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TENSION BENDING RATCHETING TESTS OF 304 STAINLESS STEEL

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Tension Bending Ratcheting Tests of 304 Stainless Steel

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ABSTRACT

This paper discusses results of an experimental program conducted to investigate the strain ratcheting behavior of 304 stainless steel under various combinations of applied membrane load and displacement controlled cyclic bending strain. Tests were performed on uniaxial specimens at temperatures of 70°F (21°C) and 550°F (288°C). Bending strain, ratchet strain and axial displacement of the specimens were monitored throughout the tests. Membrane stress to monotonic yield stress ratios of 2/3, 1/2, and 1/3 were tested with pseudo-elastic bending stress to yield stress ratios ranging from 1.4 to 10.7. Test output was in the form of plots of cumulative axial membrane strain versus cycles up to the point of shakedown, i.e., the point at which no additional progressive strain was observed. Shakedown was demonstrated in the 550°F tests but not the room temperature tests. The 550°F results are shown in terms of shakedown membrane strain versus equivalent bending stress ratio for each of the tested membrane stress ratios. The cyclic and monotonic stress-strain curves for the test materials are presented to enable the use of various models for predicting the ratcheting and

shakedown behavior. The results may be used to develop improved ratcheting and shakedown rules permitting a relaxation of the traditional ratcheting rules in the ASME Boiler and Pressure Vessel Code.

Nomenclature

$\Delta\epsilon_b$ =applied bending strain range

ϵ_s =shakedown strain

ϵ_R =applied strain range in cyclic stress strain tests

ϵ_r =ratchet strain

$\dot{\epsilon}$ =strain rate, [strain/min.]

ΔS_R =stabilized stress range

T=membrane tension

M_e =bending moment

θ_e =rotation angle

δ_x =deflection

Y_c, Y_x =shear loads

L_T =specimen length

L_G =specimen gage length

S_M =membrane stress

S_B =equivalent elastic bending stress range, $E \Delta\epsilon_b$

S_y =0.2% offset monotonic yield stress

E=Young's Modulus

Introduction

The ASME Boiler & Pressure Vessel Code (hereafter, the Code) includes a limit on the primary plus secondary stress intensity range of $3S_M$ in conjunction with the primary membrane stress of S_M . These limits are intended to provide protection against progressive deformation by the ratcheting mode. In addition to protection against ratcheting, these limits assure validity of the fatigue procedure by limiting local strains to values consistent with elastically calculated strains due to elastic shakedown of the surrounding structure. Welded seals, such as omega or canopy, are examples where the $3S_M$ limit is not easily met and where special limits are applied per NB-3227.7 of the Code which states that the ratchet limits of NB-3228.5(d) of the Code need not apply. Generally, any application of NB-3228.5 of the Code should require an evaluation for ratcheting. The particular failure mode of interest in this case is local ratcheting at a critical cross section of the seal which is subject to high secondary bending stresses induced by the motions imposed upon the seal by the surrounding structure.

A conservative basis for preventing ratcheting is available in the Bree chart (Bree, 1967) for ideal elastic-perfectly plastic material. However, this approach can be quite conservative for materials with significant cyclic hardening such as austenitic steels subject to combined steady state membrane stress and cyclic bending strain. The tension-bending test program described in this paper was designed to produce data for a range of loading parameters in order to qualify an extension of the Bree chart for monotonic ratchet strains of 1% and greater. The data were developed on Alloy 600 and 304 stainless steel (SS) at room temperature and 550°F (288°C). The cyclic and monotonic properties for the test materials were well characterized to permit prediction of the data by various constitutive models. Results of tests on Alloy 600 were previously reported by

Larson, *et al* (1995).

Material Stress Strain Properties

The 304SS material used in the tension bending tests had monotonic 0.2% offset yield stresses near Code values. The actual values were 32.5 and 18.2 ksi (224 and 126 MPa) at room temperature and 550°F (288°C), respectively versus values listed in Code material property tables of 30 and 18.75 ksi (207 and 129 MPa). The strain rate in these basic tests was 0.05/min. An additional test at a strain rate of 0.005/min was performed to provide information on the strain rate effect. The monotonic stress strain curves are presented in Figure 1. Young's modulus for this material was assumed to be 28.3×10^6 psi (195×10^3 MPa) at room temperature and 25.8×10^6 psi (178×10^3 MPa) at 550°F (288°C). Ramberg-Osgood type stress strain curves shown in the figure were obtained using the NLFIT (Marquardt, 1963) non-linear curve fitting program.

Cyclic stress strain curves were also developed at both room temperature and 550°F (288°C). An hourglass specimen with diametral strain control was utilized in these tests. Cyclic strain data were obtained from both multiple specimen tests and single specimen tests in which the cyclic strain range was increased after stabilization was achieved at a given strain range. The room temperature results are summarized in Table 1 and the 550°F (288°C) data is given in Table 2.

