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LOCKHEED MARTIN



**FIELD EVALUATION OF A HORIZONTAL  
WELL RECIRCULATION SYSTEM  
FOR GROUNDWATER TREATMENT:  
PILOT TEST AT THE CLEAN TEST SITE  
PORTSMOUTH GASEOUS DIFFUSION PLANT  
PIKETON, OHIO**

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## Abbreviations, Acronyms, and Initialisms

amsl	above mean sea level
bgs	below ground surface
BH	borehole
CE	construction engineer
cm	centimeter
CMSs	corrective measures studies
CTS	Clean Test Site
d	day
DNAPL	dense nonaqueous-phase liquid
DOE	U.S. Department of Energy
ERWM	Environmental Restoration and Waste Management
ETS	Environmental Technology Section
ft	feet
g	grams
gal	gallons
h	hour
HDPE	high density polyethylene
HSO	health and safety officer
ID	inside diameter
in.	inch
K	hydraulic conductivity
kg	kilograms
L	liter
lb	pound
m	meter
$\mu$ g	micrograms
$\mu$ m	micron
min	minute(s)
mL	milliliter
mV	millivolt
ng	nanogram
NTU	nephelometric turbidity unit
OD	outside diameter
ORNL	Oak Ridge National Laboratory
PORTS	Portsmouth Gaseous Diffusion Plant
ppm	parts per million

psi	pounds per square inch
PZ	piezometer
PVC	polyvinyl chloride
s	second
TCE	trichloroethene
U.S.	United States
vs	versus
yd	yard

### Acknowledgment

Identifying, testing, and implementing innovative technologies will be required in order to meet the expectations identified in the Ten Year Plan. The Portsmouth Gaseous Diffusion Plant (PORTS) has hosted and funded many technology demonstrations. The cooperative working relationship with the regulator community, a history of successfully moving from the demonstration stage to remediation of an existing unit, and the available technical support have combined to make PORTS an ideal site for field demonstrating new ideas.

Many individuals and organizations have contributed to the successful completion of this project. Without the financial support and management assistance of the U.S. Department of Energy (DOE) Office of Environmental Restoration and Lockheed Martin Energy Systems (LMES) at PORTS, this project could not have been accomplished. The project team is grateful to the following PORTS individuals for their support to the project:

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## Executive Summary

This report presents the results of field testing a horizontal well recirculation system at the Portsmouth Gaseous Diffusion Plant (PORTS). The recirculation system uses a pair of horizontal wells, one for groundwater extraction and treatment and the other for reinjection of treated groundwater, to set up a recirculation flow field. The induced flow field from the injection well to the extraction well establishes a sweeping action for the removal and treatment of groundwater contaminants. The overall purpose of this project is to study treatment of mixed groundwater contaminants that occur in a thin water-bearing zone not easily targeted by traditional vertical wells. The project involves several research elements, including treatment-process evaluation, hydrodynamic flow and transport modeling, pilot testing at an uncontaminated site, and pilot testing at a contaminated site. The results of the pilot test at an uncontaminated site, the Clean Test Site (CTS), are presented in this report.

Two horizontal wells were installed in October 1994 at the CTS to test the horizontal recirculation concept. The wells, with horizontal sections 70 m (230 ft) long, were installed at a depth of 9 m (30 ft) using a directional drilling rig. The wells were placed along the bedrock surface beneath a 0.6 to 2 m (2 to 6 ft) thick zone of moderately permeable, unconsolidated fluvial deposits. The horizontal sections were constructed with ductile porous filter, an innovative well material produced in Germany by Schumacher Umwelt- und Trenntechnik GmbH. This was the first installation and testing of this well filter material in the United States. The well filters have a pore size of 300  $\mu\text{m}$  and are composed of sintered spheres of high density polyethylene. Drilling and installation of the wells were completed in six days. A network of piezometers was also installed to assess the hydraulic influence of the horizontal well recirculation system on the surrounding groundwater flow field.

Hydraulic tests of well performance showed that a hydraulic gradient of 0.15 could be induced between the wells, an increase of two orders of magnitude over the preexisting gradient. A bromide tracer test showed that the entire flow field between the wells was affected by the recirculation system, with bromide transport dominated by advection in higher-permeability areas and by diffusion in lower-permeability areas. A follow-on elution test provided removal of approximately 77% of the injected bromide mass during a period of 20 days. The tracer test and elution test results indicate that the horizontal well recirculation system shows great promise for application at a contaminated site.

Clogging of the extraction well filter during the tracer test and elution test resulted in deterioration of well performance. It was determined that the method of well development recommended by the filter manufacturer, low rate pumping, was inadequate. During the fall of 1995, the horizontal wells were developed by a more aggressive method that included water jetting and overpumping. Hydraulic tests conducted immediately after well development showed markedly improved well performance. During the fall of 1996, a 60-day recirculation test was performed with no evidence of clogging. These results indicate that water jetting and overpumping are the proper methods for developing wells constructed with the ductile porous filter.

Additional work at PORTS includes testing of the horizontal well recirculation system at a contaminated site, the results of which will be covered in a separate report. The project was jointly funded by the U.S. Department of Energy (DOE) EM-50, Office of Science and Technology, Subsurface Contaminants Focus Area, and by DOE EM-40 through PORTS.

## 1. Introduction

This report presents the results from field tests of a horizontal well recirculation system at the Clean Test Site (CTS) of the Portsmouth Gaseous Diffusion Plant (PORTS), Piketon, Ohio. The field work for this project included the following tasks: (1) characterization of the geology of the CTS, (2) installation of two horizontal wells and 22 piezometers at the CTS, (3) hydrodynamic testing of the horizontal wells and piezometers, and (4) evaluation of the horizontal well recirculation system using pumping tests, tracer tests, and an elution test.

Horizontal wells are a component of the recirculation remedial technology being developed by Oak Ridge National Laboratory (ORNL). The installation and testing of a recirculation treatment system is one phase of a research and development project entitled "*In Situ* Treatment of Mixed Contaminants in Groundwater (OR141002)". This project is jointly funded by the U.S. Department of Energy (DOE) Office of Technology Development and PORTS Environmental Restoration and Waste Management (ERWM). The overall purpose of this three-year project is to study in situ treatment of mixed contaminants in groundwater using recirculation-well networks coupled with treatment modules. The mixed contaminants are volatile organic compounds such as trichloroethene (TCE) and radionuclides such as technetium. The project began in October 1993 and involves several key research elements, including treatment-process evaluation and screening, hydrodynamic flow and transport modeling, bench- and pilot-scale experimentation, and full-scale field demonstration at a DOE site (ORNL 1994).

PORTS ERWM is performing corrective measures studies (CMSs) to evaluate clean-up technologies for groundwater contamination at PORTS. This project will support those CMSs that address TCE and technetium contamination in groundwater by providing information on several groundwater treatment processes and by providing information necessary to evaluate the feasibility of using a horizontal well recirculation system for treatment of groundwater contamination at PORTS.

The CTS at PORTS was chosen as an appropriate location for determining the feasibility of installing and operating a recirculation treatment system. Upon successful testing of the system (successful installation, development, and hydrodynamic operation of the horizontal wells and recirculation system at a useful rate), a follow-on project is planned to demonstrate the use of a recirculation treatment system at a PORTS location with contaminated groundwater.

### 1.1 Objectives

Objectives for the evaluation of a recirculation treatment system at the CTS are as follows:

- Demonstrate innovative or alternative methods of installing horizontal wells;
- Determine the accuracy (depth control and lateral control) with which horizontal wells can be placed in a shallow, thin aquifer system;

- Determine achievable pumping rates and aquifer hydrodynamics associated with a horizontal well recirculation system at the CTS.

## 1.2 Organization

The remainder of this report is organized as follows:

- Section 2 describes the CTS and results of the site characterization.
- Section 3 describes the horizontal well installation and initial development by pumping.
- Section 4 describes the piezometer installation and development.
- Section 5 describes the results of hydrodynamic tests of the piezometers and wells.
- Section 6 describes the results of tracer tests of the recirculation flow field.
- Section 7 describes the results of a bromide-elution test.
- Section 8 describes the use of a water-jetting development method to develop the horizontal wells and improve their performance.
- Section 9 presents conclusions from the results of the field work and lessons learned.

## 2. Background

### 2.1 Facility Description

PORTS is a federal facility owned by DOE. The plant is operated by Lockheed Martin Utility Services under a contract with the United States Enrichment Corporation, a government-owned corporation. Lockheed Martin Energy Systems performs ERWM activities as well as the site management required by DOE. The 15.75 km<sup>2</sup> (3,892 acre) federal reservation lies in Pike County, Ohio, between the cities of Chillicothe and Portsmouth and is approximately 113 km (70 miles) south of Columbus, Ohio (Fig. 2.1).

PORTS has been in operation since 1954 and is used to enrich uranium for commercial nuclear reactors. The PORTS process uses molecular diffusion techniques to separate the <sup>235</sup>U isotope from the <sup>238</sup>U isotope. PORTS consists of a complex cascade of compressors and converters through which gaseous uranium hexafluoride feed is processed. The plant has an extensive support complex that consists of machine shops, laboratories, utilities, and decontamination facilities. As a result of plant operations, PORTS generates a wide variety of wastes, including low-level radioactive wastes, spent solvents, polychlorinated biphenyl-contaminated oils, electroplating wastes, paint wastes, metal sludges, acids, and caustics.

### 2.2 Site Description

The CTS is located northwest of the intersection of Hewes Street and Perimeter Road and east of the X-230K Holding Pond (Fig. 2.2). The topography of the CTS is relatively level, with a drainage area along the western boundary and a hill adjacent to the eastern boundary of the site (Fig. 2.3). The CTS lies outside of the security fence of the plant and is in an uncontaminated area.

### 2.3 Site Characterization

The ORNL Environmental Technology Section (ORNL/ETS) characterized the geology of the CTS during the spring and summer of 1994 by collecting soil samples with a hollow-stem-auger drilling rig and a GeoProbe™ rig. The geologic data collected from this site characterization were used to guide the placement of the horizontal wells.

The soil above bedrock at the CTS is composed of unconsolidated Quaternary fluvial and lacustrine deposits. These deposits are characterized by 4.6 to 6.7 m (15 to 22 ft) of low-permeability clays and silts known as the Minford member, which is underlain by 0.6 to 2 m (2 to 6 ft) of moderately permeable sandy gravels, gravelly sands, and silty sands known as the Gallia member. The bedrock underlying the Quaternary deposits is composed of Mississippian-age Sunbury shale and Berea sandstone and shale. The Sunbury is a very low permeability shale unit that underlies the Gallia at the site.

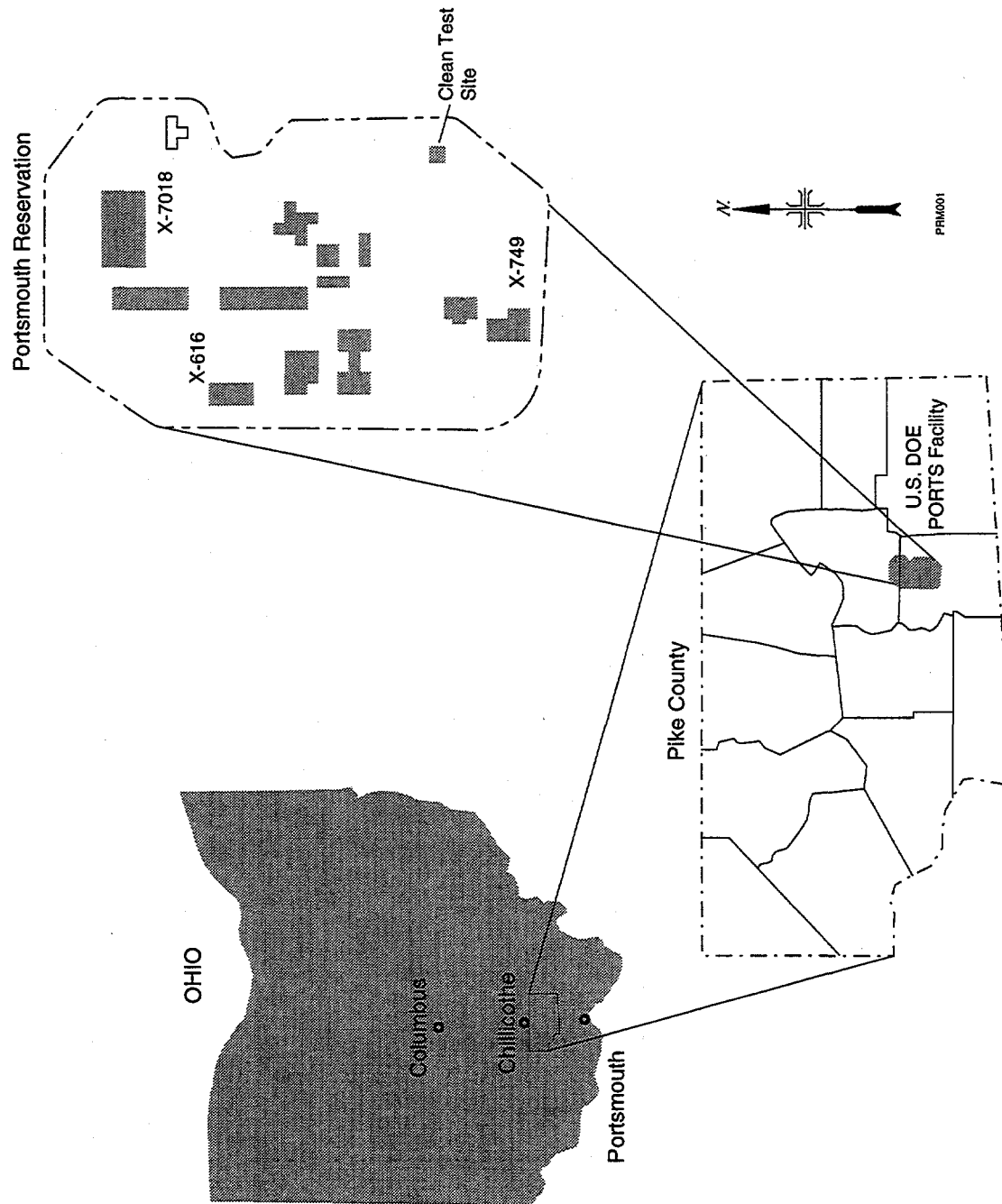
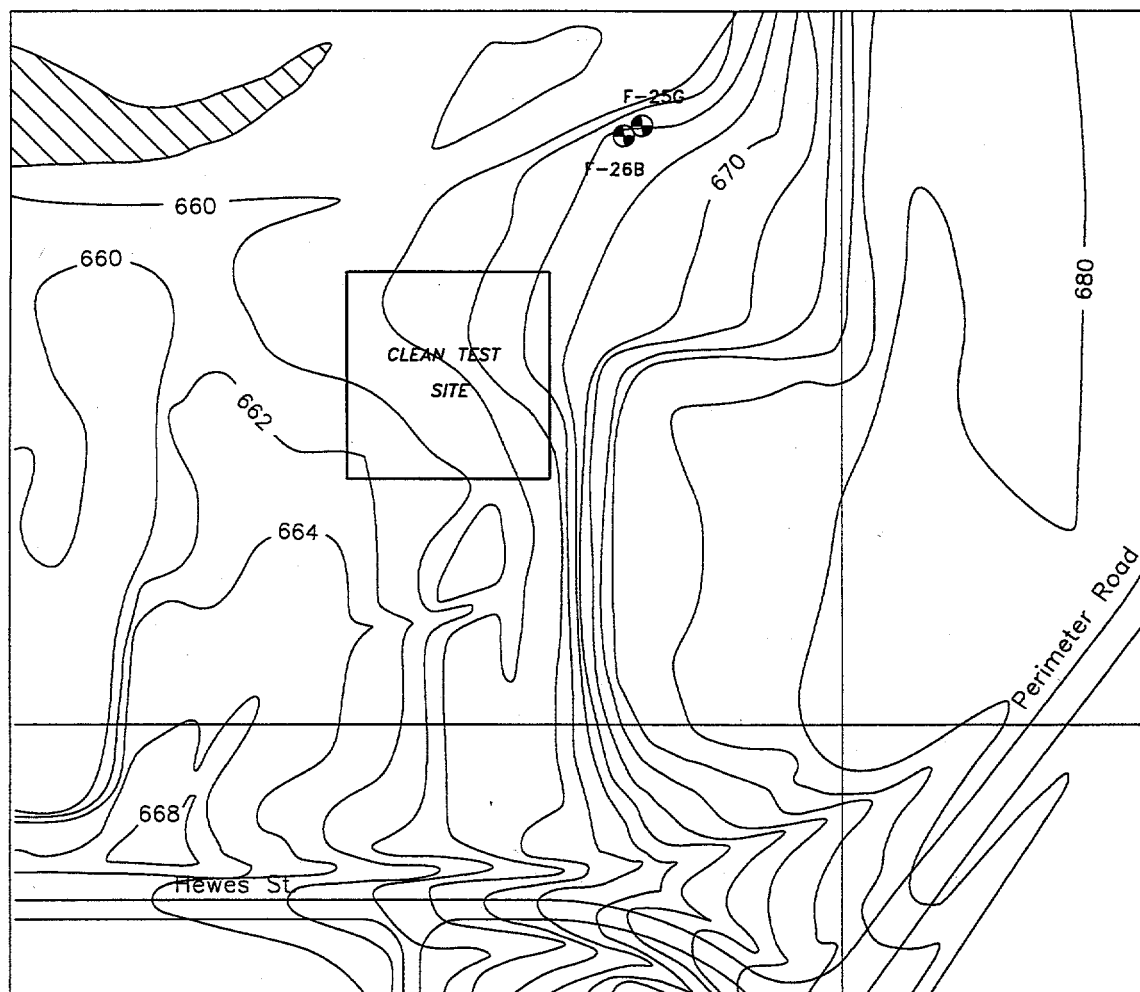


Fig. 2.1. Location of Portsmouth Gaseous Diffusion Plant.

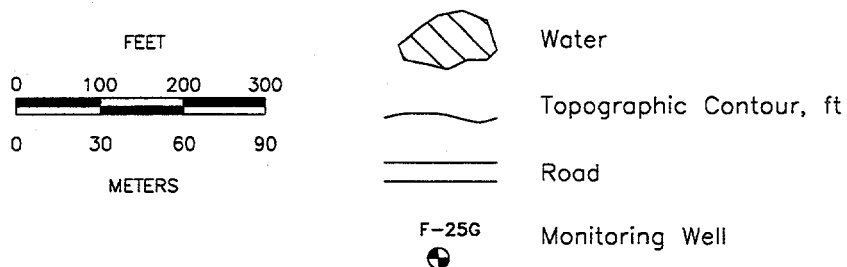


Fig. 2.2. Location of the Clean Test Site.





Portsmouth Facility  
Surface Topography at CTS



Source: PORTS ER/WM

Fig. 2.3. Topography of the Clean Test Site.

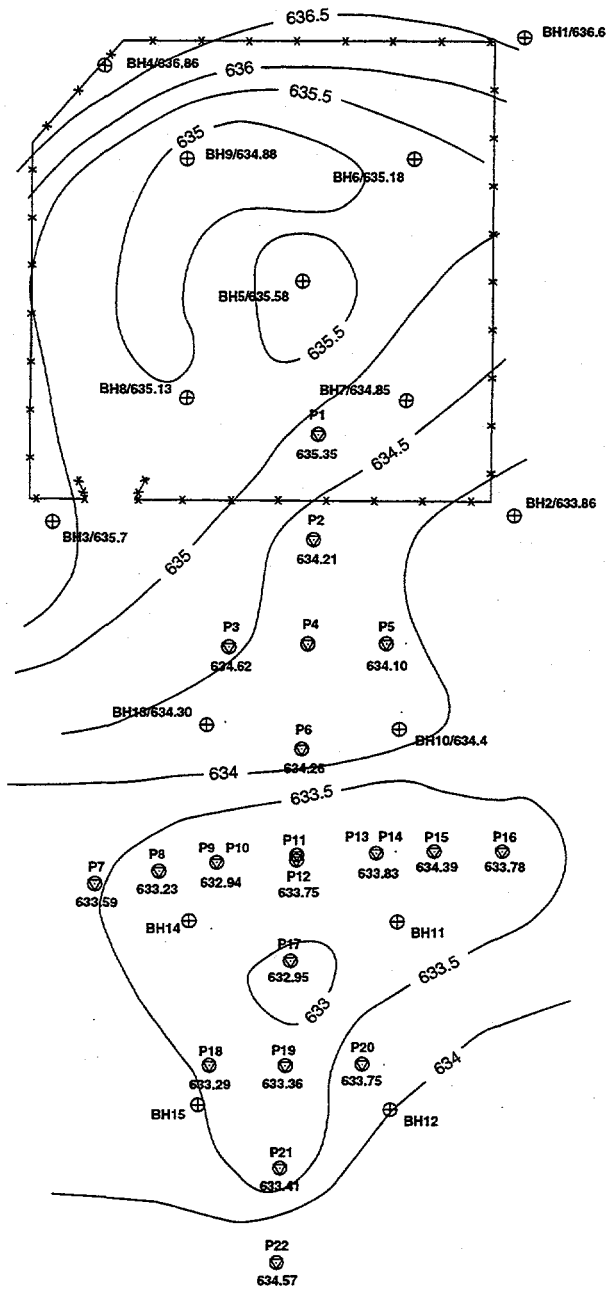
The fenced area of the CTS is 73 m by 76 m (240 ft by 250 ft) (Fig. 2.2). During characterization nine boreholes were installed to bedrock at a depth of approximately 9 m (30 ft). The borehole locations are numbered 1 through 9 in Fig. 2.4. Drilling was accomplished using an all-terrain CME 55 drill rig. The rig used 15.9-cm (6.25-in.) outside diameter (OD) by 8.3-cm (3.25-in.) inside diameter (ID) hollow-stem augers. A 7.6-cm (3-in.) diameter by 1.5-m (5-ft) long CME continuous sampler was run a few centimeters ahead of the lead auger to obtain undisturbed soil samples for geologic logging. An average of three soil samples per hole were collected and analyzed for moisture content, liquid limit, plastic limit, and grain size. A detailed geologic log was prepared for each hole. Appendix A provides copies of the geologic logs and the results of the geotechnical analyses. As an example, Fig. 2.5 shows the stratigraphic sequence in borehole number 7.

Water-level measurements taken during the drilling project indicated that groundwater in the Gallia and perhaps the lower portion of the Minford is confined by the overlying clays and silts. When the confined layers were penetrated by the augers, the groundwater level rose an average of 4.1 m (13.5 ft) above the depth at which saturated sediments were first encountered during drilling. Section 3 of this report presents a potentiometric-surface map based on water-level measurements from the network of piezometers.

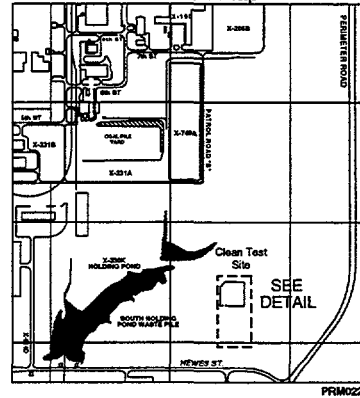
The locations of the horizontal wells extend 137 m (450 ft) south of the fenced area of the CTS. During the summer of 1994, ORNL/ETS characterized the depth and thickness of the Gallia in the area of the horizontal wells. This was accomplished by collecting soil samples with a GeoProbe rig from six locations, numbered 10 through 15 in Fig. 2.4. The GeoProbe rig used a hydraulic ram to push a 2.5-cm (1-in.) OD, hollow-steel rod into the subsurface. To collect soil samples, the GeoProbe rods were fitted with a drive point first or soil sample tube with drive point and pushed to the top of the sampling interval. Starting at a depth of approximately 4.6 m (15 ft) below ground surface (bgs), soil samples were collected continuously until the base of the Gallia was reached [at a depth of approximately 9.1 m (30 ft)].

In the area of the horizontal wells, the Gallia is approximately 0.9 to 1.1 m (3 to 3.5 ft) thick. Table 2.1 provides the surveyed elevations of the ground surface and bedrock surface for the 15 soil boring and GeoProbe locations. Figure 2.4 is a bedrock contour map for the CTS (using bedrock surface elevations from Table 2.1 for the control points). Figure 2.6 shows cross sections of the geology at the locations of the horizontal wells. This geologic information was used to guide the placement of the horizontal wells along the bedrock surface.

## DETAIL



## Location Map



## EXPLANATION

- Piezometer Location
- Borehole Location
- Bedrock Contour = 0.5 ft
- Fence

NOTE: If no elevation appears, bedrock elevation is unknown.

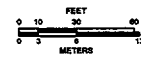


Fig. 2.4. Bedrock surface contour map for the Clean Test Site.

DEPTH (ft)

0.5

MINFORD CLAY

CL SILTY CLAY: yellowish brown (10YR 5/8) with gray mottling (10YR 5/1), firm, slightly moist, scattered organic staining.

CL SILTY CLAY: yellowish brown (10YR 5/4) becoming light gray to gray (10YR 7/1-6/1), moist, firm.

8.5

CL CLAY: reddish brown (5YR 4/4), moist, dense, common MnO staining.

MINFORD SILT

ML CLAYEY SILT: yellowish brown (10YR 6/6), moist, firm, sandy in part, angular sandstone pebble and gravels.

ML CLAYEY SILT: as above, grading to silty sand at 20'.

22

GALLIA

SM SILTY SAND: light olive brown (2.5Y 5/4) mottled with gray silt, fine grained, abundant limonite staining, moist, friable.

SM SILTY SAND: olive to olive yellow (5Y 5/4-6/6), moist, becoming wet with depth, angular pebbles.

27

SUNBURY SHALE

SHALE: black carbonaceous.

30

PSTRAT

Fig. 2.5. Stratigraphic sequence of borehole number 7.

**Table 2.1. Survey elevations of ground surface and bedrock surface at borehole locations**

<b>Borehole number</b>	<b>Ground elevation, ft amsl</b>	<b>Depth to bedrock, ft bgs</b>	<b>Bedrock elevation, ft amsl</b>
1	666.10	29.5	636.60
2	662.36	28.5	633.86
3	657.20	21.5	635.70
4	661.32	24.5	636.86
5	661.58	26.0	635.58
6	664.88	29.7	635.18
7	661.85	27.0	634.85
8	659.13	24.0	635.13
9	661.38	26.5	634.88
10	662.70	28.3	634.40
11	662.73	28.8	633.93
12	663.07	29.1	633.97
13	658.80	24.5	634.30
14	658.12	24.5	633.62
15	658.88	24.0	634.88

amsl = above mean sea level

bgs = below ground surface

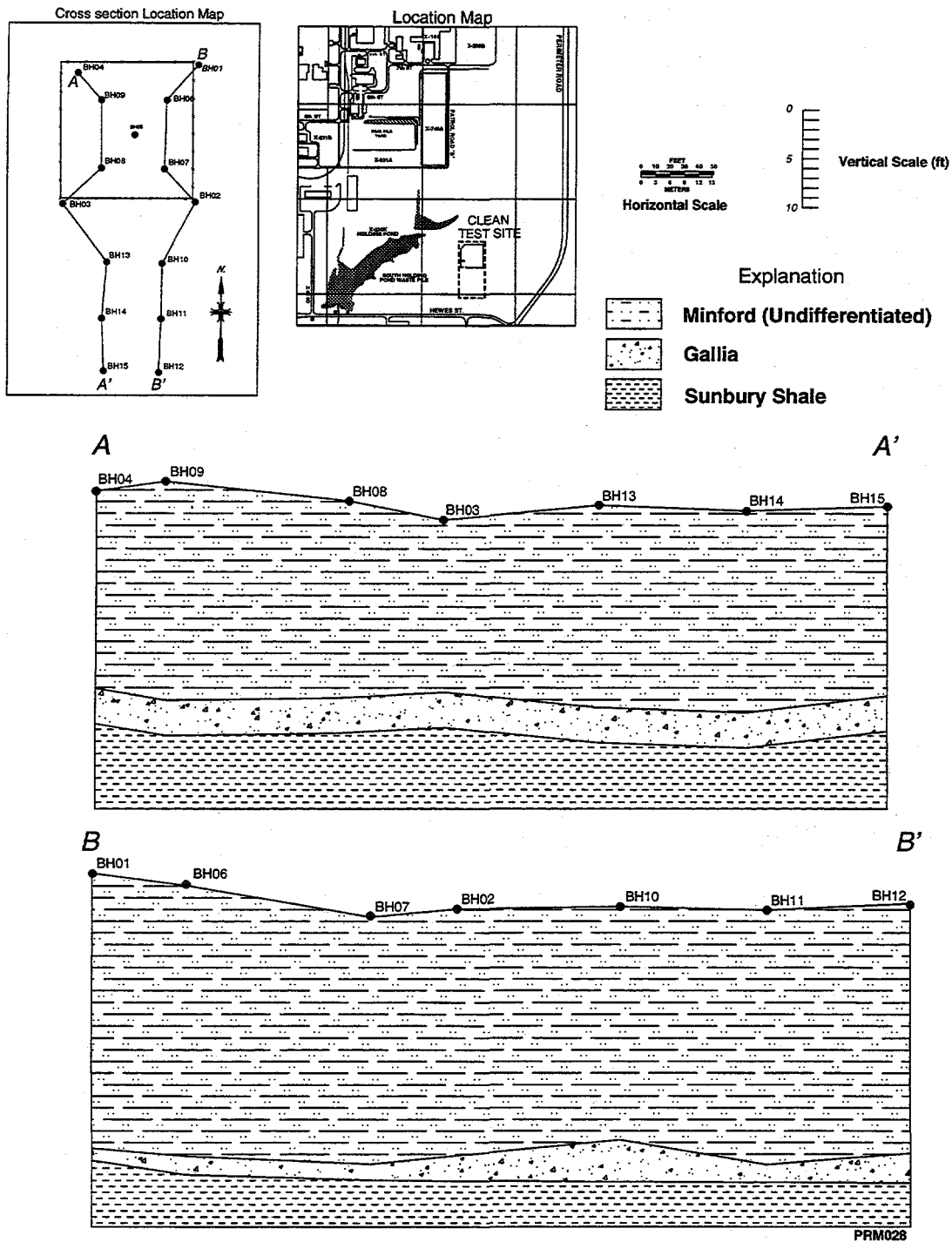


Fig. 2.6. Geologic cross sections at the locations of the horizontal wells.

### 3. Horizontal Well Installation and Development

Two horizontal wells were installed at the CTS from October 17 through October 22, 1994. Schumacher Filters America, Inc. (Schumacher America) provided the well installation service to ORNL/ETS through cooperation with FlowTex Technologie Import von Kabelverlegemaschinen GmbH (FlowTex), Schumacher Umwelt- und Trenntechnik GmbH (Schumacher), and Mears Engineering, Inc. (Mears). FlowTex directed the drilling and well installation and performed the drilling navigation, Schumacher provided porous filter materials for the wells, and Mears performed the drilling and well installation.

The horizontal wells were installed using a directional drilling rig. Because the Gallia is a thin formation, accurate control of the depth and direction of the drilling bit was essential. FlowTex used navigation equipment from Germany to provide a vertical accuracy of  $\pm 15$  cm ( $\pm 0.5$  ft) at a depth of 9.1 m (30 ft) bgs. Each well was completed to land surface at both ends (Figs. 3.1 and 3.2). The horizontal sections are approximately 70 m (230 ft) long, and the slanted sections of pipe are approximately 37 to 40 m (120 to 130 ft) long (these sections were as short as practicable, dependent on the turning radius of the drilling equipment).

Each well was constructed with ductile high-density-polyethylene (HDPE) casing [13-cm (5-in.) ID] and ductile HDPE porous filter [7.6 cm (3-in.) ID with a fitting at each end to connect to the 13 cm (5-in.) ID casing]. The porous filter, used to construct the horizontal sections of the wells, is produced by Schumacher in Germany and is supplied in the U.S. by Schumacher America. As explained in Sect. 1, one of the objectives of this project was to test the performance of this innovative well filter material. Appendix B provides a description of this porous filter. No comparable product is known to be available from U.S. manufacturers, and there are no other distributors of the Schumacher filter in the U.S.

The casing materials came to the site in 12-m (40-ft) lengths and the filter materials in 3.7-m (12-ft) lengths. Prior to installation, the well materials were butt-fused together such that the porous filter was placed within the Gallia along the bedrock surface; the blank casing extended to ground surface from both ends of the filter. The wells were expected to provide a yield of 57 L/min (15 gal/min) or more (based on PORFLO modeling of the horizontal wells performed by ORNL), with low turbidity. A Schumacher filter pore size of 300  $\mu$ m (Appendix B) was selected to provide optimum water clarity, based on the results of filtration tests conducted by Schumacher using Gallia soil samples.

The drilling method included drilling a 22-cm (8.75-in.)-diameter guided pilot hole, picking up a 20-cm (8-in.)-diameter HDPE shelter casing at the exit hole and then pulling the shelter casing back into the hole with a 30-cm (12-in.)-diameter backreamer (Fig. 3.3). The casing and filter materials for the horizontal well were housed inside the shelter casing during installation. After the shelter casing and well materials were in place, the shelter casing was pulled from the borehole, and the borehole was allowed to collapse around the well materials.

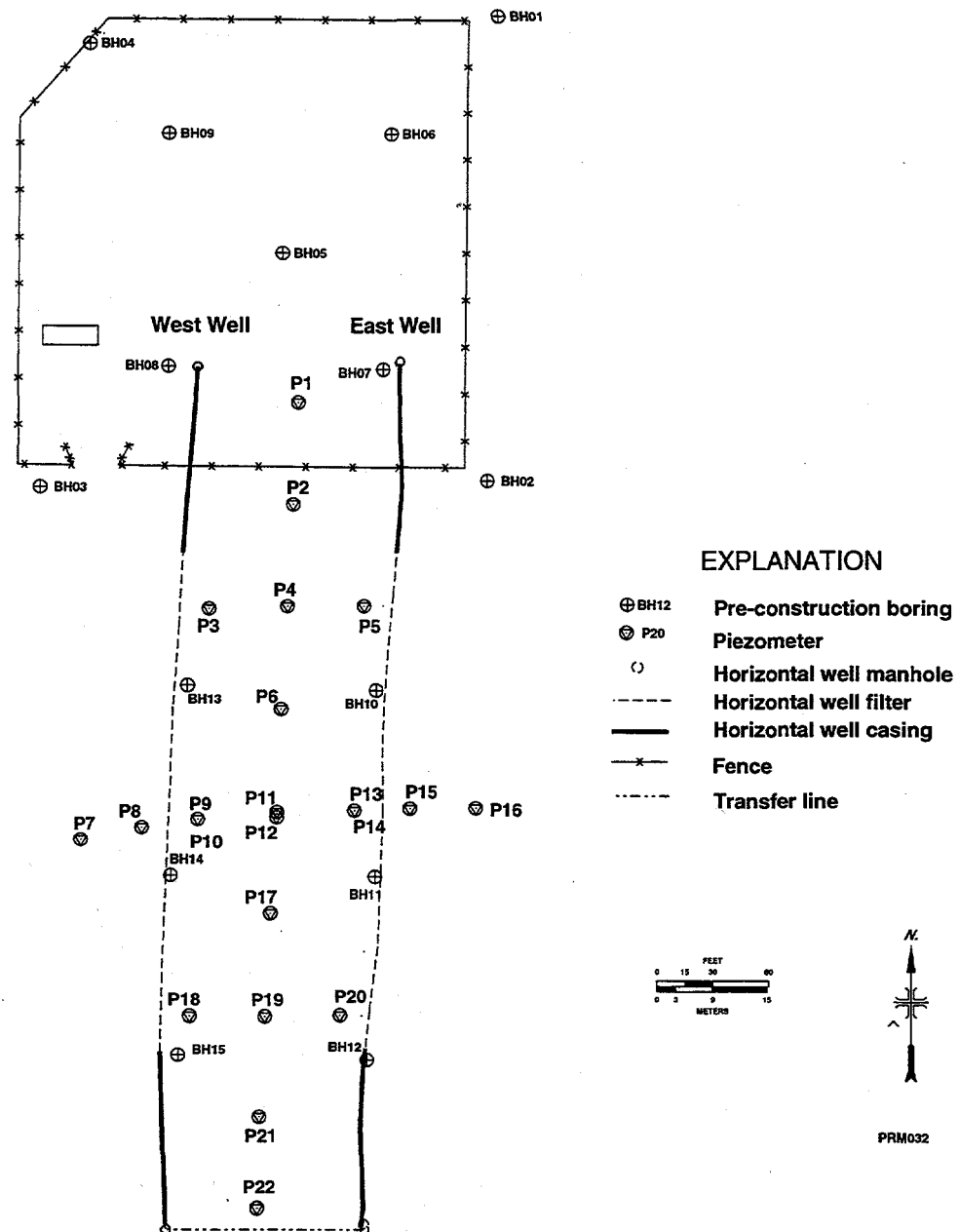


Fig. 3.1. Locations of horizontal wells and piezometers.



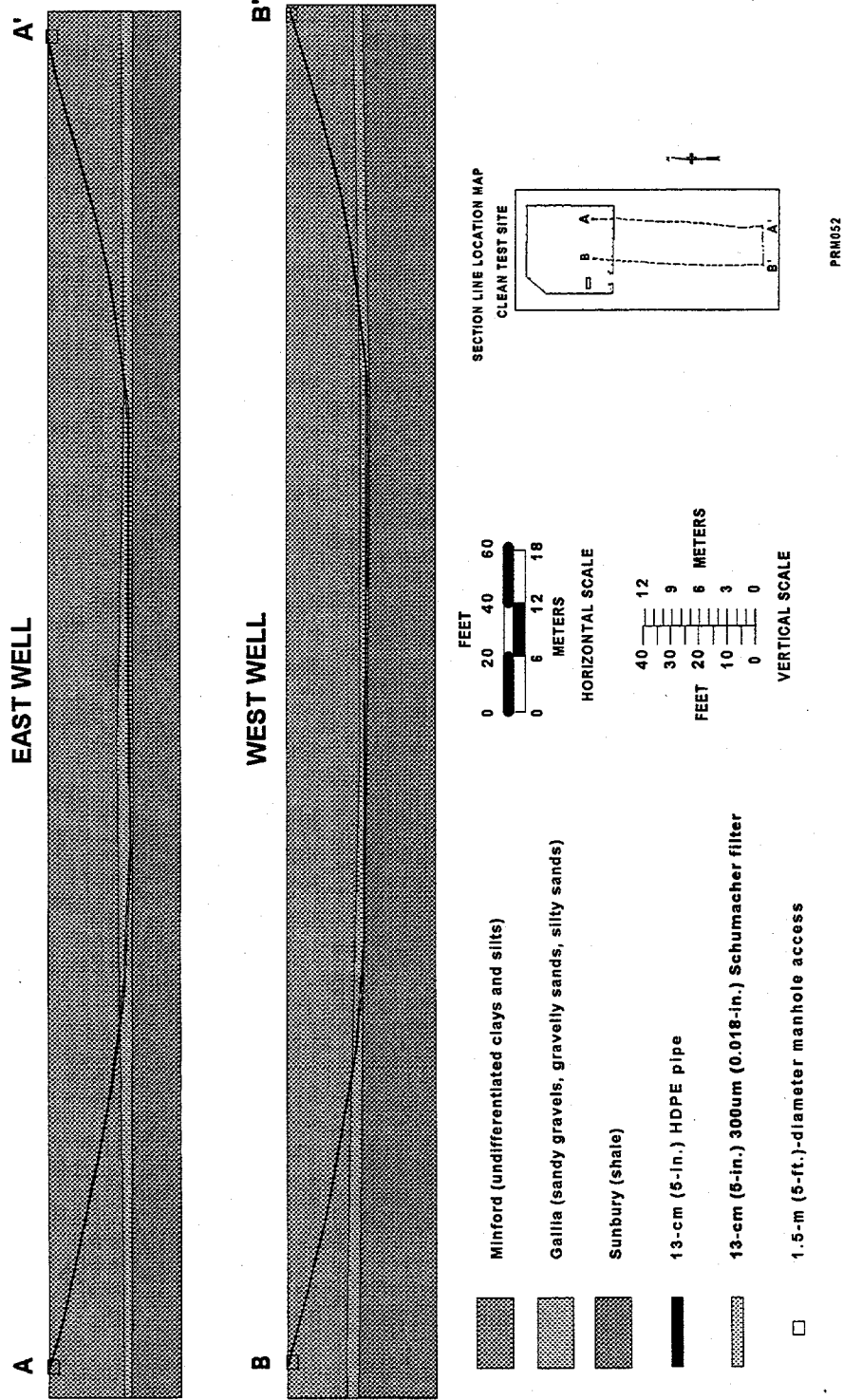


Fig. 3.2. Cross sections of the horizontal wells.

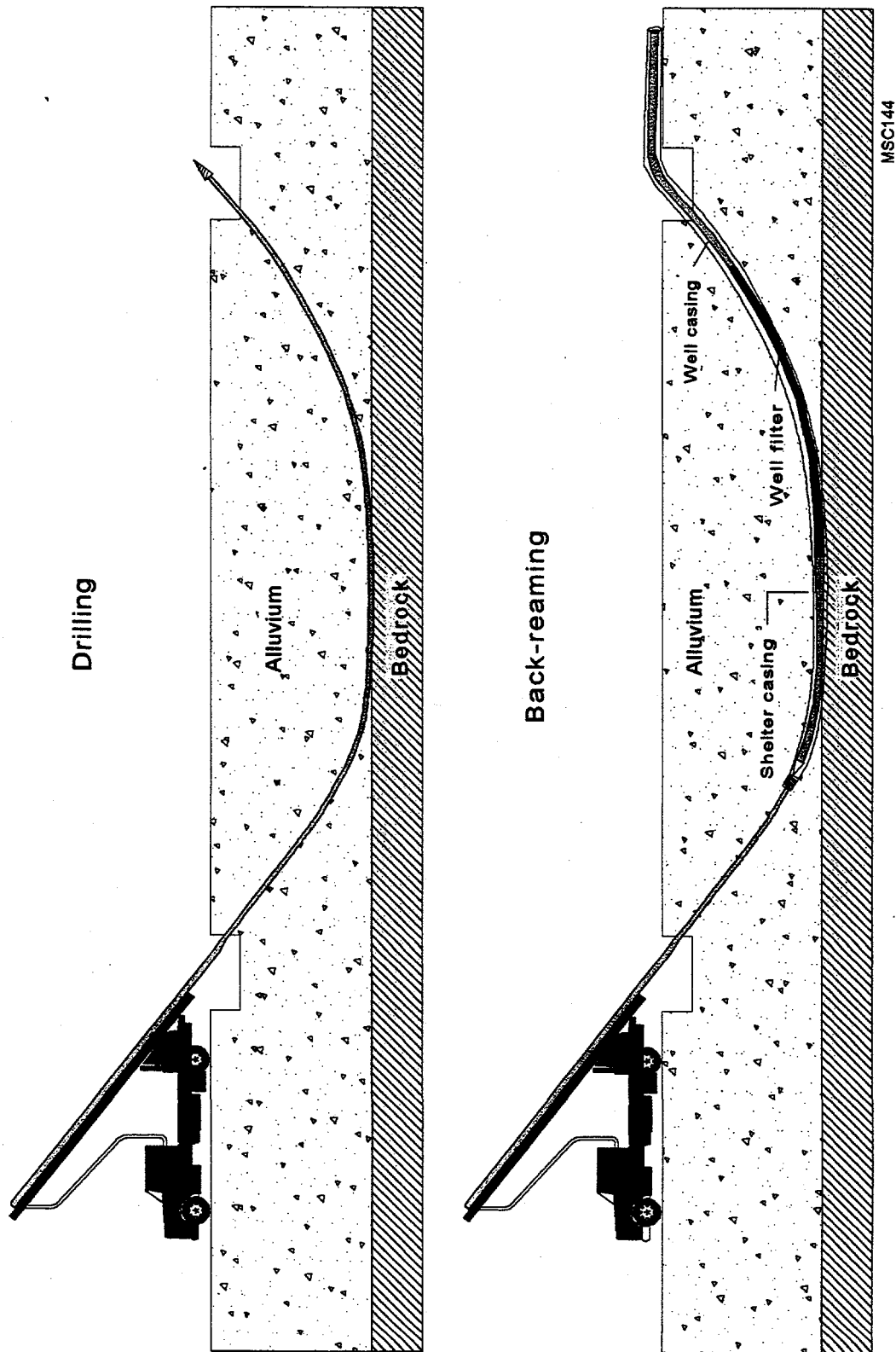


Fig. 3.3. Conceptual illustration of horizontal well drilling and installation.

Drilling fluids, both water and drilling mud, were used to keep the borehole open during both drilling and installation of the shelter casing. Soil cuttings that were generated during drilling were handled according to PORTS waste management protocol under the direction of the PORTS construction engineer (CE). Because the CTS is an uncontaminated site, the cuttings were spread neatly around the drilling locations.

The axes of the horizontal wells are approximately 30 m (100 ft) apart and extend south of the fenced area of the CTS with an orientation that is approximately north-south (Fig. 3.1). These well locations were chosen out of convenience in parallel with the topographic contours of the area (Fig. 2.3). This orientation places the well heads in a fairly level area, which kept the drilling depth as constant as possible. The bedrock surface in this area slopes gently to the southeast (Fig. 2.4). An ORNL/ETS geologist worked closely with drilling personnel to direct the drilling depth and ensure that the wells were installed at the base of the Gallia. An ORNL/ETS health and safety officer (HSO) conducted health and safety meetings with the field crew at the start of each work day and provided health and safety oversight during field work.

### 3.1 Well Installation

Preparation for the drilling activities was conducted on the first day of field work. The Mears crew of seven and FlowTex crew of three mobilized equipment to the site and attended a tailgate health and safety meeting conducted by the ORNL HSO. Afterwards, ORNL personnel set up construction zones, and Mears personnel attended a health and safety orientation for the PORTS facility. After the orientation, PORTS health and safety and health physics representatives inspected the drilling rig and support equipment. Mears personnel set up the drilling equipment at the south end of the eastern horizontal well.

Two of the Mears workers heat welded the blank sections of 13-cm (5-in.) HDPE pipe. Four blank sections were constructed, each 37-m (120-ft) long, by welding together three pieces of 12-m (40-ft)-long pipe. The heat welding was performed by lining up the ends of two pieces of pipe, squaring them off with a cutting tool, touching the ends to a heating iron until soft, and pressing the ends together at about 80 psi until cool. Each weld took approximately 30 min to complete, with all eight welds for the four sections of blank pipe completed during a 4-h period.

FlowTex personnel surveyed the ground surface along the drilling line for the east horizontal well and set up the navigation equipment for drilling. Navigation was conducted using a geomagnetic field induced by an electric cable that was laid in a loop around the length of the drilling line. The down-hole navigation assembly was attached behind the drill bit and consisted of a 9-m (30-ft) point of stainless-steel, 10-cm (4-in.)-diameter pipe that contained an inclinometer and magnetic survey tool.

Drilling of the eastern horizontal well began on the second day of field work. Mears personnel used a fire hose to fill the 11,355-L (3,000-gal) water tank on the support truck. This water was used to aid drilling operations. Four of the Mears personnel worked at the drilling rig: a driller, a crane operator, and two helpers to assist with the drill pipe. Two welders from Mears butt-fused together the porous filter for the eastern well. The filter was

allowed to cure overnight before installation of the well materials. The Mears supervisor coordinated the drilling effort. FlowTex personnel included the project director, drilling supervisor, and navigation specialist. A backhoe operator from PORTS provided support to the drilling by digging the entrance hole and mud pits, removing excess mud from the pits, and maneuvering the well materials. The start pit and cuttings pit were each approximately 1.8 m by 1.5 m (6 ft by 5 ft) and 1.2 m (4 ft) deep.

The pilot hole was drilled with a 22-cm (8.75-in.)-diameter tricone bit. The down-hole navigation assembly was attached behind the drill bit. A tricone bit normally has a jet associated with each cone. Only one of the three mud jets on the bit was used during drilling to optimize vertical drilling accuracy. Adjustment of the drilling direction was accomplished by plugging two of the jets and then rotating the bit and cone with the remaining jet in the desired direction of borehole advancement. Initial drilling was accomplished using water as the drilling fluid. Approximately 4 h of drilling was necessary to reach the base of the Gallia at 9.1 m (30 ft) vertical depth [directional drilling length of 67 m (220 ft)]. At this point, the use of a biodegradable drilling mud began, and drilling proceeded horizontally along the base of the Gallia. The lateral location of the drill bit was approximately 1.8 m (6 ft) east of the desired location; the lateral direction was corrected as the horizontal drilling proceeded. (The lateral drilling accuracy could have been improved by using all three jets, but the vertical drilling accuracy would not have been as good as with a single jet.)

The horizontal section of the pilot hole was drilled 15 cm (6 in.) above bedrock, so that when the shelter casing was installed with a larger diameter backreamer, the borehole from the backreamer would skim the bedrock surface. This would place the well materials along the bedrock surface when the shelter casing was removed.

The drilling mud was pumped at a rate of approximately 473 L/min (125 gal/min) with approximately 1.2 kg gel/m<sup>3</sup> (2.1 lb gel/yd<sup>3</sup>) water. During the first 6 h of drilling, approximately 3785 L (1000 gal) of water was lost to the formation. The remaining water returned to the start pit and was run through a mud shaker and reused. The pumping rate was not high enough to allow good gravel returns to the surface. Returns from the Gallia were primarily fine- to medium-grained sands and associated fines (silts and clays). The slower pumping rate was used to provide better control over the lateral position of the borehole. Additionally, the drilling mud weight and viscosity were kept as low as possible to minimize the buildup of a filter cake on the borehole (a higher viscosity drilling mud could carry gravel to the surface with the lower pumping rate). Along the horizontal section, the cuttings in the drilling mud return were approximately 30% more than the borehole volume. This indicates that some washout (removal of formation materials adjacent to the borehole) occurred during drilling. At a drilling length of 85 m (280 ft), circulation was lost. The drilling mud density was increased to 3 kg/m<sup>3</sup> (5.1 lb/yd<sup>3</sup>) to gain back circulation, and circulation of the drilling mud resumed.

At a drilling length of 98 m (320 ft), the drill bit was angled back toward ground surface. Lateral navigation of the drilling bit was difficult while angling up through the Gallia because as the bit angled up, it tended to veer toward the east, following the dip of the Gallia. The borehole was advanced into the Minford at a drilling length of approximately 102 m (335 ft).

Drilling was completed for the day at a drilling length of approximately 119 m (390 ft). A total of approximately 15,140 L (4000 gal) of water were used during drilling for the day.

Installation of the eastern horizontal well was completed on the third day of field work. The remaining 24 m (80 ft) of the pilot hole were drilled in approximately 2 h. The exit hole was approximately 1 m (3 ft) west of the planned location. The drill bit and navigation tool were removed from the drill string at the exit hole and were replaced with a 30-cm (12-in.)-diameter backreamer.

The heat welders butt-fused together 12 lengths of 20-cm (8-in.)-diameter by 12-m (40-ft)-long HDPE shelter casing. Each weld took approximately 20 min to complete, and the entire job of welding together the 146-m (480-ft)-long shelter casing took about 4 h to complete. The process of butt-fusing the lengths of HDPE leaves a bead inside the weld that is approximately one-half the wall thickness in height. Normally, an electric snake with a cutting tool is used to cut away the bead inside of the shelter casing. This allows the use of a smaller diameter shelter casing and, hence, a smaller diameter borehole. An electric snake was not available for this project. A 20-cm (8-in.)-diameter shelter casing was selected to allow insertion of the well materials inside the shelter casing without trimming away the bead.

The welders butt-fused a section of 37-m (120-ft)-long, 13-cm (5-in.)-diameter HDPE pipe onto each end of the porous filter, and a line of workers (all of the available drilling personnel) assisted by inserting the completed string of well materials into the shelter casing. A small bulldozer dragged the shelter casing (with the housed well materials) into place behind the backreamer. A swivel was attached to the backreamer, and the shelter casing and well materials were attached to the swivel.

The backreamer was pulled back down the exit hole to the entrance hole while pulling the shelter casing into place. A mud pit [approximately 1.8 m by 3 m by 1.2 m (6 ft by 10 ft by 4 ft) deep] was installed at the exit hole to collect cutting returns from the exit hole during backreaming. A sump pump and hose were used to cycle the drilling mud back to the drilling rig, through the mud shaker, and back into the drill stem. Backreaming was accomplished by pulling and rotating the backreamer with a pump rate of 473 L/min (125 gal/min). Backreaming through the Minford (the slanted section of the borehole) proceeded at a rate of approximately 1 m/min (3 ft/min). Backreaming through the Gallia along the horizontal section of the borehole was at a slower rate. Return samples collected during backreaming showed a combination of Gallia gravel and Sunbury shale. This indicated the backreamer was running along the surface of the Sunbury, as desired. Installation of the 146-m (480-ft)-long shelter casing was completed in approximately 5.5 h. It is notable that there were no mud blowouts during drilling and installation of the eastern horizontal well. The total volume of drilling spoils produced during drilling and installation of the eastern well was approximately 20 m<sup>3</sup> (720 ft<sup>3</sup>).

The south end of the well materials remained attached to the last piece of drilling rod (held to the rig) with a cap. A cover was placed over the north end of the well materials. The bulldozer dragged the shelter casing back out of the borehole, leaving the well materials in place. The entire shelter casing was removed in one piece in approximately 5 min. The

shelter casing was set aside for reuse during installation of the western horizontal well. For protections, plastic covers were placed over the ends of the eastern horizontal well.

During the morning of the fourth day of field work, the drilling equipment was moved 30 m (100 ft) west to the south end of the western horizontal well. Equipment breakdown and setup took approximately 4 h to complete. As with the eastern well, drilling of the western well proceeded from the south end to the north.

Drilling began with three jets on the drill bit in an attempt to improve lateral accuracy. After 1 h of drilling, circulation was lost, and mud and water bubbled to the ground surface approximately 12 m (40 ft) north of the mud pit. The drill bit was changed to one with a single jet for better vertical navigation. Drilling mud was pumped at a rate of 379 L/min (100 gal/min) and a density of 2.5 kg/m<sup>3</sup> (4.2 lb/yd<sup>3</sup>) to regain circulation. FlowTex noted that vertical accuracy could be controlled better by using a smaller diameter drill pipe commonly used in Europe. Additionally, penetration rates are higher with smaller-diameter drill pipe, and equivalent vertical control can be maintained.

After 5 h of drilling, the bit was angled along the base of the Gallia and horizontal drilling began. The cuttings returned to the surface contained approximately 90% Gallia sand and 10% Sunbury shale, indicating that drilling was proceeding along the contact of the Gallia and Sunbury, as desired. A total drilling length of approximately 76 m (250 ft) was completed for the day.

Installation of the western horizontal well was completed on the fifth day of field work. Approximately 67 m (220 ft) of drilling were necessary to complete the horizontal portion of the pilot borehole and angle back to ground surface. This was completed in 5 h. The exit hole was 1.2 m (4 ft) east of the planned location. As with the eastern well, a recirculation pit was constructed at the exit hole of the western well, the drilling subassembly was removed and replaced with a backreamer, and the well materials housed inside of the shelter casing were attached to the backreamer.

Backreaming and installation of the shelter casing took 4.5 h. During backreaming, water blew out of a borehole that had been drilled previously during characterization of the site geology. A small pit was dug at the blowout location to recover the drilling fluid [approximately 5678 L (1500 gal)] and pump it back to the mud pit at the drilling rig. After backreaming was completed, the shelter casing was removed in a single piece, and the ends of the well were covered with plastic for protection. The total volume of drilling spoils produced during drilling and installation of the western well was approximately 20 m<sup>3</sup> (720 ft<sup>3</sup>).

On the sixth day of field work, Mears personnel demobilized the drilling equipment from the site. This task was completed in 5 h. FlowTex and ORNL personnel marked the path of the horizontal wells on the ground surface. The backhoe operator from PORTS filled in the remaining mud pits and graded the disturbed areas at both well locations.

Table 3.1 summarizes the production rates and total time requirements for drilling and installation of the horizontal wells.

### 3.2 Surface Completions

At the surface, a recessed manhole was installed at each end of each well such that the blank casings from the horizontal wells terminate in the manholes (a total of four manholes; Fig. 3.1). A backhoe operator from PORTS installed two horizontal sections of 10-cm (4-in.)-ID casing between the wells. These two sections of casing terminate inside the manholes and were used to plumb the two wells together.

The manholes provide a clean, dry area for the plumbing and other equipment at the ends of the horizontal wells. The manholes are 1.2 m (4 ft) deep and are constructed of 1.5-m (5-ft)-diameter steel culvert pipe. The floor of the manholes is lined with gravel. A sump bucket was installed in the floor of each manhole so that a submersible pump can be used to remove excess water. Insulated weather-tight lids were installed over the manholes to prevent infiltration by rainwater and surface-water runoff. Four bumper posts were installed around each manhole to protect against vehicle traffic.

The surface locations of the horizontal wells were surveyed with a horizontal accuracy of  $\pm 15$  cm ( $\pm 0.5$  ft) and a vertical accuracy of  $\pm 0.3$  cm ( $\pm 0.01$  ft). To ensure the required accuracy, the survey was looped and closed. Each well is identified by stamped numbers on the side of the protective casing. The horizontal wells are numbered CTS-HW-1 (the east well in Fig. 3.1) and CTS-HW-2 (the west well in Fig. 3.1), in the order of their installation. Figure 3.2 shows surveyed cross sections of the wells based on navigation data collected during drilling.

### 3.3 Initial Well Development

FlowTex recommended that the drilling mud be allowed to break down for at least 10 days before beginning well development. FlowTex also recommended that the horizontal wells be developed by placing a pump at each end of the porous filter and pumping until the extracted water became as clear as practical.

The horizontal wells were developed by ORNL/ETS during early November 1994, following a 10-day waiting period. One generator was used for well development, so it was possible to pump from only one end of each well rather than from both ends. Each end of each well was developed with an initial pumping rate of 15 L/min (4.0 gal/min). The pumping rate was increased as time progressed and near the end of development averaged 45 to 57 L/min (12.0 to 15.0 gal/min). Development water from each well end was initially cloudy, but cleared up after about 1 h of pumping. Pumping rates, turbidity, pH, temperature, and specific conductance were monitored and recorded during the development process. The water generated during development was routed to a nearby drainage swale.

**Table 3.1 Task summary for drilling and installation of the horizontal wells**

Activity	Production rate	Total time
Casing and filter assembly	0.5 h/weld	<p>4 h to construct four sections of blank casing (two welds/section). Each section was 120 ft long.</p> <p>19 h to construct two porous well filters (19 welds/filter). Each filter was 230 ft long.</p> <p>4 h to construct the shelter casing (11 welds/casing). The shelter casing was 480 ft long.</p>
Drilling (eastern well)	39 ft/h (average rate)	12 h to drill 470 ft
Backreaming with simultaneous well installation (eastern well)	85.5 ft/h (average rate)	5.5 h to backream 470 ft
Shelter casing removal	96 ft/min	5 min to extract 480 ft shelter casing (same for eastern and western wells)
Drilling (western well)	36 ft/h (average rate)	13 h to drill 470 ft
Backreaming with simultaneous well installation (western well)	104 ft/h (average rate)	4.5 h to backream 470 ft



During development, approximately 10,100 L (2,670 gal) were removed from the north end of the west well, 69,300 L (18,320 gal) from the south end of the west well, 8100 L (2,140 gal) from the north end of the east well, and 18,000 L (4,770 gal) from the south end of the east well. A very large volume of water was extracted from the south end of the west well to verify that the water quality of the development water had stabilized. As shown in Table 3.2, there was very little difference in water quality characteristics in development water from the west and east wells, so it can be concluded that the smaller volume of water extracted from the east well was sufficient for stabilization of the water quality parameters.

As discussed in Sect. 8 of this report, extended operation of the horizontal well recirculation system revealed that this method of well development (pumping until the water became clear) was inadequate. The horizontal wells were later developed successfully by water jetting and overpumping (Sect. 8).

**Table 3.2 Water quality of development water from the horizontal wells**

	West Well	East Well
<b>Temperature, °C</b>	13.8	13.9
<b>Specific Conductance, mV/cm</b>	930	1520
<b>pH</b>	5.7	5.0
<b>Turbidity, NTU</b>	2.7	2.3

#### 4. Piezometer Installation and Development

ORNL/ETS directed the installation of 22 piezometers at the CTS during November and December 1994. Figure 3.1 shows the piezometer locations. The piezometers were constructed of 5-cm (2-in.)-ID polyvinyl chloride (PVC) with variable screen lengths [typically 0.9 to 1.2 m (3 to 4 ft)]. Nineteen of the piezometers were installed in the Gallia with depths ranging from 7.9 to 9.1 m (26 to 30 ft) bgs (Table 4.1). Three of the piezometers were installed in the Minford at a depth of approximately 6 m (20 ft) bgs (PZ-10, PZ-12, and

**Table 4.1. Piezometer survey data and screened intervals**

Piezom- eter number	Top of casing, ft amsl	Ground eleva- tion, ft amsl	Total depth, ft bgs	Screen length, ft	Screened interval, ft bgs	Bedrock elevation, ft amsl
PZ-01	661.83	660.35	28.5	3.0	22.8 to 25.8	635.35
PZ-02	661.82	660.21	27.0	4.0	22.0 to 26.0	634.21
PZ-03	661.16	659.62	25.5	3.0	21.7 to 24.7	634.62
PZ-04	662.51	660.93	25.7	2.5	23.2 to 25.7	---
PZ-05	664.64	663.10	29.0	4.0	25.0 to 29.0	636.14
PZ-06	663.89	662.26	29.0	3.5	24.5 to 28.0	635.89
PZ-07	658.60	657.09	29.0	4.0	19.5 to 23.5	634.60
PZ-08	659.19	657.73	29.0	4.5	20.0 to 24.5	634.94
PZ-09	661.93	660.44	27.5	4.0	23.5 to 27.5	633.19
PZ-10	662.08	660.44	20.0	7.0	12.0 to 19.0	---
PZ-11	663.82	662.25	29.5	4.0	24.5 to 28.5	635.32
PZ-12	663.59	662.25	20.0	10.0	9.0 to 19.0	---
PZ-13	664.65	663.08	29.5	4.0	25.5 to 29.5	633.83
PZ-14	664.81	663.08	20.0	10.0	9.0 to 19.0	---
PZ-15	662.66	661.39	29.5	3.0	24.0 to 27.0	634.39
PZ-16	663.65	662.28	29.5	4.5	24.0 to 28.5	633.78
PZ-17	663.99	662.45	29.5	4.0	25.5 to 29.5	632.95
PZ-18	662.21	660.79	29.5	4.0	23.5 to 27.5	633.29
PZ-19	664.15	662.66	29.0	5.0	24.5 to 29.0	634.16
PZ-20	664.67	663.25	29.5	4.0	25.5 to 29.5	633.75
PZ-21	663.85	662.41	29.0	4.0	25.0 to 29.0	633.66
PZ-22	663.49	662.07	29.5	3.0	24.5 to 27.5	634.57

amsl = above mean sea level  
bgs = below ground surface

PZ-14). The piezometers were used to assess the hydraulic influence of the horizontal wells on the surrounding groundwater flow system.

