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A COMPUTER PROGRAM FOR CALCULATING, TABULATING, AND
PLOTTING OUTGASSING RATES OF SELECTED GASES

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Carla L. Armstrong, and R. E. Clausen

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PLOTTING OUTGASSING RATES OF SELECTED GASES

D. S. Easton, Sandra H. Merriman,¹
Carla L. Armstrong¹, and R. E. Clausing

ABSTRACT

We have written a computer program in Fortran to be used at the Oak Ridge National Laboratory Computer Center on either an IBM 360/91 or 360/75 computer for calculating outgassing rates.

The experimental method is outlined, and the procedures for computing both total outgassing rates and rates based on measurement of partial pressures of various gases are described. Outgassing rates are calculated from the pressure drop across an orifice located between the chamber and the pumping system. Data from a residual-gas analyzer and three ion gages permit the simultaneous analysis of 12 gases. Results are available in both tabular and graphic form. The computer program is given along with a sample calculation and a series of plots of outgassing rate versus time. A Calcomp program for plotting data from a series of outgassing runs at different temperatures is also given. An example of plots of outgassing rates from a series of isothermal experiments is shown.

INTRODUCTION

We have written a computer program in Fortran to be used at the Oak Ridge National Laboratory Computer Center on either an IBM 360/91 or 360/75 computer for calculating outgassing rates.

The program was originally developed to calculate the outgassing rates of gases desorbed from NERVA fuel elements in an ultrahigh-vacuum environment.² It can be used in its present form for many other

¹Numerical Analysis Program, Mathematics Division.

²D. S. Easton and R. E. Clausing, "Outgassing of Nuclear Rocket Fuel Elements," paper presented at International Conference of the Vacuum Metallurgy Division of the American Vacuum Society, Anaheim, Calif., June 15-19, 1970. To be published as a Special Issue of The Journal of Vacuum Science and Technology.

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outgassing situations by simple changes in input constants. The equipment used to obtain input data for the calculations is included in most high-vacuum systems today.

EXPERIMENTAL METHOD

Figure 1 shows the schematic diagram of a vacuum system and the location of orifices and ion gages (P_1 , P_2 , and P_3) necessary for using this technique. The conductance of the orifice between the chamber and the pumping system should be a small fraction of the total speed of the pumping system to provide a constant pumping speed from the outgassing chamber, give high sensitivity, and prevent selective

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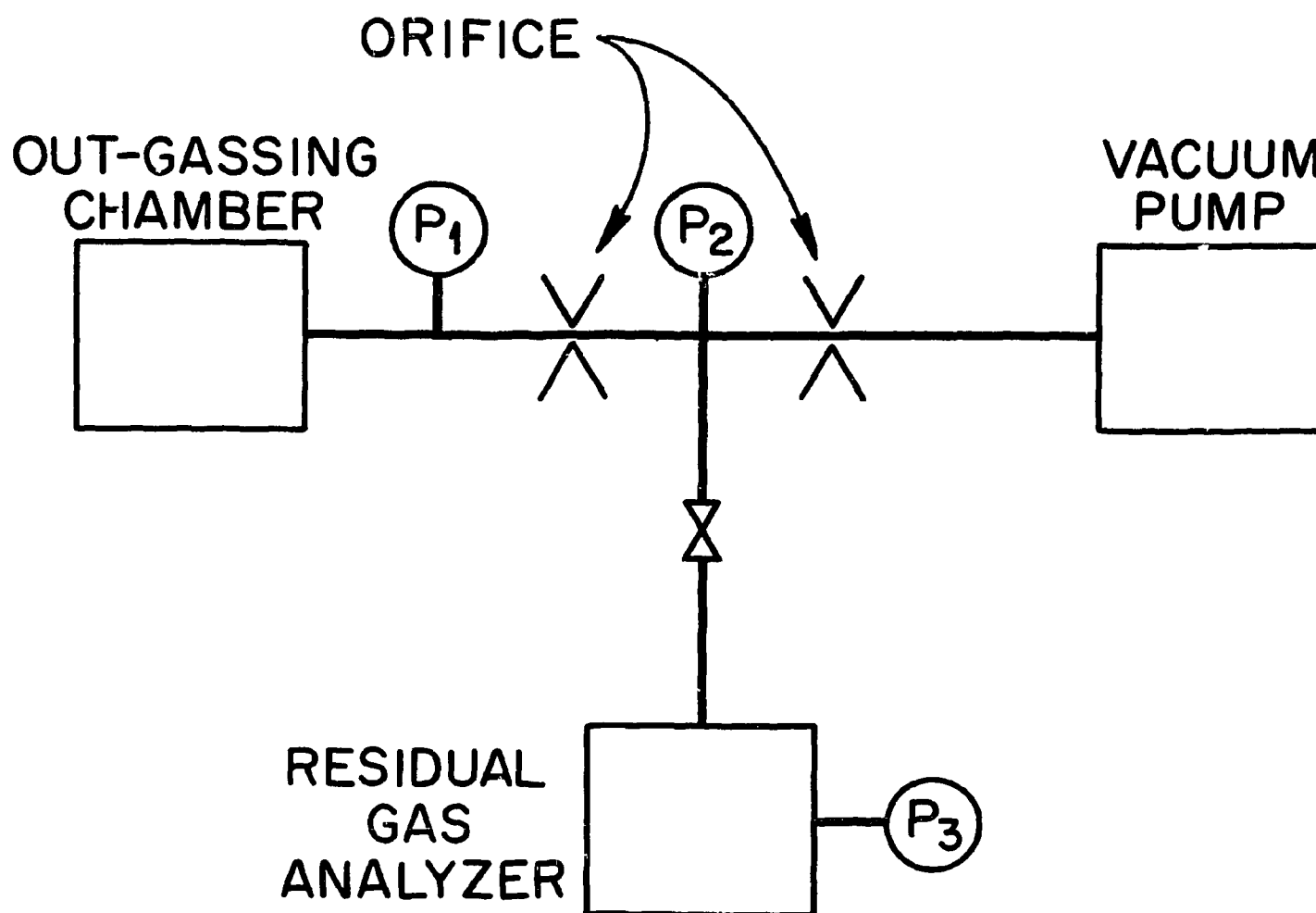


Fig. 1. Schematic Diagram of Vacuum System Showing Location of Gages and Orifice.

pumping of certain gases by the pumping system from interfering with the analysis. The outgassing rate for each gas is determined by multiplying the conductance of the orifice by the pressure drop across the orifice. (Corrections are made for gas composition, molecular weight, and temperature.) Outgassing rates in this work are given in units of torr liters per second. In order to relate to the surface area or mass of the material, the rates must be adjusted to either torr liters per second per square centimeter or torr liters per second per gram.

The program is consistent with the recommended practice for reporting outgassing data suggested by the American Vacuum Society.³ The following assumptions are made:

1. The sample and sample chamber are the only sources of gas.
2. Pumping speeds at all points of pressure measurement are limited by conductance with no selective pumping of individual gas species.
3. Steady-state flow conditions exist [in other words, the pressure changes that occur are slow in comparison to the time constant for the outgassing chamber ($\tau = 1$ sec).]
4. Ionization constants are assumed (based on values from the literature) for each gas to convert the readings of the ion gage and residual-gas analyzer to values of partial pressure in torr.

CALCULATION PROCEDURE

Pressure is measured at the following positions: P_1 - outgassing chamber, P_2 - vacuum manifold, P_3 - manifold of residual-gas analyzer.

Gases desorbed from the sample travel through a calibrated orifice between P_1 and P_2 and through a known conductance between P_2 and the pumping system. The pressure drop between these positions allows us to measure the flow of gas through the system by means of the following calculations.

³"American Vacuum Society Standard (tentative) AVS 9.1-1964," J. Vac. Sci. and Technol. 2(6) 314-319 (1965).

The outgassing rates are calculated⁴ by

$$q = K(P_1 - P_2) \quad (1)$$

where

q = outgassing rate (in torr liters per second),

K = orifice conductance (in torr liters per second),

= $3.64 [\text{area (in square centimeters)}] [(T/M)^{1/2}]$, where T is

absolute temperature in degrees Kelvin and M is molecular mass,

P_1 = pressure of outgassing chamber (in torr), and

P_2 = pressure of vacuum manifold (in torr).

In our case, the orifice conductance was 10 liters/sec for air at 300°K [3.64 times the area of the orifice (0.855 cm²) was 3.1 cm²; this value appears in lines 2130 and 2200 in the attached program (see Appendix A) and must be changed if an orifice of different diameter is used].

All pressures are corrected⁵ for temperatures other than 300°K by

$$P_{\text{corr}} = P_i (T_i / 300^\circ\text{K})^{1/2}. \quad (2)$$

In general, the pressure in manifold P_3 of the residual-gas analyzer is the same as that at P_2 ; however, in cases where the pressure is excessively high and the residual-gas analyzer is throttled by the connecting valve, a correction is made to P_2 for the individual gases (i) by the relation

$$P_{2(i)} = P_{3(i)} (P_2 / P_3). \quad (3)$$

For either the total or partial pressures, the ratio of the pressure drop across the orifice to the downstream pressure, P_2 or $P_{2(i)}$, is

$$(P_1 - P_2) / P_2 = \Delta P / P_2 = \Delta P_{(i)} / P_{2(i)}, \quad (4)$$

and the change in pressure for an individual gas is

$$\Delta P_{(i)} = (P_1 - P_2) (P_{3(i)} / P_3). \quad (5)$$

⁴Saul Dushman, Scientific Foundation of Vacuum Technique, 2nd ed., p. 91, Wiley, New York, 1965.

⁵P. A. Redhead, J. P. Hobson, and E. V. Kornelsen, in The Physical Basis of Ultrahigh Vacuum, pp. 281-287, Chapman & Hall, Ltd., London, 1968.

Therefore, the outgassing rate for gas (i) is

$$q_{(i)} = K_{(i)}(P_1 - P_2)(P_{3(i)}/P_3). \quad (6)$$

The total quantity of gas desorbed from the sample is the integral of the outgassing rate as a function of time:

$$Q = \int_{t_0}^t q(t)dt, \quad (7)$$

where

Q = total quantity of gas,

t_0 = initial time, and

t = time.

Scans of the spectra of the gas analyzer are recorded along with other data on a regular schedule. The intensities of the spectrometer peaks at 18 separate values of m/e (ratio of mass to charge), including all the major peaks of the 12 calibration gases, are recorded. These values plus the date, the accumulated time, the sample temperature, and the pressures of the outgassing chamber, vacuum manifold, and manifold of the residual-gas analyzer are put into a computer program. The program obtains a least-squares fit of a set of 18 simultaneous equations (18 values of m/e) with 12 unknowns (gases):

$$B_i = \sum_{j=1}^{12} A_{ij}X_j, \quad (8)$$

where

B_i = intensity of each peak (ion current),

A_{ij} = fractional part of gas as determined by experimental cracking pattern, and

X_j = ion current associated with each gas.

The coefficients of the equations are obtained from the cracking pattern.

The first tabular output from the computer includes the following for each data scan:

1. The pressures are corrected for thermal effects, and thermocouple readings in millivolts are changed to degrees Celsius.
2. For each peak, the measured ion current is compared with a calculated value based on the least-squares fit.

3. The tabulated ratio of P_1 to P_2 is printed to provide a check on pumping conditions of the system.

4. Ion currents are converted to corrected partial pressures, printed, and summed.

5. The partial pressures of the hydrocarbons are summed and printed separately.

6. The percentage composition is calculated and printed.

7. The outgassing rates are calculated as shown in Eq. (6).

8. The ion currents of the residual-gas analyzer are summed and divided by the pressure read from the ion gage to give a check on the total sensitivity of the residual-gas analyzer.

9. The readings from the residual-gas analyzer and the ion gage are compared by summing the partial pressures and comparing the total pressure to the reading from the ion gage after it has been corrected for composition.

The computer then sorts all the data and prints the time versus outgassing rate for each gas. These values are fitted to a power equation:

$$q = A(t/t_0)^B, \quad (9)$$

where

q = outgassing rate (in torr liters per second),

A = intercept at time t_0 (in torr liters per second),

t = time (in hours),

t_0 = one hour, and

B = slope of the curve for the log of the outgassing rate versus the log of time.

The values of A and B are tabulated for each gas. The program then integrates the fitted curve between selected times and tabulates the quantity of each gas evolved in the selected time interval.

The program includes a graphical output of the log of the outgassing rate versus the log of time. Data points and a curve are plotted for the ion gage, each gas, and the summed hydrocarbons. A composite graph containing selected gases is also available for comparison. The

experimenter may obtain a qualitative assessment of his results from the correlation coefficient and correlations of determination. These are convenient and useful for testing the fit to the relationship of Eq. (9) and for comparing the scatter in data for different gases or from different runs. The 95% confidence limits are tabulated for B and for the log of the outgassing rate (designated as log Y in the computer printout).

The program for outgassing rate, together with an example of an experiment in which outgassing data from a fuel element was taken for a period of 350 hr at a constant temperature, is included in this report as Appendix A. A second program, which compiles and plots outgassing rate as a function of temperature with time as a selected parameter, is attached as Appendix B. The input data for this program are obtained from a series of isothermal experiments. In our case, each experiment represents a separate sample hold at a different temperature.

ACKNOWLEDGMENTS

We wish to acknowledge the assistance of R. O. Williams and L. R. Lieto in the solution of Eq. (8).

APPENDIX A
FORTRAN REFERENCE LISTING

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**FTN,L,E,G.                                KEYWORDS = IF, DO, GOTO, READ, PRINT
PROGRAM OUTGAS
C
C THIS PROGRAM WAS WRITTEN TO HANDLE THE LARGE VOLUME OF DATA COLLECTED
C DURING THE OUTGASSING OF GRAPHITE IN AN ULTRA-HIGH VACUUM APPARATUS.
C THE PROGRAM USES DATA TAKEN AT INTERVALS OF TIME AND/OR TEMPERATURE
C FROM A RESIDUAL GAS ANALYZER AND ION GAGES TO CALCULATE THE FOLLOWING
C VALUES OF VARIOUS GASES (1) PARTIAL PRESSURE, (2) OUTGASSING RATE,
C (3) FIT OF THE RATE VS TIME TO AN ANALYTICAL EXPRESSION,
C (4) INTEGRATING OF THE DATA TO OBTAIN THE TOTAL QUANTITY OF GAS
C EVOLVED, (5) PROVIDES FOR GRAPHICAL PLOTTING, (6) PRINTS OUT CERTAIN
C CONTROL DATA FOR INFORMATION AND IDENTIFICATION.
C THE PROGRAM INCLUDES THESE 5 SUBROUTINES (1)PRINT, (2)LSFIT,
C (3)INTEGRAL (4)HPMINV, (5)GRAPHS.
C THE FOLLOWING DATA ARE NECESSARY FOR THE PROGRAM
C 1. DATE
C 2. ACCUMULATED TIME
C 3. TEMPERATURE OF THE SAMPLE
C 4. OUTGASSING CHAMBER PRESSURE (TORR)
C 5. VACUUM MANIFOLD PRESSURE (TORR)
C 6. RGA MANIFOLD PRESSURE (TORR)
C 7. CERTAIN SELECTED PEAKS (ION CURRENT IN AMPS) FROM A RESIDUAL
C    GAS ANALYZER.
C 8. TEMPERATURE OF THE APPARATUS.
C IN ADDITION THE CRACKING PATTERN, SENSITIVITY (AMPS/TORR), AND THE
C IONIZATION CONSTANTS (NORMALIZED TO NITROGEN) FOR EACH GAS MUST BE
C KNOWN. HOWEVER, THESE VALUES NEED NOT BE GENERATED FOR EVERY RUN
C AS DO THE VALUES LISTED ABOVE.
C FOR EACH SET OF DATA (ONE ELAPSED TIME OR TEMPERATURE), OUTPUT CONSISTS
C OF MEASURED PEAK HEIGHT, THE CALCULATED PEAK, DIFFERENCE BETWEEN
C THE MEASURED AND CALCULATED PEAK, THE PERCENT DIFFERENCE, THE
C PARTIAL PRESSURE AND OUTGASSING RATE OF EACH GAS, PERCENT OF TOTAL
C PRESSURE AND OUTGASSING FOR EACH GAS, THE SUM OF THE CURRENTS,
C TOTAL CURRENT/RGA PRESSURE, THE SUM OF THE PARTIAL PRESSURES, THE
C RGA ADJUSTED PRESSURE, AND THE DIFFERENCE IN THE RGA
C PRESSURE AND SUM.
C AN ADDITIONAL PRINT OUT SHOWS EACH GAS AND ALL THE ACCUMULATED
C OUTGASSING RATES AS A FUNCTION OF TIME OR TEMPERATURE.
C THE USER MAY SPECIFY 3 OTHER OPTIONS
C 1. BY SETTING LSQFIT=1, PROGRAM WILL PRINT A TABULATED LEAST SQUARES
C    FIT OF THE OUTGASSING RATE VS. TIME. A CURVE OF THE FORM
C     $Y = A * X^{**B}$  WILL BE FITTED TO THE DATA. IN THIS EQUATION,
C    Y=OUTGASSING RATE, A=INTERCEPT AT TIME 1, X=TIME IN HOURS,
C    AND B=SLOPE OF CURVE ON LOG-LOG PLOT.
C 2. BY SETTING INTEG=1, THE ABOVE EQUATION WILL BE INTEGRATED TO
C    SOLVE FOR THE OUTGASSING RATE AS A FUNCTION OF TIME.
C 3. A THIRD OPTION ALLOWS THE USER TO OBTAIN LOG-LOG OR LOG-LINEAR
C    PLOTS OF OUTGASSING RATE VS. TIME OR TEMPERATURE FOR EACH
C    GAS PLUS A COMPOSITE PLOT OF A SELECTION OF GASES.
C
C *** PREPARING INPUT ***
C
C ALL DATA CARDS FOLLOW THIS CONTROL CARD
C //GO.FT50F001 DD *
C
C THE FOLLOWING DATA ARE ENTERED IN COLUMNS THAT ARE RIGHT ADJUSTED.
C THE DATA CARDS OR SETS OF CARDS ARE ASSEMBLED AS FOLLOWS
C 1. CONTAINS THE VALUES OF LSQFIT AND INTEG IN COLUMN 5 AND 10
C    RESPECTIVELY. IF NEITHER OF THESE OPTIONS IS DESIRED, INCLUDE
C    A BLANK CARD.
C 2. A SET OF CARDS (NUMBER OF PEAKS * 2) CONTAINING VALUES OF THE
C    CRACKING PATTERN OF THE GASES, IN FIELDS OF 8 COLUMNS EACH.
C    FOR EACH M/E VALUE, THERE MUST BE 2 CARDS. THE FIRST CONTAINING
C    THE CRACKING PATTERN OF H, HE, CH4, H2O, N2, CO, O2, AR, C2,
C    C2H4. THE SECOND CONTAINING C2H6, C2H8.
C 3. VALUES OF THE RGA SENSITIVITY (IN AMPS/TORR) OF THE ABOVE GASES
C    IN THE SAME ORDER. 8 COLUMNS, 10 PER CARD.
C 4. CARDS CONTAINING THE IONIZATION CONSTANTS OF THE GASES. 8
C    COLUMNS, 10 PER CARD.
C 5. TEMPERATURE OF THE APPARATUS IN DEGREES C, (D), COLUMN 1-8.
C 6. 2 CARDS FOR IDENTIFICATION OF RUN, COLUMNS 1-80.
C 7. A SET OF CARDS FOR EACH TIME/TEMP. RUN CONTAINING
C    A. 1 CARD WITH THE FOLLOWING 6 VALUES IN FIELDS OF 8 COLUMNS
C       EACH, DATE(DAY AND MONTH), TIME(HOURS), TEMPERATURE
C       (MV OF CR-AL THERMOCOUPLE), CHAMBER PRESSURE(TORR),
C       VACUUM MANIFOLD PRESSURE(TORR), AND RGA MANIFOLD PRESSURE
C       (TORR).
C    B. VALUES OF ION CURRENTS OF 18 PEAKS AT M/E VALUES OF
C       2,4,12,13,14,15,16,17,18,22,26,27,28,29,30,32,40, AND 44.
C       8 COLUMNS, 8 PER CARD.
C 8. 1 BLANK CARD.
C IF PLOTS ARE DESIRED, SEE SUBROUTINE GRAPHS FOR DATA CARD DESCRIPTION
C AND INCLUDE THOSE DATA CARDS HERE. IF NO PLOTS ARE DESIRED, THIS
C CONCLUDES DATA AND THE LAST 2 CARDS IN THE DECK ARE THE FOLLOWING
C CONTROL CARDS.
C /*
C //
C

```

```

OUTG 890
OUTG 900
OUTG 910
OUTG 920
OUTG 930
OUTG 931
OUTG 932
OUTG 933
OUTG 934
OUTG 935
OUTG 940
OUTG 950
OUTG 951
OUTG 960
OUTG 970
OUTG 971
OUTG 972
OUTG 973
OUTG 974
OUTG 975
OUTG 976
OUTG 977
OUTG 980
OUTG 981
OUTG 982
OUTG 983
OUTG 990
OUTG 991
OUTG 992
OUTG 993
OUTG 994
OUT 1000
OUT 1001
OUT 1002
OUT 1003
OUT 1010
OUT 1020
OUT 1030 -----READ
OUT 1040
OUT 1050 -----DC
OUT 1060 -----READ
OUT 1070
OUT 1080 -----READ
OUT 1090 -----READ
OUT 1100
OUT 1110
OUT 1120
OUT 1130
OUT 1140
OUT 1150 -----DC
OUT 1160 -----DC
OUT 1170
OUT 1180 -----DC
OUT 1190 -----DC
OUT 1200
OUT 1210 -----DC
OUT 1220
OUT 1230
OUT 1240
OUT 1250
OUT 1260
OUT 1270
OUT 1280
OUT 1290 -----DC
OUT 1300 -----DC
OUT 1310
OUT 1320 -----DC
OUT 1330
OUT 1340
OUT 1350
OUT 1360
OUT 1370
OUT 1380
OUT 1390 -----READ
OUT 1400 -----READ
OUT 1410
OUT 1420
OUT 1430 -----PRINT
OUT 1440
OUT 1441
OUT 1450 -----PRINT
OUT 1460
OUT 1470 -----PRINT
OUT 1480
OUT 1490 -----PRINT
OUT 1500
OUT 1501
OUT 1510 -----DC
OUT 1520
OUT 1530 -----PRINT
OUT 1531
OUT 1540
OUT 1541
OUT 1542
OUT 1550 -----PRINT
OUT 1560
OUT 1570
OUT 1580
OUT 1590

```

```

C                                     OUT 1600
C READ DATE, TIME, TEMPERATURE OF RUN, CHAMBER PRESSURE, MANIFOLD PRES-OUT 1610
C SURE, RGA PRESSURE.                                     OUT 1620
C                                                         OUT 1630
C READ 10, DAY, HOURS(NC), XMLVOL, Z(1), Z(2), Z(3)      OUT 1640 -----READ
10  FORMAT (6E8.1)                                         OUT 1650
IF (DAY.EQ.C.O.AND.HOURS(NC).EQ.0.) GC TO 190             OUT 1660 IF
DO 140 I=1,3                                               OUT 1670 -----DO
I----- 140  ZZ(I)=Z(I)*G                                  OUT 1680
I-----          X=COEFF(I)                               OUT 1690
I-----          DO 145 I=1,10                             OUT 1700 -----DO
I----- 145  X=X+COEFF(I+1)*XMLVOL**I                     OUT 1710
TEMP(NC)=X                                                 OUT 1720
PRINT 11, (TETLE(IJ), IJ=1,20)                            OUT 1730 -----PRINT
11  FORMAT(1H1//1X,20A4)                                   OUT 1740
PPRINT 12, DAY, HOURS(NC), TEMP(NC), XMLVOL, Z(1), ZZ(1), Z(2), OUT 1750 -----PRINT
1  ZZ(2), Z(3), ZZ(3)                                     OUT 1751
12  FORMAT (1H, 'DATE =', F15.2/' HOURS =', F14.2/' TEMPERATURE (DEGREE OUT 1760
15 C.) =', F8.2, 10X, ' MILLIVOLTS (CR/AL) =', F8.2, 1P    OUT 1761
2/' CHAMBER PRESSURE =', E15.5, 10X, ' THERMAL CORRECTION =', E15.5/ OUT 1762
3' MANIFOLD PRESSURE =', E14.5, 10X, ' THERMAL CORRECTION =', E15.5/ OUT 1763
4' RGA PPESSURE =', E19.5, 10X, ' THERMAL CORRECTION =', E15.5// ) OUT 1764
C                                                         OUT 1770
C READ ION CURRENT FOR N PEAKS.                           OUT 1780
C                                                         OUT 1790
C READ 12, (V(I), I=1, N)                                  OUT 1800 -----READ
13  FORMAT (8E8.1)                                         OUT 1810
C                                                         OUT 1820
C SOLVE SYSTEM OF EQUATIONS. FIND COMPUTED M/E VALUES.   OUT 1830
C                                                         OUT 1840
I----- DO 155 I=1, M                                     OUT 1850 -----DO
I----- X=0                                               OUT 1860
I----- DO 150 J=1, N                                     OUT 1870 -----DO
I----- J----- 150 X=X+O(I,J)*V(J)                     OUT 1880
I----- 155  S(I)=X                                       OUT 1890
C                                                         OUT 1900 -----DO
I----- DO 165 I=1, N                                     OUT 1910
I----- X=0                                               OUT 1920 -----DO
I----- DO 160 J=1, M                                     OUT 1930
I----- J----- 160 X=X+S(J)*A(J,I)                     OUT 1940
I----- 165  C(I)=X                                       OUT 1950 -----PRINT
14  PRINT 14                                               OUT 1960
14  FORMAT (' M/E', 3X, 'MEASURED PEAK', 6X, 'CALCULATED M/E', 7X, 'DIFFER OUT 1961
1  RENCE', 9X, 'PERCENT DIFF', 10X, 'HEIGHT (AMPS)')      OUT 1970
C                                                         OUT 1980
C SUM ION CURRENTS                                         OUT 1990
C                                                         OUT 2000
U=0.                                                       OUT 2010 -----DO
I----- DO 170 I=1, N                                     OUT 2020
I----- PCNT=(C(I)-V(I))/V(I)*100.                       OUT 2030
I----- U=U+V(I)                                           OUT 2040
I----- DIFFER=C(I)-V(I)                                    OUT 2050 -----PRINT
I----- 170  PRINT 15, ME(I), V(I), C(I), DIFFER, PCNT    OUT 2060
15  FORMAT (17, 1PE15.5, 2E20.5, 2PE20.5)                 OUT 2070
RATIO=Z(1)/Z(2)                                           OUT 2080 -----PRINT
PRINT 16, RATIO                                           OUT 2090
16  FORMAT ( // ' RATIO OF GAGE P1 TO GAGE P2 =', 1PE12.5// ) OUT 2100
C                                                         OUT 2110
C COMPUTE PARTIAL PRESSURES AND OUTGASSING RATES FOR M GASES. OUT 2120
C                                                         OUT 2130
OUTGAS(NC,1)=(3.1*SQRT(D/28))*(ZZ(1)-ZZ(2))              OUT 2140
T1=(Z(1)-Z(2))/Z(3)                                       OUT 2150
W=0.0                                                      OUT 2160
X=0.0                                                      OUT 2170 -----DO
I----- DO 175 I=1, M                                     OUT 2180
I----- O1(I)=S(I)/CON(I)*G                                OUT 2190
I----- W=W+O1(I)                                           OUT 2200
I----- F1(I)=(3.1*SQRT(D/CON1(I)))*O1(I)*T1              OUT 2210
I----- 175  X=X+F1(I)                                       OUT 2220
OUTGAS(NC,2)=X                                             OUT 2230
J=0                                                        OUT 2240 -----DO
I----- DO 180 I=1, M                                     OUT 2250
I----- OUTGAS(NC,J)=F1(I)                                   OUT 2260
I----- 180  J=J+1                                           OUT 2270
OUTGAS(NC,15)=F1(2)+F1(10)+F1(11)+F1(12)                OUT 2280
H9=O1(3)+O1(10)+O1(11)+O1(12)

```

```

C
C FIND PERCENT OF TOTAL PRESSURE AND TOTAL OUTGASSING
C
      T2=Z(3)/W
      T3=100./W
      T4=100./OUTGAS(NC,2)
      WT=W*T3
      GT=OUTGAS(NC,2)*T4
      HGT=H9*T3
      PG10=OUTGAS(NC,15)*T4
      P9=0.0
I-----
I      DO 185 I=1,M
I      DT(I)=D1(I)*T3
I      PG(I)=F1(I)*T4
I----- 185  P9=D1(I)*T2/CONION(I)+P9
            P9=P9*G
            PRINT 17
17  FORMAT(' GAS',16X,'PRESSURE',12X,'PERCENT',12X,'OUTGASSING RATE',
1     7X,'PERCENT OF TOTAL',2CX,'TORR',13X,'OF TOTAL PRESSURE',5X,
2     'TORR LITERS/SEC',7X,'OUTGASSING RATE'// )
            PRINT 18,TITLE(1),TITLE(2),Z(1),OUTGAS(NC,1),TITLE(3),
1     TITLE(4),W,WT,OUTGAS(NC,2),GT,
2     (TITLE(2+I+3),TITLE(2+I+4),D1(I),DT(I),F1(I),PG(I),I=1,M),
3     TITLE(29),TITLE(30),H9,HGT,OUTGAS(NC,15),PG10
18  FORMAT (2A8,1PE12.5,26X,E18.5/(2A8,E12.5,5X,2PE16.5,5X,1PE18.5,
1     5X,2PE16.5,1P))
            TC=U/Z(3)
            DIFF=(P9-W)/W*100.
            DIFFER=P9-W
            PRINT 19,U,TC,W,P9,DIFFER,DIFF
19  FORMAT ('OSUM OF CURRENTS = ',1PE12.5,' AMPS'/' SENSITIVITY (TOTAL
1     CURRENT/RGA PRESSURE) = ',E12.5,' AMPS/TORR'/' SUMMATION PARTIAL
2     PRESSURES = ',E12.5,' TORR'/'
3     RGA ADJUSTED PRESSURE = ',E12.5,
4     ' TORR'/' DIFFERENCE (RGA ADJUSTED PRESSURE - SUMMATION PARTIAL
5     PRESSURES) = ',E12.5,' TORR'/' PERCENT DIFFERENCE = ',0PF9.3)
            GO TO 135
197 IF (NC.EQ.?) GO TO 215
            NC=NC-1
            ML=M+3
C
C SUBROUTINE PRINT PRINTS EACH GAS AND THE OUTGASSING RATES (FUNCTION
C OF TIME AND TEMPERATURE), ACCUMULATED FROM ALL THE CASES.
C
            CALL PRINT(OUTGAS,HOURS,TEMP,ML,TITLE,NC,HEADING,1)
I-----
I      DO 195 I=1,ML
I      IF(LSFIT.EQ.?) GO TO 195
I      IS=2*I-1
I      PRINT 20,TITLE(IS),TITLE(IS+1)
I      20  FORMAT(1H1/// ' GAS IS ',2A8//)
I
C
C SUBROUTINE LSFIT FINDS A AND B (IN EQUATION Y=A*X**B) BY METHOD OF
C LEAST SQUARES. (X=TIME, Y=OUTGASSING RATE)
C
I----- 195 CALL LSFIT(NC,HOURS,OUTGAS(1,I),AS(I),BS(I))
C
C PUNCH DATA FOR FUTURE USE BY SUBROUTINE COMPLET.
C
            PUNCH 21,(TITLE(IJ),IJ=1,20)
21  FORMAT (2A4)
            PUNCH 22,Z
22  PUNCH 22,(AS(I),BS(I),I=1,ML)
22  FORMAT (10ER.2)
            IF (INTEG.EQ.?) GO TO 205
I-----
I      DO 200 I=1,ML
I      IS=1*2-1
I      PRINT 22,TITLE(IS),TITLE(IS+1)
I      23  FORMAT(1H1/// ' GAS IS ',2A8//)
I
C
C SUBROUTINE INTEGRAL INTEGRATES Y=A*X**B TO FIND TOTAL OUTGASSING.
C
I----- 200 CALL INTEGRAL(AS(I),BS(I))
C
C TEST TO SEE IF PLOTS ARE DESIRED . IF SO, SET UP LIMITS FOR PLOTTING
C
205 READ (5C,74,END=215) LINE
24  FORMAT (I5)
            XAL(1)=1000.
            XAL(2)=0.
            YL(1)=.1
            YL(2)=0.
J-----
J      DO 210 J=1,NC
J      IF (HOURS(J).LT.XAL(1)) XAL(1)=HOURS(J)
J      IF (HOURS(J).GT.XAL(2)) XAL(2)=HOURS(J)
J I-----
J I      DO 210 I=1,ML
J I      IF (OUTGAS(J,I).LT.YL(1)) YL(1)=OUTGAS(J,I)
J I      IF (OUTGAS(J,I).GT.YL(2)) YL(2)=OUTGAS(J,I)
J I----- 210 CALL GRAPHS(OUTGAS,HOURS,XTITLE(1),ML,TITLE,NC,BS)
            CALL GRAPHS(OUTGAS,TEMP,XTITLE(2),ML,TITLE,NC,BS)
            CALL ADVANS
215  STOP
            END
**** STATEMENT 215 + 1 ERROR DAD2

```

TABLE OF VARIABLE NAMES

VARIABLE NAME	ARRAY DIMENSIONS	TOTAL NO ELEMENTS	ELEMENT TYPE	DECLARATION	CROSS REFERENCE TABLE (BY SEQUENCE NUMBERS)
A	(15,25)	375	REAL*4	LOCAL	930, 1060, 1220, 1330, 1490, 1930
ADVANS				SUBROUTINE	3070
AS	(20)	20	REAL*4	LOCAL	930, 2720, 2790, 2890
B	(15,15)	225	REAL*4	LOCAL	930, 1170, 1280, 1330
BLK1		204	BYTES	COMMON LABEL	900
BS	(20)	20	REAL*4	LOCAL	930, 2720, 2790, 2890, 3050, 3060
C	(25)	25	REAL*4	LOCAL	930, 1940, 2020, 2040, 2050
COEFF	(11)	11	REAL*4	LOCAL (DATA)	930, 950, 1690, 1710
CON	(15)	15	REAL*4	LOCAL	930, 1520, 1530, 2180
CONION	(15)	15	REAL*4	LOCAL	930, 1090, 1520, 1530, 2430
CON1	(15)	15	REAL*4	LOCAL (DATA)	930, 1010, 2200
D			REAL*4	LOCAL	1390, 1470, 1570, 1580, 2130, 2200
DATE	(2)	2	REAL*4	LOCAL	930, 1420, 1430, 1550
DAY			REAL*4	LOCAL	1640, 1660, 1750
DIFF			REAL*4	LOCAL	2500, 2520
DIFFER			REAL*4	LOCAL	2040, 2050, 2510, 2520
DT	(15)	15	REAL*4	LOCAL	930, 2410, 2470
D1	(15)	15	REAL*4	LOCAL	930, 2180, 2190, 2200, 2280, 2410, 2430, 2470
EATGR		4	BYTES	COMMON LABEL	910
EMAX			REAL*4	LOCAL	1280
FI	(15)	15	REAL*4	LOCAL	930, 2200, 2210, 2250, 2270, 2420, 2470
G			REAL*4	LOCAL	1580, 1680, 2190, 2440
GASES	(50)	50	REAL*8	LOCAL (DATA)	990, 930, 990, 1490
GASLEG	(50)	50	REAL*8	COMMON/HILC (DATA)	890, 920, 930, 980
GRAPH5				SUBROUTINE	3050, 3060
GT			REAL*4	LOCAL	2360, 2470
HEADING	(14)	14	REAL*8	LOCAL (DATA)	890, 930, 1000, 2620
HILC		576	BYTES	COMMON LABEL	920
HOURS	(50)	50	REAL*4	LOCAL	930, 1640, 1660, 1750, 2620, 2720, 3000, 3010, 3050
HPMINV				SUBROUTINE	1280
HQ			REAL*4	LOCAL	2280, 2370, 2470
HST			REAL*4	LOCAL	2370, 2470
I			INTEGER*4	LOCAL	1060, 1080, 1090, 1150, 1170, 1180, 1220, 1230, 1290, 1330, 1340, 1490, 1510, 1520, 1530, 1670, 1680, 1700, 1710, 1800, 1850, 1880, 1890, 1900, 1930, 1940, 2010, 2020, 2030, 2040, 2050, 2170, 2180, 2190, 2200, 2210, 2240, 2250, 2400, 2410, 2420, 2430, 2470, 2630, 2650, 2720, 2790, 2820, 2890, 3020, 3030, 3040

[illegible]

XAL	(2)	2	REAL*4	COMMON/HILO	/	920,	930,	2950*	2960*	3000*	3010*
XMLVOL			REAL*4	LOCAL		1640,	1710,	1750			
XTIT	(4)	4	REAL*8	LOCAL (DATA)		890,	930,	940,	3050,	3060	
YL	(2)	2	REAL*4	COMMON/HILO	/	920,	930,	2970*	2980*	3030*	3040*
Z	(3)	3	REAL*4	LCCAL		930,	1640,	1680,	1750,	2070,	2140, 2320,
ZZ	(3)	3	REAL*4	LOCAL		2490					
ZZ			REAL*4	LCCAL		930,	1680*	1750,	2130,	2470	
ZZ						2780					

* = VARIABLES USED ON LEFT HAND SIDE OF EQUAL SIGN

INPUT / OUTPUT TABLE

DEFINING SEQ. NO.	I/O OPERATION	LOGICAL UNIT	I/O TYPE	FORMAT USED	I/O LIST
1030	READ	50	BCD	1	LSQFIT, INTEG
1060	READ	50	BCD	2	(A(I,J), I=1,M)
1080	READ	50	BCD	2	(RGA(I), I=1,M)
1090	READ	50	BCD	2	(CONION(I), I=1,M)
1390	READ	50	BCD	10	D
1400	READ	50	BCD	3	(TETLE(IJ), IJ=1,40)
1640	READ	50	BCD	10	DAY, HOURS(NC), XMLVOL, Z(1), Z(2), Z(3)
1800	READ	50	BCD	13	(V(I), I=1,N)
2930	READ	50	BCD	24	LINE
1430	PRINT	51	BCD	4	DATE
1450	PRINT	51	BCD	5	(TETLE(IJ), IJ=1,40)
1470	PRINT	51	BCD	6	D
1490	PRINT	51	BCD	7	(GASES(I), I=1,13), ((ME(J), (A(I,J), I=1,M)), J=1,N)
1530	PRINT	51	BCD	8	(TITLE(2*I+3), TITLE(2*I+4), CONION(I), PGA(I), CON(I), I=1,M)
1550	PRINT	51	BCD	9	DATE, (TETLE(IJ), IJ=1,40)
1730	PRINT	51	BCD	11	(TETLE(IJ), IJ=1,20)
1750	PRINT	51	BCD	12	DAY, HOURS(NC), TEMP(NC), XMLVOL, Z(1), ZZ(1), Z(2), ZZ(2), Z(3), ...
1950	PRINT	51	BCD	14	
2050	PRINT	51	BCD	15	ME(I), V(I), C(I), DIFFER, PCNT
2080	PRINT	51	BCD	16	RATIO
2450	PRINT	51	BCD	17	
2470	PRINT	51	BCD	18	TITLE(1), TITLE(2), ZZ(1), OUTGAS(NC,1), TITLE(3), TITLE(4), W, ...
2520	PRINT	51	BCD	19	U, TC, W, P9, DIFFER, DIFF
2660	PRINT	51	BCD	20	TITLE(15), TITLE(15+1)
2840	PRINT	51	BCD	23	TITLE(15), TITLE(15+1)
2760	PUNCH	52	BCD	21	(TETLE(IJ), IJ=1,20)
2780	PUNCH	52	BCD	22	Z3
2790	PUNCH	52	BCD	22	(AS(I), BS(I), I=1,ML)

```

C
C
SUBROUTINE PRINT(X,HOURS,TEMP,ML,TITLE,NC,HEADING,N)

REAL*8 TITLE( 50),HEADING(14)
DIMENSION X( 50,20),HOURS( 50),TEMP( 50)
NPAGES=NC/55
IREM=NC-NPAGES*55
DO 150 I=1,ML,2
  IS=2*I-1
  IK=IS+2
  IF(NPAGES.GE.1) GO TO 100
  IF(I.GT.1) GO TO 110
  IREM=0
  LINES=NC
  JJJ=0
  GO TO 110
100  L=0
  LINES=55
  JJJ=55*L
110  DO 140 J=1,LINES
  JJ=JJJ+J
  IF(I.EQ.ML.AND.J.EQ.1) 115,120
  PRINT 1,(HEADING(I),II=N,N*6),TITLE(IS),TITLE(IS+1),HOURS(JJ),
  1 TEMP(JJ),X(JJ,I)
  FORMAT(1P1/// 1X,7A8//2A8,F7.2,3X,F9.2,5X,1PE13.5)
  GO TO 140
120  IF(I.NE.ML) GO TO 125
  PRINT 2,HOURS(JJ),TEMP(JJ),X(JJ,I)
  FORMAT(16X,F7.2,3X,F9.2,5X,1PE13.5)
  GO TO 140
125  IF(J.EQ.1) 120,135
  PRINT 3,(HEADING(I),II=N,N*6),(HEADING(I),II=N,N*6),TITLE
  1(IS),TITLE(IS+1),HOURS(JJ),TEMP(JJ),X(JJ,I),TITLE(IK),TITLE
  2(IK+1),HOURS(JJ),TEMP(JJ),X(JJ,I+1)
  3 FORMAT(1H1/// 1X,7A8,7X,7A8//2(2A8,CPF7.2,3X,F9.2,5X,1PE13.5,
  1 10X))
  GO TO 140
135  PRINT 4,HOURS(JJ),TEMP(JJ),X(JJ,I),HOURS(JJ),TEMP(JJ),X(JJ,I+1)
  4 FORMAT(16X, CPF7.2,3X,F9.2,5X,1PE13.5,26X,CPF7.2,3X,F9.2,5X,
  1 1PE13.5)
140  CONTINUE
  IF(NPAGES.EQ.0) GO TO 150
  L=L+1
  IF(L-NPAGES) 105,145,150
145  IF(IREM.EQ.0) GO TO 150
  LINES=IREM
  GO TO 110
150  CONTINUE
  RETURN
  END

PRINT 10
PRINT 20
PRINT 30
PRINT 40
PRINT 50
PRINT 60
PRINT 70
PRINT 80 -----DO
PRINT 90
PRINT 100
PRINT 110 IF
PRINT 120 IF
PRINT 130
PRINT 140
PRINT 150
PRINT 160 -----GOTO
PRINT 170
PRINT 180
PRINT 190
PRINT 200 -----DO
PRINT 210
PRINT 220 IF
PRINT 230 -----PRINT
PRINT 231
PRINT 240
PRINT 250 -----GOTO
PRINT 260 IF
PRINT 270 -----PRINT
PRINT 280
PRINT 290 -----GOTO
PRINT 300 IF
PRINT 310 -----PRINT
PRINT 311
PRINT 312
PRINT 320
PRINT 321
PRINT 330 -----GOTO
PRINT 340 -----PRINT
PRINT 350
PRINT 351
PRINT 360
PRINT 370 IF
PRINT 380
PRINT 390 IF
PRINT 400 IF
PRINT 410
PRINT 420 -----GOTO
PRINT 430
PRINT 440
PRINT 450

```

TABLE OF VARIABLE NAMES

VARIABLE NAME	ARRAY DIMENSIONS	TOTAL NO ELEMENTS	ELEMENT TYPE	DECLARATION	CROSS REFERENCE TABLE (BY SEQUENCE NUMBERS)					
HEADING	(14)	14	REAL*8	PARAMETER	10,	40,	230,	310		
HOURS	(50)	50	REAL*4	PARAMETER	10,	50,	230,	270,	310,	340
I			INTEGER*4	LOCAL	80*, 310,	90, 340	120,	220,	230,	260, 270,
II			INTEGER*4	LOCAL	230*	310*				
IK			INTEGER*4	LOCAL	100*	310				
IREM			INTEGER*4	LOCAL	70*	130*	400,	410		
IS			INTEGER*4	LOCAL	90*	100,	230,	310		
J			INTEGER*4	LOCAL	200*	210,	220,	300		
JJ			INTEGER*4	LOCAL	210*	230,	270,	310,	340	
JJJ			INTEGER*4	LOCAL	150*	190*	210			
L			INTEGER*4	LOCAL	170*	190,	380*	390		
LINES			INTEGER*4	LOCAL	140*	180*	200,	410*		
ML			INTEGER*4	PARAMETER	10,	80,	220,	260		
N			INTEGER*4	PARAMETER	10,	230,	310			
NC			INTEGER*4	PARAMETER	10,	60,	70,	140		
NPAGES			INTEGER*4	LOCAL	60*	70,	110,	270,	390	
PRINT			REAL*4	ENTRY POINT	10					
TEMP	(50)	50	REAL*4	PARAMETER	10,	50,	230,	270,	310,	340
TITLE	(50)	50	REAL*8	PARAMETER	10,	40,	230,	310		
X	(50,20)	1000	REAL*4	PARAMETER	10,	50,	230,	270,	310,	340

* = VARIABLES USED ON LEFT HAND SIDE OF EQUAL SIGN

INPUT / OUTPUT TABLE

DEFINING SEQ. NO.	I/O OPERATION	LOGICAL UNIT	I/O TYPE	FORMAT USED	I/O LIST
230	PRINT	51	BCD	1	(HEADING(I1), I1=N,N+6), TITLE(15), TITLE(15+1), HOURS(JJ), ...
270	PRINT	51	BCD	2	HOURS(JJ), TEMP(JJ), X(JJ, 1)
310	PRINT	51	BCD	2	(HEADING(I1), I1=N,N+6), (HEADING(I11), I11=N,N+6), TITLE(15), ...
340	PRINT	51	BCD	4	HOURS(JJ), TEMP(JJ), X(JJ, 1), HOURS(JJ), TEMP(JJ), X(JJ, 1+1)

```

SUBROUTINE LSFIT(NC,X,Y,AS,RS)
C
C
C **** IT IS IMPORTANT TO NOTE HERE THAT ALTHOUGH THE USE OF THE CORPE-
C LATION COEFFICIENT IS NOT LEGITIMATE IN A STATISTICAL SENSE
C BECAUSE THE X VALUES IN THIS PROGRAM ARE NOT RANDOM, IT DOES
C GIVE SOME INDICATION OF THE GOODNESS OF THE LEAST SQUARES FIT.
C
C
COMMON/BLK1/TEMP,LSQFIT
COMMON /FITTOGP/ OUTGSP( 50,20),NS( 50),HOURP( 50,20),CALCG
1 ( 50,20),I1,TEMPP( 50,20)
DIMENSION X( 50),Y( 50),D1( 50),D2( 50),TEMP( 50),
1 YLOG(50),Y2(50),XXMEAN(50)
DATA (I1=0)
I1=I1+1
N = 0
DO 100 I=1,NC
I IF (Y(I).LE.0.0.OR.X(I).LE.1.0E-02) GO TO 100
N=N+1
D1(I)=LOG(X(I))
D2(I)=LOG(Y(I))
TEMPP(N,I1)=TEMP(I)
100 CONTINUE
NS(I1)=N
IF (N.LT.2) GO TO 170
Q3=Q4=Q5=Q6=Q7=0.0
DO 105 J=1,N
J Q3=Q3+D1(J)
J Q4=Q4+D2(J)
J Q5=Q5+D1(J)*D2(J)
J Q6=Q6+D1(J)*D1(J)
J Q7=Q7+D2(J)*D2(J)
105 Q9=(FLOAT(N)*Q5-Q3*Q4)/(FLOAT(N)*Q6-Q3*Q3)
Q8=(Q4-Q3*Q9)/FLOAT(N)
T=.306
DO 110 J=1,N
J YLOG(J)=Q8+Q9*D1(J)
J Y1YC=D2(J)-YLOG(J)
J Y2(J)=Y1YC*Y1YC
110 SUMYYC=Y2(J)
DO 115 J=1,N
J SUMYYC=SUMYYC+Y2(J)
J XBAR=Q3/N
DO 120 J=1,N
J XXMEAN(J)=(D1(J)-XBAR)*(D1(J)-XBAR)
120 SUMXXB=XXMEAN(1)
DO 125 J=1,N
J SUMXXB=SUMXXB+XXMEAN(J)
125 S2=SUMYYC/(N-2)
ALPHA=Q8+Q9*XBAR
CONF8=T*SQR(S2/SUMXXB)
CONF8=T*SQR(S2/N)
XXX=(FLOAT(N)*Q6-Q3*Q3)*(FLOAT(N)*Q7-Q4*Q4)
IF (XXX.GT.0.0) GO TO 130
Q0=0.0
GO TO 135
130 Q0=(FLOAT(N)*Q5-Q3*Q4)/SQR(XXX)
135 IF(Q8.GT.174.) GO TO 170
AS=EXP(Q8)
Q02=Q0*Q0
BS=Q9
IF(LSQFIT.EQ.0) GO TO 145
IF(XXX.GT.0.0) GO TO 140
PRINT 1,AS,BS,ALPHA,CONF8,CONF8
1 FORMAT (' POWER Y=A**B WITH A = 'E13.5,' AND B = 'E13.5,/'
15X,'USING THE MODEL LOG(Y)=ALPHA+B*(LOG(X)-XBAR) WHERE XBAR=MEAN',
2 ' VALUE OF LOG(X(I)) AND ALPHA = LOG A + B * XBAR,/'
35X,' ALPHA = 'E13.5,5X,'CONFIDENCE LIMIT ON ALPHA = 'E13.5,5X,
4 'CONFIDENCE LIMIT ON B = 'E13.5
5// INDEXES CORRELATION COEFFICIENT DOES NOT EXIST. ALL DEPENDEN
6NT VALUES ARE THE SAME. BAD FIT.' //2X,
7'X',10X,'Y',12X,'Y CALC.',10X,'DIFFER.',8X,'PCT DIFF.',4X,'LOG OF
8Y',7X,'CONFIDENCE LIMIT ON LOG Y'//
GO TO 145
140 PRINT 2,AS,BS,ALPHA,CONF8,CONF8,Q0,Q02
2 FORMAT (' POWER Y=A**B WITH A = 'E13.5,' AND B = 'E13.5,/'
15X,'USING THE MODEL LOG(Y)=ALPHA+B*(LOG(X)-XBAR) WHERE XBAR=MEAN',
2 ' VALUE OF LOG(X(I)) AND ALPHA = LOG A + B * XBAR,/'
35X,' ALPHA = 'E13.5,5X,'CONFIDENCE LIMIT ON ALPHA = 'E13.5,5X,
4 'CONFIDENCE LIMIT ON B = 'E13.5
5// INDEXES CORRELATION COEFFICIENT = 'E13.5,10X,'CORRELATION
6 OF DETERMINATION = 'E13.5//2X,
7'X',10X,'Y',12X,'Y CALC.',10X,'DIFFER.',8X,'PCT DIFF.',4X,'LOG OF
8Y',7X,'CONFIDENCE LIMIT ON LOG Y'//

```

