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Effects of Oxygen Impurities on Long-Term Gaseous Hydrogen Embrittlement of Structural Steels

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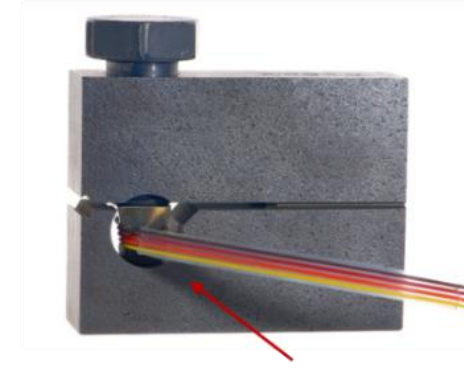
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Overview

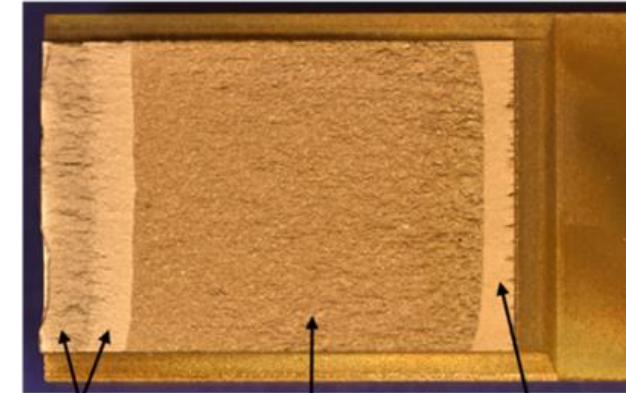
- Background and motivation
 - Examples of the mitigating effects of oxygen impurities on hydrogen embrittlement in laboratory testing
- Experimental methods
 - Long-term, constant displacement fracture tests in high pressure gaseous hydrogen environments
 - Commercial pressure vessel and pipeline steels
- Experimental results
 - Comparison of subcritical crack growth in high-pressure hydrogen and hydrogen with varying degrees of oxygen impurities
- Conclusions and future research

Wedge-opened Loaded (WOL) Sample



Reaction pin (load tup) with externally monitored strain gauge

Grade L: WOL Fracture Surface



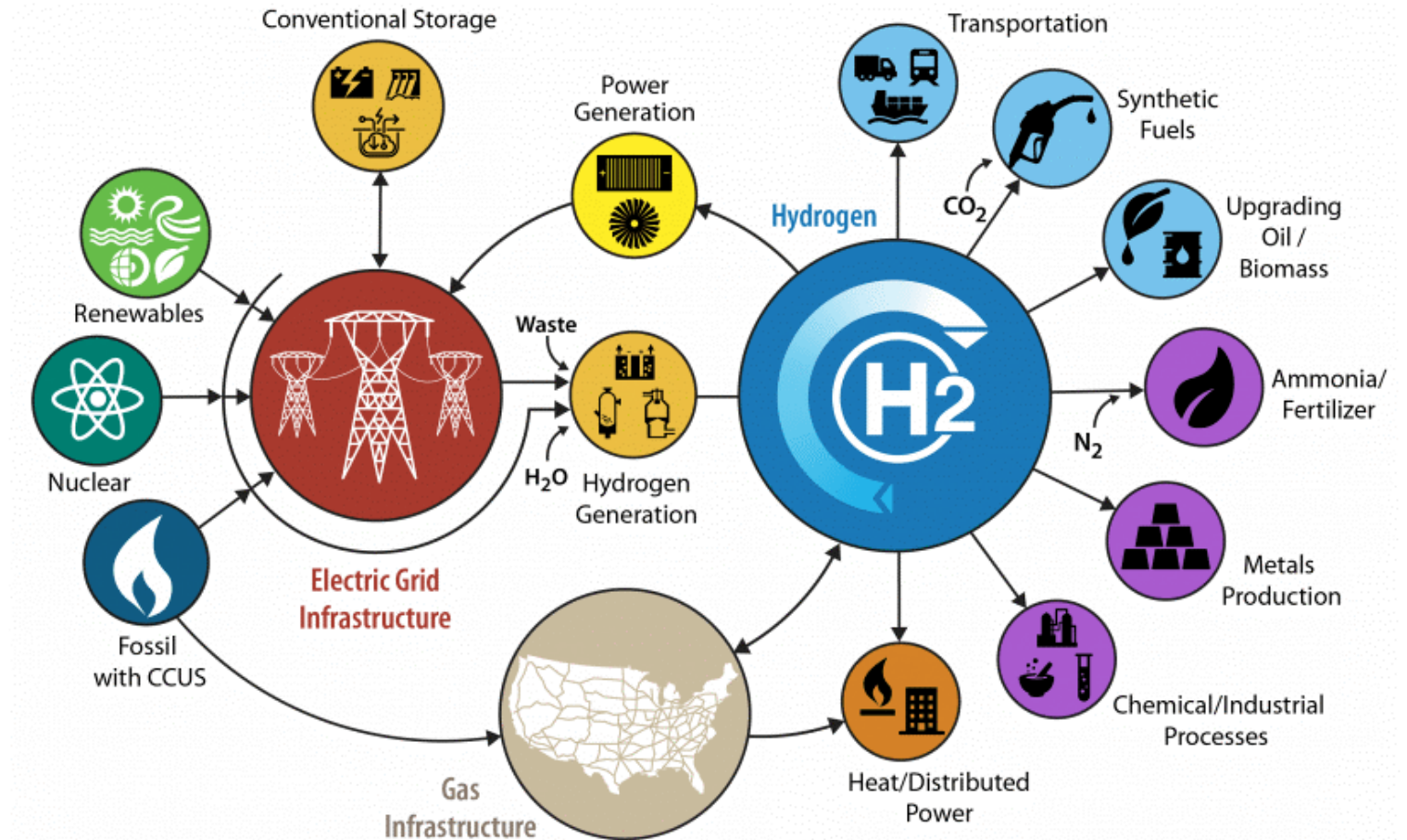
Post-test fatigue and LN₂ fracture

Fatigue precrack (in air)

Crack growth in H₂ + 100PPM O₂

Hydrogen has a key role to play in a sustainable future

- Hydrogen has many potential avenues for decarbonization across many sectors
 - Energy storage, waste energy conversion
 - Transportation
 - Residential/industrial heating and appliances
 - Steel, cement production



Hydrogen degrades fatigue and fracture resistance

- Hydrogen-assisted fracture and fatigue is influenced by:

- Materials

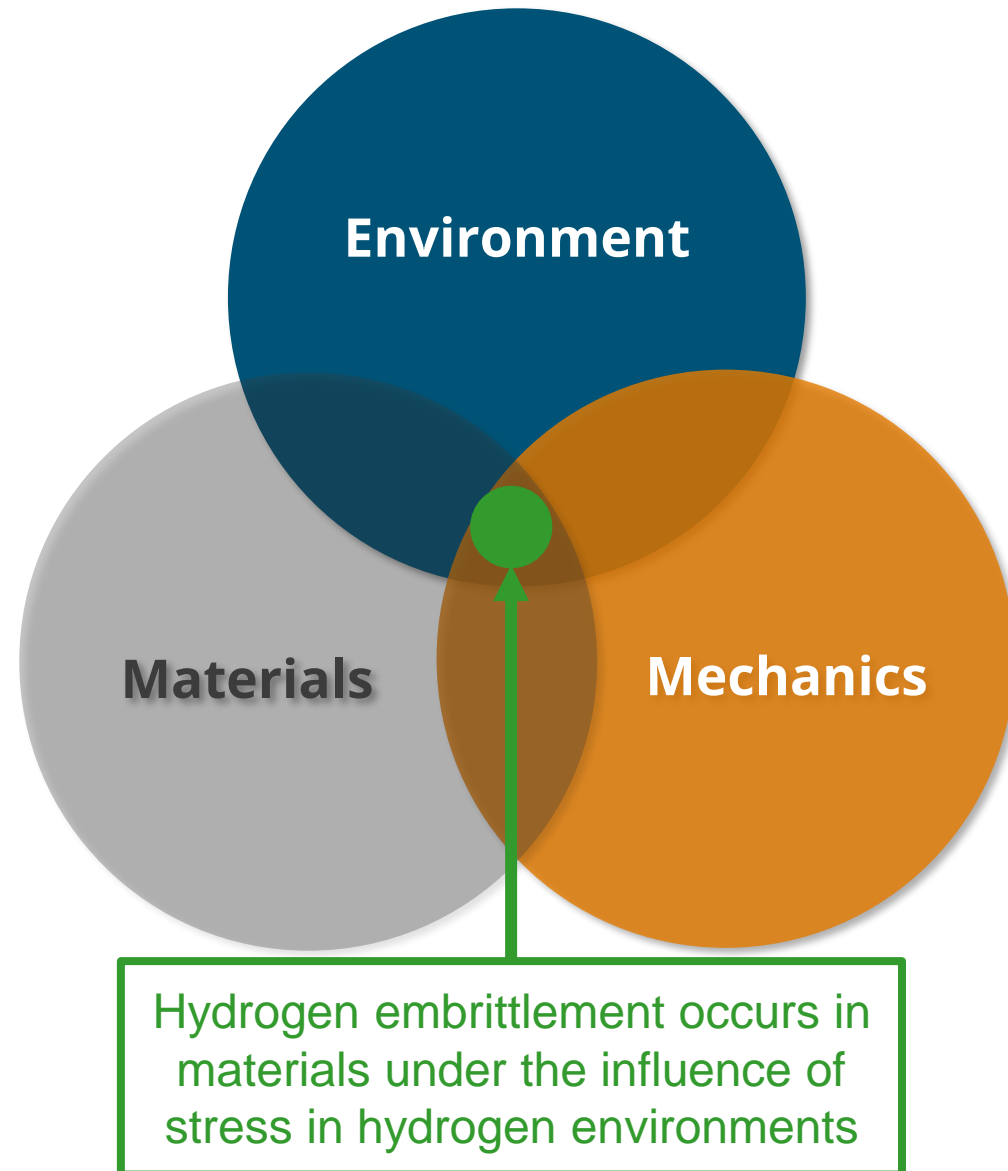
- Yield/tensile strength
- Microstructure, homogeneity, etc.

