



Presentation for IRUG - Pressurizer controllers

September 2024

Changing the World's Energy Future

Paolo Balestra



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September 2024

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RELAP5-3D Intermediate Training

Pressurizer controllers.

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Name/Org: Piyush Sabharwall/C130. Date: Aug 27, 2024.
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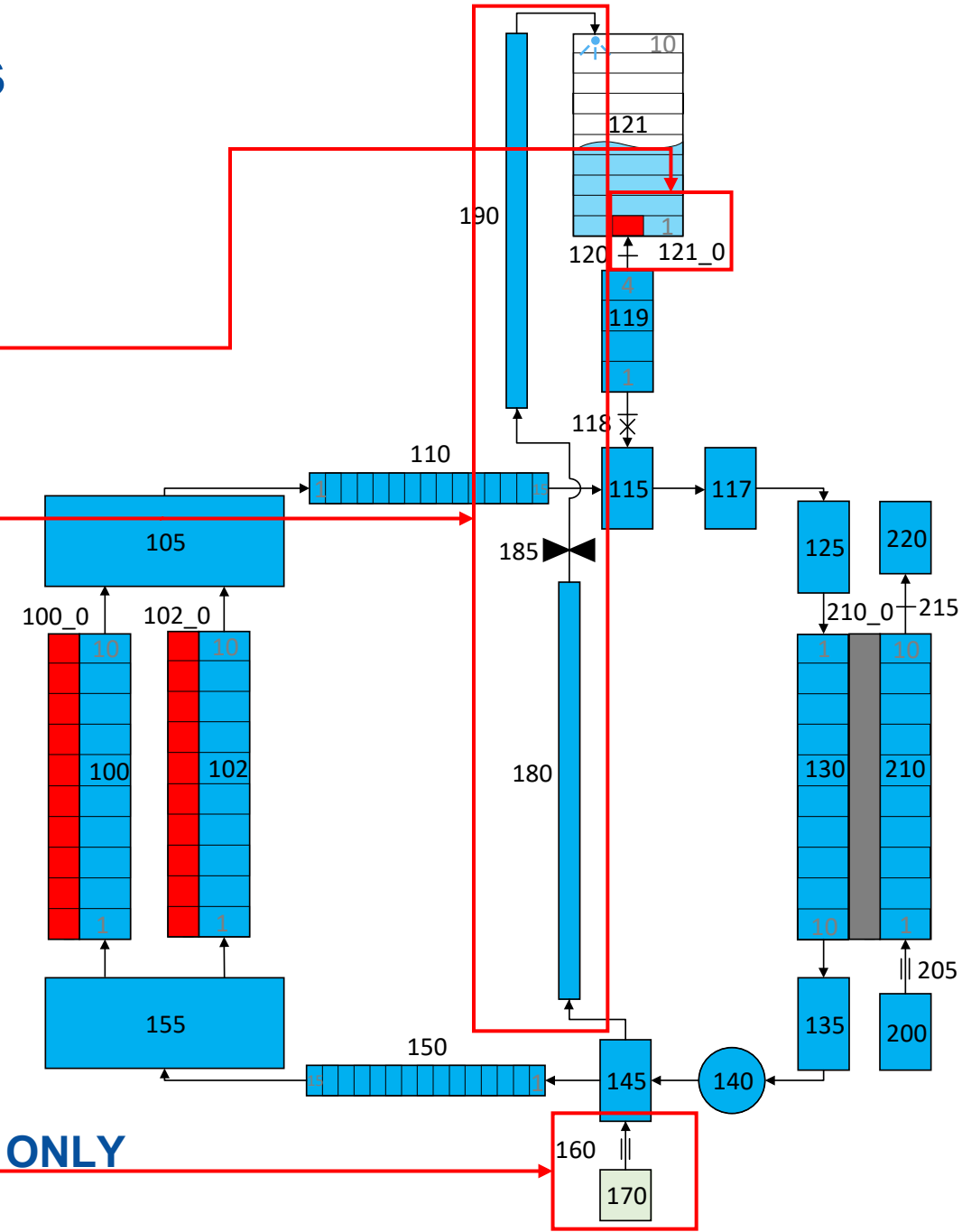
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Full Model with Pressurizer Controls

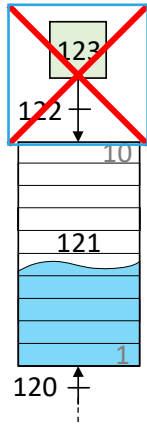
Three additional systems are integrated into the base loop:

1. Pressurizer heater (HS. 121_0) to increase the system pressure when it falls below the setpoint (15.5 MPa).
2. Spray Line (VOL 180, VLV 185, BRANCH 190) to reduce the system pressure when it exceeds the setpoint (15.5 MPa).
3. Makeup tank and pump (TDPV 170, TDJ 160) to maintain the pressurizer level at the desired setpoint (0.75 m);

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TRIPs modifications and additions



Remove the ideal pressure controller “snj122” & “tdv123”

Include TRIPs to turn ON and OFF the following control systems:

1. Makeup tank and pump activated at 0.0 s and deactivated after 1000.0 s.
2. The pressurizer spray remains active throughout the entire transient.
3. The pressurizer heater remains active throughout the entire transient.

