

1 **Nickel Enhances InPd-catalyzed Nitrate Reduction Activity and N₂ Selectivity**

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34 **Abstract**

35 Palladium-indium (PdIn) is a well-established bimetallic composition for reductively degrading
36 nitrate anions, one of the most ubiquitous contaminants in the groundwater. However, the
37 scarcity and the variable price of these rare earth and platinum group critical metals may
38 hinder their use for water treatment. Nickel (Ni), a non-precious metal in the same element
39 group as Pd, could partially replace and lower Pd usage if the resulting trimetallic composition
40 is sufficiently catalytically active. Herein, we report the synthesis and nitrate reduction catalysis
41 of activated carbon-supported "In-on-Pd-on-Ni" catalysts (InPdNi/AC). Whereas bimetallic
42 InPd/AC (0.05 wt% In, 1.3 wt% Pd) was expectedly active, trimetallic InPdNi/AC containing
43 the same In amount, much less Pd (0.1 wt%), and 1 wt% Ni, was >17 more active ($k_{\text{cat}} \approx 20$
44 vs. $349 \text{ Lmin}^{-1}\text{g}_{\text{surface-metal}}^{-1}$). X-ray photoelectron spectroscopy (XPS) and density functional
45 theory (DFT) calculations showed that Pd gained electron density from the Ni, correlating to
46 the increased nitrate reduction activity. Ammonium by-product selectivity for InPdNi/AC (18%
47 at 50% nitrate conversion) was lower compared to that of InPd/AC (48%), suggestive of higher
48 surface coverage of NO or its greater reactivity with NO_2^- which lead to more N_2 . Accounting
49 for catalyst precursor, manufacturing costs, and spent metal recovery, we calculated that Ni
50 incorporation lowered net catalyst cost significantly (from \$1028/kg to \$170/kg). The trimetallic
51 composition lowered, by ~26 times, the catalyst cost of a stirred tank reactor sized to the same
52 treatment capacity as that for the bimetallic case. The results demonstrate the partial
53 replacement of the precious metal with an earth-abundant one leads to both a higher-efficiency
54 and a lower-cost denitrification catalyst, via a materials strategy that should be beneficial for
55 other clean-water catalytic systems.

56

1 Introduction

2 Nitrate (NO_3^-) contamination in groundwater has been a pervasive problem and it is expected
3 to grow even more as the demand for agricultural fertilizer use increases and new health risks
4 are identified.^{1,2} Acute exposure to NO_3^- and its reduced form, nitrite (NO_2^-), can cause serious
5 health problems, such as blue-baby syndrome (methemoglobinemia). Current United States
6 Environmental Protection Agency (U.S. EPA) limits the maximum contaminant level (MCL) of
7 NO_3^- and NO_2^- to 10 and 1 mg-N/L, respectively.³ Cancer and hypertension continue to be
8 evaluated as additional health endpoints with the potential to reduce regulatory limits in the
9 future.⁴⁻⁶

10 Technologies including ion exchange (IX), reverse osmosis, biological treatment, and
11 electrodialysis remove NO_3^- in drinking water at smaller and larger scales.⁷⁻¹² Of these
12 physical removal technologies, IX is the most commonly used to treat NO_3^- in the U.S.^{7,9}
13 However, its main drawback (like the other processes) is that after IX resin regeneration it
14 produces NO_3^- concentrated waste brines up to 20 wt% NaCl containing nitrate, sulfate and
15 bicarbonate.¹³ While anaerobic biological treatment is common for wastewater treatment, it is
16 not used for drinking water treatment. The requirements of adding external organic (e.g., acetic
17 acid) or inorganic (e.g., hydrogen gas) electron donors limit its full-scale adoption because of
18 challenges due to active biomass growth during intermittent system operations and release of
19 extracellular byproducts into the treated drinking water.¹⁴⁻¹⁹

20 NO_3^- electroreduction has also been considered as an alternative for converting NO_3^-
21 into N_2 gas in both drinking water and wastewater treatment as electroreduction process has
22 great potential to effectively remove NO_3^- .²⁰⁻²⁵ However, achieving selective NO_3^- reduction to
23 N_2 becomes challenging when treating water with low NO_3^- concentration, which is commonly
24 found in groundwater.²⁶ Furthermore, the addition of electrolytes and chloride ions, along with
25 the requirement to maintain a high pH for effective removal, significantly limits the applicability
26 of using electrocatalytic reduction of NO_3^- in drinking water treatment applications.^{26,27}

27 Another emerging destructive approach is catalytic reduction. Since the first publication
28 of bimetallic palladium(Pd)-based $\text{NO}_3^-/\text{NO}_2^-$ reduction in 1989 by Vorlop and Tacke,²⁸ there

29 have been significant efforts to understand the reduction chemistry, to improve the catalytic
30 materials, and to develop them into a viable technology.^{29–39} Although monometallic Pd is an
31 excellent reduction catalyst for NO_2^- , it is ineffective for NO_3^- reduction.^{28,29,40,41} An
32 appropriately chosen second metal is needed to promote NO_3^- reduction. In 1997, Vorlop and
33 coworkers reported a PdIn bimetallic catalyst for NO_3^- reduction for the first time, where In
34 activates the reduction of NO_3^- to NO_2^- , and Pd is responsible for the subsequent reduction of
35 NO_2^- to the end product, either N_2 or NH_4^+ .⁴² The PdIn combination is preferred for NO_3^-
36 reduction over PdCu and PdSn compositions due to higher by-product selectivity towards N_2
37 over NH_4^+ ,^{32,36,37,42–44} and catalyst stability under various reaction conditions.^{45,46}

38 Our group showed in 2018 that (i) In-decorated Pd nanoparticles are catalytically active
39 for NO_3^- reduction, (ii) their NO_3^- reduction activity show a strong volcano-shape dependence
40 on In surface coverage, (iii) the most active PdIn composition contain two-dimensional
41 ensembles of 4-6 indium atoms, and (iv) the In metal undergoes room-temperature oxidation
42 in the presence of NO_3^- species and H_2 -driven reduction during the NO_3^- reduction reaction.³⁶
43 Through rational control of the materials composition and structure, we showed enhanced
44 catalysis when gold was incorporated⁴⁷ and when cube-shaped Pd nanoparticles were used
45 to support the In metal.³⁷

46 PdIn catalysis can be actualized in several treatment approaches, for example, in a
47 capacitive deionization flow system as a magnetically responsive dispersion,⁴⁸ and in metal
48 catalytic film reactor equipped with hydrogen-permeable hollow fibers.⁴⁹ Problematically, the
49 scarcity and volatile price of the precious metal hinder the implementation of Pd-based
50 catalytic NO_3^- treatment.²²

51 We suggest that Pd metal usage can be dramatically lowered by replacing a fraction of
52 the precious metal Pd with the base metal Ni (another Group 10 element that is a less costly
53 metal) in the form of a PdNi bimetallic composition. Hörold *et al.* (1993) and Soares *et al.*
54 (2008) reported that PdNi exhibited very low activity for NO_3^- reduction, with a very high
55 ammonium selectivity.^{41,50} Besides these works, we are unaware of other reports on this
56 bimetallic composition for NO_3^- (or NO_2^-) reduction. Other PdNi catalyzed reactions have been

57 studied demonstrating enhanced performance for reactions, such as electrocatalytic oxidation,
58 hydrogenation of organic compounds, and carbon-coupling reactions.^{51–58} We hypothesize
59 that PdNi, under proper synthesis conditions and with the addition of In metal as a promoter,
60 would be active for NO₃⁻ reduction.

61 In this work, we synthesized trimetallic catalysts by sequentially depositing Ni, Pd, and
62 In on activated carbon ("InPdNi/AC"). We selected AC as the support material because of its
63 relative inertness, high surface area, stability under both acidic and basic reaction conditions,
64 and the presence of oxygen-rich functional groups which can mitigate severe metal
65 agglomeration.^{30,59,60} We assessed their NO₃⁻ reduction activity in comparison with bimetallic
66 InPd ("InPd/AC") and monometallic catalysts, by comparing the initial reaction rate constants
67 normalized to surface metal content. We examined the origin of the enhanced catalysis
68 through x-ray diffraction (XRD), scanning transmission electron microscopy (STEM), CO
69 chemisorption, and x-ray photoelectron spectroscopy (XPS). In addition, we conducted an
70 estimation of catalyst cost via the CatCost software⁶¹ and quantified the operating cost savings
71 that stem from the higher activity and lower catalyst cost of InPdNi/AC compared to InPd/AC.

