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# A Sputter Flux Diagnostic Based Approach to Enabling Low Run-In for Sputter Deposited MoS<sub>2</sub> Solid Lubricants

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*AVS 70<sup>th</sup> International Symposium*

Tampa, FL



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# MOS<sub>2</sub> FILMS FOR EXTREME ENVIRONMENT LUBRICATION

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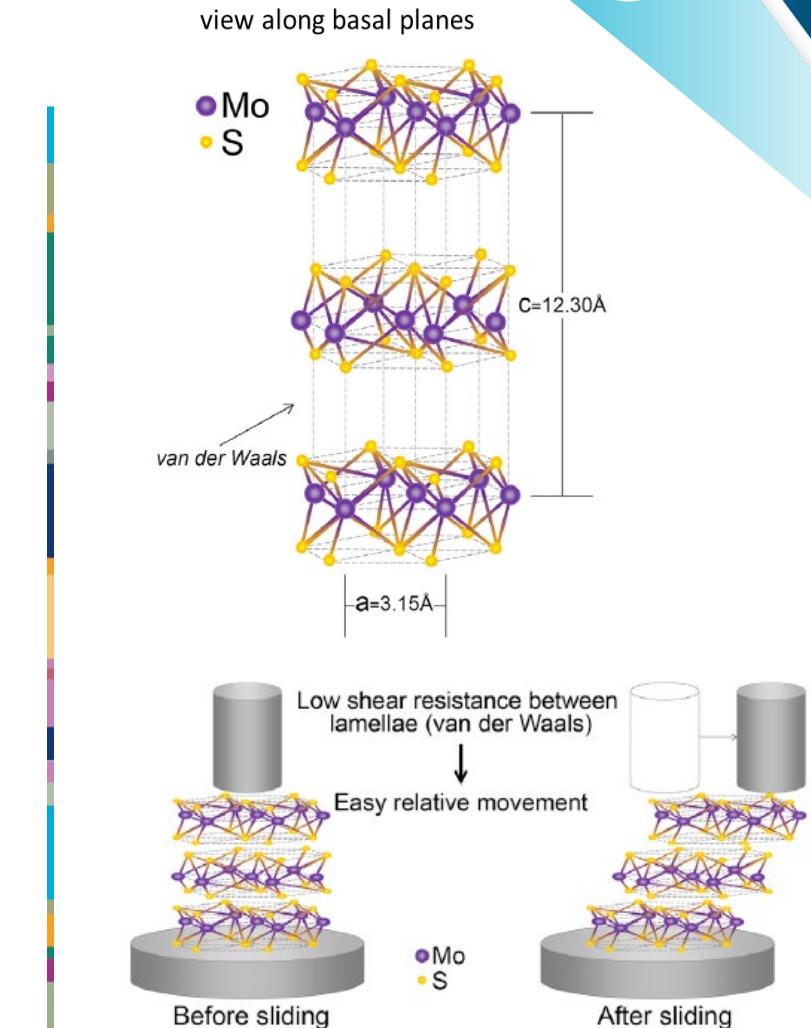


<https://shop.sdp-si.com/>



## Aerospace / precision mechanisms share similar concerns

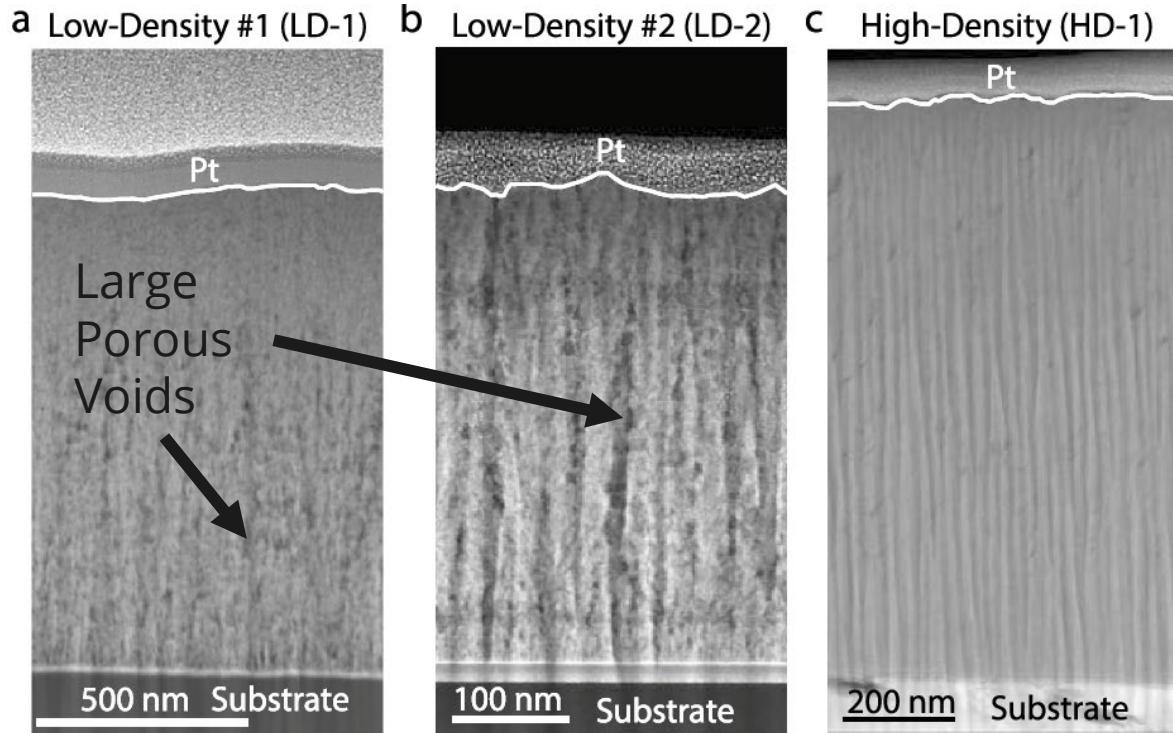
- operate in vacuum (+atomic oxygen in low earth orbit), or inert gas near  $P_{atm}$  with trace O<sub>2</sub>, H<sub>2</sub>O, outgassing species
- store months – years before use; generally non-serviceable
- operating temperatures from 50 – 300K, depending on location
- huge investments of time and money



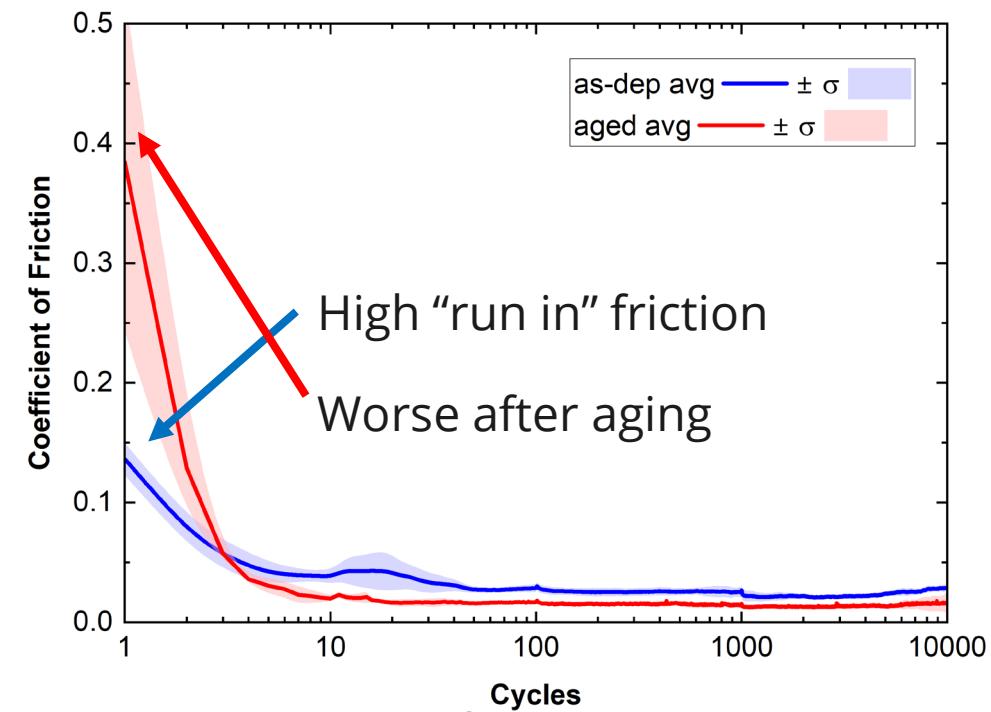
[doi.org/10.1016/j.triboint.2017.12.033](https://doi.org/10.1016/j.triboint.2017.12.033)

# PROBLEMS WITH CURRENT COATINGS

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- Commercial coating are inconsistent!
  - [doi.org/10.1007/s11249-022-01642-y](https://doi.org/10.1007/s11249-022-01642-y)
  - Same companies 6 months apart



- Films get worse with age
  - Accentuated with low cycle applications
- Lubrication is important
  - Voyager 2, Keplar, Galileo all partially failed due to lubrication

# REAL PROBLEMS FOR TRIBOLOGY (AND NASA)

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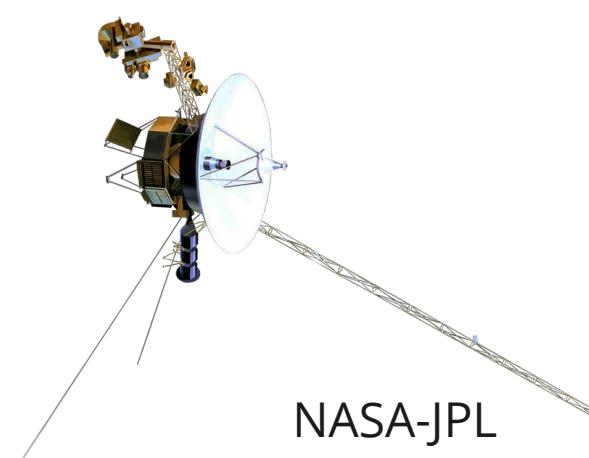


- Voyager 2: Science platform seized due to mitigation of lubricant out of motor gear shaft, delayed use for 16 months, all future experiments ran at 0.083 deg/s instead of 1deg/s<sup>(1)</sup>
- Keplar: 2/4 reaction wheels seized due to uneven lubrication of mechanical bearings causing galling, prolonged mission delays, had to use radiation pressure to compensate<sup>(2)</sup>
- Galileo: sticking of 3/18 antenna ribs in stowed position due to high friction between pins and sockets, over 100 personal did simulations and testing to report the MoS<sub>2</sub> bonding failed<sup>(3)</sup>

[1] Physics Today 43, 7, 40 (1990); doi: 10.1063/1.881251

[2] Kepler Mission Manager Update: Kepler Returns to Science Mode. (2015, April 15). Retrieved June 10, 2018, from [https://www.nasa.gov/mission\\_pages/kepler/news/keplerm-20132901.html](https://www.nasa.gov/mission_pages/kepler/news/keplerm-20132901.html)

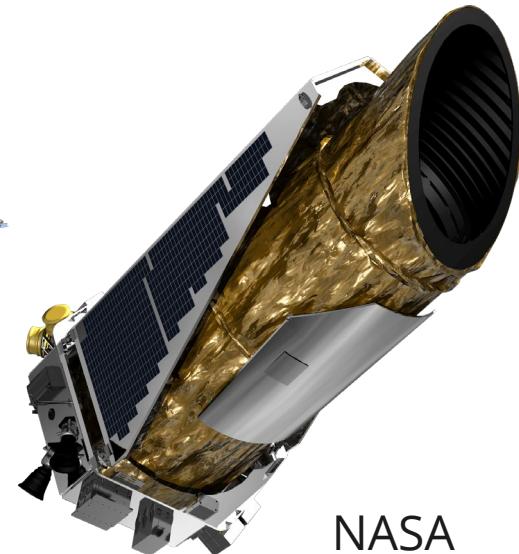
[3] Miyoshi, K. (1999). *Aerospace Mechanisms and Tribology Technology: Case Studies*.



