



Sandia
National
Laboratories

Exceptional service in the national interest

Effects of Oxygen Impurities on Long-Term Gaseous Hydrogen Embrittlement of Structural Steels

**Robert Wheeler¹, Chris San Marchi¹, Joseph
Ronevich¹, Norman Bartelt², Farid El Gabaly¹, Milan
Agnani^{1*}, Fernando Leon-Cazares¹**

¹Hydrogen and Materials Science Department, Sandia
National Laboratories Livermore, CA, USA

²Physics Department, Sandia National Laboratories
Livermore, CA, USA

*Formerly at SNL, currently at GTI Energy

Materials Science & Technology Conference October 2024

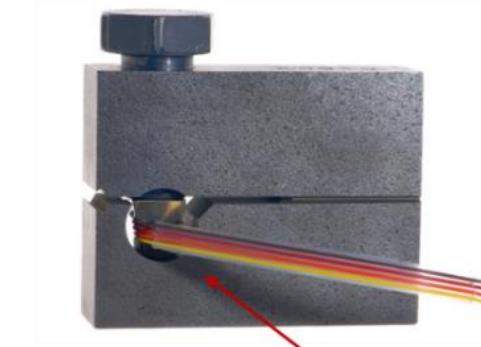
Sandia National Laboratories is a multimission laboratory managed and operated by National Technology and Engineering Solutions of Sandia LLC, a wholly owned subsidiary of Honeywell International Inc. for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525.



Overview

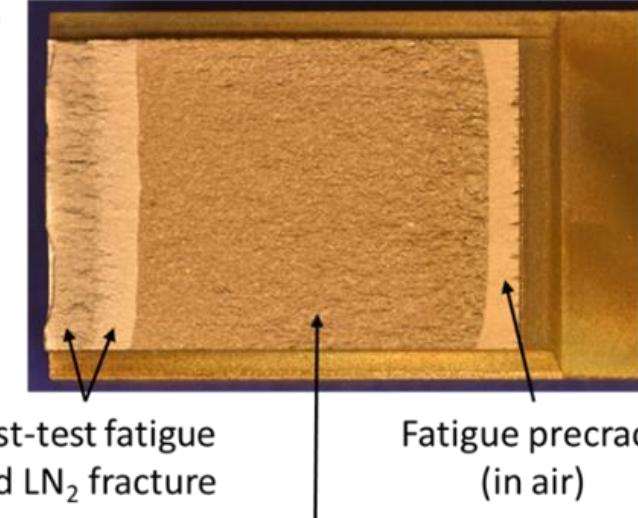
- Background and motivation
 - Examples of the mitigating effects of oxygen impurities on hydrogen embrittlement in laboratory testing
- Experimental methods
 - Long-term, constant displacement fracture tests in high pressure gaseous hydrogen environments
 - Commercial pressure vessel and pipeline steels
- Experimental results
 - Comparison of subcritical crack growth in high-pressure hydrogen and hydrogen with varying degrees of oxygen impurities
- Conclusions and future research

Wedge-opened Loaded (WOL) Sample



Reaction pin (load tup) with externally monitored strain gauge

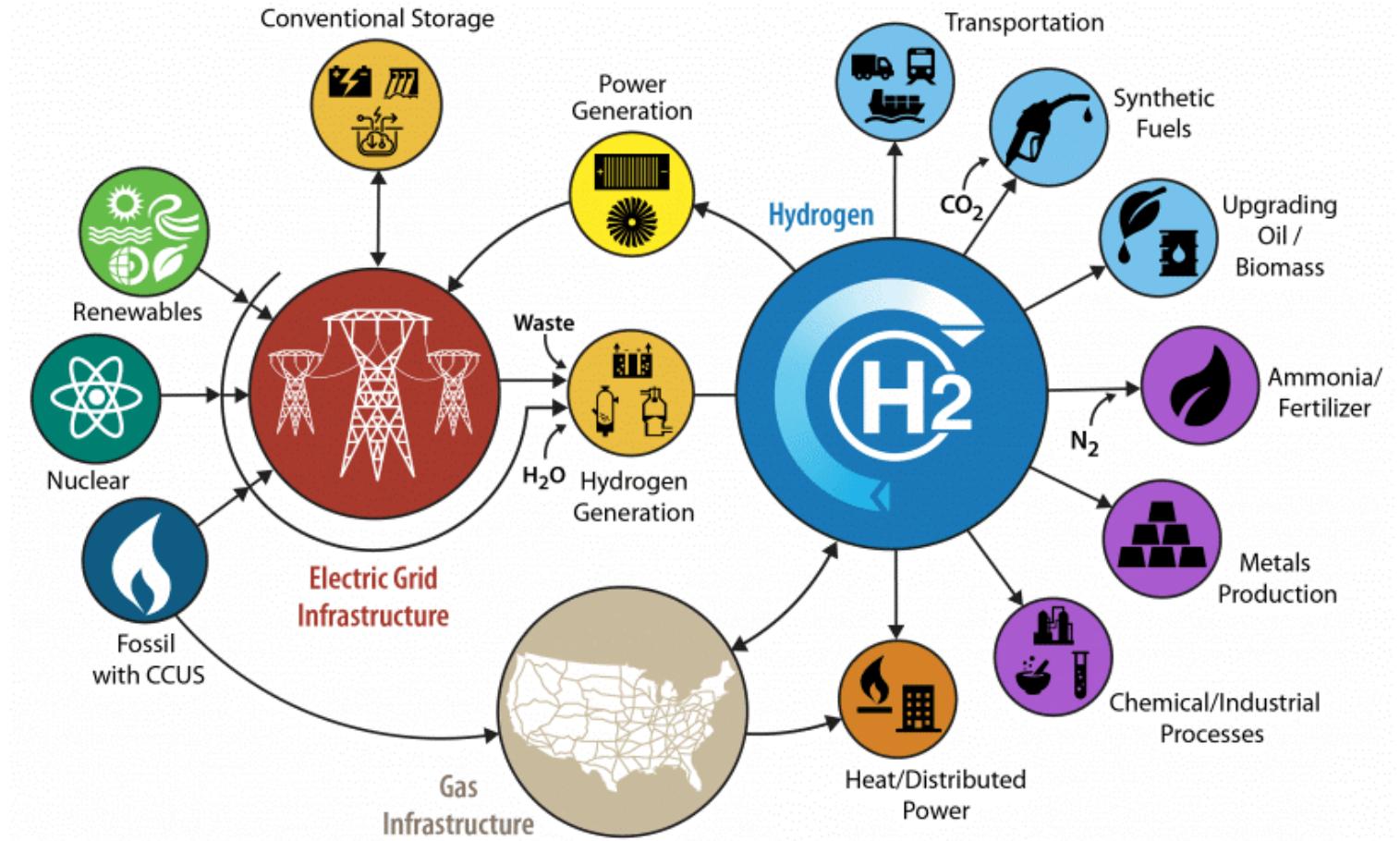
Grade L: WOL Fracture Surface



Crack growth in H₂ +
100PPM O₂

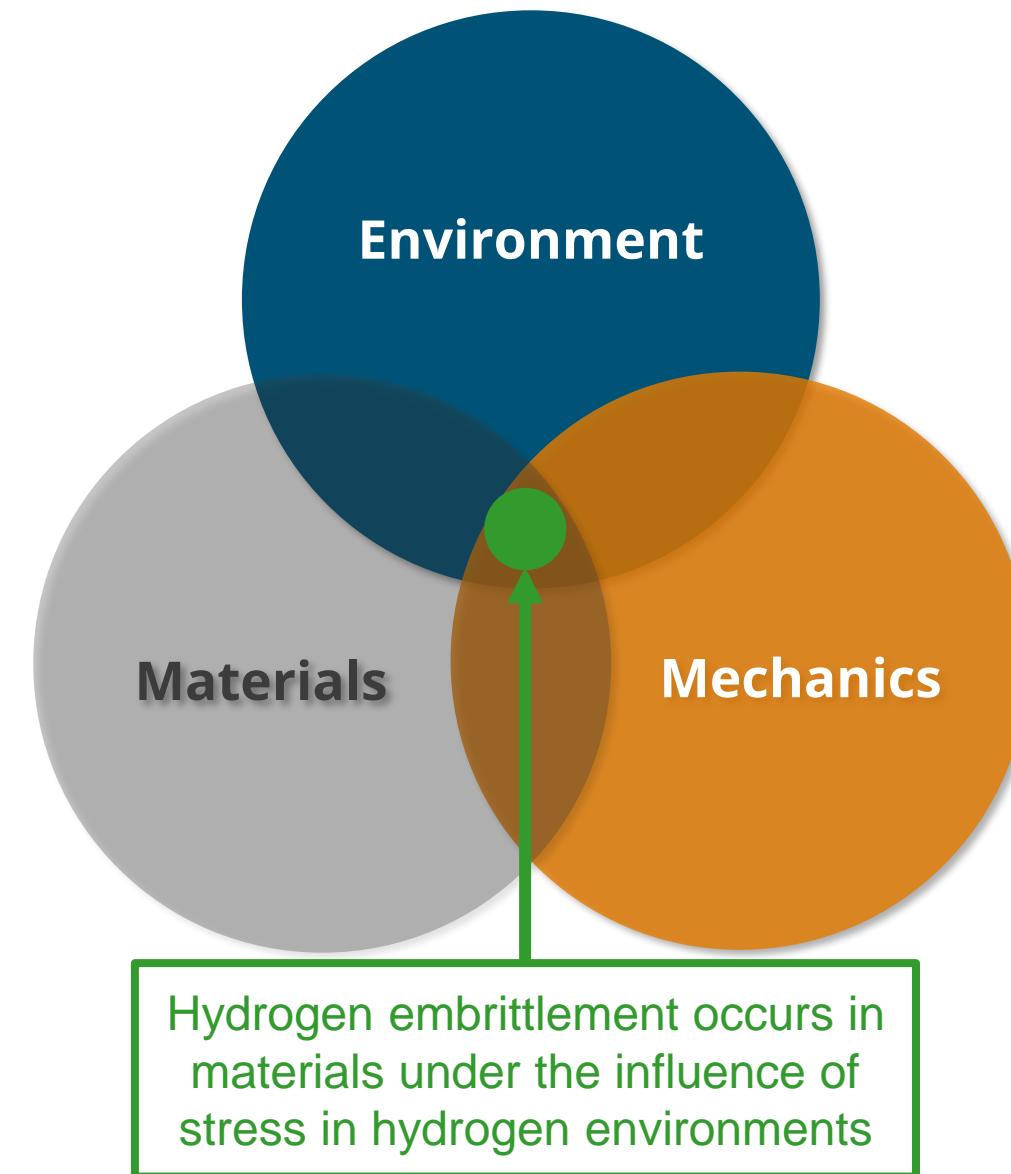
Hydrogen has a key role to play in a sustainable future

