



# Pre-Transient Characterization of MLOF-1 Test Pin

May 2025

*Changing the World's Energy Future*

Allison Roberts Probert, Colby B Jensen, Jason L Schulthess



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**May 2025**

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# Pre-Transient Characterization of MLOF-1 Test Pin

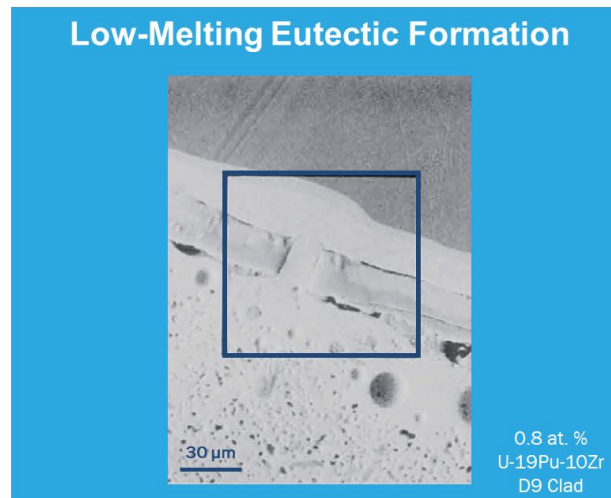
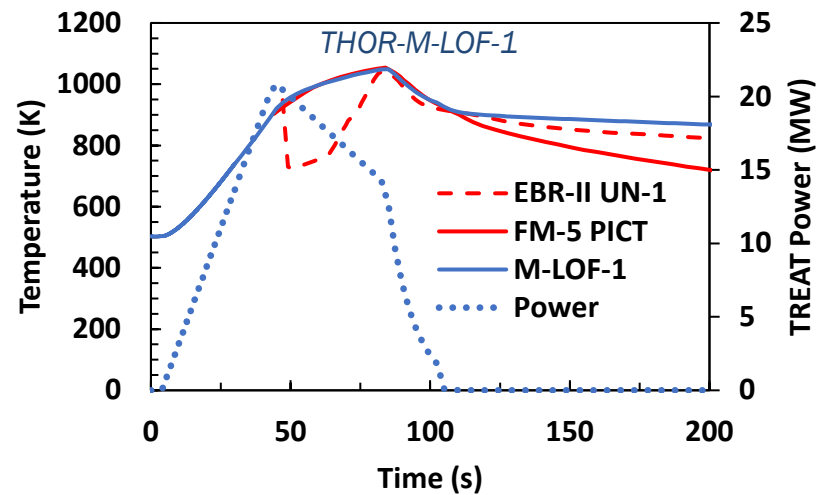
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83415, USA

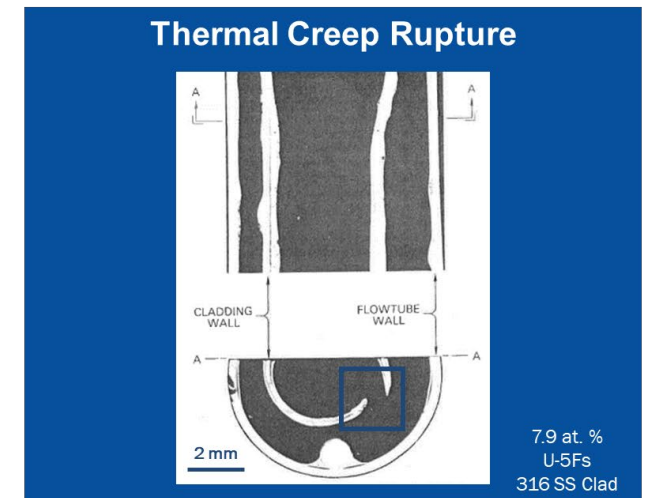
INL/CON-25-84678

# Addressing Gaps in Transient Behavior of Metallic Fuel

- THOR-M will study irradiated metallic fuel performance in transient overpower and loss of flow conditions
- Evaluate in-pile LOF performance, like historic furnace test FM-5
- Measure in-pin fuel expansion, cladding deformation, axial location and detailed characterization of any potential failure sites



Bauer et al. Nuclear Fuel Cycles, 1990



Bauer et al. Technical Report, 1989

Pin Burnup

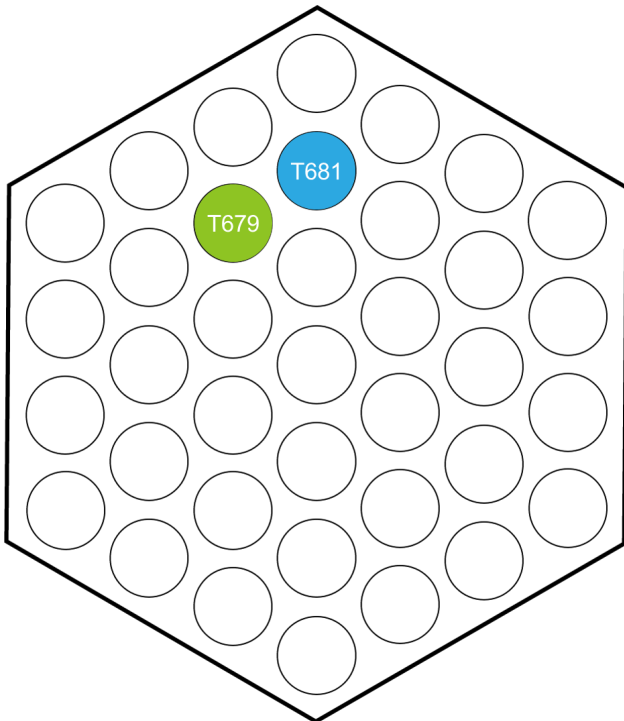
# THOR-M-LOF Test Plan and Pin Specifications

## IV. Comparisons drawn between pre- and post-transient results and historical irradiation/test database

I. Pre-transient non-destructive and destructive examination using test and sibling pins

II. Full pin LOF irradiation in TREAT

III. Post-transient non-destructive and destructive examination on test pin



	Test Pin	Sibling Pin
Subassembly and Pin ID	X430A-T679	X430A-T681
Composition	U-10Zr	U-10Zr
Fuel Diameter (mm)	5.71	5.71
Cladding Material	HT-9	HT-9
Cladding Outer Diameter (mm)	7.37	7.37
Cladding Thickness (mm)	0.406	0.406
Plenum to Fuel Volume Ratio	1.4	1.4
Smear Density	75%	75%

