



Exceptional service in the national interest

# Comparative Failure Analysis of Components Exposed to Multi-Axis & Single-Axis Vibration Testing

Thomas Brown <sup>(1)</sup> <sup>(2)</sup>, Jelena Paripovic <sup>(1)</sup>, Glen Throneberry <sup>(1)</sup>, Kevin Cross <sup>(1)</sup>, Washington DeLima <sup>(3)</sup>, Martin Sanchez <sup>(1)</sup>, and Stephen Aulbach <sup>(1)</sup>

SANDIA NATIONAL LABORATORIES <sup>(1)</sup>

UNIVERSITY OF TEXAS – AUSTIN <sup>(2)</sup>

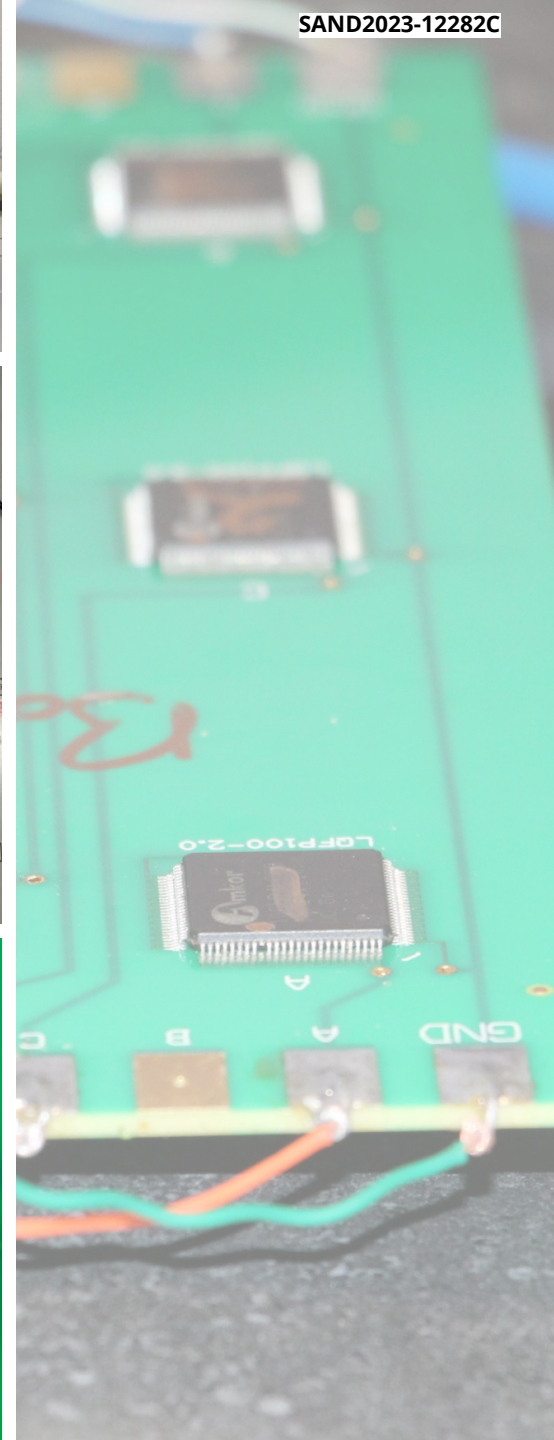
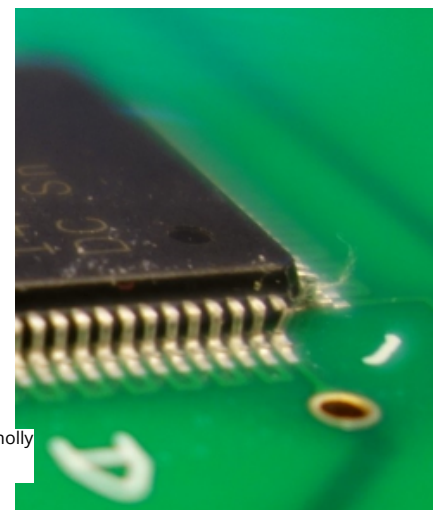
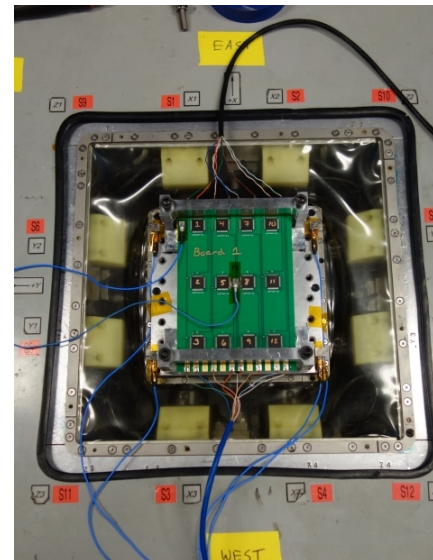
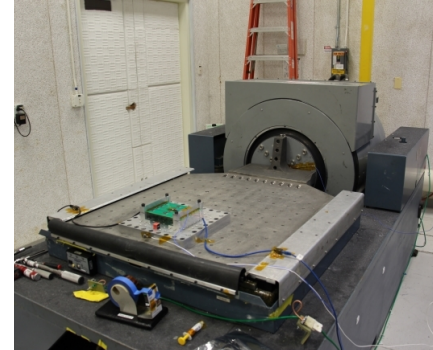
KANSAS CITY NATIONAL SECURITY CAMPUS <sup>(3)</sup>

IMAC 2023



Sandia National Laboratories is a multimission laboratory managed and operated by National Technology and Engineering

Sandia, LLC, a wholly owned subsidiary of Honeywell International Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525.



SAND2023-12282C

# Motivation & Background

---

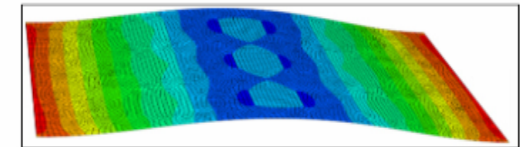
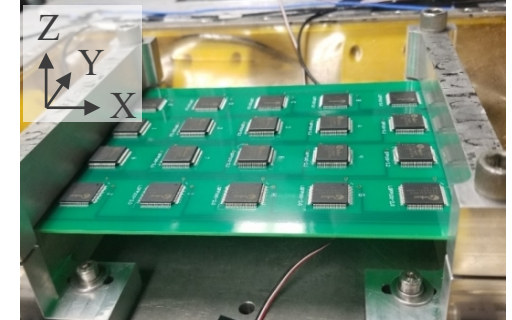
- Dynamic field environment may not be represented well by a single-axis shaker test
  - System component boundary conditions and impedances are ignored
  - Laboratory testing may contain different boundary conditions
- Evidence of difference in fatigue life and failure modes when comparing multiple-degree-of-freedom (MDOF) and single-degree-of-freedom (SDOF) testing (*Gregory, D., Bitsie, F., Smallwood, D.O.*)
- Aim to understand how MDOF and SDOF testing affect component time to failure (TTF)
- Different internal boundary conditions of a SDOF shaker and MDOF shaker
  - SDOF: other five degrees of freedom are constrained
  - MDOF: allows the armature to move unconstrained in the other degrees of freedom



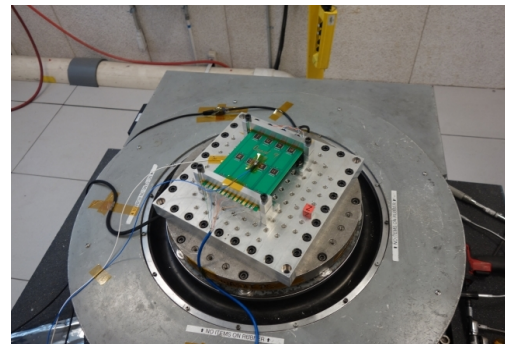


# Testing Approach

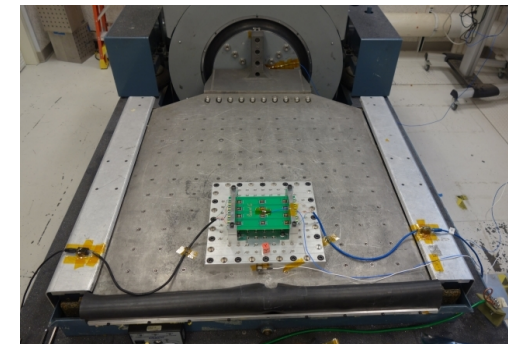
- Initial testing began at KCNSC and the University of Maryland
  - TE6-900 shaker with X and Z excitation
  - Similar printed wiring assembly (PWA) board in a clamped-clamped fixture
- Testing on both **UD T1000 (1DoF)** shakers and **TE6-900 (6DoF)** shaker
  - Single-axis excitation on T1000 (*1DoF*)
  - Single-axis excitation on TE6-900 (*6DoF, unconstrained translation/rotation*)
  - Tri-axis excitation on TE6-900 (*6DoF, unconstrained rotation*)
- Frequency ranges:
  - 100-400 Hz
  - 100-2000 Hz
- 5 g<sub>RMS</sub> per axis



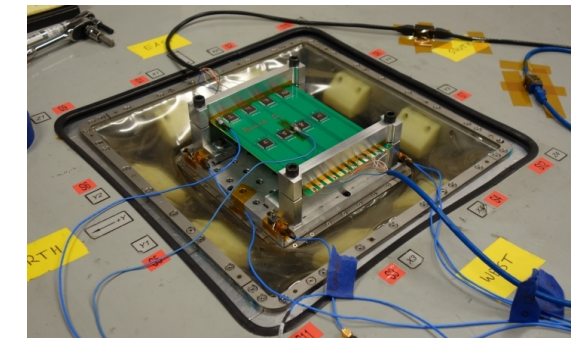
FEA model and PWA board from KCNSC



UD T1000 (Z-axis excitation tests)



UD T1000 (slip table, X and Y-axis excitation tests)