NASA-JPL



NASA



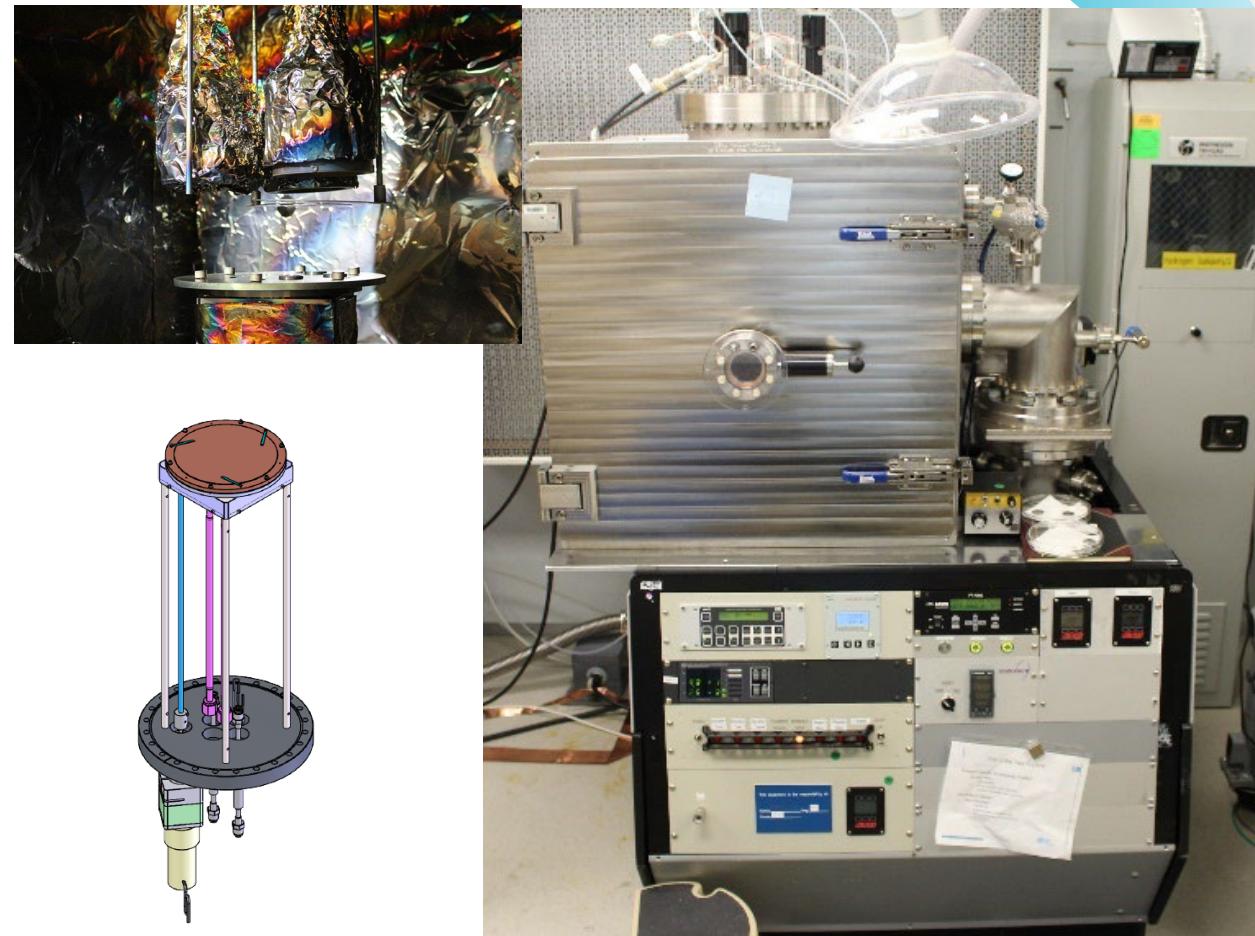
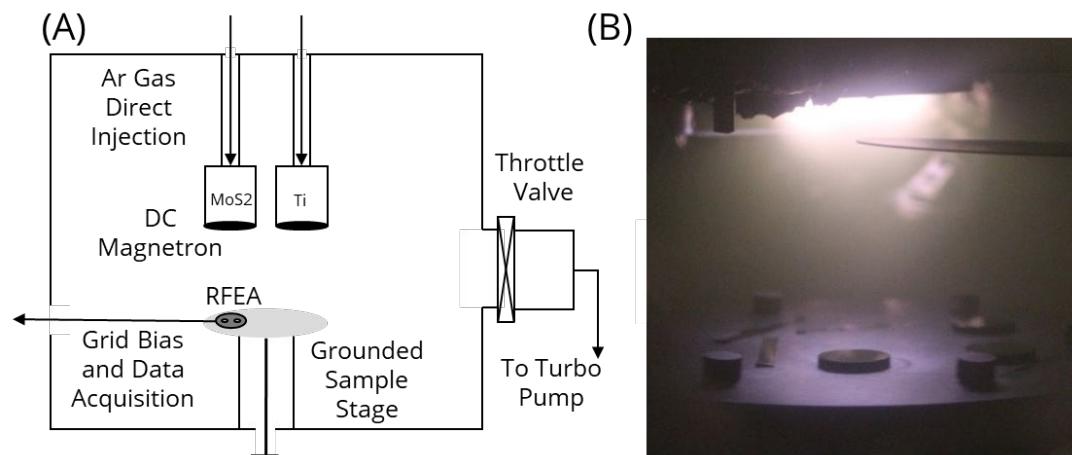
NASA

# SNL MoS<sub>2</sub> Thin Film Synthesis Capability

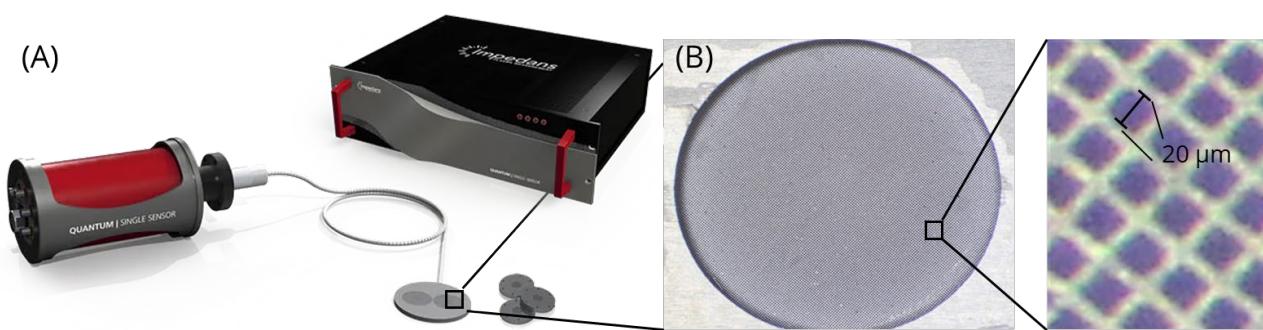
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- **Rapid turnaround for testing hypotheses**
- Filled a gap in capabilities for in-house research and production of PVD solid lubricants
  - Develop process-structure-property understanding to speed up responses to mission needs
  - **Collaborate with production** to solve production issues
  - **Increase efficiency vs external vendor**
  - **Built for ~1/4 the price of a commercial tool**
- **~150 deposition runs per year**
  - Supporting research and many development projects
- **Built for flexibility**
- Multiple RF, DC, Pulsed DC and HIPIMS power supplies with HIPIMS bias capable stage with liquid cooling

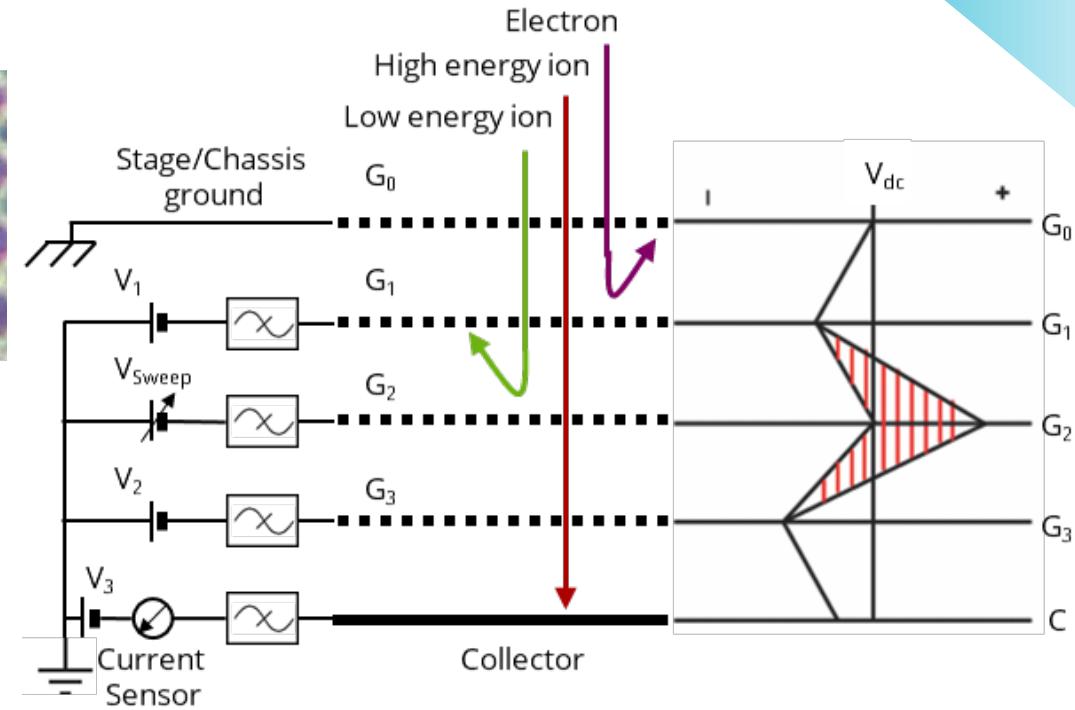


- 3 in. sputter cathodes
- 2x RF, 1x DC, 1x P-DC, 2x HIPIMS



## What Is an RFEA?

- Used industrially for “fingerprinting” – a method of transferring proven processes across different equipment setups
- Measures ion flux, the ion energy distribution, deposition rate and, deposition material ionization
- Isolates the effects of varying deposition conditions on plasma behavior
- Allows for direct correlation between plasma characteristics and film material properties