- Environment

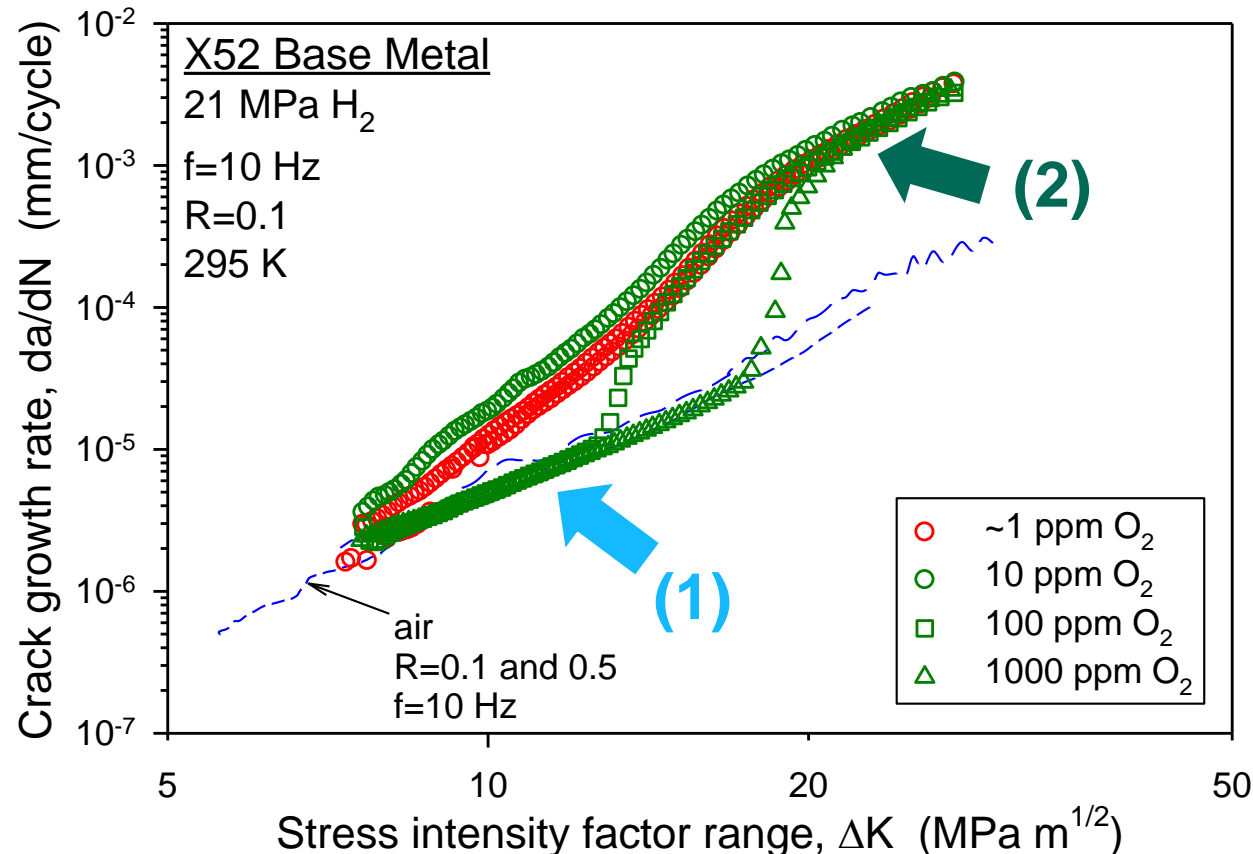
- Partial pressure of hydrogen
- Impurities (e.g., O_2)
- Temperature

- Mechanics

- Stress state
- Stress (pressure) cycling
- Residual stresses/work hardening



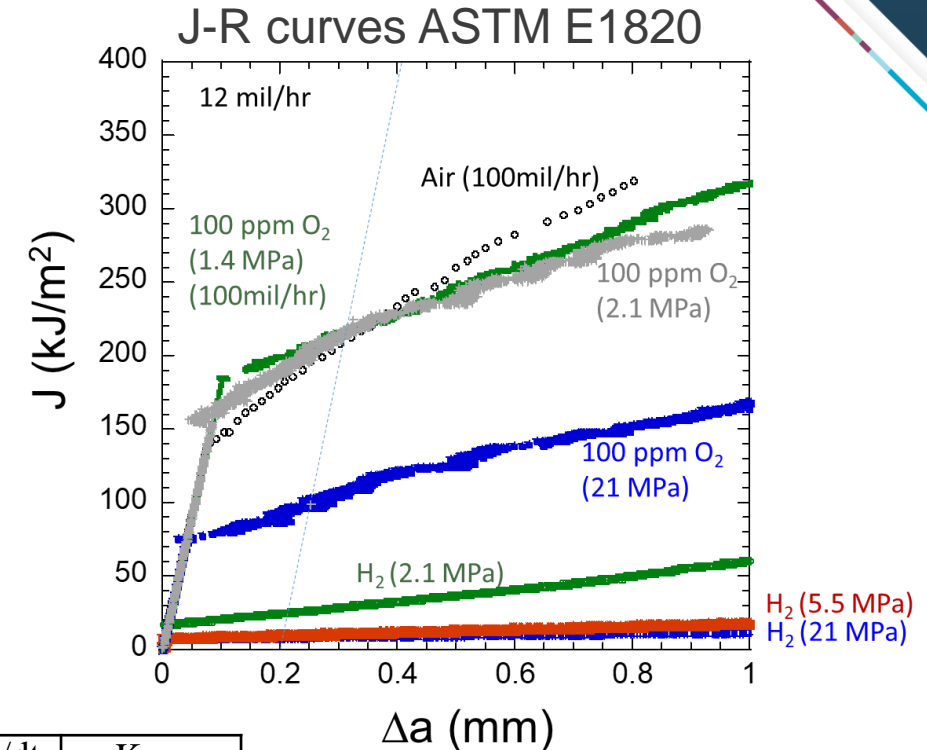
Oxygen is known to affect measurements of fatigue



- Numerous examples of trace gases mitigating fatigue crack growth rate (FCGR) in laboratory conditions
- Example:
 - (1) Oxygen reduces FCGR comparable to air
 - (2) Oxygen has no effect on FCGR in H_2

Oxygen moderated hydrogen-assisted fracture

- Fracture toughness K_{JQH} values decreased by over 60% in pure H_2 at 2.1 MPa
- In 21 MPa mixed gas (100 ppm O_2), fracture toughness decreased by only 30% relative to air
 - In pure H_2 at 21 MPa, relative decrease was 80%
- At lower pressures (1.4-2.1 MPa) in mixed gas, no effect of hydrogen was measured