72

73 **2. Materials and Methods**

74 **2.1. Materials**

75 Nickel(II) chloride hexahydrate (NiCl₂·6H₂O, >95%), potassium tetrachloropalladate(II)
76 (K₂PdCl₄, >98%), indium(III) chloride tetrahydrate (InCl₃·4H₂O, >97%), potassium nitrate
77 (KNO₃, > 99%) were purchased from Sigma Aldrich. Hydrogen gas (H₂, 99.999%), carbon
78 dioxide gas (CO₂, 99.995%), dinitrogen gas (N₂, 99.999%), argon gas (Ar, 99.999%), diluted
79 hydrogen gas in argon (10%H₂/Ar), and diluted carbon monoxide gas in helium (10%CO/He)
80 were purchased from Airgas. Activated carbon (AC, G-60, ~100 mesh, specific surface area
81 500 – 1000 m²/g) was purchased from Darco. All experiments were conducted using deionized
82 (DI) water (>18.2 MΩcm, Barnstead NANOpure Diamond). Deaerated deionized (DDI) water
83 was prepared by purging N₂ for 15 min. Pd stock solution (5 g-Pd/L) and In stock solution (2
84 g-In/L) were prepared by dissolving 460.1 mg K₂PdCl₄ and 153.2 mg InCl₃·4H₂O, respectively,

85 in 30 mL DI water. Lastly, NO_3^- stock solution (5 g- NO_3^- /L) was prepared by dissolving 244.6
86 mg KNO_3 in 30 mL DI water.

87

88 **2.2. Catalyst Synthesis**

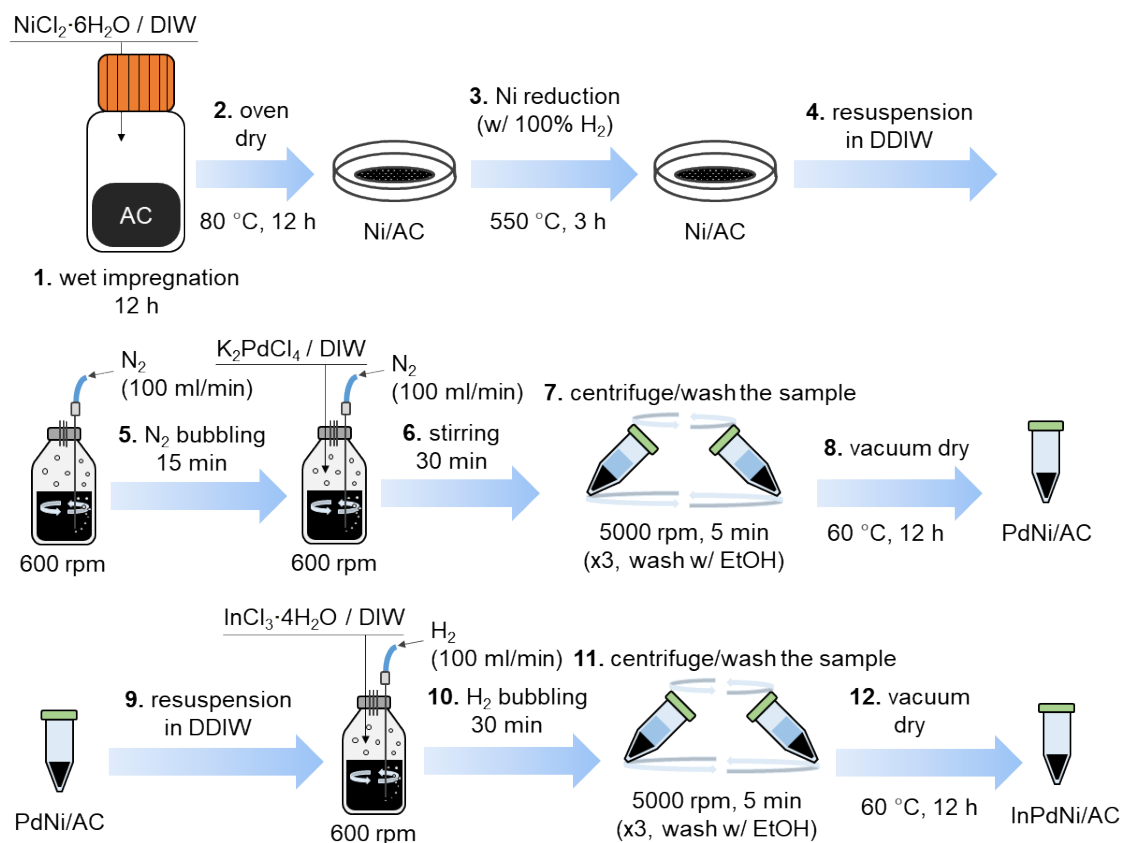
89 **2.2.1. Ni/AC Catalyst**

90 Ni metal supported on AC was prepared via wetness impregnation of AC, with a target Ni
91 loading of 1.0 wt%. 163.63 mg of $\text{NiCl}_2 \cdot 6\text{H}_2\text{O}$ were dissolved in 5 mL of DI water and slowly
92 dripped into an AC suspension (4 g of AC and 15 mL of DI water) and stirred for 12 h at 300
93 rpm. The resulting material was not filtered, but rather, the resulting suspension was oven
94 dried at 80 °C overnight. The dried powder was then heated under H_2 at 550 °C for 3 h (after
95 a ramp rate of 35 °C/min), cooled to room temperature, and purged out the H_2 with Ar gas for
96 15 min before taking out the sample. The final material was termed "Ni1.0/AC".

97

98 **2.2.2. PdNi/AC Catalyst**

99 "PdNi/AC" was prepared via wetness impregnation of Ni1.0/AC, with a target Pd loading of
100 0.3 wt%. 1.0 g of Ni1.0/AC was suspended in 15 mL of DDI water, purged with N_2 at 100
101 mL/min flow for 15 min to deoxygenate, and stirred at 600 rpm in a septum-sealed 40-mL
102 bottle. Then 0.599 mL Pd stock solution was injected, and the mixture was stirred for 30 min
103 under bubbling N_2 (100 mL/min). Afterwards, the solid was separated from the solution through
104 centrifugation and dispersed in ethanol; this washing procedure was carried out a total of three
105 times. Finally, the sample was vacuum-dried in an oven at 60 °C overnight (Scheme 1).



106

107

Scheme 1. Illustration of synthesis steps for InPdNi/AC

108

109 2.2.3. InPdNi/AC Catalyst

110 InPdNi/AC with a target loading of 0.05 wt% In was prepared using PdNi/AC (Scheme 1). The

111 In addition assumes that all the In precursor is fully reduced onto the Pd surface.³⁶ 0.5 g of

112 PdNi/AC was suspended in 15 mL of DDI water, bubbled with H_2 at 100 ml/min flow for 15 min

113 to reduce any oxidized surface Pd, and stirred at 600 rpm. Then 144 μL of In stock solution

114 was injected into the synthesis flask and stirred for another 30 min. Afterwards, the solid was

115 separated, washed, and dried as described in the Section 2.2.2.

116

117 2.2.4. Other Catalyst Compositions

118 Bimetallic InPd metal supported on AC was synthesized for the comparison. First, Pd metal

119 supported on AC was prepared via wetness impregnation of AC, with a target Pd loading of

120 0.3 and 1.3 wt%. 1.581 and 0.361 mL of Pd stock solution was slowly dripped into an AC

121 suspension (0.6 g of AC and 15 mL of DI water) and stirred for 12 h at 300 rpm. The resulting
122 suspension was oven dried at 80 °C overnight. The dried powder was then heated under H₂
123 at 150 °C for 1 h (ramp rate of 15 °C/min), cooled to room temperature, and purged out with
124 Ar gas for 15 min before taking out the sample. The materials were termed "Pd0.3/AC" and
125 "Pd1.3/AC".

126 "InPd0.3/AC" and "InPd1.3/AC" were prepared by adding In stock solution and bubbling
127 H₂, simultaneously, to Pd0.3/AC and Pd1.3/AC. 0.5 g of Pd0.3/AC and Pd1.3/AC catalysts
128 were suspended in 15 mL of DDI water, bubbled with H₂ at 100 ml/min flow for 15 min to
129 reduce any oxidized surface Pd, and stirred at 600 rpm. Subsequently 127 and 125 µL of In
130 stock solution, respectively, was injected to coat In on Pd and stirred for another 30 min.
131 Afterwards, the solid was separated, washed, and dried as described in the Section 2.2.2.