* TRIP INPUT

* Cont'd	Var. Cosnst.	Param. Latch	Rela. Timeof	Var.	Pram.
505	time	0	gt	null	0
+	1.00E+06	n	-1.0		*
506	time	0	gt	null	0
+	1.00E+06	n	-1.0		*
507	time	0	lt	null	0
+	1.00E+06	n	0.0		*
508	time	0	lt	null	0
+	1.00E+06	n	0.0		*
509	time	0	lt	null	0
+	1.00E+06	n	0.0		*
510	time	0	gt	null	0
+	1.00E+06	n	-1.0		*

* Pump motor trip (False = Electricity to the Motor, True = Motor OFF)

* Control the power table (False = Steady State, True = SCRAM)

* Makeup volume (True = ON, False = OFF)

* Pressurizer spray (True = ON, False = OFF)

* Pressurizer heater (True = ON, False = OFF)

* Control the Secondary side MFR (False = Steady State, True = MFR change)

Existing components modifications

* Branch component (#145)

* Name Type

1450000	brch145	branch
*	Junc. No'	icc
1450001	2	1
*	Area	Length
1450101	5.86E-03	0.5
*	Elev.	Wall
1450102	0.0	5.00E-05
*	Area-Y	Length-Y
1450181	0.0	0.086
*	ebt	Pres.
1450200	3	1.55E+07
*	From	To
1451101	145010000	150000000
*	AF	AR
1451102	0.0	0.0
*	From	To
1452101	145010000	180000000
*	AF	AR
1452102	0.0	0.0
* Init. Co	Liq. Mfl.	Vap. Mfl.
1451201	28.442	0.0
1452201	0.0	0.0
*		

Adding a junction to branch 145, located downstream of the pump, to connect the lower part of the spray line (vol180).

* Init.	Coebt	Pres.	Temp.	Qual.	Null
* Cont'd	Null	Vol. No'			
1191201	003	1.55E+07	586.0	0.0	0.0
+	0.0	4			
*					
* Init.	Coebt	Pres.	Temp.	Qual.	Null
* Cont'd	Null	Vol. No'			
1211201	003	1.55E+07	586.0	0.0	0.0
+	0.0	5			
* Init.	Coebt	Pres.	Qual.	Null	Null
* Cont'd	Null	Vol. No'			
1211202	002	1.55E+07	1.0	0.0	0.0
+	0.0	10			

- Adjusting the initial temperatures of the surge line (pipe119) and the pressurizer (pipe121) to match the hot leg to which they are connected.
- Although the temperatures of these components will eventually equalize with the hot leg, this process occurs very slowly due to the stagnant fluid within them, as they are not part of the main flow path.
- This modification is intended to accelerate the temperature equalization.

Existing components modifications

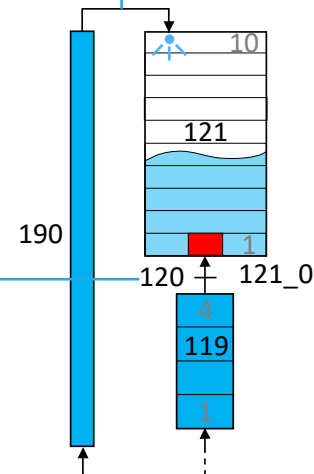
* Pressurizer component (#121) - Pressurizer

* Name	Type				
1210000	prz121	prizer			
* Geometry	No'vols.	surgjN	intfhxl	intfhxv	multl
* Cont'd		multv	droplsiz	sprayjN	mixcoeff.
1210001	10	120000000	0.0	0.0	0
+	0	0.0	190010000	0.0	
* Geometry	Area	Vol. No'			
1210101	3.24E-02	10			
* Geometry	Length	Vol. No'			
1210301	0.15	10			
* Geometry	Ver. Ang.	Vol. No'			
1210601	90.0	10			
* Geometry	Elevation	Vol. No'			
1210701	0.15	10			

- Change the component type from “pipe” to “prizer” this will require additional words on card 1210001

- The "prizer" component needs to know which junction belongs to the surge line (junction 120000000) and which one belongs to the spray line (junction 190010000).

- The rest of the parameters are needed to control the mixing of the droplets and the droplets size, default parameters will be used.



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Existing components modifications

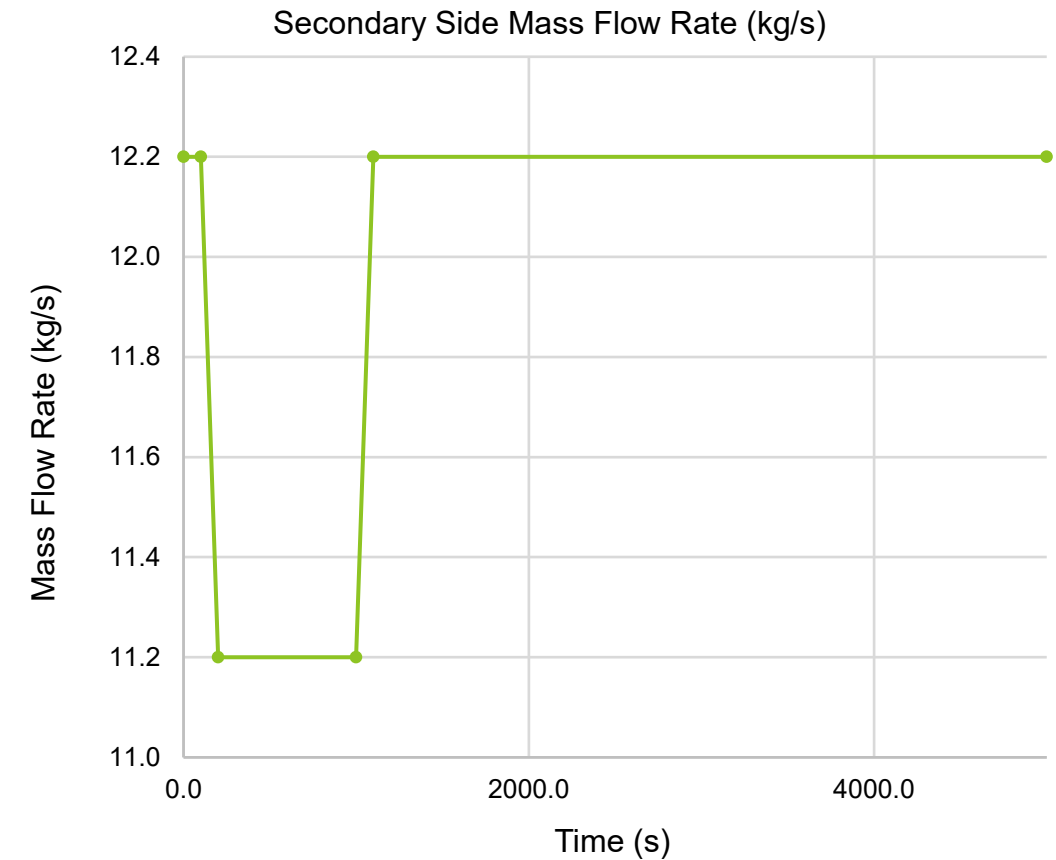
* Time dependent junction (#205) - 2nd side Flow B.C.

