



# Advances in Floating Offshore Vertical-Axis Wind Turbine Design



Brandon Ennis



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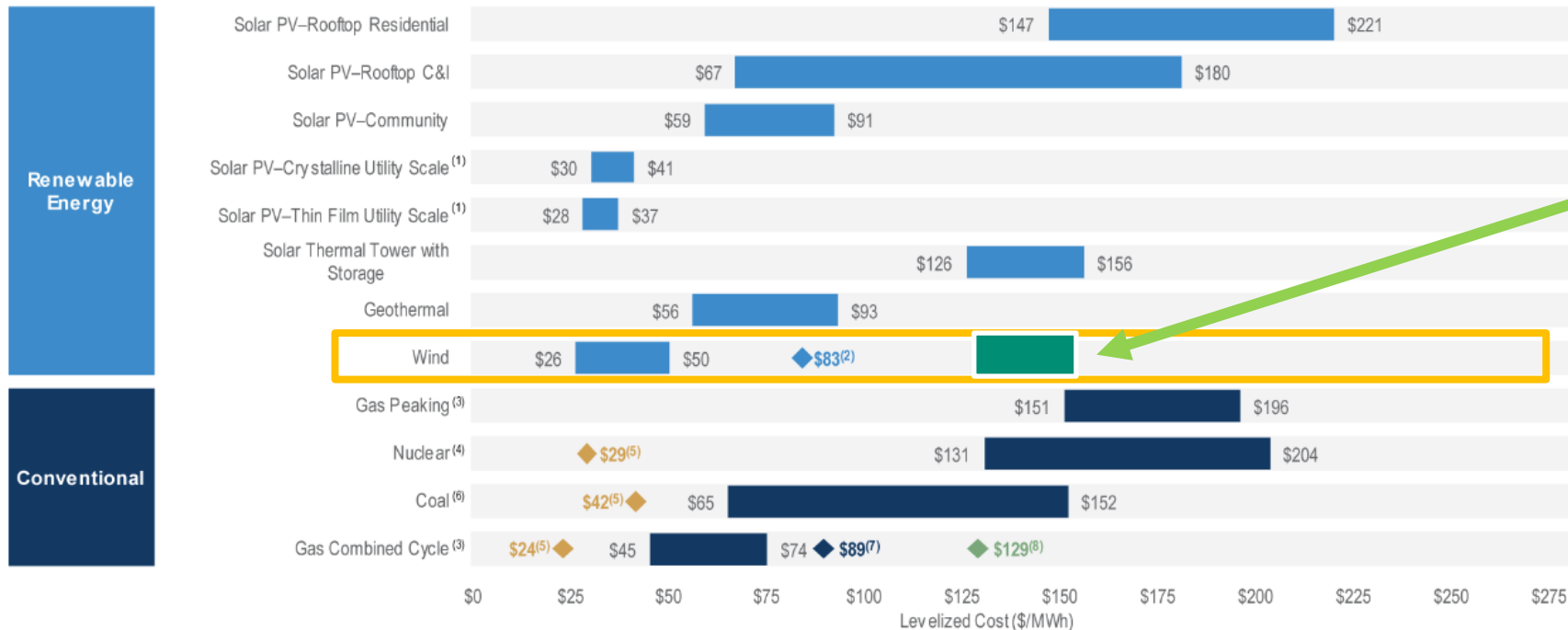
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# Energy Generation in US: Unsubsidized LCOE Comparison



## Levelized Cost of Energy Comparison—Unsubsidized Analysis

Selected renewable energy generation technologies are cost-competitive with conventional generation technologies under certain circumstances



Source: Lazard estimates.

Note: Here and throughout this presentation, unless otherwise indicated, the analysis assumes 60% debt at 8% interest rate and 40% equity at 12% cost. Please see page titled "Levelized Cost of Energy Comparison—Sensitivity to Cost of Capital" for cost of capital sensitivities. These results are not intended to represent any particular geography. Please see page titled "Solar PV versus Gas Peaking and Wind versus CCGT—Global Markets" for regional sensitivities to selected technologies.

- (1) Unless otherwise indicated herein, the low case represents a single-axis tracking system and the high case represents a fixed-tilt system.
- (2) Represents the estimated implied midpoint of the LCOE of offshore wind, assuming a capital cost range of approximately \$2,500 – \$3,600/MW.
- (3) The fuel cost assumption for Lazard's global, unsubsidized analysis for gas-fired generation resources is \$3.45/MMBTU.
- (4) Unless otherwise indicated, the analysis herein does not reflect decommissioning costs, ongoing maintenance-related capital expenditures or the potential economic impacts of federal loan guarantees or other subsidies.
- (5) Represents the midpoint of the marginal cost of operating fully depreciated gas combined cycle, coal and nuclear facilities, inclusive of decommissioning costs for nuclear facilities. Analysis assumes that the salvage value for a decommissioned gas combined cycle or coal asset is equivalent to its decommissioning and site restoration costs. Inputs are derived from a benchmark of operating gas combined cycle, coal and nuclear assets across the U.S. Capacity factors, fuel, variable and fixed operating expenses are based on upper- and lower-quartile estimates derived from Lazard's research. Please see page titled "Levelized Cost of Energy Comparison—Renewable Energy versus Marginal Cost of Selected Existing Conventional Generation" for additional details.
- (6) High end incorporates 90% carbon capture and storage. Does not include cost of transportation and storage.
- (7) Represents the LCOE of the observed high case gas combined cycle inputs using a 20% blend of "Blue" hydrogen, (i.e., hydrogen produced from a steam-methane reformer, using natural gas as a feedstock, and sequestering the resulting CO<sub>2</sub> in a nearby saline aquifer). No plant modifications are assumed beyond a 2% adjustment to the plant's heat rate. The corresponding fuel cost is \$5.20/MMBTU, assuming \$1.39/kg for Blue hydrogen.
- (8) Represents the LCOE of the observed high case gas combined cycle inputs using a 20% blend of "Green" hydrogen, (i.e., hydrogen produced from an electrolyzer powered by a mix of wind and solar generation and stored in a nearby salt cavern). No plant modifications are assumed beyond a 2% adjustment to the plant's heat rate. The corresponding fuel cost is \$10.05/MMBTU, assuming \$4.15/kg for Green hydrogen.



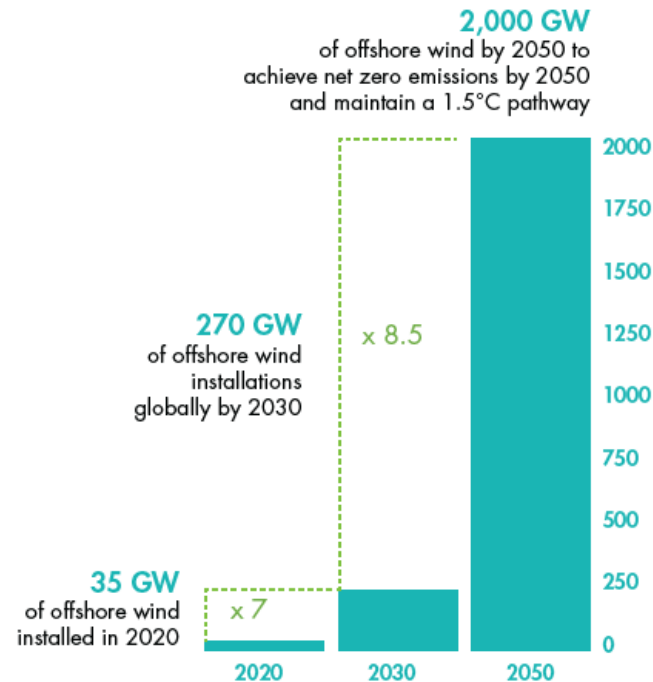
# Global development of offshore wind energy



- To meet the IEA and IRENA 1.5°C global warming scenario, forecasts predict more than 2,000 GW of installed offshore wind capacity by 2050 (compared to ~56 GW installed to date)
- This will require floating offshore sites to be developed

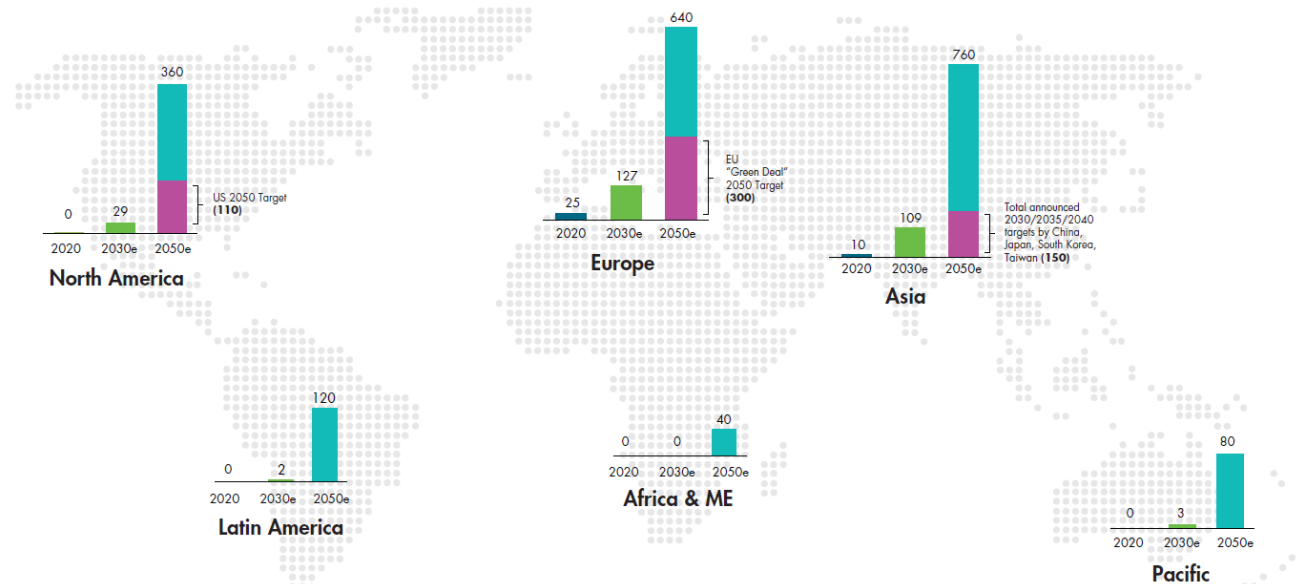
## Closing the offshore wind gap by 2050

Unit: GW



Source: GWEC Market Intelligence; IRENA World Energy Transitions Outlook 2021.