132 Bimetallic InNi supported on AC was prepared with a target In loading of 0.05 wt%. 0.5
133 g of Ni1.0/AC was suspended in 15 mL of DDI water, purged with H₂ at 100 mL/min flow for
134 15 min and stirred at 600 rpm in a septum-sealed 40-mL bottle. Then 125 µL of In stock
135 solution was injected, and the mixture was stirred for 30 min under bubbling H₂ (100 mL/min).
136 Afterwards, the solid was separated, washed, and dried as described in the Section 2.2.2.

137

138 **2.3. Catalyst Characterization**

139 N₂ adsorption isotherms were obtained using an Autosorb-iQ-MP and conducted at the
140 temperature of liquid-N₂ (-196.2 °C). Prior to the measurements, the sample underwent a 12
141 h degassing process under vacuum conditions at approximately 2 mmHg at 200 °C. The
142 surface areas were determined by applying the Brunauer-Emmett-Teller (BET) model.

143 High-angle annular dark-field scanning transmission electron microscopy (HAADF-
144 STEM) imaging and energy dispersive X-ray spectroscopy (EDX) elemental mapping were
145 performed using a Thermo Scientific Titan Themis3 at an acceleration voltage of 300 kV. Prior
146 to use, TEM grids (ultrathin carbon film on lacey carbon supported film with 300-mesh gold,
147 Ted Pella) were vacuum-heated at 150 °C overnight to remove any volatile hydrocarbons. A
148 given catalyst was dispersed in ethanol and sonicated for 5 min, and the ethanol/powder

149 dispersion was droplet-deposited onto the grid. The grid was vacuum heated again at 150 °C
150 overnight to remove the ethanol and hydrocarbons.

151 Bulk metal content of the catalysts was quantified using inductively coupled plasma
152 optical emission spectroscopy (ICP-OES, Perkin Elmer Optima 8300) after aqua regia acid
153 digestion of the materials.

154 XRD patterns were obtained by Rigaku Smartlab II instrument using Cu-K α radiation in
155 step size of 0.1° and speed at 10°/min, in the 2 θ range of 30° to 55°. Crystal phase analysis
156 was performed using the powder XRD analysis software (PDXL2) and mean grain size was
157 obtained with the Scherrer equation.⁶²

158 XPS data was collected by using a PHI Quantera SXM (ULVAC-PHI. Inc) with
159 monochromatic Al K α radiation (1486.7 eV). Samples were heat treated at 150 °C under H₂
160 for 1 h before the measurements of In 3d, Pd 3d, and Ni 2p core levels under UHV conditions.
161 All the binding energy of each core-level electron was calibrated by the respective C 1s peak
162 of graphitic carbon (284.5 eV).⁶³ CasaXPS software was used to fit the spectra and calculate
163 surface metal compositions.

164 CO chemisorption was conducted with Micromeritics AutoChem II 2920. 50 mg of quartz
165 wool was loaded into the U-shape glass tube, followed by loading 70 mg of catalyst. The
166 sample was pretreated by reducing catalysts at 150 °C (10 °C/min ramp rate) under constant
167 flow of 10% H₂/Ar (50 cm³/min) for 1 h and switched the atmosphere to He under constant
168 flow of 50 cm³/min. The sample was then cooled down to 35 °C for CO chemisorption. Multiple
169 pulses of CO (10% in He, 500 μ L) was injected into the glass tube, and the amount of
170 unabsorbed CO was monitored by the thermal conductivity detector (TCD) until a constant
171 peak area was observed. The total amount of adsorbed CO quantified in this manner allows
172 calculations of Pd dispersion.

173 The calculation for In deposited catalysts was done under the assumption that all of the
174 metallic In and In₂O₃ has no effect on the CO chemisorption.⁶⁴ In addition, the calculation for
175 Ni containing catalysts was conducted under the assumption that the exposed Ni surface had
176 no influence on CO chemisorption. This assumption was made due to the relatively low

177 pretreatment temperature (150 °C) which was insufficient for the reduction of surface oxidized
178 Ni that was formed during the synthesis.

179 The exposed Pd (E_{Pd}) and total Pd (T_{Pd}) values were calculated assuming a 1:1 CO:Pd
180 stoichiometry^{65,66} as follows:

$$E_{Pd, \mu\text{mol}/g_{\text{cat}}} = \frac{C_Q}{22414} \times 10^6 \quad \text{Eq. 1}$$

$$T_{Pd, \mu\text{mol}/g_{\text{cat}}} = \frac{CW \times (\text{Pd, wt}\%)}{106.42 \times CW} \times 10^6 \quad \text{Eq. 2}$$

181 where C_Q is the total adsorbed CO ($\text{cm}^3/g_{\text{cat}}\text{-STP}$), 22414 is molar density of CO at STP
182 (cm^3/mol), 10^6 is unit conversion from mol to μmol , CW is catalyst weight (g), Pd,wt% is wt%
183 of Pd of catalyst, and 106.42 is the Pd atomic weight (g/mol).

184 The number of Pd binding site ($\#/g_{\text{cat}}$) was calculated using the exposed Pd (E_{Pd}):

$$\text{Numbers of Pd binding site, } \#/g_{\text{cat}} = E_{Pd} \times 10^{-6} \times N_A \quad \text{Eq. 3}$$

185 where, 10^{-6} is unit conversion from μmol to mol and N_A is Avogadro's number (6.022×10^{23}
186 mol^{-1}).

187

188 **2.4. Catalyst Activity Characterization**

189 Similar to our previous experiments,^{36,67} catalytic reduction of NO_3^- experiments were
190 conducted in a batch system at room temperature (23 °C). All experiments were conducted in
191 a 120-mL screw-cap glass bottle with polytetrafluoroethylene (PTFE) threads and PTFE-
192 silicone septum. All catalysts were heat treated at 150 °C under H_2 for 1 h before testing
193 catalyst activity. Before taking out the catalysts after heat treatment, the samples were
194 passivated under Ar for 15 min to prevent rapid oxidation of carbon. 50 mg of catalyst was
195 added to 49.5 mL DIW and mixed slightly by hand (catalysts loading, $g_{\text{cat}} = 1 \text{ g/L}$). The solution
196 was then simultaneously bubbled with CO_2 and H_2 (both at 100 mL/min) for 15 min to maintain
197 the solution to pH 4-6 and to use it as an electron donor, respectively, and to remove dissolved
198 oxygen and fill the headspace with H_2 and CO_2 prior to introduction of NO_3^- stock solution.
199 Subsequently, 0.5 mL of NO_3^- stock solution was injected into the sealed reactor to initiate the

200 catalytic reduction. The initial concentration of NO_3^- was 11.3 mg-N/L (50 mg- NO_3^- /L).

201 During the reaction, 1.5 mL aliquots were periodically extracted and immediately filtered
202 by 0.22 μm polyethersulfone syringe filter and analyzed the aliquots with ion-chromatography
203 (IC, Thermo Scientific Dionex Aquion IC System; Dionex Ionpac AS23&AG23 for NO_3^- / NO_2^-
204 and CS12A&CG12A for ammonium, NH_4^+) for NO_3^- , NO_2^- , and NH_4^+ . The limits of detection
205 for this method were 0.1 ppm NO_3^- , 0.1 ppm NO_2^- , and 0.1 ppm NH_4^+ .

206 The reaction was carried out under mixing with a Teflon-coated magnetic stir bar at 600
207 rpm. We prepared two sets of each trimetallic InPdNi/AC and bimetallic InPd/AC catalysts and
208 ran the NO_3^- reduction reaction to check reproducibility.

209 The observed initial rate constant (k_{obs} , min^{-1}) was determined by assuming pseudo-first
210 order depending on the NO_3^- concentration within the first 15 min of reaction with the following
211 equation (Figure S1),

$$-\frac{dC_{\text{NO}_3^-}}{dt} = k_{\text{obs}}C_{\text{NO}_3^-} \quad \text{Eq. 4}$$

212 where, $C_{\text{NO}_3^-}$ and t is the concentration of NO_3^- and time, respectively. As NO_3^- reduction is
213 driven by the involvement of both exposed Pd and In, rather than Ni, the initial rate constant
214 was normalized to surface active metal concentration (determined from CO chemisorption
215 measurements of exposed Pd and from the assumption that all deposited In atoms are
216 exposed):

$$k_{\text{cat}} = \frac{k_{\text{obs}}}{[\{g_{\text{cat}}/\text{L} \times (\text{Pd,wt}\%) \times (E_{\text{Pd}}/T_{\text{Pd}})\} + \{g_{\text{cat}}/\text{L} \times (\text{In,wt}\%)\}]} \quad \text{Eq. 5}$$

217 where, Pd,wt% and In,wt% are wt% of Pd and In, respectively, and $E_{\text{Pd}}/T_{\text{Pd}}$ is the fraction of
218 Pd atoms of a catalysts exposed to the surface. The denominator in the above equation (Eq.
219 5) represents the reactor content of surface active Pd and In (units of $g_{\text{surface-Pd+In}}\text{L}^{-1}$).