- Hydrogen has many potential avenues for decarbonization across many sectors
 - Energy storage, waste energy conversion
 - Transportation
 - Residential/industrial heating and appliances
 - Steel, cement production

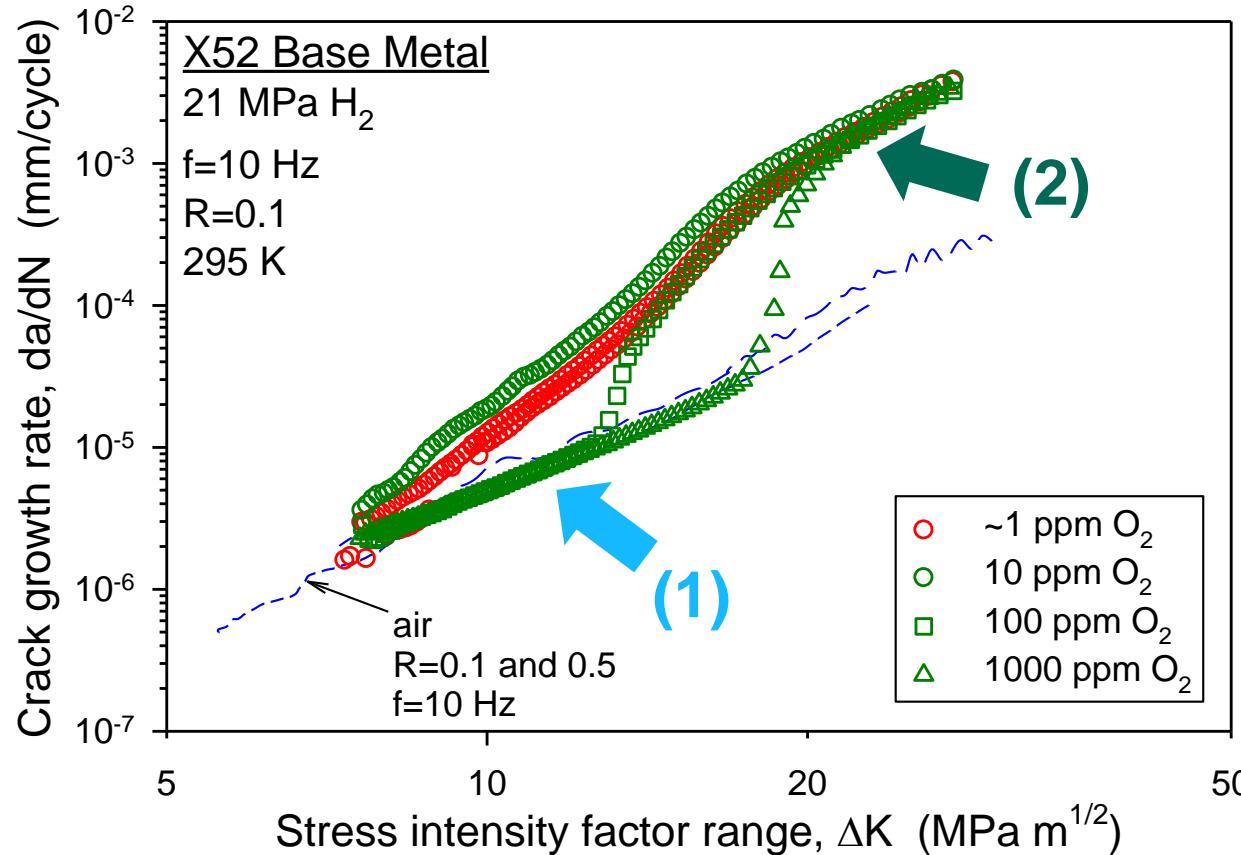


Hydrogen degrades fatigue and fracture resistance

- Hydrogen-assisted fracture and fatigue is influenced by:
 - Materials
 - Yield/tensile strength
 - Microstructure, homogeneity, etc.
 - Environment
 - Partial pressure of hydrogen
 - Impurities (e.g., O₂)
 - Temperature
 - Mechanics
 - Stress state
 - Stress (pressure) cycling
 - Residual stresses/work hardening



Oxygen is known to affect measurements of fatigue

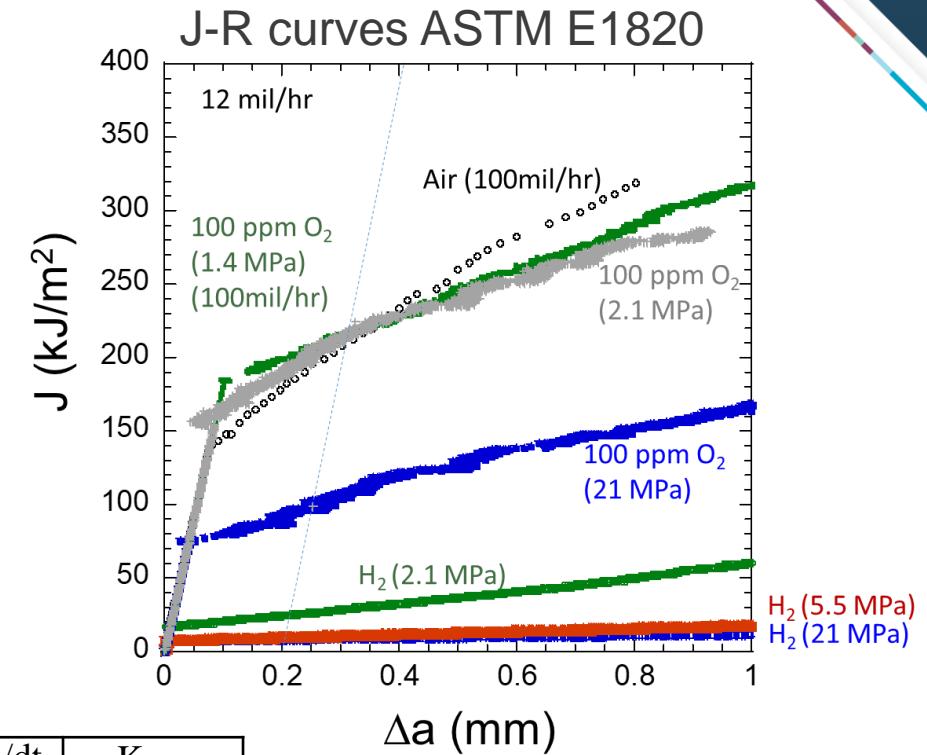


- Numerous examples of trace gases mitigating fatigue crack growth rate (FCGR) in laboratory conditions
- Example:
 - (1) Oxygen reduces FCGR comparable to air
 - (2) Oxygen has no effect on FCGR in H_2

Oxygen moderated hydrogen-assisted fracture



- Fracture toughness K_{JQH} values decreased by over 60% in pure H_2 at 2.1 MPa
- In 21 MPa mixed gas (100 ppm O_2), fracture toughness decreased by only 30% relative to air
 - In pure H_2 at 21 MPa, relative decrease was 80%
- At lower pressures (1.4-2.1 MPa) in mixed gas, no effect of hydrogen was measured