As reflected in the last column of Table 1, the room temperature results show that stress ranges developed by stepping down from higher strain ranges are somewhat higher than the corresponding stress ranges in the step up phase. This behavior is particularly evident by comparing results for specimen SC1 with results for specimens SC2, SC3, SC16 and SC5 suggesting that strain amplitude and order effects are important. The 550°F data in Table 2 show little effect of prior cycling during the step up phase but

do show an effect during the step down phase. Table 3 summarizes results of multiple specimen tests at 550°F. The results agree very well with the average results for the multiple step tests in Table 2. As shown in the last column of Table 3, decreasing the strain rate increased the cyclic hardening response of the material. The cyclic stress-strain curves shown in Figure 2 were obtained by fitting data from the step up phase to the Ramberg-Osgood type equation using NLFIT (Marquardt, 1963). The observation that cyclic history effects is important particularly of room temperature for 304 stainless steel is consistent with the findings of Jaske (1973), Conway and Stentz (1988), and Conway, *et al* (1975).

Tension Bending Test Apparatus

The basic test concept used to produce the combined tension and bending loading is illustrated schematically in Figure 3. The specimen is loaded axially in tension by a dead weight load T which develops a primary membrane stress, σ_M . The ends of the specimen are then rotated cyclically ($\pm\theta_e$) to produce the desired bending strain range (secondary stress range), $\Delta\epsilon_b$. One end of the specimen is free to translate axially so ratcheting (progressive growth) can take place. The loading concept is intended to produce essentially a combination of pure bending and axial force in the gage length, L_G . The pure bending condition can be approached but not fully attained because the axial force causes a contribution to the bending moment when the specimen is bent out of its plane. The test specimen, Figure 4, was designed to minimize the strain variation along the gage length by keeping it as short as possible and varying the thickness. Figure 5 is a photograph of the loading assembly and apparatus.

Instrumentation

Six uniaxial strain gages were located on the specimen; two on opposite sides of each shoulder

to measure the elastic bending strains and two on opposite sides of the gage mid-length to measure the membrane strain. For the measurement of membrane strain in the gage section, high elongation type gages were used in the room temperature tests and temperature resistant gages were used in the 550°F tests.

Load cells were located on both the horizontal driving ram and vertical shaft of the tension bending loading assembly. The output of the vertical load cell served as a check on the consistency of axial loading applied during cycling. The cyclic loading required to deflect the specimen during bending can be determined from the output of the horizontal load cell and was useful in calculating the strains in the elastic region of the specimens should the strain gages malfunction. A special elongation gage was used for back-up measurement of the axial growth of the specimen. Elongation was converted to strain using an effective gage length of 0.825 inches. The final cumulative strains were also checked by determining the increase in the gage length from before and after measurements of scribe lines.

Data collection during a test was accomplished through an 8-channel Beckman Recorder so that output from the strain gages and load cells versus cycles could be continuously recorded. A parallel circuit was used to record data at peak values by momentarily stopping the specimen at its maximum right and left displacements.

Results of Room Temperature Tests

The results of the room temperature tests are summarized in Figures 6 and 7. Figure 6 shows cumulative strain versus cycles for an applied membrane stress of $2/3 S_y$ and four different bending strain ranges shown in the figures as S_B/S_y where $S_B = E\Delta\epsilon_b$. As seen in Figure 6 and 7, shakedown was obtained for specimen SB1 only. Since it was thought that shakedown should occur for a strain hardening material, an investigation

into possible test problems was performed and an elongation gage was added as a check on the strain gage readings.

Figure 7 shows results for an applied membrane stress of $1/2 S_y$. Again, shakedown was not obtained and the strain estimates based on elongation of the gage length verified the strain gage measurements. High elongation strain gages were chosen for the room temperature tests because it was felt they would survive the expected high cumulative strains. However, testing of several specimens in bending only (no membrane load) demonstrated that the gage drift is small on a per cycle basis but can introduce significant cumulative error in the monotonic strain when the cycles exceed about 1000. The dashed curves in Figures 6 and 7 show the estimated corrections based on elimination of the gage drift. In Figure 6, it appears that gage error could account for the lack of shakedown. However, this is not the case in Figure 7. The load instrumentation indicated that the bending moment in the gage section stabilized in less than 1000 cycles.

It is apparent from Figures 6 and 7 that many cycles may be required to reach complete shakedown at room temperature. This prolonged shakedown period is considered due to time and history dependent cyclic strain hardening affects that are more pronounced at room temperature than at elevated temperature.

Results of 550°F (288°C) Tests

The initial test procedure was to test a single specimen at a given membrane load ratio, S_M/S_y and equivalent bending stress ratio, S_B/S_y . Results of these tests are shown in Figures 8, 9, and 10.

Cumulative strain versus cycles for the 550°F tests at a membrane load of $2/3 S_y$ are shown in Figure 8. The data for specimens SB10 and SB13 show that shakedown definitely occurred. The strain

gage data for specimens SB8 and SB11 show that shakedown was nearly achieved. Strains were measured with both high temperature strain gages and an elongation gage and show agreement over the survival time of the gages. Also, final strains were estimated by pre and post scribe line measurements and these agree with the final values measured by the elongation gages. Because shakedown was demonstrated in these tests, the test procedure was revised to take advantage of this and make more economical use of the specimens.