220 The by-product selectivity to NH_4^+ ($S_{\text{NH}_4^+}$) and NO_2^- ($S_{\text{NO}_2^-}$) were calculated using following
221 equations:

$$S_{\text{NH}_4^+} = \left(\frac{C_{\text{NH}_4^+}}{C_0 - C} \right) \times 100 \quad \text{Eq. 6}$$

$$S_{\text{NO}_2^-} = \left(\frac{C_{\text{NO}_2^-}}{C_0 - C} \right) \times 100 \quad \text{Eq. 7}$$

222 where, C_0 , C , $C_{\text{NH}_4^+}$, and $C_{\text{NO}_2^-}$ are initial NO_3^- molar concentration, NO_3^- molar concentration at
223 time t , NH_4^+ molar concentration at time t , and NO_2^- concentration at time t , respectively. As
224 previous reports show only a trace amount of NO and N_2O is formed as an intermediate
225 product, NO_2^- and NH_4^+ are the major reaction products from PdIn catalysts.^{44,68} Therefore, we
226 only considered NO_2^- and NH_4^+ for the selectivity.

227

228 **2.5. DFT Computational Method**

229 Periodic boundary condition DFT calculations were carried out as implemented in the Vienna
230 ab-initio Simulation Package (VASP),⁶⁹ using the Perdew-Burke-Ernzerhof (PBE) functional in
231 the framework of the Generalized Gradient Approximation (GGA).⁷⁰ Projector-augmented
232 wave pseudopotentials explicitly include the Ni 3d and 4s, Pd 4d, and In 5s and 5p electrons.⁷¹
233 The wavefunction was constructed from a summation of planewaves with energies up to 400
234 eV. There was less than a 0.01 eV difference in structure energies calculated at 500 eV as
235 opposed to 400 eV, with no change in the attributed charge per atom.

236 The PdNi structure of PdNi/AC catalyst was chosen as a model to demonstrate the
237 electron transfer effect. It was represented as a (111)-terminated slab model of Ni consisting
238 of $7 \times 7 \times 4$ Ni atoms, which was chosen as it is the lowest-energy surface termination.⁷² The
239 bottom two layers of Ni were considered fixed to their equilibrium lattice positions. Upon the
240 Ni slab were placed two layers of Pd atoms in a triangular pyramidal shape, to represent the
241 Pd island. The Brillouin zone was sampled with a $4 \times 4 \times 1$ Γ -centered Monkhorst-Pack k-point
242 mesh,⁷³ as there was less than 0.01 eV difference in structure energy when calculated with a
243 $5 \times 5 \times 1$ mesh. At least 18 Å of vacuum space was included in the direction perpendicular to the
244 slab surface to minimize spurious self-interactions between the slab and its own periodic
245 image. Additionally, dipole corrections to the slab were included in the Z-direction, in
246 accordance with the method of Neugebauer *et al.*⁷⁴ Dispersion corrections were not included.
247 Structure geometries were considered converged when forces on all the atoms were less than

248 0.01 eV/Å, and SCF convergence was reached when the energy changed by less than 1×10^{-5}
249 eV. Total electronic charge on each atom was accounted for by the Bader charge method,
250 as implemented by Tang *et al.*⁷⁵

251 **2.6. Cost Estimation of Catalysts**

252 Instead of using only gram-scale metal prices, we estimated the catalyst cost that uses metal
253 prices (from August 2024) extrapolated to kilogram amounts and the various costs associated
254 with catalyst manufacture. We used a cost estimation software called CatCost™, for pre-
255 commercial catalysts,⁷⁶ to consider a hypothetical purchase order of 907 kg (1 US ton) used
256 in a continuously-stirred tank reactor (CSTR). This software provides a methodology to
257 calculate cost based on standard manufacturing techniques scaled up from the synthesis
258 procedures described for InPdNi/AC (Section 2.2.1-3), and for InPd1.3/AC (Section 2.2.4).
259 Detailed information and calculations are provided in the Supporting Information S1.

260

261 **3. Results and Discussion**

262 **3.1. Catalyst Compositions**

263 We first determined the metal content of all synthesized catalysts via the ICP-OES elemental
264 analysis (Table 1). Nearly all catalysts reached the target metal loadings within 10% error.

265

266 Table 1. Target and ICP-OES-measured metal catalyst compositions

Catalysts	Metal	Target (wt%)	Measured (wt%)	Atomic ratio In : Pd (at%)
InPd0.1Ni1.0/AC	In	0.05	0.052	38 : 62
	Pd	0.3	0.094	
	Ni	1.0	0.99	
InPd1.3/AC	In	0.05	0.044	3 : 97
	Pd	1.3	1.3	
InPd0.3/AC	In	0.05	0.045	12 : 88
	Pd	0.3	0.3	
InNi1.0/AC	In	0.05	0.051	
	Ni	1.0	0.98	
Pd0.1Ni1.0/AC	Pd	0.3	0.094	
	Ni	1.0	0.99	

Pd1.3/AC	Pd	1.3	1.3
Pd0.3/AC	Pd	0.3	0.3
Ni1.0/AC	Ni	1.0	1.0

267

268 The Pd content of the PdNi/AC and InPdNi/AC catalysts did not match the targeted wt%
 269 loading, with measured Pd loadings that were 3× lower than the targeted loadings. We
 270 repeated the PdNi/AC synthesis two more times and found the measured Pd loading to be
 271 consistent and to be 3× lower than the target Pd loading. The measured Pd loading for
 272 PdNi/AC is 0.094 (± 0.0006) wt%. We attribute this lower-than-expected Pd content to weak
 273 interaction between PdCl₄⁻ species and the Ni surface during the synthesis procedure
 274 (Scheme 1), leading to detachment and loss of PdCl₄⁻ species from Ni surface during the
 275 repeated washing process.

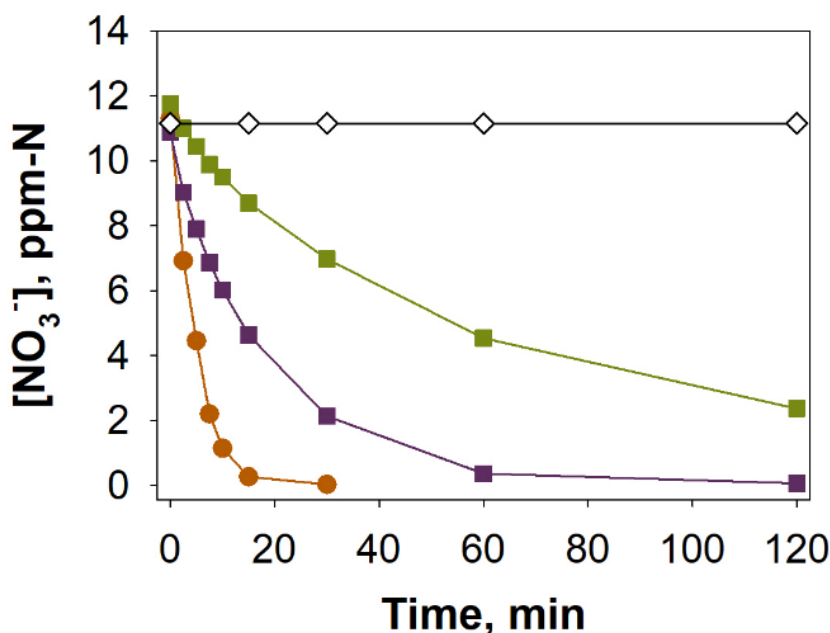
276 The measured Pd loading for the trimetallic InPdNi/AC catalyst showed similar Pd
 277 composition (0.093 wt%) to PdNi/AC catalyst, indicating the In deposition step did not change
 278 the Pd and Ni composition. For the sake of clarity, we use "Pd0.1Ni1.0/AC" and
 279 "InPd0.1Ni1.0/AC" terms to refer to these catalyst materials henceforth.

280

281 3.2. Catalytic Nitrate Reduction Behavior

282 Catalytic nitrate reduction occurred for materials containing both Pd and In (Figure 1), as
 283 expected.^{36,37} Whereas the two bimetallic InPd compositions converted >96% of NO₃⁻ within
 284 60 min (InPd1.3/AC) and >79% of NO₃⁻ within 120 min (InPd0.3/AC), trimetallic
 285 InPd0.1Ni1.0/AC was even more active.