```

J----- 145 DO 165 J=1,N
J          W7=EXP(D1(J))
J          W8=EXP(D2(J))
J          W9=AS*W7**Q9
J          Q4=W9/W8-1.
J          Z7=W9-W8
J          CONF= T*SQRT(S2*(1/N+XXMEAN(J)/SUMXXB+1.0))
J          IF (Q4.LT.0.)GO TO 150
J          Q4=IFIX(1000.*Q4+.5)/10.
J          GO TO 155
J          150 Q4=IFIX(1000.*Q4-.5)/10.
J          155 IF(LSQFIT.EQ.0) GO TO 160
J          PRINT 3,W7,W8,W9,Z7,Q4,YLOG(J),CONF
J          160 OUTGSP(J,I1)=W8
J          HJURP(J,I1)=W7
J          CALOG(J,I1)=W9
J----- 165 CONTINUE
J          3  FORMAT (F7.2,1P6E15.4)
J          RETURN
J          170 PRINT 4,N
J          4  FORMAT(1H1,'THE SUBROUTINE LSFIT WHICH PERFORMS A LEAST SQUARES FIT
J          IF WAS CALLED, BUT IT IS IMPOSSIBLE TO PERFORM SUCH A FIT BECAUSE'
J          2' THERE ARE EITHER TOO FEW DATA POINTS (N=0 OR 1) OR THE OUTGASSINLS
J          3G RATES ARE SO SMALL THEY ARE'/' MEANINGLESS (N.GT.1). IN THIS PARLS
J          4TICULAR CASE N= ',I3)
J          NS(I1)=0
J          AS=BS=0.0
J          CONTINUE
J          RETURN
J          END
LSFI 680 -----DO
LSFI 690
LSFI 700
LSFI 710
LSFI 720
LSFI 730
LSFI 740
LSFI 750 IF
LSFI 760
LSFI 770 -----GOTO
LSFI 780
LSFI 790 IF
LSFI 800 -----PRINT
LSFI 810
LSFI 820
LSFI 830
LSFI 840
LSFI 850
LSFI 860
LSFI 870 -----PRINT
LSFI 880
LSFI 881
LSFI 882
LSFI 883
LSFI 884
LSFI 890
LSFI 900
LSFI 910
LSFI 920
LSFI 930

```

TABLE OF VARIABLE NAMES

VARIABLE NAME	ARRAY DIMENSIONS	TOTAL NO ELEMENTS	ELEMENT TYPE	DECLARATION	CROSS REFERENCE TABLE (BY SEQUENCE NUMBERS)
ALPHA			REAL*4	LOCAL	490* 630, 660
AS			REAL*4	PARAMETER	10, 580* 630, 660, 710, 900*
BLK1		204	BYTES	COMMON LABEL	100
BS			REAL*4	PARAMETER	10, 600* 630, 660, 900*
CALOG	(50,20)	1000	REAL*4	COMMON/FITTOGR /	110, 830*
CONF			REAL*4	LOCAL	740* 800
CONFA			REAL*4	LOCAL	510* 630, 660
CONFB			REAL*4	LOCAL	500* 630, 660
D1	(50)	50	REAL*4	LOCAL	120, 190* 270, 290, 300, 360, 440, 690
D2	(50)	50	REAL*4	LOCAL	120, 200* 280, 290, 310, 370, 700
EXP			REAL*4	FUNCTION	580, 690, 700
FITTOGR		16204	BYTES	COMMON LABEL	110
FLCAT			REAL*4	FUNCTION	320, 330, 520, 560
HOURP	(50,20)	1000	REAL*4	COMMON/FITTOGR /	110, 820*
I			INTEGER*4	LOCAL	160* 170, 190, 200, 210
IFIX			INTEGER*4	FUNCTION	760, 780
I1			INTEGER*4	COMMON/FITTOGR / (DATA)	110, 130, 140* 210, 230, 810, 820, 830, 890
J			INTEGER*4	LOCAL	260* 270, 280, 290, 300, 310, 350* 360, 370, 380, 400* 460, 470, 680* 690, 700, 740, 800, 810, 820, 830
LOGF			REAL*4	FUNCTION	190, 200
LSFIT			INTEGER*4	ENTRY POINT	10
LSOFIT			INTEGER*4	COMMON/BLK1 /	100, 610, 790
N			INTEGER*4	LOCAL	150* 180* 190, 200, 210, 230, 240, 260, 320, 330, 350, 400, 420, 430, 460, 480, 510, 520, 560, 680, 740, 870
NC			INTEGER*4	PARAMETER	10, 160
NS	(50)	50	INTEGER*4	COMMON/FITTOGR /	110, 230* 890*
CUTGSP	(50,20)	1000	REAL*4	COMMON/FITTOGR /	110, 810*
Q0			REAL*4	LOCAL	540* 560* 590, 660
Q02			REAL*4	LOCAL	590* 660
Q3			REAL*4	LOCAL	250* 270* 320, 330, 420, 520, 560
Q4			REAL*4	LOCAL	250* 280* 320, 330, 520, 560, 720* 750, 760* 780* 800
Q5			REAL*4	LOCAL	250* 290* 320, 560
Q6			REAL*4	LOCAL	250* 300* 320, 520
Q7			REAL*4	LOCAL	250* 310* 520
Q8			REAL*4	LOCAL	320* 360, 490, 570, 580
Q9			REAL*4	LOCAL	320* 330, 360, 490, 600, 710
SQPT			REAL*4	FUNCTION	500, 510, 560, 740
SUMXXB			REAL*4	LOCAL	450* 470* 500, 740
SUMYYC			REAL*4	LOCAL	390* 410* 480
SZ			REAL*4	LOCAL	480* 500, 510, 740

T			REAL*4	LOCAL	340*	500,	510,	740
TEMP	(50)	50	REAL*4	COMMON/BLK1 /	100,	120,	210	
TEMPP	(50,20)	1000	REAL*4	COMMON/FITTOGR /	110,	210*		
w7			REAL*4	LOCAL	690*	710,	800,	820
w8			REAL*4	LOCAL	700*	720,	730,	800, 810
w9			REAL*4	LOCAL	710*	720,	730,	800, 830
X	(50)	50	REAL*4	PARAMETER	10,	120,	170,	190
XBAR			REAL*4	LOCAL	420*	440,	490	
XXMEAN	(50)	50	REAL*4	LOCAL	120,	440*	450,	470, 740
XXX			REAL*4	LOCAL	520*	530,	560,	620
Y	(50)	50	REAL*4	PARAMETER	10,	120,	170,	200
YIYC			REAL*4	LOCAL	370*	380		
YLOG	(50)	50	REAL*4	LOCAL	120,	360*	370,	800
Y2	(50)	50	REAL*4	LOCAL	120,	380*	390,	410
Z7			REAL*4	LOCAL	730*	800		

* = VARIABLES USED ON LEFT HAND SIDE OF EQUAL SIGN

INPUT / OUTPUT TABLE					
DEFINING SEQ. NO.	I/O OPERATION	LOGICAL UNIT	I/O TYPE	FORMAT USED	I/O LIST
630	PRINT	51	BCD	1	AS,BS,ALPHA,CONFA,CONFB
660	PRINT	51	BCD	2	AS,BS,ALPHA,CONFA,CONFB,CO,Q02
800	PRINT	51	BCD	3	W7,W8,W9,Z7,Q4,YLCG(J),CCNF
870	PRINT	51	BCD	4	N

*** STATEMENT 6 + EFFCP CAD2

TABLE OF VARIABLE NAMES

VARIABLE NAME	ARRAY DIMENSIONS	TOTAL NO ELEMENTS	ELEMENT TYPE	DECLARATION	CROSS REFERENCE TABLE (BY SEQUENCE NUMBERS)						
ABS			REAL*4	FUNCTION	250						
AS			REAL*4	PARAMETER	10,	100,	120,	170,	190,	260	
BS			REAL*4	PARAMETER	10,	100,	120,	170,	190,	260	
EXTRA	(6)	6	REAL*4	LOCAL (DATA)	60,	80,	250,	260			
I			INTEGER*4	LOCAL	140*, 310,	150, 330,	160, 340,	170, 390*	180, 400	220,	270,
ICOUNT			INTEGER*4	LOCAL (DATA)	40,	90*	210,	360			
INTEGRAL			INTEGER*4	ENTRY POINT	10						
I1			INTEGER*4	LOCAL	240*	250,	260				
J			INTEGER*4	LOCAL	110*, 290	200*	210,	220,	230,	270,	310,
CRTLS			REAL*4	LOCAL	260*	270					
Q			REAL*4	LOCAL	170*	190*	210,	270,	310		
T	(3,20)	60	REAL*4	LOCAL (DATA)	50, 270,	80, 310,	150, 330,	160, 340	170,	180,	220,
TOTAL	(100)	100	REAL*4	LOCAL (DATA)	70,	80,	210*	270,	310,	400	
TT			REAL*4	LOCAL	150*	160,	170,	180,	190,	330*	340
TTT			REAL*4	LOCAL	180*	190,	230,	250,	270,	310	
T1	(100)	100	REAL*4	LOCAL	80,	220*	400				
T2	(100)	100	REAL*4	LOCAL	80,	230*	400				

* = VARIABLES USED ON LEFT HAND SIDE OF EQUAL SIGN

INPUT / OUTPUT TABLE

DEFINING SEQ. NO.	I/O OPERATION	LOGICAL UNIT	I/O TYPE	FORMAT USED	I/O LIST
120	PRINT	51	BCD	1	AS,BS
270	PRINT	51	BCD	2	T(1,I),TTT,Q,TOTAL(J),ORTLS
310	PRINT	51	BCD	3	T(1,I),TTT,Q,TOTAL(J)
370	PRINT	51	BCD	4	
400	PRINT	51	BCD	5	T1(I),T2(I),TOTAL(I)
430	PRINT	51	BCD	6	

```

SUBROUTINE HPMINV(A,N,B,M,ELEAST,ITER,EMAX)
C
C
C THIS IS ORNL F04022 OF 2-68
C F1 UCSD HPMINV
C HIGH PRECISION MATRIX INVERSION
C
C DIMENSION A(15,15),B(15,15),E(15,15),IPIVOT(15),JPIVOT(15),PROW(15),C(15)
C EQUIVALENCE (C,PROW)
C
C INITIALIZATION
C
C 100 L=N-1
J----- 105 DO 125 J=0,L
J 110 I=15+J
J K----- 115 DO 125 K=1,N
J K 120 I=I+1
J--K----- 125 B(I)=A(I)

J----- 130 DO 140 J=1,N
J 135 IPIVOT(J)=0
J----- 140 JPIVOT(J)=0

I----- 145 DO 320 I=1,N
I C
I C SEARCH FOR PIVOT ELEMENT
I C
I 150 BMAX=0.0
I 155 I=N-1
I J----- 160 DO 220 J=0,L
I J 165 IF(JPIVOT(J+1)-1)170,220,220
I J K----- 170 I=15+J
I J K 175 DO 215 K=1,N
I J K 180 I=I+1
I J K 185 IF(IPIVOT(K)-1)190,215,215
I J K 190 X=ABS(B(I))
I J K 195 IF (BMAX-X)200,215,215
I J K 200 BMAX=X
I J K 205 IROW=I-J+15
I J K 210 JCOL=J+1
I J K----- 215 CONTINUE
I J----- 220 CONTINUE
I 225 IPIVOT(IROW)=JCOL
I 230 JPIVOT(JCOL)=IROW
I 235 PIVOT=B(IROW,JCOL)
I C
I C REPLACE PIVOT COLUMN WITH ROW MULTIPLIERS
I C
I K----- 240 DO 265 K=1,N
I K 245 IF(IROW-K)250,260,250
I K 250 B(K,JCOL)=-B(K,JCOL)/PIVOT
I K 255 GO TO 265
I K 260 B(K,JCOL)=1.0/PIVOT
I K----- 265 CONTINUE
I C
I C REDUCE NON PIVOT COLUMNS
I C
I 270 DO 275 I=1,N
I I----- 275 PROW(I)=B(IROW,I)

I J----- 280 DO 320 J=1,N
I J 285 IF(JCOL-J)290,320,290
I J K----- 290 DO 315 K=1,N
I J K 295 IF(IROW-K)300,310,300
I J K 300 B(K,J)=B(K,J)+B(K,JCOL)*PROW(J)
I J K 305 GO TO 315
I J K 310 B(K,J)=B(K,J)/PIVOT
I J K----- 315 CONTINUE
I--J----- 320 CONTINUE
I C
I C INTERCHANGE ROWS AND COLUMNS
I C
I----- 325 DO 340 I=1,N
I 330 J=JPIVOT(I)
I K----- 335 DO 340 K=1,N
I--K----- 340 C(I,K)=B(J,K)
I 345 LL=N-1
J----- 350 DO 390 J=0,LL
J 355 I=15+J
J 360 K=IPIVOT(J+1)
J 365 L=15*(K-1)
J J----- 370 DO 390 JJ=1,N
J J 375 I=I+1
J J 380 L=L+1
J J 385 B(I)=E(L)
J--J----- 390 CONTINUE
J 395 IF(M)570,570,400

```

```

HPMIN 1C
HPMIN 20
HPMIN 30
HPMIN 40
HPMIN 50
HPMIN 60
HPMIN 70
HPMIN 80
HPMIN 81
HPMIN 90
HPMI 100
HPMI 110
HPMI 120
HPMI 130
HPMI 140 -----DO
HPMI 150
HPMI 160 -----DO
HPMI 170
HPMI 180

HPMI 190 -----DO
HPMI 200
HPMI 210

HPMI 220 -----DO
HPMI 230
HPMI 240
HPMI 250
HPMI 260
HPMI 270
HPMI 280 -----DO
HPMI 290 IF
HPMI 300
HPMI 310 -----DO
HPMI 320
HPMI 330 IF
HPMI 340
HPMI 350 IF
HPMI 360
HPMI 370
HPMI 380
HPMI 390
HPMI 400
HPMI 410
HPMI 420
HPMI 430
HPMI 440
HPMI 450
HPMI 460
HPMI 470 -----DO
HPMI 480 IF
HPMI 490
HPMI 500 -----GOTO
HPMI 510
HPMI 520
HPMI 530
HPMI 540
HPMI 550
HPMI 560 -----DO
HPMI 570

HPMI 580 -----DO
HPMI 590 IF
HPMI 600 -----DO
HPMI 610 IF
HPMI 620
HPMI 630 -----GOTO
HPMI 640
HPMI 650
HPMI 660
HPMI 670
HPMI 680
HPMI 690
HPMI 700 -----DO
HPMI 710
HPMI 720 -----DO
HPMI 730
HPMI 740
HPMI 750 -----DO
HPMI 760
HPMI 770
HPMI 780
HPMI 790 -----DO
HPMI 800
HPMI 810
HPMI 820
HPMI 830
HPMI 840 IF

```

```

C
C      COMPUTE E=I-(A*B) AND FIND LARGEST ABSOLUTE VALUE
C
      400 ITER=0
      405 KK=0
      410 EMAX=0.0
J----- 415 DO 475 J=1,N
J
J I----- 420 DO 475 I=1,N
J I----- 425 E(I,J)=0.0
J I K----- 430 DO 435 K=1,N
J I K----- 435 E(I,J)=E(I,J)+A(I,K)*B(K,J)
J I----- 440 IF(I-J)455,445,455
J I----- 445 E(I,J)=1.0-E(I,J)
J I----- 450 GO TO 460
J I----- 455 E(I,J)=-E(I,J)
J I----- 460 Y=ABS(E(I,J))
J I----- 465 IF(EMAX-Y)470,475,475
J I----- 470 EMAX=Y
J----- 475 CONTINUE
      480 IF(KK-1)485,570,570
      485 IF(EMAX-ELEAST)570,570,490
      490 ITER=ITER+1
C
C      COMPUTE I+E
C
I----- 495 DO 505 I=1,N
I----- 500 J=I
I----- 505 E(I,J)=E(I,J)+1.0
C
C      COMPUTE ENRICHED INVERSE, B=B(I+E)
C
I----- 510 DO 550 I=1,N
I
I J----- 515 DO 525 J=1,N
I J----- 520 C(J)=0.0
I J K----- 525 DO 530 K=1,N
I J K----- 530 C(J)=C(J)+B(I,K)*E(K,J)
I J----- 535 CONTINUE
I
I L----- 540 DO 545 L=1,N
I L----- 545 B(I,L)=C(L)
I----- 550 CONTINUE
      555 IF(ITER-M)410,560,560
      560 KK=KK+1
      565 GO TO 410
      570 RETURN
      END

```