*	Name	Type		
2050000	tdj205	tmdpjun		
* Geometry	From	To	Area	
2050101	200010000	210000000	0	
* Data control	Option	Trip no'		
2050200	1	510		
* Data	Time	Liq. Vel.	Vap. Vel.	Interface vel.
2050201	-1.0	12.2	0.0	0.0
2050202	0.0	12.2	0.0	0.0
2050203	100.0	12.2	0.0	0.0
2050204	200.0	11.2	0.0	0.0
2050205	1000.0	11.2	0.0	0.0
2050206	1100.0	12.2	0.0	0.0
2050207	1.0E+06	12.2	0.0	0.0

*

Set up the secondary-side time-dependent junction (tdj205) for the secondary-side upset:

1. The mass flow rate will decrease by 1 kg/s over 100s, starting at 100.0s.
2. The mass flow rate will return to its original value over 100s starting at 1000.0s.



Spray Line

- A 2 cm diameter pipe is modeled with 2 volumes, covering a total length of 6.9431817 meters.
- This length corresponds to the height from the pump follower (BRANCH145) to the top of the 10th volume of the pressurizer (PIPE121).
- Servo valve used to simulate the spray valve opening and closing based on the signal from control variable 73

```
*****
```

* Volume component (#180) - Lower part of the spray line					
*	Name	Type			
1800000	vol180	snglvol			
*	Area	Length	Volume	Hor. Ang.	Ver. Ang.
1800101	3.14E-04	6.0	0.0	0.0	90.0
*	Elev.	Wall rough	Dh	tlpvbfe	
1800102	6.0	5.00E-05	0.0	0000000	
*	ebt	Pres.	Temp.		
1800200	003	1.55E+07	552.6		

```
*****
```

```
*****
```

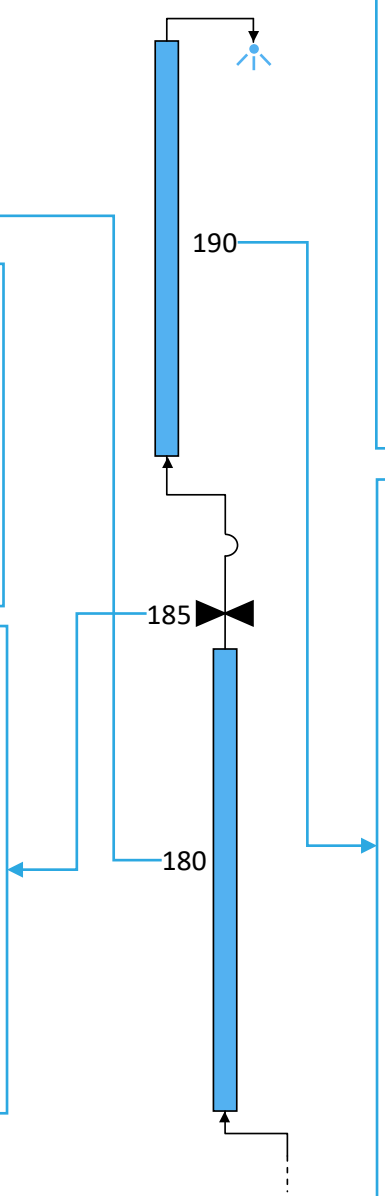
* Valve component (#185) - Spray valve					
*	Name	Type			
1850000	vlv185	valve			
* Geometry					
	From	To	Area	AF	AR
*	Cont'd	jefvcahs			
1850101	180010000	190000000	3.14E-04	9.0	9.0
+	00000100				
* Init. Co					
	Option	Liq. Vel.	Vap. Vel.	Intf. Vel	
1850201	1	0.0	0.0	0.0	
*	VLV Type				
1850300	srvvlv				
*	CntrlVar No'				
1850301	73				

```
*****
```

```
*****
```

* Branch component (#190) - Upper part of the spray line					
*	Name	Type			
1900000	brch190	branch			
*	Junc. No'	icc			
1900001	1	1			
*	Area	Length	Volume	Hor. Ang.	Ver. Ang.
1900101	3.14E-04	0.9431817	0.0	0.0	90.0
*	Elev.	Wall rough	Dh	tlpvbfe	
1900102	0.9431817	5.0E-05	0.0	0000000	
*	ebt	Pres.	Temp.		
1900200	003	1.55E+07	552.6		
*	From	To	Area		
1901101	190010000	121010000	0.0		
*	AF	AR	jefvcahs		
1901102	0.0	0.0	00000100		
* Init. Co					
	Liq. Mfl.	Vap. Mfl.	Intf. Vel		
1901201	28.442	0.0	0.0		