286



287
 288 Figure 1. Concentration-time profiles of NO₃⁻ for InPd0.1Ni1.0/AC (●), InPd1.3/AC (■),
 289 InPd0.3/AC (■), and InNi1.0/AC (◇). Reaction conditions: 600 rpm stirring rate, 1 atm pressure
 290 (50/50 H₂/CO₂), pH ~ 4-6, temperature = 23 °C, catalyst charge = 1.0 g_{cat}/L (reactor content of
 291 surface active Pd and In = 0.7, 2.8, and 0.9 mg_{surface-PdIn}/L, respectively).

292
 293 Its initial rate constant (k_{obs}) was ~4 and ~13 times larger than those for InPd1.3/AC and
 294 InPd0.3/AC, respectively. It converted >98% of NO₃⁻ within 15 min, even though the material
 295 contained less Pd (0.094 wt%, Table 1) and the reactor contained less total Pd (Table 2). To
 296 compare catalytic activity further, we calculated reaction rate constants normalized to the
 297 combined mass of Pd and In accessible to the reaction, as both metals participate in the nitrate
 298 reduction reaction. The fraction of Pd atoms of a catalysts exposed to the surface (E_{Pd}/T_{Pd})
 299 was determined via CO chemisorption analysis and all In atoms were assumed to be exposed
 300 (the details of which are provided in Supporting Information S2 and Table S5).

301 The surface site normalized rate constant (k_{cat}) of InPd0.1Ni1.0/AC was higher than
 302 those of InPd1.3/AC and InPd0.3/AC, by ~18 and ~16 times, respectively. The catalytic
 303 reactions were carried twice; the concentration-time profiles confirmed data consistency.
 304 (Figure S4). Furthermore, InPd0.1Ni1.0/AC was compared to the previously reported InPd
 305 catalysts. The k_{cat} for InPd0.1Ni1.0/AC (349 Lmin⁻¹g_{surface metal}⁻¹) was 46 times higher than that

306 of 40 sc% In-on-Pd NPs ($7.6 \text{ Lmin}^{-1}\text{g}_{\text{surface metal}}^{-1}$), as reported by Guo et al. (2018).³⁶
 307 Additionally, with respect to the initial rate constant normalized to the total Pd and In,
 308 InPd0.1Ni1.0/AC ($169 \text{ Lmin}^{-1}\text{g}_{\text{total Pd+In}}^{-1}$) was ~24 times higher than In-on-Pd₈₀Au₂₀ NPs (7
 309 $\text{Lmin}^{-1}\text{g}_{\text{total Pd+In}}^{-1}$), as reported by Guo et al. (2022).⁴⁷

310

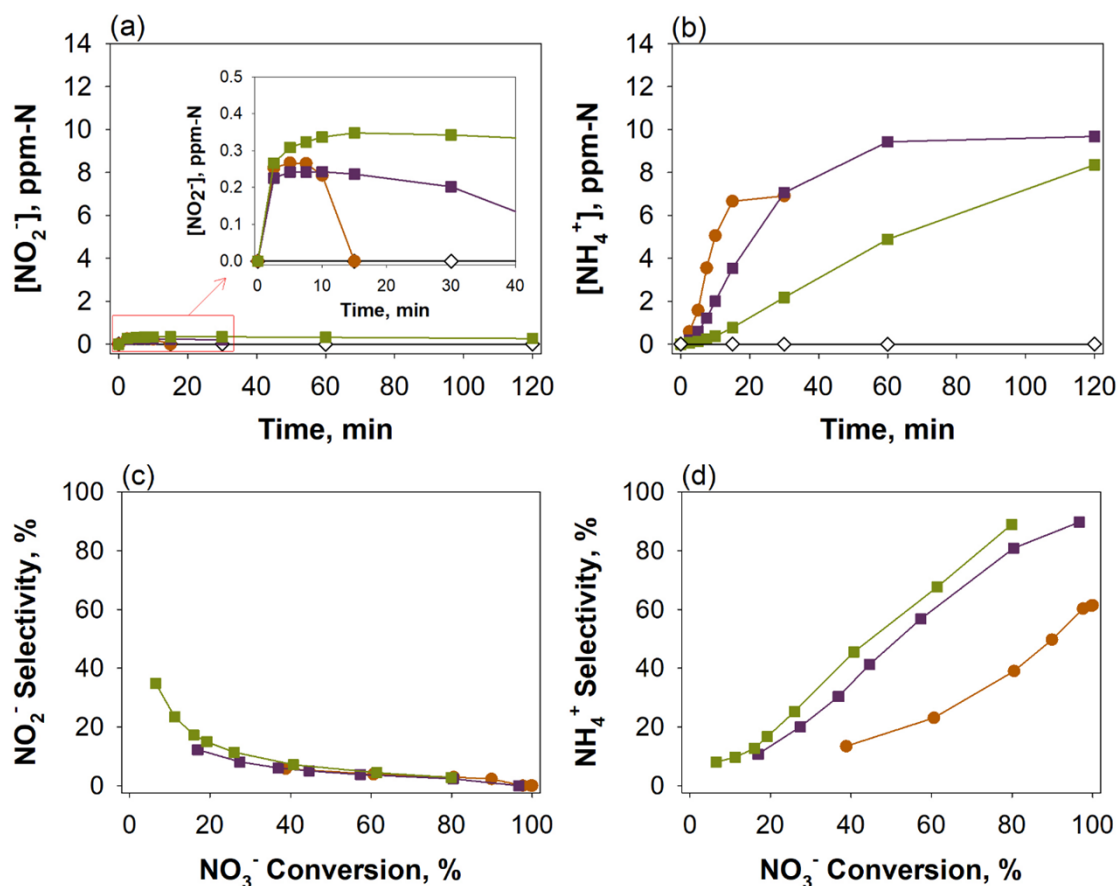
311 Table 2. Comparison of catalytic nitrate reduction rate constants and metal content of reactor

Samples	k_{obs} (10^{-2} min^{-1})	k_{cat} ($\text{Lmin}^{-1}\text{g}_{\text{surface metal}}^{-1}$)	Reactor Content of Surface Active Pd and In ($\text{mg}_{\text{surface-Pd+In}}\text{L}^{-1}$)
InPd0.1Ni1.0/AC	24.7	349	0.7
InPd1.3/AC	5.6	19.9	2.8
InPd0.3/AC	1.9	22	0.9
InNi1.0/AC	0	0	Not applicable
Pd0.1Ni1.0/AC	0	0	Not applicable
Pd0.3/AC	0	0	Not applicable
Pd1.3/AC	0	0	Not applicable
Ni1.0/AC	0	0	Not applicable

312

313 The active catalysts generated both NO_2^- and NH_4^+ as reaction products (Figure 2). The
 314 amount of generated NO_2^- increased rapidly in the first few minutes and then decreased
 315 gradually over time (Figure 2a, inset).^{29,36} NO_2^- selectivity decreased with NO_3^- conversion, as
 316 the NO_2^- anions underwent reduction on the exposed Pd sites (Figure 2c).

317



318
 319 Figure 2. Concentration-time profiles of (a) NO₂⁻ and (b) NH₄⁺ and (c,d) corresponding
 320 selectivity-conversion plots for InPd0.1Ni1.0/AC (●), InPd1.3/AC (■), InPd0.3/AC (■), and
 321 InNi1.0/AC (◇). Reaction conditions: 600 rpm stirring rate, 1 atm pressure (50/50 H₂/CO₂), pH
 322 ~ 4-6, temperature = 23 °C, catalyst charge = 1.0 g_{cat}/L.

