

UCM/MMP cookoff models for explosives containing RDX

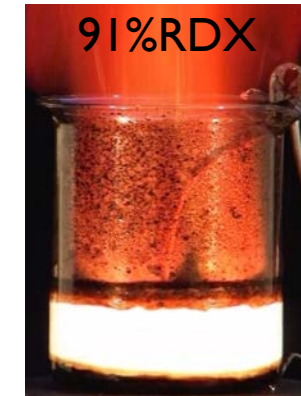
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June 18-June 20, 2023 John McIntyre Convention Center, The University of Edinburgh, Scotland



Comp-B3



Comp-C4



Semtex 1H



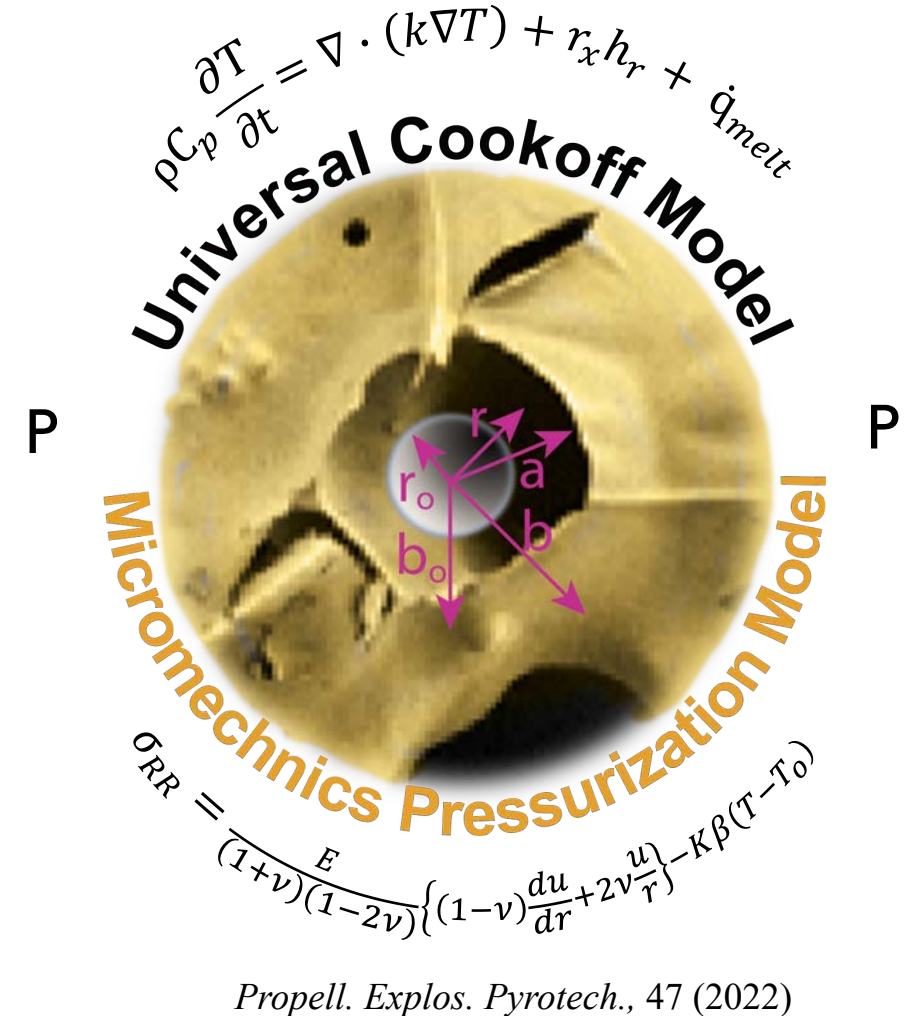
Audrie L. Aragon

Introduction

(avoid high temperatures and confinement)



Name	Comp. (wt.%), formula	Mw _x g/mol	O ₂ bal.	ρ _{co} , kg/m ³	h _f kJ/mol	D ^b km/s	T _a K
Comp-B3	RDX/TNT (60/40) C _{4.58} H _{5.6} N _{4.82} O ₆	224.2	-42.6	1742	16.9	7.81	2651
Comp-C4	RDX/DOA/PIB/Oil 91/5.3/2.1/1.6 C _{3.83} H _{7.5} N _{5.2} O _{5.23}	211.5	-46.1	1659	16.8	7.90	2471
PBX 9407	RDX/VCTFE (94/6) C _{3.1} H _{5.9} N _{5.6} O _{5.6} Cl _{0.18} F _{0.18}	221.8	-24.2	1799	18.4	8.37	2880
PBXN-109	RDX/AL/HTPB/DOA 64/20/8/8 C _{1.61} H _{2.94} N _{1.44} O _{1.51} AL _{0.62}	83.4	-78.7	1656	-4.7	7.24 ^c	2033
RDX	RDX (100) C ₃ H ₆ N ₆ O ₆	222.1	-21.6	1806	69	8.78	2930
Semtex 1H	RDX/PETN/Binder/Plastici. 65.5(max)/25(min)/2.5/11.6 or 43/43/2.5/11.5 C _{4.8} H _{8.86} N _{3.8} O _{6.51}	224.0	-53.7	1581	-226	7.45	2164
XTX-8004	RDX/Sylgard™ 182 (80/20) C _{2.57} H ₆ N _{3.44} O _{3.86} Si _{0.43}	158.9	-51.8	1579	-176	7.72	2260