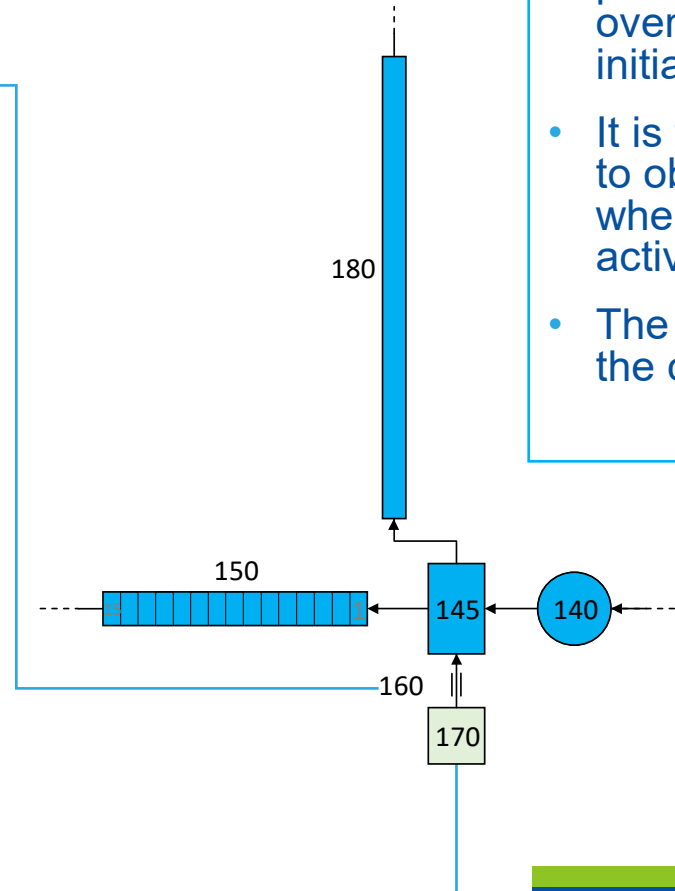
```
*****
```



Makeup Tank and Pump

```
*****
* Time dependent junction (#160) - Makeup pump
*
* Name      Type
1600000    tdj160    tmdpjun
* Geometry  From      To      Area
1600101    170000000  145000000  0.04
* Data control  Option  Trip no'  CntrlV Nm  CntrlV no'
1600200      0        0        cntrlvar    83
*
* Data      Time      Liq. Vel.  Vap. Vel.  Interface vel.
1600201     -10.0     -10.0      0.0       0.0
1600202      10.0      10.0      0.0       0.0
*****
```

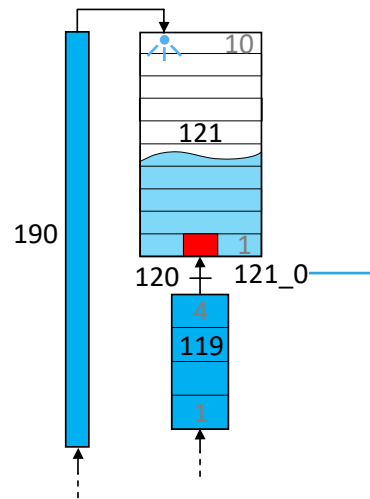
```
*****
* Time dependent volume (#170) - Makeup tank
*
* Name      Type
1700000    tdv170    tmdpvol
* Geometry  Area      Length  Volume  Hor. Ang.  Ver. Ang.
* cont'd    Elev. Chg. Wall rough.  Hydro. D.  tlpvbf
1700101     10.0      1.0     0.0     0.0      90.0
1700102      1.0      0.0     0.0     0
* Data control  ebt      Trip no'
1700200        3        0
* Data      Time      Pres.      Temp.
1700201       0      1.55E+07  552.6
*****
```



- The time-dependent junction (TDJ160) adds or removes cold water from the TDV170 at 552.6 K into the pump follower volume (BRANCH145).
- This system is initially used to prevent the pressurizer from overflowing or drying out during the initial stabilization period.
- It is then deactivated after 1000s to observe how the level changes when the spray or the heater is activated.
- The mass flow rate is controlled by the control variable 83

Pressurizer Heaters

- The heater in the pressurizer is simulated using the heat structure HS121_0
- HS121_0 represent 20 metallic rods with 5cm radius
- HS121_0 is coupled on the right side with the volume 1 of the pressurizer (PIPE121)
- The power source is controlled by the control variable 76



* Pressurizer proportional heater (HS #121_0)					
*	Axial vols	Radial vols	Type	S-S init.	Left coor.
11210000	1	5	2	0	0.0
* HS mesh					
	Location	Format			
11210100	0	1			
	No' interv	Right coor.			
11210101	4	0.05			
* HS mater					
	Mat. No'	No' interval			
11210201	1	4			
* HS heat					
	Source	No' interval			
11210301	1.0	4			
* Init. Te					
	Option				
11210400	0				
* Init. Te					
	Temp.	Radial vols.			
11210401	552.6	5			
* Left					
	B-Cdefinition	Increment	HT type	Area type	Area data
* Cont'd					
	HS No'				
11210501	0	0	0	1	3.0
+					
	1				
* Right					
	B-Cdefinition	Increment	HT type	Area type	Area data
* Cont'd					
	HS No'				
11210601	121010000	0	1	1	3.0
+					
	1				
* Heat src					
	Source typ	Source coe	Left mod.	Right mod.	HS No'
11210701	10076	1.0	0.0	0.0	1
*					
	Hydro. D.	For. Lengt	Rev. Lengt	For. Grid	Rev. Grid L.
* Cont'd					
	For. Grid	Rev. Grid	Loc. Boili	HS No'	
11210901	0.0	1.0	1.0	0.0	0.0
+					
	0.0	0.0	1.0	1	
*					

