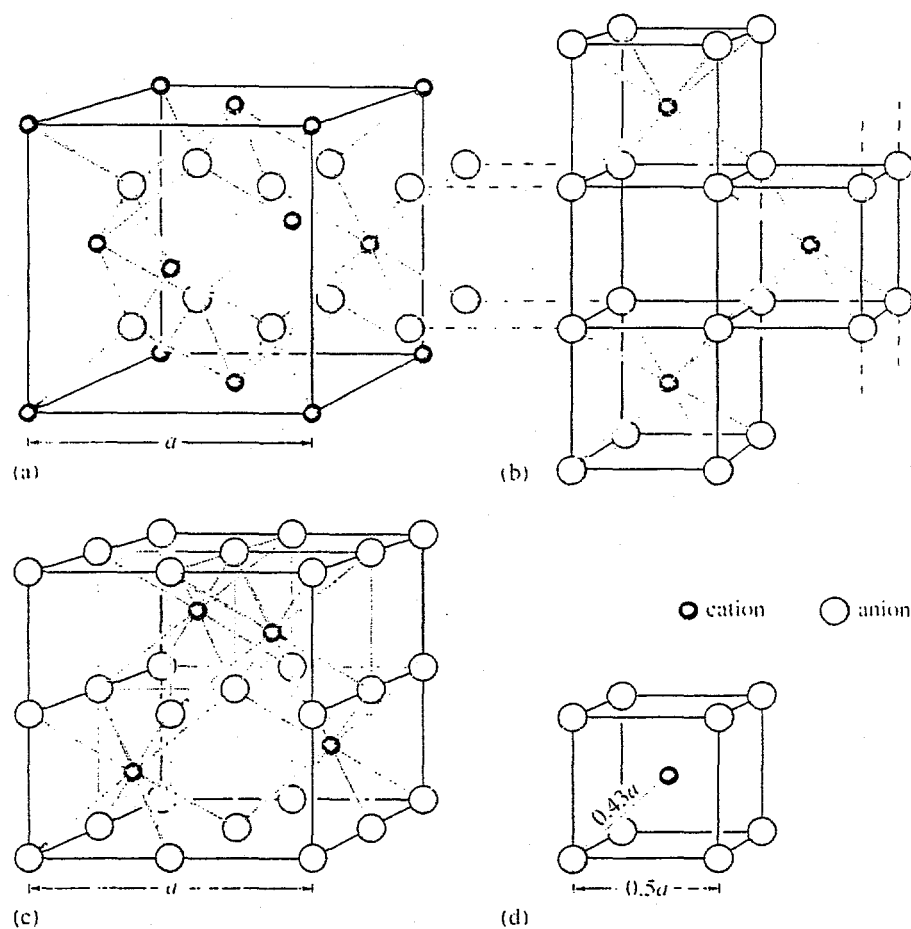


Figure 1.30 The crystal structure of fluorite (CaF_2). (a) Unit cell as a ccp array of cations. (b) and (c) The same structure redrawn as a primitive cubic array of anions: the unit cell is marked by a coloured outline in (c). (d) Relationship of unit cell dimensions to the primitive anion cube (the octant).

Proper doping not only stabilizes the crystal structure but also can greatly increase the ionic conductivity by introducing vacancies in the oxygen ion lattice. Figure 1, reproduced from Steele¹⁸, illustrates the successful doping of the fluorite crystal structure compounds of oxides such as the zirconias and cerias

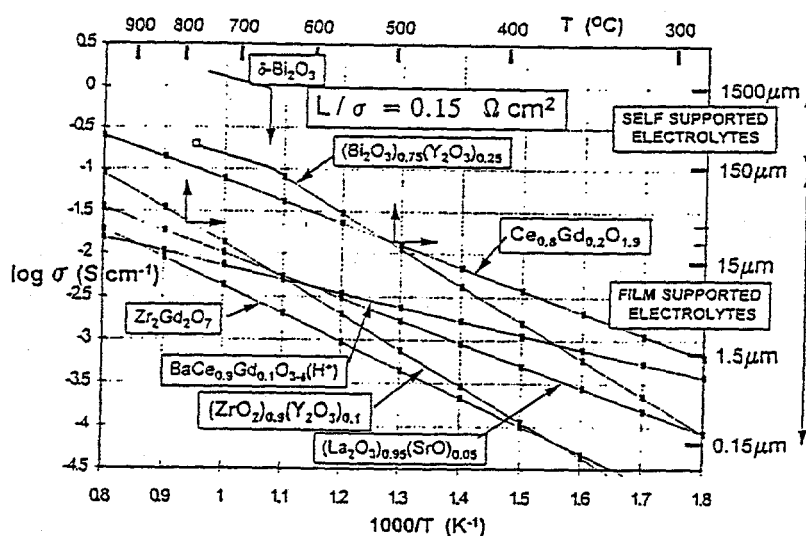


Figure 1: Specific Ionic Conductivity values for selected oxide electrolytes as a Function of Reciprocal Temperature.

Properly doped ZrO_2 has been termed a "superionic" conductor. However, the use of Zirconium can not be immediately transferred to carbides. ZrC does not have the fluorite crystal structure. Even more troublesome is the fact that ZrC is a moderately good electronic conductor at $8300 \text{ ohm}^{-1} \text{ cm}^{-1}$.¹⁹ Electronic conductivity in a solid electrolyte would short-circuit the fuel cell or battery it was used in. Some carbides do have low electronic conductivity. CaC_2 has an electronic conductivity of $0.0017 \text{ ohm}^{-1} \text{ cm}^{-1}$, but not the fluorite structure.²⁰

Chemically, the fluorite structure has the formula RX_2 where R is a cation and X is an anion and the ionic radii of R is greater than 0.73 times that of the ionic radius of X. Table 2 lists carbides that have the fluorite crystal structure at elevated temperature.²¹

TABLE 2

Fluorite Structure Carbide Characteristics

COMPOUND	TRANSITION TEMPERATURE alpha to beta, Celsius
* EuC_2	350
* CeC_2	1050
* LaC_2	1060
* NdC_2	1150
* SmC_2	1170
* GdC_2	1240
* TbC_2	1288
* HoC_2	1300
* ErC_2	1310
* YC_2	1324
* TmC_2	1355
* LuC_2	1450

Loe et al²² have shed considerable light on the fundamentals of stabilizing the beta (fluorite) crystal structure of the lanthanide carbides. Loe demonstrated a relationship, when changing from the high-temperature cubic fluorite structure to the tetragonal structure, between the transition temperature, T_t , of lanthanide dicarbide solid solutions, and the lattice strain energy, as represented by the square of the cell volume difference, ΔV , for 50% mole solid solutions. The following graph from Loe²² illustrates the transition temperature depression for 50% additions of other lanthanide carbides to LaC_2 . Notice that the depression of transition temperature is greater than 500 degrees Centigrade for the mixture 50% LaC_2 / 50% GdC_2 .

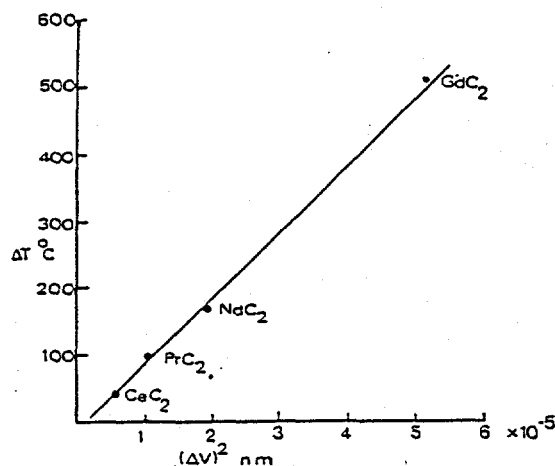


Figure 2: Depression of Solvent Transformation Temperatures when LaC₂ 50 mole% is Solute Against Cell Volume Difference Squared

Loe makes the prediction that when "these strains exceed 16 kJoule/mole, nucleation of the tetragonal polymorph is prevented and the cubic phase is stabilized to room temperature." ²³ Stabilization to room temperature would be very desirable to prevent phase transition thermal cracking in a fuel cell electrolyte undergoing repeated large temperature variations during operation.