## Where could 2,000 GW of offshore wind by 2050 be built?



Unit: GW

Source: GWEC Market Intelligence

■ Installations as of 2020

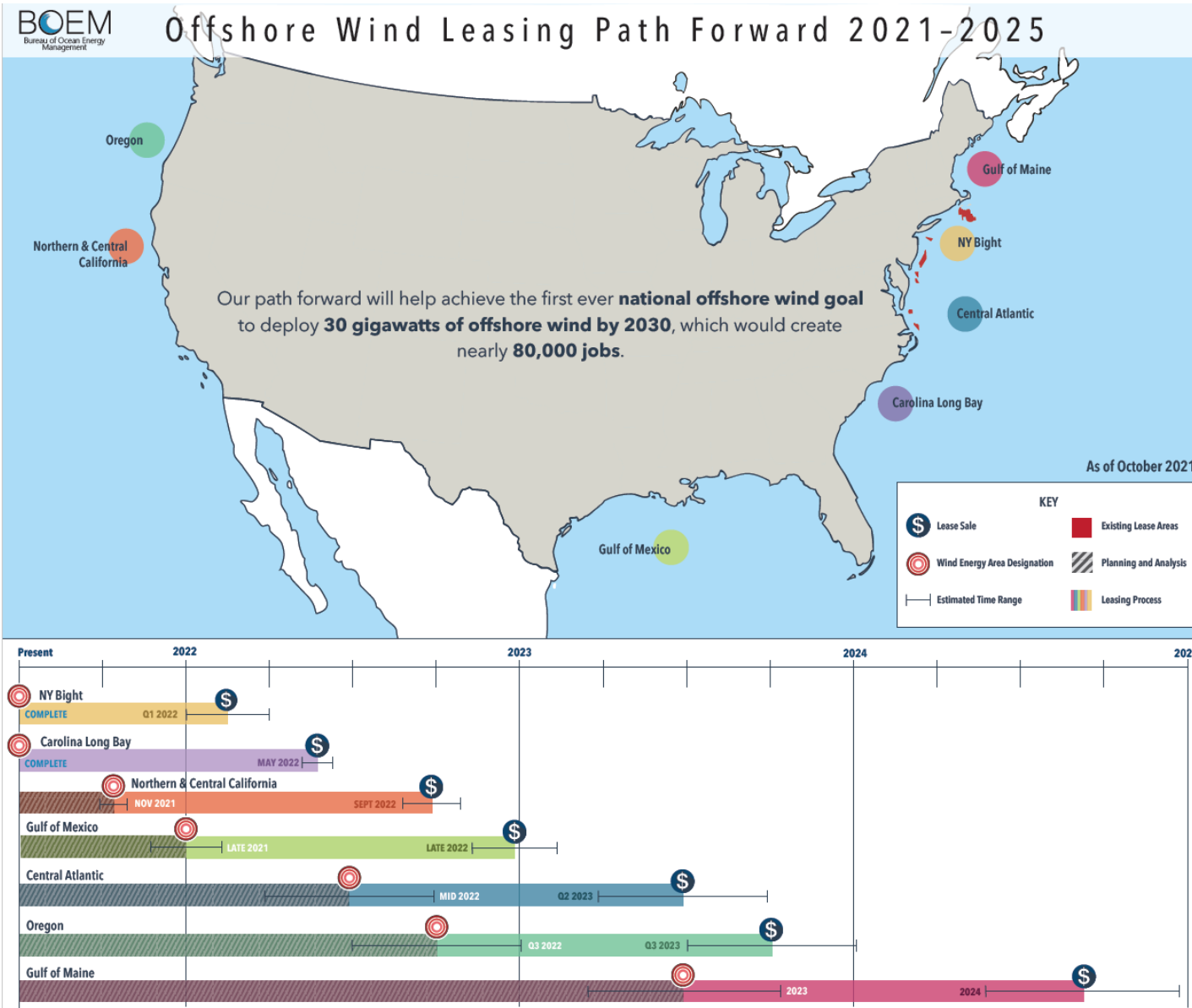
■ Installations by 2030 under current policies