323
 324 NH₄⁺ concentrations increased continuously with reaction time for the active catalysts
 325 (Figure 2b). At 50% conversion, NH₄⁺ selectivity for InPd0.1Ni1.0/AC (18%) was 2.6× and 3×
 326 lower than those for InPd1.3/AC (48%) and InPd0.3/AC (55%) (Figure 2d). However,
 327 compared to the previously reported NH₄⁺ selectivities for 40 sc% In-on-Pd NPs (<1.5%) and
 328 In-on-Pd₈₀Au₂₀ NPs (<5%),^{36,47} the NH₄⁺ selectivity for InPd0.1Ni1.0/AC is relatively high.
 329 Drinking water applications favor as low ammonium by-product as possible, and production of
 330 N₂ is preferred. We note these NH₄⁺ selectivity values are higher compared to the unsupported
 331 In-on-Pd NPs from our previous work (~5%),³⁶ which we attribute to catalyst support effects.
 332 OH⁻ anions form as NO₃⁻ and NO₂⁻ anions reduce on the metal surface, but their diffusion into
 333 the bulk solution is constrained by the small AC pores, leading to localized higher pH within

334 the pores.^{77,78} As reported in literature, high pH values favor the formation of NH_4^+ over N_2 .⁷⁹⁻
335 ⁸¹ Thus, our use of AC likely resulted in the buildup of basicity within its pores during the
336 catalytic reaction, generating more NH_4^+ compared to catalysts on larger-pore supports (*e.g.*,
337 porous alumina oxides) and other unsupported catalysts.^{77,78,82,83}

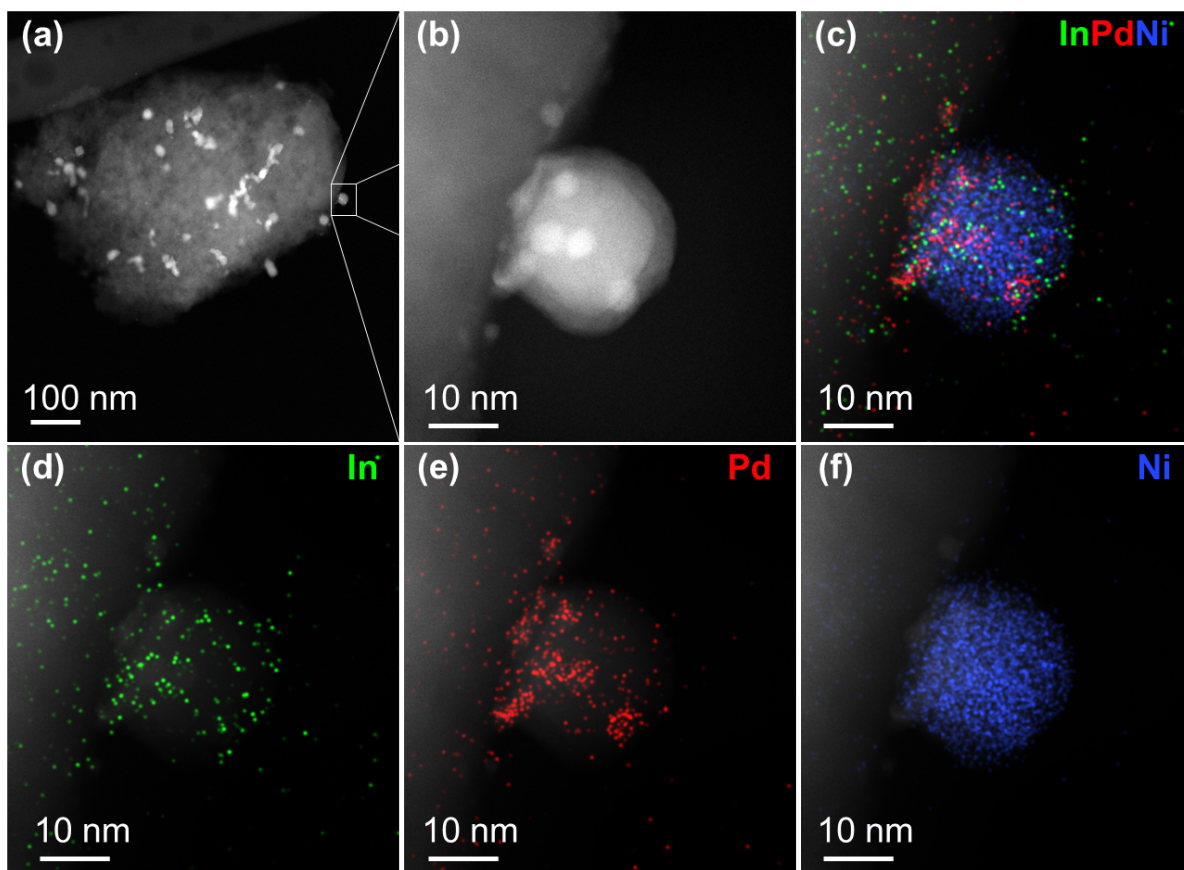
338

339 **3.3. Metal Structure of the Trimetallic Catalyst**

340 To elucidate the origin of the enhanced NO_3^- reduction performance of $\text{InPd}_{0.1}\text{Ni}_{1.0}/\text{AC}$, we
341 examined the metal distribution of $\text{InPd}_{0.1}\text{Ni}_{1.0}/\text{AC}$ via HAADF-STEM (Figure 3). Ni particles
342 are located on the AC surface, which are ~16 nm in size, similar to the XRD-derived grain size
343 (Table S6). Pd domains were found primarily on the Ni particle surface, and were ~3-5 nm in
344 size; Pd was not detected through XRD (Figure S5), due to the low Pd content and too-small-
345 to-detect grains.

346

347



348

349 Figure 3. (a) A representative HAADF-STEM, (b) a higher-magnification, and (c) a composite
 350 elemental map image of the trimetallic InPd_{0.1}Ni_{1.0}/AC. (d-f) Energy-dispersive x-ray
 351 spectroscopy (EDX) individual maps of (d) In, (e) Pd, and (f) Ni elements.

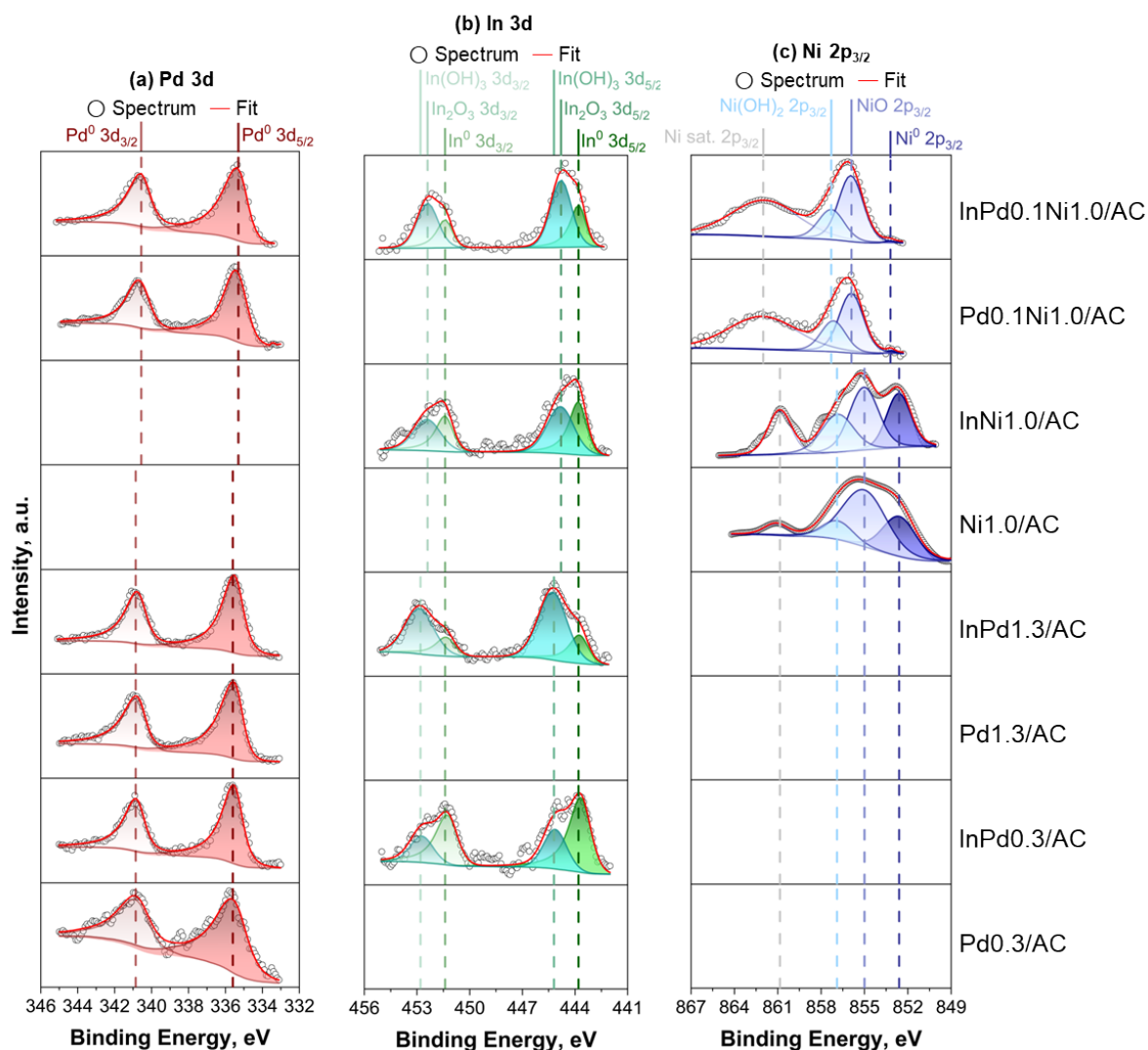
352 In atoms are located mostly near the Pd atoms. Knowing that the number of Pd binding
 353 sites is lower after In deposition on Pd_{0.1}Ni_{1.0}/AC and the number of Pd binding site covered
 354 by In is similar across the In-containing catalysts (Table S5), we conclude that In atoms are
 355 situated on top of Pd, and that InPd_{0.1}Ni_{1.0}/AC essentially has an "In-on-Pd-on-Ni" metal
 356 arrangement.