Sammells et al ²⁴ have made important contributions to the basic science of systematic selection of electrolytes and dopants to improve electrolyte performance. By examining the "free volume" of the lattice structure of both perovskite and fluorite oxides, they have postulated that the activation energy for ionic conduction goes down with decreasing free volume for fluorite crystal structures. (They also postulate the opposite effect for oxides of perovskite crystal structure.) Sammells defines "free volume" as the difference between the volume of the crystallographic unit cell and the volumes occupied by the constituent ions resident at lattice sites. This relationship is illustrated in the Figure 3. ²⁴

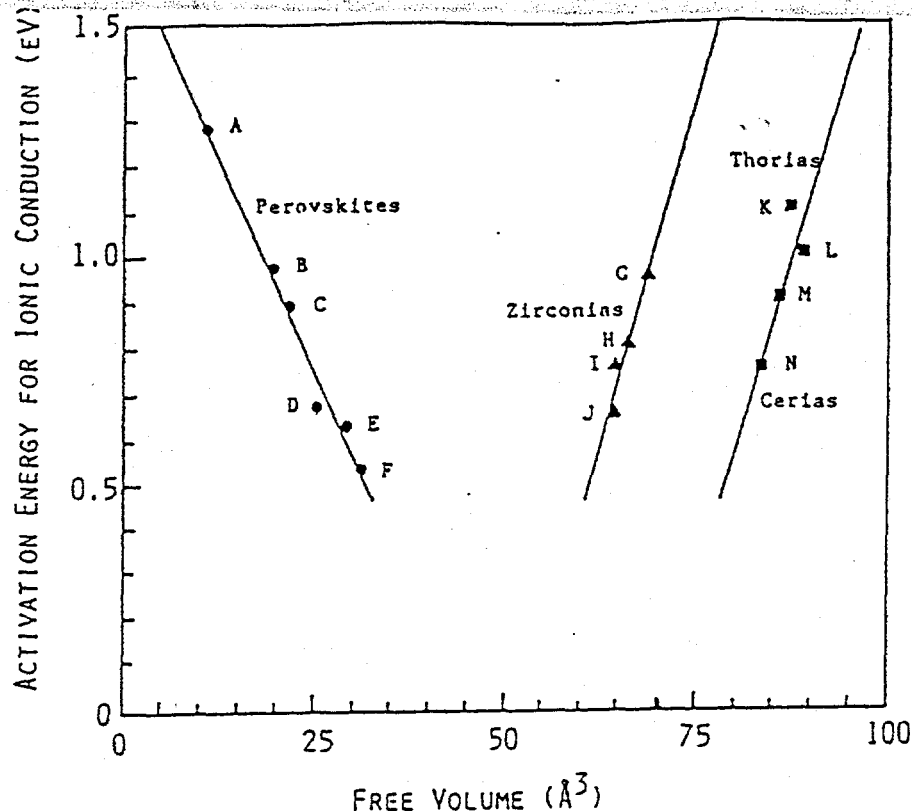
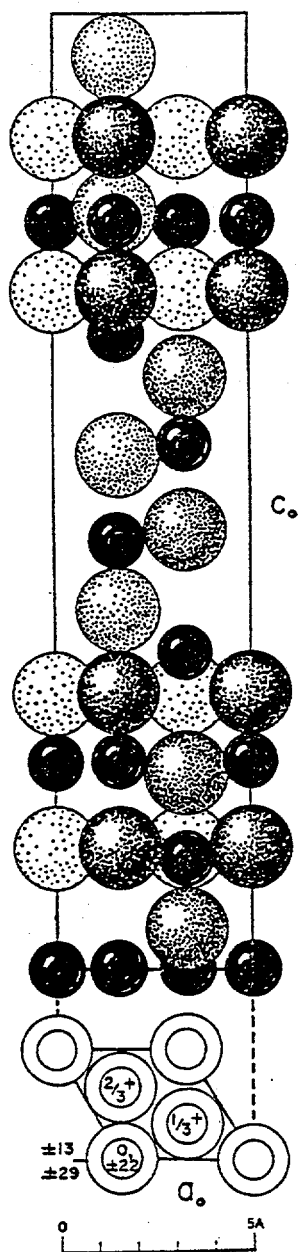


Figure 3: Correlation of Activation Energies for Anion Transport in Solid Electrolytes
As a Function of Free Volume

Aluminum carbide, Al_4C_3 , is also an interesting candidate for carbon-ion conduction. In aluminum carbide, carbon has two distinct positions. As stated by Wells ⁷, "The structure... is rather more complex...It is sufficient to note that each carbon atom is surrounded by Al atoms at distances from 1.90 to 2.22 angstroms, the shortest C-C distance being 3.16 Å. As in Be_2C therefore, there are discrete C atoms, accounting for the hydrolysis to CH_4 ." Figure 1.40, reproduced from Wyckoff ¹⁴ is a depiction of the aluminum carbide structure. Note that the distinct carbon atoms in the center of the drawing constitute a "layer" along which anion conduction might occur.

Aluminum carbide and beryllium carbide have distinct carbon-ions in their crystal structure at room temperature. At high temperature, the lanthanide carbides have the fluorite crystal structure well known for anion conduction, and may also have distinct carbon-ions in their structure. Based on these considerations, our experimental procedures to develop a solid carbon ion electrolyte have focused on rare earth carbides, especially cerium carbide, and the carbides of aluminum and beryllium.

Figure 1.40: Two Projections of the elongated hexagonal Al_4C_3 Structure. In the upper Projection the Carbon atoms are black.



Experimental Procedures

The sequence of laboratory research procedures necessary to develop a solid carbon-ion electrolyte and to determine the ionic conductivity of carbon-ions in this electrolyte can be broken down into the following series of steps:

1. Launch an exhaustive and continuing literature search for all relevant past research on carbides, crystal structures of carbides, carbon diffusivity in carbides and basic thermodynamic qualities of carbides.
2. Procure materials and equipment for the production and analysis of carbides.
3. Perfect a method to produce a repeatable geometric shape of carbide. The carbide could conceivably be a pressed and sintered pellet, a casting from the molten state, a single crystal, or a suitably thick film. The preferred geometric shape would have the following characteristics:
 - a. Mathematically simple so that diffusion equations are readily applied.
(Irregular shapes could be approximately solved by computer modeling, however.)
 - b. Flat surfaced in at least one dimension so that analysis techniques such as SIMS (Secondary Ion Mass Spectroscopy), XRD (X-Ray Powder Diffraction), and SEM (Scanning Electron Microscope) are readily applicable.

A pressed and sintered, (or hot pressed) pellet would seem to be the preferred geometry, but a cast pellet or ingot might also be acceptable if surface roughness and contamination could be controlled to acceptable limits. Casting has potential advantages in the area of introducing dopants to the carbides in a more uniform manner than pressing and

sintering mixtures of powders.

4. Uniformly alloy the carbide with other elements, or "dopants," to

- a. Stabilize the preferred crystal structure so that this phase of the carbide exists over the entire temperature range in which the carbide would be used as an electrolyte. This requirement is not theoretically necessary, but is instead a practical requirement, as phase changes in a solid electrolyte over its operating temperature range will usually result in cracking and resultant failure of the fuel cell. DTA (Differential Thermal Analysis) techniques should, in theory, be a fast and low cost method of detecting the phase transition temperatures. High Temperature X-Ray Powder Diffraction is another method to exactly quantify the transition temperature and crystal structure.
- b. Decrease the electronic conductivity. This will eliminate parasitic losses in the fuel cell.
- c. Decrease the "free volume" (as per Sammells). This will decrease the activation energy for ionic conduction.
- d. Introduce defects in the crystal structure. This will further decrease the activation energy for ionic conduction.

5. Produce the geometric shapes from the doped carbide solid electrolytes.

6. Determine the ionic conductivity of carbon-ions in the electrolytes.

Historically, ionic conductivity measurements have been made by either of two methods: electrochemical cells or tracer diffusion. In the electrochemical cell method, generally four probes are affixed to the cell. The probes can be electronically conductive, ionically conductive, or both.

The current and voltage applied can be either alternating current of varying frequency, or direct current. The cell is then raised to the operating temperature of interest and the current and voltage drop measured.