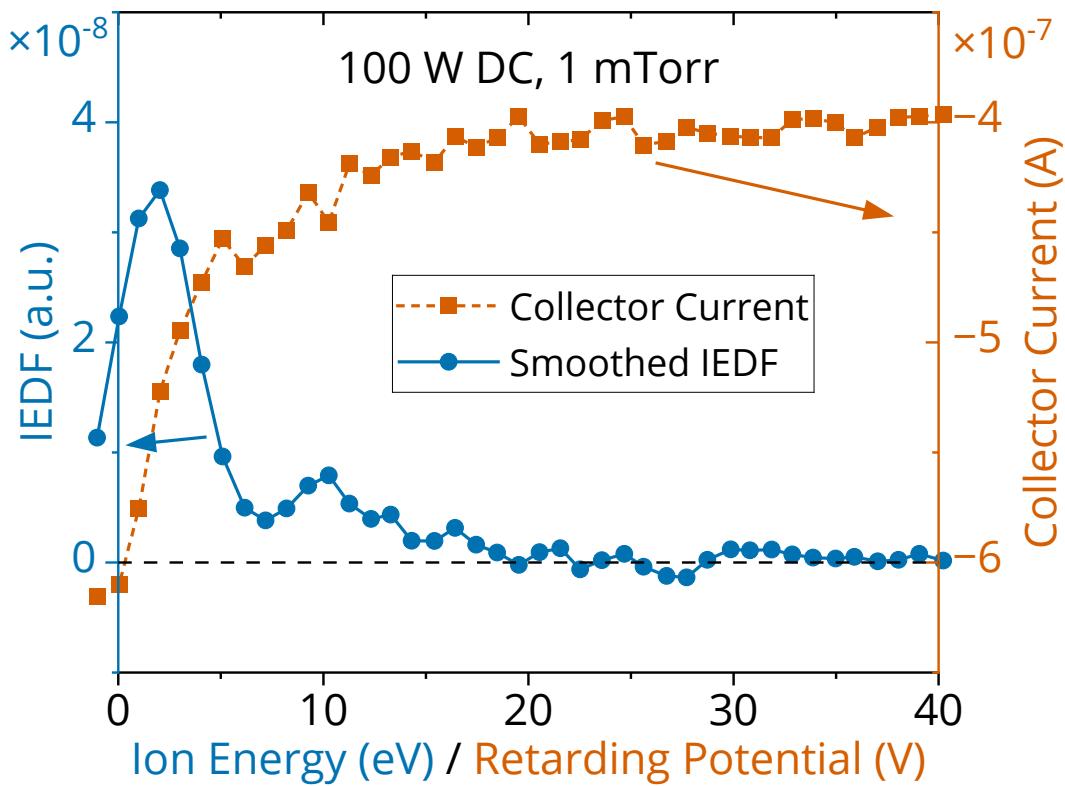


## How does this thing work?

- Grid 0 ( $G_0$ ) - holes less than Debye length to prevent plasma formation. Held at stage bias (ground)
- Grid 1 ( $G_1$ ) - Electron repulsion grid (-60 V)
- Grid 2 ( $G_2$ ) - Discriminator grid, sweeps to control ion flux based on energy
- Grid 3 ( $G_3$ ) - Secondary electron suppression grid (-70 V)
- Collector (C) - QCM and collector (-60 V)

# WHAT ARE WE MEASURING

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## I-V Curves

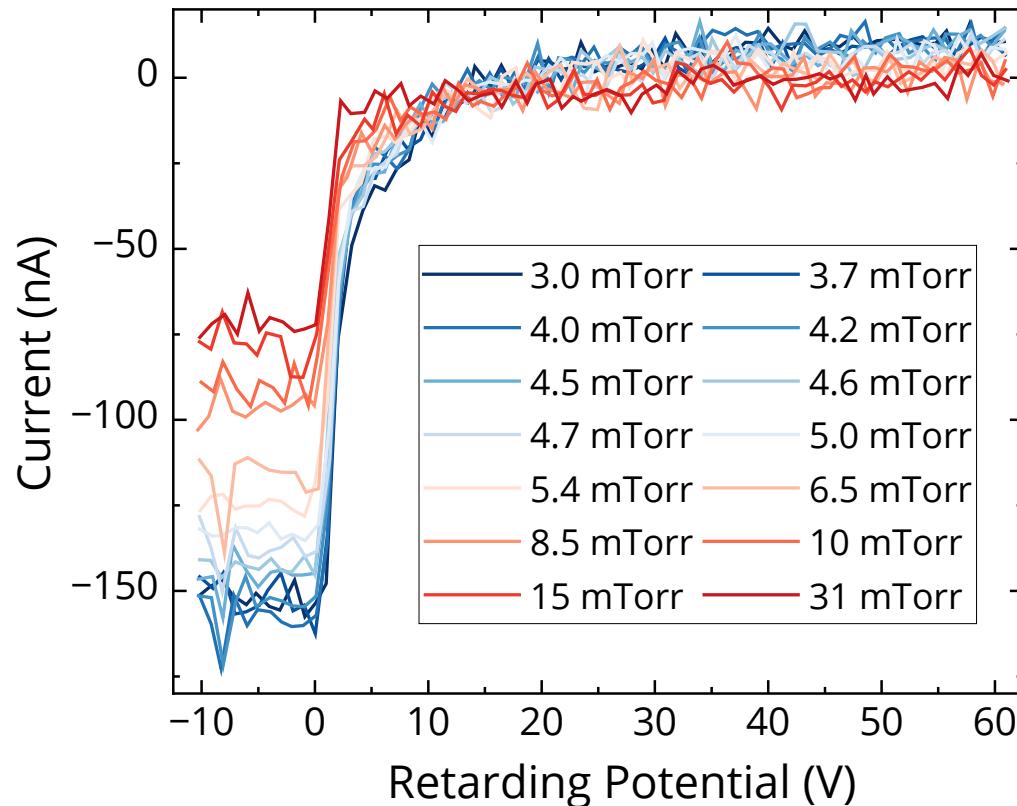
- The “retarding potential” represents the voltage on Grid 2 (ion repulsion) and the current is measured by the collector.
- A drop in current represents ion repulsion at that potential.
- The total drop in current is proportional to the total ion flux.

$$IEDF = \frac{dI}{dV} = f(E)$$

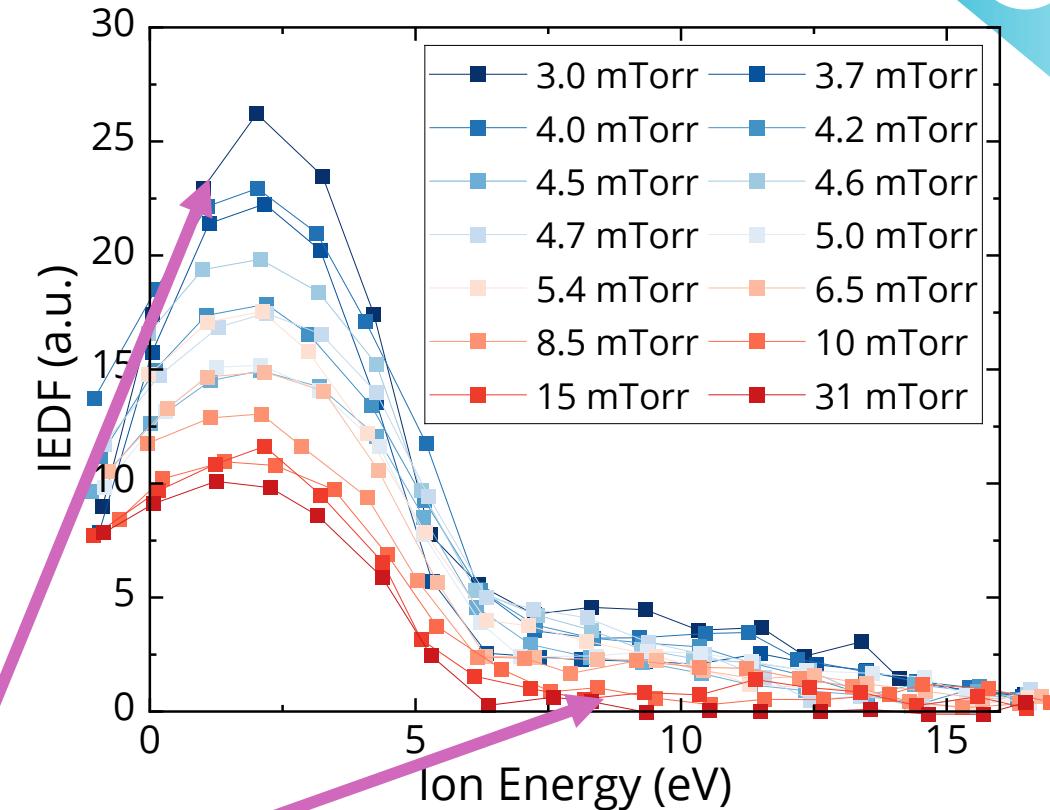
Where I is ion current, V is retarding potential and E is ion energy

- Savitzky-Golay smoothing is employed to minimize distortion in the ion energy distribution function (IEDF).<sup>7</sup>
- The IEDF represents the probability an ion has a specific kinetic energy.