```

HPMI 850
HPMI 860
HPMI 870
HPMI 880
HPMI 890
HPMI 900
HPMI 910 -----DO
HPMI 920 -----DO
HPMI 930
HPMI 940 -----DO
HPMI 950
HPMI 960 IF
HPMI 970
HPMI 980 -----GOTO
HPMI 990
HPM 1000
HPM 1010 IF
HPM 1020
HPM 1030
HPM 1040 IF
HPM 1050 IF
HPM 1060
HPM 1070
HPM 1080
HPM 1090
HPM 1100 -----DO
HPM 1110
HPM 1120
HPM 1130
HPM 1140
HPM 1150
HPM 1160 -----DO
HPM 1170 -----DO
HPM 1180
HPM 1190 -----DO
HPM 1200
HPM 1210
HPM 1220 -----DO
HPM 1230
HPM 1240
HPM 1250 IF
HPM 1260
HPM 1270 -----GOTO
HPM 1280
HPM 1290

```

TABLE OF VARIABLE NAMES

VARIABLE NAME	ARRAY DIMENSIONS	TOTAL NO ELEMENTS	ELEMENT TYPE	DECLARATION	CROSS REFERENCE TABLE (BY SEQUENCE NUMBERS)							
A	(15,15)	225	REAL*4	PARAMETER	10,	80,	180,	950				
ABSF			REAL*4	FUNCTION	340,	1000						
B	(15,15)	225	REAL*4	PARAMETER	10,	80,	180*	340,	430,	490*	510*	
					570,	620*	640*	730,	820*	950,	1200,	
					1230*							
BMAX			REAL*4	LOCAL	260*	350,	360*					
C	(15)	15	REAL*4	LOCAL (EQUIVALENCE)	80,	90,	1180*	1200*	1230			
E	(15,15)	225	REAL*4	LOCAL	80,	730*	820,	930*	950*	970*	990*	
					1000,	1120*	1200					
ELEAST			REAL*4	PARAMETER	10,	1050						
EMAX			REAL*4	PARAMETER	10,	900*	1010,	1020*	1050			
HPMINV			REAL*4	ENTRY POINT	10							
I			INTEGER*4	LOCAL	150*	170*	180,	300*	320*	340,	370,	
					560*	570,	700*	710,	730,	760*	800*	
					820,	920*	930,	950,	960,	970,	990,	
					1000,	1160*	1170,	1180,	1160*	1200,	1230	
II			INTEGER*4	LOCAL	220*							
IPIVOT	(15)	15	INTEGER*4	LOCAL	80,	200*	230,	410*	770			
IRON			INTEGER*4	LOCAL	370*	410,	470,	430,	480,	570,	610	
ITER			INTEGER*4	PARAMETER	10,	880*	1060*	1250				
J			INTEGER*4	LOCAL	140*	150,	190*	200,	210,	280*	290,	
					300,	370,	380,	580*	590,	620,	640,	
					710*	730,	750*	760,	770,	910*	920,	
					950,	960,	970,	990,	1000,	1110*	1120,	
					1170*	1180,	1200					
JCOL			INTEGER*4	LOCAL	280*	410,	420,	430,	490,	510,	590,	
					620*							
JJ			INTEGER*4	LOCAL	790*							
JPIVOT	(15)	15	INTEGER*4	LOCAL	80,	210*	250,	420*	710			
K			INTEGER*4	LOCAL	160*	210*	330,	470*	480,	490,	510,	
					600*	610,	620,	640,	720*	730,	770*	
					780,	940*	950,	1150*	1200			
KK			INTEGER*4	LOCAL	890*	1040,	1260*					
L			INTEGER*4	LOCAL	130*	140,	270*	280,	780*	810*	820,	
					1220*	1230						
LL			INTEGER*4	LOCAL	740*	750						
M			INTEGER*4	PARAMETER	10,	840,	1250					
N			INTEGER*4	PARAMETER	10,	130,	160,	190,	220,	270,	310,	
					470,	560,	580,	600,	700,	720,	740,	
					790,	910,	920,	940,	1100,	1160,	1170,	
					1190,	1220						
PIVOT			REAL*4	LOCAL	430*	490,	510,	640				
PPCW	(15)	15	REAL*4	LOCAL (EQUIVALENCE)	80,	90,	570*	620				
X			REAL*4	LOCAL	340*	350,	360					
Y			REAL*4	LOCAL	1000*	1010,	1020					

* * VARIABLES USED ON LEFT HAND SIDE OF EQUAL SIGN

INPUT / OUTPUT TABLE					
DEFINING SEQ. NO.	I/O OPERATION	LOGICAL UNIT	I/O TYPE	FORMAT USED	I/O LIST

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SUBROUTINE GRAPHS(OUTGAS,HOURS,XTIT,PL,TITLL,NC,BS)
C
C
C *** PLOTTING OPTIONS ***
C IF PLOTS ARE DESIRED, THEY ARE REQUESTED BY THE FOLLOWING DATA CARDS
C (PLACE AFTER THE BLANK CARD IN THE MAIN PROGRAM). COLUMNS 1-5,
C RIGHT ADJUSTED.
C 1. 1 CARD. FOR POINTS ONLY SET=-1
C   FOR POINTS CONNECTED BY A LINE, SET=1
C THE NEXT 6 CARDS REPRESENT 6 PLOTTING OPTIONS OF OUTGASSING RATE VS.
C TIME AND ARE REPRESENTED BY THE INTEGERS P(1)-P(6) WHICH ARE
C DESCRIBED BELOW. IF ANY OPTION IS OMITTED, PLACE A 0 IN COLUMN 5 OR
C INCLUDE A BLANK CARD. IF THE SIGN OF P(1)-P(6) IS NEGATIVE, A FITTED
C LINE TO THE EXPRESSION  $Y=A \cdot X^B$  WILL BE DRAWN.
C CARD 1. P(1), LOG OUTGASSING RATE VS. LOG TIME
C   FOR PLOTS, SET=1 OR -1 (FITTED)
C   FOR NO PLOTS, SET=0
C CARD 2. P(2), LOG OUTGASSING VS. LINEAR TIME
C   FOR PLOTS, SET=1 OR -1
C   FOR NO PLOTS, SET=0
C CARD 3. P(3), LOG OUTGASSING RATE VS. LOG TIME OF SELECTED GASES.
C   SET VALUE EQUAL TO THE NUMBER OF GASES TO BE PLOTTED.
C   FOLLOW THIS NUMBER BY THE FIRST 4 LETTERS OF EACH GAS AND
C   PRECEDE EACH BY A SPACE. EXAMPLE 2 C3H8 HYDR TOTA
C   ***EXCEPTION*** USE WATR TO REPRESENT WATER VAPOR.
C CARD 4. P(4), SAME AS P(3) EXCEPT LOG-LINEAR.
C CARD 5. P(5), LOG OUTGASSING RATE VS. LOG TIME. COMPOSITE GRAPH
C   WHICH INCLUDES ALL GASES.
C   FOR PLOT, SET=15 OR -15
C   FOR NO PLOT, SET=0
C CARD 6. P(6), SAME AS P(5) EXCEPT LOG-LINEAR.
C THE NEXT 6 CARDS REPRESENT 6 PLOTTING OPTIONS OF OUTGASSING RATE VS.
C TEMPERATURE AND VALUES ARE SET THE SAME AS P(1)-P(6). THERE IS NO
C OPTION FOR ADDING FITTED LINES, THEREFORE ALL VALUES ARE POSITIVE.
C
C ****NOTE****THERE MUST BE 13 DATA CARDS IN ALL FOR PLOTTING.
C
C THE LAST 2 CARDS IN THE DECK ARE THE FOLLOWING CONTROL CARDS
C /*
C //
C
C   REAL *P TTL,TITLL,XTIT,TTT,GASLEG
C   INTEGER P(6)
C   COMMON /FITTCGR/ OUTGSP( 50,20),NS( 50),HOURP( 50,20),CALOG
C 1   ( 50,20),T1,TEMPP( 50,20)
C   COMMON /FILO/ XAL,YL,TETLE,GASLEG
C   COMMON /EATGCO/ LINE
C   DIMENSION XA(2),YA(2),XAL(2),TTL(6,20),ICPA(25),BUF(3000),YL(2),
C 1   HOURS( 50),OUTGAS( 50,20),TITLL( 50),XTIT(4),TTT(20),TETLE(40),
C 2   GASLEG(50),BS(20)
C   DATA (ITIME=1)
C   DATA (TTL=20(9H 1)
C   DATA (XA=1.0E-02,1.0E+03),(YA=1.0E-10,1.0E+01)
C
C   XA=LOG SCALE X, YA=LOG SCALE Y
C   XAL=LINEAR SCALE X, YL=LINEAR SCALE Y
C IF PLOTTING OUTGASSING VS. TEMPERATURE, CHANGE LIMITS ON X AXIS TO
C CORRESPOND TO TEMPERATURE, INSTEAD OF TIME.
C
C   IF (ITIME.EQ.1) GO TO 110
C   XAL(1)=1000.
C   XAL(2)=0.
C J----- DO 100 J=1,NC
C J         IF (HOURS(J).LT.XAL(1)) XAL(1)=HOURS(J)
C J----- 100 IF (HOURS(J).GT.XAL(2)) XAL(2)=HOURS(J)
C
C J----- DO 105 J=1,PL
C J
C J 1----- DO 105 I=1,50
C J--1----- HOURP(I,J)=TEMPP(I,J)
C 110 CONTINUE
C   NOUTH=0
C   CALL QQQCPA(9,.08)
C   CALL QQQCPA(10,LINE)
C
C READ PLOTTING OPTIONS
C

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```

GRAPH 10
GRAPH 20
GRAPH 30
GRAPH 40
GRAPH 50
GRAPH 60
GRAPH 70
GRAPH 80
GRAPH 90
GRAPH 100
GRAPH 110
GRAPH 120
GRAPH 130
GRAPH 140
GRAPH 150
GRAPH 160
GRAPH 170
GRAPH 180
GRAPH 190
GRAPH 200
GRAPH 210
GRAPH 220
GRAPH 230
GRAPH 240
GRAPH 250
GRAPH 260
GRAPH 270
GRAPH 280
GRAPH 290
GRAPH 300
GRAPH 310
GRAPH 320
GRAPH 330
GRAPH 340
GRAPH 350
GRAPH 360
GRAPH 370
GRAPH 380
GRAPH 390
GRAPH 400
GRAPH 410
GRAPH 420
GRAPH 430
GRAPH 440
GRAPH 450
GRAPH 460
GRAPH 470
GRAPH 480
GRAPH 481
GRAPH 482
GRAPH 490
GRAPH 500
GRAPH 510
GRAPH 520
GRAPH 530
GRAPH 540
GRAPH 550
GRAPH 560
GRAPH 570
GRAPH 580 IF
GRAPH 590
GRAPH 600
GRAPH 610 -----DO
GRAPH 620 IF
GRAPH 630 IF
GRAPH 640 -----DO
GRAPH 650 -----DO
GRAPH 660
GRAPH 670
GRAPH 680
GRAPH 690
GRAPH 700
GRAPH 710
GRAPH 720
GRAPH 730

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I----- DO 115 I=1,6
I          READ 1,P(I),(TTL(I,J),J=1,15)
I          1  FORMAT(15,15A5)
I----- 115  CONTINUE

I----- DO 180 I=1,6
I          IF(P(I).EQ.0) GO TO 180
I          NP=ABS(P(I))
I          GO TO (165,165,135,130,120,120) I
I
I          C
I          C THIS SECTION PLOTS OPTIONS 3,4,5,6. EACH OF THESE OPTIONS PRODUCES
I          C ONLY 1 GRAPH.
I          C SET UP LEGEND FOR PLOTTING ALL GASES ON 1 PLOT.
I          C
I          J----- 120  DO 125 J=1,ML
I          J          CECODE(5,2,GASLEG(J))  TTL(I,J)
I          J          FORMAT(A5)
I          J----- 125  CONTINUE
I          IF(I.EQ.5) GO TO 135
I          130  CALL QQQCPA(5,5)
I          CALL SETPLT(XAL,YA,2,'YLOG','MECH',0.,0.,BUF,3000)
I          GO TO 140
I          135  CALL QQQCPA(5,6,25)
I          CALL SETPLT(XA,YA,2,'LOG','MECH',0.,0.,BUF,3000)
I          140  NSYM=0
I          CALL TITLE(.2,'SELECTED GASES',XTIT ,*OUTGASSING RATE (TORP-LITERS/SEC)%)
I          CALL SYMBOL(.1,10.25,.1 ,TETLE(1),0.,80)
I          C
I          C TEST TO SEE IF NAMES OF GASES ON DATA CARDS ARE CORRECT. IF NOT, THAT
I          C GAS IS NOT PLOTTED.
I          C
I          K----- DO 160 K=1,NP
I          K
I          K J----- DO 145 J=1,ML
I          K J          IF(1COMPARE(TTL(I,K),GASLEG(J),5 1.EQ.0) 150,145
I          K J----- 145  CONTINUE
I          K          PRINT 3,I
I          K          FORMAT('1 THE INPUT CARD WITH P',I1,',ETC. IS WRONG. CHECK THE NAME',
I          K          'ES. LINES WITH UNRECOGNIZED NAMES WILL BE OMITTED FROM THE PLOT.')
I          K          GO TO 160
I          K          150  IF (NS(J).LT.2) GO TO 160
I          K          CALL PAYPLT(HOURP(1,J),OUTGSP(1,J),NS(J))
I          K
I          K          C
I          K          C TEST TO SEE IF A FITTED LINE IS DESIRED.
I          K          C
I          K          IF(P(I).GT.0) GO TO 155
I          K          CALL QQQCPA(10,0)
I          K          CALL LINPLT(HOURP(1,J),CALOG(1,J),NS(J),0,0)
I          K          CALL QQQCPA(10,LINE)
I          K          155  NSYM=NSYM+1
I          K          TTT(NSYM)=TTL(I,K)
I          K----- 160  CONTINUE
I          YBOX=.2+.2*NSYM
I          CALL LEGEND('LEGEND',C ,--NSYM,TTT(1),-2,1.,YBOX ,6.75,10.)
I          GO TO 160
I          C
I          C THIS SECTION PLOTS OPTIONS 1 AND 2, 1 PLOT PER GAS.
I          C
I          165  IF(NBOTH.EQ.1) GO TO 1PC
I          J----- DO 175 J=1,ML
I          J          IF(P(I).EQ.0) GO TO 170
I          J          IF(NS(J).LT.2) GO TO 170
I          J          CALL QQQCPA(5,6,25)
I          J          CALL SETPLT(XA,YA,2,'LOG','MECH',0.,0.,BUF,3000)
I          J          CALL TITLE(.2,'',XTIT ,*OUTGASSING RATE (TORP-LITERS/SEC)%)
I          J          1C1%)
I          J          CALL SYMBOL(.5,10.25,.21,TITLL(2*J-1),0.,16)
I          J          CALL SYMBOL(.1,10.25,.1 ,TETLE(1),0.,80)
I          J          CALL PAYPLT(HOURP(1,J),OUTGSP(1,J),NS(J))
I          J          IF(P(I).GT.0) GO TO 170
I          J          CALL SYMBOL(4.,10.25,.14,'SLOPE = ',C.,A)
I          J          CALL NUMBER(5.,10.25,.14,BS(J),0.,7H(EIC.3))
I          J          CALL QQQCPA(10,C)
I          J          CALL LINPLT(HOURP(1,J),CALOG(1,J),NS(J),0,C)
I          J          CALL QQQCPA(10,LINE)
I          J          170  IF(P(2).EQ.0) GO TO 175
I          J          IF(NS(J).LT.2) GO TO 175
I          J          CALL QQQCPA(5,5)
I          J          CALL SETPLT(XAL,YA,2,'YLOG','MECH',0.,0.,BUF,3000)
I          J          CALL TITLE(.2,'',XTIT ,*OUTGASSING RATE (TORP-LITERS/SEC)%)
I          J          1C1%)
I          J          CALL SYMBOL(.5,10.25,.21,TITLL(2*J-1),0.,16)
I          J          CALL SYMBOL(.1,10.25,.1 ,TETLE(1),0.,80)
I          J          CALL PAYPLT(HOURP(1,J),OUTGSP(1,J),NS(J))
I          J          NBOTH=1
I          J          IF(P(2).GT.0) GO TO 175
I          J          CALL QQQCPA(10,0)
I          J          CALL LINPLT(HOURP(1,J),CALOG(1,J),NS(J),0,0)
I          J          CALL QQQCPA(10,LINE)
I          J----- 175  CONTINUE
I          180  CONTINUE
I          185  ITIME=2
I          RETURN
I          END

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TABLE OF VARIABLE NAMES

VARIABLE NAME	ARRAY DIMENSIONS	TOTAL NO ELEMENTS	ELEMENT TYPE	DECLARATION	GPSS REFERENCE TABLE (BY SEQUENCE NUMBER)
BS	(20)	20	REAL*4	PARAMETER	10, 400, 1410
BUF	(3000)	3000	REAL*4	LOCAL	400, 930, 940, 1340, 1400
CALOG	(50,20)	1000	REAL*4	COMMON/FITTCO /	450, 1180, 1410, 1460
EATOGF		4	BYTES	COMMON LABEL	470
FITTCO		16204	BYTES	COMMON LABEL	450
GASLEG	(50)	50	REAL*8	COMMON/HILO /	430, 460, 480, 880, 1080
GRAPHS			REAL*4	EMPTY POINT	10
HILO		576	BYTES	COMMON LABEL	460
HOURP	(50,20)	1000	REAL*4	COMMON/FITTCO /	450, 460, 1120, 1140, 1180, 1430, 1410, 1460
HOURS	(50)	50	REAL*4	PARAMETER	10, 400, 620, 670
I			INTEGER*4	LOCAL	450, 460, 480, 910, 1060, 1080, 1140, 1110
IABS			INTEGER*4	FUNCTION	800
ICOMPARE			INTEGER*4	FUNCTION	1040
ICPA	(20)	20	INTEGER*4	LOCAL	600
ITIME			INTEGER*4	LOCAL (DATA)	490, 500, 1400*
II			INTEGER*4	COMMON/FITTCO /	450
J			INTEGER*4	LOCAL	430, 440, 450, 460, 480, 490, 500, 510, 520, 530, 540, 550, 560, 570, 580, 590, 600, 610, 620, 630, 640, 650, 660, 670, 680, 690, 700, 710, 720, 730, 740, 750, 760, 770, 780, 790, 800, 810, 820, 830, 840, 850, 860, 870, 880, 890, 900, 910, 920, 930, 940, 950, 960, 970, 980, 990, 1000, 1010, 1020, 1030, 1040, 1050, 1060, 1070, 1080, 1090, 1100, 1110, 1120, 1130, 1140, 1150, 1160, 1170, 1180, 1190, 1200, 1210, 1220, 1230, 1240, 1250, 1260, 1270, 1280, 1290, 1300, 1310, 1320, 1330, 1340, 1350, 1360, 1370, 1380, 1390, 1400, 1410, 1420, 1430, 1440, 1450, 1460, 1470, 1480, 1490, 1500, 1510, 1520, 1530, 1540, 1550, 1560, 1570, 1580, 1590, 1600, 1610, 1620, 1630, 1640, 1650, 1660, 1670, 1680, 1690, 1700, 1710, 1720, 1730, 1740, 1750, 1760, 1770, 1780, 1790, 1800, 1810, 1820, 1830, 1840, 1850, 1860, 1870, 1880, 1890, 1900, 1910, 1920, 1930, 1940, 1950, 1960, 1970, 1980, 1990, 2000, 2010, 2020, 2030, 2040, 2050, 2060, 2070, 2080, 2090, 2100, 2110, 2120, 2130, 2140, 2150, 2160, 2170, 2180, 2190, 2200, 2210, 2220, 2230, 2240, 2250, 2260, 2270, 2280, 2290, 2300, 2310, 2320, 2330, 2340, 2350, 2360, 2370, 2380, 2390, 2400, 2410, 2420, 2430, 2440, 2450, 2460, 2470, 2480, 2490, 2500, 2510, 2520, 2530, 2540, 2550, 2560, 2570, 2580, 2590, 2600, 2610, 2620, 2630, 2640, 2650, 2660, 2670, 2680, 2690, 2700, 2710, 2720, 2730, 2740, 2750, 2760, 2770, 2780, 2790, 2800, 2810, 2820, 2830, 2840, 2850, 2860, 2870, 2880, 2890, 2900, 2910, 2920, 2930, 2940, 2950, 2960, 2970, 2980, 2990, 3000, 3010, 3020, 3030, 3040, 3050, 3060, 3070, 3080, 3090, 3100, 3110, 3120, 3130, 3140, 3150, 3160, 3170, 3180, 3190, 3200, 3210, 3220, 3230, 3240, 3250, 3260, 3270, 3280, 3290, 3300, 3310, 3320, 3330, 3340, 3350, 3360, 3370, 3380, 3390, 3400, 3410, 3420, 3430, 3440, 3450, 3460, 3470, 3480, 3490, 3500, 3510, 3520, 3530, 3540, 3550, 3560, 3570, 3580, 3590, 3600, 3610, 3620, 3630, 3640, 3650, 3660, 3670, 3680, 3690, 3700, 3710, 3720, 3730, 3740, 3750, 3760, 3770, 3780, 3790, 3800, 3810, 3820, 3830, 3840, 3850, 3860, 3870, 3880, 3890, 3900, 3910, 3920, 3930, 3940, 3950, 3960, 3970, 3980, 3990, 4000, 4010, 4020, 4030, 4040, 4050, 4060, 4070, 4080, 4090, 4100, 4110, 4120, 4130, 4140, 4150, 4160, 4170, 4180, 4190, 4200, 4210, 4220, 4230, 4240, 4250, 4260, 4270, 4280, 4290, 4300, 4310, 4320, 4330, 4340, 4350, 4360, 4370, 4380, 4390, 4400, 4410, 4420, 4430, 4440, 4450, 4460, 4470, 4480, 4490, 4500, 4510, 4520, 4530, 4540, 4550, 4560, 4570, 4580, 4590, 4600, 4610, 4620, 4630, 4640, 4650, 4660, 4670, 4680, 4690, 4700, 4710, 4720, 4730, 4740, 4750, 4760, 4770, 4780, 4790, 4800, 4810, 4820, 4830, 4840, 4850, 4860, 4870, 4880, 4890, 4900, 4910, 4920, 4930, 4940, 4950, 4960, 4970, 4980, 4990, 5000, 5010, 5020, 5030, 5040, 5050, 5060, 5070, 5080, 5090, 5100, 5110, 5120, 5130, 5140, 5150, 5160, 5170, 5180, 5190, 5200, 5210, 5220, 5230, 5240, 5250, 5260, 5270, 5280, 5290, 5300, 5310, 5320, 5330, 5340, 5350, 5360, 5370, 5380, 5390, 5400, 5410, 5420, 5430, 5440, 5450, 5460, 5470, 5480, 5490, 5500, 5510, 5520, 5530, 5540, 5550, 5560, 5570, 5580, 5590, 5

TITLE	(14)	40	REAL*4	COMMON/FILE	/	44C.	480.	990.	1170.	1110		
TITLE				SUBROUTINE		920.	1150.	1490				
TITLE	(150)	90	REAL*8	PARAMETER		10.	470.	480.	1140.	1160		
TITLE	(14,20)	120	REAL*8	LOCAL (DATA)		430.	480.	500.	750.	980.	1060.	1210
TITLE	(120)	20	REAL*4	LOCAL		430.	480.	1210*	1240			
TA	(12)	2	REAL*4	LOCAL (DATA)		480.	510.	980.	1140			
BA	(12)	2	REAL*4	COMMON/FILE	/	440.	480.	190*	1270*	120*	130*	130.
BT	(14)	4	REAL*8	PARAMETER		10.	470.	480.	1140.	1150.	1490	
TA	(12)	2	REAL*4	LOCAL (DATA)		480.	510.	970.	1140.	1160.	1480	
TR			REAL*4	LOCAL		1270*	1240					
VL	(12)	2	REAL*4	COMMON/FILE	/	440.	480.					

* = VARIABLES USED ON LEFT HAND SIDE OF EQUAL SIGN

INPUT / OUTPUT TABLE

DEFINING SEQ. NO.	I/O OPERATION	LOGICAL UNIT	I/O TYPE	FORMAT USED	I/O LIST
220	CE200E	4		2	17611.J1
740	#E20	40	BCD	1	*111,177(11.J1),J=1,151
1040	#PRINT	11	BCD	7	1

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IEF2851 AS.G3.P31177.C10155.DURFEE.PLI PASSED
IEF2851 VOL SER NOS= ZZZZZZ.
IEF2851 SYS1.LINKLIB PASSED
IEF2851 VOL SER NOS= MVT17P.
IEF2851 SYS70287.T181233.PV000.CLAD.FJNBLIB PASSED
IEF2851 VOL SER NOS= YYYYYY.
IEF2851 SYS70287.T181233.SV000.CLAD.PCPO0045 SYSOUT
IEF2851 VOL SER NOS= XXXXXX.
IEF2851 SYS70287.T181233.PV000.CLAD.FJCBLIB DELETED
IEF2851 VOL SER NOS= YYYYYY.
IEF2851 SYS70287.T181233.PV000.CLAD.FTSYSIN PASSED
IEF2851 VOL SER NOS= 222222.

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CLAD GC 22.07.24 10-14-70
CPU SEC.= 149.18// I/O REQUESTS= 185// REGION ALLOC.=1536K// MACH. USE SEC.= 156.58// REGION USED=1526K

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IEF2851 AS.G3.P31177.C10155.DURFEE.PLI KEPT
IEF2851 VOL SER NOS= ZZZZZZ.
IEF2851 SYS1.LINKLIB KEPT
IEF2851 VOL SER NOS= MVT17P.
IEF2851 SYS70287.T181233.PV000.CLAD.FTSYSIN DELETED
IEF2851 VOL SER NOS= 222222.

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CLAD MODEL=75 12723 22.07.25 10-14-70
TOTAL CPU SEC.= 314.71//TOTAL I/O REQUESTS= 2403//MAX. REGION ALLOC.=1536K//TOTAL MACH. USE SEC.= 418.03//MAX. REGION USED=1526K

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* * NOTICE * * THE MAXIMUM REGION YOU REQUESTED DURING THIS JOB WAS 1536K, BUT YOU COULD RUN IN LESS SINCE MAX. REGION USED=1526K
*****

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*** CURRENT DATE IS 10-22-70 ***

NERVA XE-II FUEL ELEMENT OUTGASSING PROGRAM

DEWEY EASTON

RUN NO. 101, 600-C, 350 HR AT 50 DEG

APPARATUS TEMPERATURE (D) = 60.

*** CRACKING PATTERN ***

M/E	H	HELIUM	METHANE	WATER VAPOR	NITROGEN	CO	OXYGEN	ARGON	CO2	C2H4	C2H6	C2H8
2	1.0000	0.0	0.0070	0.0	0.0	0.0	0.0	0.0	0.0	0.0250	0.0040	0.0040
4	0.0	1.0000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0010	0.0	0.0	0.0200	0.0	0.0	0.0250	0.0120	0.0030	0.0050
13	0.0	0.0	0.0090	0.0	0.0	0.0	0.0	0.0	0.0	0.0160	0.0060	0.0050
14	0.0	0.0	0.0450	0.0	0.0000	0.0060	0.0	0.0	0.0	0.0400	0.0200	0.0250
15	0.0	0.0	0.0000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0270	0.0200
16	0.0	0.0	1.0000	0.0280	0.0	0.0080	0.0700	0.0	0.0544	0.0	0.0030	0.0130
17	0.0	0.0	0.0120	0.0660	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	1.0000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0100	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.5060	0.1930	0.0850
27	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.5440	0.2840	0.0000
28	0.0	0.0	0.0	0.0	1.0000	1.0000	0.0	0.0	0.1640	1.0000	1.0000	0.7180
29	0.0	0.0	0.0	0.0	0.0100	0.0100	0.0	0.0	0.0	0.0280	0.2000	1.0000
30	0.0	0.0	0.0	0.0	0.0	0.0020	0.0	0.0	0.0	0.0	0.2440	0.0220
32	0.0	0.0	0.0	0.0	0.0	0.0	1.0000	0.0	0.0	0.0	0.0	0.0
40	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0000	0.0	0.0	0.0	0.0
44	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0000	0.0	0.0	0.4400

*** CORRECTION CONSTANTS ***

IONIZATION * RGA SENSITIVITY = MASTER
CONSTANT AMPS/TORR

H	0.4600	0.4848	0.2230
HELIUM	0.1630	0.2577	0.0420
METHANE	1.4000	0.4400	0.6160
WATER VAPOR	1.0000	0.7000	0.7000
NITROGEN	1.0000	1.1000	1.1000
CO	1.0100	1.1980	1.2100
OXYGEN	1.0700	0.8252	0.8830
ARGON	1.1400	0.8333	0.5500
CO2	1.4000	1.0000	1.4000
C2H4	1.0000	0.4900	0.8820
C2H6	2.6500	0.5613	1.5099
C2H8	3.5600	0.3052	1.2000

*** CURRENT DATE IS 10-22-70 ***

RUN NO. 101, 600-C, 350 HR AT 50 DEG

GUN NO. 101, 600-C, 350 HP AT 50 DEG

DATE = 2-12

HOURS = 2.00

TEMPERATURE (DEGREE C.) = 40.25

MILLIVOLTS (CR/AL) = 2.00

CHAMBER PRESSURE = 1.69000E-05

THERMAL CORRECTION = 1.78052E-05

MANIFOLD PRESSURE = 2.59000E-06

THERMAL CORRECTION = 2.72872E-06

RGA PRESSURE = 3.35000E-06

THERMAL CORRECTION = 3.52044E-06

M/E	MEASURED PPM HEIGHT (INPS)	CALCULATED M/E	DIFFERENCE	PERCENT DIFF
2	5.90000E-08	5.85008E-08	-2.34475E-13	-39.74221E-05
4	1.00000E-12	1.00000E-12	0.0	0.0
12	1.25000E-08	6.10352E-09	-6.39648E-09	-51.17183E 00
13	8.00000E-10	-7.68606E-10	-1.58606E-09	-19.85797E 01
14	4.70000E-09	2.56036E-09	-2.13964E-09	-45.52614E 00
15	7.50000E-09	1.58629E-09	-5.91371E-09	-78.84745E 01
16	6.90000E-08	6.36319E-08	-6.26007E-09	-90.67196E-01
17	4.95000E-07	5.04640E-07	9.6407E-09	19.47970E-01
18	1.90000E-06	1.85767E-06	-2.2223E-09	-12.25424E-02
22	3.50000E-09	-3.91450E-10	-3.89145E-09	-11.11841E 01
24	3.40000E-09	-1.05078E-08	-1.41027E-08	-41.17429E 01
27	5.60000E-09	1.85157E-09	1.22157E-09	21.77671E 01
28	4.05000E-07	4.05252E-07	2.5252E-10	62.31721E-01
29	1.10000E-07	1.03702E-07	-6.29768E-09	-57.25166E-01
30	4.30000E-09	3.51787E-09	-7.88125E-10	-18.29207E 00
32	1.75000E-09	1.75551E-09	4.55145E-10	25.67743E-01
40	2.00000E-09	2.00000E-09	0.0	0.0
44	4.60000E-09	5.05009E-09	4.50009E-10	10.84692E 00

RATIO OF GAGE P1 TO GAGE P2 = 4.52500E 00

GAS	PRESSURE Torr	PERCENT OF TOTAL PRESSURE	OUTGASING RATE Torr LITERS/SEC	PERCENT OF TOTAL OUTGASING RATE
GAGE P1	1.78052E-05		1.43178E-04	
TOTAL	3.49012E-06	50.99000E 00	2.79629E-04	50.99000E 00
H	2.82457E-07	81.14300E-01	4.82637E-05	17.35000E 00
HELIUM	7.50000E-12	72.07180E-01	3.02045E-10	17.43111E-01
NEUTRANE	-1.55665E-09	-17.77200E-02	-1.21620E-04	-43.45000E-02
WATER VAPOR	2.88617E-08	82.07000E 00	1.62477E-04	72.09976E 00
NITROGEN	1.11740E-09	32.10000E-02	9.10297E-07	72.41619E-02
CO	7.14947E-07	91.07140E-01	1.44730E-05	64.14503E-01
OXYGEN	1.84552E-08	47.45450E-02	7.13344E-07	25.91576E-02
ARGON	7.21812E-09	67.77660E-02	6.47488E-09	27.96100E-02
CO2	-2.56884E-09	-84.46740E-02	-1.07315E-04	-47.96267E-02
CH4	-4.86425E-09	-13.73012E-02	-2.10261E-04	-75.18854E-02
C2H6	1.84007E-09	47.13000E-02	7.23760E-08	27.07780E-02
CH3	8.02870E-09	23.76740E-02	3.21600E-08	14.29387E-02
HYDROCARBONS	2.30145E-09	48.71736E-02	-2.07418E-09	-50.15588E-04

SUM OF CURRENTS = 3.10150E-06 AMPS

SENSITIVITY (TOTAL CURRENT/PPM DIFFERENCE) = 4.25020E-01 AMPS/PPM

SUMMATION PARTIAL PRESSURES = 3.49012E-06 Torr

RGA ADJUSTED PRESSURE = 3.87000E-06 Torr

DIFFERENCE (RGA ADJUSTED PRESSURE - SUMMATION PARTIAL PRESSURES) = 3.80588E-07 Torr

PERCENT DIFFERENCE = 10.073

RUN NO. 101, ACC-C, 350 MP AT 50 DEG
 CA°C = 2.14
 HOURS = 70.50
 TEMPERATURE DEVIATION C.I. = 49.25
 CHAMBER PRESSURE = 9.10000E-07
 WALL/CLD PRESSURE = 1.40000E-07
 GGA PRESSURE = 1.90000E-07

MILLIVOLTS (C/AL) = 2.00
 THERMAL CORRECTION = 4.78748E-07
 THERMAL CORRECTION = 1.47499E-07
 THERMAL CORRECTION = 1.89442E-07

W/E	MEASURED FROM MEICM (AMP)	CALCULATED W/E	DIFFERENCE	DIFFERENCE C/AL
2	0.80000E-06	0.79999E-06	-4.20326E-14	-49.44410E-06
4	1.70000E-12	1.00000E-12	0.0	0.0
12	1.10000E-06	1.71200E-06	6.12000E-07	94.18130E 00
13	4.70000E-11	-2.14747E-11	-7.14747E-11	-14.20193E 01
14	3.20000E-10	3.21787E-10	2.01787E-10	62.93750E 00
15	4.40000E-10	-3.27074E-10	-7.67074E-10	-17.11030E 01
16	7.90000E-08	4.78748E-08	4.78748E-08	10.53042E 00
17	1.40000E-08	1.56774E-08	1.67748E-08	9.52944E-01
18	5.70000E-09	5.64177E-09	-7.07418E-10	-93.95440E-02
22	1.90000E-10	7.57940E-10	4.79400E-10	14.71792E 00
24	2.70000E-10	3.19273E-10	4.92732E-11	20.79706E 00
27	5.60000E-10	4.98203E-10	-4.17403E-11	-17.97914E 00
28	5.70000E-09	4.19195E-09	-2.19010E-10	-41.74011E-02
29	7.70000E-10	4.94814E-10	-2.74186E-10	-32.94924E 00
30	2.90000E-10	7.49016E-10	-7.09016E-10	-11.70473E 00
32	2.70000E-09	2.19427E-09	-4.97246E-10	-10.92000E-01
47	8.90000E-11	8.90000E-11	0.0	0.0
48	1.10000E-08	1.49997E-08	-4.99970E-11	-12.11404E-02

44117 25 2500 01 70 5000 01 = 4.90000E 00

W/E	MEASURED FROM MEICM (AMP)	CALCULATED W/E	DIFFERENCE	DIFFERENCE C/AL
70.00 01	4.90000E-07	4.90000E-07	0.0	0.0
70.00 02	1.40000E-07	1.40000E-07	0.0	0.0
70.00 03	4.90000E-07	4.90000E-07	0.0	0.0
70.00 04	1.40000E-07	1.40000E-07	0.0	0.0
70.00 05	4.90000E-07	4.90000E-07	0.0	0.0
70.00 06	1.40000E-07	1.40000E-07	0.0	0.0
70.00 07	4.90000E-07	4.90000E-07	0.0	0.0
70.00 08	1.40000E-07	1.40000E-07	0.0	0.0
70.00 09	4.90000E-07	4.90000E-07	0.0	0.0
70.00 10	1.40000E-07	1.40000E-07	0.0	0.0
70.00 11	4.90000E-07	4.90000E-07	0.0	0.0
70.00 12	1.40000E-07	1.40000E-07	0.0	0.0
70.00 13	4.90000E-07	4.90000E-07	0.0	0.0
70.00 14	1.40000E-07	1.40000E-07	0.0	0.0
70.00 15	4.90000E-07	4.90000E-07	0.0	0.0
70.00 16	1.40000E-07	1.40000E-07	0.0	0.0
70.00 17	4.90000E-07	4.90000E-07	0.0	0.0
70.00 18	1.40000E-07	1.40000E-07	0.0	0.0
70.00 19	4.90000E-07	4.90000E-07	0.0	0.0
70.00 20	1.40000E-07	1.40000E-07	0.0	0.0
70.00 21	4.90000E-07	4.90000E-07	0.0	0.0
70.00 22	1.40000E-07	1.40000E-07	0.0	0.0
70.00 23	4.90000E-07	4.90000E-07	0.0	0.0
70.00 24	1.40000E-07	1.40000E-07	0.0	0.0
70.00 25	4.90000E-07	4.90000E-07	0.0	0.0
70.00 26	1.40000E-07	1.40000E-07	0.0	0.0
70.00 27	4.90000E-07	4.90000E-07	0.0	0.0
70.00 28	1.40000E-07	1.40000E-07	0.0	0.0
70.00 29	4.90000E-07	4.90000E-07	0.0	0.0
70.00 30	1.40000E-07	1.40000E-07	0.0	0.0
70.00 31	4.90000E-07	4.90000E-07	0.0	0.0
70.00 32	1.40000E-07	1.40000E-07	0.0	0.0
70.00 33	4.90000E-07	4.90000E-07	0.0	0.0
70.00 34	1.40000E-07	1.40000E-07	0.0	0.0
70.00 35	4.90000E-07	4.90000E-07	0.0	0.0
70.00 36	1.40000E-07	1.40000E-07	0.0	0.0
70.00 37	4.90000E-07	4.90000E-07	0.0	0.0
70.00 38	1.40000E-07	1.40000E-07	0.0	0.0
70.00 39	4.90000E-07	4.90000E-07	0.0	0.0
70.00 40	1.40000E-07	1.40000E-07	0.0	0.0
70.00 41	4.90000E-07	4.90000E-07	0.0	0.0
70.00 42	1.40000E-07	1.40000E-07	0.0	0.0
70.00 43	4.90000E-07	4.90000E-07	0.0	0.0
70.00 44	1.40000E-07	1.40000E-07	0.0	0.0
70.00 45	4.90000E-07	4.90000E-07	0.0	0.0
70.00 46	1.40000E-07	1.40000E-07	0.0	0.0
70.00 47	4.90000E-07	4.90000E-07	0.0	0.0
70.00 48	1.40000E-07	1.40000E-07	0.0	0.0
70.00 49	4.90000E-07	4.90000E-07	0.0	0.0
70.00 50	1.40000E-07	1.40000E-07	0.0	0.0
70.00 51	4.90000E-07	4.90000E-07	0.0	0.0
70.00 52	1.40000E-07	1.40000E-07	0.0	0.0
70.00 53	4.90000E-07	4.90000E-07	0.0	0.0
70.00 54	1.40000E-07	1.40000E-07	0.0	0.0
70.00 55	4.90000E-07	4.90000E-07	0.0	0.0
70.00 56	1.40000E-07	1.40000E-07	0.0	0.0
70.00 57	4.90000E-07	4.90000E-07	0.0	0.0
70.00 58	1.40000E-07	1.40000E-07	0.0	0.0
70.00 59	4.90000E-07	4.90000E-07	0.0	0.0
70.00 60	1.40000E-07	1.40000E-07	0.0	0.0
70.00 61	4.90000E-07	4.90000E-07	0.0	0.0
70.00 62	1.40000E-07	1.40000E-07	0.0	0.0
70.00 63	4.90000E-07	4.90000E-07	0.0	0.0
70.00 64	1.40000E-07	1.40000E-07	0.0	0.0
70.00 65	4.90000E-07	4.90000E-07	0.0	0.0
70.00 66	1.40000E-07	1.40000E-07	0.0	0.0
70.00 67	4.90000E-07	4.90000E-07	0.0	0.0
70.00 68	1.40000E-07	1.40000E-07	0.0	0.0
70.00 69	4.90000E-07	4.90000E-07	0.0	0.0
70.00 70	1.40000E-07	1.40000E-07	0.0	0.0
70.00 71	4.90000E-07	4.90000E-07	0.0	0.0
70.00 72	1.40000E-07	1.40000E-07	0.0	0.0
70.00 73	4.90000E-07	4.90000E-07	0.0	0.0
70.00 74	1.40000E-07	1.40000E-07	0.0	0.0
70.00 75	4.90000E-07	4.90000E-07	0.0	0.0
70.00 76	1.40000E-07	1.40000E-07	0.0	0.0
70.00 77	4.90000E-07	4.90000E-07	0.0	0.0
70.00 78	1.40000E-07	1.40000E-07	0.0	0.0
70.00 79	4.90000E-07	4.90000E-07	0.0	0.0
70.00 80	1.40000E-07	1.40000E-07	0.0	0.0
70.00 81	4.90000E-07	4.90000E-07	0.0	0.0
70.00 82	1.40000E-07	1.40000E-07	0.0	0.0
70.00 83	4.90000E-07	4.90000E-07	0.0	0.0
70.00 84	1.40000E-07	1.40000E-07	0.0	0.0
70.00 85	4.90000E-07	4.90000E-07	0.0	0.0
70.00 86	1.40000E-07	1.40000E-07	0.0	0.0
70.00 87	4.90000E-07	4.90000E-07	0.0	0.0
70.00 88	1.40000E-07	1.40000E-07	0.0	0.0
70.00 89	4.90000E-07	4.90000E-07	0.0	0.0
70.00 90	1.40000E-07	1.40000E-07	0.0	0.0
70.00 91	4.90000E-07	4.90000E-07	0.0	0.0
70.00 92	1.40000E-07	1.40000E-07	0.0	0.0
70.00 93	4.90000E-07	4.90000E-07	0.0	0.0
70.00 94	1.40000E-07	1.40000E-07	0.0	0.0
70.00 95	4.90000E-07	4.90000E-07	0.0	0.0
70.00 96	1.40000E-07	1.40000E-07	0.0	0.0
70.00 97	4.90000E-07	4.90000E-07	0.0	0.0
70.00 98	1.40000E-07	1.40000E-07	0.0	0.0
70.00 99	4.90000E-07	4.90000E-07	0.0	0.0
70.00 100	1.40000E-07	1.40000E-07	0.0	0.0

70.00 01 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 02 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 03 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 04 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 05 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 06 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 07 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 08 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 09 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 10 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 11 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 12 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 13 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 14 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 15 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 16 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 17 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 18 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 19 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 20 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 21 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 22 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 23 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 24 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 25 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 26 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 27 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 28 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 29 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 30 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 31 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 32 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 33 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 34 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 35 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 36 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 37 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 38 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 39 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 40 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 41 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 42 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 43 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 44 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 45 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 46 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 47 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 48 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 49 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 50 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 51 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 52 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 53 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 54 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 55 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 56 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 57 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 58 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 59 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 60 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 61 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 62 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 63 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 64 1.40000E-07 1.40000E-07 0.0 0.0
 70.00 65 4.90000E-07 4.90000E-07 0.0 0.0
 70.00 66 1.40000E-07

RUN NO. 101, 600-C, 350 MP AT 50 DEG
 DATE = 2.14
 HOURS = 46.75
 TEMPERATURE (DEGREES C.) = 49.25
 CHAMBER PRESSURE = 2.90000E-07
 MANIFOLD PRESSURE = 4.50000E-08
 RGA PRESSURE = 6.50000E-08

MILLIVOLTS (CP/AL) = 2.00
 THERMAL CORRECTION = 3.05534E-07
 THERMAL CORRECTION = 4.74104E-08
 THERMAL CORRECTION = 6.84817E-08

M/F	MEASURED PFAK HEIGHT (AMPS)	CALCULATED M/E	DIFFERENCE	PERCENT DIFF
2	4.40000E-09	4.35556E-09	-3.90795E-14	-88.81791E-05
4	1.00000E-13	1.00000E-13	0.0	0.0
12	7.00000E-09	1.10072E-09	-4.80927E-09	-82.98944E 00
13	2.00000E-11	1.67586E-11	-1.12414E-11	-40.14784E 00
14	1.60000E-10	-1.19721E-09	-1.35721E-09	-84.82546E 01
15	2.30000E-10	1.95708E-10	-3.42920E-11	-14.90955E 00
16	1.70000E-09	2.04157E-09	3.41568E-10	20.09225E 00
17	2.85000E-09	3.29269E-09	4.42697E-10	15.53307E 00
18	1.25000E-08	1.23693E-08	-1.30743E-10	-10.45947E-01
22	1.80000E-10	1.90075E-10	1.00749E-11	55.97189E-01
26	9.00000E-11	1.26240E-10	3.63403E-11	40.37810E 00
27	1.40000E-10	1.31580E-10	-2.84197E-11	-17.76231E 00
28	2.20000E-08	2.21224E-08	1.22412E-10	55.64194E-02
29	3.00000E-10	2.46142E-10	-5.38576E-11	-17.95253E 00
30	1.20000E-10	-1.51914E-10	-2.71914E-10	-22.65950E 01
32	6.00000E-10	5.73014E-10	-2.69857E-11	-44.97625E-01
40	2.00000E-11	2.00000E-11	0.0	0.0
44	1.00000E-09	1.91063E-08	1.06326E-10	55.96082E-02

RATIO OF GAGE P1 TO GAGE P2 = 6.44444E 00

GAS	PRESSURE TORR	PERCENT OF TOTAL PRESSURE	OUTGASSING RATE TORR LITERS/SEC	PERCENT OF TOTAL OUTGASSING RATE
GAGE P1	3.05534E-07		2.75951E-04	
TOTAL	7.02461E-08	99.99998E 00	5.79018E-06	99.99997E 00
H	2.07157E-08	29.49020E 00	2.72335E-06	60.17815E 00
HELIUM	2.50818E-12	35.70563E-04	2.67402E-10	51.52080E-04
METHANE	3.52169E-10	50.13360E-02	1.87727E-08	36.16968E-02
WATER VAPOR	1.86169E-08	26.50233E 00	9.35635E-07	19.02702E 00
NITROGEN	-1.54157E-08	-21.94522E 00	-6.21182E-07	-11.06843E 00
CO	3.07400E-08	43.76041E 00	1.23869E-06	23.06594E 00
CHYGEN	6.83728E-10	97.33323E-02	2.57718E-08	49.65490E-02
ARGON	2.21812E-11	31.57438E-03	7.47609E-10	14.40816E-03
CO2	1.43040E-08	20.36272E 00	4.59790E-07	89.59014E-01
C2H4	6.77920E-10	96.50676E-02	2.73172E-08	52.63237E-02
C2H6	-6.50683E-10	-92.60035E-02	-2.53227E-08	-49.78967E-02
C2H2	1.97100E-10	28.07258E-02	6.22891E-09	12.21327E-02
HYDROCARBONS	5.74904E-10	82.11218E-02	2.71061E-08	52.22565E-02

SUM OF CURRENTS = 7.33380E-08 AMPS
 SENSITIVITY (TOTAL CURRENT/PGA PRESSURE) = 1.00751E 00 AMPS/TORR
 SUMMATION PARTIAL PRESSURES = 7.02461E-08 TORR
 RGA ADJUSTED PRESSURE = 8.77425E-08 TORR
 DIFFERENCE (PGA ADJUSTED PRESSURE - SUMMATION PARTIAL PRESSURES) = 1.74964E-08 TORR
 PERCENT DIFFERENCE = 24.907

RUN NO. 101, 600-C, 350 HR AT 30 DEG

DATE = 2.15

HOURS = 63.25

TEMPERATURE (DEGREES C.) = 40.25

CHAMBER PRESSURE = 2.21000E-07

MANIFOLD PRESSURE = 2.40000E-08

GAGE PRESSURE = 5.00000E-08

MILLIVOLTS (CP/ALI) = 2.00

THERMAL CORRECTION = 2.32838E-07

THERMAL CORRECTION = 3.58212E-08

THERMAL CORRECTION = 5.26792E-08

W/F	MEASURED PEAK HEIGHT (AMPS)	CALCULATED W/F	DIFFERENCE	PERCENT DIFF
2	2.85000E-09	3.84966E-09	-4.26326E-14	-11.07340E-04
4	1.00000E-12	1.00000E-12	0.0	0.0
12	6.00000E-10	6.43034E-10	4.30340E-11	71.72334E-01
13	2.00000E-11	8.70471E-12	-1.12923E-11	-56.46640E-00
14	1.20000E-10	1.46305E-10	1.63049E-11	12.54221E-00
15	1.95000E-10	1.09484E-10	-8.53159E-11	-43.75174E-00
16	1.25000E-09	1.31533E-09	6.53142E-11	52.25136E-01
17	1.90000E-09	1.92724E-09	2.72393E-11	14.33648E-01
18	7.25000E-09	7.24026E-09	-9.73444E-12	-13.42680E-02
22	1.45000E-10	1.44695E-10	-3.04756E-13	-21.01756E-02
26	5.00000E-11	6.50376E-11	5.03762E-12	83.97035E-01
27	1.10000E-10	1.05272E-10	-4.72848E-12	-42.98619E-01
28	1.70000E-10	1.69979E-09	-2.09610E-12	-12.33070E-03
29	2.25000E-10	2.46484E-10	2.44842E-11	10.88187E-00
30	9.00000E-11	8.53395E-11	-4.66049E-12	-51.78327E-01
32	2.45000E-10	3.25835E-10	8.16720E-12	33.35601E-01
40	1.10000E-11	1.10000E-11	0.0	0.0
44	1.45000E-09	1.44556E-09	-4.38405E-12	-30.23480E-03

RATIO OF GAGE P1 TO GAGE P2 = 6.50000E-00

GAS	PRESSURE TORR	PERCENT OF TOTAL PRESSURE	OUTGASSING RATE TORR LITERS/SEC	PERCENT OF TOTAL OUTGASSING RATE
GAGE P1	2.22838E-07		2.10624E-04	
TOTAL	5.33299E-08	66.99998E-00	4.14510E-04	66.99998E-00
H	1.81752E-08	34.08134E-00	2.71906E-06	65.59694E-00
HELIUM	2.40818E-12	47.02239E-04	2.45329E-10	64.01010E-04
METHANE	1.89493E-10	35.53298E-02	1.07229E-08	24.17983E-02
WATER VAPOR	1.79277E-08	20.43410E-00	5.43421E-07	13.10994E-00
NITROGEN	4.21817E-10	76.05728E-02	1.68655E-08	40.68780E-02
CO	1.27862E-09	22.66375E-00	4.82240E-07	11.65830E-00
OXYGEN	4.05500E-10	76.07768E-02	1.51660E-08	36.58770E-02
ARGON	1.21997E-11	22.57631E-03	4.08106E-10	98.45491E-04
CO2	1.08890E-08	20.41856E-00	3.47309E-07	83.78775E-01
C2H6	2.65598E-11	68.55345E-03	1.46173E-09	35.26402E-03
C2H4	1.40978E-10	30.17645E-02	6.21619E-09	14.99647E-02
C3H8	5.20545E-11	97.61041E-03	1.66030E-09	40.05451E-03
HYDROCARBON	4.36034E-10	82.22576E-02	1.93610E-08	46.70815E-02

SUM OF CURRENTS = 4.76811E-09 AMPS

SENSITIVITY (TOTAL CURRENT/GAGE PRESSURE) = 5.53621E-01 AMPS/TORR

SUMMATION PARTIAL PRESSURES = 5.33288E-08 TORR

GAGE ADJUSTED PRESSURE = 7.03411E-08 TORR

DIFFERENCE (GAGE ADJUSTED PRESSURE - SUMMATION PARTIAL PRESSURES) = 1.70123E-09 TORR

PERCENT DIFFERENCE = 21.901

RUN NO. 101, 600-C, 350 MP AT 50 DEG

DATE = 2.16

HOURS = 75.00

TEMPERATURE (DEGREES C.) = 49.25

CHAMBER PRESSURE = 1.67000E-07

MANIFOLD PRESSURE = 2.50000E-08

SGA PRESSURE = 4.00000E-09

MILLIVOLTS (CP/AL) = 2.00

THERMAL CORRECTION = 1.71731E-07

THERMAL CORRECTION = 2.63391E-08

THERMAL CORRECTION = 4.21426E-08

M/E	MEASURED PEAK HEIGHT (AMPS)	CALCULATED M/E	DIFFERENCE	PERCENT DIFF
2	3.05000E-05	3.05000E-05	-4.44080E-15	-14.56030E-05
4	1.00000E-13	1.00000E-13	0.0	0.0
12	5.00000E-10	4.21756E-10	-7.82441E-11	-15.64982E 00
13	1.50000E-11	7.70095E-12	-7.29904E-12	-48.66029E 00
14	1.10000E-10	9.72606E-11	-1.27394E-11	-11.58125E 00
15	1.60000E-10	8.48679E-11	-7.51321E-11	-46.95755E 00
16	5.50000E-10	1.01550E-09	6.65000E-11	69.36836E-01
17	1.10000E-09	9.43147E-10	-1.56853E-10	-14.25936E 00
18	3.50000E-09	3.53922E-09	3.92213E-11	11.20607E-01
22	1.25000E-10	1.21931E-10	-3.06905E-12	-24.55269E-01
26	5.50000E-11	1.61979E-11	-3.58421E-11	-65.16747E 00
27	8.50000E-11	1.18741E-10	3.37410E-11	39.69530E 00
28	1.00000E-08	1.00007E-08	6.60805E-13	66.08047E-04
29	1.95000E-10	1.63811E-10	-8.91076E-12	-47.62571E-01
30	7.50000E-10	7.27092E-10	-1.29077E-11	-17.21023E-01
32	5.80000E-10	2.74793E-10	-5.20717E-12	-18.59704E-01
40	1.30000E-11	1.30000E-11	0.0	0.0
44	1.20000E-08	1.15982E-08	-1.81188E-12	-15.09903E-03

PA-TIC OF GAGE P1 TO GAGE P2 = 6.52000E 00

GAS	PRESSURE TORR	PERCENT OF TOTAL PRESSURE	OUTGASSING RATE TORR LITERS/SEC	PERCENT OF TOTAL OUTGASSING RATE
GAGE P1	1.71731E-07		1.55434E-06	
TOTAL	3.54100E-08	99.99998E 00	2.76237E-06	99.99998E 00
H	1.44979E-08	40.70178E 00	2.00075E-06	72.42888E 00
HELIUM	2.50218E-12	70.41514E-04	2.44755E-10	88.60216E-04
METHANE	2.44344E-10	68.95740E-02	1.15219E-08	43.15811E-02
WATER VAPOR	5.32688E-09	14.95670E 00	2.45040E-07	88.70435E-01
NITROGEN	3.50972E-10	98.59248E-02	1.25448E-08	46.86123E-02
CO	5.20461E-09	14.61151E 00	1.01560E-07	69.49114E-01
OXYGEN	3.27886E-10	92.05140E-02	1.13123E-08	40.95141E-02
ARGON	1.44178E-11	40.47675E-03	4.44909E-10	16.10605E-03
CO2	9.17587E-09	25.76048E 00	2.60075E-07	97.73293E-01
C2H4	-1.23817E-09	-34.75524E-01	-4.66556E-08	-16.53121E-01
C2H6	2.10156E-09	58.99945E-01	7.48832E-09	27.10832E-01
C3H8	-3.89908E-10	-10.91825E-01	-1.14425E-08	-41.42289E-02
HYDROCARBONS	7.18875E-10	20.18194E-01	2.56972E-08	90.75062E-01

SUM OF CURRENTS = 3.28781E-08 AMPS

SENSITIVITY (TOTAL CURRENT/SGA PRESSURE) = 8.21957E-01 AMPS/TORR

SUMMATION PARTIAL PRESSURES = 3.56155E-08 TORR

SGA ADJUSTED PRESSURE = 5.84415E-08 TORR

DIFFERENCE (SGA ADJUSTED PRESSURE - SUMMATION PARTIAL PRESSURES) = 2.28215E-09 TORR

PERCENT DIFFERENCE = 64.070

RUN NO. 101, 600-C, 2°C HD AT 50 DEG

DATE = 2.10

HOURS = 137.00

TEMPERATURE (DEGREES C.) = 49.25

CHAMBER PRESSURE = 7.25000E-08

MANIFOLD PRESSURE = 1.10000E-08

RGA PRESSURE = 2.10000E-08

MILLIVOLTS (CP/AL) = 2.00
THERMAL CORRECTION = 7.63834E-08
THERMAL CORRECTION = 1.15892E-00
THERMAL CORRECTION = 2.21249E-08

M/E	MEASURED PFAK HEIGHT (AMPS)	CALCULATED M/E	DIFFERENCE	PERCENT DIFF
2	2.50000E-09	2.50000E-09	-3.77474E-15	-15.09903E-05
4	1.00000E-12	1.00000E-12	0.0	0.0
12	3.20000E-10	3.40664E-10	2.06664E-11	65.20200E-01
13	1.10000E-11	2.00271E-11	1.89271E-11	17.20467E 01
14	6.20000E-11	1.02078E-10	4.0077E-11	64.60916E 00
15	5.20000E-10	4.37312E-10	-4.82687E-10	-52.46603E 00
16	6.00000E-10	1.05882E-09	3.78827E-10	55.70985E 00
17	4.05000E-10	4.01383E-10	-3.61644E-12	-89.29483E-02
18	1.50000E-09	1.48657E-09	-1.34226E-11	-89.54057E-02
22	5.00000E-11	8.20327E-11	3.20327E-11	64.06551E 00
26	2.00000E-11	7.18024E-12	-2.18154E-11	-75.24014E 00
27	2.20000E-11	5.08550E-11	3.88550E-11	58.92200E 00
28	7.50000E-09	7.45407E-09	-5.02705E-12	-67.02787E-02
29	9.00000E-11	2.12488E-10	1.22488E-10	13.60980E 01
30	3.00000E-11	-1.06242E-11	-4.06242E-11	-13.54140E 01
32	1.10000E-10	5.00722E-11	-2.90278E-11	-27.20705E 00
40	5.00000E-12	5.00000E-12	0.0	0.0
44	8.20000E-09	8.27525E-09	7.525E-11	25.00165E-02

RATIO OF GAGE P1 TO GAGE P2 = 6.59051E 00

GAS	DIFFUSION TODD	PERCENT OF TOTAL DIFFUSION	OUTGASSING RATE TODD LITERS/SEC	PERCENT OF TOTAL OUTGASSING RATE
GAGE P1	7.63834E-08		6.52492E-07	
TOTAL	2.65480E-08	66.05038E 00	1.62062E-06	66.06907E 00
H	1.17000E-09	44.3737E 00	1.58109E-06	75.48422E 00
HELIUM	2.50818E-12	64.40252E-04	7.07627E-10	11.35547E-03
METHANE	8.40000E-10	31.65647E-01	3.51636E-08	19.21886E-01
WATER VAPOR	2.27742E-09	86.21704E-01	8.77677E-08	47.75176E-01
NITROGEN	-1.17460E-10	-41.64370E-02	-3.48000E-09	-19.04042E-02
CO	5.42726E-09	20.40076E 00	1.45649E-07	9.75066E-01
CHYGEN	5.56433E-11	25.54059E-02	2.75911E-09	15.76231E-02
ARGON	5.54530E-12	20.87140E-02	1.45254E-10	79.39100E-04
CO2	4.17334E-09	22.23571E 00	1.44182E-07	84.24647E-01
C2H4	3.24823E-11	12.22548E-02	1.01607E-09	55.58224E-03
C2H6	-7.68460E-11	-28.62476E-02	-2.22442E-09	-12.70477E-02
C3H8	1.51558E-10	57.15706E-02	3.78615E-09	20.46355E-02
HYDROCARBONS	5.56726E-10	25.59000E-02	7.76421E-09	20.57361E-01

SUM OF CURRENTS = 2.24441E-08 AMPS

SENSITIVITY (TOTAL CURRENT/DC DIFFUSION) = 1.07253E 00 AMPS/TODD

SUMMATION PARTIAL DIFFUSIONS = 2.65480E-08 TODD

RGA ADJUSTED DIFFUSION = 2.15745E-08 TODD

DIFFERENCE (RGA ADJUSTED DIFFUSION - SUMMATION PARTIAL DIFFUSIONS) = 5.20756E-09 TODD

PERCENT DIFFERENCE = 19.477

RUN NO. 101, 500-C, 340 MB AT 50 DEG
 DATE = 2.10
 MCUPS = 141.25
 TEMPERATURE (CEG) = 49.25
 CHAMBER PRESSURE = 5.09999E-08
 MANIFOLD PRESSURE = 1.40000E-08
 PGA PRESSURE = 2.10000E-08
 MILLIVOLTS (CP/AL) = 2.00
 THERMAL CORRECTION = 9.58743E-08
 THERMAL CORRECTION = 1.47499E-08
 THERMAL CORRECTION = 2.21249E-08

M/E	MEASURED PEAK HEIGHT (AMPS)	CALCULATED M/E	DIFFERENCE	PERCENT DIFF
2	2.95000E-05	2.55000E-05	-3.77476E-15	-14.80207E-05
4	1.30000E-13	1.00000E-13	0.0	0.0
12	2.70000E-10	7.85734E-10	1.97342E-11	72.08971E-01
13	1.00000E-11	6.57619E-12	-3.02381E-12	-30.23811E-01
14	5.40000E-11	6.04301E-11	4.43014E-12	79.10954E-01
15	8.15000E-11	8.41494E-11	2.66842E-12	32.74136E-01
16	5.50000E-10	5.87069E-10	2.50121E-12	45.68155E-01
17	3.15000E-10	3.07678E-10	-7.32170E-12	-23.24349E-01
18	1.15000E-09	1.15206E-09	7.05924E-12	7.90645E-02
22	5.00000E-11	7.14678E-11	2.14678E-11	42.93688E-01
26	2.50000E-11	7.03436E-11	3.34366E-12	12.85485E-01
27	4.00000E-11	3.68848E-11	-3.11523E-12	-77.88074E-01
28	6.00000E-09	6.75941E-09	7.5941E-10	12.65700E-01
29	7.00000E-11	7.05401E-11	5.401E-12	7.71644E-02
30	2.50000E-11	2.63282E-11	1.3282E-12	5.31275E-01
32	5.70000E-11	6.72310E-11	2.7101E-12	4.75560E-02
40	5.50000E-12	6.50000E-12	0.0	0.0
44	7.15000E-05	7.14950E-05	-4.07300E-13	-5.69361E-04

RATIO OF GAGE P1 TO GAGE P2 = 6.50000E-08

GAS	PRESSURE TORR	PERCENT OF TOTAL PRESSURE	OUTGASSING RATE TORR LITER/SEC	PERCENT OF TOTAL OUTGASSING RATE
GAGE P1	9.58743E-08	66.00000E-01	8.67272E-07	59.95998E-01
TOTAL	2.43700E-08	46.43700E-01	7.22438E-06	79.37999E-01
H	1.20378E-08	15.50000E-01	1.76558E-06	11.69430E-01
HELIUM	2.50000E-12	72.08971E-01	2.60126E-10	40.89269E-01
METHANE	1.75412E-10	71.20739E-01	5.09410E-09	38.11049E-01
WATER VAPOR	1.73300E-05	45.58512E-01	8.47728E-08	19.56158E-01
NITROGEN	1.11704E-10	15.72576E-01	4.75124E-09	83.05549E-01
CO	4.71329E-05	42.74414E-01	1.64755E-07	17.15771E-01
CHYGEN	1.04085E-10	29.60436E-01	3.81653E-09	10.62870E-01
ARGON	7.20889E-12	27.09298E-01	7.36427E-10	75.42823E-01
CO2	5.37970E-09	16.45222E-01	1.57065E-09	70.60224E-01
C2H4	4.00638E-11	10.16733E-01	1.67405E-09	78.29576E-01
C2H6	4.63201E-11	50.93823E-01	4.47888E-11	20.17573E-01
C3H8	1.67510E-12	10.72411E-01	1.23864E-09	55.68461E-01
HYDROCARBONS	2.61140E-10	10.72411E-01	1.23864E-09	55.68461E-01

SUM OF CURRENTS = 1.92771E-06 AMPS
 SENSITIVITY (TOTAL CURRENT/PGA PRESSURE) = 9.17956E-01 AMPS/TORR
 SUMMATION PARTIAL PRESSURES = 2.43700E-08 TORR
 PGA ADJUSTED PRESSURE = 7.36123E-08 TORR
 DIFFERENCE (PGA ADJUSTED PRESSURE - SUMMATION PARTIAL PRESSURES) = 4.92422E-09 TORR
 PERCENT DIFFERENCE = 37.336

RUN NO. 101, 600-C, 350 MP AT 50 DEG
 DATE = 2.22
 HOURS = 210.50
 TEMPERATURE (CEGDEES C.) = 49.2F
 CHAMBER PRESSURE = 6.11000E-08
 MANIFOLD PRESSURE = 9.40000E-08
 VACUUM PRESSURE = 2.10000E-08
 MILLIVOLTS (C/P11) = 2.00
 THERMAL CORRECTION = 4.43728E-08
 THERMAL CORRECTION = 9.90391E-09
 THERMAL CORRECTION = 2.21249E-08

M/C	MEASURED PRESSURE HEIGHT (AMPS)	CALCULATED M/F	DIFFERENCE	PERCENT DIFF
2	2.55000E-09	2.55000E-09	-3.99600E-15	-15.67373E-05
4	1.00000E-13	1.00000E-13	0.0	0.0
12	3.20000E-10	3.29760E-10	9.76000E-12	30.50200E-01
13	9.50000E-12	4.48600E-12	-5.01400E-12	-53.11602E-01
14	5.40000E-11	5.05400E-11	-3.46000E-12	-64.05720E-01
15	6.90000E-11	7.51400E-11	6.14000E-12	89.13027E-01
16	5.90000E-10	5.71701E-10	-1.82900E-12	-31.00885E-01
17	1.70000E-10	1.42928E-10	-2.70720E-12	-15.93176E-01
18	6.10000E-10	6.11900E-10	1.90000E-12	31.16431E-02
22	2.00000E-11	7.10104E-11	5.10104E-11	255.05222E-01
26	2.25000E-11	7.61563E-11	5.36563E-11	238.42784E-01
27	2.90000E-11	3.55633E-11	6.66333E-12	229.76034E-01
28	8.75000E-09	8.74947E-09	-5.30000E-13	-6.05242E-04
29	9.00000E-11	9.24590E-11	2.45900E-12	27.33542E-01
30	4.00000E-11	4.14000E-11	1.40000E-12	35.00000E-01
32	5.40000E-11	5.46500E-11	6.50000E-13	12.03704E-01
40	5.00000E-12	5.00000E-12	0.0	0.0
44	7.10000E-09	7.05000E-09	-5.00000E-13	-6.90170E-04

RATIO OF GAGE P1 TO GAGE P2 = 6.00000E-00

GAS	PRESSURE TORR	PERCENT OF TOTAL PRESSURE	OUTGASSING RATE TORR LITERS/SEC	PERCENT OF TOTAL OUTGASSING RATE
GAGE P1	4.43728E-08	66.66666E-00	5.82212E-07	69.99997E-00
TOTAL	7.51248E-08	100.00000E-00	8.31248E-07	100.00000E-00
H	1.70400E-08	22.82222E-00	2.25712E-07	27.14286E-00
HELIUM	2.50000E-12	0.03333E-00	1.00000E-10	0.01210E-00
METHANE	1.45600E-10	1.93889E-00	1.70600E-09	20.52381E-00
WATER VAPOR	5.21000E-10	6.93611E-00	7.02300E-09	8.44790E-00
NITROGEN	-1.00000E-11	-0.01333E-00	-5.00000E-10	-0.60121E-00
O	4.52000E-08	60.18182E-00	1.14100E-07	13.72222E-00
CHYGEN	4.52100E-11	0.00601E-00	1.40550E-09	0.16961E-00
ARGON	5.40000E-12	0.00719E-00	1.22100E-10	0.14625E-00
CO2	5.24000E-08	6.97619E-00	1.12100E-07	13.48525E-00
CH4	1.25700E-11	0.01673E-00	1.41510E-10	0.17086E-00
C2H6	7.57200E-11	0.01008E-00	1.02400E-09	0.12327E-00
C2H2	-2.67000E-12	-0.03556E-00	-5.00000E-11	-0.60121E-00
HYDROCARBONS	7.50640E-10	10.00589E-00	7.04100E-09	8.46250E-00

SUM OF CURRENTS = 7.04921E-04 AMPS
 SENSITIVITY (TOTAL CURRENT/RAW PRESSURE) = 0.7813E-01 AMPS/TORR
 SUMMATION PARTIAL PRESSURES = 7.51248E-08 TORR
 RGA ADJUSTED PRESSURE = 7.30822E-08 TORR
 DIFFERENCE (RGA ADJUSTED PRESSURE - SUMMATION PARTIAL PRESSURES) = 2.05047E-09 TORR
 PERCENT DIFFERENCE = 0.2729E-00

RUN NO. 101, 600-C, 350 HR AT 50 DEG

DATE = 2.25

HOURS = 223.25

TEMPERATURE (DEGREES C.) = 49.25

CHAMBER PRESSURE = 4.55000E-08

MANIFOLD PRESSURE = 7.00000E-08

PGA PRESSURE = 1.05000E-08

MILLIVOLTS (CP/AL) = 2.00
THERMAL CORRECTION = 4.79372E-08
THERMAL CORRECTION = 7.37495E-09
THERMAL CORRECTION = 1.10624E-08

M/E	MEASURED PEAK HEIGHT (MPPS)	CALCULATED M/E	DIFFERENCE	PERCENT DIFF
2	2.10000E-09	2.10000E-09	-2.88458E-15	-13.74561E-05
4	1.00000E-13	1.00000E-13	0.0	0.0
12	1.20000E-10	1.20141E-10	1.41514E-11	15.95948E-00
13	7.00000E-12	4.41365E-12	-2.58635E-12	-38.48468E-00
14	2.55000E-11	4.01035E-11	4.60351E-12	12.96764E-00
15	5.80000E-11	5.44110E-11	-1.58902E-12	-27.39690E-01
16	2.35000E-10	2.35389E-10	2.89244E-13	16.56359E-02
17	6.10000E-11	5.54186E-11	-1.58136E-12	-25.92393E-01
18	2.20000E-10	2.20406E-10	4.05995E-13	18.45430E-02
22	2.35000E-11	2.34533E-11	-4.66571E-14	-19.85410E-02
26	2.20000E-11	7.24183E-11	4.18204E-11	19.01382E-01
27	3.10000E-11	3.06443E-11	-3.55646E-13	-11.47244E-01
28	4.45000E-09	4.44949E-09	-5.11501E-13	-11.49642E-03
29	5.90000E-11	5.97513E-11	7.51330E-13	12.73430E-01
30	1.90000E-11	1.97839E-11	7.83928E-13	41.29399E-01
32	1.70000E-11	1.69600E-11	-3.09742E-14	-18.27072E-02
40	1.15000E-11	1.15000E-11	0.0	0.0
44	2.25000E-09	2.24997E-09	-4.34319E-13	-18.48167E-03

RATIO OF GAGE P1 TO GAGE P2 = 6.50000E-00

GAS	PRESSURE TORR	PERCENT OF TOTAL PRESSURE	OUTGASSING RATE TORR LITERS/SEC	PERCENT OF TOTAL OUTGASSING RATE
GAGE P1	4.70372E-09		4.73637E-07	
TOTAL	1.57054E-08	99.99997E-00	1.47171E-06	99.99997E-00
H	9.91444E-09	63.12776E-00	1.45415E-06	86.98574E-00
HELIUM	2.50818E-12	15.97017E-03	2.60126E-10	15.56045E-03
METHANE	1.12609E-10	71.75392E-02	5.84373E-09	34.95653E-02
WATER VAPOR	3.21731E-10	21.12208E-01	1.62183E-08	97.01599E-02
NITROGEN	5.08599E-11	32.38367E-02	1.95366E-09	11.92586E-02
CO	3.42413E-09	21.80222E-00	1.34223E-07	80.29057E-01
OXYGEN	3.02477E-11	12.85214E-02	7.42420E-10	44.41126E-03
ARGON	1.27542E-11	81.20883E-03	4.18291E-10	25.02169E-03
CO2	1.76497E-09	11.22799E-00	5.1908E-08	33.01451E-01
C2H4	2.01324E-11	12.84528E-02	1.14196E-09	48.31099E-03
C2H6	3.34800E-11	21.31746E-02	1.24788E-09	75.84333E-03
C2H8	8.44281E-12	53.75729E-03	2.64007E-10	15.79260E-03
HYDROCARBONS	1.83748E-10	11.65564E-01	8.51758E-09	50.95120E-02

SUM OF CURRENTS = 9.82009E-09 AMPS

SENSITIVITY (TOTAL CURRENT/PGA PRESSURE) = 9.35247E-01 AMPS/TORR

SUMMATION PARTIAL PRESSURES = 1.57054E-08 TORR

PGA ADJUSTED PRESSURE = 1.88277E-08 TORR

DIFFERENCE (PGA ADJUSTED PRESSURE - SUMMATION PARTIAL PRESSURES) = 2.13204E-09 TORR

PERCENT DIFFERENCE = 10.642

RUN NO. 101, 300-C, 350 HR AT 50 DEG

DATE = 2.28

HOURS = 350.25

TEMPERATURE (DEGREES C.) = 49.25

CHAMBER PRESSURE = 3.12000E-08

MANIFOLD PRESSURE = 4.90000E-09

RGA PRESSURE = 7.40000E-09

MILLIVOLTS (CR/AL) = 2.00

THERMAL CORRECTION = 3.28712E-08

THERMAL CORRECTION = 5.05711E-09

THERMAL CORRECTION = 7.79638E-09

M/F	MEASURED PEAK HEIGHT (AMPS)	CALCULATED M/F	DIFFERENCE	PERCENT DIFF
2	1.66000E-09	1.66000E-09	-2.88658E-15	-17.38903E-05
4	1.90000E-13	1.00000E-13	0.0	0.0
12	9.20000E-11	9.79177E-11	5.91367E-12	64.27901E-01
13	4.40000E-12	2.79632E-12	-1.60367E-12	-36.44714E 00
14	2.50000E-11	2.63918E-11	1.39184E-12	55.67382E-01
15	3.50000E-11	3.50768E-11	7.68274E-14	21.95070E-02
16	1.68000E-10	1.67733E-10	-2.66606E-13	-15.86941E-02
17	4.15000E-11	3.92294E-11	-2.27156E-12	-54.73701E-01
18	1.45000E-10	1.45614E-10	6.14453E-13	42.37603E-02
22	1.70000E-10	1.81901E-11	-1.51810E-10	-89.29956E 00
26	1.18000E-11	1.11569E-11	-6.43085E-13	-54.49876E-01
27	1.50000E-11	1.56520E-11	6.52048E-13	43.46989E-01
28	2.95000E-09	2.94983E-09	-1.70530E-13	-57.80686E-04
29	3.80000E-11	3.71630E-11	-8.37025E-13	-22.02697E-01
30	1.10000E-11	1.17341E-11	7.34142E-13	66.74015E-01
32	1.20000E-11	1.20209E-11	2.03109E-14	17.43324E-02
40	4.50000E-12	4.50000E-12	0.0	0.0
44	1.92000E-09	1.82140E-09	-9.86000E-12	-76.98357E-03

RATIO OF GAGE P1 TO GAGE P2 = 6.50000E 00

GAS	PRESSURE TORR	PERCENT OF TOTAL PRESSURE	OUTGASSING RATE TORR LITERS/SEC	PERCENT OF TOTAL OUTGASSING RATE
GAGE P1	3.28712E-08		2.97351E-07	
TOTAL	1.18222E-08	99.99997E 00	1.26236E-04	99.99998E 00
H	7.83891E-09	66.25066E 00	1.11866E-06	88.54619E 00
HELIUM	2.50918E-12	21.19794E-02	2.53096E-10	20.03357E-02
METHANE	7.05494E-11	59.62496E-02	2.55950E-09	20.17491E-02
WATER VAPOR	2.19163E-10	18.52261E-01	1.04753E-08	82.52031E-02
NITROGEN	4.15394E-11	35.10724E-02	1.58431E-09	12.54043E-02
CO	2.23495E-09	18.88909E 00	8.52374E-08	67.46889E-01
CHYGEN	1.43435E-11	12.12246E-02	5.11724E-10	40.50518E-03
ARGON	4.99077E-12	42.17956E-02	1.59255E-10	12.60570E-03
CO2	1.26889E-09	11.56517E 00	4.16483E-09	32.96632E-01
C2H4	1.21442E-11	11.10895E-02	5.01316E-10	39.68110E-03
C2H6	1.85341E-11	15.66411E-02	6.82915E-10	54.05552E-03
C3H8	4.77799E-12	40.78126E-02	1.45970E-10	11.50664E-03
HYDROCARBONS	1.07006E-10	90.43557E-02	4.88910E-09	38.69923E-02

SUM OF CURRENTS = 7.20320E-09 AMPS

SENSITIVITY (TOTAL CURRENT/RGA PRESSURE) = 6.73418E-01 AMPS/TORR

SUMMATION PARTIAL PRESSURES = 1.18222E-08 TORR

RGA ADJUSTED PRESSURE = 1.35670E-08 TORR

DIFFERENCE (RGA ADJUSTED PRESSURE - SUMMATION PARTIAL PRESSURES) = 1.73571E-09 TORR

PERCENT DIFFERENCE = 14.66

GAS	HOURS	TEMP	OUTGASSING RATE	GAS	HOURS	TEMP	OUTGASSING RATE
GAGE P1	2.00	49.2°	1.61178E-04	TOTAL	2.00	49.25	2.25629E-04
	20.50	49.2°	8.67274E-06		20.50	49.25	1.48687E-05
	31.00	49.2°	4.76431E-06		31.00	49.25	6.65044E-07
	46.00	49.25	2.72572E-06		46.00	49.25	4.95571E-07
	46.7°	49.25	2.75051E-06		46.75	49.25	5.19018E-06
	63.25	49.25	2.16424E-06		63.25	49.25	4.14510E-06
	75.00	49.2°	1.55434E-06		75.00	49.2°	2.76237E-06
	137.00	49.25	6.52603E-07		137.00	49.2°	1.82963E-06
	141.2°	49.7°	8.67273E-07		141.25	49.2°	2.22438E-06
	210.50	49.2°	5.82313E-07		210.50	49.25	1.50908E-06
	293.25	49.2°	4.22627E-07		293.25	49.25	1.67171E-06
	350.2°	49.25	2.67251E-07		350.2°	49.25	1.26336E-06

GAS	HOURS	TEMP	OUTGASSING RATE
H	7.00	49.25	4.82617E-05
	20.50	49.25	7.16635E-06
	31.00	49.25	3.32662E-06
	46.00	49.25	2.52671E-06
	49.75	49.25	3.12335E-06
	43.75	49.25	2.71506E-06
	75.00	49.25	2.00075E-06
	137.00	49.25	1.35105E-06
	141.25	49.25	1.74555E-06
	210.50	49.25	1.18575E-06
	243.75	49.25	1.45615E-06
	350.25	49.25	1.31866E-06

GAS	HOURS	TEMP	OUTGASSING RATE
HELIUM	2.00	49.75	1.02745E-10
	20.50	49.75	3.02481E-10
	31.00	49.25	2.59076E-10
	46.00	49.25	2.64126E-10
	49.75	49.25	2.67402E-10
	43.25	49.25	2.65325E-10
	75.00	49.25	2.44755E-10
	137.00	49.25	2.07763E-10
	141.25	49.25	2.60126E-10
	210.50	49.25	1.74456E-10
	243.25	49.25	2.60124E-10
	350.25	49.25	2.53096E-10

GAS	HOURS	TEMP	OUTGASSING RATE	GAS	HOURS	TEMP	OUTGASSING RATE
METHANE	2.00	49.25	-1.2067CF-QE	WATER VAPOR	2.00	49.25	1.62677E-C4
	20.00	49.25	-5.64452E-QE		20.00	49.25	4.86692E-C4
	31.00	49.25	1.89125E-C4		31.00	49.25	1.76923E-C4
	46.00	49.25	2.15455E-C4		46.00	49.25	8.98532E-C7
	46.75	49.25	1.47727E-C4		46.75	49.25	9.35635E-C7
	63.25	49.25	1.66278E-C4		63.25	49.25	5.42421E-C7
	75.00	49.25	1.15219E-C4		75.00	49.25	7.45040E-C7
	137.00	49.25	2.51634E-C4		137.00	49.25	4.71477E-C8
	141.25	49.25	9.6567CF-C4		141.25	49.25	8.47728E-C8