A CME-55 all-terrain drilling rig, utilizing 21-cm (8.25-in.)-OD by 11-cm (4.25-in.)-ID augers, and standard well construction practices were used to install the piezometers. Auger cuttings generated during drilling were handled in accordance with PORTS waste management protocol under the direction of the PORTS CE. Because the CTS is an uncontaminated site, the auger cuttings were spread neatly around the drilling locations.

A detailed geologic log of each borehole was prepared by collecting and logging soil samples with a 1.5-m (5-ft)-long continuous sampler. The sampler was run a few centimeters ahead of the lead auger to obtain undisturbed soil samples. Appendix C provides the geologic logs and piezometer construction diagrams.

The piezometers were constructed with PVC screens and are screened across the entire thickness of the Gallia member, with the well points resting on Sunbury shale in most cases. Screen lengths vary depending on the thickness of the Gallia. In most cases, the screened interval is 0.9 to 1.2 m (3 to 4 ft) long (Table 4.1). PVC riser casing extends from the top of the screened interval to approximately 76 cm (30 in.) above ground surface. All screen-to-casing and casing-to-casing couplings are flush-threaded. No glues or lubricants were used. The annular space was filled with a 10/20 grade silica sand pack. To minimize influence from the overlying Minford silt, the sand packs were extended a minimum distance above the screened interval. In most cases, the top of the sand pack was 15 cm (6 in.) above the top of the screened interval. A bentonite seal was placed on top of the sand pack to within 0.9 m (3 ft) of ground surface using 1-cm (3/8-in.) bentonite chips. From 0.9 m (3 ft) bgs to the surface, concrete was used to install locking protective casings over the piezometers. Four bumper posts were then installed around each piezometer.

Upon completion, the piezometers were developed by ORNL personnel. Due to the low flow rates encountered, the piezometers were developed with a water jetting tool. Development continued until the water removed from the piezometers was as clear as practical. Development times for each piezometer ranged from 2 to 4 h. Because groundwater at the CTS is uncontaminated, the water that was generated during development was routed to nearby drainage swales.

The locations of the piezometers were surveyed with a horizontal accuracy of  $\pm 15$  cm ( $\pm 0.5$  ft) and a vertical accuracy of  $\pm 0.3$  cm ( $\pm 0.01$  ft). To ensure the required accuracy, the survey was looped and closed. The piezometers are locked and keyed alike with locks supplied by PORTS. Each piezometer is identified by stamped numbers on the side of the protective casing. The piezometers are numbered as: CTS-PZ-01, CTS-PZ-02, etc.

After the network of piezometers was installed and developed, water levels in the piezometers were allowed to stabilize for at least 24 h. Following stabilization, water levels were measured to allow the construction of a baseline potentiometric map shown as Fig. 4.1. Table 4.1 provides land-surface elevations for the control points used to construct the map. Water-level measurements from all of the piezometers completed in the Gallia were measured within as short a time period as possible (approximately 1 h) to provide a view of horizontal flow directions and gradients at the CTS. Baseline water levels in the three piezometers completed in the Minford were also measured and recorded during this time period.

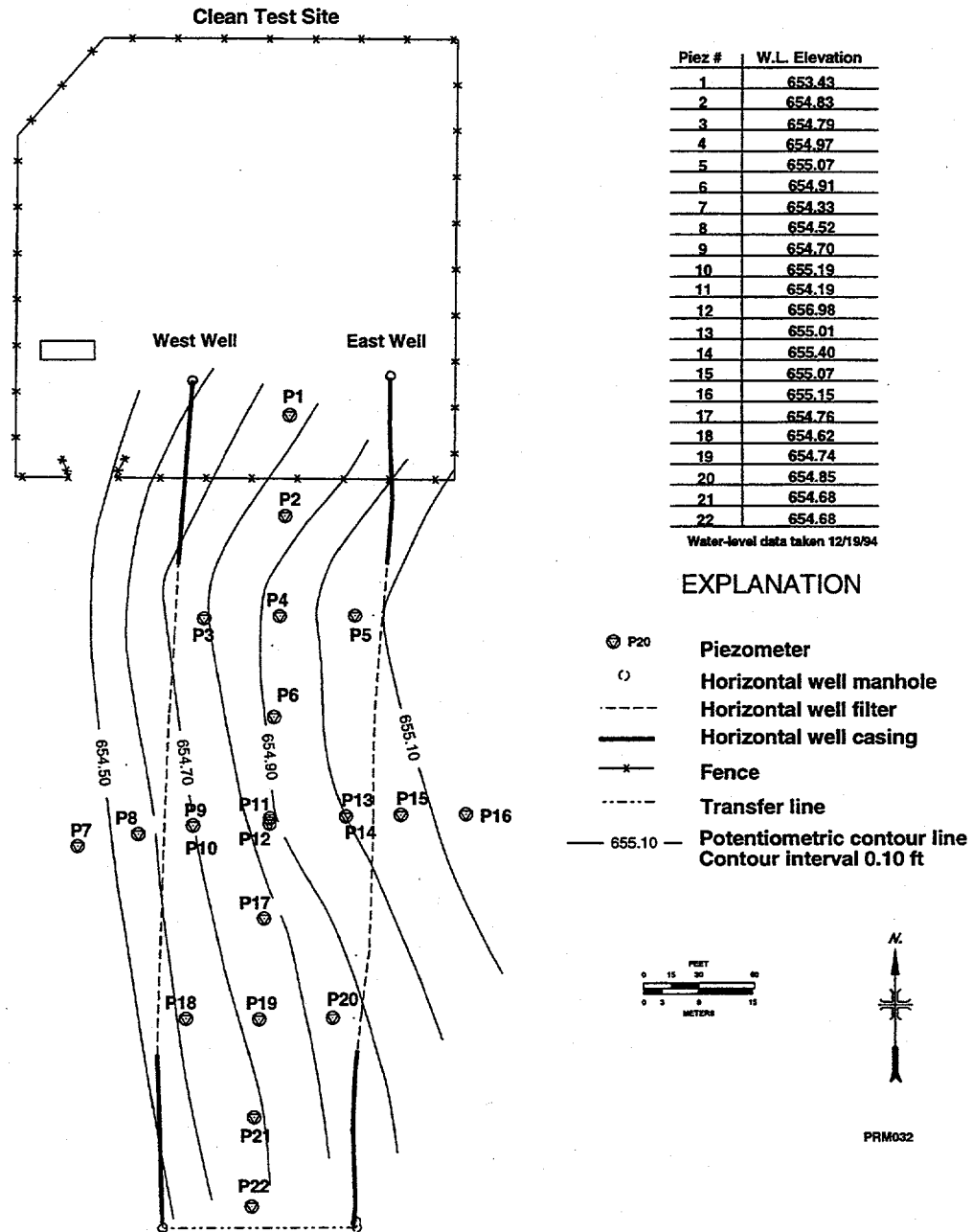


Fig. 4.1. Baseline potentiometric surface map.

## 5. Hydraulic Evaluation of the Horizontal Well Recirculation System

### 5.1 Introduction

This section discusses tests conducted at the CTS to evaluate aquifer characteristics and the hydraulic performance of the horizontal well recirculation system. The goals of these tests were to determine the efficiency of the horizontal wells and the impact of subsurface heterogeneities. Single-well tests were conducted on 22 piezometers to measure the hydraulic conductivity of the Minford and Gallia members. The results of these tests were compared to estimate the degree and distribution of heterogeneity in the region surrounding the horizontal wells.

Three pumping tests were conducted on the horizontal wells. Each horizontal well was pumped independently to measure yield, area of influence, and hydraulic characteristics of the Gallia. The final test was a dual-well recirculation test that consisted of pumping one horizontal well and injecting into the other.

### 5.2 Theoretical Development

Horizontal wells have been used by the oil industry for years in an attempt to increase production from depleted or low permeability reservoirs (Gilman and Jargon 1992; PEI 1992). Enhanced recovery using horizontal wells has been reported in the literature, with the highest degree of success seen in fractured systems. According to Gilman and Jargon (1992), horizontal wells can be expected to provide both higher rates of recovery and significant incremental recovery in lower permeability formations and essentially accelerated recovery in high permeability reservoirs with marginal increases in ultimate recovery. Expanding horizontal wells to the environmental field for the recovery of groundwater contamination has been discussed by Kaback et al. (1989), and Langseth (1990).

The hydraulic performance of horizontal wells has been evaluated analytically by Ferris (1950), Hantush and Papadopoulos (1962), Lohman (1979), Suzuki and Nanba (1990), and Edwards (1991). Horizontal wells have been numerically analyzed by Speake et al. (1992) and Langseth (1990). The impact of formation damage on the efficiency of horizontal wells is discussed by Renard et al. (1990) and Suzuki and Nanba (1990).

To calculate the hydraulic properties of the aquifer at the CTS, several analyses were considered. The most in-depth numerical analysis of horizontal wells is provided by Hantush and Papadopoulos (1962). Solutions for flow to a horizontal well are obtained by treating the well as a line sink. If a horizontal well is operated in an infinite confined aquifer of uniform thickness ( $b$ ), and of uniform transmissivity ( $T$ ) and storativity ( $S$ ), the drawdown ( $s_r$ ) induced by the well lateral is given by the following equations:

$$\begin{aligned}
 s_i = & \frac{Q}{4\pi T} \left( \frac{\alpha}{l} W \left( \frac{\alpha^2 + \beta^2}{4vt} \right) - \frac{\delta}{l} W \left( \frac{\delta^2 + \beta^2}{4vt} \right) \right. \\
 & + \frac{2}{\sqrt{4vt}} \left[ L_0 \left( \frac{\alpha}{\sqrt{4vt}}, \frac{\beta}{\sqrt{4vt}} \right) - L_0 \left( \frac{\delta}{\sqrt{4vt}}, \frac{\beta}{\sqrt{4vt}} \right) \right] \exp \left( -\frac{\beta^2}{4vt} \right) \\
 & \left. + \frac{2}{\sqrt{4vt}} \sum_1 \left[ F \left( \frac{\alpha}{\sqrt{4vt}}, \frac{\beta}{\sqrt{4vt}}, \frac{n\pi}{b} \right) - F \left( \frac{\delta}{\sqrt{4vt}}, \frac{\beta}{\sqrt{4vt}}, \frac{n\pi}{b} \right) \right] \cos \frac{n\pi z}{b} \cos \frac{n\pi z}{b} \right)
 \end{aligned} \quad (1)$$

$$v = \frac{T}{S}$$

$$\alpha = r \cos (\theta - \theta_i) - r_c \quad (2)$$

$$\beta = r \sin (\theta - \theta_i)$$

$$\delta = r \cos (\theta - \theta_i) - l^1$$

$$\begin{aligned}
 Lo(u, \pm w) &= \int_0^u \frac{\beta^2 e^{-\beta^2}}{w^2 + \beta^2} d\beta \\
 r &= \sqrt{x^2 - y^2}
 \end{aligned} \quad (3)$$

$$l^1 = r_c + l_1$$

$$F(u, \pm x, y) = -F(-\mu \pm x, y) = \int_0^u W(x^2 + \beta^2, y\sqrt{x^2 + \beta^2}) \quad (4)$$

where

- $l$  = length of well,
- $K$  = hydraulic conductivity,
- $t$  = time,

and  $W(x,y)$  is the well function for a leaky aquifer. The functions  $L_o(u,w)$  and  $F(u,x,y)$  can be tabulated for a practical range of parameters involved. To our knowledge, however, type curves based on Hantush and Papadopoulos (1962) solutions have not been developed. Consequently, their solutions could not be applied when analyzing pumping test data from the CTS. It was necessary to consider other solutions available in the literature.

Lohman (1979) reports a solution developed by Ferris (1950) for determining the decline in head at any distance from a drain (e.g., horizontal well) discharging water at a constant rate from a confined aquifer. The equation is based on the assumption that the aquifer is homogeneous, isotropic, semi-infinite, and the drain completely penetrates the aquifer. For horizontal wells, complete penetration is assumed to imply that the well is located at the base of the aquifer. The equation may be written as

$$T = \frac{Q^*x}{2s} \left[ \frac{e^{-u^2}}{u\sqrt{\pi}} - 1 + \frac{2}{\sqrt{\pi}} \int_0^{x/2\sqrt{Tt/S}} e^{-u^2} du \right] \quad (5)$$

$$u = x \sqrt{\frac{S}{4Tt}} \quad (6)$$

$$S = \frac{4Ttu^2}{x^2} \quad (7)$$

where

- $x$  = distance from drain or horizontal well to observation point,
- $Q^*$  = pumping rate per unit length of well,
- $S$  = storativity,

and where the bracket part of Eq. (5) may be written as  $D(u)$ , the drain function, to yield

$$T = \frac{Q^*x}{2s} D(u)_q \quad (8)$$

A type curve for this equation is presented in Lohman (1979).

Edwards (1991) presents an analytical solution for a horizontal well in an unconfined aquifer based on Darcy's law as

$$K = \frac{2Qx}{L(h_2^2 - h_1^2)} \quad (9)$$

where  $L$  equals the length of screen and  $h$  equals the height of the water at distances  $r_1$  and  $r_2$ . Adapting this solution for a confined aquifer by assuming  $h_2^2 - h_1^2 = (h_2 + h_1)(h_2 - h_1)$  and  $(h_2 + h_1) = 2b$ , then Eq. (9) becomes

$$K = \frac{Qx}{bL(h_2 - h_1)} \quad (10)$$

In Sect. 5.4, the methods developed by Ferris (1950) and Edwards (1991) are used to evaluate data from the horizontal well pumping tests and to calculate hydraulic properties of the Gallia member at the CTS.

### 5.3 Piezometer Hydraulic Tests

Bail and slug tests were conducted on 22 piezometers to measure the hydraulic conductivity of the Gallia and overlying Minford member. Variations in hydraulic conductivity were used to evaluate the heterogeneity of the system. Muck et al. (1996) presents test results from the individual piezometers. These test results are summarized below.

Hydraulic conductivity values for the Minford range from  $2 \times 10^{-5}$  to  $4 \times 10^{-5}$  cm/s (0.05 to 0.10 ft/d). These values are within the expected range for a silty-clay formation. The Gallia shows a large range in permeability values of  $7 \times 10^{-6}$  to  $6 \times 10^{-3}$  cm/s (0.02 to 18 ft/d). These values are typical for a silty clay to sandy formation. Large variations in hydraulic conductivity indicate that the Gallia exhibits a large degree of heterogeneity. Heterogeneity based on the hydraulic tests is supported by results of the geologic investigation that showed large variations in Gallia thickness and lithology across the site.

Figure 5.1 shows hydraulic conductivity values for the individual piezometers. The presence of zones or channels of higher permeability can be inferred from these results. Two higher permeability zones trend from PZ-05 to PZ-09 and from PZ-20 to PZ-09. Whether these individual channels are part of a historical meander in the Gallia member is only speculative based on the limited amount of information; however, it is clear that there are permeable zones or channels in the Gallia capable of transporting most of the groundwater in the vicinity of the CTS.



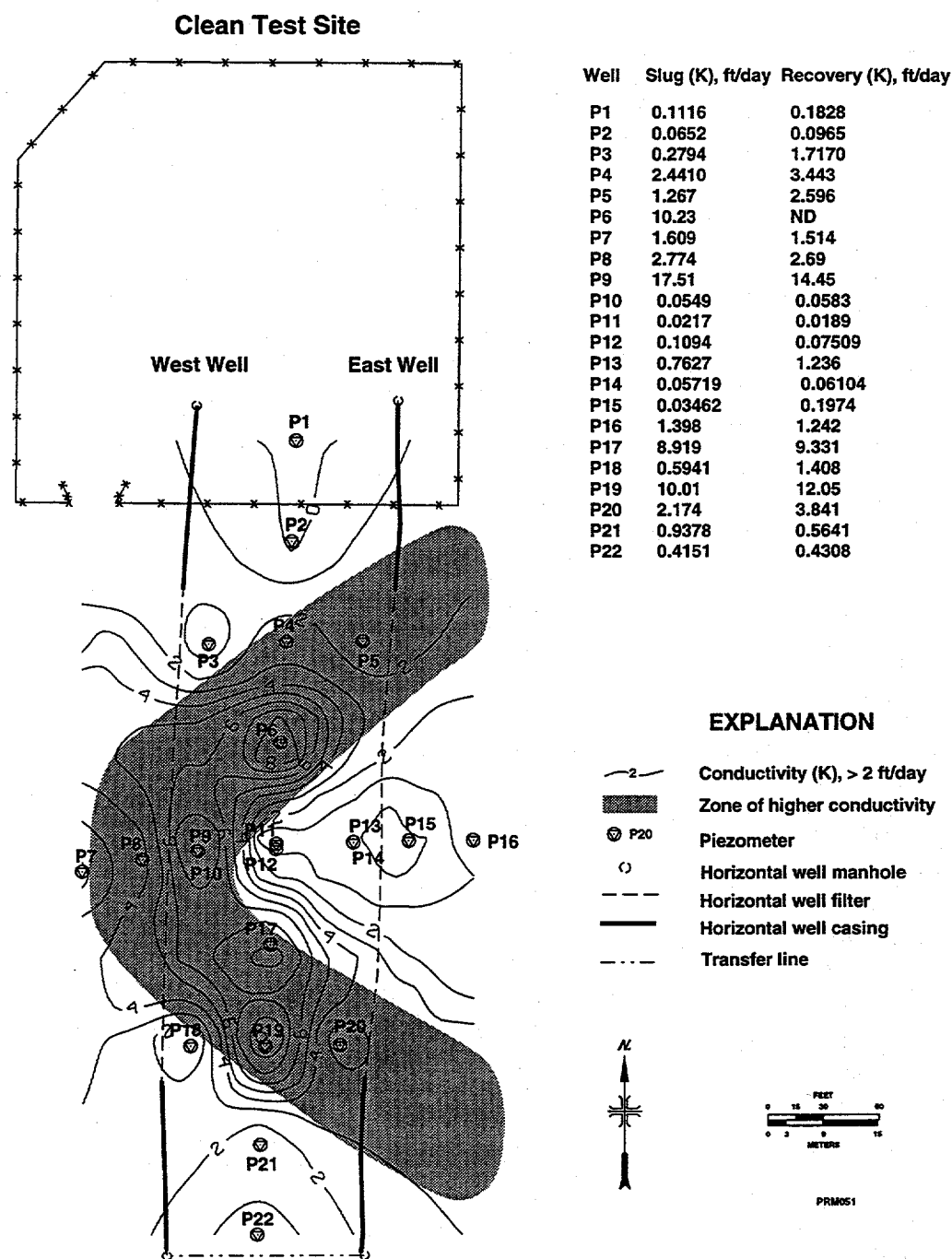


Fig. 5.1. Hydraulic conductivity values based on single-well tests and the distribution of K at the CTS.

## 5.4 Horizontal Well Pumping Tests

Each horizontal well pumping test was conducted by placing a 3-in. submersible pump at the base of the well next to the filter. A flow totalizer was connected to the discharge line to monitor pumping rates. Water from the single horizontal well tests was routed by fire hoses to a drainage ditch. Pumping rates were allowed to vary less than 2% during the individual pumping tests. For the recirculation tests, two pumping rates were tested, and each flow rate was held at a consistent level.

Water-levels were monitored using pressure transducers and water-level indicators. Seven piezometers were equipped with pressure transducers for continuous water-level measurements. Water levels in 22 piezometers were periodically measured by hand with a water-level indicator and were recorded in the field logbook. In addition, water levels in each end of the horizontal wells were periodically monitored during the tests. Data from the pressure transducers are presented in Appendices D, E, and F.

Pretests were conducted to determine the optimal pumping rate. The eastern horizontal well produced approximately 57 L/min (15 gal/min) for 4 h before going dry. A rate of 45 L/min (12 gal/min) was selected for both individual horizontal wells tests. The pumping rate was increased to 57 and 76 L/min (15 and 20 gal/min) for the dual-well horizontal recirculation tests.

A minimum pumping test of 24 h was conducted on each horizontal well. Conventional curve-matching analyses were performed in the field to ensure that the duration of the tests were sufficient to assess aquifer boundary conditions. The recirculation test was conducted for a longer period of time to assess different pumping rates and well efficiency. Based on the results of the pumping tests, it was possible to determine the yield of the individual horizontal wells, the recirculation rate, the extent of drawdown, and the influence of heterogeneities in the Gallia on the horizontal well recirculation system.

### 5.4.1 West Well Pumping Test

#### 5.4.1.1 Well Yield

The west horizontal well was pumped at a rate of 45 L/min (12 gal/min) for 25 h. At the end of the test, there were approximately 1.9 m (6.2 ft) of available drawdown in the horizontal well. To operate the well for an extended period of time, the pumping rate would need to be decreased to approximately 38 L/min (10 gal/min).

#### 5.4.1.2 Aquifer Response to Pumping

The area of influence for horizontal wells refers to the aquifer region affected by the pumping. For vertical wells, the radius of influence is commonly calculated to illustrate the boundary where groundwater will eventually be extracted by the well. Since horizontal wells are line sinks or sources, a radial term is not appropriate in describing the region of influence. Figure 5.2 is a contour plot of drawdown values in response to pumping the west horizontal

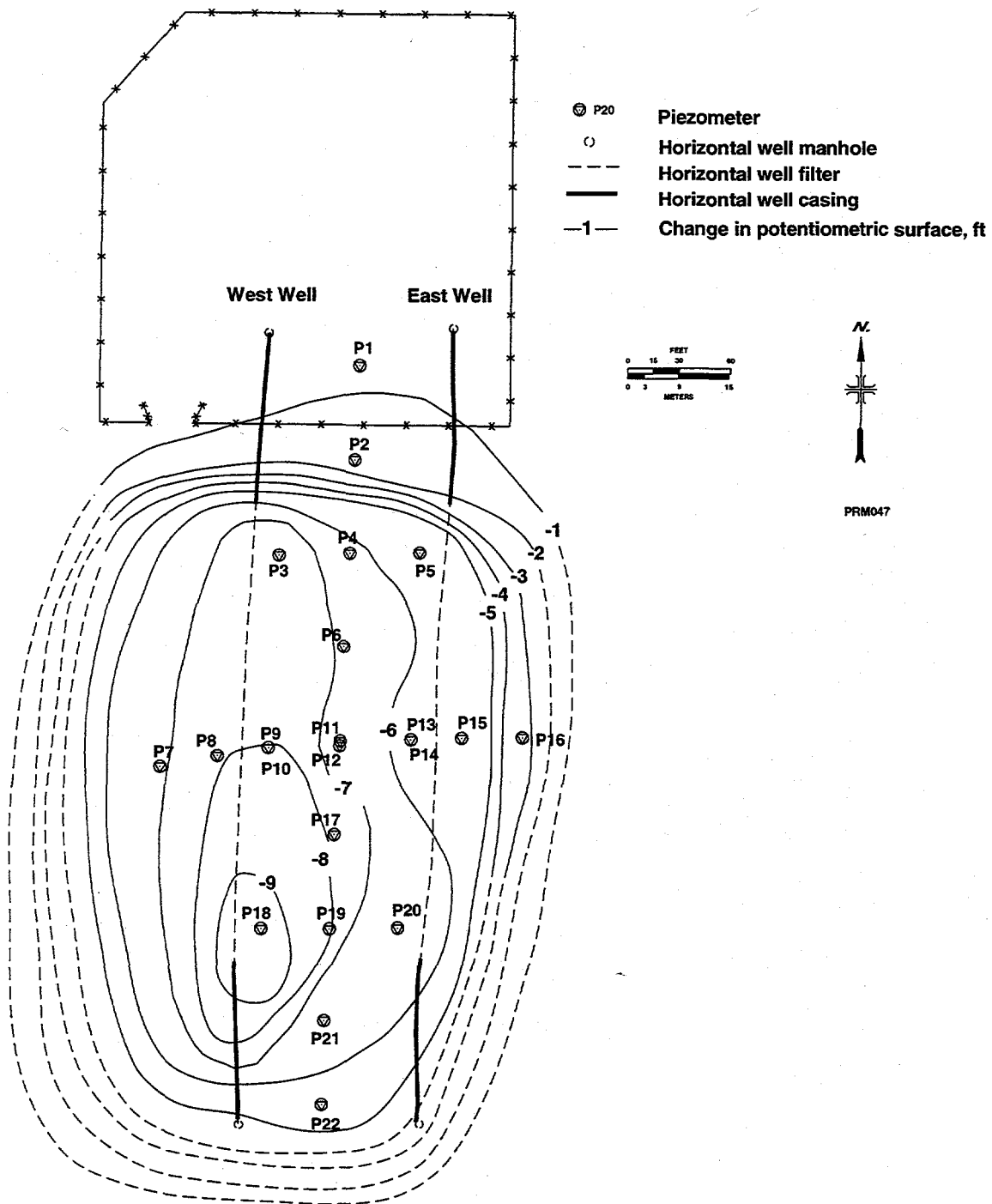


Fig. 5.2. Extent of drawdown in the Gallia resulting from pumping the west horizontal well for 24 h.

well. As noted earlier, drawdown in the Gallia will be controlled by the geometry of the horizontal wells and the hydrogeologic heterogeneity.

Individual drawdown curves for the west well pumping test are presented in Fig. 5.3. The main difference between the pumping test results for the east and west horizontal wells is the location of the maximum area of drawdown. For the west well pumping test, the southern portion of the well shows the maximum amount of drawdown. These results suggest that the permeability of the Gallia is relatively low in the southern portion of this well. This explanation is supported by the bail test data that indicate a zone of lower permeability in the area of piezometer PZ-18 (Fig. 5.1).

#### 5.4.1.3 Hydraulic Characteristics

Drawdown vs time plots for selected piezometers that were monitored using pressure transducers are presented in Appendix D. Conventional Theis curve analysis was conducted as part of the software plotting program. However, this analysis is based on a vertical well with radial horizontal flow conditions. Using the method for a line sink developed by Ferris (1950), transducer data from PZ-08 collected during the west well pumping test was compared to a type curve presented in Lohman (1979).

Figure 5.4 shows a logarithmic plot of  $D(u)$  vs  $u^2$  for water-level data collected from piezometer PZ-08 during the west well pumping test. As shown, a reasonable match to the type curve was obtained based on a homogeneous, isotropic, semi-infinite area extent system.

Similar results were obtained for curve matching analyses using data for other piezometers. These results indicated that no significant boundaries were encountered during the pumping test. A transmissivity of  $1.2 \text{ cm}^2/\text{s}$  ( $110 \text{ ft}^2/\text{d}$ ) and storativity value of 0.020 were calculated. Using an average Gallia thickness of 1.2 m (4 ft), a resulting hydraulic conductivity value of  $9.5 \times 10^{-3} \text{ cm/s}$  ( $27 \text{ ft/d}$ ) can be estimated based on the horizontal well pumping test. This value is substantially higher than that from the single-well tests. However, this is consistent with similar comparisons at other field sites that show pumping test conductivity values as much as an order of magnitude higher than those from single-well pumping tests (Kearl et al. 1988).

The analysis modified from Edwards (1991) yields a hydraulic conductivity value of  $1.3 \times 10^{-3} \text{ cm/s}$  ( $3.8 \text{ ft/d}$ ). This value is significantly lower than predicted by Ferris (1950) and may reflect hydraulic inefficiencies or clogging of the well filter resulting in lower than predicted water levels in the horizontal well. If Eq. (10) is integrated over the limits of  $x_1$  and  $x_2$  to incorporate two piezometers instead of one piezometer and the horizontal well, then the hydraulic conductivity increases to  $2.6 \times 10^{-2} \text{ cm/s}$  ( $75 \text{ ft/d}$ ).

## WEST WELL DRAWDOWNS

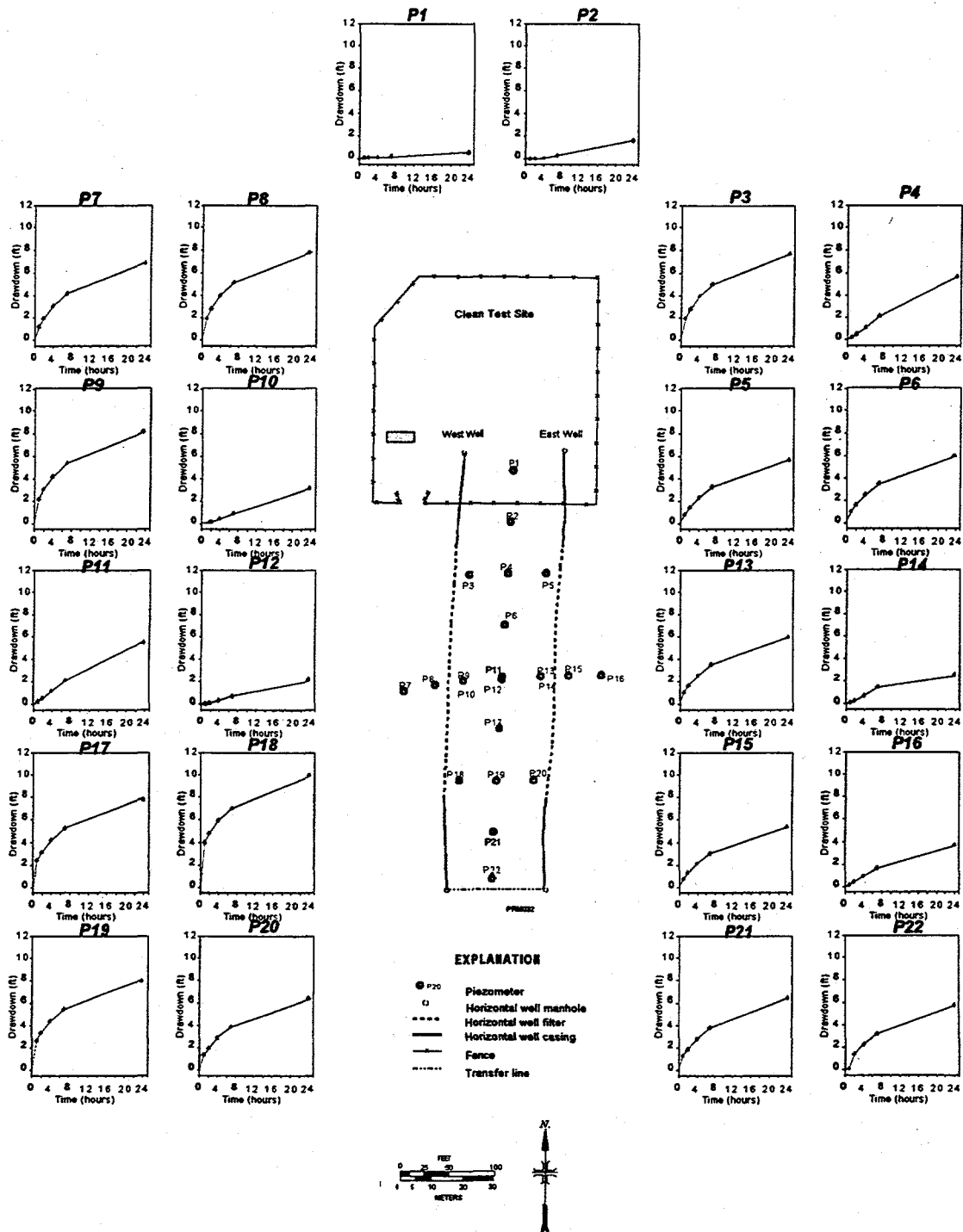


Fig. 5.3. Drawdown graphs for individual piezometers during the west well pumping test.

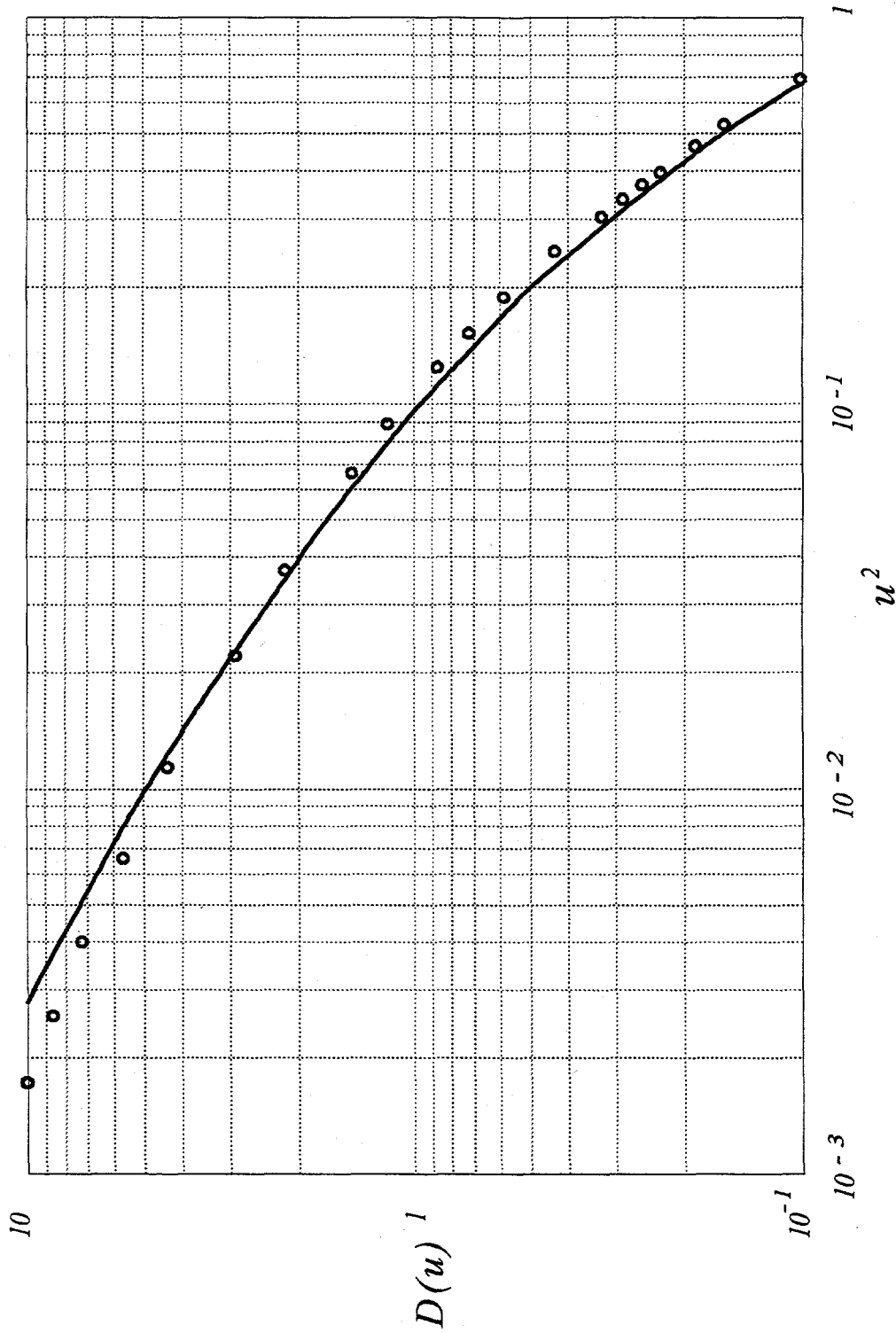


Fig. 5.4. Type curve for a line sink using PZ-08 drawdown data from the west well pumping test.

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These changes in calculated hydraulic conductivity resulting from whether the horizontal well or a second vertical well is used as an observation point indicate that the horizontal well was inefficient and was clogged during the pumping test. As discussed in Sect. 5.5, the west well filter continued to clog during extended operation, indicating that the initial well development method was inadequate. The west well was later developed successfully using a pressure-jetting method (Sect. 8). The higher conductivity calculated by Eq. (10) using two piezometers as compared to Eq. (5) also indicates that  $(h_2 + h_1) = 2b$  is a poor assumption for this system because of the thickness of the confined Gallia combined with the relatively large drawdowns induced by pumping.

#### 5.4.2 East Well Pumping Test

##### 5.4.2.1 Well Yield

The east horizontal well was pumped at a rate of 46.6 L/min (12.3 gal/min) for 26 h. At the end of the test, there were only approximately 0.6 m (2 ft) of available drawdown in the horizontal well. To operate the well for an extended period of time, the pumping rate would need to be decreased to a rate of approximately 38 L/min (10 gal/min).

##### 5.4.2.2 Aquifer Response to Pumping

Results similar to those of the west well pumping test were observed for the east well pumping test. Figure 5.5 illustrates drawdown for the individual piezometers in response to the east well pumping test. Variations in drawdown among the piezometers is a function of location with respect to the horizontal well that is being pumped and variations in permeability. As expected, as the distance from the pumping horizontal well increases, the amount of drawdown decreases. The impact of permeability variations is less clear. Minford piezometers (PZ-10, PZ-12, and PZ-14) show a significant decrease in the amount of drawdown compared to adjacent Gallia piezometers (PZ-09, PZ-11, and PZ-13). This is expected considering the large variations in permeability. It is important to note, however, that water from the Minford is being drawn into the Gallia.

Defining aquifer heterogeneity within the Gallia from the individual piezometer drawdown curves is less clear. Comparing drawdown curves for PZ-09, which shows a high relative permeability based on single-well hydraulic tests, to PZ-11, which yielded a significantly lower permeability, shows similar amounts of drawdown. However, the drawdown in PZ-09 occurs more rapidly than in PZ-11, indicating that the more-permeable sections of the Gallia drain more quickly than the less-permeable regions. Similar results are shown for the area south of the horizontal wells, characterized by PZ-21 and PZ-22, compared with the area north of the horizontal wells, characterized by PZ-01 and PZ-02. Piezometers PZ-21 and PZ-22, which are in a region of high permeability, showed more drawdown at earlier times compared to the less-permeable area surrounding PZ-01 and PZ-02. Distinctions in the rate and magnitude of drawdown as a function of permeability within the Gallia are not as apparent for other piezometers in the CTS.

## EAST WELL DRAWDOWNS

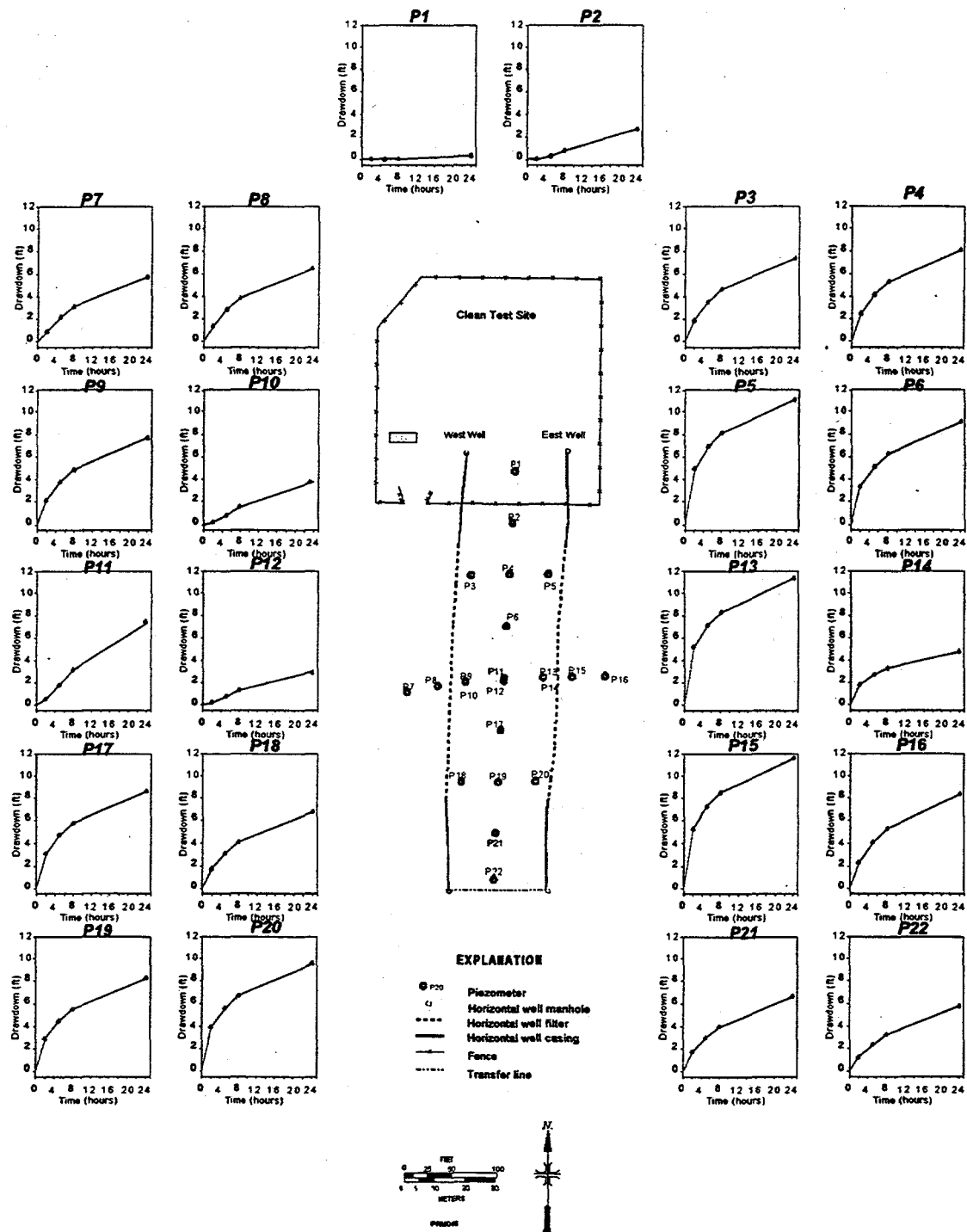


Fig. 5.5. Drawdown graphs for individual piezometers during the east well pumping test.



The maximum area of drawdown for the east well pumping test is near the center of the horizontal well (Fig. 5.6). This observation would agree with the theoretical predictions for a horizontal well in a homogeneous isotropic aquifer presented by Hantush and Papadopoulos (1962). However, there appears to be slightly more drawdown in the northern portion of the horizontal well. Minor permeability contrasts between PZ-05 and PZ-20 do not explain this difference.

A large area of the Gallia is influenced by pumping the east horizontal well. More than 2.2 m (7 ft) of drawdown is observed at the west horizontal well. It is clear that the recirculation wells could be spaced farther apart and still influence the region between the wells with area of influence.

#### **5.4.2.3 Hydraulic Characteristics**

Drawdown vs time curves for the piezometers equipped with transducers are presented in Appendix E. Analysis of the data based on Ferris (1950) yielded similar results to those of the west well pumping test. No significant boundaries were encountered during the test.

#### **5.4.3 Dual Well Pumping Test**

With the dual well pumping tests, water was extracted from the south end of the west horizontal well. The extracted water was then injected into the south end of the east horizontal well. This mode of operation establishes a horizontal recirculation cell between the two wells.

##### **5.4.3.1 Well Yield**

Comparing pumping rates of the individual horizontal wells with the pumping rate during dual-well recirculation shows that it is possible to double the pumping rates under recirculation conditions. The injection well behaves as a constant-head boundary for the extraction well. Consequently, it is possible to pump the extraction well at a higher rate during recirculation than during extraction alone. After 48 h of pumping, 83 L/min (22 gal/min) were pumped and reinjected. The higher pumping rates resulted in higher hydraulic gradients between the horizontal wells.

##### **5.4.3.2 Aquifer Response to Pumping**

Individual piezometer drawdown, or displacement, and a contour map of water-level changes during recirculation tests are presented in Fig. 5.7. Areas of maximum drawdown or displacement are enhanced during recirculation. For the east horizontal or injection well, the northern area shows the maximum amount of displacement. For the west horizontal or extraction well, the southern area shows the maximum drawdown. Although not directly supported by the single-well permeability data, the water-level contour map indicates that the

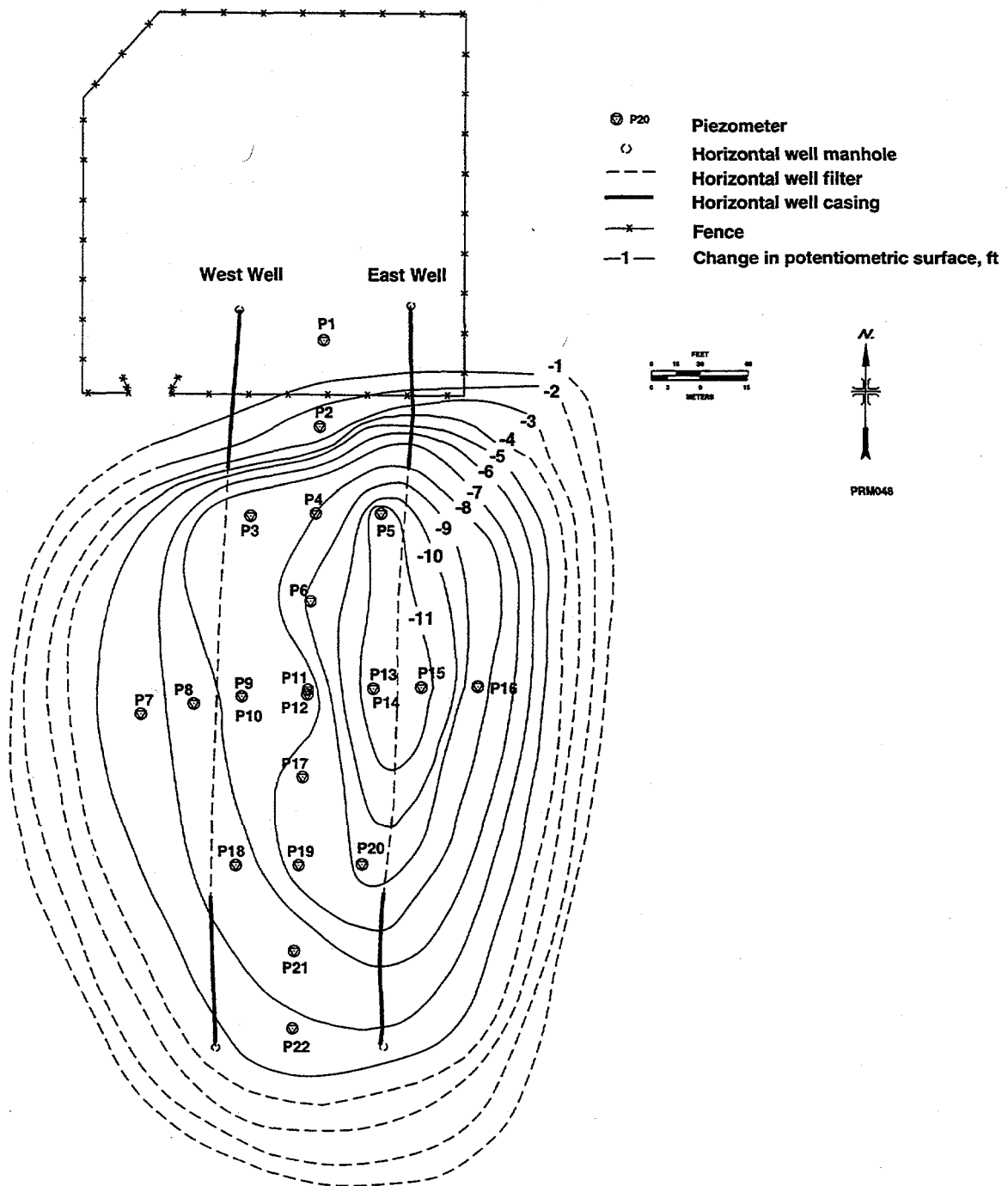


Fig. 5.6. Extent of drawdown in the Gallia resulting from pumping the east horizontal well for 24 h.

## Recirculation Drawdown Contour

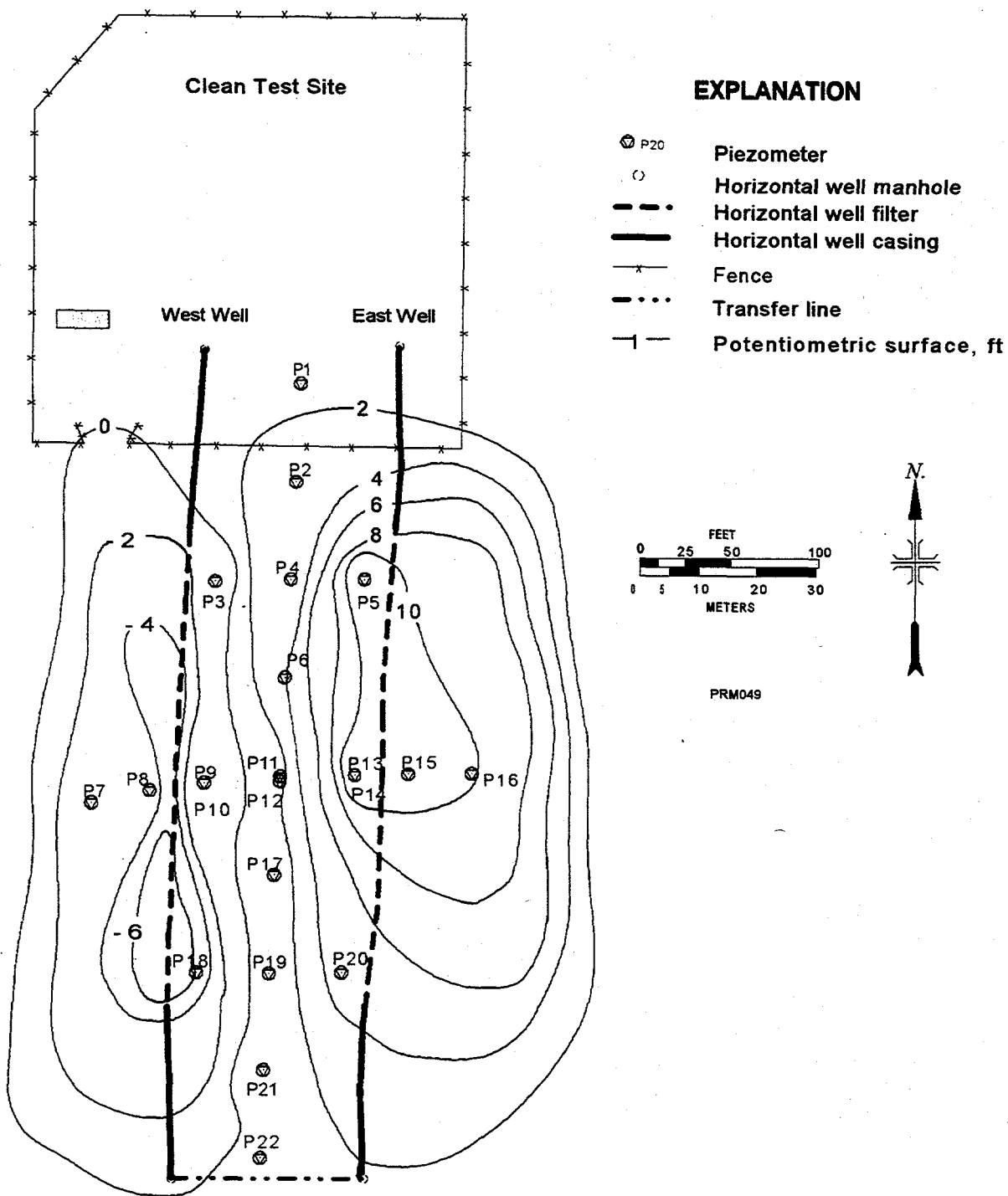


Fig. 5.7. Water-level changes in response to dual well horizontal recirculation.

maximum hydraulic gradient will occur in a northeast to southwest direction between the recirculation wells. This direction agrees with one of the zones of higher permeability defined by the single-well tests.

#### 5.4.3.3 Hydraulic Characteristics

No hydraulic analysis was conducted on the pumping test data from the recirculation tests. Boundary effects from either the injection or pumping can be qualitatively inferred from the pumping test data presented in Appendix F.

### 5.5 Well-Filter Efficiency

To evaluate the efficiency of the porous well filter, it was necessary to conduct a long-term pumping test. This was accomplished during the tracer test, which is discussed in Sect. 6. The horizontal well recirculation system was initially operated at a rate of 80 L/min (20 gal/min). However, after 69 h of pumping, air began entering the horizontal extraction well. Consequently, the pumping rate was reduced to 68 L/min (18 gal/min). Once again, air began entering the horizontal extraction well after two days of pumping at this lower rate. The pumping rate was further reduced to 57 L/min (15 gal/min). A final rate of 30 L/min (8 gal/min) maintained a safe yield in the horizontal extraction well. It was possible to maintain this recirculation rate for 19 days.

The drawdown data from the adjacent piezometers show that quasi-steady-state conditions were established in the Gallia shortly after the initial pumping began. It was after these conditions were established that air began entering the horizontal extraction well. Consequently, deterioration in the efficiency of the porous well filter and not the ability of the Gallia to deliver water to the well was responsible for the decreasing pumping rates.

Porous filter deterioration is believed to be the result of a low-permeability skin developing around the horizontal well filter. Based on the manufacturer's instructions, low-volume pumping was used to develop the horizontal wells. Sediment content in the development water decreased quickly, and the horizontal wells yielded clear water after limited pumping.

This development approach did not remove the fine-grained material from the surrounding formation or fine material introduced during the drilling process. During long-term pumping, this fine-grained material formed a skin of lower permeability surrounding the well filter, which decreased the well efficiency.

Based on the lack of pressure increase observed on the injection side during the recirculation test, a low-permeability skin did not develop around the injection well. Because water was forced out of the porous well filter, fines were not able to clog the formation surrounding the injection well.

As discussed in Sect. 8, it was necessary to redevelop the horizontal wells by modifying conventional well development methods such as water jetting and surging for horizontal well applications. During redevelopment of the wells, the fine-grained material surrounding the

porous well filter was mobilized, brought into the horizontal well, and removed to develop a permeable skin surrounding the porous filter.

## 5.6 Discussion

Hydraulic testing results for the horizontal well recirculation system indicate a heterogeneous water-bearing zone of moderate permeability. Single-well testing showed hydraulic conductivity values that varied by over two orders of magnitude in the Gallia member. Pumping test results suggested that large-scale features such as permeable channels are not major components of the Gallia member in the CTS. However, the sensitivity of horizontal well pumping tests to detect aquifer boundaries is unclear. The issue of image well theory for horizontal line sinks has not been fully explored at this time.

Piezometers completed in the overlying Minford member yielded several feet of drawdown during the pumping tests. These data indicate that the Minford is contributing water to the Gallia. The amount of water contributed by the Minford does not appear significant compared to the Gallia. Once again, however, this is based on pumping test curves for a line sink.

Water levels in the piezometers were slow to recover to prepumping levels. Piezometers located in the portions of the Gallia that are lower in permeability were extremely slow to recover. Water levels measured 24 h after completion of the pumping tests consistently showed a recovery of only approximately two thirds of the static levels. Because of the large area impacted by the horizontal wells, recharge from the surrounding area must travel a large distance to replenish water levels.

Recirculation tests showed that it was possible to increase the average hydraulic gradient to 0.15 between the wells. The hydraulic gradient remained fairly consistent between the horizontal wells, with some variations due to heterogeneity. Under these conditions, water will travel approximately two orders of magnitude faster than under ambient conditions, with only permeability controlling groundwater flow velocities between the horizontal wells.

Further research and hydraulic analyses using numerical models would be necessary to complete a comprehensive description of the Gallia and Minford hydrodynamics. Such analyses were beyond the scope of this project.

## 6. Tracer Test

### 6.1 Introduction

This section discusses the results of a bromide tracer test conducted on the horizontal well recirculation system. Results of hydraulic tests and colloidal borescope measurements are compared with the tracer data to provide additional data to assess the heterogeneity of the Gallia. Piezometers in the overlying Minford were also sampled to determine the impact of circulating fluids on these fine-grained sediments.

The purpose of the tracer test was to measure travel time and distribution and concentration of tracers in the vicinity of the horizontal recirculation wells. Understanding travel time is important in determining the number of pore volumes per unit time that can be recirculated by the well system. The distribution and concentration of tracers based on piezometer sampling data provide an understanding of the impact of heterogeneity on recirculation efficiency. It is widely recognized that subsurface heterogeneity is a controlling influence on the distribution of contaminants and the hydrodynamic pathways that provide access to the contaminants.

Three tracers were selected for the test: 1) an ionic tracer, bromide (as potassium bromide); 2) a fluorescent dye, fluorescein; and 3) a colloidal tracer, SNOMAX, an ice-nucleating active-bacteria product. This report focuses on the results of the bromide tracer test. Muck et al. (1996) discusses the fluorescein and SNOMAX tracer test results.

### 6.2 Description of the Bromide Tracer

Bromide and chloride are the most commonly used ionic tracers. This type of tracer is introduced to the subsurface as a salt (e.g., potassium bromide) where it ionizes in water, resulting in separate charged species (anions and cations). In most cases, anions (e.g.,  $\text{Br}^-$ ) are not affected by the aquifer medium and serve as excellent conservative tracers (i.e., they travel with the same velocity and direction as the water). Bromide was chosen as a tracer due to its low background concentration in soils, high solubility, and low toxicity. Analysis for ionic tracers can be conducted in the field using test kits or ion-selective electrodes. More accurate analysis is possible in the laboratory using ion chromatography. However, laboratory analyses are expensive and require a longer turn-around time.

### 6.3 Stock Tracer Concentration

Crystalline potassium bromide (12.5 kg) was mixed in a 1,890-L (500-gal) tank containing groundwater before injection into the east horizontal well (see Sect. 6.5.1). Samples from the tank were collected for analysis prior to injection. The calculated bromide concentration in the stock solution was 4,425 mg/L. The actual bromide concentration (mean value of three samples) was 3,396 mg/L.

The measured bromide concentration in stock tracer samples was approximately 25% less than the calculated concentration. This difference is attributed to incomplete solubilization of the KBr crystals. The ambient temperature at the time of injection was approximately 25°F (-4°C). The tank solution was mixed for less than one hour due to concerns that the solution would freeze after addition of the SNOMAX. This relatively short mixing time, combined with a cold water temperature, resulted in reduced dissolution of the KBr crystals.

#### 6.4 Bromide Analysis

Analysis for bromide was performed in the on-site field laboratory at PORTS using an ion-specific electrode. This method of analysis was chosen due to its reliability and relative ease of use in the field. Moreover, sample results were quickly available.

Bromide concentrations were determined using an Orion™ Model 94-35 bromide electrode and a Model 90-02 double junction reference electrode. Output from the electrodes was measured in millivolts on a Beckman Model 34 pH meter. To reduce potential interference, an ionic strength adjustor of 5 M NaNO<sub>3</sub> was added at the rate of 2% by volume to all samples and standards. A daily calibration curve was produced by measuring a series of bromide standards (0.0, 0.8, 1.6, 3.2, 8.0, 80, and 800 mg/L). Millivolt readings for each standard were entered into a linear regression program, and a standard curve was determined. The standard curve was then used to convert sample millivolt readings to bromide concentrations. All calibration and sample data were recorded on logsheets and in the project laboratory notebook.

No significant problems were encountered during bromide analyses. Although some variability was observed in the standard curve calculation on a day-to-day basis, this variability is typical for electrochemical analyses. Routine maintenance during the project included replacing the filling solutions on the reference electrode and cleaning the bromide electrode with polishing strips.

#### 6.5 Field Methods

##### 6.5.1 Injection of Tracer

A 1,890-L (500-gal) tank was used to mix the tracer solution prior to injection. A series of valves connected the mixing tank to the piping between the horizontal wells. Prior to injecting the tracer solution, the recirculation system was operated for 26 h to establish quasi-steady-state groundwater flow conditions. Water was routed from the extraction well to the mixing tank approximately 2 h prior to injection. Tracers were added to the tank and mixed with a submersible pump located at the base of the tank. Immediately prior to and during the injection, the tracer concentrations were repeatedly measured in the mixing tank.

During the injection of the tracer solution, water from the extraction well was routed to a nearby ditch. The tracer solution in the mixing tank was pumped at the same rate into the horizontal injection well as the pump rate from the horizontal extraction well. After the

tracer solution was injected, water from the extraction well was immediately rerouted to the injection well. Sampling of piezometers adjacent to the injection well began immediately.

The injection procedure resulted in a net deficit of 1,890 L (500 gal) of water for the first day of the tracer test. Preferably, the mixing tank should have been filled several days prior to the test, and the water-bearing zone allowed to recover. Unfortunately, the SNOMAX tracer is temperature sensitive and with January temperatures well below 0°C, it was not possible to leave groundwater exposed for several days.

### 6.5.2 Well Sampling

Thirty-three piezometers and the effluent from the extraction well were monitored to assess the rate and extent of tracer migration. The piezometers were completed primarily in the Gallia member with a limited number completed in the overlying Minford member. Nineteen of the piezometers were constructed of 5-cm (2-in.) diameter PVC screened across the entire thickness of the Gallia. Three 5-cm (2-in.) diameter PVC piezometers were completed in the overlying Minford. The remaining 11 piezometers were constructed of 2.5-cm (1-in.) diameter PVC casing and screen and were installed using the U2CRT mobile drilling truck. Figure 6.1 shows the piezometer locations.

Because of differences in piezometer sizes and installation techniques, there is a possibility of sampling variances between the two piezometer types. The 5-cm (2-in.) piezometers were installed with sand packs and were adequately developed. Clear water was obtained from these piezometers throughout the duration of the tests. Conversely, the 2.5-cm (1-in.) piezometers yielded less water with a higher turbidity and may not be as hydraulically connected to the surrounding formation as the 5-cm (2-in.) piezometers. In addition, drilling difficulties during the installation of the 2.5-cm (1-in.) piezometers resulted in screened intervals that range from the lower Minford to the upper Gallia. This variance is useful for assessing heterogeneity in the Gallia and the impact on the overlying Minford. However, these differences must be considered when comparing sampling data from both types of piezometers. Table 6.1 provides well completion information for the individual piezometers, and the completed well logs are provided in Appendix C.

Water sampling methodology was controlled by the need for an efficient sampling program that rapidly obtained representative samples from the screened portion of the piezometers. It was anticipated that between two to three thousand water samples would be collected as part of the tracer test. Consequently, permanent sampling tubes were installed in each piezometer with the open portion in the middle of the screen. Using the micropurge method discussed by Kearn et al. (1994), piezometers were sampled at a rate of 600 mL/min (0.16 gal/min). Purging consisted of removing 1 L (0.3 gal) of water then collecting the sample. This purge volume corresponds to approximately two sampling tube volumes. It is believed that this approach yielded water that was representative of the groundwater surrounding the piezometers; sampling required only 3 to 5 min to complete. The uniformity of the chemistry results discussed in the following sections supports this sampling methodology.