357 XPS analysis of the trimetallic and bimetallic compositions provided information about
 358 Pd, In, and Ni oxidation states within the x-ray penetration depth (<10 nm) of the material
 359 (Figure 4). For Pd 3d core level (Figure 4a), an asymmetric Pd⁰ 3d_{5/2} peak at 335.3 eV
 360 (InPd_{0.1}Ni_{1.0}/AC and Pd_{0.1}Ni_{1.0}/AC) or 335.5 eV (InPd_{1.3}/AC, Pd_{1.3}/AC, InPd_{0.3}/AC, and
 361 Pd_{0.3}/AC) was coupled with the respective Pd⁰ 3d_{3/2} peak (located 5.3 eV higher due to the
 362 spin-orbital splitting).^{84,85}

363 For the In 3d peak observed in the catalysts (Figure 4b), both the asymmetric metallic
364 In^0 and symmetric oxidized In^{3+} were observed: In^0 $3d_{5/2}$ (In^{3+} $3d_{5/2}$) peak at 443.8 eV (444.7
365 eV, In_2O_3) for $\text{InPd}0.1\text{Ni}1.0/\text{AC}$; 443.8 eV (445.2 eV, $\text{In}(\text{OH})_3$) for $\text{InPd}1.3/\text{AC}$; and 443.7 eV
366 (445.1 eV, $\text{In}(\text{OH})_3$) for $\text{InPd}0.3/\text{AC}$, coupled with their respective In $3d_{3/2}$ peaks located 7.6
367 eV higher.^{86,87} As expected, oxidized In was observed for both the trimetallic and bimetallic
368 compositions, which is due to the facile oxidation of In when exposed to air.⁸⁸

369 $\text{Ni}1.0/\text{AC}$ and $\text{InNi}1.0/\text{AC}$ showed corresponding peaks of Ni^0 , NiO , and $\text{Ni}(\text{OH})_2$ at 852.6,
370 855.0, and 856.9 eV, respectively, while bimetallic $\text{Pd}0.1\text{Ni}1.0/\text{AC}$ and trimetallic
371 $\text{InPd}0.1\text{Ni}1.0/\text{AC}$ showed peaks at 853.2, 855.9, and 857.3 eV, respectively.⁸⁹

372



373
 374 Figure 4. XPS spectra at the (a) Pd 3d, (b) In 3d, and (c) Ni 2p_{3/2} core levels of trimetallic,
 375 bimetallic, and monometallic compositions.

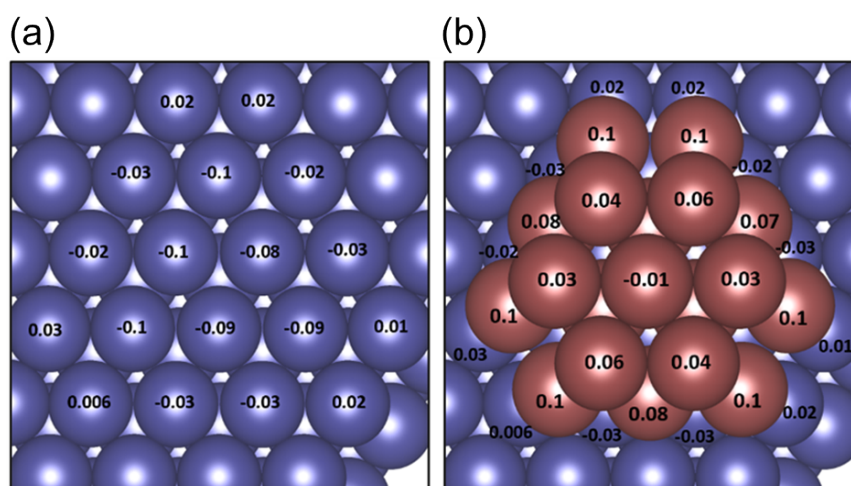
376
 377 With the bimetallic catalysts (InPd0.3/AC and InPd1.3/AC), we observed no difference
 378 in the Pd 3d binding energies nor in the In 3d binding energies, both matching well with those
 379 reported for Pd 3d and In 3d. This indicates insufficient electronic interaction between In and
 380 Pd at their interface to alter their binding energies.

381 However, the Pd⁰ 3d_{5/2} binding energy of the trimetallic InPd0.1Ni1.0/AC (335.3 eV)
 382 shifted to a lower binding energy (by 0.2 eV) compared to the InPd and Pd catalysts. The Ni
 383 in trimetallic catalyst showed a positive shift of 0.6 eV compared to the monometallic Ni1.0/AC,

384 while no peak shift is observed for In; the same can be observed in Pd_{0.1}Ni_{1.0}/AC catalyst.
385 The observed peak shift in both Pd and Ni indicates that Pd has a higher electron density and
386 Ni has a lower electron density. Overall, the electron transfer (from Ni to Pd) leads to a change
387 in the surface electronic structure of both metals, driven by their electronegativity difference.⁵⁴

388 To corroborate the Pd-Ni metal electronic interactions, DFT calculations were performed.
389 Figure 5 shows the difference in electron density Δe ($|e^-|$) of the bimetallic catalyst at the
390 junction between Ni and Pd atoms. The Ni atoms at the center of the junction (Figure 5a) were
391 depleted of roughly 0.1 electrons per atom, while the Ni atoms around the base of the Pd
392 island had smaller (~ 0.02 electrons) charge deviations. The bottom layer of Pd atoms (Figure
393 S7) localized much of the transferred charge, particularly around the perimeter of the island,
394 where the charge surplus was ~ 0.1 electrons per atom. The three Pd atoms at the center of
395 the base layer (Figure S7), as well as the Pd atoms comprising the top layer of the island
396 (Figure 5b), localized a smaller portion of the charge transferred, roughly ~ 0.02 - 0.05 electrons
397 per atom. DFT results show electron donation from the Ni atoms to the Pd atoms (as
398 evidenced by the mean Δe values).

399



400

401 Figure 5. Δe values ($|e^-|$) of Pd or In atoms according to Bader charge analysis of PdNi
402 structure modeled as a Ni slab (blue-colored atoms) supporting a three-dimensional ensemble
403 of Pd atoms (red-colored atoms) shown in (b) and not in (a). Blue: Ni atoms, Red: Pd atoms).

404

405 **3.4. Mechanistic Explanation of Enhanced Nitrate Reduction for the Trimetallic Catalyst**

406 The widely accepted mechanism governing NO_3^- reduction by InPd catalysts involves two
407 distinct active sites, In and Pd. The step that limits the reaction rate is facilitated by metallic
408 In, which adsorbs NO_3^- ($\text{NO}_{3(\text{ads})}^-$) and reduces it to NO_2^- ($\text{NO}_{2(\text{ads})}^-$). Then the Pd sites play a
409 dual role in the subsequent process: first, they reduce $\text{NO}_{2(\text{ads})}^-$ to eventually form N_2 and/or
410 NH_4^+ ; and second, they generate hydrogen adatoms from H_2 necessary to reduce the oxidized
411 In, regenerating the metallic In.³⁸

412 We propose a similar mechanism for the trimetallic catalyst, in which the Ni itself does
413 not participate in any of these surface reaction steps but it affects the reaction through the
414 earlier-discussed electronic effects. The initial step involves the reduction of $\text{NO}_{3(\text{ads})}^-$ on In
415 sites to form $\text{NO}_{2(\text{ads})}^-$, followed by the migration of $\text{NO}_{2(\text{ads})}^-$ to a Pd site or its desorption from
416 the In site into the bulk solution ($\text{NO}_{2(\text{aq})}^-$). When the $\text{NO}_{2(\text{ads})}^-$ on Pd site remains isolated from
417 other N-species (intermediate daughter species of NO_2^- , such as $\text{NO}_{(\text{ads})}$ and $\text{N}_{(\text{ads})}$, or $\text{NO}_{2(\text{aq})}^-$), the favored outcome is the formation of NH_4^+ . However, if additional surface N-species
418 are present at neighboring Pd sites, N_2 formation favors via the coupling amongst N-species
419 and/or the reaction of $\text{NO}_{(\text{ads})}$ with $\text{NO}_{2(\text{aq})}^-$ in an Eley-Rideal-like mechanism.^{68,90,91}