Team Tensor TE6-900

# 6DoF TE6-900 Shaker Setup

## Hardware

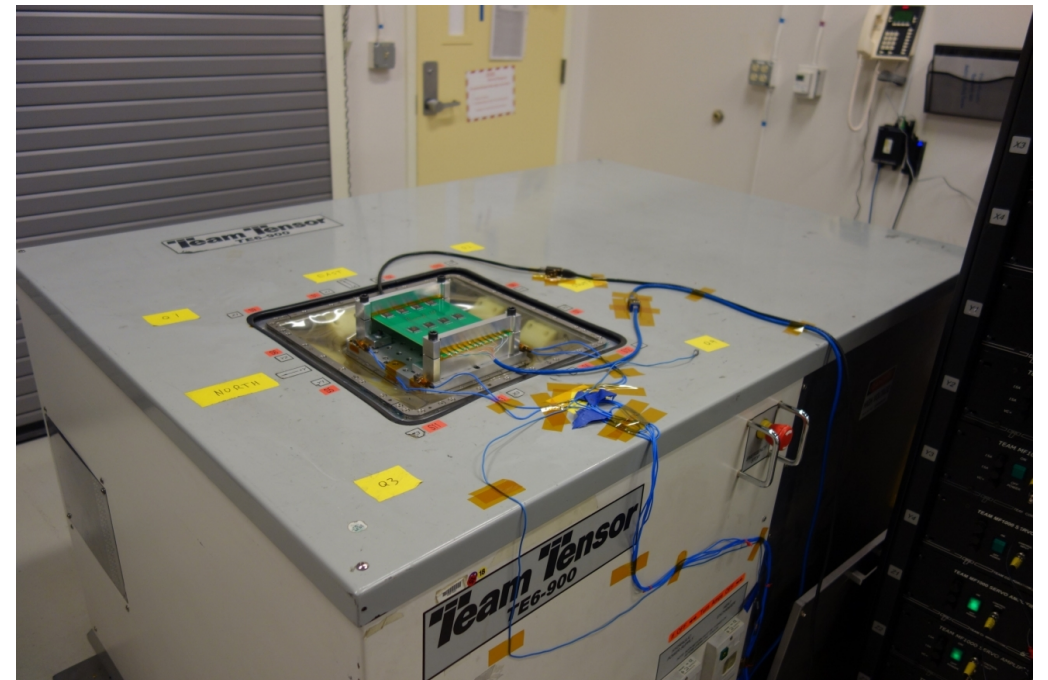
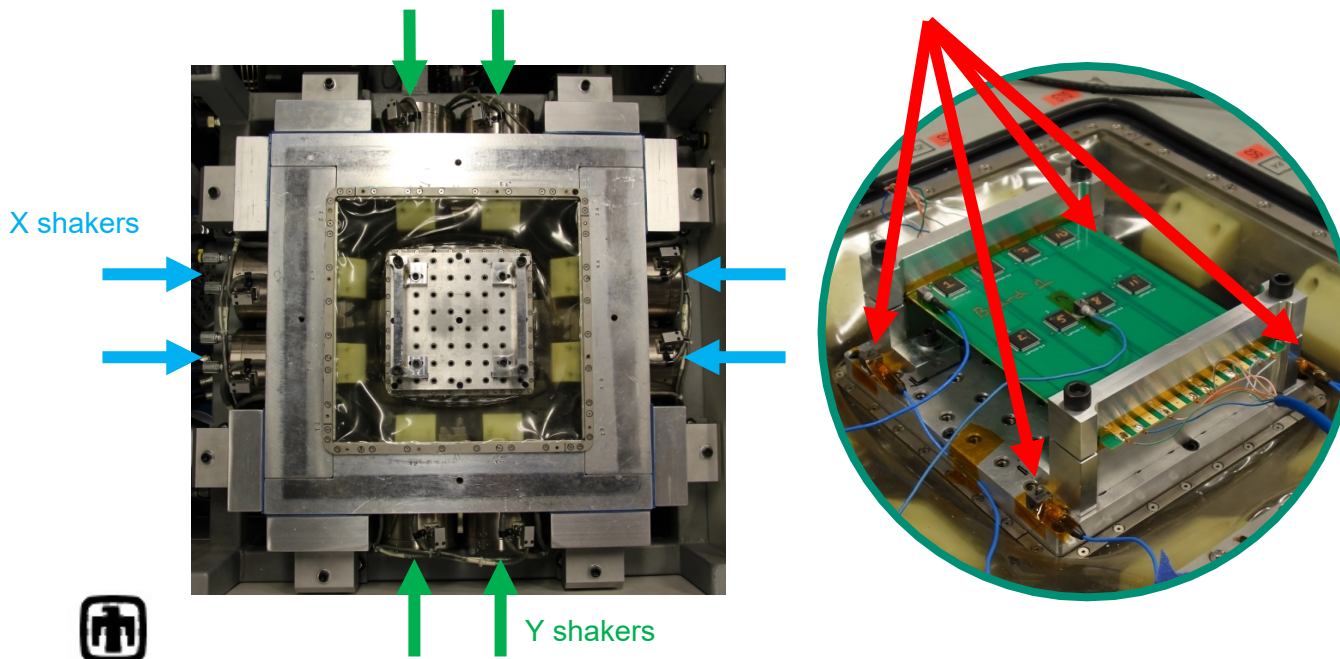
- Team Tensor TE6-900
- National Instruments PXIe Chassis
  - Accelerometer input
  - Drive voltage output
- Tri-axis base control accelerometers on corners of table



NI Chassis



Amplifier rack

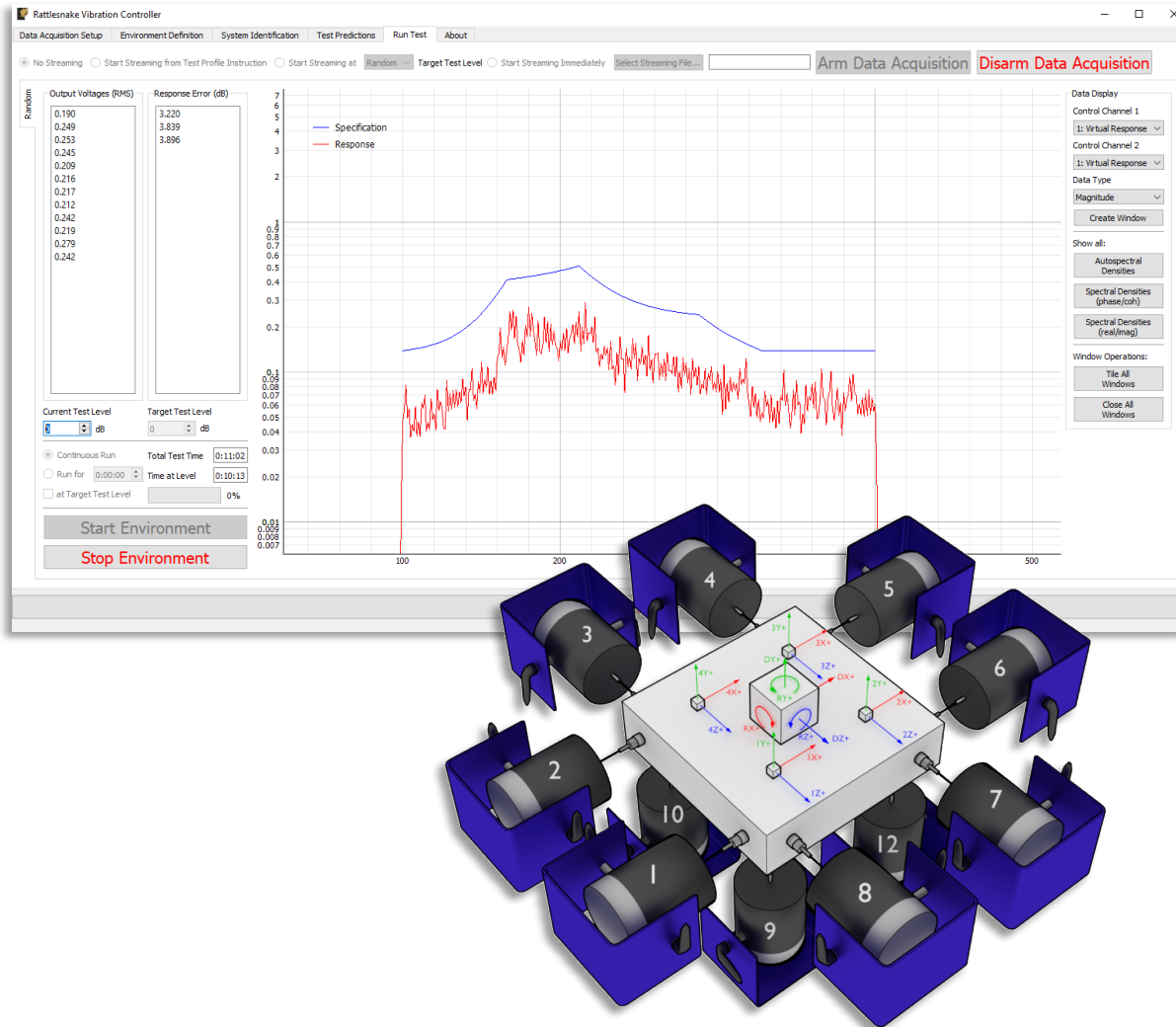


Team Tensor TE6-900





# Shaker Software Setup



## Rattlesnake Vibration Controller

- Python based multi-input-multi-output (MIMO) controller
- Interfaces with NI DAQmx (also LAN-XI)
- Developed at SNL-NM by D. Rohe, et al.
- Source code available on GitHub
  - <https://github.com/sandialabs/rattlesnake-vibration-controller>

## Usage

- MIMO Random Environment
- 12 accelerometer input channels
  - 3 additional channels from board-mounted accelerometer (used for pre and post-test workmanship)
- 12 drive voltage output channels