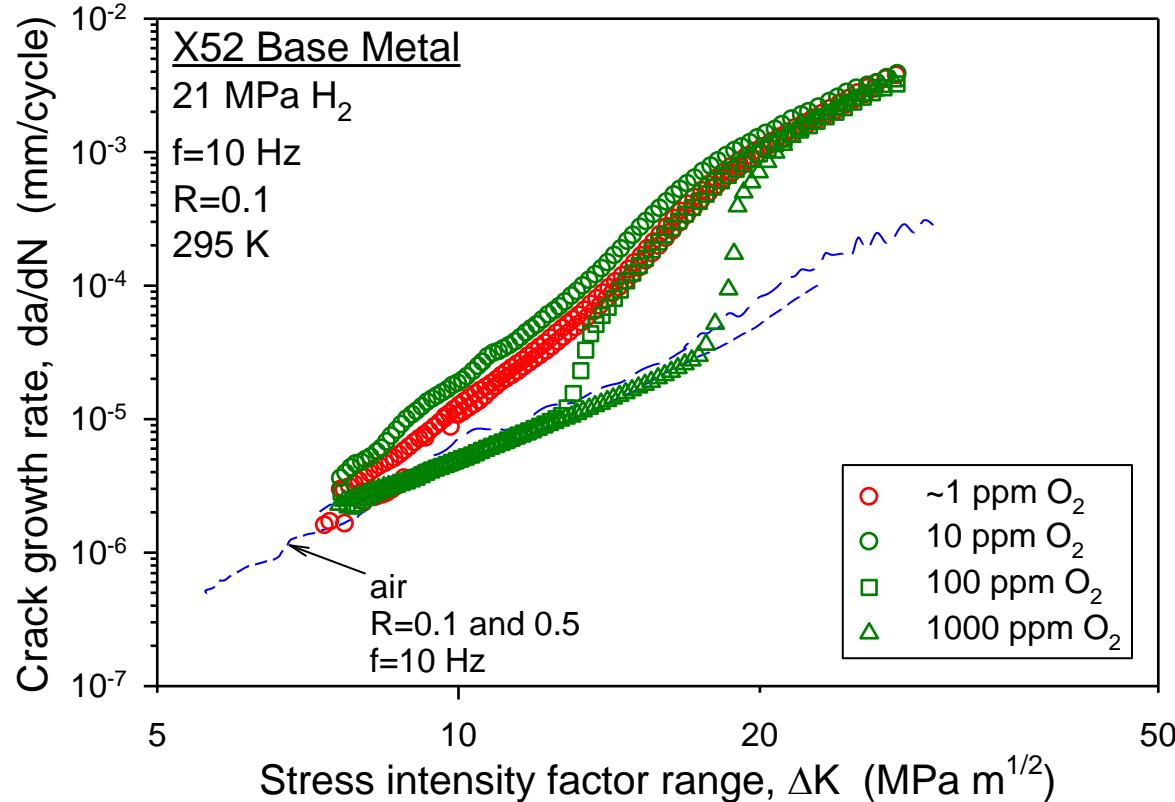


60 - 80% reduction

30% reduction

Sample ID	Environment	Test Pressure (MPa)	Actuator rate (mm/hr)	da/dt (m/s)	K_{JQH} (MPa m ^{1/2})
X100-51	Air	-	2.5	5.0E-7	217
X100-52	Air	-	2.5	1.4E-7	202
X100-5	H_2	21	0.3	8.5E-7	43
X100-6	H_2	5.5	0.3	3.6E-7	47
X100-7	H_2	2.1	0.3	1.7E-7	75
X100-53	$H_2 + 100$ ppm O_2	21	0.3	1.1E-7	151
X100-55	$H_2 + 100$ ppm O_2	2.1	0.3	7.4E-8	222
X100-56	$H_2 + 100$ ppm O_2	1.4	2.5	1.0E-7	222

Oxygen has been shown to mitigate hydrogen embrittlement in laboratory tests



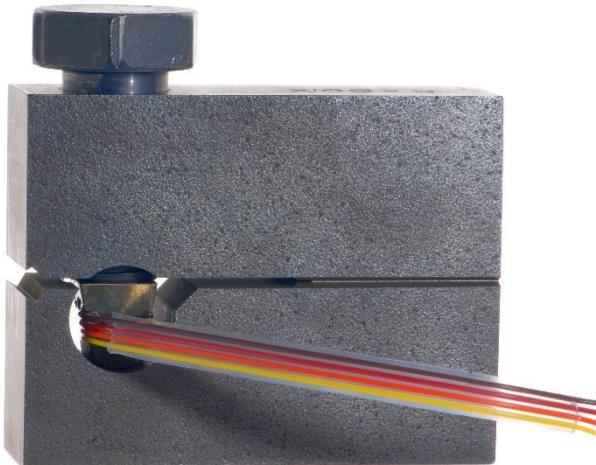
- Fatigue and fracture measurements can be significantly impacted by oxygen impurities
- Fatigue crack growth tests are typically performed at 1 Hz (\pm decade)
 - $da/dN = 10^{-5}$ mm/cycle
 - Time for $\Delta a = 1\text{mm}$: ~ 1 day
 - 1 day = 0.02% of 10 year life
- Are the time scales of a typical laboratory fatigue test sufficient to demonstrate kinetics over decades?
 - More accurately simulate the mechanical/environmental conditions that components see when in use
 - Does trace oxygen have long term mitigation effects on hydrogen embrittlement?

Sustained load testing can be executed over periods of days to weeks to months to years

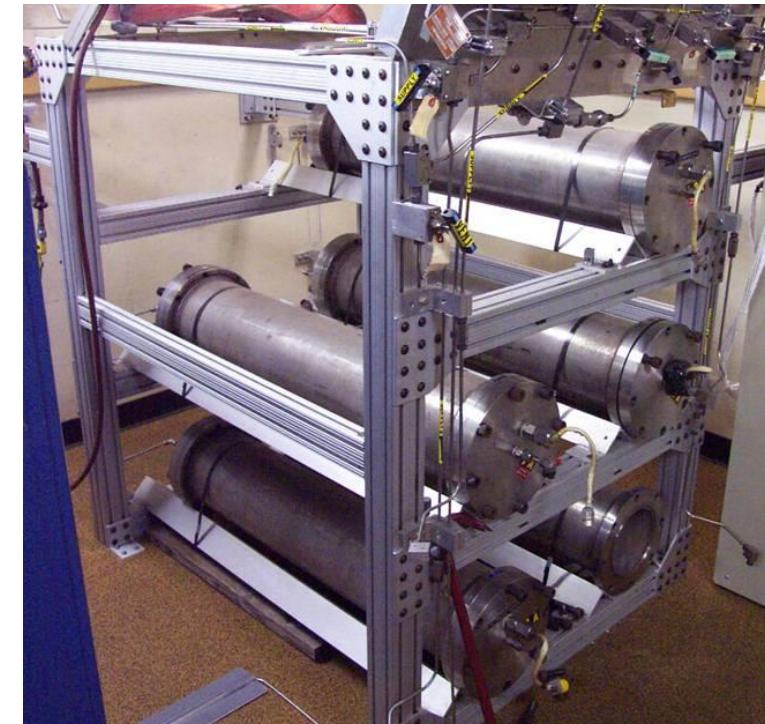


- Fixed (constant) displacement fracture tests
- Fatigue pre-cracked and loaded in ambient air
- Placed in pressure vessels & pressurized up to 140 MPa gaseous environment
 - Experiments in this study were performed at 103 MPa
- Instrumented reaction pins allow for the determination of incubation time
- Directly compare subcritical crack growth in hydrogen and mixed gas environments