In tracer diffusion, the electrolyte is coated or brought into contact with an element that can be readily detected by some analytical means. The electrolyte is then annealed at the operating temperature of interest. After annealing, the electrolyte is analyzed for the amount of the tracer along its dimensions in either a continuous or sectional manner.

In this research it was originally proposed that an electrochemical cell be used to test each potential carbide electrolyte at 1500 C using conventional four probe contact measurements and varying frequency alternating current.²⁵ As the research proceeded, it was determined that tracer diffusion would be a simpler, more versatile, and less costly technique.

The tracer diffusion method adopted is as follows: Coat the carbide shape on one surface with a layer of a carbon isotope suitable for use as a tracer. The carbon isotopes most used as tracers in other research efforts have been Carbon-13 and Carbon-14. Carbon-13 has the advantage that it is stable, non-radioactive and closest in mass to Carbon-12. Carbon-14 has potential advantages in that it can make use of the wide range of "radioactive carbon dating" technology that has been developed in anthropology. Its obvious principle disadvantage is its radioactivity, which precludes its use in many instruments that must not be contaminated with radioactivity.

In this research Carbon-13 will be used as the tracer. Carbon-13 was selected due to its non-radioactive advantages and its closeness in mass to the natural carbon that would actually be used in fuel cell operation. In addition, many of the specific scientific instruments needed to conduct the research are located in facilities that prohibit the use of even minute amounts of radioactive materials.

7. Anneal the carbon coated electrolyte pellet in a environment controlled for temperature, atmosphere and time. The annealing process be allow the carbon isotope tracer to diffuse into the carbide to a depth that can be accurately measured.

8. Analyze the carbon isotope content of the pellet after annealing.

If the geometry of the carbide is one of the simple shapes that allows a mathematical solution to the diffusion equations, then the diffusion co-efficient can be readily calculated. For example if a Carbon-13 isotope coating of purity C_0 can be approximated as a perfect film of thickness b at one end of a long rod (the pellet's length), then the final concentration of the carbon isotope at any distance x along the pellet's length after an annealing time T_a is given by the equation ²⁶:

$$\text{Concentration C-13 (x,t)} = [(b C_0) / 2(\text{square root } (\pi T_a D))] \exp \{-x / 4D T_a\}$$

where D is the diffusion co-efficient of Carbon-13 in the lanthanide carbide. Once the diffusion coefficient is known, the conductivity can be found from the equation:

$$\text{Conductivity} = [D \times N_i \times q^2] / [R \times T \times (\text{Molar Volume of the Carbide})].$$

Here we also assume that the diffusion co-efficient of Carbon-12 would be similar, or of approximately the same magnitude, as that of Carbon-13.

SIMS is one method of analyzing this carbon concentration.

Another possible method would be to slice thin layers from the pellet and spectrographically analyze each layer. In this research SIMS will be the method used to determine the carbon diffusion characteristics.

Low cost carbon-13 (\$255/gram) and carbon-12 (\$71/gram) isotopes of 99.9% purity have only recently become available.²⁷ (Normal carbon is $\overline{98.89\%}$ carbon-12 and 1.11% carbon-13.) In addition to the amorphous carbon powders, the simple sugar, d-Glucose, synthesized with in excess of 99% Carbon-13 making up the carbon atom component of its structure, is now available a modest cost (\$244/gram).

The Carbon-13 powder, with the Carbon-13 glucose sugar acting as a binder, might be hot pressed into a Carbon-13 sputtering target, for use in depositing a layer of Carbon-13 onto the end

surface of a carbide pellet. Another possible binder for the production of a sputter target would be petroleum tar, which is widely used in the commercial production of carbon rods and carbon molds.

In fabricating carbide pellets, several precautions are in order. All the carbides will react with water to form a mixed gaseous product of methane, acetylene, and higher hydrocarbons. Therefore, any water vapor present, such as that in the starting materials, the glass of containers, the atmospheres of glove boxes, in dies, absorbed in crucible materials, or in relatively minute concentrations in whatever inert gas is chosen for the atmosphere in an annealing furnace, will degrade the product. A common failure mode is the formation of internal gas pockets of sufficient pressure to lead to disintegration of the desired geometric shape.

With this overview of the experimental procedures to be followed, the following section presents a summary of the work that has been carried out.

Laboratory Experiments Carried Out To Date

Laboratory experiments carried out to date in the field of carbon-ion solid electrolytes have been such that they can be roughly classified into seven different categories:

1. Formation of Pressed and Sintered Carbide Pellets.

Approximately twenty attempts have been made to press and sinter cerium carbide, lanthanum carbide or aluminum carbide. The powders used have varied from irregular lumps of less than 2mm to finely ground minus 325 mesh material which was ball milled in an inert atmosphere of argon inside a glove box. Binders of sucrose, glucose, benzene and Rohm & Haas BE7-MEK (a methyl ethyl ketone solvent binder that totally evaporates at 400C) have been tried. Pressing has been under a 32 Ton capacity hydraulic press in hardened steel dies of 0.5 and 0.9 inch diameter. Dies have been bought commercially and built in the machine shop. An electric surround heater was purchased for the dies capable of 500C, and pressing has been attempted cold, heated prior to pressing and heated after pressurizing. Pressures up to 10,000 atmospheres

have been achieved, although failure of dies due to inelastic compressive strain of the piston has occurred more than once.

Despite all of the above described efforts, no successful pellets have been produced. All pellets have had such weak pre-sintered strength that they cracked during dismounting from the die, or while sintering in the argon atmosphere annealing furnace. It is the opinion of the investigator that the correct binder for the carbides has not been found.

However, as discussed in the following two sections, success has been achieved in forming solid carbide samples by means of casting ingots in an arc melt furnace. As discussed in Section Six, these are the materials that have been used for the x-ray evaluations carried out at the High Temperature Materials Laboratory at Oak Ridge National Laboratories.

2. Formation of Melted Carbide Castings.

Small circular castings of aluminum, lanthanum, cerium, zirconium, titanium, calcium and barium carbide have been successfully made in the arc melt furnace. Although operation of the arc melt furnace is somewhat of an art (and an art that requires extensive practice), it has been found that by starting with very low argon gas pressures and low electric arc currents, castings can be made directly from fine powders of the carbides.

3. Synthesis of Carbides Directly in the Arc Melt Furnace.

After learning to make castings from the powders of cerium carbide and lanthanum carbide on a trial basis, it was decided to use the arc melt furnace to synthesize carbides directly from the elemental metal and carbon. These experiments were in the main successful. Aluminum carbide was successfully made, but later x-ray diffraction revealed it to have substantial elemental aluminum and graphite as major contaminants. Cerium and lanthanum carbides have been made, but x-ray diffraction revealed that the products were a mixture of the carbides $\text{Ce}_2\text{C}_3/\text{CeC}_2$ and

$\text{La}_2\text{C}_3/\text{LaC}_2$, rather than solely the dicarbide that was desired. An experiment in which elemental lanthanum was reacted with 99.9% pure carbon-13 resulted in almost exactly the opposite of the desired result: A relatively pure La_2C_3 with almost no LaC_2 was made and confirmed by x-ray diffraction.

4. Formation of Pressed and Sintered Carbon Sputter Targets.

The standard one inch sputter target is a metal (usually copper, tungsten, tantalum or stainless steel) disk 1.00 inch in diameter and 0.250 inches thick that has a hollowed-out center cavity that is 0.900 inches in diameter and 0.125. Into this cavity is inserted a material for sputtering. The material is bonded in place by soldering or shrink fitting. For the purposes of sputter coating a carbon layer onto carbides, a standard carbon one inch sputter target has been purchased from a commercial supplier. Attempts to have a commercial supplier build a carbon-13 isotope sputter target have been unsuccessful as of this date. Sixteen different suppliers have been contacted, but all have refused to even quote the job. Commercial carbon sputter targets are made by machining on a lathe a graphite rod down to the required dimensions. As no pre-made carbon rods of carbon-13 are available, suppliers have been reluctant to take on the "one-off" order.

Attempts have been made by the investigator to make a carbon-13 sputter target by pressing and sintering. These attempts have been considered practice and have been made with natural carbon, rather than expensive carbon-13 itself. After receiving valuable advice and a proprietary tar binder from Great Lakes Carbon Incorporated in Morganton NC, a natural carbon material target was made using 20% by weight petroleum tar binder. This practice target appears had sufficient strength.