Makeup Tank and Pump controllers

* Pressurizer level error (setpoint 0.75m out of 1.5m)

20500800	lvlset	sum	-1.0	0.0	0
20500801	-0.75	1.0	przlvl	121	

* Presurizer makeup pump mass flow rate (min -10.0 m/s, Max 10.0 m/s)

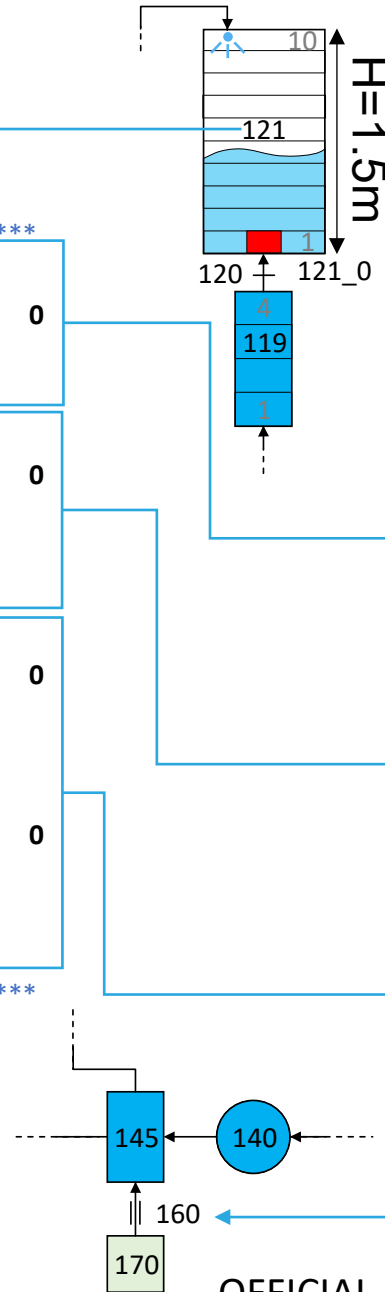
20500810	lvlprint	prop-int	1.0	0.0	0
+	3	-10.0	10.0		
20500811	1.0E-01	5.0E-05	cntrlvar	80	

* Presurizer makeup pump switch

20500820	mmswitch	tripunit	1.0	1.0	0
20500821	507				

* Presurizer makeup pump mass flow rate

20500830	pzrpres	mult	1.0	0..0	0
20500831	cntrlvar	81			
20500832	cntrlvar	82			



$$L_f(t) = \int_0^H \alpha_f(t) dh \approx \sum_{n=1}^{10} 0.15 \cdot \alpha_f^n(t)$$

α_f = volume liquid fraction

H = pressurizer height

$$err(t) = L_f(t) - 0.75$$

$$s(t) = 1.0e-1 \cdot err(t) + 5.0e-5 \cdot \int_0^t err(t) dt$$

$[-10.0 < s(t) < 10.0]$

$$mfr(t) = s(t) \cdot TRIP507(t)$$

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Pressurizer heaters controllers

* Pressurizer pressure error

20500700	prsset	sum	1.0	0.0	0
20500701	-1.55E+07	1.0	p	121100000	

*

* Pressurizer power (min 0.0 W, Max 2.0kW)

20500710	prsprnt	prop-int	1.0	0.0	0
+	3	0.0	2000.0		
20500711	1.0E-02	5.0E-12	cntrlvar	70	

*

* Pressurizer heater switch

20500720	mmswitch	tripunit	1.0	1.0	0
20500721	509				

*

* Pressurizer heat

20500730	pzrpres	mult	1.0	0.0	0
20500731	cntrlvar	74			
20500732	cntrlvar	75			

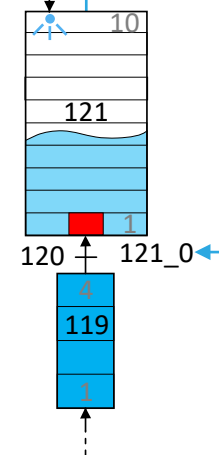
*

$$err(t) = P(t) - 15.5e+07$$

$$s(t) = 1.0e-2 \cdot err(t) + 5.0e-12 \cdot \int_0^t err(t) dt$$

$$[0.0 < s(t) < 2.0e+03]$$

$$area(t) = s(t) \cdot TRIP509(t)$$



Steady state simulations suggested comparison plot list

Variable Name	Variable Number	Description
p	121100000	Pressure at the top of the pressurizer (Pa)
tempf	115010000	Main loop temperature at the surge line connection (K)
pmpvel	140	Pump velocity (rad/s)
mflowfj	145010000	Main loop liquid mass flow rate (kg/s)

Transient Simulations with ACTIVE controllers

```
*****
*
*      TRIP INPUT
*****
*
*      Var.      Param.      Rela.      Var.      Pram.
*      Cosnst.   Latch      Timeof
* Cont'd
505      time      0          gt          null      0
+      1.00E+06    n          -1.0
506      time      0          gt          null      0
+      1.00E+06    n          -1.0
507      time      0          lt          null      0
+      0.0         n          -1.0
508      time      0          lt          null      0
+      1.00E+06    n          0.0
509      time      0          lt          null      0
+      1.00E+06    n          0.0
510      time      0          gt          null      0
+      0.0         n          0.0
*
```

* Pump motor trip (False = Electricity to the Motor, True = Motor OFF)

* Control the power table (False = Steady State, True = SCRAM)

* Makeup volume (True = ON, False = OFF)

* Pressurizer spray (True = ON, False = OFF)

* Pressurizer heater (True = ON, False = OFF)

* Control the Secondary side MFR (False = Steady State, True = MFR change)

Start the transient on the secondary side at time 0.0s

Turn OFF the makeup volume at time 0.0s, not needed for the transient.