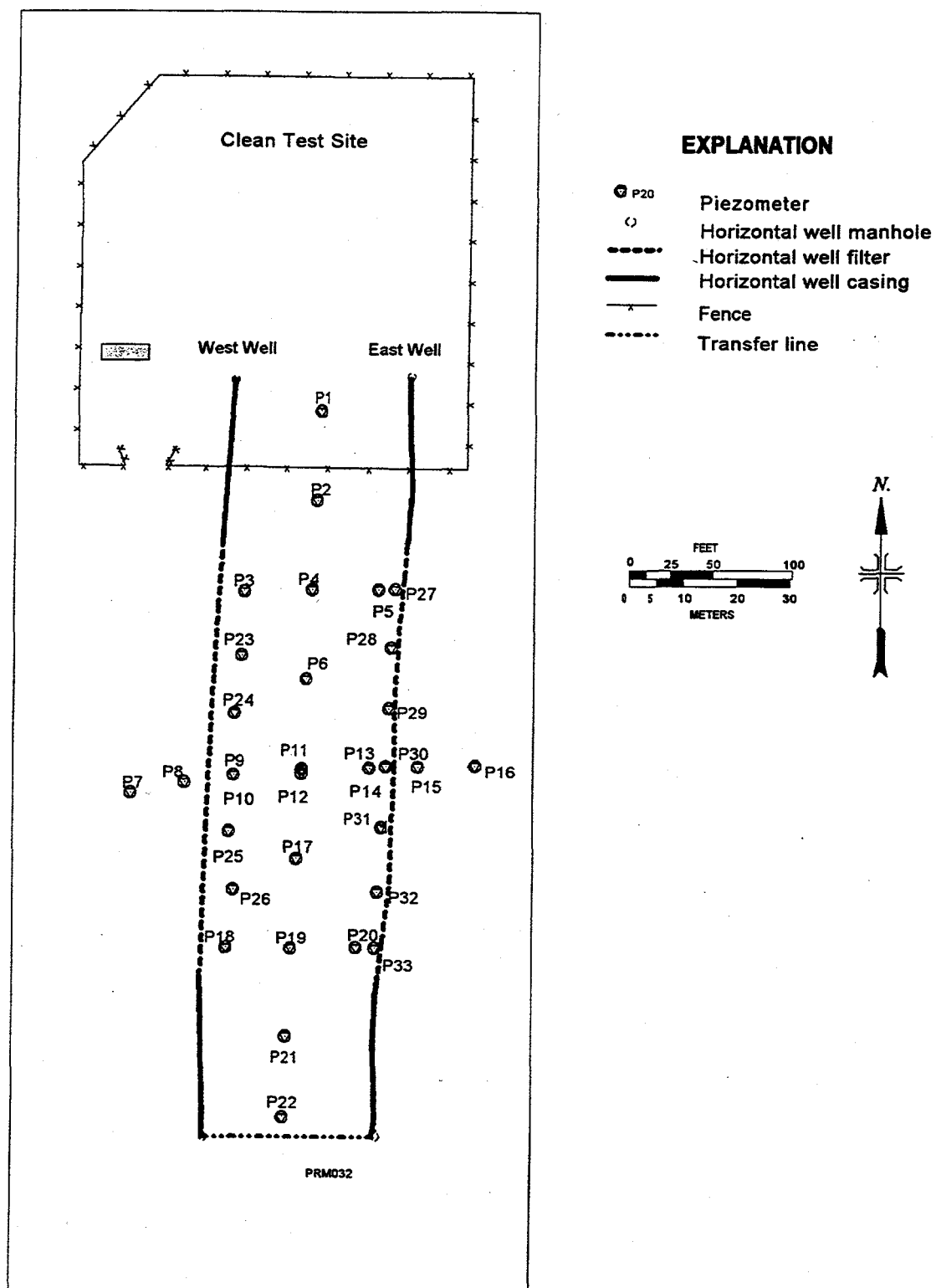


Fig. 6.1. Locations of piezometers sampled during the horizontal recirculation tracer test.

Table 6.1. Piezometer response to the bromide tracer test

Piezometer	Diameter, cm	Stratigraphic Member	Average hydraulic K, cm/s ( $\times 10^{-4}$ )	Time to peak concentration <sup>a</sup> , days	Peak concentration, mg/L	Comments
PZ-01	5	Gallia	0.52	No peak		Outside main flow field; no tracer detected
PZ-02	5	Gallia	0.28	No peak		Outside main flow field; no tracer detected
PZ-03	5	Gallia	3.5	14 to 16	14	No clear peak; diffusion controlled
PZ-04	5	Gallia	10	3.8	46	Minor spread on breakthrough peak
PZ-05	5	Gallia	9.0	0.8	95	Sharp breakthrough peak
PZ-06	5	Gallia	36	1.4	53	Sharp breakthrough peak
PZ-07	5	Gallia	5.5	No peak	4	Slight increase in bromide near end of test
PZ-08	5	Gallia	9.7	No peak	9	Outside main flow field; increased to background value (diffusion controlled)
PZ-09	5	Gallia	56	3.1	38	Broad breakthrough peak
PZ-10	5	Minford	0.20	No peak		No bromide detected
PZ-11	5	Gallia	0.069	2.0	46	Broad breakthrough peak
PZ-12	5	Minford	0.32	No peak		No bromide detected
PZ-13	5	Gallia	3.5	0.8	52	Sharp breakthrough peak
PZ-14	5	Minford	0.21	3.1		Broad breakthrough peak
PZ-15	5	Gallia	0.41	0.77	102	Outside main flow field; sharp breakthrough peak

Table 6.1. (continued)

Piezometer	Diameter, cm	Stratigraphic Member	Average hydraulic K, cm/s ( $\times 10^{-4}$ )	Time to peak concentration <sup>a</sup> , days	Peak concentration, mg/L	Comments
PZ-16	5	Gallia	4.6	4.8	39	Outside main flow field; broad breakthrough peak
PZ-17	5	Gallia	32	1.4	30	Broad breakthrough or dual sharp peaks
PZ-18	5	Gallia	3.5	3.1	26	Broad breakthrough peak
PZ-19	5	Gallia	39	1.35	57	Sharp breakthrough peak
PZ-20	5	Gallia	11	0.33	111	Sharp breakthrough peak
PZ-21	5	Gallia	2.6	5.1	29	Outside main flow field; broad breakthrough peak
PZ-22	5	Gallia	1.5	No peak		Outside main flow field; no bromide detected
PZ-23	2.5	0.3 m into Gallia (no lithified zone in this well)	NT	No peak		No bromide detected
PZ-24	2.5	Minford	NT	No peak		No bromide detected
PZ-25	2.5	0.5 m into the Gallia	NT	No peak		No bromide detected
PZ-26	2.5	0.7 m into Gallia above and within lithified zone	NT	No peak		One bromide detection, probably analytical error
PZ-27	2.5	Minford	NT	No peak		No bromide detected
PZ-28	2.5	Minford	NT	No peak		No bromide detected

Table 6.1. (continued)

Piezometer	Diameter, cm	Stratigraphic Member	Average hydraulic K, cm/s ( $\times 10^{-4}$ )	Time to peak concentration <sup>a</sup> , days	Peak concentration, mg/L	Comments
PZ-29	2.5	Minford	NT	No peak		No bromide detected
PZ-30	2.5	0.7 m into Gallia above lithified zone	NT	0.10	119	Sharp breakthrough peak
PZ-31	2.5	0.8 m into Gallia above lithified zone	NT	2.0	45	Sharp breakthrough peak
PZ-32	2.5	Minford	NT	0.14	36	Sharp breakthrough peak
PZ-33	2.5	Minford	NT	No peak		No bromide detected

<sup>a</sup> time that the highest bromide concentration occurred

NT = not tested

An ISCO automated sampler was connected between the horizontal wells to obtain discrete samples of groundwater from the extraction well. Initially, samples were taken every hour, which was later reduced to every 2 h. Results from the horizontal extraction well sampling indicated arrival times for the tracers and the concentrations of tracers being recirculated in the system.

### 6.6 Horizontal Well Performance During Tracer Test

Ideally, a constant pumping rate should have been maintained during the tracer test. Unfortunately, because the well efficiency of the horizontal extraction well continued to deteriorate during the test, the pumping rate was reduced several times as shown in Table 6.2. The variable pumping rate complicated the tracer test and must be considered in interpreting the test results.

**Table 6.2. Pumping schedule during the horizontal recirculation tracer test**

Date	Time	Total time since tracer injection, h	Pumping rate, L/min
02/10/95	1400	0	76
02/12/95	0900	43	68
02/14/95	0845	90.75	57
02/16/95	1500	145	45
02/18/95	1630	194.5	38
02/24/95	1200	334	30
03/15/95	1630	794.5	30

### 6.7 Tracer Test Results

The sampling strategy consisted of automated sampling of the horizontal extraction well and selected sampling of the piezometers. All of the 5-cm (2-in.) piezometers were sampled each day. Additional sampling focused initially on piezometers immediately adjacent to the horizontal injection well and then concentrated on piezometers that detected the arrival of the tracers. The goal of the piezometer sampling was to determine the arrival peak of the tracers at each location as definitively as possible.

The horizontal-extraction-well and piezometer breakthrough curves for the bromide tracer are presented in Figs. 6.2 and 6.3. Muck et al. (1996) presents a complete tabulation of the bromide data. A brief description of individual piezometer characteristics, time when peak concentrations of bromide occurred, and descriptions of peak characteristics are presented in Table 6.1.

The terms sharp and broad peaks refer to the amount of time for the initial slug of bromide tracer to move past the piezometer. The broader the peak, the more influence dispersion and diffusion had on the transport of the tracer. The main flow field refers to the area directly between the horizontal recirculation wells.

#### 6.7.1 Horizontal Extraction Well Results

An inspection of the bromide data from the horizontal extraction well yields several interesting observations. These include the initial breakthrough of bromide tracer, the initial peak in concentration, repeated peaks in bromide concentration, and the general downward trend in bromide concentration as a function of time. Bromide was detected in the horizontal extraction well 21 h after injection. This breakthrough time is significantly shorter than could be accounted for by the average permeability of the Gallia member between the horizontal wells even considering the high values of dispersivity.

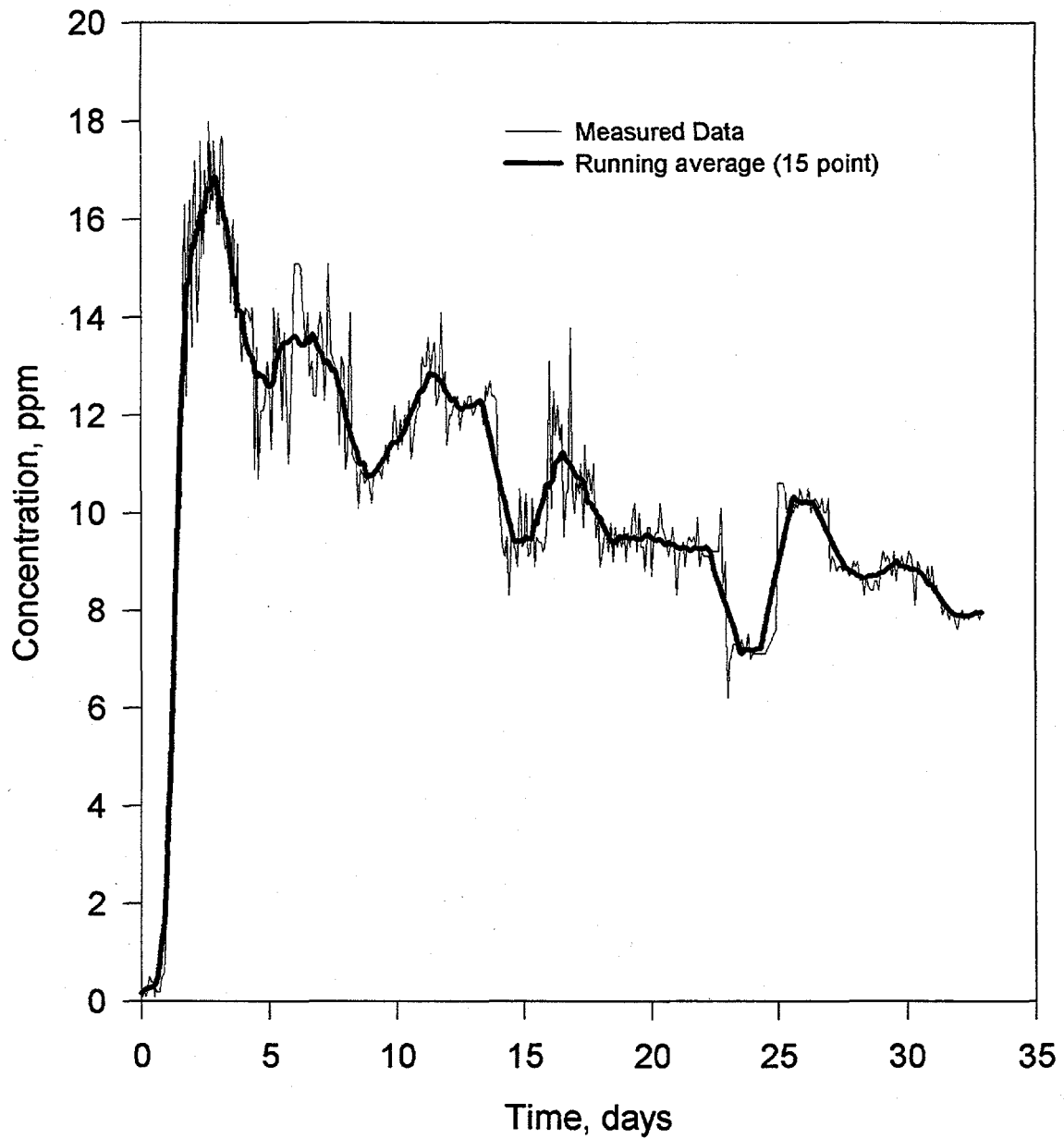
The initial peak in bromide concentration, which represents the average bulk groundwater flow, occurred after 2.6 days. Once again, this value indicates a groundwater velocity higher than predicted by hydraulic values from pumping tests. Numerous peaks occurred after the initial peak. Although the accuracy of the bromide measurements is estimated to be  $\pm 1$  ppm, data averaging supports the cyclic trend. The first three peaks occurred after a similar volume of water had passed between the wells. Volume is a better indicator than time of the recurrence interval of bromide peaks since the pumping rate was changed during the test. After the first three peaks, the trend became less well-defined. These secondary peaks appear to be additional breakthrough curves as the tracer was being recirculated.

After the initial breakthrough, bromide concentrations in the horizontal extraction well ranged from 8 to 14 ppm for the duration of the tracer test. Since this water was reinjected into the horizontal injection well, this range of bromide concentrations represents background values in the region of the saturated zone influenced by the horizontal well recirculation system.

Throughout the remainder of this section, the term background concentrations will refer to bromide concentrations of water reinjected into the horizontal recirculation system after the initial breakthrough peak.

Finally, bromide concentrations declined with time during the test. This decline could reflect losses due to diffusion or to bromide escaping from the system. As tracers migrated through the more-permeable portions of the Gallia, a portion of the mass was lost by diffusion into adjacent zones of lower permeability. Escape of tracer from the recirculation flow field is

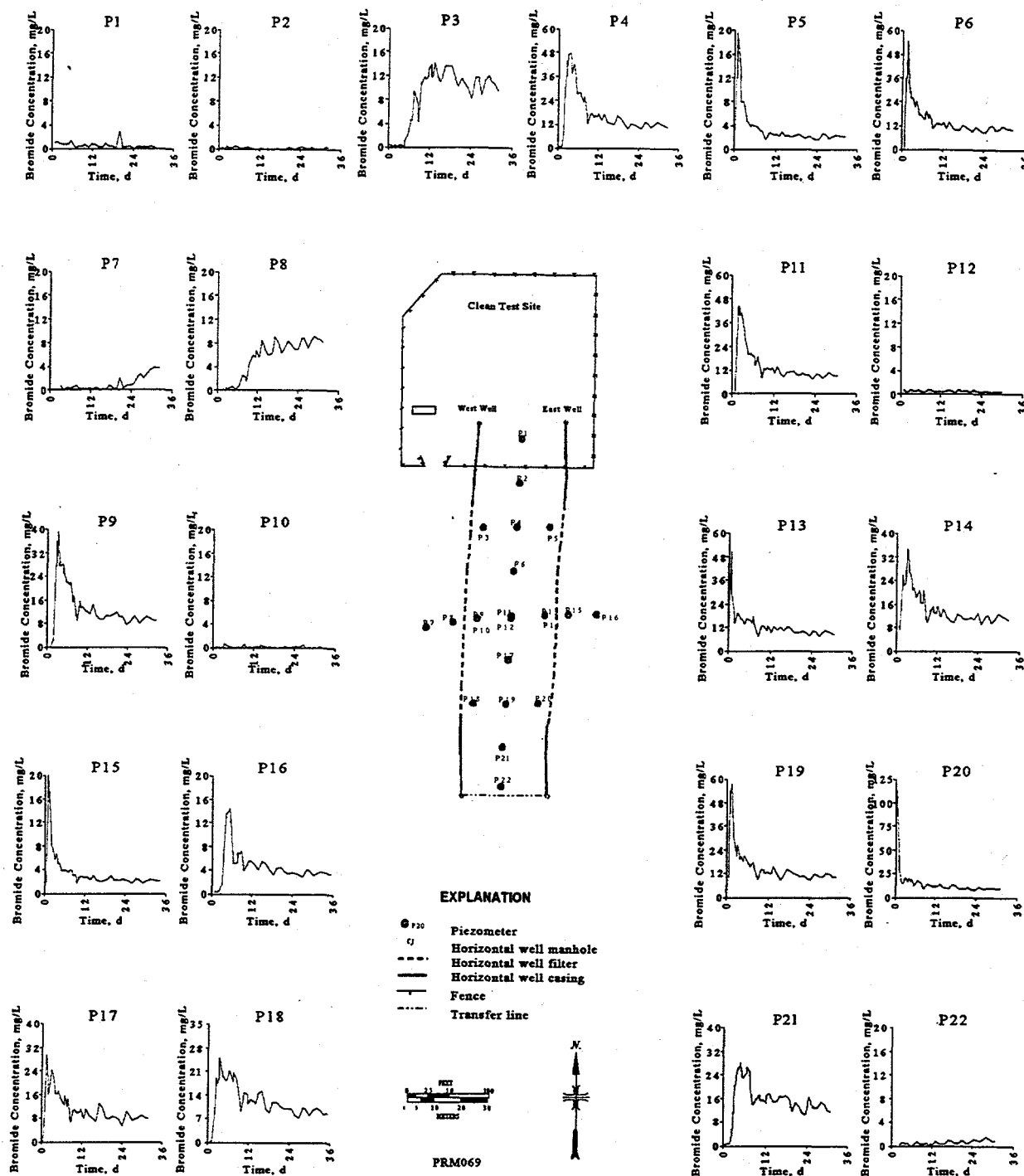
## Extraction Well



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Fig. 6.2. Bromide concentrations from the horizontal extraction well during the tracer test.

## Bromide Breakthrough Curves





also possible. The amount of water captured on the upgradient side of the horizontal well recirculation system is lost on the downgradient side to maintain a mass balance. Consequently, some of the tracer was lost on the downgradient side of the flow field.

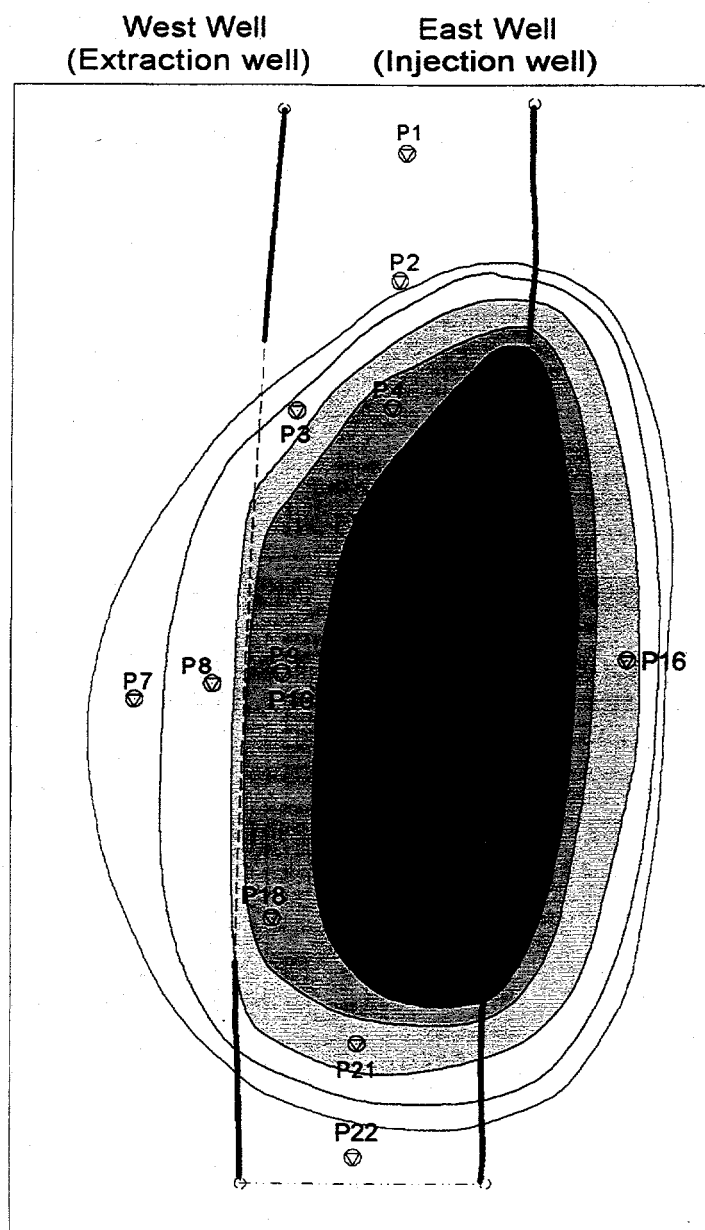
### 6.7.2 Gallia Member Piezometer Results

Sampling data from piezometers completed in the Gallia yielded information on the rate and extent of tracer movement between the horizontal wells. The goal of the piezometer sampling was to assess the uniformity with which the tracer moved in the Gallia and to estimate the degree of heterogeneity in the Gallia. Based on the bromide data from the piezometers, the following statements can be made about the behavior of tracer in the Gallia member:

- Piezometers showed different breakthrough characteristics, indicating heterogeneity in the Gallia.
- Sharp breakthrough peaks were observed, followed by a relatively large decrease in bromide concentrations for piezometers near the injection well compared with downgradient piezometers.
- Sharp breakthrough peaks were observed for piezometers in the more-permeable portions of the Gallia.
- Secondary peaks similar to those observed in the horizontal extraction well were not evident in the piezometers.
- After initial breakthrough peaks occurred, bromide concentrations declined to background values of 8 to 14 ppm for all piezometers where bromide was detected.
- Some piezometers showed no indication of the tracers.
- Breakthrough was observed in all Gallia piezometers located in the area between the ends of the well filters (the main flow field).

Figure 6.4 displays breakthrough times based on bromide analysis for the individual piezometers. These data show the tracer moving at a higher rate near the center of the extraction well. This flow pattern is consistent with preferential flow patterns identified using single-well hydraulic tests. On the other hand, the piezometers do not identify the preferential flow zone responsible for the tracer detected in the horizontal extraction well less than one day after injection. This evidence suggests that preferential flow zones are limited in extent and, therefore, not easily detected by the piezometers. However, large flow zones with higher than average hydraulic conductivities are present and are defined by the piezometers.

Sharp breakthrough peaks in the piezometers adjacent to the horizontal injection well were expected because of the limited time available for hydrodynamic dispersion and diffusion to spread and dilute the tracer. PZ-20 showed a sharp peak that rapidly dropped off to a bromide concentration that was approximately an order of magnitude lower than the peak

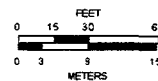


### Legend

#### Breakthrough time    Piezometers

1 Day	5,6,11,13,15,17,19,20
2 Days	4,9,18
3 Days	16,21
10 Days	3,8
30 Days	7

⊙ P20	Piezometer
( )	Horizontal well manhole
---	Horizontal well filter
---	Horizontal well casing
---	Transfer line



PRM032A

Fig. 6.4. Extent of bromide breakthrough at selected time intervals.

concentration. However, as the tracer moved farther along the flow path toward the horizontal extraction well, peak bromide concentrations decreased as dispersion and diffusion became more important. This was evident in piezometers near the horizontal extraction well. For example, PZ-18 showed an initial peak of only twice the background bromide concentration.

Sharp breakthrough peaks were observed for piezometers located within the higher-permeability zones of the Gallia defined by Fig. 5.1 in Sect. 5.4. Peak bromide concentrations in these wells ranged from 3 to 10 times higher than background values. The sharp breakthrough peaks are attributed to the minimal time available for hydrodynamic dispersion and diffusion to spread and dilute the tracer in the zones of higher permeability. Outside of the permeable zones, broader breakthrough peaks of lower bromide concentrations were typical.

Tracers were not detected in PZ-01 and PZ-02, indicating that the recirculation flow field does not impact the north of the horizontal well filters. This area yielded hydraulic conductivity values that did not exceed  $7 \times 10^{-5}$  cm/s (0.2 ft/d). As expected, low permeability sediments greatly reduce the movement of the tracers. Conversely, tracers did reach PZ-21, but not PZ-22. Comparing the hydraulic conductivities of piezometers beyond the south end of the horizontal well filters, PZ-21 yielded the highest value, showing the effect of permeability control on tracer movement in this region.

The bromide concentration curve for PZ-03 is of particular interest. This piezometer is beyond the permeable zone defined by the single-well test and discussed in Sect. 5.4. Nearly 7 days were required for the tracer to reach this piezometer compared with 3 to 4 days for other piezometers located at the same distance from the injection well (PZ-09 and PZ-18). Once the bromide tracer reached PZ-03, concentrations ranged from approximately 8 to 14 ppm. Both PZ-09 and PZ-18 showed bromide peaks that exceeded background values. Since bromide concentrations in PZ-03 equaled background values instead of displaying the sharp peaks typical of advection-dominated flow, this evidence suggests that diffusion controlled the movement of bromide tracer in the lower-permeability area surrounding PZ-03.

### 6.7.3 Minford Member Piezometer Results

PZ-14 and PZ-32 were the only Minford piezometers that showed detections of bromide. The reason PZ-14 showed bromide appears to be due to both a sand zone noted in the geologic log that is not typical of the Minford at other locations and the nearness of PZ-14 to the horizontal injection well. PZ-32 is located closer to the injection well (1.5 m) than PZ-14; however, no geologic log is available for this piezometer. The lack of bromide in the remaining Minford piezometers across the test site indicates that this unit is not in direct

hydraulic communication with the underlying Gallia. This lack of hydraulic communication is the direct result of the low permeability of the Minford. Although the Minford can yield minor amounts of water as shown by the pumping analyses, advection-dominated flow is not typical in this member.

#### **6.7.4 Test Results for the 2.5-cm-diameter Piezometers**

As noted earlier, the installation and construction of the 2.5-cm (1-in.) piezometers differed from the larger 5-cm (2-in.) piezometers, which could bias test results. Of the 11 small-diameter piezometers, bromide tracer was detected in only PZ-30, PZ-31, and PZ-32. These piezometers are all located 1.5 m (5 ft) from the injection well. PZ-30 and PZ-31 are completed in the upper portion of the Gallia, while PZ-32 is in the Minford. The proximity of these piezometers to the injection well explains the presence of the tracer.

Three of the 2.5-cm (1-in.) piezometers near the horizontal extraction well (PZ-23, PZ-25, and PZ-26) are completed in the upper 0.5 m (1.6 ft) of the Gallia member. None showed detections of bromide tracer. There are three possibilities to explain the absence of tracer in these piezometers. First, the piezometers are located in low-permeability portions of the Gallia. This explanation seems unlikely since all 5-cm (2-in.) piezometers between the recirculation wells yielded tracer. The second possibility is that within the Gallia member, the lower portion is a preferential flow zone. This explanation is complicated by the third possibility that the 2.5-cm (1-in.) piezometers are not in as direct hydraulic communication with the Gallia as are the 5-cm (2-in.) piezometers.

#### **6.8 Colloidal Borescope Measurements**

The colloidal borescope was placed in several piezometers to measure the impact of the horizontal well recirculation system on groundwater flow velocities. A detailed description of the colloidal borescope is presented by Kearl et al. (1994). Briefly, using the colloidal borescope, it is possible to obtain a direct measurement of groundwater velocity without relying on a Darcian solution.

The colloidal borescope was used to quantify groundwater flow velocities during the tracer tests. Flow rates and directions were measured in the majority of the 5-cm (2-in.) piezometers. Measurement results for selected piezometers are presented in Table 6.3 and Appendix G.

The majority of piezometers yielded swirling, nondirectional flow patterns typical of the nonpreferential flow zones that have been observed at other field sites. Notable exceptions were PZ-06, PZ-09, and PZ-19, which all showed consistent flow velocities in steady flow directions. These piezometers also yielded the highest hydraulic conductivity values observed at the site. Borescope measurements and the hydraulic test results suggest the existence of a preferential flow zone or channel that trends from the north end of the east horizontal well through piezometers PZ-06 and PZ-09 and a second channel from the south end of the east

**Table 6.3. Groundwater velocity measurements  
in selected piezometers using the colloidal borescope**

Piezometer	Direction <sup>a</sup> (azimuth)	Rate <sup>b</sup> , cm/s
PZ-04	260°	0.0042
PZ-06	225°	0.037
PZ-09	288°	0.013
PZ-19	295°	0.0122
PZ-22	340°	0.0013

<sup>a</sup> Zero azimuth was set to true north.

<sup>b</sup> Flow rates have been corrected for the influence of the wellbore and screen pack.

horizontal well through piezometers PZ-19 and PZ-09. For all of the piezometers listed in Table 6.3, groundwater flow velocities that were observed with the colloidal borescope exceeded calculated values based on measured hydraulic values and Darcy's Law.

## 6.9 Discussion

Several factors influenced the horizontal recirculation tracer test. These factors included heterogeneity or preferential flow zones in the Gallia, recirculation of tracers at lower concentrations than the initial slug, the escape of tracers from the downgradient side of the recirculation flow field, and retardation of the tracers. Tracers that migrate along preferential flow zones can reenter the injection well and reach the extraction well before tracers in a slower flow zone reach the extraction well for the first time. Consequently, a breakthrough curve for the horizontal extraction well may consist of several superimposed breakthrough curves.

An important goal of the tracer test was to determine the influence of aquifer heterogeneity on possible source-remediation strategies. Heterogeneity exerts an important influence on the distribution and concentration of the tracers. Consequently, measuring the arrival and concentration of tracers at specified locations in the region between the horizontal wells can provide insight into the efficiency of a dual-well horizontal recirculation system in remediating discrete contaminant source areas.

Bromide was detected in 16 of the 19 5-cm (2-in.) diameter piezometers completed in the Gallia. These 16 piezometers include all of the piezometers located between the horizontal well filters and those piezometers located upgradient and downgradient of the horizontal well filters. The three piezometers in which bromide was not detected are located north of the north end (PZ-01 and PZ-02) and south of the south end (PZ-22) of the horizontal well filters. The presence of bromide in the remaining 16 piezometers indicates that the flow field

established by the horizontal well recirculation system was thoroughly penetrated by the bromide tracer.

Arrival times for the tracers differed significantly from one piezometer to another. This is attributed to the distance from the injection well and varying hydraulic conductivity values discussed in the previous section. Advection-dominated transport was apparent in areas immediately downgradient of the horizontal injection well and in zones of higher permeability between the wells. In the zones of lower permeability, the effects of dispersion and diffusion increased as the distance from the injection well increased.

Not all of the 2.5-cm (1-in.) piezometers completed in the Gallia member showed tracers. None of the 2.5-cm (1-in.) piezometers near the horizontal extraction well showed detections of bromide. These piezometers are completed in the Minford and the upper portions of the Gallia. The lack of bromide compared with the 5-cm (2-in.) piezometers may be due to different installation techniques or preferential flow in the lower portions of the Gallia.

The only Minford piezometers where bromide was detected were PZ-14 and PZ-32. The lithologic log for PZ-14 shows a sandy lens in the Minford at this location. It is assumed that this sandy lens is in hydraulic connection with the horizontal injection well that is only 5 m (15 ft) from PZ-14. This sandy lens is not typical in other piezometers completed in the Minford. PZ-32 is located only 1.6 m (5 ft) from the horizontal injection well, with the screened interval immediately above the Gallia member. Because bromide was found in only two of the Minford piezometers, it appears that contamination present in the Minford member at other PORTS locations would not be significantly impacted by a horizontal well recirculation system.

Comparing colloidal borescope velocity measurements with tracer test results provides some interesting relationships. The tracer test showed that bromide reached the extraction well 21 h after being introduced into the injection well. Using the highest observed hydraulic conductivity for the entire facility of  $1.8 \times 10^{-2}$  cm/s (50 ft/d), an assumed porosity of 0.20, and neglecting dispersion, it would take 2.6 days for the tracer to reach the extraction well. However, the velocity measured in PZ-06 of 0.037 cm/s (105 ft/d) yields an initial breakthrough resulting from preferential flow zones of approximately 23 h, similar to the time measured by the tracer.

If the velocities of 0.0122 and 0.013 cm/s (35 and 37 ft/d) measured in PZ-19 and PZ-09 represent the average seepage velocity in the area between the recirculation wells under pumping conditions, this would result in a predicted breakthrough time of approximately 2.8 days. This value is in excellent agreement with the first bromide peak in the horizontal extraction well of approximately 2.6 days.

## 7. Elution Test

### 7.1 Introduction

A bromide-elution test was performed at the CTS as a follow-on to the bromide tracer test. The purpose of the elution test was to observe the removal of bromide tracer from the recirculation flow field with time. The injection and extraction wells were operated for 20 days. The initial flow rate was 8 gal/min (1,820 L/h) for 12 days, but due to continued well clogging, the flow rate was reduced to 6 gal/min (1,360 L/h) for the last 8 days. To elute bromide from the flow field, clean water from a nearby fire hydrant was routed to the injection well, and groundwater from the extraction well was discharged to ground surface in a nearby drainage swale.

Groundwater samples for bromide analysis were collected from the extraction well and piezometers PZ-01 through PZ-22 (Fig. 7.1). Section 6.2.1 describes the bromide tracer, Sect. 6.4.1 describes the equipment and methods used for field analysis of water samples for bromide concentration, and Sect. 6.5.2 describes the water sampling methodology. Muck et al. (1996) presents a complete tabulation of the bromide data. The accuracy of the bromide measurements is estimated to be  $\pm 1$  mg/L, so analytical results discussed in the text are rounded to the nearest whole number. Plots of bromide concentration vs time were prepared to show the removal rate of bromide (Figs 7.1 and 7.2). Water samples for bromide analysis were also collected from the fire hose during the test to monitor the concentration of bromide in the injected water (Fig. 7.3). Table 7.1 summarizes observations of bromide concentrations in water samples from the piezometers.

For the first 12 days of the elution test, water samples were collected daily from the injection water, daily from PZ-01 through PZ-22, and every two hours from the extraction well. Note that the elution test was not in the original scope of work for this project and was performed using available personnel. For the last eight days of the elution test, personnel were not available on a daily basis to collect water samples, so no samples were collected from the injection water or the piezometers. Instead, an auto sampler collected water samples once every eight hours from the extraction well.

### 7.2 Elution Test Results

The fire-hydrant source of injection water contained a bromide concentration of 1 to 2 mg/L (Fig. 7.3). This is considered the background concentration of bromide when interpreting the elution test results. Several trends that were noted in the tracer test results are also evident in the elution test results:

- The elution rates of the piezometers differ, indicating heterogeneity in the Gallia.
- Consistent with the tracer test results, no bromide was detected in PZ-01 and PZ-02. These piezometers lie north of the horizontal well filters and outside of the main flow field.

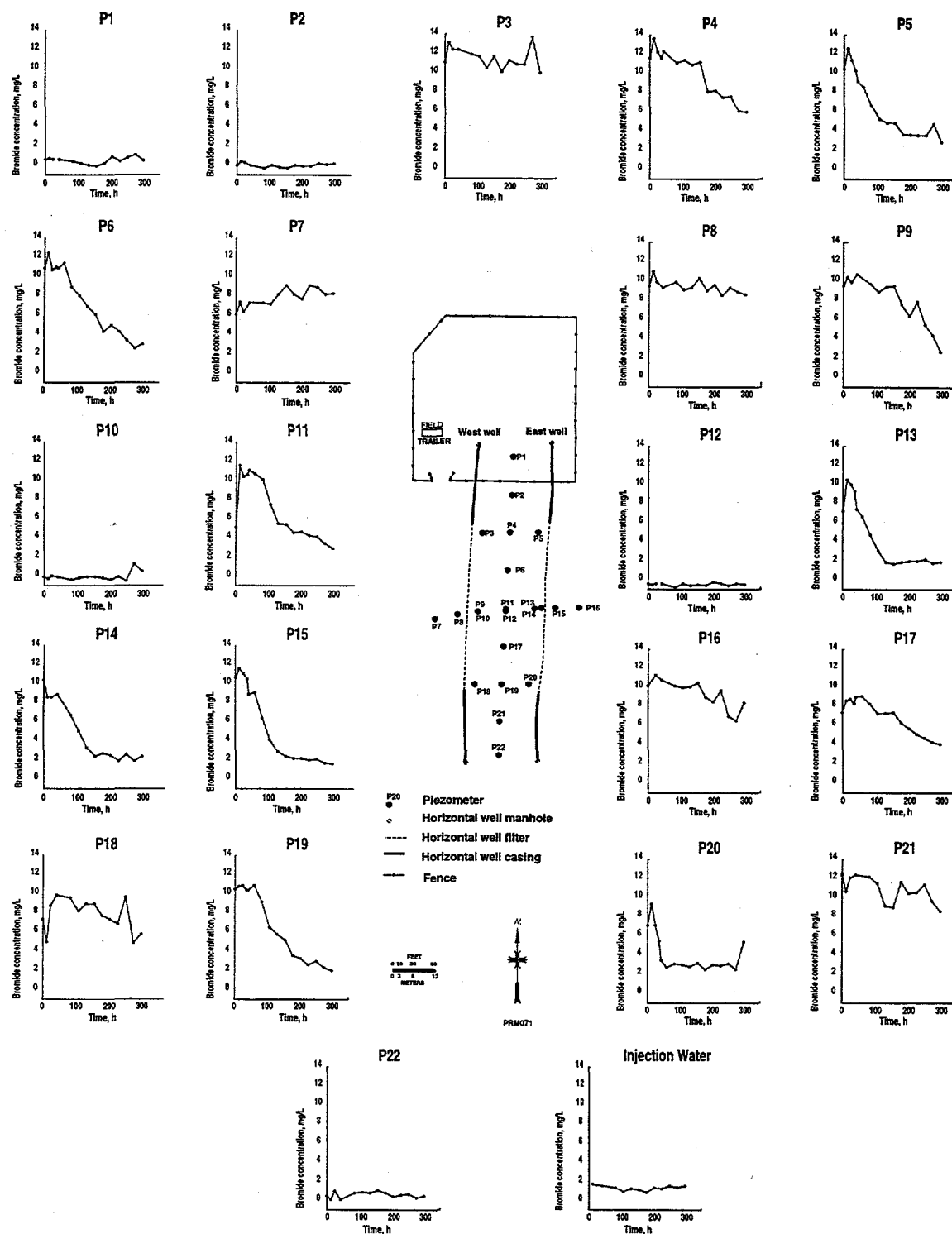


Fig. 7.1. Bromide concentrations in individual piezometers during the elution test.



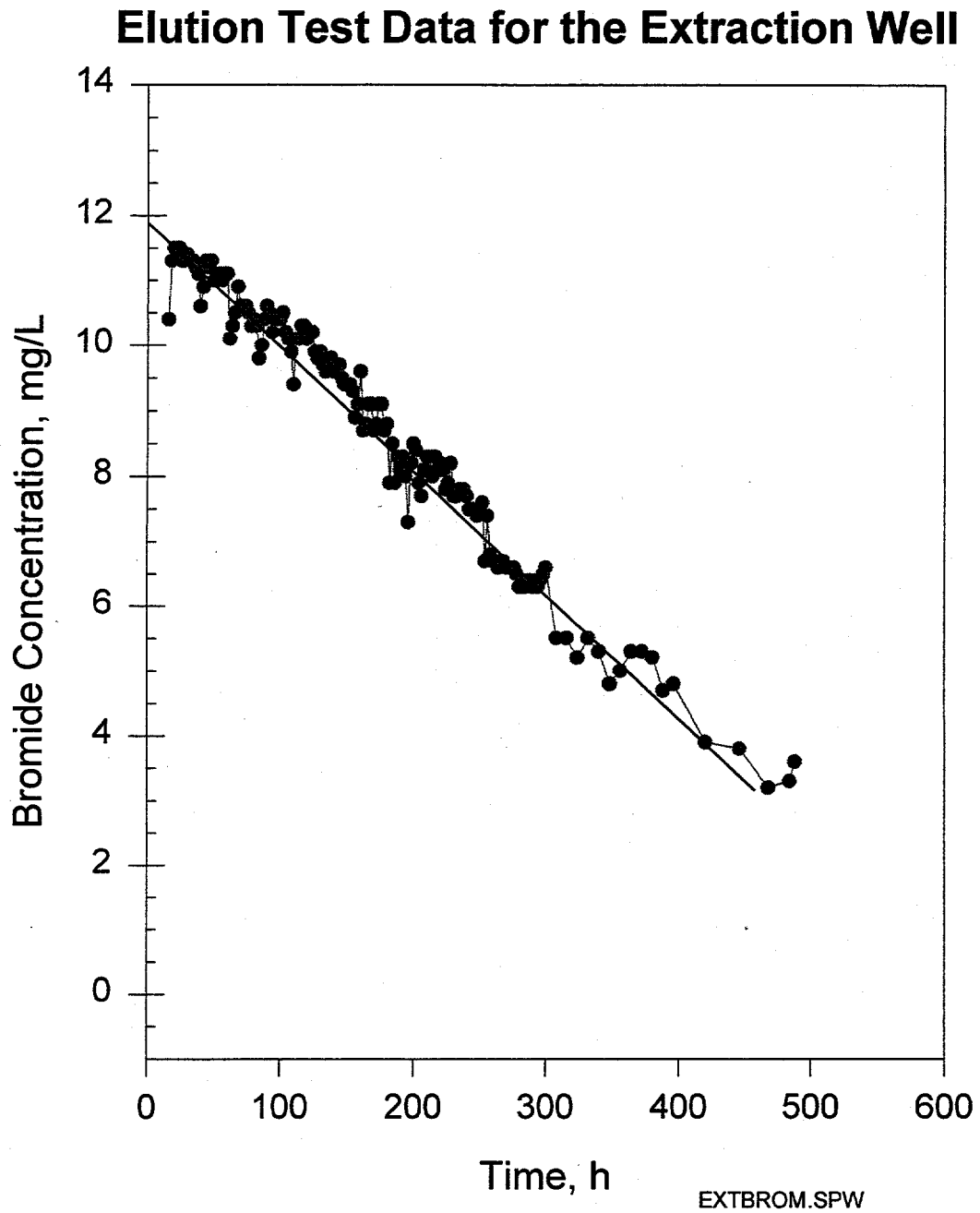


Fig. 7.2. Bromide concentrations in the horizontal extraction well during the elution test.

### Bromide Concentrations in Injection Water During Elution Test

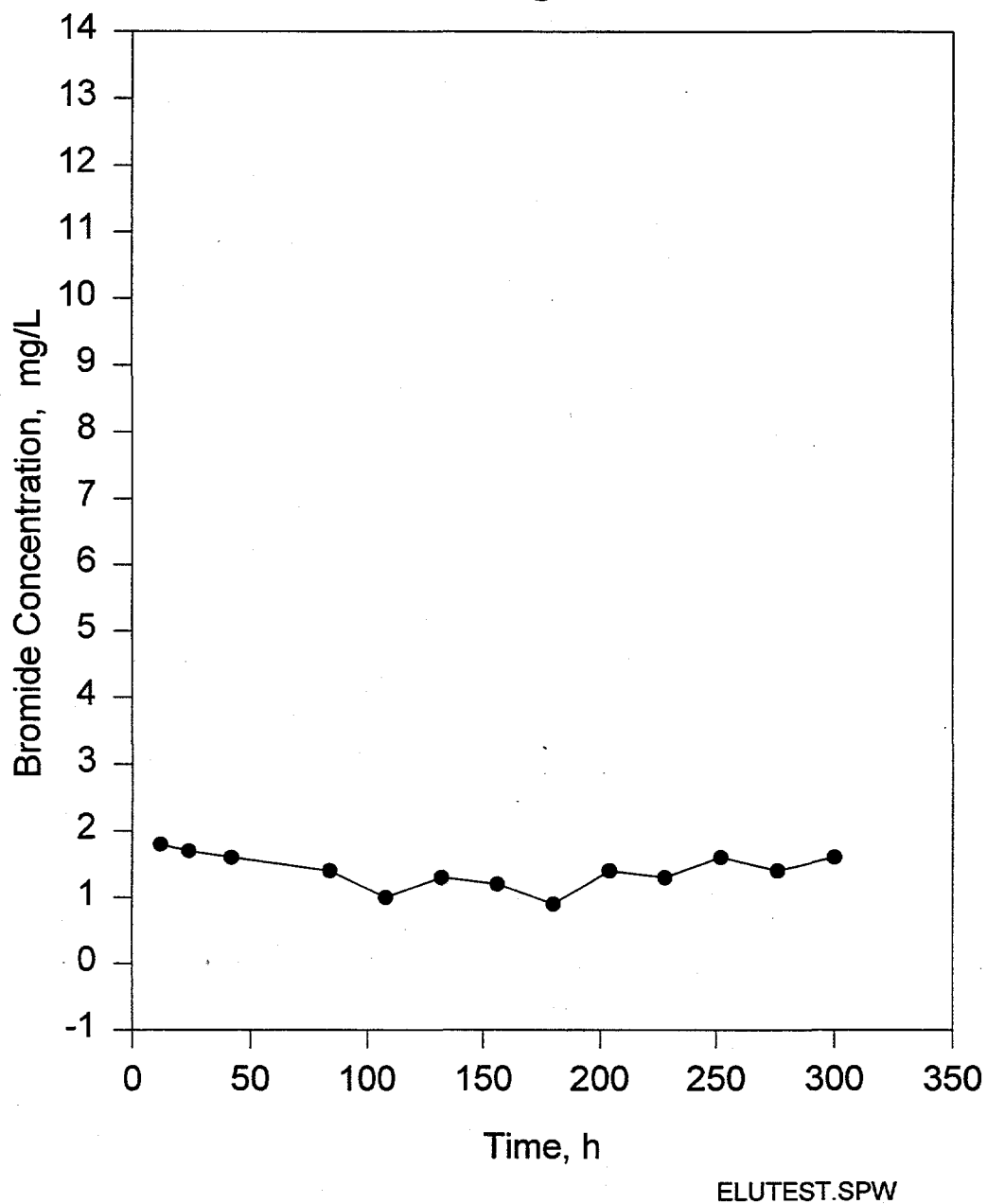


Fig. 7.3. Bromide concentrations in the fire-hydrant water during the elution test.

Table 7.1. Observations of bromide concentrations in piezometers during the elution test

Piezometer number	Formation	Average hydraulic K, cm/s ( $\times 10^{-4}$ )	Initial Br <sup>-</sup> , mg/L	Final Br <sup>-</sup> , mg/L	Comments
PZ-01	G	0.52	1	1	No initial Br <sup>-</sup> ; no change during test
PZ-02	G	0.28	0	0	No initial Br <sup>-</sup> ; no change during test
PZ-03	G	3.5	11	10	Little, if any, decrease in Br <sup>-</sup>
PZ-04	G	10	12	6	Moderate decrease in Br <sup>-</sup> (from 12 to 6 mg/L in 12 days)
PZ-05	G	9.0	11	3	Rapid decrease in Br <sup>-</sup> (from 11 to 5 mg/L in four days), then slow decrease in Br <sup>-</sup> (from 5 to 3 mg/L in eight days)
PZ-06	G	36	11	3	Rapid decrease in Br <sup>-</sup> (from 11 to 3 mg/L in ten days), then constant Br <sup>-</sup> at 3 mg/L
PZ-07	G	5.5	6	8	Slight increase in Br <sup>-</sup>
PZ-08	G	9.7	10	9	Little, if any, decrease in Br <sup>-</sup>
PZ-09	G	56	10	3	A delay of three days, followed by moderate decrease in Br <sup>-</sup> (from 10 to 3 mg/L in nine days)
PZ-10	M	0.20	0	1	No initial Br <sup>-</sup> ; no change during test
PZ-11	G	0.069	12 <sup>a</sup>	3	Rapid decrease in Br <sup>-</sup> (from 12 to 5 mg/L in seven days), then slow decrease in Br <sup>-</sup> (from 5 to 3 mg/L in five days)
PZ-12	M	0.32	0	0	No initial Br <sup>-</sup> ; no change during test
PZ-13	G	3.5	7	2	Rapid decrease in Br <sup>-</sup> (from 11 to 2 mg/L in five days), then constant Br <sup>-</sup> at 2 mg/L

Table 7.1. (continued)

Piezometer number	Formation	Average hydraulic K, cm/s ( $\times 10^{-4}$ )	Initial Br <sup>-</sup> , mg/L	Final Br <sup>-</sup> , mg/L	Comments
PZ-14	M	0.21	10	2	Rapid decrease in Br <sup>-</sup> (from 10 to 3 mg/L in five days), then fairly constant Br <sup>-</sup> at 2 to 3 mg/L
PZ-15	G	0.41	11	2	Rapid decrease in Br <sup>-</sup> (from 11 to 2 mg/L in six days), then constant Br <sup>-</sup> at 2 mg/L
PZ-16	G	4.6	10	8	Slow decrease in Br <sup>-</sup> (from 10 to 8 mg/L in 12 days)
PZ-17	G	32	7	4	Slow decrease in Br <sup>-</sup> (from 7 to 4 mg/L in 12 days)
PZ-18	G	3.5	7	6	Little, if any, decrease in Br <sup>-</sup>
PZ-19	G	39	11	2	A delay of one day, followed by a rapid decrease in Br <sup>-</sup> (from 11 to 3 mg/L in seven days), then a slow decrease in Br <sup>-</sup> (from 3 to 2 mg/L in four days)
PZ-20	G	11	7	5	Rapid decrease in Br <sup>-</sup> (from 7 to 3 mg/L in three days), then constant Br <sup>-</sup> at 3 mg/L (except for last sample, at 5 mg/L)
PZ-21	G	2.6	12	9	Slow decrease in Br <sup>-</sup> (from 12 to 9 mg/L in 12 days)
PZ-22	G	1.5	1	1	No initial Br <sup>-</sup> ; no change during test

G = Gallia  
M = Minford

a = The second groundwater sample from PZ-11 with a bromide concentration of 12 mg/L is considered more representative of initial conditions than the first groundwater sample with a bromide concentration of 5 mg/L.

Note: The fire-hydrant source of injection water during the elution test contained a bromide concentration of 1 to 2 mg/L. This is considered the background bromide concentration when interpreting the elution test results.

- Of the three piezometers close to the extraction well and within the flow field between the wells (PZ-03, PZ-09, and PZ-18), a much greater elution of bromide was observed in PZ-09. Little, if any, decrease in bromide concentrations occurred in PZ-03 and PZ-18. These observations are consistent with the tracer test results that indicated a preferential flow zone in the area of PZ-09 and a low-flow zone in the area of PZ-03.
- The moderate to rapid decreases in bromide concentrations in PZ-04, PZ-05, PZ-06, PZ-09, PZ-19, and PZ-20 are consistent with the relatively high hydraulic conductivity values determined from these piezometers (Table 7.1) and the preferential flow zones discussed in Sect. 6.
- Little, if any, decrease in bromide concentration occurred in PZ-08. This observation is consistent with the observation during the tracer test that this piezometer lies outside of the main flow field. Changes in bromide concentrations in this area are diffusion controlled.
- Consistent with the tracer test observations, no bromide was observed in the Minford piezometers PZ-10 and PZ-12, indicating that this unit is not in direct hydraulic communication with the underlying Gallia. As with the tracer test, the rapid decrease in bromide concentration in the Minford piezometer PZ-14 is attributed to the unique sand zone noted in the geologic log for this piezometer and the close proximity of PZ-14 to the horizontal injection well.
- The rapid decrease in bromide concentrations in PZ-13 and PZ-15 is attributed to the close proximity of these piezometers to the injection well. A rapid response to the injection of tracer was also observed in these piezometers due to the limited time available for hydrodynamic dispersion and diffusion to spread and dilute the tracer (Sect. 6). Changes in bromide concentrations in this area are controlled primarily by advection.
- The slow elution of bromide observed in PZ-16 is consistent with the observation during the tracer test that this piezometer lies outside of the main flow field. Changes in bromide concentrations in this area are diffusion-controlled.
- Consistent with the tracer test results, elution of bromide from PZ-21 occurred slowly, and no bromide was detected in PZ-22. These piezometers lie south of the horizontal well filters and outside of the main flow field. Changes in bromide concentration in the area of PZ-21 are diffusion-controlled.

Final bromide concentrations were in the range of 2 to 3 mg/L in PZ-05, PZ-06, PZ-09, PZ-11, PZ-13, PZ-14, PZ-15, PZ-19, and PZ-20. This range of concentrations is close to the background concentration in the injected water. As described above, these piezometers are located in the preferential flow zones between the wells and the area adjacent to the injection well. Bromide transport was dominated by advection in these areas, such that bromide concentrations during the elution test dropped rapidly to near-background levels. The stabilization of bromide concentrations at 2 to 3 mg/L in PZ-05, PZ-09, PZ-11, and PZ-19

indicates a transition to diffusion-dominated transport of bromide in these areas. If no bromide were present in the injected water, further reductions in bromide concentrations would occur slowly over an extended period of time.

Transport of bromide was dominated by diffusion in the areas outside of the preferential flow zones and at a distance from the injection well as shown by the elution test data for PZ-03, PZ-07, PZ-08, PZ-16, PZ-17, PZ-18, and PZ-21. Because bromide elution either occurred slowly or was not evident in these areas, bromide concentrations did not approach background levels during the time period of this test. If the elution test had been of longer duration, it is expected that bromide concentrations would have slowly declined to near-background concentrations in this set of piezometers.

Figure 7.2 presents bromide data for the horizontal extraction well and indicates a trend of decreasing bromide concentration as a function of time. Across the 20-day period of the test, bromide concentrations in the extraction well steadily decreased from an initial concentration of approximately 12 mg/L to a final concentration of approximately 3 mg/L. Linear regression of the extraction well data using the least squares method yielded the following relationship between bromide concentration and time:

$$Y = -0.0188 X + 11.7$$

where

$$\begin{aligned} Y &= \text{bromide concentration in the extraction well effluent, mg/L} \\ X &= \text{time, h} \end{aligned}$$

The correlation coefficient ( $r$ ) for this data set is  $-0.987$ , indicating a linear relationship between bromide concentration and time. (A perfectly linear relationship would yield  $r = -1.0$ , compared with  $r = 0.0$  for a non-linear relationship.) This linear relationship suggests that bromide elution from the recirculation flow field was dominated by advection during the time period of the test. If the elution test had been of longer duration, it is expected that bromide concentrations would have gradually stabilized at near-background concentrations of 2 to 3 mg/L as bromide transport became dominated by diffusion.

This transition from advection- to diffusion-dominated transport is often observed in pump-and-treat groundwater systems and soil-vapor-extraction systems in which contaminant concentrations drop rapidly at first and then slowly with time (U.S. EPA 1989a, 1989b). The transition to diffusion-dominated transport limits the effectiveness of these systems because long-term operation provides only a slight reduction in the remaining contaminant mass. Of interest is the short-term reduction in contaminant mass provided during advection-dominated transport. The mass of bromide removed from the recirculation flow field by advection-dominated transport can be estimated by calculating the area under the line on Fig. 7.2 (units of mg/L/h) and multiplying by the rate of extraction (units of L/h).

During the first 282 h of the elution test, the bromide concentration in the extracted groundwater dropped from approximately 12 to 6 mg/L, with a flow rate of 1,820 L/h (48 gal/h). During the final 192 h of the elution test, the bromide concentration in the extracted groundwater dropped from approximately 6 to 3 mg/L, with a flow rate of 1,360 L/h (40

gal/h). The combined mass removal of bromide for the duration of the test was approximately 5.8 kg (13 lb). From Table 6.1, the mass of bromide injected into the recirculation flow field during the tracer test was approximately 6.4 kg (14 lb) [3,396 mg/L in a solution volume of 1,890 L (50 gal)]. Using an average bromide concentration of 1.4 mg/L for the injected fire-hydrant water, approximately 1.1 kg (2.4 lb) of bromide was injected into the recirculation flow field during the elution test. This gives a total of approximately 7.5 kg (16.5 lb) of bromide that was injected into the system. By comparing this mass to the mass of bromide removed, the bromide mass reduction during the elution test was approximately 77%.

These calculations suggest that, in the absence of adsorption, approximately three-quarters of a fluid injected into the Gallia will be transported in a timely fashion by advection. One quarter will be lost by diffusion into lower-permeability material or will escape from hydraulic containment. It is likely that diffusive losses would decrease with time as the solution concentration in lower-permeability sediments equilibrated with the solution concentration in the preferential flow zones.

These results also suggest that a horizontal well recirculation system in a contaminated area of the Gallia at PORTS may be capable of extracting 75% of the dissolved contaminant mass in a short period of time (assuming a recirculation flow system similar to the one at the CTS; a contaminant solute that behaves conservatively, in a manner similar to bromide; and an advection-dominated transport period of approximately one month). As a note of caution, in a groundwater system that is contaminated by dense nonaqueous-phase liquid (DNAPL), the dissolved portion of the contaminant mass typically represents a very small fraction of the total contaminant mass. Mobilization of the DNAPL into the recirculation flow field would be necessary to effect a large reduction in the total contaminant mass. This might be accomplished through the use of surfactants or other methods to increase the proportion of contaminant mass that is dissolved in the contaminated groundwater.

## 8. Development of the Horizontal Wells

### 8.1 Introduction

As described in Sects. 5.5, 6.6, and 7.1, performance of the extraction well (west horizontal well) deteriorated due to well clogging during long-term operation. The sustainable pumping rate dropped from 76 L/min to 23 L/min (20 gal/min to 6 gal/min) during an operating period of 53 days. This decline was due to clogging of the porous filter in the extraction well. No significant pressure increase was observed during the injection of water into the east horizontal well, suggesting that clogging was not a problem for the east horizontal well.

Initially, three possible mechanisms were considered to be responsible for the clogging. These mechanisms included mineral precipitation in the well filter, biofouling due to iron bacteria, and skin effects due to clayey material in the surrounding porous media. Laboratory tests using water pumped through a core section of the Gallia member and a cross section of porous well filter yielded iron oxide deposits. These deposits were analyzed and found to be goethite ( $\text{FeO}(\text{OH})$ ). Once dried, the goethite precipitate was friable but relatively insoluble. The log of the equilibrium constant ( $K_{eq}$ ) for goethite is -42, indicating a very low solubility (Drever 1988).

During September 1995, water samples were collected from the extraction well and analyzed for bacteria. Iron related bacteria were found to be present in the water samples. These bacteria included *klebsiella*, *pseudomonads*, and *enterobacter*. Well clogging due to iron bacteria is common in the larger water-producing aquifers in the region.

Clogging of the formation surrounding the porous well filter is the remaining mechanism that was considered. Based on recommendations from the porous filter manufacturer, the wells were pumped for development. No mechanical or chemical development was performed on the wells. The concern with the recommended development method is that fines remaining in the formation surrounded the porous well filter and formed a low-permeability skin that reduced the hydraulic efficiency of the horizontal extraction well.

### 8.2 Field Program

During October 1995, field personnel from ORNL-Grand Junction developed the horizontal wells using a water-jetting method. Prior to development, pumping tests were performed on the extraction well to provide a baseline of well performance. The well was pumped at a rate of 38 L/min (10 gal/min), and the water level in the horizontal well dropped below the pump intake after 32 min. Following a 3-h recovery period, the well was pumped at a reduced rate of 28 L/min (7.5 gal/min) for 72 min before the water level dropped below the pump intake.

Also prior to development, a borehole video camera was used to inspect the porous well filter and casing in both of the horizontal wells. A frontal mirror on the video camera allowed viewing of the side walls. Another video inspection was performed after the completion of well development to visually assess the effects of well development.



Based on the laboratory test results, the well development program included both mechanical and chemical treatment. Mechanical development consisted of water jetting and overpumping. Driscoll (1979) presents data that indicate water jetting and overpumping are upwards to 40% more efficient than other well development methods such as surging. A specially designed eight-nozzle jetting tool with a discharge velocity exceeding 30.5 m/s (100 ft/s) per nozzle was used to mechanically agitate the porous well filter and the adjacent formation. A submersible pump on the opposite end of the horizontal well was pumped at the maximum allowable rate to remove sediment from the well. Three full days of jetting and overpumping were performed on each of the horizontal wells.

After jetting and overpumping, the horizontal wells were shock chlorinated to kill iron bacteria. Calcium hypochloride was mixed with 1,890 L (500 gal) of water to yield a chlorine solution that exceeded 1,000 mg/L. The solution was injected using the jetting tool along the entire length of the well filter until all 1,890 L (500 gal) were injected. The process was repeated for the remaining horizontal well. The chlorine was allowed to remain overnight in the horizontal wells. The following morning, the wells were jetted and overpumped. Excess chlorine removed from the wells was neutralized using a mixing tank with sodium sulfite. Well jetting and overpumping continued for another two days after shock chlorination.

After completion of the well development, pumping tests were performed on both of the horizontal wells and the results were compared with the earlier pump tests conducted prior to the tracer tests. These data were used to assess the effectiveness of the well development program.

### 8.3 Development Results

The video survey conducted prior to development yielded some unexpected results. The horizontal extraction well, which had shown a significant decrease in yield, showed little evidence of clogging. A fine layer of sediment was located on the bottom of the well filter, but there was no evidence of microbial problems or incrustations on the well filter. The appearance of the injection well, however, was very different. A thick layer of gelatinous material coated the well filter on all sides. This material appeared to be organic in nature. The well filter openings were approximately 50% clogged with this material, yet the injection well showed no pressure increases during operation that would indicate a clogging problem.

