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and the DIII-D TEAM**

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**ABSTRACT**

Two approaches to achieving long-time scale stabilization of the ideal kink mode with a real, finite conductivity wall are considered: plasma rotation and active feedback control. DIII-D experiments have demonstrated stabilization of the resistive wall mode (RWM) by sustaining beta greater than the no-wall limit for up to 200 ms, much longer than the wall penetration time of a few ms. These plasmas are typically terminated by an  $m=3$ ,  $n=1$  mode as the plasma rotation slows below a few kHz. Recent temperature profile data shows an ideal MHD mode structure, as expected for the resistive wall mode at beta above the no-wall limit. The critical rotation rate for stabilization is in qualitative agreement with recent theories for dissipative stabilization in the absence of magnetic islands. However, drag by small-amplitude RWMs or damping of stable RWMs may contribute to an observed slowing of rotation at high beta, rendering rotational stabilization more difficult. An initial open-loop active control experiment, using non-axisymmetric external coils and a new array of saddle loop detectors, has yielded encouraging results, delaying the onset of the RWM.

## 1. INTRODUCTION

Stabilization of low- $n$  kink modes by a conducting wall is crucial for high beta, steady state "advanced tokamak" scenarios. Operation at high beta allows a more compact and economical fusion plasma with a large fraction of bootstrap current. Good alignment of the bootstrap current with the equilibrium current density profile, important for minimizing the requirements on external current drive systems, is achieved with broad current density profiles and broad pressure profiles. Such broad profiles have a low beta limit in the absence of a wall, but strong coupling to a nearby conducting wall can improve the stability limit by as much as a factor of 2 or 3 [1-3].

Two approaches to achieving long-time scale stabilization with a real, finite conductivity wall are being considered: plasma rotation and active feedback control. Ideal MHD theory predicts that for a plasma which would be stabilized by an ideal wall, non-zero wall resistivity leads to an unstable "resistive wall mode" with a growth time on the order of the wall's magnetic field penetration time  $\tau_w$  and a real frequency  $\omega \sim \tau_w^{-1}$ , and which is not stabilized by sub-Alfvenic plasma rotation [4]. However, more detailed theories show that the addition of dissipation in the plasma allows stabilization by sub-sonic plasma rotation [5,6]. Furthermore, external kink modes can drive islands in a resistive plasma, allowing stabilization by plasma rotation frequencies as low as  $\Omega \sim \tau_w^{-1}$  [7,8].

DIII-D experiments [9,10] confirm many of the important qualitative features of these more recent theories. In discharges with broad current density profiles, beta values reach up to 1.4 times the ideal  $n=1$  kink mode limit calculated without a wall, but remain within the stable range calculated with an ideal wall at the position of the DIII-D vacuum vessel. Beta greater than the no-wall limit has been sustained for up to 200 ms, much longer than the wall penetration time  $\tau_w \leq 6$  ms, which indicates that the resistive wall mode has been stabilized [Fig. 1(a)]. As the rotation slows, these plasmas are typically terminated by an  $n=1$  mode which begins to grow as the plasma rotation at the  $q=3$  surface decreases below 1-2 kHz, consistent with a loss of rotational stabilization [Fig. 1(b)]. The mode typically has a growth time of 2-8 ms and a real frequency  $\omega \lesssim \tau_w^{-1}$ , as expected for a resistive wall mode. The poloidal structure of this nearly stationary mode, as measured with saddle loops on the exterior surface of the vacuum vessel (Fig. 2), is predominantly  $m=3$  and ballooning toward the large major radius side, consistent with an instability driven by the large current density and pressure gradient in the outer part of the plasma.