The procedure used in the remaining 550°F tests was designed to maximize the data obtained from a single specimen. The multiple step cyclic stress strain data in Tables 1 and 2 show that the effect of prior cycling on the cyclic properties is small if the cyclic strain range is increased after stabilization for a given strain range. Therefore, the applied bending strain range was set relatively low in the first test block and the specimen was cycled until the membrane strain ceased to increase with further cycling. A second test block with a higher bending strain range was then initiated. By repeating this process, a single specimen could be used to generate shakedown data for several different bending strain ranges for a particular value of membrane stress. Figures 9 and 10 show examples of this. In Figure 9, cumulative strain at shakedown for a S_M/S_y ratio of $1/2$ was determined for six different equivalent elastic bending strain range ratios. In Figure 10, shakedown was demonstrated for five different S_B/S_y ratios with $S_M/S_y = 1/3$.

Hold times of up to an hour were incorporated at various times in these tests and showed negligible effect on cumulative strain.

Interpretation of Results

The results of these tests demonstrate that shakedown can be difficult to achieve in 304 stainless steel at room temperature probably due to

cyclic strain rate effects that are more pronounced at room temperature than at elevated temperature. A contributing factor to the prolonged ratcheting at room temperature is the relatively low strain hardening of the monotonic stress strain curve and the fact that decreasing strain rates lead to lower stress magnitudes for a given strain. This is seen in Figure 1 by comparing the 0.05/min. strain rate results with the 0.005/min. curve. Pronounced strain rate effects are not observed at 550°F (288°C) as seen in Figure 2. The center core of the specimen essentially carries the membrane load and this section is controlled by the monotonic strain rate effects rather than cyclic stress-strain effects since only the outer fibers of the specimen are cycled by bending. Thus, a prolonged shakedown period is experienced at room temperature as the monotonic strain rate decreases the monotonic stress-strain curve as shakedown is approached

The results for the elevated temperature are of more practical interest since many pressure vessel and piping applications involve temperatures greater than room temperature. Also, the test matrix for the elevated temperature tests include tests with membrane-to-yield stress ratio down to 1/3 which is typical of ASME B&PV code applications. Therefore, lack of shakedown at room temperature is not considered critical to the application of results. The results of the 550°F tests are summarized in Table 4 and plotted in Figure 11.

For each value of $[S_M/S_y]$, the 550°F (288°C) data were fit to an equation of the form

$$\epsilon_S = B_1 [S_B/S_y]^2 \quad (1)$$

using the NLFIT (Marquardt, 1963) program. Using the data in Table 4, the following results were obtained

$$\epsilon_S = 0.02524 [S_B/S_y]^2 \text{ for } [S_M/S_y] = 1/3 \quad (2)$$

$$\epsilon_S = 0.07195 [S_B/S_y]^2 \text{ for } [S_M/S_y] = 1/2 \quad (3)$$

$$\epsilon_S = 0.1162 [S_B/S_y]^2 \text{ for } [S_M/S_y] = 2/3 \quad (4)$$

These equations are compared to the data in Figure 11.

Although shakedown was not demonstrated in the room temperature tests, the ratchet strain can be obtained from Figures 6 and 7 for a particular number of cycles. For example, the ratchet strains for 200 cycles given in Table 5 were obtained from Figure 6 and 7 for various values of S_B/S_y and S_M/S_y .

The thermal stress ratchet limit in the ASME B&PV Code is given by Paragraph NB-3222.5 which provides two cases. Case 1 is for linear variation of the thermal stress through the wall and Case 2 is for parabolic constantly increasing variation of temperature through the wall. The results provided herein are cast in terms of the ASME Code procedure and shown graphically in Figure 12. The present results are analogous with Case 1 where the bending stress is equivalent to the thermal stress. The 0% strain curve in Figure 12 represents the Code limit boundary on ratchet strain given by the equations

$$S_B/S_y = 1/[S_M/S_y] \text{ for } [S_M/S_y] \leq 0.5 \quad (5)$$

$$S_B/S_y = 4[1 - S_M/S_y] \text{ for } 0.5 < S_M/S_y \leq 1.0$$

The curves for strains of 1%, 2% and 3% were constructed from the best fit lines in Figure 10 and give the locus of actual shakedown for the material tested in this program. These curves were obtained using NLFIT to fit equations of the form $[S_B/S_y] = B/[S_M/S_y]$ using $[S_B/S_y]$ values from Equations (2), (3), and (4) for 1%, 2% and 3% shakedown strain at $[S_M/S_y] = 1/3, 1/2, \text{ and } 2/3$. The equations for 1%, 2%, and 3% ratchet strain are