Single mechanism for 7 explosives



Product Hierarchy

(equilibrium at 400 K and 1 bar)

Comp-B3	$C_{4.58}H_{5.6}N_{4.82}O_6 \rightarrow 2.54 H_2O + 2.41 N_2 + 1.73 CO_2 + 0.13 CH_4 + 2.72 C$ Comp-B3 $\rightarrow$ 6.81 Gas + 2.72 C
Comp-C4	$C_{3.83}H_{7.5}N_{5.2}O_{5.23} \rightarrow 3.14 H_2O + 2.60 N_2 + 1.09 CO_2 + 0.3 CH_4 + 0.01 H_2 + 2.43 C$ Comp-C4 $\rightarrow$ 7.14 Gas + 2.44 C
PBX 9407	$C_{3.1}H_{5.9}N_{5.6}O_{5.6}Cl_{0.18}F_{0.18} \rightarrow 2.51 H_2O + 2.82 N_2 + 1.57 CO_2 + 0.18 HCL + 0.18 HF + 0.13 CH_4 + 1.40 C$ PBX 9407 $\rightarrow$ 7.37 Gas + 1.40 C
PBXN-109	$C_{1.61}H_{2.94}N_{1.44}O_{1.51}Al_{0.62} \rightarrow 1.08 H_2O + 0.72 N_2 + 0.215 CO_2 + 0.195 CH_4 + 0.62 AL + 1.2 C$ PBXN-109 $\rightarrow$ 2.21 Gas + 0.62 AL + 1.20 C
RDX	$C_3H_6N_6O_6 \rightarrow 2.7 H_2O + 3 N_2 + 1.65 CO_2 + 0.15 CH_4 + 1.2 C$ RDX $\rightarrow$ 7.5 Gas + 1.2 C
Semtex 1H	$C_{4.8}H_{8.86}N_{3.8}O_{6.51} \rightarrow 3.75 H_2O + 1.9 N_2 + 1.38 CO_2 + 0.34 CH_4 + 3.08 C$ Semtex 1H $\rightarrow$ 7.37 Gas + 3.08 C
XTX-8004	$C_{2.57}H_6N_{3.44}O_{3.86}Si_{0.43} \rightarrow 2.0 H_2O + 1.72 N_2 + 0.40 CO_2 + 0.40 CH_4 + 1.77 C + 0.43 SiO_2$ XTX-8004 $\rightarrow$ 1.77 Gas + 1.77 C + 0.43 SiO ₂

Molar average properties

Kinetic Model



(Universal Cookoff Model/MicroMechanics Pressurization Model)

Energy equation

$$\rho_b C_p \frac{\partial T}{\partial t} = \nabla \cdot (k \nabla T) + h_r r_x + \dot{q}_{melt}$$

First order decomposition



RDX/TNT



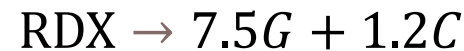
RDX/DOA/PIB/Oil



RDX/VCTFE



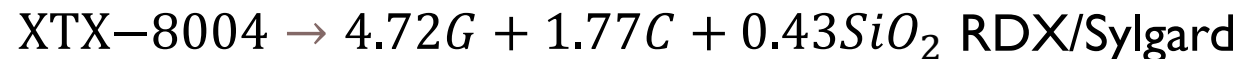
RDX/Al/HTPB/DOA



RDX

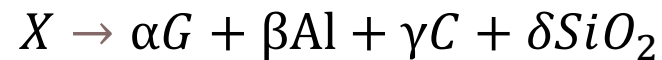


RDX/PETN/Binder/Plastici.



RDX/Sylgard

Mechanism



Rate equation

$$r_x = A \left(\frac{P}{P_o} \right)^n \lambda T^m \exp \left[-\frac{(E + \xi \sigma)}{T} \right] [X]$$

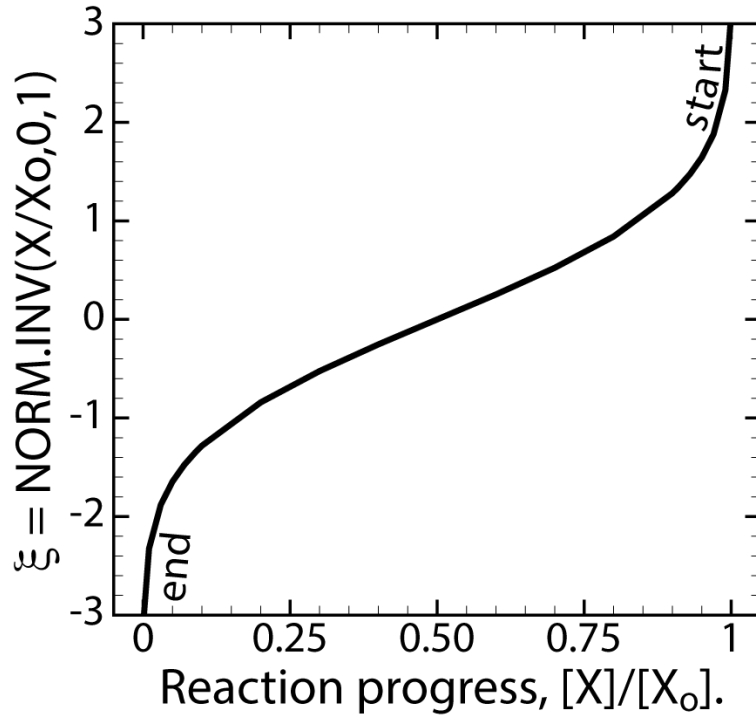
Explosive decomposes into gases and condensed species