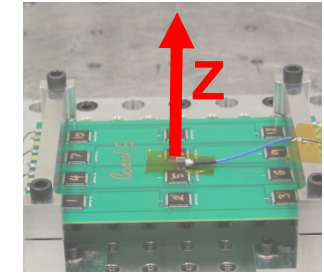
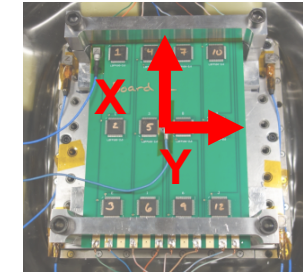
*T1000 tests run using Spectral Dynamics*



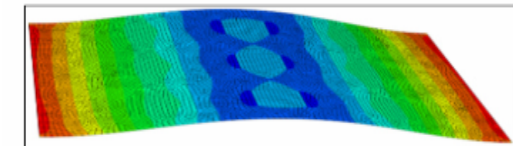


# Determining Test Specifications

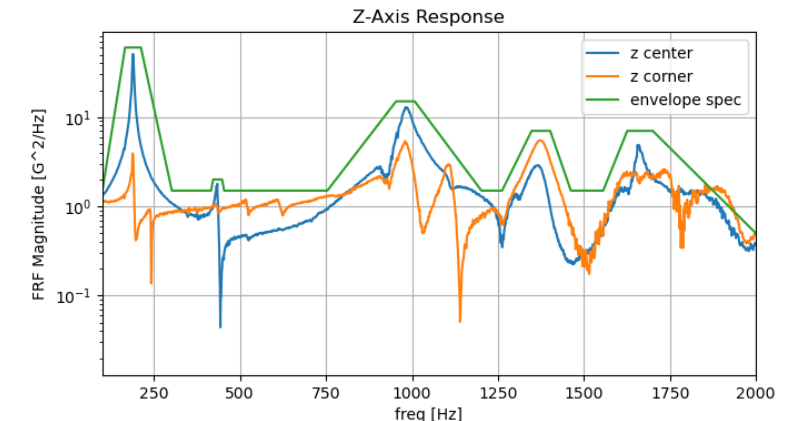
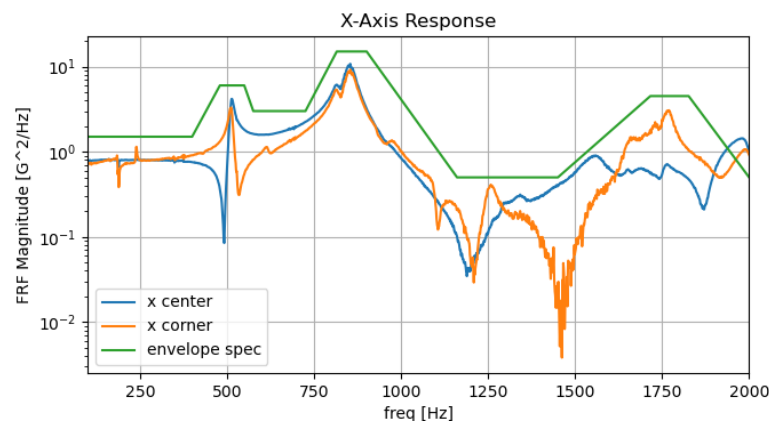
- Aiming to achieve failure with a reasonable test duration
- Ran a series of buzz tests
  - Operational modal analysis
  - X, Y, Z, and XYZ
  - 100-2000 Hz, 1.4  $g_{RMS}$  per axis
- Used buzz test response to identify modal frequencies
- Constructed an envelope to target those modes
  - Two specs, 100-400 Hz and 100-2000 Hz
  - Each spec scaled to 5  $g_{RMS}$



Mode Frequencies		
X	Y	Z
500 Hz	240 Hz	190 Hz
850 Hz	1100 Hz	980 Hz
1760 Hz	1780 Hz	1370 Hz



190 Hz bending mode



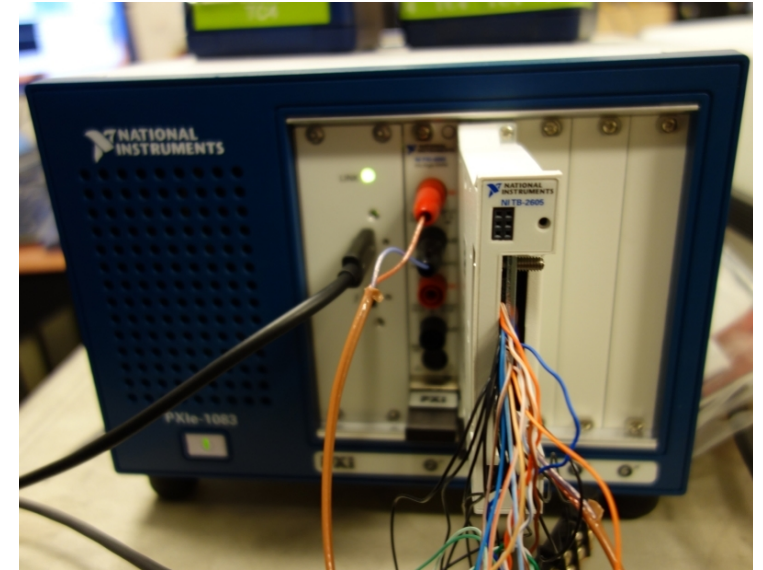
# PWA Board Data Acquisition

## Software

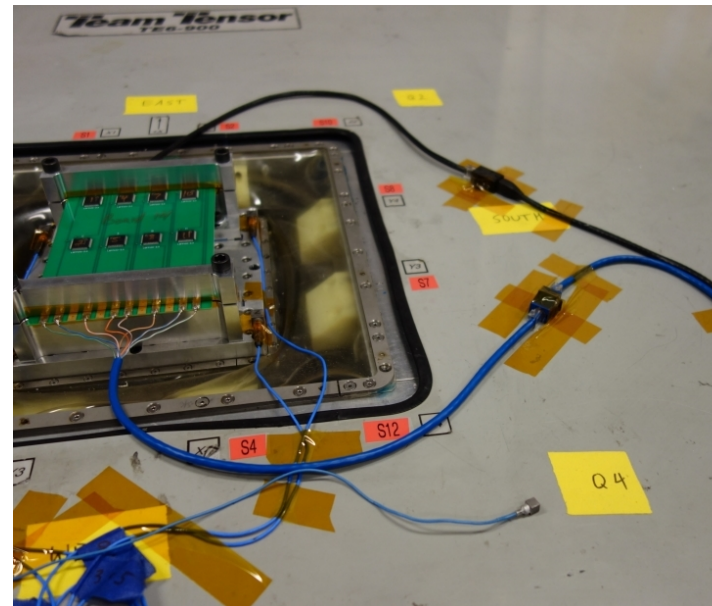
- MATLAB control script
- Measures resistance of each chip to determine failure
- Switches sequentially between 12 chips on PWA board

## Hardware

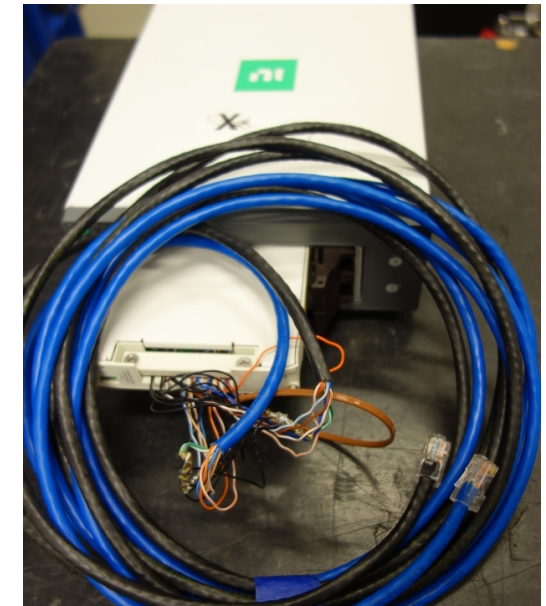
- Ethernet cabling from switch to PWA boards
- Ethernet strands soldered to contact pads
- National Instruments chassis
  - Switch – mechanical relay array
  - DMM – 2-wire resistance measurements
- Chips numbered 1-12



NI Chassis w/ switch & DMM



Ethernet connections from board to chassis

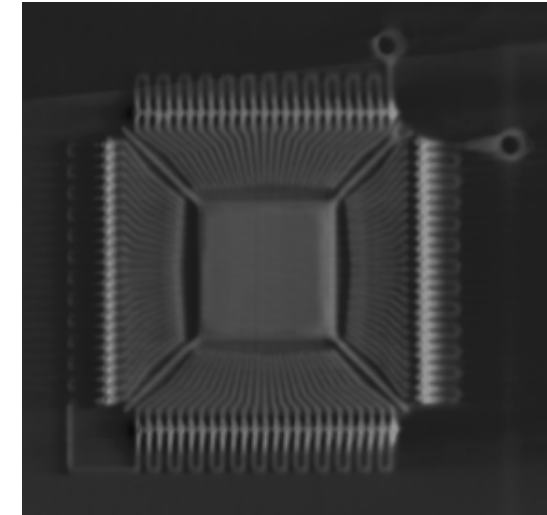


2<sup>nd</sup> NI Chassis w/ switch & DMM

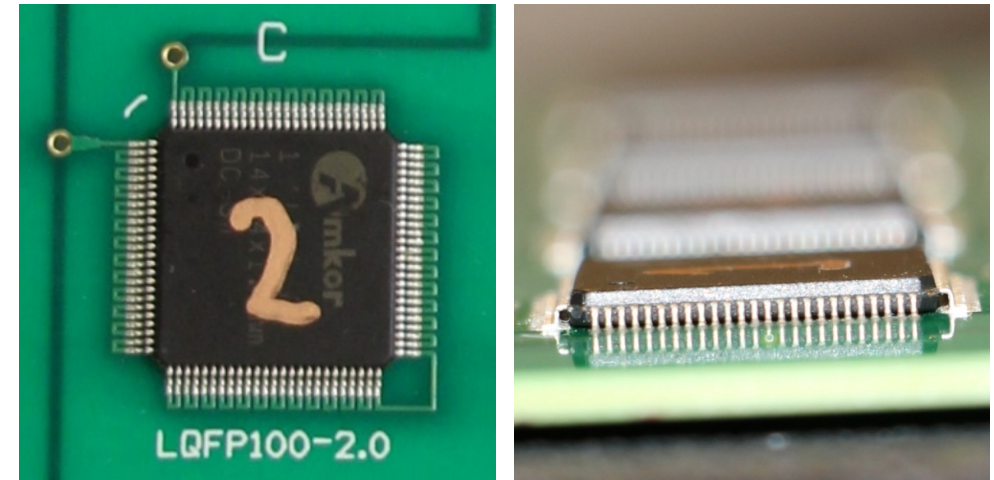


# Failure Criteria

- Observations during initial testing
  - Resistances fluctuate as chips begin to fail
    - Often return to nominal resistance even after failed readings begin to show
  - Resistance trends upward until stabilizing at a much higher reading or breaking continuity
- Resistance readings captured by data recorder dependent on length of ethernet cable
- Resistance increase indicative of chip failure
  - 100% change in nominal resistance ( $\approx 2.2 \Omega$ ) constitutes a failed reading
  - 20 consecutive failed readings constitutes a chip failure