■ Regional forecast by 2050, based on 2,000 GW global target

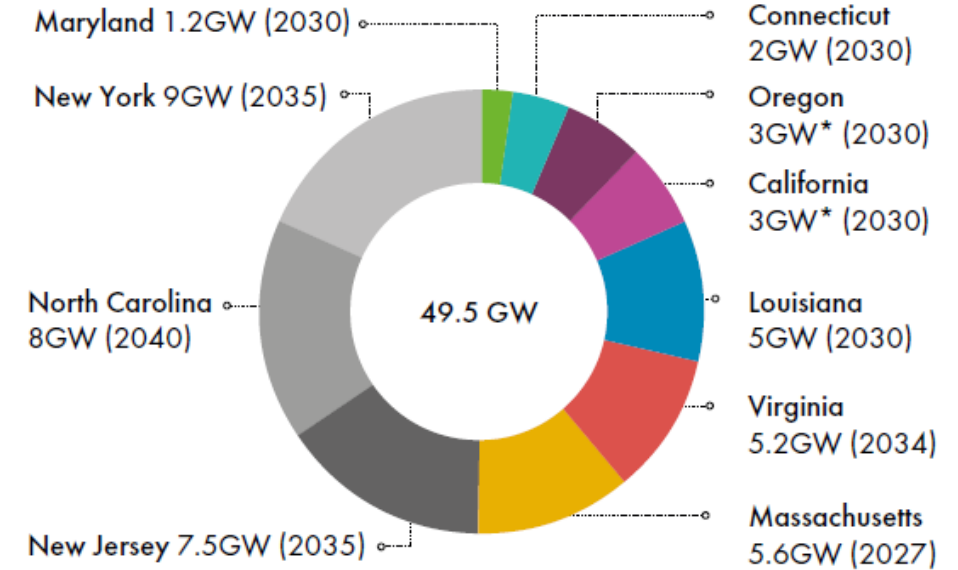
■ Current regional or national targets



# The advent of the offshore wind industry in the US



## US State-level offshore wind development targets

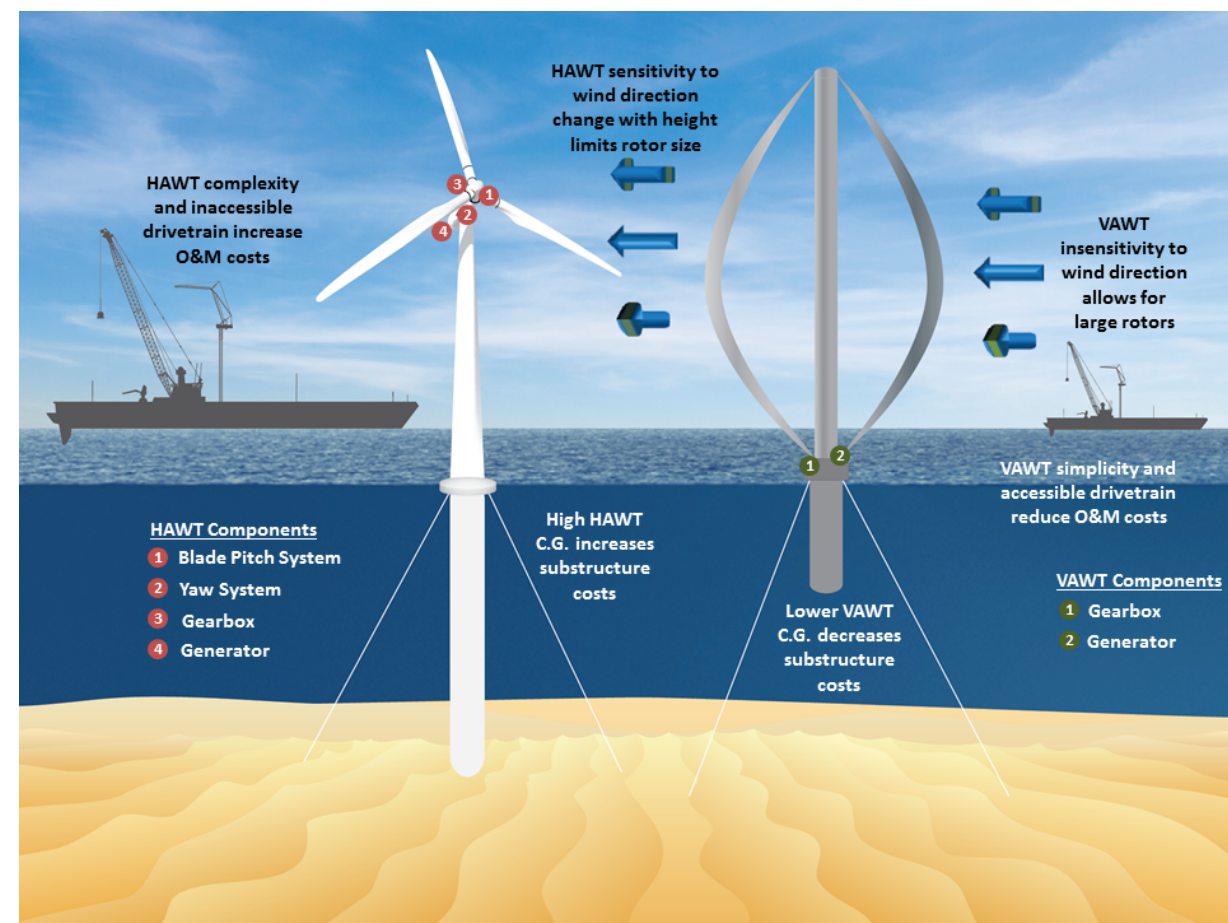


\*Announced plan, not yet signed by law

# Could VAWTs be a solution for floating offshore wind?



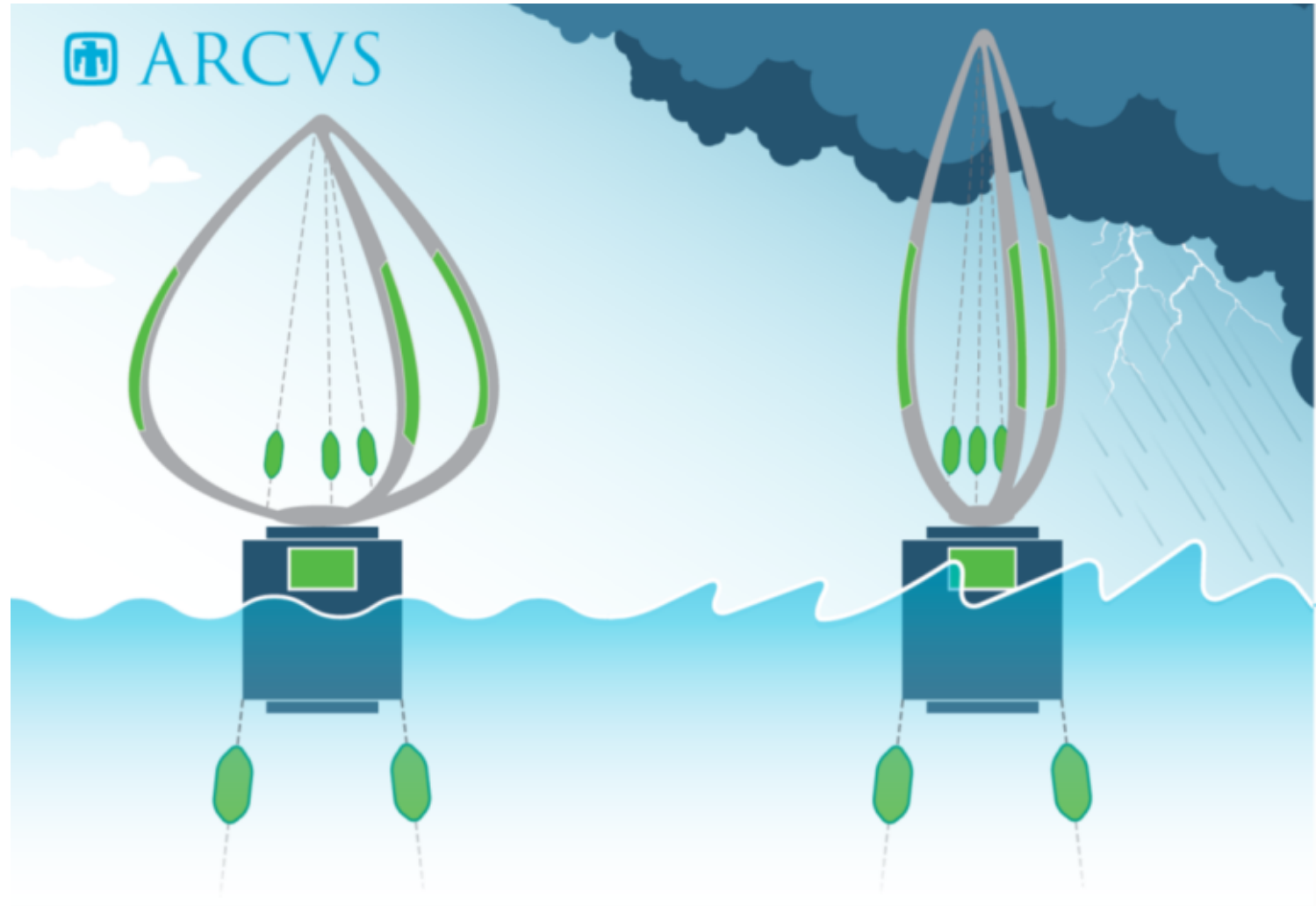
- For floating offshore wind, the platform costs are the single largest contributor to the LCOE
- Turbine costs represent 65% of wind plant costs for land-based sites compared to around 20% for floating offshore sites
- VAWTs are being studied as a lower cost solution for floating offshore wind energy **which have several benefits, including:**
  - (1) Lower center of gravity, which reduces topside moment of inertia and resulting platform costs
  - (2) Reduced O&M costs through removal of active components and platform-level placement of drivetrain
  - (3) Improved energy capture over HAWTs at multi-MW scales
  - (4) Insensitive to wind shear, wind veer, and gravitational load cycles



# A VAWT designed for floating offshore sites



- The ARCUS rotor is a towerless VAWT that replaces the traditional rigid tower with prestressed blades and tensioned center supports (U.S. 11,421,650 B2)
- In previous Sandia studies, the tower represented ~80% of the rotor mass

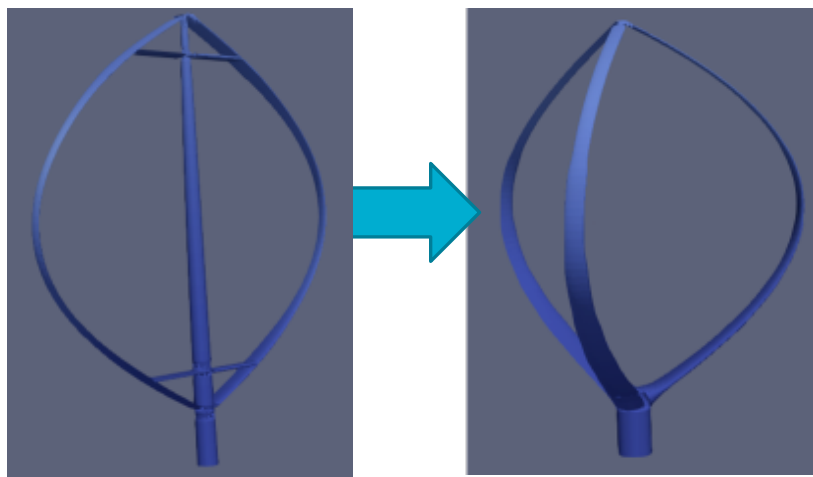


The ARCUS Darrieus VAWT has been designed by Sandia to address the high costs of floating offshore wind.

# ARCUS Turbine Design Optimization

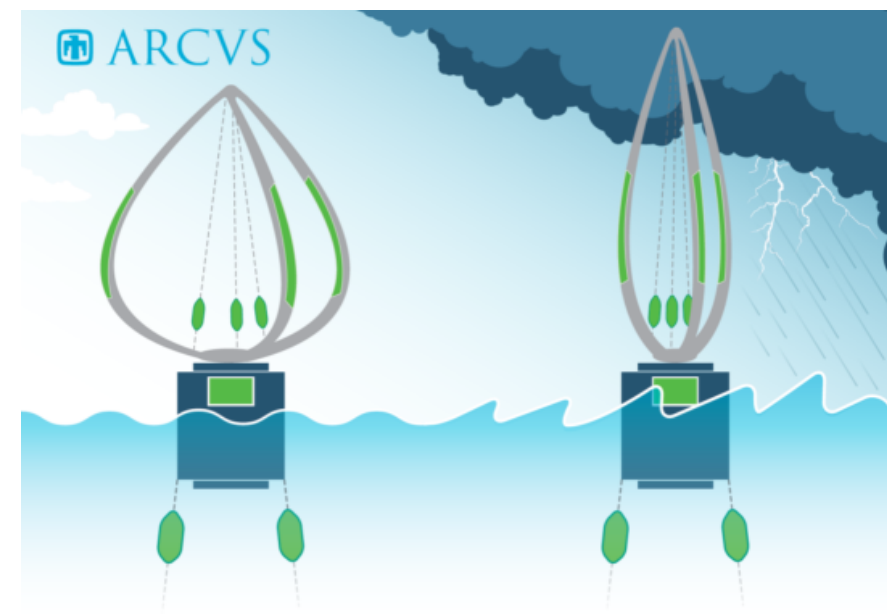
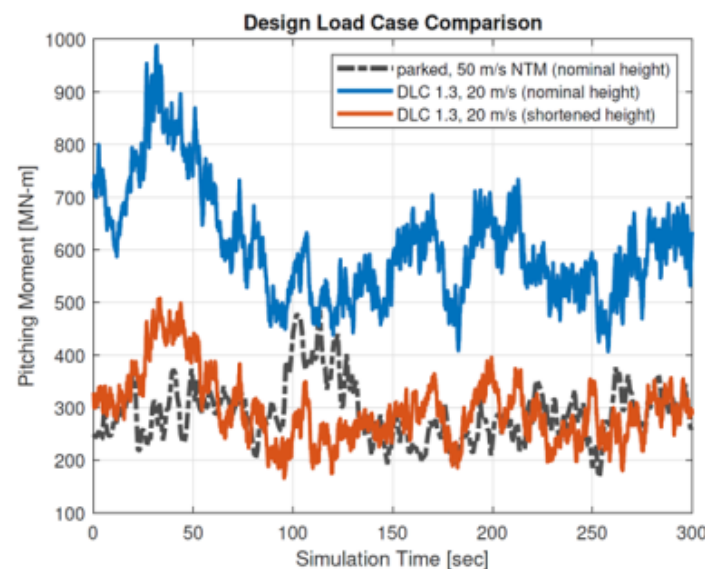
- The towerless ARCUS design enables an efficient use of materials, shifting away from compressive strains
- Rotor area control to reduce loads in high winds
- Project has been funded by ARPA-e within the U.S. Department of Energy for concurrent design of the floating VAWT system