Wedge-opened loaded (WOL) test sample



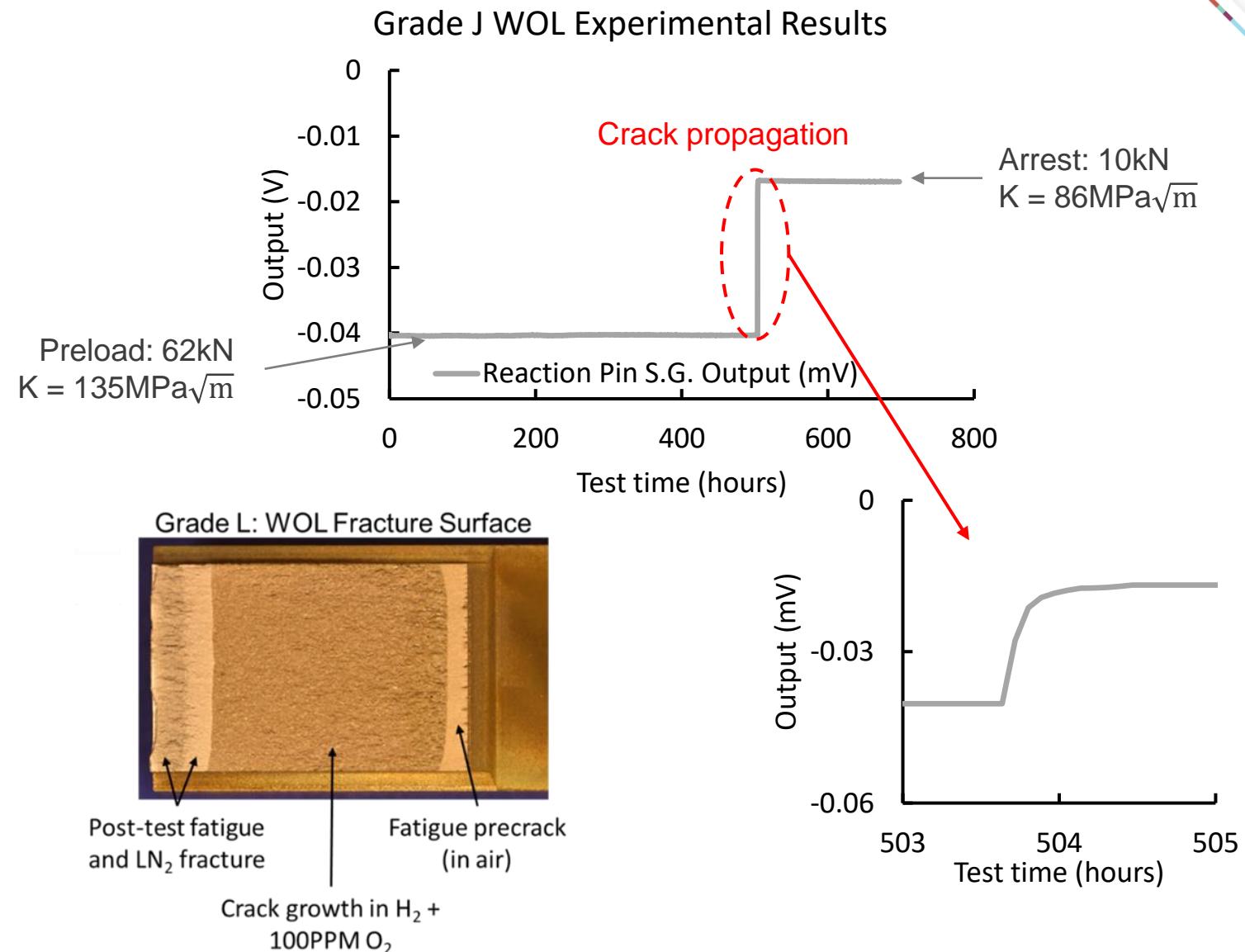
Pressure vessels for medium and long term experiments



ASTM E1681 – Threshold Stress Intensity Factor for Environment-Assisted Cracking

Crack initiation and growth rates were measured during constant displacement fracture experiments

- Instrumented reaction pins allow for determination of incubation time and crack growth rates
 - Continuous data collection throughout the duration of the experiments
- Time between the initial crack propagation and arrest can range between seconds to hours
 - With a constant displacement, the crack growth rates can be determined from the load on the reaction pin
- Post-test fatigue and heat tinting are used to mark fracture surfaces



Material selection and fracture surfaces

- SA372 Grade J steel
 - Heat A: $YS = 700 \text{ MPa}$
 - Heat B: $YS = 750 \text{ MPa}$
- SA372 Grade L steel
 - $YS = 730 \text{ MPa}$
- X100 pipeline steel
 - $YS = 760 \text{ MPa}$
- Precipitation Hardened 13-8 stainless steel
 - $YS = 1480 \text{ MPa}$