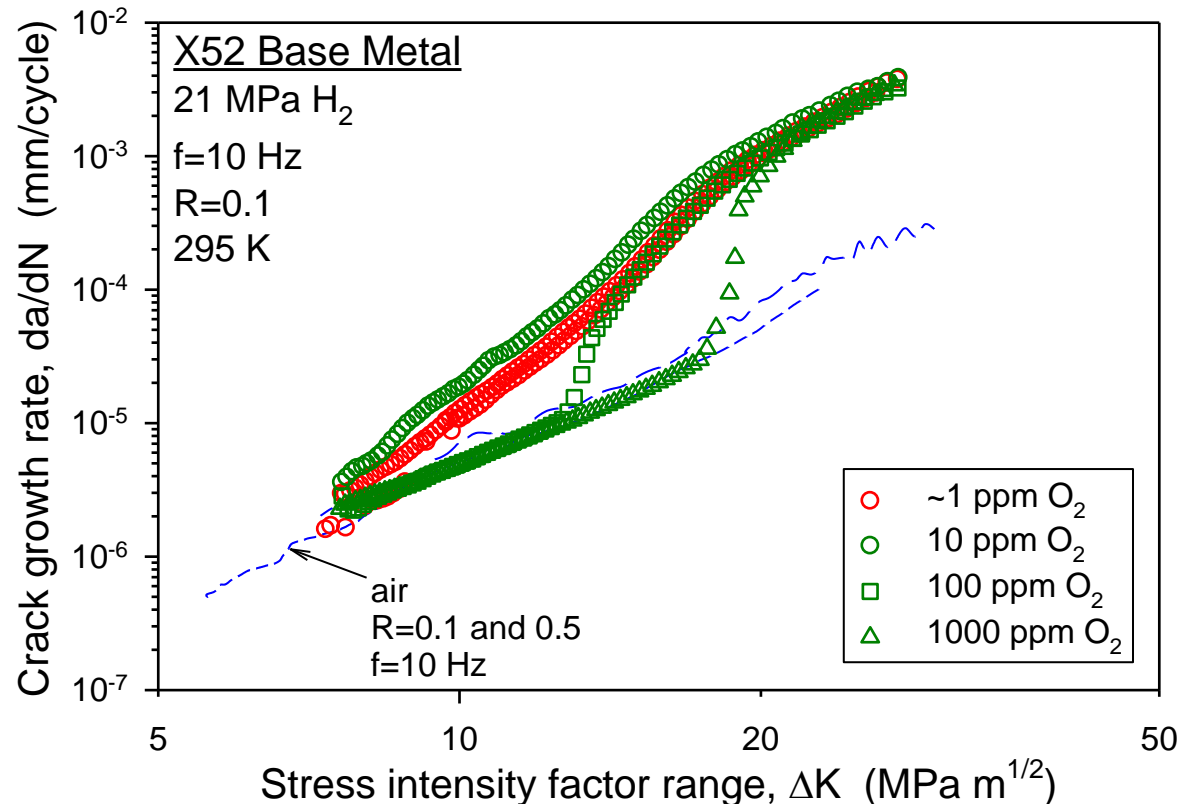


Sample ID	Environment	Test Pressure (MPa)	Actuator rate (mm/hr)	da/dt (m/s)	K_{JQH} (MPa $m^{1/2}$)
X100-51	Air	-	2.5	5.0E-7	217
X100-52	Air	-	2.5	1.4E-7	202
X100-5	H2	21	0.3	8.5E-7	43
X100-6	H2	5.5	0.3	3.6E-7	47
X100-7	H2	2.1	0.3	1.7E-7	75
X100-53	H2 + 100 ppm O2	21	0.3	1.1E-7	151
X100-55	H2 + 100 ppm O2	2.1	0.3	7.4E-8	222
X100-56	H2 + 100 ppm O2	1.4	2.5	1.0E-7	222

60 - 80% reduction

30% reduction

Oxygen has been shown to mitigate hydrogen embrittlement in laboratory tests



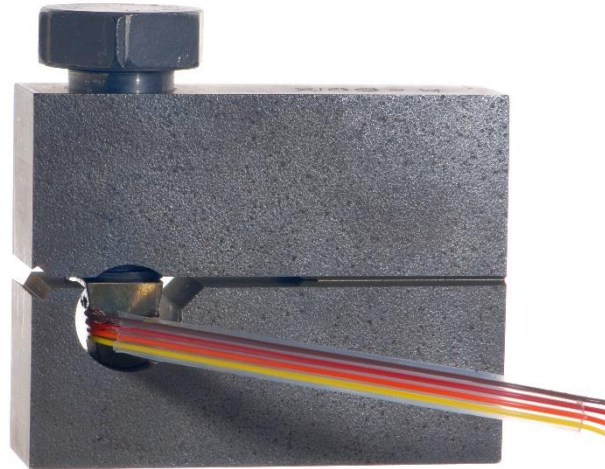
- Fatigue and fracture measurements can be significantly impacted by oxygen impurities
- Fatigue crack growth tests are typically performed at 1 Hz (\pm decade)
 - $da/dN = 10^{-5}$ mm/cycle
 - Time for $\Delta a = 1$ mm: ~1 day
 - 1 day = 0.02% of 10 year life
- Are the time scales of a typical laboratory fatigue test sufficient to demonstrate kinetics over decades?
 - More accurately simulate the mechanical/environmental conditions that components see when in use
 - Does trace oxygen have long term mitigation effects on hydrogen embrittlement?

Sustained load testing can be executed over periods of days to weeks to months to years



- Fixed (constant) displacement fracture tests
- Fatigue pre-cracked and loaded in ambient air
- Placed in pressure vessels & pressurized up to 140 MPa gaseous environment
 - Experiments in this study were performed at 103MPa
- Instrumented reaction pins allow for the determination of incubation time
- Directly compare subcritical crack growth in hydrogen and mixed gas environments

Wedge-opened loaded (WOL) test sample



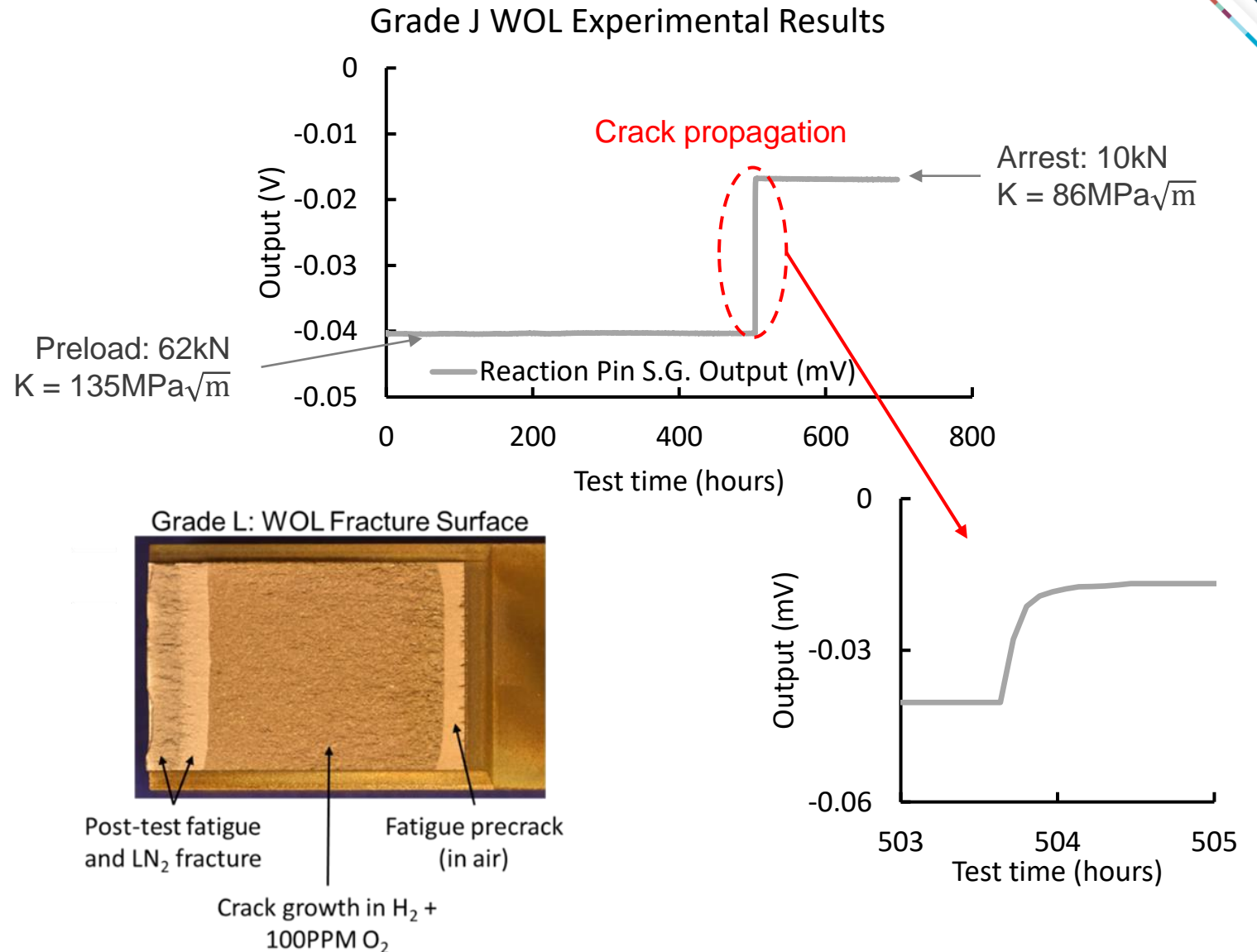
Pressure vessels for medium and long term experiments