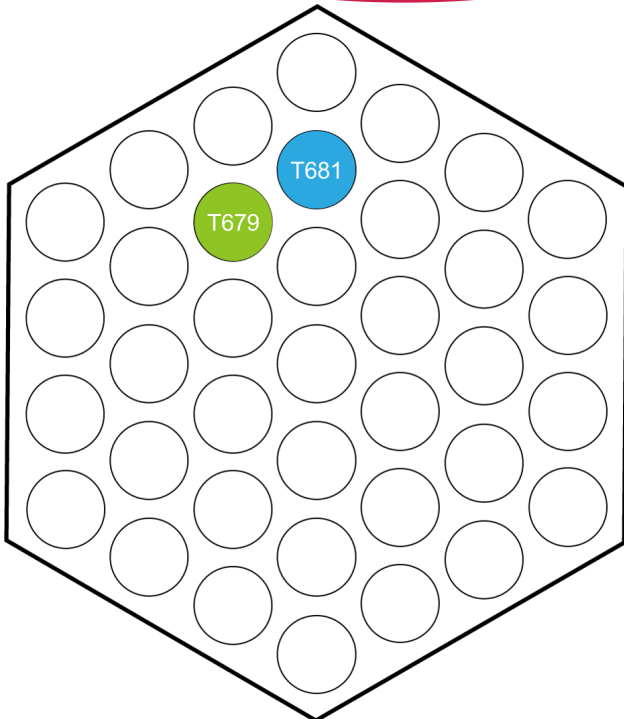
# THOR-M-LOF Test and Sibling Pin Irradiation Histories

IV. Comparisons drawn between pre- and post-transient results and historical irradiation/test database

I. Pre-transient non-destructive and destructive examination using test and sibling pins

II. Full pin LOF irradiation in TREAT

III. Post-transient non-destructive and destructive examination on test pin



	Test Pin	Sibling Pin
Subassembly and Pin ID	X430A-T679	X430A-T681
Composition	U-10Zr	U-10Zr
Calculated Peak Burnup (at.%)	7.4	7.3
Pin Peak Power (kW/m)	49.2	49.2
Pin Peak Clad. Temp (°C)	579	569
Pin Peak Fuel Center Temp. (°C)	675	667
Pin Fast Fluence ( $\times 10^{22}$ n/cm <sup>2</sup> )	20.6	20.6

# Status of Planned Pre-Transient Characterization

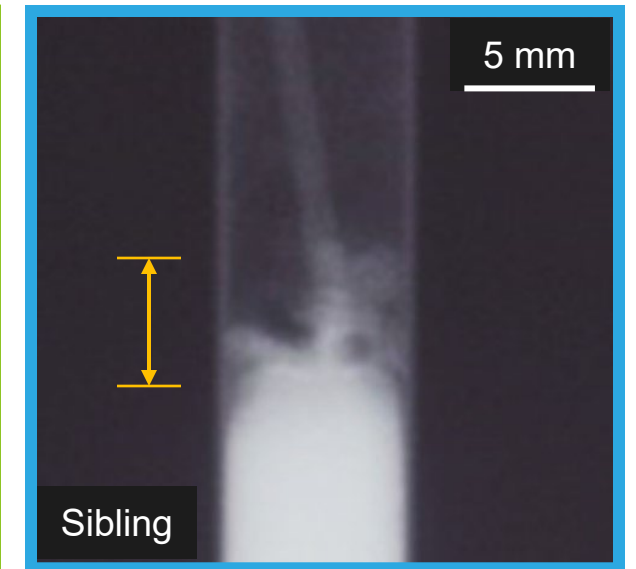
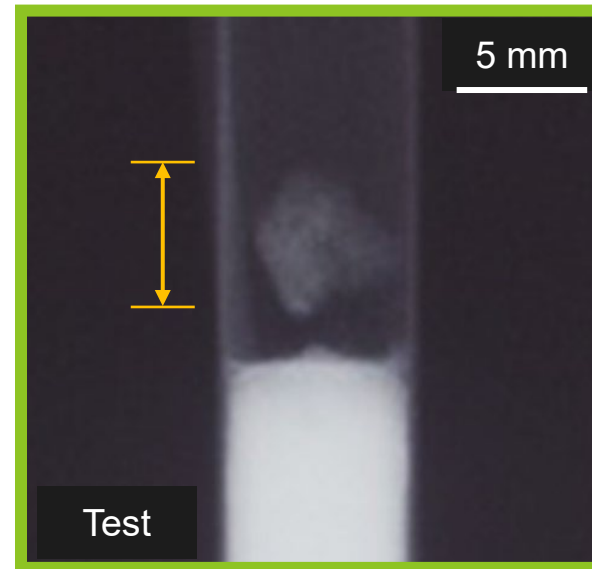
Examination		X430A-T681	X430A-T679
Non-Destructive	Visual (VEM)	C	C
	Neutron Radiography (NR)	C	C
	Element Contact Profilometry (ECP)	C	C
	Precise Gamma Scan (PGS)	C	C
Destructive	Fission Gas Assay, Sample, and Recharge (GASR)	C	-
	Optical Microscopy (OM)	C	-
	Scanning Electron Microscopy (SEM)	FW	-
	Electron Probe Microanalysis (EPMA)	FW	-
	Laser Flash Analysis (LFA)	FW	-
	Burnup (BU) Analysis	FW	-



# Axial fuel strain and fluff structure length measured with neutron radiography



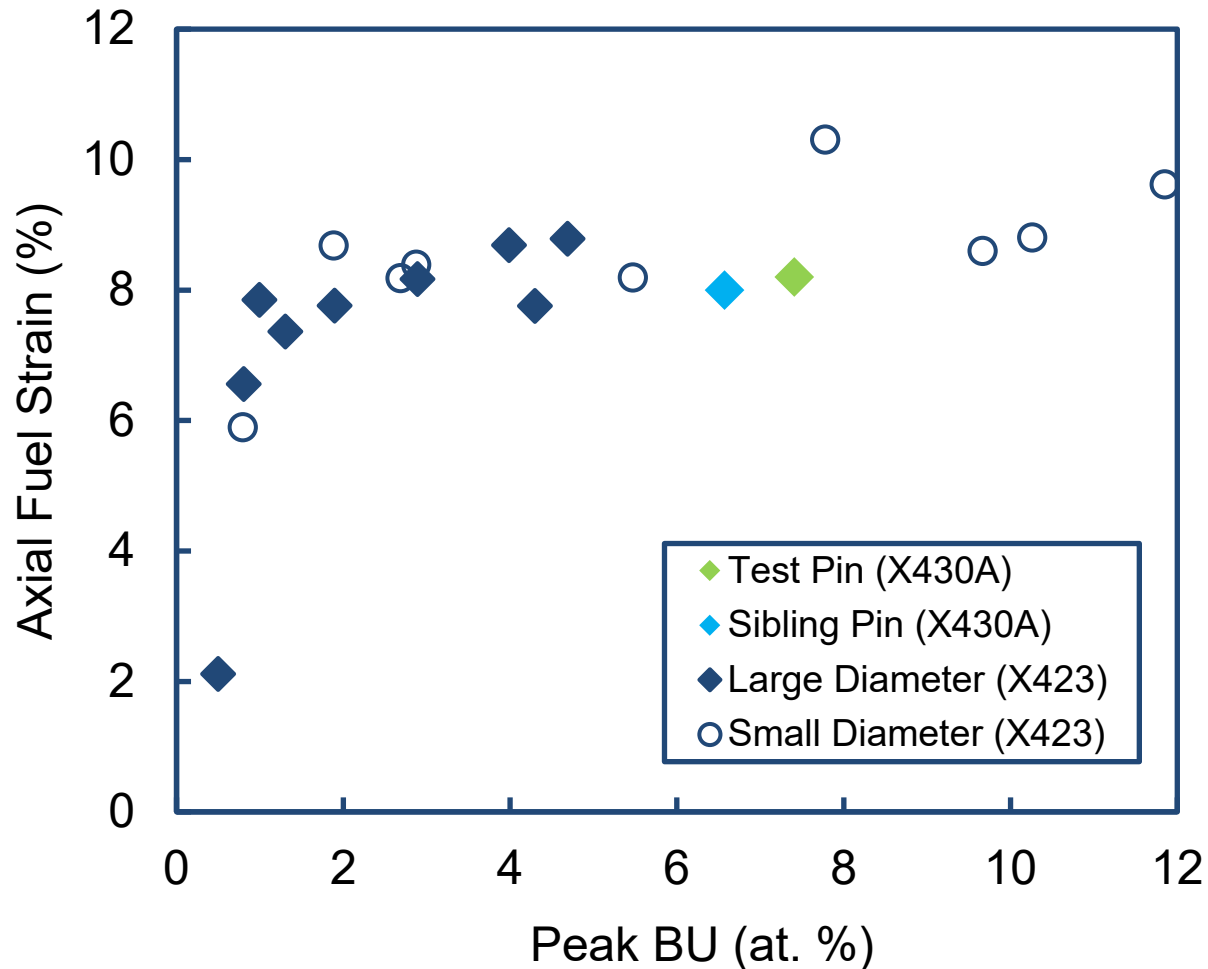
Pin	Test	Sibling
Fuel Pin ID	T-679	T-681
Peak BU (at. %)	7.4	7.3
Axial Strain (%)	8.2	8.0
Fluff Length (cm)	0.44	0.71