In many cases, temperature profiles measured with electron cyclotron emission show an ideal-like mode structure, without islands (Fig. 3), as expected for an ideal kink mode which has

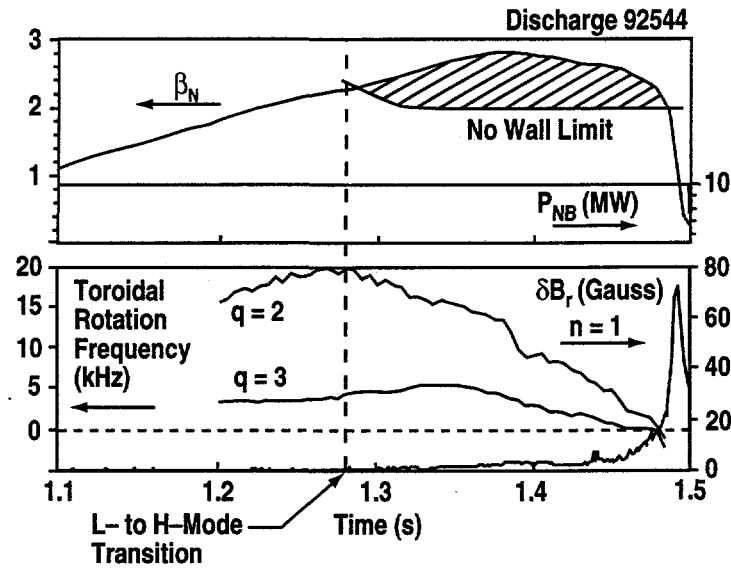


FIG. 1. Time evolution of a wall-stabilized DIII-D discharge (92544). (a) Normalized beta,  $\beta_N = \beta(aB/I)$  and neutral beam power. (b) Plasma rotation frequency from charge exchange recombination spectroscopy at two radial locations, and the  $B_r$  amplitude of the non-rotating  $n=1$  mode from the saddle loop array.

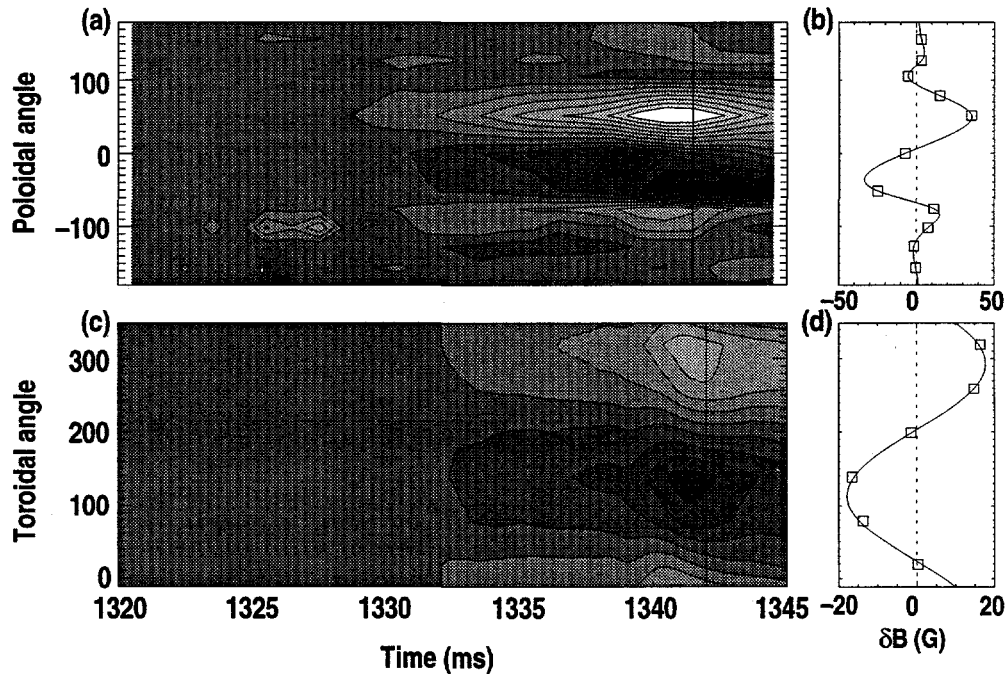


FIG. 2. Contour plots of  $n=1$  mode amplitude versus time and spatial angle (a,c) and amplitude versus spatial angle at the time of peak amplitude (b,d) showing poloidal (a,b) and toroidal (c,d) mode structure.