It should be noted that 80% of the natural carbon contained in the tar binder prior to sintering remains in the sputter target after sintering. Therefore 80% of 20% of the original weight of the target body will be natural carbon from the binder. If the sputter target is, for example, 0.8

grams of 99.9% carbon-13 isotope and 0.2 grams of tar binder, then the final weight will be $0.8 + 0.2(80\%) = .96$ grams. The final percent by weight of carbon-13 isotope will be $0.8 \text{ grams } (99.9\%) + 0.16 \text{ grams } (1.11\%) / 0.96 \text{ grams} = 83.4\%$. As the natural percentage of carbon-13 in earthly things containing carbon is 1.11%, this represents an enrichment of $(83.4 / 1.11) = 75$ to 1.

To date approximately 5 attempts have been made to fabricate a sputter target with a carbon powder that analyses 99% Carbon-13. As of this date, targets can now be routinely produced up to the green pressed stage of fabrication. These green pressed targets are dense and have smooth outer surfaces, as a good target needs.

A major advance has been the addition of approximately 5% by weight carbon fibers to the carbon powder prior to pressing. These carbon fibers re-inforce the pressed material in a manner similar to the re-inforcement that steel "re-bar" adds to poured concrete. The carbon fibers are of natural carbon composition however. (98.9% Carbon-12 and 1.1% Carbon-13)

Another advance has been the use of acetone as a dispersant for the petroleum tar binder. The acetone is added to the mixture of carbon-13 powder, carbon fibers and petroleum tar after these three items have been weighed and mixed. The acetone is then allowed to disperse the tar evenly over the surface area of the carbon-13 powder and the fibers. The acetone is then removed by vacuum distillation prior to pressing. It has been found that complete removal of the acetone is crucial, as this volatile liquid will out-gas during sintering and fragment the pressed target.

5. Differential Thermal Analysis Detection of Carbide Transition Temperatures.

Differential Thermal Analysis has been attempted as a method of detecting the alpha to beta transformation temperature of cerium and lanthanum carbide in the temperature range of 1000 to 1500C. At these temperatures, the carbides are prone to quickly hydrolyze if any water vapor is present. Using an inert atmosphere of ultra-high-purity argon and water trapping filters, several runs appeared to show a transition temperature of approximately 1170 C. This transition

temperature did not appear to be lowered or raised in a statistically significant manner when the carbides were doped at 8 mole % with Ba, Ca, Ti and Zr carbides, or with 10 mole% ZrN.

The peaks shown at the transition point in DTA were small, and did not always appear again (with the expected temperature change hysteresis) upon cooling. However, high temperature x-ray diffraction later confirmed (see below) both that the transition temperature is in the range of 1100-1300 C, and that the doping of these carbides did not change the transition temperatures measurably. It may possible to use DTA to measure changes in transition temperature if:

1. Larger samples weights are used to lesson the effect of surface oxidation and to increase the magnitude of the transition energy peak to well above the resolution of the DTA machine's capability.
2. Optimum heating and cooling rates are found that are suited to the carbides.

6. X-Ray Diffraction analysis of crystal structures and transition temperatures.

The investigator was fortunate to have a proposal accepted by The High Temperature Materials Laboratory (HTML) at Oak Ridge National Laboratories to use their high temperature X-Ray Diffraction equipment to determine the crystal structure and transition temperatures of pure and doped cerium carbides and lanthanum carbides. Room temperature X-Ray Diffraction was also run on pure and doped aluminum carbides. Three weeks have been spent making these runs, and another week is planned in January of 1996. The results of these runs are ongoing and voluminous, but will briefly be summarized here.

X-Ray Diffraction Patterns confirm that cerium dicarbide transforms to the fluorite prototype crystal structure in a very sluggish transition in the temperature range of 1350-1400C. Upon cooling the cerium dicarbide, the phase transition will not occur at 1100C after a waiting period of four hours, but occurs within 30 minutes at 1050C. Figure 4 is a X-Ray peak spectra of cerium dicarbide showing its transformation at high temperature.

Lanthanum dicarbide transforms into a pseudo-fluorite structure above a transition in the temperature range of 1350-1400C. The pseudo-fluorite pattern has each of the fluorite peaks split, indicating that the cubic symmetry is distorted into a symmetry that is slightly tetragonal. This may also indicate that the carbon-ions in LaC_2 are double carbons. Figure 5 is a comparison of the X-Ray peak spectra of lanthanum dicarbide and cerium dicarbide in their high temperature crystal structures. Notice the split peaks of lanthanum dicarbide.

The X-Ray Diffraction patterns of cerium and lanthanum dicarbides doped with Ba, Be, Li, Mg and Zr indicate that these dopants are miscible in the dicarbide, except for ZrC where greater than 35 mole% ZrC resulted in a pattern with peaks indicating that free ZrC is present as a second phase. The alpha crystal structure of the dicarbides (tetragonal CaC_2 type) and the beta crystal structure of the dicarbide (fluorite CaF_2 type) remained the same for all dopants and dopant amounts.

X-Ray Diffraction carried out at Oak Ridge yielded interesting results concerning aluminum, lanthanum and beryllium carbides. Figures 6 and 7 are patterns of aluminum carbide and lanthanum carbide doped with 40 mole% beryllium carbide respectively. Note that the beryllium appears to be miscible in both. Aluminum carbide and lanthanum carbide doped with 5 - 25 mole% beryllium carbide showed similar patterns. Lines for Be_2C were either not found or so low that they were near noise level.

Dopant mole percentage levels were calculated from the stoichiometric amounts of elements added prior to casting in the arc melt furnace. It is recommended that the samples previously X-Rayed, and all future samples, be analyzed by chemical methods in an independent commercial laboratory to ascertain their true elemental analysis. It cannot be assumed that a dopant added to the melted carbide ended up in the resultant casting, as the casting action in the arc melt furnace can at times be vigorous, sputtering and boiling.