	210.00	49.25	5.72644E-C4		210.00	49.25	3.02331E-C8
	283.25	49.25	5.84373E-C4		283.25	49.25	1.62183E-C8
	350.25	49.25	3.5555CF-C4		350.25	49.25	1.04252E-C8

GAS	MMPS	TEMP	OUTGASSING RATE
NITROGEN	2.00	49.25	5.16287E-07
	20.50	49.25	1.54402E-07
	31.00	49.25	2.42340E-08
	46.00	49.25	1.17757E-08
	46.75	49.25	-6.21182E-07
	53.25	49.25	1.68675E-08
	75.00	49.25	1.25448E-08
	137.00	49.25	-3.48500E-09
	141.25	49.25	4.25124E-09
	210.50	49.25	-5.74731E-10
	283.25	49.25	1.95366E-09
	350.25	49.25	1.58431E-09

GAS	HOURS	TEMP	OUTGASSING RATE
CC	2.00	49.25	1.44739E-05
	20.50	49.25	1.64668E-06
	31.00	49.25	9.62183E-07
	46.00	49.25	5.67974E-07
	46.75	49.25	1.23869E-06
	53.25	49.25	4.82249E-07
	75.00	49.25	1.91960E-07
	137.00	49.25	1.69699E-07
	141.25	49.25	7.84756E-07
	210.50	49.25	1.71618E-07
	283.25	49.25	1.34223E-07
	350.25	49.25	8.52374E-08

GAS	HOURS	TEMP	OUTGASSING RATE	GAS	HOURS	TEMP	OUTGASSING RATE
OXYGEN	2.00	49.25	7.13244E-07	ARGON	2.00	49.25	8.47488E-08
	20.50	49.25	1.15067E-07		20.50	49.25	3.60700E-09
	31.00	49.25	5.45142E-08		31.00	49.25	1.22387E-09
	46.00	49.25	2.66436E-08		46.00	49.25	6.64788E-10
	46.75	49.25	2.57718E-08		46.75	49.25	7.47809E-10
	63.25	49.25	1.51660E-08		63.25	49.25	4.08106E-10
	75.00	49.25	1.13123E-08		75.00	49.25	4.44909E-10
	137.00	49.25	2.76811E-09		137.00	49.25	1.45256E-10
	141.25	49.25	3.81653E-09		141.25	49.25	2.36425E-10
	210.50	49.25	1.60557E-09		210.50	49.25	1.22110E-10
	283.25	49.25	7.42429E-10		283.25	49.25	4.18291E-10
	350.25	49.25	5.11726E-10		350.25	49.25	1.59255E-10

GAS	HOURS	TEMP	OUTGASSING RATE
CO2	2.00	49.25	-1.07315E-06
	20.50	49.25	9.82696E-07
	31.00	49.25	5.64232E-07
	46.00	49.25	4.05505E-07
	46.75	49.25	4.59799E-07
	63.25	49.25	3.47309E-07
	75.00	49.25	2.69975E-07
	137.00	49.25	1.54182E-07
	141.25	49.25	1.68226E-07
	210.50	49.25	1.12192E-07
	283.25	49.25	5.51908E-08
	350.25	49.25	4.16483E-08

GAS	HOURS	TEMP	OUTGASSING RATE
C2H4	2.00	49.25	-2.10261E-06
	20.50	49.25	1.71498E-08
	31.00	49.25	2.71479E-09
	46.00	49.25	2.52605E-09
	46.75	49.25	2.73172E-09
	63.25	49.25	1.46173E-09
	75.00	49.25	-4.56654E-08
	137.00	49.25	1.01697E-09
	141.25	49.25	1.57046E-09
	210.50	49.25	3.41511E-10
	283.25	49.25	1.14196E-09
	350.25	49.25	5.01316E-10

GAS	HOURS	TEMP	OUTGASSING RATE
C2H6	2.00	49.25	7.23769E-08
	20.50	49.25	1.99923E-08
	31.00	49.25	1.47132E-08
	46.00	49.25	9.85088E-09
	46.75	49.25	-2.53227E-08
	63.25	49.25	6.21619E-09
	75.00	49.25	7.48832E-08
	137.00	49.25	-2.32443E-09
	141.25	49.25	1.67405E-09
	210.50	49.25	1.92667E-09
	283.25	49.25	1.26788E-09
	350.25	49.25	6.82915E-10

GAS	HOURS	TEMP	OUTGASSING RATE
C3H8	2.00	49.25	3.21609E-06
	20.50	49.25	1.17645E-08
	31.00	49.25	3.33914E-09
	46.00	49.25	1.71731E-09
	46.75	49.25	6.33891E-09
	63.25	49.25	1.66030E-09
	75.00	49.25	-1.14425E-08
	137.00	49.25	3.78615E-09
	141.25	49.25	4.48785E-11
	210.50	49.25	-5.60622E-11
	283.25	49.25	2.64007E-10
	350.25	49.25	1.45707E-10

GAS	HOURS	TEMP	OUTGASSING RATE
HYDROCARBONS	2.00	49.25	-2.03418E-08
	20.50	49.25	-7.53860E-09
	31.00	49.25	3.96796E-08
	46.00	49.25	3.56402E-08
	46.75	49.25	2.71061E-08
	62.25	49.25	1.93610E-08
	75.00	49.25	2.96972E-08
	137.00	49.25	3.76421E-08
	141.25	49.25	1.23864E-08
	210.50	49.25	7.64177E-09
	283.25	49.25	8.51788E-09
	350.25	49.25	4.88510E-09

GAS IS GAGE P1

POWER $Y=A \cdot X^B$ WITH $A = 0.31595E-03$ AND $B = -0.12029E 01$

USING THE MODEL $\text{LOG}(Y) = \text{ALPHA} + B \cdot (\text{LOG}(X) - \text{XBAR})$ WHERE $\text{XBAR} = \text{MEAN VALUE OF LOG}(X(I))$ AND $\text{ALPHA} = \text{LOG } A + B \cdot \text{XBAR}$,
 $\text{ALPHA} = -0.13073E 02$ CONFIDENCE LIMIT ON ALPHA = $0.52332E-01$ CONFIDENCE LIMIT ON B = $0.68519E-01$

INDEXES CORRELATION COEFFICIENT = $-0.99694E 00$ CORRELATION OF DETERMINATION = $0.99390E 00$

X	Y	Y CALC.	DIFFER.	PCT DIFF.	LOG OF Y	CONFIDENCE LIMIT ON LOG Y
2.00	1.4118E-04	1.3725E-04	-2.9929E-05	-1.4800E 01	-8.8937E 00	3.9872E-01
20.50	8.6727E-06	8.3502E-06	-3.2249E-07	-3.7000E 00	-1.1493E 01	3.2936E-01
31.00	4.7444E-06	5.0775E-06	3.1310E-07	6.6000E 00	-1.2191E 01	3.2377E-01
46.00	2.7257E-06	3.1585E-06	4.3273E-07	1.5900E 01	-1.2665E 01	3.2069E-01
46.75	2.7598E-06	3.0976E-06	3.3809E-07	1.2300E 01	-1.2685E 01	3.2061E-01
63.25	2.1062E-06	2.1533E-06	4.7083E-08	2.2000E 00	-1.3049E 01	3.1985E-01
75.00	1.5543E-06	1.7542E-06	1.9992E-07	1.2900E 01	-1.3253E 01	3.2001E-01
137.00	6.9269E-07	8.4085E-07	1.5715E-07	2.2700E 01	-1.3978E 01	3.2397E-01
141.25	8.6727E-07	8.1018E-07	-4.8091E-08	-5.5000E 00	-1.4015E 01	3.2431E-01
210.50	5.8231E-07	5.0604E-07	-7.5269E-08	-1.2900E 01	-1.4495E 01	3.2994E-01
283.25	4.3364E-07	3.5472E-07	-7.8919E-08	-1.8200E 01	-1.4852E 01	3.3551E-01
350.25	2.9735E-07	2.7477E-07	-2.2584E-08	-7.6000E 00	-1.5107E 01	3.4019E-01

GAS IS TOTAL

POWER $Y=A \cdot X^B$ WITH $A = 0.28180E-02$ AND $B = -0.58854E 00$

USING THE MODEL $\text{LOG}(Y)=\text{ALPHA}+B \cdot (\text{LOG}(X)-\text{XBAR})$ WHERE $\text{XBAR}=\text{MEAN VALUE OF LOG}(X(I))$ AND $\text{ALPHA} = \text{LOG } A + B \cdot \text{XBAR}$.
 $\text{ALPHA} = -0.12294E 02$ CONFIDENCE LIMIT ON ALPHA = $0.20808E 00$ CONFIDENCE LIMIT ON B = $0.15441E 00$

INDEXES CORRELATION COEFFICIENT = $-0.97779E 00$ CORRELATION OF DETERMINATION = $0.95606E 00$

X	Y	Y CALC.	DIFFER.	PCT DIFF.	LOG OF Y	CONFIDENCE LIMIT ON LOG Y
2.00	2.2563E-04	1.4202E-04	-8.3606E-05	-2.7100E 01	-8.8595E 00	8.9855E-01
20.50	1.4869E-05	1.4230E-05	-6.3824E-07	-4.3000E 00	-1.1160E 01	7.4225E-01
31.00	6.4505E-06	9.4551E-06	2.8047E-06	4.2200E 01	-1.1569E 01	7.2965E-01
46.00	4.9357E-06	6.4008E-06	1.4651E-06	2.9700E 01	-1.1959E 01	7.2270E-01
46.75	5.1902E-06	6.2993E-06	1.1091E-06	2.1400E 01	-1.1975E 01	7.2253E-01
63.25	4.1451E-06	4.6722E-06	5.2707E-07	1.2700E 01	-1.2274E 01	7.2081E-01
75.00	2.7624E-06	3.9479E-06	1.1855E-06	4.2900E 01	-1.2442E 01	7.2118E-01
137.00	1.8296E-06	2.1762E-06	3.4660E-07	1.8900E 01	-1.3038E 01	7.3011E-01
141.25	2.2244E-06	2.1115E-06	-1.1289E-07	-5.1000E 00	-1.3068E 01	7.3088E-01
210.50	1.5091E-06	1.4233E-06	-8.5726E-08	-5.7000E 00	-1.3463E 01	7.4365E-01
283.25	1.6717E-06	1.0614E-06	-6.1034E-07	-3.6500E 01	-1.3756E 01	7.5611E-01
350.25	1.2634E-06	8.6043E-07	-4.0292E-07	-3.1900E 01	-1.3966E 01	7.6665E-01

GAS IS H

POWER $Y=A \cdot X^B$ WITH $A = 0.56309E-04$ AND $B = -0.71696E 00$

USING THE MODEL $\log(Y)=\alpha+B(\log(X)-\bar{x})$ WHERE $\bar{x}$ =MEAN VALUE OF $\log(X(I))$ AND $\alpha = \log A + B * \bar{x}$,
 $\alpha = -0.12773E 02$ CONFIDENCE LIMIT ON $\alpha = 0.16994E 00$ CONFIDENCE LIMIT ON $B = 0.12611E 00$

INDEXES CORRELATION COEFFICIENT = -0.97208E 00

CORRELATION OF DETERMINATION = 0.94493E 00

X	Y	Y CALC.	DIFFER.	PCT DIFF.	LOG OF Y	CONFIDENCE LIMIT ON LOG Y
2.00	4.8263E-05	3.4257E-05	-1.4006E-05	-2.9000E 01	-1.0282E 01	7.2385E-01
20.50	7.1063E-06	6.4581E-06	-6.4821E-07	-9.1000E 00	-1.1950E 01	6.0620E-01
31.00	3.3266E-06	4.8010E-06	1.4744E-06	4.4300E 01	-1.2247E 01	5.5591E-01
46.00	2.9867E-06	3.6179E-06	6.3115E-07	2.1100E 01	-1.2570E 01	5.9024E-01
46.75	3.1234E-06	3.5762E-06	4.5280E-07	1.4500E 01	-1.2541E 01	5.9009E-01
63.25	2.7191E-06	2.8794E-06	1.6029E-07	5.9000E 00	-1.2758E 01	5.8869E-01
75.00	2.0009E-06	2.5482E-06	5.4748E-07	2.7400E 01	-1.2880E 01	5.8379E-01
137.00	1.3811E-06	1.6544E-06	2.7332E-07	1.9800E 01	-1.3312E 01	5.9629E-01
141.25	1.7456E-06	1.6186E-06	-1.4702E-07	-8.3000E 00	-1.3334E 01	5.9691E-01
210.50	1.1857E-06	1.2159E-06	3.0204E-08	2.5000E 00	-1.3620E 01	6.0727E-01
283.25	1.4542E-06	9.8282E-07	-4.7133E-07	-3.2400E 01	-1.3833E 01	6.1752E-01
350.25	1.1187E-06	6.4405E-07	-2.7461E-07	-2.4500E 01	-1.3995E 01	6.2613E-01

GAS IS HELIUM

POWER $Y=A \cdot X^B$ WITH $A = 0.22867E-09$ AND $B = -0.62743E-01$

USING THE MODEL $\log(Y) = \alpha + B(\log(X) - \bar{\log(X)})$ WHERE $\bar{\log(X)}$ = MEAN VALUE OF $\log(X(I))$ AND $\alpha = \log A + B * \bar{\log(X)}$,
 $\alpha = -0.22102E 02$ CONFIDENCE LIMIT ON $\alpha = 0.25016E-01$ CONFIDENCE LIMIT ON $B = 0.63090E-01$

CORRELATION COEFFICIENT = $-0.60141E 00$ CORRELATION OF DETERMINATION = $0.36169E 00$

INDEXES	X	Y	Y CALC.	DIFFER.	PCT DIFF.	LOG OF Y	CONFIDENCE LIMIT ON LOG Y
	2.00	3.0305E-10	3.1447E-10	1.1421E-11	3.8000E 00	-2.1880E 01	3.6713E-01
	20.50	3.0348E-10	2.7111E-10	-3.2369E-11	-1.0700E 01	-2.2028E 01	3.0327E-01
	31.00	2.5008E-10	2.6406E-10	1.3983E-11	5.6000E 00	-2.2055E 01	2.9812E-01
	46.00	2.6413E-10	2.5750E-10	-6.6266E-12	-2.5000E 00	-2.2080E 01	2.9528E-01
	46.75	2.6740E-10	2.5723E-10	-1.0167E-11	-3.8000E 00	-2.2081E 01	2.9521E-01
	62.25	2.6533E-10	2.5233E-10	-1.2004E-11	-4.5000E 00	-2.2100E 01	2.9451E-01
	75.00	2.4476E-10	2.4960E-10	4.8424E-12	2.0000E 00	-2.2111E 01	2.9466E-01
	137.00	2.0776E-10	2.4020E-10	3.2432E-11	1.5600E 01	-2.2150E 01	2.9831E-01
	141.25	2.4013E-10	2.3973E-10	-2.0397E-11	-7.8000E 00	-2.2152E 01	2.9862E-01
	210.50	1.7466E-10	2.2271E-10	5.4053E-11	3.3800E 01	-2.2177E 01	3.0380E-01
	262.25	2.6013E-10	2.2933E-10	-3.0767E-11	-1.1800E 01	-2.2196E 01	3.0693E-01
	350.25	2.5310E-10	2.2625E-10	-2.6852E-11	-1.0600E 01	-2.2209E 01	3.1323E-01

GAS IS METHANE

POWER $Y=A \cdot X^B$ WITH $A = 0.18228E-06$ AND $B = -0.60775E 00$

USING THE MODEL $\text{LOG}(Y)=\text{ALPHA}+B \cdot (\text{LOG}(X)-\text{XBAR})$ WHERE XBAR =MEAN VALUE OF $\text{LOG}(X(I))$ AND $\text{ALPHA} = \text{LOG } A + B \cdot \text{XBAR}$,
 $\text{ALPHA} = -0.18206E 02$ CONFIDENCE LIMIT ON ALPHA = $0.28308E 00$ CONFIDENCE LIMIT ON B = $0.48301E 00$

INDEXES CORRELATION COEFFICIENT = $-0.7155CE 00$ CORRELATION OF DETERMINATION = $0.51104E 00$

X	Y	Y CALC.	DIFFER.	PCT DIFF.	LOG OF Y	CONFIDENCE LIMIT ON LOG Y
31.00	1.8913E-08	2.3432E-08	4.5156E-09	2.3500E 01	-1.7569E 01	1.3425E 00
46.00	2.1546E-08	1.8435E-08	-3.1108E-09	-1.4400E 01	-1.7809E 01	1.2719E 00
46.75	1.9773E-08	1.8255E-08	-1.5180E-09	-2.8000E 00	-1.7819E 01	1.2696E 00
63.25	1.0023E-08	1.5191E-08	5.1684E-09	5.1600E 01	-1.8003E 01	1.2337E 00
75.00	1.1022E-08	1.2697E-08	1.7750E-09	1.4000E 01	-1.8106E 01	1.2208E 00
127.00	3.5164E-08	9.4972E-09	-2.5666E-08	-7.3000E 01	-1.8472E 01	1.2195E 00
141.25	9.0962E-09	9.3225E-09	2.2636E-10	2.5000E 00	-1.8401E 01	1.2213E 00
210.50	5.7297E-09	7.3153E-09	1.5856E-09	2.7700E 01	-1.8733E 01	1.2605E 00
283.25	5.8478E-09	6.1078E-09	2.6298E-10	4.5000E 00	-1.8914E 01	1.3075E 00
350.25	3.5504E-09	5.3684E-09	1.8080E-09	5.0000E 01	-1.9042E 01	1.3405E 00

GAS IS WATER VAPOR

POWER $Y=A \cdot X^B$ WITH $A = 0.10832E-02$ AND $B = -0.15173E 01$

USING THE MODEL $\log(Y)=\alpha+B(\log(X)-\bar{X})$ WHERE $\bar{X}$ IS MEAN VALUE OF $\log(X)$ AND $\alpha = \log A + B * \bar{X}$,
 $\alpha = -0.14818E 02$ CONFIDENCE LIMIT ON $\alpha = 0.21406E 00$ CONFIDENCE LIMIT ON $B = 0.15885E 00$

INDEXES CORRELATION COEFFICIENT = $-0.9361E 00$ CORRELATION OF DETERMINATION = $0.92726E 00$

X	Y	Y CALC.	DIFFER.	PCT DIFF.	LOG OF Y	CONFIDENCE LIMIT ON LOG Y
2.00	1.6268E-04	2.8678E-04	1.2410E-04	7.6300E 01	-8.1568E 00	9.2437E-01
20.50	4.9649E-06	3.3087E-06	-1.5582E-06	-3.2000E 01	-1.2619E 01	7.6258E-01
31.00	1.7692E-06	1.4972E-06	-2.7200E-07	-1.5400E 01	-1.3412E 01	7.5062E-01
46.00	8.8853E-07	7.0253E-07	-1.8600E-07	-2.1800E 01	-1.4169E 01	7.4247E-01
46.75	5.3563E-07	6.8108E-07	-2.5456E-07	-2.7200E 01	-1.4200E 01	7.4329E-01
53.25	5.4242E-07	3.8150E-07	-1.6192E-07	-2.9800E 01	-1.4779E 01	7.4153E-01
75.00	2.4504E-07	2.7517E-07	3.0125E-08	1.2300E 01	-1.5106E 01	7.4191E-01
137.00	8.7369E-08	8.6481E-08	-8.8820E-10	-8.0000E-01	-1.6281E 01	7.5109E-01
141.25	8.4774E-08	8.1749E-08	-3.0247E-09	-3.6000E 00	-1.6320E 01	7.5188E-01
210.50	3.0233E-08	3.8043E-08	7.8100E-09	2.5800E 01	-1.7085E 01	7.6492E-01
282.25	1.6218E-08	2.1533E-08	5.3145E-09	3.2800E 01	-1.7654E 01	7.7784E-01
350.25	1.0425E-08	1.4332E-08	3.9067E-09	3.7500E 01	-1.8061E 01	7.8868E-01

GAS IS NITROGEN

POWER $Y=A \cdot X^B$ WITH $A = 0.19097E-05$ AND $B = -0.11869E 01$

USING THE MODEL $LOG(Y)=ALPHA+B*(LOG(X)-XBAR)$ WHERE $XBAR=$ MEAN VALUE OF $LOG(X(I))$ AND $ALPHA = LOG A + B * XBAR$,
 $ALPHA = -0.17902E 02$ CONFIDENCE LIMIT ON $ALPHA = 0.37753E 00$ CONFIDENCE LIMIT ON $B = 0.25661E 00$

INDEXES CORRELATION COEFFICIENT = $-0.97052E 00$ CORRELATION OF DETERMINATION = $0.94193E 00$

X	Y	Y CALC.	DIFFER.	PCT DIFF.	LOG OF Y	CONFIDENCE LIMIT ON LOG Y
2.00	5.1029E-07	8.3684E-07	3.2656E-07	6.4400E 01	-1.3991E 01	1.4140E 00
20.50	1.5460E-07	5.2975E-08	-1.0163E-07	-6.5700E 01	-1.6753E 01	1.1506E 00
31.00	3.2534E-08	3.2426E-08	-1.0841E-10	-3.0000E-01	-1.7244E 01	1.1415E 00
46.00	1.3776E-08	2.0299E-08	6.5225E-09	4.7400E 01	-1.7713E 01	1.1332E 00
63.25	1.6866E-08	1.3910E-08	-2.9559E-09	-1.7600E 01	-1.8091E 01	1.1333E 00
75.00	1.2945E-08	1.1363E-08	-1.5820E-09	-1.2200E 01	-1.8293E 01	1.1357E 00
141.25	4.3513E-09	5.3602E-09	1.0089E-09	2.3200E 01	-1.9044E 01	1.1592E 00
282.25	1.9937E-09	2.3471E-09	3.5337E-10	1.7700E 01	-1.9870E 01	1.2100E 00
350.25	1.5843E-09	1.8242E-09	2.3692E-10	1.5100E 01	-2.0122E 01	1.2303E 00

GAS IS CO

POWER $Y=A**X**P$ WITH $A = 0.29162E-04$ AND $P = -0.66733E 00$

USING THE MODEL $LOG(Y)=ALPHA+B*(LOG(X)-XBAR)$ WHERE $XBAR=$ MEAN VALUE OF $LOG(X(I))$ AND $ALPHA = LOG A + P * XBAR$,
 $ALPHA = -0.14509E 02$ CONFIDENCE LIMIT ON $ALPHA = 0.22473E 00$ CONFIDENCE LIMIT ON $B = 0.17048E 00$

INDEXES CORRELATION COEFFICIENT = $-0.97361E 00$ CORRELATION OF DETERMINATION = $0.94792E 00$

X	Y	Y CALC.	DIFFER.	PCT DIFF.	LOG OF Y	CONFIDENCE LIMIT ON LOG Y
2.00	1.4474E-05	1.4409E-05	1.2443E-07	5.0000E-01	-1.1134E 01	9.9203E-01
20.50	1.6469E-06	1.4341E-06	-2.1256E-07	-1.2900E 01	-1.3455E 01	8.1947E-01
31.00	8.4218E-07	9.4042E-07	8.7238E-08	1.0100E 01	-1.3867E 01	8.0556E-01
46.00	5.6747E-07	6.4050E-07	7.2529E-08	1.2800E 01	-1.4261E 01	7.9780E-01
46.75	1.2387E-06	6.3025E-07	-6.0842E-07	-4.9100E 01	-1.4277E 01	7.9770E-01
63.25	4.8325E-07	4.6822E-07	-1.7030E-08	-3.5000E 00	-1.4579E 01	7.9580E-01
75.00	1.9196E-07	3.9736E-07	2.0140E-07	1.0400E 02	-1.4740E 01	7.9621E-01
137.00	1.4970E-07	2.1566E-07	4.5980E-08	2.7100E 01	-1.5349E 01	8.0607E-01
141.25	1.8476E-07	2.0922E-07	2.4440E-08	1.3200E 01	-1.5390E 01	8.0691E-01
210.50	1.7162E-07	1.4054E-07	-3.1080E-08	-1.8100E 01	-1.5778E 01	8.2091E-01
283.25	1.3472E-07	1.0453E-07	-2.0698E-08	-2.2100E 01	-1.6074E 01	8.3477E-01
350.25	8.5238E-08	8.4578E-08	-6.5900E-10	-8.0000E-01	-1.6286E 01	8.4641E-01

GAS IS OXYGEN

POWER $Y=A \cdot X^B$ WITH $A = 0.52863E-05$ AND $B = -0.14759E 01$

USING THE MODEL $LOG(Y)=ALPHA+B*(LOG(X)-XBAR)$ WHERE $XBAR=$ MEAN VALUE OF $LOG(X(I))$ AND $ALPHA = LOG A + B * XBAR$,
 $ALPHA = -0.19318E 02$ CONFIDENCE LIMIT ON $ALPHA = 0.34868E 00$ CONFIDENCE LIMIT ON $B = 0.25876E 00$

INDEXES	CORRELATION COEFFICIENT = -0.97244E 00	CORRELATION OF DETERMINATION = 0.94565E 00				
X	Y	Y CALC.	DIFFER.	PCT DIFF.	LOG OF Y	CONFIDENCE LIMIT ON LOG Y
2.00	7.1334E-07	1.8952E-06	1.1819E-06	1.6470E 02	-1.3176E 01	1.5057E 00
20.50	1.1507E-07	6.0521E-08	-5.4546E-08	-4.7400E 01	-1.6620E 01	1.2438E 00
31.00	5.0515E-08	3.2818E-08	-2.1697E-08	-3.9800E 01	-1.7232E 01	1.2227E 00
46.00	2.6644E-08	1.8201E-08	-8.3434E-09	-3.1300E 01	-1.7816E 01	1.2111E 00
46.75	2.5772E-08	1.7868E-08	-7.9041E-09	-3.0700E 01	-1.7840E 01	1.2108E 00
63.25	1.5166E-08	1.1423E-08	-3.7427E-09	-2.4700E 01	-1.8289E 01	1.2079E 00
75.00	1.1312E-08	8.8773E-09	-2.4352E-09	-2.1500E 01	-1.8540E 01	1.2085E 00
137.00	2.7981E-09	3.6396E-09	8.4149E-10	3.0100E 01	-1.9431E 01	1.2235E 00
141.25	3.8166E-09	3.4787E-09	-3.3789E-10	-8.9000E 00	-1.9477E 01	1.2248E 00
210.50	1.6056E-09	1.9276E-09	3.2100E-10	2.0100E 01	-2.0067E 01	1.2460E 00
283.25	7.4243E-10	1.2423E-09	4.6984E-10	6.7200E 01	-2.0506E 01	1.2670E 00
350.25	5.1172E-10	9.0734E-10	3.9561E-10	7.7200E 01	-2.0820E 01	1.2847E 00

GAS IS ARGON

POWER $Y=A \times X^B$ WITH $A = 0.10525E-06$ AND $B = -0.12105E 01$

USING THE MODEL $\text{LOG}(Y)=\text{ALPHA}+B \times (\text{LOG}(X)-\text{XBAR})$ WHERE $\text{XBAR}=\text{MEAN VALUE OF LOG}(X(I))$ AND $\text{ALPHA} = \text{LOG } A + B \times \text{XBAR}$,
 $\text{ALPHA} = -0.21112E 02$ CONFIDENCE LIMIT ON ALPHA = $0.40614E 00$ CONFIDENCE LIMIT ON B = $0.30139E 00$

INDEXES CORRELATION COEFFICIENT = $-0.94647E 00$ CORRELATION OF DETERMINATION = $0.89581E 00$

X	Y	Y CALC.	DIFFER.	PCT DIFF.	LOG OF Y	CONFIDENCE LIMIT ON LOG Y
2.00	$8.4749E-08$	$4.5478E-08$	$-3.9271E-08$	$-4.6300E 01$	$-1.6906E 01$	$1.7538E 00$
20.50	$3.6070E-09$	$2.7183E-09$	$-8.8873E-10$	$-2.4600E 01$	$-1.9723E 01$	$1.4488E 00$
31.00	$1.2739E-09$	$1.6477E-09$	$4.2381E-10$	$3.4600E 01$	$-2.0224E 01$	$1.4242E 00$
46.00	$6.6479E-10$	$1.0219E-09$	$3.5708E-10$	$5.3700E 01$	$-2.0702E 01$	$1.4106E 00$
46.75	$7.4781E-10$	$1.0021E-09$	$2.5425E-10$	$3.4000E 01$	$-2.0721E 01$	$1.4103E 00$
62.25	$4.0811E-10$	$6.9499E-10$	$2.8688E-10$	$7.0300E 01$	$-2.1027E 01$	$1.4069E 00$
75.00	$4.4491E-10$	$5.6545E-10$	$1.2054E-10$	$2.7100E 01$	$-2.1293E 01$	$1.4076E 00$
137.00	$1.4526E-10$	$2.7268E-10$	$1.2742E-10$	$8.7700E 01$	$-2.2023E 01$	$1.4251E 00$
141.25	$2.3643E-10$	$2.6278E-10$	$2.6354E-11$	$1.1100E 01$	$-2.2060E 01$	$1.4265E 00$
210.50	$1.2211E-10$	$1.6212E-10$	$4.0014E-11$	$3.2800E 01$	$-2.2542E 01$	$1.4513E 00$
283.25	$4.1830E-10$	$1.1319E-10$	$-3.0511E-10$	$-7.2500E 01$	$-2.2902E 01$	$1.4758E 00$
350.25	$1.5926E-10$	$8.7533E-11$	$-7.1724E-11$	$-4.5000E 01$	$-2.3159E 01$	$1.4964E 00$

GAS IS CO2

POWER $Y=A \cdot X^B$ WITH $A = 0.23905E-04$ AND $B = -0.10436E 01$

USING THE MODEL $\log(Y) = \text{ALPHA} + B \cdot (\log(X) - \bar{X})$ WHERE $\bar{X}$ = MEAN VALUE OF $\log(X(I))$ AND $\text{ALPHA} = \log A + B \cdot \bar{X}$,
 $\text{ALPHA} = -0.15320E 02$ CONFIDENCE LIMIT ON $\text{ALPHA} = 0.11308E 00$ CONFIDENCE LIMIT ON $B = 0.12772E 00$

INDEXES		CORRELATION COEFFICIENT = -0.98751E 00			CORRELATION OF DETERMINATION = 0.97518E 00		
X	Y	Y CALC.	DIFFER.	PCT DIFF.	LOG OF Y	CONFIDENCE LIMIT ON LOG Y	
20.50	9.8270E-07	1.0223E-C6	5.9598E-08	4.0000E 00	-1.3793E 01	4.1902E-01	
31.00	5.6423E-07	6.6396E-07	9.5731E-08	1.7700E 01	-1.4225E 01	3.9829E-01	
46.00	4.0550E-07	4.3982E-07	3.4370E-08	8.5000E 00	-1.4637E 01	3.8425E-01	
46.75	4.5980E-07	4.3246E-C7	-2.7335E-08	-5.9000E 00	-1.4654E 01	3.8381E-01	
63.25	3.4731E-07	3.1546E-07	-3.1844E-08	-9.2000E 00	-1.4969E 01	3.7749E-01	
75.00	2.6997E-07	2.6407E-C7	-5.8995E-09	-2.2000E 00	-1.5147E 01	3.7564E-01	
137.00	1.5418E-07	1.4082E-C7	-1.3361E-08	-8.7000E 00	-1.5776E 01	3.7917E-01	
141.25	1.6823E-07	1.3640E-C7	-3.1824E-08	-1.8900E 01	-1.5808E 01	3.7976E-01	
210.50	1.1220E-07	8.9951E-C8	-2.2246E-08	-1.9800E 01	-1.6224E 01	3.9102E-01	
263.25	5.5191E-08	6.5989E-C8	1.0758E-08	1.9600E 01	-1.6524E 01	4.0339E-01	
350.25	4.1648E-08	5.2875E-C8	1.1226E-08	2.7000E 01	-1.6755E 01	4.1414E-01	

GAS IS C2H4

POWER $Y=A \cdot X^B$ WITH $A = 0.33025E-06$ AND $B = -0.1126E 01$

USING THE MODEL $\text{LOG}(Y) = \text{ALPHA} + B \cdot (\text{LOG}(X) - \text{XBAR})$ WHERE $\text{XBAR} = \text{MEAN VALUE OF LOG}(X(I))$ AND $\text{ALPHA} = \text{LOG } A + B \cdot \text{XBAR}$,
 $\text{ALPHA} = -0.19904E 02$ CONFIDENCE LIMIT ON ALPHA = $0.66462E 00$ CONFIDENCE LIMIT ON B = $0.71705E 00$

INDEXES CORRELATION COEFFICIENT = $-0.78935E 00$

CORRELATION OF DETERMINATION = $0.62150E 00$

X	Y	Y CALC.	DIFFER.	PCT DIFF.	LOG OF Y	CONFIDENCE LIMIT ON LOG Y
20.50	1.7150E-08	1.0582E-08	-6.1675E-09	-3.6000E 01	-1.8327E 01	2.3543E 00
31.00	2.7148E-08	6.8014E-09	4.1766E-09	1.5380E 02	-1.8743E 01	2.2364E 00
46.00	2.5261E-08	4.6174E-09	1.8914E-09	7.4900E 01	-1.9238E 01	2.1561E 00
46.75	2.7317E-08	4.3377E-09	-2.2980E-08	-8.4100E 01	-1.9256E 01	2.1536E 00
63.25	1.4617E-09	3.0855E-09	1.6238E-09	1.1110E 02	-1.9597E 01	2.1169E 00
137.00	1.0170E-09	1.2915E-09	2.7451E-10	2.7000E 01	-2.0467E 01	2.1232E 00
141.25	1.5705E-09	1.2478E-09	-3.2268E-10	-2.0500E 01	-2.0502E 01	2.1264E 00
210.50	3.4161E-10	7.9597E-10	4.5446E-10	1.3310E 02	-2.0951E 01	2.1882E 00
283.25	1.1420E-09	5.6568E-10	-5.7229E-10	-5.0100E 01	-2.1284E 01	2.2567E 00
350.25	5.0132E-10	4.4846E-10	-5.2842E-11	-1.0500E 01	-2.1525E 01	2.3165E 00

GAS IS C2H6

POWER $Y=A \cdot X^B$ WITH $A = 0.27142E-06$ AND $B = -0.88767E 00$

USING THE MODEL $\log(Y) = \text{ALPHA} + B \cdot (\log(X) - \bar{X})$ WHERE $\bar{X}$ = MEAN VALUE OF $\log(X(I))$ AND $\text{ALPHA} = \log A + B \cdot \bar{X}$,
 $\text{ALPHA} = -0.18781E 02$ CONFIDENCE LIMIT ON $\text{ALPHA} = 0.74167E 00$ CONFIDENCE LIMIT ON $B = 0.51057E 00$

INDEXES CORRELATION COEFFICIENT = -0.81714E 00

CORRELATION OF DETERMINATION = 0.66773E 00

X	Y	Y CALC.	DIFFER.	PCT DIFF.	LOG OF Y	CONFIDENCE LIMIT ON LOG Y
2.00	7.2377E-09	1.4670E-07	7.4223E-08	1.0270E 02	-1.5735E 01	2.9275E 00
20.50	1.0002E-08	1.8588E-08	-1.4038E-09	-7.0000E 00	-1.7801E 01	2.4122E 00
31.00	1.4713E-08	1.2877E-08	-1.8264E-09	-1.2500E 01	-1.8168E 01	2.3717E 00
46.00	9.8500E-09	9.0713E-09	-7.7968E-10	-7.9000E 00	-1.8518E 01	2.3502E 00
63.25	6.2167E-09	6.8275E-09	6.2132E-10	1.0000E 01	-1.8801E 01	2.3434E 00
75.00	7.4883E-09	5.8778E-09	-6.9006E-09	-9.2200E 01	-1.8952E 01	2.3474E 00
141.25	1.6750E-09	3.3509E-09	1.6760E-09	1.0010E 02	-1.9514E 01	2.3830E 00
210.50	1.0257E-09	2.2516E-09	4.2455E-10	2.2100E 01	-1.9868E 01	2.4273E 00
283.25	1.2679E-09	1.8060E-09	5.3900E-10	4.2500E 01	-2.0132E 01	2.4707E 00
350.25	6.2292E-10	1.4965E-09	8.1259E-10	1.1010E 02	-2.0320E 01	2.5069E 00

GAS IS C3H8

POWER $Y=A \times X^B$ WITH $A = 0.51192E-05$ AND $B = -0.1878PF 01$

USING THE MODEL $\log(Y) = \text{ALPHA} + B * (\log(X) - \text{XBAR})$ WHERE $\text{XBAR} = \text{MEAN VALUE OF } \log(X(I))$ AND $\text{ALPHA} = \log A + B * \text{XBAR}$.
 $\text{ALPHA} = -0.19762F 02$ CONFIDENCE LIMIT ON ALPHA = $0.53290E 00$ CONFIDENCE LIMIT ON B = $0.65650E 00$

INDEXES CORRELATION COEFFICIENT = $-0.91915E 00$ CORRELATION OF DETERMINATION = $0.84484E 00$

X	Y	Y CALC.	DIFFER.	PCT DIFF.	LOG OF Y	CONFIDENCE LIMIT ON LOG Y
2.00	3.2161E-06	1.3919E-06	-1.8242E-06	-5.6700E 01	-1.3485E 01	3.6762E 00
20.50	1.1765E-08	1.7564E-08	5.7904E-09	4.9300E 01	-1.7857E 01	3.0243E 00
31.00	3.3392E-09	8.0756E-09	4.7365E-09	1.4180E 02	-1.8634E 01	2.9763E 00
46.00	1.7173E-09	3.8473E-09	2.1299E-09	1.2400E 02	-1.9376E 01	2.9532E 00
46.75	6.3399E-09	3.7321E-09	-2.6068E-09	-4.1100E 01	-1.9406E 01	2.9527E 00
63.25	1.6603E-09	2.1150E-09	4.5465E-10	2.7400E 01	-1.9974E 01	2.9510E 00
137.00	3.7862E-09	4.0505E-10	-3.2911E-09	-8.6900E 01	-2.1424E 01	3.0068E 00
141.25	4.4870E-11	4.6744E-10	4.2256E-10	9.4160E 02	-2.1484E 01	3.0108E 00
283.25	2.5401E-10	1.2647E-10	-1.3754E-10	-5.2100E 01	-2.2701E 01	3.1342E 00
350.25	1.4537E-10	8.4865E-11	-6.0506E-11	-4.1600E 01	-2.3190E 01	3.1839E 00

GAS IS HYDROCARBONS

POWER $Y=A \cdot X^B$ WITH $A = 0.65026E-06$ AND $B = -0.77585E 00$

USING THE MODEL $\log(Y) = \alpha + B(\log(X) - \bar{\log(X)})$ WHERE $\bar{\log(X)}$ = MEAN VALUE OF $\log(X(I))$ AND $\alpha = \log A + B * \bar{\log(X)}$,
 $\alpha = -0.17828E 02$ CONFIDENCE LIMIT ON $\alpha = 0.30004E 00$ CONFIDENCE LIMIT ON $B = 0.37901E 00$

INDEXES CORRELATION COEFFICIENT = $-0.8779CE 00$ CORRELATION COEFFICIENT OF DETERMINATION = $0.73509E 00$

X	Y	Y CALC.	DIFF.	PCT DIFF.	LOG OF Y	CONFIDENCE LIMIT ON LOG Y
31.00	3.9680E-08	4.5292E-08	5.6120E-09	1.4100E 01	-1.6910E 01	1.0515E 00
46.00	3.5641E-08	3.2346E-08	-2.2945E-09	-6.4000E 00	-1.7216E 01	9.9621E-01
46.75	2.7106E-08	3.2030E-08	5.8242E-09	2.1500E 01	-1.7229E 01	9.9434E-01
63.25	1.9361E-08	2.6046E-08	6.6849E-09	3.4500E 01	-1.7463E 01	9.4629E-01
75.00	2.9698E-08	2.2821E-08	-6.9769E-09	-2.3200E 01	-1.7596E 01	9.5617E-01
137.00	3.7642E-08	1.4300E-08	-2.3342E-08	-6.2000E 01	-1.8063E 01	9.5519E-01
141.25	1.7386E-08	1.3665E-08	1.5782E-09	1.2700E 01	-1.8087E 01	9.5658E-01
210.50	7.9418E-09	1.0247E-08	2.3057E-09	2.9000E 01	-1.8396E 01	9.8726E-01
283.25	8.5176E-09	8.1292E-09	-3.7878E-10	-4.4000E 00	-1.8627E 01	1.0241E 00
350.25	4.8892E-09	6.6031E-09	2.0139E-09	4.1200E 01	-1.8791E 01	1.0570E 00

GAS IS GAGE P1

TOTAL OUTGASSING (Q), INTEGRATION OF $Y=A \times X^B$
 A = 0.31595E-03 B = -0.12029E 01

INITIAL TIME HOURS	FINAL TIME HOURS	OUTGASSING(Q) TORR-LITERS	TOTAL Q (ALL PREVIOUS GASES)	OUTGASSING RATE TORR-LITERS/SEC
0.1	0.1	0.0	0.0	
0.1	0.2	11.73473E-01	0.0	
0.1	0.3	17.87178E-01	0.0	
0.1	0.4	21.92580E-01	0.0	
0.1	0.5	24.91832E-01	0.0	
0.1	0.6	27.26165E-01	0.0	
0.1	0.7	29.17639E-01	0.0	
0.1	0.8	30.78728E-01	0.0	
0.1	0.9	32.17239E-01	0.0	
0.1	1.0	33.38368E-01	0.0	31.59505E-05
0.1	2.0	40.73835E-01	0.0	
0.1	4.0	47.12809E-01	0.0	
0.1	6.0	50.46980E-01	0.0	
0.1	8.0	52.67647E-01	0.0	
0.1	10.0	54.30676E-01	0.0	19.80207E-06
0.1	20.0	58.91623E-01	0.0	
0.1	40.0	62.92096E-01	0.0	
0.1	60.0	65.01539E-01	0.0	
0.1	80.0	66.40030E-01	0.0	
0.1	100.0	67.42023E-01	0.0	12.41086E-07
0.1	200.0	70.30917E-01	0.0	
0.1	400.0	72.81914E-01	0.0	
0.1	600.0	74.13177E-01	0.0	
0.1	800.0	74.99978E-01	0.0	
0.1	1000.0	75.62899E-01	0.0	77.78453E-08
0.1	2000.0	77.44966E-01	0.0	
0.1	4000.0	79.02290E-01	0.0	
0.1	6000.0	79.84550E-01	0.0	
0.1	8000.0	80.38945E-01	0.0	
0.1	10000.0	80.79014E-01	0.0	48.75112E-10
1.0	2000.0	44.06601E-01	0.0	
1.0	4000.0	45.67911E-01	0.0	
1.0	6000.0	46.46182E-01	0.0	
1.0	8000.0	47.00582E-01	0.0	
1.0	10000.0	47.40645E-01	0.0	48.75112E-10
10.0	2000.0	23.14292E-01	0.0	
10.0	4000.0	24.71603E-01	0.0	
10.0	6000.0	25.53873E-01	0.0	
10.0	8000.0	26.08274E-01	0.0	
10.0	10000.0	26.48336E-01	0.0	48.75112E-10
100.0	2000.0	10.02946E-01	0.0	
100.0	4000.0	11.60255E-01	0.0	
100.0	6000.0	12.42527E-01	0.0	
100.0	8000.0	12.96926E-01	0.0	
100.0	10000.0	13.36990E-01	0.0	48.75112E-10

GAS IS TOTAL

TOTAL OUTGASSING (Q), INTEGRATION OF $Y=A \times X^B$
 A = 0.28180E-03 B = -0.58854E 00

INITIAL TIME HOURS	FINAL TIME HOURS	OUTGASSING(Q) TORR-LITERS	TOTAL Q (ALL PREVIOUS GASES)	OUTGASSING RATE TORR-LITERS/SEC
0.1	0.1	0.0	0.0	
0.1	0.2	68.75567E-02	0.0	
0.1	0.3	10.92255E-01	0.0	
0.1	0.4	13.80682E-01	0.0	
0.1	0.5	16.04974E-01	0.0	
0.1	0.6	17.88665E-01	0.0	
0.1	0.7	19.44271E-01	0.0	
0.1	0.8	20.79288E-01	0.0	
0.1	0.9	21.98551E-01	0.0	
0.1	1.0	22.05372E-01	0.0	28.17996E-05
0.1	2.0	20.11387E-01	0.0	
0.1	4.0	27.22973E-01	0.0	
0.1	6.0	41.41836E-01	0.0	
0.1	8.0	44.40217E-01	0.0	
0.1	10.0	46.72403E-01	0.0	28.93340E-05
0.1	20.0	52.97246E-01	0.0	
0.1	40.0	61.27913E-01	0.0	
0.1	60.0	65.58006E-01	0.0	
0.1	80.0	68.64323E-01	0.0	
0.1	100.0	71.02673E-01	0.0	29.70696E-07
0.1	200.0	78.46923E-01	0.0	
0.1	400.0	85.97106E-01	0.0	
0.1	600.0	90.38680E-01	0.0	
0.1	800.0	93.53272E-01	0.0	
0.1	1000.0	95.97952E-01	0.0	30.50118E-08
0.1	2000.0	10.35206E 00	0.0	
0.1	4000.0	11.13232E 00	0.0	
0.1	6000.0	11.58572E 00	0.0	
0.1	8000.0	11.90867E 00	0.0	
0.1	10000.0	12.15994E 00	0.0	31.31669E-09
1.0	2000.0	80.56682E-01	0.0	
1.0	4000.0	88.26948E-01	0.0	
1.0	6000.0	92.80242E-01	0.0	
1.0	8000.0	96.03263E-01	0.0	
1.0	10000.0	98.54561E-01	0.0	31.31669E-09
10.0	2000.0	56.89651E-01	0.0	
10.0	4000.0	64.59618E-01	0.0	
10.0	6000.0	69.13214E-01	0.0	
10.0	8000.0	72.36744E-01	0.0	
10.0	10000.0	74.87522E-01	0.0	31.31669E-09
100.0	2000.0	32.59282E-01	0.0	
100.0	4000.0	40.29650E-01	0.0	
100.0	6000.0	44.83045E-01	0.0	
100.0	8000.0	48.05994E-01	0.0	
100.0	10000.0	50.57262E-01	0.0	31.31669E-09

GAS IS H

TOTAL OUTGASSING (Q), INTEGRATION OF $Y=A \times X^B$
 $A = 0.56309E-04$ $B = -0.71696E-00$

INITIAL TIME HOURS	FINAL TIME HOURS	OUTGASSING(Q) TORR-LITERS	TOTAL Q (ALL PREVIOUS GASES)	OUTGASSING RATE TORR-LITERS/SEC
0.1	0.1	0.0	0.0	
0.1	0.2	80.90323E-03	80.90323E-03	
0.1	0.3	13.61311E-02	13.61311E-02	
0.1	0.4	17.93426E-02	17.93426E-02	
0.1	0.5	21.53691E-02	21.53691E-02	
0.1	0.6	24.65416E-02	24.65416E-02	
0.1	0.7	27.41820E-02	27.41820E-02	
0.1	0.8	29.91197E-02	29.91197E-02	
0.1	0.9	32.19122E-02	32.19122E-02	
0.1	1.0	34.29549E-02	34.29549E-02	56.30936E-06
0.1	2.0	45.81561E-02	45.81561E-02	
0.1	4.0	68.70868E-02	68.70868E-02	
0.1	6.0	81.60306E-02	81.60306E-02	
0.1	8.0	91.69196E-02	91.69196E-02	
0.1	10.0	10.01034E-01	10.01034E-01	10.80494E-06
0.1	20.0	12.98917E-01	12.98917E-01	
0.1	40.0	16.61369E-01	16.61369E-01	
0.1	60.0	19.08795E-01	19.08795E-01	
0.1	80.0	21.02386E-01	21.02386E-01	
0.1	100.0	22.63787E-01	22.63787E-01	20.73302E-07
0.1	200.0	28.35382E-01	28.35382E-01	
0.1	400.0	35.30874E-01	35.30874E-01	
0.1	600.0	40.05646E-01	40.05646E-01	
0.1	800.0	43.77119E-01	43.77119E-01	
0.1	1000.0	46.86824E-01	46.86824E-01	39.78354E-08
0.1	2000.0	57.83628E-01	57.83628E-01	
0.1	4000.0	71.18178E-01	71.18178E-01	
0.1	6000.0	80.29186E-01	80.29186E-01	
0.1	8000.0	97.41966E-01	97.41966E-01	
0.1	10000.0	93.36266E-01	93.36266E-01	76.33867E-09
1.0	2000.0	54.40673E-01	54.40673E-01	
1.0	4000.0	67.75224E-01	67.75224E-01	
1.0	6000.0	76.86241E-01	76.86241E-01	
1.0	8000.0	83.99041E-01	83.99041E-01	
1.0	10000.0	89.93311E-01	89.93311E-01	76.33867E-09
10.0	2000.0	47.82594E-01	47.82594E-01	
10.0	4000.0	61.17145E-01	61.17145E-01	
10.0	6000.0	70.28161E-01	70.28161E-01	
10.0	8000.0	77.40961E-01	77.40961E-01	
10.0	10000.0	83.35231E-01	83.35231E-01	76.33867E-09
100.0	2000.0	35.19839E-01	35.19839E-01	
100.0	4000.0	48.54390E-01	48.54390E-01	
100.0	6000.0	57.65407E-01	57.65407E-01	
100.0	8000.0	64.78209E-01	64.78209E-01	
100.0	10000.0	70.72477E-01	70.72477E-01	76.33867E-09

GAS IS HELIUM

TOTAL OUTGASSING (C), INTEGRATION OF $Y=A*X**B$
 A = 0.32867E-09 B = -0.63743E-01

INITIAL TIME HOURS	FINAL TIME HOURS	OUTGASSING(Q) TORR-LITERS	TOTAL Q (ALL PREVIOUS GASSES)	OUTGASSING RATE TORR-LITERS/SEC
0.1	0.1	0.0	0.0	
0.1	0.2	13.37067E-08	80.90335E-03	
0.1	0.3	26.30704E-08	13.61313E-02	
0.1	0.4	38.95609E-08	17.93430E-02	
0.1	0.5	51.40796E-08	21.52656E-02	
0.1	0.6	63.70099E-08	24.65422E-02	
0.1	0.7	75.86346E-08	27.41827E-02	
0.1	0.8	87.91529E-08	29.91205E-02	
0.1	0.9	99.87116E-08	32.19132E-02	
0.1	1.0	11.17425E-07	34.2559E-02	32.86746E-11
0.1	2.0	22.71964E-07	45.81983E-02	
0.1	4.0	44.81239E-07	68.70912E-02	
0.1	6.0	66.17933E-07	81.60722E-02	
0.1	8.0	87.08825E-07	91.60284E-02	
0.1	10.0	10.76629E-06	10.01044E-01	28.38072E-11
0.1	20.0	20.73559E-06	12.98937E-01	
0.1	40.0	39.81250E-06	16.61408E-01	
0.1	60.0	58.26288E-06	19.08854E-01	
0.1	80.0	76.31726E-06	21.02462E-01	
0.1	100.0	94.08337E-06	22.63881E-01	24.50646E-11
0.1	200.0	18.01674E-05	28.35561E-01	
0.1	400.0	34.48037E-05	35.21219E-01	
0.1	600.0	50.42004E-05	40.06149E-01	
0.1	800.0	66.01089E-05	43.77778E-01	
0.1	1000.0	81.35170E-05	46.87637E-01	21.16110E-11
0.1	2000.0	15.56847E-04	57.85185E-01	
0.1	4000.0	29.79240E-04	71.21157E-01	
0.1	6000.0	43.54920E-04	80.33541E-01	
0.1	8000.0	57.01001E-04	87.47607E-01	
0.1	10000.0	70.25760E-04	93.43201E-01	18.27240E-11
1.0	2000.0	15.55729E-04	54.42226E-01	
1.0	4000.0	29.78132E-04	67.78203E-01	
1.0	6000.0	43.53802E-04	78.90595E-01	
1.0	8000.0	56.99577E-04	84.04740E-01	
1.0	10000.0	70.24646E-04	90.00335E-01	18.27240E-11
10.0	2000.0	15.46080E-04	47.84740E-01	
10.0	4000.0	29.68483E-04	61.20112E-01	
10.0	6000.0	43.44154E-04	70.32505E-01	
10.0	8000.0	56.90325E-04	77.46611E-01	
10.0	10000.0	70.14996E-04	82.42245E-01	18.27240E-11
100.0	2000.0	14.62763E-04	35.21301E-01	
100.0	4000.0	28.85166E-04	48.57275E-01	
100.0	6000.0	42.60838E-04	57.65667E-01	
100.0	8000.0	56.07009E-04	64.83814E-01	
100.0	10000.0	69.31677E-04	70.79609E-01	18.27240E-11

GAS IS METHANE

TOTAL OUTGASSING (Q), INTEGRATION OF $Y=A \times X^B$
 A = 0.18888E-06 B = -0.60775E 00

INITIAL TIME HOURS	FINAL TIME HOURS	OUTGASSING(Q) TORR-LITERS	TOTAL Q (ALL PREVIOUS GASES)	OUTGASSING RATE TORR-LITERS/SEC
0.1	0.1	0.0	0.0	
0.1	0.2	21.95041E-05	21.12282E-03	
0.1	0.3	37.84562E-05	13.65098E-02	
0.1	0.4	50.75890E-05	17.98505E-02	
0.1	0.5	61.82843E-05	21.55875E-02	
0.1	0.6	71.62043E-05	24.72583E-02	
0.1	0.7	80.46371E-05	27.45873E-02	
0.1	0.8	88.56840E-05	30.00062E-02	
0.1	0.9	96.07822E-05	32.28740E-02	
0.1	1.0	10.30664E-04	34.35865E-02	18.88811E-08
0.1	2.0	15.72582E-04	49.97709E-02	
0.1	4.0	22.83421E-04	68.93746E-02	
0.1	6.0	27.98170E-04	81.88354E-02	
0.1	8.0	32.16354E-04	92.01447E-02	
0.1	10.0	35.74827E-04	10.04619E-01	46.60573E-09
0.1	20.0	49.11240E-04	13.03847E-01	
0.1	40.0	66.65215E-04	16.68073E-01	
0.1	60.0	75.35334E-04	19.16788E-01	
0.1	80.0	85.67156E-04	21.11428E-01	
0.1	100.0	98.51709E-04	22.73732E-01	11.49978E-09
0.1	200.0	13.14628E-03	28.48710E-01	
0.1	400.0	17.47713E-03	35.48696E-01	
0.1	600.0	20.61112E-03	40.26760E-01	
0.1	800.0	22.15718E-03	44.00935E-01	
0.1	1000.0	25.33571E-03	47.12576E-01	28.27526E-10
0.1	2000.0	33.47625E-03	58.18661E-01	
0.1	4000.0	44.15512E-03	71.65311E-01	
0.1	6000.0	51.88809E-03	80.85428E-01	
0.1	8000.0	58.17037E-03	88.05867E-01	
0.1	10000.0	63.55560E-03	94.06846E-01	70.01486E-11
1.0	2000.0	32.44536E-03	54.74673E-01	
1.0	4000.0	42.12418E-03	68.21324E-01	
1.0	6000.0	50.85720E-03	77.41451E-01	
1.0	8000.0	57.13543E-03	84.61880E-01	
1.0	10000.0	62.52468E-03	90.62850E-01	70.01486E-11
10.0	2000.0	26.90147E-03	48.14040E-01	
10.0	4000.0	40.58030E-03	61.60692E-01	
10.0	6000.0	48.21222E-03	70.80218E-01	
10.0	8000.0	54.55554E-03	78.01246E-01	
10.0	10000.0	59.98085E-03	84.02225E-01	70.01486E-11
100.0	2000.0	22.62460E-03	25.44924E-01	
100.0	4000.0	34.30343E-03	48.91578E-01	
100.0	6000.0	42.03645E-03	58.11703E-01	
100.0	8000.0	48.21865E-03	65.22132E-01	
100.0	10000.0	52.70595E-03	71.22112E-01	70.01486E-11

GAS IS WATER VAPOR

TOTAL OUTGASSING (C), INTEGRATION OF Y=A**X**B
 A = 0.10832E-02 B = -0.19172E 01

INITIAL TIME HOURS	FINAL TIME HOURS	OUTGASSING(Q) TORR-LITERS	TOTAL Q (ALL PREVIOUS GASES)	OUTGASSING RATE TORR-LITERS/SEC
0.1	0.1	0.0	0.0	
0.1	0.2	16.53447E CC	16.61559E CC	
0.1	0.3	22.31395E CC	22.45045E CC	
0.1	0.4	25.28929E CC	25.46913E CC	
0.1	0.5	27.11299E CC	27.32896E CC	
0.1	0.6	28.34947E CC	28.59673E CC	
0.1	0.7	29.2451CE CC	29.57008E CC	
0.1	0.8	29.92488E CC	30.22488E CC	
0.1	0.9	30.45514E CC	30.7820CE CC	
0.1	1.0	30.89049E CC	31.23447E CC	10.83217E-04
0.1	2.0	32.89066E CC	33.39041E CC	
0.1	4.0	33.94971E CC	34.63907E CC	
0.1	6.0	34.31990E CC	35.12873E CC	
0.1	8.0	34.51047E CC	35.4306CE CC	
0.1	10.0	34.62727E CC	35.62188E CC	13.10353E-06
0.1	20.0	34.86923E CC	36.17307E CC	
0.1	40.0	34.99734E CC	36.66547E CC	
0.1	60.0	35.04213E CC	36.95891E CC	
0.1	80.0	35.06519E CC	37.17661E CC	
0.1	100.0	35.07932E CC	37.35304E CC	15.85111E-08
0.1	200.0	35.1086CE CC	37.95727E CC	
0.1	400.0	35.12409E CC	38.67278E CC	
0.1	600.0	35.12949E CC	39.15623E CC	
0.1	800.0	35.13228E CC	39.5322CE CC	
0.1	1000.0	35.1340CE CC	39.84697E CC	19.17482E-10
0.1	2000.0	35.13754E CC	40.95619E CC	
0.1	4000.0	35.13940E CC	42.30470E CC	
0.1	6000.0	35.14088E CC	43.22549E CC	
0.1	8000.0	35.14041E CC	43.94627E CC	
0.1	10000.0	35.14063E CC	44.54747E CC	23.19554E-12
1.0	2000.0	42.47037E-01	97.2171CE-01	
1.0	4000.0	42.48911E-01	11.07024E CC	
1.0	6000.0	42.49566E-01	11.99102E CC	
1.0	8000.0	42.49904E-01	12.71178E CC	
1.0	10000.0	42.50111E-01	13.31297E CC	23.19554E-12
10.0	2000.0	51.02554E-02	53.24295E-01	
10.0	4000.0	51.21301E-02	66.72822E-01	
10.0	6000.0	51.27854E-02	75.93603E-01	
10.0	8000.0	51.31279E-02	82.14368E-01	
10.0	10000.0	51.33296E-02	89.15555E-01	23.19554E-12
100.0	2000.0	55.22232E-03	36.03148E-01	
100.0	4000.0	60.09699E-03	46.51674E-01	
100.0	6000.0	60.75231E-03	58.72455E-01	
100.0	8000.0	61.08962E-03	65.93222E-01	
100.0	10000.0	61.25644E-03	71.94407E-01	23.19554E-12

GAS IS NITROGEN

TOTAL OUTGASSING (Q), INTEGRATION OF Y=A*X**B
 A = 0.19097E-05 B = -0.11869E 01

INITIAL TIME HOURS	FINAL TIME HOURS	OUTGASSING(Q) TORR-LITERS	TOTAL Q (ALL PREVIOUS GASES)	OUTGASSING RATE TORR-LITERS/SEC
0.1	0.1	0.0	0.0	
0.1	0.2	68.73100E-04	16.62245E 00	
0.1	0.3	10.49981E-03	22.46096E 00	
0.1	0.4	12.91127E-03	25.48204E 00	
0.1	0.5	14.69446E-03	27.34366E 00	
0.1	0.6	16.09726E-03	28.61287E 00	
0.1	0.7	17.24653E-03	29.52732E 00	
0.1	0.8	18.21570E-03	30.74305E 00	
0.1	0.9	19.05074E-03	30.80104E 00	
0.1	1.0	19.78226E-03	31.25424E 00	19.09718E-07
0.1	2.0	24.25188E-03	33.41466E 00	
0.1	4.0	28.17845E-03	34.66724E 00	
0.1	6.0	30.25030E-03	35.16998E 00	
0.1	8.0	31.62795E-03	35.46222E 00	
0.1	10.0	32.64667E-03	35.66657E 00	12.41892E-08
0.1	20.0	35.55227E-03	36.20862E 00	
0.1	40.0	38.10670E-03	36.70351E 00	
0.1	60.0	39.45405E-03	36.99825E 00	
0.1	80.0	40.34997E-03	37.21665E 00	
0.1	100.0	41.01240E-03	37.39404E 00	80.76029E-10
0.1	200.0	42.90257E-03	38.00020E 00	
0.1	400.0	44.56306E-03	38.71732E 00	
0.1	600.0	45.43921E-03	39.20166E 00	
0.1	800.0	46.02184E-03	39.57922E 00	
0.1	1000.0	46.45265E-03	39.89342E 00	52.51830E-11
0.1	2000.0	47.68181E-03	41.00386E 00	
0.1	4000.0	48.76164E-03	42.35345E 00	
0.1	6000.0	49.33143E-03	43.27481E 00	
0.1	8000.0	49.71027E-03	43.99997E 00	
0.1	10000.0	49.99044E-03	44.59744E 00	34.15278E-12
1.0	2000.0	27.89957E-03	57.49605E-01	
1.0	4000.0	28.97941E-03	11.09921E 00	
1.0	6000.0	29.54917E-03	12.02057E 00	
1.0	8000.0	29.92804E-03	12.74171E 00	
1.0	10000.0	30.20820E-03	13.34318E 00	34.15278E-12
10.0	2000.0	15.05514E-03	53.39306E-01	
10.0	4000.0	16.11499E-03	66.88936E-01	
10.0	6000.0	16.68476E-03	76.10288E-01	
10.0	8000.0	17.06362E-03	83.21431E-01	
10.0	10000.0	17.34378E-03	89.32899E-01	34.15278E-12
100.0	2000.0	66.69413E-04	36.09817E-01	
100.0	4000.0	77.49248E-04	40.59422E-01	
100.0	6000.0	82.19017E-04	56.80774E-01	
100.0	8000.0	86.97879E-04	66.01519E-01	
100.0	10000.0	89.78070E-04	72.03385E-01	34.15278E-12

GAS IS CO

TOTAL OUTGASSING (Q), INTEGRATION OF $Y=AX^{**}B$
 $A = 0.29163E-04$ $B = -0.99733E 00$

INITIAL TIME HOURS	FINAL TIME HOURS	OUTGASSING(Q) TORR-LITERS	TOTAL Q (ALL PREVIOUS GASES)	OUTGASSING RATE TORR-LITERS/SEC
0.1	0.1	0.0	0.0	
0.1	0.2	72.3618E-03	16.65484E 00	
0.1	0.3	11.48000E-02	22.57574E 00	
0.1	0.4	14.45172E-02	25.62695E 00	
0.1	0.5	16.82545E-02	27.51195E 00	
0.1	0.6	18.74050E-02	28.80020E 00	
0.1	0.7	20.35699E-02	29.74099E 00	
0.1	0.8	21.75781E-02	30.46066E 00	
0.1	0.9	22.99371E-02	31.03098E 00	
0.1	1.0	24.09077E-02	31.49524E 00	29.16291E-06
0.1	2.0	21.38365E-02	23.72845E 00	
0.1	4.0	38.68250E-02	35.05405E 00	
0.1	6.0	42.95700E-02	35.56854E 00	
0.1	8.0	45.99258E-02	35.92213E 00	
0.1	10.0	48.34692E-02	36.14798E 00	29.34312E-07
0.1	20.0	55.67572E-02	36.76537E 00	
0.1	40.0	63.01448E-02	37.32369E 00	
0.1	60.0	67.32015E-02	37.67154E 00	
0.1	80.0	70.37448E-02	37.92068E 00	
0.1	100.0	72.74754E-02	38.12151E 00	29.52437E-08
0.1	200.0	80.12125E-02	38.80141E 00	
0.1	400.0	87.50593E-02	39.56342E 00	
0.1	600.0	91.83682E-02	40.12003E 00	
0.1	800.0	94.90979E-02	40.52832E 00	
0.1	1000.0	97.25780E-02	40.86635E 00	29.70679E-09
0.1	2000.0	10.47164E-01	42.05101E 00	
0.1	4000.0	11.21500E-01	43.47495E 00	
0.1	6000.0	11.65021E-01	44.43982E 00	
0.1	8000.0	11.95949E-01	45.19101E 00	
0.1	10000.0	12.19979E-01	45.81743E 00	29.89032E-10
1.0	2000.0	80.61673E-02	10.55578E 00	
1.0	4000.0	88.05030E-02	11.67072E 00	
1.0	6000.0	92.40338E-02	12.64460E 00	
1.0	8000.0	95.40513E-02	13.60666E 00	
1.0	10000.0	97.80911E-02	14.52216E 00	29.89032E-10
10.0	2000.0	56.36557E-02	56.02025E-01	
10.0	4000.0	63.80317E-02	73.26967E-01	
10.0	6000.0	68.15628E-02	82.63850E-01	
10.0	8000.0	71.24800E-02	90.43911E-01	
10.0	10000.0	73.65101E-02	96.69408E-01	29.89032E-10
100.0	2000.0	21.96855E-02	29.29505E-01	
100.0	4000.0	26.40256E-02	53.52448E-01	
100.0	6000.0	43.75566E-02	62.18330E-01	
100.0	8000.0	44.84730E-02	70.70392E-01	
100.0	10000.0	46.25035E-02	76.95899E-01	29.89032E-10

GAS IS OXYGEN

TOTAL OUTGASSING (Q), INTEGRATION OF $Y=AX+XB$
 $A = 0.52863E-05$ $B = -0.14759E-01$

INITIAL TIME HOURS	FINAL TIME HOURS	OUTGASSING(Q) TORR-LITERS	TOTAL Q (ALL PREVIOUS GASES)	OUTGASSING RATE TORR-LITERS/SEC
0.1	0.1	0.0	0.0	
0.1	0.2	32.87502E-03	16.72871E-02	
0.1	0.3	49.05873E-03	22.62480E-02	
0.1	0.4	58.17152E-03	25.68512E-02	
0.1	0.5	64.42261E-03	27.57637E-02	
0.1	0.6	69.05586E-03	28.86925E-02	
0.1	0.7	72.66915E-03	29.81355E-02	
0.1	0.8	75.59007E-03	30.53624E-02	
0.1	0.9	78.01565E-03	31.10898E-02	
0.1	1.0	80.07234E-03	31.57530E-02	52.86282E-07
0.1	2.0	91.29369E-03	32.81978E-02	
0.1	4.0	99.23966E-03	35.15338E-02	
0.1	6.0	10.26451E-02	35.70148E-02	
0.1	8.0	10.51093E-02	36.02724E-02	
0.1	10.0	10.65940E-02	36.25456E-02	17.50926E-08
0.1	20.0	11.02107E-02	36.87567E-02	
0.1	40.0	11.29758E-02	37.44666E-02	
0.1	60.0	11.41698E-02	37.78571E-02	
0.1	80.0	11.48668E-02	38.03557E-02	
0.1	100.0	11.53785E-02	38.22688E-02	57.99411E-10
0.1	200.0	11.66095E-02	38.91801E-02	
0.1	400.0	11.74923E-02	39.70990E-02	
0.1	600.0	11.79878E-02	40.23703E-02	
0.1	800.0	11.81252E-02	40.64644E-02	
0.1	1000.0	11.82880E-02	40.98468E-02	19.20881E-11
0.1	2000.0	11.86559E-02	42.16960E-02	
0.1	4000.0	11.86883E-02	42.59393E-02	
0.1	6000.0	11.91192E-02	44.55894E-02	
0.1	8000.0	11.91978E-02	45.31110E-02	
0.1	10000.0	11.92518E-02	45.93688E-02	63.62347E-13
1.0	2000.0	35.62350E-03	10.59440E-02	
1.0	4000.0	35.91588E-03	12.01863E-02	
1.0	6000.0	36.04688E-03	12.98365E-02	
1.0	8000.0	36.12552E-03	13.73570E-02	
1.0	10000.0	36.17647E-03	14.36134E-02	63.62347E-13
10.0	2000.0	12.10187E-03	59.15126E-03	
10.0	4000.0	12.36425E-03	72.35361E-03	
10.0	6000.0	12.52525E-03	83.04375E-03	
10.0	8000.0	12.60380E-03	90.56515E-03	
10.0	10000.0	12.65784E-03	94.82065E-03	63.62347E-13
100.0	2000.0	33.17350E-04	26.32922E-03	
100.0	4000.0	34.05734E-04	52.57058E-03	
100.0	6000.0	37.40733E-04	63.22070E-03	
100.0	8000.0	39.15376E-04	70.74211E-03	
100.0	10000.0	38.72222E-04	74.66741E-03	63.62347E-13

GAS IS ARGON

TOTAL OUTGASSING (Q), INTEGRATION OF $Y=A \times X^B$
 $A = 0.10525E-06$ $B = -0.12105E 01$

INITIAL TIME HOURS	FINAL TIME HOURS	OUTGASSING(Q) TORR-LITERS	TOTAL Q (ALL PREVIOUS GASES)	OUTGASSING RATE TORR-LITERS/SEC
0.1	0.1	0.0	0.0	
0.1	0.2	39.67902E-05	16.72911E 00	
0.1	0.3	60.34311E-05	22.62540E 00	
0.1	0.4	73.97069E-05	25.68585E 00	
0.1	0.5	81.98707E-05	27.57721E 00	
0.1	0.6	91.82887E-05	28.87016E 00	
0.1	0.7	98.22825E-05	29.81683E 00	
0.1	0.8	10.36062E-04	30.53726E 00	
0.1	0.9	10.82259E-04	31.11077E 00	
0.1	1.0	11.22626E-04	31.57642E 00	10.52470E-08
0.1	2.0	13.66989E-04	33.82114E 00	
0.1	4.0	15.78172E-04	35.15495E 00	
0.1	6.0	16.88152E-04	35.70316E 00	
0.1	8.0	17.60682E-04	36.02899E 00	
0.1	10.0	18.13991E-04	36.25636E 00	64.81410E-10
0.1	20.0	19.64482E-04	36.87762E 00	
0.1	40.0	20.94539E-04	37.44875E 00	
0.1	60.0	21.62268E-04	37.78786E 00	
0.1	80.0	22.06936E-04	38.03777E 00	
0.1	100.0	22.39767E-04	38.23911E 00	39.91674E-11
0.1	200.0	23.32445E-04	38.52033E 00	
0.1	400.0	24.12561E-04	38.71221E 00	
0.1	600.0	24.54752E-04	40.24024E 00	
0.1	800.0	24.81761E-04	40.64891E 00	
0.1	1000.0	25.01979E-04	40.98717E 00	24.58257E-12
0.1	2000.0	25.59966E-04	42.17224E 00	
0.1	4000.0	26.08392E-04	43.59683E 00	
0.1	6000.0	26.34069E-04	44.66157E 00	
0.1	8000.0	26.51019E-04	45.31374E 00	
0.1	10000.0	26.63462E-04	45.93923E 00	15.13911E-13
1.0	2000.0	14.34430E-04	10.55583E 00	
1.0	4000.0	14.85766E-04	12.02012E 00	
1.0	6000.0	15.11444E-04	12.98516E 00	
1.0	8000.0	15.29385E-04	13.73722E 00	
1.0	10000.0	15.40824E-04	14.36288E 00	15.13911E-13
10.0	2000.0	74.50636E-05	50.15871E-01	
10.0	4000.0	79.43900E-05	73.40155E-01	
10.0	6000.0	82.00780E-05	83.05194E-01	
10.0	8000.0	83.70187E-05	90.57251E-01	
10.0	10000.0	84.94705E-05	96.83914E-01	15.13911E-13
100.0	2000.0	31.92875E-05	30.33141E-01	
100.0	4000.0	34.88142E-05	53.57426E-01	
100.0	6000.0	39.43022E-05	63.22666E-01	
100.0	8000.0	41.12430E-05	70.74622E-01	
100.0	10000.0	42.36647E-05	77.00185E-01	15.13911E-13

GAS IS CO2

TOTAL OUTGASSING (C), INTEGRATION OF Y=A**X**B
 A = 0.23905E-04 B = -0.10436E 01

INITIAL TIME HOURS	FINAL TIME HOURS	OUTGASSING(Q) TORR-LITERS	TOTAL Q (ALL PREVIOUS GASES)	OUTGASSING RATE TORR-LITERS/SEC
0.1	0.1	0.0	0.0	
0.1	0.2	64.95859E-02	16.75407E 00	
0.1	0.3	10.20565E-02	22.72745E 00	
0.1	0.4	12.75236E-02	25.81383E 00	
0.1	0.5	14.78735E-02	27.72508E 00	
0.1	0.6	16.39750E-02	29.03413E 00	
0.1	0.7	17.74083E-02	29.99202E 00	
0.1	0.8	18.91257E-02	30.72639E 00	
0.1	0.9	19.93452E-02	31.30925E 00	
0.1	1.0	20.84323E-02	31.78484E 00	23.90458E-06
0.1	2.0	26.71007E-02	34.08832E 00	
0.1	4.0	32.42004E-02	35.47914E 00	
0.1	6.0	35.67557E-02	36.05991E 00	
0.1	8.0	37.95146E-02	36.40849E 00	
0.1	10.0	39.69694E-02	36.65222E 00	21.62284E-07
0.1	20.0	45.01188E-02	37.32773E 00	
0.1	40.0	50.16873E-02	37.95042E 00	
0.1	60.0	53.11387E-02	38.31898E 00	
0.1	80.0	55.17216E-02	38.58948E 00	
0.1	100.0	56.75101E-02	38.80661E 00	19.55889E-08
0.1	200.0	61.55863E-02	39.53592E 00	
0.1	400.0	66.22334E-02	40.37454E 00	
0.1	600.0	68.88729E-02	40.92970E 00	
0.1	800.0	70.74508E-02	41.35640E 00	
0.1	1000.0	72.17724E-02	41.70894E 00	17.69193E-09
0.1	2000.0	76.52596E-02	42.53750E 00	
0.1	4000.0	80.74533E-02	44.40398E 00	
0.1	6000.0	83.15507E-02	45.23311E 00	
0.1	8000.0	84.83917E-02	45.16212E 00	
0.1	10000.0	86.13100E-02	45.80063E 00	16.00310E-10
1.0	2000.0	85.68272E-02	44.15266E 00	
1.0	4000.0	89.90209E-02	47.61514E 00	
1.0	6000.0	92.31182E-02	48.60827E 00	
1.0	8000.0	93.99563E-02	49.37727E 00	
1.0	10000.0	95.28774E-02	49.01575E 00	16.00310E-10
10.0	2000.0	96.82907E-02	62.84161E-01	
10.0	4000.0	91.04835E-02	77.50638E-01	
20.0	6000.0	93.45832E-02	87.39775E-01	
20.0	8000.0	95.14222E-02	95.08773E-01	
10.0	10000.0	96.43406E-02	10.14725E 00	16.00310E-10
100.0	2000.0	99.77464E-02	41.30850E-01	
100.0	4000.0	93.59643E-02	55.97368E-01	
100.0	6000.0	96.40404E-02	65.86504E-01	
100.0	8000.0	98.08814E-02	73.55503E-01	
100.0	10000.0	99.37668E-02	79.93984E-01	16.00319E-10

GAS IS C2H4

TOTAL OUTGASSING (C), INTEGRATION OF $Y=A \cdot X^{**}B$
 A = 0.33025E-06 P = -0.11268E 01

INITIAL TIME HOURS	FINAL TIME HOURS	OUTGASSING (Q) TORR-LITERS	TOTAL Q (ALL PREVIOUS GASES)	OUTGASSING RATE TORR-LITERS/SEC
0.1	0.1	0.0	0.0	
0.1	0.2	10.56466E-04	16.79512E 00	
0.1	0.3	16.32744E-04	22.72008E 00	
0.1	0.4	20.24009E-04	25.81584E 00	
0.1	0.5	23.17824E-04	27.72730E 00	
0.1	0.6	25.51786E-04	29.03668E 00	
0.1	0.7	27.45416E-04	29.99475E 00	
0.1	0.8	29.10121E-04	30.72529E 00	
0.1	0.9	30.53104E-04	31.31244E 00	
0.1	1.0	31.79203E-04	31.79801E 00	33.02455E-08
0.1	2.0	35.68079E-04	34.09229E 00	
0.1	4.0	46.90565E-04	35.48383E 00	
0.1	6.0	50.84664E-04	36.06490E 00	
0.1	8.0	53.52244E-04	36.41383E 00	
0.1	10.0	55.53175E-04	36.65886E 00	24.66010E-09
0.1	20.0	61.42747E-04	37.33386E 00	
0.1	40.0	66.81744E-04	37.95705E 00	
0.1	60.0	69.76023E-04	38.32506E 00	
0.1	80.0	71.75833E-04	38.59665E 00	
0.1	100.0	73.25869E-04	38.81393E 00	18.41415E-10
0.1	200.0	77.65744E-04	39.54367E 00	
0.1	400.0	81.68589E-04	40.38271E 00	
0.1	600.0	83.88337E-04	40.93758E 00	
0.1	800.0	85.37535E-04	41.36493E 00	
0.1	1000.0	86.46573E-04	41.71788E 00	13.75020E-11
0.1	2000.0	89.78035E-04	42.54664E 00	
0.1	4000.0	92.78845E-04	43.41378E 00	
0.1	6000.0	94.42537E-04	43.90256E 00	
0.1	8000.0	95.54241E-04	44.17168E 00	
0.1	10000.0	96.38011E-04	44.31026E 00	10.26755E-12
1.0	2000.0	97.08832E-04	44.58446E 00	
1.0	4000.0	98.96645E-04	45.62524E 00	
1.0	6000.0	99.63737E-04	45.81454E 00	
1.0	8000.0	99.75145E-04	45.88345E 00	
1.0	10000.0	99.58808E-04	45.82221E 00	10.26755E-12
10.0	2000.0	94.24862E-04	62.87585E-01	
10.0	4000.0	97.25676E-04	77.54363E-01	
10.0	6000.0	98.85766E-04	87.42664E-01	
10.0	8000.0	99.07170E-04	95.12774E-01	
10.0	10000.0	99.84829E-04	10.15134E 00	10.26755E-12
100.0	2000.0	16.57167E-04	41.32542E-01	
100.0	4000.0	19.52581E-04	55.95320E-01	
100.0	6000.0	21.17072E-04	65.88620E-01	
100.0	8000.0	22.28482E-04	73.57731E-01	
100.0	10000.0	22.12141E-04	79.06296E-01	10.26755E-12

GAS IS C2H6

TOTAL OUTGASSING (C), INTEGRATION OF Y=A* $X^{**}B$
 A = 0.27147E-04 P = -0.28747E 00

INITIAL TIME HOURS	FINAL TIME HOURS	OUTGASSING (C) TORR-LITERS	TOTAL Q (ALL PREVIOUS GASFS)	OUTGASSING RATE TORR-LITERS/SEC
0.1	0.1	0.0	0.0	
0.1	0.2	54.38270E-05	14.79565E CC	
0.1	0.3	88.21357E-05	22.72995E CC	
0.1	0.4	11.31685E-04	25.81697E CC	
0.1	0.5	13.30886E-04	27.72871E CC	
0.1	0.6	14.97351E-04	29.03818E CC	
0.1	0.7	16.40854E-04	29.95638E CC	
0.1	0.8	17.67151E-04	30.73107E CC	
0.1	0.9	18.80136E-04	31.31432E CC	
0.1	1.0	19.82478E-04	31.78998E CC	27.14726E-08
0.1	2.0	26.86236E-04	34.09497E CC	
0.1	4.0	34.48715E-04	35.48726E CC	
0.1	6.0	35.21866E-04	36.06891E CC	
0.1	8.0	42.71256E-04	36.41809E CC	
0.1	10.0	45.50148E-04	36.66341E CC	35.15420E-09
0.1	20.0	54.62412E-04	37.33931E CC	
0.1	40.0	64.48545E-04	37.96352E CC	
0.1	60.0	70.62014E-04	38.33019E CC	
0.1	80.0	75.14536E-04	38.60416E CC	
0.1	100.0	78.75752E-04	38.82181E CC	45.53108E-10
0.1	200.0	90.57291E-04	39.55772E CC	
0.1	400.0	10.33452E-03	40.39304E CC	
0.1	600.0	11.12907E-03	40.54870E CC	
0.1	800.0	11.71517E-03	41.37663E CC	
0.1	1000.0	12.16200E-03	41.72975E CC	58.97098E-11
0.1	2000.0	13.71333E-03	42.56017E CC	
0.1	4000.0	15.36757E-03	44.47862E CC	
0.1	6000.0	16.39665E-03	45.41893E CC	
0.1	8000.0	17.15574E-03	46.18693E CC	
0.1	10000.0	17.76168E-03	46.82802E CC	76.37620E-12
1.0	2000.0	11.73096E-03	11.17015E CC	
1.0	4000.0	13.28510E-03	12.63862E CC	
1.0	6000.0	14.41415E-03	13.62895E CC	
1.0	8000.0	15.17326E-03	14.39882E CC	
1.0	10000.0	15.77921E-03	15.02790E CC	76.37820E-12
10.0	2000.0	91.63190E-04	62.96748E-C1	
10.0	4000.0	10.81747E-03	77.65180E-C1	
10.0	6000.0	11.84652E-03	87.55506E-C1	
10.0	8000.0	12.60555E-03	95.25378E-C1	
10.0	10000.0	13.21153E-03	10.16455E CC	76.37820E-12
100.0	2000.0	58.37578E-04	41.38370E-C1	
100.0	4000.0	74.61823E-04	56.06812E-C1	
100.0	6000.0	85.20912E-04	65.57140E-C1	
100.0	8000.0	92.75989E-04	73.67010E-C1	
100.0	10000.0	98.85937E-04	80.06182E-C1	76.37820E-12

GAS IS C2H6

TOTAL OUTGASSING (Q), INTEGRATION OF $Y=A \times X^B$
 $A = 0.1192E-05$ $B = -0.18798E 01$

INITIAL TIME HOURS	FINAL TIME HOURS	OUTGASSING(Q) TORR-LITERS	TOTAL Q (ALL PREVIOUS GASES)	OUTGASSING RATE TORR-LITERS/SEC
0.1	0.1	0.0	0.0	
0.1	0.2	72.37452E-03	16.86803E 00	
0.1	0.3	98.23432E-03	22.82819E 00	
0.1	0.4	11.17321E-02	25.92870E 00	
0.1	0.5	12.00867E-02	27.84880E 00	
0.1	0.6	12.57558E-02	29.16397E 00	
0.1	0.7	12.95582E-02	30.12633E 00	
0.1	0.8	13.31350E-02	30.86418E 00	
0.1	0.9	13.56438E-02	31.44995E 00	
0.1	1.0	13.76783E-02	31.92764E 00	51.19220E-07
0.1	2.0	14.72446E-02	34.24220E 00	
0.1	4.0	15.24469E-02	35.63569E 00	
0.1	6.0	15.43058E-02	36.22321E 00	
0.1	8.0	15.52799E-02	36.57336E 00	
0.1	10.0	15.58764E-02	36.81927E 00	67.66527E-09
0.1	20.0	15.71409E-02	37.49644E 00	
0.1	40.0	15.78285E-02	38.13135E 00	
0.1	60.0	15.80742E-02	38.49107E 00	
0.1	80.0	15.82024E-02	38.76234E 00	
0.1	100.0	15.82818E-02	38.98009E 00	89.43903E-11
0.1	200.0	15.84489E-02	39.71117E 00	
0.1	400.0	15.85398E-02	40.55157E 00	
0.1	600.0	15.85723E-02	41.10727E 00	
0.1	800.0	15.85892E-02	41.53522E 00	
0.1	1000.0	15.85997E-02	41.88334E 00	11.82192E-12
0.1	2000.0	15.86219E-02	43.11879E 00	
0.1	4000.0	15.86339E-02	44.58725E 00	
0.1	6000.0	15.86382E-02	45.57766E 00	
0.1	8000.0	15.86404E-02	46.34746E 00	
0.1	10000.0	15.86418E-02	46.98445E 00	15.62620E-14
1.0	2000.0	20.94360E-03	11.19113E 00	
1.0	4000.0	20.95562E-03	12.65588E 00	
1.0	6000.0	20.95991E-03	13.64591E 00	
1.0	8000.0	20.96215E-03	14.41976E 00	
1.0	10000.0	20.96353E-03	15.05895E 00	15.62420E-14
10.0	2000.0	27.45449E-04	62.99493E-01	
10.0	4000.0	27.57451E-04	77.67837E-01	
10.0	6000.0	27.61783E-04	87.58270E-01	
10.0	8000.0	27.63944E-04	95.28142E-01	
10.0	10000.0	27.65381E-04	10.16731E 00	15.62420E-14
100.0	2000.0	34.00357E-05	61.38719E-01	
100.0	4000.0	35.20492E-05	56.07163E-01	
100.0	6000.0	35.45419E-05	45.07496E-01	
100.0	8000.0	35.65822E-05	37.67359E-01	
100.0	10000.0	35.84609E-05	30.06541E-01	15.62620E-14

GAS IS HYDROCARBONS

TOTAL OUTGASSING (C), INTEGRATION OF $Y=A \times X^R$
 $A = 0.65026E-06$ $R = -0.775PEE 00$

INITIAL TIME HOURS	FINAL TIME HOURS	OUTGASSING(C) TORR-LITERS	TOTAL C (ALL PREVIOUS GASES)	OUTGASSING RATE TORR-LITERS/SEC
0.1	0.1	0.0	0.0	
0.1	0.2	10.47697E-04	16.86803E 00	
0.1	0.3	17.40406E-04	22.82819E 00	
0.1	0.4	22.71507E-04	25.92870E 00	
0.1	0.5	27.07698E-04	27.84880E 00	
0.1	0.6	30.80651E-04	29.16397E 00	
0.1	0.7	34.08088E-04	30.12633E 00	
0.1	0.8	37.01019E-04	30.86418E 00	
0.1	0.9	39.66787E-04	31.44995E 00	
0.1	1.0	42.10532E-04	31.92764E 00	65.02601E-08
0.1	2.0	56.69899E-04	34.24220E 00	
0.1	4.0	80.16519E-04	35.63966E 00	
0.1	6.0	93.72279E-04	36.22321E 00	
0.1	8.0	10.41174E-03	36.57336E 00	
0.1	10.0	11.26546E-03	36.81527E 00	10.89538E-08
0.1	20.0	14.20679E-03	37.49644E 00	
0.1	40.0	17.64255E-03	38.12135E 00	
0.1	60.0	19.91418E-03	38.49107E 00	
0.1	80.0	21.65584E-03	38.76224E 00	
0.1	100.0	23.08625E-03	38.98099E 00	18.25563E-09
0.1	200.0	28.01459E-03	39.71117E 00	
0.1	400.0	33.77131E-03	40.55157E 00	
0.1	600.0	37.57751E-03	41.10727E 00	
0.1	800.0	40.46573E-03	41.53522E 00	
0.1	1000.0	42.89251E-03	41.86824E 00	30.58805E-10
0.1	2000.0	51.15010E-03	43.11679E 00	
0.1	4000.0	60.75575E-03	44.58725E 00	
0.1	6000.0	67.17318E-03	45.57756E 00	
0.1	8000.0	72.06279E-03	46.24746E 00	
0.1	10000.0	76.07853E-03	46.88645E 00	51.25149E-11
1.0	20000.0	86.93956E-03	48.19113E 00	
1.0	40000.0	96.55573E-03	49.25058E 00	
1.0	60000.0	102.56259E-03	49.64991E 00	
1.0	80000.0	107.85220E-03	49.84197E 00	
1.0	100000.0	111.86800E-03	49.95895E 00	51.25149E-11
10.0	200000.0	129.88443E-03	50.96493E 01	
10.0	400000.0	149.53030E-03	51.79327E 01	
10.0	600000.0	165.90773E-03	52.58270E 01	
10.0	800000.0	180.79734E-03	53.28142E 01	
10.0	1000000.0	194.51308E-03	53.91673E 01	51.25149E-11
100.0	2000000.0	226.06384E-03	54.38871E 01	
100.0	4000000.0	27.70951E-02	56.07163E 01	
100.0	6000000.0	44.08697E-02	65.97465E 01	
100.0	8000000.0	48.97657E-02	72.67365E 01	
100.0	10000000.0	52.99238E-02	80.06561E 01	51.25149E-11

TOTAL OUTGASSING

INITIAL TIME HOURS	FINAL TIME HOURS	TOTAL O
0.1	0.1	0.0
0.1	0.2	1.68480E 01
0.1	0.3	2.28282E 01
0.1	0.4	2.59287E 01
0.1	0.5	2.78488E 01
0.1	0.6	2.91640E 01
0.1	0.7	3.01263E 01
0.1	0.8	3.08642E 01
0.1	0.9	3.14500E 01
0.1	1.0	3.19276E 01
0.1	2.0	3.42422E 01
0.1	4.0	3.56397E 01
0.1	6.0	3.62232E 01
0.1	8.0	3.65734E 01
0.1	10.0	3.69192E 01
0.1	20.0	3.74964E 01
0.1	40.0	3.81214E 01
0.1	60.0	3.84911E 01
0.1	80.0	3.87623E 01
0.1	100.0	3.89601E 01
0.1	200.0	3.97112E 01
0.1	400.0	4.05516E 01
0.1	600.0	4.11073E 01
0.1	800.0	4.15352E 01
0.1	1000.0	4.18823E 01
0.1	2000.0	4.31188E 01
0.1	4000.0	4.45872E 01
0.1	6000.0	4.55776E 01
0.1	8000.0	4.63475E 01
0.1	10000.0	4.69866E 01
1.0	2000.0	1.11911E 01
1.0	4000.0	1.26566E 01
1.0	6000.0	1.36499E 01
1.0	8000.0	1.44198E 01
1.0	10000.0	1.50590E 01
10.0	2000.0	6.29946E 00
10.0	4000.0	7.76794E 00
10.0	6000.0	8.75827E 00
10.0	8000.0	9.52814E 00
10.0	10000.0	1.01672E 01
100.0	2000.0	4.12872E 00
100.0	4000.0	6.60716E 00
100.0	6000.0	8.59750E 00
100.0	8000.0	9.36737E 00
100.0	10000.0	9.90654E 00