**5 MW Rotor Mass Reduction: 52.1%**



**181,888 kg**

**87,030 kg**



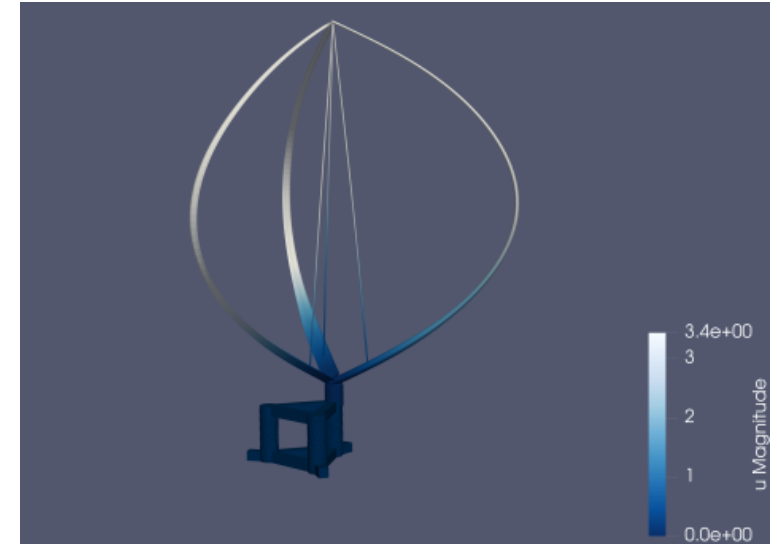
	ARCUS VAWT	Reference HAWT
Topside mass estimate (-)	<b>1.0</b>	<b>1.45</b>
Center of gravity	<b>23 m</b>	<b>75 m</b>
Thrust overturning moment, tow-out (-)	<b>3.2</b>	<b>1.0</b>



# Platform Identification and Design Optimization



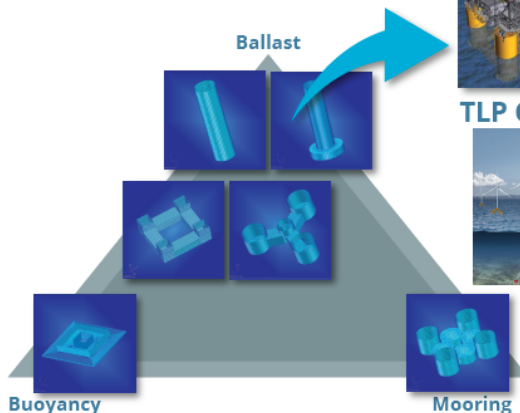
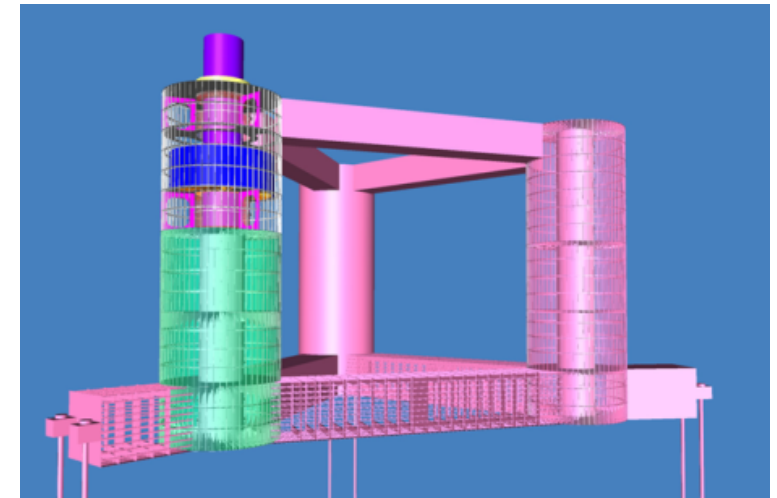
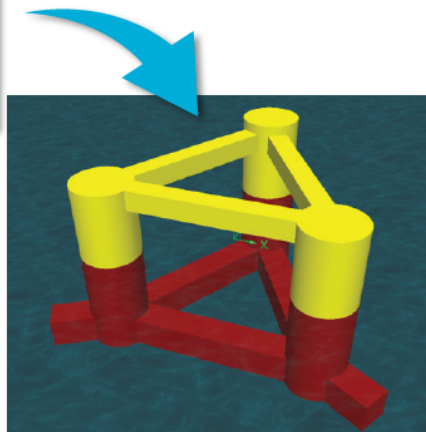
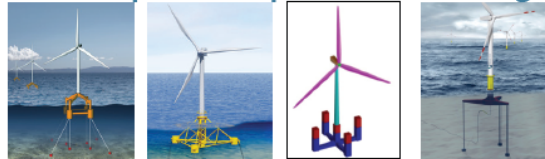
- A three-column tension-leg platform (TLP) has been identified to optimally reduce mass and cost
  - Quayside integration of turbine
  - Self-stable during tow-out for ease of installation
- Optimization of platform hull and global performance reduces costs by >25% relative to baseline platform
- Detailed scantling design to produce cost models