Low Density Fluff Structures at the top of the fuel column

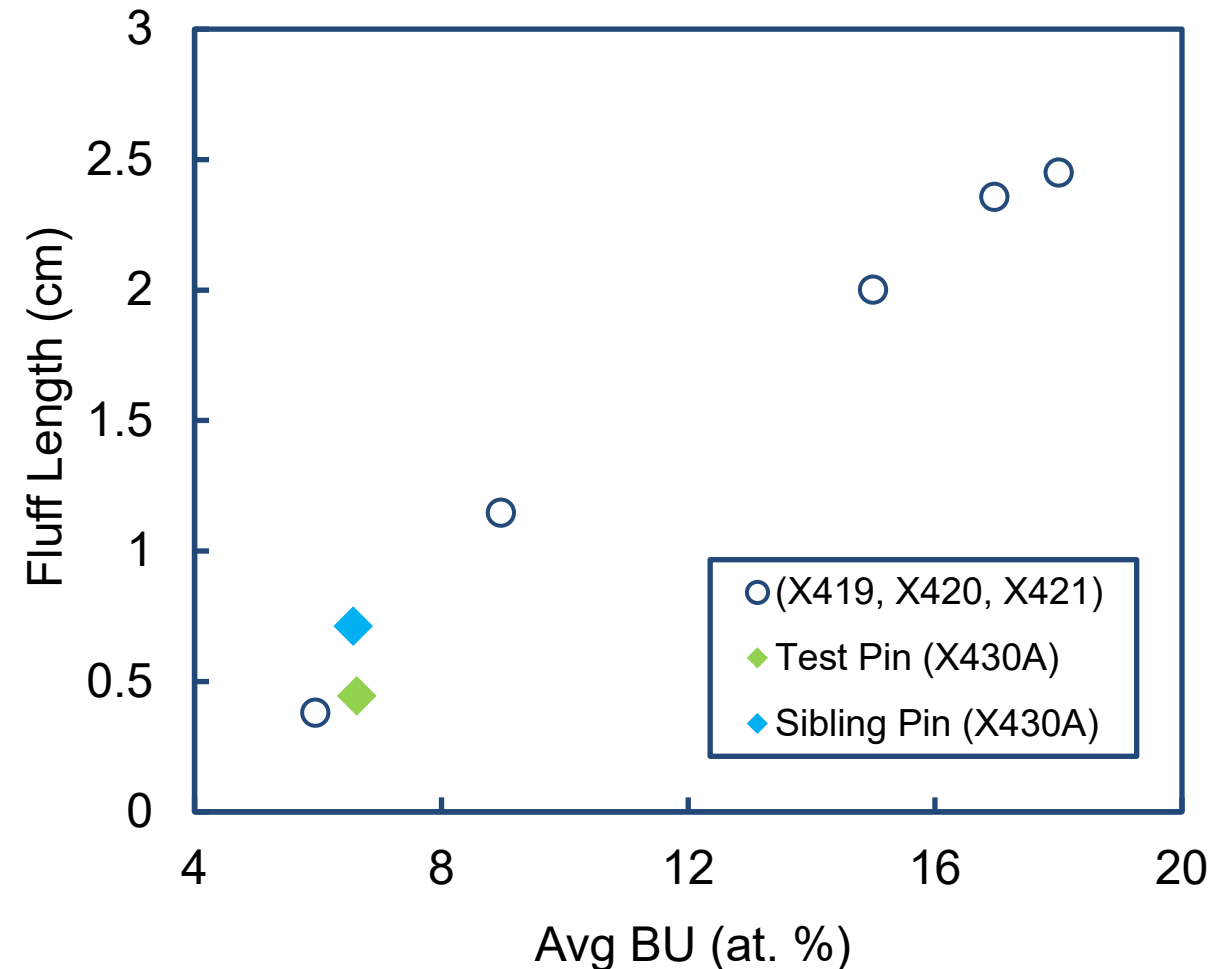
# Axial fuel strain and fluff structure length compare well with reported values

Typical behavior observed for U-Zr alloys  
To consider: X423 ran at lower temp. and 316SS-clad



