



Exceptional service in the national interest

Operational Analysis of a Structure with Intermittent Impact

Submission #14282

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Outline

- Motivation
- Structure Configurations & Testing
- Finite Element Model
- Operational Deflection Shapes Implementation
- ODS Results
- Conclusions



Motivation

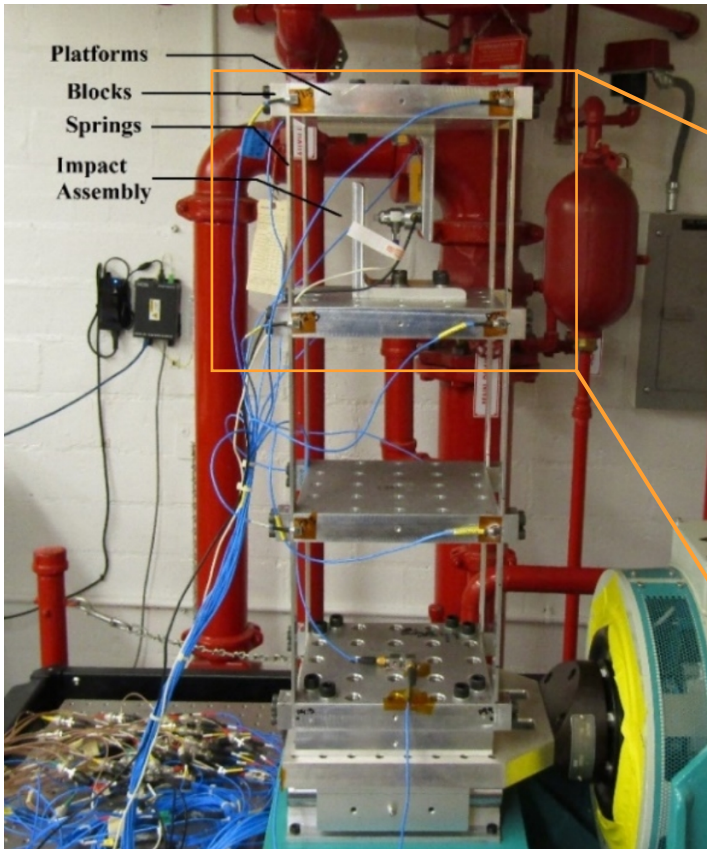
- Modal parameters give key insight regarding structural response to dynamic excitation
 - Also are an important step in model validation and calibration
- Modal testing is not always a priority
- Vibration data can be used to *estimate* modal parameters when modal testing not possible
- We do this by calculating operational deflection shapes (ODS)
 - However, nonlinear response and high level of excitation may affect these predictions

We are using an academic structure to investigate the effects of intermittent impact and varying levels of excitation on ODS!

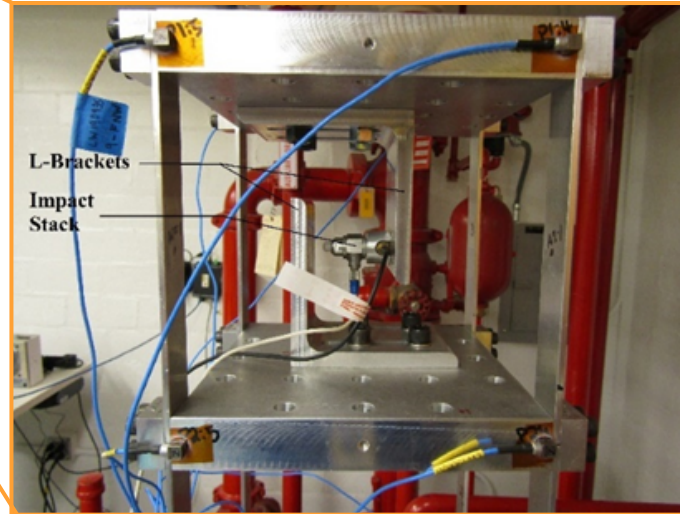


Structure Configurations and Testing

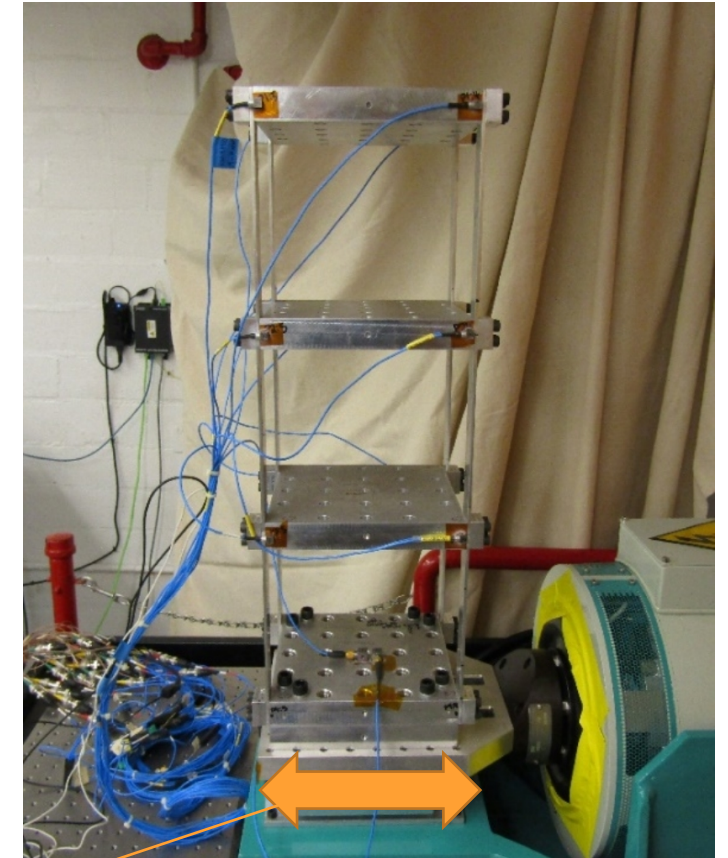
Structure designed to respond with intermittent impact and was vibration tested at various excitation levels (0.57 Grms to 3 Grms)



Structure with impact assembly



Closeup of impact assembly



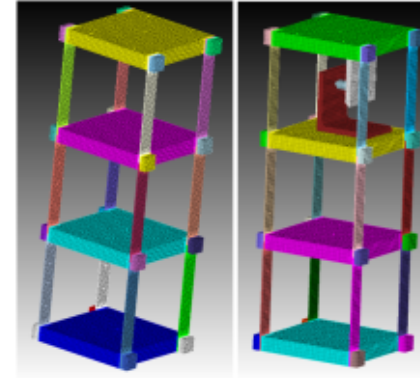
Direction of vibration

Structure without impact assembly

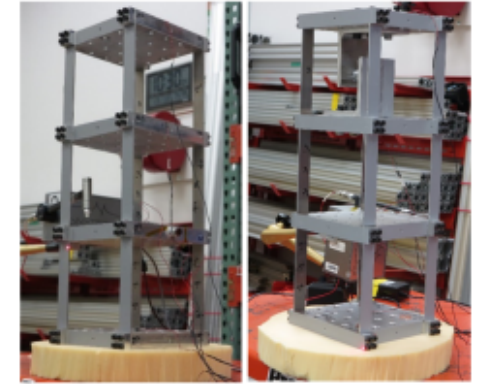


Finite Element Model Calibration

- Ideally modal testing would be done to serve as “true” mode shapes and frequencies
- Ironically, schedule didn’t allow for this
- Instead we compared to finite element model
 - Used existing LDV modal data for structure in free-free boundary condition to calibrate the FEM