TLP Concepts currently in Operation for Oil and Gas Production



TLP Concepts developed for HAWT designs

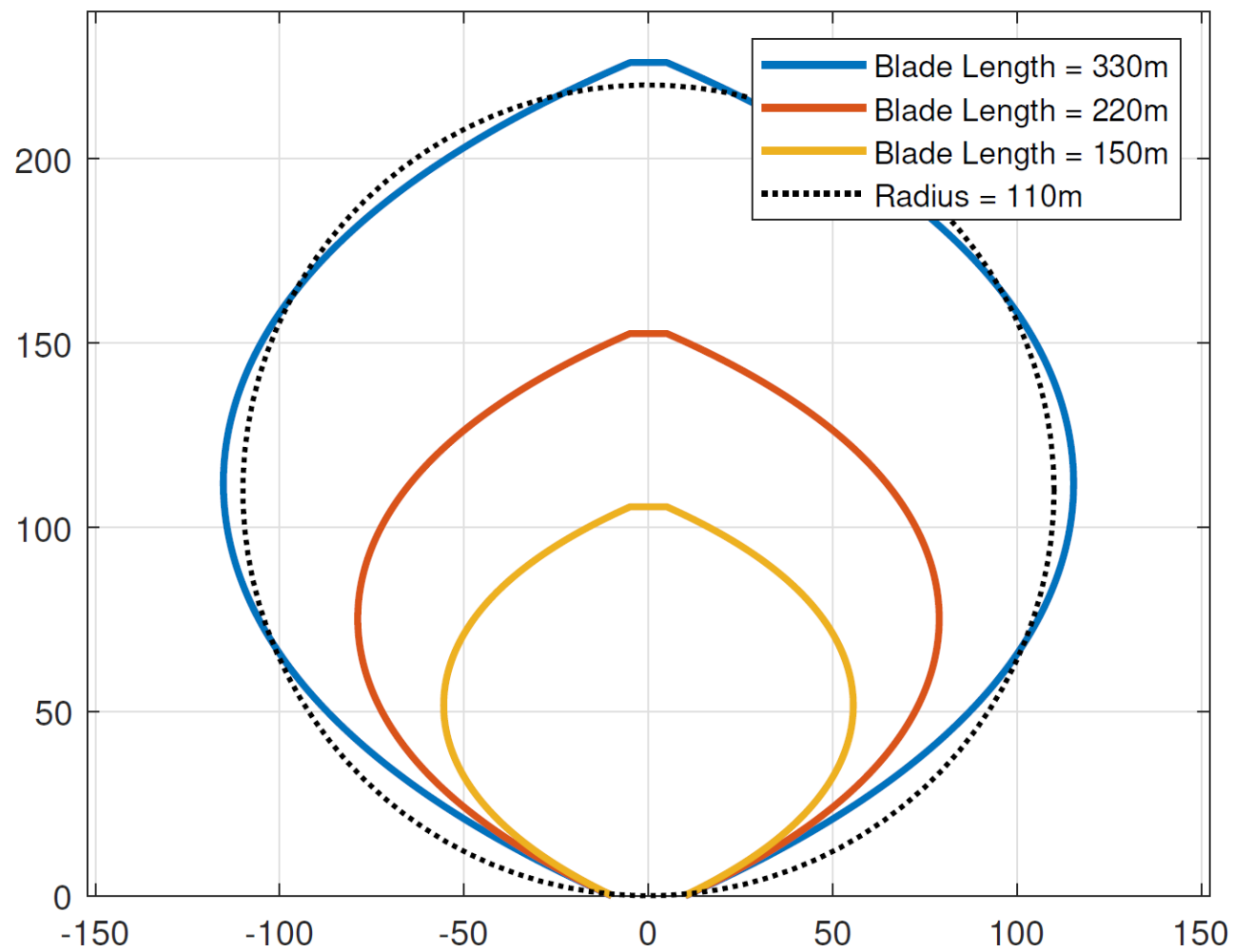




# Reference ARCUS Design Definition – Scaling Trends



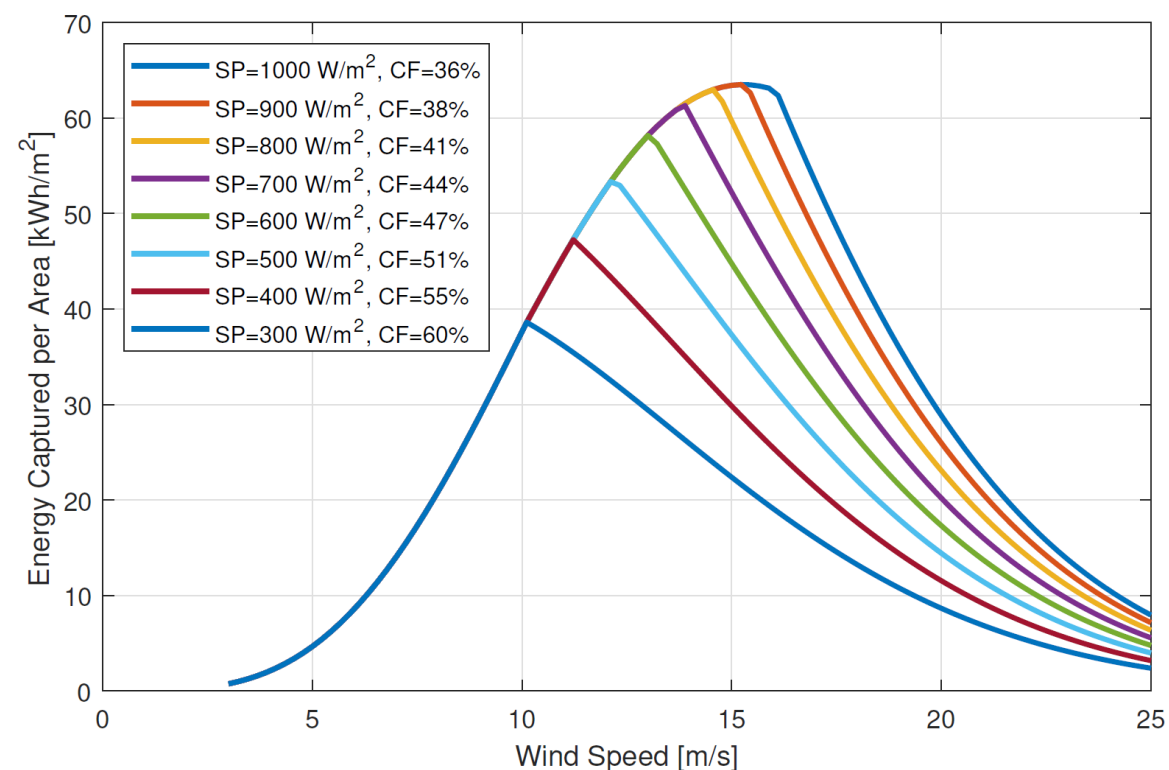
- Performed a turbine scaling study to identify a turbine size that achieves the most optimal system LCOE
  - Turbine sizes with 1x, 2x, and 4x swept areas
- Balance of system, installation, and operations & maintenance costs dominate for smaller power capacity turbines
- Platform designs were developed for the three reference VAWT sizes to understand capital cost trends



# VAWT Scaling Trends – Energy Production



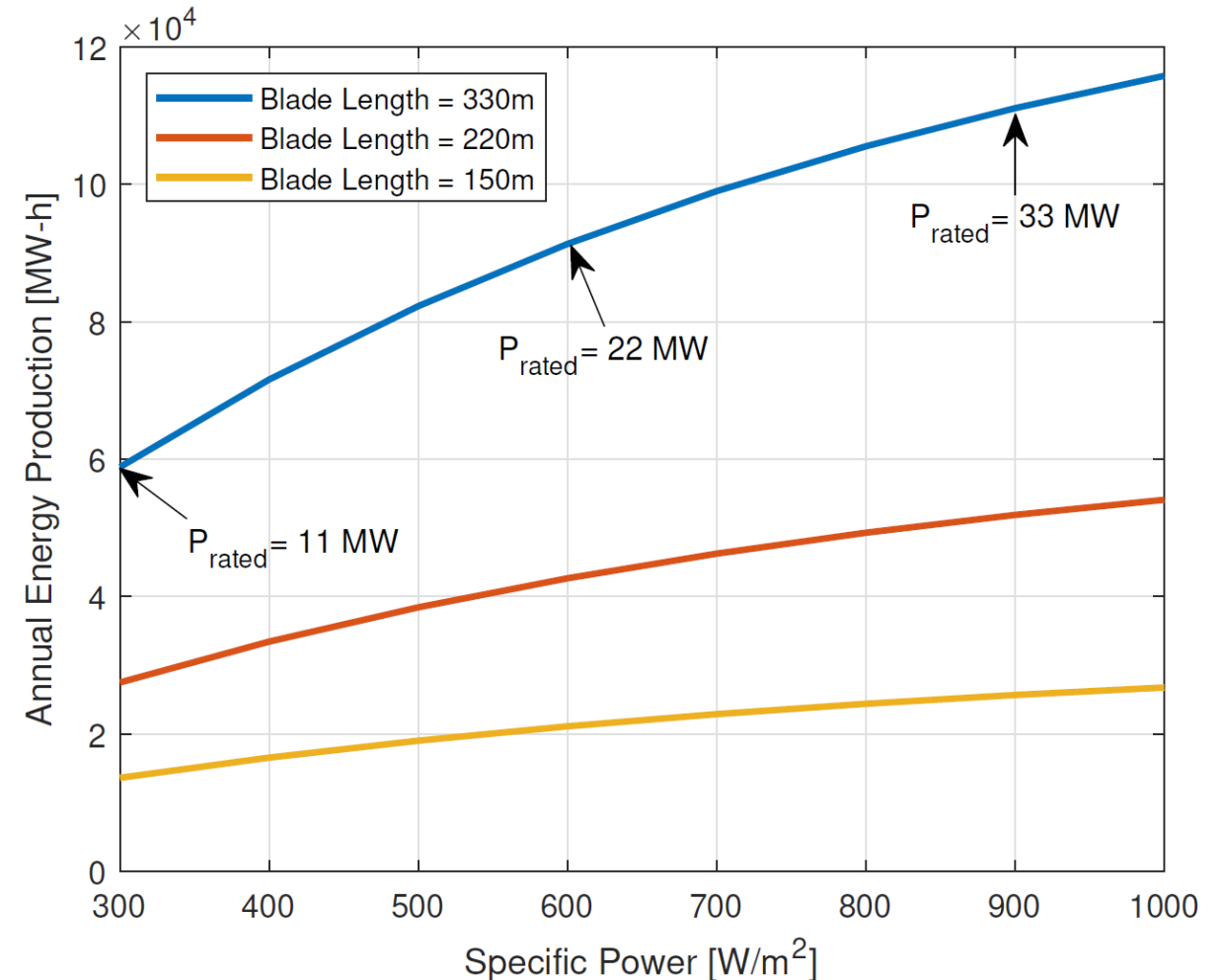
- The annual energy production is the numerator of the LCOE equation, scales annual costs
- The rated power per rotor swept area is a design variable (specific power, SP) that affects energy production and capacity factor (CF)
- Modern offshore wind turbines have a  $SP = 300\text{--}350 \text{ W/m}^2$
- For the IEC Class 1 wind speed distribution, there is a meaningful amount of energy at high wind speeds



# VAWT Scaling Trends – Energy Production



- For high wind resource sites, typical of offshore sites in the US, there is value to designing with a larger generator
- Going from 300  $\text{W/m}^2$  to 600  $\text{W/m}^2$  increases energy capture by ~50%
- VAWTs enable this design approach due to their low placement of the drivetrain
  - The additional generator mass for a VAWT is less meaningful to associated turbine and platform costs