Rate acceleration



Distributed activation energy

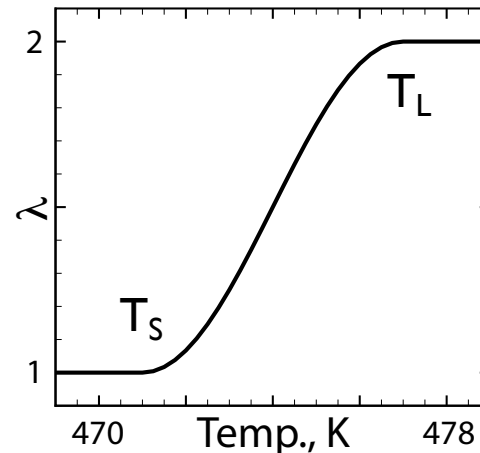
$$r_x = A \left(\frac{P}{P_o} \right)^n \lambda T^m \exp \left[-\frac{(E + \xi \sigma)}{T} \right] [X]$$



$$r_x = A \left(\frac{P}{P_o} \right)^n \lambda T^m \exp \left[-\frac{(E + \xi \sigma)}{T} \right] [X]$$

$$\lambda = \begin{cases} 1, & T \leq T_S \\ 1 + 0.5 \left(1 - [\lambda_m - 1] \cos \left[\pi \frac{(T - T_S)}{(T_S - T_L)} \right] \right), & T_S < T < T_L \\ \lambda_m, & T \geq T_L \end{cases}$$

Phase change



Kinetic parameters

Name	n	m	E, K	σ, K	RDX: λ _m
Comp-B3	0.35	1.5	24500	-500	2
Comp-C4	0.16	2	25063	-1000	2
PBX 9407	0.23	0.5	22560	-400	10
PBXN-109	0.295	-1	17997	-400	2
RDX	0.295	3	29772	-400	4
Semtex1H	0 ^a	-0.5	17200	-500	1
XTX-8004	0.15	3	28020	-1000	1

Temperature, reaction extent, and phase change accelerate rates

Effective capacitance method



$$\rho_b \mathbf{C}_p \frac{\partial T}{\partial t} = \nabla \cdot (\mathbf{k} \nabla T) + h_r r_x + \dot{q}_{melt}$$

Details

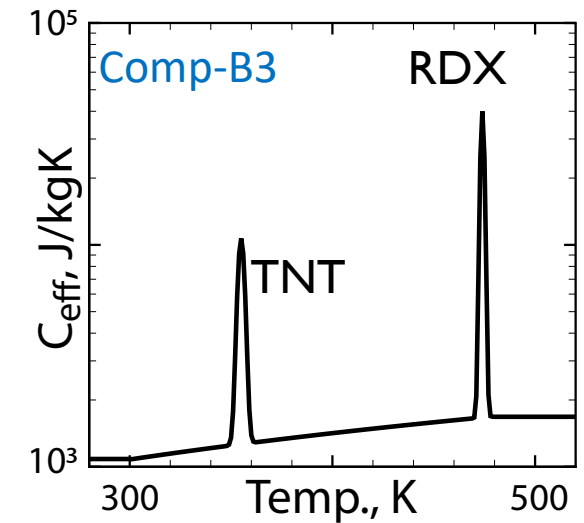
Thermophysical properties

$$C_{eff} = C_p + \frac{\omega h_l}{\sigma \sqrt{2\pi}} e^{-\frac{z^2}{2}}$$

$$\sigma = \frac{(T_m - T_s)}{3}$$

$$z = \frac{(T - T_m)}{\sigma}$$

Name	T, K	C _p , J/kgK	T, K	k, W/mK (ρ _b , kg/m ³)
Comp-B3	300	1084	300	0.2 (1710)
	350	1240	440	0.2 (1710)
	477	1680	477	0.8 ^b (1710)
Comp-C4	300	1004	300	0.16 (1500)
	600	1818	600	0.16 (1500)
PBX 9407	273	1008	400	0.20 (1625)
	482	1681	478	0.20 (1625)
PBXN-109	300	1500	300	0.4 (1650)
	600	1500	600	0.4 (1650)
RDX	300	1004	300	0.20 (1650)
	623	1760	600	0.20 (1650)
Semtex1H	300	1145	300	0.18 (1530)
	400	1470	500	0.24 (1530)
XTX-8004	298	1100	300	0.2 (1550)
	460	1520	600	0.2 (1550)