$$1\% \text{ strain; } S_B/S_y = 2.014/[S_M/S_y] \quad (6)$$

$$2\% \text{ strain; } S_B/S_y = 2.849/[S_M/S_y] \quad (7)$$

$$3\% \text{ strain; } S_B/S_y = 3.489/[S_M/S_y] \quad (8)$$

These equations are plotted with supporting data in Figure 12. The curves represent boundaries between regimes of bounded ratcheting. For a particular ratchet strain, shakedown is obtained after ratcheting up to the ratchet strain. The regime to the left of a ratcheting strain curve represents the regime of stabilized shakedown for that particular ratchet strain while the regime to the right represents continuing ratcheting to some higher value. The regime to the left of the zero percent strain line represents the region of elastic shakedown with no accumulated ratchet strain while the region to the right represents safe ratchet strain up to a particular value. For example, the 1% curve represents the locus of bending stress ratio and membrane stress ratio which results in 1% cumulative membrane ratchet strain. This suggests the possibility of relaxing Code rules when a permanent membrane strain of 1% can be tolerated in the component.

Conclusion

The shakedown behavior of 304 SS at room temperature and 550°F (288°C) has been investigated. A significant database on shakedown has been generated and is supported by detailed characterization of the monotonic and cyclic properties of the material. The shakedown data demonstrates that the ASME Code ratchet rules are conservative and suggests that the rules could be relaxed at low values of S_M/S_y when some small amount of membrane straining is not objectionable.

Acknowledgments

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TABLE 1
CYCLIC STRESS STRAIN RESULTS ROOM TEMPERATURE

e_R	S_R (SC1) ksi(MPa)	S_R (SC2) ksi(MPa)	S_R (SC3) ksi(MPa)	S_R (SC16) ksi(MPa)	S_R (SC5) ksi(MPa)	S_R (AVE) ksi(MPa)
0.002	53.5 (369)	-	-	-	-	53.5 (369)
0.005	75.4 (520)	64.7 (446)	-	-	-	70.1 (484)
0.010	87.7 (605)	80.0 (552)	81.5 (562)	-	-	83.1 (573)
0.015	96.1 (663)	88.3 (609)	88.8 (613)	92.5 (638)	-	91.4 (630)
0.020	105.2(726)	94.4 (651)	94.9 (655)	99.9 (689)	103.6(715)	99.6 (687)
0.025	123.4(851)	102.7(708)	99.9 (689)	108.8(751)	124.2(857)	111.8(771)
0.030	161.4(1113)	114.4(789)	105.1(725)	139.6(963)	140.6(970)	132.2(912)
0.025	-	-	102.0(704)	132.5(914)	134.5(928)	123.0(848)
0.020	-	-	93.9 (648)	124.3(857)	125.2(864)	115.9(799)
0.015	-	-	-	112.9(779)	116 (800)	114.5(790)
0.010	-	-	-	-	106.7(736)	106.7(736)

TABLE 2
CYCLIC STRESS STRAIN RESULTS, 550°F, $e_R = 0.03/\text{min}$

e_R	S_R (SC15) ksi(MPa)	S_R (SC7) ksi(MPa)	S_R (SC8) ksi(MPa)	S_R (SC9) ksi(MPa)	S_R (SC12) ksi(MPa)	S_R (AVE) ksi(MPa)
0.002	35.4(244)	-	-	-	-	35.4(244)
0.005	46.7(322)	46.7 (322)	-	-	-	46.7(322)
0.010	70.2(484)	68.8(475)	70.8(489)	-	-	69.9(482)
0.015	87.3 (602)	85.3 (589)	86.3 (595)	90.3 (623)	-	87.3 (602)
0.020	100.7(695)	98.5 (680)	101.7(702)	101.6(701)	104.8(723)	101.5(700)
0.025	113.0(780)	113.9(786)	114.0(787)	114.0(787)	114.0(787)	113.8(785)
0.030	123.4(851)	123.3(851)	123.3(851)	123.2(850)	123.2(850)	123.3(851)
0.025	-	114.0(787)	116.0(800)	115.0(794)	117.0(807)	115.5(797)
0.020	-	-	98.6 (680)	106.8(737)	105.7(729)	103.7(716)
0.015	-	-	-	102.7(709)	94.5 (652)	98.6 (680)
0.010	-	-	-	-	76.0 (524)	76.0 (524)

Notes: e_R = Applied strain range
 S_R (SC1) = Stabilized Stress Range (Specimen Identity)

TABLE 3
MULTIPLE SPECIMEN TESTS AT 550°F

Specimen	ϵ_R	S_R ($\dot{\epsilon} = 0.03/\text{min}$) ksi (MPa)	S_R ($\dot{\epsilon} = 0.0003/\text{min}$) ksi (MPa)
SC10	0.005	45.20(312)	74.97(517)
SC11	0.015	87.30(602)	98.80(682)
SC13	0.025	115.90(800)	122.23(843)

TABLE 4
SUMMARY OF 550°F (288°C) TEST RESULTS

Specimen	Test Block	S_M/S_Y	S_B/S_Y	$\epsilon_r(1)$
SB10	1	2/3	2.85	0.012
SB13	1	2/3	2.17	0.007
SB11	1	2/3	5.27	0.029
SB8	1	2/3	4.85	0.030
SB6	1	1/2	2.57	0.004
SB6	2	1/2	3.28	0.010
SB6	3	1/2	4.13	0.014
SB6	4	1/2	5.84	0.026
SB6	5	1/2	6.41	0.029
SB6	6	1/2	7.84	0.043
SB7	1	1/3	2.57	0.001
SB7	2	1/3	4.42	0.004
SB7	3	1/3	7.13	0.013
SB7	4	1/3	8.69	0.019
SB7	5	1/3	10.69	0.029