Large amounts of sediment were removed during the well development process. Clay particles were the dominant size fraction observed in the discharge water. There was a distinct difference in the sediment type yielded by the two horizontal wells. The horizontal extraction well showed dark grey clayey material typical of the Sunbury shale, while the horizontal injection well showed reddish, clayey material typical of the iron-stained Gallia member. This is consistent with the completion designs of the wells. Although both wells are located along the contact of the Sunbury and Gallia, a large portion of the extraction well filter is completed partially into the Sunbury. The injection well is completed entirely within the Gallia member.

The jetting tool injected water over 15-cm (6-in) intervals and agitated the surrounding formation with a surging action. This small interval yielded enough sediment to cloud the entire discharge from 70 m (230 ft) of well filter. This observation suggests that significant quantities of sediment were removed from the wells. However, the amount of sediment did not decrease after three days of jetting, further suggesting that only a portion of the fine-grained material surrounding the well filter was removed by the development process.

After shock chlorination and additional development, two series of pumping tests were conducted to evaluate the effectiveness of the development program. The first series of tests consisted of individual 12-h duration pumping tests for each of the horizontal wells. The west horizontal well maintained a flow rate of 43 L/min (11.4 gal/min) and the east horizontal well maintained a flow rate of 34 L/min (9 gal/min). This compares favorably with the individual pumping tests conducted immediately after the well installation at a rate of 46 L/min (12 gal/min) for each of the wells (Sect. 5.4). A notable improvement in the efficiency of the west well is also evident because the baseline pumping test conducted just prior to the water-jetting development program indicated that this well could yield 38 L/min (10 gal/min) for a period of only ½ h (Sect. 8.1).

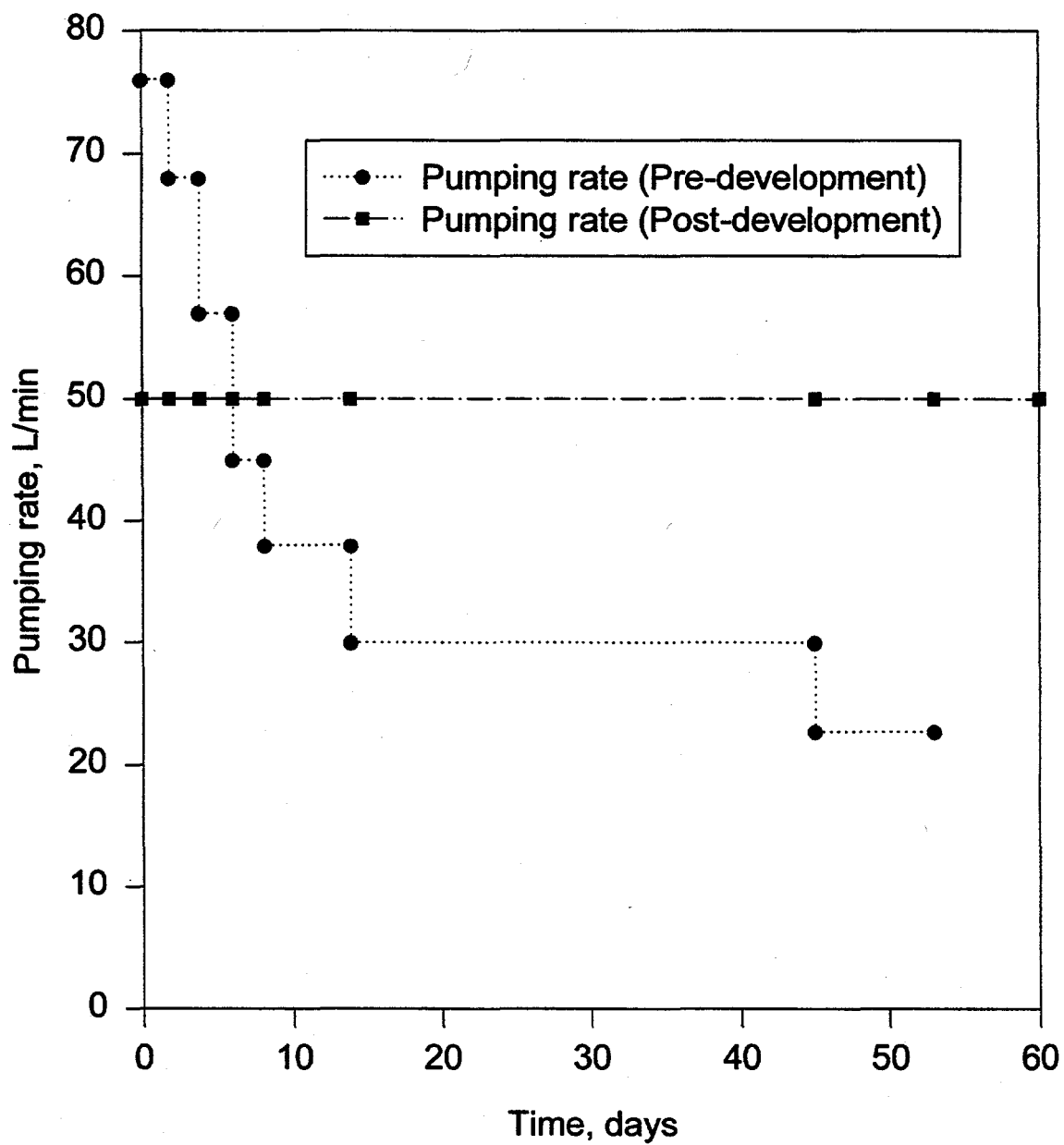
After the well development program, a dual-well pumping test was performed for 9 days at a recirculation rate of 57 L/min (15 gal/min) with a maximum drawdown of 1.8 m (5.8 ft). A hiatus in the field program at the CTS then occurred until September 1996. At this time, the recirculation system was operated continuously for a period of 60 days at a rate of 50 L/min (13 gal/min), with no deterioration in the performance of the extraction well. Results of the long-term recirculation test are presented in Fig. 8.1. The pumping rate as a function of time for the post-development test is compared to the declining pumping rate observed during the tracer test and elution test. It was possible to maintain a 50 L/min (13 gal/min) rate after development, while during the tracer test and elution test the pumping rate declined from an initial rate of 76 L/min (20 gal/min) to 23 L/min (6 gal/min) due to well clogging. Figure 8.1 shows that the developed horizontal extraction well maintained a consistent pumping rate with no indication of clogging.

#### 8.4 Discussion

Based on the results of the well development program, it appears that fine-grained material in the formation was responsible for clogging the porous well filter and decreasing the well efficiency. Well development using jetting and overpumping significantly increased the efficiency of the horizontal wells.

Development recommendations by the filter manufacturer of low flow pumping until clear water is obtained are not appropriate for fine-grained heterogeneous formations like the Gallia member. Similar to vertical wells, horizontal wells must be mechanically and/or chemically developed to produce and maintain adequate quantities of water.

## Extraction Well



prm001.spw

Fig. 8.1. Comparison of the horizontal recirculation rate, pre- and post-development.

An initial concern of the well development process was that the porous well filter would act as a diffuser thus decreasing agitation of the surrounding formation by the water jets. Based on the development results, it is possible to agitate the surrounding formation. This agitation does appear to be limited considering that the larger particle-size fraction is not removed during the development process.

A preventative program is recommended to reduce the development of bacterial growth in the injection well. Although no increases in injection pressures were observed during operation, it is expected that eventually the bacteria will clog the injection well. It possible to continually inject low concentrations of chlorine directly into the injection well to prevent bacterial growth.

The water-jetting and overpumping development technique generated significant quantities of water. Approximately 18,900 L (5,000 gal) of water was generated each day during well development. For a contaminated area, onsite treatment may be necessary to handle the large quantity of contaminated development water.

## 9. Conclusions

This report presents the results of field testing a horizontal well recirculation system at the CTS at PORTS. The recirculation system uses a pair of horizontal wells, one for groundwater extraction and the other for reinjection, to set up a recirculation flow field. The two horizontal wells were installed in October 1994 at a depth of 9 m (30 ft) using a directional drilling rig. The horizontal sections of the wells are 70 m (230 ft) long and were placed along the bedrock surface at the base of the Gallia member, a 0.6 to 2 m (2 to 6 ft) thick zone of moderately permeable, unconsolidated fluvial deposits. The wells were placed with a vertical accuracy of  $\pm 15$  cm ( $\pm 0.5$  ft). The horizontal sections were constructed with ductile porous filter, an innovative well material produced in Germany by Schumacher. This was the first installation and testing of this well filter material in the U.S. The well filters have a pore size of 300  $\mu$ m and are composed of sintered spheres of HDPE. Drilling and installation of the wells were completed in six days. A network of piezometers was also installed to assess the hydraulic influence of the horizontal well recirculation system on the surrounding groundwater flow field.

Hydraulic testing results for the horizontal well recirculation system indicate that the Gallia is a heterogeneous water-bearing zone. Single-well testing showed hydraulic conductivity values that varied by over two orders of magnitude in the Gallia member and indicated the presence of zones or channels of higher conductivity. Hydraulic tests of the horizontal well recirculation system showed that a hydraulic gradient of 0.15 could be induced between the wells, an increase of two orders of magnitude over the preexisting gradient. Under these conditions, water will travel approximately two orders of magnitude faster than under ambient conditions, with only permeability controlling groundwater flow velocities between the horizontal wells.

A bromide tracer test showed that the entire flow field between the wells was affected by the recirculation system, with bromide transport dominated by advection in higher-permeability areas and by diffusion in lower-permeability areas. A follow-on elution test provided removal of approximately 77% of the injected bromide mass during a period of 20 days. The tracer test and elution test results indicate that the horizontal well recirculation system shows great promise for application at a contaminated site.

Comparing colloidal borescope velocity measurements with tracer test results provides some interesting relationships. The tracer test showed that bromide reached the extraction well 21 h after being introduced into the injection well. Using the highest observed hydraulic conductivity for the entire facility of  $1.8 \times 10^{-2}$  cm/s (50 ft/d), an assumed porosity of 0.20, and neglecting dispersion, it would take 2.6 days for the tracer to reach the extraction well. However, the velocity measured in PZ-06 of 0.037 cm/s (105 ft/d) yields an initial breakthrough resulting from preferential flow zones of approximately 23 h, similar to the time measured by the tracer.

If the velocities of 0.0122 and 0.013 cm/s (35 and 37 ft/d) measured in PZ-19 and PZ-09 represent the average seepage velocity in the area between the recirculation wells under pumping conditions, this would result in a predicted breakthrough time of approximately 2.8

days. This value is in excellent agreement with the first bromide peak in the horizontal extraction well of approximately 2.6 days.

Clogging of the extraction well filter during the tracer test and elution test resulted in deterioration of well performance. It was determined that the method of well development recommended by the filter manufacturer, low rate pumping, was inadequate. During the fall of 1995, the horizontal wells were developed by a more aggressive method that included water jetting and overpumping. Hydraulic tests conducted immediately after well development showed markedly improved well performance. During the fall of 1996, a 60-day recirculation test was performed with no evidence of clogging. These results indicate that water jetting and overpumping is the proper method for developing wells constructed with the ductile porous filter.

Additional work at PORTS includes field testing of the horizontal well recirculation system at X-701B, a site with TCE and technetium groundwater contamination (ORNL 1995). During this field test, a groundwater treatment system will be linked with the horizontal well recirculation system to test the effectiveness of the recirculation system for groundwater treatment. A description of the treatment system and the results of the pilot test will be presented in a separate report after completion of the test.

## 10. References

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## **Appendix A**

### **Geologic Logs and Geotechnical Data for Boreholes at the Clean Test Site**

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# Borehole Summary Information

## OAK RIDGE NATIONAL LABORATORY

Prepared By: C.A. Muhr	Date: 3/22/94	Page: 1 OF 1
Hole No.: BH01	Ground Elevation:	
Total Depth: 28.5' Rig Type: CME 55	Location: CSTA NE Corner	
Auger Size: 6.25" O.D.	Sample Type: 5' Continuous Barrel	
Project: CSTA Prelim Sampling	Data Verified By: M.E. Mumby	Date: 4/5/94

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	LITHOLOGY	DESCRIPTION
0				Humus soil, saturated, standing water on surface.
2	CS			OL CLAYEY SILT: yellowish brown (10YR 5/8) mottled with gray (10YR 5/1) silt, blocky, saturated to approximately 8", moist to 5", numerous root hairs.
4				
6	CS			CL SILTY CLAY: yellowish brown (10YR 5/8) with a light brownish gray (10YR 6/2) mottle, firm to very firm, moist, slightly calcareous from 7.0 to 7.3'.
8				
10				
12	CS			ML SILT: light brownish gray (10YR 6/2), firm, moist, 11.8 to 12'.
14				CL SILTY CLAY: yellowish brown (10YR 5/6), common lenses of gray (10YR 6/1) silt to clayey silt, firm to very firm, slightly moist, increasing black MnO staining or organic debris.
16				SM SILTY SAND: yellowish brown (10YR 5/6) to gray (10YR 6/1), fine to very fine grained, dry to slightly moist.
18	CS			ML SILT: yellowish brown (10YR 5/4-5/6), moist, occasional very fine grained sandstone pebbles scattered MnO staining.
20				Driller reported water table at approximately 20', no indications of water in sample.
22	CS			
24	SP			Note: Due to drilling conditions, changed from continuous sampler to 2 foot split spoon sampler at 23'.
26	SP			ML SILT: as above with occasional angular to sub-angular gravels to 4cm.
28	SP			SM SILTY SAND: gray (5Y 5/1) with a light olive gray (5Y 6/2) mottle, fine to very fine grained, micaceous, moist becoming wet by 28', common pebbles and gravels from 28.3 to 28.5'.
30				
32				T.D. 28.5'.

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# Borehole Summary Information

OAK RIDGE NATIONAL LABORATORY

Prepared By: C. A. Muhr Date: 3/23/94 Page: 1 OF 1  
 Hole No.: BH02 Ground Elevation: \_\_\_\_\_  
 Total Depth: 29.2' Rig Type: CME 55 Location: CSTA SE Corner  
 Auger Size: 6.25" O.D. Sample Type: 5' Continuous Barrel  
 Project: CSTA Prelim Sampling Data Verified By: M.E. Mumby Date: 4/5/94

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	LITHOLOGY	DESCRIPTION
0				Organic rich soil 0-1'. dark yellowish brown.
2	CS			CL/OL CLAYEY SILT: yellowish brown (10YR 5/6) with a gray (10YR 6/1) silty clay mottle, firm, slightly moist, blocky, scattered limonite staining, decreasing moisture below 2'.
4				
6				
8	CS			CL CLAYEY SILT: as above, occasional light gray, subrounded, sandstone and siltstone pebbles ranging in size from 1 to 3cm. common MnO staining.
10				
12	CS			SM SILTY SAND: yellowish brown (10YR 5/8), abundant limonite staining, decreasing MnO staining becoming absent by 11.5'. moist, scattered sandstone and siltstone pebbles.
14				
16				
18	CS			SM SILTY SAND/SANDY SILT: color as above, moist, decreasing sandstone and siltstone pebbles.
20				Driller reports water table at approximately 19', water observed on sampler at that depth.
22	CS			SM SILTY SAND: yellowish brown to dark yellowish brown, firm, wet, abundant limonite staining, no pebbles observed.
24	SP			SM SILTY SAND: yellowish brown to dark reddish brown (10YR 5/8-5YR 3/2), wet, increasing pebbles and gravel especially right above the bedrock contact.
26	SP			No Recovery from 25 to 27'. probable silty sand as above.
28	SP			SM SILTY SAND: as above with common pebbles and gravels increasing right above bedrock contact.
30				Top of Bedrock 28.5' (Sunbury Shale).
32				SHALE: dark gray to black, carbonaceous.

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# Borehole Summary Information

OAK RIDGE NATIONAL LABORATORY

Prepared By: C.A. Muhr		Date: 3/23/94		Page: 1 OF 1	
Hole No.: BH03		Ground Elevation:			
Total Depth: 19.2' Rig Type: CME 55		Location: CSTA SW Corner			
Auger Size: 6.25" O.D.		Sample Type: 5' Continuous Barrel			
Project:		Data Verified By: M.E. Mumby		Date: 4/5/94	

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	LITHOLOGY	DESCRIPTION
0				Organic rich soil 0-1'. dark yellowish brown (10YR 4/6), saturated to .8', moist below
2	CS			CL/OL SILTY CLAY: yellowish brown (10YR 5/6) with a gray (10YR 6/1) silty clay mottle, firm, slightly moist, blocky, abundant limonite staining, common black organic material.
4				
6	CS			CL CLAYEY SILT: light brownish gray (10YR 6/2) with a light yellowish brown (10YR 6/4) mottle, very firm, moist, decreasing limonite and organic staining.
8				
10				CL CLAY: reddish brown (5YR 4/4), stiff, dense, moist, traces of light green clay interbedded throughout interval.
12	CS			CL CLAY: light gray (5YR 6/1) and reddish brown (5YR 4/4), mottled, very firm, moist.
14				SM SILTY SAND: yellowish brown (10YR 5/6), medium to fine grained, saturated.
				CL SILTY CLAY: brownish yellow (10YR 6/8), moist.
16				SM SILTY SAND: as above.
	CS			CL SILTY CLAY: gray (10YR 5/1), homogeneous, wet.
18				
				GM SILTY GRAVEL: dark gray (10YR 4/1), angular to sub-angular gravels to 4cm, saturated.
20				
22				Auger refusal at 19.2'.

orn1

OAK RIDGE NATIONAL LABORATORY

Borehole Summary Information

Prepared By: C.A. Muhr Date: 3/23/94 Page: 1 OF 1  
 Hole No.: BH04 Ground Elevation:  
 Total Depth: 23.2' Rig Type: CME 55 Location: CSTA  
 Auger Size: 6.25" O.D. Sample Type: 5' Continuous Barrel  
 Project: CSTA Prelim. Sampling Data Verified By: M.E. Mumbv Date: 4/5/94

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	LITHOLOGY	DESCRIPTION
0				Organic rich soil 0-.5'. dark brown .
2	CS			CL SILTY CLAY: yellowish brown (10YR 5/8) with a gray (10YR 5/1) mottle. firm, slightly moist. lesser amounts of gray clay than seen in boreholes 1, 2, and 3. common black organic stain present from 3 to 4'.
4				
6	CS			
8				CL SILTY CLAY: yellowish brown (10YR 5/4) with a gray (10YR 5/1) mottle. moist. noticeable root fibers and possible MnO stain. scattered light brown siltstone gravels from 9-9.5'.
10				
12	CS			CL CLAY: reddish brown (5YR 4/4) with a gray (10YR 5/8) mottle. stiff, moist, dense. sharp contact above and below. mineralized zone 1-2mm on basal contact.
14				
16				CL SILTY CLAY: yellowish brown (10YR 5/6) with a gray (10YR 5/1) mottle. dense, moist.
18	CS			SP SAND: yellowish brown (10YR 5/6). medium to fine grained. angular. common iron staining. wet. common interbedded red (2.5YR 3/6) clay.
20				ML CLAYEY SILT: yellowish brown (10YR 5/4) with a gray (10YR 5/1) mottle. wet.
22	CS			ML CLAYEY SILT: light gray (10YR 6/1). wet.
24				GM GRAVEL: dark gray. sand/silt matrix. wet. dark gray matrix is possibly derived from weathering of the Sunbury Shale. Auger Refusal at 23.2'.

orn1

# Borehole Summary Information

OAK RIDGE NATIONAL LABORATORY

Prepared By: C. A. Muhr Date: 3/24/94 Page: 1 OF 1  
 Hole No.: BH05 Ground Elevation: \_\_\_\_\_  
 Total Depth: 24.2' Rig Type: CME 55 Location: CSTA  
 Auger Size: 6.25" O.D. Sample Type: 5' Continuous Barrel  
 Project: CSTA Prelim. Sampling Data Verified By: M. E. Mumby Date: 4/5/94

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	LETHOLOGY	DESCRIPTION
0				Organic humus, 0-1'.
2	CS			CL SILTY CLAY: yellowish brown (10YR 5/8) with a gray (10YR 5/1) mottle, firm, slightly moist, common black organic stain.
4				
6				
8	CS			CL SILTY CLAY: yellowish brown (10YR 5/4) with a gray (10YR 5/1) mottle, moist, abundant limonite staining.
10				
12				CL CLAYEY SILT: as above.
14	CS			CL CLAY: reddish brown (5YR 4/4) with a gray (10YR 5/8) mottle, stiff, moist, dense, fairly sharp contact above and below.
16				
18	CS			CL CLAYEY SILT: brownish yellow (10YR 6/6), firm, moist, abundant limonite staining with small zones of iron mineralization, mineralized zones are friable to some degree.
20				SM SILTY SAND: brownish yellow (10YR 6/8), common gravels and pebbles up to 4cm, abundant limonite stain, wet.
22	CS			ML SILT: brownish yellow (10YR 6/6), wet, grading to a fine grained silty sand.
24				SM SILTY SAND: brownish yellow (10YR 6/6), wet, common gravel.
26				T.D. 24.2' Auger Refusal. Sampler contained approximately 1cm of olive sandstone bedrock.
28				
30				

orn1

OAK RIDGE NATIONAL LABORATORY

Borehole Summary Information

Prepared By: C.A. Muhr Date: 3/24/94 Page: 1 OF 1  
 Hole No.: BH06 Ground Elevation: \_\_\_\_\_  
 Total Depth: 30.0' Rig Type: CME 55 Location: CSTA  
 Auger Size: 6.25" O.D. Sample Type: 5' Continuous Barrel  
 Project: CSTA Prelim. Sampling Data Verified By: M.E. Mumby Date: 4/5/94

DEPTH (FEET)	SAMPLE TYPE	SAMPLE ID#	LITHOLOGY	DESCRIPTION
0				Organic dark brown soil 0-1'.
2	CS			CL SILTY CLAY: yellowish brown (10YR 5/8) with a gray (10YR 5/1) mottle, firm, slightly moist, common black organic stain, numerous root hairs to 4'.
4				
6				
8	CS			CL SILTY CLAY: yellowish brown (10YR 5/4) with a gray (10YR 5/1) mottle, moist, abundant roots and root hairs up to 1cm.
10				
12	CS			CL CLAYEY SILT: as above, increasing silt content right above red clay contact, very limonitic zone at 12.5'.
14				CL CLAY: reddish brown (5YR 4/4), moist, dense.
16				ML SILT: brownish yellow (10YR 6/6), moist, crumbly, grading to a silty sand with depth, occasional angular pebbles and gravels, traces of black organic stain at 19'.
18	CS			
20				
22	CS			SM SILTY SAND: light olive brown (2.5Y 5/6), fine grained, abundant limonite staining, scattered black organic or MnO stain, becoming wet at approximately 24'.
24				
26				
28	CS			GM SILTY GRAVEL: olive (5Y 4/4), angular to sub-angular sandstone gravels in a sandy silt matrix, abundant limonite stain, wet.
30				SHALE: black, carbonaceous. (Sunbury Shale) T.D. 30'.
32				
34				

ornl

# Borehole Summary Information

## OAK RIDGE NATIONAL LABORATORY

Prepared By: C. A. Muhr		Date: 3/24/94	Page: 1 OF 1
Hole No.: BH07		Ground Elevation:	
Total Depth: 30.0'		Rig Type: CME 55	Location: CSTA
Auger Size: 6.25" O.D.		Sample Type: 5' Continuous Barrel	
Project: CSTA Prelim. Sampling		Data Verified By: M.E. Mumby	Date: 4/6/94

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	LITHOLOGY	DESCRIPTION
0				Organic dark brown soil 0-.5'.
2	CS			CL SILTY CLAY: yellowish brown (10YR 5/8) with a gray (10YR 5/1) mottle, firm, slightly moist, common black organic stain.
4				
6	CS			CL SILTY CLAY: yellowish brown (10YR 5/4) becoming light gray to gray (10YR 7/1-6/1), moist, firm
8				CL CLAY: reddish brown (5YR 4/4), moist, dense, common MnO staining.
10				ML CLAYEY SILT: yellowish brown (10YR 6/6), moist, firm, sandy in part, common angular sandstone pebbles and gravels to 2.5cm.
12	CS			
14				
16	CS			ML CLAYEY SILT: as above, occasional rounded to subrounded pebbles to 2.5cm, grading to a silty sand at 20 to 21'.
18				
20				
22	CS			
24				SM SILTY SAND: light olive brown (2.5Y 5/4), mottled with a gray silt, fine grained, abundant limonite staining, moist, friable, no pebbles.
26				SM SILTY SAND: olive to olive yellow (5Y 5/4-6/6), moist becoming wet abundant angular to subangular pebbles.
28	CS			
30				SHALE: black, carbonaceous. (Sunbury Shale)
32				T.D. 30'.
34				



orn1

# Borehole Summary Information

OAK RIDGE NATIONAL LABORATORY

Prepared By: C.A. Muhr Date: 3/24/94 Page: 1 OF 1  
 Hole No.: BH08 Ground Elevation: \_\_\_\_\_  
 Total Depth: 24.0' Rig Type: CME 55 Location: CSTA  
 Auger Size: 6.25" O.D. Sample Type: 5' Continuous Barrel  
 Project: CSTA Prelim. Sampling Data Verified By: M.E. Mumby Date: 4/6/94

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	LITHOLOGY	DESCRIPTION
0				Organic dark brown soil 0-.5'.
2	CS			CL SILTY CLAY: yellowish brown (10YR 5/8) with a gray (10YR 5/1) mottle, firm, slightly moist, common black organic and limonite stain.
4				
6	CS			
8				CL SILTY CLAY: light brownish gray (10YR 6/2) with a light yellowish brown (10YR 6/4) clay mottle, moist, firm, common light olive silt nodules between 7.5 and 9.5'.
10				
12	CS			CL CLAY: yellowish brown, firm, moist, several interbedded lenses of yellow (10YR 7/2) silt, high plasticity.
14				CL CLAY: reddish brown (5YR 4/4), moist, dense, common MnO staining.
16				
18	CS			CL SILTY CLAY: yellowish brown (10YR 5/6) with a gray (10YR 5/1) silt mottle, firm, moist. SM SILTY SAND: brownish yellow, fine grained, saturated.
20				CL CLAY: dark gray (10YR 4/1), highly plastic, wet.
22	CS			GM SILTY GRAVEL: dark gray to olive gravels, saturated.
24				
26				
28				
30				T.D. 30'.

ornl

# Borehole Summary Information

OAK RIDGE NATIONAL LABORATORY

Prepared By: <u>C.A. Muhr</u>			Date: <u>3/24/94</u>	Page: <u>1 OF 1</u>
Hole No.: <u>BH09</u>			Ground Elevation: _____	
Total Depth: <u>25.0'</u>			Rig Type: <u>CME 55</u>	Location: <u>CSTA</u>
Auger Size: <u>6.25" O.D.</u>			Sample Type: <u>5' Continuous Barrel</u>	
Project: <u>CSTA Prelim. Sampling</u>			Data Verified By: <u>M.E. Mumby</u>	Date: <u>4/6/94</u>

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	LITHOLOGY	DESCRIPTION
0				Organic dark brown soil 0-1'.
2	CS			CL SILTY CLAY: yellowish brown (10YR 5/8) with a gray (10YR 5/1) mottle. firm, slightly moist. common black organic and limonite stain.
4				
6				
8	CS			
10				CL SILTY CLAY: yellowish brown (10YR 5/4) with a gray (10YR 5/1) silt to silty clay mottle. firm, moist. lower plasticity in zones with a higher silt content.
12	CS			
14				CL CLAY: reddish brown (5YR 4/4). moist. dense. common MnO staining.
16				
18	CS			CL SILTY CLAY: yellowish brown (10YR 5/6) with a gray (10YR 5/1) silt mottle. firm, moist.
20				SM SILTY SAND: brownish yellow, fine grained. saturated. limonitic zone on basal contact. CL SILTY CLAY: as above. wet.
22	CS			CL CLAY: gray to dark gray (10YR 5/1-4/1). silty in part. wet.
24				GM SILTY GRAVEL: dark gray to olive gravels. in a sandy silt matrix saturated.
26				T.D. 30'
28				
30				

# SUMMARY OF LABORATORY TEST RESULTS

Hole No.	Sample No.	Sample Type*	Depth (ft)	Natural Moisture (%)	UNIT WEIGHT (PCF)		SPECIFIC GRAVITY	ATTERBERG LIMITS		Unified Soil Classification	Other Test **	Soil Description
					Wet	Dry		Liquid Limit (%)	Plasticity Index (%)			
BH-1-05		SS	5.0	23.4			2.66	49	31	CL		CLAY, silty, light yellowish brown mottled gray with roots
BH-1-13.5		SS	13.0 - 13.5	32.4			2.63	64	38	CH		CLAY, silty, reddish-brown mottled black
BH-1-22		SS	21.5 - 22.0	21.2			2.67	27	15	CL		CLAY, silty, light yellowish brown mottled brown with weathered shale fragments
BH-2-05		SS	4.5 - 5.0	22.6			2.60	33	14	CL		CLAY, silty, light yellowish brown mottled gray and brown with rock fragments
BH-2-14		SS	13.5 - 14.0	22.6			2.69	26	12	CL		CLAY, silty, slightly sandy, tan
BH-2-28		SS	27.5 - 28.0	19.1			2.75	31	13	CL		CLAY, silty, dark yellowish brown with rock fragments
BH-3-09		SS	8.5 - 9.0	24.5			2.66	50	28	CL		CLAY, silty, tan mottled light gray
BH-3-12		SS	11.5 - 12.0	35.5			2.73	72	49	CH		CLAY, silty, light brown mottled gray
BH-3-19		SS	18.5 - 19.0	17.7			2.68	23	11	CL		CLAY, silty, dark greenish brown with rock fragments
BH-4-07		SS	6.5 - 7.0	26.7			2.69	60	35	CH		CLAY, silty, light brown mottled gray and yellowish-brown
BH-4-15		SS	14.5 - 15.0	31.0			2.69	69	43	CH		CLAY, silty, light brown mottled gray

\*ST-SHELBY TUBE SAMPLE, SS-SPLIT SPOON SAMPLE, B-BAG SAMPLE  
\*\*TEST RESULTS REPORTED ON OTHER SHEETS:

C-CONSOLIDATION  
S-SIEVE OR GRAIN SIZE ANALYSIS  
U-UNCONFINED COMPRESSION TEST

P-PROCTOR TEST  
D-DIRECT SHEAR TEST  
T-TRIAXIAL TEST

DATA CHECKED BY Jh

GA Technical Services

# SUMMARY OF LABORATORY TEST RESULTS

		UNIT WEIGHT (PCF)		SPECIFIC GRAVITY	ATTERBERG LIMITS		Unified Soil Classification	Other Test **	Soil Description	Project: <u>Portsmouth ODI Mini Characterization</u> Project Number: <u>0-4267-0088</u> Date: <u>May 20, 1994</u>
Hole No.	Sample No.	Sample Type*	Depth (ft)	Natural Moisture (%)	Wet	Dry	G <sub>s</sub>	Liquid Limit (%)	Plasticity Index (%)	
BH-4-21		SS	20.5 - 21.0	36.7			2.72	48	26	CLAY, silty, brown mottled gray and reddish-brown
BH-5-08		SS	7.5 - 8.0	32.3			2.69	69	44	CLAY, silty, light brown mottled gray
BH-5-13		SS	12.5 - 13.0	39.9			2.70	46	25	CLAY, silty, light brown mottled gray yellowish-brown and reddish-brown
BH-5-19		SS	18.5 - 19.0	20.7			2.66	26	11	CLAY, silty, yellowish-brown mottled light gray with rock fragments
BH-5-23		SS	22.5 - 23.0	30.9			2.70	28	15	CLAY, silty slightly sandy light yellowish-brown
BH-6-02		SS	1.5 - 2.0	25.9			2.62	41	25	CLAY, silty, light yellowish-brown
BH-6-18		SS	17.5 - 18.0	21.7			2.65	26	13	CLAY, silty, light yellowish-brown
BH-6-29		SS	28.5 - 29.0	14.3			2.69			CLAY, silty, dark brown with rock fragments
BH-7-12		SS	11.5 - 12.0	20.7			2.70	28	14	CLAY, silty, slightly sandy, light yellowish-brown
BH-7-20		SS	19.5 - 20.0	19.3			2.65	30	14	CLAY, silty, slightly sandy, yellowish-brown
BH-7-26		SS	25.5 - 26.0	17.3			2.65	29	12	CLAY, silty, dar brown

\*ST-SHELBY TUBE SAMPLE, SS-SPLIT SPOON SAMPLE, B-BAG SAMPLE

\*\*TEST RESULTS REPORTED ON OTHER SHEETS:

C-CONSOLIDATION  
S-SIEVE OR GRAIN SIZE ANALYSIS  
U-UNCONFINED COMPRESSION TEST

P-PROCTOR TEST  
D-DIRECT SHEAR TEST  
T-TRIAXIAL TEST

DATA CHECKED BY 

GA Technical Services

## JURY TEST RESULTS

[illegible]

\*ST: SHELBY TUBE SAMPLE. SS: SPLIT SPOON SAMPLE. B-BAG SAMPLE

•••TEST RESULTS REPORTED ON OTHER SHEETS:

## C-CONSOLIDATION

### S-SIEVE OR GRAIN SIZE ANALYSIS

## U-UNCONFINED COMPRESSION TEST

## P-PROCTOR TEST

## D-DIRECT SHEAR TEST

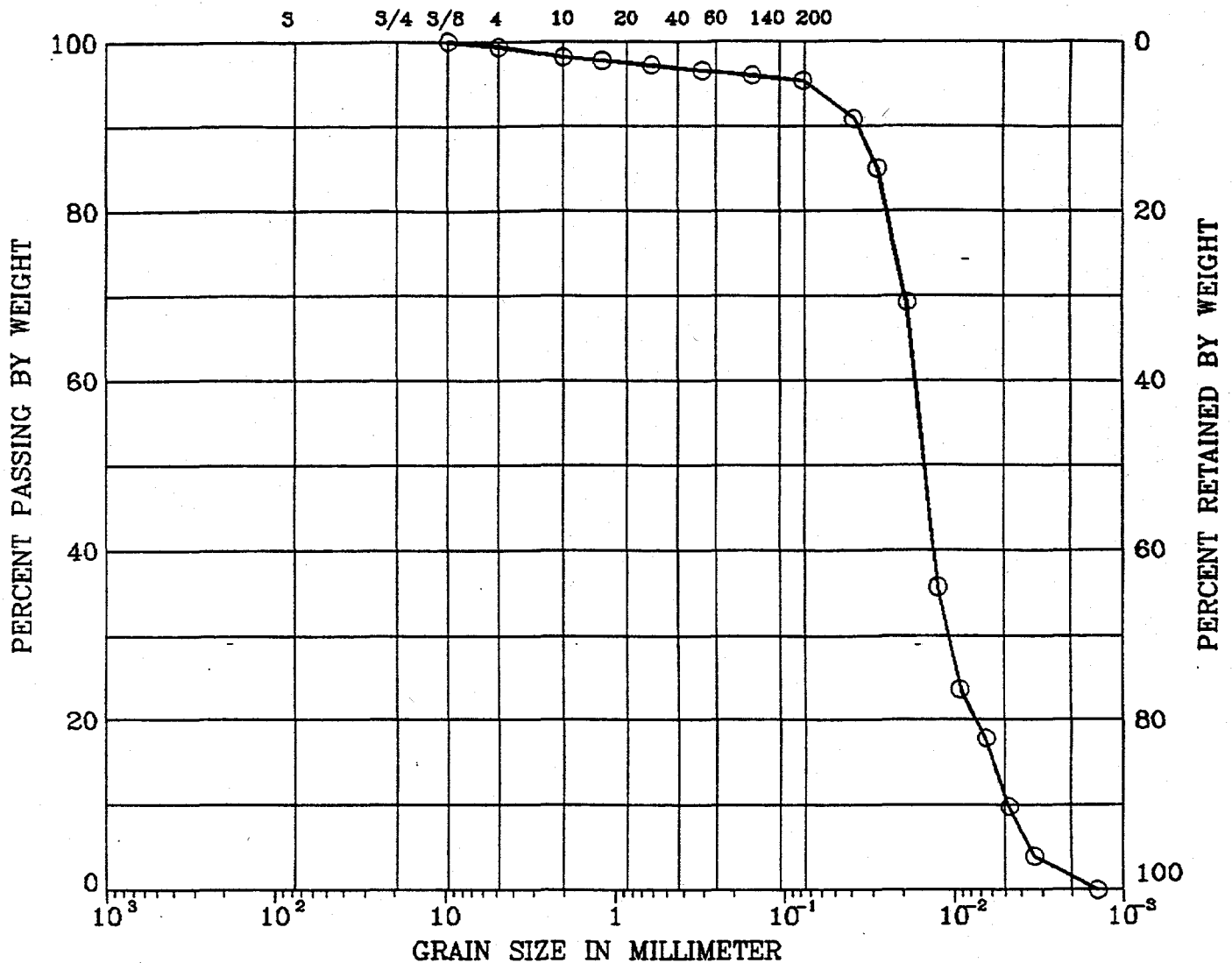
## T-TRIAxIAL TEST

**DATA CHECKED BY**

# GA Technical Services

# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



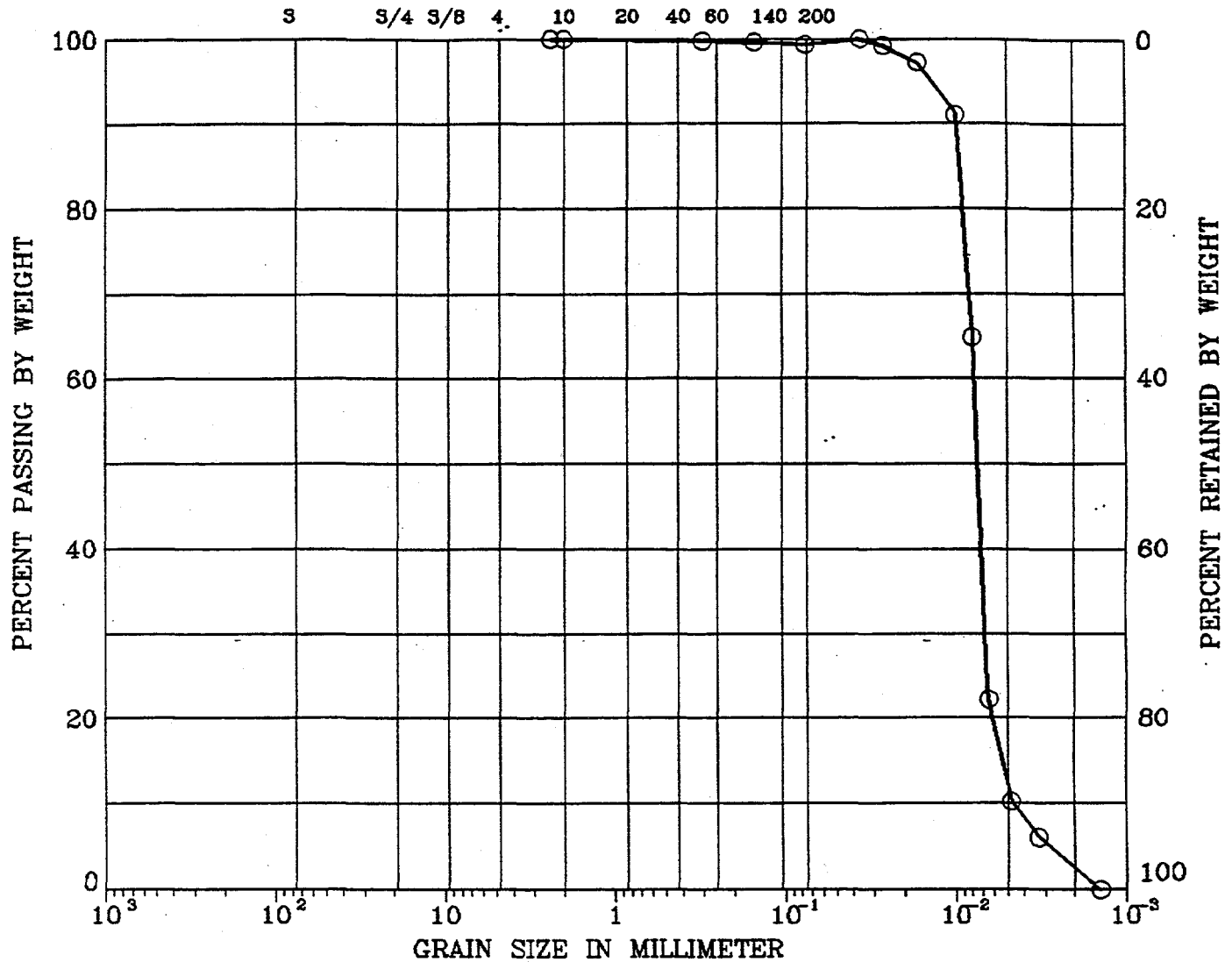
SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION
○	BH1-05	5.0	49	31	CLAY, silty, lt yelsh br, mott gr, w/ rts USC=CL

Remark : Martin Marietta Energy Systems, Inc.

Project No.0-4267	Portsmouth - OTD Mini Characterization
OGDEN ENVIRONMENTAL	GRAIN SIZE DISTRIBUTION April 5, 1994

# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION	
○	BH1-13.5	13-13.5	64	38	CLAY, silty, rdsh br, mott blk	USC=CH

Remark : Martin Marietta Energy Systems, Inc.

Project No.0-4267

Portsmouth - OTD Mini Characterization

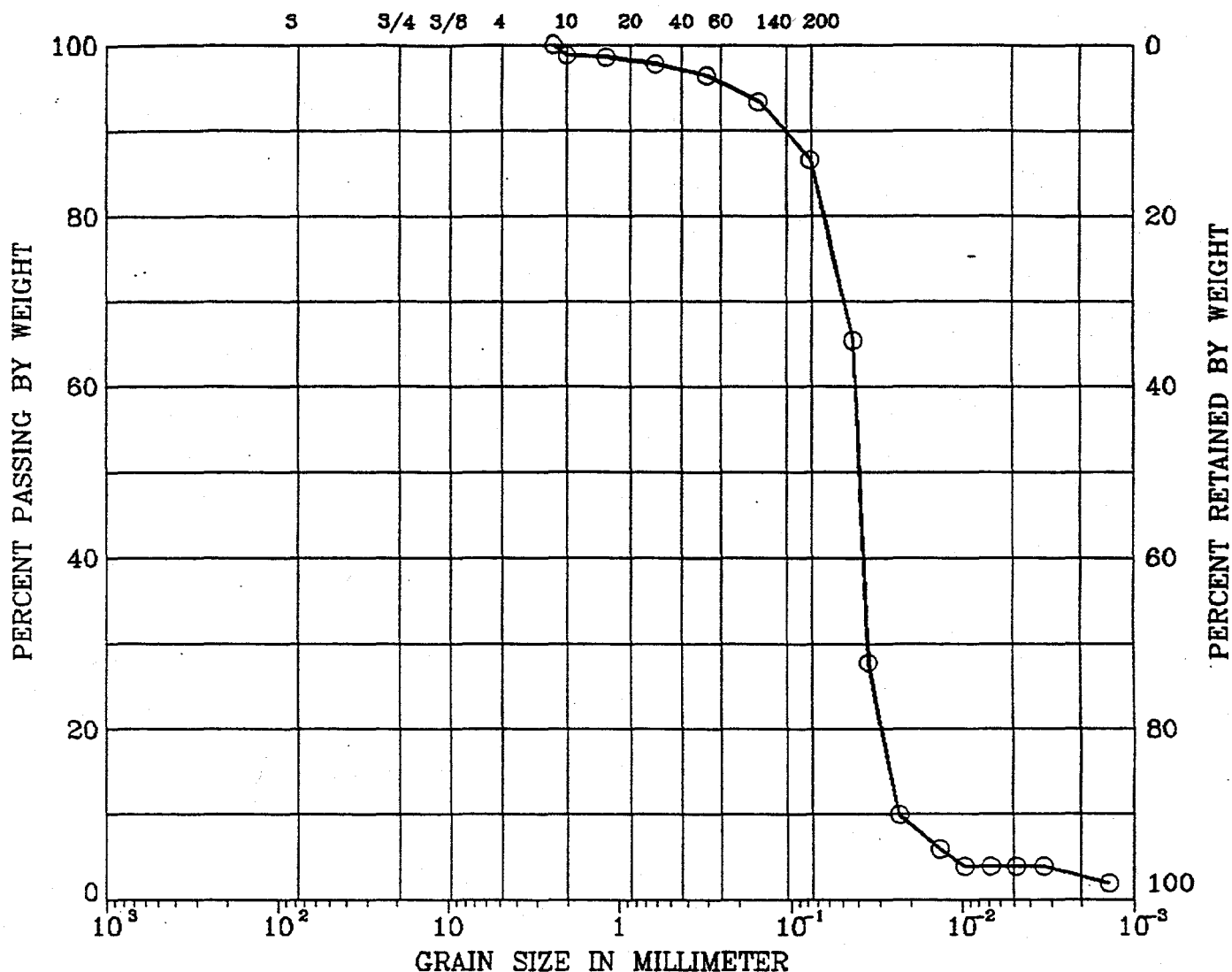
**OGDEN**  
ENVIRONMENTAL

**GRAIN SIZE DISTRIBUTION**

April 5, 1994

# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION
○	BH1-22	21.5-22	27	15	CLAY, silty, lt ylsch br mott br w/sh frags USC=CL

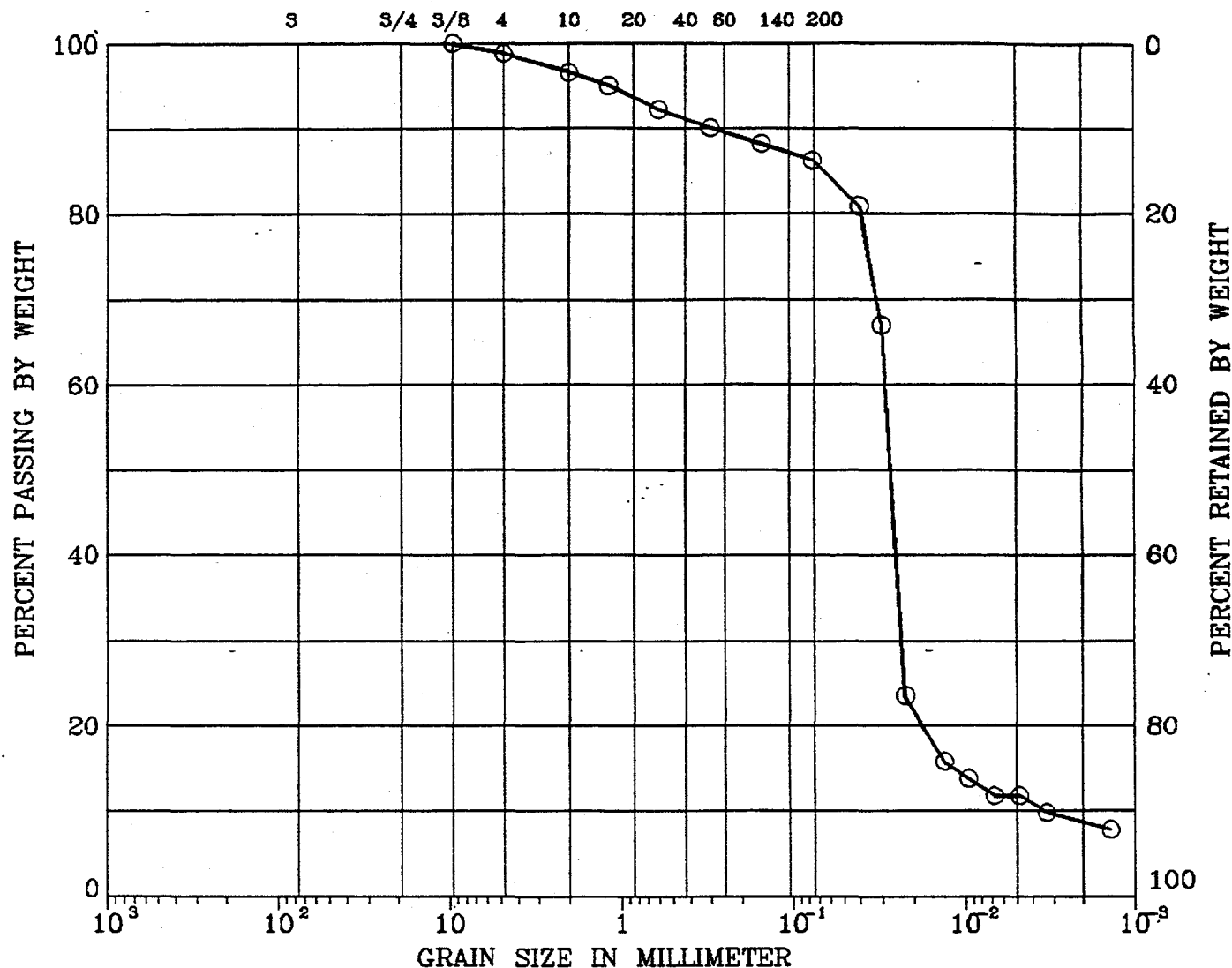
Remark : Martin Marietta Energy Systems, Inc.

Project No.0-4267	Portsmouth - OTD Mini Characterization
OGDEN ENVIRONMENTAL	GRAIN SIZE DISTRIBUTION April 5, 1994



# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION
○	BH2-05	4.5-5.0	33	14	CLAY, silty, lt yish br mott gr & br w/rk frags USC=CL

Remark : Martin Marietta Energy Systems, Inc.

Project No.0-4267

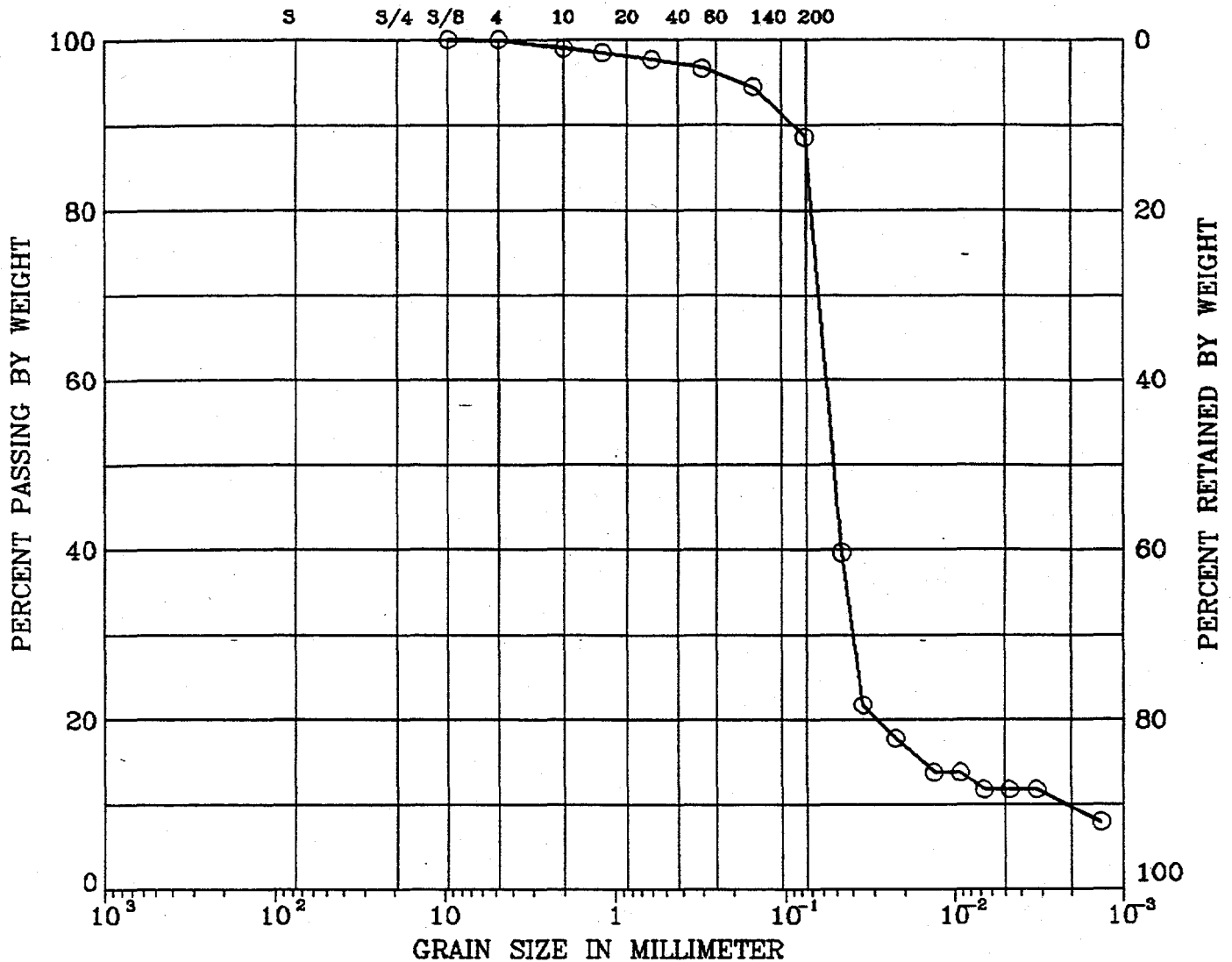
Portsmouth - OTD Mini Characterization

**OGDEN**  
ENVIRONMENTAL

**GRAIN SIZE DISTRIBUTION** April 5, 1994

# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION	
○	BH2-14	13.5-14	26	12	CLAY, silty, yellowish brown	USC=CL

Remark : Martin Marietta Energy Systems, Inc.

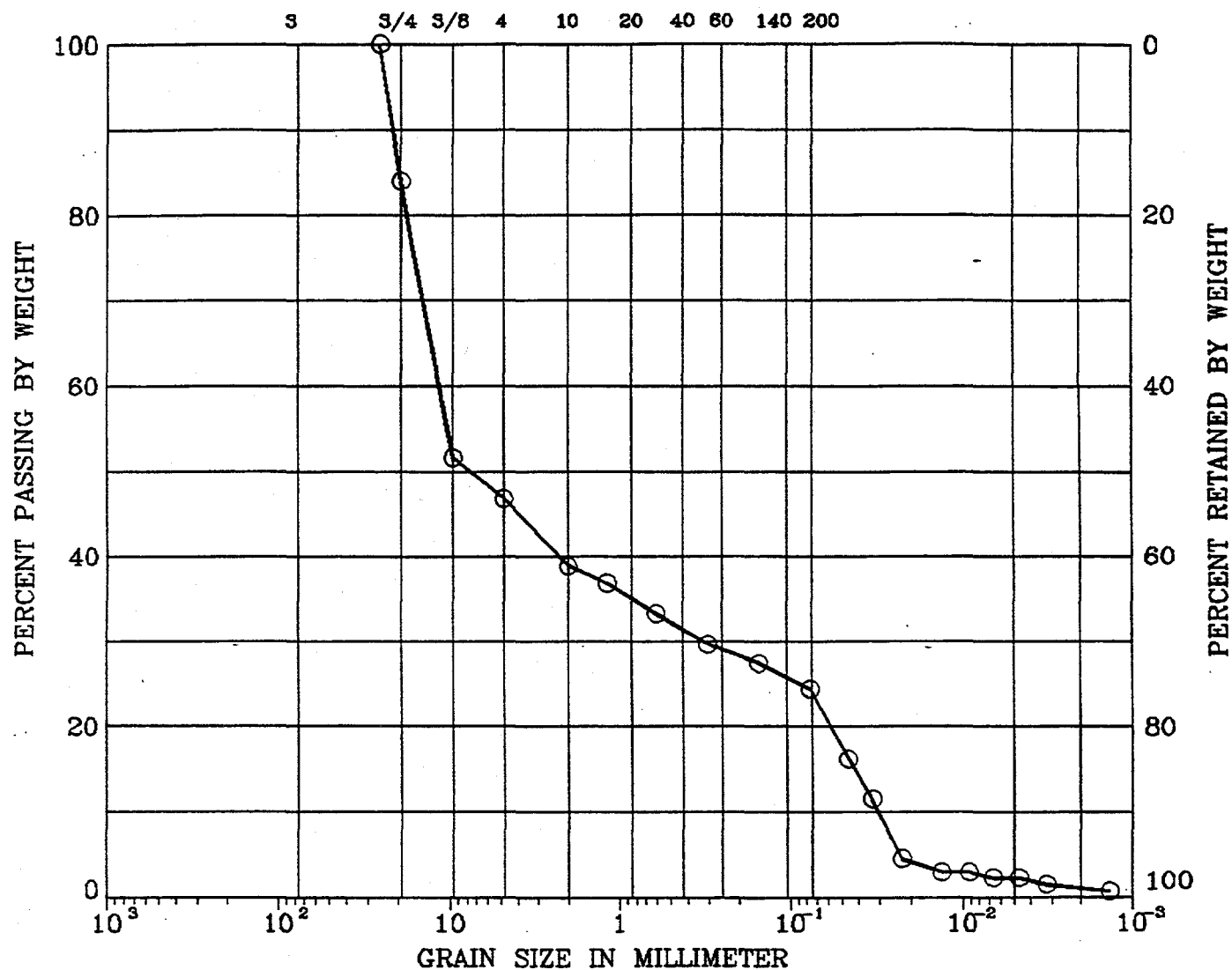
Project No.0-4267

Portsmouth - OTD Mini Characterization

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GRAIN SIZE DISTRIBUTION April 5, 1994

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



<u>SYMBOL</u>	<u>BORING</u>	<u>DEPTH</u> (ft)	<u>LL</u> (%)	<u>PI</u> (%)	<u>DESCRIPTION</u>
○	BH2-28	27.5-28	50	28	CLAY, silty, dk yellowish br, w/ rk frags USC=GC

Project No.0-4267

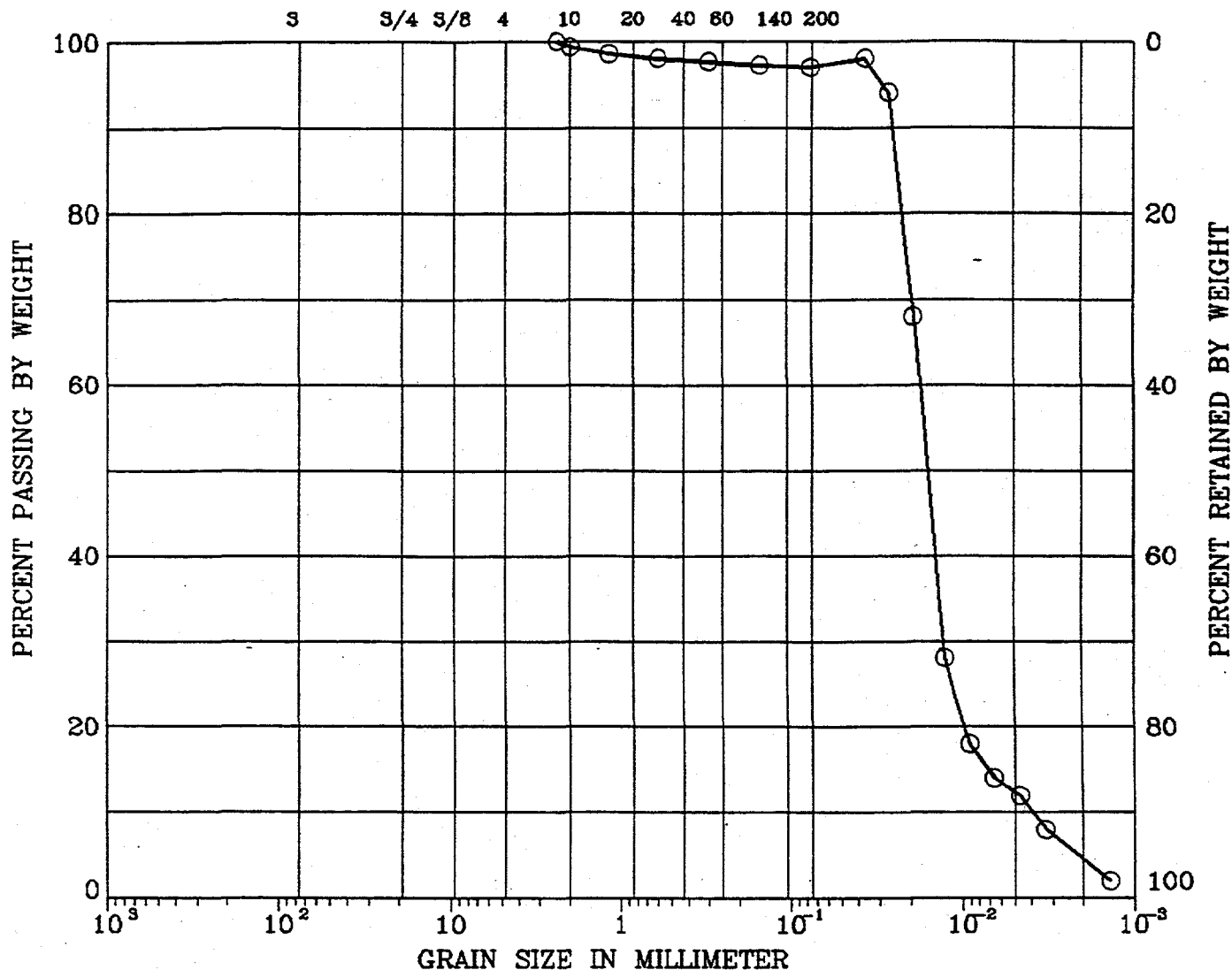
## Portsmouth - OTD Mini Characterization

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ENVIRONMENTAL**

# GRAIN SIZE DISTRIBUTION April 5, 1994

# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION	
○	BH3-09	8.5-9.0	50	28	CLAY, silty, tan mottled light gray	USC=CL

Remark : Martin Marietta Energy Systems, Inc.