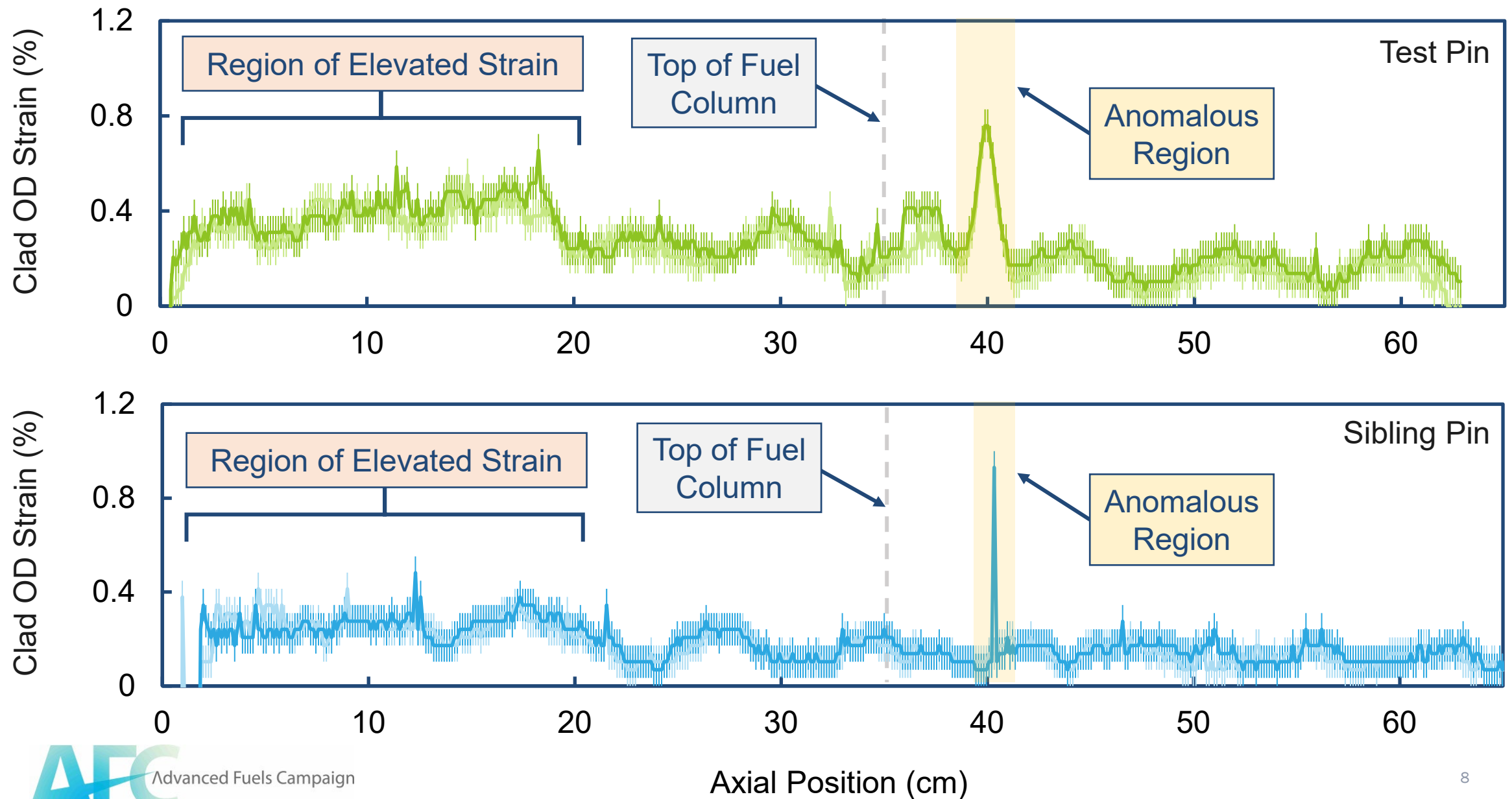
Hofman, G. L., et al. "Swelling behavior of U-Pu-Zr fuel" Metall Trans (1990)

Aligns well with fluff structure trend for U-Zr alloys  
To consider: Smaller diameter pins and D9-clad

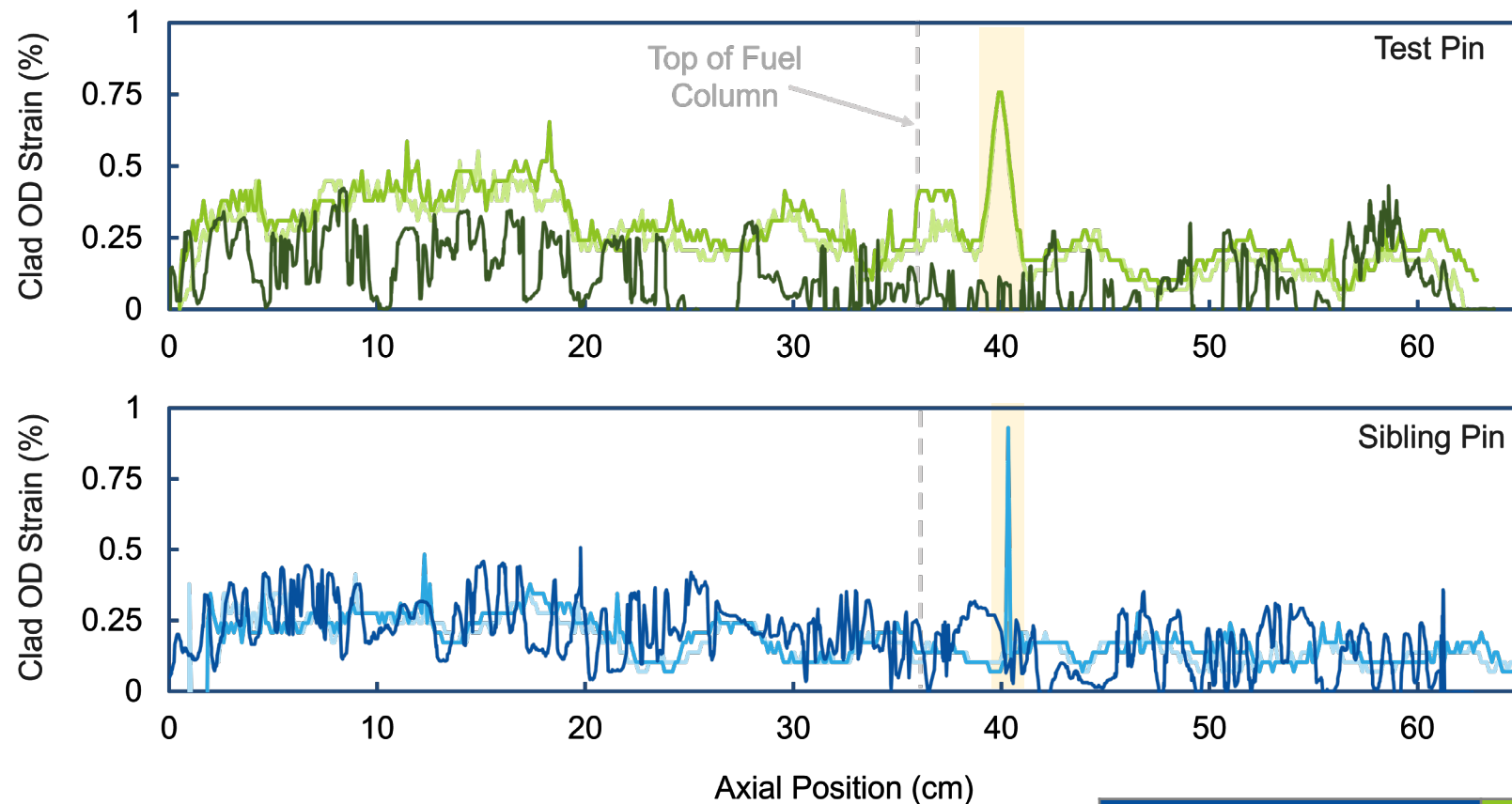


Fay, J., et al. "An analysis of fluff formation in metallic fuel via data analyzes from EBR-II experiments and BISON fuel code modeling" JNM (2022)