Melting components:
RDX, TNT, PETN

Name	Melt: 471-477 K h _f : 160000 J/kg	350-360 K 98450 J/kg	413-415 K 177000 J/kg
	ω _{RDX}	ω _{TNT}	ω _{PETN}
Comp-B3	0.60	0.4	0
Comp-C4	0.91	0	0
PBX 9407	0.94	0	0
PBXN-109	0.64	0	0
RDX	1.00	0	0
Semtex1H	0.43	0	0.43
XTX-8004	0.80	0	0

Phase changes are modeled thermodynamically

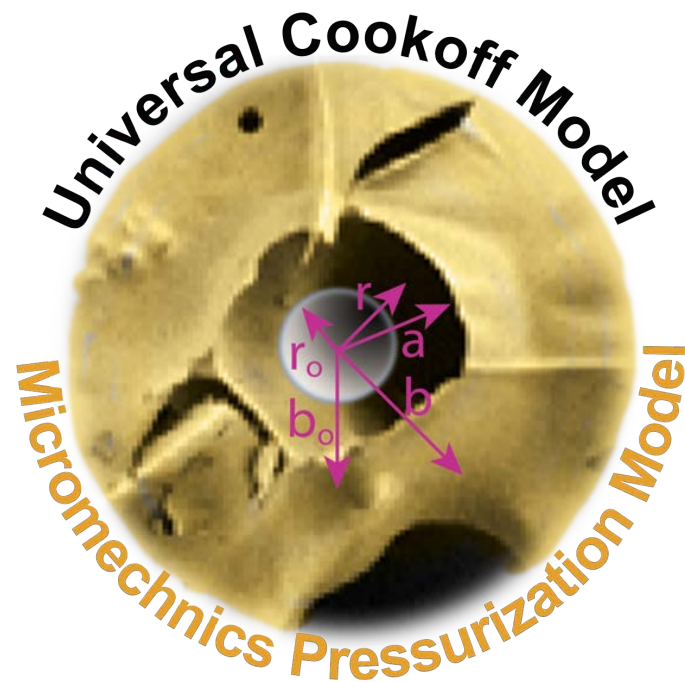
Micromechanics pressurization (MMP) model



Initial explosive is impermeable to gases

Basics

- Analytical solution of spherical elastic solid
- Tracks evolving defect radii
- Includes decomposition and thermal strain
- Includes mechanical strain and compressibility
- Damage based on maximum pore pressure
- Predicts evolution of permeability



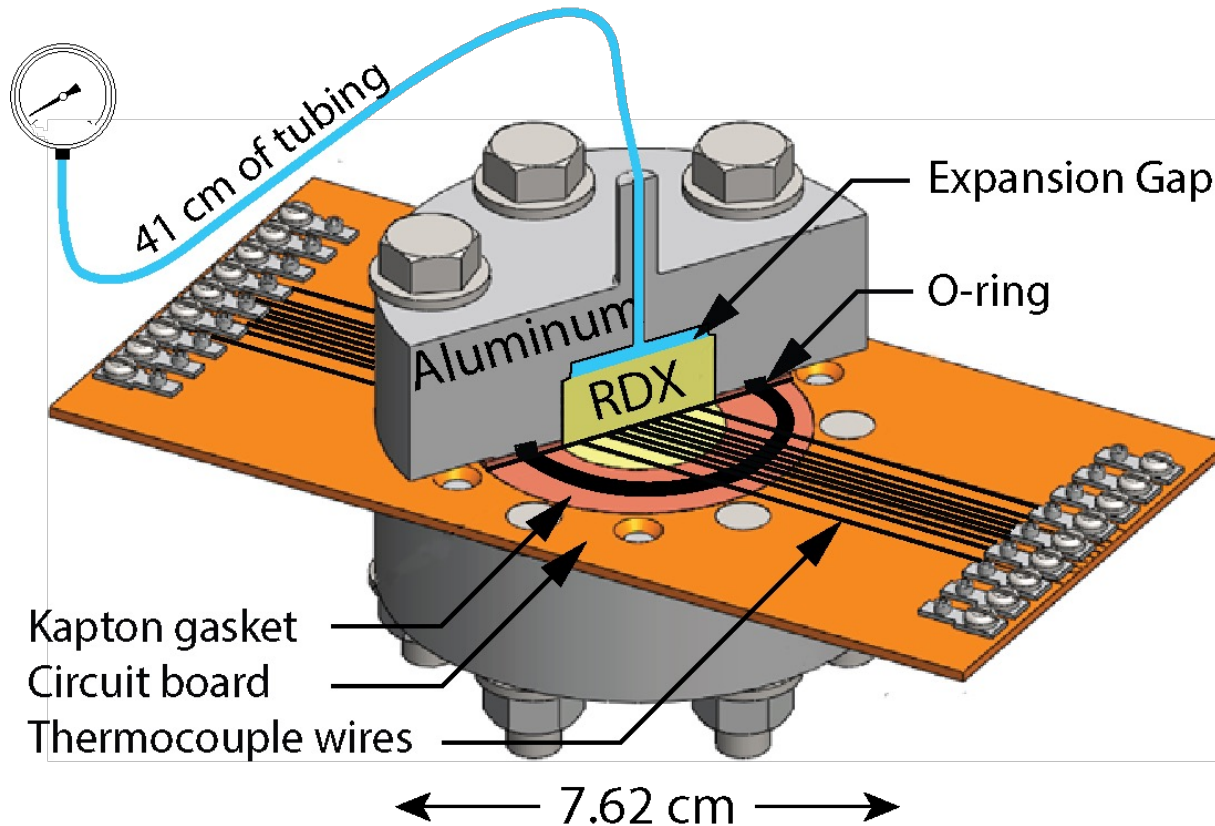
Thermal expansion, thermal damage, and abrupt gas release