(1) ratchet strain

TABLE 5
SUMMARY OF ROOM TEMPERATURE RESULTS

Specimen	Test Block	S_M/S_Y	S_B/S_Y	$\epsilon_{200}(1)$
SB1	1	2/3	7.2	0.071
SB2	1	2/3	1.77	0.009
SB2	2	2/3	2.52	0.025
SB3	1	2/3	4.2	0.040
SB4	1	1/2	2.78	0.014
SB5	1	1/2	1.43	0.002
SB14	1	-	4.96	0.036

Note: (1) ϵ_{200} = Ratchet strain at 200 cycles.

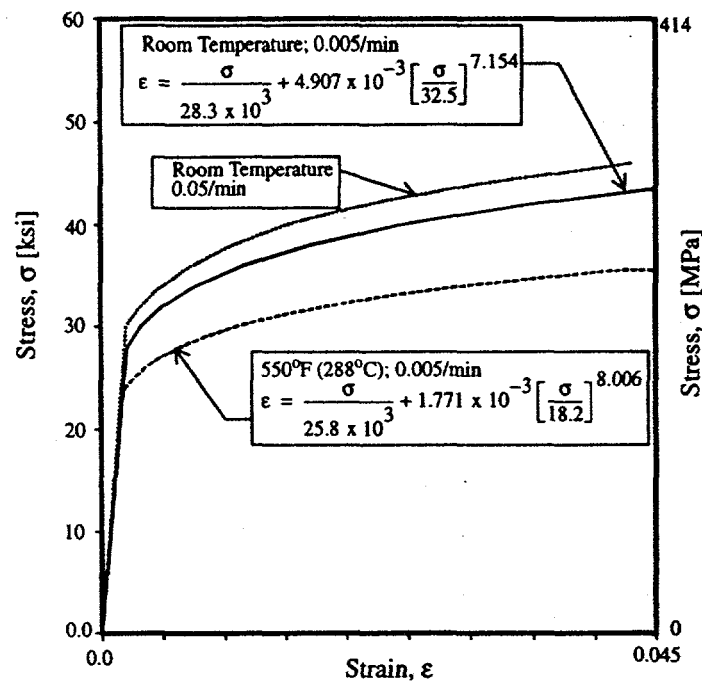