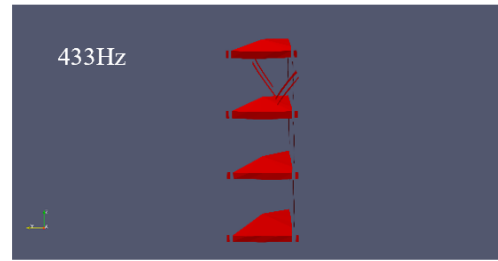
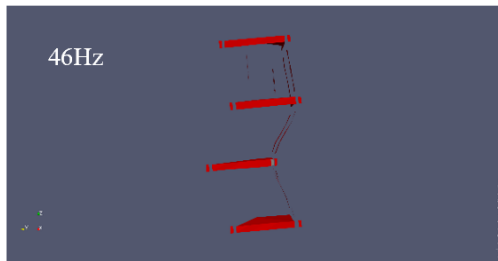


Finite Element Models

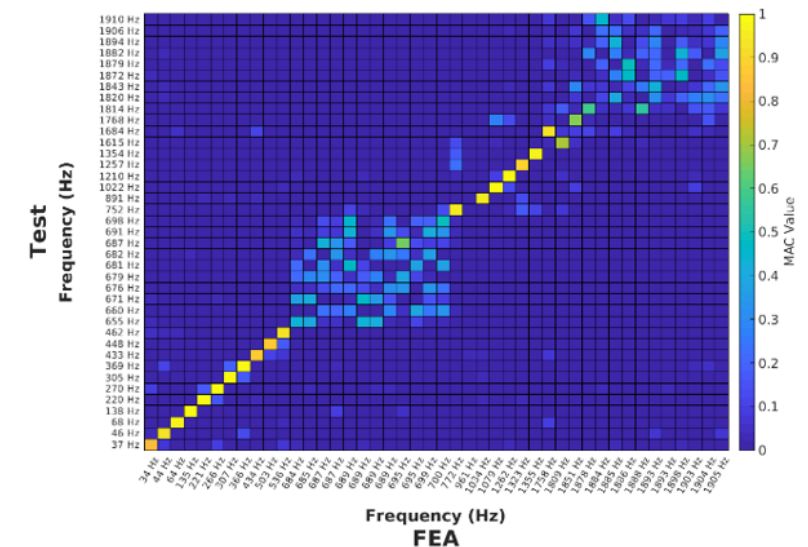
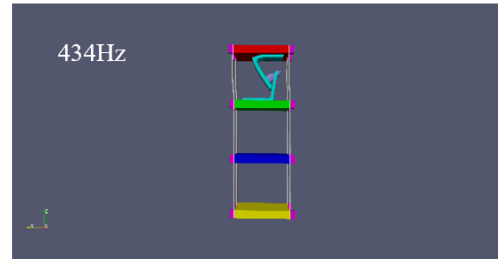
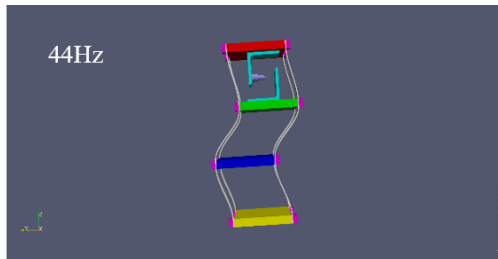


Free-Free Modal Test

Modal Test Mode Shapes



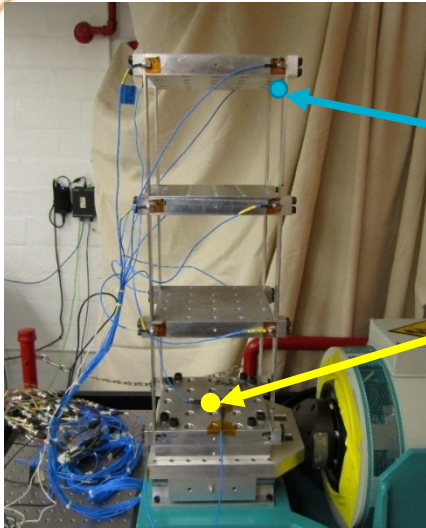
FEM Mode Shapes



MAC showing model calibration



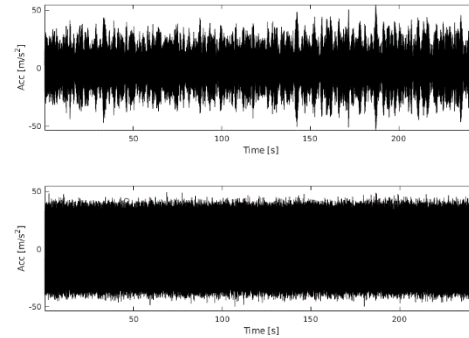
ODS Calculation Process



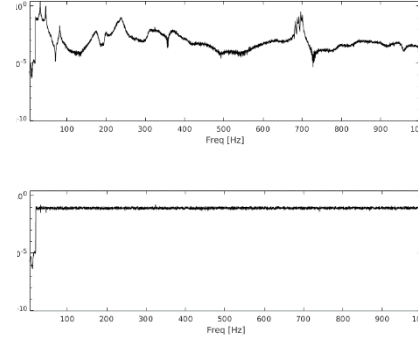
Response Node

Reference Node

Time Response



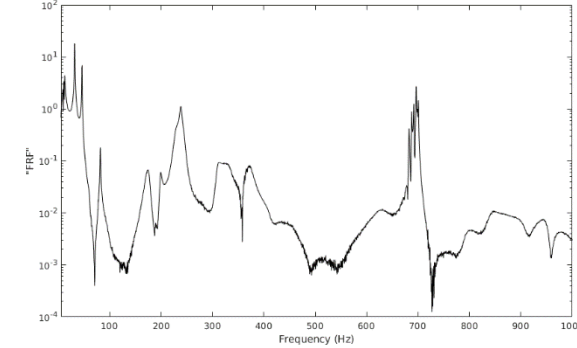
Frequency Response



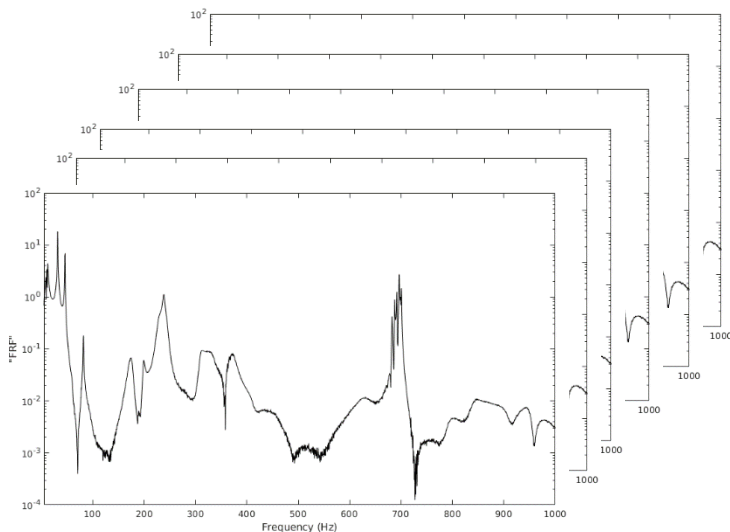
Averaged



Transfer Function
aka "FRF"