SITI and ODTX

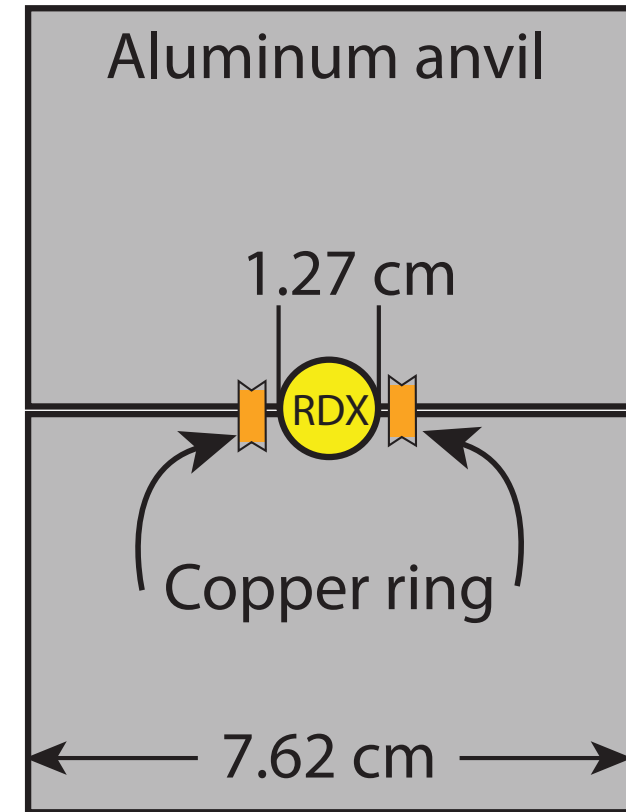
(time to thermal ignition)