FIGURE 4
X-Ray Patterns of Cerium Dicarbide showing alpha to beta Transformation

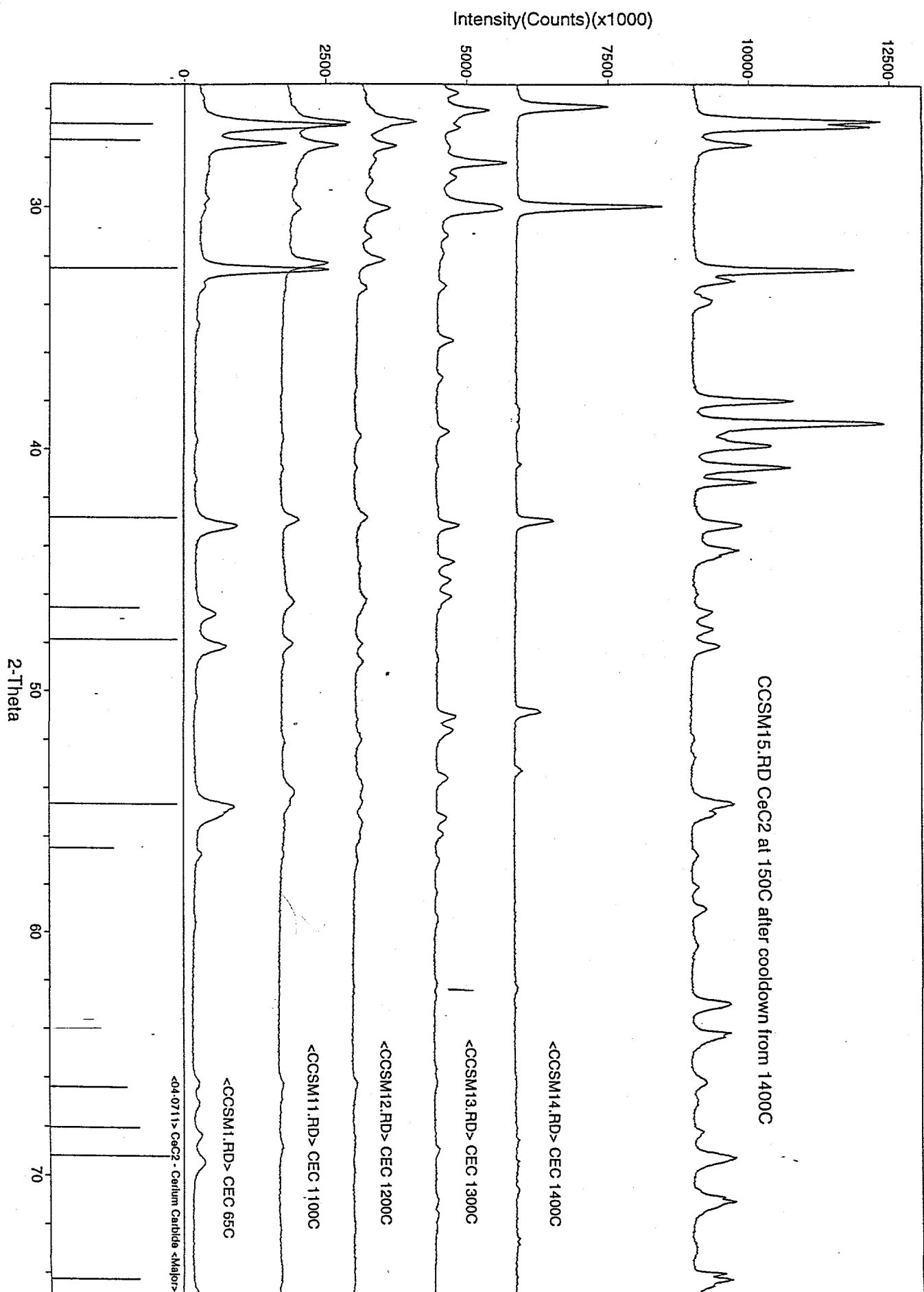


FIGURE 5

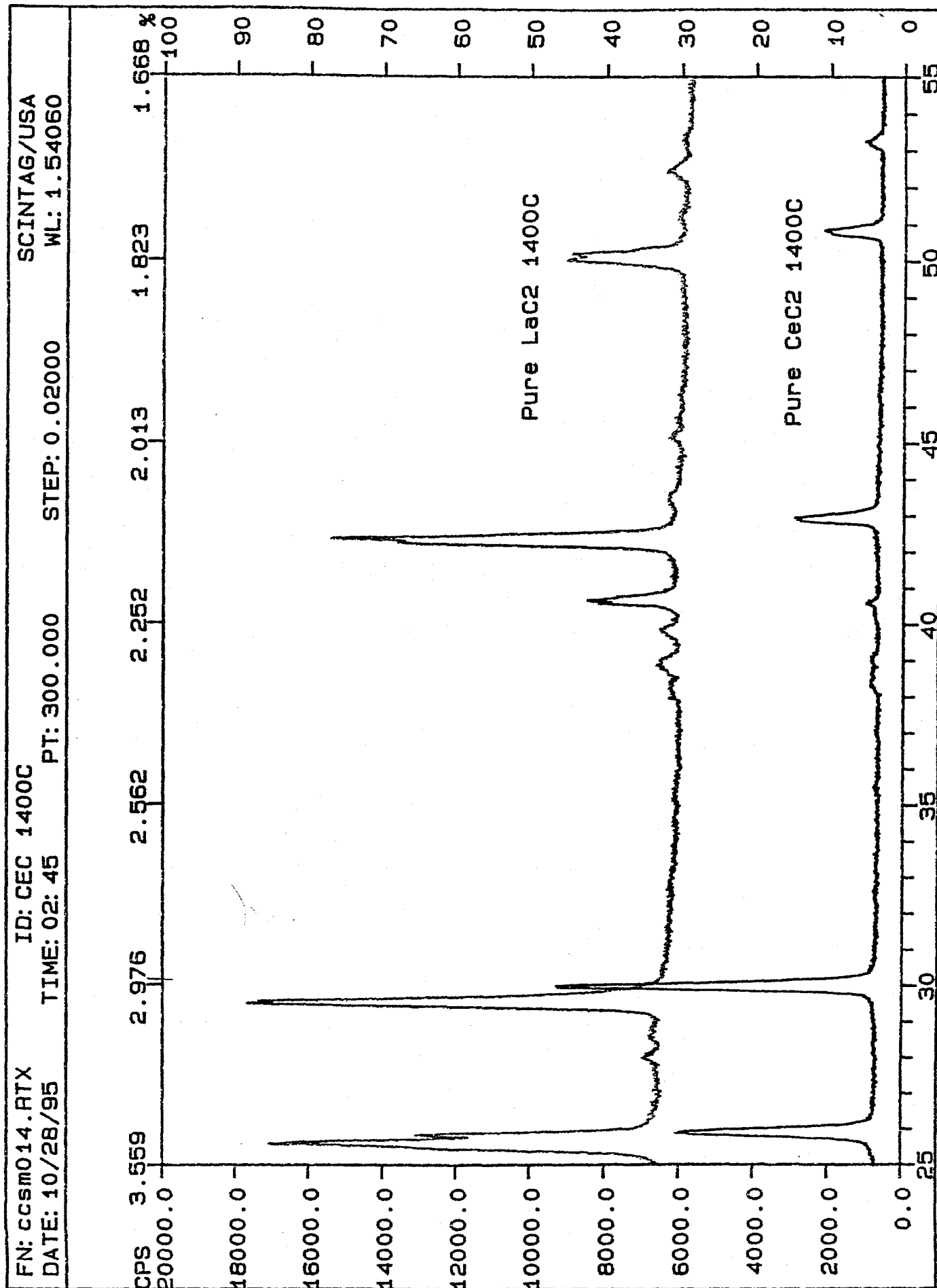


FIGURE 6

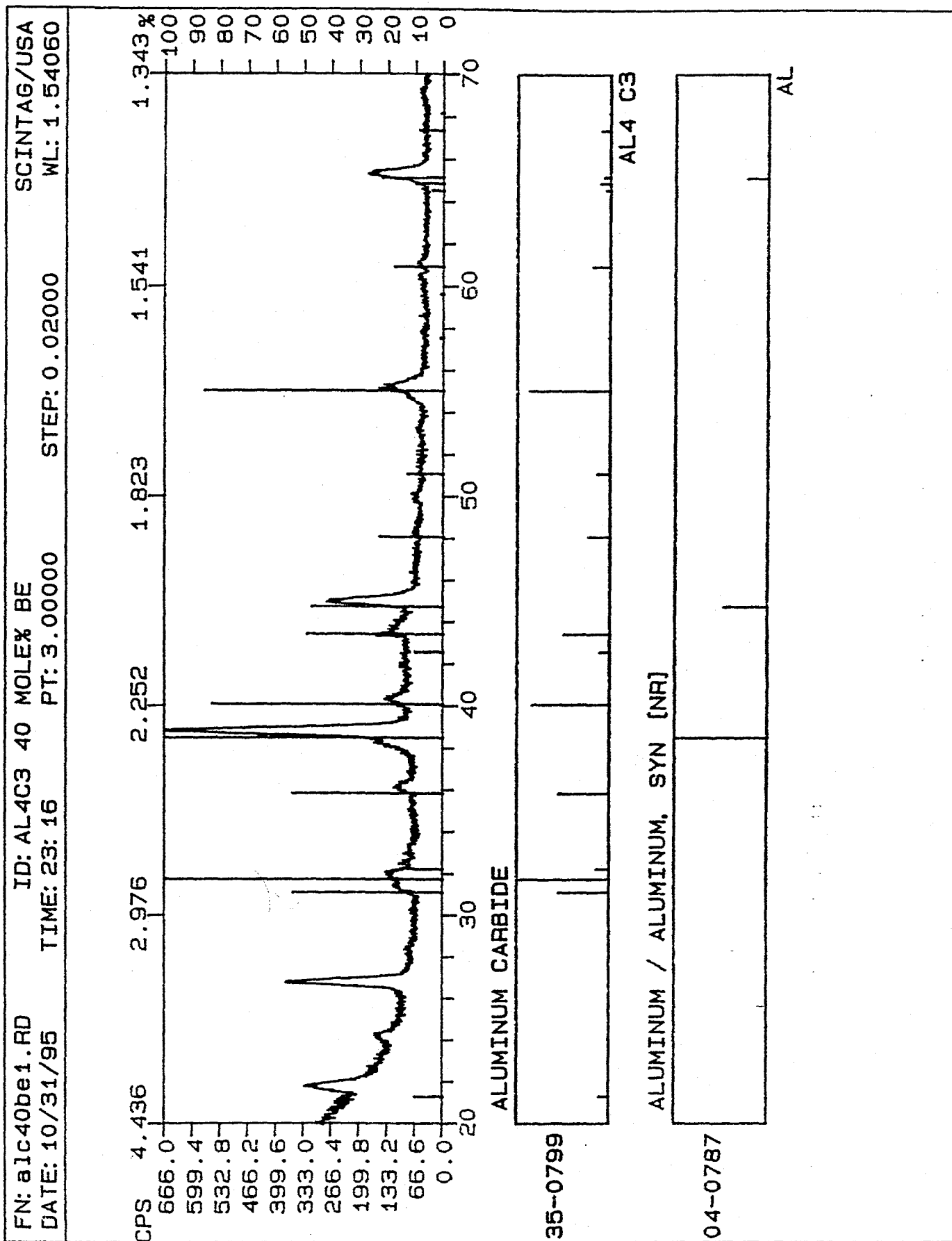
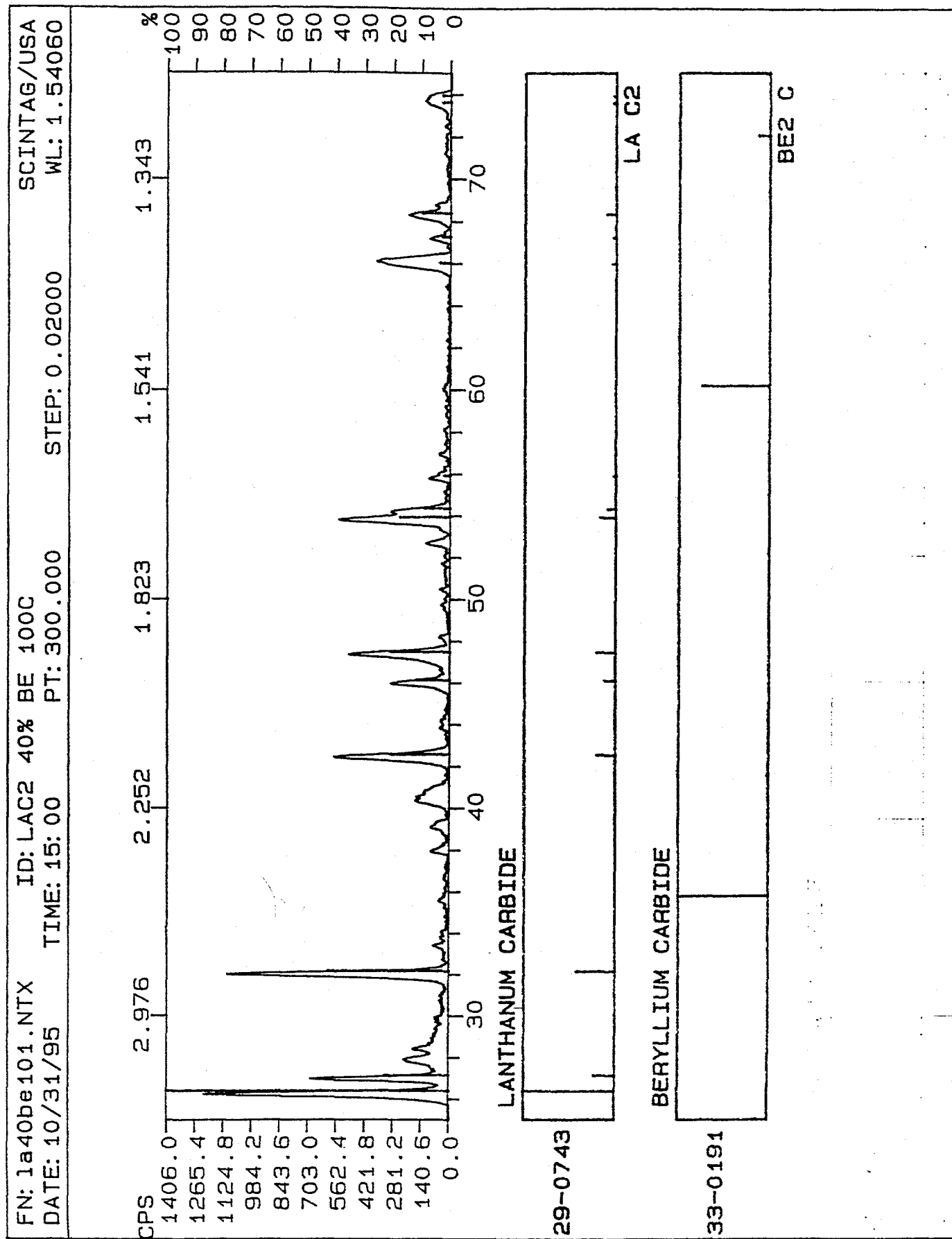


FIGURE 7



7. Secondary Ion Mass Spectroscopy analysis of carbon isotopes.

The investigator was fortunate to receive from the Micro-Electronics Center of North Carolina (MCNC) a scholarship to be trained in the use of a Perkins-Elmer Model 1200 Secondary Ion Mass Spectrometer. This (SIMS) instrument has a resolution of approximately 1 part in 500 atomic mass-electrostatic charge units. At this level of resolution, the SIMS instrument should be easily capable of resolving the difference between a carbon-12 ion (12.00000 amu) and a carbon-13 ion (13.00335).

There is a potential problem of resolving the difference between the complex ion carbon-12 hydrogen-1 (13.007825 amu) and a singular carbon-13 ion (13.00335). The difference .004475 amu, is approximately one part in 200. ($1 / .004475 = 223$) Due to the solubility of hydrogen in stainless steel, and the wide spread use of stainless steel in the construction of vacuum chambers used in analytical instruments, it cannot be expected that all hydrogen can be eliminated from the atmosphere surrounding a sample undergoing analysis. This is not expected to be a significant problem due to the following factors:

a. A carbon-12 / hydrogen-1 ion will usually have a different charge on it than a carbon-13 ion.

b. Water reacts with carbides, forming the gas methane, which then leaves the solid.

This makes the carbides somewhat "self-desiccating."

c. The ions used in SIMS can be the doublet of the element in question. This greatly lessens the effect of hydrogen, as a hydrogen containing ion of the same mass would have to consist of four atoms. Such multi-atom ions are very unlikely to be produced in the ion sputtering of the SIMS instrument. For example,