```

1EF285I  SYS70265,7094821,8V000,CLAE,FJ0BL1P  PASSED
1EF285I  VOL SEP ACT= CL1R01.
1EF285I  SYS70265,7094821,8V000,CLAE,P0000044  SYSCUT
1EF285I  VOL SEP ACT= XXXXXX.
1EF285I  SYS70265,7094821,8V000,CLAE,FJ0BL1P  DELETED
1EF285I  VOL SEP ACT= CL1R01.
1EF285I  SYS70265,7094821,8V000,CLAE,UT2C  CFILETFD
1EF285I  VOL SEP ACT= 222222.
1EF285I  SYS70265,7094821,8V000,CLAE,P0000045  SYSCUT
1EF285I  VOL SEP ACT= P00000.
1EF285I  SYS70265,7094821,8V000,CLAE,SC000046  SYSIN
1EF285I  VOL SEP ACT= YYYYYY.
1EF285I  SYS70265,7094821,8V000,CLAE,SC000046  CFILETFD
1EF285I  VOL SEP ACT= YYYYYY.

```

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0116  GC 19,50,29 10-22-70
CPU SEC.= 260.77// I/O REQUESTS= 139// REGION ALLOC.= 250K// MACH. USE SEC.= 270.67// REGION USED= 126K

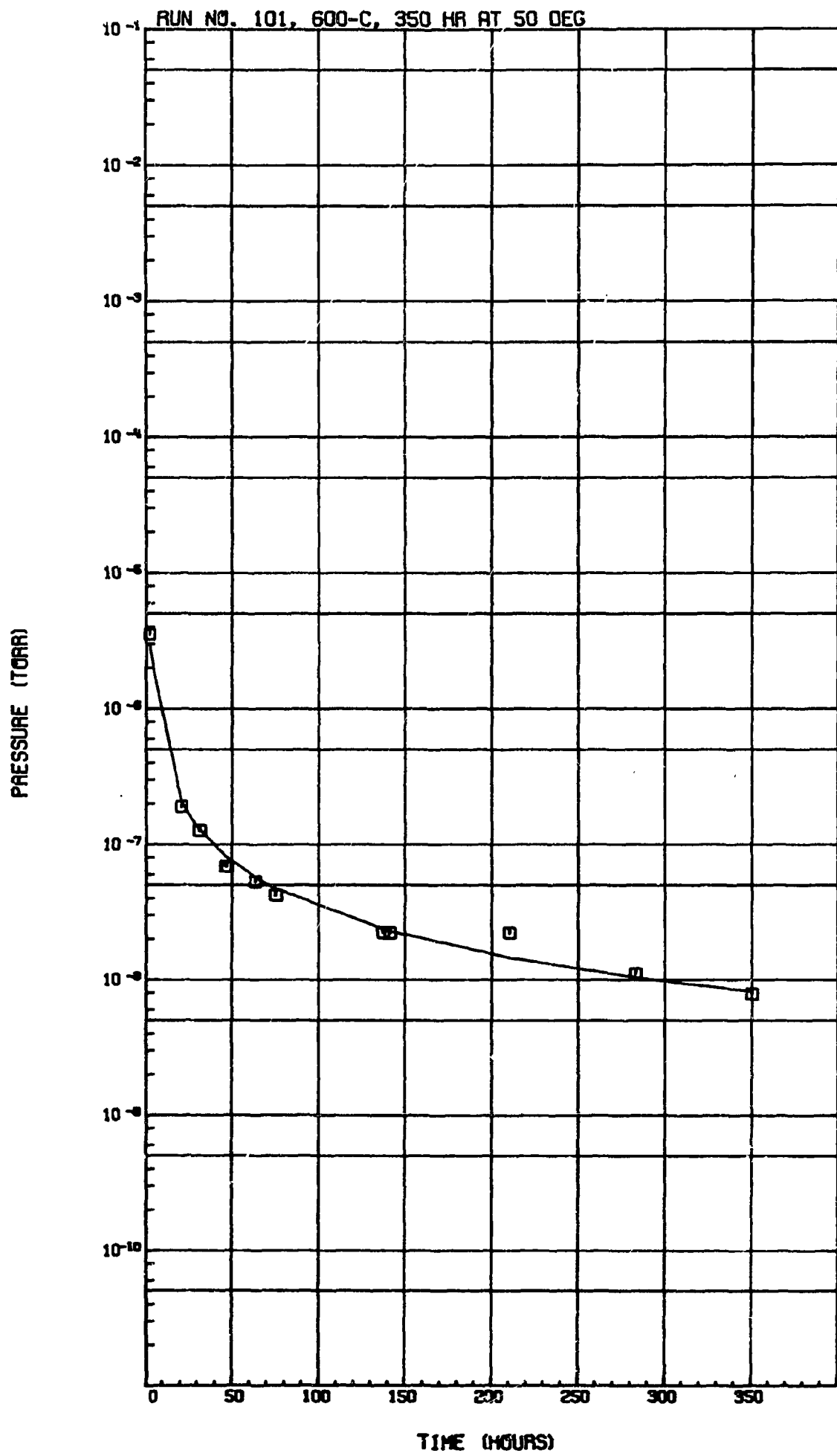
```

```

CLAE MODEL=75 12223 19,50,29 10-22-70
TOTAL CPU SEC.= 355.78//TOTAL I/O REQUESTS= 1463//MAX. REGION ALLOC.= 470K//TOTAL MACH. USE SEC.= 269.15//MAX. REGION USED= 420K

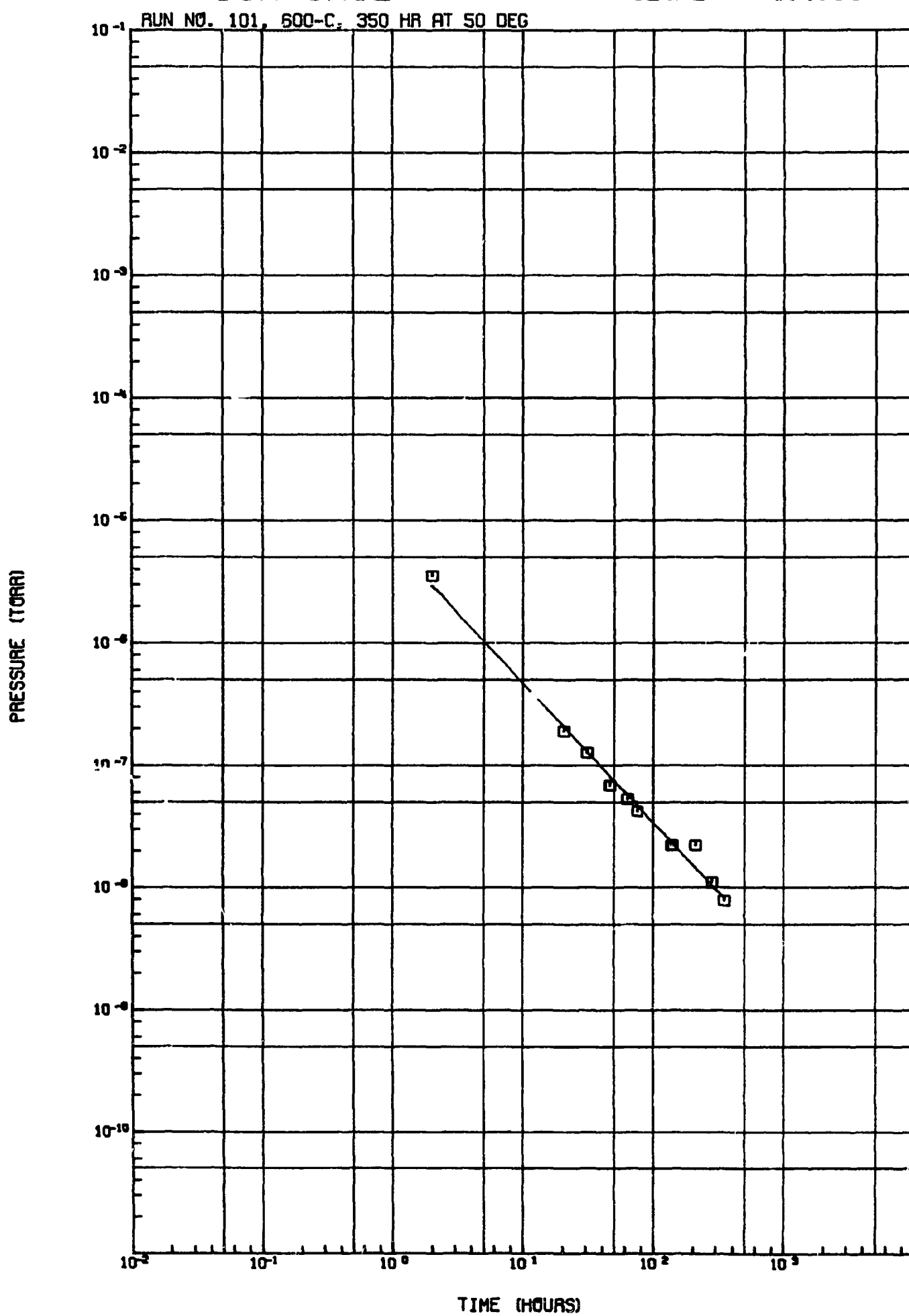
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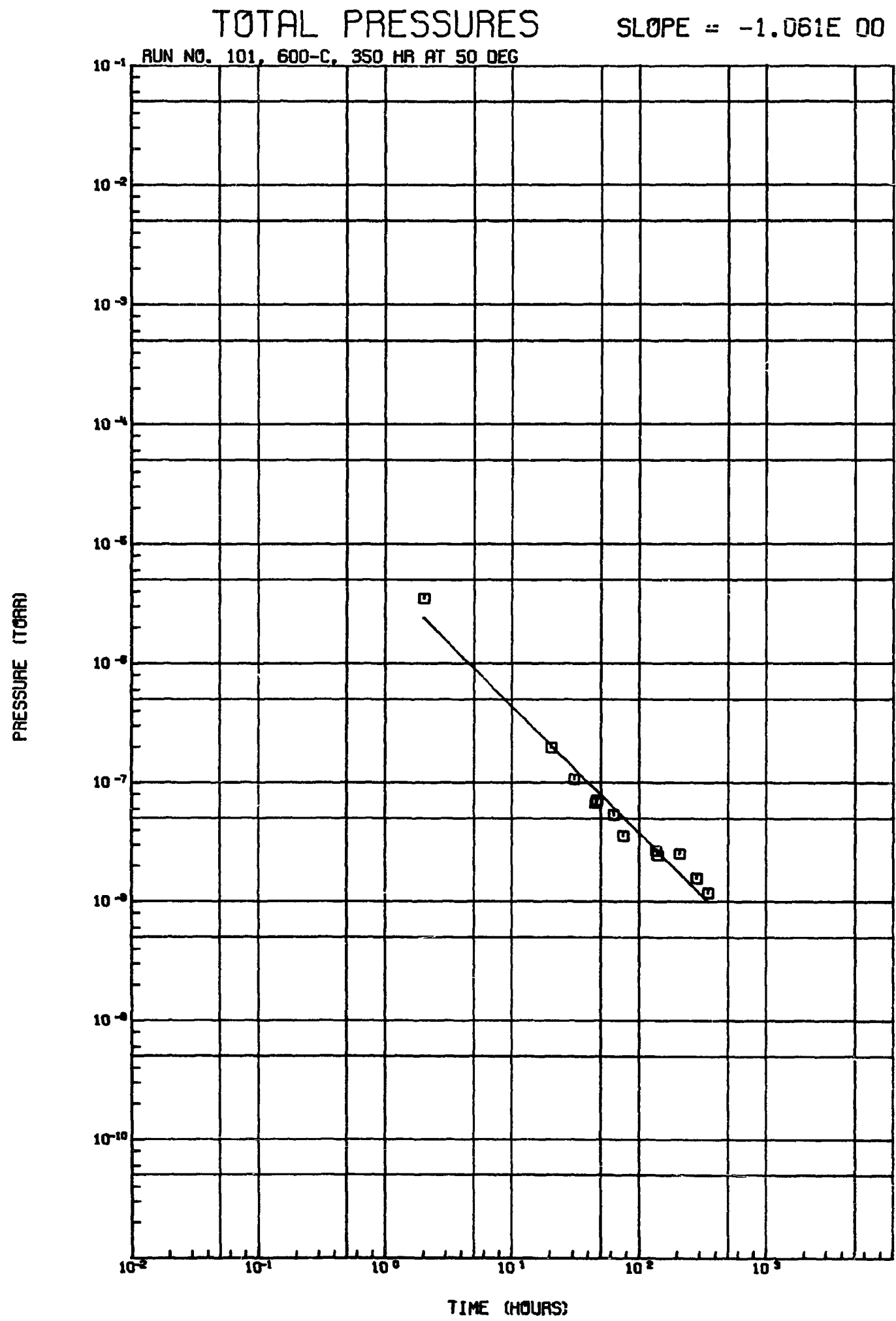
ION GAGE



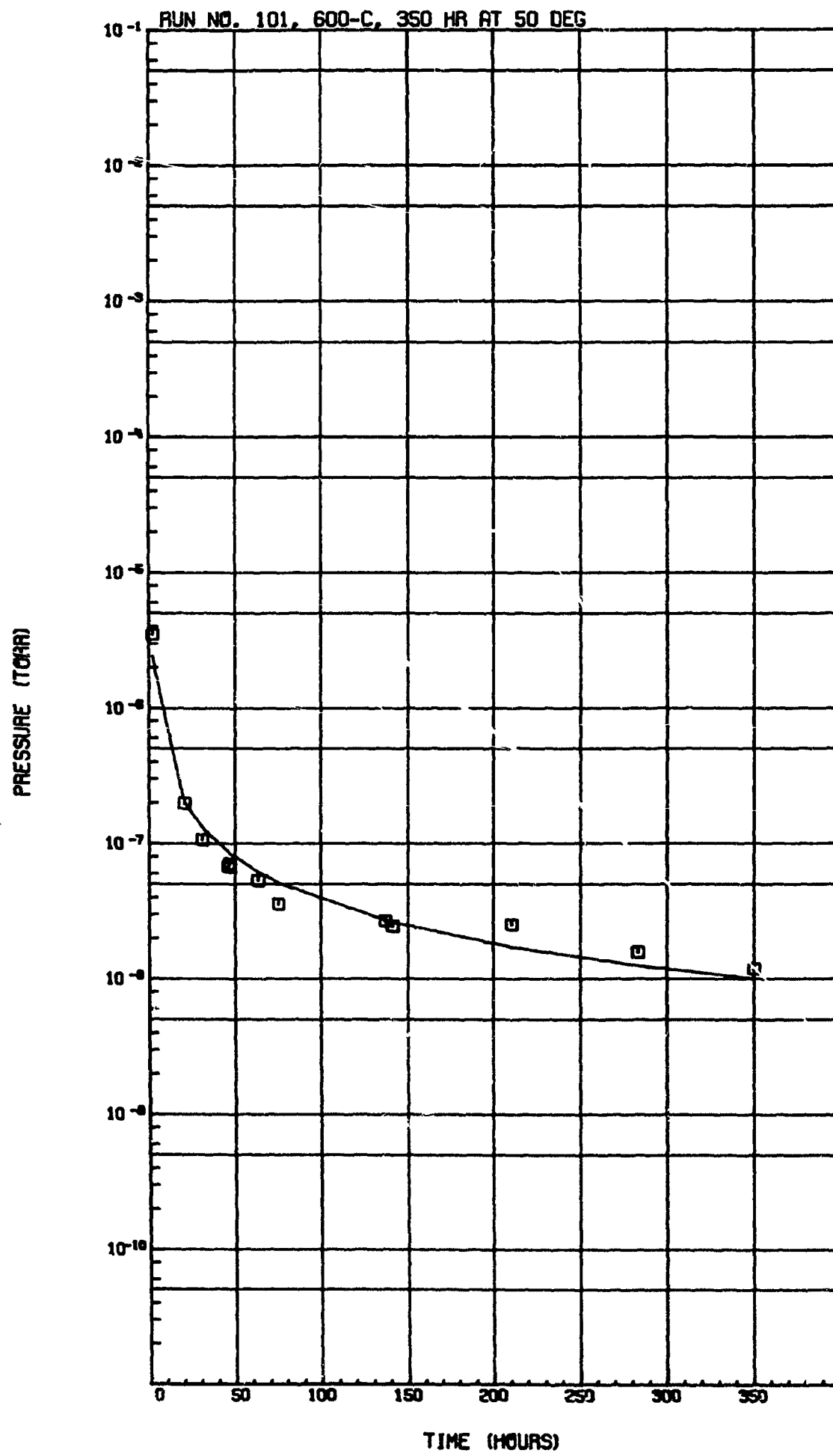
ION GAGE

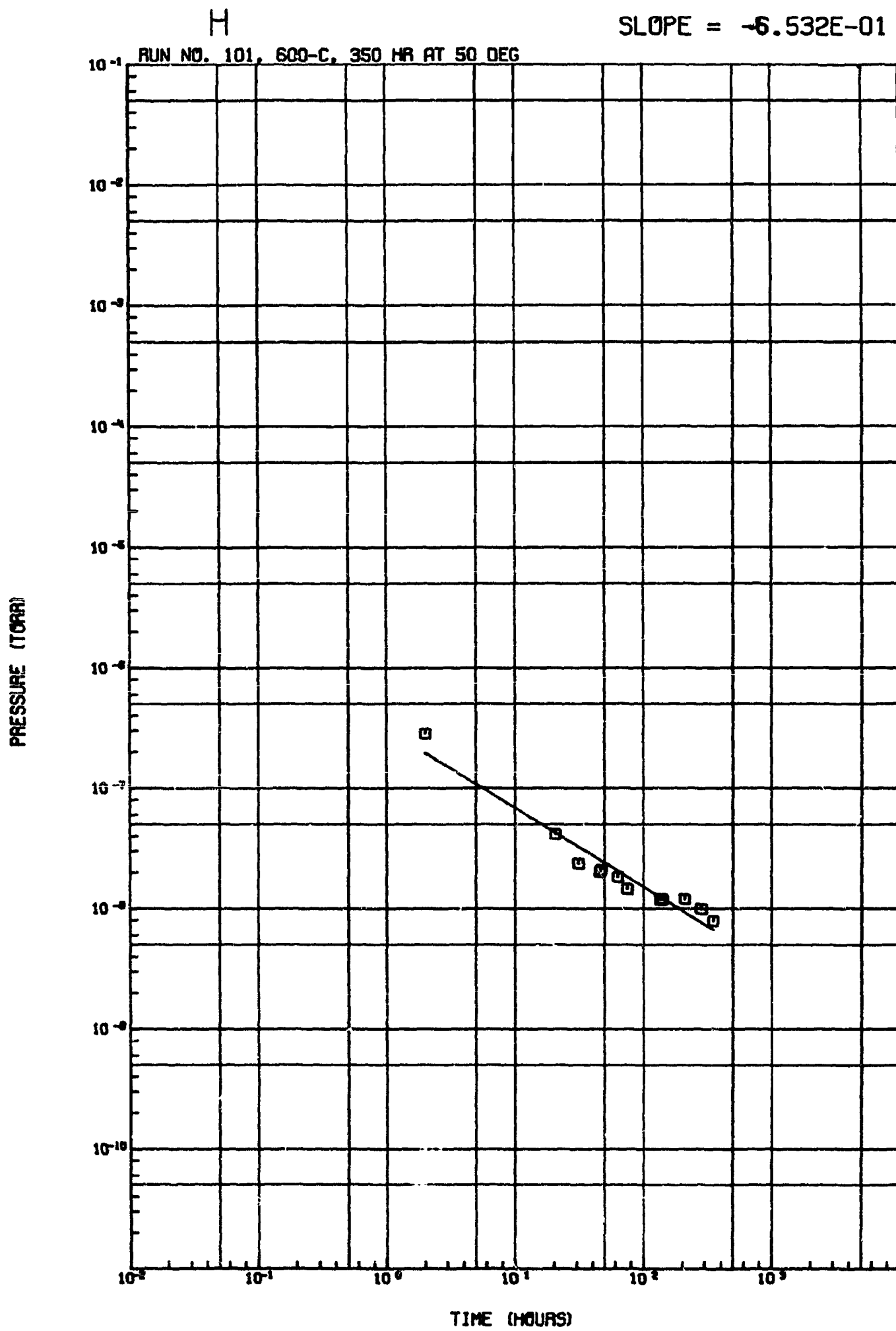
SLOPE = -1.139E 00

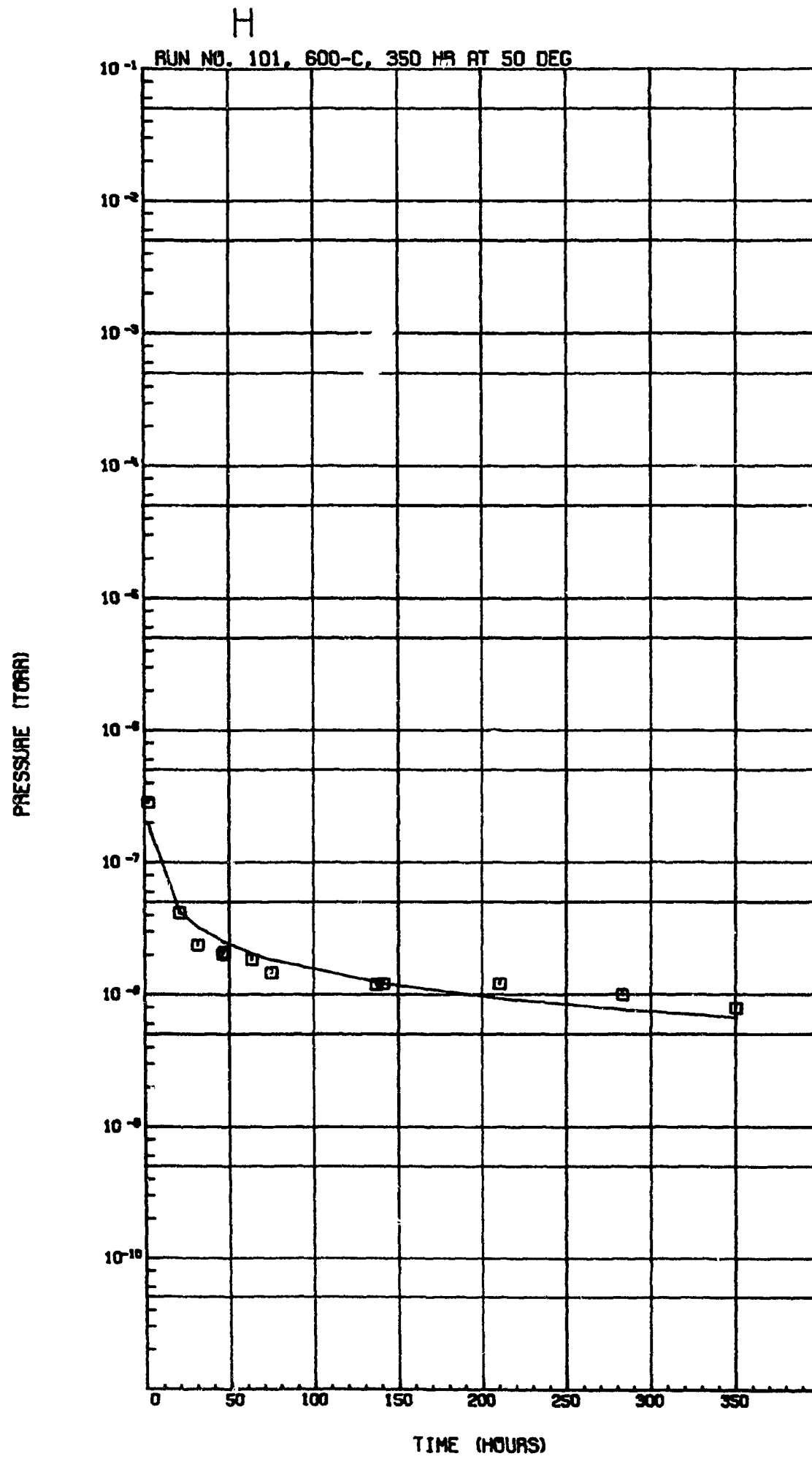




TOTAL PRESSURES



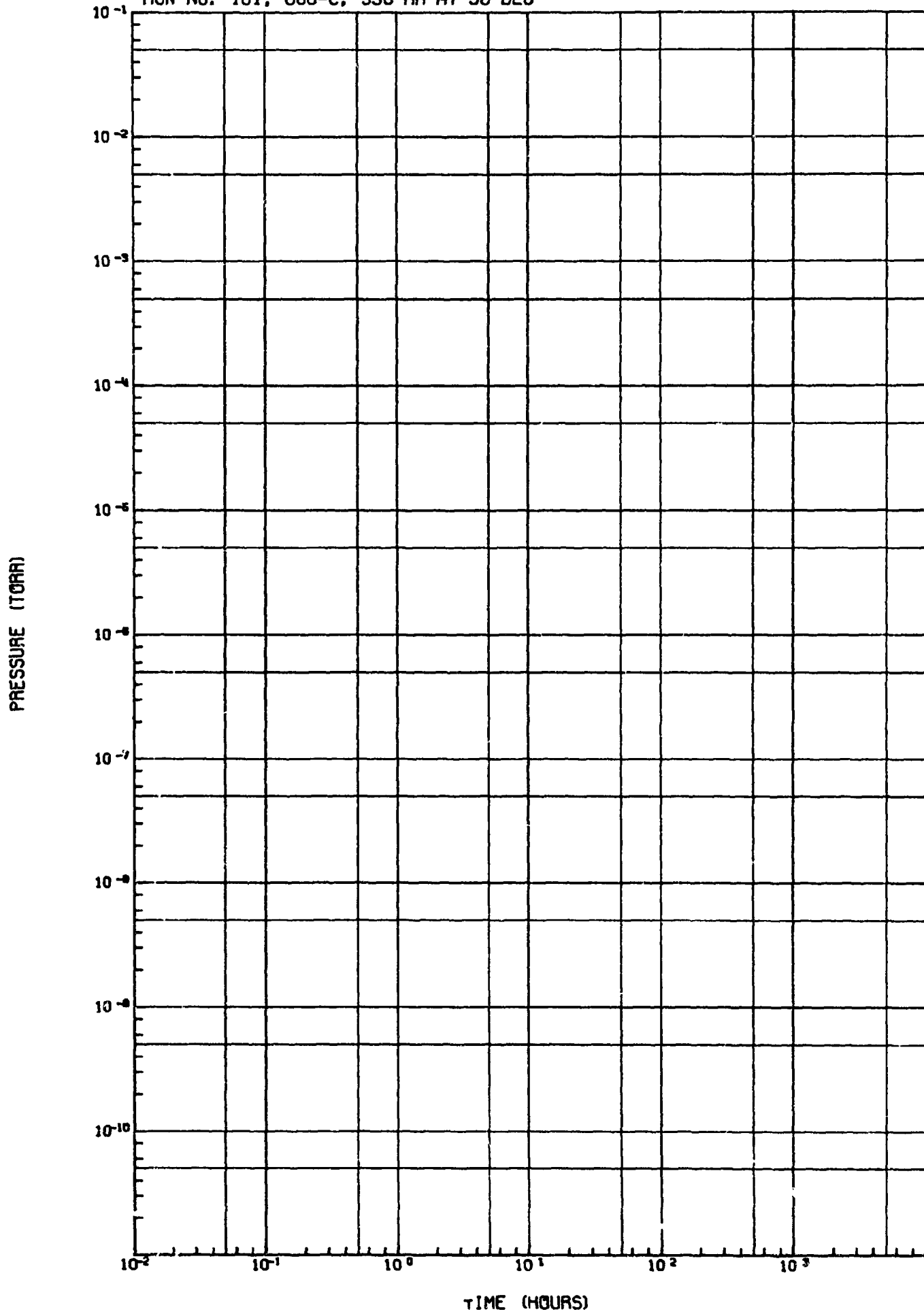




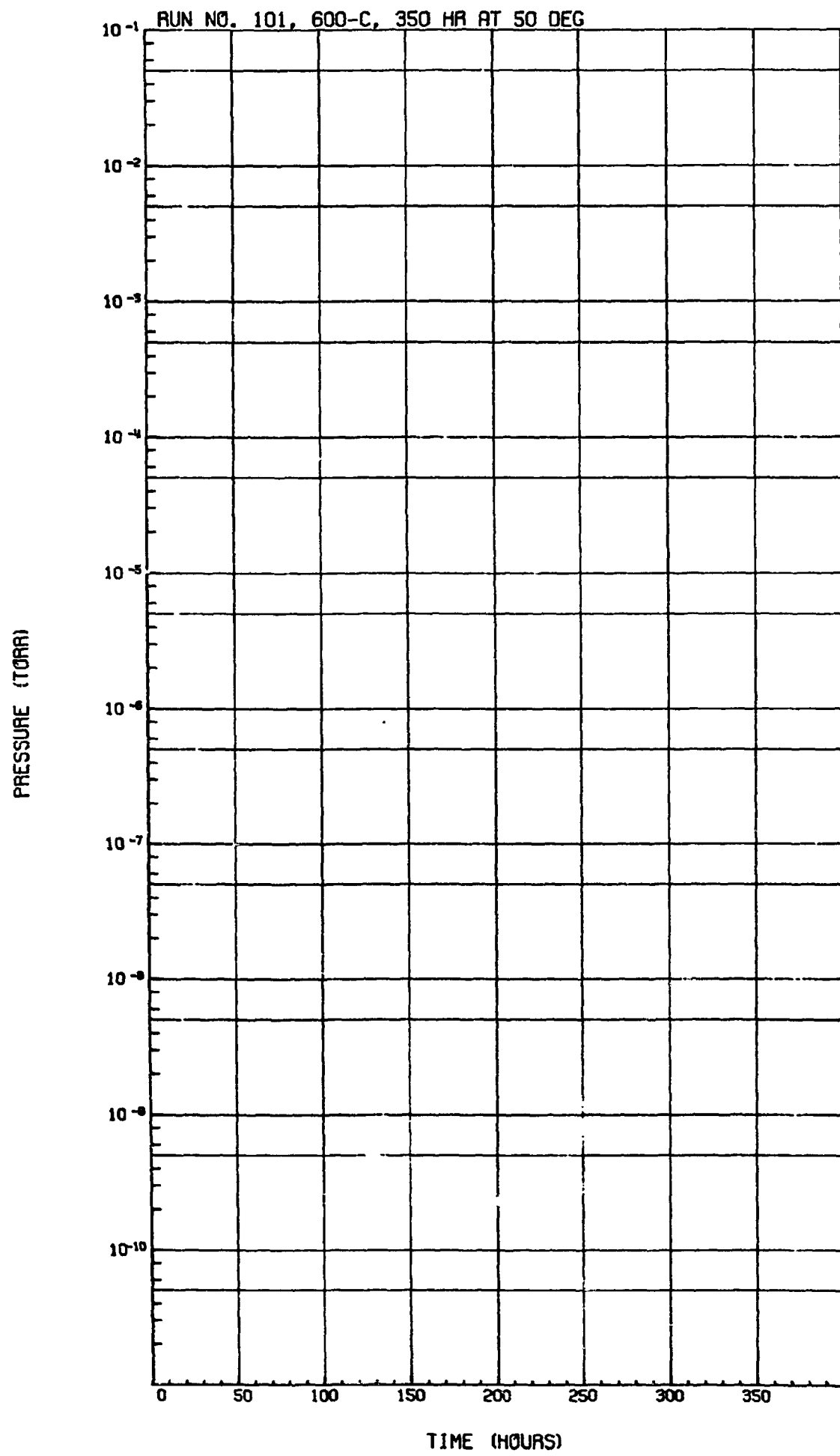
HELIUM

SLOPE = $-5.975E-05$

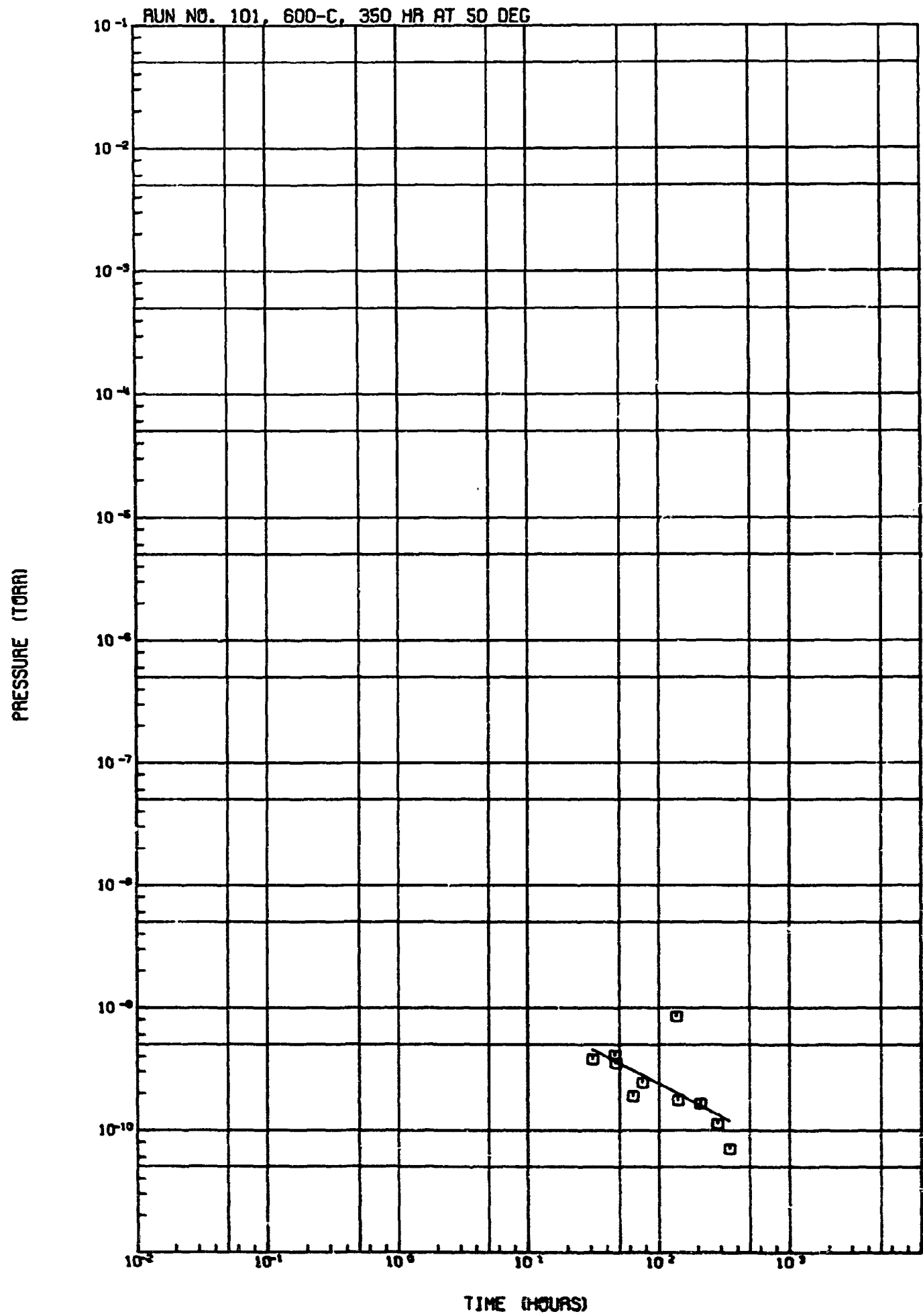