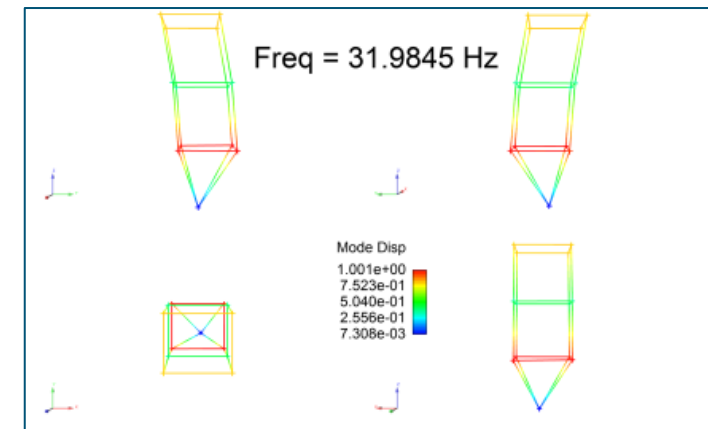
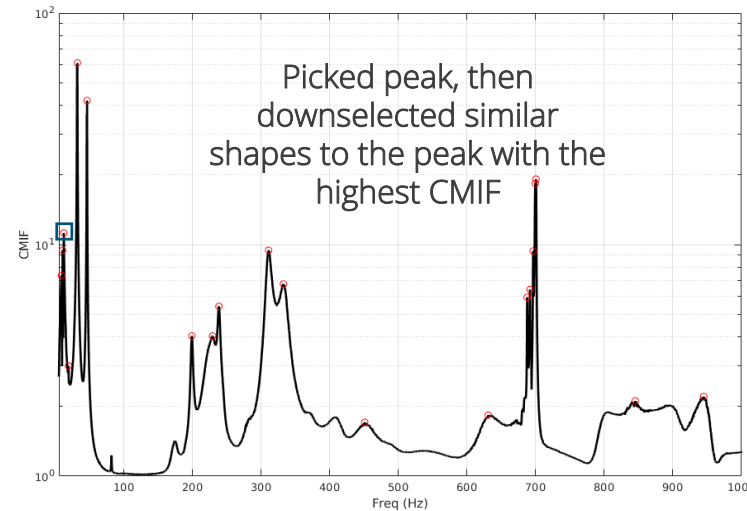


"FRF" at each measurement location



SVD

Complex Mode Indicator Function
(CMIF)





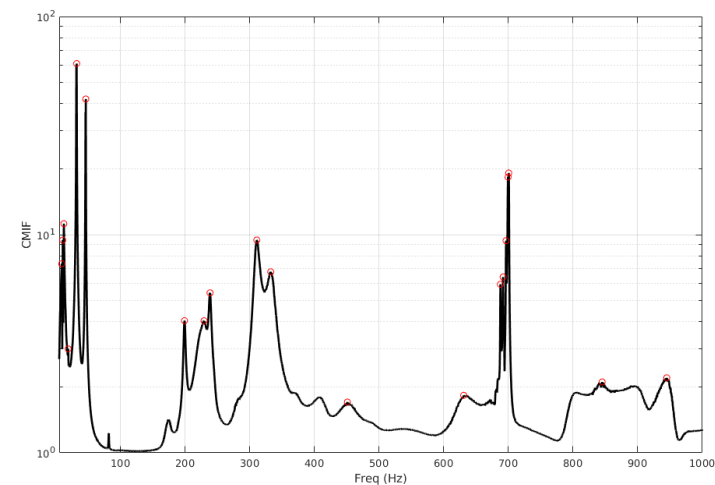
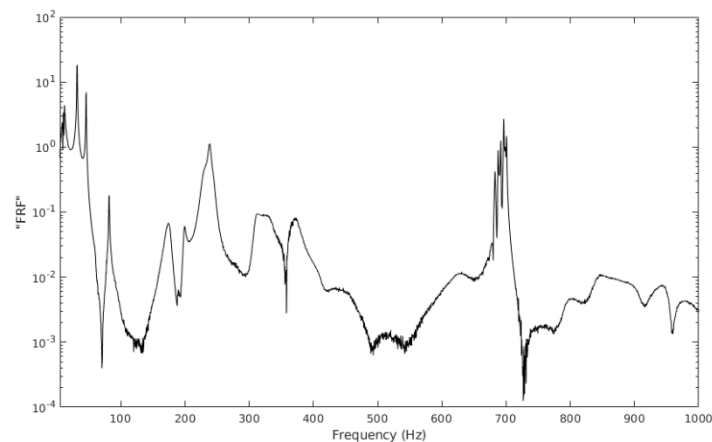
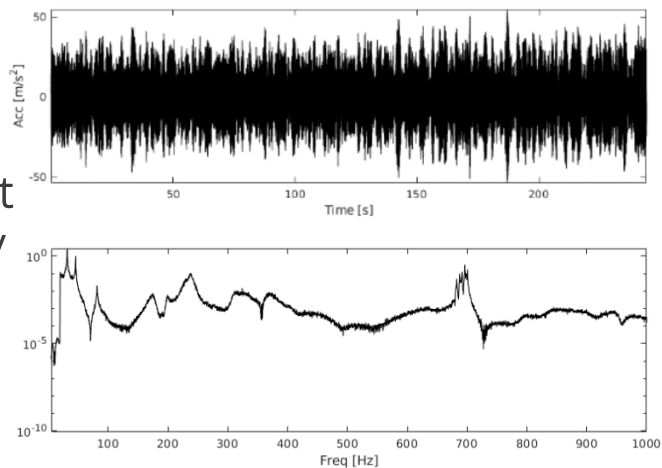
CMIF Comparison

Measurement

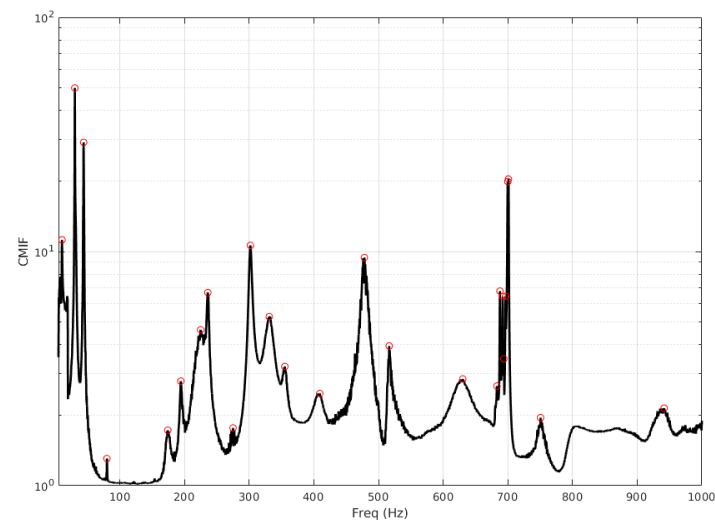
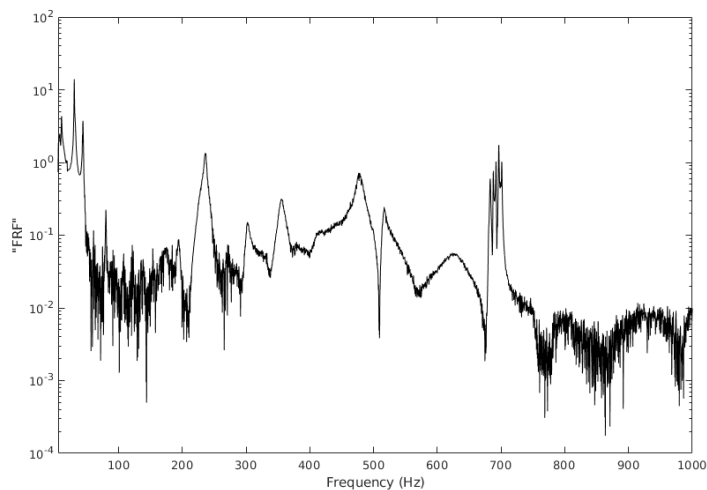
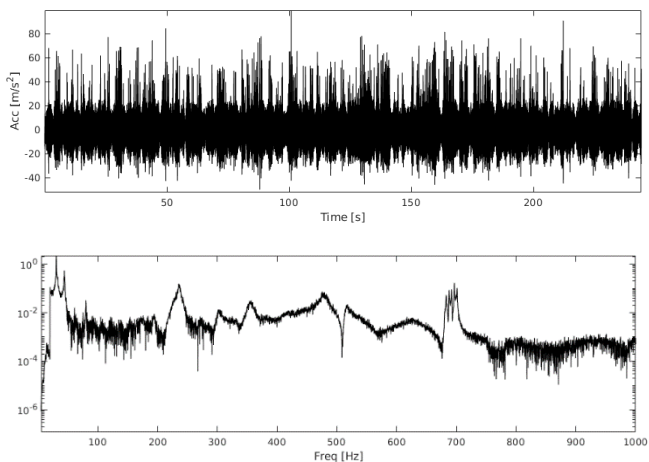
"FRF"