CT scan of a single chip



top and side profile



# Completed Tests

- Certain test series abandoned following early testing
  - SDOF X-axis and Y-axis tests produced no failures
  - 100-2000 Hz tests ran upward of 6 hours
  - *Neither test series was used in further analysis due to limited data*
- Three specifications were prioritized for further testing
  - Z-axis, 100-400 Hz, T1000
  - Z-axis, 100-400 Hz, TE6-900
  - XYZ-axes, 100-400 Hz, TE6-900
- Workmanship test conducted before and after each test
  - Accelerometer in the center of the board\*
  - Check for changes in frequency response

\*removed during time-to-failure test

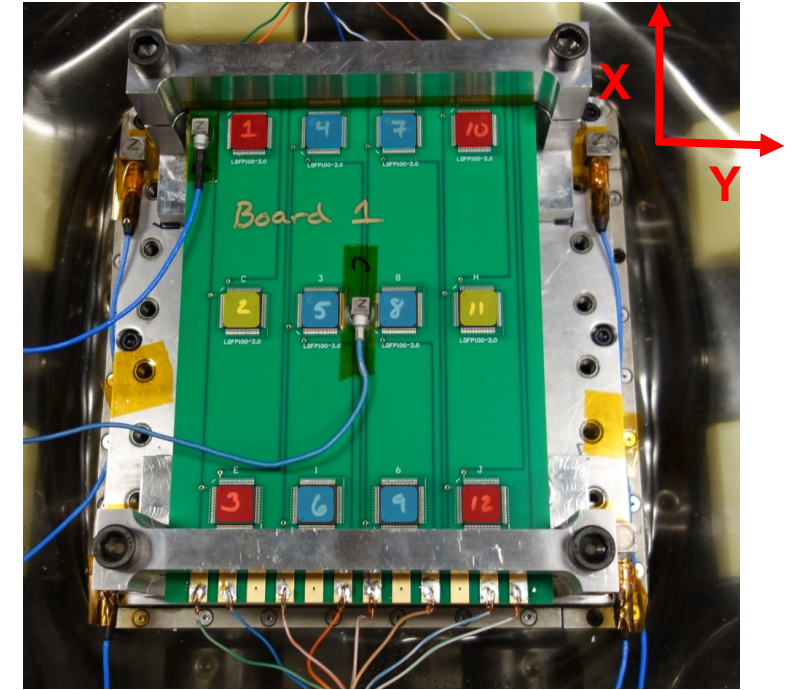
Axes	Levels	Frequency	Shaker	Duration (minutes)
Z	5 g <sub>RMS</sub>	100-400 Hz	T1000	31
Z	5 g <sub>RMS</sub>	100-400 Hz	T1000	27
Z	5 g <sub>RMS</sub>	100-400 Hz	T1000	24
Z	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	26
Z	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	39
Z	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	31
Z	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	28
Z	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	25
Z	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	28
Z	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	33
XYZ	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	52
XYZ	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	32
XYZ	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	52
XYZ	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	47
XYZ	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	31
XYZ	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	26
XYZ	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	29
XYZ	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	33
XYZ	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	32

Showing only tests included in analysis, duration refers to the time of the last chip failure

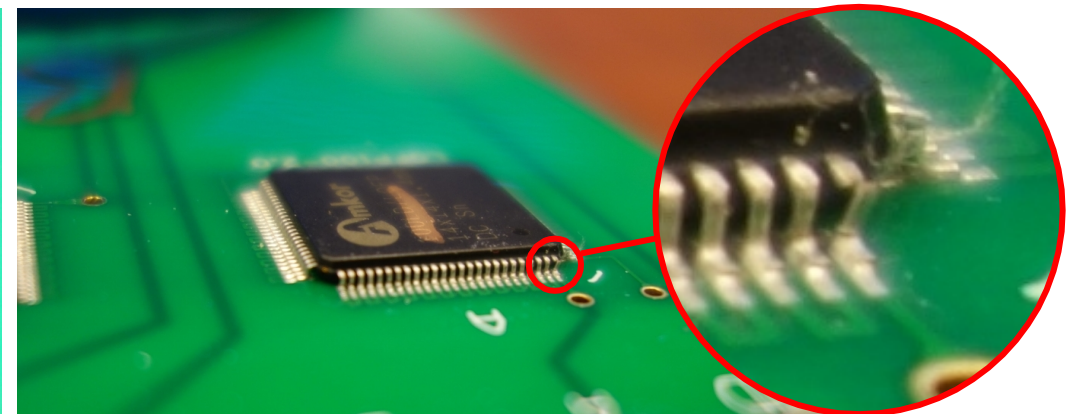
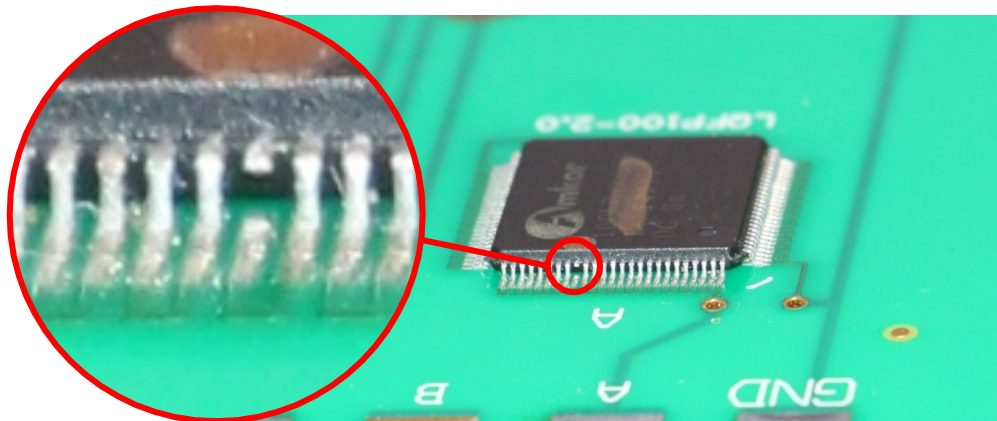