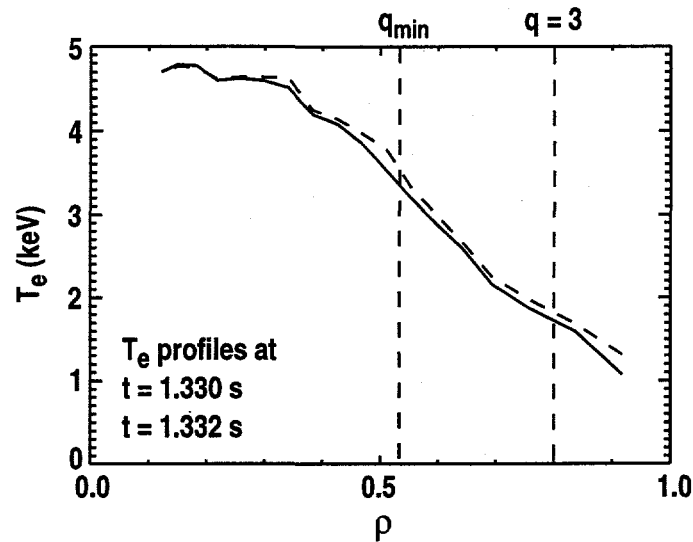


FIG. 3. Electron temperature profiles from electron cyclotron emission before (broken line) and during (solid line) the growth of a resistive wall mode (96519). Magnetic data indicates that the maximum inward displacement at the plasma edge is near the toroidal location of the ECE diagnostic.

lost its wall stabilization. The broad displacement of the  $T_e$  profile in Fig. 3 is consistent with a global kink mode structure, and the radial displacement of  $\sim 1$  cm in the outer part of the profile is consistent with the measured mode amplitude of  $\sim 50$  G at the wall. By itself, a single  $T_e$  profile measurement cannot conclusively rule out the existence of an island. However, in this and other discharges, the outer portion of the  $T_e$  profile rises or falls consistent with an ideal MHD mode structure, given the toroidal phase inferred from magnetic measurements. The temperature perturbation profile agrees well with predictions by the GATO stability code. The growth of a stationary mode in the presence of significant plasma rotation also indicates the absence of islands. (In some cases, electron cyclotron emission and beam emission spectroscopy measurements do show evidence of stationary island formation, but at beta below the ideal no-wall limit.)



## 2. ROTATIONAL STABILIZATION

Plasma rotation is one possible means for long time-scale stabilization by a resistive wall. Vacuum field measurements show that the DIII-D vacuum vessel wall penetration time for an imposed  $n=1$  radial magnetic field can be approximated by a 2-pole response with time constants of 7 ms and 1–3 ms. This agrees well with calculations using the SPARK 3D electromagnetic code which show that the time constant for the lowest  $n=1$  eigenmode of the DIII-D vacuum vessel is about 5.8 ms, followed by about 3 ms for the next eigenmodes. Stabilization for longer times in the experiment indicates that plasma rotation is important.

The existence of a critical rotation frequency for stabilization is clearly demonstrated by a series of reproducible discharges in which the rotation rate was modified through magnetic braking by an applied magnetic perturbation. As the magnetic braking field was increased [Fig. 4(a)], the plasma rotation decelerated more rapidly, and the onset of the resistive wall mode occurred earlier, corresponding to a fixed value of the rotation [Fig. 4(b)].