FIGURE 1. ROOM TEMPERATURE AND 550°F (288°C) MONOTONIC STRESS STRAIN CURVE

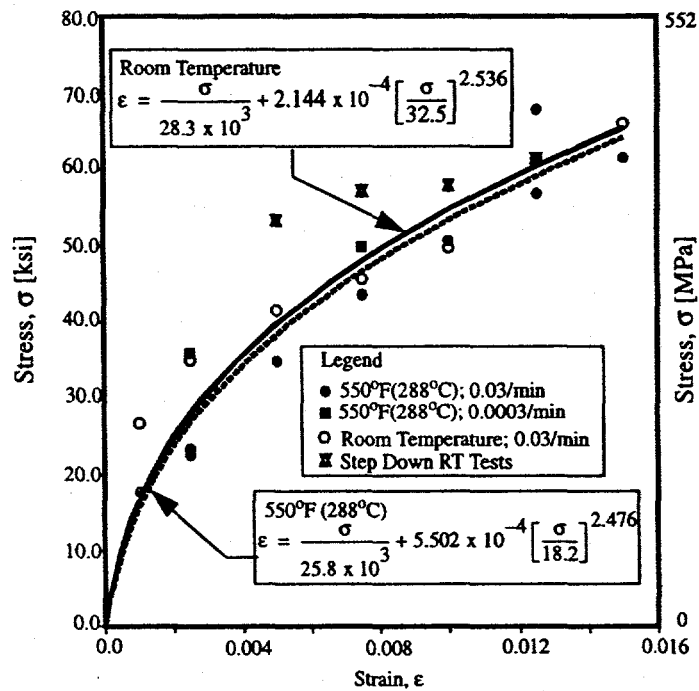


FIGURE 2. ROOM TEMPERATURE AND 550°F (288°C) CYCLIC STRESS STRAIN CURVES

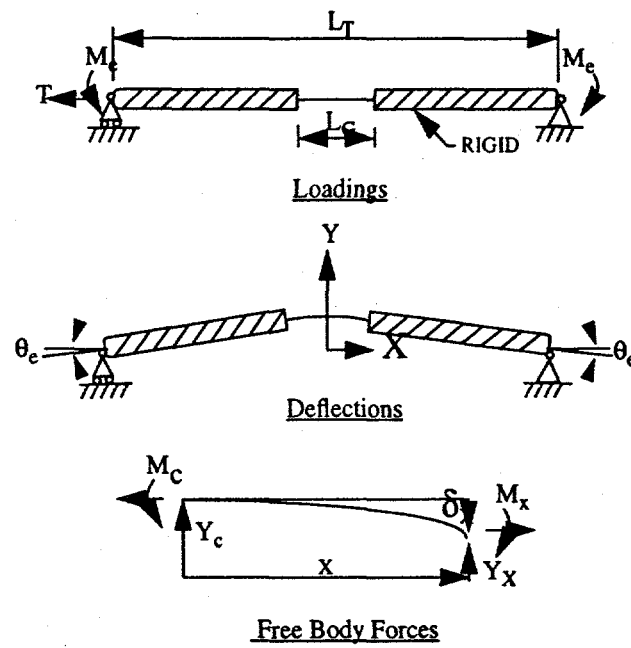


FIGURE 3. TENSION BENDING TEST CONCEPT

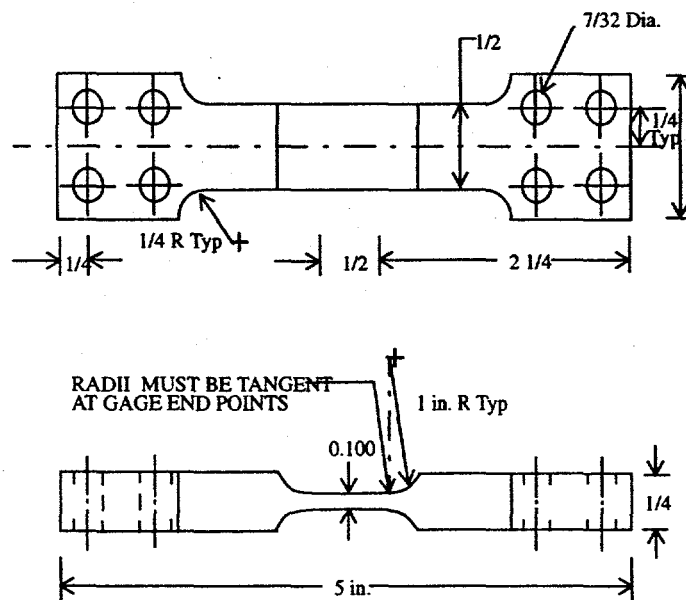


FIGURE 4. TENSION BENDING TEST SPECIMEN

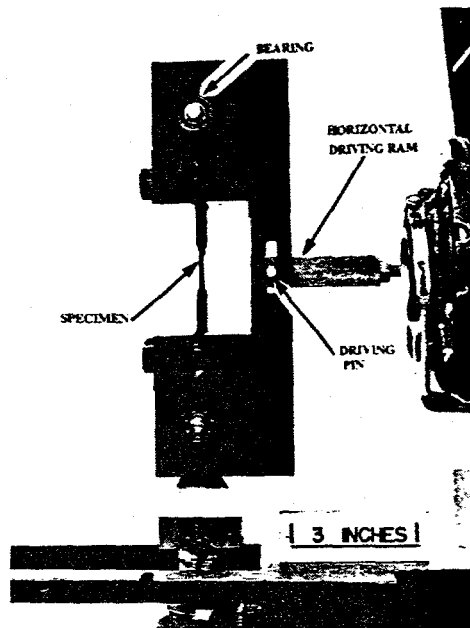