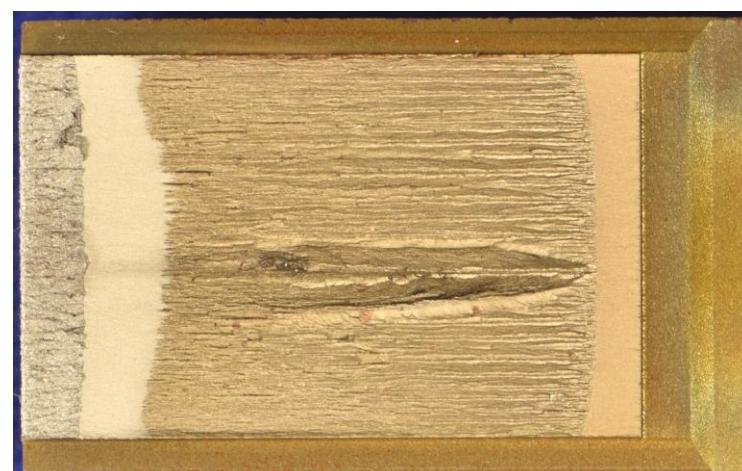
Grade L



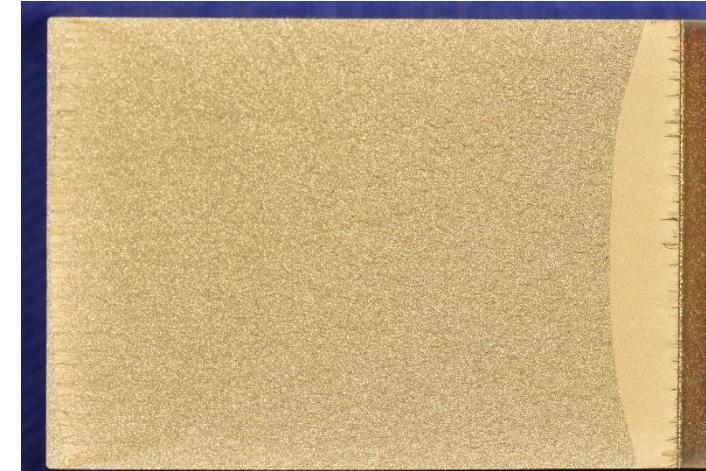
Grade J



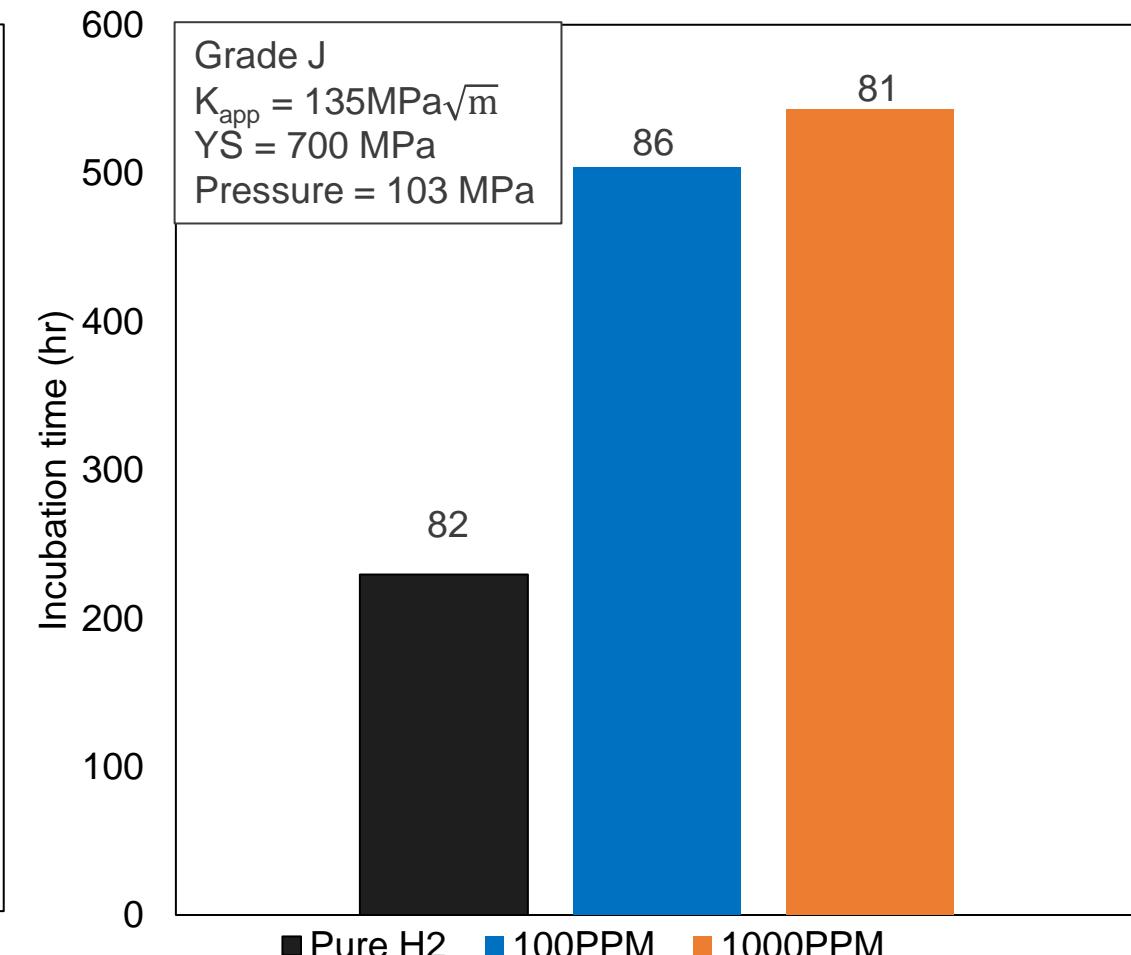
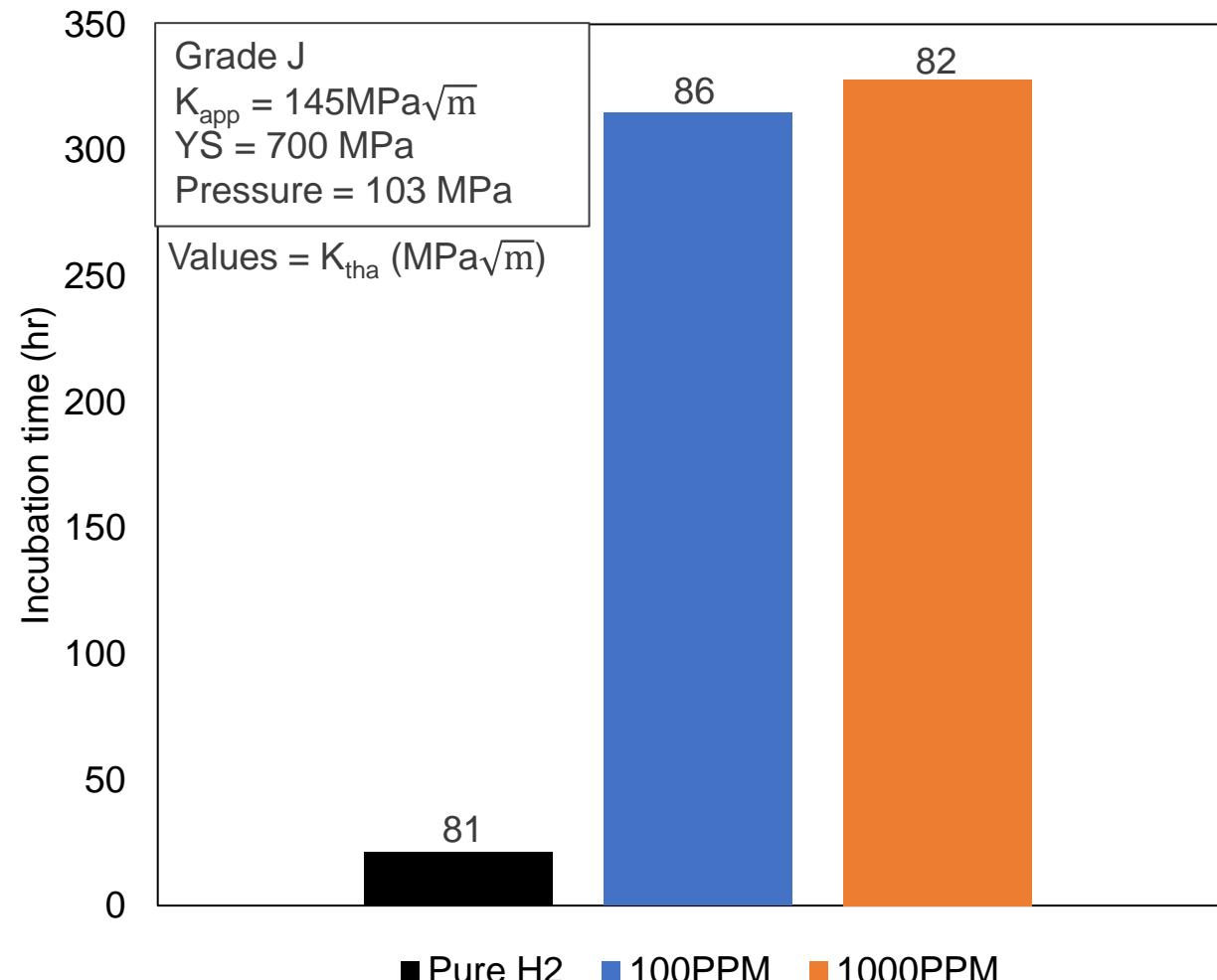
X100



13-8

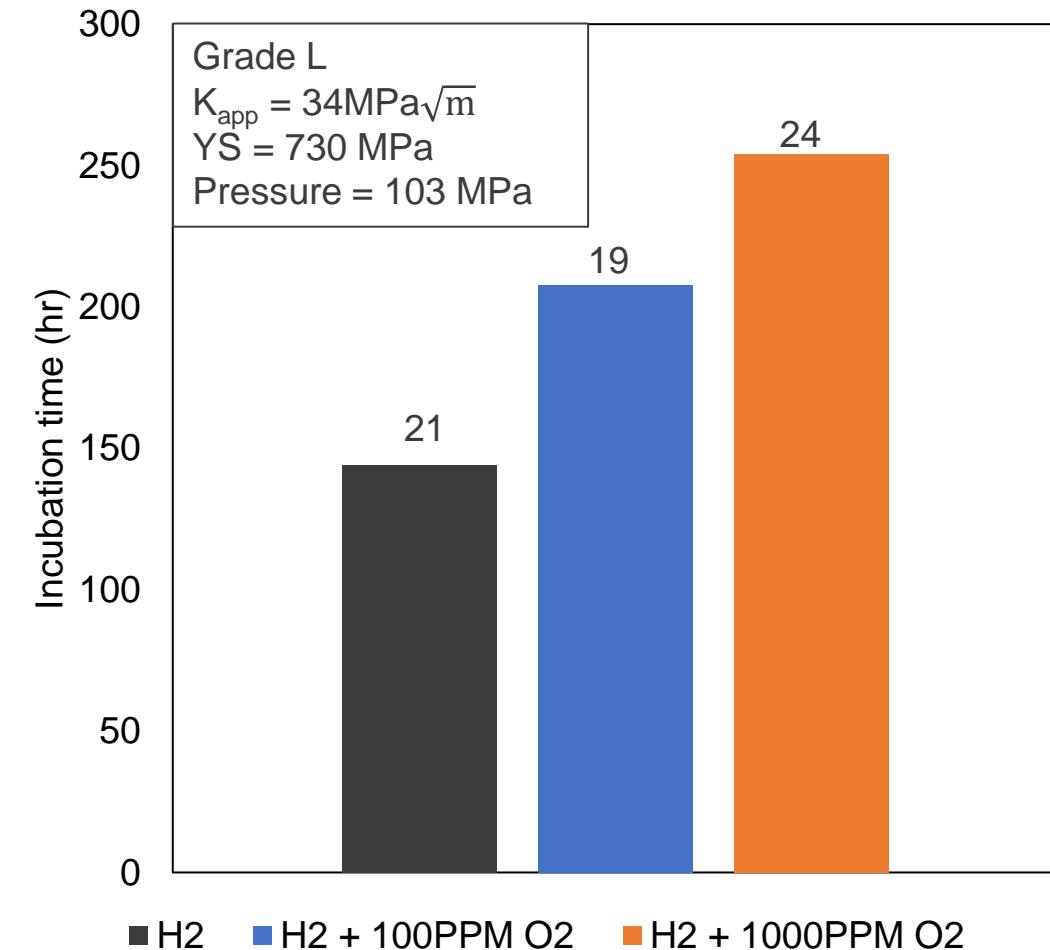
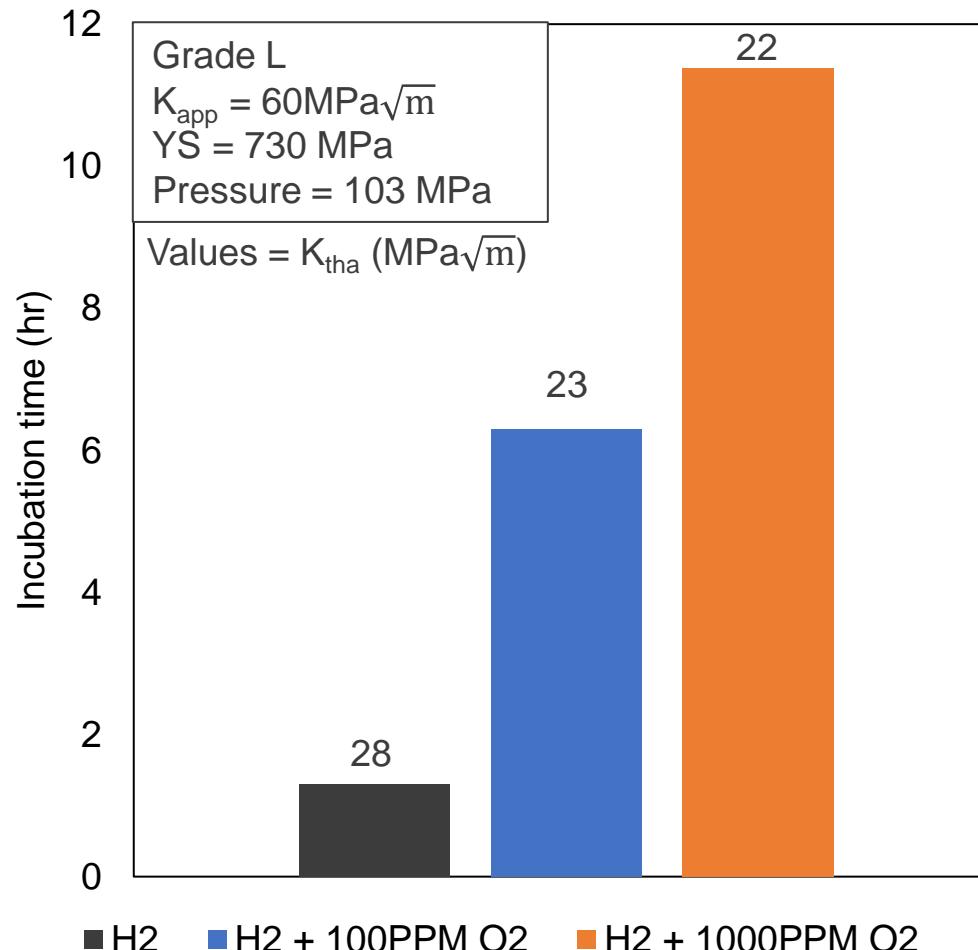