Sandia Instrumented Thermal Ignition



One Dimensional Time-to-eXplosion

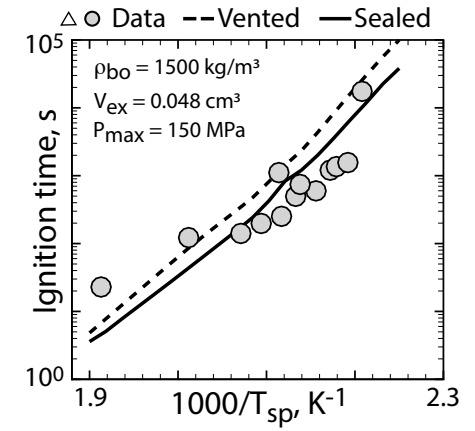
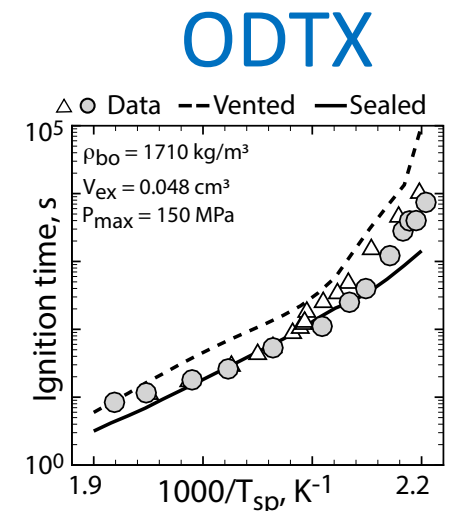
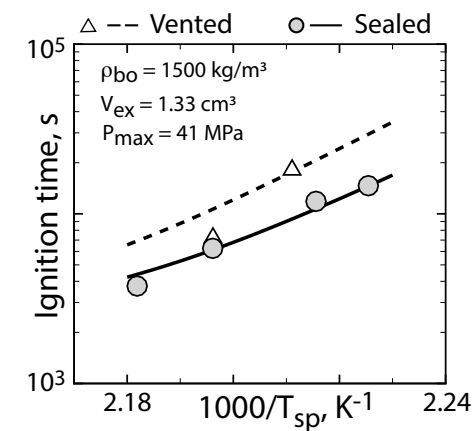
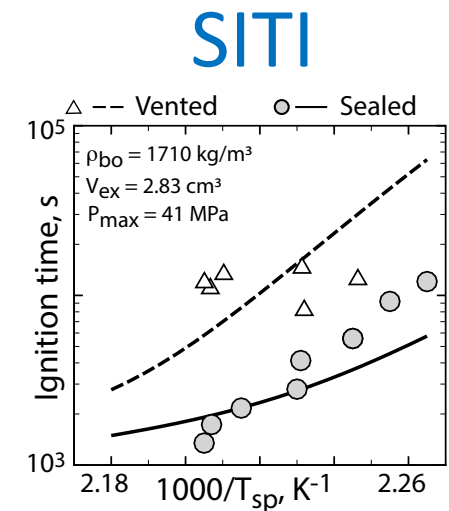
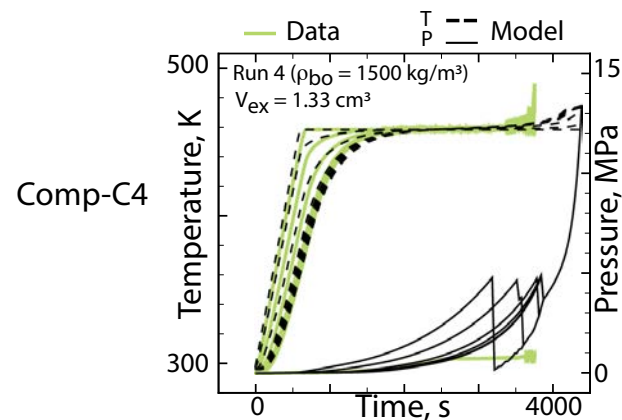
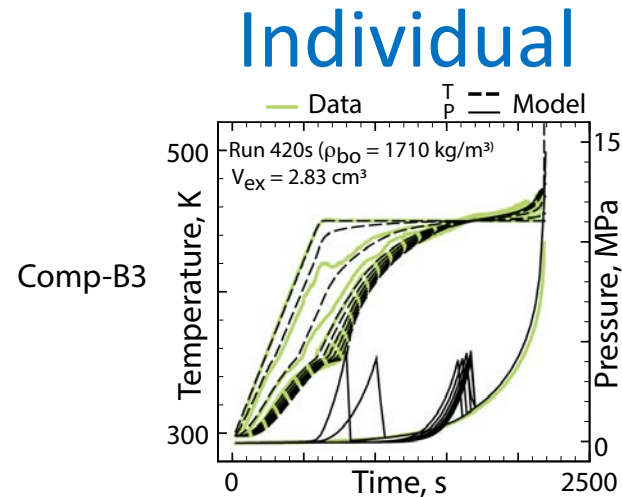