FIGURE 5. TENSION-BENDING TEST; SPECIMEN HOLDING JIG

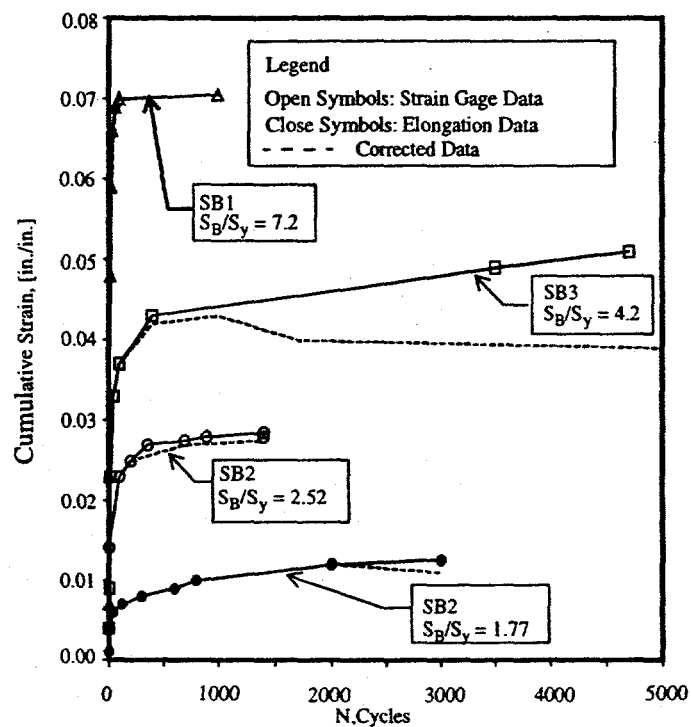


FIGURE 6. CUMULATIVE STRAIN VS. CYCLES; ROOM TEMPERATURE; $S_M/S_y = 2/3$

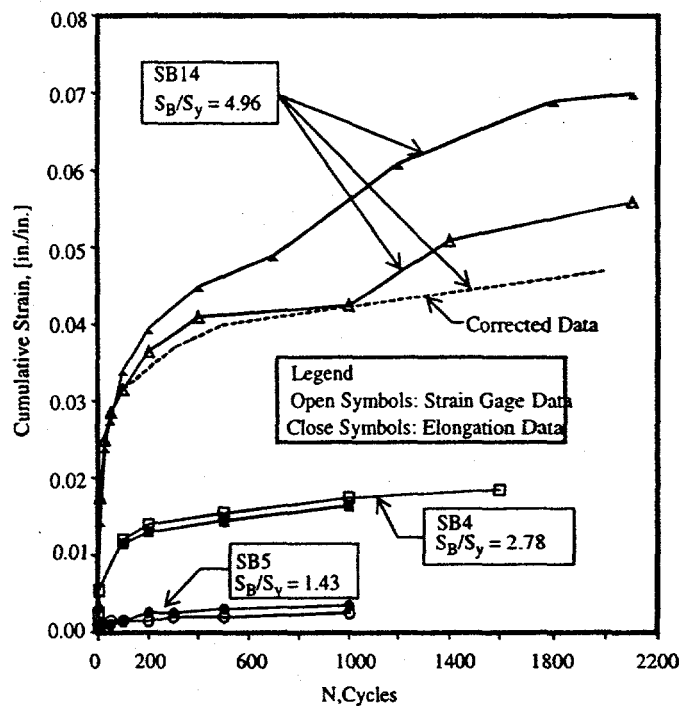


FIGURE 7. CUMULATIVE STRAIN VS. CYCLES; ROOM TEMPERATURE; $S_M/S_y = 1/2$

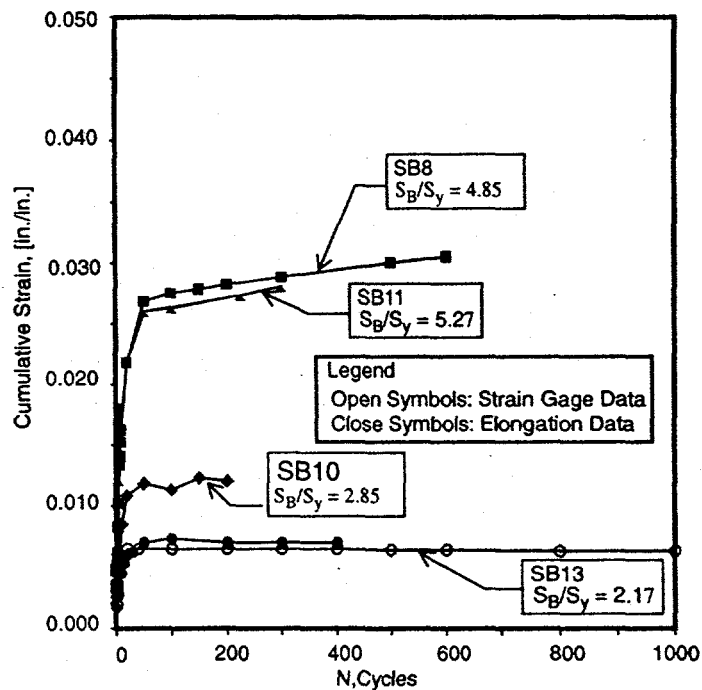


FIGURE 8. CUMULATIVE STRAIN VS. CYCLICS; 550°F (288°C); $S_M/S_y = 2/3$