# PRESSURE SERIES DATA



- Secondary peak at pressures lower than 5 mTorr  $\sim 10$  eV
  - Ar ions + the start of MoS<sub>2</sub> ionization
- Peak Ion density  $\sim 4$  mTorr



**Deposition Conditions**

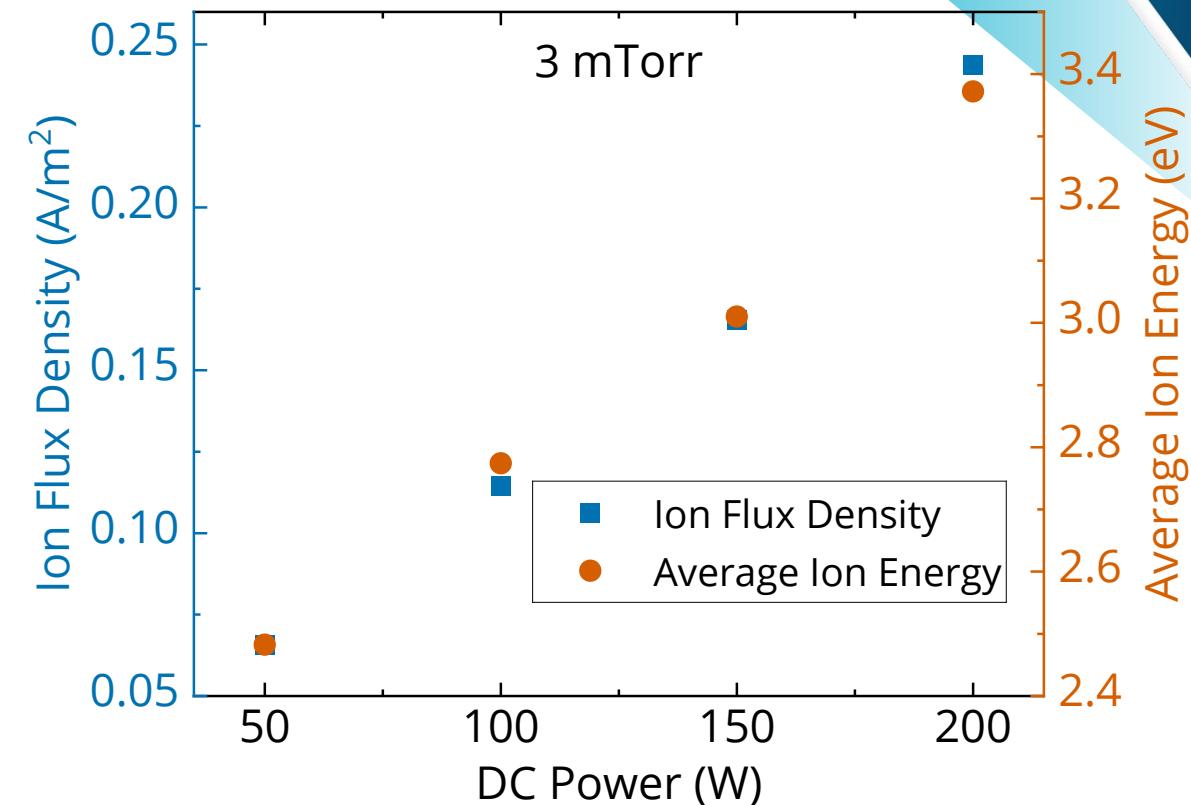
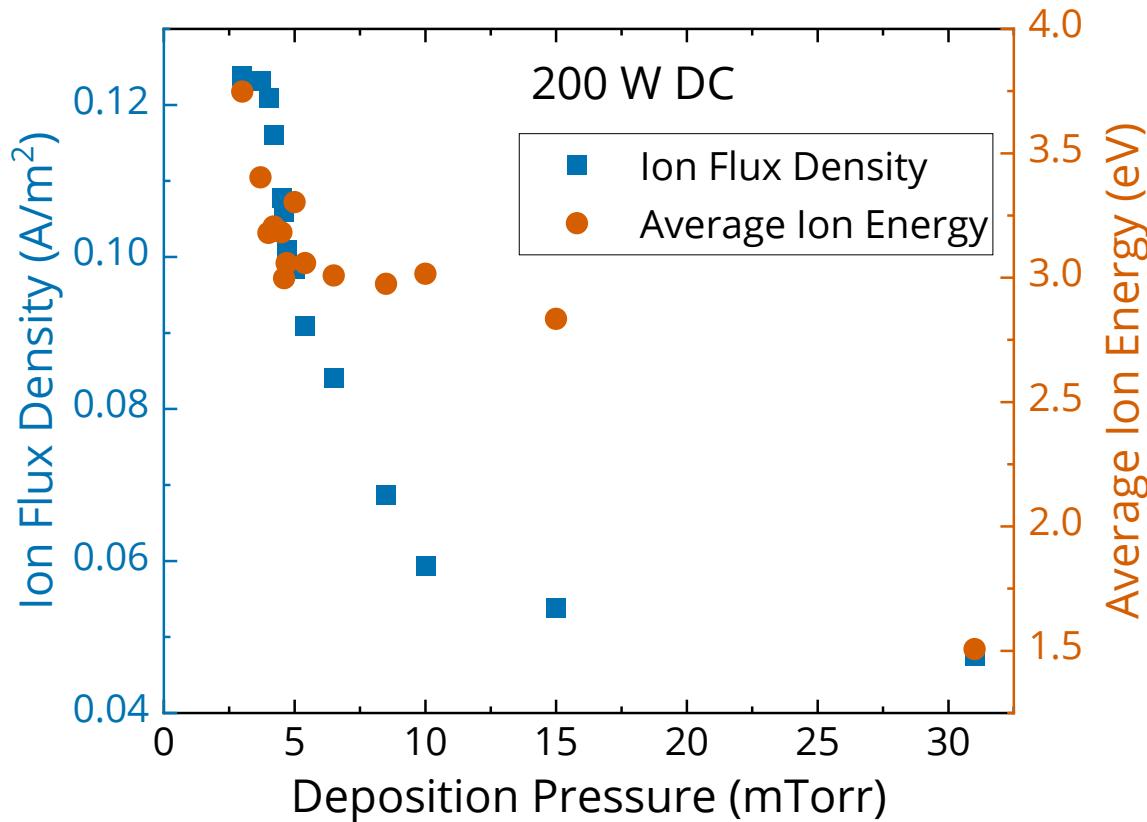
- Base pressure:  $< 1 \times 10^{-6}$  Torr
- Target to substrate distance: 4 in.
- Target diameter: 3 in.
- Ti adhesion layer thickness: 100 nm
- MoS<sub>2</sub> thickness: 1  $\mu$ m

**Sensor Conditions**

- Positioned directly under the target – in line with the deposition flux

# ION FLUX DENSITY AND AVERAGE ION ENERGY

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$$E_{AVG} = \frac{\int_{E_{min}}^{E_{max}} E f(E) dE}{\int_{E_{min}}^{E_{max}} f(E) dE}$$

$$J_{ion} = \frac{\int_{E_{min}}^{E_{max}} f(E) dE}{AT}$$

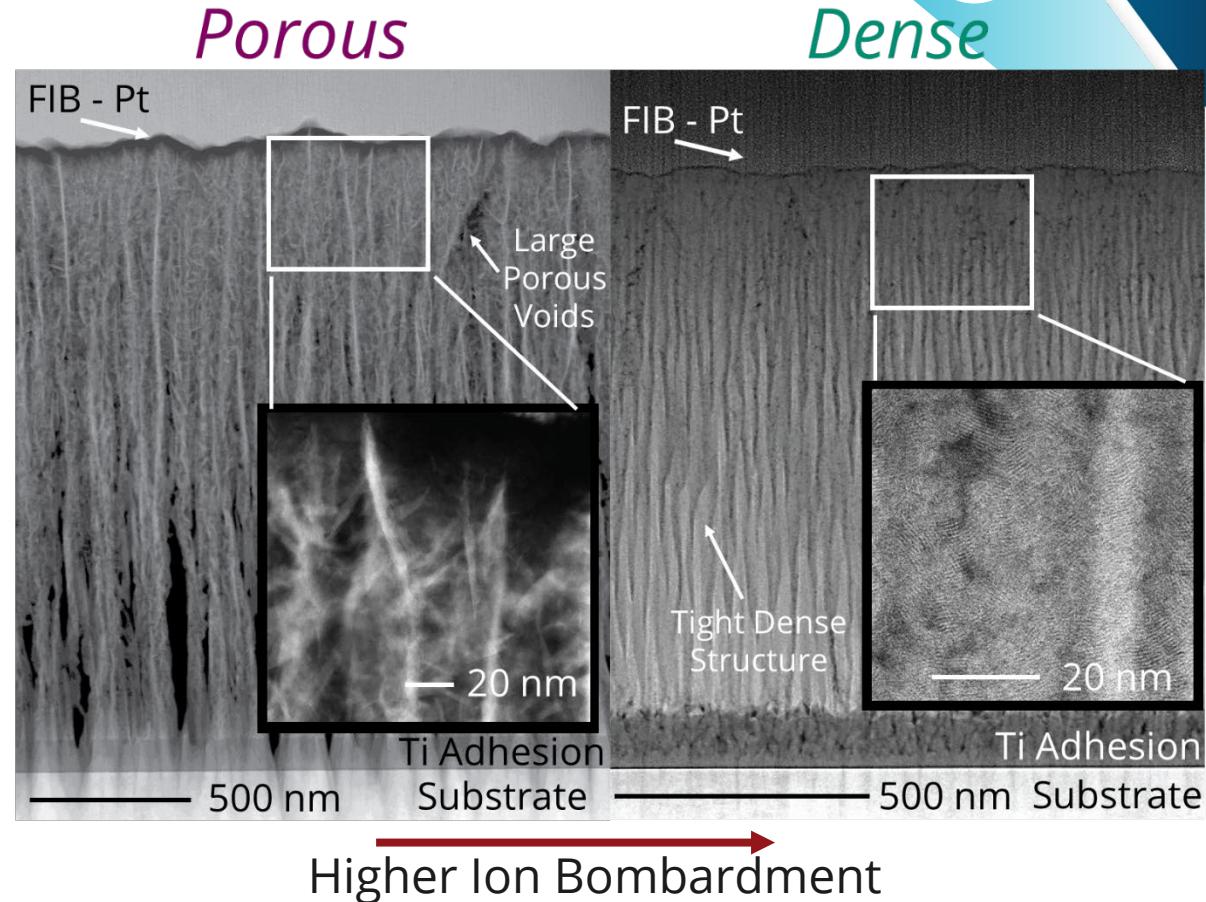
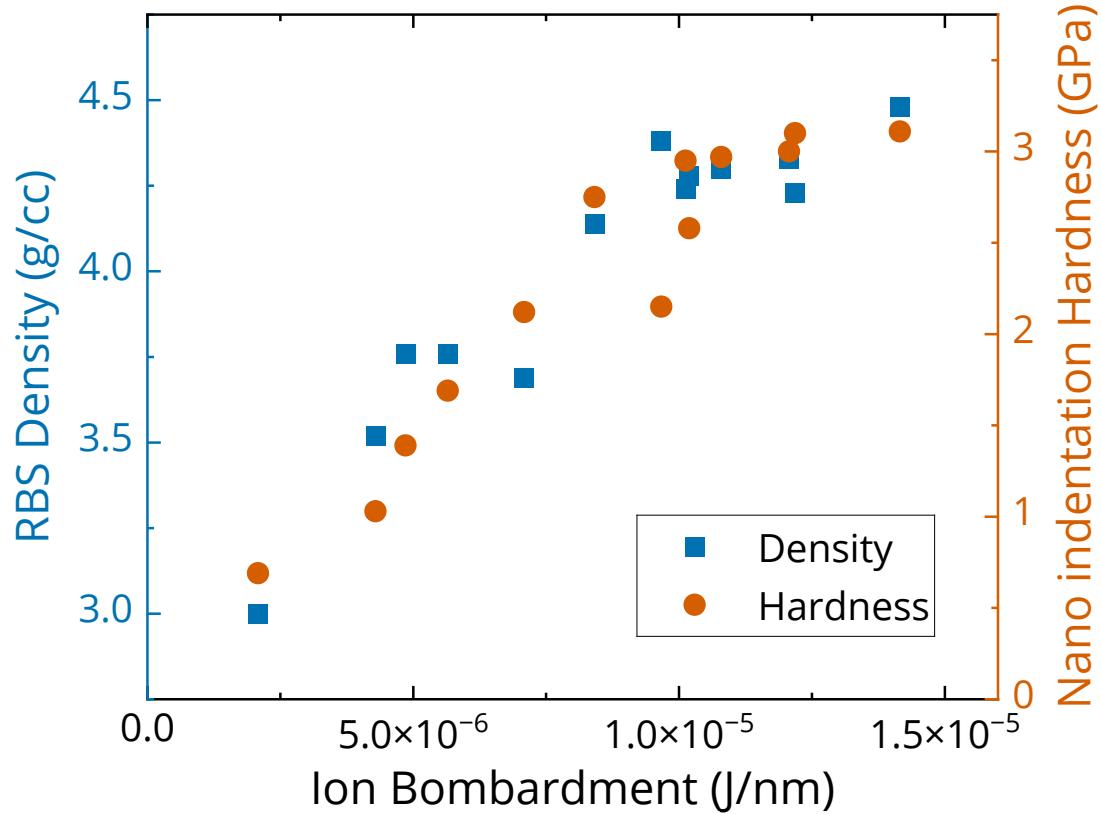
Where I is ion current, V is retarding potential and E is ion energy, A is the area of the aperture and T is the transmission of each of the 4 grids