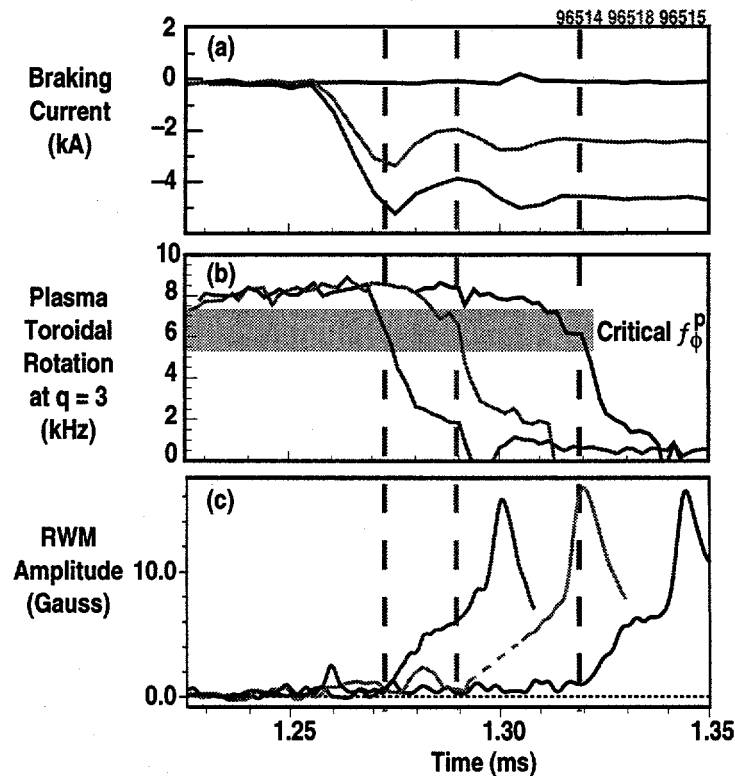


FIG. 4. Three discharges with varying amounts of magnetic braking (96514, 96518, 96515). (a) C-coil current applying an  $n=1$  magnetic perturbation. (b) Plasma rotation frequency at the  $q=3$  surface. (c)  $n=1$  mode amplitude, with C-coil field subtracted. The onset time of the resistive wall mode in each discharge is shown by a vertical line. The inferred critical rotation frequency is shown as a horizontal shaded band.

The experimental data allow us to distinguish at least qualitatively between predicted mechanisms for stabilization. The observed critical rotation frequency  $\Omega = 2\pi f \sim 1\text{--}4 \times 10^4 \text{ s}^{-1}$  at the  $q=3$  surface disagrees with the predictions  $\Omega \sim \tau_w^{-1} \leq 3 \times 10^2 \text{ s}^{-1}$  of theories which include driven islands, and  $\Omega \sim \tau_A^{-1} > 10^6 \text{ s}^{-1}$  of ideal MHD theory. The agreement is somewhat closer with predictions  $\Omega \sim 0.05 \tau_A^{-1} \sim 10^5 \text{ s}^{-1}$  of theories where the ideal mode is stabilized by dissipation which occurs through coupling to sound waves. The observed critical rotation speed is typically at least 10% of the ion acoustic speed, and thus may be consistent with coupling to sound waves.

We speculate that the much more rapid central rotation of  $\Omega \sim 1\text{--}2 \times 10^5 \text{ s}^{-1}$  could also contribute to stabilization, and may account for the variation of the critical rotation frequency. Sound wave coupling and dissipation occur at resonant surfaces, while strong shaping and toroidicity couple poloidal modes so that all integer  $q$  surfaces are important in this global  $n=1$  instability. To date, the discharges which significantly exceed the no-wall beta limit have  $q_{\min} \leq 2$ , placing the  $q=2$  surface in a region of strong rotation (Fig. 1, for example). The critical rotation frequency at the  $q=3$  surface in these discharges is 1–2 kHz. Discharges with  $q_{\min} > 2$  and hence no  $q=2$  surface tend to have a resistive wall mode onset at lower beta and larger rotation, indicating that rotational stabilization is less effective. The discharges in Fig. 4, for example, have  $q_{\min} \approx 2.3$  and develop an RWM at  $\beta_N \sim 2.2$  with a rotation frequency at the  $q=3$  surface greater than 6 kHz.

The plasma rotation is observed to gradually slow in discharges which exceed the no-wall limit, eventually leading to loss of rotational stabilization as in Fig. 1. Comparison of timing in several discharges shows that this slowing does not correlate with the presence of rotating MHD activity, the H-mode transition, or the onset of ELMs. Possible explanations include electromagnetic drag due to a resistive wall mode saturated at small amplitude or drag due to the continuum resonances of a stable resistive wall mode [3]. Figure 5 shows the measured rate of rotational slowing (solid points) caused by magnetic braking and by a large-amplitude resistive wall mode, for the three discharges of Fig. 4. The deceleration rate varies as  $\delta B_r^2$  as expected for the torque caused by a magnetic perturbation (here  $\delta B_r$  at the  $q=3$  surface is estimated from saddle loop measurements, assuming a radial variation  $\delta B_r \propto (r_0/r)^{m+1}$ , where  $r_0$  is the radius of the source current). The magnitude of the deceleration is in reasonable agreement with the force per unit area of  $dF/dS = -\frac{2}{\pi} \frac{\delta B_r^2}{\mu_0} M_p$  predicted in the absence of magnetic islands [8],