# Typical diametral strain value and location, but anomaly above fuel



# Mild strain accumulation in X430A, but still within expected values

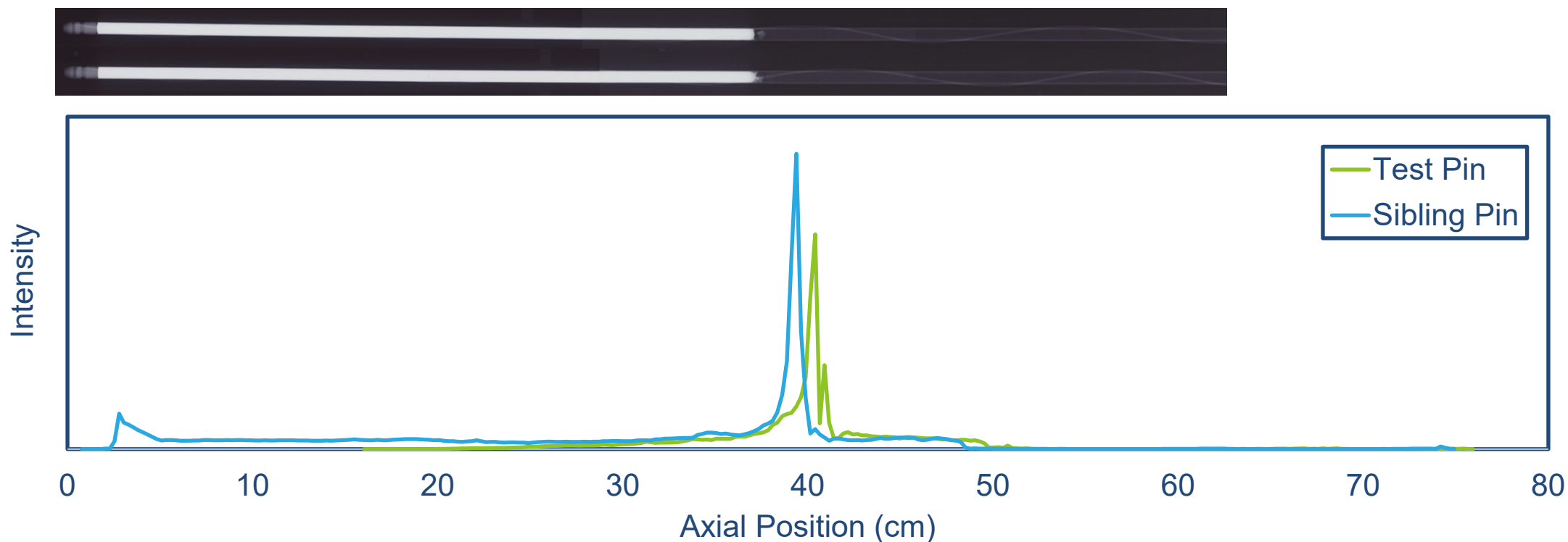


- Peak above fuel column attributed to loose wire wrap present on the pins
- Strain in lower half of the fuel column shown to be statistically larger than upper half
- Modest and expected outer cladding strain behavior

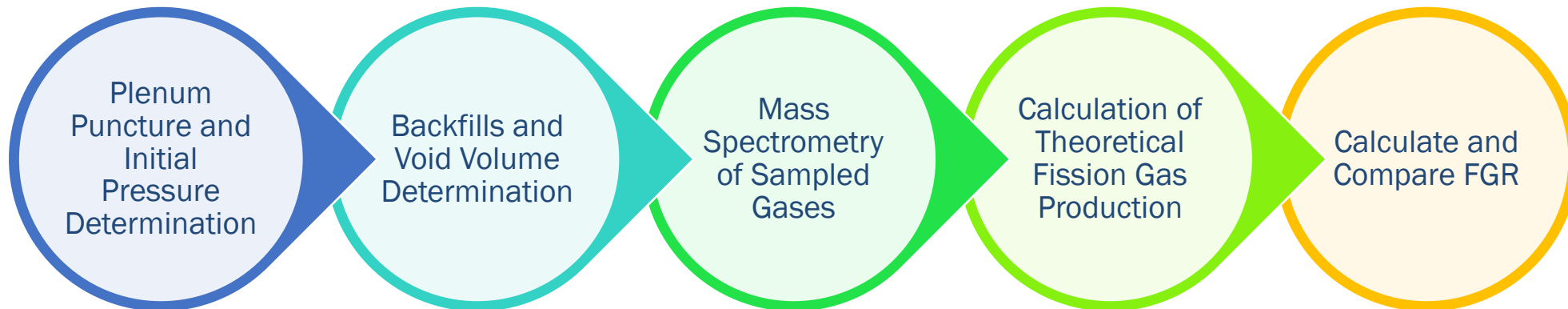
Pin	Test		Sibling	
Fuel Pin ID	T-679		T-681	
Peak BU (at. %)	5.1	7.4	5.1	7.3
Max. Clad Strain (%)	0.24	0.68	0.34	0.34

# Axial distribution of Cs-137 measured using Precise Gamma Scanning

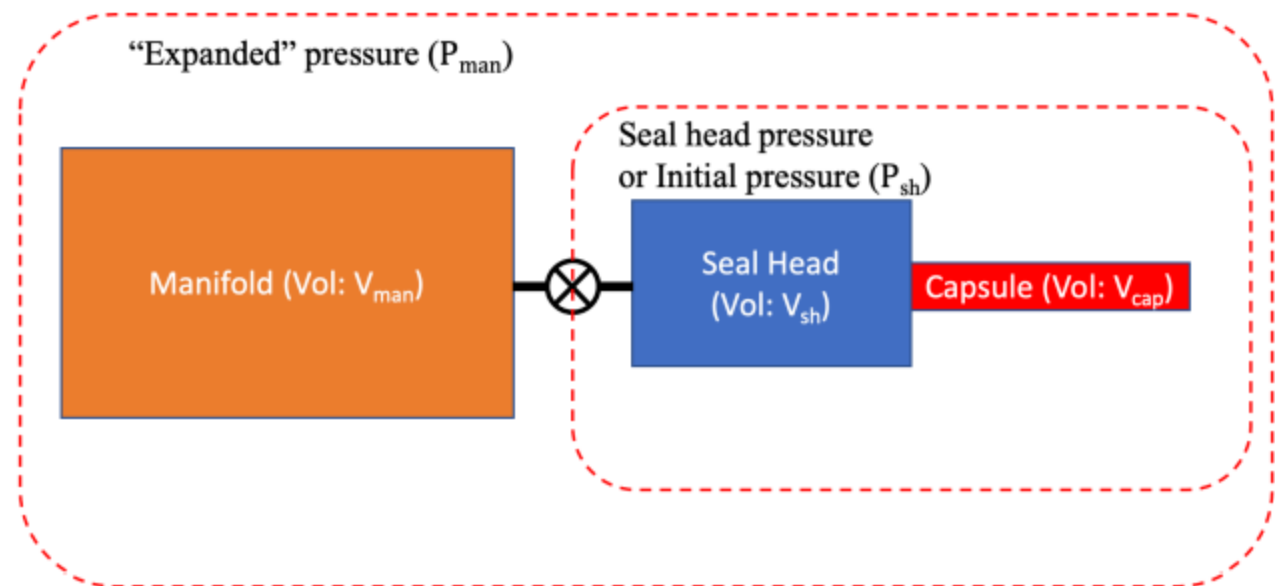
- Increased concentration of Cs-137 above the fuel column within Na bond, which suggests fuel is intact
- Limited undulation along the fuel column, which agrees with no visible features from radiography