Grade J: 100PPM & 1000PPM O₂ delay incubation time



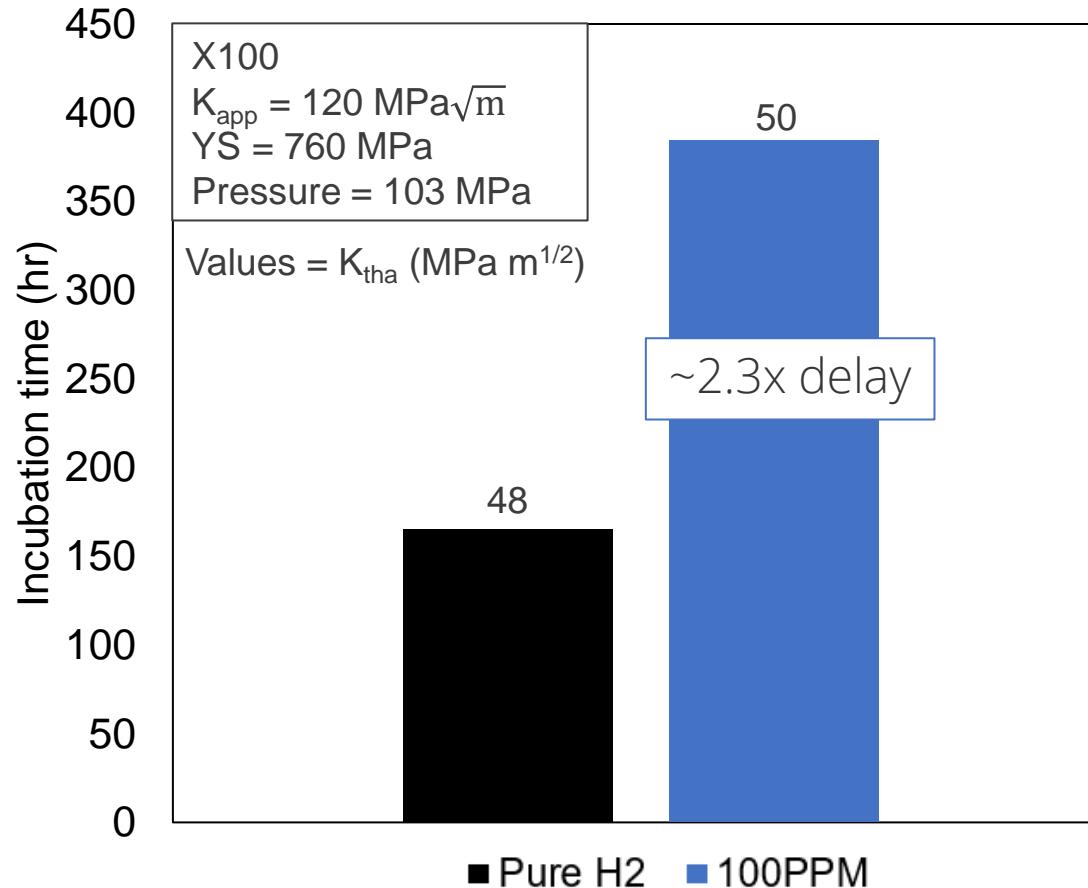
- The Grade J material showed delays of 15x at a higher preload ($K_{app} = 145 \text{ MPa}\sqrt{\text{m}}$) and a 2.2x increase at a lower preload ($K_{app} = 135 \text{ MPa}\sqrt{\text{m}}$)
- K thresholds were within $\pm 5 \text{ MPa}\sqrt{\text{m}}$ of average for both the pure and mixed gas conditions

Grade L: 100PPM & 1000PPM O₂ delay incubation time

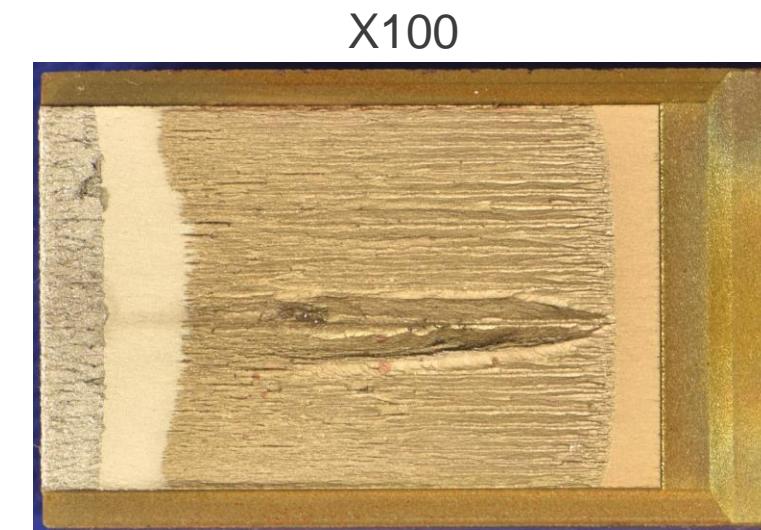


- Grade L had a 5x delay at higher preload ($K_{app} = 60 \text{ MPa}\sqrt{\text{m}}$) and a 1.5x delay at lower preload ($K_{app} = 34 \text{ MPa}\sqrt{\text{m}}$)
- Similar crack arrest thresholds for all test conditions

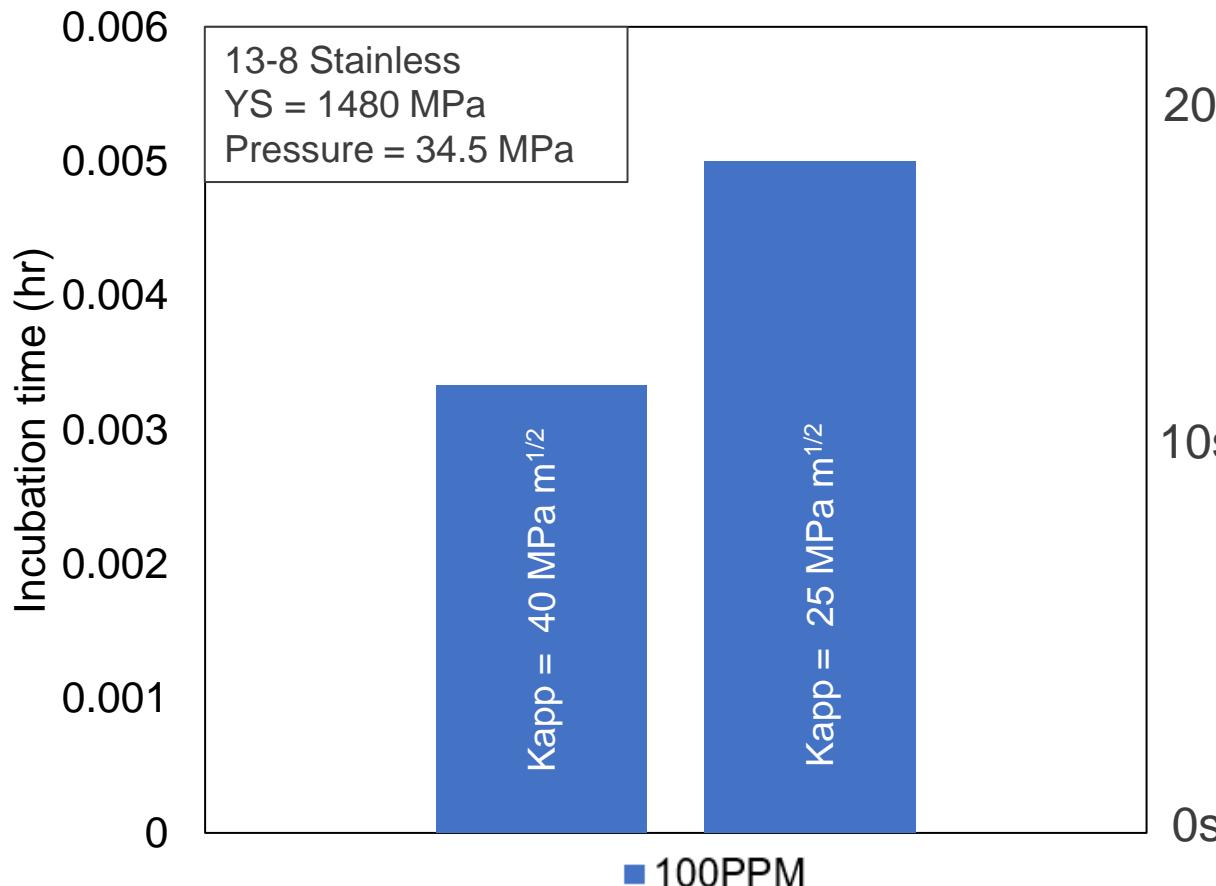
100PPM O₂ delays incubation time for X100, but 13-8 fractured immediately