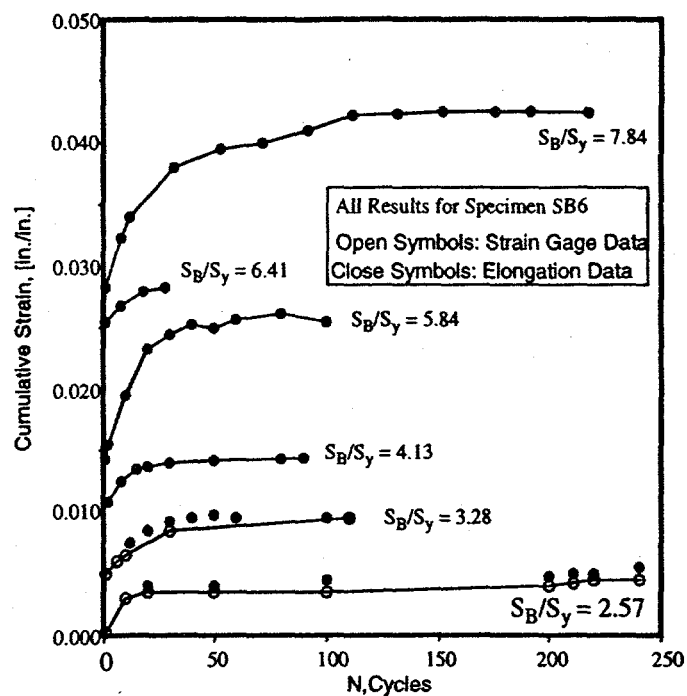


FIGURE 9. CUMULATIVE STRAIN VS. CYCLES; 550°F (288°C); $S_M/S_Y = 1/2$

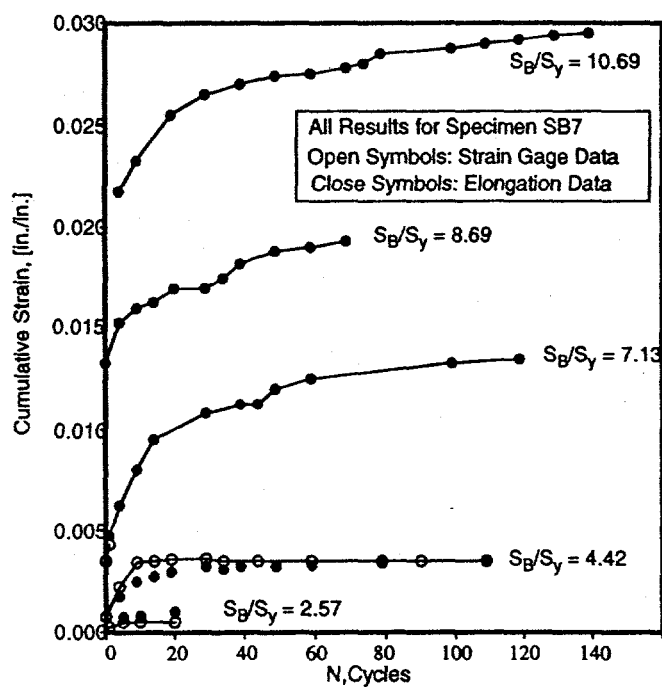


FIGURE 10. CUMULATIVE STRAIN VS. CYCLES; 550°F (288°C); $S_M/S_Y = 1/3$

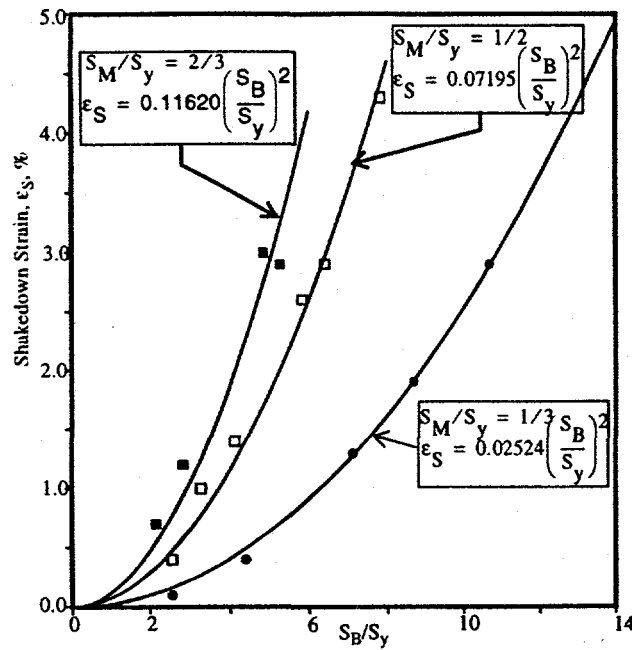


FIGURE 11. SHAKEDOWN STRAIN VS. BENDING STRESS; 550°F (288°C)

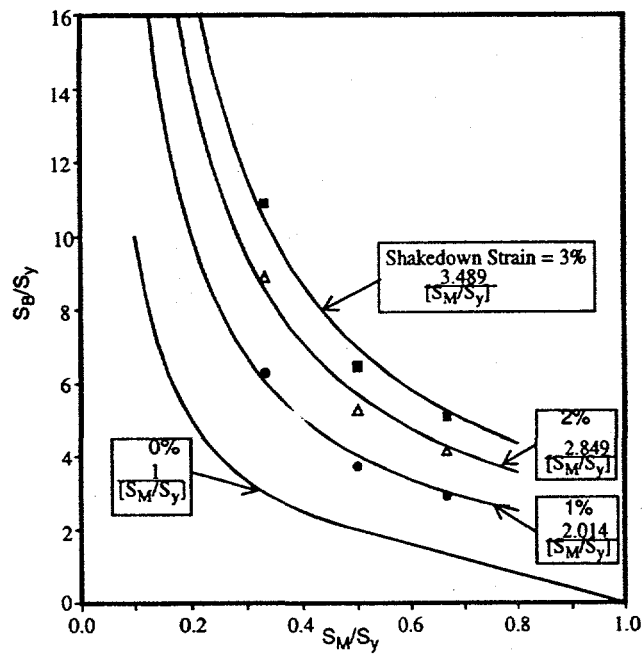


FIGURE 12. SHAKEDOWN DIAGRAM