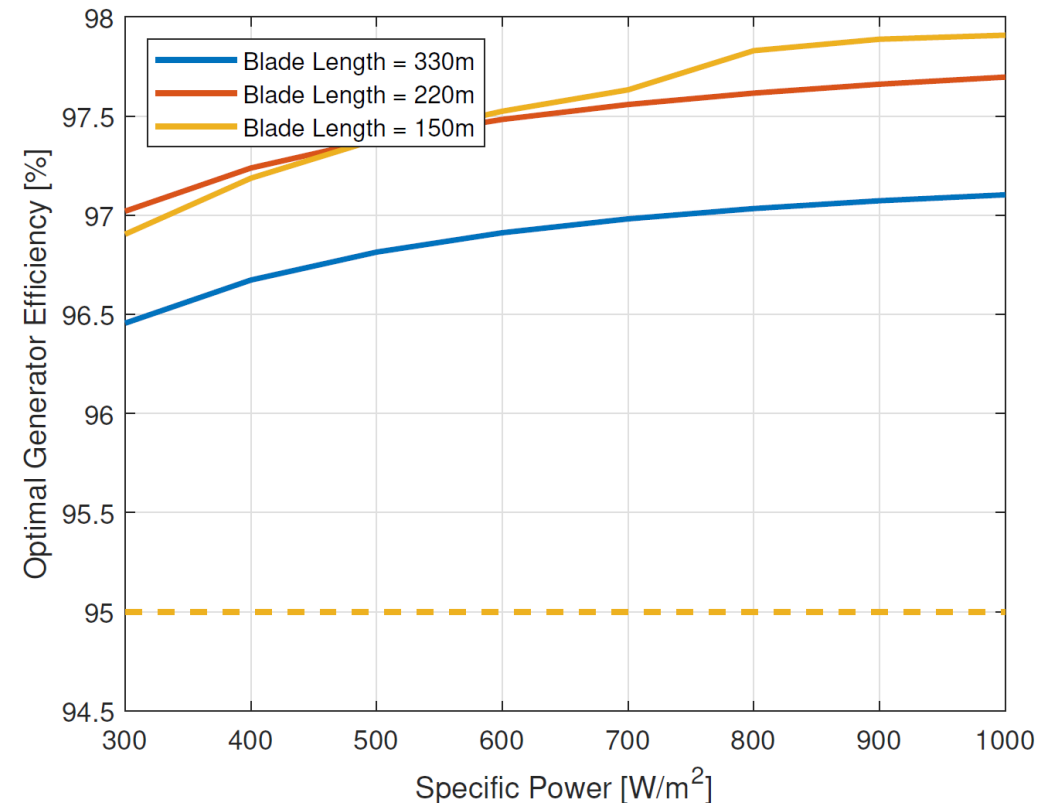
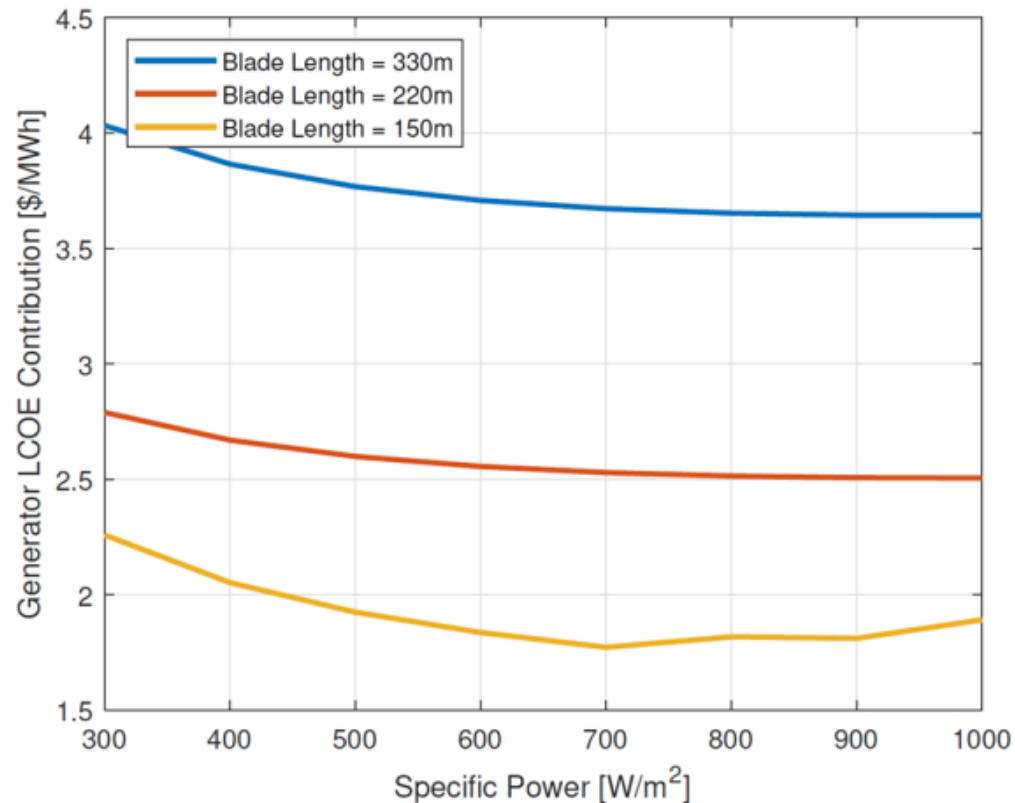


# VAWT Scaling Trends – Optimal Generator Design



- Generator optimization using NREL tool GeneratorSE to minimize LCOE relative to a reference baseline value where cost (CG) and efficiency affect LCOE, assuming  $LCOE^B = \$70/\text{MWh}$  in the analysis:

$$LCOE = \frac{\eta_G^B}{\eta_G} \left( \frac{(C_G - C_G^B) \cdot FCR}{AEP_{aero} \cdot \eta_G^B} + LCOE^B \right)$$

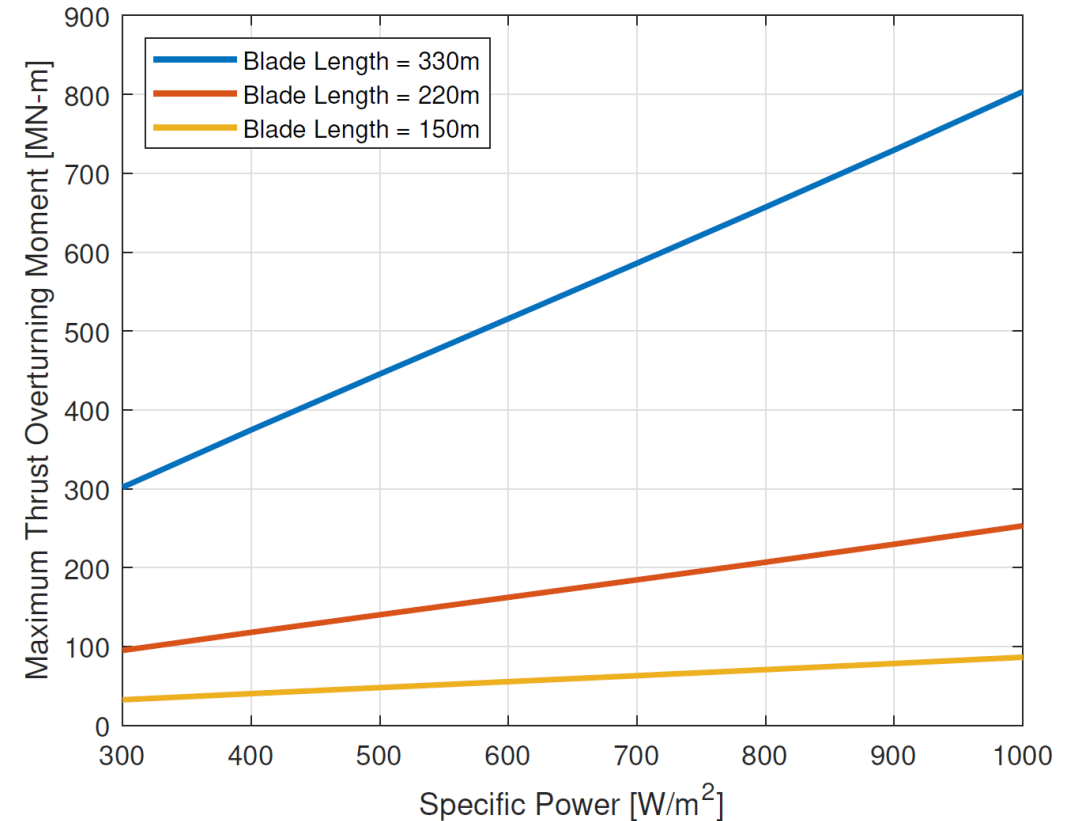




# VAWT Scaling Trends – Turbine Loads on Platform



- However, for turbines with a larger swept area there is also a higher center of pressure, so the increased thrust force is also at a higher elevation
- Thrust overturning moment is substantially higher for larger turbines, which must be resisted by the floating platform