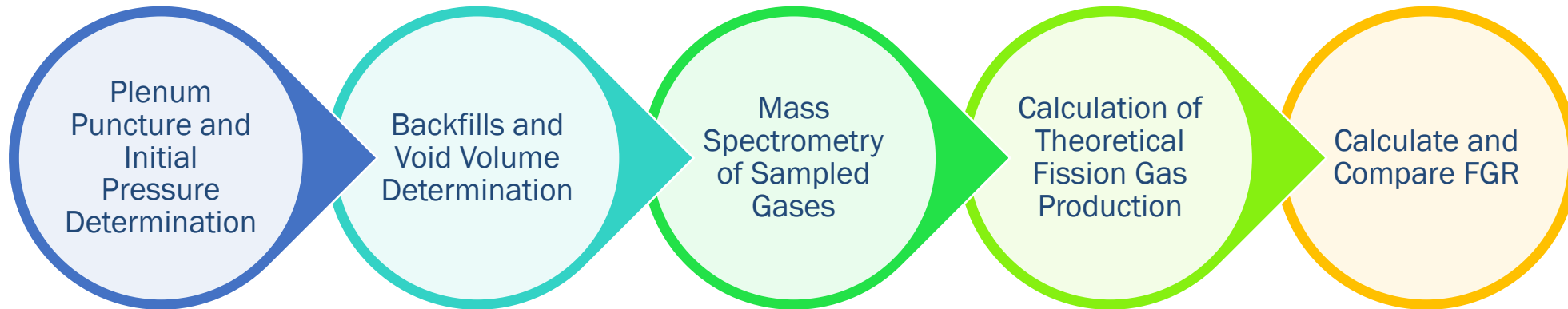
# Fission gas analyzed from destructive examination of sibling pin



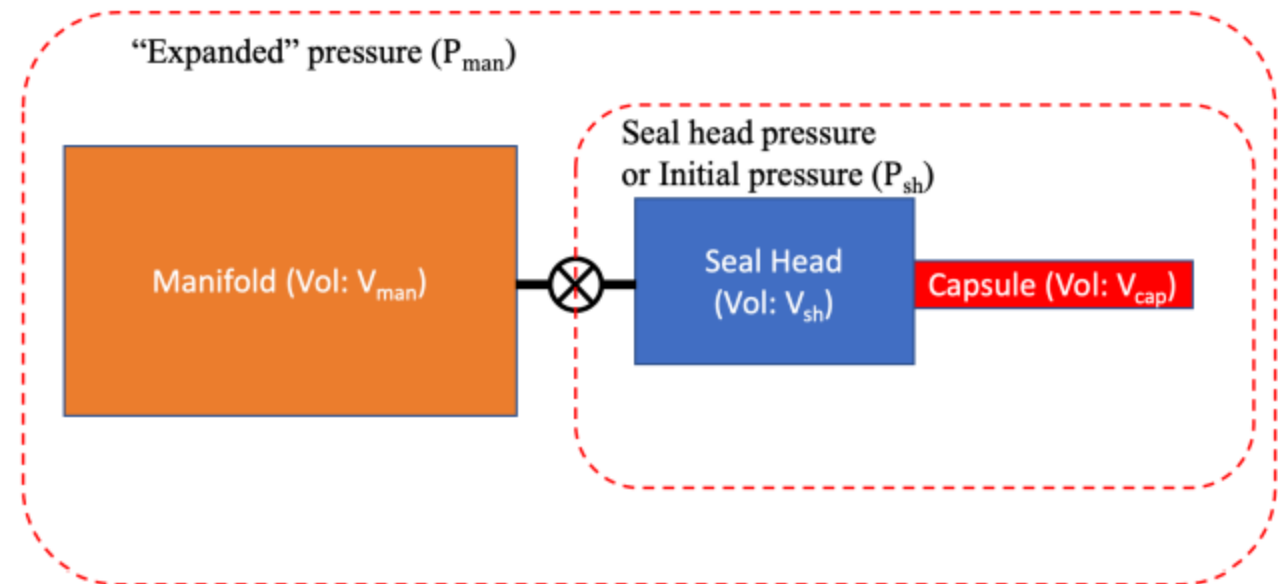
- Initial laser the upper plenum region of a fuel element (capsule)
- Releases fission gas into the seal head
- Record the gas pressure in the seal head
- Release the fission gas from seal head to manifold and record expanded pressure



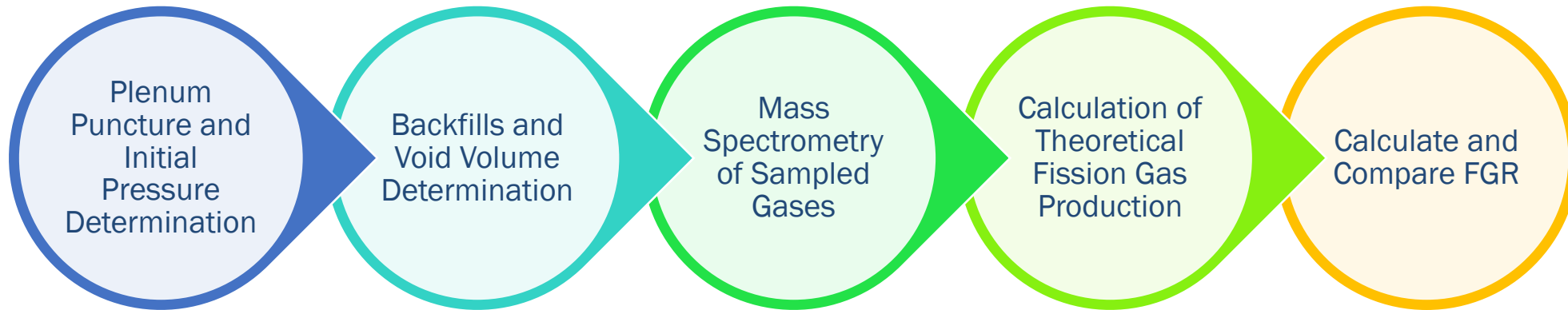
# Fission gas analyzed from destructive examination of sibling pin