# Chip Failure Observations

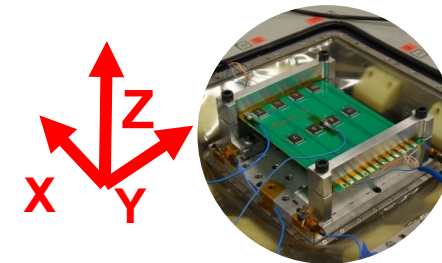
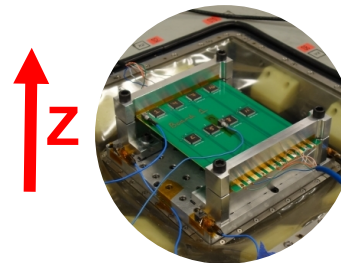
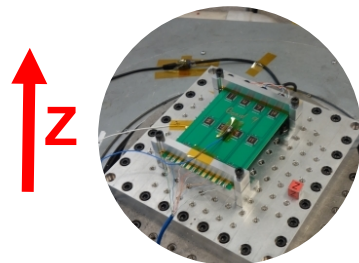
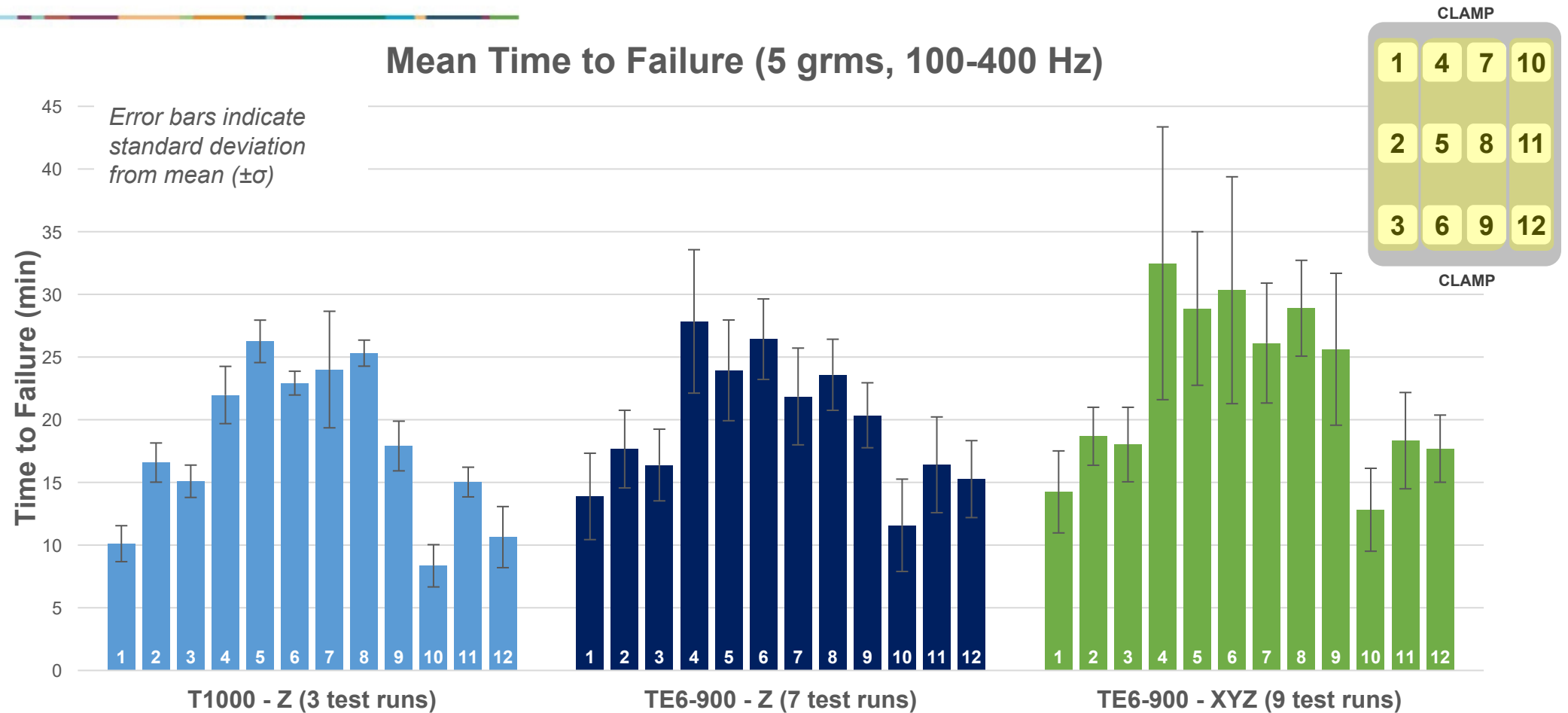
- Chip leads fatigue over the course of a few minutes
- Resistance readings fluctuate and trend upward
  - Some stabilize in the  $k\Omega$  or  $M\Omega$  range
  - Many lose continuity entirely
- Leads fail along edges parallel to clamps
- X-axis and Y-axis tests produce no failures



- First group to fail
- Second group to fail
- Third group to fail



# Test Results – Mean Time to Failure



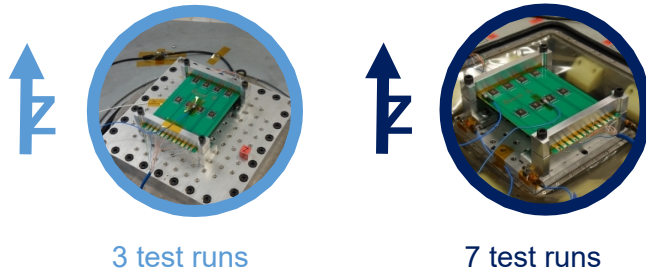
Red axis labels indicate excitation axes for each test series



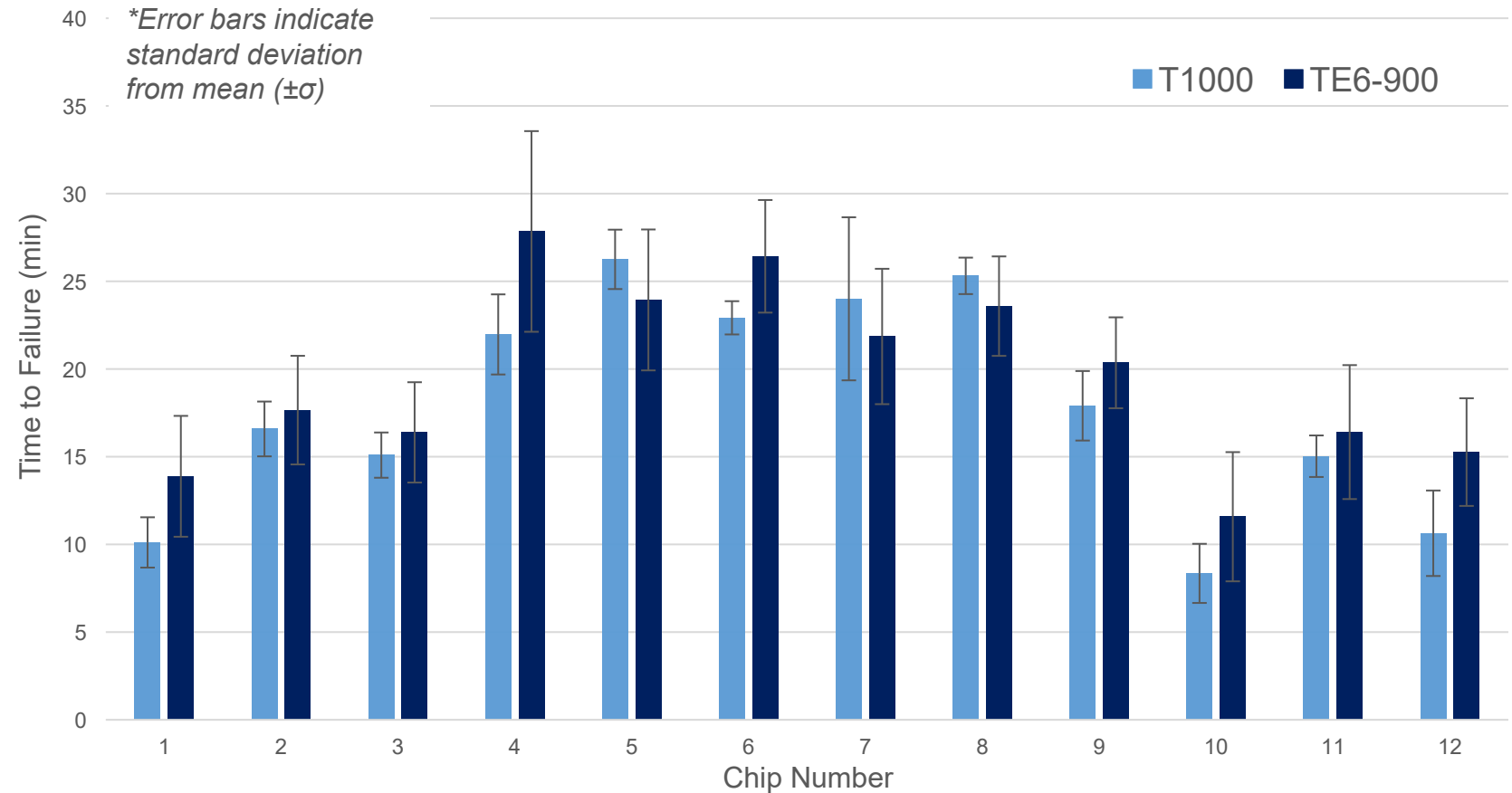
# Test Results – T1000 vs TE6-900

1	4	7	10
2	5	8	11
3	6	9	12

- Comparable results from SDOF and MDOF shakers
- Additional 5 degrees of freedom do not appear to substantially raise or lower the average TTF
- Larger deviation between tests on TE6-900



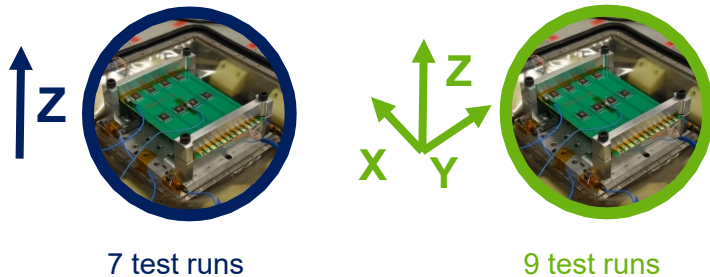
Mean Time to Failure - T1000 vs TE6-900, Z-axis excitation  
(5 grms, 100-400 Hz)