RUN NO. 101, 600-C, 350 HR AT 50 DEG



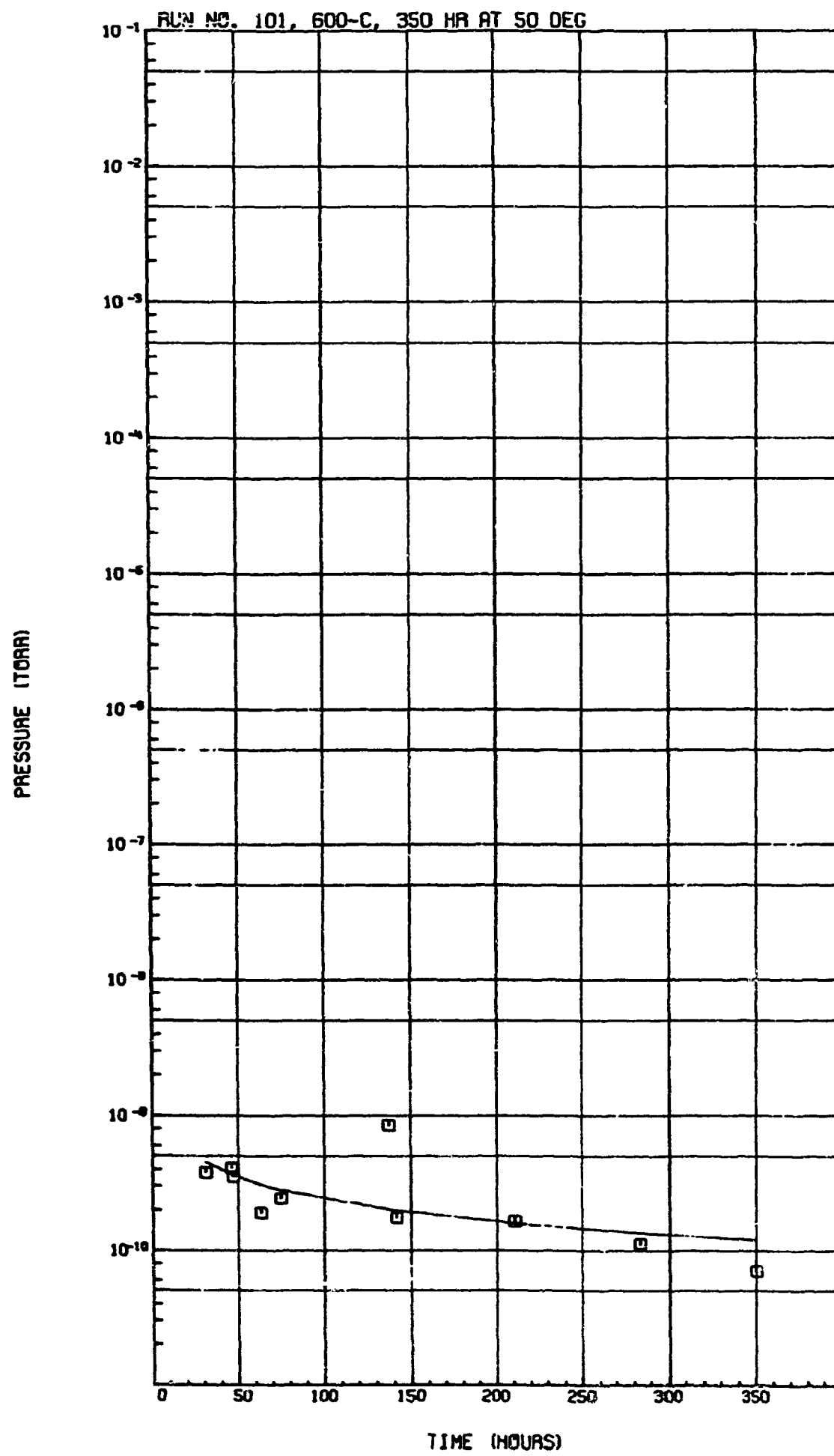
HELIUM



METHANE

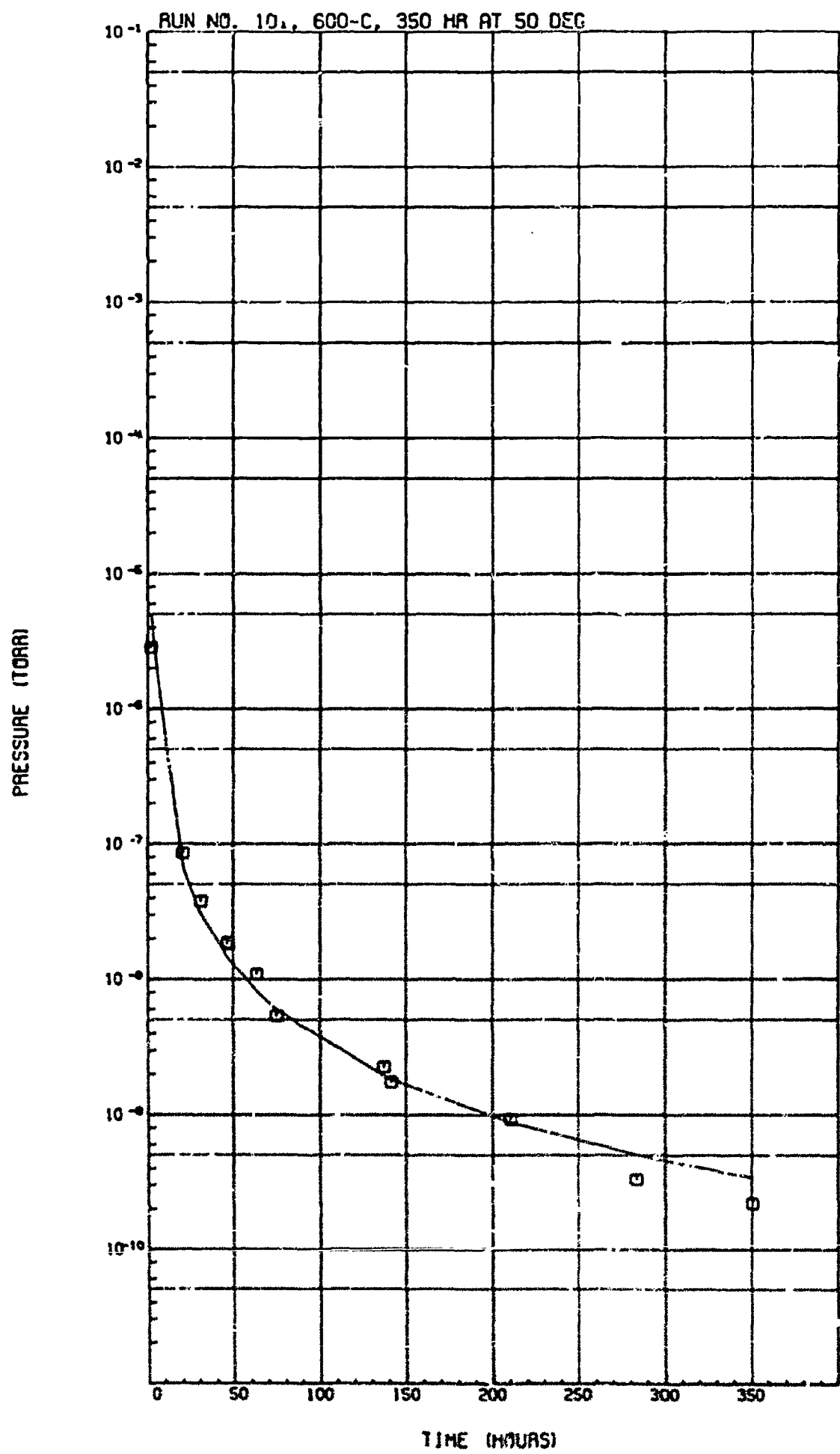
SLOPE = $-5.498E-01$ 

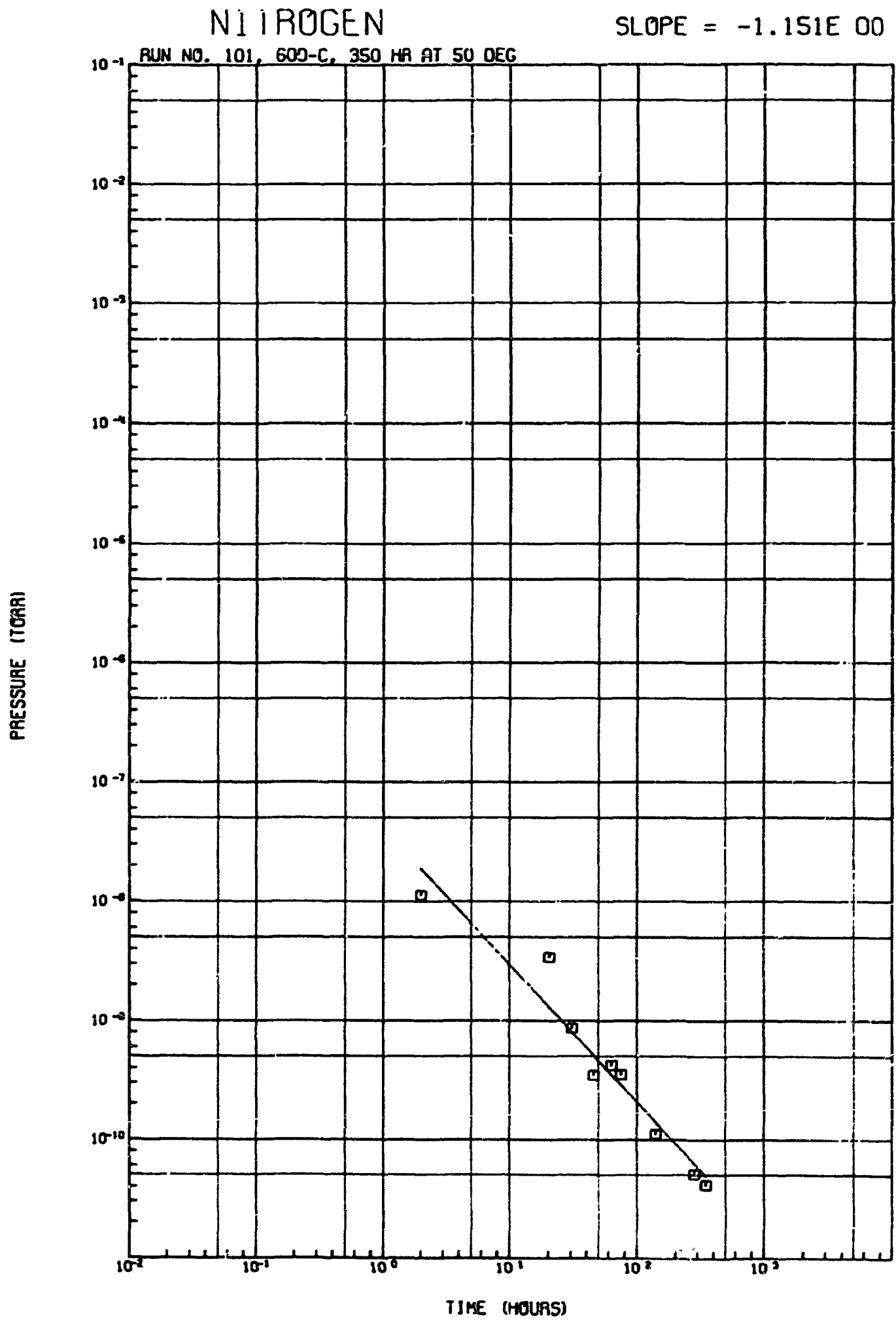
METHANE



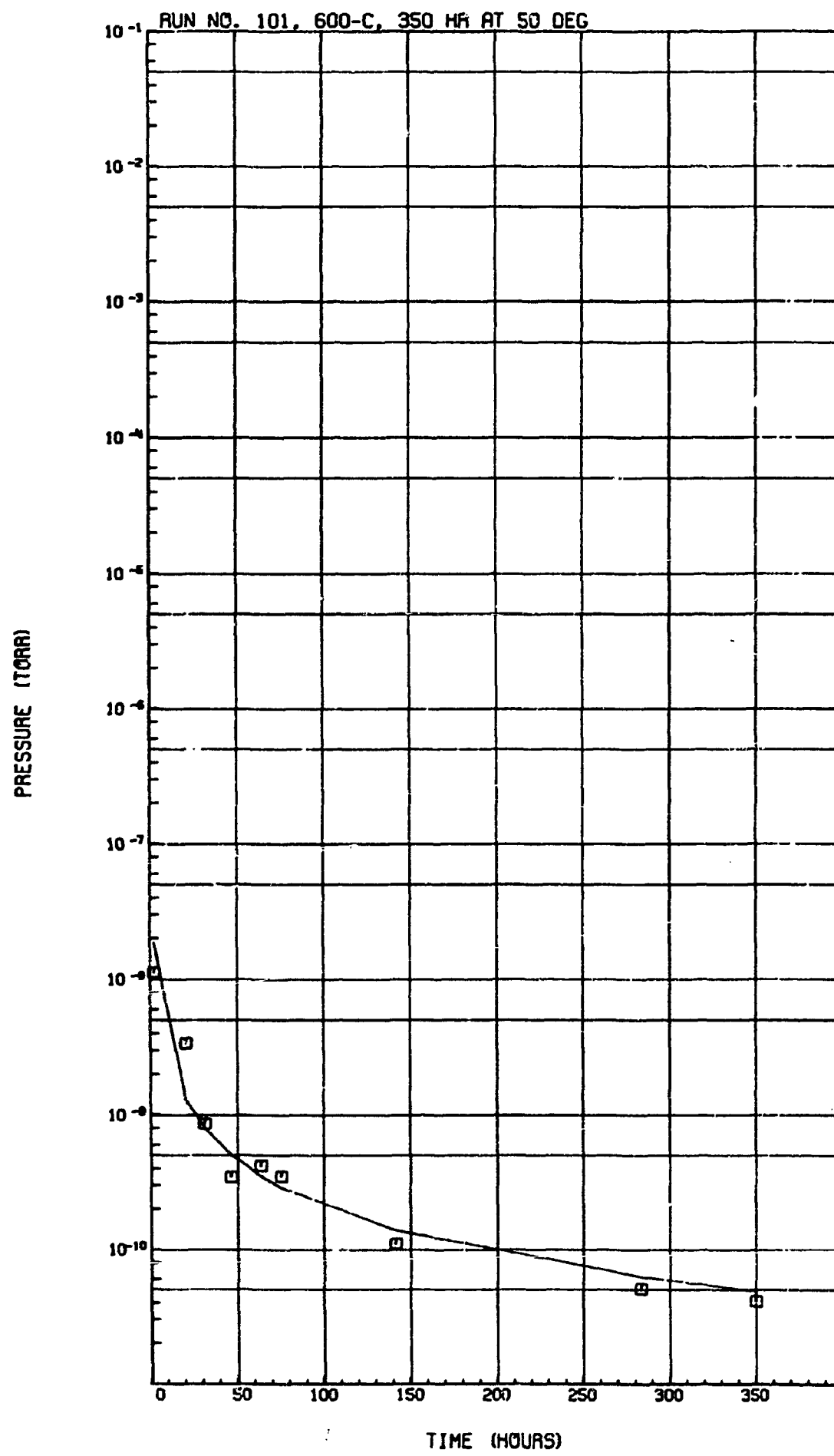


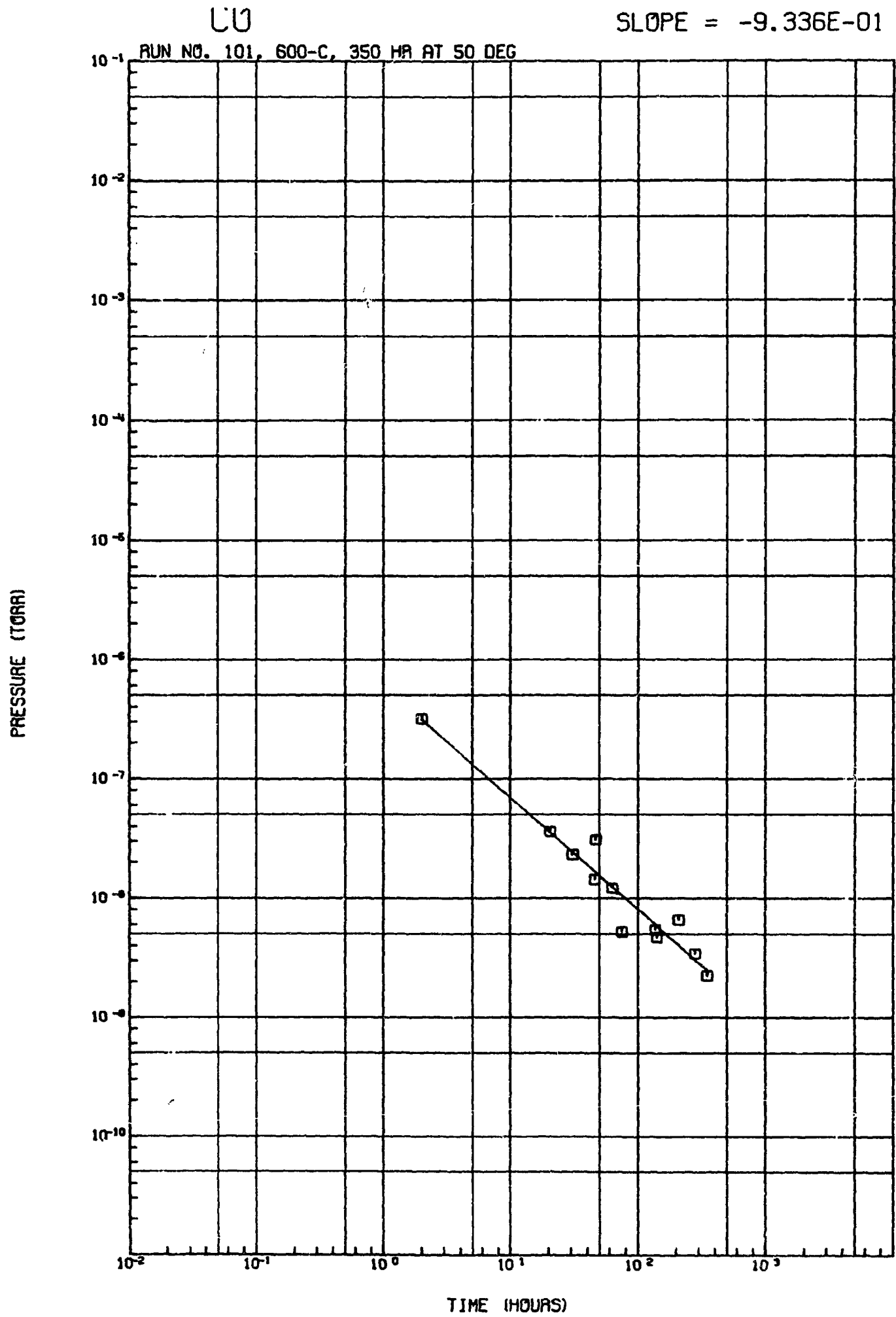
WATER VAPOR



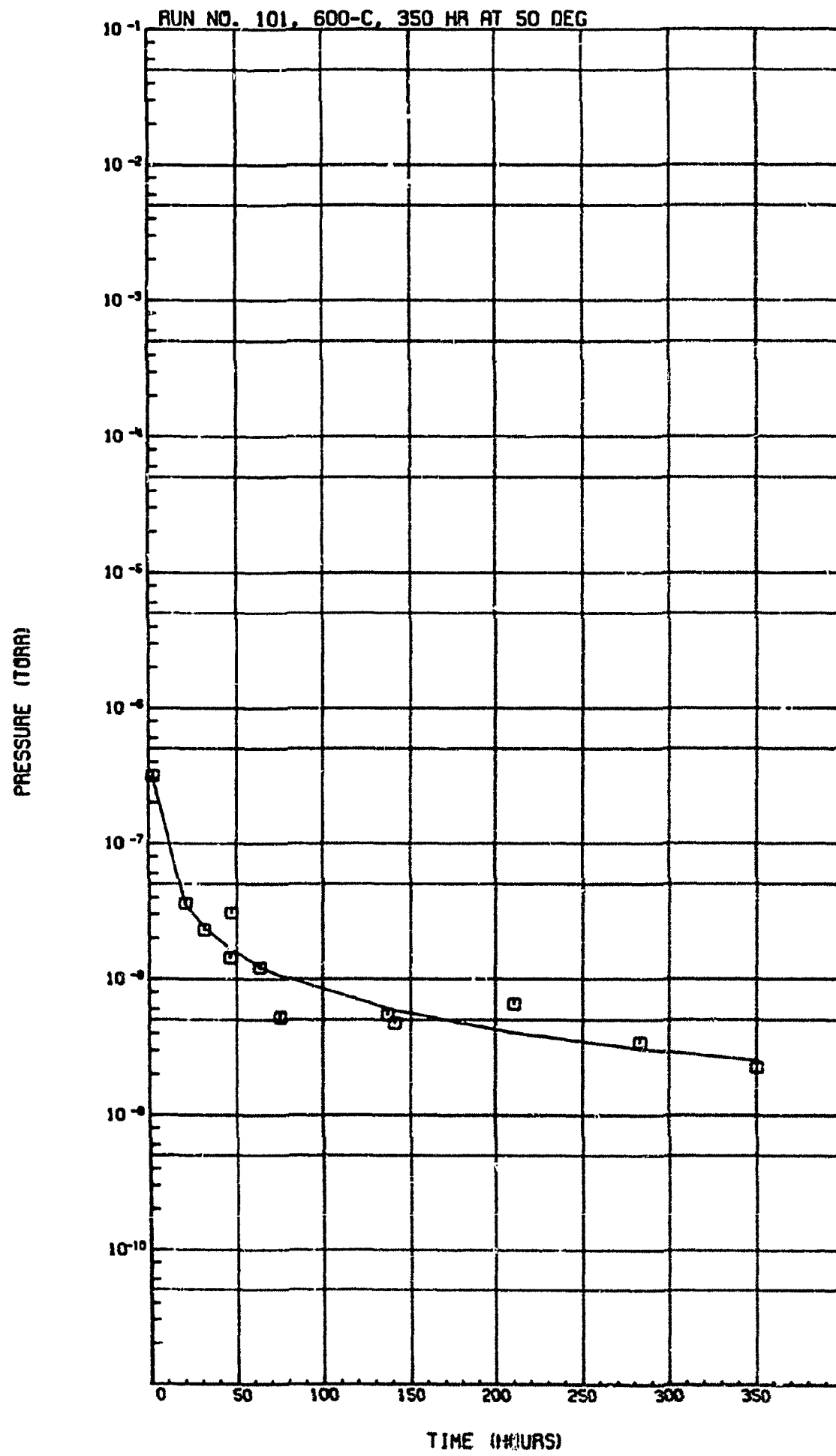


NITROGEN



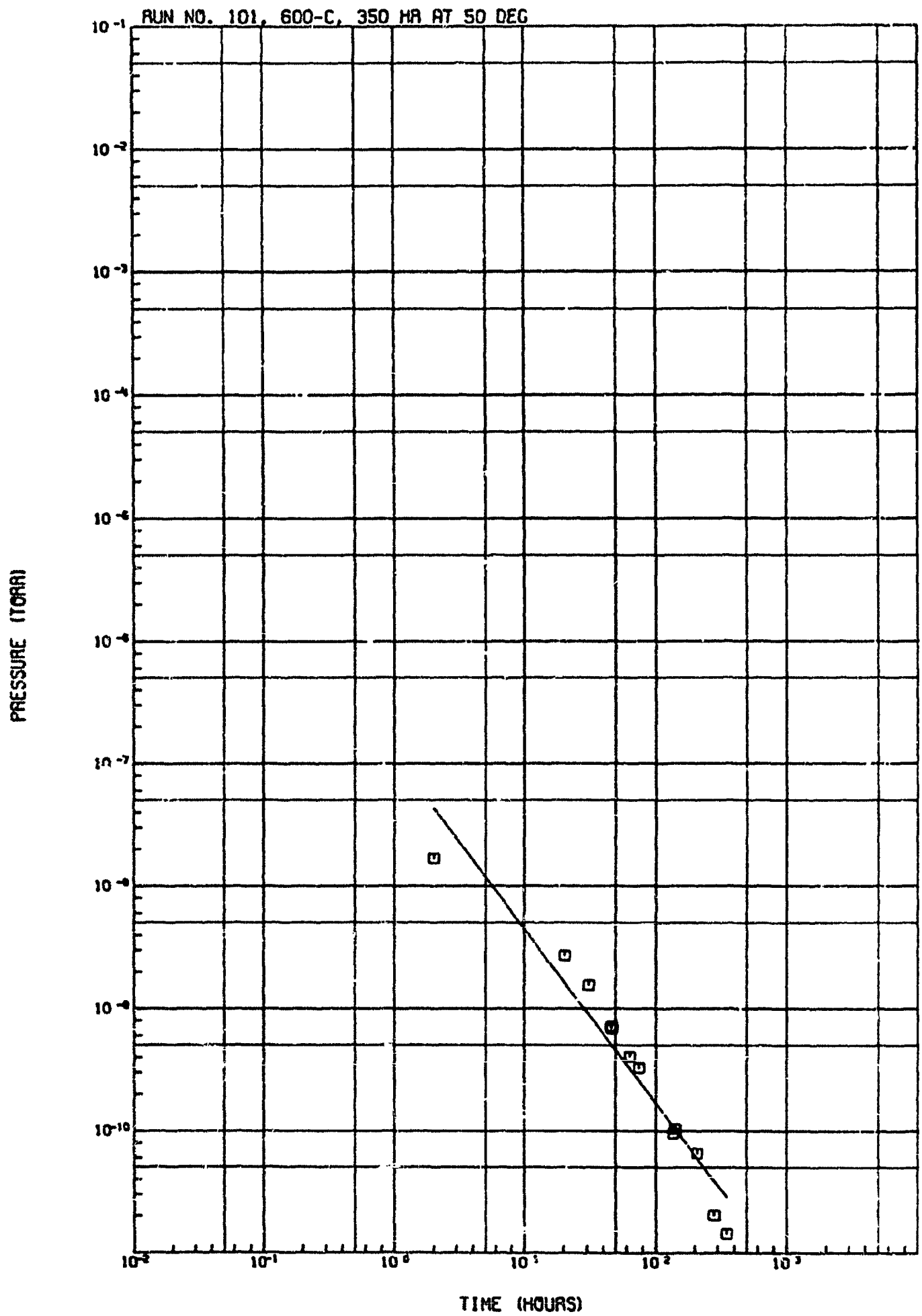


C0

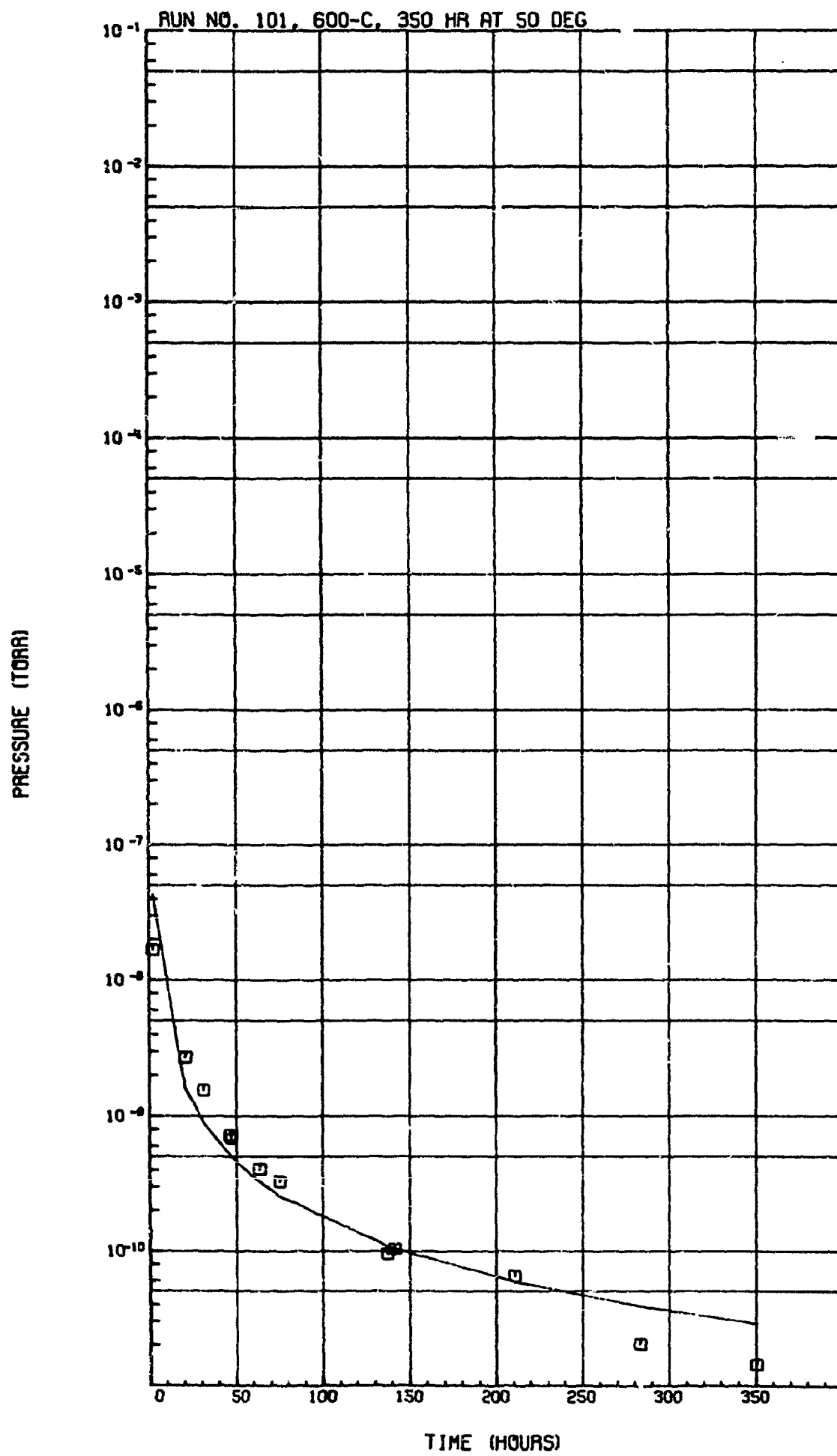


OXYGEN

SLOPE = -1.416E 00



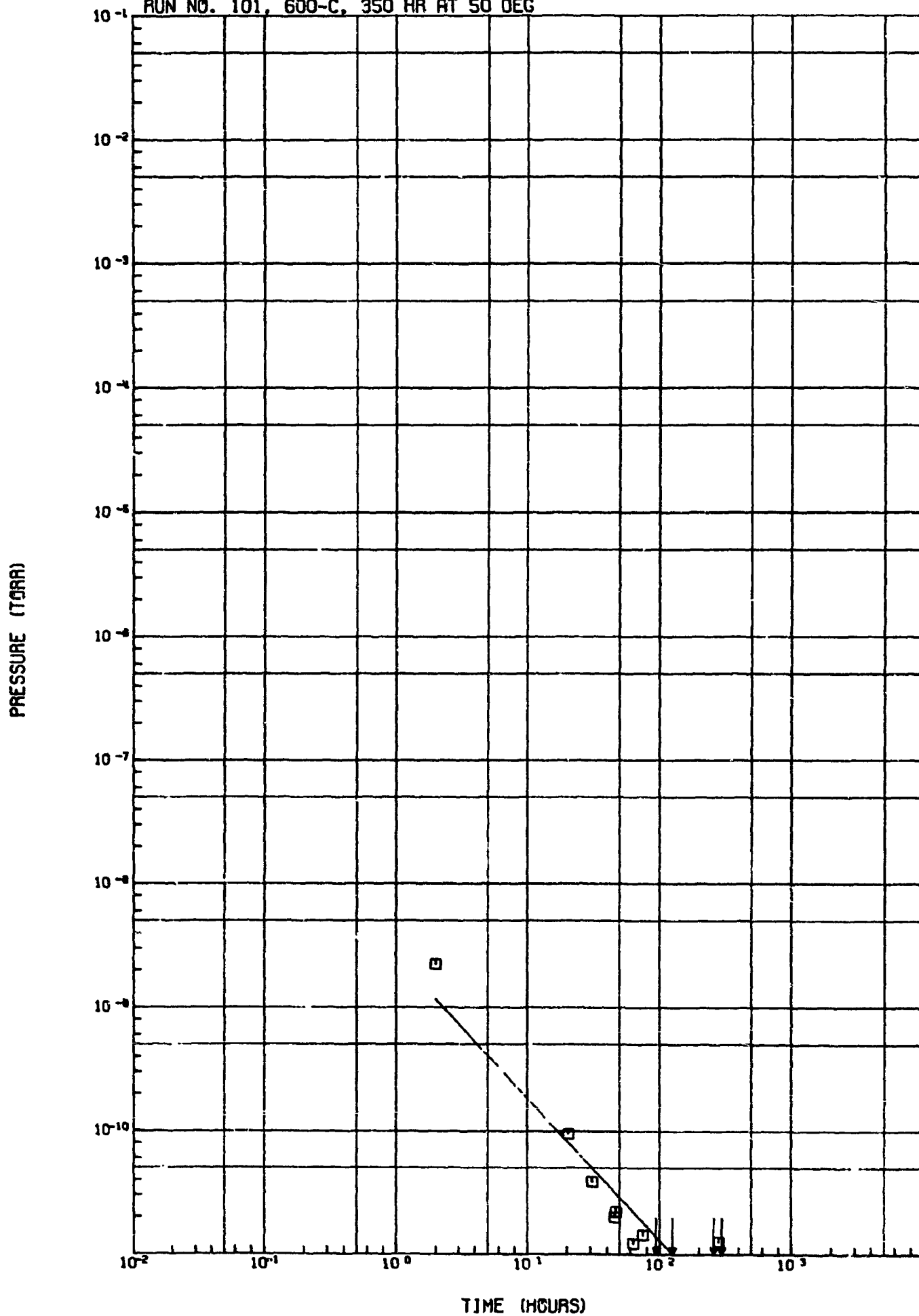
OXYGEN

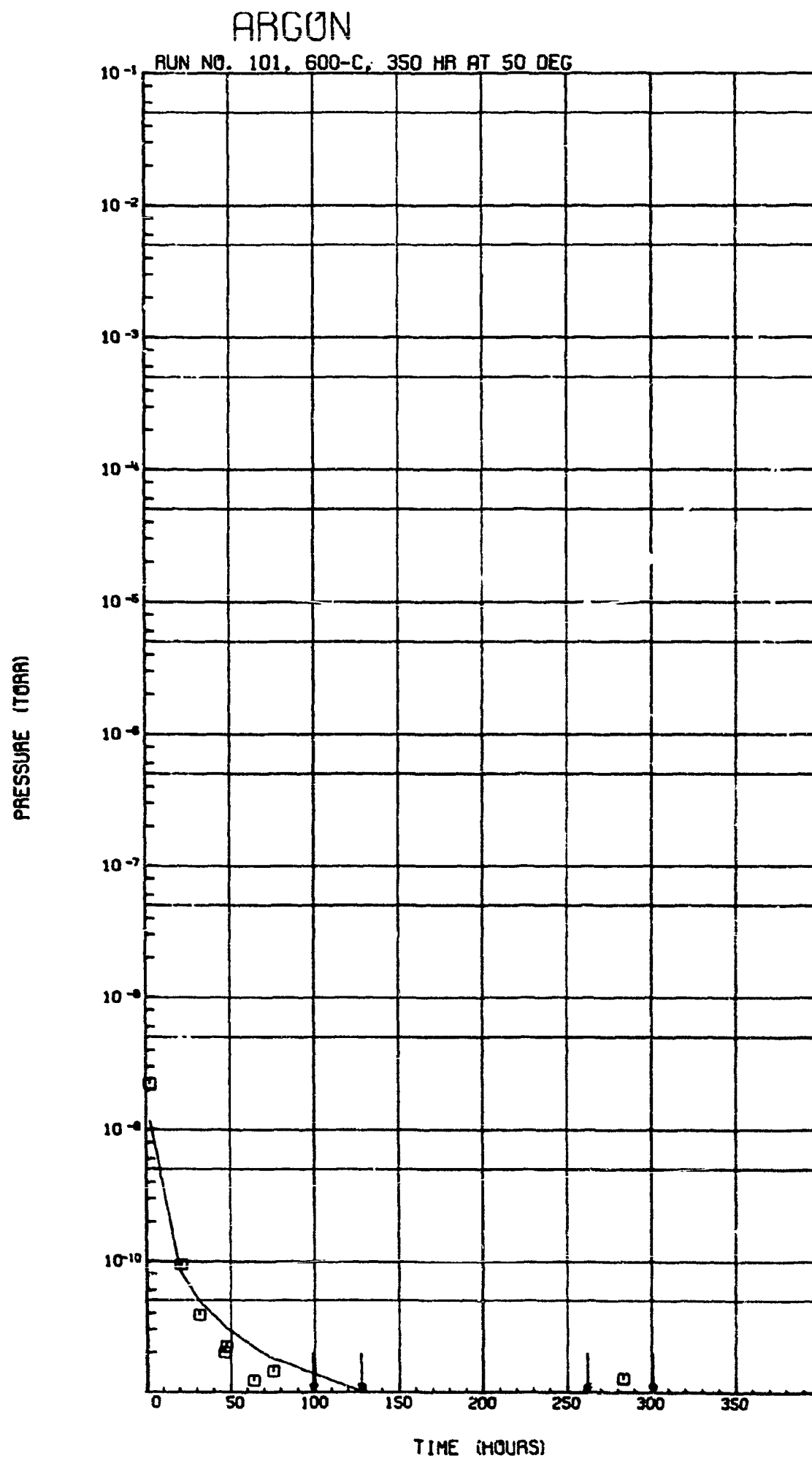


ARGON

SLOPE = -1.147E 00

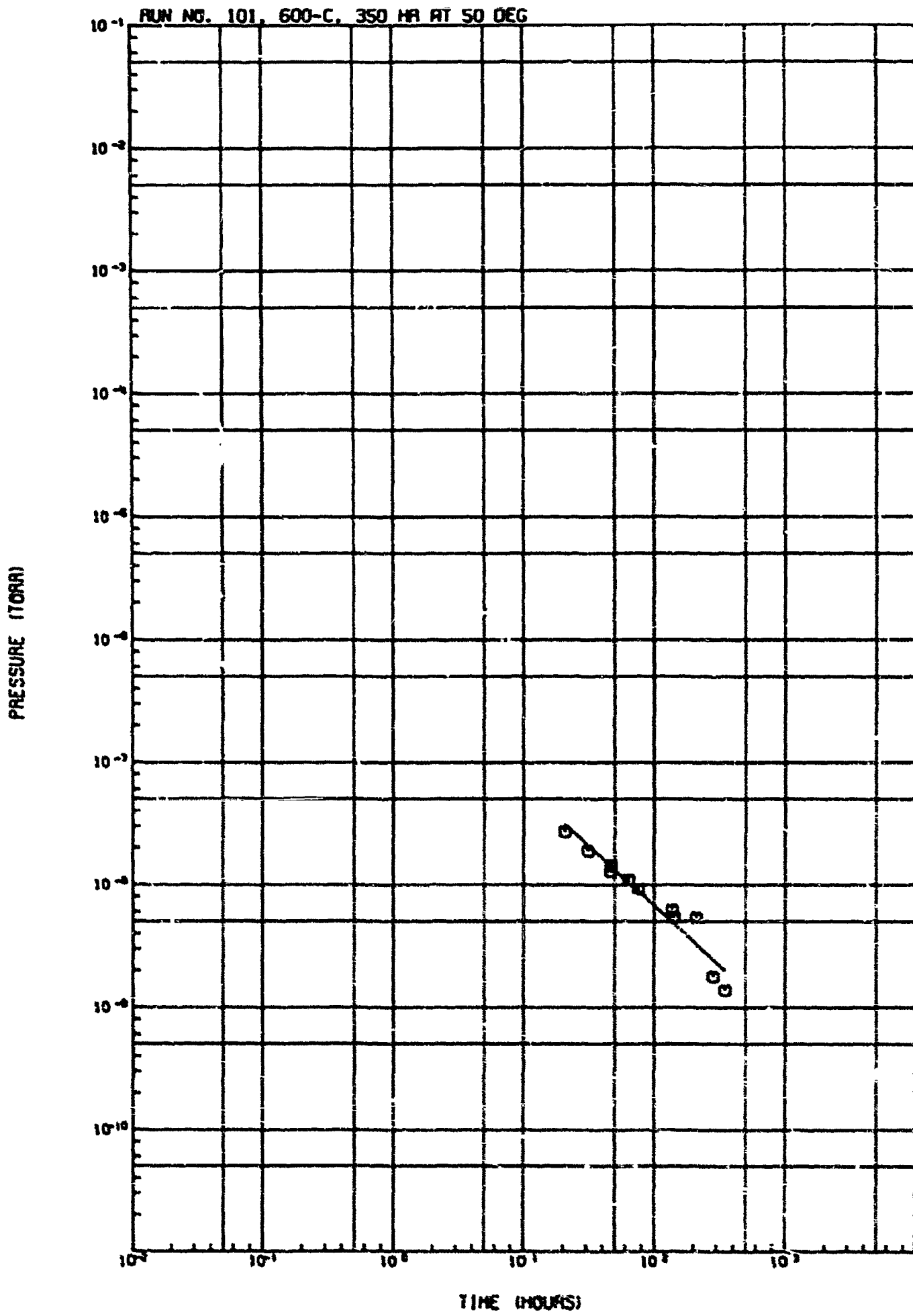
RUN NO. 101, 600-C, 350 HR AT 50 DEG



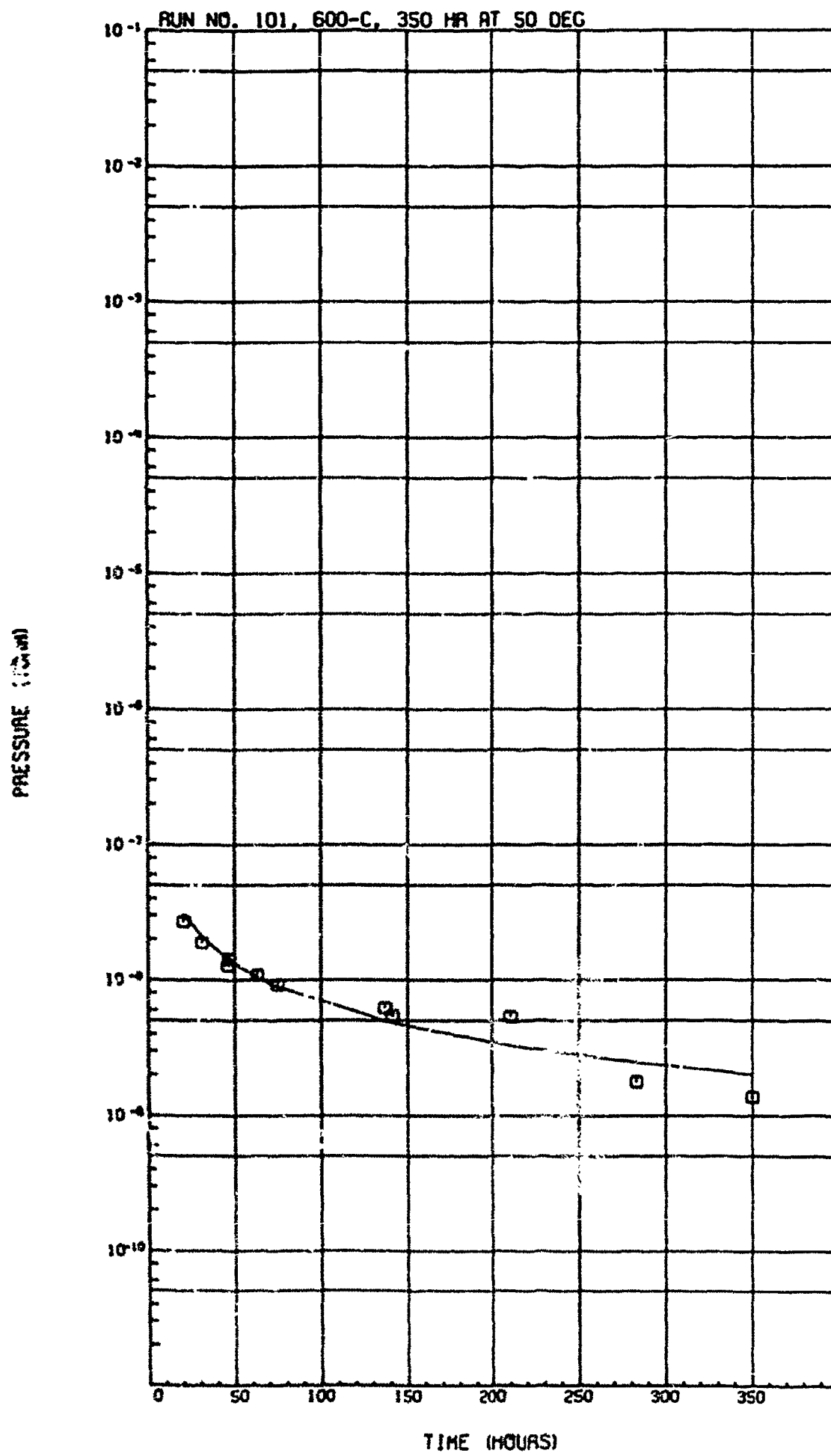


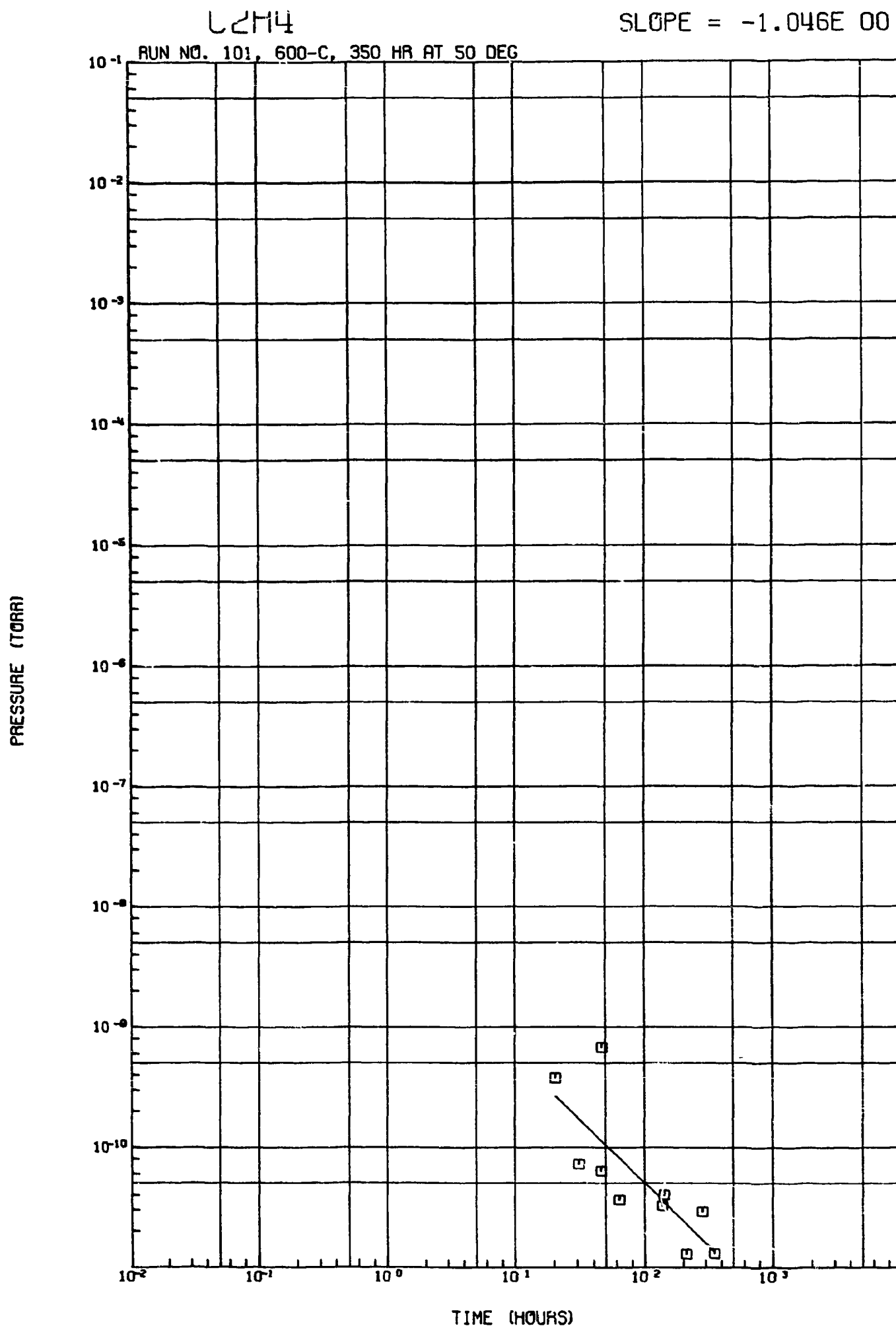
C02

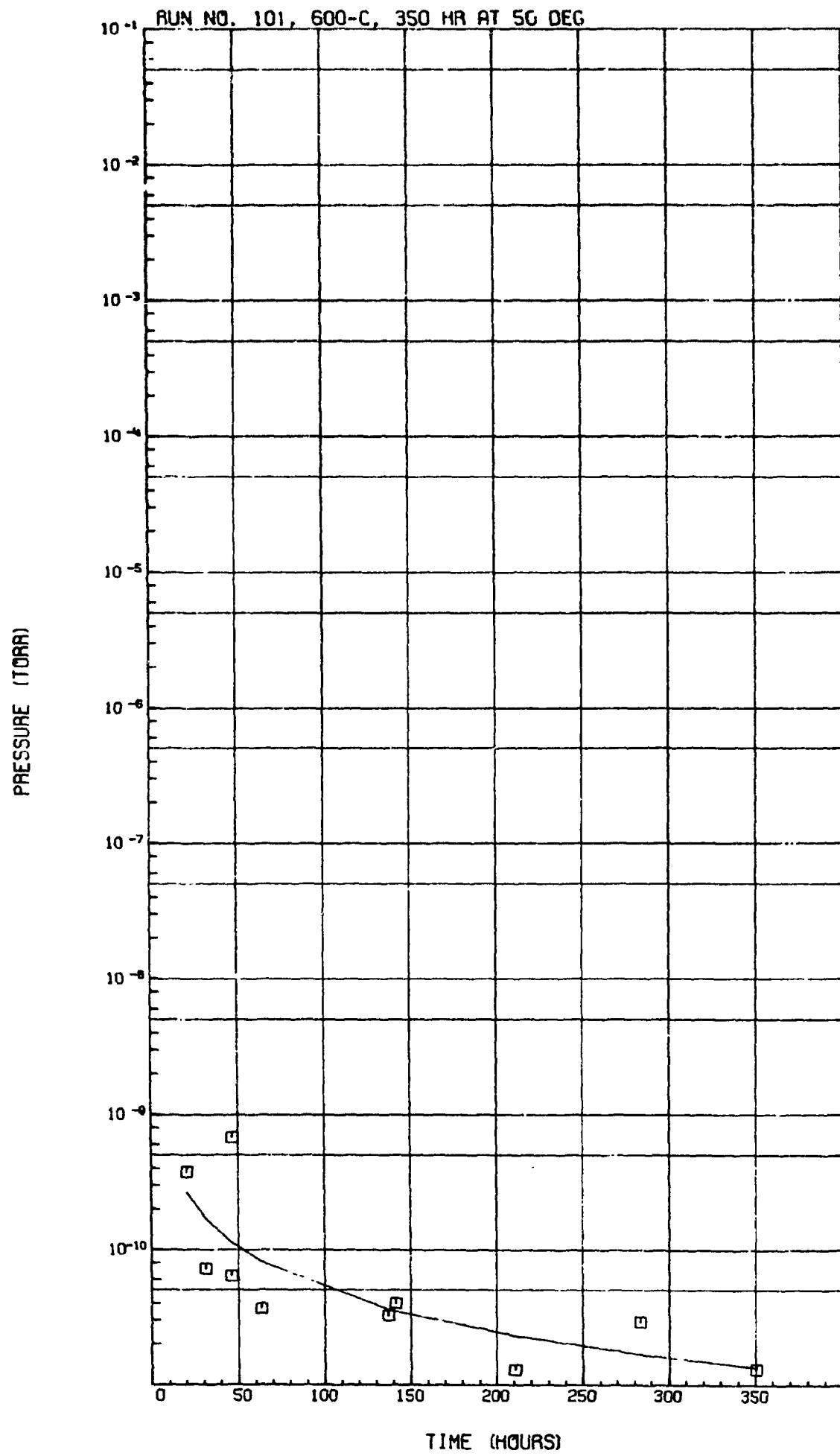
SLOPE = -9.637E-01



C02

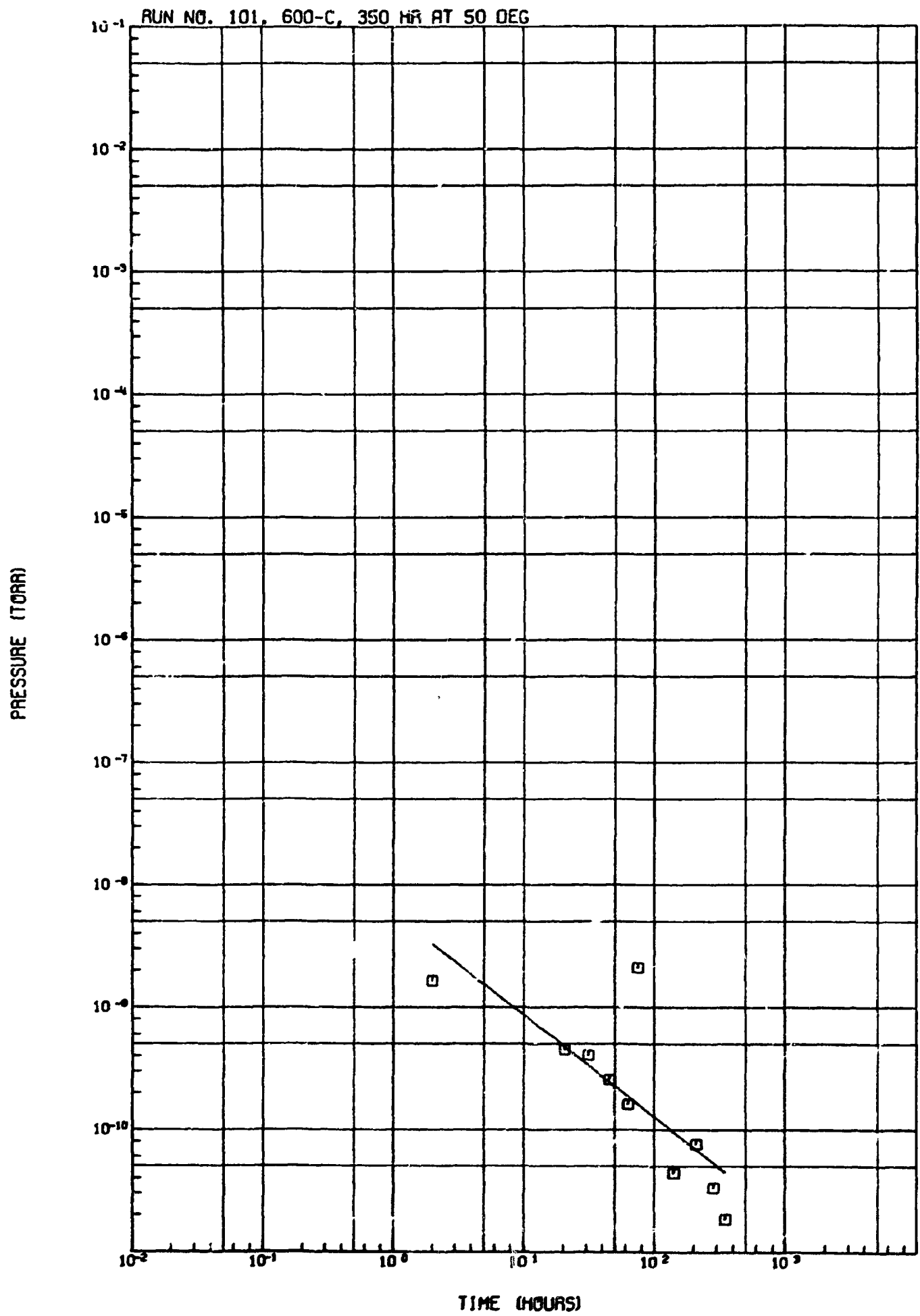




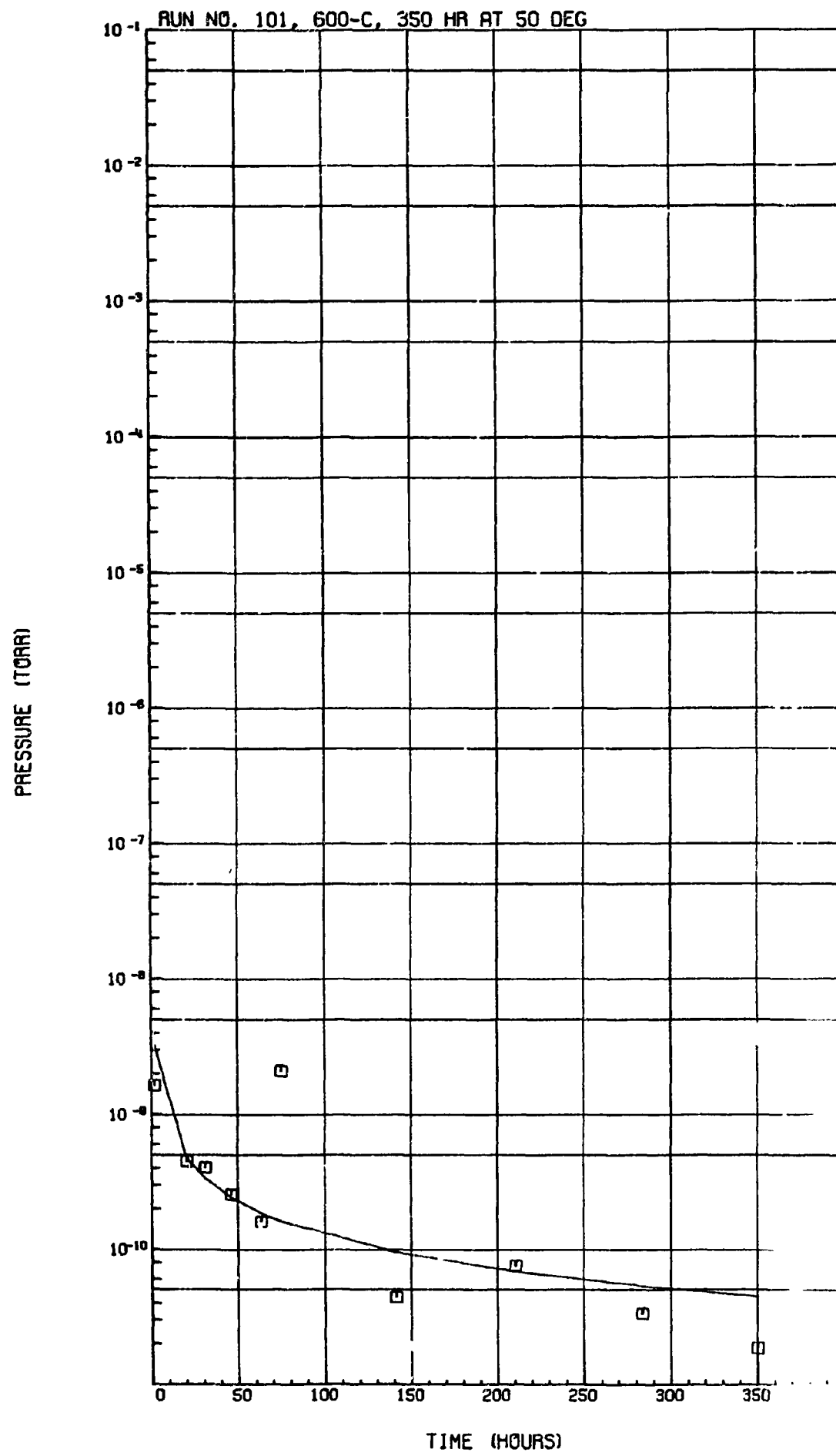
C₂H₄

C2H6

SLOPE = -8.299E-01

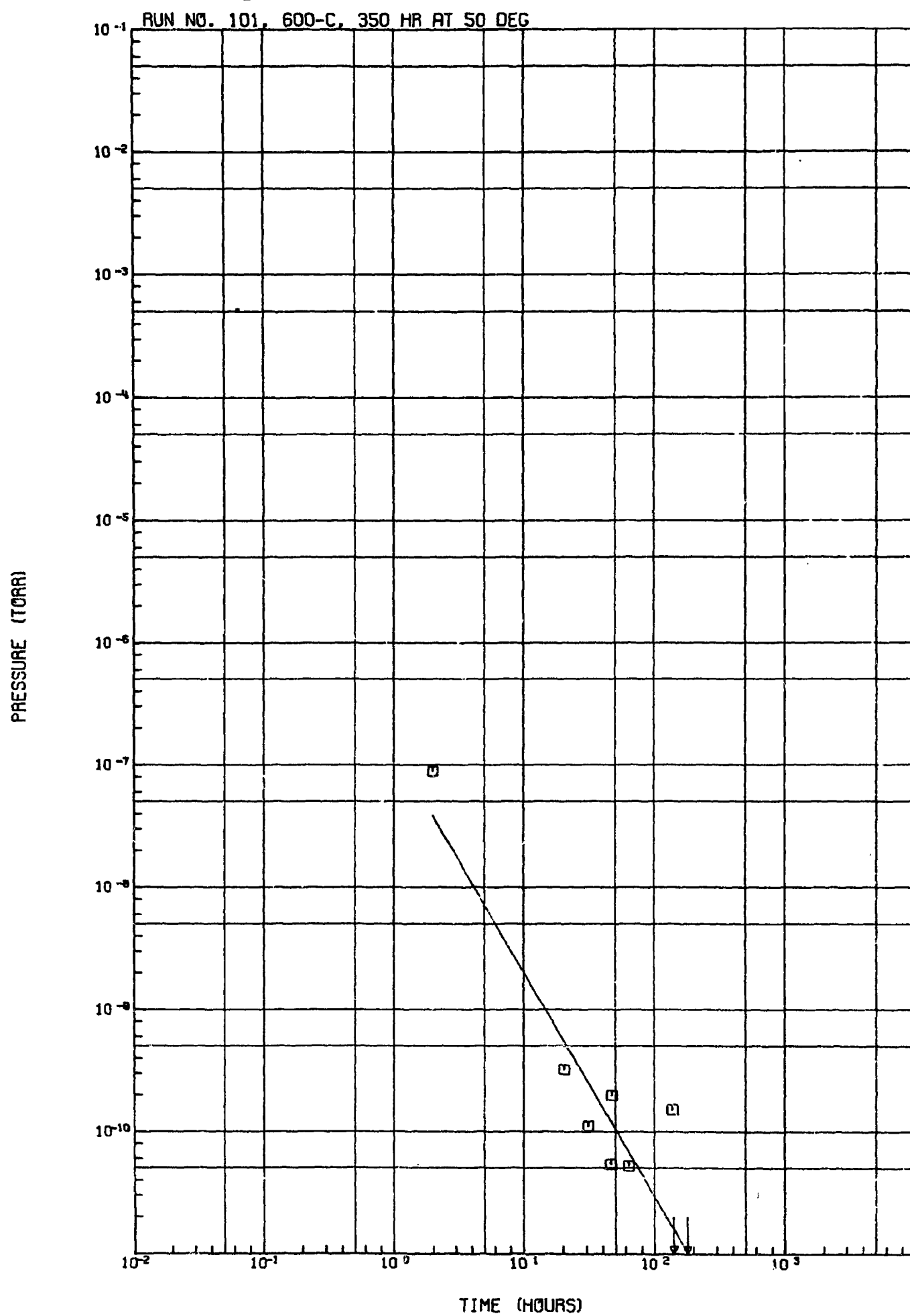


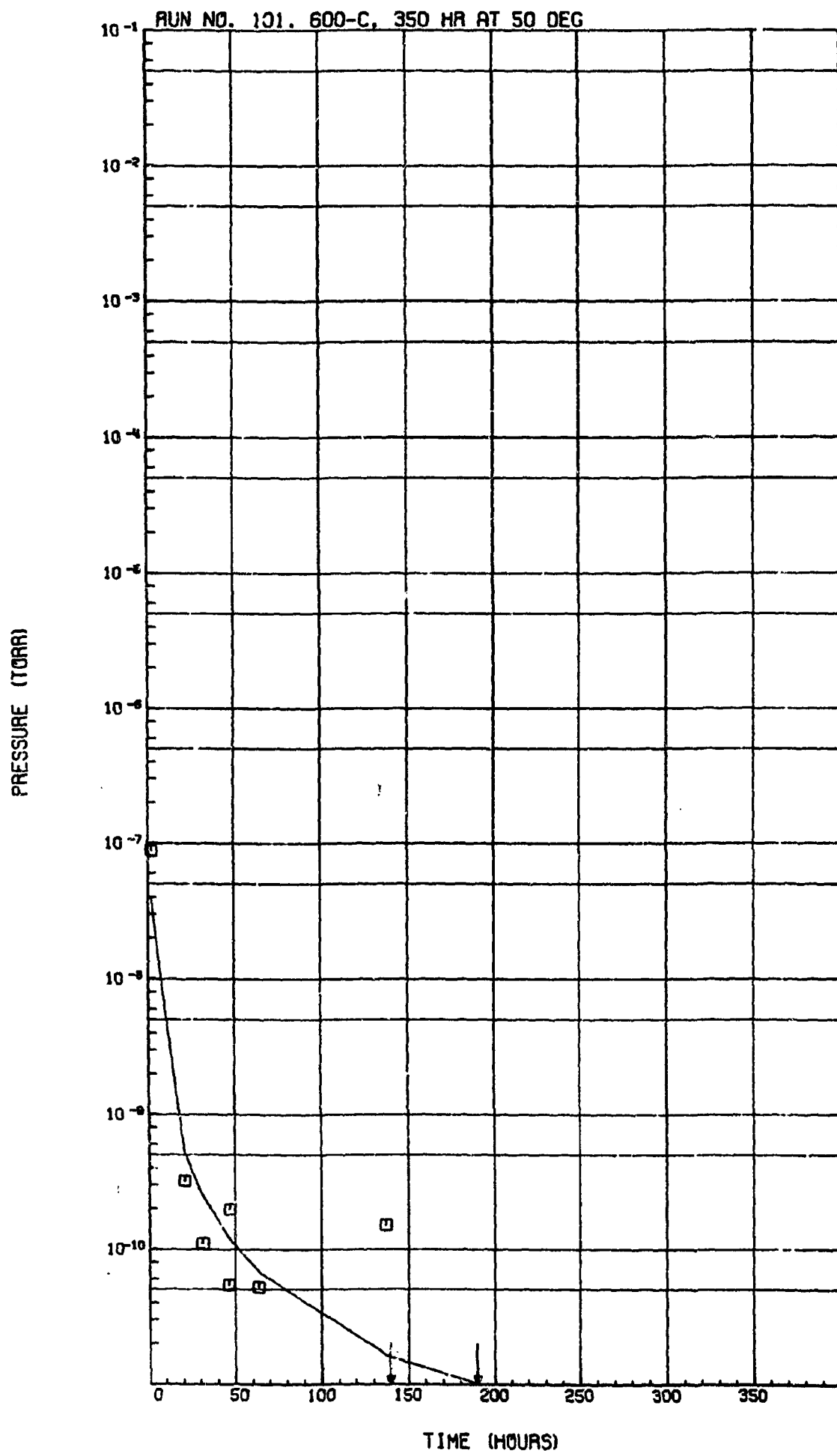
C2H6



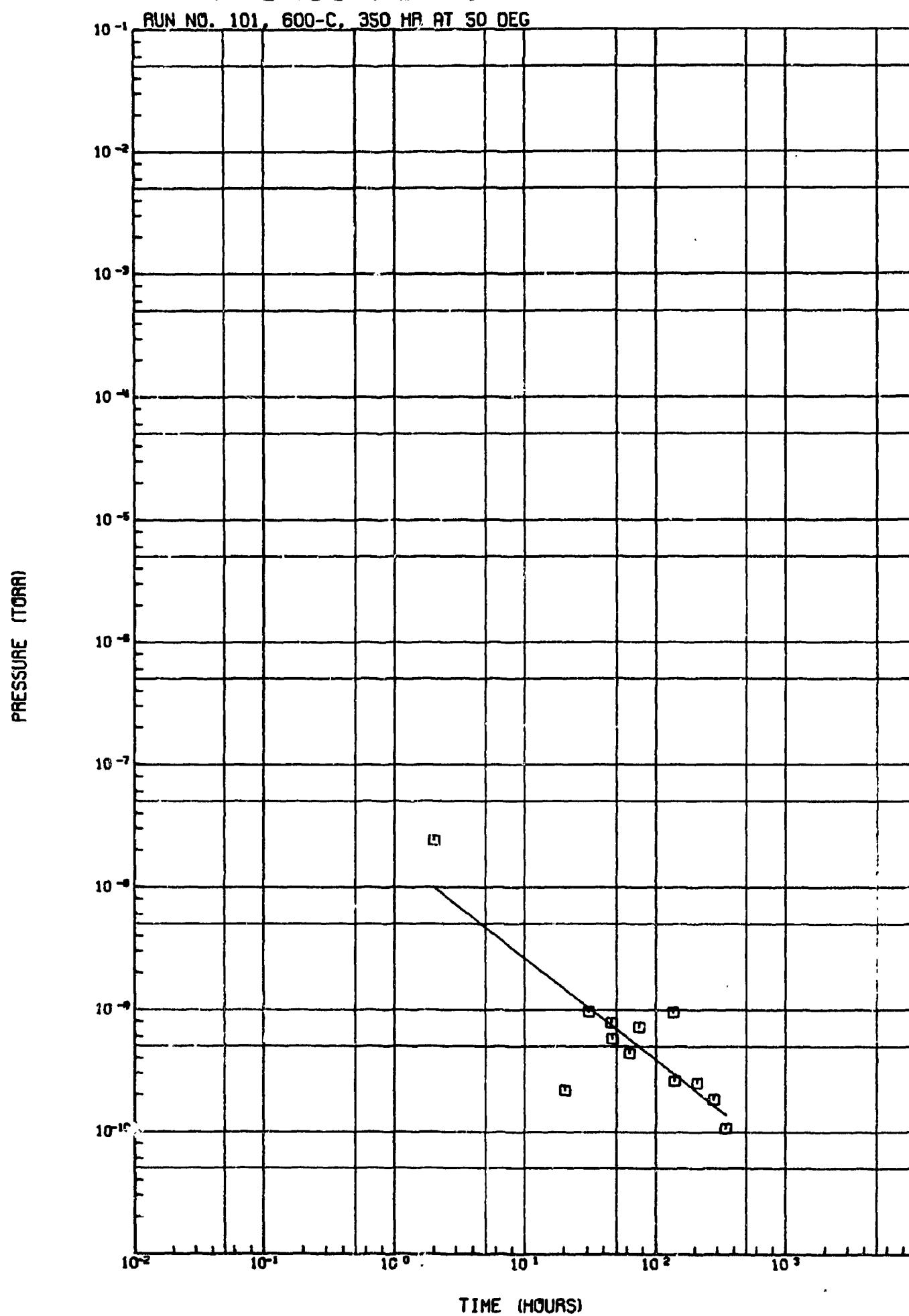
C3H8

SLOPE = -1.834E 00

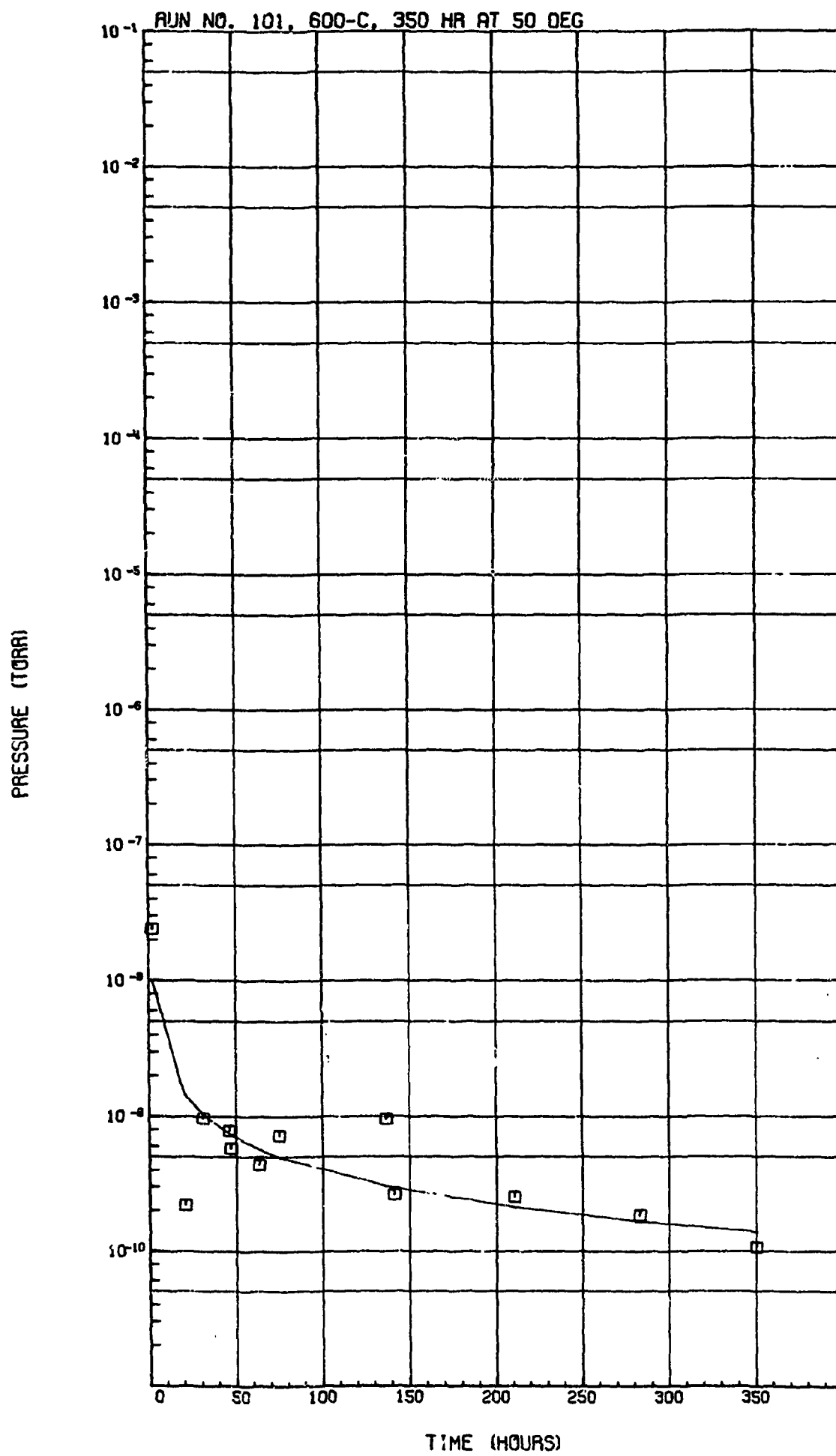


C3H8

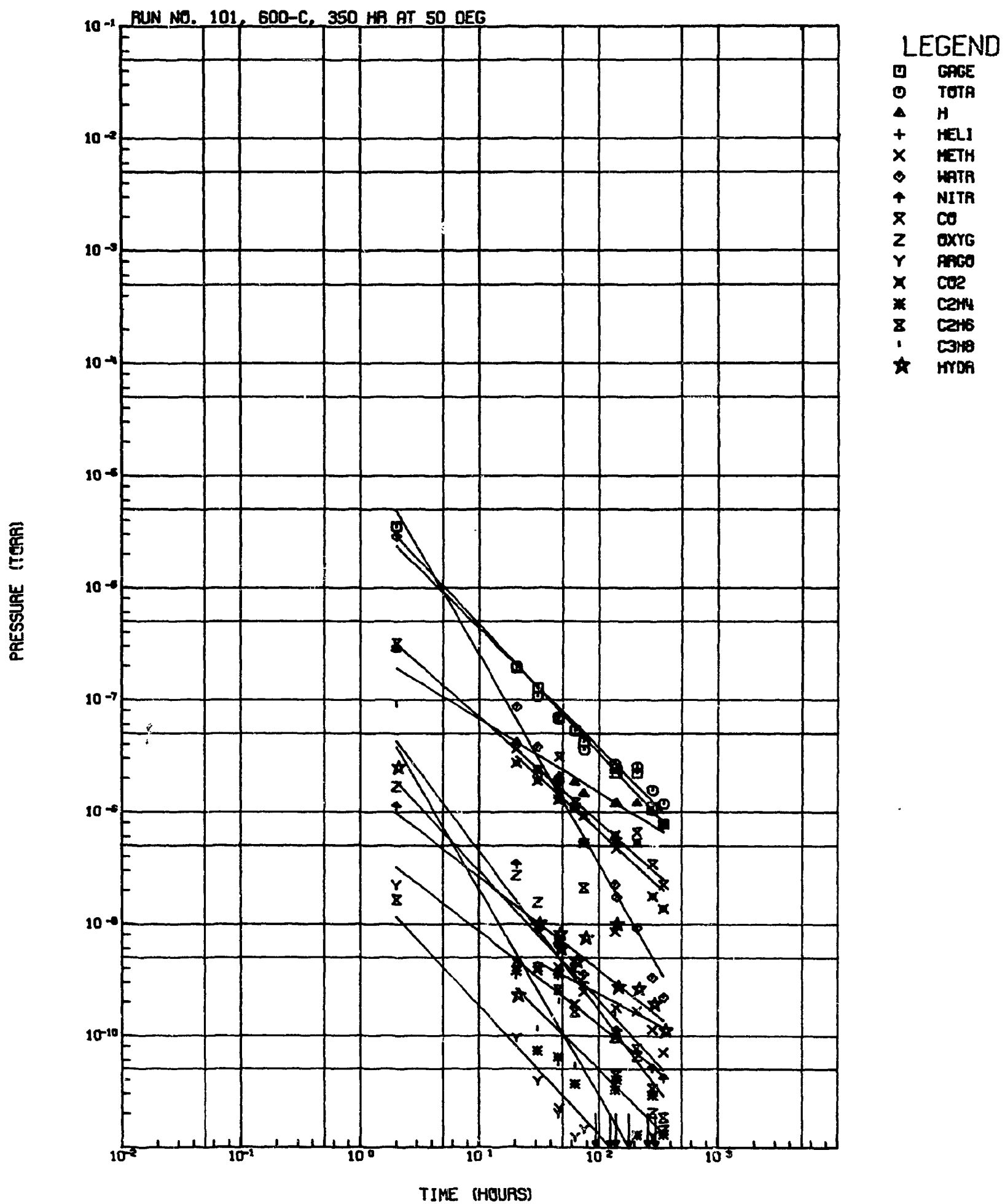
HYDROCARBONS

SLOPE = $-8.274E-01$ 

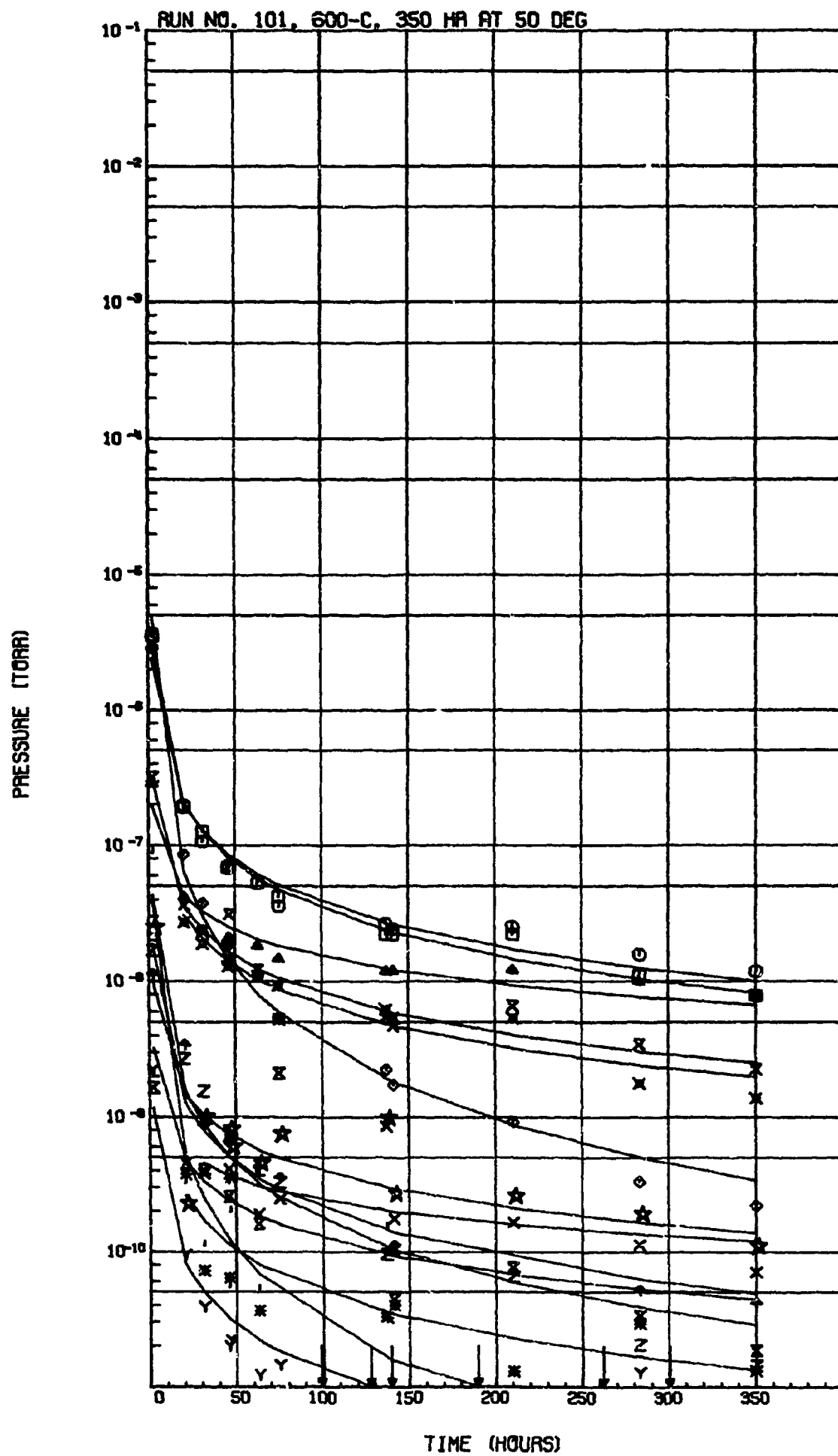
HYDROCARBONS



SELECTED GASES



SELECTED GASES



LEGEND

- GAGE
- TOTAL
- ▲ H
- + HELI
- × METH
- ◇ WATER
- * NITR
- X CO
- Z OXYG
- Y ARGO
- x CO₂
- * C₂H₄
- X C₂H₆
- C₃H₈
- ★ HYDR

APPENDIX B
PROGRAM TO USE COMPILOT