- Sampled fission gas collected in bottle
- Mass spectrometry to determine molar % of fission gas composition
- In mass spectrometry report air contamination of sample was reported
  - Determined by  $3 \leq N_2/O_2 \leq 5$
- Correction factor applied based on natural  $N_2/O_2$  and  $Ar/O_2$  ratios and  $O_2$  as the tracer



# Fission gas analyzed from destructive examination of sibling pin



- Theoretical Fission Gas Production calculated based on total fissions in the fuel pin
- Kr/Xe ratio used to determine probability of fission from U-235 or Pu-239
- ENDF/B-VII.1 library for a 500 keV neutron interaction with U-235 and Pu-239

$$(n_{X'})_{predicted} = BU_{avg} \cdot \frac{\rho_{fuel} \cdot V_{fuel}}{\bar{M}} \cdot \pi_X \cdot Y_X$$

$(n_{X'})_{predicted}$  = Predicted yield of daughter fission product (mol)

$BU_{avg}$  = average fuel pin burnup (at. %)

$\rho_{fuel}$  = fuel density (g/cm<sup>3</sup>)

$V_{fuel}$  = fuel volume (cm<sup>3</sup>)

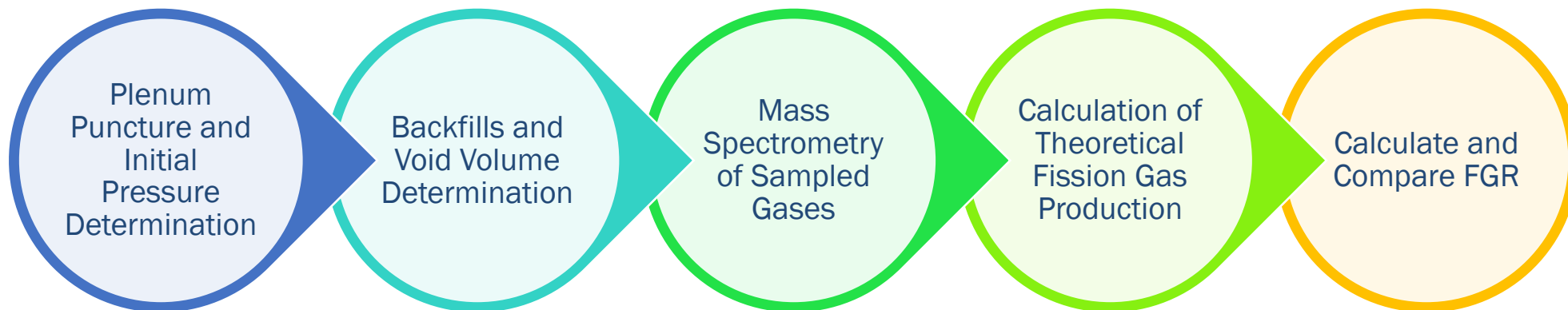
$\bar{M}$  = weighted average molar mass of heavy metal composition (g/mol)

$\pi_X$  = probability of fission from parent nucleus

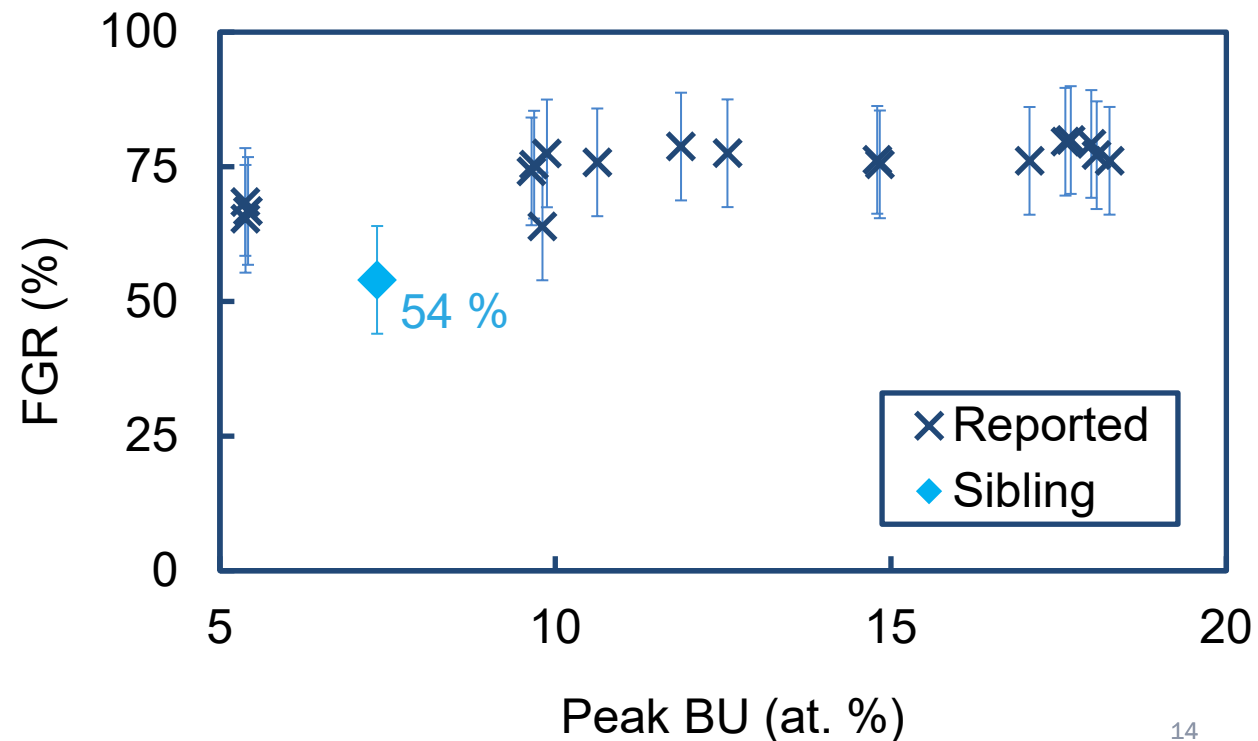
$Y_X$  = expected atomic yield of daughter fission product from parent nucleus



# Measured Fission Gas Release Lower than Expected



- Air contamination likely during sample bottle removal from GASR system, shipping, or attachment to mass spectrometer
- Correction provided by PNNL increased FGR 44% → 54%
  - Higher than expected N %
- Considered decay half life contribution
- Potentially affected by non-uniform mixing