Project No.0-4267

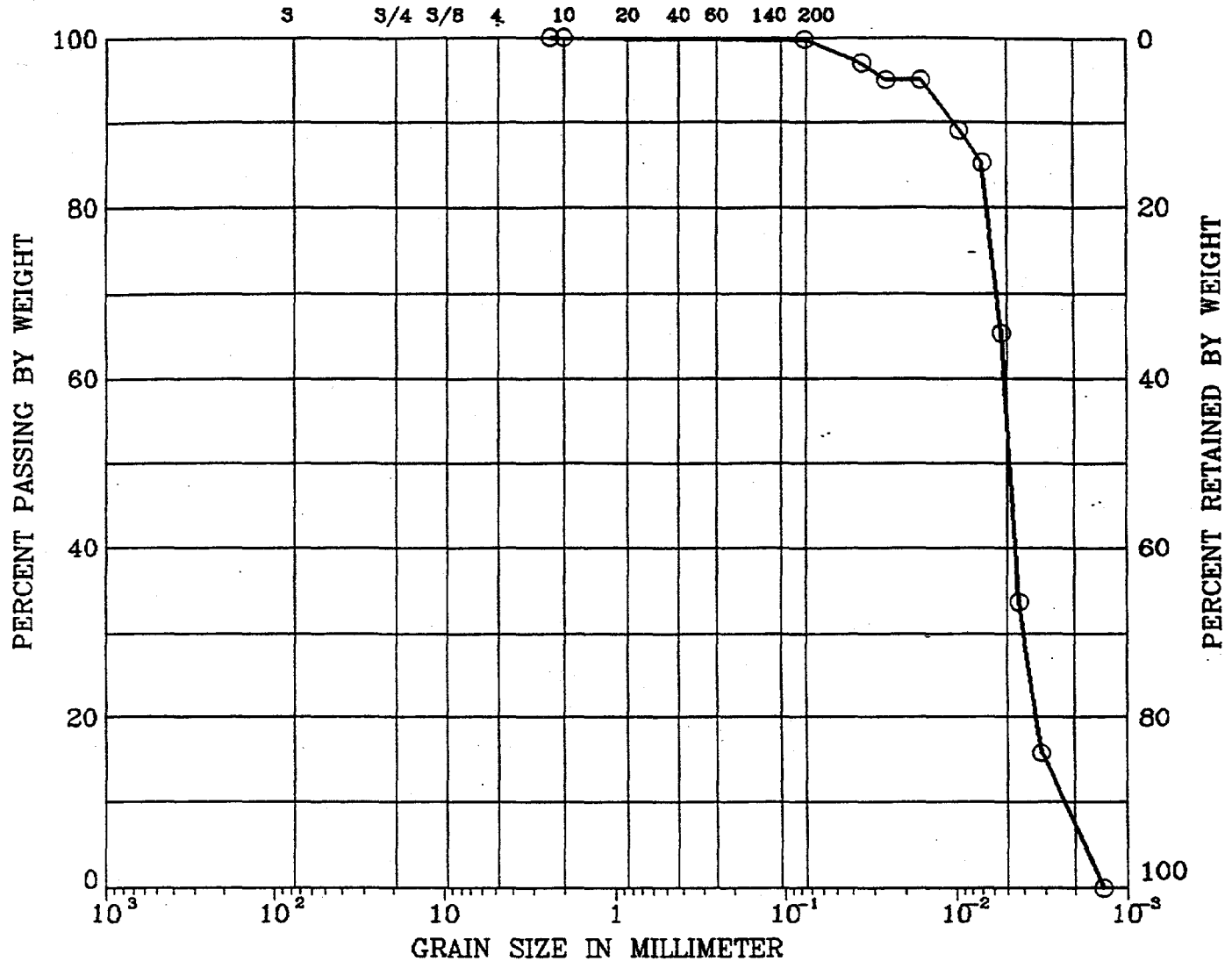
Portsmouth - OTD Mini Characterization

**OGDEN**  
ENVIRONMENTAL

**GRAIN SIZE DISTRIBUTION** April 5, 1994

# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION	
○	BH3-12	11.5-12	72	49	CLAY, silty, light brown mottled gray	USC=CH

Remark : Martin Marietta Energy Systems, Inc.

Project No.0-4267

Portsmouth - OTD Mini Characterization

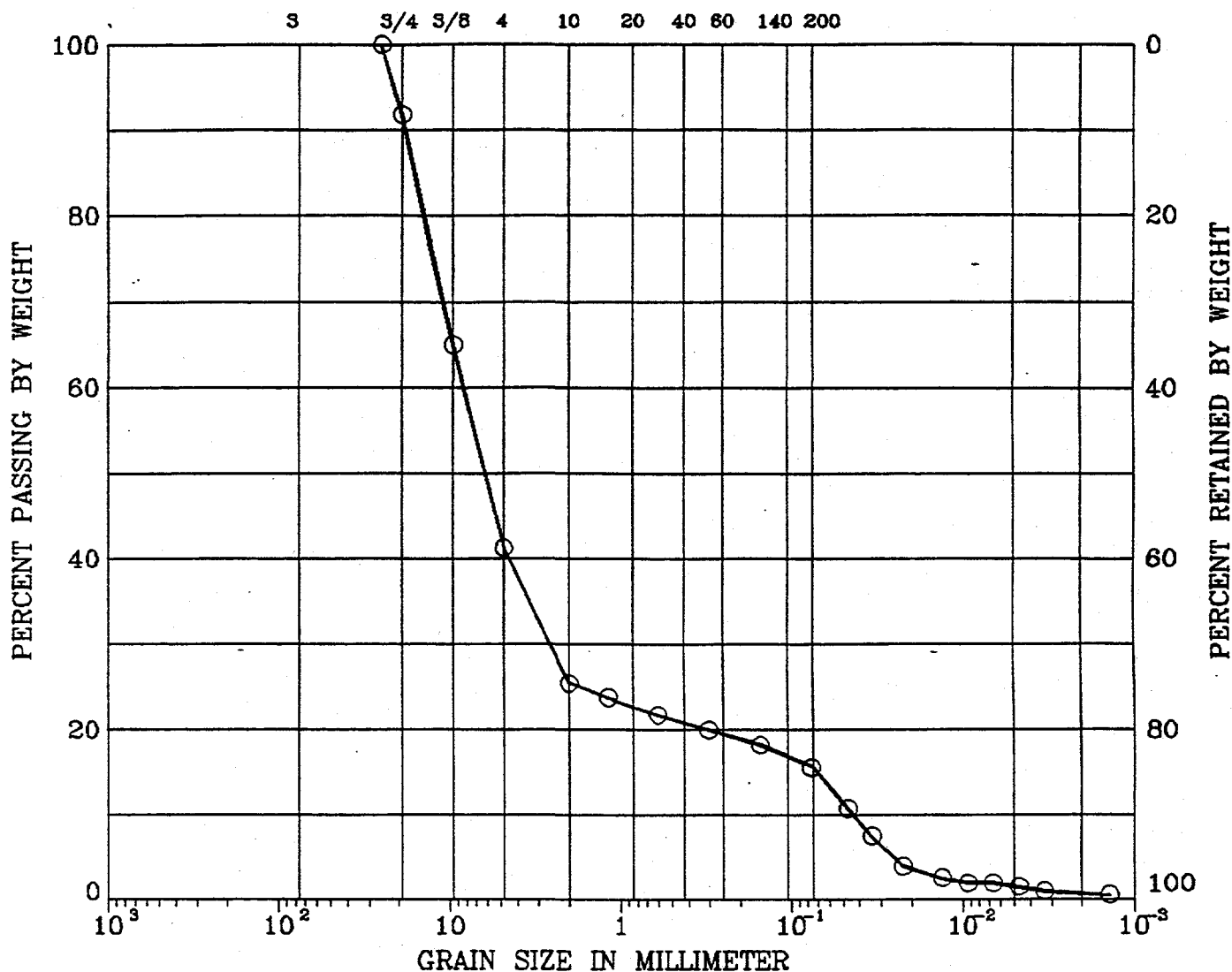
**OGDEN**  
ENVIRONMENTAL

**GRAIN SIZE DISTRIBUTION**

April 5, 1994

# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION	
○	BH3-19	18.5-19	23	11	CLAY, silty, dk grnsh br w/ rk frags	USC=GC

Remark : Martin Marietta Energy Systems, Inc.

Project No.0-4267

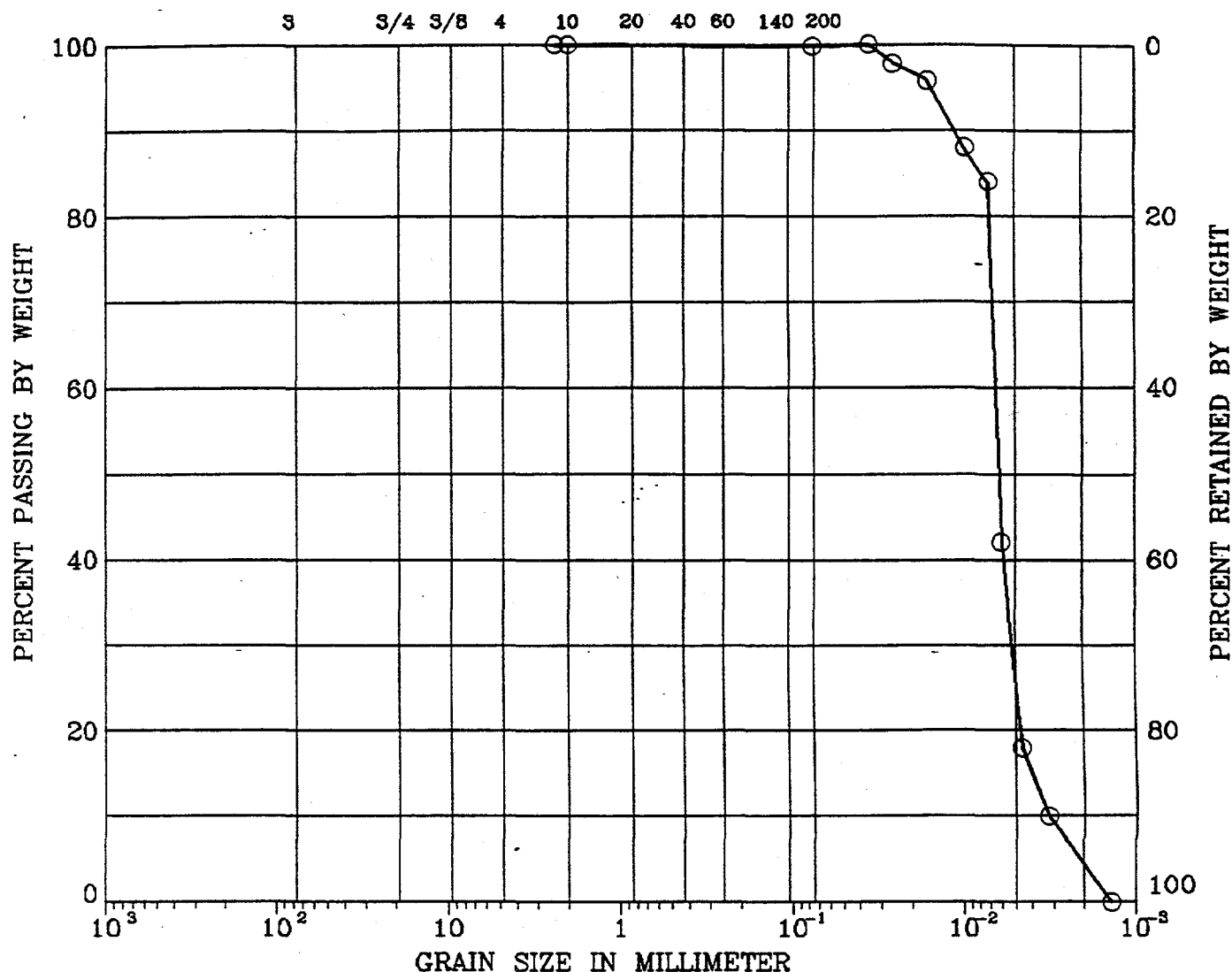
Portsmouth - OTD Mini Characterization

**OGDEN**  
ENVIRONMENTAL

**GRAIN SIZE DISTRIBUTION** April 5, 1994

# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION	
○	BH4-07	6.5-7.0	60	35	CLAY, silty lt br mott gr & yelsh br	USC=CH

Remark : Martin Marietta Energy Systems, Inc.

Project No.0-4267

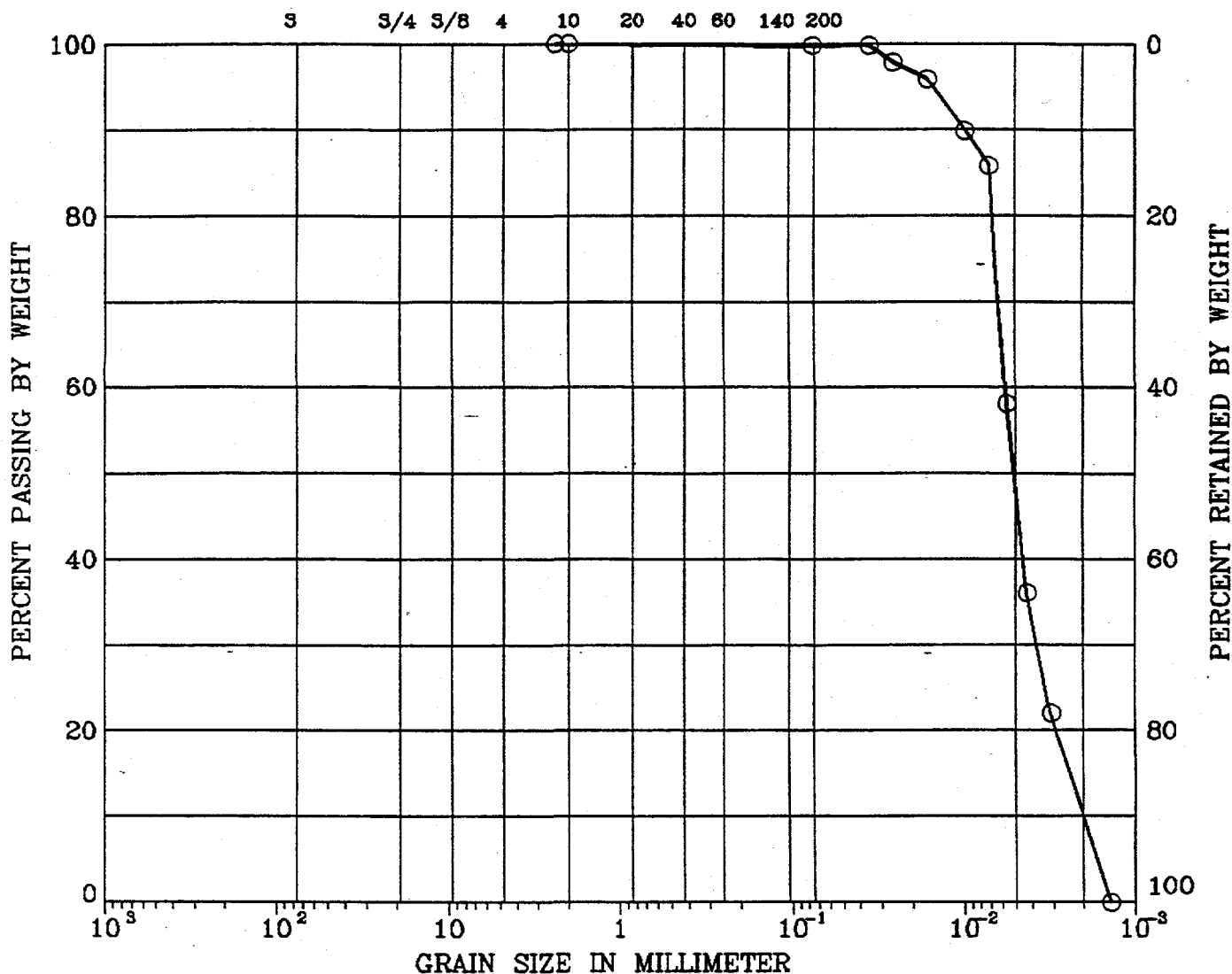
Portsmouth - OTD Mini Characterization

**OGDEN**  
ENVIRONMENTAL

**GRAIN SIZE DISTRIBUTION** April 5, 1994

# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION	
○	BH4-15	14.5-15	69	43	CLAY, silty, light brown mottled gray	USC=CH

Remark : Martin Marietta Energy Systems, Inc.

Project No.0-4267

Portsmouth - OTD Mini Characterization

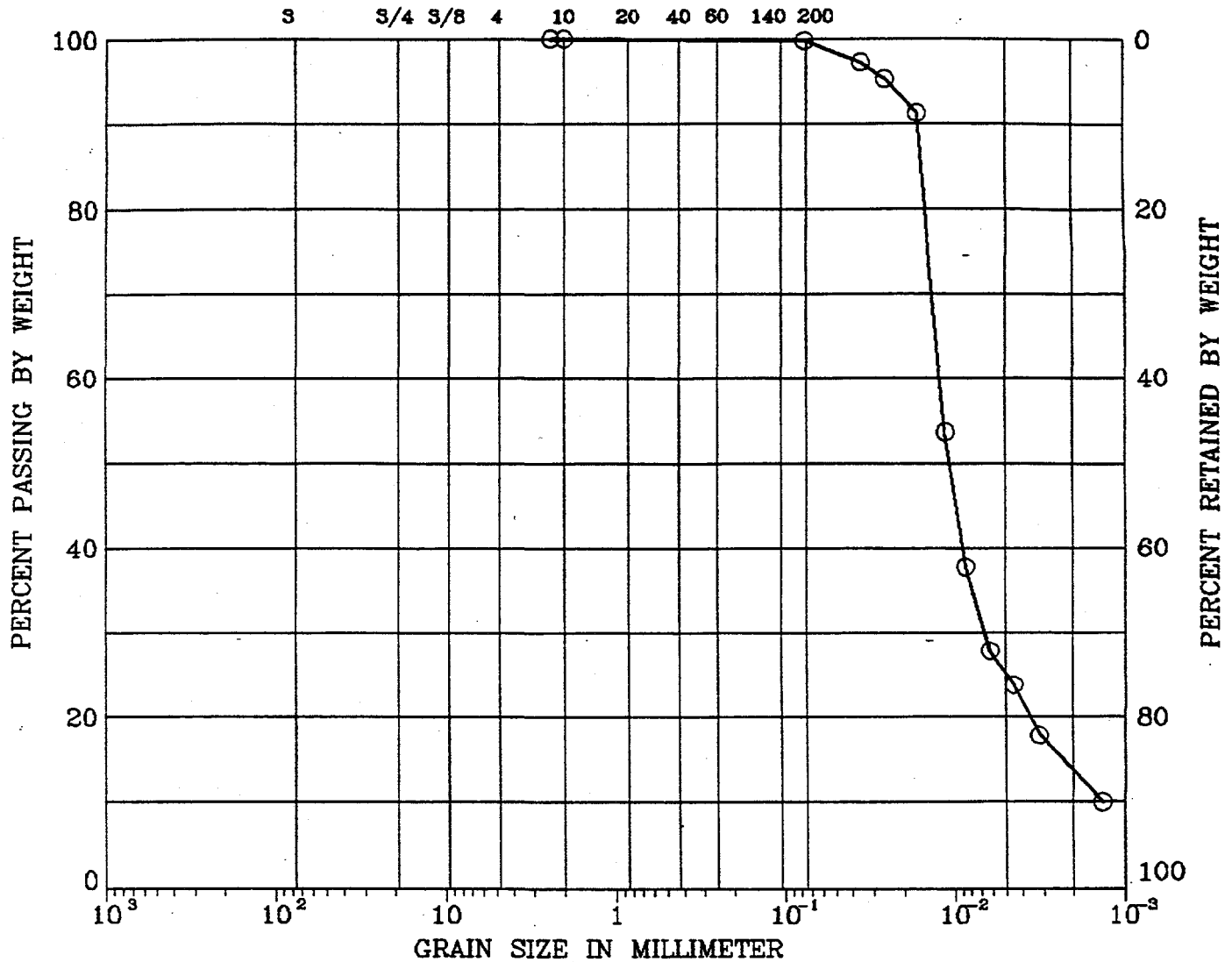
**OGDEN**  
ENVIRONMENTAL

**GRAIN SIZE DISTRIBUTION** April 5, 1994



# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION	
○	BH4-21	20.5-21	48	26	CLAY, silty br mott gr & rdsh br	USC=CL

Remark : Martin Marietta Energy Systems, Inc.

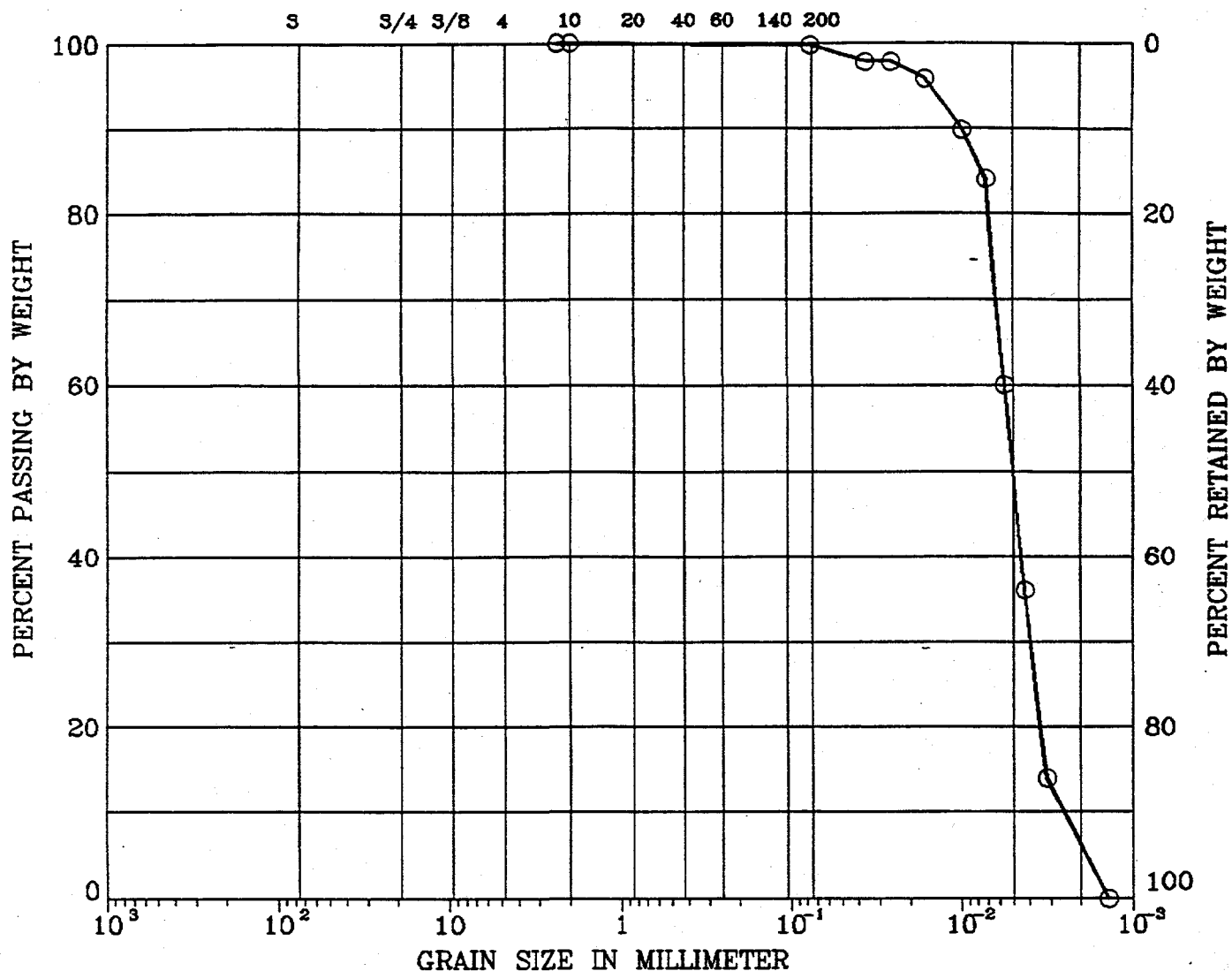
Project No.0-4267

Portsmouth - OTD Mini Characterization

**OGDEN**  
ENVIRONMENTAL

**GRAIN SIZE DISTRIBUTION** April 5, 1994

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



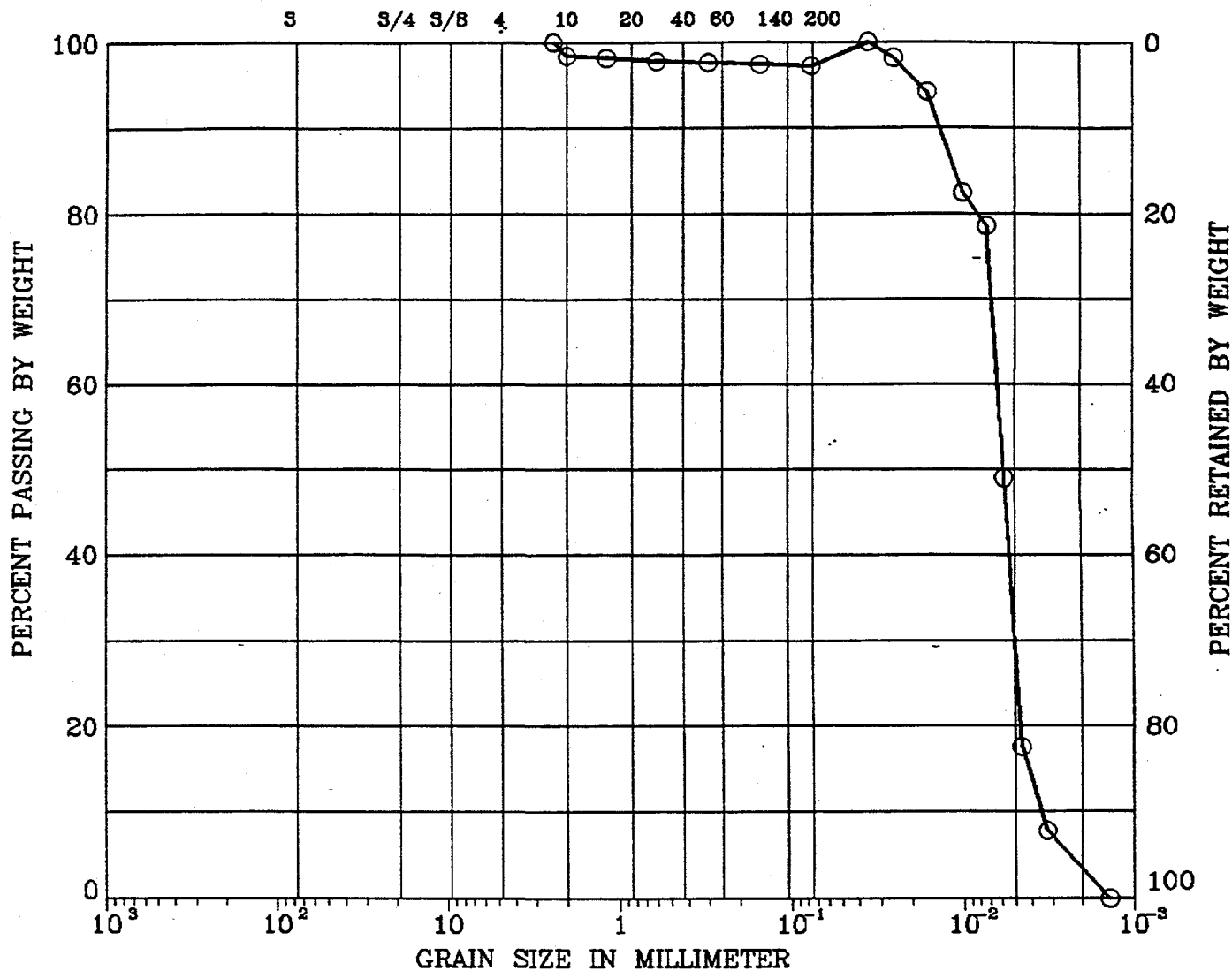
<u>SYMBOL</u>	<u>BORING</u>	<u>DEPTH</u> <u>(ft)</u>	<u>LL</u> <u>(%)</u>	<u>PI</u> <u>(%)</u>	<u>DESCRIPTION</u>
○	BH5-8	7.5-8.0	69	44	CLAY, silty, light brown mottled gray USC=CH

Remark : Martin Marietta Energy Systems, Inc.

Project No.0-4267	Portsmouth - OTD Mini Characterization
OGDEN ENVIRONMENTAL	GRAIN SIZE DISTRIBUTION April 5, 1994

# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION
○	BH5-13	12.5-13	46	25	CLAY, slty, lgt br mott gr, yelsh br rdsh br USC=CL

Remark : Martin Marietta Energy Systems, Inc.

Project No.0-4267

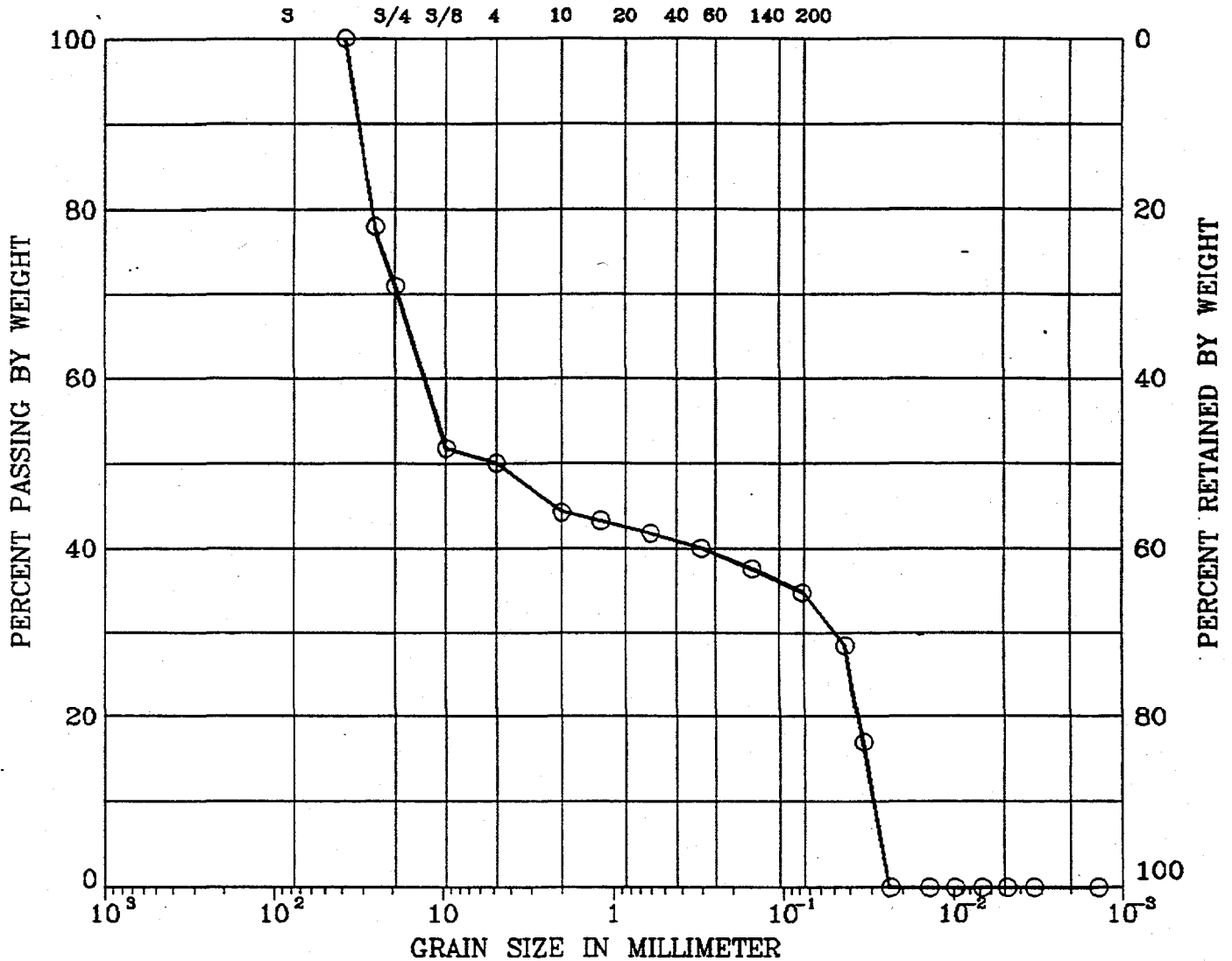
Portsmouth - OTD Mini Characterization

**OGDEN**  
ENVIRONMENTAL

**GRAIN SIZE DISTRIBUTION** April 5, 1994

# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. Sieve Size in Inches			U.S. Standard Sieve No.			Hydrometer



SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION
○	BH5-19	18.5-19	26	11	CLAY, silty yelsh br mott lt gr w/rk frags USC=GC

Remark : Martin Marietta Energy Systems, Inc.

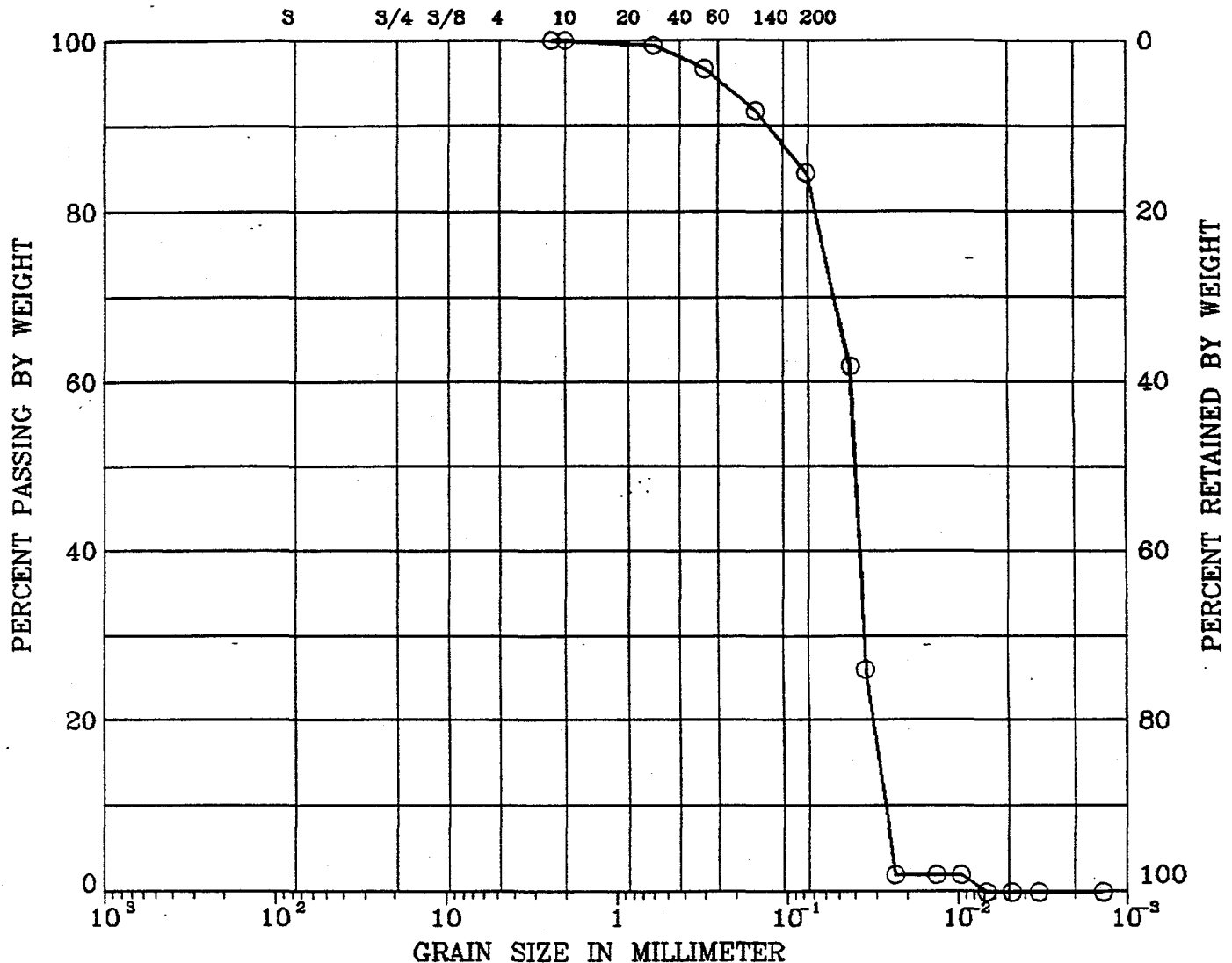
Project No.0-4267

Portsmouth - OTD Mini Characterization

**OGDEN**  
ENVIRONMENTAL

**GRAIN SIZE DISTRIBUTION** April 5, 1994

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



<u>SYMBOL</u>	<u>BORING</u>	<u>DEPTH</u> <u>(ft)</u>	<u>LL</u> <u>(%)</u>	<u>PI</u> <u>(%)</u>	<u>DESCRIPTION</u>	
○	BH5-23	22.5-23	28	15	CLAY,slty, sl sdy, lt yelsh br	USC=CL

Project No.0-4267

## Portsmouth - OTD Mini Characterization

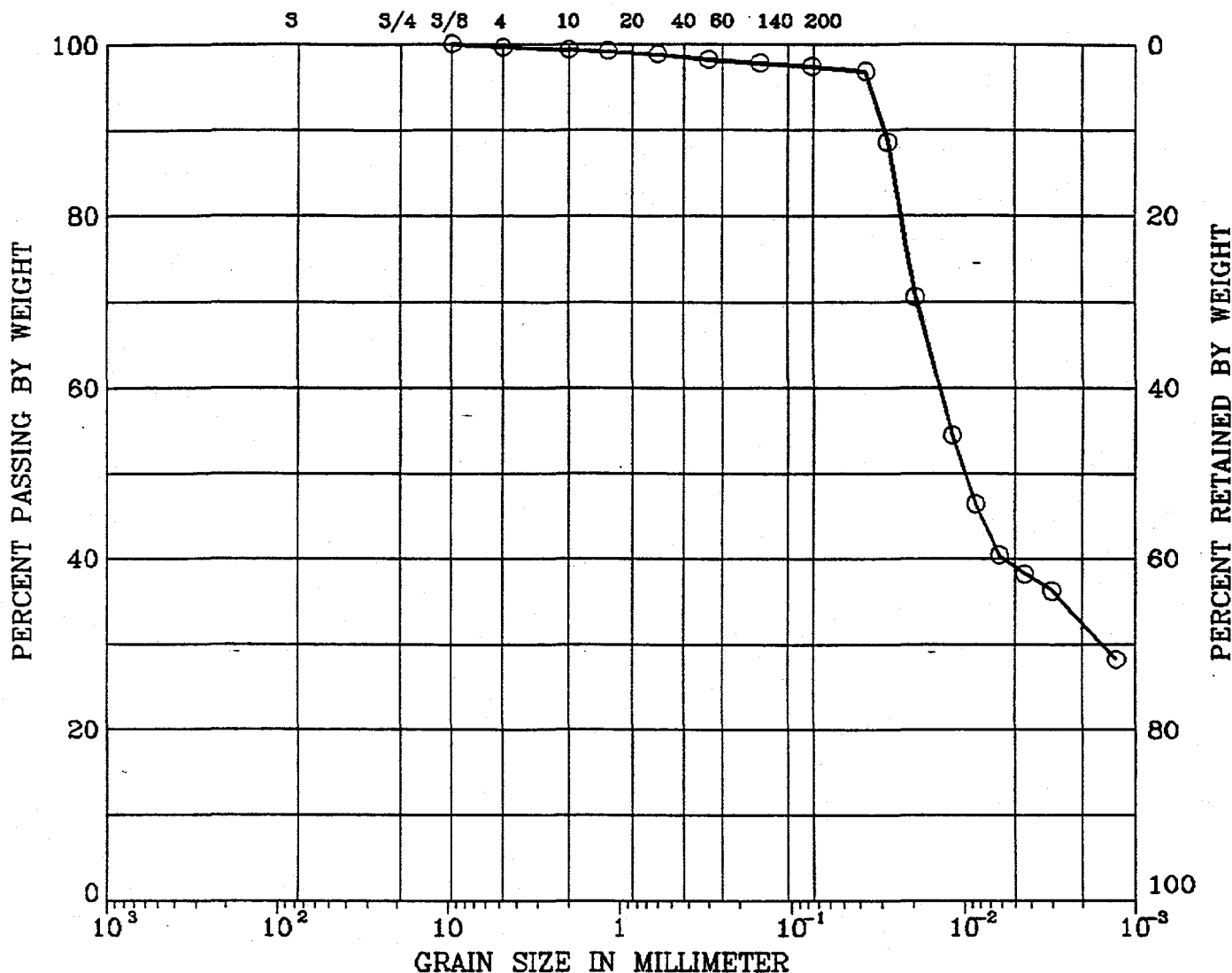
**OGDEN**  
**ENVIRONMENTAL**

## GRAIN SIZE DISTRIBUTION

April 5, 1994

# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION	USC
○	BH6-02	1.5-2.0	41	25	CLAY, silty, light yellowish brown	USC=CL

Remark : Martin Marietta Energy Systems, Inc.

Project No.0-4267

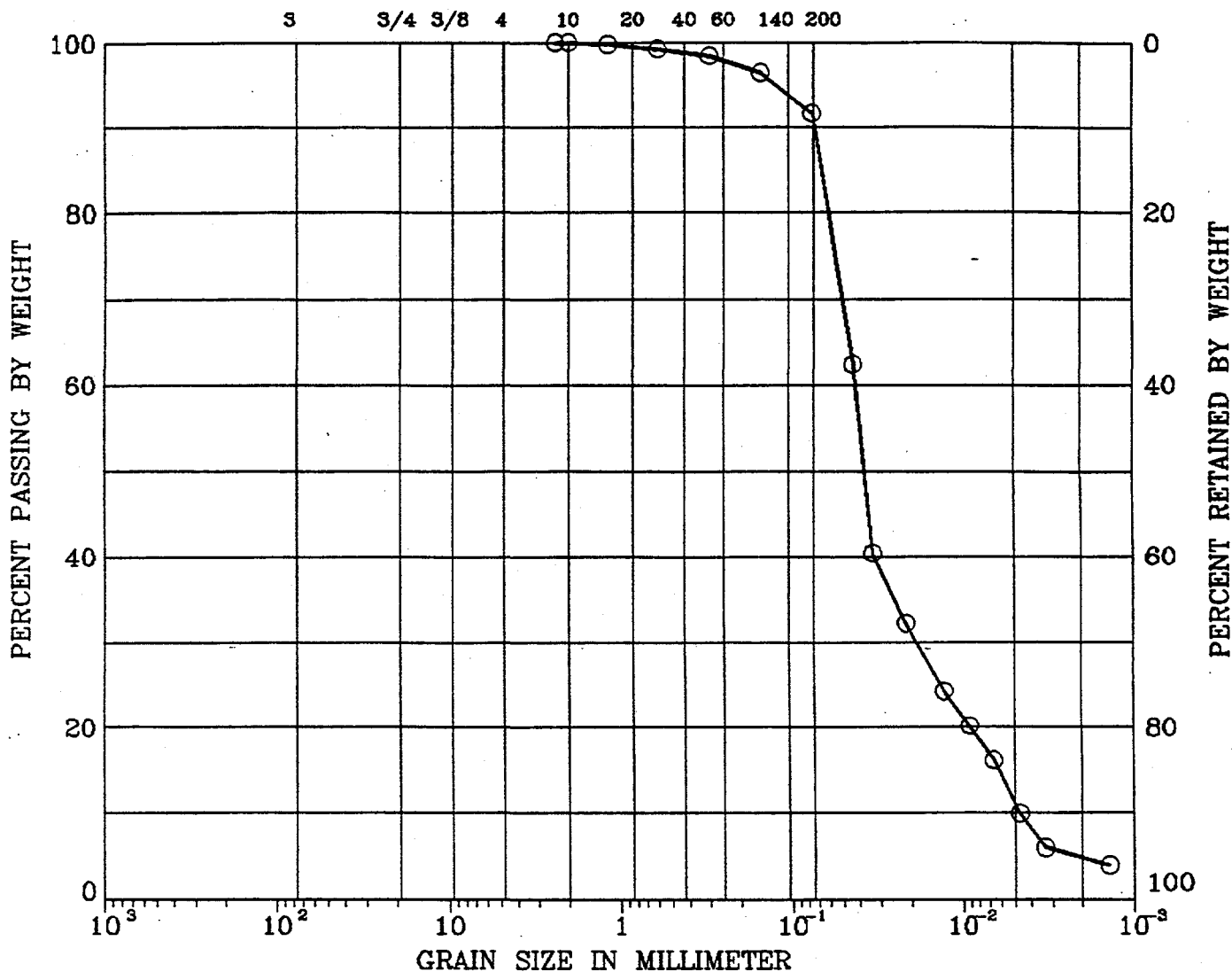
Portsmouth - OTD Mini Characterization

**OGDEN**  
ENVIRONMENTAL

**GRAIN SIZE DISTRIBUTION** April 5, 1994

# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION
○	BH6-18	17.5-18	26	13	CLAY, silty, light yellowish brown USC=CL

Remark : Martin Marietta Energy Systems, Inc.

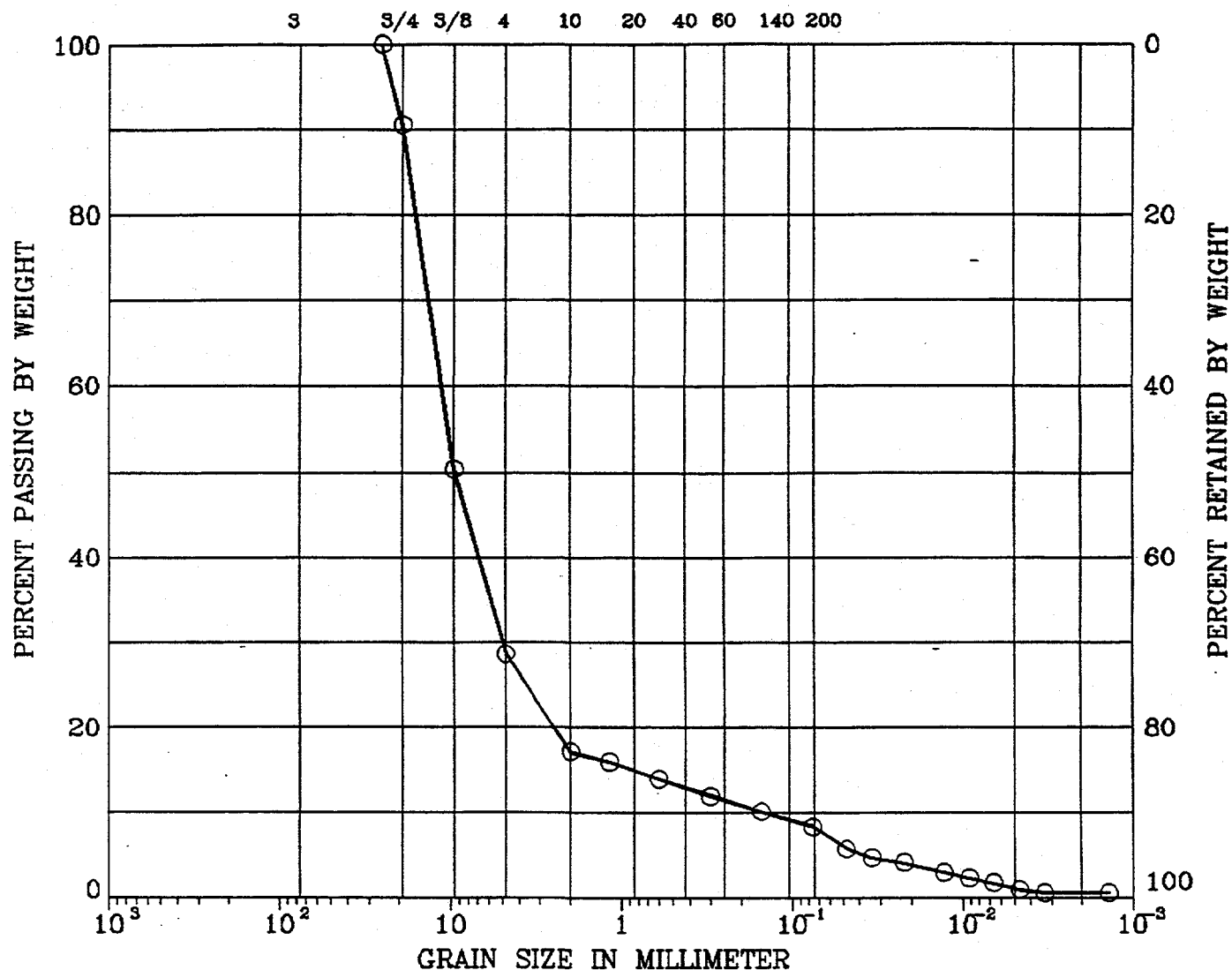
Project No.0-4267

Portsmouth - OTD Mini Characterization

**OGDEN**  
ENVIRONMENTAL

**GRAIN SIZE DISTRIBUTION** April 5, 1994

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



<u>SYMBOL</u>	<u>BORING</u>	<u>DEPTH</u> <u>(ft)</u>	<u>LL</u> <u>(%)</u>	<u>PI</u> <u>(%)</u>	<u>DESCRIPTION</u>
○	BH6-29	28.5-29			CLAY, silty, dk rdsh br, w/ rk frags USC=GP

Remark : Martin Marietta Energy Systems, Inc.

Project No.0-4267

## Portsmouth - OTD Mini Characterization

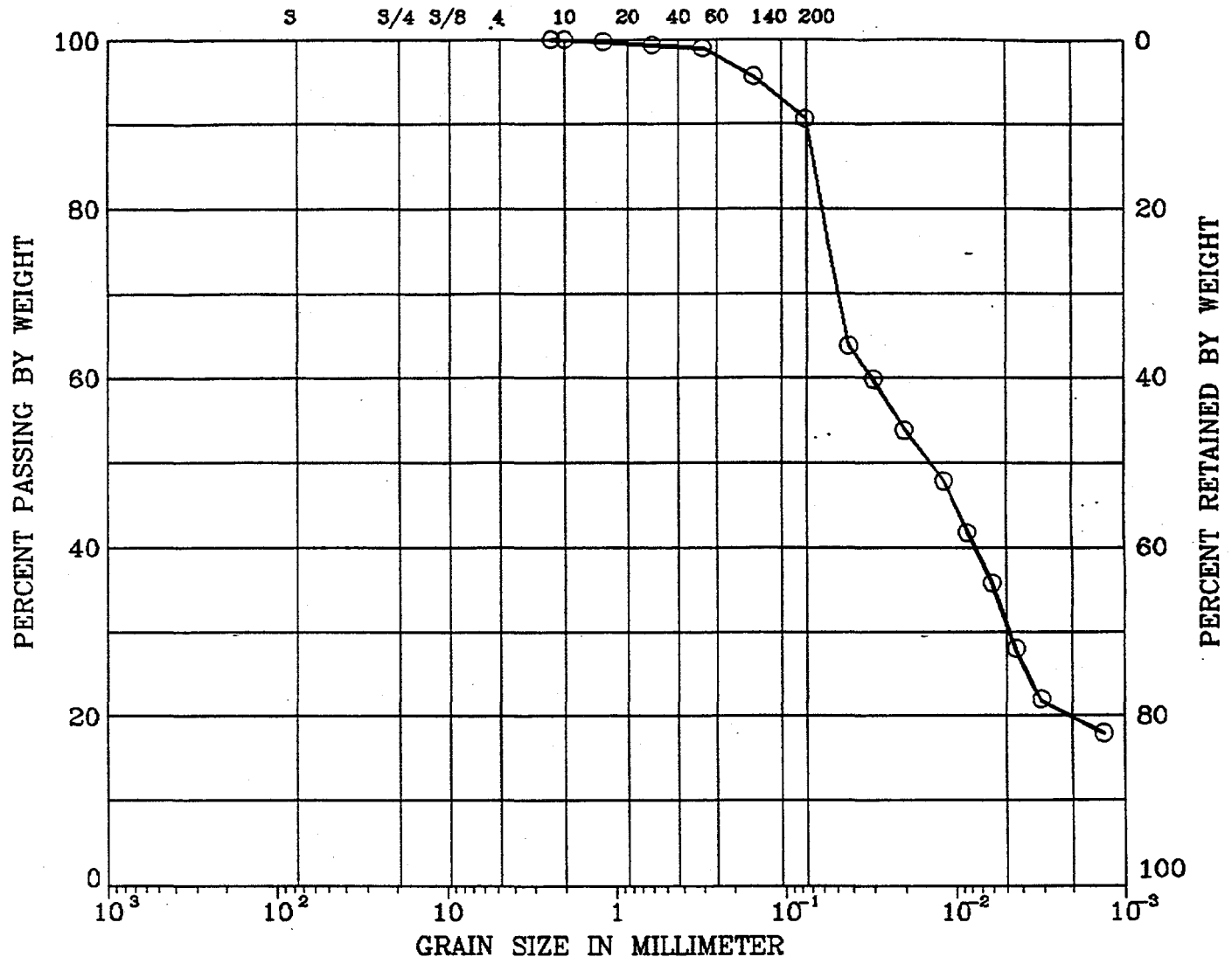
**OGDEN**  
**ENVIRONMENTAL**

# GRAIN SIZE DISTRIBUTION April 5, 1994



# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



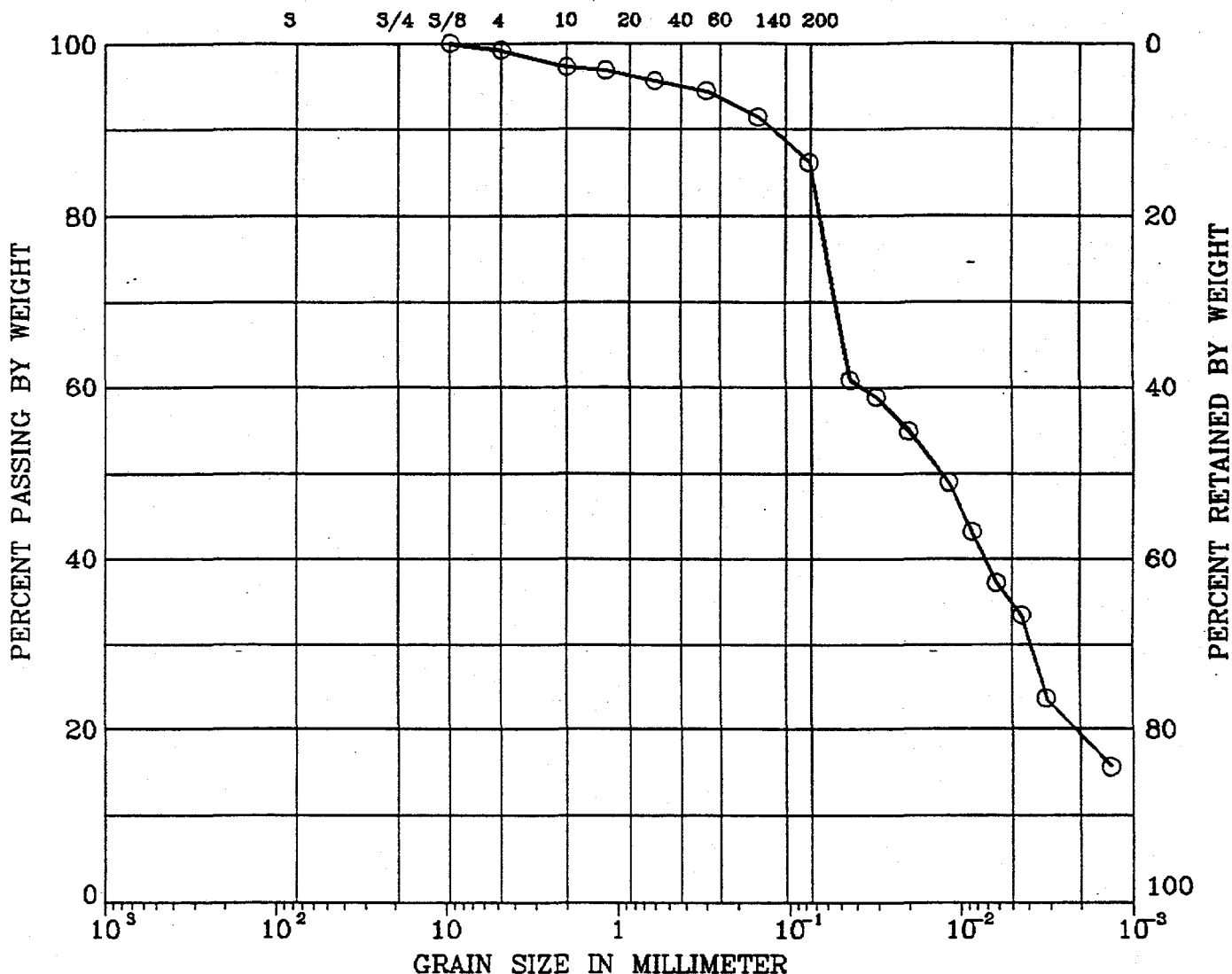
SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION	USC
○	BH7-12	11.5-12	28	14	CLAY, silty, sl sdy, light yelsh br	USC=CL

Remark : Martin Marietta Energy Systems, Inc.

Project No.0-4267	Portsmouth - OTD Mini Characterization
OGDEN ENVIRONMENTAL	GRAIN SIZE DISTRIBUTION April 5, 1994

# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION	
○	BH7-20	19.5-20	30	14	CLAY, silty, sl sdy, yelsh br	USC=CL

Remark : Martin Marietta Energy Systems, Inc.

Project No.0-4267

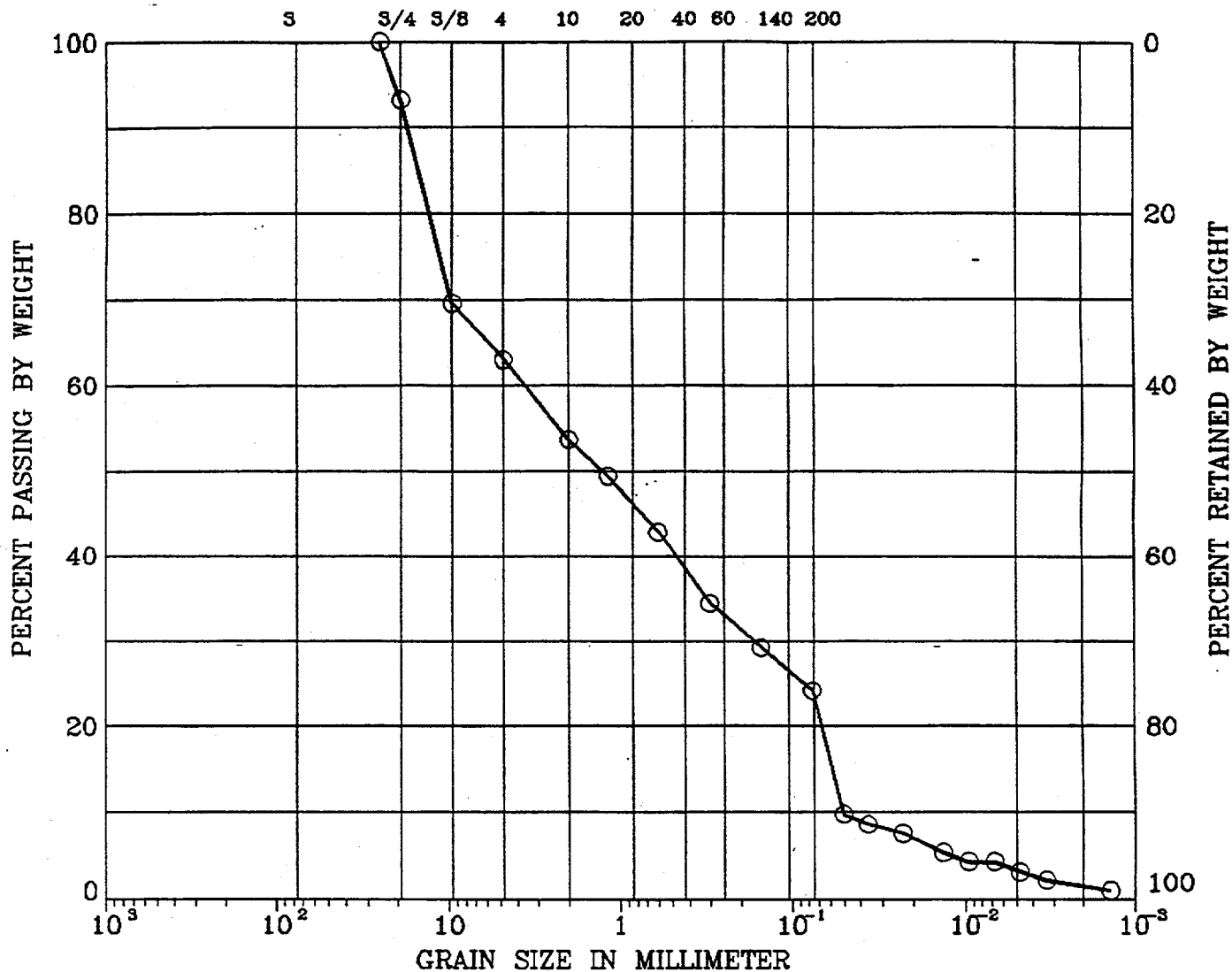
Portsmouth - OTD Mini Characterization

**OGDEN**  
ENVIRONMENTAL

**GRAIN SIZE DISTRIBUTION** April 5, 1994

# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION	
○	BH7-26	25.5-26	29	12	CLAY, slty, sdy, dark brown	USC=SC

Remark : Martin Marietta Energy Systems, Inc.