- Both ion flux density and average ion energy increase with increased sputter power – resulting from increased accelerating voltage and amperage.
- Lower deposition pressure dramatically increases average ion energy – resulting from an increased mean free path.
- Lower pressure / higher power conditions produce higher energy ions – a well studied phenomenon.<sup>8</sup>

Garofano, V., Montpetit, F., Glad, X., Gangwar, R. K. & Stafford, L. Experiments and kinetic modeling of the ion energy distribution function at the substrate surface during magnetron sputtering of silver targets in radio frequency argon plasmas. *Journal of Vacuum Science & Technology A* **37** (2019).

# RELATING TO MATERIAL AND TRIBOLOGICAL PROPERTIES

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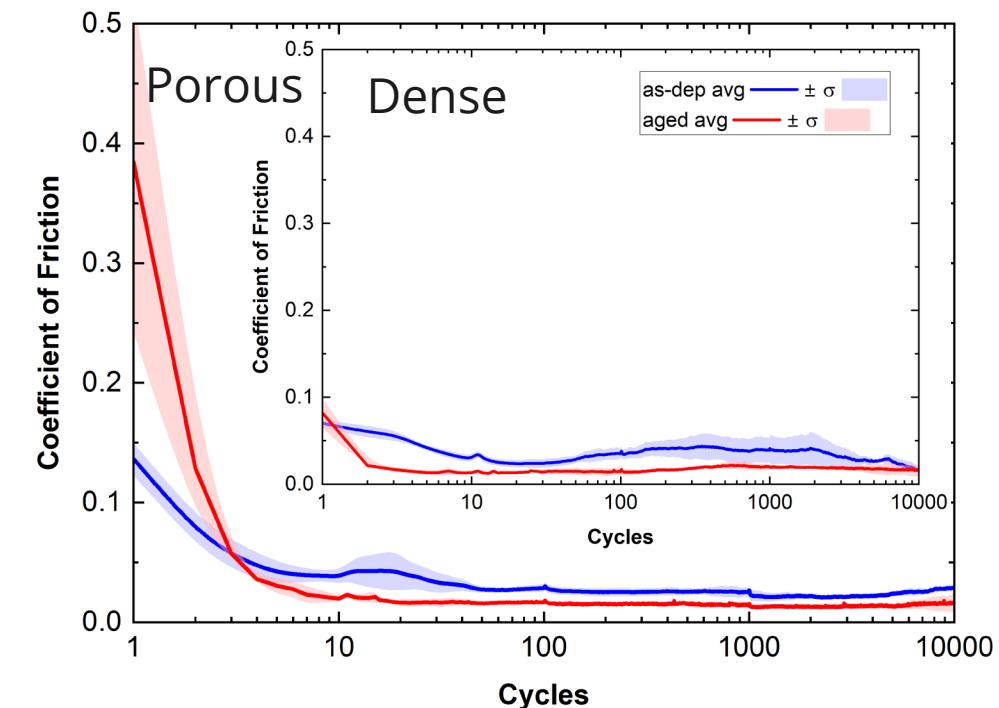
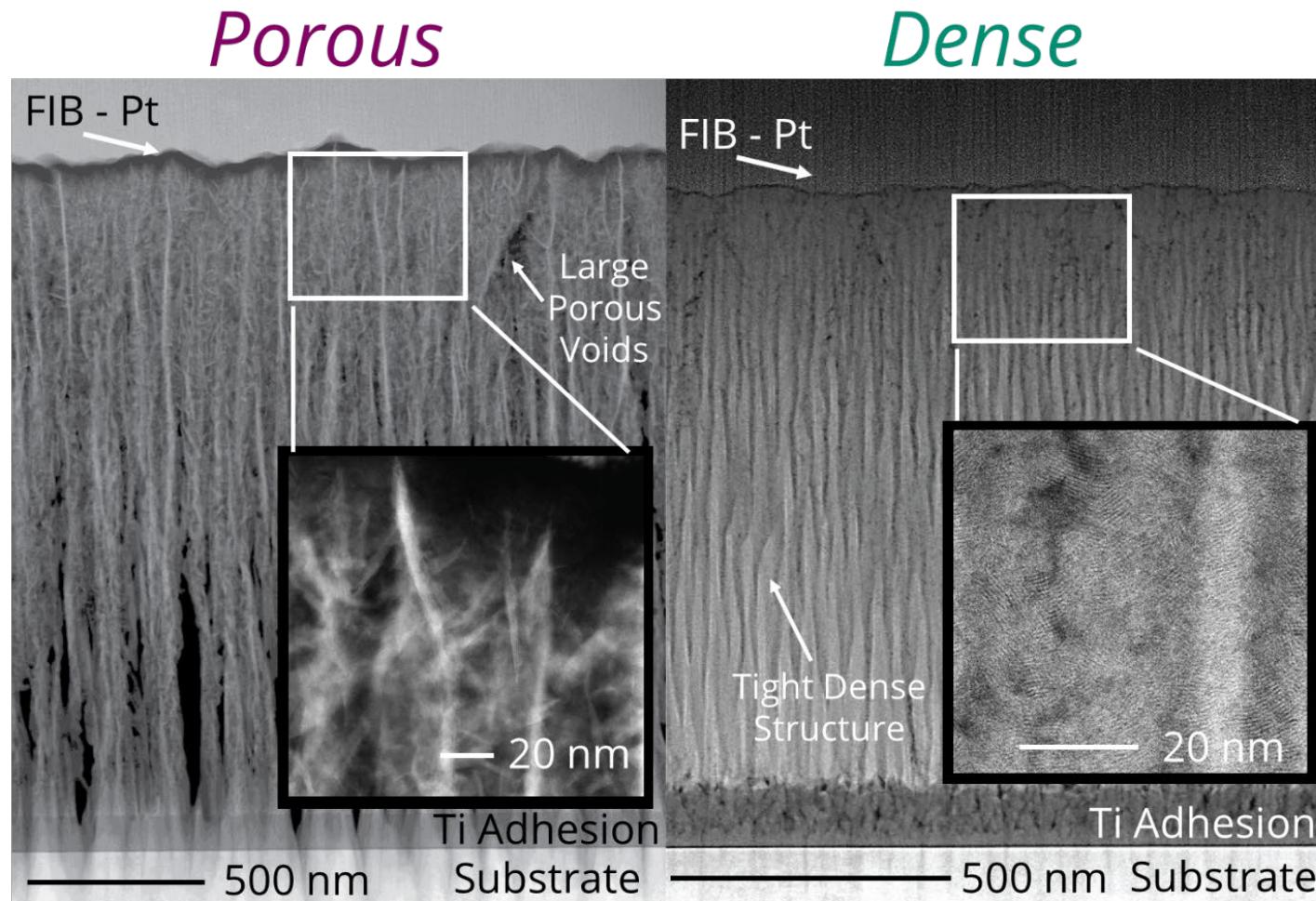
- Increased ion bombardment increases hardness of the film
  - This is well established for more controlled ion beam assisted depositions<sup>9</sup>

- This can be directly seen in TEM of the deposited films
  - Low bombardment films as significantly more porous

(9) Smidt, F. Use of ion beam assisted deposition to modify the microstructure and properties of thin films. *International Materials Reviews* **35**, 61-128 (1990).