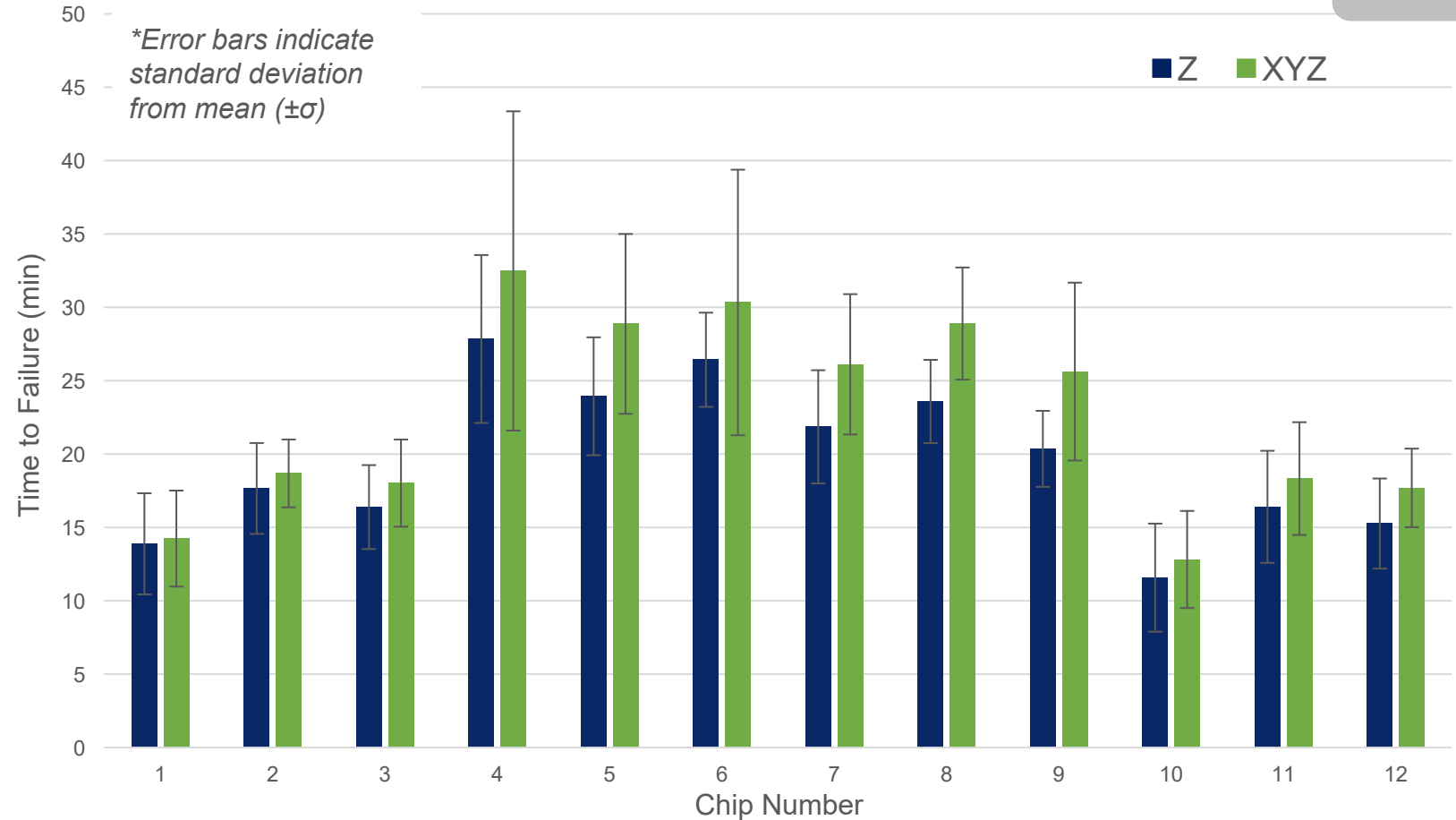
# Test Results – Z vs XYZ (TE6-900)

1	4	7	10
2	5	8	11
3	6	9	12

- Average TTF increased for every chip during 3-axis excitation compared to Z-axis excitation
- Standard deviation increase indicates less consistency among MDOF tests (particularly for chips 4-9)

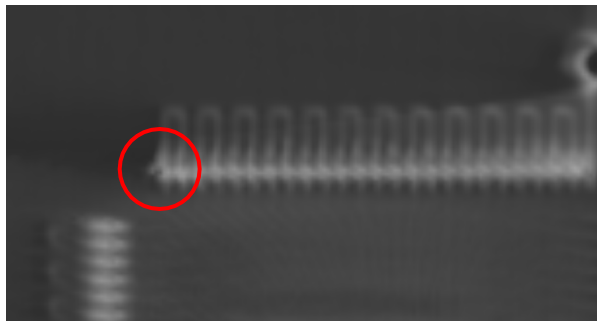
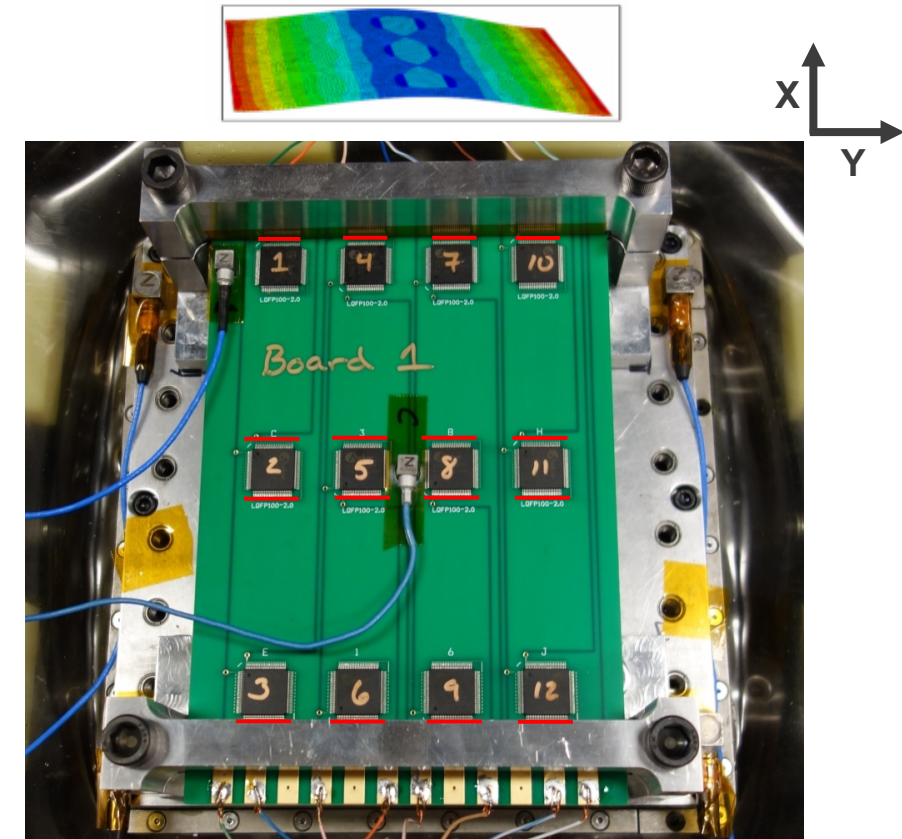


Mean Time to Failure (TE6-900, 5 grms, 100-400 Hz)

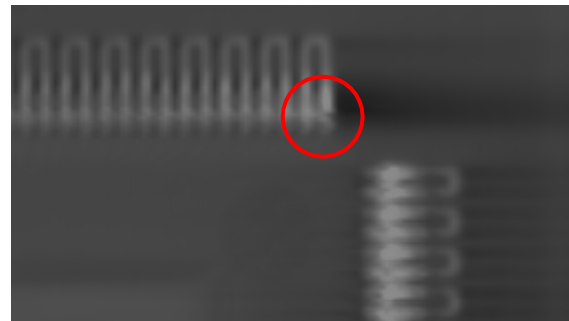


# Test Results

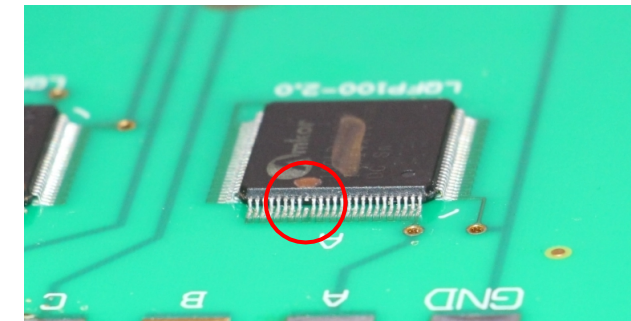
- The bending mode at 190 Hz results in maximum stress near the center and outer edges of the board where it is clamped.
- Leads fail from fatigue due to displacement from the 190 Hz Z-axis bending mode
- From inspection of boards with visible damage (bottom right) as well a CT scan of a single failed board, failures have been localized to the zones marked in red.



Broken lead along top edge of chip 10



Top left corner of chip 8

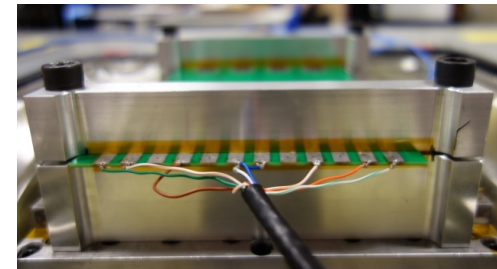


Top of chip 1



# Conclusions and Future Work

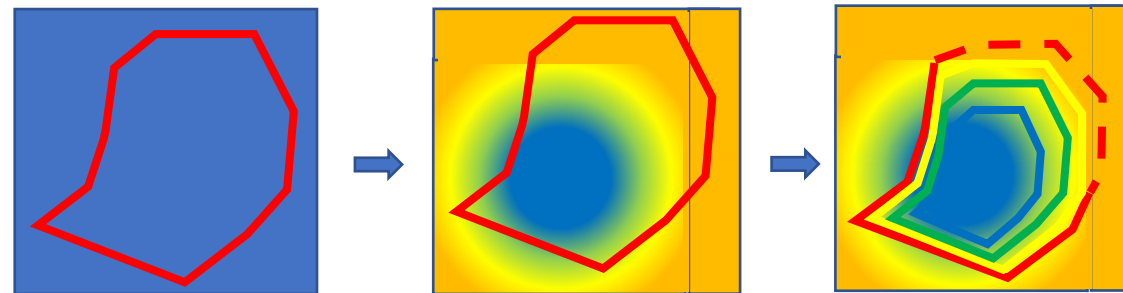
- Evidence of comparable single-axis test results on SDOF and MDOF shakers
- Increased TTF for multi-axis excitation tests, particularly for certain chips
  - Sequential axis testing appears to be more conservative than simultaneous
- Expand test parameters to possibly include:
  - Higher  $g_{\text{RMS}}$  levels
  - Temperature variation
  - Different fixturing
  - Include rotational specifications
- Performance Envelopes
  - Future Goal: Construct accurate component performance envelopes using MDOF shaker



Current clamp fixtures



Team Tensor 18kN



+confidence in analysis  
& testing techniques

+UQ in performance

# Acknowledgements

---

Paul Titus

Michael Denison

Adam Mitchell

SNL Vibration Test Lab

Sandia National Labs

Kansas City National Security Campus





# Questions?



# References

---

1. Mayes, R.L., Lopp, G.K., Paripovic, J., Nelson, G.D. Schultz, R.A., Testing a Component on a Fixture to Reproduce System Accelerations. In *Proceedings of the 65<sup>th</sup> Institute of Environmental Sciences and Technology Conference*, Las Vegas, Nevada, 2019
2. Berman, M.B. “Inadequacies in Uniaxial Stress Screen Vibration Testing.” *Journal of the IEST*, Vol. 44, No. 4, Fall 2001, pp. 20-30.
3. French, R.M., Handy, R., and Cooper, H L. “Comparison of Simultaneous and Sequential Single Axis Durability Testing”, *Experimental Techniques*, Vol. 30, No. 5, September/October, 2006, pp. 32-37.
4. Gregory, D., Bitsie, F., Smallwood, D.O. “Comparison of the Response of a Simple Structure to Single Axis and Multi Axis Random Vibration Inputs”, Technical report, Sandia National Lab. (SNL-NM), Albuquerque, NM, USA 2009.
5. Daborn, P. M., Ind, P. R., and Ewins, D. J. “Replicating Aerodynamic Excitation in the Laboratory”, *Topics in Modal Analysis*, Volume 7. Springer, New York, NY, 2014. 259-272.
6. Beale, D., Owens, B., and Schultz, R. “Analysis of IMMAT Full-Field Responses”, Technical report, Sandia National Lab. (SNL-NM), Albuquerque, NM, USA 2019.