an ion of charge -1, made of two carbon-12 atoms (amu 24.00000) can be analysed for.

Similarly, an ion of charge -1, and two carbon-13 atoms can be detected. The presence of

the percentage of these doublets can be calibrated to the carbon content of the sample.

In June of 1996, The SIMS instrument at MCNC successfully analysed the carbon-12 versus carbon-13 content of two samples of cerium-erbium dicarbide. Sample #1 was a 25 atomic % cerium, 25 atomic % erbium, 50 atomic % carbon-13 material with the stoichiometric designation $Ce_{.5} Er_{.5} C_2$.

Sample #1 was a ingot approximately 10mm in diameter and 4 mm high, cast in the arc melt furnace, that after casting had had a 5mm in diameter flat surface ground onto the top of the sample. The grinding of the sample was done in an argon gas atmosphere within a glove box. The grinding apparatus was a 18,000 rpm miniature milling machine with an alumina (Al_2O_3) grinding tool. Alumina was selected for the grinding tool (over SiC, WC or diamond impregnated matrix) because the alumina could not contaminate the surface of the sample with any carbon-12 atoms.

The flat, ground surface of Sample #1 was then arc-evaporation coated with a 3 micron deep coating of natural carbon (98.9 atomic % carbon-12 and 1.1 atomic % carbon-13). The coating was done in a Pelco Model 100 Arc-Evaporation Unit in an argon atmosphere of 10 millibar.

Arc-evaporation carbon coating was selected after earlier trials with RF sputtering of carbon onto carbide samples showed that the sputtering process was long (14 hours to deposit 70,000 angstroms of carbon) and that the sputtered carbon coating did not have good adhesion. The Arc-evaporation carbon-coating had good adhesion and was quick (30 minutes coating time).