Transient Simulations with controller DISABLED

```
*****
*
*      TRIP INPUT
*****
*
*      Var.      Param.      Rela.      Var.      Pram.
*      Cosnst.   Latch      Timeof
* Cont'd
505      time      0          gt          null      0
+      1.00E+06    n          -1.0
506      time      0          gt          null      0
+      1.00E+06    n          -1.0
507      time      0          lt          null      0
+      0.0         n          -1.0
508      time      0          lt          null      0
+      0.0         n          -1.0
509      time      0          lt          null      0
+      0.0         n          -1.0
510      time      0          gt          null      0
+      0.0         n          0.0
*
```

* Pump motor trip (False = Electricity to the Motor, True = Motor OFF)

* Control the power table (False = Steady State, True = SCRAM)

* Makeup volume (True = ON, False = OFF)

* Pressurizer spray (True = ON, False = OFF)

* Pressurizer heater (True = ON, False = OFF)

* Control the Secondary side MFR (False = Steady State, True = MFR change)

Turn OFF the pressurizer spray at time 0.0s

Turn OFF the pressurizer heater at time 0.0s

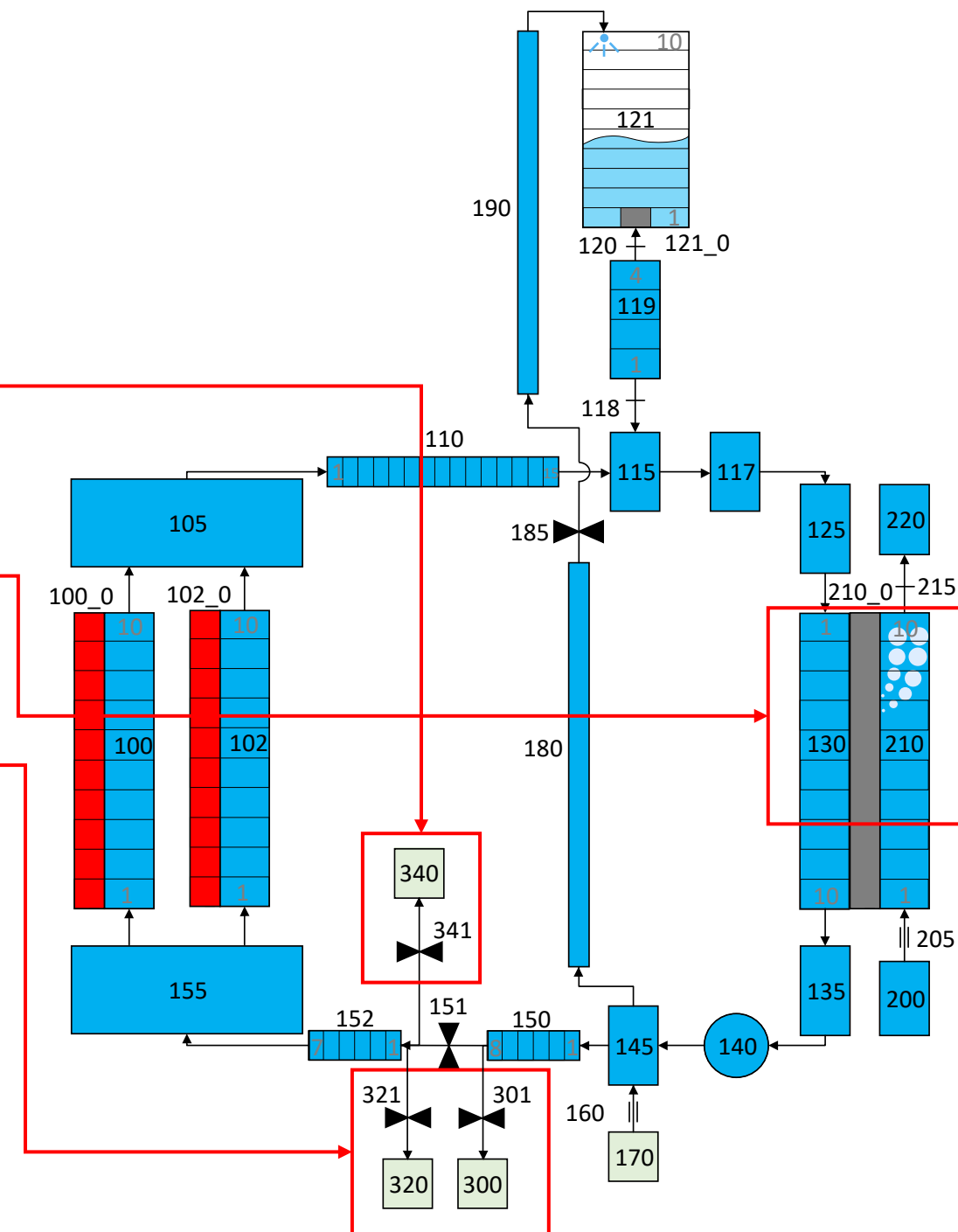
Transient simulations suggested comparison plot list

Variable Name	Variable Number	Description
p	121100000	Pressure at the top of the pressurizer (Pa)
przlvl	121	Pressurizer level, max 1.5m (m)
cntrlvar	73	Spray valve normalized area (//)
mflowfj	185000000	Spray valve liquid mass flow rate (kg/s)
cntrlvar	76	Power in the pressurizer heaters (W)
httemp	121000101	Heater's centerline temperature (K)
tempf	115010000	Main loop temperature at the surge line connection (K)

Full Model with LOCA breaks

Additional valves and time dependent volumes to simulate the breaks:

3. One trip valve with a 1cm diameter flow area and a time dependent volume are added to simulate the small break.
2. The secondary side now operates as a boiling system, with reduced pressure and mass flow rate ensuring that the fluid reaches its boiling point before exiting the secondary side.
3. Three trip valves and two time dependent volumes are added to simulate the double guillotine break.