# Appendix

# All Tests Completed to Date

Axes	Levels	Frequency	Shaker	Duration (H:M:S)
X	5 g <sub>RMS</sub>	100-400 Hz	T1000	6:00:00
Y	5 g <sub>RMS</sub>	100-400 Hz	T1000	6:00:00
Y	5 g <sub>RMS</sub>	100-2000 Hz	T1000	6:00:00
Z	3.5 g <sub>RMS</sub>	100-2000 Hz	TE6-900	4:51:37
Z	5 g <sub>RMS</sub>	100-2000 Hz	T1000	3:00:16
Z	5 g <sub>RMS</sub>	100-2000 Hz	T1000	1:36:18
Z	5 g <sub>RMS</sub>	100-2000 Hz	T1000	2:11:22
Z	5 g <sub>RMS</sub>	100-400 Hz	T1000	0:30:34
Z	5 g <sub>RMS</sub>	100-400 Hz	T1000	0:27:25
Z	5 g <sub>RMS</sub>	100-400 Hz	T1000	0:23:54
Z	3.5 g <sub>RMS</sub>	100-400 Hz	TE6-900	1:32:01
Z	3.5 g <sub>RMS</sub>	100-400 Hz	TE6-900	3:40:58
Z	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	0:25:38
Z	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	0:38:43
Z	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	0:31:02
Z	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	0:28:04
Z	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	0:25:13
Z	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	0:27:49
Z	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	0:32:52

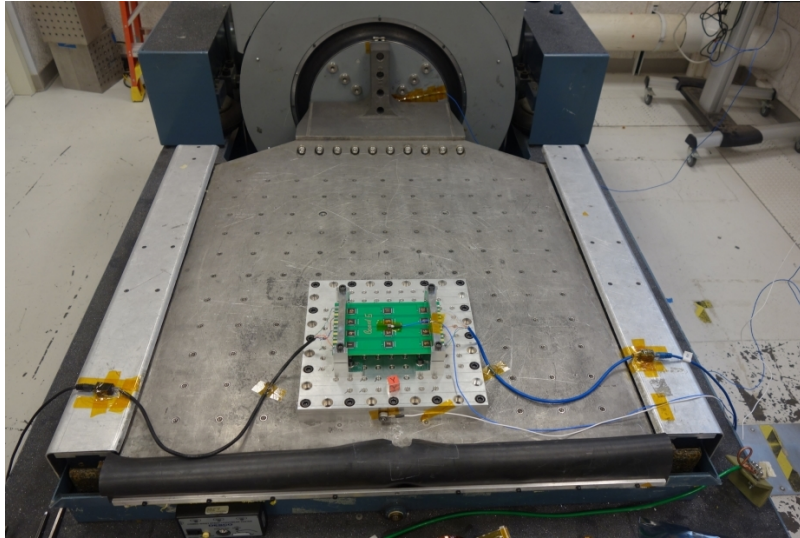
XYZ	3.5 g <sub>RMS</sub>	100-2000 Hz	TE6-900	4:00:00
XYZ	3.5 g <sub>RMS</sub>	100-400 Hz	TE6-900	3:34:52
XYZ	3.5 g <sub>RMS</sub>	100-400 Hz	TE6-900	4:36:06
XYZ	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	0:52:09
XYZ	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	0:31:46
XYZ	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	0:51:45
XYZ	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	0:46:47
XYZ	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	0:30:48
XYZ	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	0:25:58
XYZ	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	0:28:58
XYZ	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	0:33:08
XYZ	5 g <sub>RMS</sub>	100-400 Hz	TE6-900	0:32:05

Test duration listed as either TTF of final chip, or the time at which the test was manually stopped, tests used for analysis are highlighted

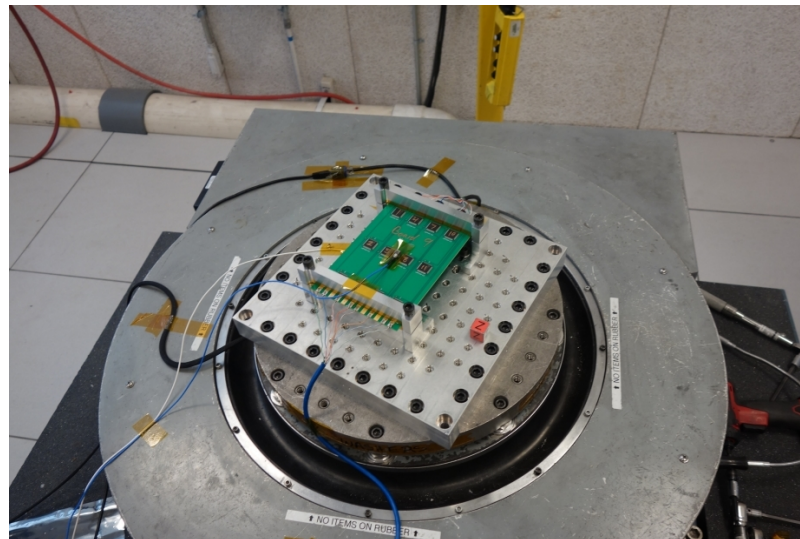
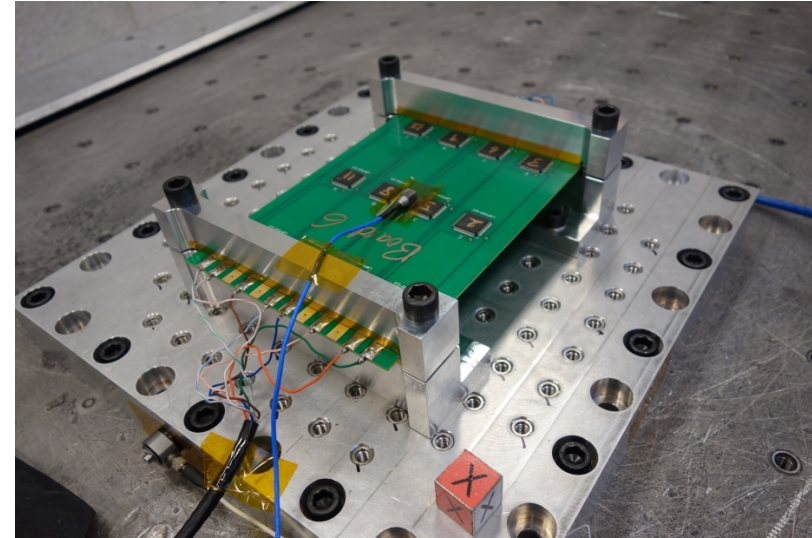