# Sibling pin sectioned for optical imaging, laser, and burnup analysis



Transverse Metallography Mount

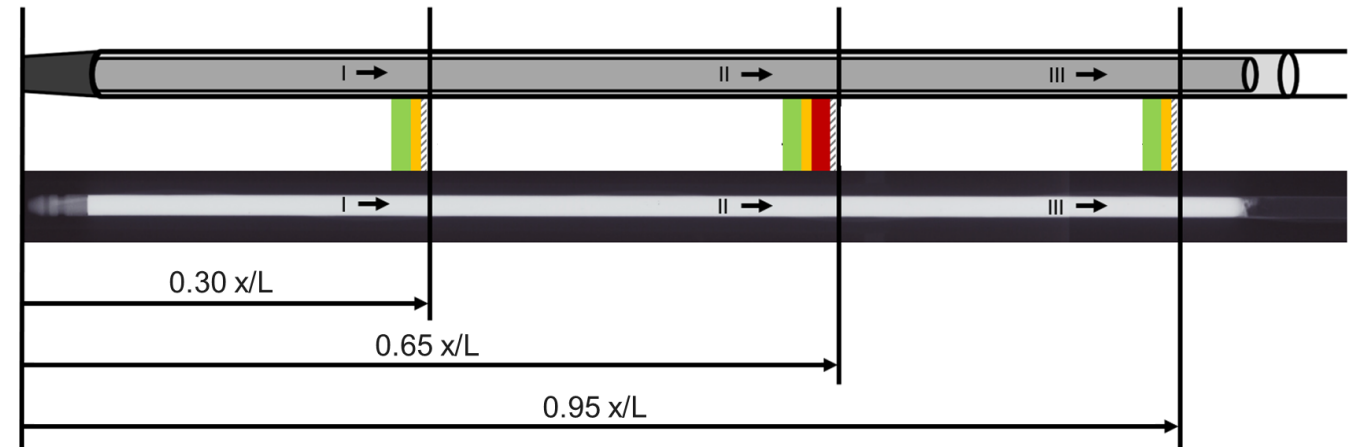


Laser Flash Analysis Sample

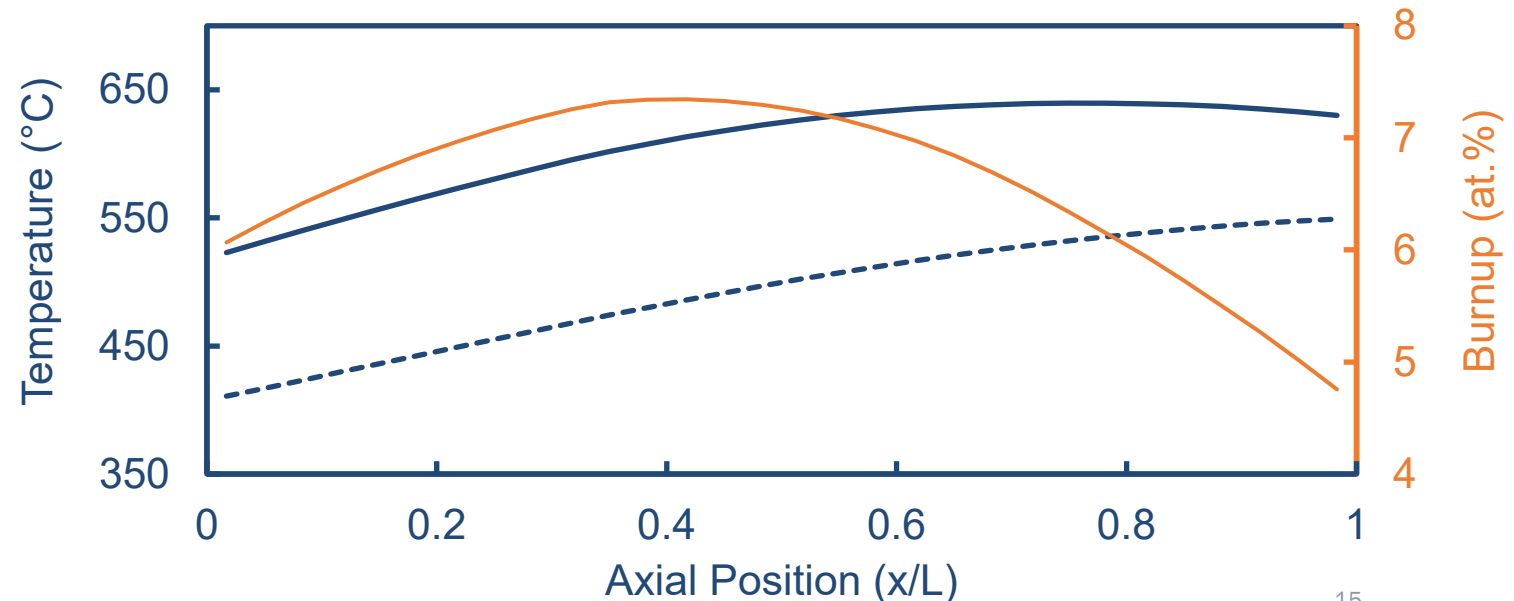


Burnup Analysis Sample

- 3 LFA samples sectioned for future work
- 1 burnup sample sectioned for future work
- 3 met mounts sectioned to be analyzed for microstructural properties under varied conditions:
  - $0.30\ x/L \rightarrow$  High Burnup, Low Temp.
  - $0.65\ x/L \rightarrow$  High Burnup, High Temp.
  - $0.95\ x/L \rightarrow$  Low Burnup, High Temp.



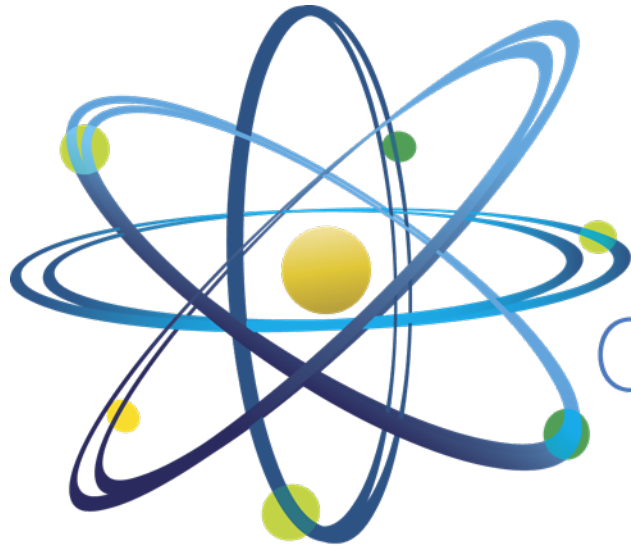
----- Inner Cladding    — Fuel Centerline    — EOL Burnup



# Summary and Future Work

- Confirmation of test and sibling pin suitability:
  - No visual corrosion from storage
  - No uncharacteristic features observed in radiography
- Established baseline steady-state behavior
  - Axial elongation within range of reported values for U-10Zr
  - Fluff structure length aligns with reported values for U-10Zr of similar burnup
  - Diametral strain within range of reported values for U-10Zr
  - Cs-137 distribution consistent with expected results for Na-bonded pins
  - Measured steady-state fission gas release, which will inform transient fission gas measurements
- Sibling pin metallography, SEM, EPMA, LFA, and BU will be analyzed
  - Informs microstructure, composition, FCCI behavior, and thermal properties
- Comparisons to Post-Test Pin PIE to extract contribution of transient behavior

**Thank you  
Questions?**



Clean. **Reliable. Nuclear.**



Advanced Fuels Campaign