421 Rapid reduction of NO_3^- to NO_2^- can be correlated to the electron transfer from Ni to Pd,
422 similar to mechanisms proposed for other hydrogenation reactions.^{54,92} We suggest the
423 electron-rich Pd atoms (adjacent to Ni atoms) promotes the reduction of NO_3^- and the
424 regeneration of oxidized In, accelerating the reduction kinetics of NO_3^- . Likewise, NO_2^-
425 undergoes rapid reduction on the Pd sites (Figure S6), aligning with the understanding that
426 electron rich Pd enhances the NO_2^- reduction reaction.⁹³ The enhanced reduction of NO_3^- to
427 NO_2^- on In surface and NO_2^- to NO on Pd surface results in a higher surface coverage of N-
428 species on Pd, thereby promoting the possibility of coupling of N-species that leads to the
429 formation of more N_2 . This notion is consistent with the observed lower ammonium selectivity
430 for InPd0.1Ni1.0/AC (18% at 50% nitrate conversion), compared to those for the bimetallics
431 (48% and 55%, Section 3.2).

432

433 **3.5. Catalyst Cost Estimation Based on Precursors and Large-Scale Manufacturing**

434 The simplest and most common method to estimate catalyst cost is to perform a weighted
435 average (using the percentile composition) of each component multiplied by the spot price of
436 the metals and support (Table S1). This approach projects the cost of InPd1.3/AC and
437 InPd0.1Ni1.0/AC to be \$391/kg and \$30/kg, respectively (Table S2). The trimetallic cost is
438 >12× lower, but these values do not reflect manufacturing costs and do not use metal
439 precursor cost.

440 The CatCost estimation software offers a solution for approximating the expenses
441 associated with producing catalysts in the pre-commercial stage. It leverages well-accepted
442 methods and industry-standard resources to give useful insights throughout the various
443 phases of catalyst research and development (Scheme S1),⁶¹ accounting for the extrapolated
444 cost of precursor salts, materials, and processing steps. This approach projects “catalyst
445 purchase cost” for InPd1.3/AC and InPd0.1Ni1.0/AC to be \$1388 and \$190 per kg of catalyst,
446 respectively (Table S3). This more realistic estimation indicates the trimetallic catalyst
447 purchase cost is 86% lower than that of the bimetallic catalyst.

448 An improved comparison of catalyst purchase cost should also consider the value of the
449 catalyst at the *end* of its useful life. In this regard, the CatCost estimation software further
450 evaluates the “spent catalyst value” by assessing three distinct options for spent catalyst: i)
451 metals recovery, ii) sale, and iii) landfill. The software evaluates the value of each option and
452 automatically chooses the most appropriate one. For both catalysts, the most favorable option
453 was metals recovery since the recoverable Pd value (\$26.45/kg for trimetallic and \$368.43/kg
454 for bimetallic catalyst) is much higher than the other two options (Figure S12a and S13a).
455 Considering expenses for the total recovery fees related to the metal recovery (\$6.85/kg for
456 the trimetallic and \$12.07/kg for the bimetallic), the spent catalyst value for InPd0.1Ni1.0/AC
457 catalysts (\$19.6/kg) was ~18× lower compared to InPd1.3/AC (\$356.35/kg). Overall, the “net
458 catalyst cost” for InPd1.3/AC and InPd0.1Ni1.0/AC was calculated respectively as \$1028 and
459 \$170 per kg of catalyst (83% less).

460

461 **3.6. Hypothetical Catalytic Reactor Performance Comparison**

462 To illustrate the benefits of the improved nitrate reduction catalyst in a different manner, we
463 estimated the treatment effectiveness of the two catalysts used in a CSTR (e.g., a Berty-type
464 configuration in which the catalyst material does not exit the effluent). We considered the
465 simple scenario in which the CSTR (charged with either catalyst at 1 kg per 1000 L reactor
466 volume) treats an influent nitrate concentration of 50 mg-N/L, such that the effluent
467 concentration is 10 mg-N/L. To reach this 80% nitrate conversion, the required hydraulic
468 residence time (τ) is ~16 and ~71 min, respectively, for InPd0.1Ni1.0/AC and InPd1.3/AC. The
469 trimetallic catalyst-containing CSTR is thus ~4.4× effective, *i.e.*, 4.4× more water can be
470 treated (Supporting Information S1.1). If the less effective bimetallic catalyst is substituted into
471 the trimetallic catalyst-containing CSTR (operating at $\tau = \sim 16$ min), the resulting reactor would
472 not reach 80% nitrate conversion (~48%) and would not satisfy the 10 mg-N/L effluent target
473 concentration (~26 mg-N/L). These calculations indicate a substantial gain in nitrate treatment
474 performance resulting from the incorporation of Ni into the InPd catalyst.

475 The trimetallic catalyst (\$170/kg) costs six times less the bimetallic (\$1028/kg), and so
476 we contend that it is ~26 times less expensive to use the trimetallic for the same treatment
477 capacity. Further work is needed to design a Pd-based catalytic destruction treatment system
478 and to evaluate its commercial viability against current available technologies through
479 techno-economic analysis. We expect that water matrix effects will lower catalyst activity but it
480 is not yet known to what extent. Catalytic materials stability considerations require quantitative
481 assessment of any potential leaching that may lead to metal loss, catalyst attrition, and long-
482 term treatment performance degradation. And, the trimetallic catalyst would require further
483 improvement with regard to nitrate reduction selectivity; ideally, ammonium should not be
484 formed.

485

486

487 **4. Conclusion**

488 We designed and synthesized a trimetallic catalyst active for nitrate reduction. Showcasing
489 the benefits of the incorporated Ni metal, catalytic activity and N₂ selectivity of the trimetallic
490 composition were significantly greater compared to bimetallic InPd. HAADF-STEM analysis
491 showed the In-on-Pd-on-Ni metal nanostructure supported on activated carbon, which
492 reflected the sequential nature of the synthesis procedure. XPS and DFT calculations revealed
493 electron transfer from Ni to Pd, rendering Pd electronically rich and more catalytically active.
494 Metal precursor cost, manufacturing cost at the multi-kg scale, and spent metal recovery value
495 are more appropriate parameters than metal spot prices for realistic catalyst cost estimation.
496 Ni incorporation lowered the net catalyst cost by 83% according to a CatCost analysis, such
497 that the trimetallic composition was six times less expensive than the bimetallic composition.
498 Using a simple continuously-stirred tank reactor model, we estimated the trimetallic catalyst
499 improves treatment effectiveness by >4 times and lowers the catalyst cost by 26 times to
500 achieve the same treatment capacity as for the bimetallic catalyst. This study demonstrates
501 and explains the catalytic performance improvements of Ni incorporation into the InPd nitrate
502 reduction catalyst, which should be advantageous for other clean-water reactions.

503

504 **5. Associated Content**

505 **Supporting Information**

506 Detailed cost estimation of catalysts; CO chemisorption, BET surface area, XRD, and XPS
507 analysis; bulk-scale cost extrapolation; duplicated reaction results; NO₂⁻ reaction result; Bader
508 charge analysis of PdNi; Step method synthesis process of catalysts; and CatCost estimation
509 results

510

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521

522 **7. Author Contributions**

523 **Kiheon Hong** Investigation leader, conceptualization, data curation, formal analysis, writing –
524 original draft; **Daniel J. Rivera** investigation, visualization, writing – review & editing; **Juan A.**
525 **Donoso** investigation, visualization, writing – review & editing; **Bongki Shin** investigation,
526 visualization; **Hunter P. Jacobs** review & editing; **Byeong Jun Cha** review & editing;
527 **Kimberly N. Heck** review & editing; **Welman C. Elias** review & editing; **Paul Westerhoff**
528 project administration, review & editing; **Yimo Han** resources, review & editing; **Christopher**
529 **L. Muhich** resources, review & editing; **Michael S. Wong** conceptualization, funding
530 acquisition, supervision, project administration, writing – review & editing

531

532 **8. Notes**

533 The authors declare no competing financial interest.

534

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541

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