ASTM E1681 – Threshold Stress Intensity Factor for Environment-Assisted Cracking

Crack initiation and growth rates were measured during constant displacement fracture experiments

- Instrumented reaction pins allow for determination of incubation time and crack growth rates
 - Continuous data collection throughout the duration of the experiments
- Time between the initial crack propagation and arrest can range between seconds to hours
 - With a constant displacement, the crack growth rates can be determined from the load on the reaction pin
- Post-test fatigue and heat tinting are used to mark fracture surfaces



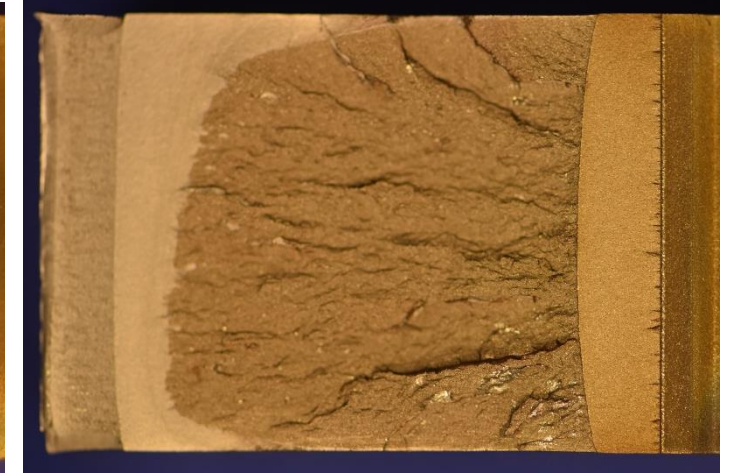
Material selection and fracture surfaces

- SA372 Grade J steel
 - Heat A: YS = 700 MPa
 - Heat B: YS = 750 MPa
- SA372 Grade L steel
 - YS = 730 MPa
- X100 pipeline steel
 - YS = 760 MPa
- Precipitation Hardened 13-8 stainless steel
 - YS = 1480 MPa

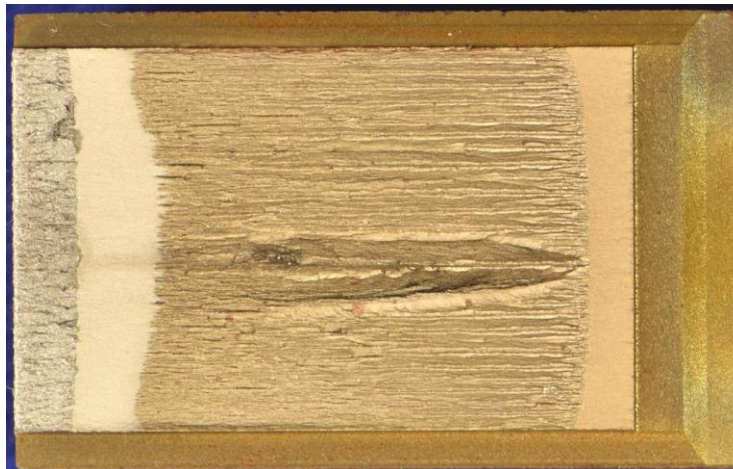
Grade L



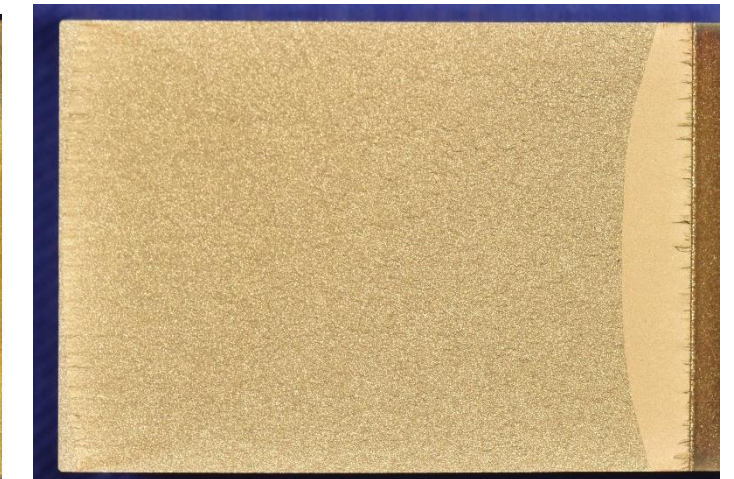
Grade J



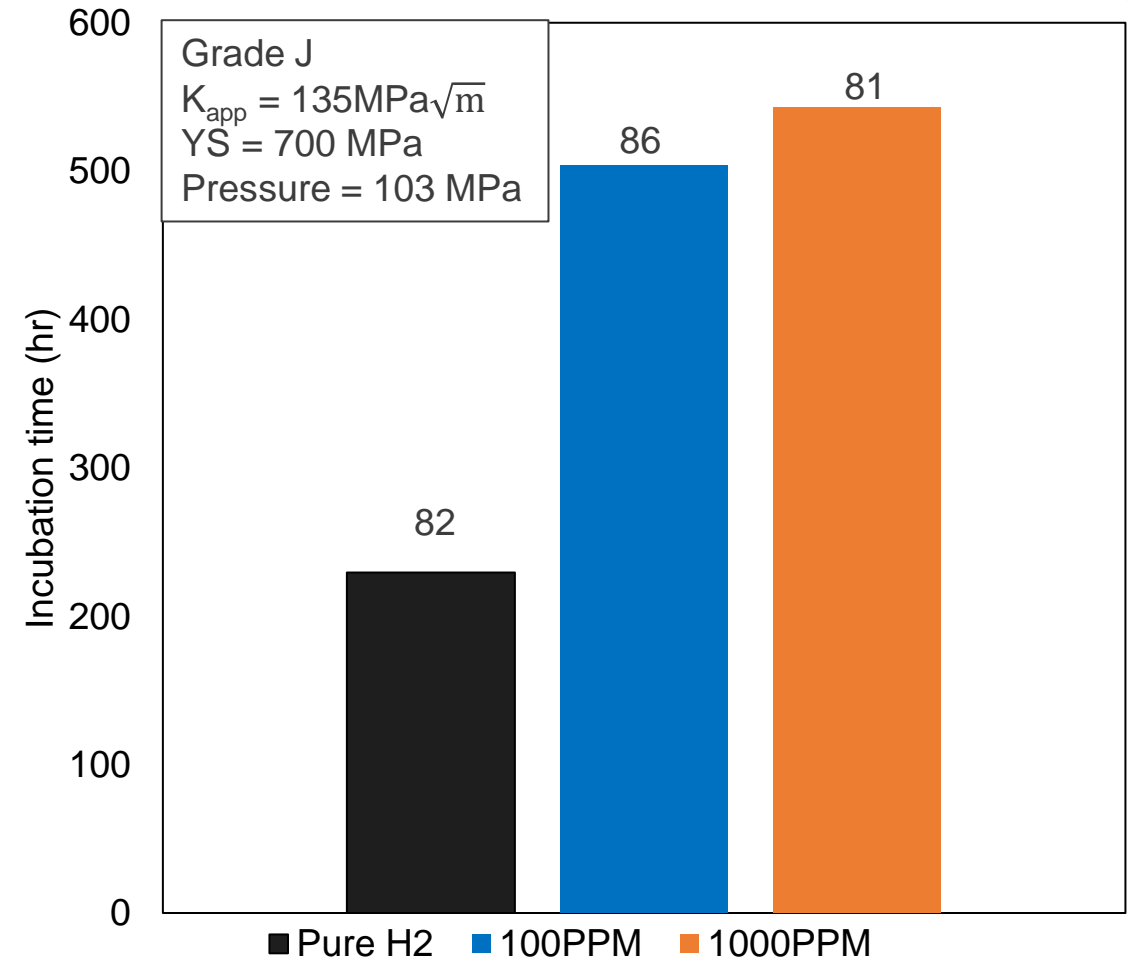
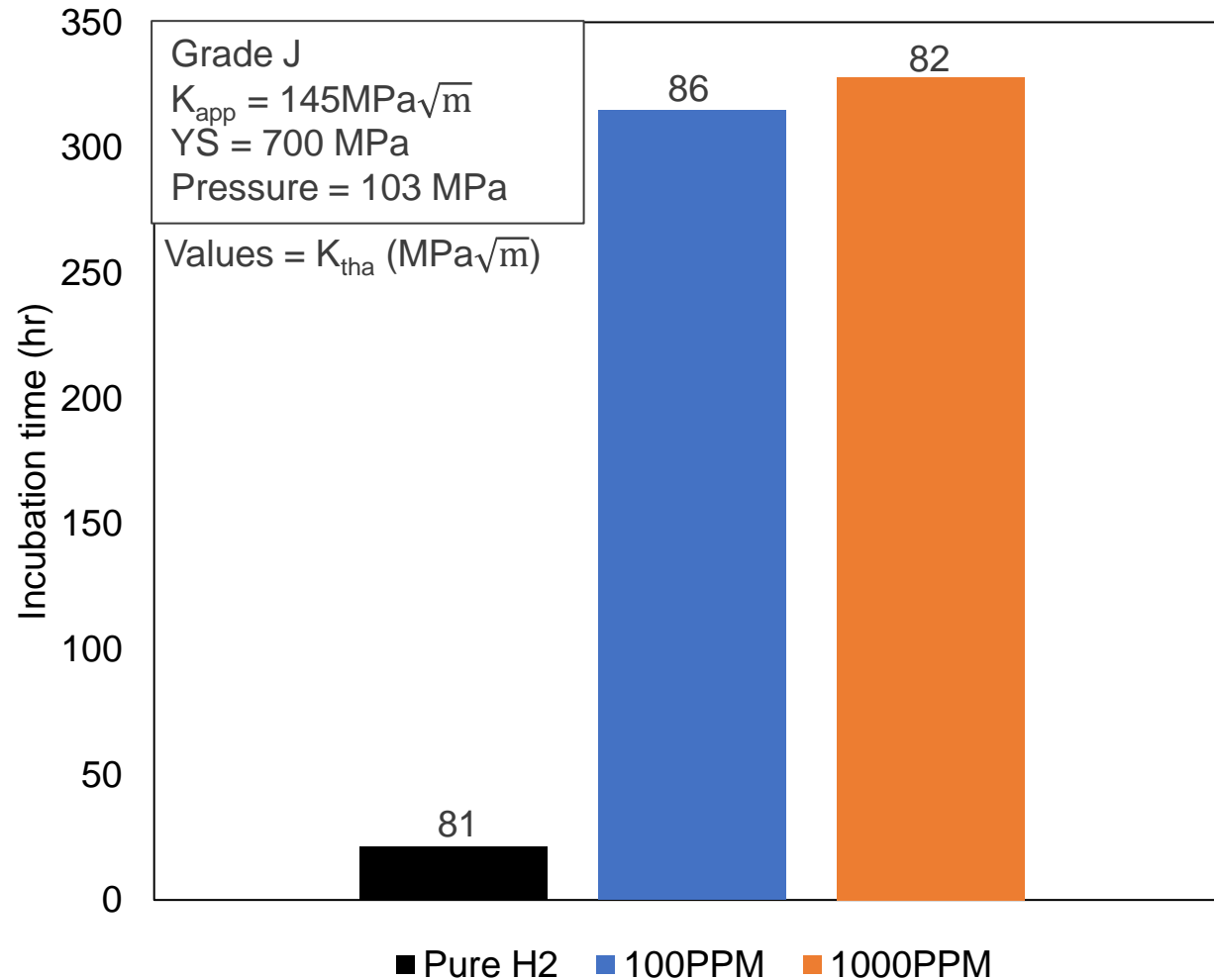
X100