CMIF

No Impact
Assembly



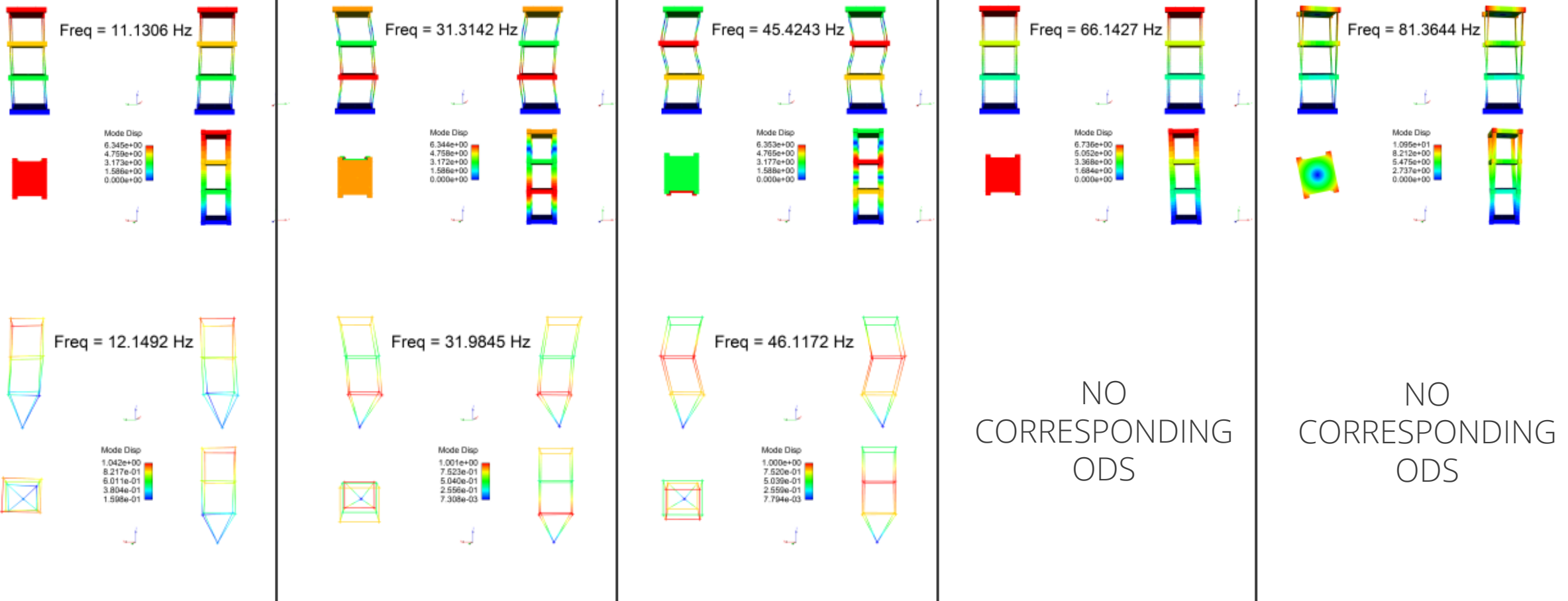
Impact
Assembly





ODS vs. FEM Shapes – No Impact Assembly (1.5 Grms)

FEM

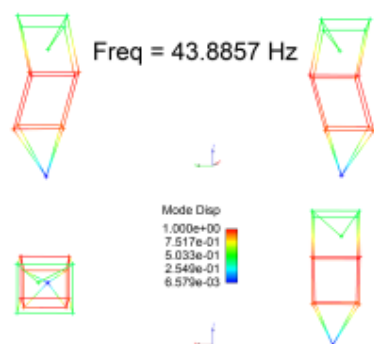
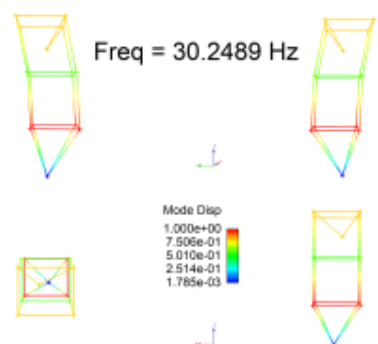
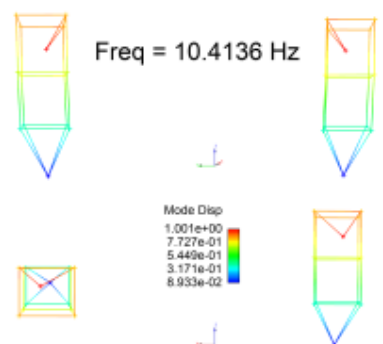
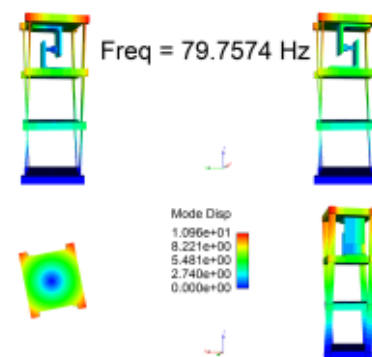
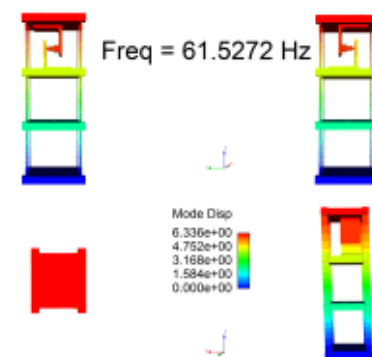
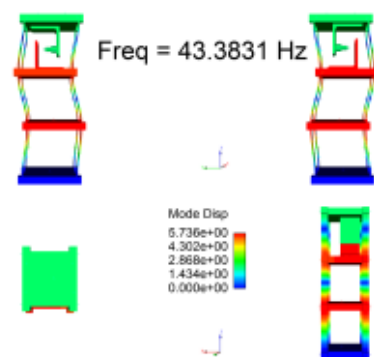
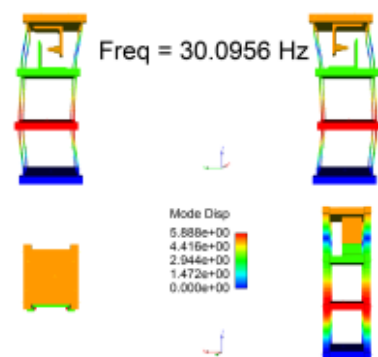
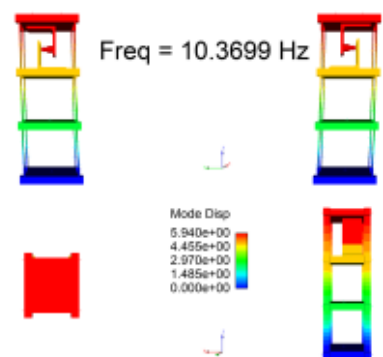