where  $M_p$  is the poloidal Alfvén Mach number. The observed deceleration of  $\sim 0.1 \text{ kHz/ms}$  as the discharge of Fig. 1 exceeds the no-wall stability limit (open circle in Fig. 5) could be consistent with a perturbation  $\delta B_r \sim 10\text{--}20 \text{ G}$  at the  $q=3$  surface, or 2–3 G at the saddle loops, which is near

the threshold for detection in this case. Further experimental and theoretical work is needed to determine whether this represents an inherent problem for rotational stabilization.

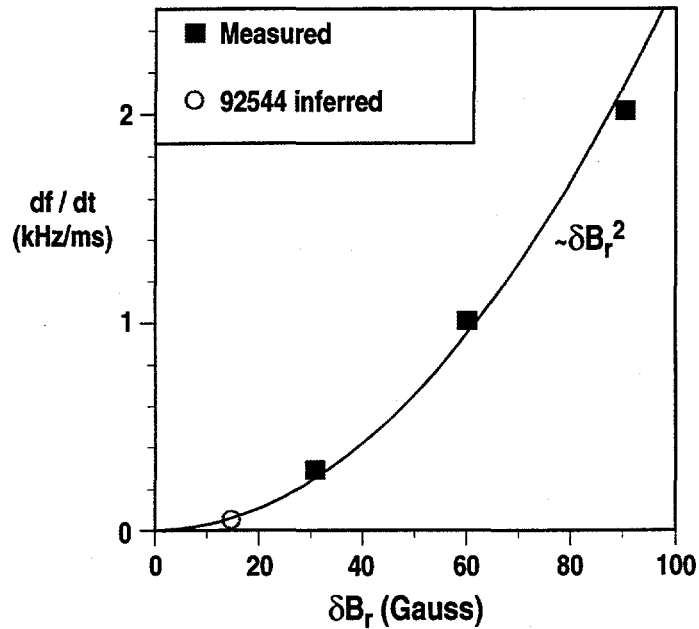


FIG. 5. Measured rate of rotational slowing versus  $\delta B_r$  at the  $q=3$  surface due to applied magnetic braking and a large-amplitude resistive wall mode (solid circles, discharges 96514, 96518, 96515). Measured rate of slowing and inferred  $\delta B_r$  for a strongly wall-stabilized discharge (open circle, discharge 92544).

### 3. ACTIVE CONTROL

The slow growth and rotation of the resistive wall mode should permit active feedback stabilization by non-axisymmetric coils outside the vacuum vessel, without the need for plasma rotation. Active suppression of resistive wall modes may also help to maintain rotation. Several approaches have been proposed, including the "smart shell" [11,12] where the feedback control is designed to maintain a net zero change in radial magnetic field at the resistive wall, and the "fake rotating shell" [13] in which a phase shift applied to the response mimics the effect of a rotating wall. These schemes will be tested in active control experiments which are planned for DIII-D, initially using the existing error field coil (C-coil). A set of six midplane saddle loops for mode detection have recently been installed, matched in geometry to the six toroidal segments of the C-coil.

A preliminary experiment in open-loop control has been performed, with encouraging results for feedback control experiments. A series of discharges was established having a resistive wall mode at a reproducible onset time and spatial phase. Then the C-coil was programmed to produce a static  $n=1$  magnetic perturbation with a spatial phase opposing the mode, beginning at the anticipated onset time. (The lack of bipolar power supplies required this  $n=1$  perturbation to be superimposed on a constant  $n=3$  bias field; other experiments established that this  $n=3$  field has no detectable effect on plasma stability.) As seen in Fig. 6, in the stabilized discharge the electron temperature, beta, and plasma rotation hesitate at the anticipated onset time, then continue at constant or increasing values. In contrast, these parameters decrease rapidly in the comparison shot without the stabilizing  $n=1$  field. These results suggest that the resistive wall mode was stabilized by the opposing  $n=1$  field. Although complicated by the rapidly changing applied fields, analysis of the saddle loop data indicates that the instability was delayed by at least 20 ms.