# VAWT Scaling Trends – Platform Capital Costs



## VAWT TLP Cost Estimate Comparison – Cycle 1

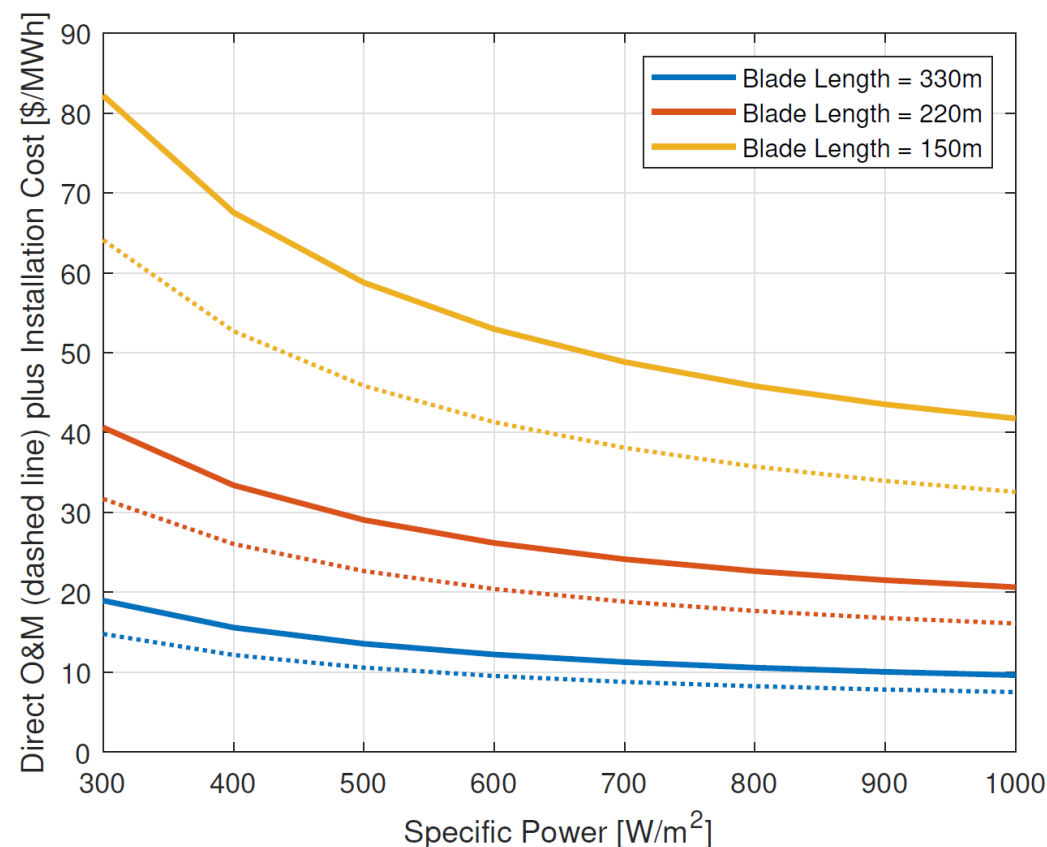
- Platforms were designed by partner FPS Engineering & Technology for the three reference VAWT sizes based on weight and wind loads
- Cycle 1 design mass estimates are higher than the final system, and the designs are not fully optimized
- However, the trends are considered representative and favor larger systems within the bounds of the study

VAWT TLP Cost Summary V1 (10-25-2021)				
		330 m Blade	220 m Blade	150 m Blade
Principal Dimensions	Unit	TLP211004_33	TLP210601_22	TLP211005_15
Draft	[m]	20.0	20.0	18.0
<b>Displacement</b>	<b>[mT]</b>	<b>11,251</b>	<b>9,037</b>	<b>6,381</b>
Turbine + Generator	[mT]	980	475	235
Flexible Riser Vertical loads	[mT]	50	50	50
<b>Total System Payload</b>	<b>[mT]</b>	<b>1,030</b>	<b>525</b>	<b>285</b>
Hull Primary Steel Wt (UCF+Tower Base+Hull)	[mT]	2,972	2,434	1,830
Other Steel Weight (Outfitting, Anodes, etc)	[mT]	673	544	396
<b>Total Steel weight</b>	<b>[mT]</b>	<b>3,644</b>	<b>2,978</b>	<b>2,225</b>
Marine System + Marine Growth	[mT]	135	109	77
Ballast Weight	[mT]	1,341	1,526	794
<b>Total Platform Weight</b>	<b>[mT]</b>	<b>5,966</b>	<b>4,979</b>	<b>3,254</b>
Tendon Pretension/Tendon	[mT]	850	650	500
<b>Tendon Pretension</b>	<b>[mT]</b>	<b>5,100</b>	<b>3,900</b>	<b>3,000</b>
Number of Tendons	-	6	6	6
Tendon Outer Diameter x Wall Thickness	[in x in]	30" x 1.150"	26" x 0.900"	22" x 0.850"
Dry Weight / Tendon	[mT]	47.0	32.0	25.5
Estimated Hull Unit Cost	\$/ mT	10,000	10,000	10,000
Estimated Tendon Unit Cost	\$/ mT	5,750	5,750	5,750
<b>Hull Cost</b>	<b>\$</b>	<b>36,442,639</b>	<b>29,778,568</b>	<b>22,254,469</b>
<b>Tendon Cost</b>	<b>\$</b>	<b>1,622,660</b>	<b>1,104,842</b>	<b>879,251</b>
<b>Fabrication Cost Summary</b>	<b>\$</b>	<b>38,065,299</b>	<b>30,883,410</b>	<b>23,133,721</b>
<b>Installation Cost</b>	<b>\$</b>	<b>4,191,500</b>	<b>4,191,500</b>	<b>4,191,500</b>
<b>Operation and Maintenance Cost</b>	<b>\$</b>	<b>1,123,200</b>	<b>1,123,200</b>	<b>1,123,200</b>
<b>Total Cost</b>	<b>\$</b>	<b>43,379,999</b>	<b>36,198,110</b>	<b>28,448,421</b>
Electrical Power Generation	MW	22.3	10.4	5.1
<b>Estimated MW Cost</b>	<b>\$/W</b>	<b>1.95</b>	<b>3.48</b>	<b>5.58</b>

# VAWT Scaling Trends – O&M, Platform Installation Costs



- Some balance of system costs are independent of the physical design for utility-scale systems
  - Platform tow-out and installation is considered equivalent
  - Direct Operations and Maintenance costs are primarily vessel charters and crew labor
- The only way to reduce the impact of these fixed-type costs on LCOE is through increased energy production
  - Costs become very meaningful for lower energy production designs



# VAWT Scaling Trends – System Design Summary



- The largest reference blade length was chosen (swept area of  $R = \sim 110\text{m}$ ) due to the impact on decreasing balance of system costs and platform capital costs
- Balances cost reductions with blade manufacturing considerations

<b>(<math>SP_{\text{design}} = 600 \text{ W/m}^2</math>)</b>	<b>150m Blade Length (5.1 MW)</b>	<b>220m Blade Length (10.4 MW)</b>	<b>330m Blade Length (22.3 MW)</b>
Annual energy production [-]	1.0	2.0	4.3
Maximum thrust overturning moment [-]	1.0	2.9	9.4
Combined direct O&M and platform installation LCOE contribution [\$/MWh]	53.0	26.2	12.2
Cycle 1 platform and tendon cost estimate [\$/MWh]	78.5	49.4	27.6

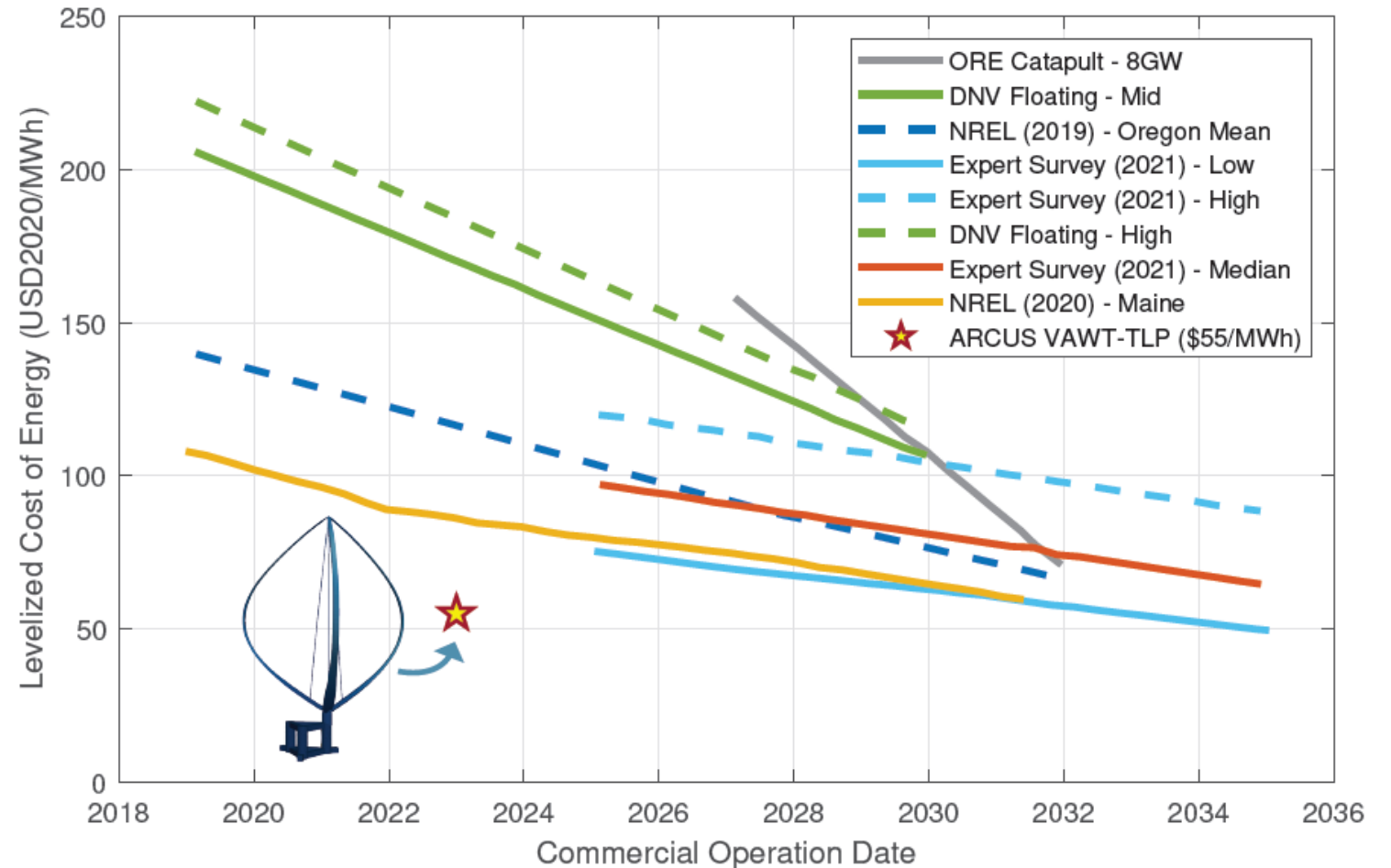


# ARCUS-TLP Optimized System Design



## ARCUS compared with a reference HAWT:

- 30% lower turbine mass
- 70% lower center of gravity
- 45% increase in energy capture
- \$55/MWh levelized cost of energy prediction
- Effectively enables a Tension-Leg Platform