Sample #2 was identical to Sample #1, including the natural carbon coating, except that Sample #2 was annealed in a vacuum furnace at an pressure of 2 microns of mercury for one hour at a temperature of 934 Centigrade.

Both Samples #1 and #2 were analysed by SIMS at the Microelectronics Center of North Carolina. The primary ion beam was cesium, the acceleration voltage was 7 kilovolts and the ion current was 685 nano-amps. After analysis, the craters produced by the ion sputtering beam where

measured in a Scanning Electron Microscope. These voltage and amp setting were found to have produced a crater formation rate of 1300 angstroms per minute.

Figure 8 is a SIMS profile plot of ion counts versus time for Sample #1, the control ingot that was not annealed. Figure 9 is a similar plot for Sample #2, the annealed ingot. In both plots traces are seen for carbon-12 (marked "12") carbon-13 (marked "13", etc) the doublet of carbon-12 ("24") and the doublet of carbon-13. Traces are also present for Cerium-140, Erbium-166 and Tungsten-184.

The effect of the rapid diffusion of carbon-12 into the samples is readily apparent if one contrasts Figure 8 with Figure 9. If one models this diffusion as the case where a thick tracer coating is allowed to diffuse into an semi-infinite solid, the appropriate equation, as given by Shewman ²⁹, is:

$$\text{Concentration (x,t)} = (C'/2) [1 + \text{error function} \{ x / 2 \text{ square root } (Dt) \}]$$

Wherein:

x = distance in centimeters from initial boundary between tracer film and solid

t = time in seconds

C' = initial concentration in atomic % of tracer element

D = Diffusion constant (units of cm²/sec)

This equation can be solved for D at any point along the SIMS profile by converting the time to a distance using the 1300 angstrom/ minute cratering rate. At 100 minutes, the plot for carbon-12 and carbon-13 is nearing their steady state values. Solving for D at this point yields a value of D of 7.7×10^{-10} cm²/sec. Similar values for D, varying by approximately one order of magnitude, are found by solving at other points between 50 and 150 minutes.

This is an extremely encouraging result for the Diffusion Constant of cerium-erbium dicarbide. For comparison, the Diffusion Constants of several oxide and fluoride ion solid electrolytes that have the fluorite crystal structure are shown in Figure 10, reproduced here from

Inaba and Tagawa³⁰, who summarize the results from many studies. Note that at a temperature of 934 Centigrade/ 1207 Kelvin ($1000/1207 = .83$) The Diffusion constant of cerium erbium dicarbide would lie just below that of CaF_2 .

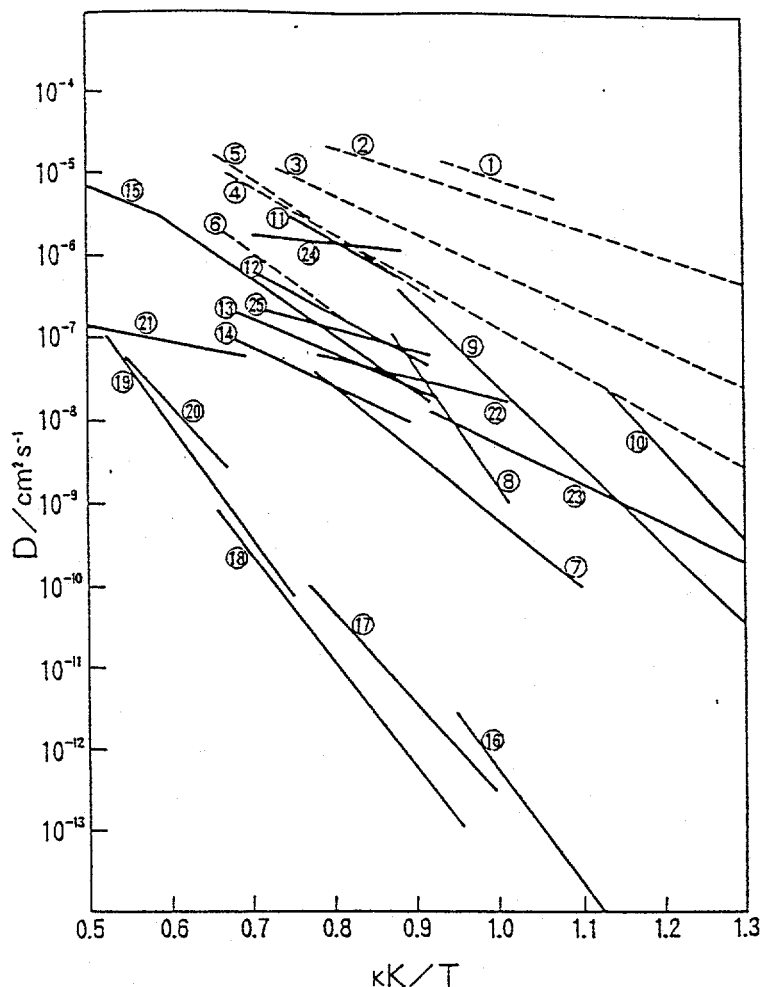


Fig. 10 Diffusion constants of anion sublattice in various fluorite compounds. The broken lines show the diffusion constants calculated using the Nernst-Einstein equation and the data shown in Fig. 1[1]. The solid lines show the diffusion constants obtained from the literatures. ① $\delta\text{-Bi}_2\text{O}_3$, ② $\text{Ce}_{1.8}\text{Gd}_{0.2}\text{O}_{1.9}$, ③ $(\text{ZrO}_2)_{0.9}(\text{Y}_2\text{O}_3)_{0.1}$, ④ $(\text{CaO})_{0.13}(\text{ZrO}_2)_{0.87}$, ⑤ $(\text{ThO}_2)_{0.93}(\text{Y}_2\text{O}_3)_{0.07}$, ⑥ $(\text{CaO})_{0.12}(\text{HfO}_2)_{0.88}$, ⑦ $\text{Zr}_{0.85}\text{Ca}_{0.15}\text{O}_{1.85}$ [28], ⑧ CaF_2 [30], ⑨ BaF_2 [31], ⑩ SrCl_2 [31], ⑪ $\text{Ce}_{0.6}\text{Y}_{0.4}\text{O}_{1.8}$ [32], ⑫ $\text{Ce}_{0.8}\text{Y}_{0.2}\text{O}_{1.9}$ [32], ⑬ $\text{Ce}_{0.9}\text{Y}_{0.1}\text{O}_{1.95}$ [32], ⑭ CeO_2 [32], ⑮ $\text{Zr}_{0.85}\text{Ca}_{0.15}\text{O}_{1.85}$ [33], ⑯ UO_2 [34], ⑰ PuO_2 [35], ⑱ UO_2 [36], ⑲ ThO_2 [37], ⑳ ThO_2 [38], ㉑ UO_{2-x} ($x = 0.01$) [39], ㉒ PuO_{2-x} ($x = 0.01$) [40], ㉓ UO_{2+x} ($x = 0.01$) [41], ㉔ CeO_8 [32], ㉕ $\text{CeO}_{1.92}$ [32].