Closed-loop feedback experiments in the near future will be aimed at comparing control algorithms and demonstrating improved stability. New bipolar power supplies to be procured in 1999 and 2000 will increase the power available for feedback stabilization. Numerical modeling with the VALEN 3D electromagnetic code [14] indicates that feedback stabilization using the existing 6-segment C-coil can produce a measurable ( $\sim 15\%$ – $20\%$ ) increase in beta over the no-wall limit. Modeling also shows that an extension of the C-coil with additional segments above and below the midplane can double the margin over the no-wall stability limit by allowing better coupling to the helical mode structure. Experimental validation of the models with the existing midplane coil set will provide support for the design of the extended coil set.

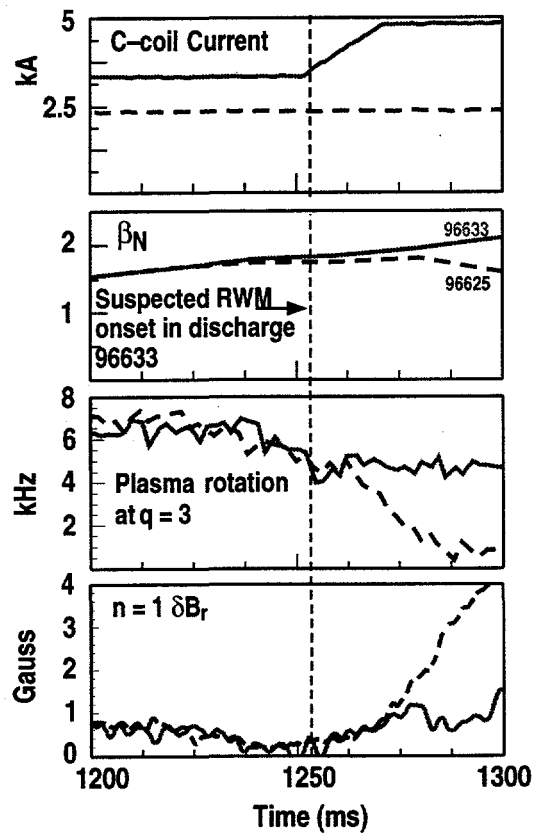


FIG. 6. Comparison of a discharge with a static  $n=1$  perturbation applied to oppose the resistive wall mode (solid curves, discharge 96633) and a discharge without the perturbation (broken curves, discharge 96625). (a) C-coil current. (The non-zero dc level represents an  $n=3$  bias field.) (b) Normalized beta. (c) Plasma rotation frequency at the  $q=3$  surface. (d)  $n=1$  mode amplitude, with C-coil field subtracted.

#### 4. SUMMARY

DIII-D experiments have shown that a resistive wall can stabilize a rotating plasma at beta values well above the ideal no-wall limit, for durations much longer than the resistive wall penetration time for  $n=1$  magnetic fields. The predicted resistive wall mode has been observed as the plasma rotation decreases below a critical value of a few kHz, and the ideal structure of the mode has been confirmed. The critical rotation frequency for stabilization may be consistent with theories which include dissipation by coupling to sound waves to provide stabilization in the absence of islands. Long-duration sustainment of wall-stabilized plasmas has been hindered by a slowing of rotation as beta exceeds the no-wall limit. We conjecture that the slowing may result from drag caused by a small-amplitude resistive wall mode or by continuum resonances of the stabilized resistive wall mode. Modeling predicts that feedback stabilization using non-axisymmetric coils can provide a significant increase over the no-wall beta limit. In a preliminary open-loop experiment, the onset of the resistive wall mode was postponed for several wall penetration times, an encouraging result for closed-loop feedback experiments.

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