SITI is ramp and hold, ODTX is constant temperature

Measurements and Predictions



SITI run #420s

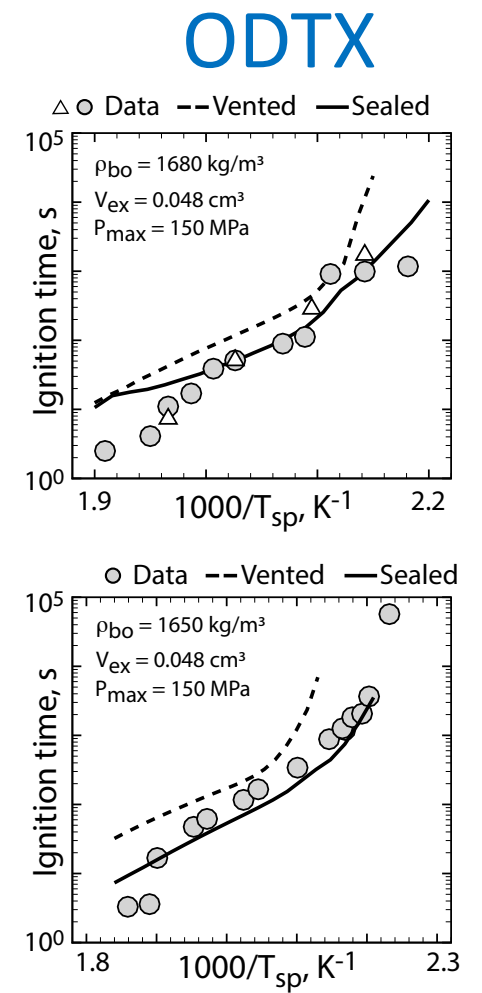
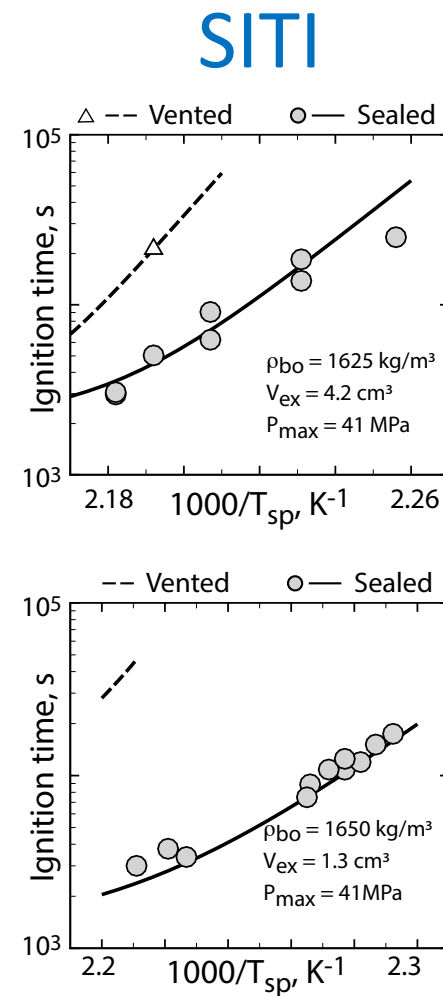
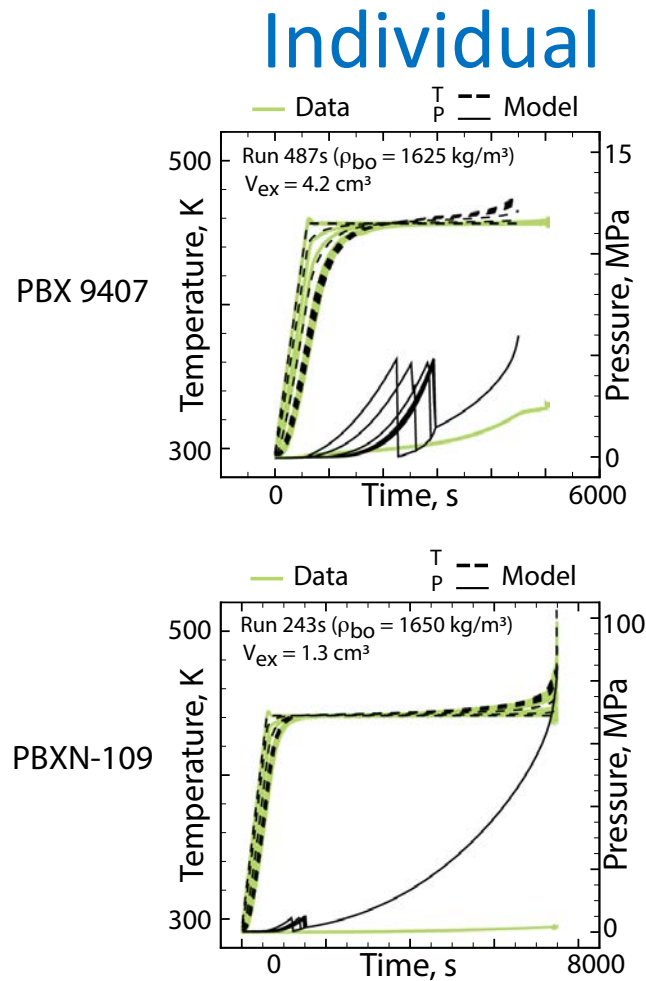


Temperature, pressure, ignition time

Measurements and Predictions



PBXN-109 SITI run #243s



Temperature, pressure, ignition time

Measurements and Predictions



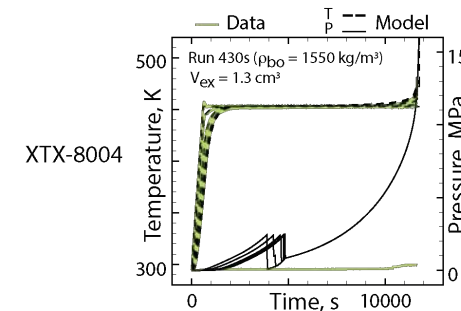
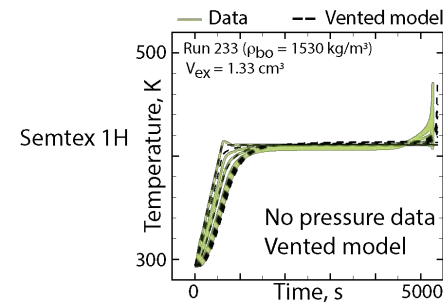
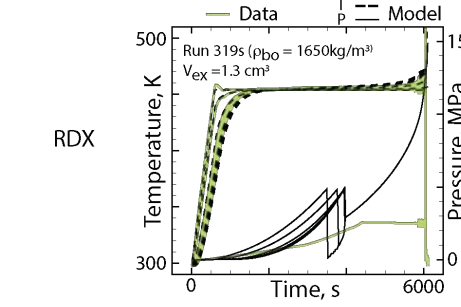
Semtex 1H #228



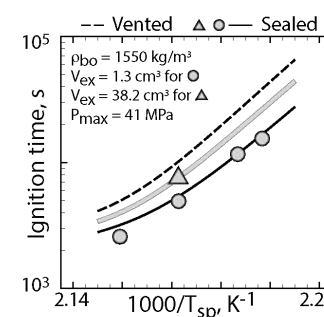
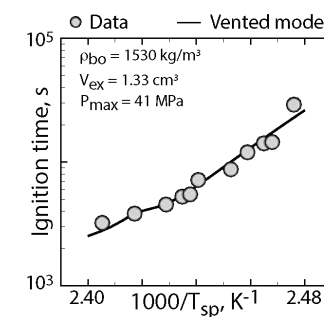
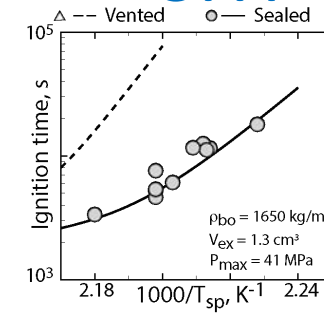
XTX-8004 #430