- X100 also saw a significant delay with the addition of 100PPM O₂



100PPM O₂ delays incubation time for X100, but 13-8 fractured immediately

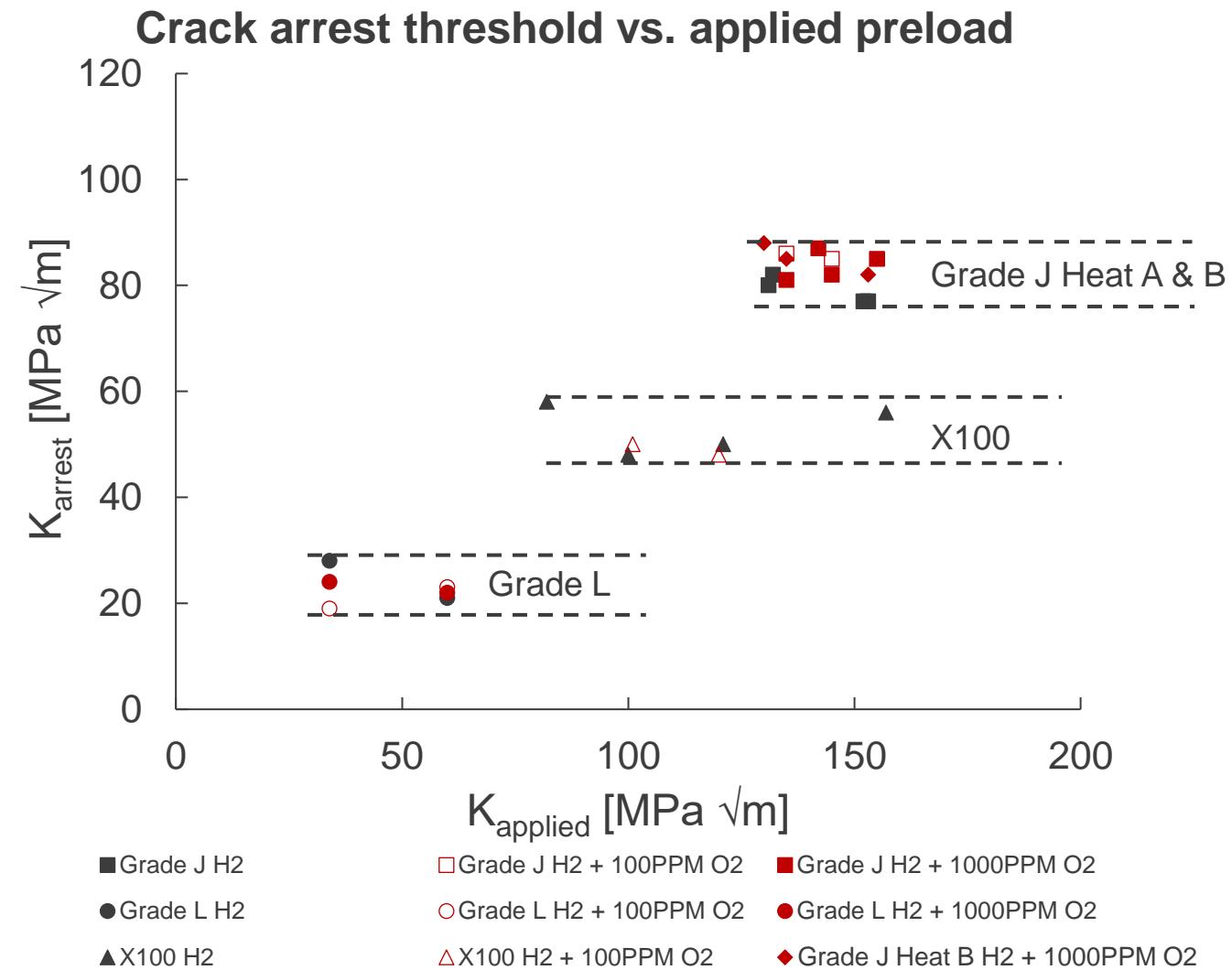


- Both 13-8 samples fractured ($a/W > 97\%$) within seconds of exposure to H₂ + 100PPM O₂
 - At reduced pressures (< 40 MPa)



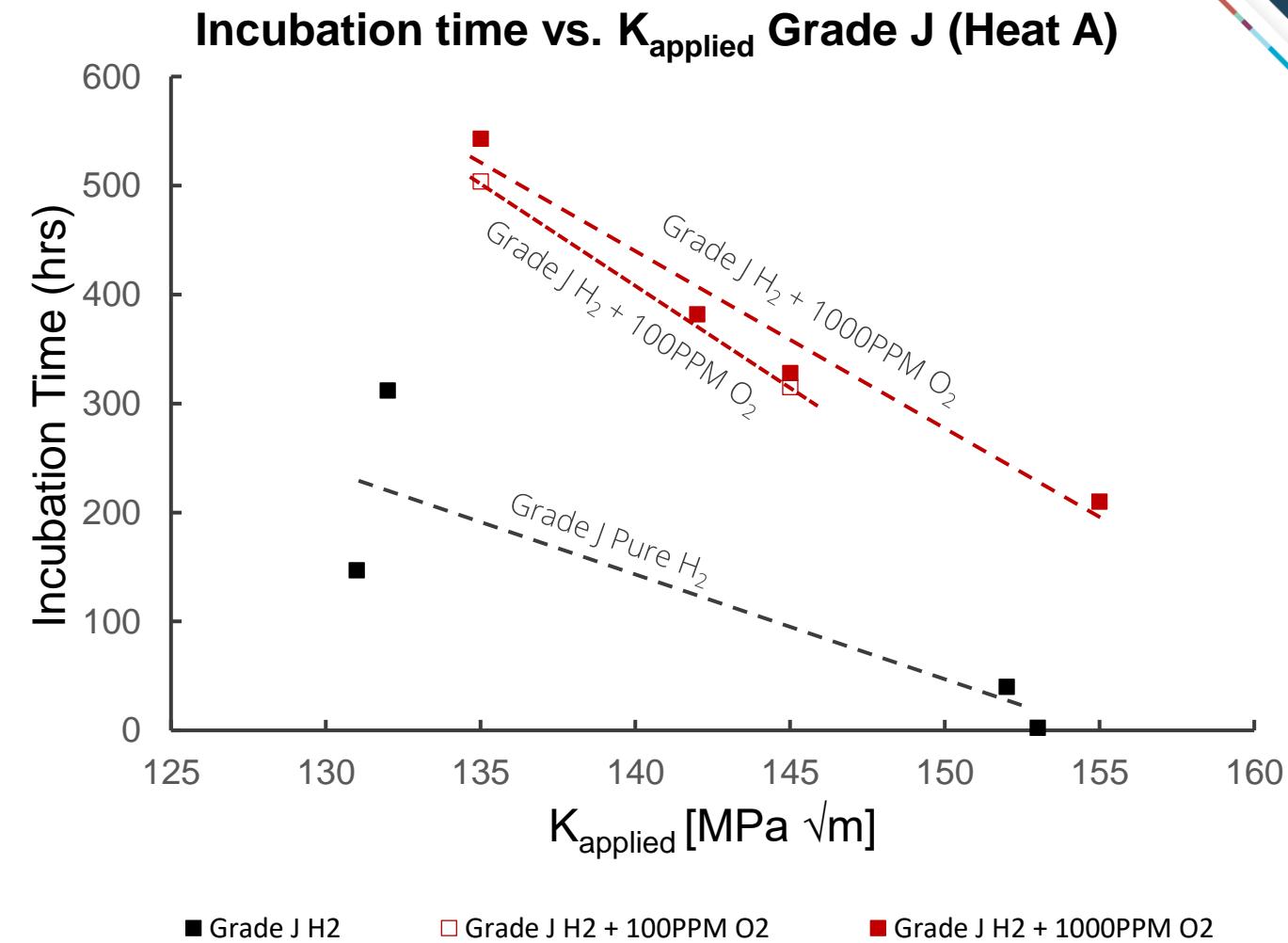
Summary and Conclusions

- Constant displacement fracture tests were carried out in pure hydrogen and mixed gas (100 and 1000PPM oxygen) environments at 103MPa (15ksi)
- K_{arrest} appears to be independent from oxygen content
 - All tests with pure hydrogen and oxygen impurities fall within an apx. $10 \text{ MPa} \sqrt{\text{m}}$ range