```

**FTN, L.E.G.                                KEYWORDS = IF, DO, GOTO, READ, PRINT
C      PROGRAM TO USE COMPLYOT -- SEE COMPLYOT FOR DATA INSTRUCTIONS
C
C      PLOTS OUTGASSING RATE VS TEMPERATURE FOR SEVERAL RUNS
C      ML=NUMBER OF VALUES (TOTAL, ION GAGE, HYDROCARBONS)
C
C      REAL*8 TITLE
C      DIMENSION TITLE(100)
C      DATA (TITLE=RM GAGE P1, RM, RM TOTAL, RM, RM
1          RM H, RM, RM HELIUM, RM, RM
2          RM METHANE, RM, RM
3          RM WATER V, RM, RM, RM NITROGE, RM, RM
4          RM CO, RM, RM OXYGEN, RM, RM
5          RM ARGON, RM, RM CO2, RM, RM
6          RM C2H4, RM, RM C2H6, RM, RM
7          RM C3H8, RM, RM HYDROCA, RM, RM)
C      ML=15
C      CALL COMPLYOT(TITLE, ML)
C      STOP
C      END

```

10
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95
96
97
100
110
120
130

TABLE OF VARIABLE NAMES

VARIABLE NAME	ARRAY DIMENSIONS	TOTAL NO ELEMENTS	ELEMENT TYPE	DECLARATION	CROSS REFERENCE TABLE (BY SEQUENCE NUMBERS)			
COMPLYOT				SUBROUTINE	110			
ML			INTEGER*4	LOCAL	100*	110		
TITLE	(100)	100	REAL*8	LOCAL (DATA)	70,	80,	90,	110

* = VARIABLES USED ON LEFT HAND SIDE OF EQUAL SIGN

INPUT / OUTPUT TABLE

DEFINING SEQ. NO.	I/O OPERATION	LOGICAL UNIT	I/O TYPE	FORMAT USEQ	I/O LIST
-------------------	---------------	--------------	----------	-------------	----------

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SUBROUTINE COMPL0T(TITL1,ML)
C
C THIS ROUTINE PRODUCES COMPOSITE PLOTS OF OUTGASSING VS. TEMPERATURE
C COMPILED FROM SEPARATE RUNS, EACH RUN REPRESENTING A DIFFERENT SAMPLE
C AND TEMPERATURE.
C A DESCRIPTION OF THE VARIABLES USED IS
C P13--NUMBER OF RUNS
C ML--NUMBER OF PLOTS, WHICH IS EQUAL TO THE NUMBER OF GASES +3
C (TOTAL, ION GAGE, AND HYDROCARBONS)
C T--NUMBER OF TIME POINTS CONSIDERED. 10 IS THE MAXIMUM.
C L--SET TO 0 FOR POINTS TO BE CONNECTED BY A LINE.
C SET TO -1 FOR POINTS ONLY.
C IPLOT--SET TO 1 TO OBTAIN PLOTS OF RATE VS. 1/TEMPERATURE.
C SET TO 0 OR LEAVE BLANK FOR NO 1/T PLOT
C TIME--ARRAY WHICH CONTAINS THE TIME POINTS (IN HOURS) TO COMPARE
C EACH RUN.
C TEMP--TEMPERATURE OF EACH RUN
C A,B--VARIABLES FROM EQUATION Y=A*X**B. READ IN FOR EACH GAS TO
C COMPUTE OUTGASSING RATE AS A FUNCTION OF TIME.
C INPUT CONSISTS OF THE FOLLOWING CARDS OR SETS OF CARDS.
C THESE CARDS FOLLOW THE CONTROL CARD
C //GO.FT50F001 DD *
C
C 1. 1 CARD CONTAINING THE INTEGER VALUES OF P13,T,L,IPLOT IN COLUMNS
C 5,10,15, AND 20 RESPECTIVELY.
C 2. 1 CARD CONTAINING THE SELECTED TIME POINTS IN HOURS.
C COLUMNS OF 10 (RIGHT ADJUSTED), 5 PER CARD.
C 3. A SET OF CARDS FOR EACH RUN CONTAINING
C A. TITLE CARD. COLUMNS 1-80.
C B. TEMPERATURE IN DEGREES C. COLUMN 8, RIGHT ADJUSTED.
C C. SET OF CARDS CONTAINING M(NUMBER OF GASES) + 3 SETS OF
C VALUES OF A AND B, ALTERNATELY ENTERED IN COLUMNS OF 8,
C 10 PER CARD.
C THIS CONCLUDES DATA AND THE LAST 2 CARDS IN THE DECK ARE THE FOLLOWING
C CONTROL CARDS
C /*
C //
C
C INTEGER P13,T
C REAL * 8 TITL1,PUNT11,T2,XTITLE
C DATA (XTITLE(1)=8HTEMPERAT,8HURE(C.),8H1/TEMPER,8HATURE(K.,8H)$
C 1
C )
C DIMENSION TITL1(100),PUNT11(10,100),A(15,100),B(15,100),TEMP(100),
C 10(100,10),TIME(10),MILQ(2),XHILO(4),BUF(3000),INDEX(7),D1(100,10)
C 2,02(10),TEM1(20),TEM2(200),XTITLE(10),JSYM(11),LNTHS(10)
C READ 1,P13,T,L,IPLOT
C 1 FORMAT (4I5)
C READ 2,(TIME(I),I=1,T)
C 2 FORMAT (5F10.0)
C PRINT 3,P13
C 3 FORMAT (1H1,54X,1H*** COMPOSITE DATA ***1//46V,1HTHE NUMBER OF EXPERCCMP 500
C 1MENTAL RUNS IS ',I3//)
C DO 100 I=1,T
C JSYM(I)=2
C LNTHS(I)=2
C JSYM(T+1)=-1
C CALL QQQCPA(5,5,1)
C CALL QQQCPA(20,0)
C DO 105 J=1,P13
C READ 4,(PUNT11(I,J),I=1,10)
C 4 FORMAT (10A8)
C CALL REPLACE(PUNT11(I,J),20,1,'$')
C 105 READ 5,TEMP(I),(A(I,J),B(I,J),I=1,ML)
C 5 FORMAT (E8.2/(10E8.2))
C
C ARRANGE TEMPERATURES IN ASCENDING ORDER.
C
C IP13=P13-1
C DO 125 I=1,IP13
C IP1=I+1
C DO 125 J=IP1,P13
C IF (TEMP(I)-TEMP(J))126,125,11C
C 110 T1=TEMP(I)
C TEMP(I)=TEMP(J)
C TEMP(J)=T1
C DO 115 K=1,10
C T2=PUNT11(K,I)
C PUNT11(K,I)=PUNT11(K,J)
C 115 PUNT11(K,J)=T2
C
C DO 120 K=1,ML
C T1=A(K,I)
C A(K,I)=A(K,J)
C A(K,J)=T1
C T1=B(K,I)
C B(K,I)=B(K,J)
C 120 B(K,J)=T1
C 125 CONTINUE
C
C COMPL 10
C COMPL 20
C COMPL 30
C COMPL 40
C COMPL 50
C COMPL 60
C COMPL 70
C COMPL 80
C COMPL 90
C COMPL 100
C COMPL 110
C COMPL 120
C COMPL 130
C COMPL 140
C COMPL 150
C COMPL 160
C COMPL 170
C COMPL 180
C COMPL 190
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C COMPL 660
C COMPL 670
C COMPL 680
C COMPL 690
C COMPL 700
C COMPL 710
C COMPL 720
C COMPL 730
C COMPL 740
C COMPL 750
C COMPL 760
C COMPL 770
C COMPL 780
C COMPL 790
C COMPL 800
C COMPL 810
C COMPL 820
C COMPL 830
C COMPL 840
C COMPL 850

```

*** STATEMENT 285 + ? ERROF DAD2

TABLE OF VARIABLE NAMES

VARIABLE NAME	ARRAY DIMENSIONS	TOTAL NO ELEMENTS	ELEMENT TYPE	DECLARATION	CROSS REFERENCE TABLE (BY SEQUENCE NUMBERS)						
A	(15,100)	1500	REAL*4	LOCAL	440, 1230,	610, 1280	790,	800*	810*	930,	940,
ADVANS				SUBROUTINE	1540						
B	(15,100)	1500	REAL*4	LOCAL	440, 1230,	610, 1280	820,	830*	840*	930,	940,
BUF	(3000)	3000	REAL*4	LOCAL	440,	1120					
COMPLT			REAL*4	ENTRY POINT	10						
HILD	(2)	2	REAL*4	LOCAL	440,	1050*	1060*	1120			
I			INTEGER*4	LOCAL	470*, 680, 800, 1150,	510*, 700, 820, 1230,	520, 710, 830, 1280	530, 720, 860*	580*, 750, 870,	610*, 760, 930,	670*, 790, 940,
INDEX	(7)	7	INTEGER*4	LOCAL	440,	1470*	1500*	1510,	1530		
IPLOT			INTEGER*4	LOCAL	450,	1390					
IP1			INTEGER*4	LOCAL	680*	690					
IP13			INTEGER*4	LOCAL	660*	670					
ISYM			INTEGER*4	LOCAL	1200*	1270*	1330,	1340*			
J			INTEGER*4	LOCAL	570*, 730, 920*, 1230,	580, 760, 930, 1250,	600, 770, 940, 1280,	610, 800, 970, 1300,	690*, 810, 980, 1310,	700, 830, 990, 1320	720, 840, 1210*
JJ			INTEGER*4	LOCAL	890*	960*	970				
JSYM	(11)	11	INTEGER*4	LOCAL	440,	520*	540*	1140			
J1			INTEGER*4	LOCAL	1230*	1250*					
K			INTEGER*4	LOCAL	740*, 810, 1170*, 1470,	750, 820, 1180, 1520*	760, 830, 1290*, 1530	770, 840, 1300,	780*, 900*, 1310,	790, 930, 1320,	800, 970, 1460*
L			INTEGER*4	LOCAL	450,	1160					
LABEL				SUBROUTINE	1140						
LEGEND				SUBROUTINE	1510,	1530					
LINPLT				SUBROUTINE	1180,	1330					
LNTHS	(10)	10	INTEGER*4	LOCAL	440,	530*	1140				
ML			INTEGER*4	PARAMETER	10,	610,	780,	860			
MOD			INTEGER*4	FUNCTION	1480,	1500					
NINDEX			INTEGER*4	LOCAL	1450*	1460,	1490*	1500,	1520		
NPLNT			INTEGER*4	LOCAL	1110*, 1400	1120,	1130,	1180,	1220,	1330,	1350*
NP13			INTEGER*4	LOCAL	910*	950*	980,	990,	1040,	1170,	1180
NUMY			INTEGER*4	LOCAL	1040*	1170					
O	(100,10)	1000	REAL*4	LOCAL	440,	930*	970,	1250,	1320		
O1	(100,10)	1000	REAL*4	LOCAL	440,	970*	1180				
O2	(10)	10	REAL*4	LOCAL	440,	1320*	1330				
P13			INTEGER*4	LOCAL	410, 1210,	450, 1450,	490, 1480,	570, 1500	660,	690,	920,
QQQCPA				SUBROUTINE	550,	560,	1160,	1190			
REPLACE				SUBROUTINE	600						
RUNTIME	(10,100)	1000	REAL*8	LOCAL	420, 1230,	440, 1510,	580, 1530	600,	750,	760*	770*

SETPLT				SUBROUTINE	1120						
SYMBOL				SUBROUTINE	1150						
T		INTEGER*4	LOCAL		410, 1250	450, 1290	470, 1330	510,	540,	900,	1040,
TEMP	(100)	100	REAL*4	LOCAL	440, 990	610, 1230	700, 1300	710- 1310	720*	730*	980,
TEM1	(20)	20	REAL*4	LOCAL	440,	1300*	1310*	1330			
TEM2	(200)	200	REAL*4	LOCAL	440,	980*	990*	1180			
TIME	(10)	10	REAL*4	LOCAL	440,	470,	930,	1140,	1250		
TITLE				SUBROUTINE	1130						
TITL1	(100)	100	REAL*8	PARAMETER	10,	420,	440,	870,	1150		
T1			REAL*4	LOCAL	710*	730,	790*	810,	820*	840	
T2			REAL*8	LOCAL	420,	750*	770				
XHILD	(4)	4	REAL*4	LOCAL	440,	1070*	1080*	1090*	1100*	1120	
XTITLE	(10)	10	REAL*8	LOCAL (DATA)	420,	430,	440,	1130			

* = VARIABLES USED ON LEFT HAND SIDE OF EQUAL SIGN

INPUT / OUTPUT TABLE					
DEFINING SEQ. NO.	I/O OPERATION	LOGICAL UNIT	I/O TYPE	FORMAT USED	I/O LIST
450	READ	50	BCD	1	P13,T,L,I PLOT
470	READ	50	BCD	2	(TIME(I),I=1,T)
580	READ	50	BCD	4	(RUNIT(I,J),I=1,10)
610	READ	50	BCD	5	TEMP(J),(A(I,J),B(I,J),I=1,ML)
490	PRINT	51	BCD	3	P13
870	PRINT	51	BCD	6	TITL1(2*I-1),TITL1(2*I)
1230	PRINT	51	BCD	7	(RUNIT(J1,J),J1=1,9),TEMP(J),A(I,J),B(I,J)
1250	PRINT	51	BCD	8	(TIME(J1),C(J,J1),J1=1,T)

```

IEF285I  A5.G3.P31177.C10155.DURFEE.PLI      PASSED
IEF285I  VOL SER NOS= ZZZZZZ.
IEF285I  SYS1.LINKLIB                          PASSED
IEF285I  VOL SER NOS= MVT17P.
IEF285I  SYS70287.T181233.RV000.DSE1.FJ0BLIB  PASSED
IEF285I  VOL SER NOS= YYYYYY.
IEF285I  SYS70287.T181233.SV000.DSE1.P0000038  SYSOUT
IEF285I  VOL SER NOS= XXXXXX.
IEF285I  SYS70287.T181233.RV000.DSE1.FJ0BLIB  DELETED
IEF285I  VOL SER NOS= YYYYYY.
IEF285I  SYS70287.T181233.RV000.DSE1.FTSYSIN  PASSED
IEF285I  VOL SER NOS= 222222.

```

```

DSE1      GO                21.55.10 10-14-70
          CPU SEC.= 27.82//  I/O REQUESTS= 103//  REGION ALLOC.=1536K//  MACH. USE SEC.= 21.94//  REGION USED=1526K

```

```

IEF285I  A5.G3.P31177.C10155.DURFEE.PLI      KEPT
IEF285I  VOL SER NOS= ZZZZZZ.
IEF285I  SYS1.LINKLIB                          KEPT
IEF285I  VOL SER NOS= MVT17P.
IEF285I  SYS70287.T181233.RV000.DSE1.FTSYSIN  DELETED
IEF285I  VOL SER NOS= 222222.

```

```

DSE1      MODEL=75 12223    21.55.12 10-14-70
TOTAL CPU SEC.= 78.20//TOTAL I/O REQUESTS= 1521//MAX. REGION ALLOC.=1536K//TOTAL MACH. USE SEC.= 139.14//MAX. REGION USED=1526K

```

*** COMPOSITE DATA ***

THE NUMBER OF EXPERIMENTAL RUNS IS 5

GAGE P1

GAGE P1

107-205--Y-12-A
 TEMPERATURE = 205.00 A = 0.20200E-04 B = -0.75152E-00

TIME (HRS.)	CUTGASSING RATE
1.0	2.02000E-05
10.0	7.5757E-06
100.0	6.74374E-07
1000.0	1.12406E-07

108-518--Y-12-B
 TEMPERATURE = 518.00 A = 0.43200E-04 B = -0.51104E-00

TIME (HRS.)	CUTGASSING RATE
1.0	5.32000E-05
10.0	7.75671E-06
100.0	0.52001E-07
1000.0	1.16841E-07

109-446--Y-12-C
 TEMPERATURE = 446.00 A = 0.39600E-03 B = -0.71533E-00

TIME (HRS.)	CUTGASSING RATE
1.0	7.06000E-04
10.0	7.62616E-05
100.0	1.46864E-05
1000.0	2.82870E-06

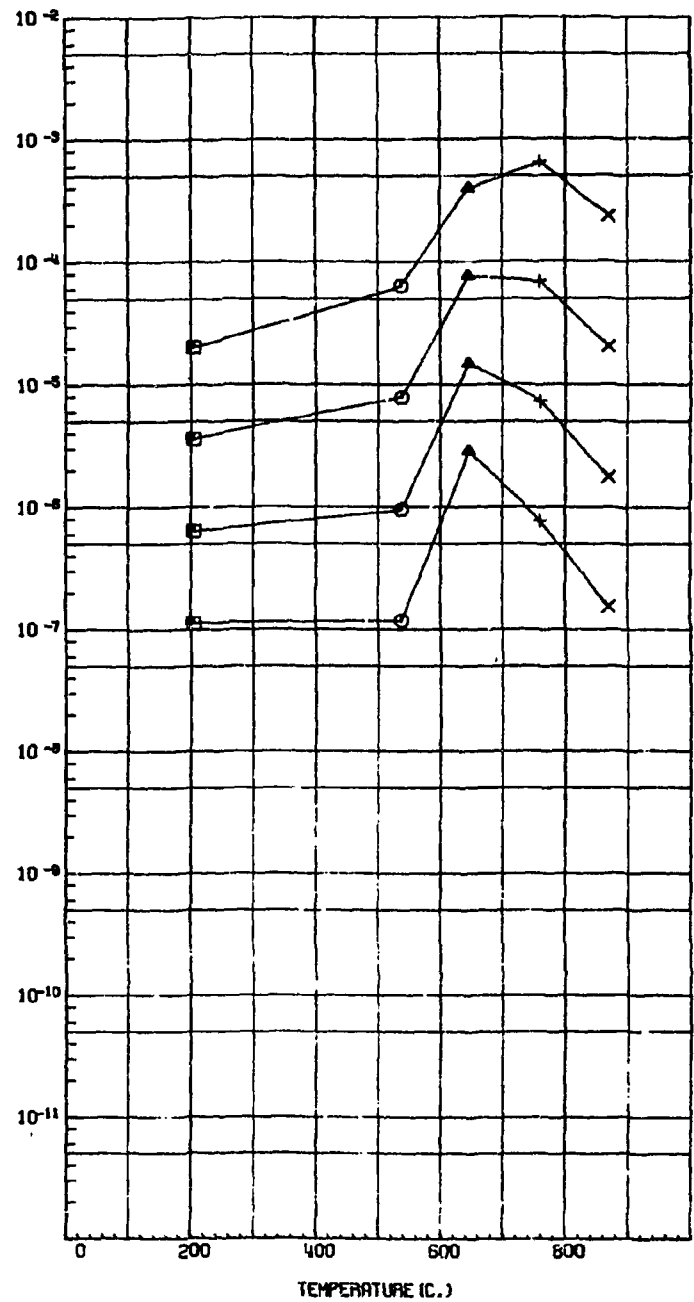
110-740--Y-12-D
 TEMPERATURE = 740.00 A = 0.61700E-03 B = -0.57441E-00

TIME (HRS.)	CUTGASSING RATE
1.0	4.47000E-04
10.0	6.01260E-05
100.0	7.27571E-06
1000.0	7.72101E-07

106-4-870--Y-12-E
 TEMPERATURE = 870.00 A = 0.23200E-03 B = -0.10613E-00

TIME (HRS.)	CUTGASSING RATE
1.0	2.32000E-04
10.0	2.01460E-05
100.0	1.74640E-06
1000.0	1.51911E-07

CUTGASSING RATE (TORR-LITERS/SEC) AT TIMES (HOURS) = 1.00, 10.00, 100.00, 1000.00.