13-8

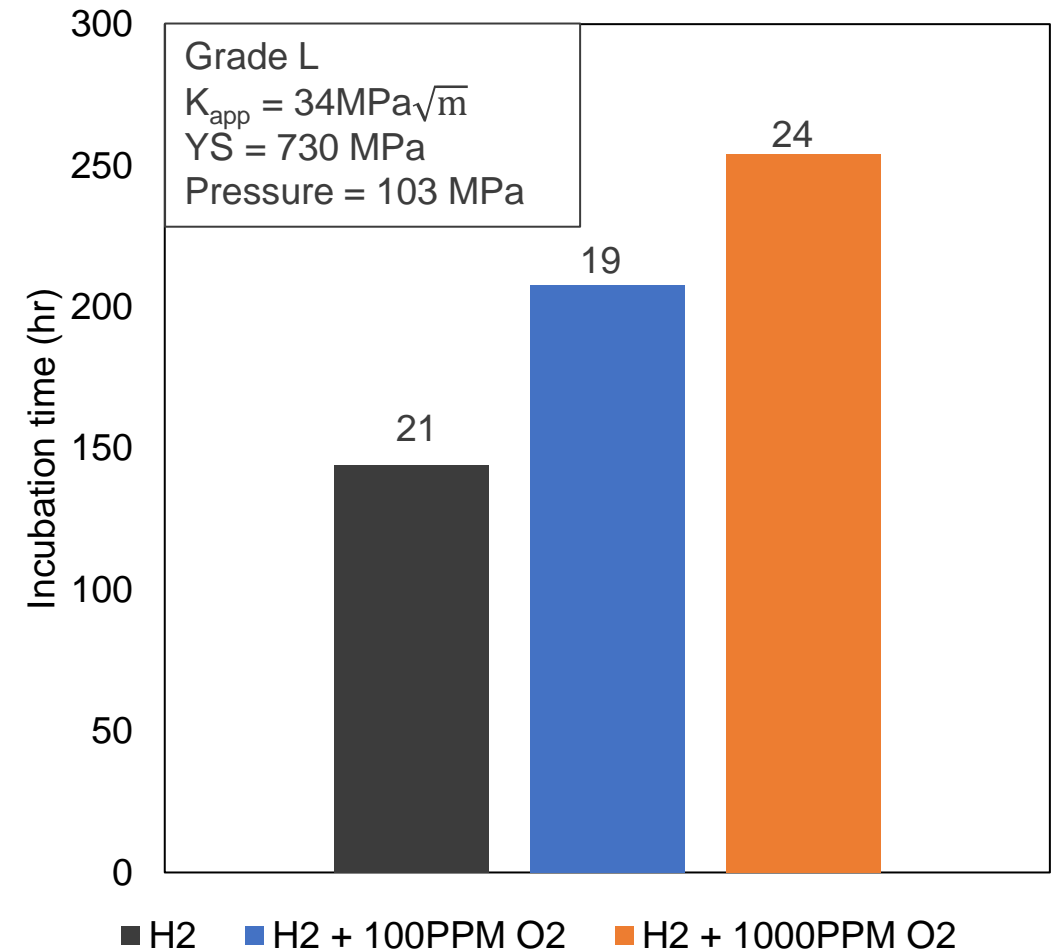
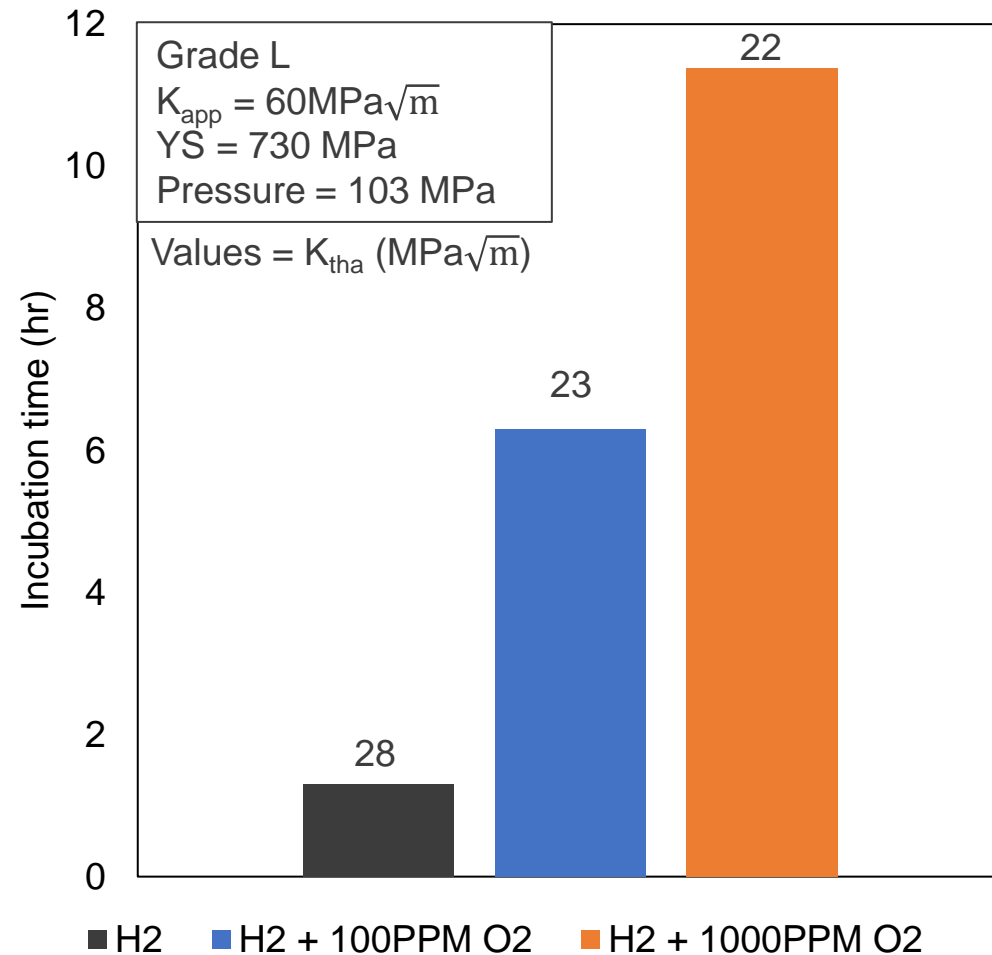