ODS

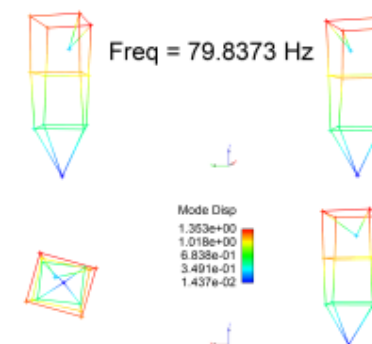


ODS vs. FEM Shapes – With Impact Assembly (1.5 Grms)

FEM



NO
CORRESPONDING
ODS



ODS



ODS vs. Finite Element Model

- Tables show ODS that are consistent with FEM mode shapes
- Note that ODS for structure WITH impact assembly has fewer missing mode predictions

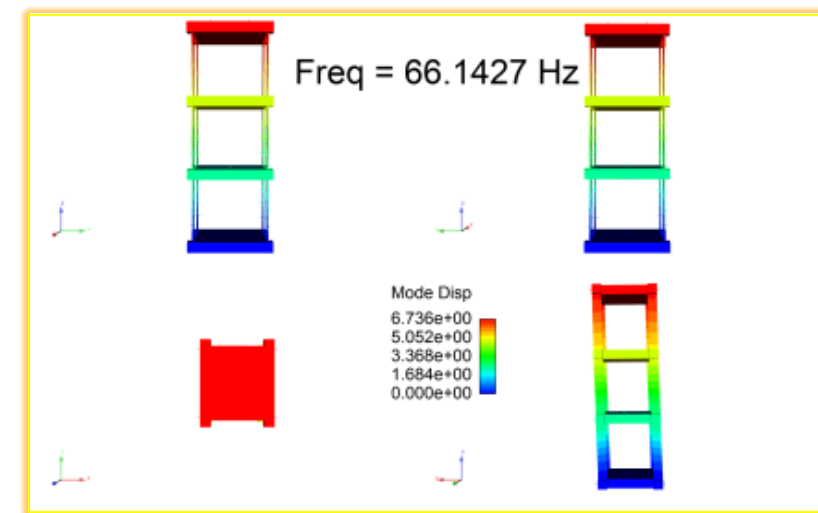


Table 4 High consistency frequencies for structure with impact assembly

| - | Finite Element Model | ODS: 0.57Grms | ODS: 0.95Grms | ODS: 1.06Grms | ODS: 1.5Grms | ODS: 2.12Grms | ODS: 3Grms |
|------------------------|----------------------|---------------|---------------|---------------|--------------|---------------|------------|
| Modal Frequencies (Hz) | 10 | | | 11 | 10 | 10 | 11 |
| | 30 | 30 | 30 | 30 | 30 | 30 | 30 |
| | 43 | 43 | 44 | 43 | 44 | 44 | 44 |
| | 62 | | | | | | |
| | 80 | 80 | 80 | 80 | 80 | 80 | 80 |
| | 192 | 195 | 195 | 195 | 194 | 194 | 193 |
| | 235 | 236 | 236 | 236 | 236 | 236 | 236 |
| | 302 | 303 | 302 | 302 | 302 | | 301 |
| | 355 | 357 | 356 | 356 | 355 | 353 | |
| | 460 | | | | | | |
| | 486 | 480 | 479 | 480 | 478 | 478 | 476 |
| | 531 | | | | | | |
| | 684-700 | 683-701 | 683-701 | 683-701 | 683-701 | 683-701 | 683-701 |
| | 711 | 752 | 752 | 752 | 751 | 750 | 748 |
| | 821 | | | | | | |

WITH Impact Assembly

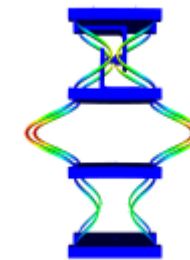
Table 5 High consistency frequencies for structure without impact assembly

| - | Finite Element Model | ODS: 0.57Grms | ODS: 0.95Grms | ODS: 1.06Grms | ODS: 1.5Grms | ODS: 2.12Grms | ODS: 3Grms |
|--------------------------|----------------------|---------------|---------------|---------------|--------------|---------------|------------|
| Natural Frequencies (Hz) | 11 | | | | | | 11 |
| | 31 | 31 | 32 | 31 | 32 | 31 | 31 |
| | 45 | 46 | 46 | 46 | 46 | 46 | 46 |
| | 66 | | | | | | |
| | 81 | | | 82 | | 82 | 82 |
| | 198 | 200 | 199 | 199 | 199 | 198 | 198 |
| | 237 | 238 | 238 | 238 | 238 | 239 | 239 |
| | 315 | 313 | 312 | 311 | 311 | 310 | 311 |
| | 361 | | | | | | |
| | 510 | | | | | | |
| | 684-700 | 688-701 | 688-701 | 688-701 | 688-700 | 688-700 | 688-700 |
| | 803 | | | | | | |
| | 831 | 846 | 846 | 843 | 845 | 844 | 842 |

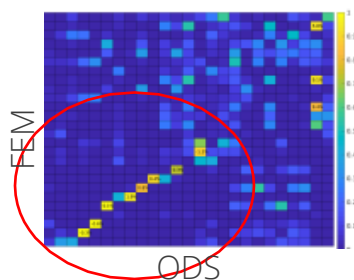
WITHOUT Impact Assembly



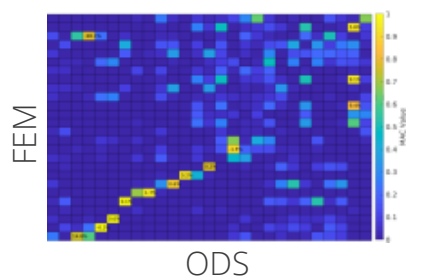
ODS vs. FEM Modal Assurance Criterion (MAC) Plots