Project No.0-4267

Portsmouth - OTD Mini Characterization

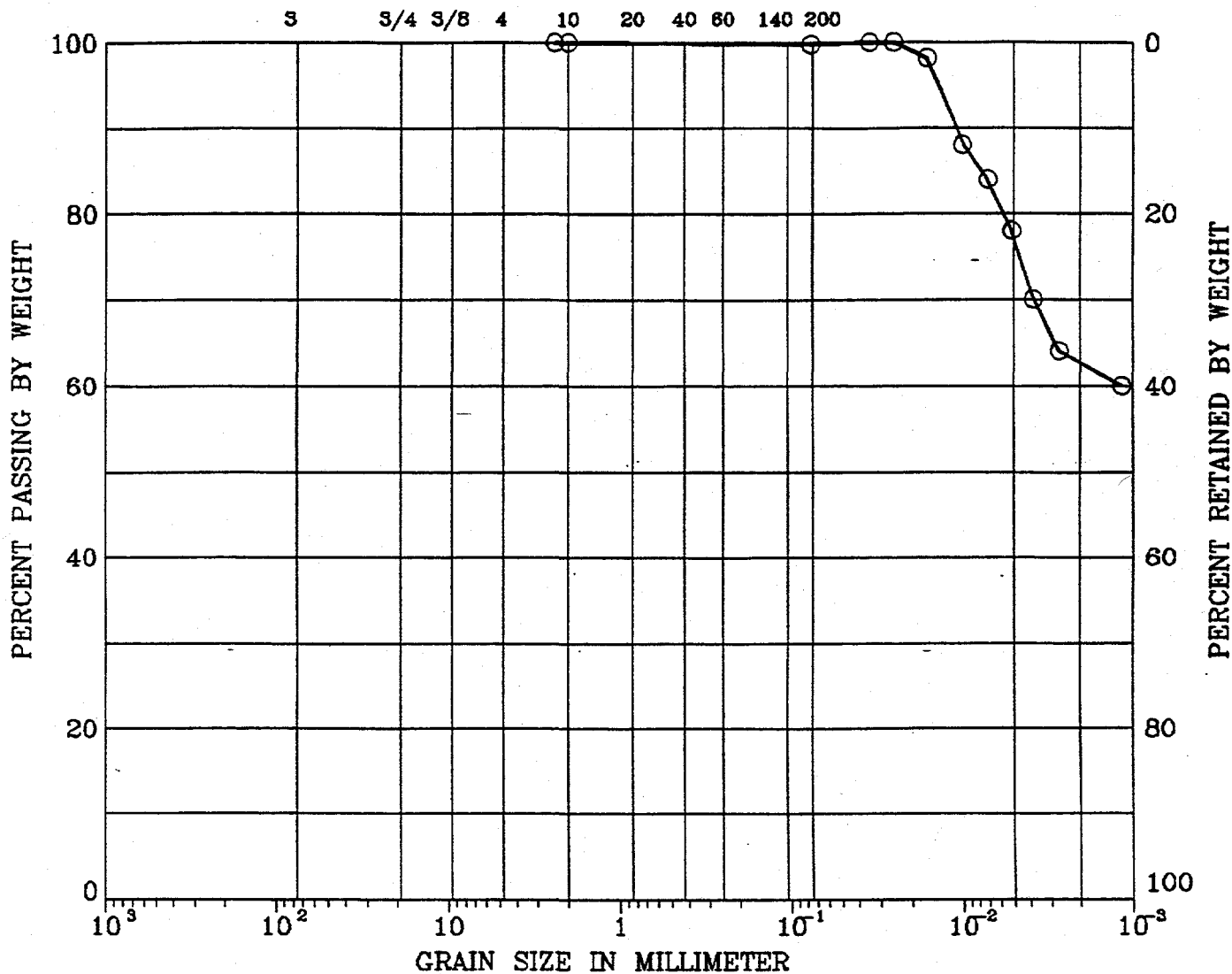
**OGDEN**  
ENVIRONMENTAL

**GRAIN SIZE DISTRIBUTION**

April 5, 1994

# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION	
○	BH8-13	12.5-13	61	41	CLAY, silty, reddish brown	USC=CH

Remark : Martin Marietta Energy Systems, Inc.

Project No.0-4267

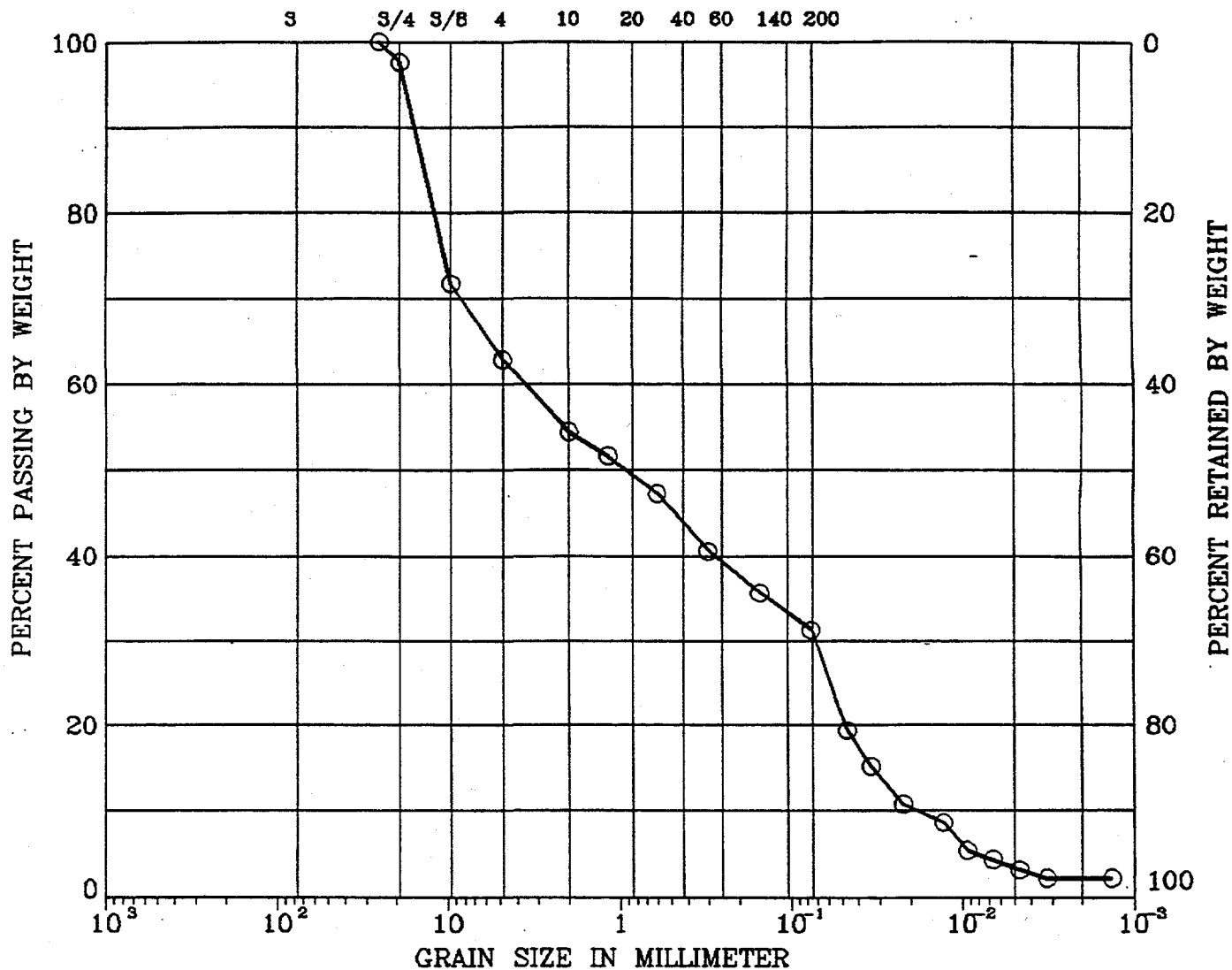
Portsmouth - OTD Mini Characterization

**OGDEN**  
ENVIRONMENTAL

**GRAIN SIZE DISTRIBUTION** April 5, 1994

# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION
○	BH8-22	21.5-22	26	12	CLAY, slty, dk br mott dk gr w/ rk frags USC=GC

Remark : Martin Marietta Energy Systems, Inc.

Project No.0-4267

Portsmouth - OTD Mini Characterization

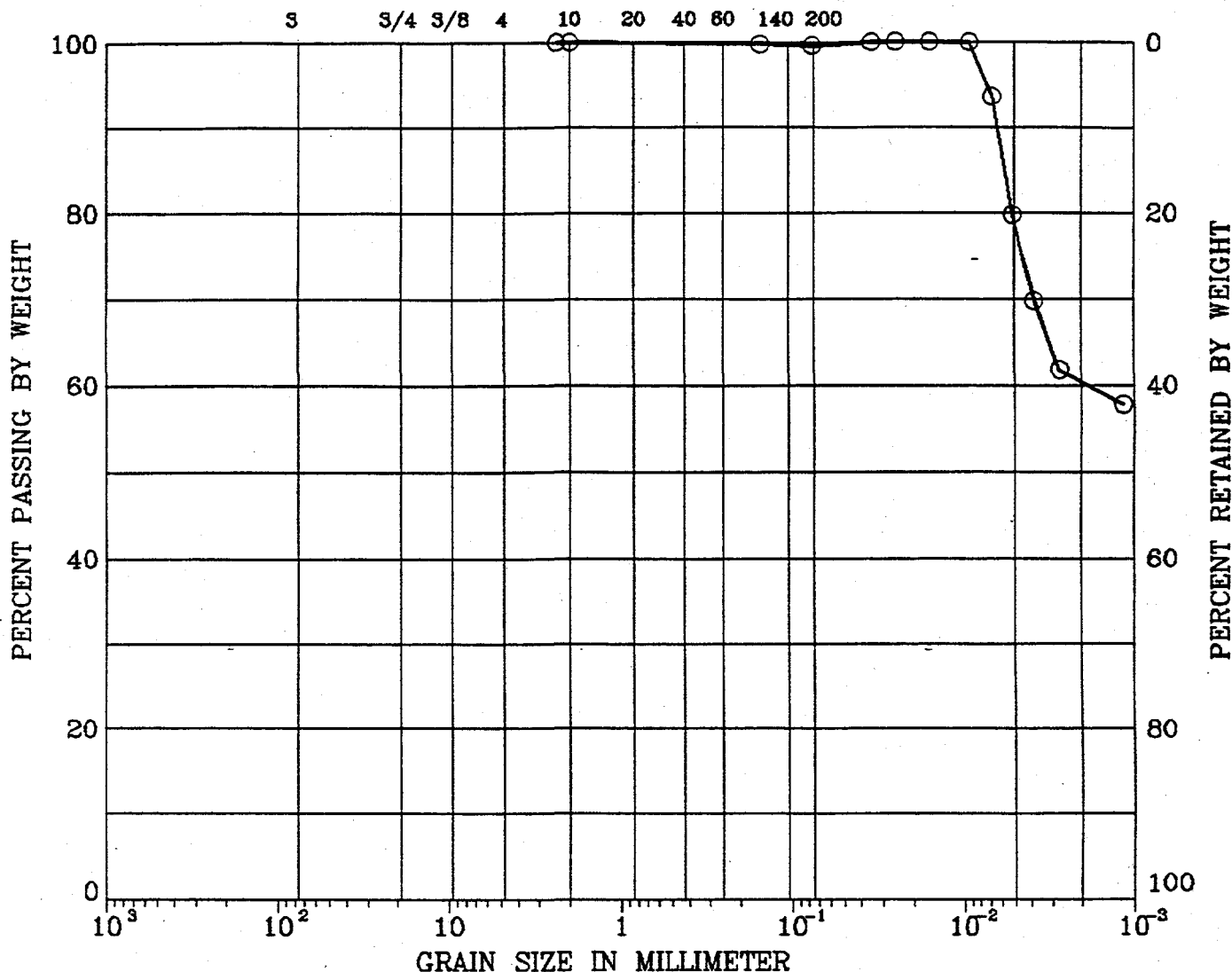
**OGDEN**  
ENVIRONMENTAL

**GRAIN SIZE DISTRIBUTION**

April 5, 1994

# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION
○	BH9-09	8.5-9.0	71	48	CLAY, slty, lt rdsh br mott gr and yelsh br USC=CH

Remark : Martin Marietta Energy Systems, Inc.

Project No. 0-4267

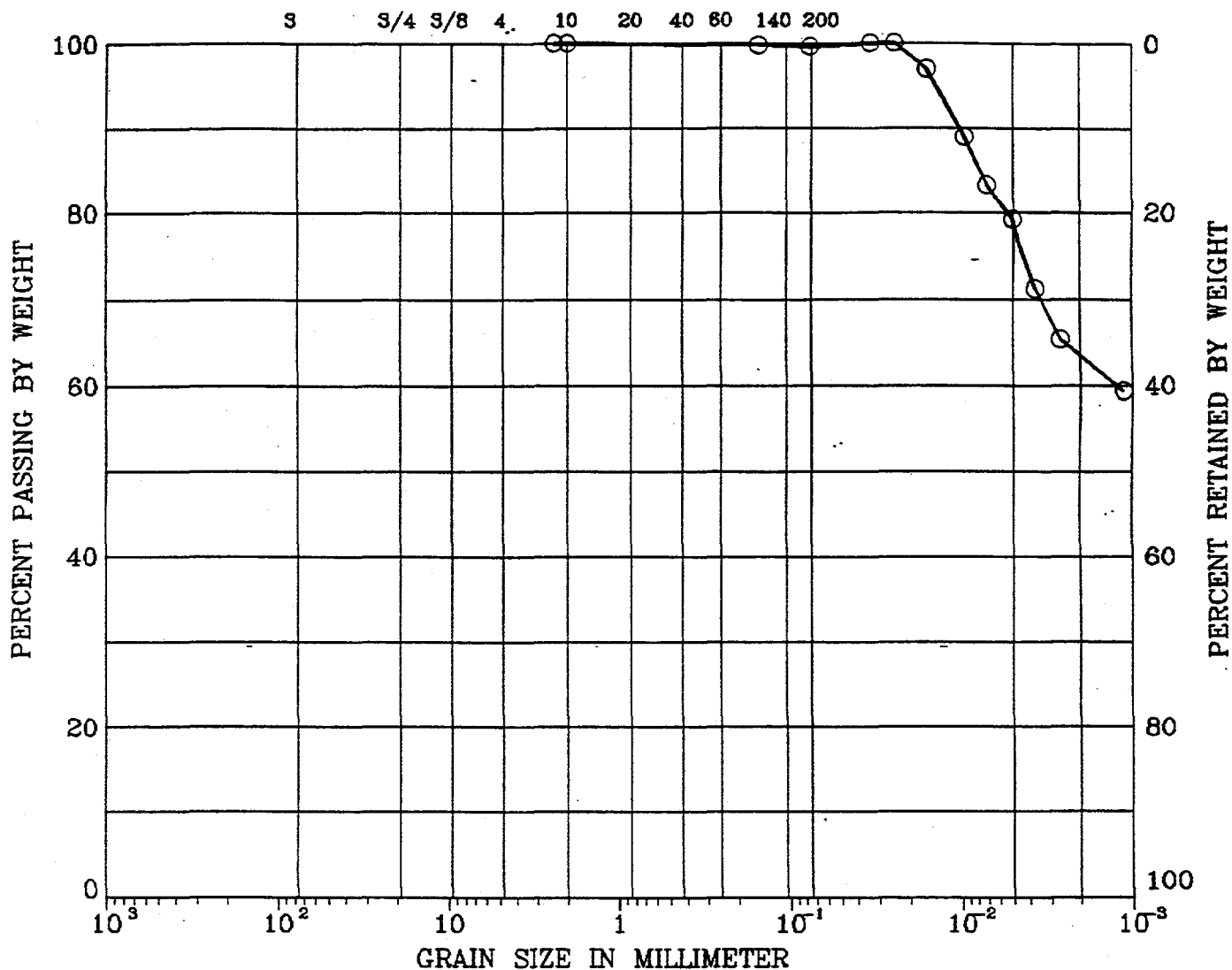
Portsmouth - OTD Mini Characterization

**OGDEN**  
ENVIRONMENTAL

**GRAIN SIZE DISTRIBUTION** April 5, 1994

# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION	
○	BH9-21	20.9-21	53	28	CLAY, silty, gray, mott rdsh br	USC=CH

Remark : Martin Marietta Energy Systems, Inc.

Project No.0-4267

Portsmouth - OTD Mini Characterization

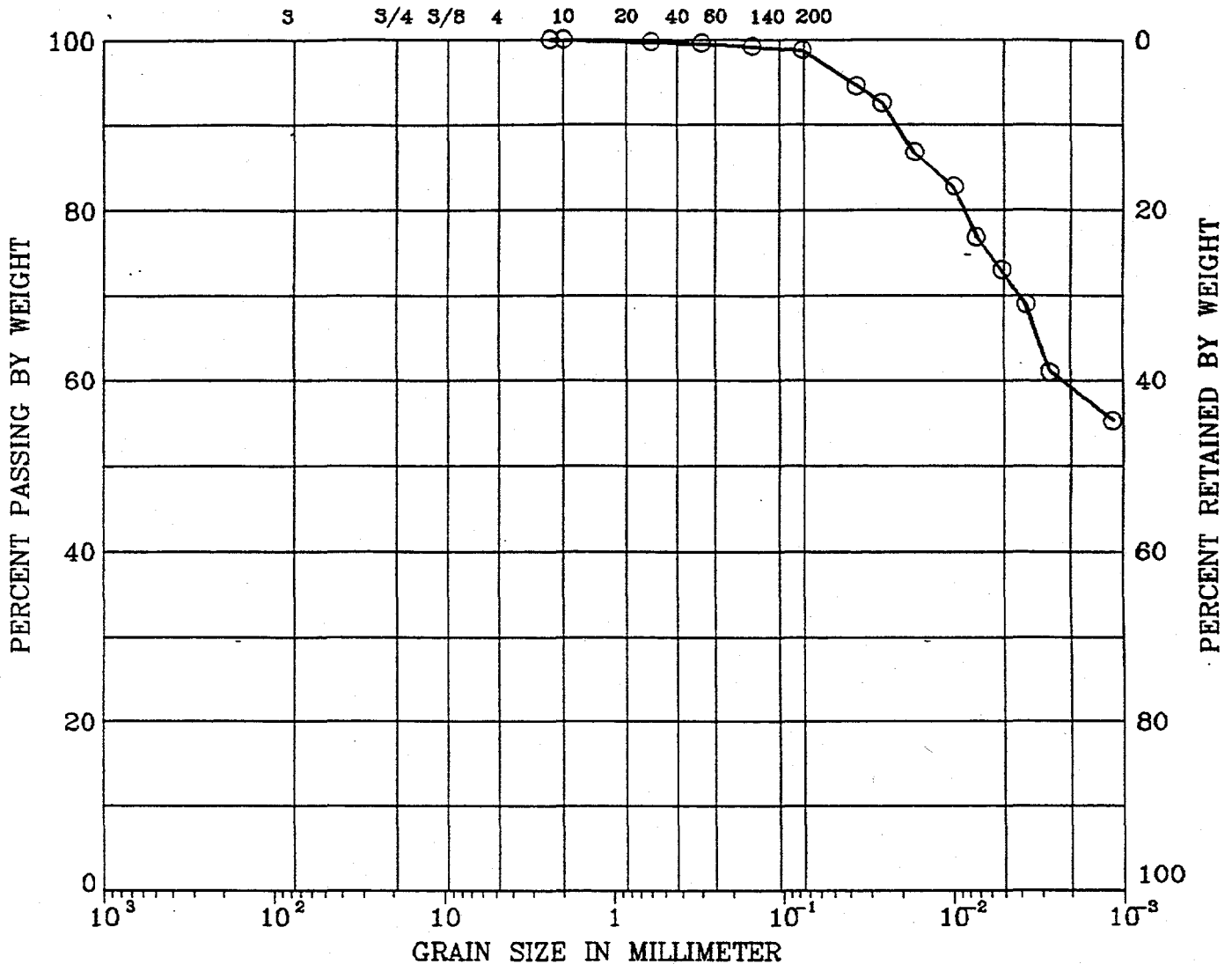
**OGDEN**  
ENVIRONMENTAL

**GRAIN SIZE DISTRIBUTION**

April 5, 1994

# UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN INCHES			U.S. STANDARD SIEVE No.			HYDROMETER



SYMBOL	BORING	DEPTH (ft)	LL (%)	PI (%)	DESCRIPTION	
○	BH9-21.5	21-21.5	51	26	CLAY, silty, gray, mott greenish br	USC=CH

Remark : Martin Marietta Energy Systems, Inc.

Project No.0-4267

Portsmouth - OTD Mini Characterization

**OGDEN**  
ENVIRONMENTAL

**GRAIN SIZE DISTRIBUTION**

April 5, 1994



## **Appendix B**

### **Vendor Information for Schumacher Porous Filters**



**SCHUMACHER**  
Umwelt- und Trenntechnik  
Ein Unternehmen der Kraftanlagen-Gruppe

## Well filters for remediation of contaminated soils and groundwater





**SCHUMACHER**

Umwelt- und Trenntechnik

Ein Unternehmen der Kraftanlagen-Gruppe

## In situ remediation of contaminated soils

The in situ cleaning of contaminated soils is a very urgent task in environmental protection. SCHUMACHER developed new parts for clean up techniques to be used for soils and groundwater. A new porous well filter consisting of pure polyethylene is very useful especially in fine grain soil types.

SCHUMACHER well filters have very specific advantageous properties for well design in the saturated and unsaturated zone.

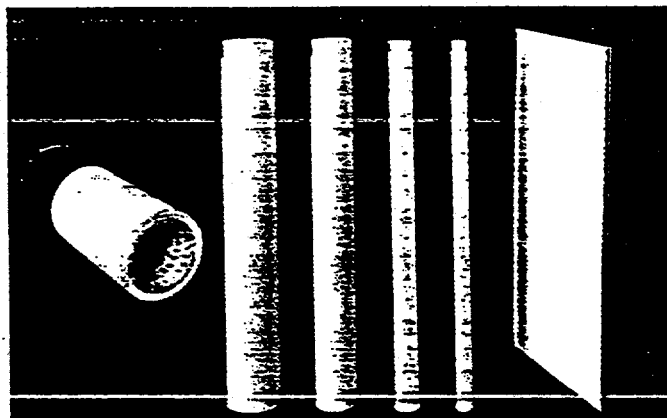
Proving ground for horizontal filter wells



### Properties

- homogeneous pore size distribution
- same chemical resistance as high density polyethylene
- hydrophobic character  
oliphilic behaviour
- low weight
- high permeability for water and air

These properties show excellent advantages compared to conventional well screens.



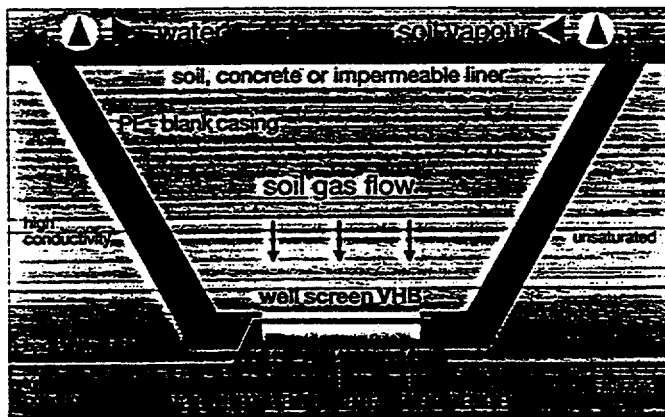
SCHUMACHER filter elements

### Advantages

- the homogeneous pore size distribution supports a laminar fluid flow through the filter across its total surface
- clogging and incrustation are avoided
- the hydrophobic character can be used to keep soil water outside the well
- the permeability of the filter to oil ensures an excellent separation of groundwater and oil

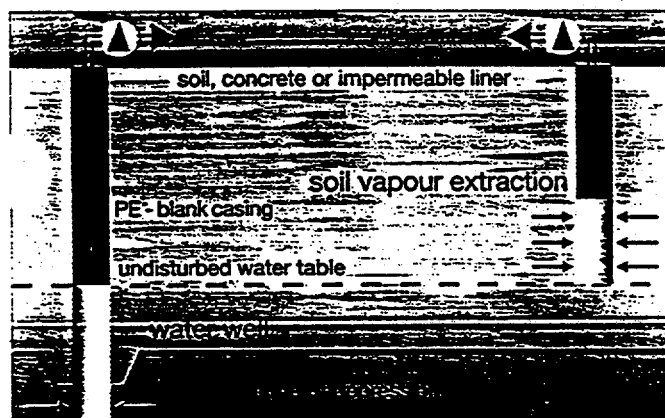


SEM photography of fracture surface



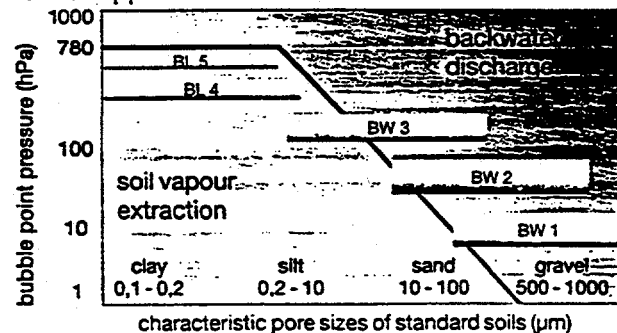
Horizontal filter well

- SCHUMACHER well filters are physiologically unobjectable.
- High mechanical strength allows the application in vertical and horizontal wells.
- Low weight and the standardized connections make transportation and installation very cost effective.
- The homogeneous porosity of SCHUMACHER well filters makes a gravel pack unnecessary and minimizes drilling diameters.
- Due to their ductility, SCHUMACHER well filters adapt to curved and horizontal wells by guided trenchless horizontal drillings (FlowTex-System).



Vertical filter well

field of application for SCHUMACHER well screens



Field of application of SCHUMACHER filter wells

### Applications

SCHUMACHER well filters are produced with five different water entry values and five different permeabilities, covering a wide spectrum of applications. Especially under difficult conditions in fine grain soil types a contamination treatment can be carried out with

- soil vapour extraction
- back water discharge
- groundwater discharge
- gas or nutrient injection

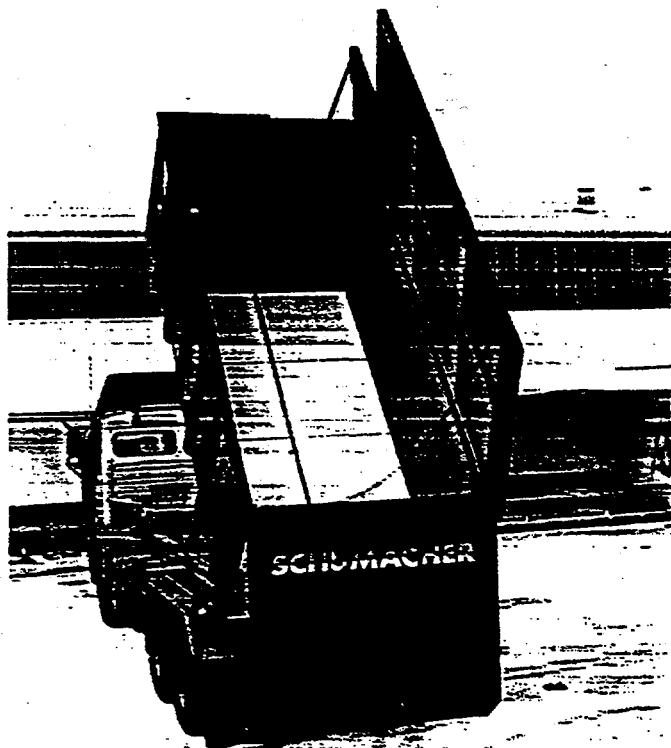
## Ex situ remediation of contaminated soils

Ex situ techniques can also be supported by SCHUMACHER filter media. Excavated contaminated soil is cleaned in a mobile container system.

The container features two different sections:

The large one is equipped with a permeable layer of porous polyethylene for the extraction of soil vapour and other fluids.

The smaller section accomodates the process engineering components such as activated carbon barrels, catalytic combustion, blower, or power generator.



Container system for ex situ remediation

### Advantages

- very flexible for different types of contaminations and fluids
- riskless and safe transportation with conventional container trucks
- "on the road" soil vapour extraction avoids contamination of the atmosphere
- applications in on-site and off-site remediation

### Construction principles

1. The extraction section is filled with contaminated soil.
2. The contaminated soil air is extracted by passing the evacuated porous layer of the container.
3. The soil air cleaning is carried out in the small section, using the required techniques.
4. After decontamination, the soil can be used for refilling, or has to be deposited on a land fill.

#### Germany

Schumacher Umwelt- und  
Trenntechnik GmbH

ir Flügela 70  
J-74564 Crailsheim  
Tel.: 07951/302-0  
Tlx: 74372 schcr d  
Fax: 07951/26807

#### France

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DMF S.A.

Z.I. 25, Rue Gay Lussac  
B.P. 38  
95502 Gonesse Cedex  
Tél.: 1/39.85.93.14  
Tlx: 688018  
Fax: 1/39.85.91.62

#### Japan

Nihon Schumacher  
K.K.

Toyo Bldg. 12-20  
Jingumae 6-Chome  
Shibuya-Ku, Tokyo  
Tel.: 81/3/34091531  
Tlx: 25561  
Fax: 81/3/34861678

#### U.S.A

Schumacher  
Filters America Inc.

P.O. Box 8040  
Asheville  
NC 28 814-8040  
Tel.: 704/252/9000  
Fax: 704/253/7773

## **Appendix C**

### **Geologic Logs and Completion Diagrams for Piezometers at the Clean Test Site**

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# Well Summary Information

OAK RIDGE NATIONAL LABORATORY

Prepared By: M.E. Mumby Date: 11/30/94 Page: 1 OF 1  
 Hole No.: CTS-PZ01 Casing Elevation: 661.83' Ground Elevation: 660.35'  
 Total Depth: 25.8' No. of Compl.: 1 Rig Type: CME-550 ATV Location: CTS-Horz. Wells  
 Auger Size: 8.25" x 4.25" Sample Type: 5' Continuous Barrel  
 Project: Ports CTS-Horz Wells Data Verified By: M.T. Muck Date: 1/9/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE ENVY	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					PT HUMUS: dark brown (7.5YR 3/2), soft, very moist, abundant organic material and roots.
1					
2	CS				
3					CL SILTY CLAY: yellowish brown (10YR 5/8), soft, increasing firmness with depth, scattered gray mottle, common small roots and root pores usually 1mm or less, increasing clay content with depth.
4					
5					
6	CS				
7					CL CLAY: yellowish brown (10YR 5/6), stiff, slightly moist, common gray (10YR 6/1) mottle, occasional small roots, scattered FeO and MnO staining, alternating beds of gray (10YR 6/1) clayey silt from 7.5 to 9.5', thicknesses range from 3mm to 1.5cm, interval appears varved.
8					
9					
10					
11	CS				CL CLAY: reddish brown (2.5YR 4/4), stiff, slightly moist, common MnO staining, grades back to a yellowish brown color by 11.5'.
12					SM SILTY SAND: light olive gray (5Y 6/2), sand is fine grained, subrounded, moderately well sorted, predominantly quartz, scattered sandstone and chert gravels to 2cm (.75").
13					
14					
15					
16	CS				ML CLAYEY SILT: brownish yellow (10YR 6/6), soft to slightly crumbly, moist, common fine to medium grained sand, scattered MnO staining, occasional FeO stained zones with some FeO nodules.
17					
18					
19					
20	CS				ML SILT: color as above, moist, moisture content increasing with depth, common fine to medium grained sand, occasional gravels to .6cm (.25").
21					
22					
23	CS				GM SANDY/SILTY GRAVEL: olive brown (2.5Y 4/4), subrounded predominantly sandstone gravels to 5cm (2") with occasional fragments of larger gravels in a sand silt matrix, wet.
24					
25	CS				Auger refusal at 23.3', probable large cobble, adjust sampler up 1", drilled to 28.5' (auger refusal).
26					
27					SHALE: very dark gray, earthy, platy, dry.
28					T.D. 28.5
29					
30					

orn1

# Well Summary Information

OAK RIDGE NATIONAL LABORATORY

Prepared By: M.E. Mumby Date: 11/30/94 Page: 1 OF 1  
 Hole No.: CTS-P202 Casing Elevation: 661.82' Ground Elevation: 660.21'  
 Total Depth: 27.0' No. of Compl.: 1 Rig Type: CME-550 ATV Location: CTS-Horz. Wells  
 Auger Size: 8.25" x 4.25" Sample Type: 5' Continuous Barrel  
 Project: Ports CTS-Horz Wells Data Verified By: M.T. Muck Date: 1/9/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
1					
2					
3					
4					
5					
6					
7					
8					
9					
10					
11					
12					
13					
14					
15					
16					
17					
18					
19					
20					
21					
22					Auger to 22.0'.
23					
24					
25	CS				
26					
27					
28					
29					
30					

ML Clayey Silt: yellowish brown (10YR 5/8), soft, moist, becoming wet at 22.2'.  
 SM SILTY SAND: yellowish brown (10YR 5/6), fine to medium grained, sub-round to sub-angular, moderately sorted, saturated.  
 GM SILTY GRAVEL: yellowish brown to brown (10YR 5/6-3/3), predominantly sub-rounded sandstone and chert gravels and occasional limestone gravels to 6cm (2.5") in a sandy silt matrix, wet, noticeable increase in sand content below 25', abundant shale fragments at 25.75', top of shale at 26.0'.  
 SHALE: very dark gray, earthy, platy, dry.  
 T.D. 27.0'.



orn1

# Well Summary Information

OAK RIDGE NATIONAL LABORATORY

Prepared By: M.E. Mumby Date: 11/30/94 Page: 1 OF 1  
 Hole No.: CTS-PZ03 Casing Elevation: 661.16' Ground Elevation: 659.62'  
 Total Depth: 25.5' No. of Compl.: 1 Rig Type: CME-550 ATV Location: CTS-Horz. Wells  
 Auger Size: 8.25" x 4.25" Sample Type: 5' Continuous Barrel  
 Project: Ports CTS-Horz Wells Data Verified By: M.T. Muck Date: 1/9/95

DEPTH (FEET)	SAMPLE TYPE	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0				PT HUMUS: dark brown (10YR 4/3), abundant grass, roots, and organic debris.
1				
2	CS			CL SILTY CLAY: color as above, soft, moist, wet in some zones, abundant roots and root pores predominantly 1mm or less, occasional roots to 1cm common organic debris, appears reworked, possible fill.
3				
4				
5				
6	CS			CL SILTY CLAY: brown (10YR 5/3) with a gray (10YR 6/1) mottle, firm, moist, abundant yellowish brown (10YR 5/8) FeO staining, common open pores up to 2mm, occasional small roots <1mm, occasional MnO staining.
7				
8				
9				CL CLAY: mottled yellowish brown (10YR 5/8) and light olive gray (5Y 6/2), stiff, slightly damp, occasional MnO staining.
10				
11	CS			CL CLAY: reddish brown (2.5YR 4/4), very stiff, slightly damp, common MnO fracture fill, grades back to a yellowish brown from 10 to 10.5'.
12				
13				
14				ML CLAYEY SILT: brownish yellow (10YR 6/6), soft, very low plasticity, moist, fairly homogeneous, slightly sandy, sand content increasing with depth.
15				
16	CS			ML CLAYEY SILT: as above, becoming very sandy, grades to a silty sand by 18', occasional sub-rounded gravels to 2.5cm (1").
17				
18				
19				
20	CS			SM SILTY SAND: brownish yellow (10YR 6/8), soft to friable, moist, very fine to medium grained, sub-angular, poorly sorted, predominantly quartz occasional dark accessory minerals, a majority of the sand grains are FeO stained to some degree.
21				
22	CS			SM SILTY SAND: strong brown (7.5Yr 4/6), friable, very moist, very fine to medium grained, sub-angular, poorly sorted, predominantly quartz with scattered limestone and chert grains, entire interval is FeO stained, occasional MnO staining, scattered dark accessory minerals.
23				
24	CS			Limestone cobble at approximately 23.8', auger refusal, pulled sampler. Run back in hole with a 1.5" splitspoon, pounded through cobble. Pull splitspoon run back in with sampler and drill to auger refusal.
25				
26				GM SANDY/SILTY GRAVEL: color as above, sub-round to occasional round sandstone, chert and occasional limestone gravels to 5cm (2") with fragments of larger gravels in a sand silt matrix, saturated, good upward fining sequence of sand from 23.8 to 25', sand is very fine to coarse grained.
27				
28				
29				
30				
31				
32				
33				SHALE: very dark gray, platy, dry.
34				Auger refusal and T.D. at 25.5'.

orn1

# Well Summary Information

OAK RIDGE NATIONAL LABORATORY

Prepared By: M.E. Mumby Date: 12/01/94 Page: 1 OF 1  
 Hole No.: CTS-PZ04 Casing Elevation: 662.51' Ground Elevation: 660.93'  
 Total Depth: 25.7' No. of Compl.: 1 Rig Type: CME-550 ATV Location: CTS-Horz. Wells  
 Auger Size: 8.25" x 4.25" Sample Type: 5' Continuous Barrel  
 Project: Ports CTS-Horz Wells Data Verified By: M.T. Muck Date: 01/09/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
1					
2					
3					
4					
5					
6					
7					
8					
9					
10					
11					
12					
13					
14					
15					
16					
17					
18					
19					
20					
21					
22					
23					
24					
25	CS				
26					
27					
28					
29					
30					

Auger to 22.0'.

SM SILTY SAND: brownish yellow (10YR 6/6), soft to friable, very moist becoming wet by 23', very fine grained, sub-angular to sub-round moderately well sorted, scattered black accessory minerals, FeO stained.

SW GRAVELLY SAND: dark yellowish brown (10YR 6/6), fine to coarse grained, sub-angular to sub-round scattered well rounded grains, predominantly quartz with common limestone, chert and very fine grained sandstone grains, gravels are sandstone and chert to 2.5cm (1"), grades to a silty gravel at approximately 25' with gravels to 5cm (2"), scattered larger fragments, occasional weathered shale fragments.

Auger refusal at 25.7', cobble.  
T.D. 25.7'.

orn1

# Well Summary Information

OAK RIDGE NATIONAL LABORATORY

Prepared By: M.E. Mumby Date: 12/01/94 Page: 1 OF 1  
 Hole No.: CIS-PZ05 Casing Elevation: 664.64 Ground Elevation: 663.10  
 Total Depth: 29.0 No. of Compl.: 1 Rig Type: CME-550 ATV Location: CIS-Horz. Wells  
 Auger Size: 8.25" x 4.25" Sample Type: 5' Continuous Barrel  
 Project: Ports CIS-Horz Wells Data Verified By: M.T. Muck Date: 01/09/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
1					
2	CS				FILL: light yellowish brown to brownish yellow (10YR 6/4-6/6), soft to firm, very moist, predominantly silty clay with scattered gravel and occasional sand, abundant roots up 1.5cm in diameter, common FeO staining, common organic debris to 1'.
3					
4					
5					
6	CS				No sample recovery from 4 to 9', possible cobble.
7					
8					
9					
10					
11	CS				Partial recovery from 9 to 14', large cobble in shoe. Appears to be Minford Silt.
12					
13					
14					
15					
16	CS				SM SILTY SAND: brownish yellow (10YR 6/8), soft to friable, sand is very fine grained (vfU), sub-angular, well sorted, abundant FeO staining, occasional black accessory minerals, large vertical fracture present throughout the entire sample interval, MnO fracture fill.
17					
18					
19					
20					
21	CS				SM SILTY SAND: as above, moist with moisture content increasing with depth.
22					
23					
24					
25					SM SILTY SAND: color as above, predominantly very fine grained with thin lenses (1-2mm) of very fine to medium grained sand, lenses are poorly sorted, sub-round, and clean, predominantly quartz with common chert grains, becoming wet by 25'.
26	CS				GM SILTY/SANDY GRAVEL: dark yellowish brown (10YR 3/6), sub-rounded chert and sandstone gravels to 5cm (2") occasional limestone gravel, scattered fragments of larger cobbles in a silt sand matrix, entire gravel interval is heavily FeO stained, wet.
27					
28					
29					SHALE: very dark gray, earthy, platy, dry.
30					T.D. 29.0'

orn1

# Well Summary Information

OAK RIDGE NATIONAL LABORATORY

Prepared By: M.E. Mumby Date: 12/02/94 Page: 1 OF 1  
 Hole No.: CTS-PZ06 Casing Elevation: 663.89' Ground Elevation: 662.26'  
 Total Depth: 29.0' No. of Compl.: 1 Rig Type: CME-550 ATV Location: CTS-Horz. Wells  
 Auger Size: 8.25" x 4.25" Sample Type: 5' Continuous Barrel  
 Project: Ports CTS-Horz Wells Data Verified By: M.T. Muck Date: 1/9/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
1					
2					
3					
4					
5					
6					
7					
8					
9					
10					
11					
12					
13					
14					
15					
16					
17					
18					
19					
20					
21					
22	CS				
23					
24					
25					
26					
27	CS				
28					
29					
30					

Auger to 19.5'.

SM SILTY SAND: brownish yellow (10YR 6/6), crumbly wet, sand is very fine to fine grained (vfU-fL), sub-angular to sub-round, moderately sorted, abundant MnO staining, grain size increasing with depth.

GM SANDY GRAVEL: yellowish brown (10YR 5/6), sub-rounded sandstone, chert, and limestone gravels from 2.5 to 10cm (2-4") and fragments of larger gravel in a silty sand matrix, sand is predominantly medium to coarse grained, sub-angular to well rounded quartz and chert, entire interval is heavily FeO stained, semi consolidated with limonite cement from 26 to 27', wet.

SHALE: very dark gray, earthy, platy, dry.

T.D. 29.0'.

**ornl**

Well Summary Information  
OAK RIDGE NATIONAL LABORATORY

Prepared By: M.E. Mumby Date: 12/04/94 Page: 1 OF 1  
Hole No.: CTS-PZ07 Casing Elevation: 658.60' Ground Elevation: 657.09'  
Total Depth: 24.5' No. of Compl.: 1 Rig Type: CME-550 ATV Location: CTS-Horz. Wells  
Auger Size: 8.25" x 4.25" Sample Type: 5' Continuous Barrel  
Project: Ports CTS-Horz Wells Data Verified By: M.T. Muck Date: 01/09/95

DEPTH FEET	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
1					
2					
3					
4					
5					
6					
7					
8					
9					
10					
11					
12					
13					
14					
15					
16					
17					
18					
19					
20					
21					
22	CS				
23					
24					
25					
26					
27					
28					
29					
30					

Auger to 19.5'.

Trace lower Minford in top of sampler.

GM SILTY GRAVEL: dark yellowish brown to strong brown (10YR 4/6-7.5YR 4/6), sub-rounded sandstone, chert, and limestone gravels to 5cm (2"), scattered fragments of larger gravel, all in a sandy silt matrix, wet, heavily FeO stained, lithified zone from approximately 22-22.8', cemented with limonite.

SHALE: very dark gray, earthy, platy, dry.

T.D. 29.0'.

**ornl**

# Well Summary Information

OAK RIDGE NATIONAL LABORATORY

Prepared By: M.E. Mumby Date: 12/04/94 Page: 1 OF 1  
 Hole No.: CTS-P208 Casing Elevation: 659.19 Ground Elevation: 657.73  
 Total Depth: 24.5' No. of Compl.: 1 Rig Type: CME-550 ATV Location: CTS-Horz. Wells  
 Auger Size: 8.25" x 4.25" Sample Type: 5' Continuous Barrel  
 Project: Ports CTS-Horz Wells Data Verified By: M.T. Muck Date: 01/09/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE ID#	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
1					
2					
3					
4					
5					
6					
7					
8					
9					
10					
11					
12					
13					
14					
15					
16					
17					
18					
19					
20					
21					
22	CS				
23					
24					
25					
26					
27					
28					
29					
30					

Auger to 19.5'.

Lower Minford.

GM SILTY/SANDY GRAVEL: strong brown (7.5YR 4/6) sub-rounded sandstone, chert and limestone gravels to 5cm (2") with scattered fragments of larger gravel in a sandy silt matrix, wet, lithified to some degree from 22-23', cemented with limonite cement, entire sample interval is heavily FeO stained, silt content increasing with depth.

SHALE: very dark gray, earthy, platy, dry.

T.D. 29.0'.

Prepared By: M.E. Mumby Date: 12/04/94 Page: 1 OF 1  
Hole No.: CTSP709.10 Casing Elevation: 09-661.93' 10-662.08' Ground Elevation: 660.44'  
Total Depth: 27.5' No. of Compl.: 2 Rig Type: CME-550 ATV Location: CTS-Horz. Wells  
Auger Size: 8.25" x 4.25" Sample Type: 5' Continuous Barrel  
Project: Ports CTS-Horz Wells Data Verified By: M.T. Muck Date: 01/09/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
1					
2					
3					
4					
5					
6					
7					
8					
9					
10					
11					
12	CS				CL SILTY CLAY: mottled yellowish brown (10YR 6/8) and gray (10YR 6/1). firm to stiff, damp, common FeO staining, clay content increasing with depth.
13					
14					
15					
16					
17	CS				CL CLAY: mottled yellowish red (5YR 6/6) and greenish gray (5GY 6/1). stiff, damp, moderate to fairly high plasticity, scattered MnO staining.
18					
19					
20					
21					
22	CS				ML SANDY SILT: olive yellow (2.5Y 6/6). soft to friable, wet, abundant FeO staining, sand is very fine grained, sub-angular to sub-round occasional black accessory minerals, occasional MnO staining.
23					
24					
25					
26	CS				SM SANDY SILT: brownish yellow (10YR 6/8) friable, damp, abundant FeO staining, sand is fine grained, grain size increasing with depth, becomes fine to medium grained by 23'.
27					
28					
29					
30					
					GM SANDY/SILTY GRAVEL: yellowish brown (10YR 5/8), sub-rounded to well rounded chert, sandstone, and scattered limestone gravels to 5cm (2") with scattered fragments of larger gravel in a sand/silt matrix, saturated, fining upwards sequence of sand from 25-26.5', grades from a coarse grained sand at 26.5' to a fine grained sand at 25', grades to a clayey gravel at approximately 27', entire interval is heavily FeO stained.
					SHALE: very dark gray, earthy, platy, dry.
					T.D. 27.5'.

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# Well Summary Information

OAK RIDGE NATIONAL LABORATORY

Prepared By: M.E. Mumby Date: 12/03/94 Page: 1 OF 1  
 Hole No.: CTS-PZ11 Casing Elevation: 663.82' Ground Elevation: 662.25'  
 Total Depth: 29.5' No. of Compl.: 1 Rig Type: CME-550 ATV Location: CTS-Horz. Wells  
 Auger Size: 8.25" x 4.25" Sample Type: 5' Continuous Barrel  
 Project: Ports CTS-Horz Wells Data Verified By: M.T. Muck Date: 01/09/95

DEPTH FEET	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
1					
2					
3					
4					
5					
6					
7					
8					
9					
10					
11					
12	CS				
13					
14					
15					
16					
17	CS				
18					
19					
20					
21					
22	CS				
23					
24					
25					
26					
27	CS				
28					
29					
30					

Auger to 9.5'.

SM SANDY SILT: brownish yellow (10YR 6/6), soft to crumbly, wet, sand is very fine grained, sub-angular, abundant, FeO and MnO staining, occasional nodules of both, scattered gravels and occasional cobbles to 8cm (4").

SM SANDY SILT: as above, increasing silt content with depth.

SM SILT: yellowish brown (10YR 5/8), crumbly, moist, slightly sandy, becomes sandy at 24', sand is fine to medium grained, with scattered coarse grained sand, predominantly quartz and chert, abundant FeO staining.

GM SANDY GRAVEL: dark yellowish brown (10YR subrounded gravels to 5cm (2") and scattered cobble fragments >10cm (4"), gravels consist of sandstone, chert and occasional limestone in a sandy silt matrix, saturated, lithified with limonite cement from 27.5 to 28.5', entire interval is heavily FeO stained.

SHALE: very dark gray, earthy, platy, dry.

T.D. 29.5'.



**ornl**

Well Summary Information  
OAK RIDGE NATIONAL LABORATORY

Prepared By: M.E. Mumby Date: 12/04/94 Page: 1 OF 1  
Hole No.: CTS-PZ12 Casing Elevation: 669.59' Ground Elevation: 662.25'  
Total Depth: 20.0' No. of Compl.: 1 Rig Type: CME-550 ATV Location: CTS-Horz. Wells  
Auger Size: 8.25" x 4.25" Sample Type: 5' Continuous Barrel  
Project: Ports CTS-Horz Wells Data Verified By: M.T. Muck Date: 01/09/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
1					
2					Auger to 20.0'.
3					
4					
5					
6					
7					
8					
9					
10					
11					
12					
13					
14					
15					
16					
17					
18					
19					
20					T.D. 20.0'.
21					
22					
23					
24					
25					
26					
27					
28					
29					
30					

Prepared By: M.E. Mumby Date: 12/03/94 Page: 1 OF 1  
Hole No.: CTSPZ13.14 Casing Elevation: 13-664.65' 14-664.81' Ground Elevation: 663.08'  
Total Depth: 29.5' No. of Compl.: 2 Rig Type: CME-550 ATV Location: CIS-Horz. Wells  
Auger Size: 8.25" x 4.25" Sample Type: 5' Continuous Barrel  
Project: Ports CIS-Horz Wells Data Verified By: M.T. Muck Date: 01/09/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					FILL: yellowish brown (10YR 5/6), soft, very moist predominantly silty clay with scattered small pebble gravel, abundant roots and root pores to approximately 2'. occasional coarse grained sand becomes dark brown from 3.5 to 4'. appears to be the original ground surface, common roots, root pores and organic debris.
1					
2	CS				
3					
4					
5					
6					
7	CS				CL SILTY CLAY: mottled yellowish brown (10YR 6/8) and gray (10YR 6/1), crumbly to soft, slightly damp, abundant FeO staining, occasional nodules occasional sub-rounded gravels to 1.9cm (.75").
8					
9					
10					CL SILTY CLAY: as above, occasional gravels to 5cm (2"), becomes gravelly from 11 to 11.5' (Top of Minford Silt).
11					
12	CS				
13					
14					SM SILTY SAND: brownish yellow (10YR 5/8), very soft to friable, wet, sand is very fine grained sub-round, well sorted, common FeO staining, occasional MnO staining.
15					
16					
17	CS				SM SILTY SAND: as above, increasing silt content wet.
18					
19					
20					SM SANDY SILT: yellowish brown (10YR 5/8), soft to crumbly, damp, sand is predominantly very fine grained to approximately 23', increasing fine to medium grained sand below 23' common FeO staining.
21					
22	CS				
23					
24					SM SILTY SAND: color as above, very fine to medium grained, sub-angular to round, poorly sorted, predominantly quartz with common chert and limonite grains, becoming wet at 25'.
25					GM SANDY/SILTY GRAVEL: dark yellowish brown (10YR 4/6), subrounded sandstone, chert, and scattered limestone gravels to 5cm (2") with scattered fragments of larger gravel in a sand/silt matrix, wet, entire interval is heavily FeO stained, lithified from 28 to 29', cemented with limonite.
26					
27	CS				
28					
29					SHALE: very dark gray, earthy, platy, dry.
30					

T.D. 29.5'

orn1

# Well Summary Information

OAK RIDGE NATIONAL LABORATORY

Prepared By: M.E. Mumby Date: 12/02/94 Page: 1 OF 1  
 Hole No.: CTS-PZ15 Casing Elevation: 662.66' Ground Elevation: 661.39'  
 Total Depth: 28.0' No. of Compl.: 1 Rig Type: CME-550 ATV Location: CTS-Horz. Wells  
 Auger Size: 8.25" x 4.25" Sample Type: 5' Continuous Barrel  
 Project: Ports CTS-Horz Wells Data Verified By: M.T. Muck Date: 01/09/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE ID#	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
1					
2					
3					
4					
5					
6					
7					
8					
9					
10					
11					
12					
13					
14					
15					
16					
17					
18					
19					
20					
21					
22					
23					Auger to 23'.
24	CS				Lower Minford.
25					GM SANDY GRAVEL: yellowish brown (10YR 5/8) sub-
26					round to round sandstone, chert, and occasional
27	CS				limestone gravels to 5cm (2"), occasional
28					cobbles >10cm (4") in a silty sand matrix, wet.
29					sand is fine to very coarse grained sub-angular
30					to sub-rounded quartz and chert, entire interval
					is FeO stained.
					SHALE: very dark gray, earthy, platy, dry.
					T.D. 29.5'.

orn1

# Well Summary Information

OAK RIDGE NATIONAL LABORATORY

Prepared By: M.E. Mumby Date: 12/02/94 Page: 1 OF 1  
 Hole No.: CTS-PZ16 Casing Elevation: 663.65' Ground Elevation: 662.28'  
 Total Depth: 29.5' No. of Compl.: 1 Rig Type: CME-550 ATV Location: CTS-Horz. Wells  
 Auger Size: 8.25" x 4.25" Sample Type: 5' Continuous Barrel  
 Project: Ports CTS-Horz Wells Data Verified By: M.T. Muck Date: 01/09/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
1					
2	CS				CL SILTY CLAY: light yellowish brown (10YR 6/4), firm, moist, abundant brownish yellow (10YR 7/1) mottle, common organic debris to 1", abundant roots and root channels to 1mm, scattered FeO nodules (Limonite?).
3					
4					
5					
6					
7	CS				CL SILTY CLAY: predominantly yellowish brown (10YR 5/8), very firm moist, common light gray (10YR 7/1) mottle, scattered very small open pores 1mm or less, common gravels to 1.8cm, occasional to 2.5cm (1"), abundant FeO staining occasional nodules, increasing silt content with depth.
8					
9					
10					
11					
12	CS				Partial recovery from 9.5 to 14.5'.
13					
14					
15					
16					
17	CS				SM SILTY SAND: brownish yellow (10YR 6/6), very soft, wet, very fine grained, sub-angular, well sorted, scattered fine grained sand, occasional dark accessory minerals, common FeO staining, occasional black carbonaceous or MnO debris or staining.
18					
19					
20	CS				SM SANDY SILT: color as above, crumbly, moist, sand is predominantly very fine grained, increasing fine grained sand at approximately 18' increasing chert grains at 18', grades to a silty sand by 20', alternating zones of very fine grained sand as above and zones of fine to medium grained sand that is sub-angular to well rounded, poorly sorted, abundant chert grains present in the fine to medium grained zones, entire interval from 19 to 21' is slightly FeO stained, scattered red chert gravels to 2.5cm (1").
21					
22					
23	CS				GM SANDY/SILTY GRAVEL: dark yellowish brown (10YR 4/6), sub-rounded sandstone, chert and occasional limestone gravels to 5cm (2"), in a sand silt matrix, wet, heavily FeO stained.
24					
25					
26					
27	CS				SW SAND: color as above, predominantly medium to coarse grained, scattered fine grained, sub-round to well rounded, poorly sorted, grains are predominantly quartz and chert with the chert comprising a majority of the coarse grains, abundant limonite nodules and grains, common gravel to 1.8cm (.75"), saturated, grades back to a silty gravel at approximately 27'.
28					
29					
30					SHALE: very dark gray, earthy, platy, dry. T.D. 29.5'.

Well Summary Information

Prepared By: M.E. Mumby Date: 12/05/94 Page: 1 OF 1  
 Hole No.: CTS-PZ17 Casing Elevation: 663.99' Ground Elevation: 662.45'  
 Total Depth: 29.5' No. of Compl.: 1 Rig Type: CME-550 ATV Location: CTS-Horz. Wells  
 Auger Size: 8.25" x 4.25" Sample Type: 5' Continuous Barrel  
 Project: Ports CTS-Horz Wells Data Verified By: M.T. Muck Date: 01/09/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
1					
2					
3					
4					
5					
6					
7					
8					
9					
10					
11					
12					
13					
14					
15					
16					
17					
18					
19					
20					
21					
22	CS				
23					
24					
25					
26					
27	CS				
28					
29					
30					

Auger to 19.5'.

SM SANDY SILT: brownish yellow (10YR 6/8), soft, to crumbly, moist, abundant FeO staining and nodules, sand is very fine grained, increasing grain size and chert content with depth.

SM SILTY SAND: color as above, friable, becoming wet br 25', sand is fine to medium grained, sub-angular to well rounded, predominantly quartz and chert with scattered limonite grains.

GM SILTY GRAVEL: dark yellowish brown (10YR 4/4) sub-rounded sandstone, chert, and occasional limestone gravels to 5cm (2"), occasional fragments of larger gravels in a sandy silt matrix wet, lithified zone from 26.5 to 27.5' cemented with limonite, entire interval is heavily FeO stained, trace weathered shale at tip of sampler shoe.

T.D. 29.5'.

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# Well Summary Information

OAK RIDGE NATIONAL LABORATORY

Prepared By: M.E. Mumby Date: 12/06/94 Page: 1 OF 1  
 Hole No.: CTS-PZ18 Casing Elevation: 662.21' Ground Elevation: 660.79'  
 Total Depth: 28.0' No. of Compl.: 1 Rig Type: CME-550 ATV Location: CTS-Horz. Wells  
 Auger Size: 8.25" x 4.25" Sample Type: 5' Continuous Barrel  
 Project: Ports CTS-Horz Wells Data Verified By: M.T. Muck Date: 01/09/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
1					
2					
3					
4					
5					
6					
7					
8					
9					
10					
11					
12					
13					
14					
15					
16					
17					
18					
19					
20					
21	CS				SM SANDY SILT: brownish yellow (10YR 6/8), soft, to friable, very moist, sand is predominantly very fine grained, sub-angular to sub-rounded with grain size increasing to fine grained with depth, common FeO nodules.
22					
23					
24					
25	CS				GM SANDY GRAVEL: dark yellowish brown (10YR 4/4) sub-rounded sandstone, chert, and occasional limestone gravels to 5cm (2"), occasional fragments of larger gravels in a silty sand matrix, wet, lithified zone from 24.5 to 26', cemented with limonite, entire interval is heavily FeO stained.
26					
27					
28					SHALE: very dark gray earthy, platy, dry.
29					T.D. 29.5'.
30					

ornl

# Well Summary Information

Prepared By: M.E. Mumby Date: 12/05/94 Page: 1 OF 1  
 Hole No.: CTS-PZ19 Casing Elevation: 664.15' Ground Elevation: 662.66'  
 Total Depth: 29.0' No. of Compl.: 1 Rig Type: CME-550 ATV Location: CTS-Horz. Wells  
 Auger Size: 8.25" x 4.25" Sample Type: 5' Continuous Barrel  
 Project: Ports CTS-Horz Wells Data Verified By: M.T. Muck Date: 01/09/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
1					
2					
3					
4					
5					
6					
7					
8					
9					
10					
11					
12					
13					
14					
15					
16					
17					
18					
19					
20					
21					
22	CS				SM SILT: brownish yellow (10YR 6/8), soft to slightly crumbly in spots, very moist, slightly sandy <20% abundant FeO staining, sand content increasing by 24'.
23					
24					
25					
26					
27	CS				GM SILTY/SANDY GRAVEL: yellowish brown (10YR 5/8), sub-rounded sandstone, chert, and occasional limestone gravels to 5cm (2"), occasional fragments of larger gravels in a silt/sand matrix, wet, lithified zone from 26 to 27.25', cemented with limonite, entire interval is heavily FeO stained, scattered shale fragments present in the lithified zone.
28					
29					SHALE: very dark gray earthy, platy, dry.
30					T.D. 28'.

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# Well Summary Information

OAK RIDGE NATIONAL LABORATORY

Prepared By: M.E. Mumby Date: 12/05/94 Page: 1 OF 1  
 Hole No.: CTS-PZ20 Casing Elevation: 664.67' Ground Elevation: 663.25'  
 Total Depth: 29.5' No. of Compl.: 1 Rig Type: CME-550 ATV Location: CTS-Horz. Wells  
 Auger Size: 8.25" x 4.25" Sample Type: 5' Continuous Barrel  
 Project: Ports CTS-Horz Wells Data Verified By: M.T. Muck Date: 01/09/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE ID	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
1					
2					
3					
4					
5					
6					
7					
8					
9					
10					
11					
12					
13					
14					
15					
16					
17					
18					
19					
20					
21					
22	CS				SM SILT: yellowish brown (10YR 5/8), soft to crumbly, very moist, sandy in some zones, these zones are wet, abundant FeO staining, sand content increasing by 24'.
23					
24					
25					
26					
27	CS				GM SILTY/SANDY GRAVEL: yellowish brown to dark yellowish brown (10YR 5/8-4/4), sub-rounded sandstone, chert and occasional limestone gravels, to 5cm (2") occasional fragments of larger gravels in a silt/sand matrix, wet, lithified zone from 27 to 28', cemented with limonite, entire interval is heavily FeO stained, scattered shale fragments present in the lithified zone, weathered shale at bottom of sample interval (29.5').
28					
29					
30					

Auger to 19.5'.

SM SILT: yellowish brown (10YR 5/8), soft to crumbly, very moist, sandy in some zones, these zones are wet, abundant FeO staining, sand content increasing by 24'.

GM SILTY/SANDY GRAVEL: yellowish brown to dark yellowish brown (10YR 5/8-4/4), sub-rounded sandstone, chert and occasional limestone gravels, to 5cm (2") occasional fragments of larger gravels in a silt/sand matrix, wet, lithified zone from 27 to 28', cemented with limonite, entire interval is heavily FeO stained, scattered shale fragments present in the lithified zone, weathered shale at bottom of sample interval (29.5').

T.D. 29.5'.



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# Well Summary Information

OAK RIDGE NATIONAL LABORATORY

Prepared By: M.E. Mumby Date: 12/06/94 Page: 1 OF 1  
 Hole No.: CTS-PZ21 Casing Elevation: 663.85' Ground Elevation: 662.41'  
 Total Depth: 29' No. of Compl.: 1 Rig Type: CME-550 ATV Location: CTS-Horz. Wells  
 Auger Size: 8.25" x 4.25" Sample Type: 5' Continuous Barrel  
 Project: Ports CTS-Horz Wells Data Verified By: M.T. Muck Date: 01/09/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE IDTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
1					
2					
3					
4					
5					
6					
7					
8					
9					
10					
11					
12					
13					
14					
15					
16					
17					
18					
19					
20					
21					
22	CS				SM SANDY SILT: brownish yellow (10YR 5/8), soft to friable, very moist, sand is predominantly very fine grained, sub-angular to sub-rounded, grain size increasing with depth, common FeO staining.
23					
24					
25					
26	CS				GM SANDY GRAVEL: dark yellowish brown (10YR 4/4), sub-rounded sandstone, chert and occasional limestone gravels, to 5cm (2") in a silty sand matrix, wet, lithified zone from 26.5 to 27.2' cemented with limonite, entire interval is heavily FeO stained.
27					
28					
29					
30					

Auger to 19.5'.

SM SANDY SILT: brownish yellow (10YR 5/8), soft to friable, very moist, sand is predominantly very fine grained, sub-angular to sub-rounded, grain size increasing with depth, common FeO staining.

GM SANDY GRAVEL: dark yellowish brown (10YR 4/4), sub-rounded sandstone, chert and occasional limestone gravels, to 5cm (2") in a silty sand matrix, wet, lithified zone from 26.5 to 27.2' cemented with limonite, entire interval is heavily FeO stained.

T.D. 29'.

**ornl**

Well Summary Information  
OAK RIDGE NATIONAL LABORATORY

Prepared By: M.E. Mumby Date: 12/06/94 Page: 1 OF 1  
Hole No.: CTS-PZ22 Casing Elevation: 663.49' Ground Elevation: 662.07'  
Total Depth: 29.5' No. of Compl.: 1 Rig Type: CME-550 ATV Location: CTS-Horz. Wells  
Auger Size: 8.25" x 4.25" Sample Type: 5' Continuous Barrel  
Project: Ports CTS-Horz Wells Data Verified By: M.T. Muck Date: 01/09/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
1					
2					
3					
4					
5					
6					
7					
8					
9					
10					
11					
12					
13					
14					
15					
16					
17					
18					
19					
20					
21					
22	CS				
23					
24					
25					
26					
27	CS				
28					
29					
30					

Auger to 19.5'.