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TRIPs modifications and additions

* EXPANDED PLOT VARIABLES

*	VarNam	VarNum	
20800001	htpowg	1000001*	Heat structure power source
20800002	pmpmt	140*	Pump motor torque

* TRIP INPUT

*	Var.	Param.	Rela.	Var.	Pram.
* Cont'd	Cosnst.	Latch	Timeof		
505	time	0	gt	null	0
+	1.00E+06	n	-1.0		*
506	time	0	gt	null	0
+	1.00E+06	n	-1.0		*
507	time	0	lt	null	0
+	1.00E+06	n	0.0		*
508	time	0	lt	null	0
+	1.00E+06	n	0.0		*
509	time	0	lt	null	0
+	1.00E+06	n	0.0		*
510	time	0	gt	null	0
+	1.00E+06	n	-1.0		*
511	time	0	gt	null	0
+	1.00E+06	n	-1.0		*
512	time	0	gt	null	0
+	1.00E+06	n	-1.0		*

*	Trip	Op.	Trip	Latch	Timeof
605	-505	and	-505	n	0.0*
612	-512	and	-512	n	0.0*

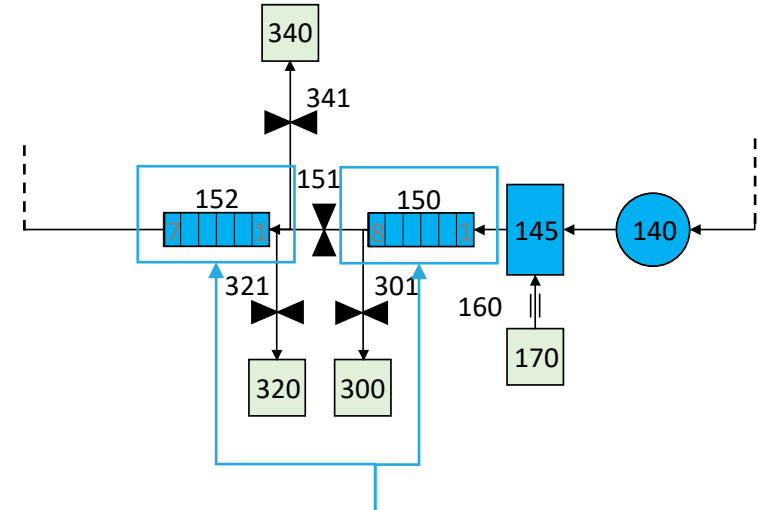
Add the expanded plot variables to plot the pump motor torque and the power in the heaters.

Include TRIPs to open and close the trip valves to simulate the two different LOCA.

Existing components modifications

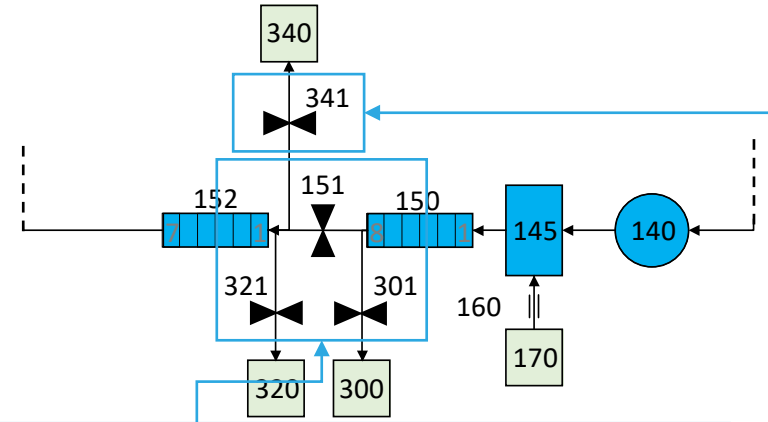
* Pipe component (#150)

Name	Type
1500000	pipe150
* Geometry	No' vols. 8
1500001	
* Geometry	Area 5.858E-03
1500101	
* Geometry	Length 0.667
1500301	
* Geometry	Ver. Ang. 0.0
1500601	
* Geometry	Elevation 0.0
1500701	
* Geometry	Wall rough 5.00E-05
1500801	
* Init. Co	ebt
* Cont'd Null Vol. No'	
1501201	
+	
* Jct. con	Option 1
1501300	
* Jct. dat	Liq. Mfl. 28.442
1501301	
*	



- Reduce the number of volumes from 15 to 8 and the number of junctions from 14 to 7. The rest of the options are unchanged.
- To model the rest of the cold leg a new component with number 152 instead of 150 and 7 volumes instead of 8 and 6 junctions instead of 7 will be added to the model.

Valves that open to simulate the breaks



* Valve component (#151)					
	Name	Type			
1510000	vlv151	valve			
* Geometry	From	To	Area	AF	AR
	Cont'd	jefvcahs			
1510101	150010000	152000000	5.86E-03	1.0	1.0
+	00000100				
* Init. Co	Option	Liq. Vel.	Vap. Vel.	Intf.Vel	
1510201	1	28.442	0.0	0.0	
	VLV Type				
1510300	trpvlv				
	Trip No'				
1510301	612				

* Valve component (#301)					
	Name	Type			
3010000	vlv301	valve			
* Geometry	From	To	Area	AF	AR
	Cont'd	jefvcahs			
3010101	150010000	300000000	5.86E-03	1.0	1.0
+	00000100				
* Init. Co	Option	Liq. Vel.	Vap. Vel.	Intf.Vel	
3010201	1	0.0	0.0	0.0	
	VLV Type				
3010300	trpvlv				
	Trip No'				
3010301	512				

- Three trip valves to simulate the double guillotine break. Two opens thanks to when TRIP 512 is True and one close following the complement TRIP 612
- One trip valve to simulate the small break LOCA that open when TRIP 511 is True.