# Remaining Uncertainties for VAWTs

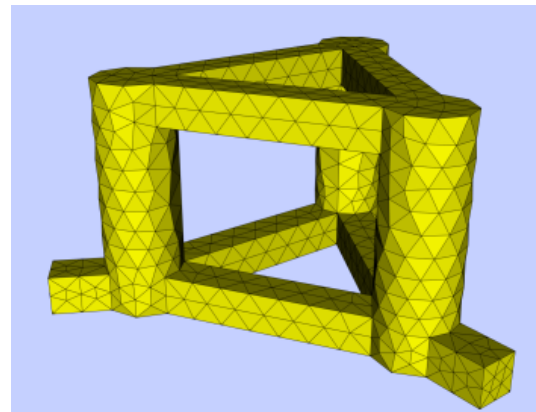
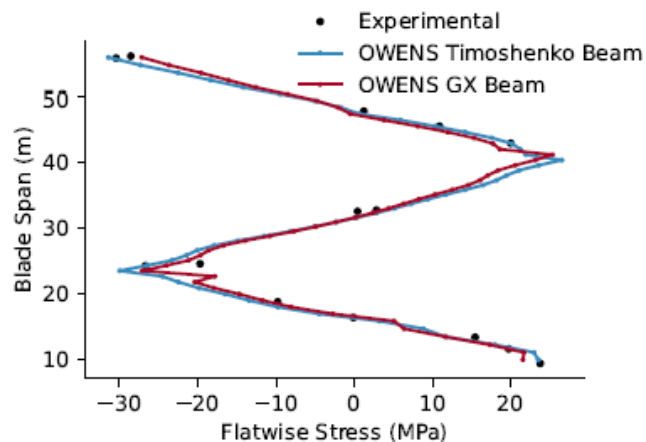
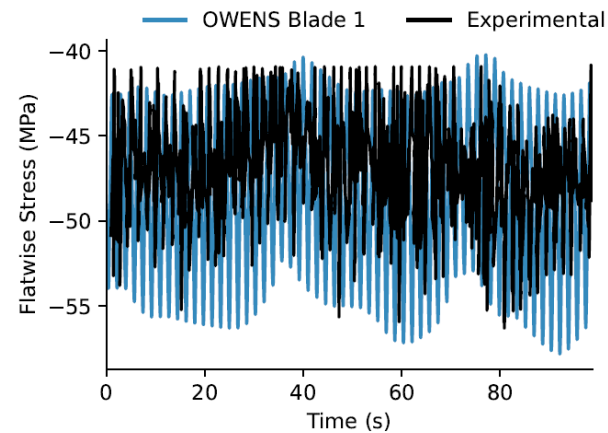
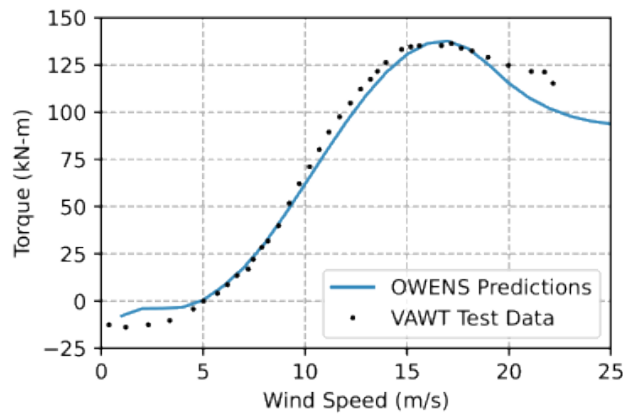


- Validated design tools appropriate for certification
- Large blade length, logistics for transportation and quayside installation
- Emergency shutdown control
- Predominant bearing loads are carried radially, not axially
- Industrialization and pilot-scale demonstration to de-risk and iterate on the design

# Development of Floating VAWT Design Optimization Tools



- Sandia's Offshore Wind Energy Simulator (OWENS) developed for design and optimization of floating VAWTs
- Required for certification of floating VAWTs and resulting commercialization



AIAA JOURNAL

## Vertical-Axis Wind Turbine Steady and Unsteady Aerodynamics for Curved Deforming Blades

Kevin R. Moore<sup>1</sup> and Brandon L. Ennis<sup>2</sup>  
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Vertical-axis wind turbines (VAWTs) have a long history with a wide variety of turbine archetypes, of which the Darrieus type is the most common. While few utility-scale VAWTs currently exist, VAWTs offer some often-stated advantages over traditional horizontal-axis wind turbines, such as being agnostic to the direction of the wind (no yaw error), reduced tower stake potential, and lower placement of the generator, which could provide particular benefit for floating offshore wind turbines. Presently, there are very few numerical design and analysis tools available for VAWTs. The Offshore Wind Energy Simulator (OWENS) tool is an aero-servo-elastic solver for simulating VAWTs and has limited functionality to simulate floating VAWTs. This article, a cross-collaboration between Sandia National Laboratories and the National Renewable Energy Laboratory, describes how OWENS has been coupled to several OpenFAST modules to support the coupled, aero-hydro-servo-elastic modeling of a floating offshore VAWT and discusses the verification of these new capabilities and features. This collaboration facilitates the development of OWENS for floating VAWT applications by coupling specific OpenFAST modules to enable additional modeling and simulation capabilities in OWENS, thus enabling the design and optimization of floating offshore VAWTs.

## Aeroelastic Validation of the Offshore Wind Energy Simulator for Vertical-Axis Wind Turbines

Kevin R. Moore<sup>1</sup> and Brandon L. Ennis<sup>2</sup>  
Sandia National Laboratories,<sup>2</sup> Albuquerque, NM 87185



Research Article

## Enabling Offshore Floating VAWT Design by Coupling OWENS and OpenFAST

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<sup>\*</sup> Correspondence: mckenzie@sandia.gov

**Abstract:** Vertical-axis wind turbines (VAWTs) have a long history with a wide variety of turbine archetypes, of which the Darrieus type is the most common. While few utility-scale VAWTs currently exist, VAWTs offer some often-stated advantages over traditional horizontal-axis wind turbines, such as being agnostic to the direction of the wind (no yaw error), reduced tower stake potential, and lower placement of the generator, which could provide particular benefit for floating offshore wind turbines. Presently, there are very few numerical design and analysis tools available for VAWTs. The Offshore Wind Energy Simulator (OWENS) tool is an aero-servo-elastic solver for simulating VAWTs and has limited functionality to simulate floating VAWTs. This article, a cross-collaboration between Sandia National Laboratories and the National Renewable Energy Laboratory, describes how OWENS has been coupled to several OpenFAST modules to support the coupled, aero-hydro-servo-elastic modeling of a floating offshore VAWT and discusses the verification of these new capabilities and features. This collaboration facilitates the development of OWENS for floating VAWT applications by coupling specific OpenFAST modules to enable additional modeling and simulation capabilities in OWENS, thus enabling the design and optimization of floating offshore VAWTs.

**Keywords:** vertical-axis wind turbine (VAWT); floating offshore wind turbine (FOWT); OWENS; OpenFAST; hydrodynamics

## 1. Introduction

Floating offshore wind turbines are a relatively young and growing technology domain that can play a significant role in decarbonizing the energy sector, particularly in geographic areas where a deep-water wind resource exists. However, additional research and development is needed to reduce the levelized cost of energy (LCOE) of floating offshore wind energy farms. This creates the need for verified and validated design tools to optimize floating offshore wind turbines and reduce their cost. One open-source, commonly used floating offshore wind turbine design and analysis tool is OpenFAST, which is an aero-hydro-servo-elastic solver developed and maintained by the National Renewable Energy Laboratory (NREL). OpenFAST is continuously being expanded to support many types of mooring systems, floating platform archetypes, and floating system dynamics and controls. OpenFAST has been extensively verified and validated for three-bladed, horizontal-axis, upwind turbines (HAWTs), but supports limited capability for vertical-axis wind turbines (VAWTs).

Vertical-axis wind turbines have a long history with a wide variety of turbine archetypes, of which the Darrieus type is the most common (though not necessarily dominant). VAWTs are more common in small wind or distributed wind applications. While few utility-scale VAWTs currently exist, VAWTs offer some often-stated advantages over HAWTs, such as being agnostic to the direction of the wind (no yaw

# Demonstration is necessary to realize the system benefits