SM SANDY SILT: light olive gray (5Y 6/2) mottled yellowish brown (10YR 5/8), soft, very moist, sand is predominantly very fine grained with the grain size increasing with depth to medium grained, grades to a silty sand at 24'.

GM SILTY GRAVEL: yellowish brown to dark yellowish brown, (10YR 5/8-4/4), sub-rounded sandstone, chert and occasional limestone gravels to 5cm (2"), in a silty sand matrix, wet, lithified zone from 26 to 26.5', cemented with limonite, entire zone is heavily FeO stained.

SHALE: very dark gray, earthy, platy, dry, occasional fractures with FeO staining along the fracture faces.  
T.D. 29.5'.

Prepared By: R.M.Schlosser Date: 01/21/95 Page: 1 OF 1  
Hole No.: CTSPZ23 Casing Elevation: \_\_\_\_\_ Ground Elevation: \_\_\_\_\_  
Total Depth: 24.0' No. of Compl.: 1 Rig Type: ORNL U2CRT Location: Clean Test Site  
Auger Size: 3" Sample Type: None  
Project: PORTS/CTS Data Verified By: M.E. Mumby Date: 02/20/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
2					
4					Auger to 21' using 3" augers. Drive "Power point" to 24'. Pull annulus seal to 24'. set 3/4" .010" slotted screen 21'-24'. #2 Frac sand 18'-20'. Bentonite chips (3/4"). 18'-surface Surface casing 4" PVC cemented in place.
6					
8					
10					
12					
14					
16					
18					
20					
22					
24					

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# Piezometer Summary Information OAK RIDGE NATIONAL LABORATORY

Prepared By: R.M. Schlosser Date: 01/22/95 Page: 1 OF 1  
 Hole No.: CTSPZ24 Casing Elevation: \_\_\_\_\_ Ground Elevation: \_\_\_\_\_  
 Total Depth: 24.5' No. of Compl.: 1 Rig Type: ORNL U2CRT Location: Clean Test Site  
 Auger Size: 4" Sample Type: None  
 Project: PORTS/CTS Data Verified By: M.E. Mumby Date: 02/20/95

DEPTH (FEET)	SAMPLE TYPE	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0				
2				
4				
6				
8				
10				
12				
14				
16				
18				
20				
22				
24				

Auger to 21.5' using 4" augers.  
 Drive "Power point" to 24.5'.  
 Pull annulus seal to 21.5', set 3/4" .010" slotted  
 screen 21.5'-24.5'.  
 #2 Frac sand 21.5'-24.5'.  
 Bentonite chips (3/4"). 21.5'-surface  
 Surface casing. 4" PVC cemented in place.

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# OAK RIDGE NATIONAL LABORATORY Piezometer Summary Information

Prepared By: R.M. Schlosser Date: 01/23/95 Page: 1 OF 1  
 Hole No.: CTSPZ25 Casing Elevation: \_\_\_\_\_ Ground Elevation: \_\_\_\_\_  
 Total Depth: 24.5' No. of Compl.: 1 Rig Type: ORNL U2CRT Location: Clean Test Site  
 Auger Size: 4" Sample Type: None  
 Project: PORTS/CTS Data Verified By: M.E. Mumby Date: 02/20/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
2					
4					
6					
8					
10					
12					
14					
16					
18					
20					
22					
24					

Auger to 23.5' using 4" augers.  
 Drive "Power point" to 24.5'.  
 Pull annulus seal to 22.5', set 3/4" .010" slotted  
 screen 22.5'-24.5'.  
 #2 Frac sand 22.5'-24.5'.  
 Bentonite chips (3/4"), 22.5'-surface  
 Surface casing. 4" PVC cemented in place.

### Piezometer Summary Information

OAK RIDGE NATIONAL LABORATORY

Prepared By: R.M. Schlosser Date: 01/24/95 Page: 1 OF 1  
Hole No.: CTSPZ26 Casing Elevation: \_\_\_\_\_ Ground Elevation: \_\_\_\_\_  
Total Depth: 25' No. of Compl.: 1 Rig Type: GRNL U2CRT Location: Clean Test Site  
Auger Size: 4" Sample Type: None  
Project: PORTS/CTS Data Verified By: M.E. Mumpby Date: 02/20/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
2					
4					Auger to 24' using 4" augers. Drive "Power point" to 25'. Pull annulus seal to 22.5', set 3/4" .010" slotted screen 22.5'-24.5'. #2 Frac sand 19.5'-22.5'. Bentonite chips (3/4"), 19.5'-surface Surface casing. 4" PVC cemented in place.
6					
8					
10					
12					
14					
16					
18					
20					
22					
24					

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# Piezometer Summary Information OAK RIDGE NATIONAL LABORATORY

Prepared By: R.M. Schlosser Date: 01/23/95 Page: 1 OF 1  
Hole No.: CTSPZ27 Casing Elevation: \_\_\_\_\_ Ground Elevation: \_\_\_\_\_  
Total Depth: 25' No. of Compl.: 1 Rig Type: ORNL U2CRT Location: Clean Test Site  
Auger Size: 4" Sample Type: None  
Project: PORTS/CTS Data Verified By: M.E. Mumby Date: 02/20/95

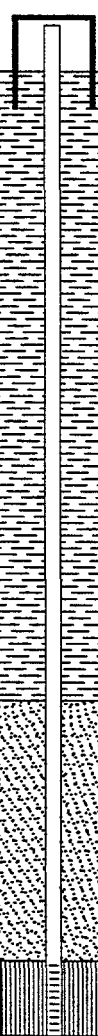
DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
2					
4					
6					
8					
10					
12					
14					
16					
18					
20					
22					
24					

Auger to 22.5' using 4" augers.  
Drive "Power point" to 25'.  
Pull annulus seal to 22.5', set 3/4" .010" slotted  
screen 22.5'-25'.  
#2 Frac sand 17'-22.5'.  
Bentonite chips (3/4"), 17'-surface  
Surface casing, 4" PVC cemented in place.

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# Piezometer Summary Information OAK RIDGE NATIONAL LABORATORY

Prepared By: R.M. Schlosser Date: 01/23/95 Page: 1 OF 1  
 Hole No.: CTSP228 Casing Elevation: \_\_\_\_\_ Ground Elevation: \_\_\_\_\_  
 Total Depth: 26' No. of Compl.: 1 Rig Type: ORNL U2CRT Location: Clean Test Site  
 Auger Size: 4" Sample Type: None  
 Project: PORTS/CTS Data Verified By: M.E. Mumpby Date: 02/20/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
2					
4					
6					
8					
10					
12					
14					
16					
18					
20					
22					
24					
26					
28					
30					

Auger to 24' using 4" augers.  
 Drive "Power point" to 26'.  
 Pull annulus seal to 24', set 3/4" .010" slotted  
 screen 24'-26'.  
 #2 Frac sand 17'-24'.  
 Bentonite chips (3/4"), 17'-surface  
 Surface casing, 4" PVC cemented in place.



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# Piezometer Summary Information

OAK RIDGE NATIONAL LABORATORY

Prepared By: R.M. Schlosser Date: 01/23/95 Page: 1 OF 1  
 Hole No.: CTSPZ29 Casing Elevation: \_\_\_\_\_ Ground Elevation: \_\_\_\_\_  
 Total Depth: 26' No. of Compl.: 1 Rig Type: ORNL U2CRT Location: Clean Test Site  
 Auger Size: 4" Sample Type: None  
 Project: PORTS/CTS Data Verified By: M.E. Mumby Date: 02/20/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE ID	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
2					
4					
6					
8					
10					
12					
14					
16					
18					
20					
22					
24					
26					
28					
30					

Auger to 24' using 4" augers.  
 Drive "Power point" to 26'.  
 Pull annulus seal to 24', set 3/4" .010" slotted  
 screen 24'-26'.  
 #2 Frac sand 7'-24'.  
 Bentonite chips (3/4"), 17'-surface  
 Surface casing. 4" PVC cemented in place.

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# Piezometer Summary Information OAK RIDGE NATIONAL LABORATORY

Prepared By: R.M. Schlosser Date: 01/24/95 Page: 1 OF 1  
 Hole No.: CTSPZ30 Casing Elevation: \_\_\_\_\_ Ground Elevation: \_\_\_\_\_  
 Total Depth: 28' No. of Compl.: 1 Rig Type: ORNL U2CRT Location: Clean Test Site  
 Auger Size: 4" Sample Type: None  
 Project: PORTS/CTS Data Verified By: M.E. Mumby Date: 02/20/95


DEPTH (FEET)	SAMPLE TYPE	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0				
2				
4				
6				
8				
10				
12				
14				
16				
18				
20				
22				
24				
26				
28				
30				

Auger to 24' using 4" augers.  
 Set 3/4" .010" slotted screen 25'-28'  
 #2 Frac sand 24'-28'  
 Bentonite chips (3/4"), 24'-surface  
 Surface casing, 4" PVC cemented in place.

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# Piezometer Summary Information OAK RIDGE NATIONAL LABORATORY

Prepared By: R.M. Schlosser Date: 01/24/95 Page: 1 OF 1  
 Hole No.: CTSPZ31 Casing Elevation: \_\_\_\_\_ Ground Elevation: \_\_\_\_\_  
 Total Depth: 28.5' No. of Compl.: 1 Rig Type: QRNL U2CRT Location: Clean Test Site  
 Auger Size: 4" Sample Type: None  
 Project: PORTS/CTS Data Verified By: M.E. Mumby Date: 02/20/95


DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
2					
4					
6					
8					
10					
12					
14					
16					
18					
20					
22					
24					
26					
28					
30					

Auger to 28.5' using 4" augers.  
 Set 3/4" .010" slotted screen 25.5'-28.5'.  
 #2 Frac sand 25'-28.5'.  
 Bentonite chips (3/4"). 25'-surface  
 Surface casing, 4" PVC cemented in place.

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# Piezometer Summary Information OAK RIDGE NATIONAL LABORATORY

Prepared By: R.M. Schlosser Date: 01/25/95 Page: 1 OF 1  
 Hole No.: CTSPZ32 Casing Elevation: \_\_\_\_\_ Ground Elevation: \_\_\_\_\_  
 Total Depth: 28.5' No. of Compl.: 1 Rig Type: ORNL U2CAT Location: Clean Test Site  
 Auger Size: 4" Sample Type: None  
 Project: PORTS/CTS Data Verified By: M.E. Mumby Date: 02/20/95


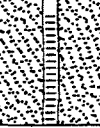
DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					
2					
4					
6					
8					
10					
12					
14					
16					
18					
20					
22					
24					
26					
28					
30					

Auger to 28.5' using 4" augers.  
 Set 3/4" .010" slotted screen 25.5'-28.5'.  
 #2 Frac sand 25'-28.5'.  
 Bentonite chips (3/4"), 25'-surface  
 Surface casing, 4" PVC cemented in place.

**ornl**

# Piezometer Summary Information OAK RIDGE NATIONAL LABORATORY

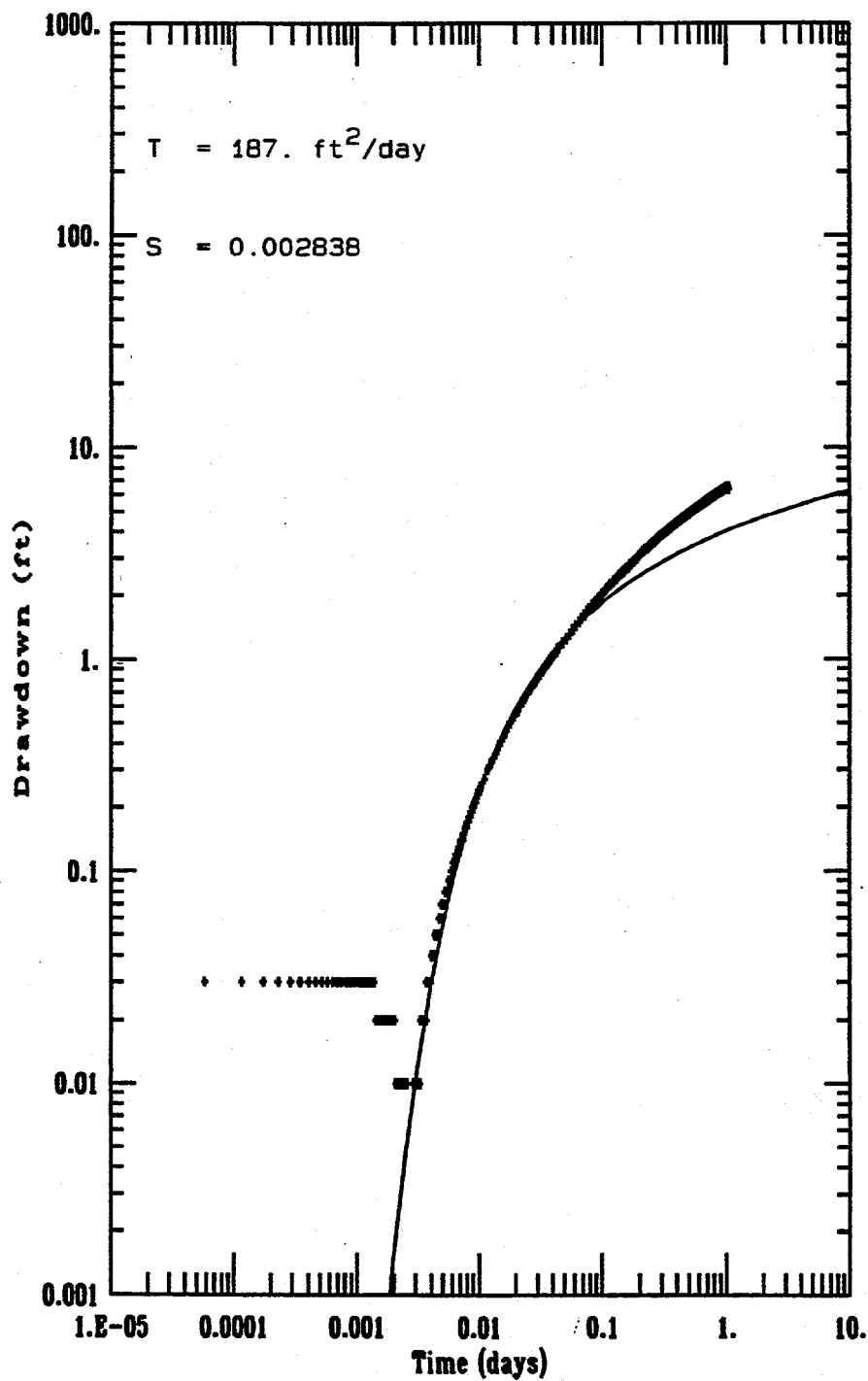
Prepared By: R.M. Schlosser Date: 01/25/95 Page: 1 OF 1  
 Hole No.: CTSPZ33 Casing Elevation: \_\_\_\_\_ Ground Elevation: \_\_\_\_\_  
 Total Depth: 28.5' No. of Compl.: 1 Rig Type: ORNL U2CRT Location: Clean Test Site  
 Auger Size: 4" Sample Type: None  
 Project: PORTS/CTS Data Verified By: M.E. Mumby Date: 02/20/95

DEPTH (FEET)	SAMPLE TYPE	SAMPLE INTV	WELL CONSTRUCTION	LITHOLOGY	DESCRIPTION
0					Auger to 28.5' using 4" augers. Set 3/4" .010" slotted screen 25.5'-28.5'. #2 Frac sand 25'-28.5'. Bentonite chips (3/4"), 25'-surface Surface casing. 4" PVC cemented in place.
2					
4					
6					
8					
10					
12					
14					
16					
18					
20					
22					
24					
26					
28					
30					