# QUESTIONS

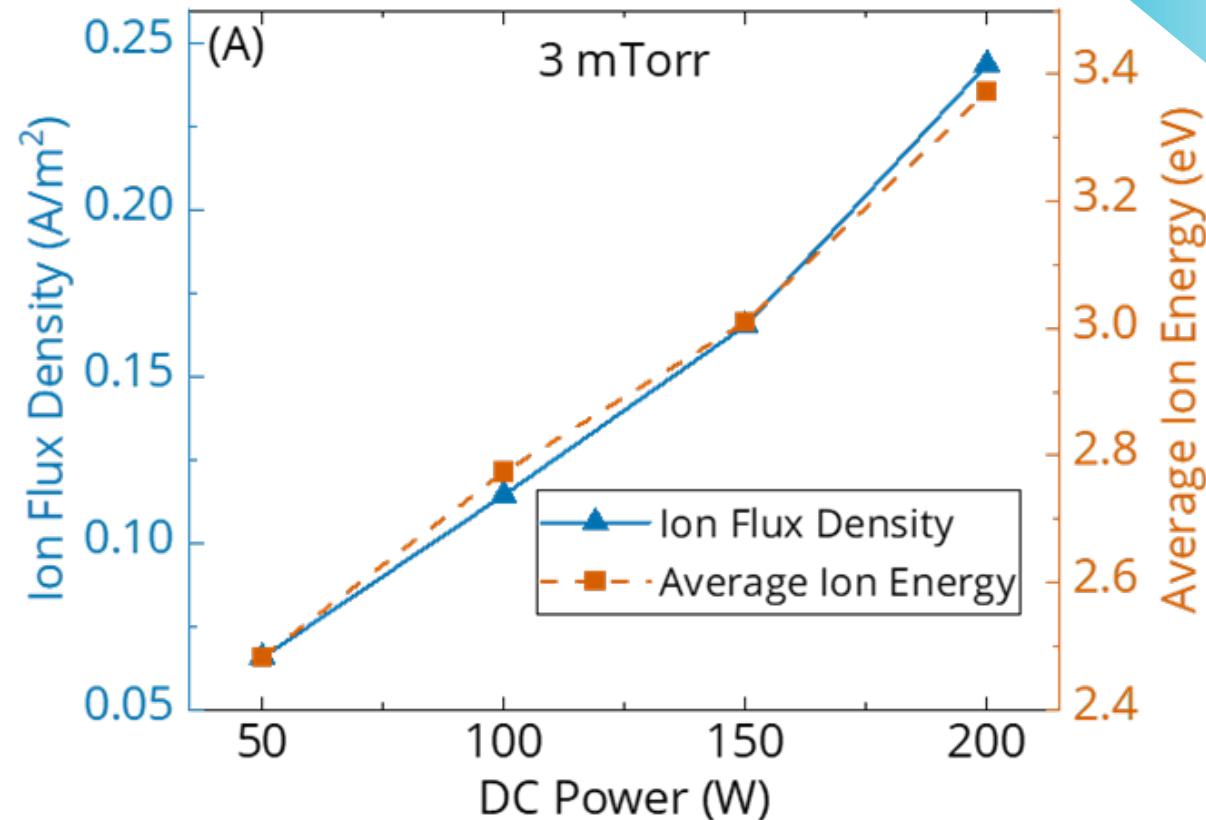
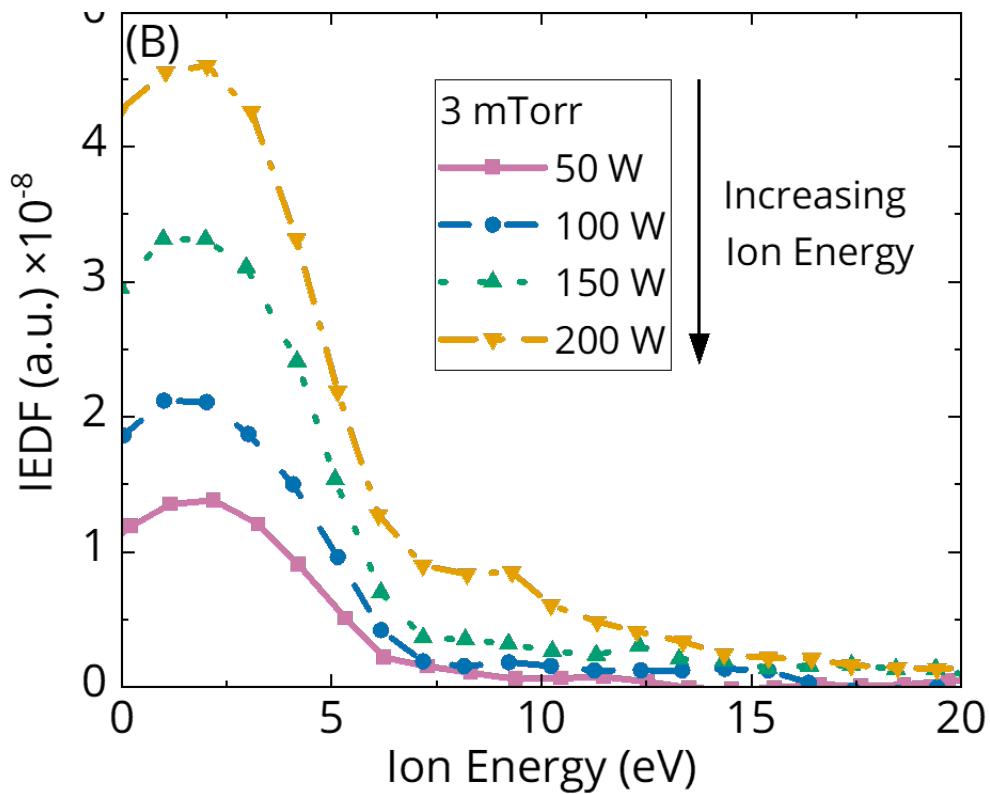
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# BACK UP SLIDES

# POWER SERIES DATA

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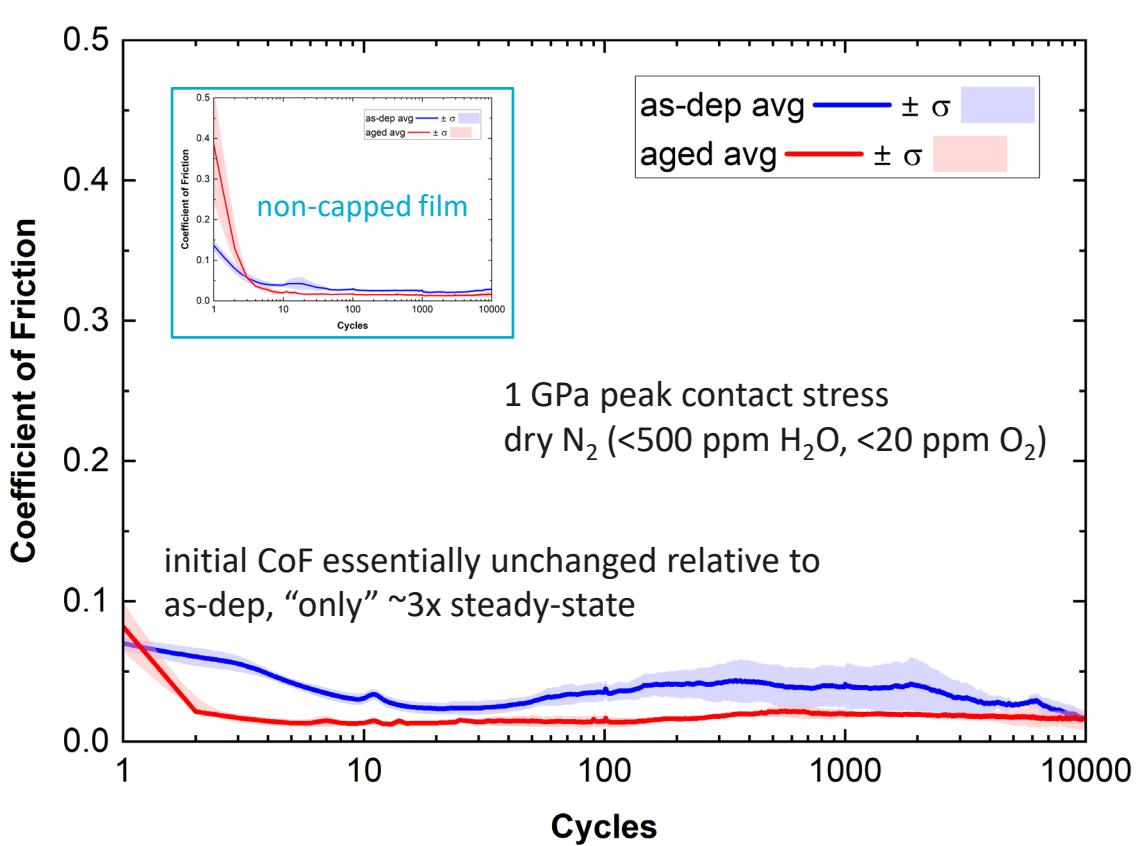
- Lower pressure / higher power conditions produce higher energy ions – a well studied phenomenon.<sup>8</sup>

$$E_{AVG} = \frac{\int_{E_{min}}^{E_{max}} Ef(E) dE}{\int_{E_{min}}^{E_{max}} f(E) dE} \quad J_{ion} = \frac{\int_{E_{min}}^{E_{max}} f(E) dE}{AT}$$