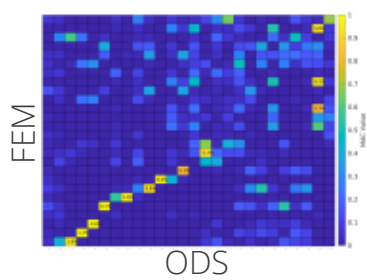
W
I
T
H



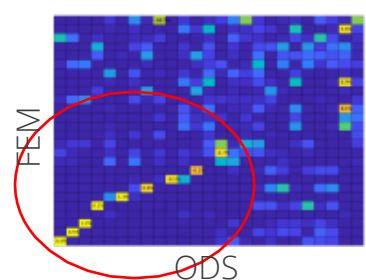
0.57 Grms



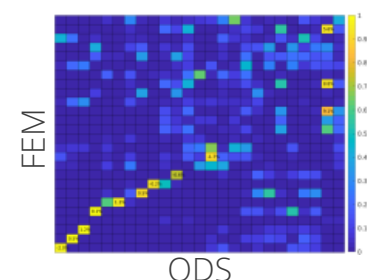
0.95 Grms



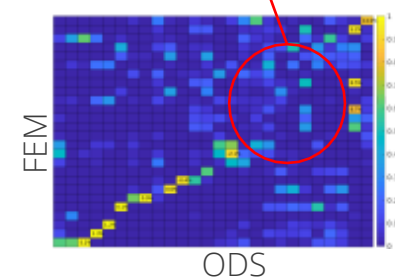
1.06 Grms



1.5 Grms

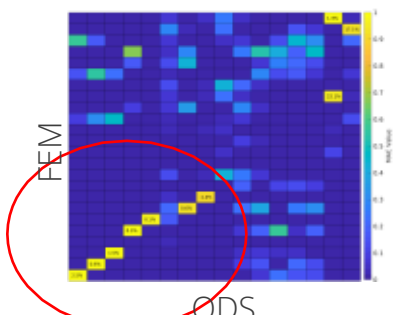
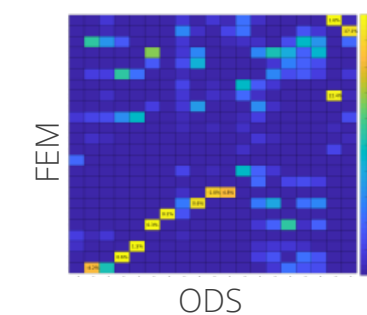
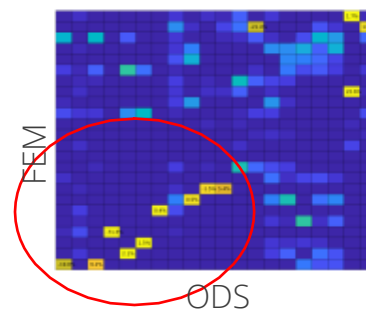
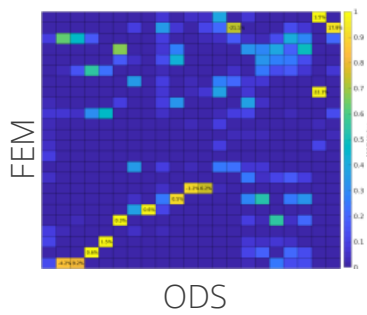
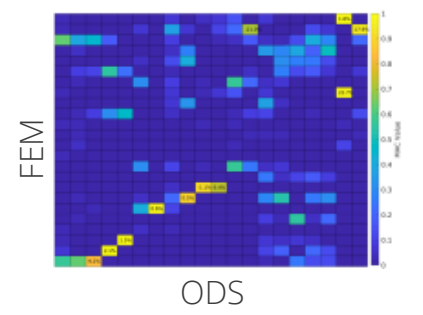
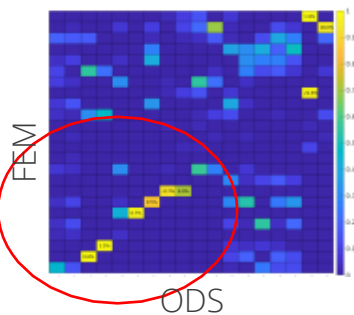


2.12 Grms



3 Grms

W
I
T
H
O
U
T



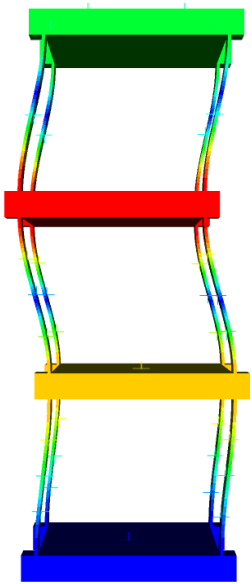
Note: Section with no consistency are spring bending modes, which weren't able to be predicted by ODS since we didn't have sensors on springs



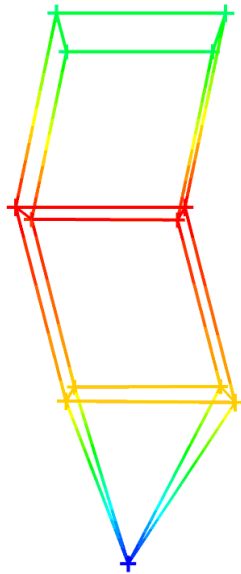
ODS vs. FEM – Representative Mode Shapes

Generally, modes shapes that were successfully predicted by ODS were predicted quite accurately (shape and frequency both very close to model)