TOTAL

107-205--Y-12-A
TEMPERATURE = 205.00 A = 0.12900E-02 B = -0.67770E 00

TIME (HRS.)	CUTGASSING RATE
1.0	1.20000E-04
10.0	2.70051E-05
100.0	5.69102E-06
1000.0	1.10533E-06

108-538--Y-12-B
TEMPERATURE = 538.20 A = 0.74000E-04 B = -0.11209E 01

TIME (HRS.)	CUTGASSING RATE
1.0	7.60000E-05
10.0	5.75327E-06
100.0	4.35527E-07
1000.0	3.25608E-08

109-646--Y-12-C
TEMPERATURE = 646.40 A = 0.35000E-03 B = -0.95358E 00

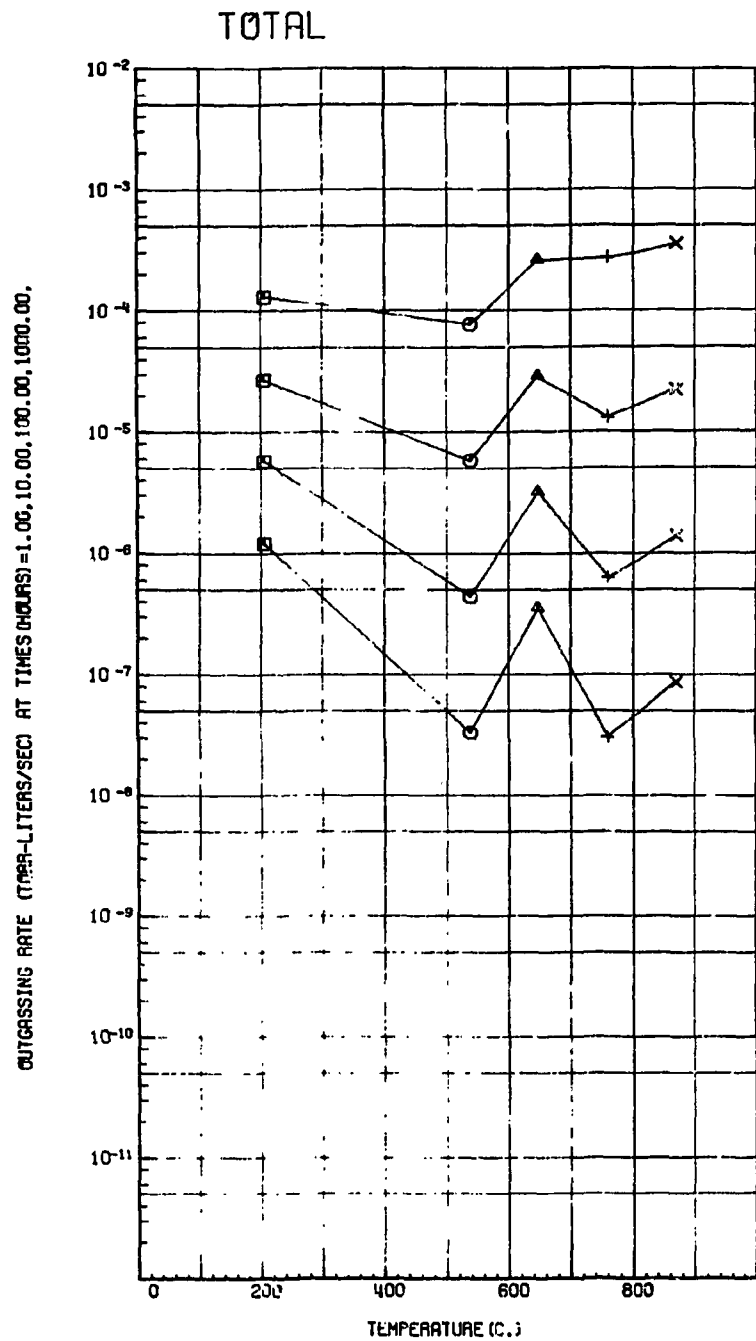
TIME (HRS.)	CUTGASSING RATE
1.0	2.58000E-04
10.0	2.87104E-05
100.0	3.19492E-06
1000.0	3.55533E-07

110-760--Y-12-D
TEMPERATURE = 760.20 A = 0.26000E-03 B = -0.13150E 01

TIME (HRS.)	CUTGASSING RATE
1.0	2.68000E-04
10.0	1.20400E-05
100.0	6.23655E-07
1000.0	3.02298E-08

106-4-870--Y-12-E
TEMPERATURE = 870.00 A = 0.35000E-03 B = -0.12038E 01

TIME (HRS.)	CUTGASSING RATE
1.0	3.50000E-04
10.0	3.19512E-05
100.0	1.26021E-06
1000.0	8.56087E-08



H

107-205--Y-12-A
TEMPERATURE = 205.00 A = 0.64700E-04 B = -0.55566E 00

TIME (HRS.)	CUTGASSING RATE
1.0	6.47000E-05
10.0	1.79288E-05
100.0	5.00708E-06
1000.0	1.39291E-06

109-538--Y-12-B
TEMPERATURE = 38.20 A = 0.10100E-04 B = -0.88279E 00

TIME (HRS.)	CUTGASSING RATE
1.0	1.01000E-05
10.0	1.32291E-06
100.0	1.73277E-07
1000.0	2.26961E-08

109-646--Y-12-C
TEMPERATURE = 64.40 A = 0.13100E-04 B = -0.10312E 01

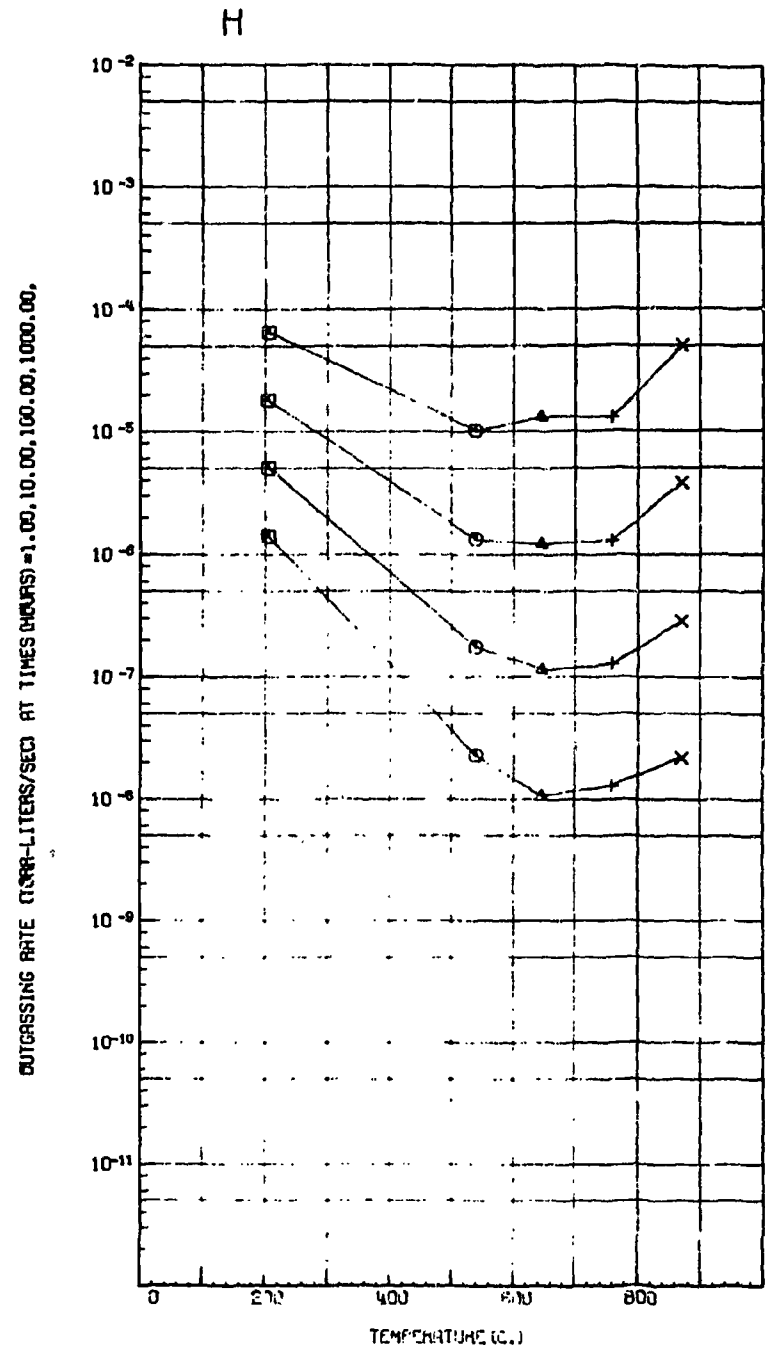
TIME (HRS.)	CUTGASSING RATE
1.0	1.31000E-05
10.0	1.21519E-06
100.0	1.13462E-07
1000.0	1.05602E-08

110-760--Y-12-D
TEMPERATURE = 760.30 A = 0.12800E-04 B = -0.10009E 01

TIME (HRS.)	CUTGASSING RATE
1.0	1.28000E-05
10.0	1.27735E-06
100.0	1.27471E-07
1000.0	1.27207E-08

106-4-R70--Y-12-D
TEMPERATURE = 870.00 A = 0.50000E-04 B = -0.11214E 01

TIME (HRS.)	CUTGASSING RATE
1.0	5.00000E-05
10.0	3.78068E-06
100.0	2.85971E-07
1000.0	2.16157E-08



HELIUM

107-205--Y-12-A
TEMPERATURE = 205.00 A = 0.24100E-05 B = -0.35931E 00

TIME (HRS.)	CUTGASSING RATE
1.0	2.41000E-06
10.0	1.03206E-06
100.0	4.41975E-07
1000.0	1.89272E-07

108-538--Y-12-P
TEMPERATURE = 538.20 A = 0.25600E-04 B = -0.12134E 01

TIME (HRS.)	CUTGASSING RATE
1.0	2.56000E-05
10.0	1.24406E-06
100.0	6.04563E-08
1000.0	2.92793E-09

109-646--Y-12-C
TEMPERATURE = 646.40 A = 0.45700E-04 B = -0.15992E 01

TIME (HRS.)	CUTGASSING RATE
1.0	4.57000E-05
10.0	1.15005E-06
100.0	2.89413E-08
1000.0	7.28213E-10

110-760--Y-12-F
TEMPERATURE = 760.30 A = 0.51500E-04 B = -0.16987E 01

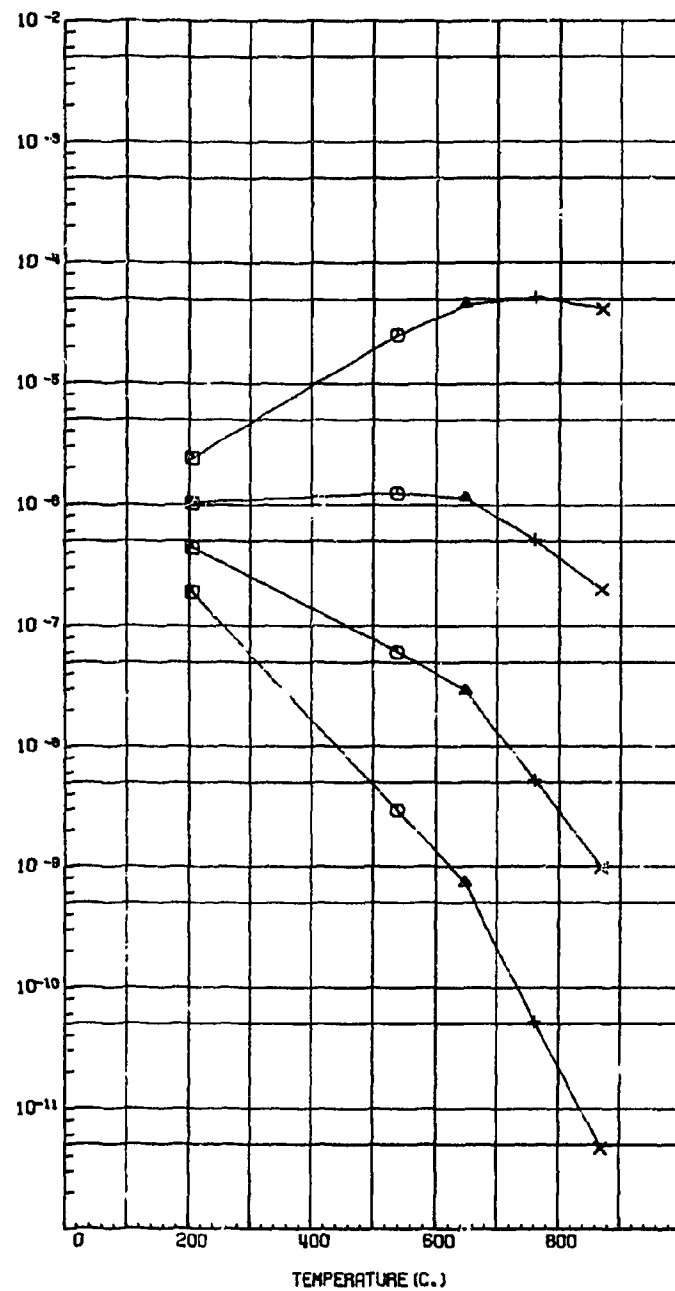
TIME (HRS.)	CUTGASSING RATE
1.0	5.15000E-05
10.0	5.16545E-07
100.0	5.18094E-09
1000.0	5.19648E-11

106-4-870--Y-12-G
TEMPERATURE = 870.00 A = 0.41200E-04 B = -0.23140E 01

TIME (HRS.)	CUTGASSING RATE
1.0	4.12000E-05
10.0	1.69640E-07
100.0	6.70284E-10
1000.0	4.70648E-12

HELIUM

OUTGASSING RATE (TORR-LITERS/SEC) AT TIMES (HOURS)=1.00,10.00,100.00,1000.00,



METHANE

107-205--Y-12-A
TEMPERATURE = 205.00 A = 0.62600E-06 B = -0.45778E 00

TIME (HRS.)	CUTGASSING RATE
1.0	6.26000E-07
10.0	2.18170E-07
100.0	7.60351E-08
1000.0	2.64593E-08

108-538--Y-12-B
TEMPERATURE = 538.70 A = 0.58100E-06 B = -0.11327E 01

TIME (HRS.)	CUTGASSING RATE
1.0	5.81000E-07
10.0	4.28022E-08
100.0	3.15338E-08
1000.0	2.32314E-10

109-646--Y-12-C
TEMPERATURE = 646.40 A = 0.12700E-05 B = -0.14540E 01

TIME (HRS.)	CUTGASSING RATE
1.0	1.27000E-06
10.0	4.46482E-08
100.0	1.56966E-09
1000.0	5.51830E-11

110-760--Y-12-D
TEMPERATURE = 760.30 A = 0.12600E-05 B = -0.10519E 01

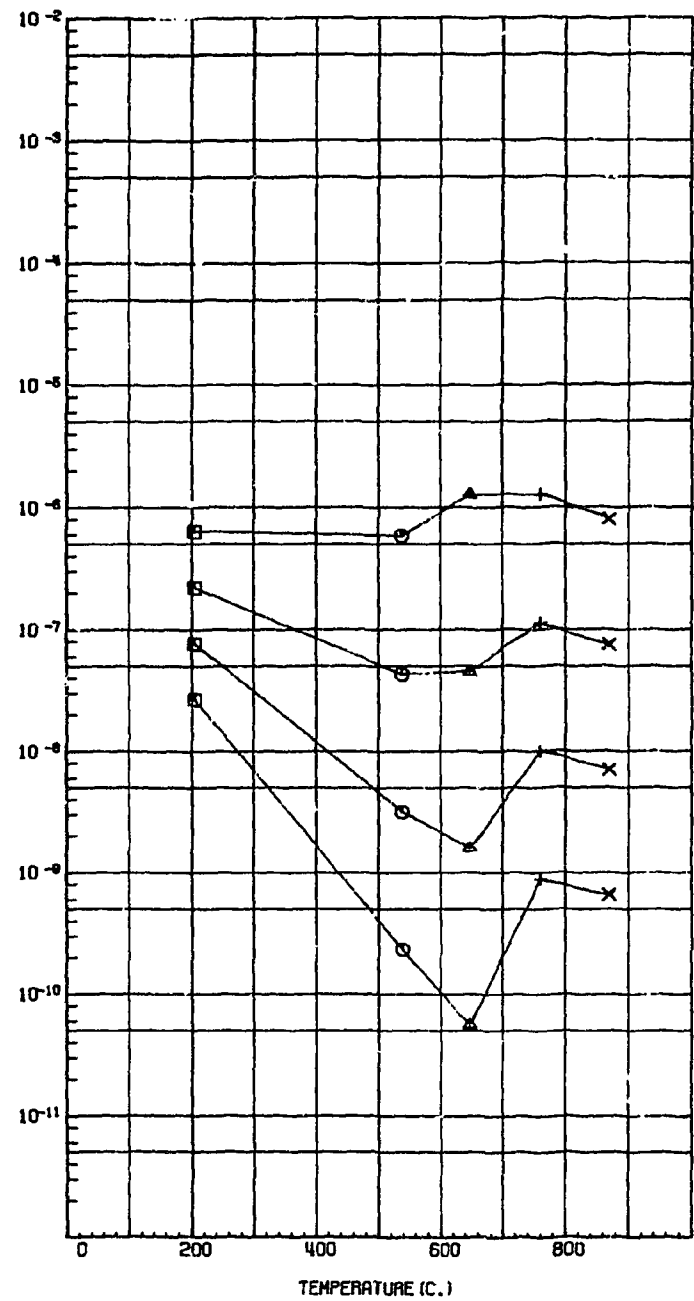
TIME (HRS.)	CUTGASSING RATE
1.0	1.26000E-06
10.0	1.11807E-07
100.0	5.92335E-08
1000.0	8.80381E-10

106-4-870--Y-12-E
TEMPERATURE = 870.00 A = 0.79500E-06 B = -0.10294E 01

TIME (HRS.)	CUTGASSING RATE
1.0	7.95000E-07
10.0	7.42663E-08
100.0	6.54337E-08
1000.0	6.49994E-10

CUTGASSING RATE (TORR-LITERS/SEC) AT TIMES (HOURS) = 1.00, 10.00, 100.00, 1000.00.

METHANE



WATER VAPOR

107-205--Y-12-A
TEMPERATURE = 205.00 A = 0.4P400F-04 B = -C.13295E 01

TIME (HRS.)	OUTGASSING RATE
1.0	4.84000E-05
10.0	2.26645E-06
100.0	1.06132E-07
1000.0	4.969P9E-09

108-538--Y-12-B
TEMPERATURE = 538.20 A = 0.25800E-04 B = -C.14517E 01

TIME (HRS.)	OUTGASSING RATE
1.0	2.58000E-05
10.0	2.11845E-07
100.0	2.22271E-08
1000.0	1.13800E-09

109-646--Y-12-C
TEMPERATURE = 646.40 A = 0.52300E-04 B = -C.15913E 01

TIME (HRS.)	OUTGASSING RATE
1.0	5.23000E-05
10.0	1.24030E-06
100.0	3.43482E-08
1000.0	8.00246E-10

110-760--Y-12-D
TEMPERATURE = 760.30 A = 0.72700E-04 B = -C.13025E 01

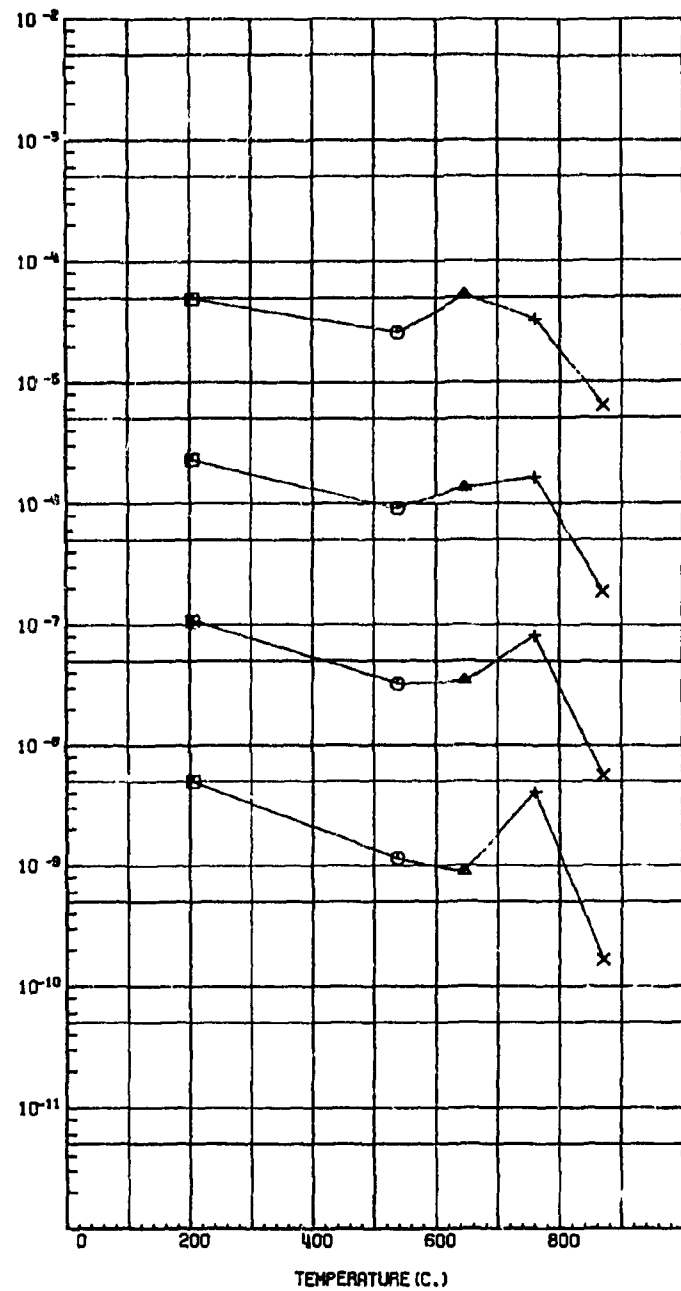
TIME (HRS.)	OUTGASSING RATE
1.0	7.27000E-05
10.0	1.62548E-06
100.0	8.11985E-08
1000.0	4.04621E-09

106-4-P70--Y-12-E
TEMPERATURE = 870.00 A = 0.63000E-05 B = -C.15276E 01

TIME (HRS.)	OUTGASSING RATE
1.0	6.30000E-06
10.0	1.86975E-07
100.0	5.54807E-09
1000.0	1.64643E-10

WATER VAPOR

OUTGASSING RATE (CORR-LITERS/SEC) AT TIMES (HOURS) = 1.00, 10.00, 100.00, 1000.00.



NITROGEN

107-205--Y-12-A
TEMPERATURE = 205.00 A = 0.80900E-06 B = -0.89592E 00

TIME (HRS.)	OUTGASSING RATE
1.0	8.09000E-07
10.0	1.02808E-07
100.0	1.30650E-08
1000.0	1.66021E-09

108-538--Y-12-B
TEMPERATURE = 538.20 A = 0.29900E-06 B = -0.11109E 01

TIME (HRS.)	OUTGASSING RATE
1.0	3.09000E-07
10.0	3.09002E-08
100.0	2.36427E-09
1000.0	1.85470E-10

109-646--Y-12-C
TEMPERATURE = 646.40 A = 0.29400E-06 B = -0.13341E 01

TIME (HRS.)	OUTGASSING RATE
1.0	2.94000E-06
10.0	1.26222E-07
100.0	6.31172E-09
1000.0	2.92447E-10

110-760--Y-12-D
TEMPERATURE = 760.30 A = 0.12700E-03 B = -0.31742E 01

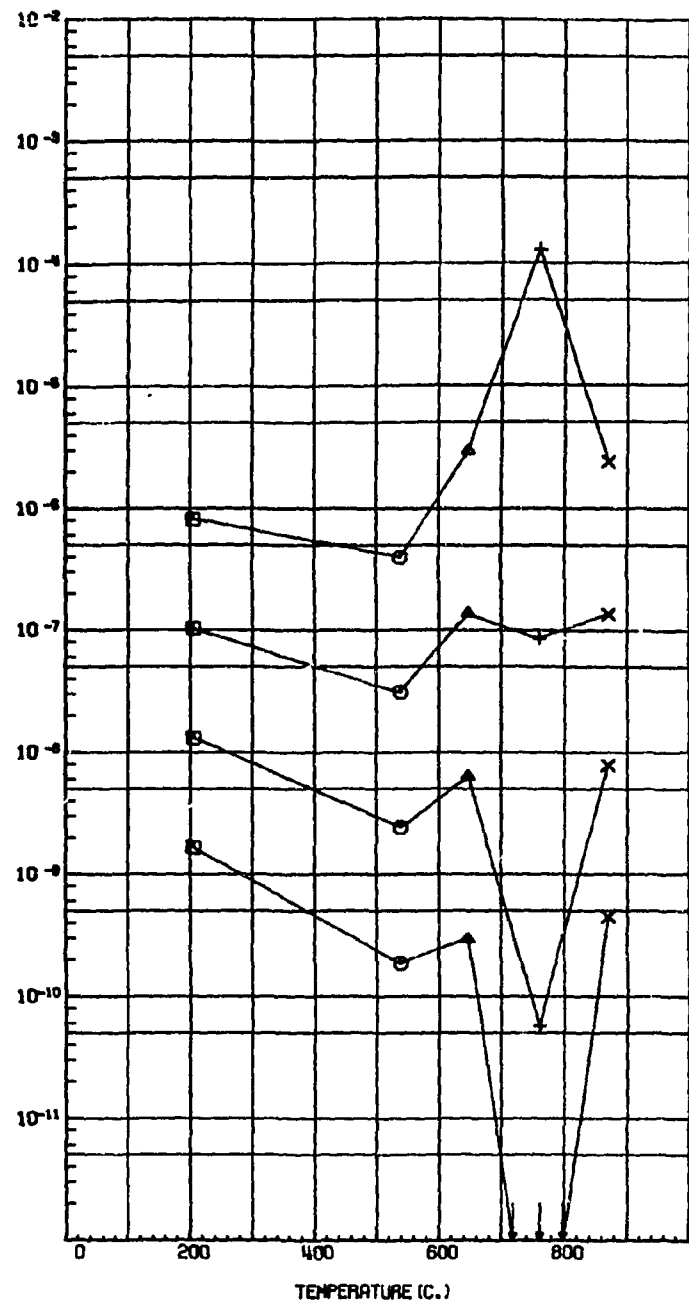
TIME (HRS.)	OUTGASSING RATE
1.0	1.27000E-04
10.0	8.30344E-08
100.0	5.65344E-11
1000.0	3.81247E-14

106-4-870--Y-12-D
TEMPERATURE = 870.00 A = 0.23600E-05 B = -0.12417E 01

TIME (HRS.)	OUTGASSING RATE
1.0	2.36000E-06
10.0	1.35274E-07
100.0	7.75278E-09
1000.0	4.44441E-10

NITROGEN

OUTGASSING RATE (TORR-LITERS/SEC) AT TIMES (HOURS) = 1.00, 10.00, 100.00, 1000.00.



C0

107-205--Y-12-A
TEMPERATURE = 205.00 A = 0.18000E-05 B = -0.48771F C0

TIME (HRS.)	CUTGASSING RATE
1.0	1.80000E-06
10.0	5.85548E-07
100.0	1.90481E-07
1000.0	6.19644E-08

108-538--Y-12-B
TEMPERATURE = 538.20 A = 0.48500E-05 B = -0.7007CF C0

TIME (HRS.)	CUTGASSING RATE
1.0	4.85000E-06
10.0	9.66143E-07
100.0	1.92461E-07
1000.0	3.83301E-08

109-646--Y-12-C
TEMPERATURE = 646.40 A = 0.10200E-03 B = -0.65871E C0

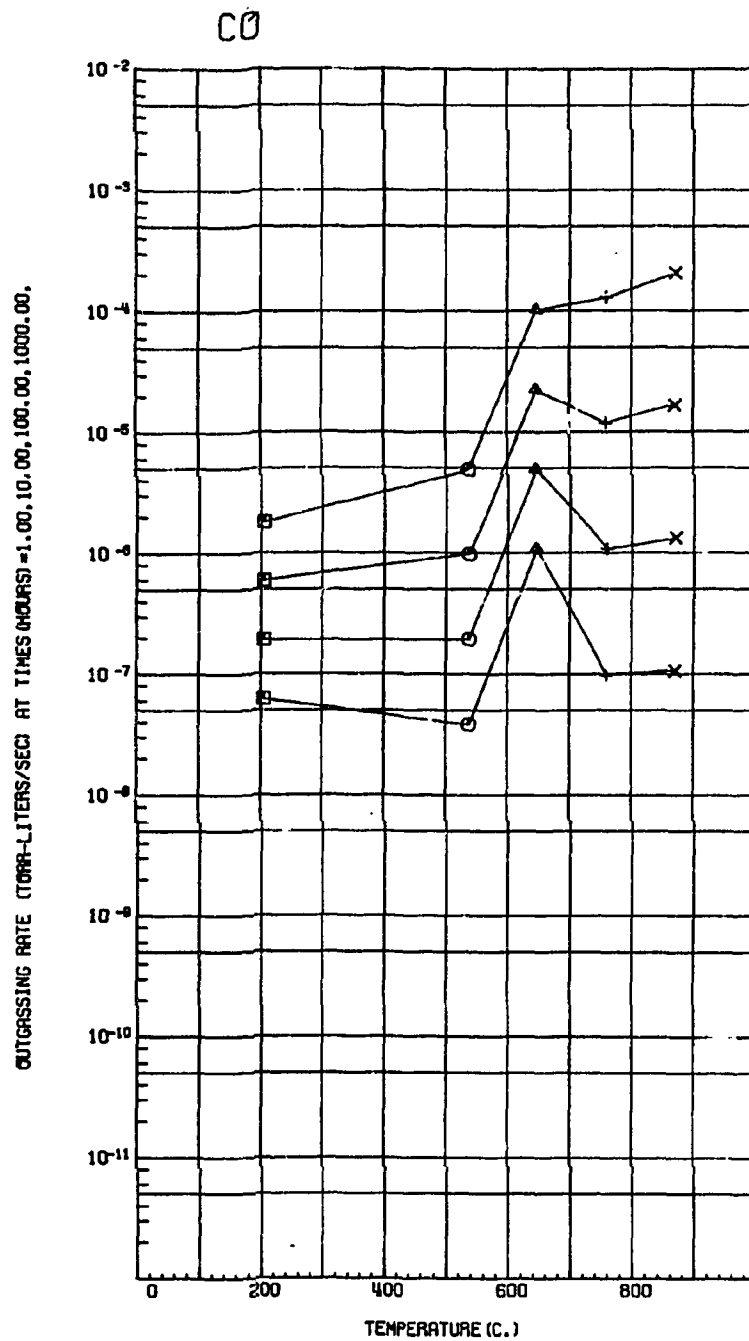
TIME (HRS.)	CUTGASSING RATE
1.0	1.02000E-04
10.0	2.23816E-05
100.0	4.91112E-06
1000.0	1.07763E-06

110-760--Y-12-D
TEMPERATURE = 760.30 A = 0.12900E-03 B = -0.10405F C1

TIME (HRS.)	CUTGASSING RATE
1.0	1.29000E-04
10.0	1.17514E-05
100.0	1.07051E-06
1000.0	5.75103E-08

10A-4-870--Y-12-E
TEMPERATURE = 870.00 A = 0.20400E-03 B = -0.10054F C1

TIME (HRS.)	CUTGASSING RATE
1.0	2.04000E-04
10.0	1.63760E-05
100.0	1.21471E-06
1000.0	1.05543E-07



OXYGEN

107-205--Y-12-A
TEMPERATURE = 205.00 A = 0.29700E-06 B = -0.72467E 00

TIME (HRS.)	CUTGASSING RATE
1.0	2.97000E-07
10.0	5.59870E-08
100.0	1.05540E-08
1000.0	1.58051E-09

108-538--Y-12-B
TEMPERATURE = 538.20 A = 0.50300E-07 B = -0.85142E 00

TIME (HRS.)	CUTGASSING RATE
1.0	5.03000E-08
10.0	7.08187E-09
100.0	9.47076E-10
1000.0	1.40281E-10

109-646--Y-12-C
TEMPERATURE = 646.40 A = 0.44800E-07 B = -0.54071E 00

TIME (HRS.)	CUTGASSING RATE
1.0	4.48000E-08
10.0	1.28994E-08
100.0	3.71414E-09
1000.0	1.06042E-09

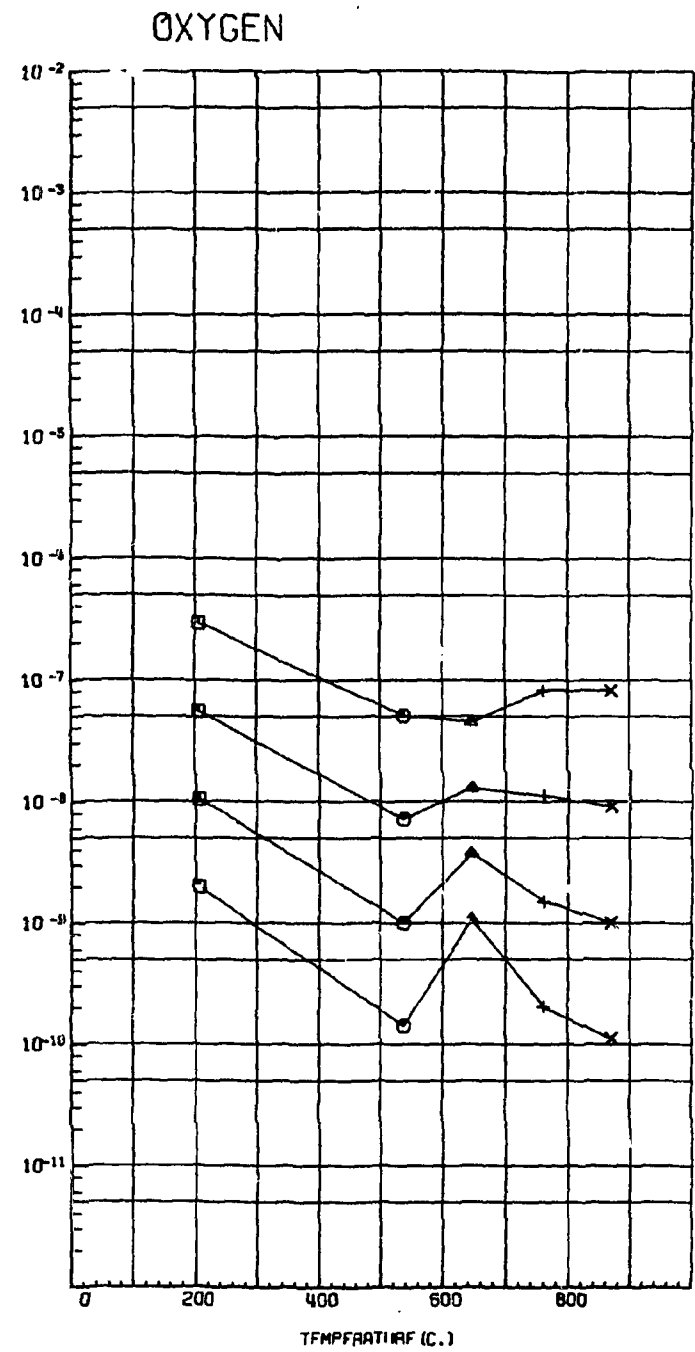
110-760--Y-12-D
TEMPERATURE = 760.20 A = 0.82200E-07 B = -0.87017E 00

TIME (HRS.)	CUTGASSING RATE
1.0	8.22000E-08
10.0	1.10841E-08
100.0	1.46442E-09
1000.0	2.01540E-10

106-4-870--Y-12-D
TEMPERATURE = 870.00 A = 0.81900E-07 B = -0.95701E 00

TIME (HRS.)	CUTGASSING RATE
1.0	8.19000E-08
10.0	6.02115E-09
100.0	9.97088E-10
1000.0	1.10084E-10

OUTGASSING RATE (TORR-LITERS/SEC) AT TIMES (HOURS) = 1.00, 10.00, 100.00, 1000.00.



ARGON

107-205--Y-12-A
TEMPERATURE = 205.00 A = 0.1960CE-06 B = -0.50198E 00

TIME (HRS.)	OUTGASSING RATE
1.0	1.96000E-07
10.0	6.16000E-08
100.0	1.94221E-08
1000.0	6.11387E-09

108-538--Y-12-B
TEMPERATURE = 538.20 A = 0.8910CE-09 B = -0.12096E 01

TIME (HRS.)	OUTGASSING RATE
1.0	8.91000E-10
10.0	4.40892E-11
100.0	3.39374E-12
1000.0	2.09440E-13

109-646--Y-12-C
TEMPERATURE = 646.40 A = 0.3000CE-06 B = -0.14669E 01

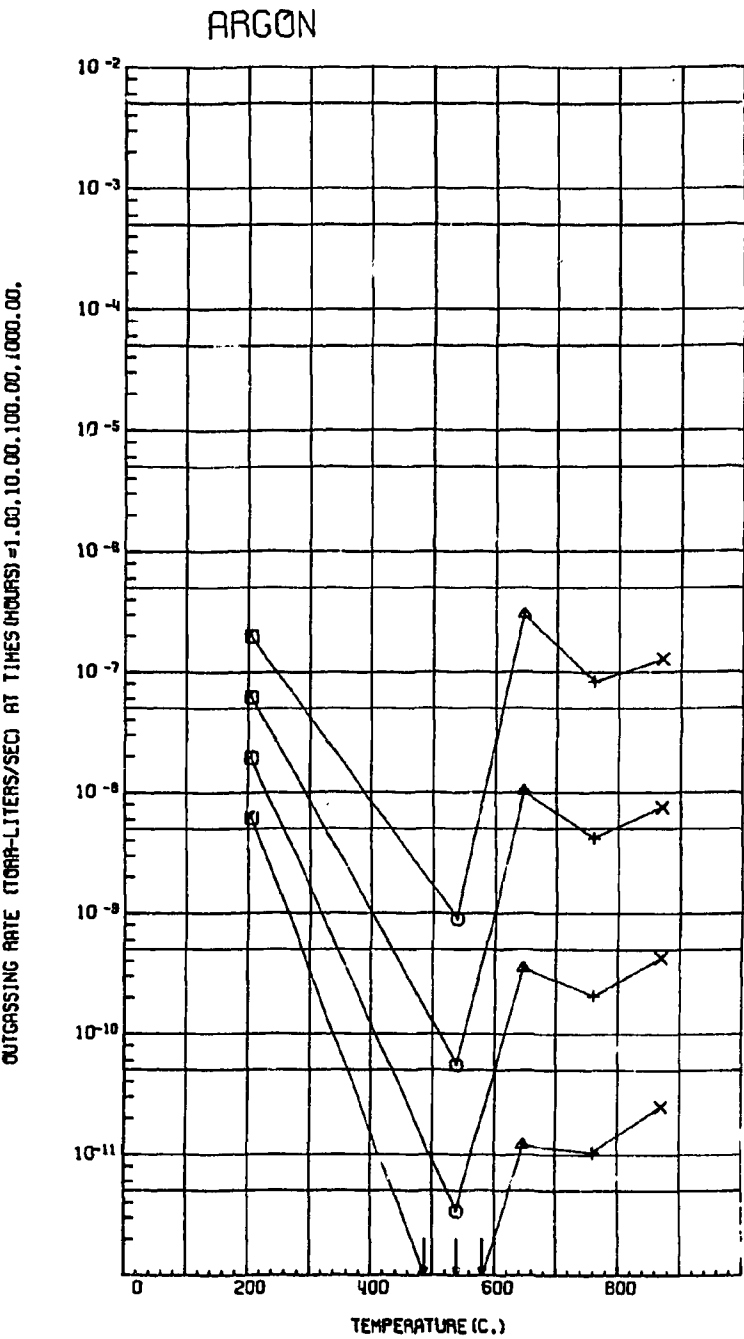
TIME (HRS.)	OUTGASSING RATE
1.0	3.00000E-07
10.0	1.02382E-08
100.0	3.46309E-10
1000.0	1.19240E-11

110-760--Y-12-D
TEMPERATURE = 760.30 A = 0.8340CE-07 B = -0.12013E 01

TIME (HRS.)	OUTGASSING RATE
1.0	8.34000E-08
10.0	4.16742E-09
100.0	2.09242E-10
1000.0	1.04056E-11

106-4-E70--Y-12-E
TEMPERATURE = 870.00 A = 0.1200CE-06 B = -0.12387E 01

TIME (HRS.)	OUTGASSING RATE
1.0	1.20000E-07
10.0	7.44542E-09
100.0	4.25724E-10
1000.0	2.48022E-11



CO2

107-205--Y-12-A
TEMPERATURE = 205.00 A = 0.16700E-05 P = -0.61453E 00

TIME (HRS.)	CUTGASSING RATE
1.0	1.67000E-06
10.0	4.05683E-07
100.0	9.85500E-08
1000.0	2.30401E-08

10P-538--Y-12-B
TEMPERATURE = 53P.20 A = 0.1230CF-05 B = -0.02810E 00

TIME (HRS.)	CUTGASSTNG PATF
1.0	1.24000F-06
10.0	1.82728F-07
100.0	2.71460E-08
1000.0	4.03278F-09

109-646--Y-12-C
TEMPERATURE = 646.40 A = 0.5710GE-05 B = -C.9C507E 00

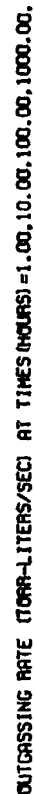
TIME (HRS.)	CUTGASSING RATE
1.0	5.7100E-06
10.0	7.10504E-07
100.0	8.84089E-08
1000.0	1.10008E-08

11C-760--Y-12-C
TEMPERATURE = 760.30 A = 0.23700E-05 B = -0.11237E 01

TIME (HRS.)	CUTGASSING RATE
1.0	2.37000E-04
10.0	1.76258E-07
100.0	1.34076E-08
1000.0	1.00844E-09

106-4-870--Y-12-D
TEMPERATURE = 870.00 A = 0.2920CF-05 b = -0.10235F 01

TIME (HRS.)	CUTGASSING RATE
1.0	2.92000E-CA
10.0	2.76620E-07
100.0	2.62050E-08
1000.0	2.48247E-09



C2H4

107-205--Y-12-A
TEMPERATURE = 205.00 A = 0.53300E-07 B = -0.83717E C0

TIME (HRS.)	CUTGASSING RATE
1.0	5.33000E-08
10.0	7.75457E-09
100.0	1.12820E-09
1000.0	1.64141E-10

108-538--Y-12-B
TEMPERATURE = 538.20 A = 0.24100E-06 B = -0.11784E C1

TIME (HRS.)	CUTGASSING RATE
1.0	2.41000E-07
10.0	1.9815E-08
100.0	1.05979E-09
1000.0	7.02780E-11

109-646--Y-12-C
TEMPERATURE = 646.40 A = 0.28400E-06 B = -0.11228E C1

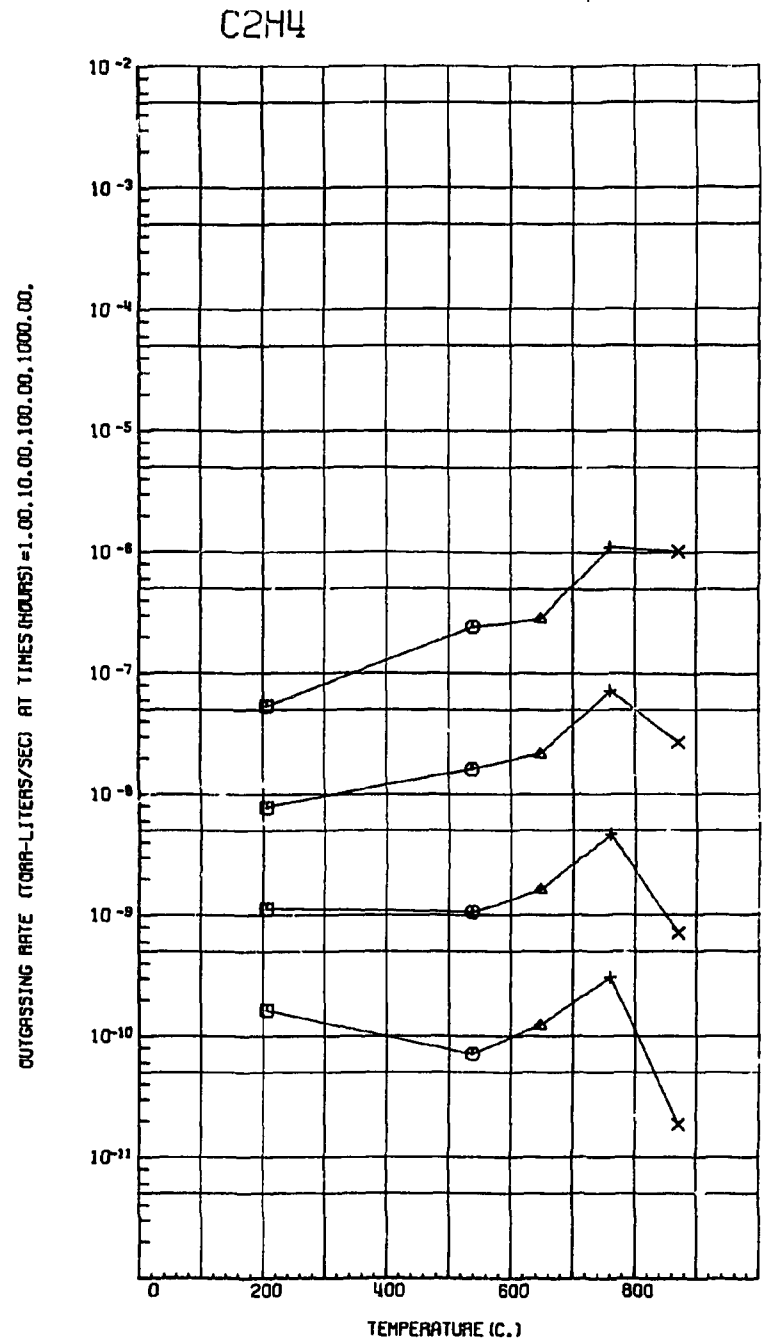
TIME (HRS.)	CUTGASSING RATE
1.0	2.84000E-07
10.0	2.14052E-08
100.0	1.61331E-09
1000.0	1.21596E-10

110-760--Y-12-C
TEMPERATURE = 760.30 A = 0.11000E-05 B = -0.11864E C1

TIME (HRS.)	CUTGASSING RATE
1.0	1.10000E-06
10.0	7.6132E-08
100.0	4.64223E-09
1000.0	3.03524E-10

106-4-870--Y-12-C
TEMPERATURE = 870.00 A = 0.10200E-05 B = -0.15801E C1

TIME (HRS.)	CUTGASSING RATE
1.0	1.02000E-06
10.0	2.62226E-08
100.0	7.05245E-10
1000.0	1.85482E-11



C2H6

107-205--Y-12-A

TEMPERATURE = 205.00 A = 0.28300E-06 B = -0.87149E 00

TIME (HRS.)	OUTGASSING RATE
1.0	2.83000E-07
10.0	3.80449E-08
100.0	5.11454E-09
1000.0	6.87569E-10

108-538--Y-12-B

TEMPERATURE = 538.20 A = 0.10700E-06 B = -0.12664E 01

TIME (HRS.)	OUTGASSING RATE
1.0	1.07000E-07
10.0	5.79408E-09
100.0	3.13751E-10
1000.0	1.60897E-11

109-646--Y-12-C

TEMPERATURE = 646.40 A = 0.11600E-06 B = -0.66804E 00

TIME (HRS.)	OUTGASSING RATE
1.0	1.16000E-06
10.0	2.48610E-07
100.0	5.32217E-08
1000.0	1.14192E-08

110-750--Y-12-E

TEMPERATURE = 750.20 A = 0.75500E-06 B = -0.15728E 01

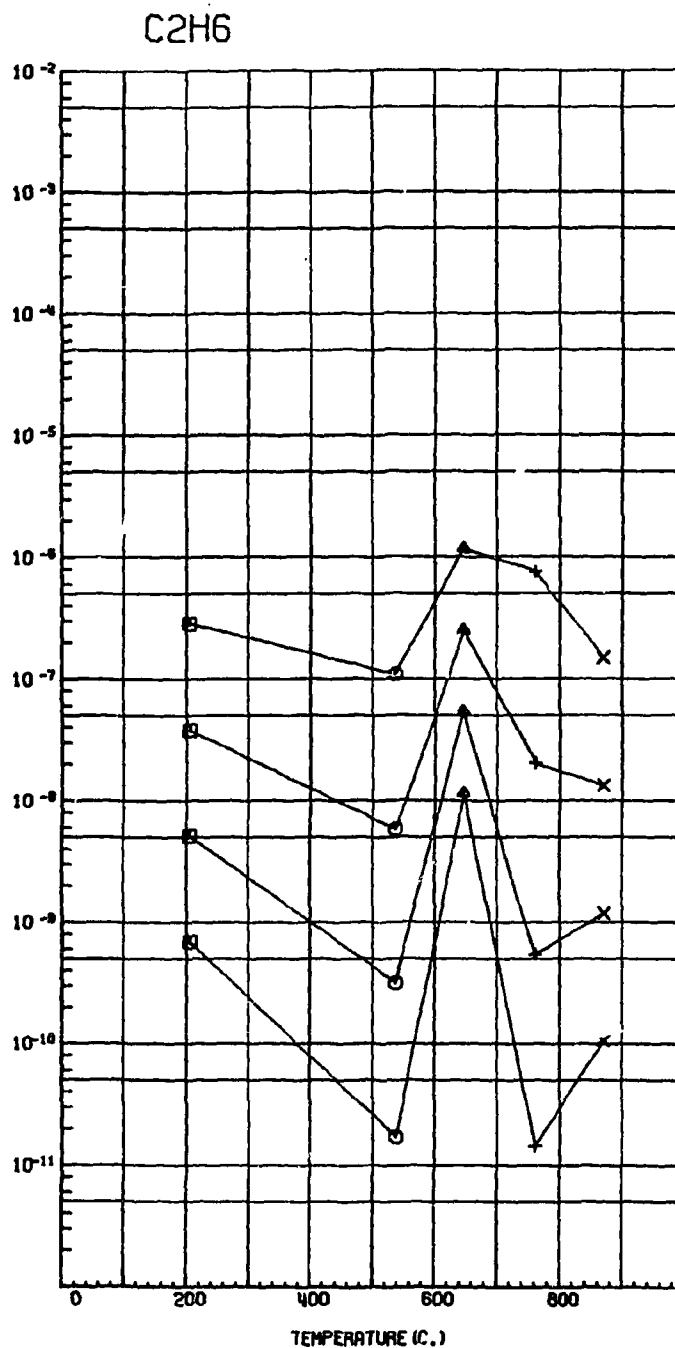
TIME (HRS.)	OUTGASSING RATE
1.0	7.55000E-07
10.0	2.01905E-08
100.0	5.35942E-10
1000.0	1.44394E-11

106-4-870--Y-12-D

TEMPERATURE = 870.00 A = 0.14000E-06 B = -0.10486E 01

TIME (HRS.)	OUTGASSING RATE
1.0	1.48000E-07
10.0	1.22311E-08
100.0	1.18221E-09
1000.0	1.05795E-10

OUTGASSING RATE (TORR-LITERS/SEC) AT TIMES (HOURS) = 1.00, 10.00, 100.00, 1000.00.



C3H8

107-205--Y-12-A
 TEMPERATURE = 205.00 A = 0.12600E-07 B = -0.75691E 00

TIME (HRS.)	OUTGASSING RATE
1.0	1.26000E-08
10.0	2.20527E-09
100.0	3.85967E-10
1000.0	6.75524E-11

108-538--Y-12-B
 TEMPERATURE = 538.20 A = 0.35600E-07 B = -0.23523E 01

TIME (HRS.)	OUTGASSING RATE
1.0	3.56000E-08
10.0	1.58180E-10
100.0	7.02831E-13
1000.0	3.12248E-15

109-646--Y-12-C
 TEMPERATURE = 646.40 A = 0.0 B = 0.0

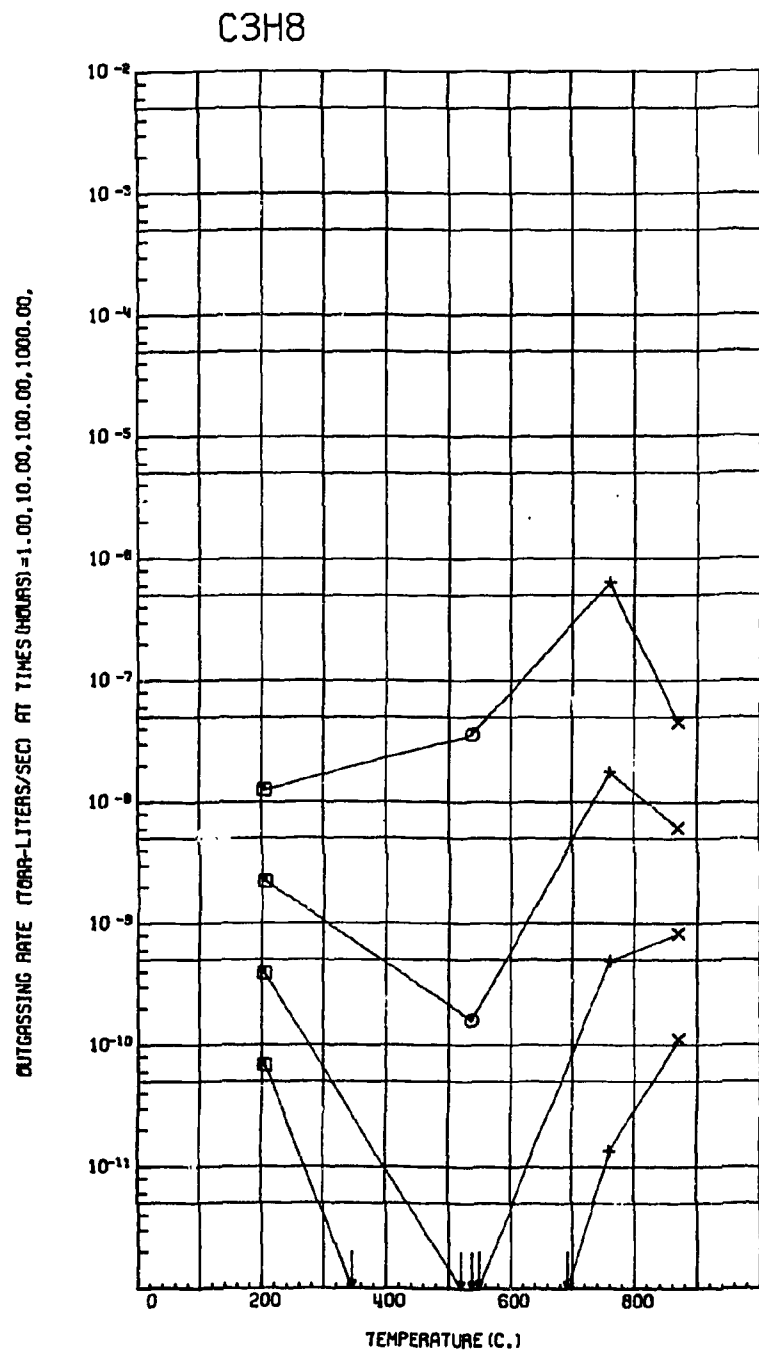
TIME (HRS.)	OUTGASSING RATE
1.0	0.0
10.0	0.0
100.0	0.0
1000.0	0.0

110-760--Y-12-D
 TEMPERATURE = 760.30 A = 0.63900E-06 B = -0.15587E 01

TIME (HRS.)	OUTGASSING RATE
1.0	6.39000E-07
10.0	1.76523E-08
100.0	4.87643E-10
1000.0	1.34711E-11

106-4-870--Y-12-D
 TEMPERATURE = 870.00 A = 0.45100E-07 B = -0.87087E 00

TIME (HRS.)	OUTGASSING RATE
1.0	4.51000E-08
10.0	6.09928E-09
100.0	9.21218E-10
1000.0	1.10570E-10



HYDROCARBONS

107-205--Y-12-A
TEMPERATURE = 205.00 A = 0.1050CF-05 B = -0.55143E 00

TIME (HRS.)	CUTGASSING RATE
1.0	1.05000E-06
10.0	2.94058E-07
100.0	8.28570E-08
1000.0	2.22755E-08

108-538--Y-12-B
TEMPERATURE = 538.20 A = 0.1010CF-05 B = -0.12055F 01

TIME (HRS.)	CUTGASSING RATE
1.0	1.01000E-06
10.0	6.29248E-08
100.0	3.92032E-09
1000.0	2.44242E-10

109-646--Y-12-C
TEMPERATURE = 646.40 A = 0.1610CF-05 B = -0.11982F 01

TIME (HRS.)	CUTGASSING RATE
1.0	1.61000E-06
10.0	1.02006E-07
100.0	4.4628CF-09
1000.0	4.0947FF-10

110-760--Y-12-D
TEMPERATURE = 760.30 A = 0.2100CF-05 B = -0.14082F 01

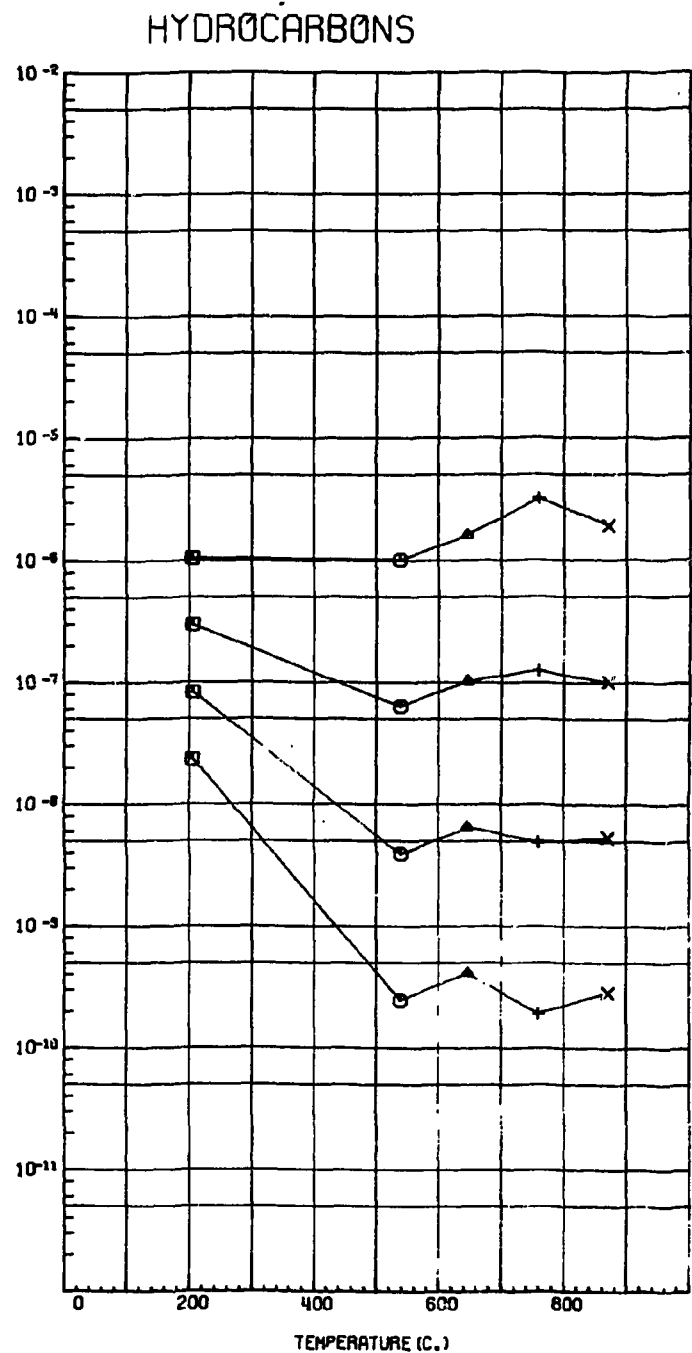
TIME (HRS.)	CUTGASSING RATE
1.0	2.10000E-06
10.0	1.24592E-07
100.0	4.86622E-09
1000.0	1.90061E-10

106-4-870--Y-12-D
TEMPERATURE = 870.00 A = 0.1900CF-05 B = -0.12742F 01

TIME (HRS.)	CUTGASSING RATE
1.0	1.90000E-06
10.0	1.01031E-07
100.0	5.27222E-09
1000.0	2.85662E-10

IHC0021 STOP 00000

OUTGASSING RATE (TORR-LITERS/SEC) AT TIMES (HOURS) = 1.00, 10.00, 100.00, 1000.00.



IEF2851	SYS70265.7094821.RV000.CLAC.FJOB18	PASSED
IEF2851	VOL SER NOS= CL1801.	
IEF2851	SYS70265.7094821.SV000.CLAC.RC000036	SYSOUT
IEF2851	VOL SER NOS= RRRRRP.	
IEF2851	SYS70265.7094821.RV000.CLAC.FJOB18	DELETED
IEF2851	VOL SER NOS= CL1801.	
IEF2851	SYS70265.7094821.RV000.CLAC.UT20	DELETED
IEF2851	VOL SER NOS= 222222.	
IEF2851	SYS70265.7094821.SV000.CLAC.RC000037	DELETED
IEF2851	VOL SER NOS= XXXXXX.	
IEF2851	SYS70265.7094821.RV000.CLAC.SC000038	SYSIN
IEF2851	VOL SER NOS= CCCCCC.	
IEF2851	SYS70265.7094821.RV000.CLAC.SC000038	DELETED
IEF2851	VOL SER NOS= CCCCCC.	

CLAC	GO	18.43.C5 10-22-70				
	CPU SEC.= 12.51//	I/O REQUESTS= 69//	REGION ALLOC.= 190K//	MACH. USE SEC.= 14.25//	REGION USED= 178K	

CLAC	MCPFL=75 12523	18.43.C5 10-22-70				
	TOTAL CPU SEC.= 35.47//TOTAL I/O REQUESTS= 876//MAX. REGION ALLOC.= 470K//TOTAL MACH. USE SEC.= 42.75//MAX. REGION USED= 420K					