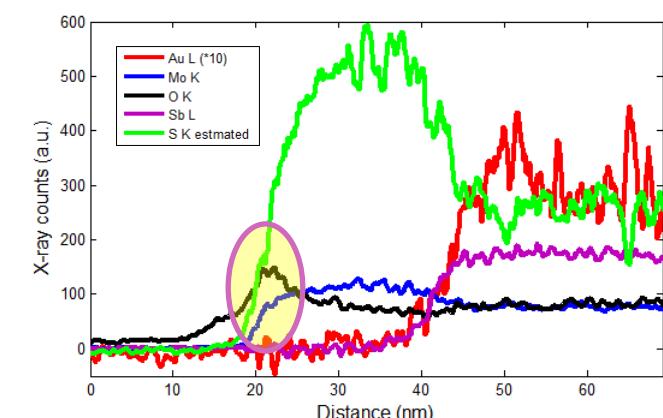
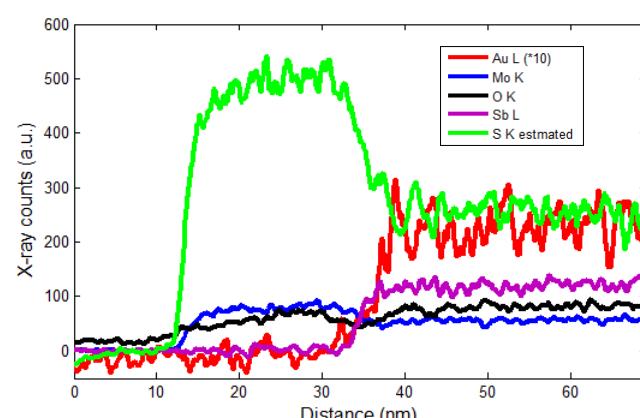
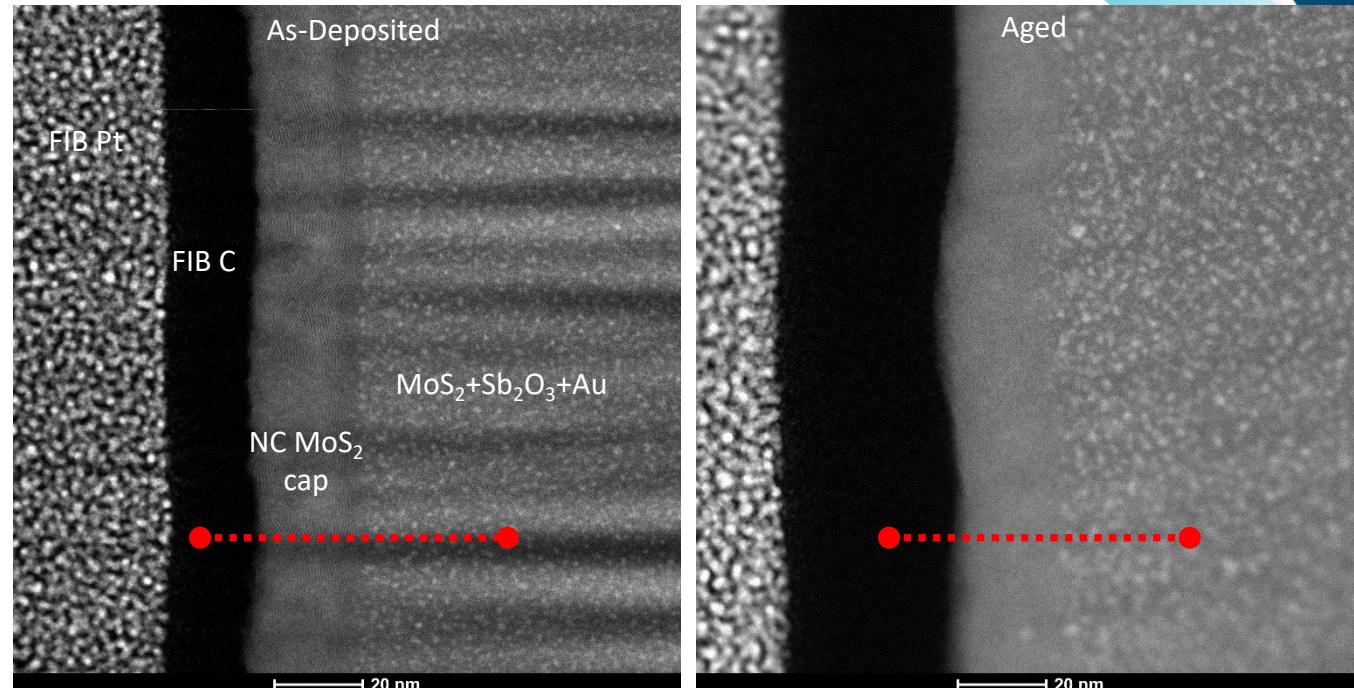
Where  $I$  is ion current,  $V$  is retarding potential and  $E$  is ion energy,  $A$  is the area of the aperture and  $T$  is the transmission of each of the 4 grids

# TRIBOLOGICAL BEHAVIOR OF MULTILAYER PVD $\text{MoS}_2$ PRE- AND POST-AGING

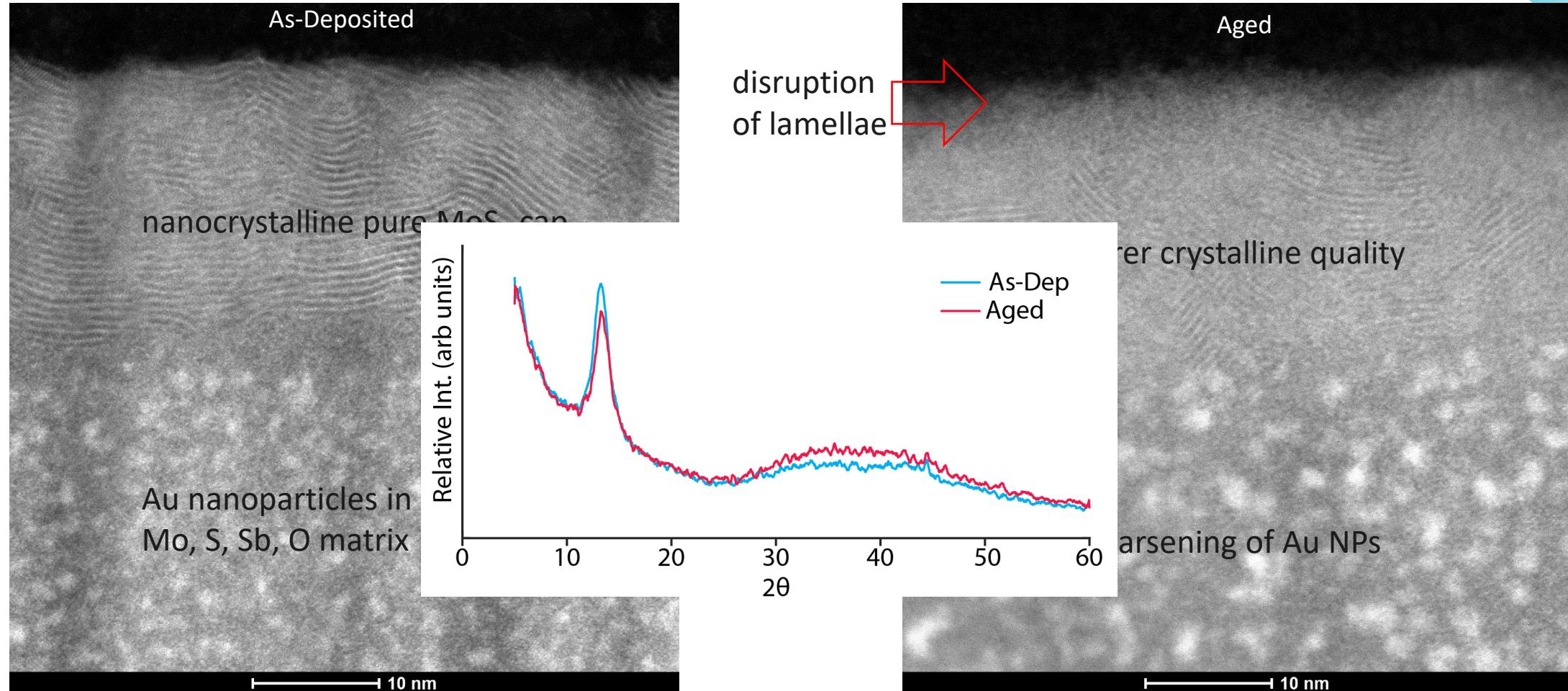
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- Starting friction is virtually unchanged in the aged film relative to the as-deposited film
- Oxygen is incorporated into the top ~5 nm of the aged film