Grade J: 100PPM & 1000PPM O₂ delay incubation time



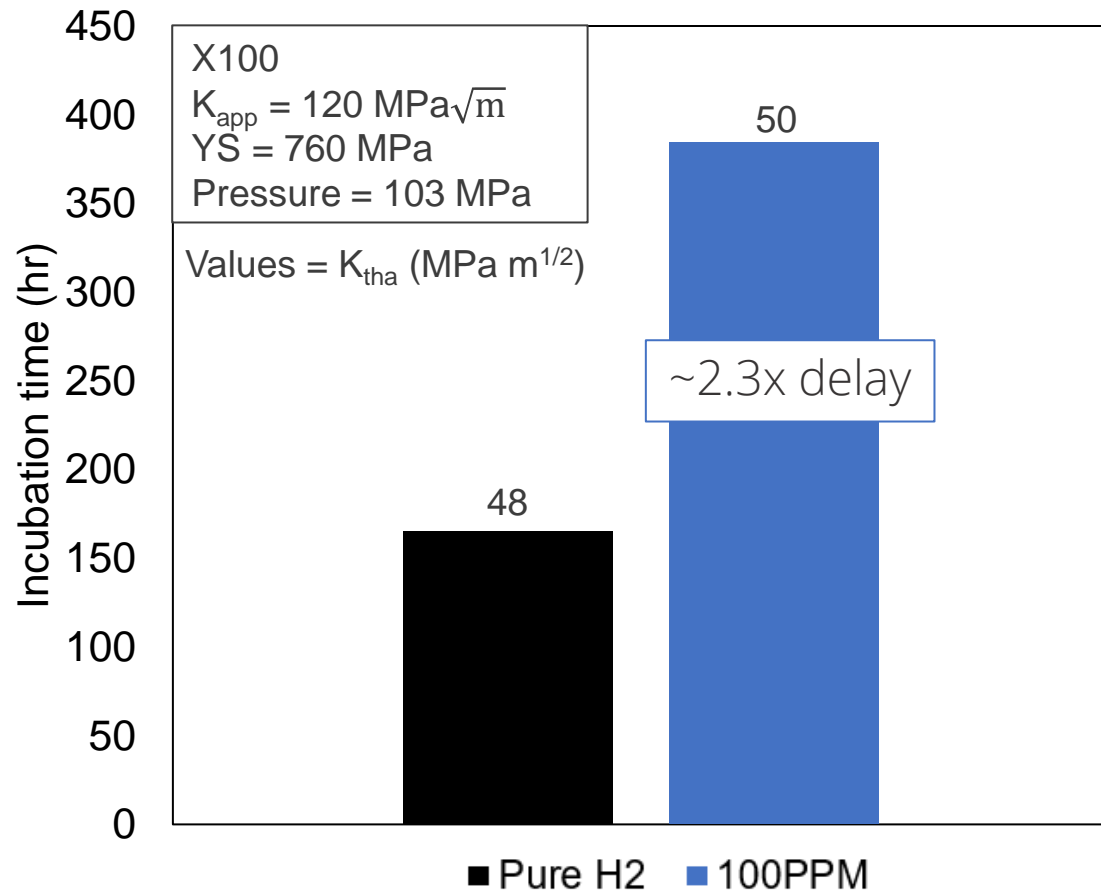
- The Grade J material showed delays of 15x at a higher preload ($K_{app} = 145 \text{ MPa}\sqrt{\text{m}}$) and a 2.2x increase at a lower preload ($K_{app} = 135 \text{ MPa}\sqrt{\text{m}}$)
- K thresholds were within $\pm 5 \text{ MPa}\sqrt{\text{m}}$ of average for both the pure and mixed gas conditions

Grade L: 100PPM & 1000PPM O₂ delay incubation time

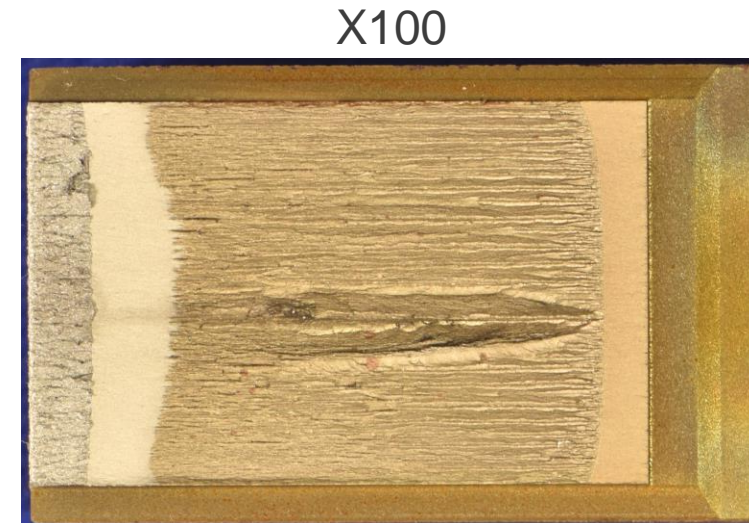


- Grade L had a 5x delay at higher preload ($K_{app} = 60 \text{ MPa}\sqrt{\text{m}}$) and a 1.5x delay at lower preload ($K_{app} = 34 \text{ MPa}\sqrt{\text{m}}$)
- Similar crack arrest thresholds for all test conditions

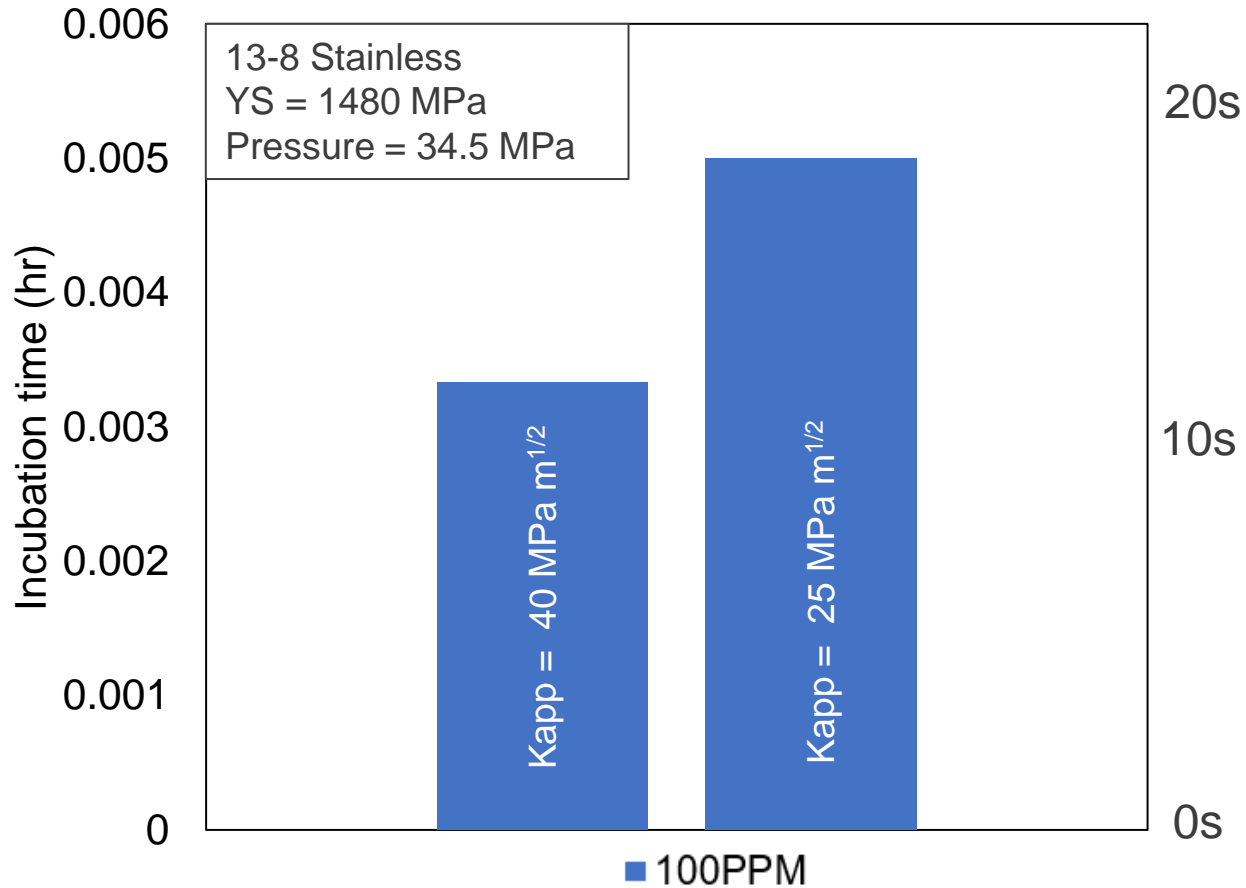
100PPM O₂ delays incubation time for X100, but 13-8 fractured immediately