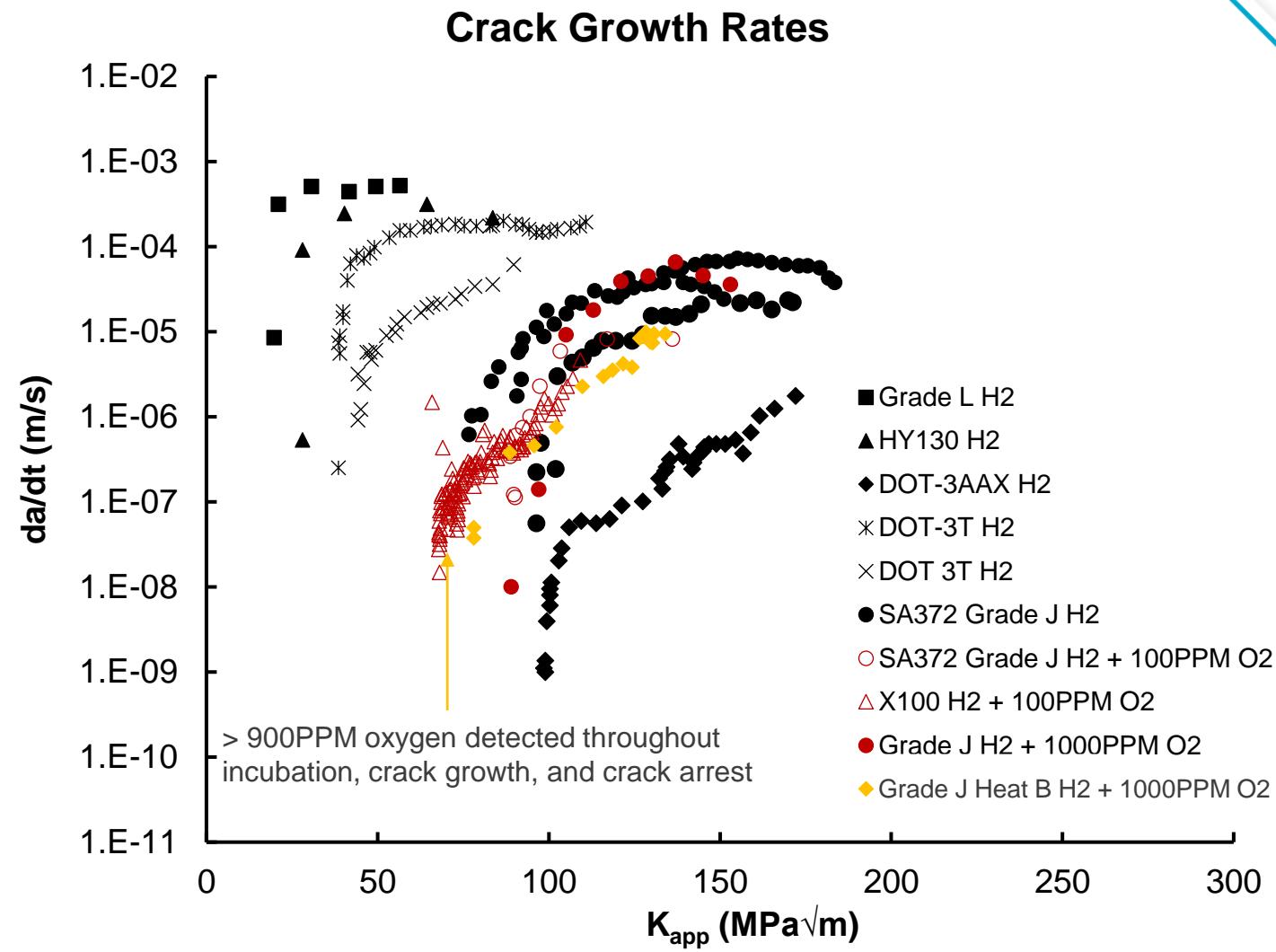
Summary and Conclusions

- Introducing 100PPM oxygen increased the incubation time by factors between 1.5x and 15x, but did not prevent crack propagation
- For the Grade L and Grade J, increasing the oxygen content from 100PPM to 1000PPM further delayed the incubation time, but had a smaller relative effect compared to the delay from pure hydrogen to hydrogen + 100PPM oxygen



Summary and Conclusions

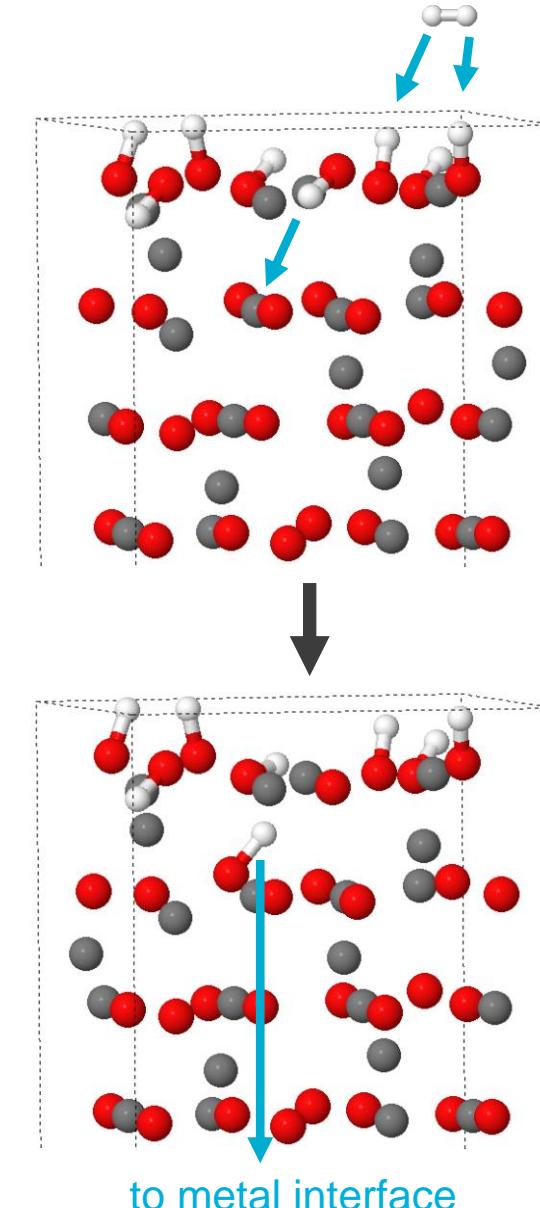
- Crack growth rates (da/dt) fall within the expected ranges from previous tests in pure hydrogen at similar pressures
- For many commonly used, laboratory testing rates, oxygen impurities can appear to mitigate hydrogen embrittlement
 - Oxygen impurities compete for surface sites with hydrogen, but only slow the uptake of hydrogen and delay the embrittlement (reduction of material properties)
- Based on this data, low oxygen impurities should not be relied upon for long-term mitigation of hydrogen embrittlement
 - Both the gas purity and testing rate are critical in order to determine representative and conservative material properties for the design of gaseous hydrogen infrastructure



Broader Research – Mechanisms

- Ongoing research is looking at determining the mechanisms behind the delay of hydrogen embrittlement in the presence of oxygen impurities
- Surface experiments:
 - Oxides form rapidly on clean steel surfaces (XPS)
 - Hydroxyls form rapidly when oxide surfaces are exposed to hydrogen (XPS)
- Modeling:
 - First principle calculations suggest hydrogen atoms can diffuse through oxides (DFT simulations, right)
- Experimental and computational observations consistently show oxides can impede but not prevent hydrogen-assisted fracture, especially on long time scales (> hours)

H atom diffusing into Fe_3O_4 from a hydroxylated surface



to metal interface

Thank you for your attention!

- Rob Wheeler - rwheel@sandia.gov
- Chris San Marchi
- Joe Ronevich
- Norman Bartelt
- Farid El Gabaly
- Milan Agnani
- Fernando Leon-Cazares

- We would like to acknowledge the Hydrogen Effects on Materials Laboratory (HEML)
 - James McNair
 - Brendan Davis
 - Keri McArthur
 - Tanner McDonnell
 - Jeff Campbell

Acknowledgement:

Sandia's Hydrogen Effects on Materials Laboratory (HEML) gratefully acknowledges sustained support from the Office of Energy Efficiency and Renewable Energy's (EERE) Hydrogen and Fuel Cell Technologies Office (HFTO) within the U.S. Department of Energy (DOE). Any subjective views or opinions that might be expressed in the presentation do not necessarily represent the views of the U.S. Department of Energy or the United States Government.