WITHOUT Impact Assembly



45 Hz

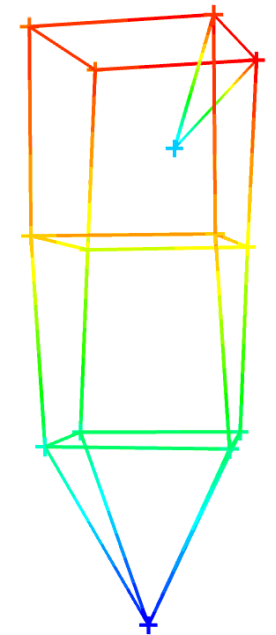


46 Hz

WITH Impact Assembly



80 Hz

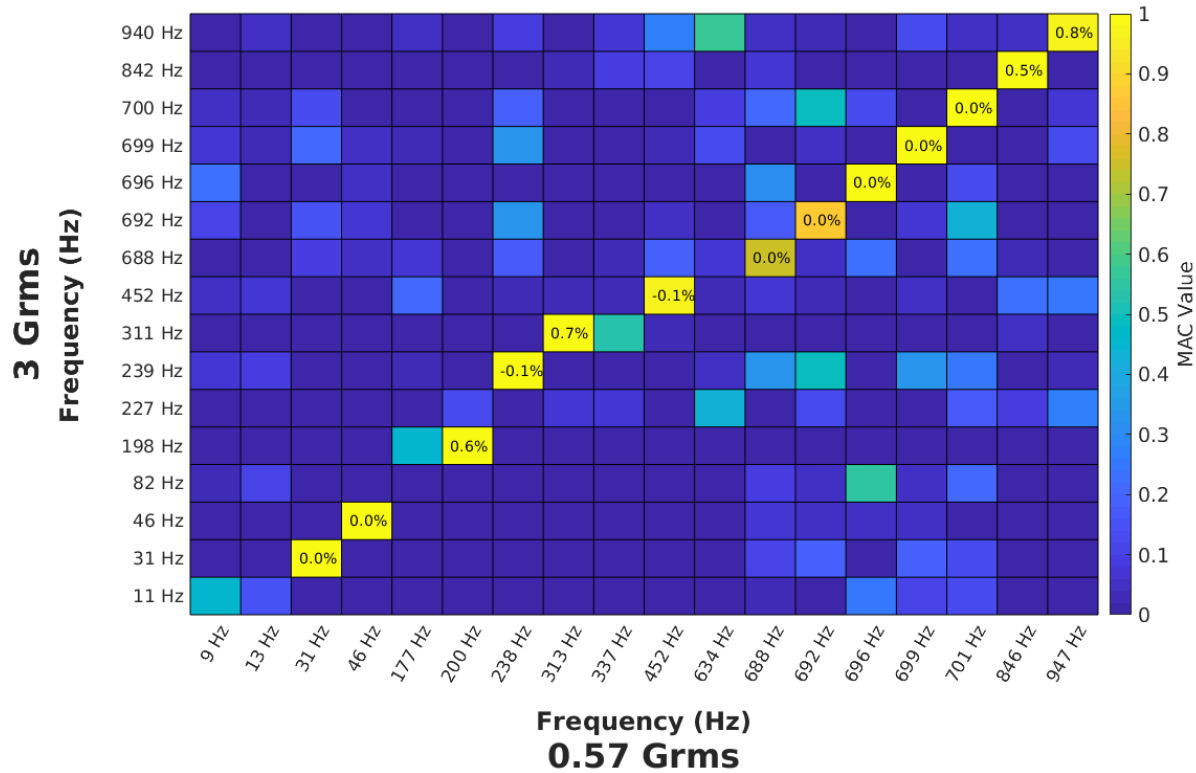


80 Hz

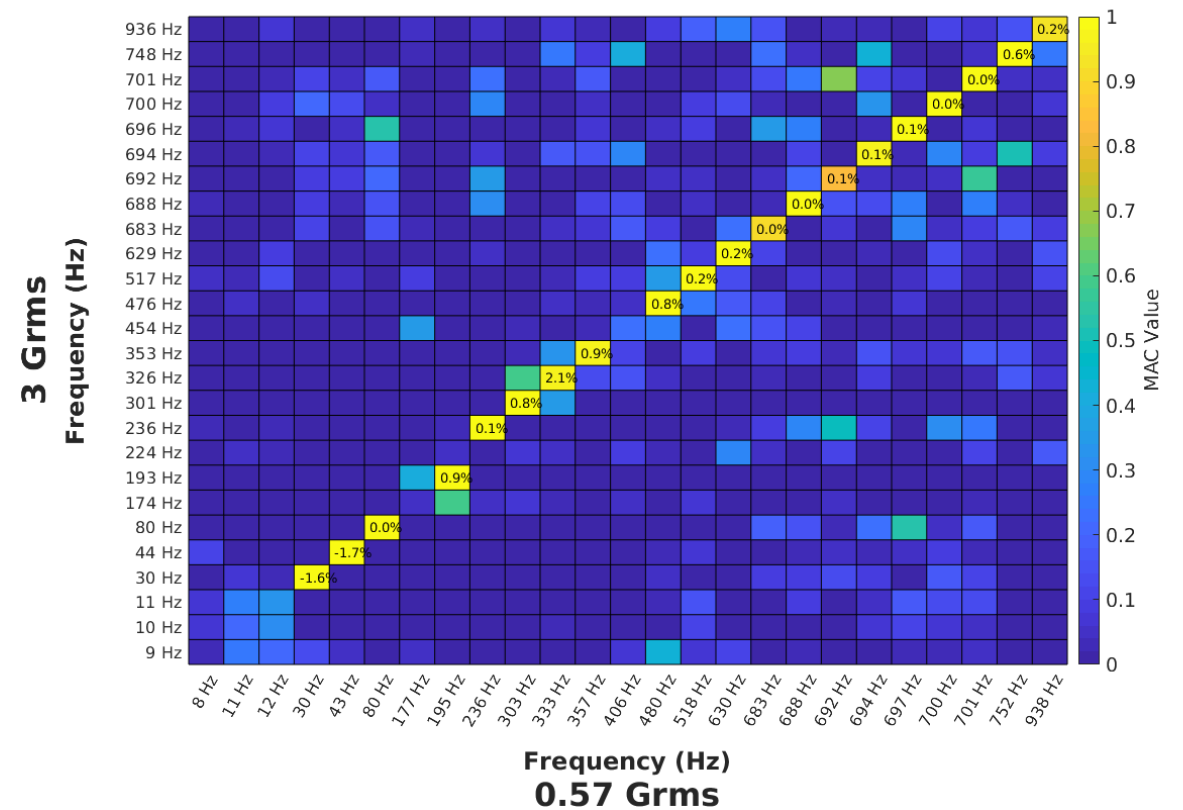


ODS Consistency – High/Low Excitation

WITHOUT IMPACT ASSEMBLY



WITH IMPACT ASSEMBLY

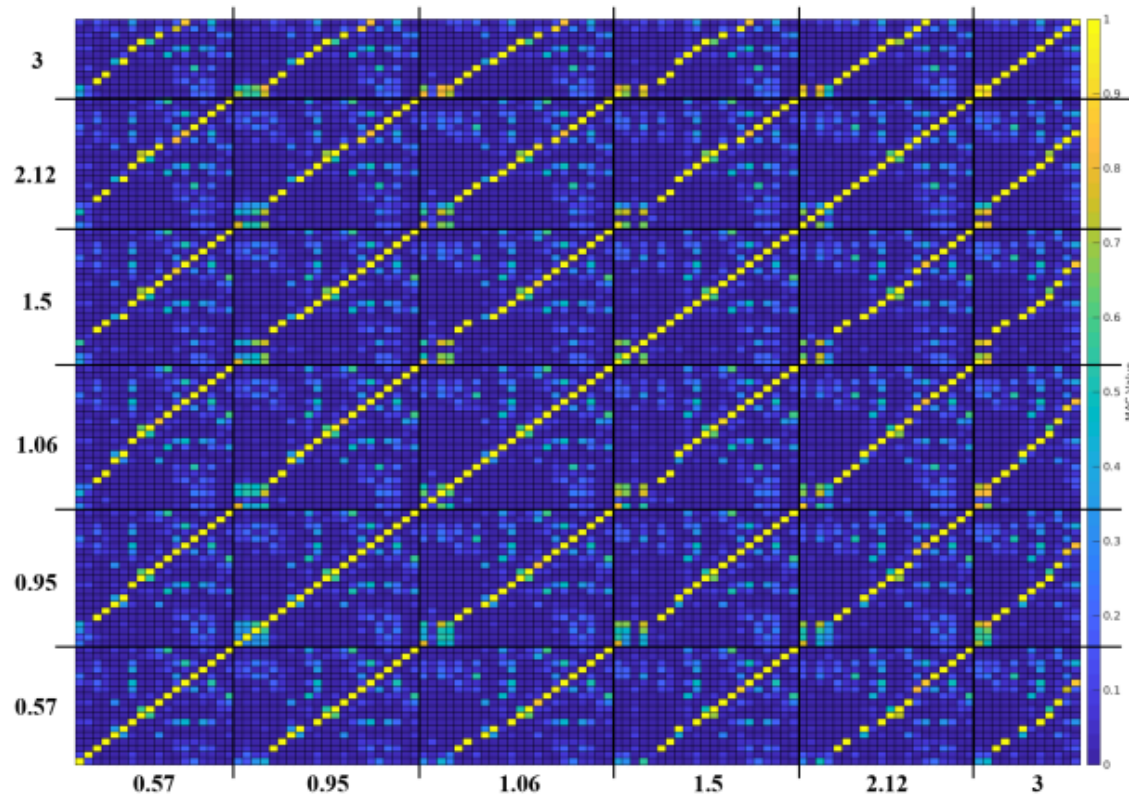




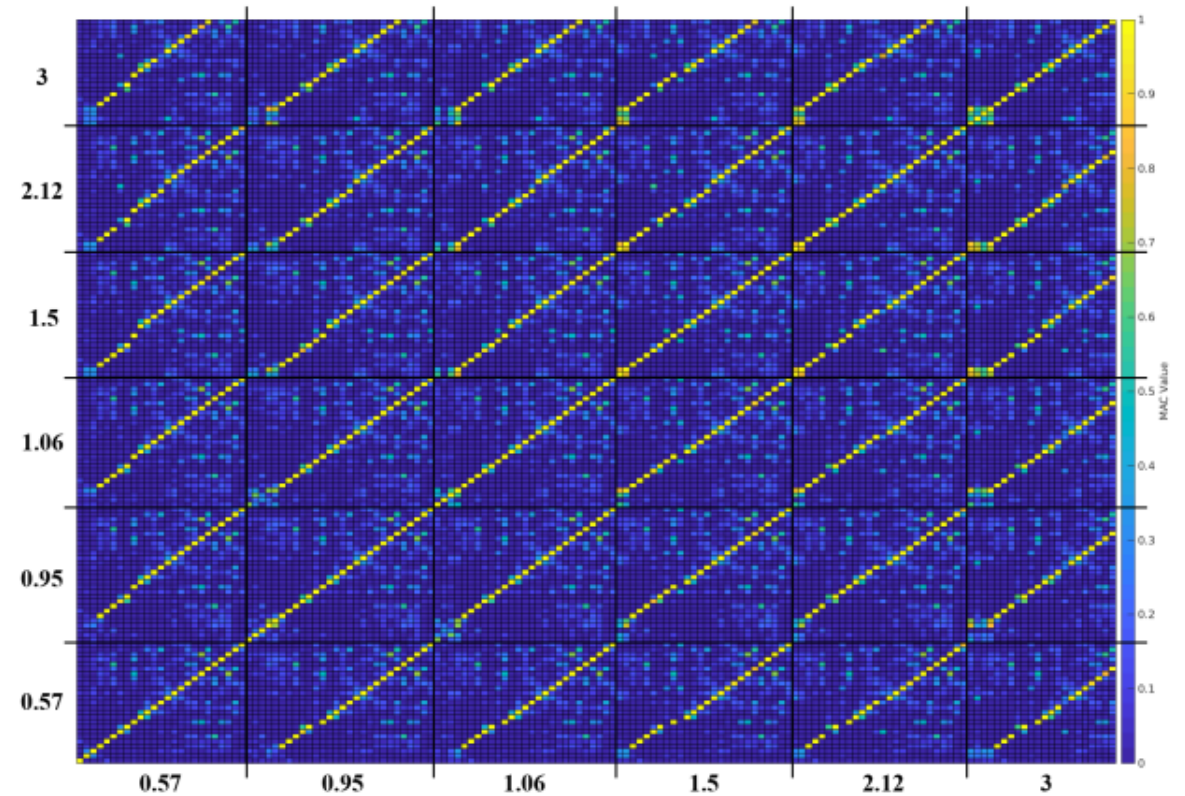
ODS Consistency – BIGMAC

Plots show degree of consistency between ODS predicted mode shapes across excitation level

- Generally, we note *higher* consistency across excitation level WITH impact assembly than WITHOUT
- Possibly due to different response characteristics from impact and asymmetry



WITHOUT Impact Assembly



WITH Impact Assembly



Conclusions

- ODS results are limited by excitation characteristics and sensor placement
 - Frequency content and excitation direction are important!
- Impact assembly results in *slightly better* prediction of modal parameters
 - BUT, it also results in prediction of additional shapes due to additional response peaks
- Increasing excitation level appears to have slightly positive effect on modal predictions
 - Possibly due to enhanced response peaks
 - If possible, use multiple excitation levels!
- Ultimately, intermittent impact and varying levels of excitation DID NOT result in vastly different results → Promising, BUT need better baseline modal data to say for sure!



References

- [1] L. Hermans and H. V. d. Auweraer, "Modal testing and analysis of structures under operational conditions: industrial applications," *Mechanical systems and signal processing*, vol. 13, no. 2, pp. 193-216, 1999.
- [2] C. Gentile and A. Saisi, "Operational modal testing of historic structures at different levels of excitation," *Construction and Building Materials*, vol. 48, pp. 1273-1285, 2013.
- [3] Siemens, "OMG! What is OMA? Operational Modal Analysis," Siemens, 10 July 2020. [Online]. Available: <https://community.sw.siemens.com/s/article/OMG-What-is-OMA-Operating-Modal-Analysis>.
- [4] P. Avitabile, *Modal testing: a practitioner's guide*, John Wiley & Sons, 2017.