- X100 also saw a significant delay with the addition of 100PPM O₂



100PPM O₂ delays incubation time for X100, but 13-8 fractured immediately

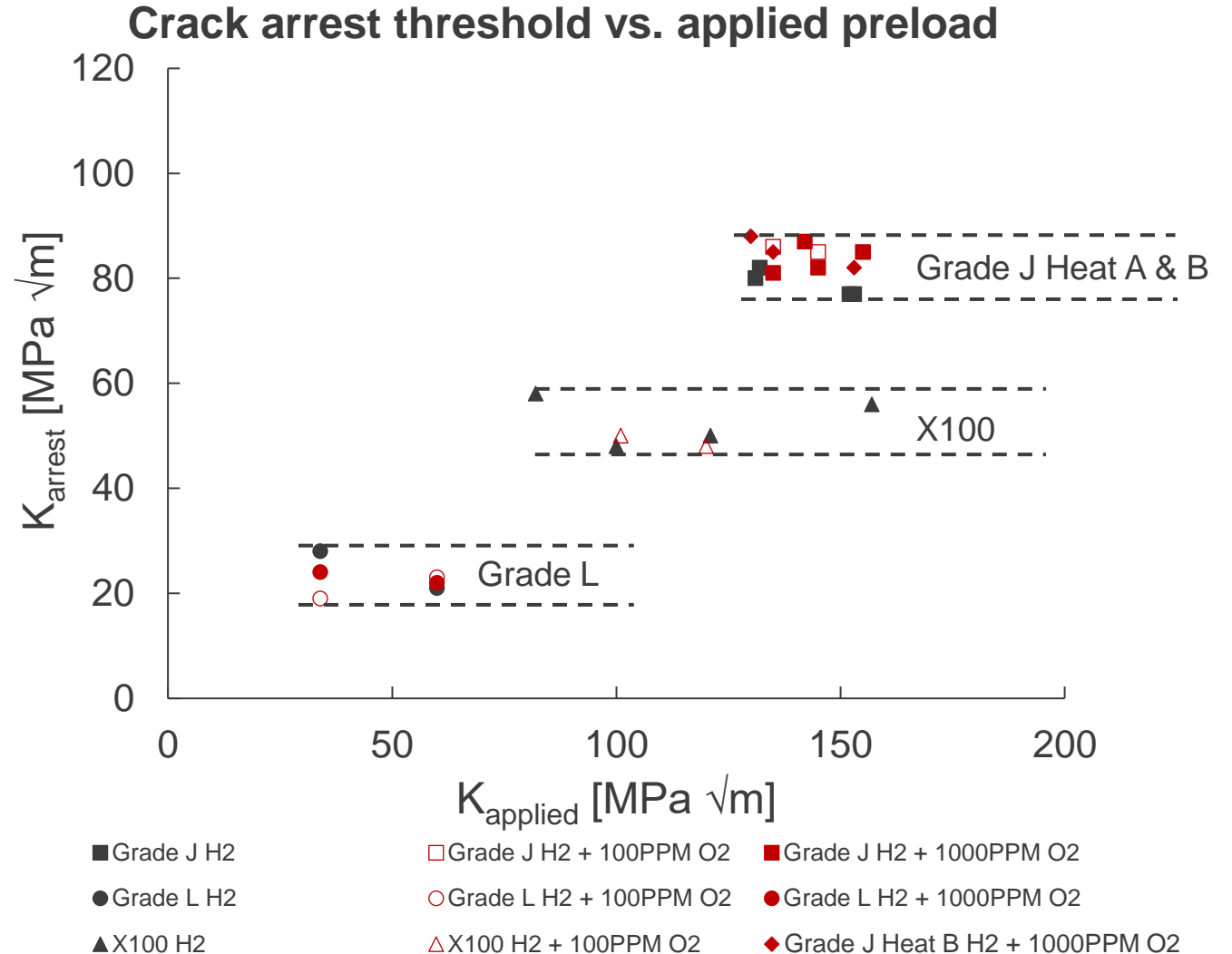


- Both 13-8 samples fractured ($a/W > 97\%$) within seconds of exposure to H₂ + 100PPM O₂
 - At reduced pressures (< 40 MPa)



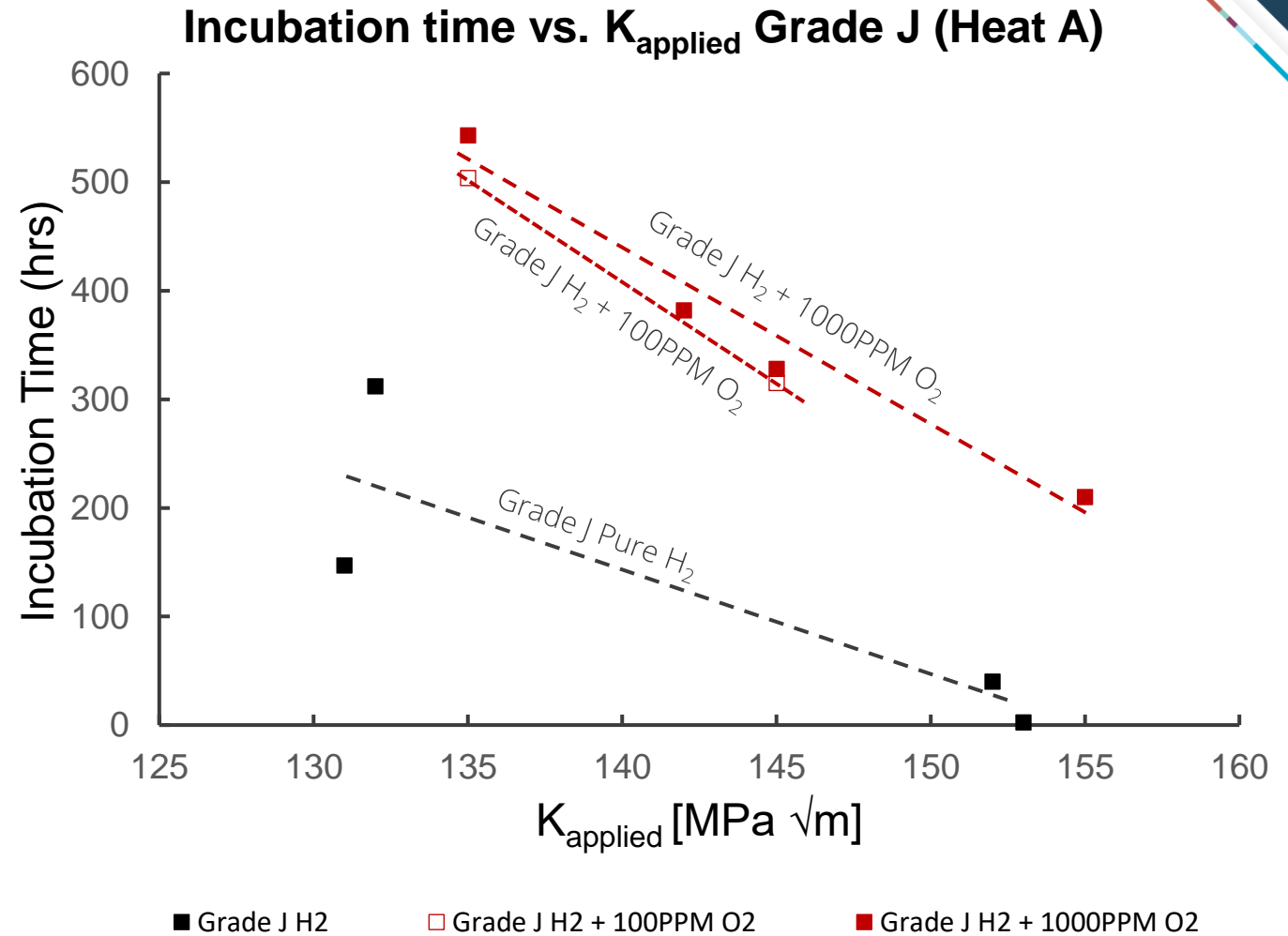
Summary and Conclusions

- Constant displacement fracture tests were carried out in pure hydrogen and mixed gas (100 and 1000PPM oxygen) environments at 103MPa (15ksi)
- K_{arrest} appears to be independent from oxygen content
 - All tests with pure hydrogen and oxygen impurities fall within an apx. $10\text{MPa}\sqrt{\text{m}}$ range