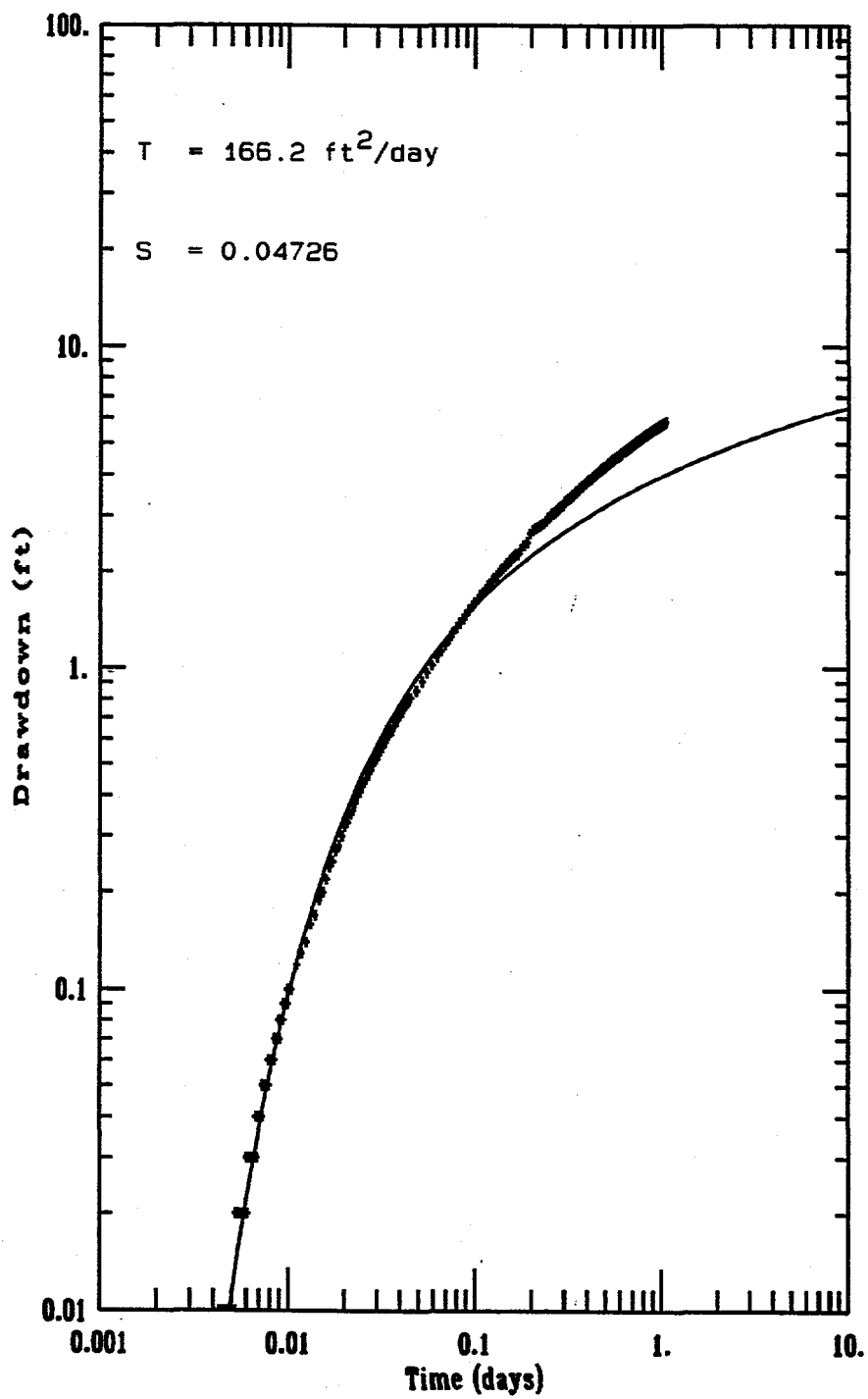
## **Appendix D**

### **Pressure Transducer Data from the West Well Pumping Test**

## West well pumping test - CTSP4

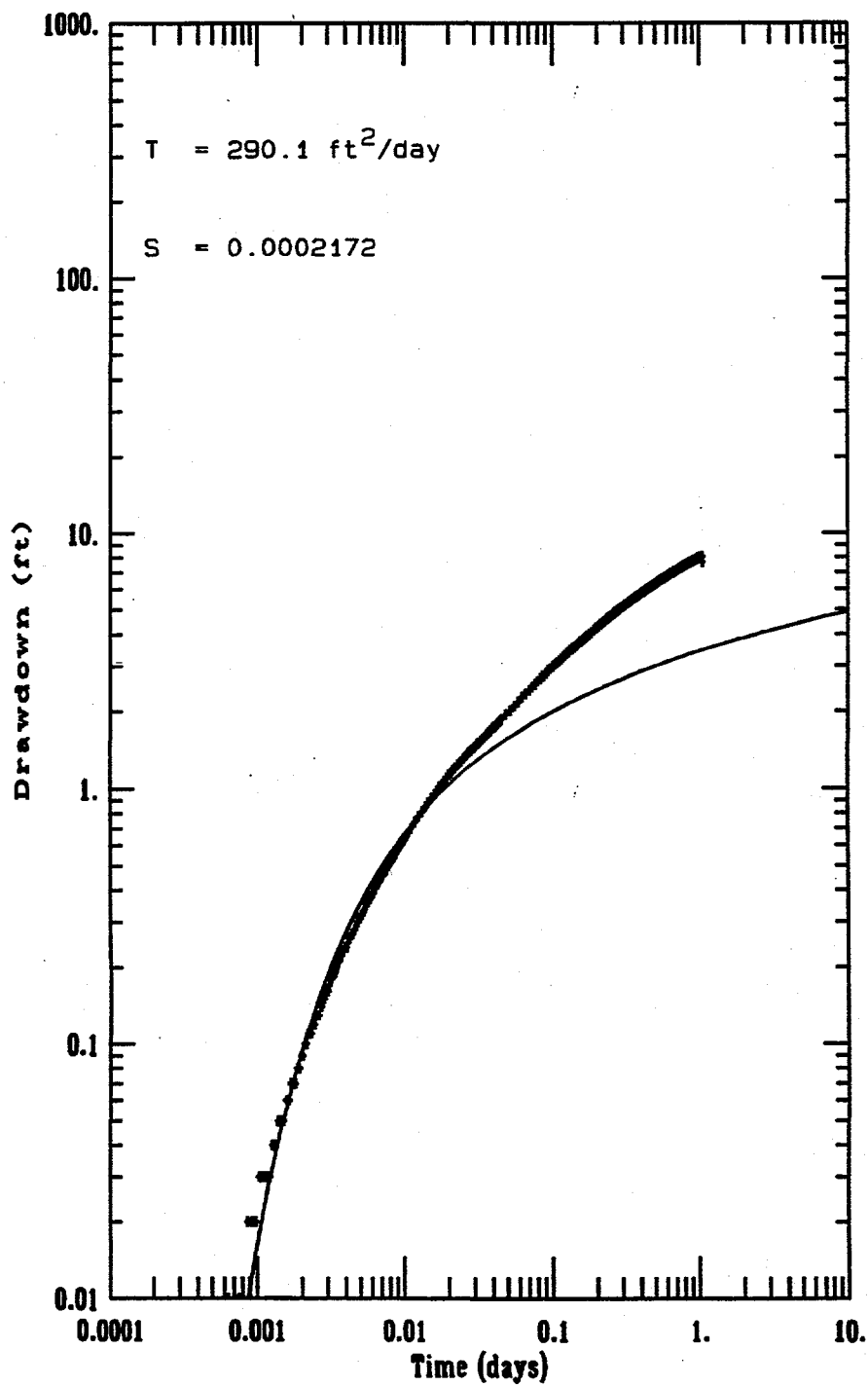


# West well pumping test - CTSP5

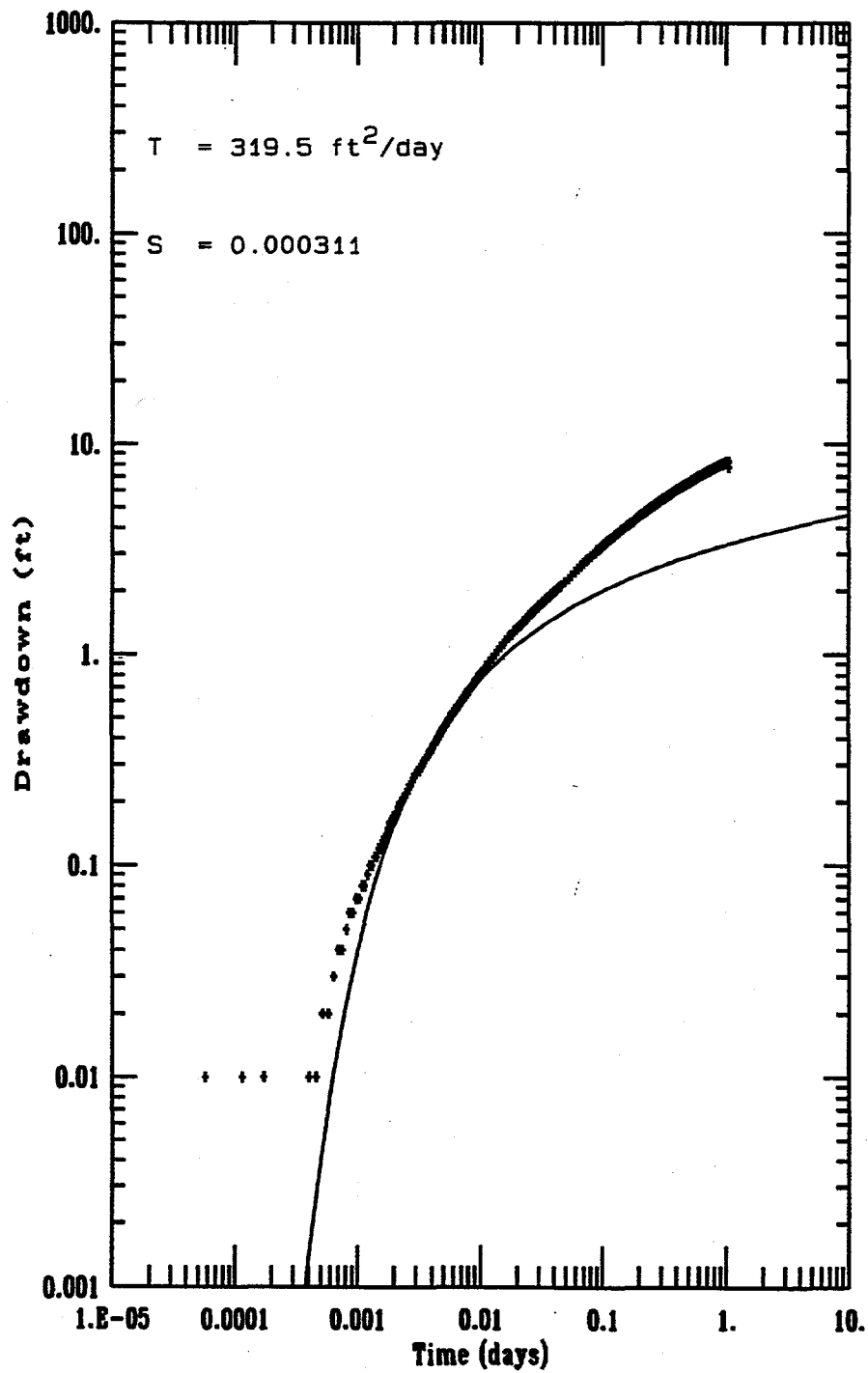




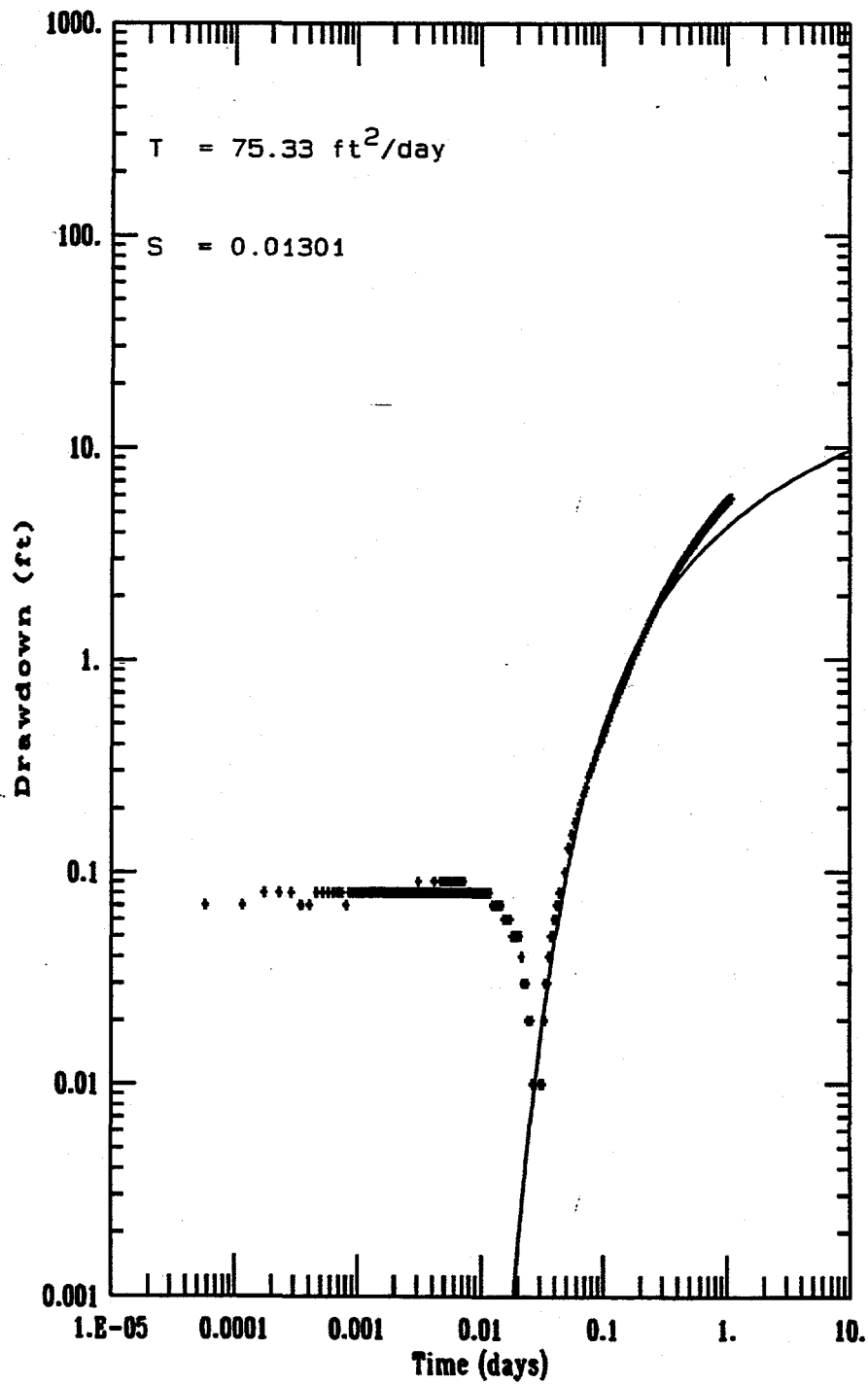
## West well pumping test - CTSP8



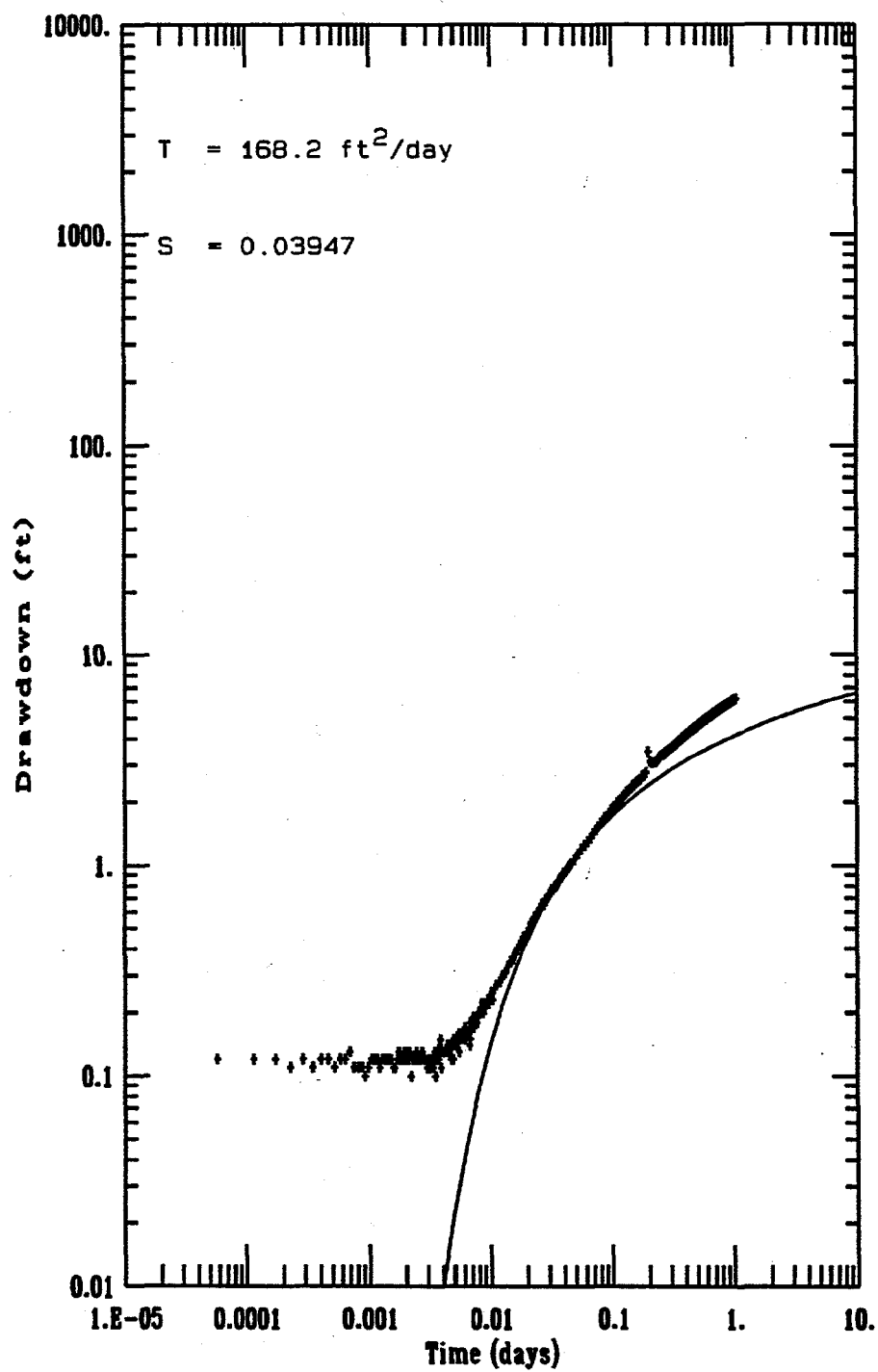
## West well pumping test - CTSP9



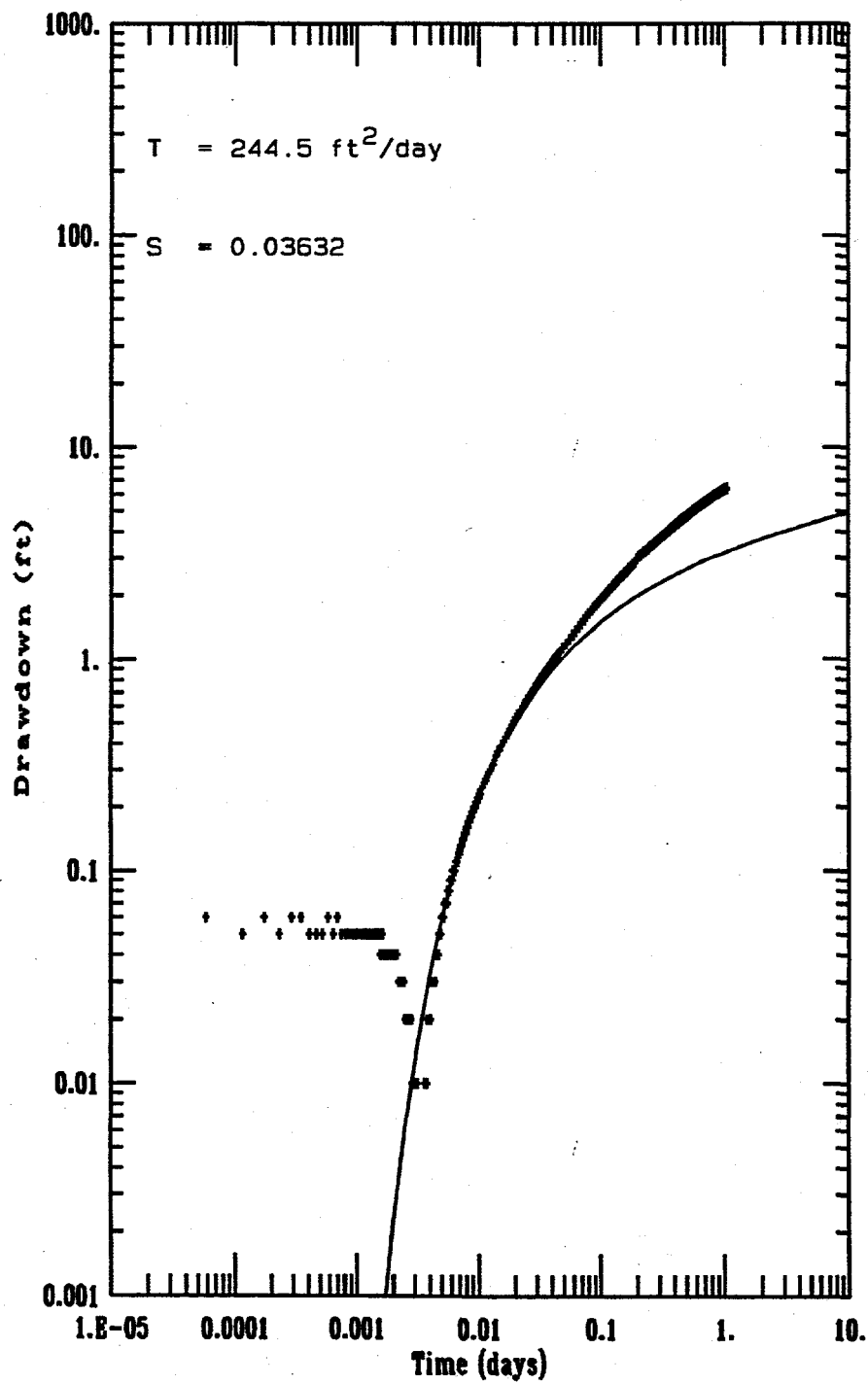
# West well pumping test - CTSP11



## West well pumping test - CTSP13



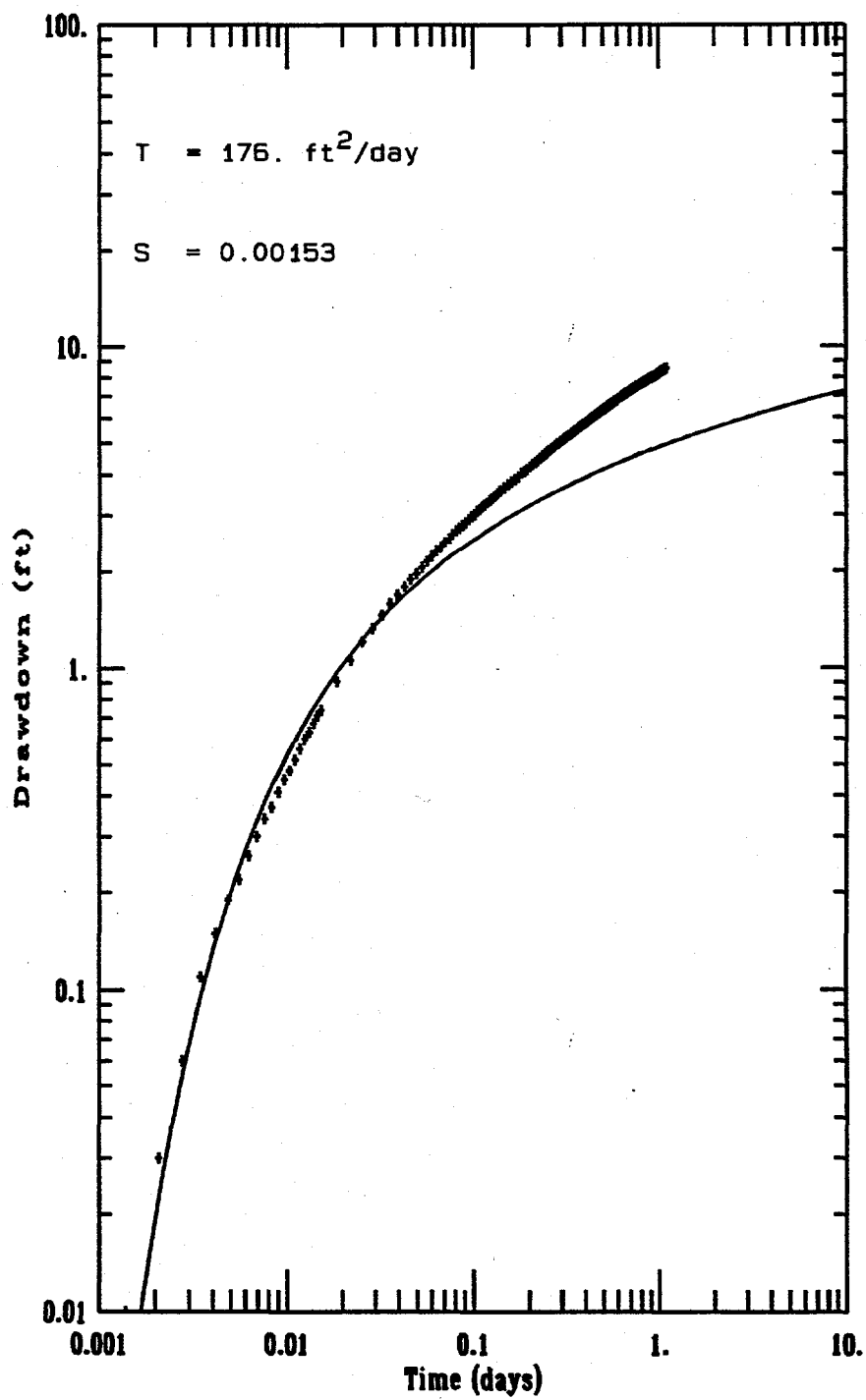
## West well pumping test - CTSP20



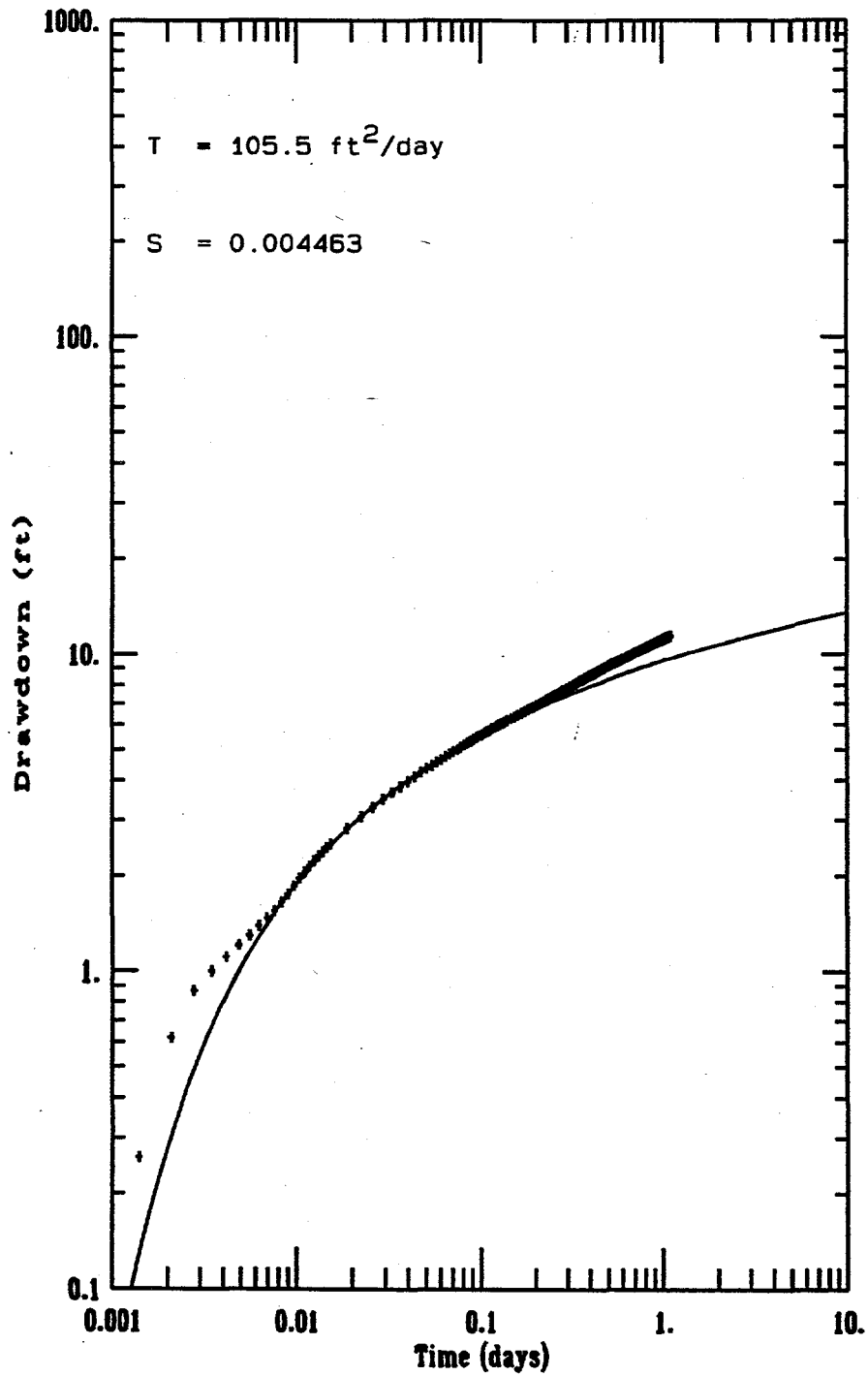
## **Appendix E**

### **Pressure Transducer Data from the East Well Pumping Test**

## East well pumping test - CTSP4

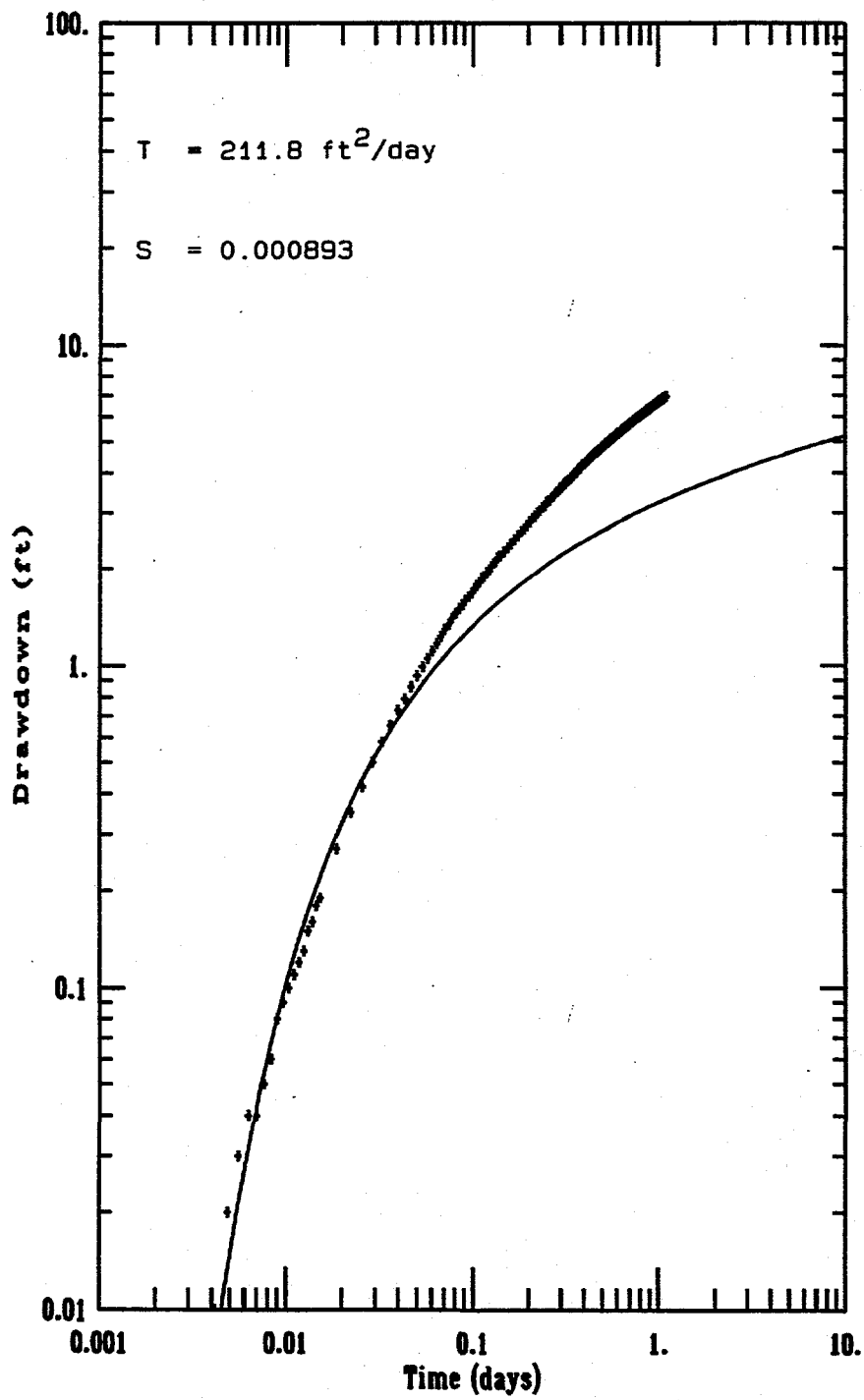


## East well pumping test - CTSP5

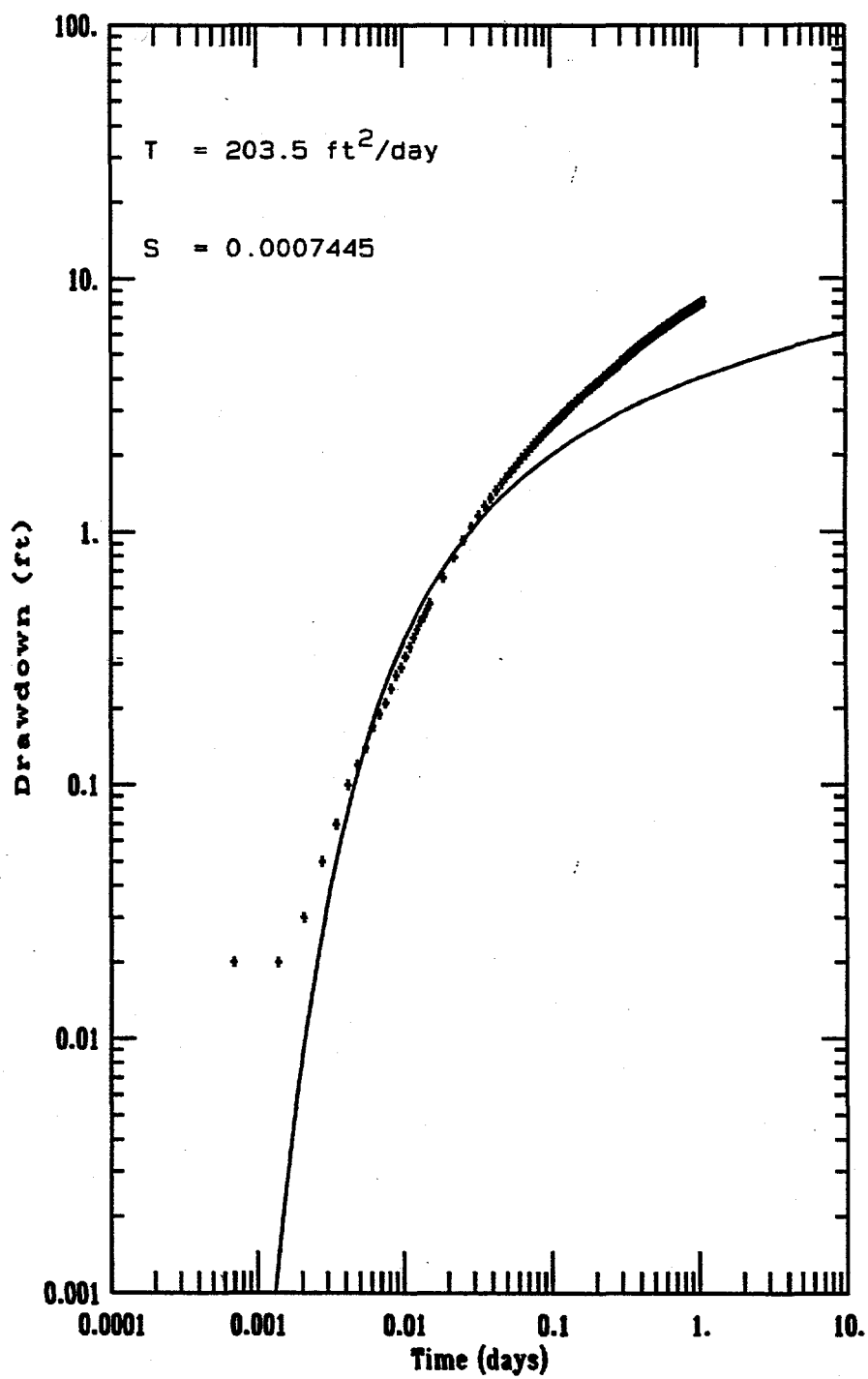




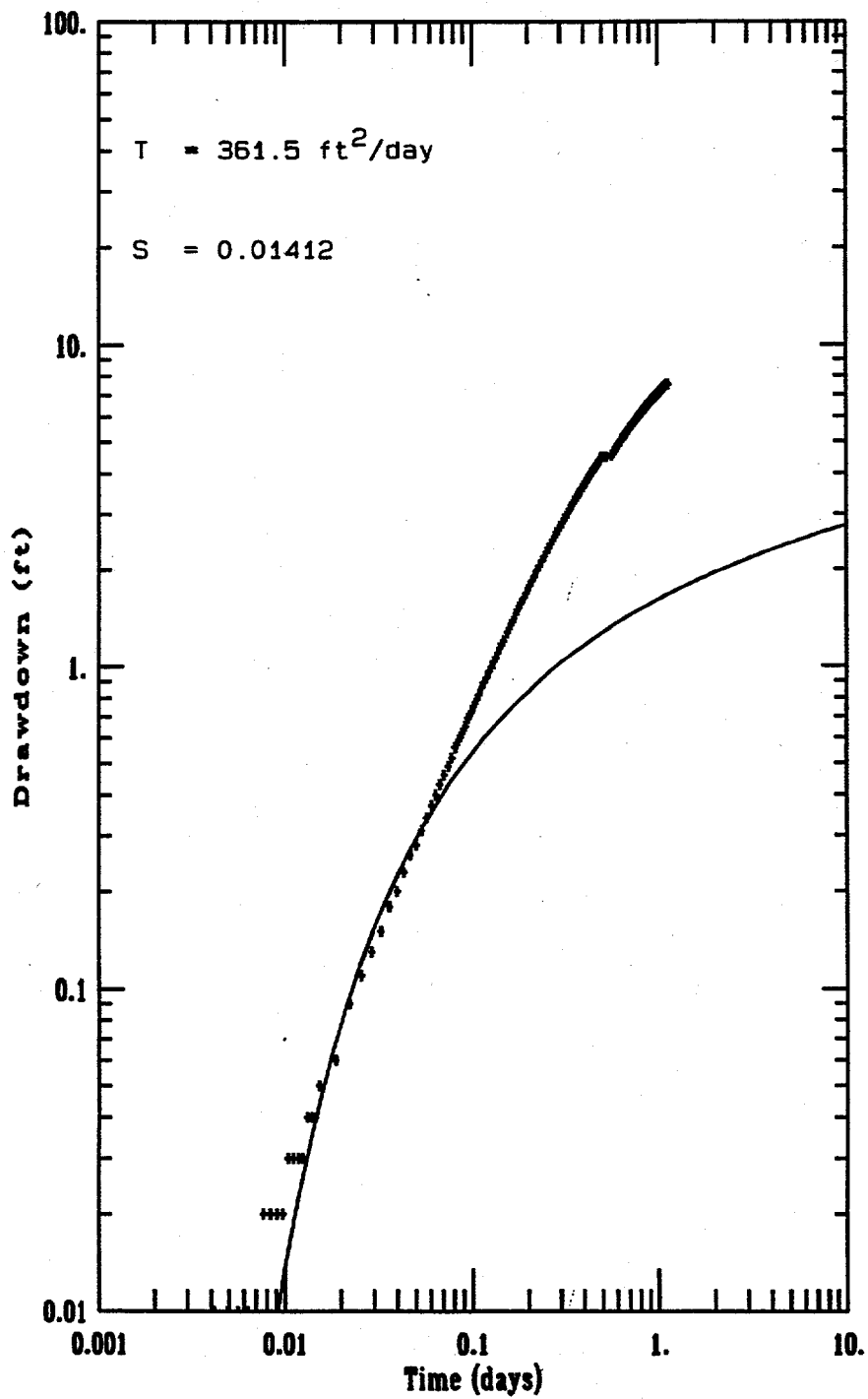
# East well pumping test - CTSP8



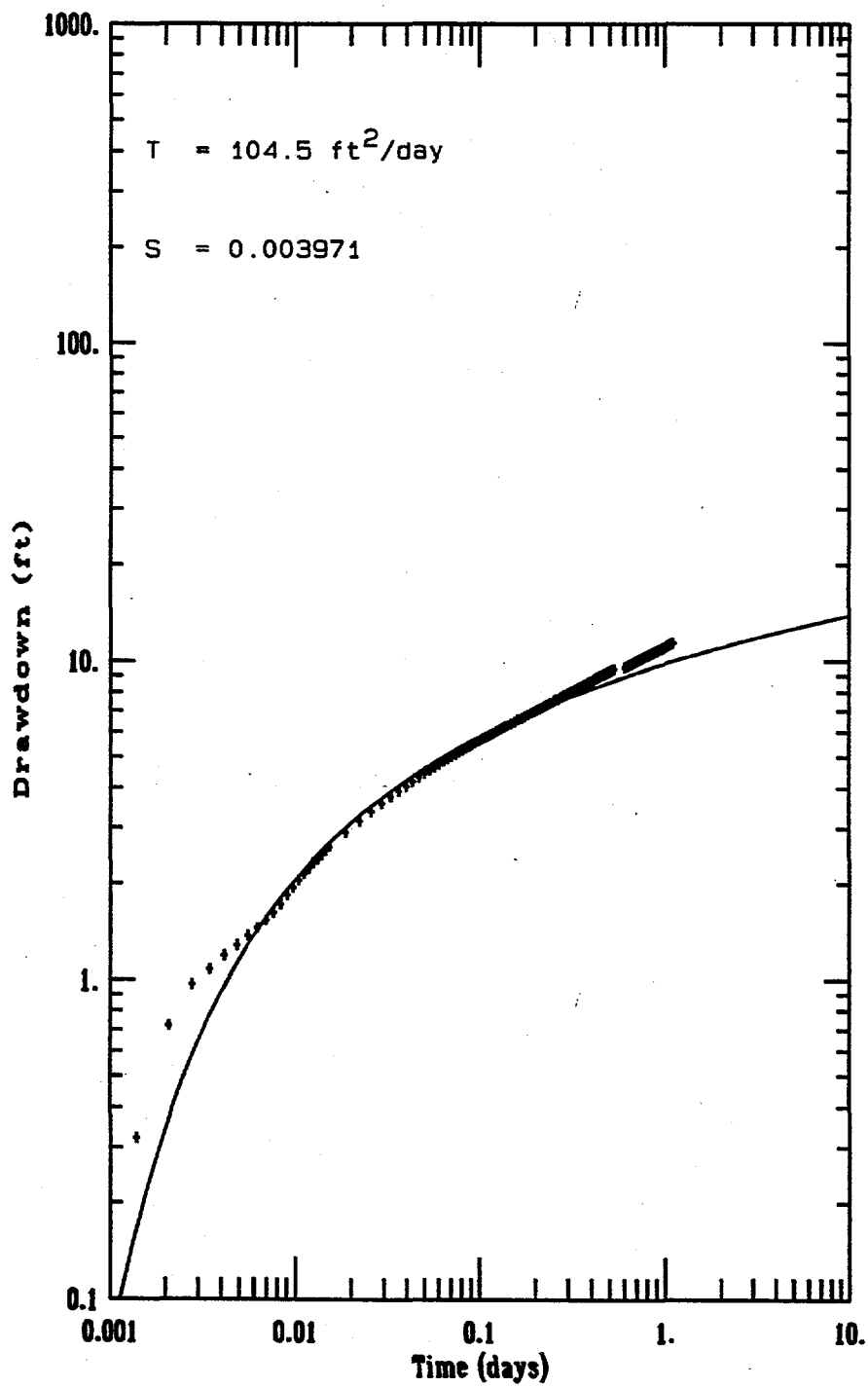
## East well pumping test - CTSP9



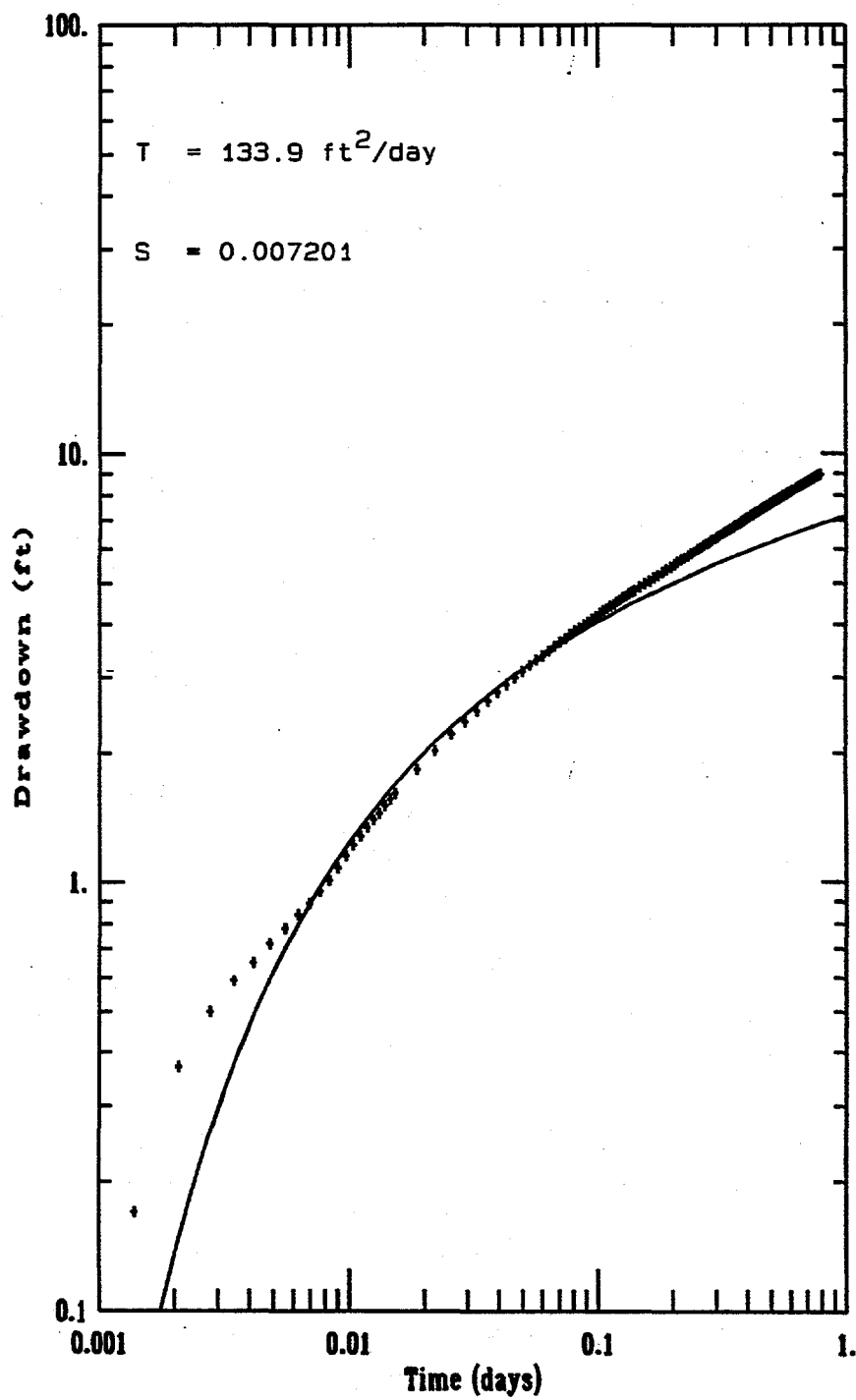
## East well pumping test - CTSP11



## East well pumping test - CTSP13



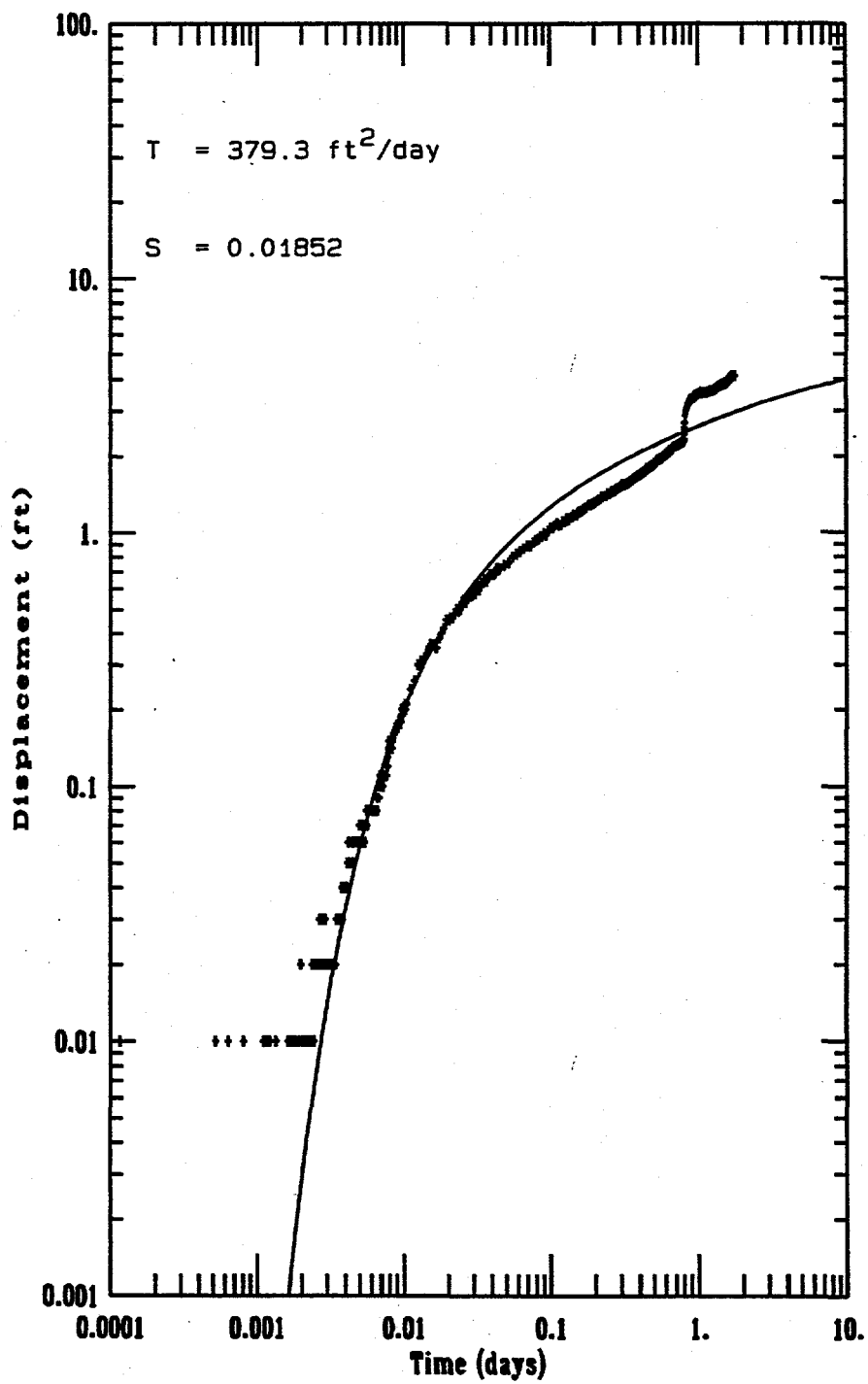
## East well pumping test - CTSP20



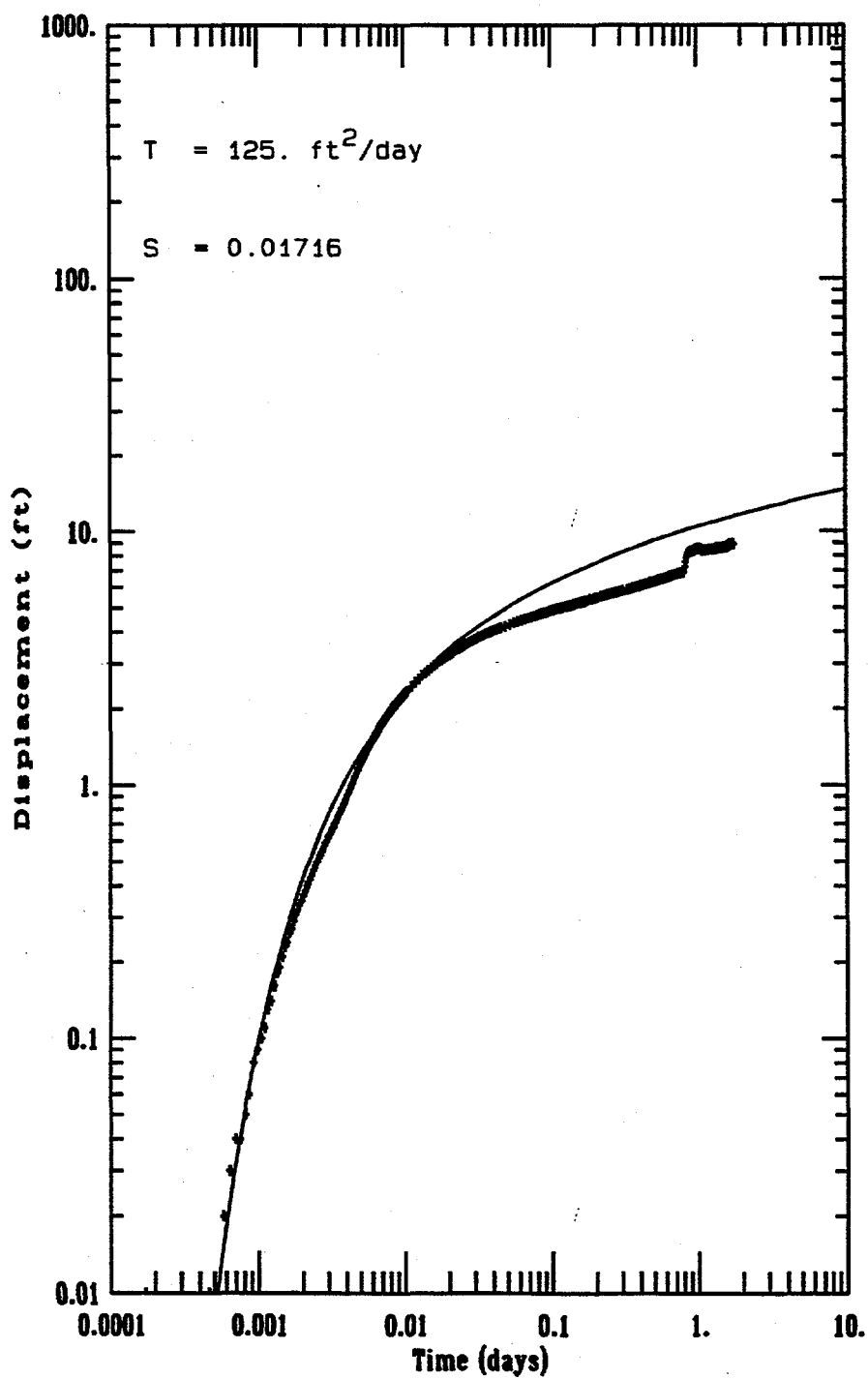
## **Appendix F**

### **Pressure Transducer Data from Dual Well Horizontal Recirculation Test**

## Recirculation Test - CTSP4

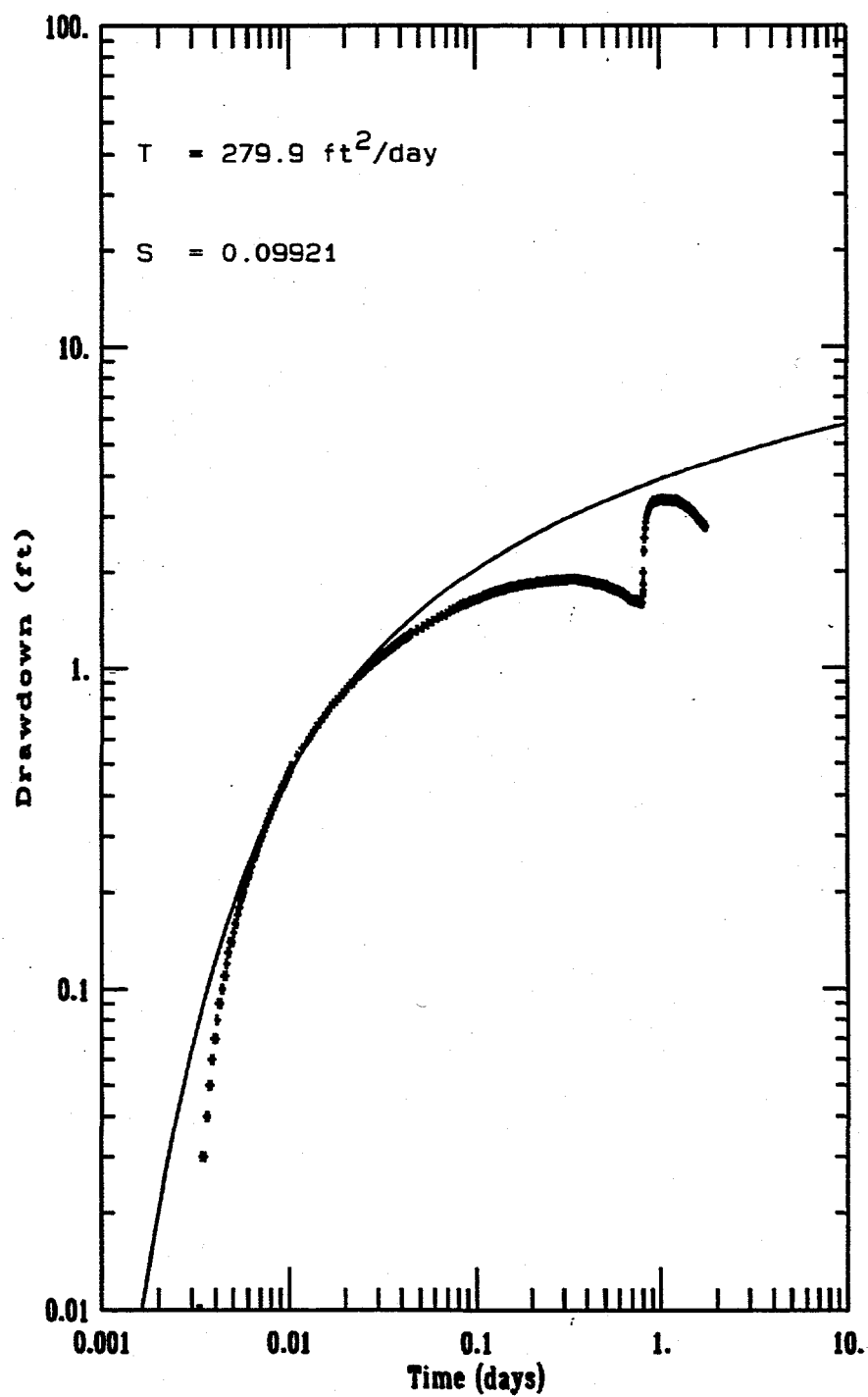


## Recirculation Test - CTSP5

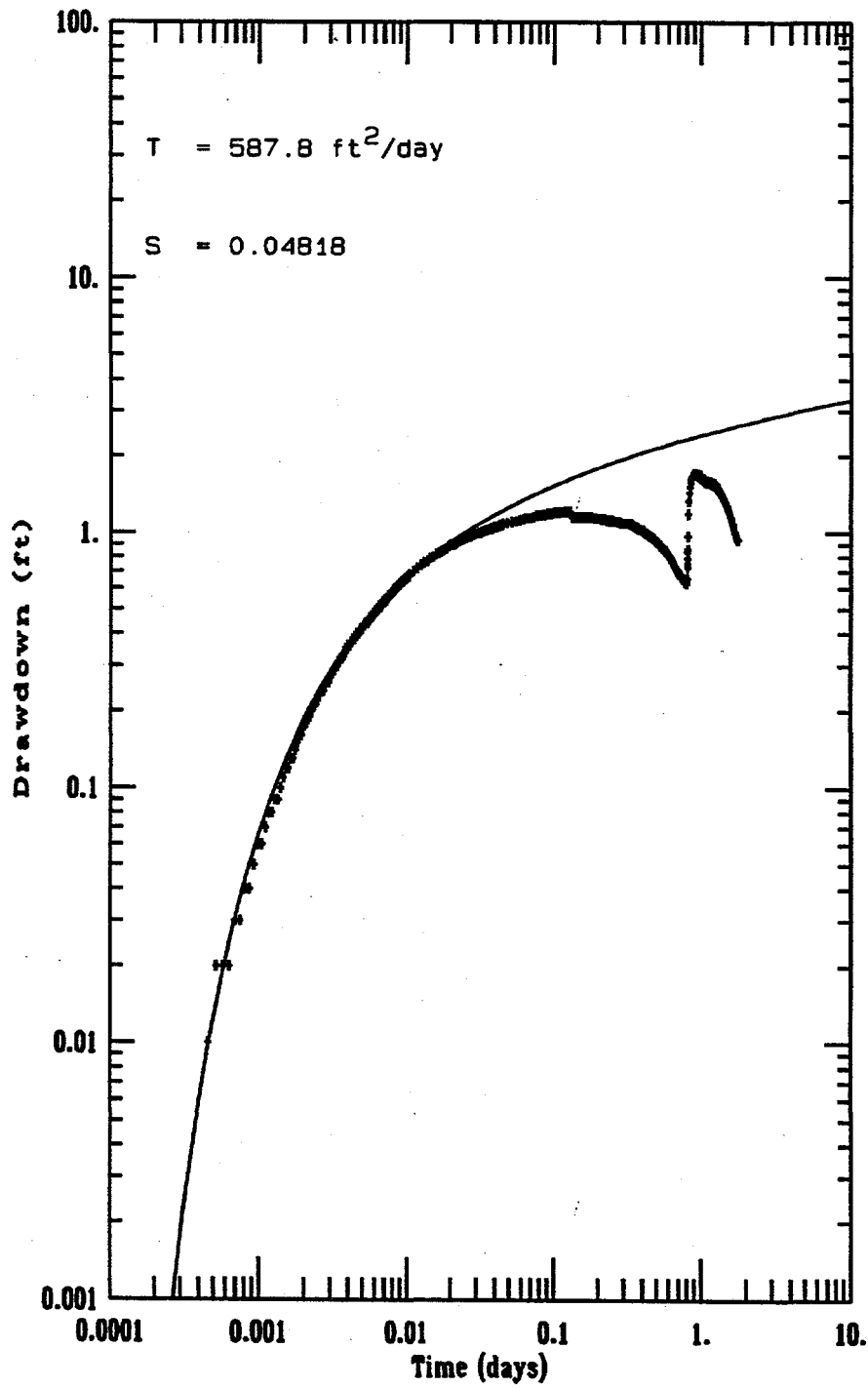




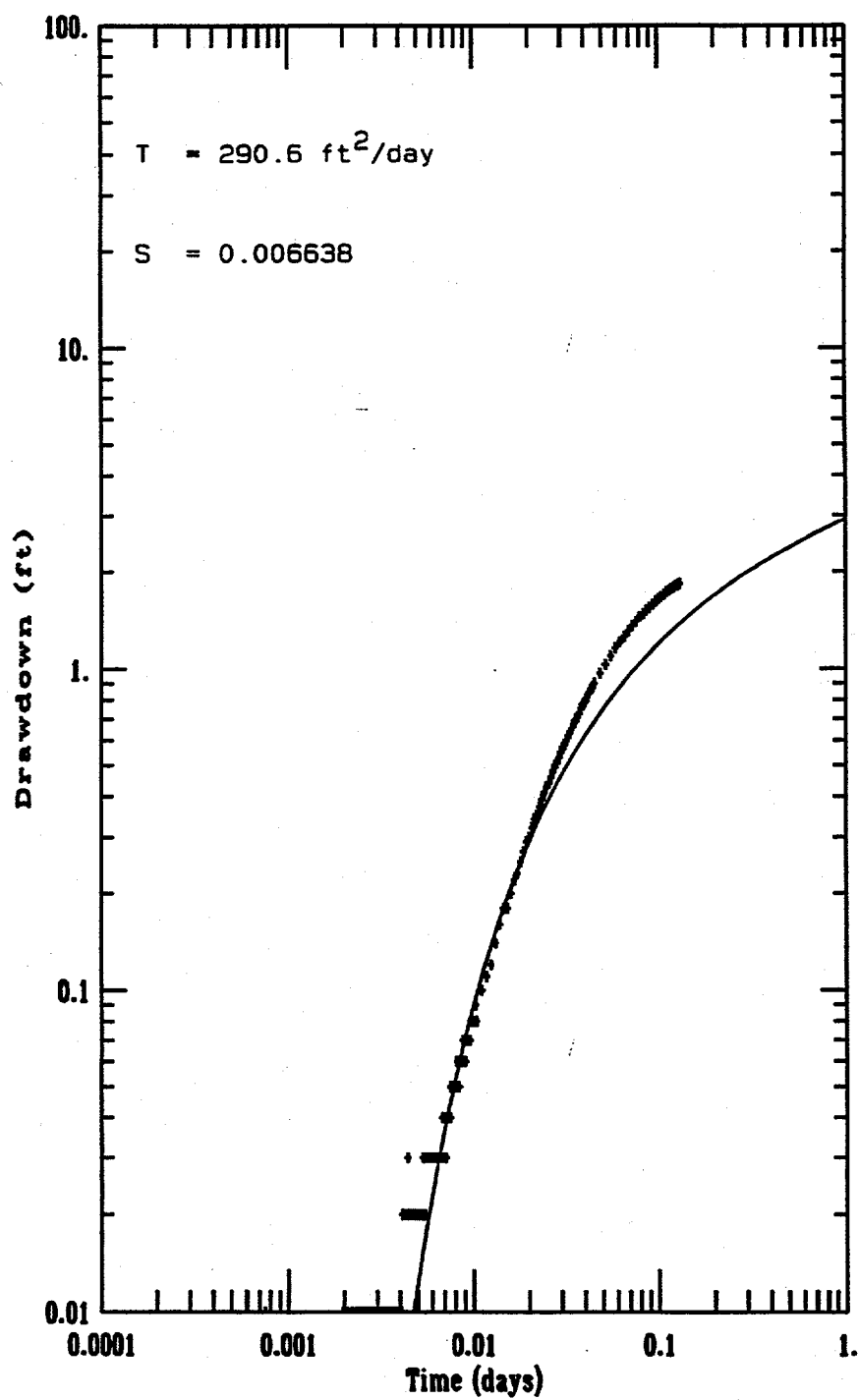
## Recirculation Test - CTSP8



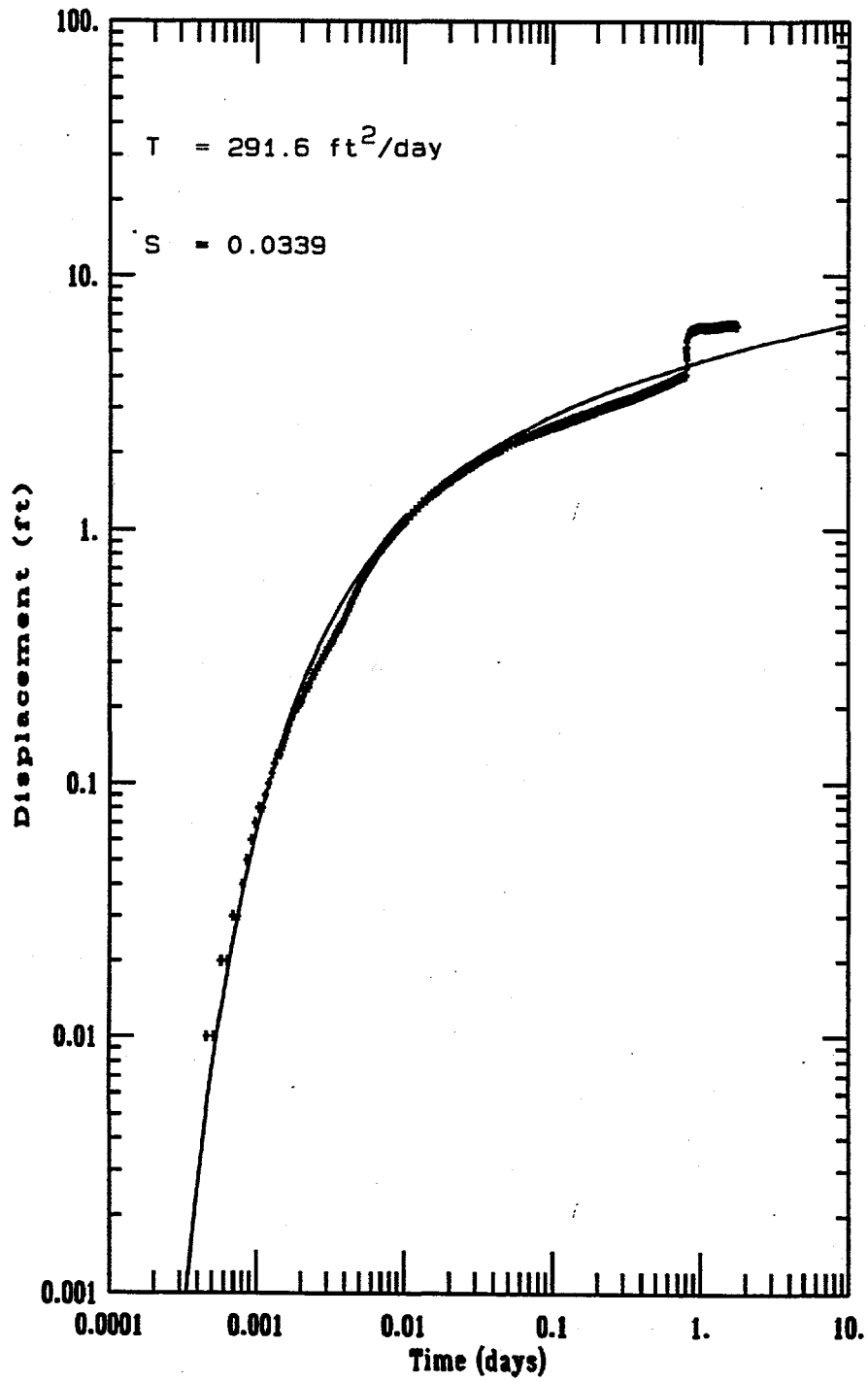
## Recirculation Test - CTSP9



## Recirculation Test - CTSP11



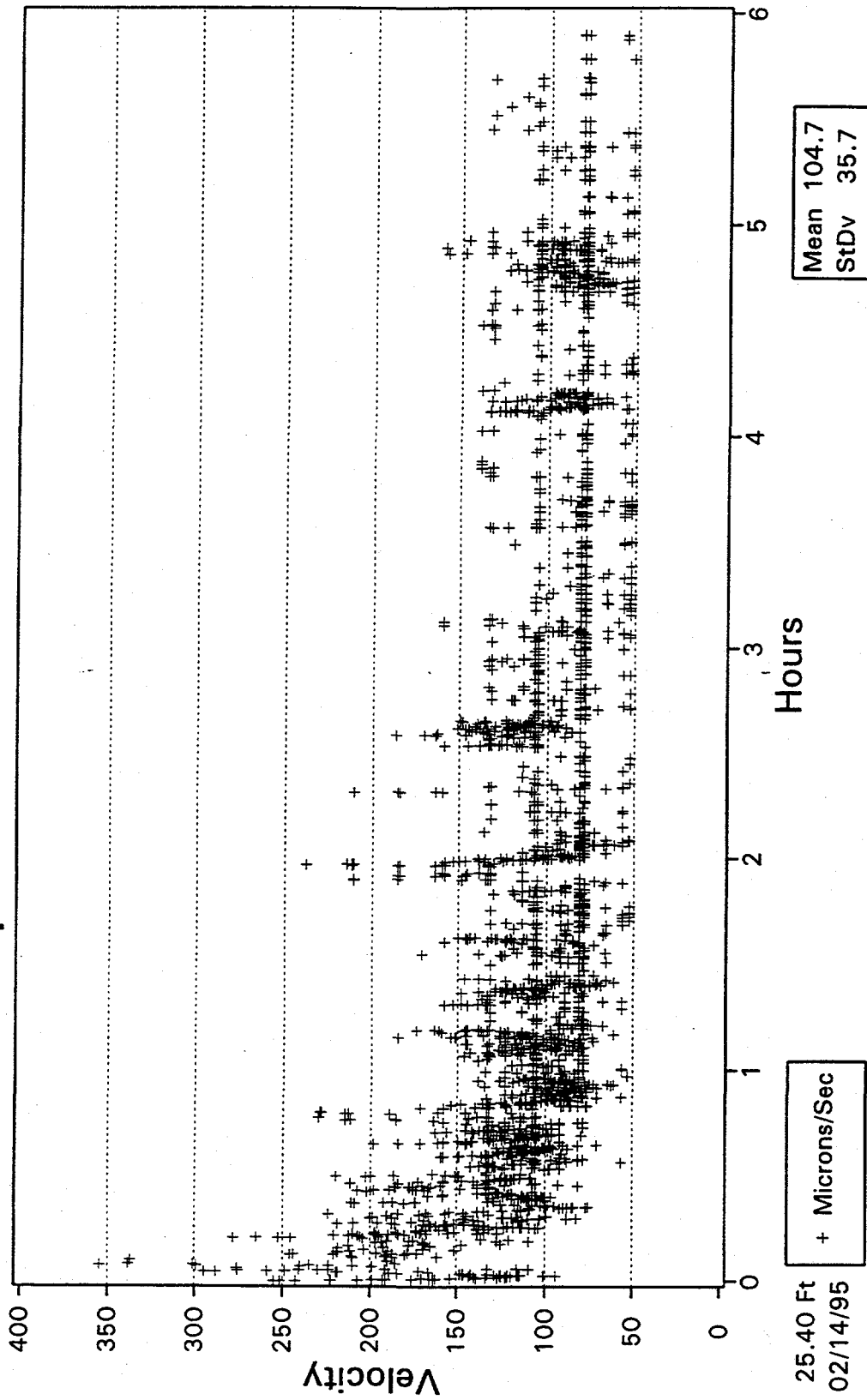
## Recirculation Test - CTSP20



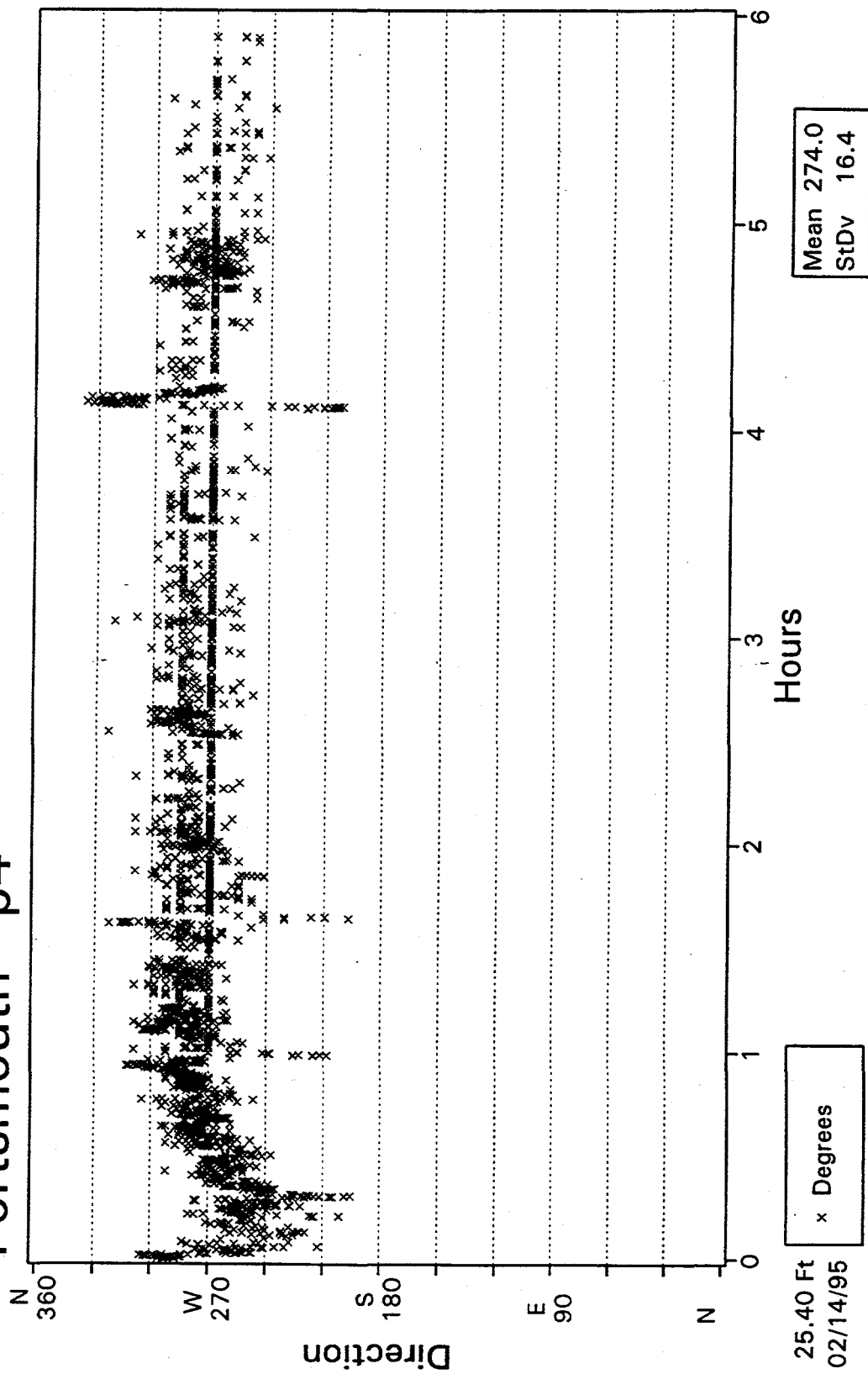
## **Appendix G**

### **Groundwater Velocity Data Gathered by the Colloidal Borescope for Selected Piezometers**

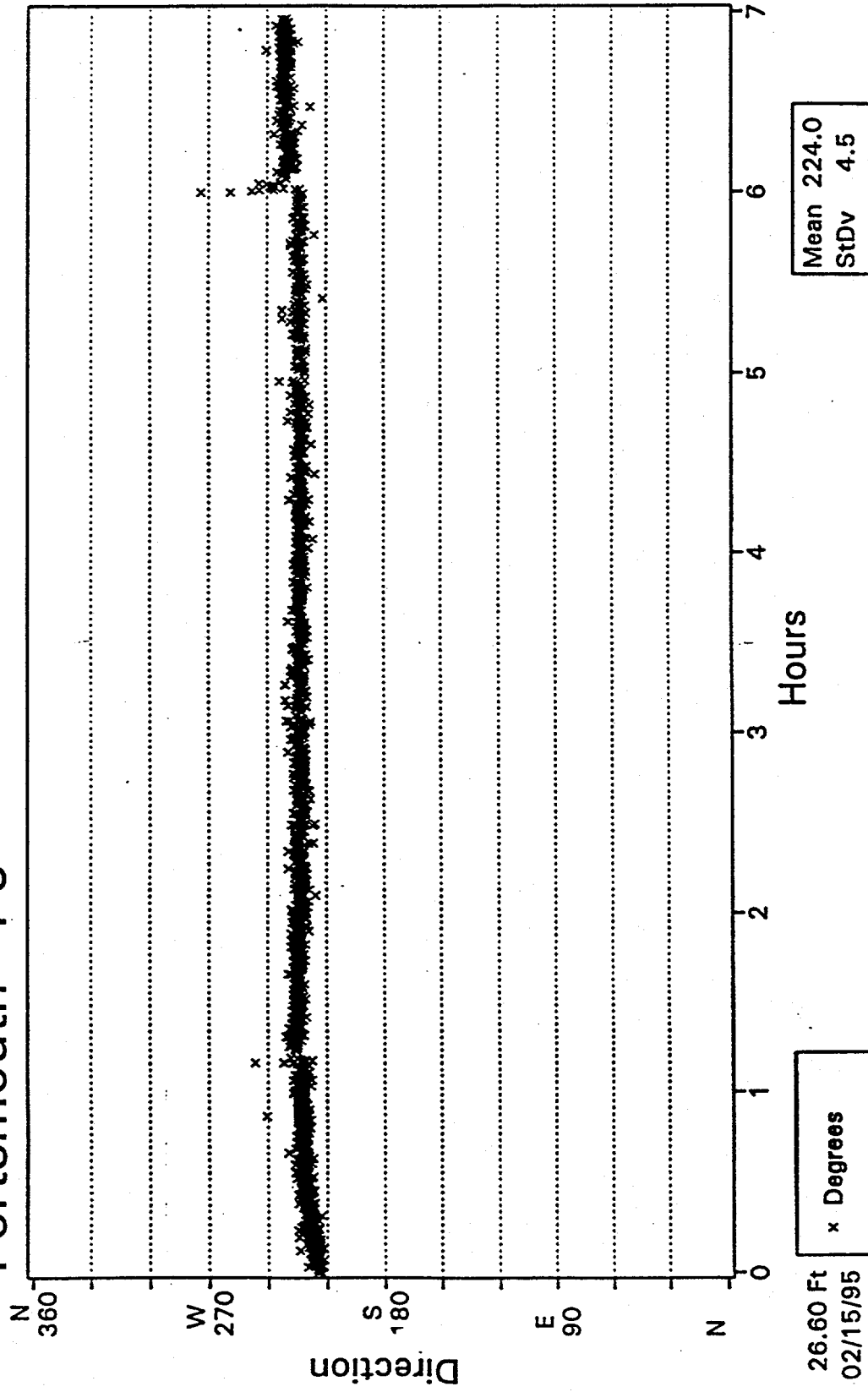
# Portsmouth p4



# Portsmouth p4

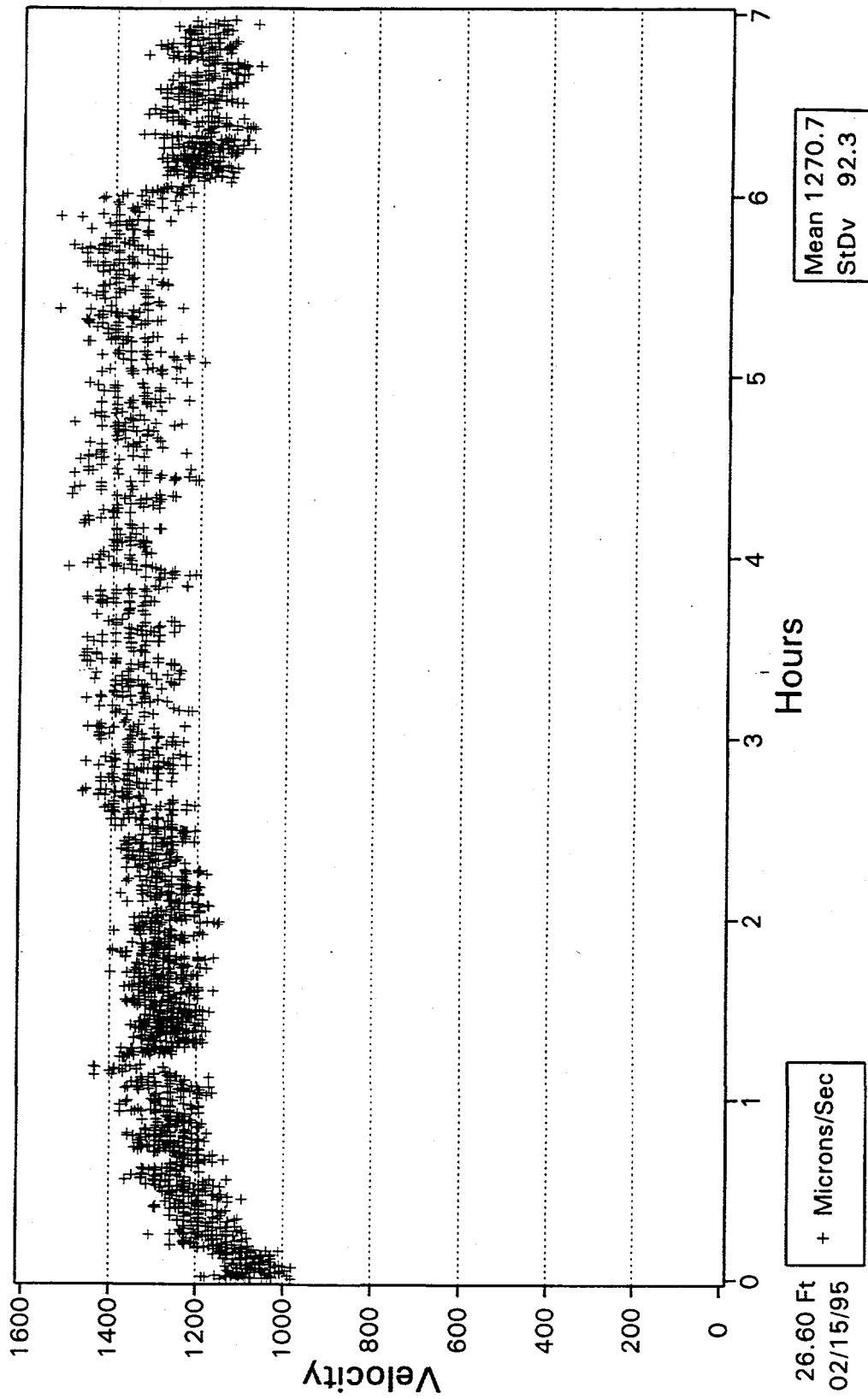


# Portsmouth P6

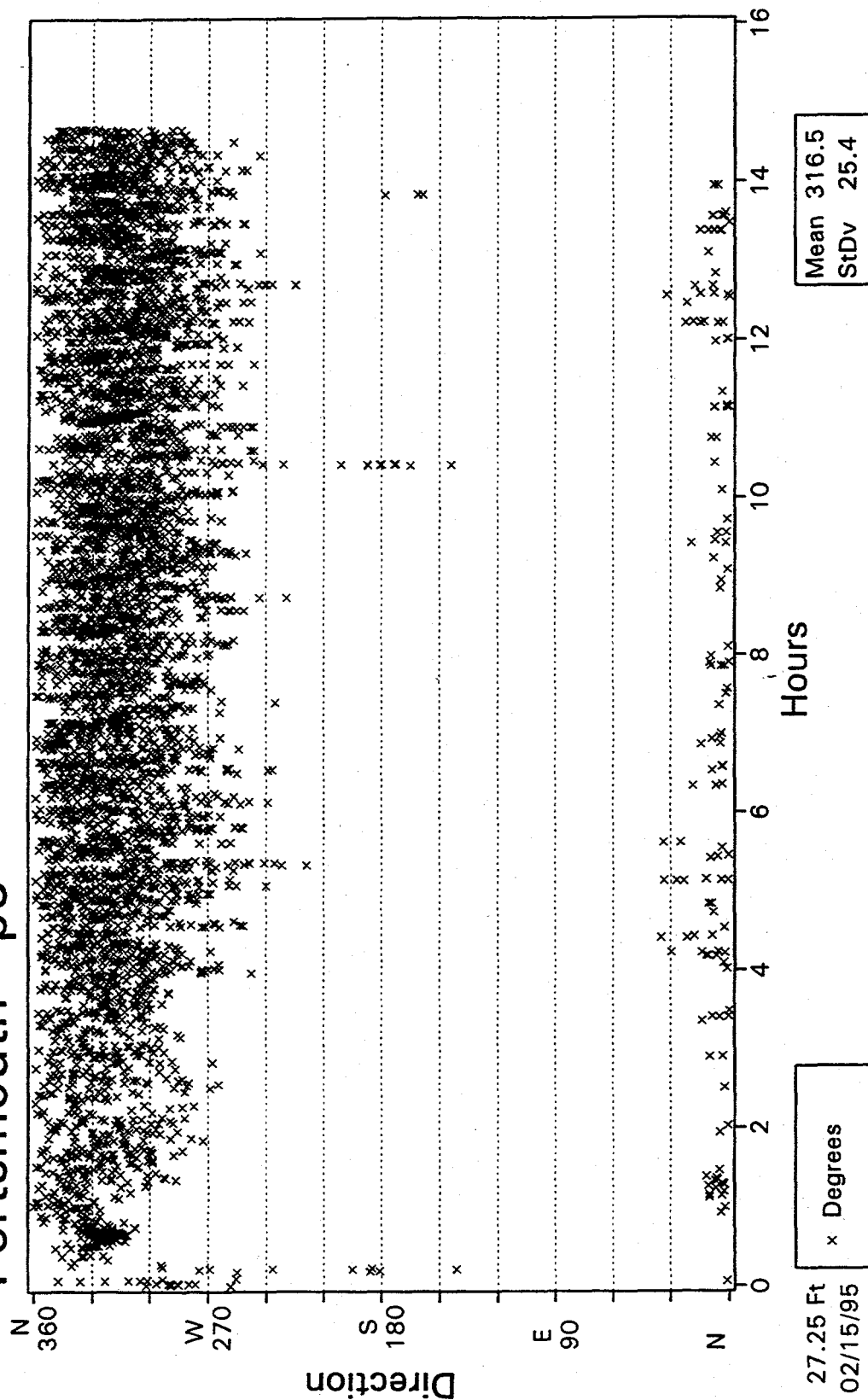




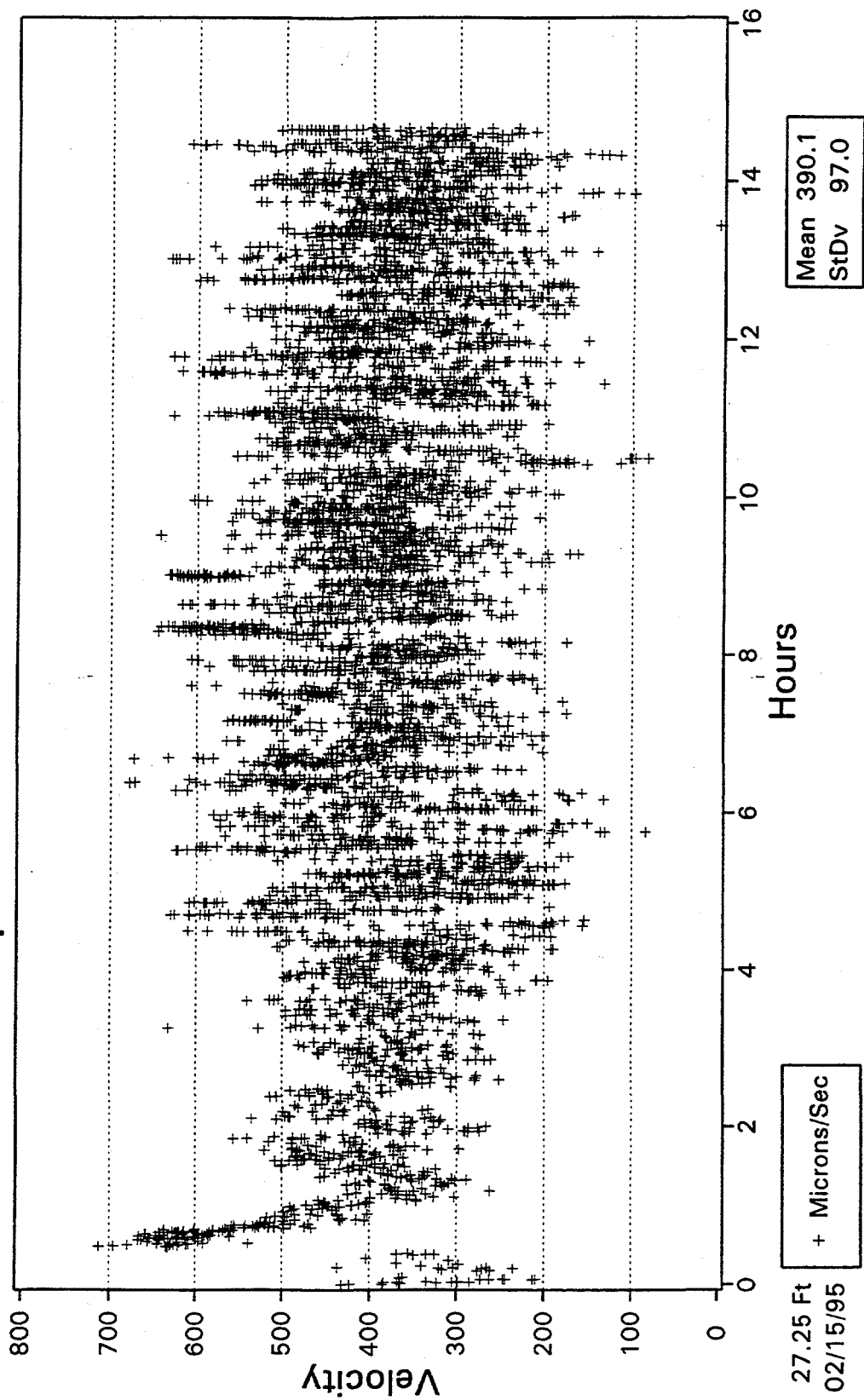
# Portsmouth P6



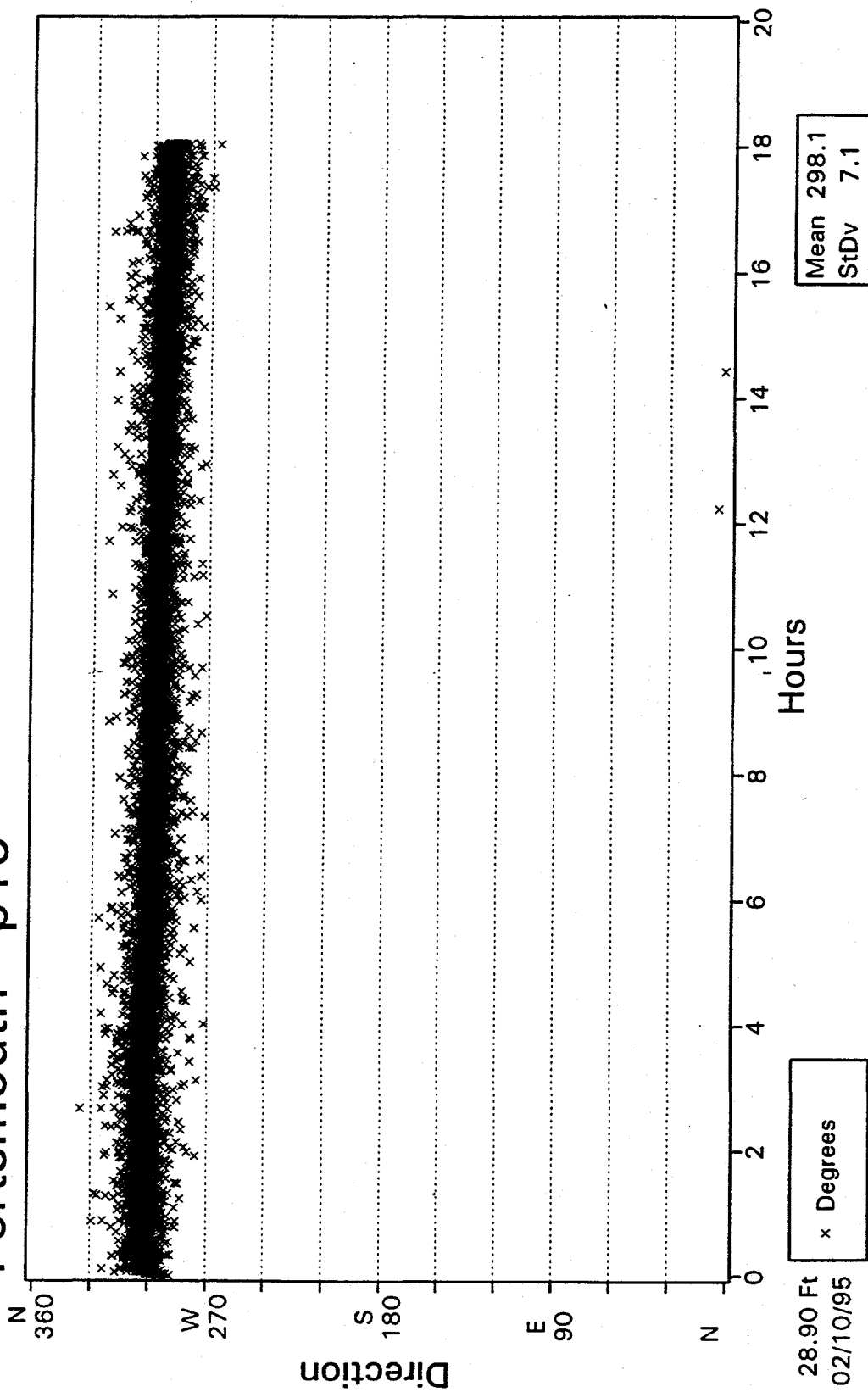
# Portsmouth p9



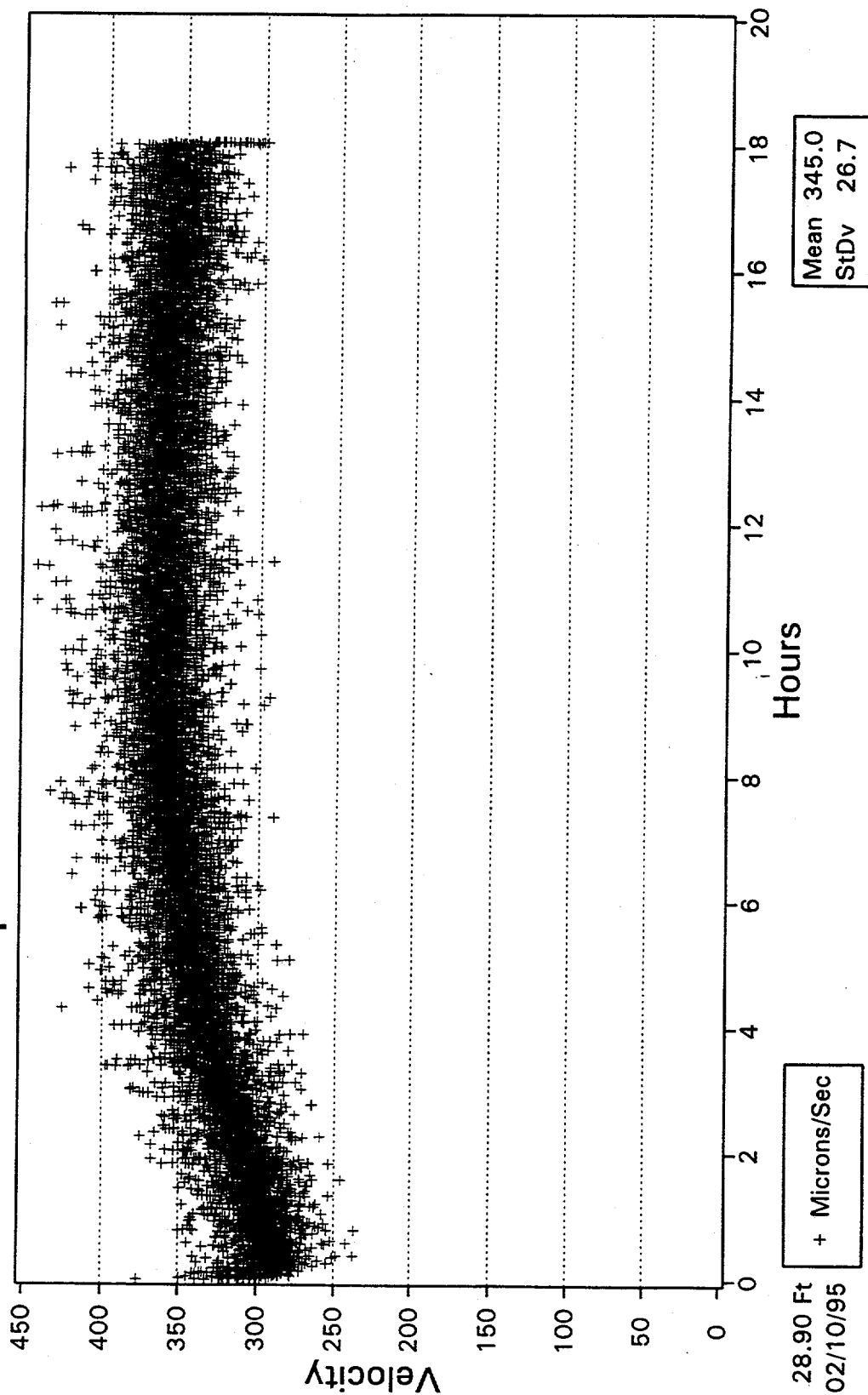
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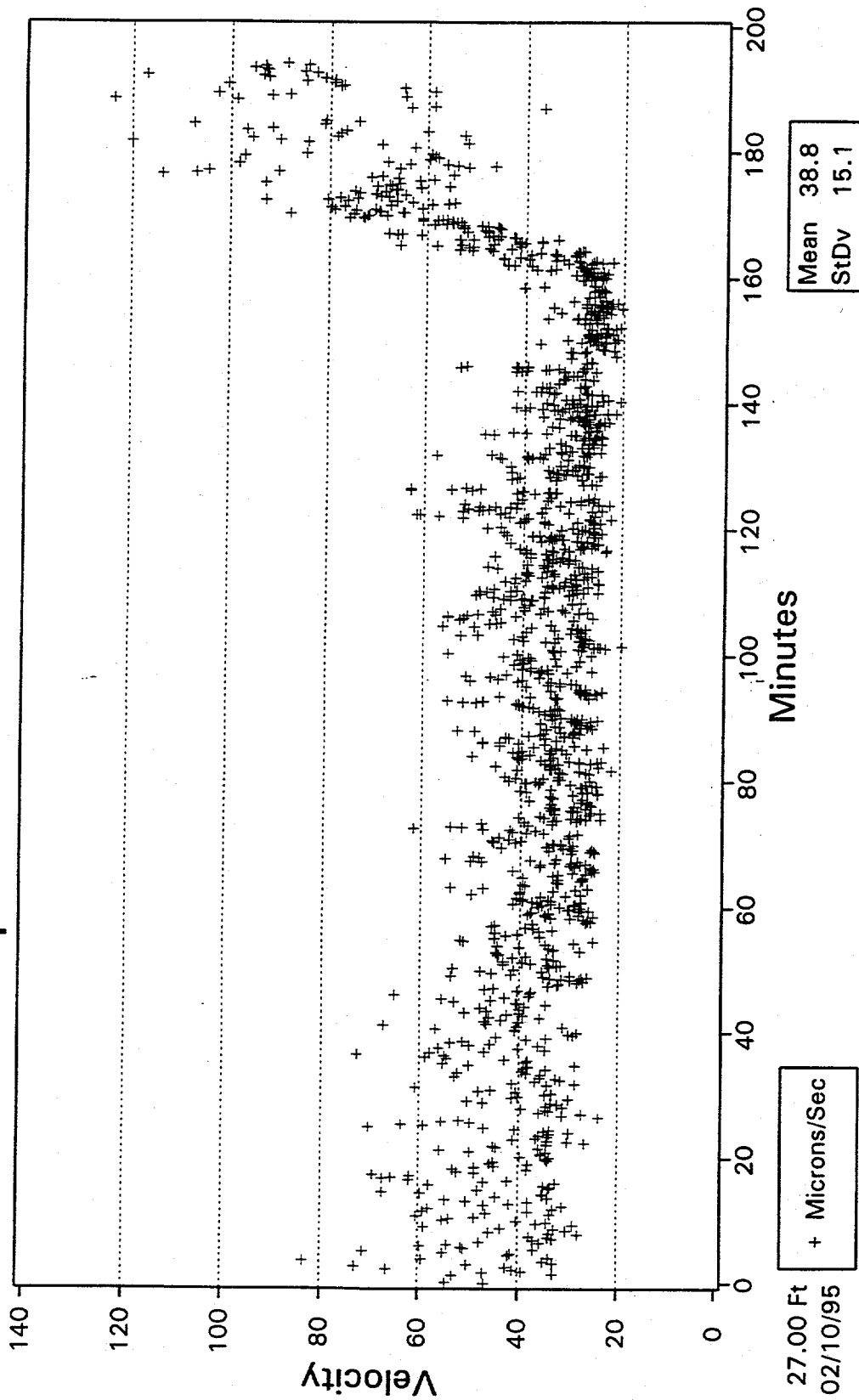
# Portsmouth p19



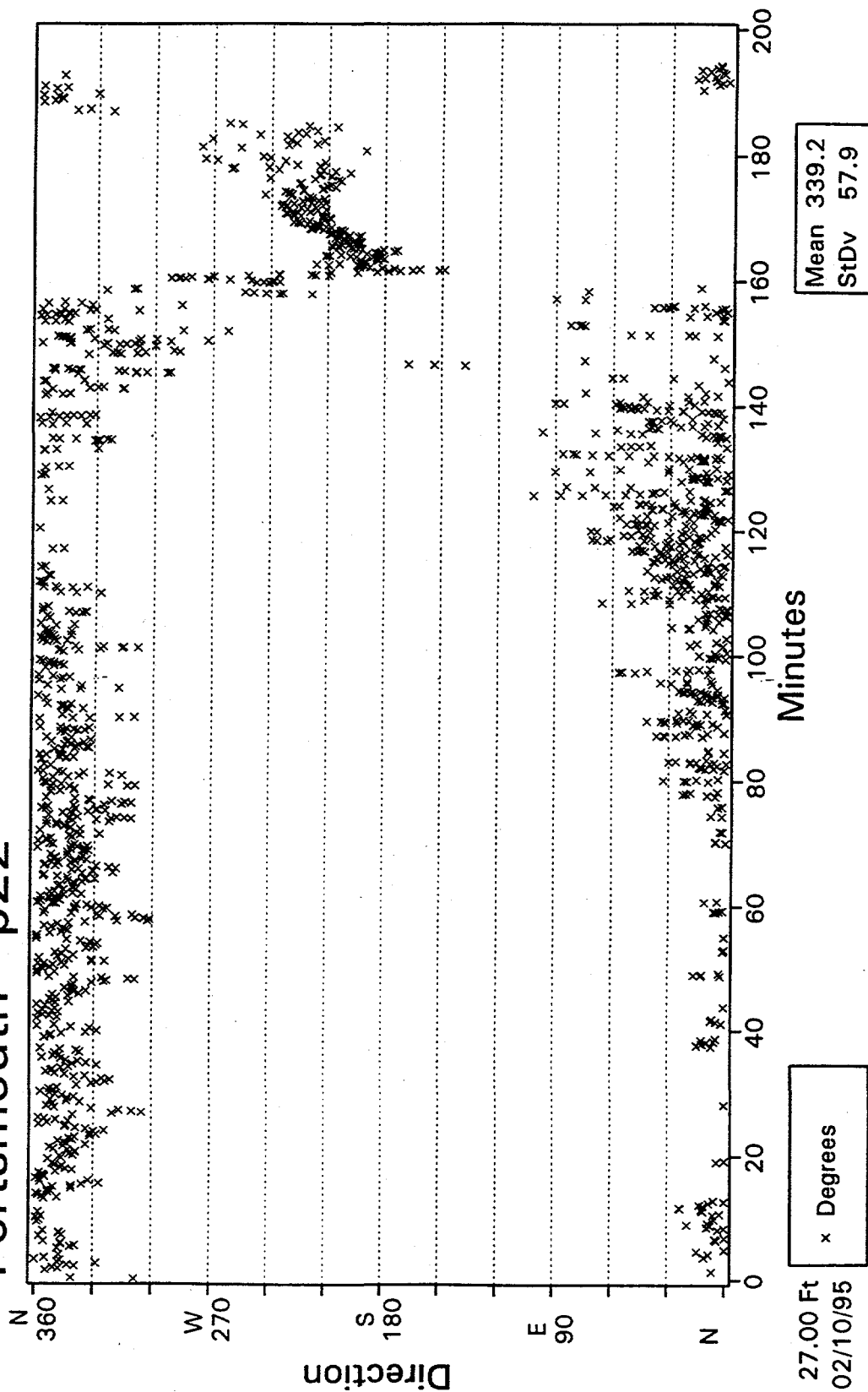
# Portsmouth p19



# Portsmouth p22



# Portsmouth p22



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