* Valve component (#341)					
	Name	Type			
3410000	vlv301	valve			
* Geometry	From	To	Area	AF	AR
	Cont'd	jefvcahs			
3410101	152000000	340000000	5.86E-03	1.0	1.0
+	00000100				
* Init. Co	Option	Liq. Vel.	Vap. Vel.	Intf.Vel	
3410201	1	0.0	0.0	0.0	
	VLV Type				
3410300	trpvlv				
	Trip No'				
3410301	511				

Steady state simulation suggested plot list

Variable Name	Variable Number	Description
p	121100000	Pressure at the top of the pressurizer (Pa)
tempf	115010000	Main loop temperature at the surge line connection (K)
pmpvel	140	Pump velocity (rad/s)
mflowfj	145010000	Main loop liquid mass flow rate (kg/s)
voidg	210100000	Secondary Side outlet Void fraction (//)
przlvl	121	Pressurizer level, max 1.5m (m)

Small break LOCA transient simulation

* TRIP INPUT

	Var.	Param.	Rela.	Var.	Pram.
	Cosnst.	Latch	Timeof		

* Cont'd

505	time	0	gt	null	0	
+	1.00E+01	n	-1.0		*	Pump motor trip (False = Electricity to the Motor, True = Motor OFF)
506	time	0	gt	null	0	
+	1.00E+01	n	-1.0		*	Control the power table (False = Steady State, True = SCRAM)
507	time	0	lt	null	0	
+	0.0	n	0.0		*	Makeup volume (True = ON, False = OFF)
508	time	0	lt	null	0	
+	0.0	n	0.0		*	Pressurizer spray (True = ON, False = OFF)
509	time	0	lt	null	0	
+	0.0	n	0.0		*	Pressurizer heater (True = ON, False = OFF)
510	time	0	gt	null	0	
+	1.00E+06	n	-1.0		*	Control the Secondary side MFR (False = Steady State, True = MFR change)
511	time	0	gt	null	0	
+	1.00E+01	n	-1.0		*	Loss of flow accident, small break (True = ON, False = OFF)
512	time	0	gt	null	0	
+	1.00E+06	n	-1.0		*	Loss of flow accident, double guillotine break (True = ON, False = OFF)

*

	Trip	Op.	Trip	Latch	Timeof	
605	-505	and	-505	n	0.0*	Pump regulation trip, True when Pump motor trip 505 is False
612	-512	and	-512	n	0.0*	Loss of flow accident, double guillotine break

Shut down the pump motor and SCRAM the power after 10s

Turn off the pressurizer pressure and level control system

Open the valves to simulate the small break LOCA after 10s.

Large break LOCA transient simulation

* TRIP INPUT

* Var. Param. Rela. Var. Param.

* Cont'd

	Var. Cosnst.	Param. Latch	Rela. Timeof	Var.	Param.	
505	time	0	gt	null	0	
+	1.00E+01	n	-1.0		*	Pump motor trip (False = Electricity to the Motor, True = Motor OFF)
506	time	0	gt	null	0	
+	1.00E+01	n	-1.0		*	Control the power table (False = Steady State, True = SCRAM)
507	time	0	lt	null	0	
+	0.0	n	0.0		*	Makeup volume (True = ON, False = OFF)
508	time	0	lt	null	0	
+	0.0	n	0.0		*	Pressurizer spray (True = ON, False = OFF)
509	time	0	lt	null	0	
+	0.0	n	0.0		*	Pressurizer heater (True = ON, False = OFF)
510	time	0	gt	null	0	
+	1.00E+06	n	-1.0		*	Control the Secondary side MFR (False = Steady State, True = MFR change)
511	time	0	gt	null	0	
+	1.00E+06	n	-1.0		*	Loss of flow accident, small break (True = ON, False = OFF)
512	time	0	gt	null	0	
+	1.00E+01	n	-1.0		*	Loss of flow accident, double guillotine break (True = ON, False = OFF)

	Trip	Op.	Trip	Latch	Timeof	
605	-505	and	-505	n	0.0	* Pump regulation trip, True when Pump motor trip 505 is False
612	-512	and	-512	n	0.0	* Loss of flow accident, double guillotine break

Shut down the pump motor and SCRAM the power after 10s

Turn off the pressurizer pressure and level control system

Open the valves to simulate the large break LOCA after 10s

Transient simulations suggested comparison plot list

Variable Name	Variable Number	Description
p	121100000	Pressure at the top of the pressurizer (Pa)
tempf	115010000	Main loop temperature at the surge line connection (K)
voidg	210100000	Secondary Side outlet Void fraction (//)
pmpmt	140	Pump motor torque (N/m)
htpowg	1000001	Power on the heating rods (W)
mflowj	151000000	Primary loop mass flow rate (kg/s)
mflowj	301000000	Large break right side mass flow rate (kg/s)
mflowj	321000000	Large break left side mass flow rate (kg/s)
mflowj	341000000	Small break mass flow rate (kg/s)
vlvarea	151	Primary loop valve normalized area (//)
vlvarea	301	Large break right side valve normalized area (//)
vlvarea	321	Large break left side valve normalized area (//)
vlvarea	341	Small break valve normalized area (//)
cntrlvar	73	Spray valve normalized area (//)
cntrlvar	76	Power in the pressurizer heaters (W)
przlvl	121	Pressurizer level, max 1.5m (m)



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