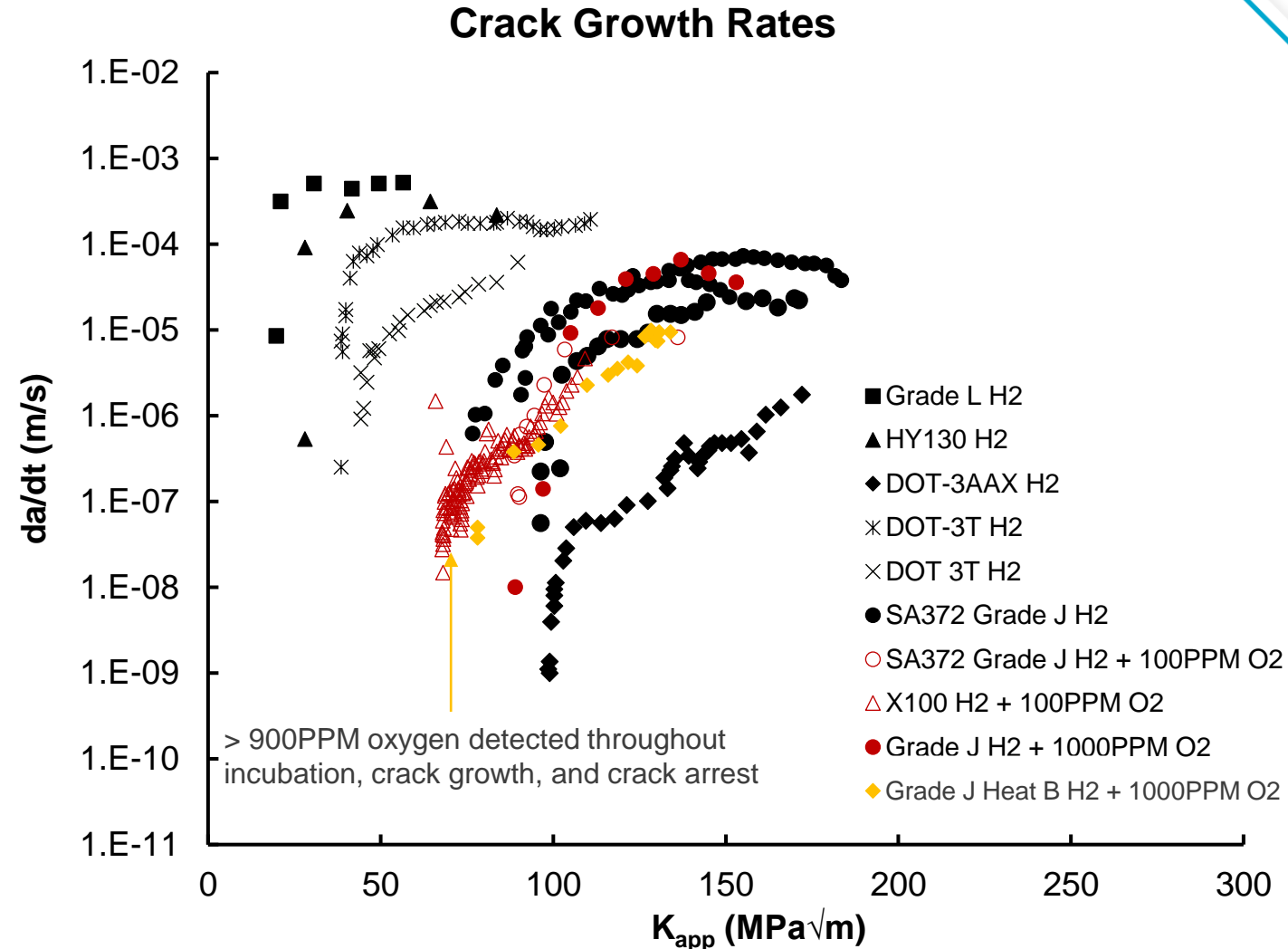
Summary and Conclusions

- Introducing 100PPM oxygen increased the incubation time by factors between 1.5x and 15x, but did not prevent crack propagation
- For the Grade L and Grade J, increasing the oxygen content from 100PPM to 1000PPM further delayed the incubation time, but had a smaller relative effect compared to the delay from pure hydrogen to hydrogen + 100PPM oxygen



Summary and Conclusions

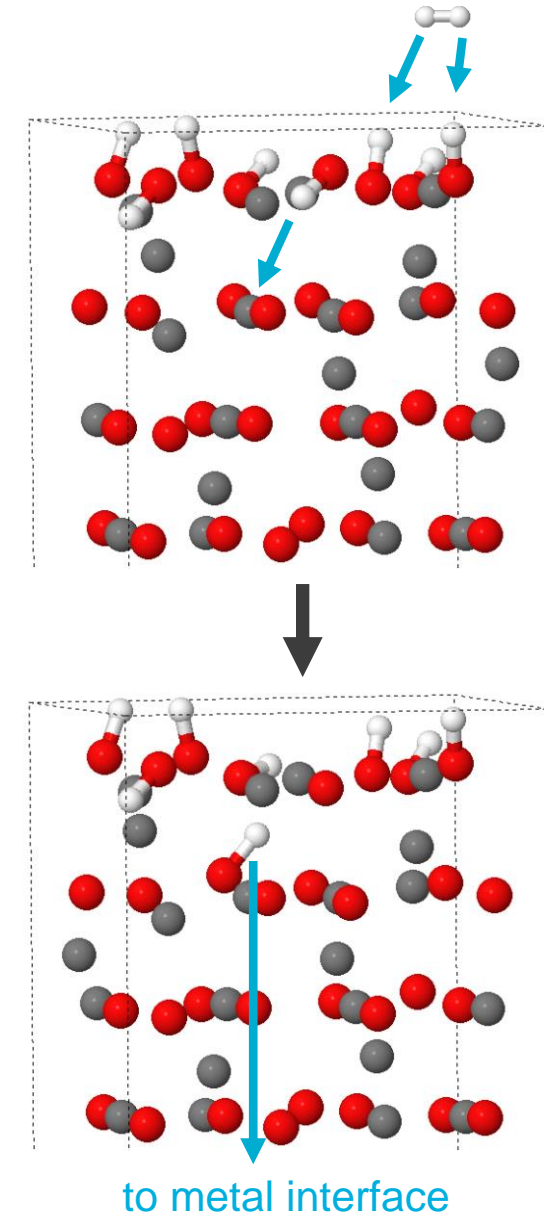
- Crack growth rates (da/dt) fall within the expected ranges from previous tests in pure hydrogen at similar pressures
- For many commonly used, laboratory testing rates, oxygen impurities can appear to mitigate hydrogen embrittlement
 - Oxygen impurities compete for surface sites with hydrogen, but only slow the uptake of hydrogen and delay the embrittlement (reduction of material properties)
- Based on this data, low oxygen impurities should not be relied upon for long-term mitigation of hydrogen embrittlement
 - Both the gas purity and testing rate are critical in order to determine representative and conservative material properties for the design of gaseous hydrogen infrastructure



Broader Research – Mechanisms

- Ongoing research is looking at determining the mechanisms behind the delay of hydrogen embrittlement in the presence of oxygen impurities
 - Surface experiments:
 - Oxides form rapidly on clean steel surfaces (XPS)
 - Hydroxyls form rapidly when oxide surfaces are exposed to hydrogen (XPS)
 - Modeling:
 - First principle calculations suggest hydrogen atoms can diffuse through oxides (DFT simulations, right)
- Experimental and computational observations consistently show oxides can impede but not prevent hydrogen-assisted fracture, especially on long time scales (> hours)

H atom diffusing into Fe_3O_4 from a hydroxylated surface



Thank you for your attention!

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