FIGURE 8

NEG. SIMS PROFILE 6/30/96 REG 10 T=194.41 MIN. SPUT. ANGLE=60.0
 FILE: 07026_30 Nat C unannealed CeErC2 BI= 685.00 nA BV= 7.00 kV
 SCALE FACTOR= 253.346 k c/s. OFFSET= 0.000 k c/s

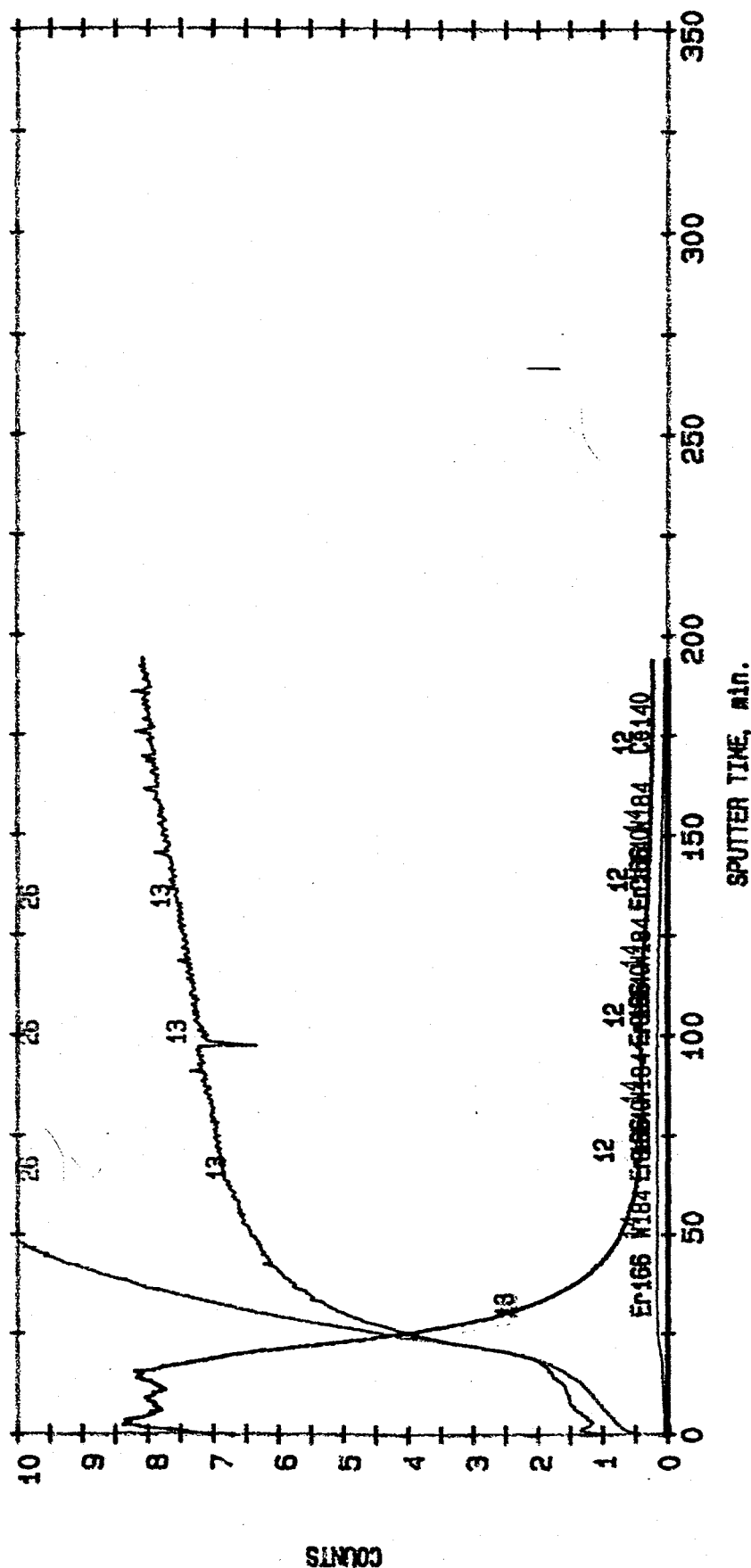
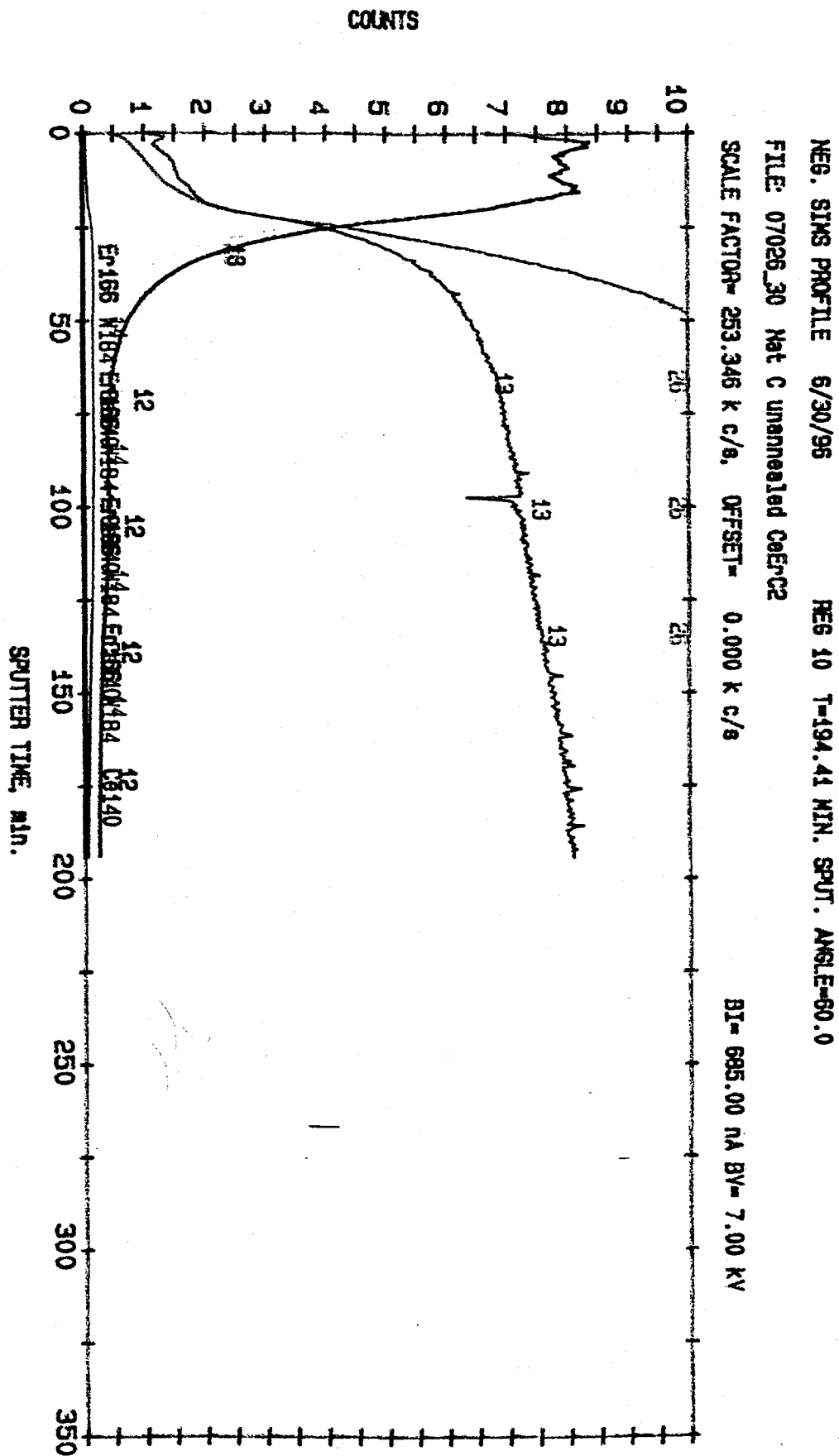


FIGURE 9



Plan for Next Quarter (12th Quarter)

In the upcoming 12th Quarter of this research project the following experimental procedures will be initiated:

1. Rare Earth Carbide ingots will be cast containing:
 - a. 50% by mole mixture of Cerium Dicarbide and Lutetium Dicarbide
 - b. 50% by mole mixture of Cerium Dicarbide and Samarium Dicarbide
 - c. 50% by mole mixture of Cerium Dicarbide and Ytterbium Dicarbide

These sample ingots will be made in the arc melt furnace and sub-divided so that each can be both x-rayed to determine the crystal structure of the mixture, and chemically analysed to determine the actual elemental composition resulting after arc melting.

2. After casting these 3 samples will be split into four sub-samples each.
3. One sub-sample will be sent off for chemical analysis to confirm elemental content.
4. The second sub-sample will be analyzed by high temperature x-ray diffraction at the facilities of the High Temperature Materials Laboratory at Oak Ridge.
5. The third sub-sample will be re-melted to form a circular pellet suitable for arc-evaporation coating with a carbon layer that will consist of 80 mole % carbon-13 isotope and 20 mole % carbon-12 isotope. These Arc-Evaporated coated sub-samples will be annealed at 900, 1200 and 1500 C under a partial pressure of argon.

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