# UD-T1000 Shaker Images



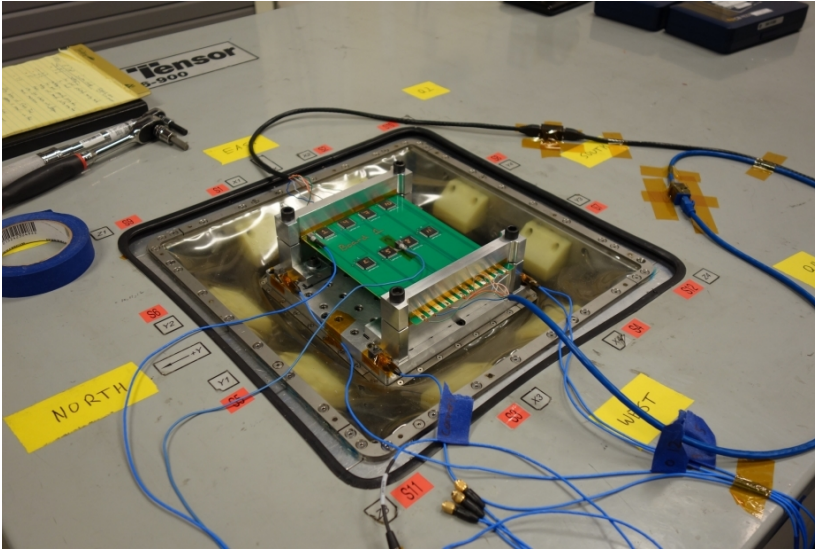
*with slip table (X and Y axis tests)*



*without slip table (Z axis tests)*

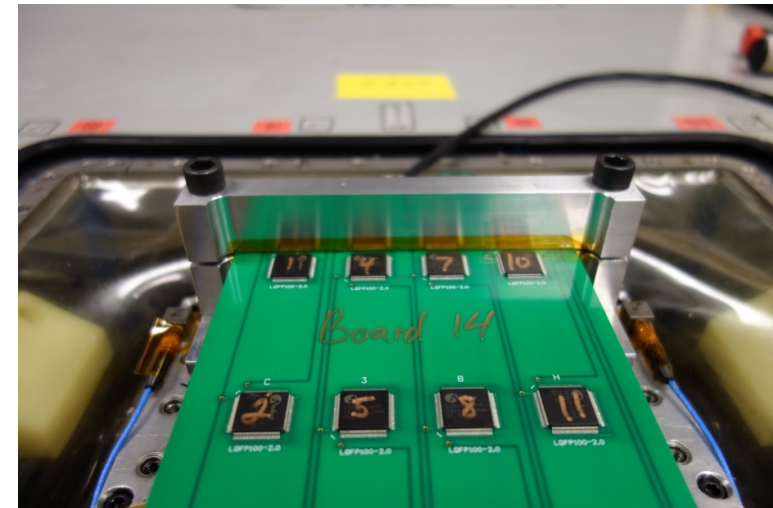
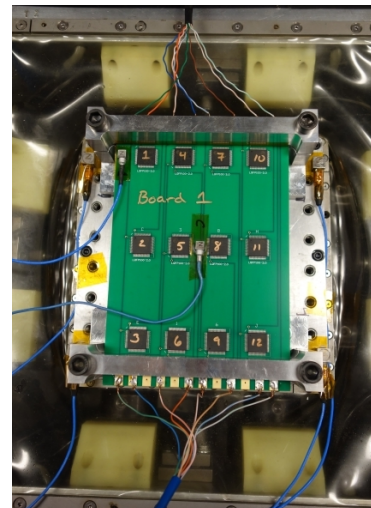
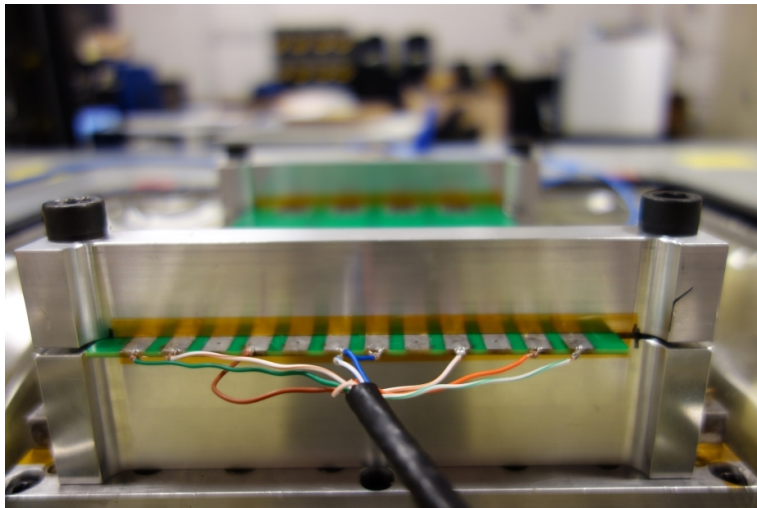


# TE6-900 Images and Specifications



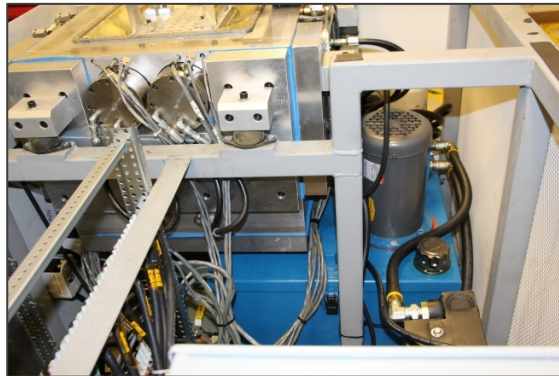
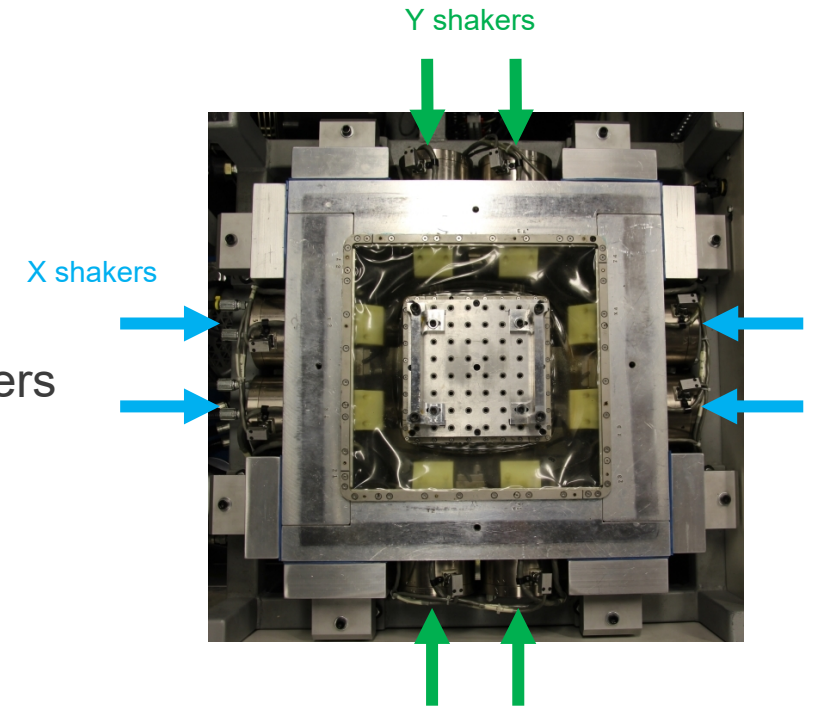
TE6-900 Specifications

	English Units	SI Units
Stroke	+/- 0.25 inch	+/- 6.4 mm
Rotation	+/- 5 deg.	.09 rad.
Velocity	60 in/sec	1525 mm/sec
Force	200 lbf	890 N
Table Wt.	9.02 lbs	4.09 kg

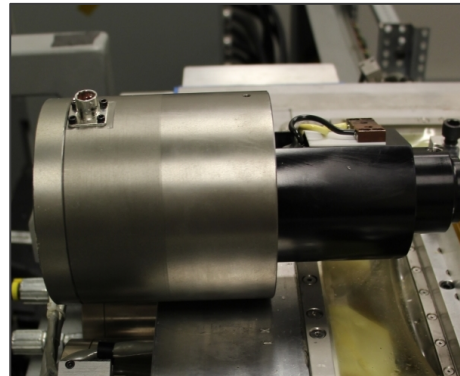


# 6DoF Shaker Operation

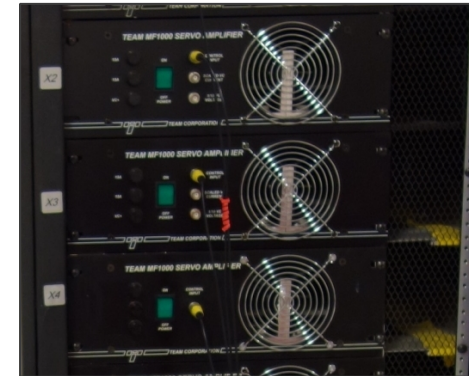
- 12 shakers, 4 per axis
- Hydraulic reservoir and pump located beneath shakers
- Hydraulic oil supplies cooling, bearing lubrication, and preload to shakers
- 3-phase power input supplies power to hydraulics, heat exchanger, shakers, and amplifiers



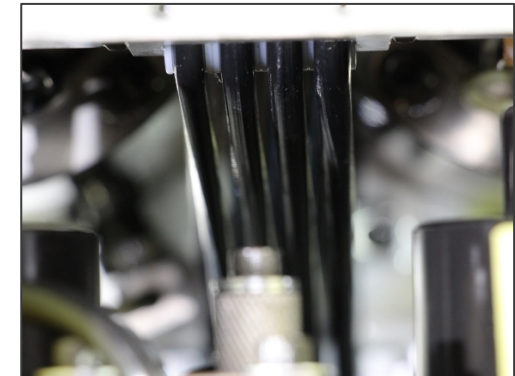
Hydraulic pump



Individual shaker removed from assembly



Amplifiers



Elastic cords holding table down, providing Z-axis pre-load



# Rattlesnake Configuration

Select Controller Type ? X

☒ MIMO Random Vibration  
☐ MIMO Transient  
☐ Time Signal Generation  
☐ Combined Environments...

OK Cancel

Data Acquisition Parameters

Hardware Selector: NI DAQmx Sample Rate: 8192 Time per Read: 0.75 Time per Write: 0.75

Sampling Parameters

Sample Rate	Samples Per Frame	Samples Per Acquire	Frame Time
2048	2048	1024	1.00
Nyquist Frequency	FFT Lines	Frequency Spacing	Test Level Ramp Time
1024.00	1025	1.00	0.50

System ID Parameters

Averaging Type	System ID Averages	Averaging Coefficient	FRF Technique
Linear	50	0.100	H1
FRF Window	Overlap Percentage	System ID RMS Voltage	Update TF During Control?
Hann	50.00	0.100	<input type="checkbox"/>

Signal Generation Parameters

COLA Window	COLA Overlap %	Window Exponent	Samples per Output
Tukey	50.00	0.50	1024

Control Parameters

Frames in CPSD	Input Channels	Control Channels	Output Channels
20	24	12	12
CPSD Window	Transform Channels	Transform Outputs	Transformation Matrices...
Hann	3	12	

Control Python Script

ake/control\_laws/buzz\_shape\_constraint.py Load

Control Python Function

buzz\_shape\_constraint\_control Class

Control Parameters

0.1

Form

Transformation Matrices

Response Transformation Matrix Add Row Remove Row Save

	1	2	3	4	5	6	7	8	9	10	11	12
1	0.25	0.0	0.0	0.25	0.0	0.0	0.25	0.0	0.0	0.25	0.0	0.0
2	0.0	0.25	0.0	0.0	0.25	0.0	0.0	0.25	0.0	0.0	0.25	0.0
3	0.0	0.0	0.25	0.0	0.0	0.25	0.0	0.0	0.25	0.0	0.0	0.25