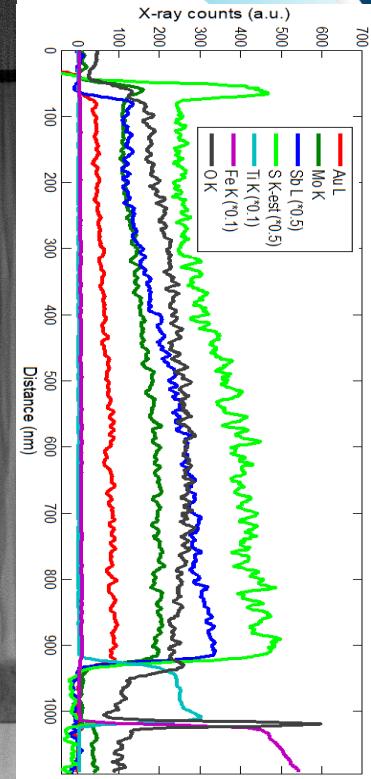
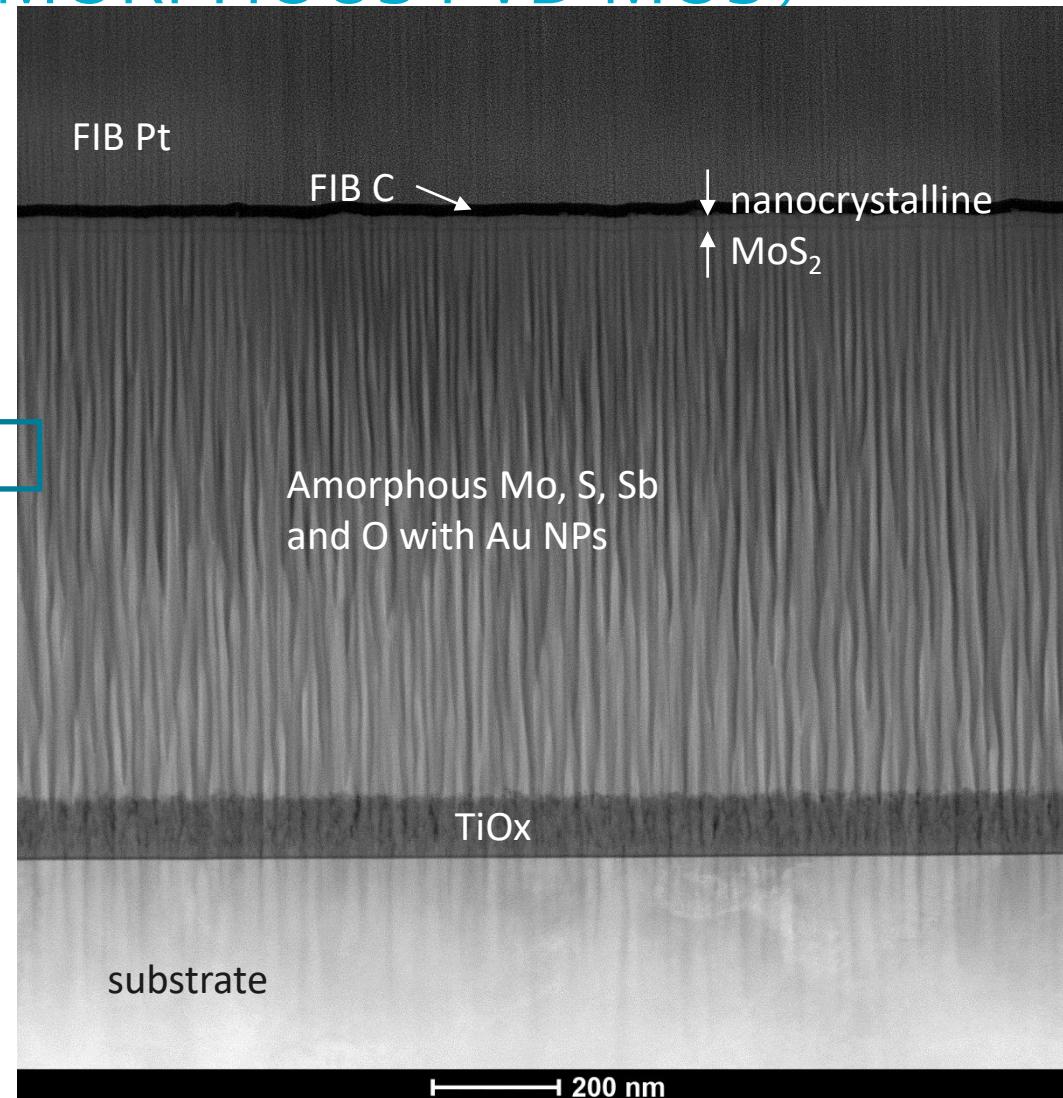
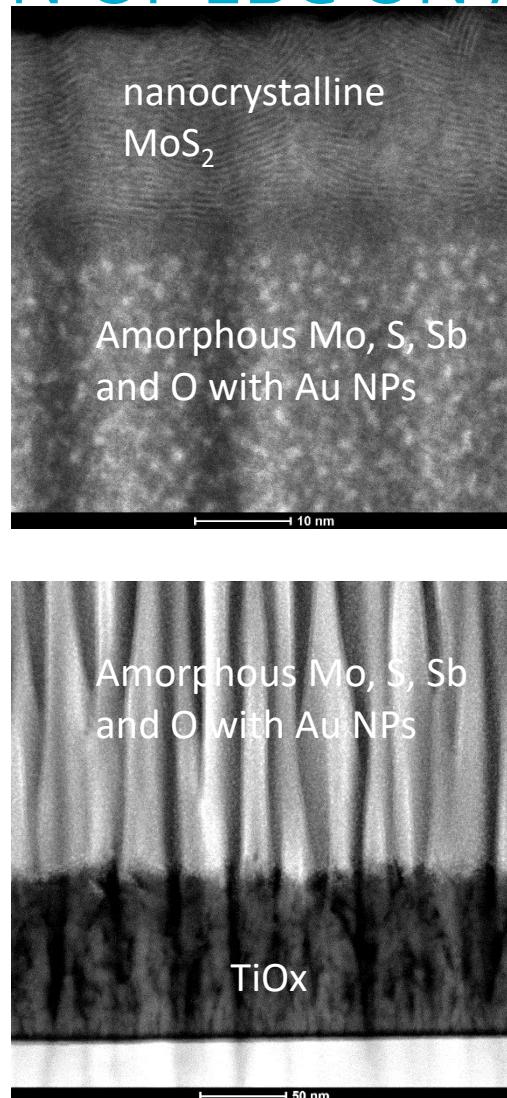
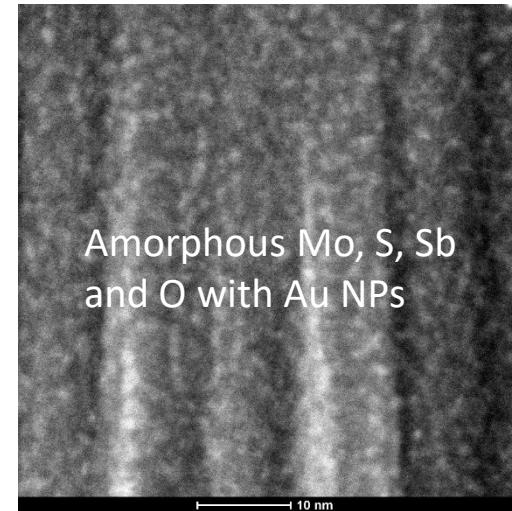


# DETAILED STRUCTURE OF MULTILAYER $\text{MOS}_2$ NEAR SURFACE, PRE- AND POST-AGING



- Accelerated aging causes disruption of the crystalline lamellae at the surface, poorer crystallinity in the nanocrystalline cap, and coarsening of Au nanoparticles in the bulk

# REALIZATION OF EBC ON AMORPHOUS PVD MOS<sub>2</sub>



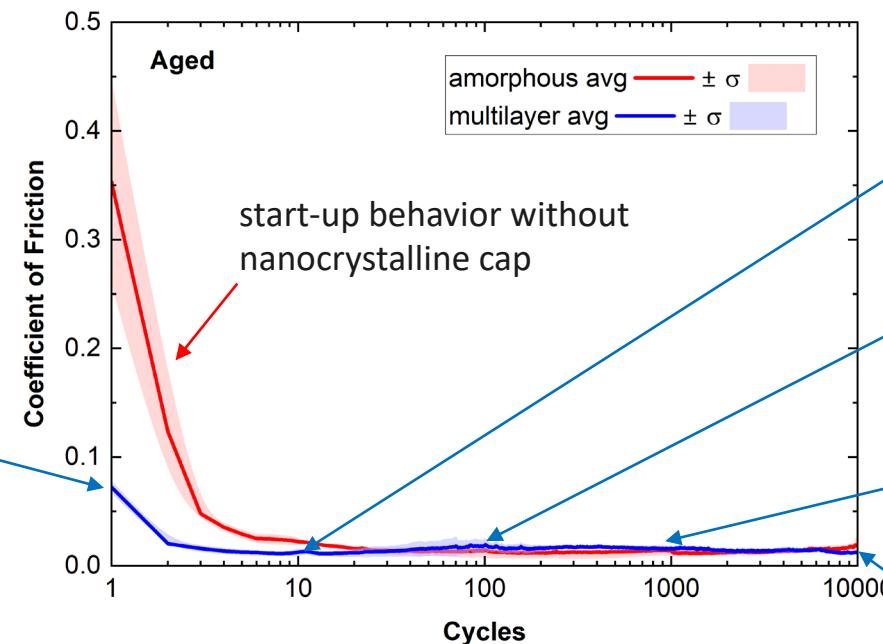
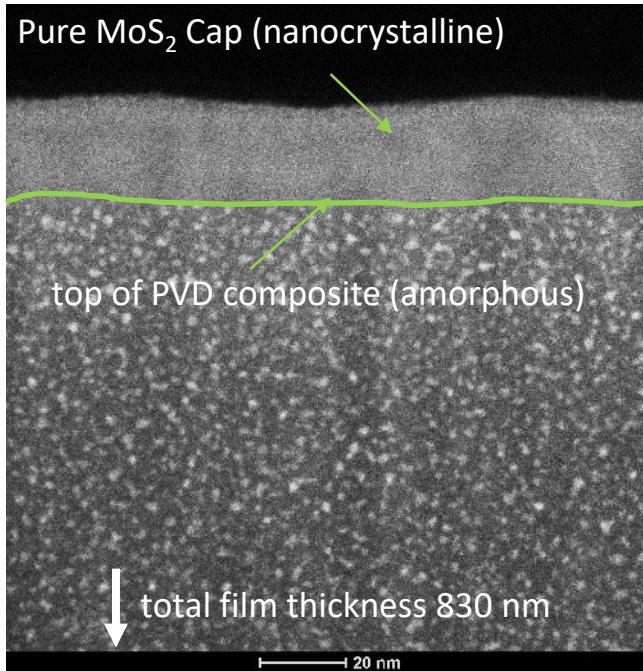
- A dense nanocrystalline pure MoS<sub>2</sub> layer was deposited on top of a dense, amorphous Sb<sub>2</sub>O<sub>3</sub> and Au-doped layer

# Low Friction Persists When the Nanocrystalline Cap is Worn Through

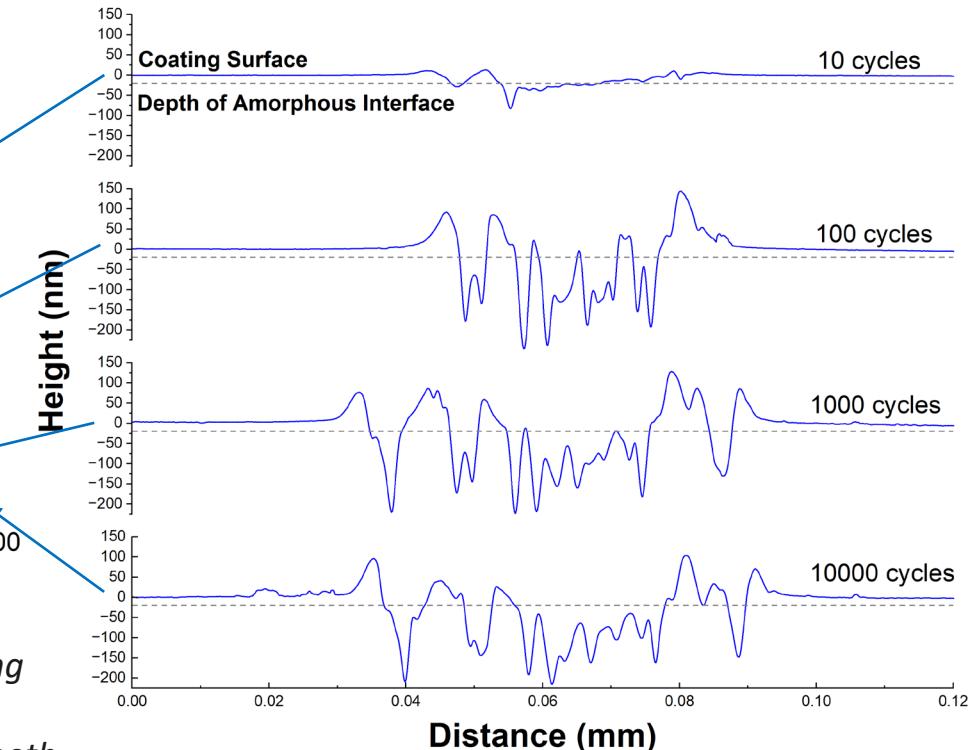
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## Multilayer Film



## Wear Track Profiles



*Hypothesis:* The nanocrystalline cap provides low starting friction and environmental stability, while stress-induced transformation below the sliding interface enables a smooth transition to low-wear bulk behavior

- No increase in friction is observed when the nanocrystalline layer is worn through over most of the track width at  $\sim 100$  cycles
  - capping of the amorphous coating allows combination of the low start-up friction of nanocrystalline pure MoS<sub>2</sub> with the wear resistance of amorphous coatings