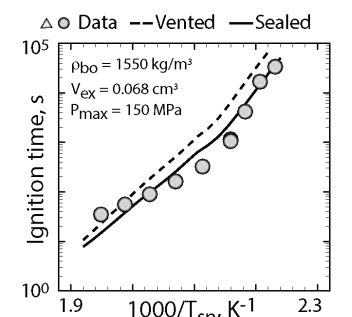
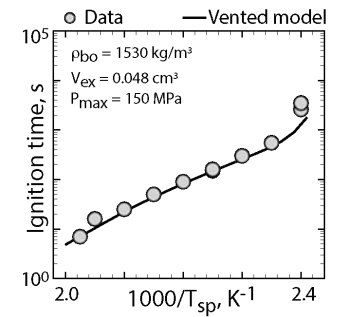
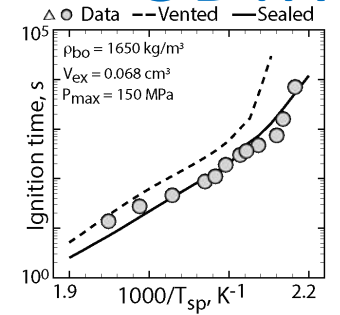
Individual



SITI



ODTX



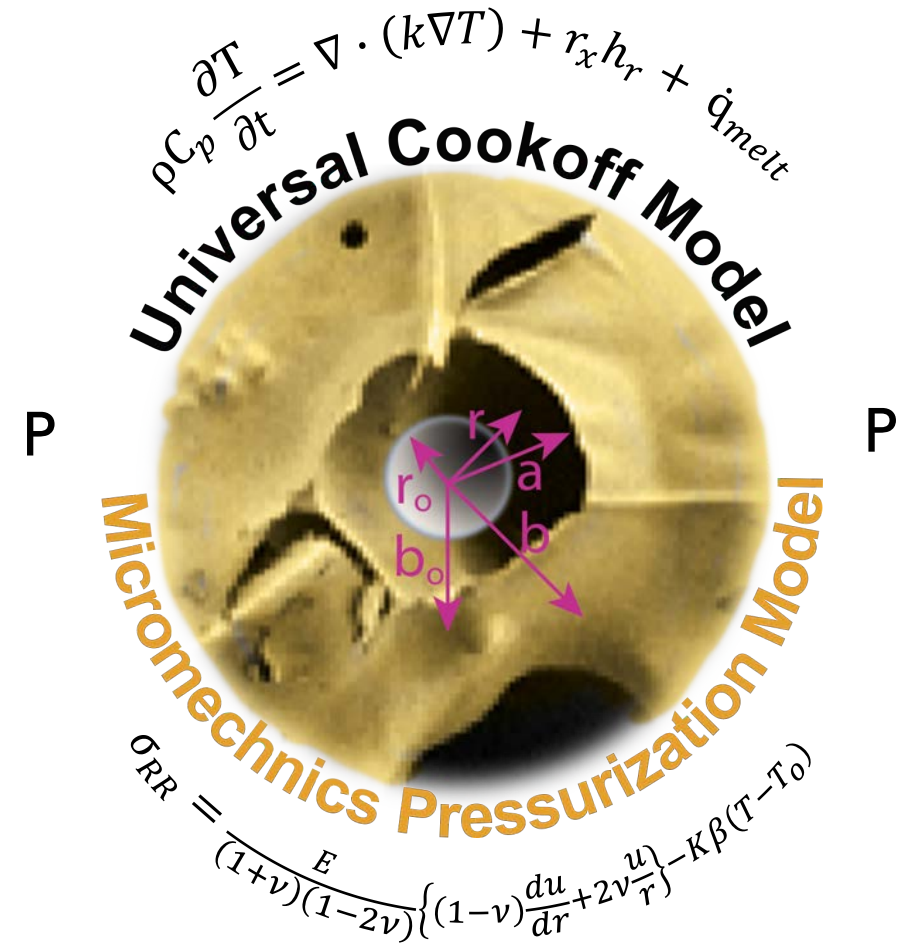
Temperature, pressure, ignition time

Summary and conclusions



- UCM/MMP model simplified
- Single autocatalytic reaction
- Acceleration by phase change
- Effective capacitance
- Validated with SITI/ODTX data

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Propell. Explos. Pyrotech., 47 (2022)

1-step UCM/MMP model for 7 HMX-based and 7 RDX-based explosives: Comp-B3, Comp-C4, EDC-37, HMX, LX-07, LX-10, LX-14, PBX 9407, PBX 9501, PBXN-109, PBXN-9, RDX, Semtex 1H, and XTX-8004