- [5] The MathWorks, Inc, "Singular Values," 2022. [Online]. Available: <https://www.mathworks.com/help/matlab/math/singular-values.html>.
- [6] CUBIT Development Team, *CUBIT Geometry and Mesh Generation Toolkit*, SAND2022-9299 W, 2022.
- [7] Sierra SD Team, *Sierra SD*, SAND2022-12518, 2022.



Questions?



Backup Slides



ODS vs. Finite Element Model

- Here, tables show all ODS alongside FEM results -> false predictions included
- Note that ODS for structure WITH impact assembly has more shapes not consistent with FEM mode shapes
 - Due to extra CMIF peaks resulting from impact

Table 2 Resonant frequencies of structure with impact assembly from finite element model and ODS

| - | Finite Element Model | ODS: 0.57Grms | ODS: 0.95Grms | ODS: 1.06Grms | ODS: 1.5Grms | ODS: 2.12Grms | ODS: 3Grms |
|------------------------------|--|--|--|--|--|---|---|
| Modal Frequencies (Hz) | 10 30 43 62 80 192 235 302 355 460 486 531 684-700 711 821 | 8 11 12 30 43 80 177 195 236 303 333 357 406 480 516 630 683-701 752 938 752 937 | 7 8 12 30 44 80 80 175 195 236 302 331 331 356 408 480 518 628 683-701 752 938 | 6 9 11 30 43 80 174 194 236 302 331 355 409 478 516 630 683-701 751 942 | 10 30 44 80 174 194 225 236 302 331 355 408 443 478 517 628 683-701 750 934 | 10 30 44 80 175 194 225 236 329 353 408 443 478 517 628 683-701 750 934 | 9 10 11 30 44 80 174 193 224 236 301 326 353 454 476 517 629 683-701 748 936 |

WITH Impact Assembly

Table 3 Resonant frequencies of structure without impact assembly from finite element model and ODS

| - | Finite Element Model | ODS: 0.57Grms | ODS: 0.95Grms | ODS: 1.06Grms | ODS: 1.5Grms | ODS: 2.12Grms | ODS: 3Grms |
|--------------------------------|--|---|---|---|---|---|---|
| Natural Frequencies (Hz) | 11 31 45 66 81 198 237 315 361 510 684-700 803 831 | 9 13 31 46 177 200 238 313 337 452 634 688-701 846 947 | 8 11 12 32 46 175 199 230 238 312 335 450 634 688-701 946 | 8 11 12 31 46 175 199 230 230 238 238 409 633 688-701 946 | 9 10 12 19 32 46 199 229 238 311 332 451 631 688-700 945 | 8 11 12 31 46 82 198 82 198 239 310 330 453 688-700 940 | 11 31 46 82 198 227 239 311 452 688-700 842 940 |

WITHOUT Impact Assembly