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Effects of Testing Rate on Hydrogen-Assisted Fracture of Ferritic Steels

Joe Ronevich*, Milan Agnani, Chris San Marchi

Sandia National Laboratories
Livermore, CA, USA



15th International Conference on Fracture (ICF15)

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Pipeline Blending CRADA

Objective - Provide scientific framework that enables blending of hydrogen into NG infrastructure

4 national laboratories

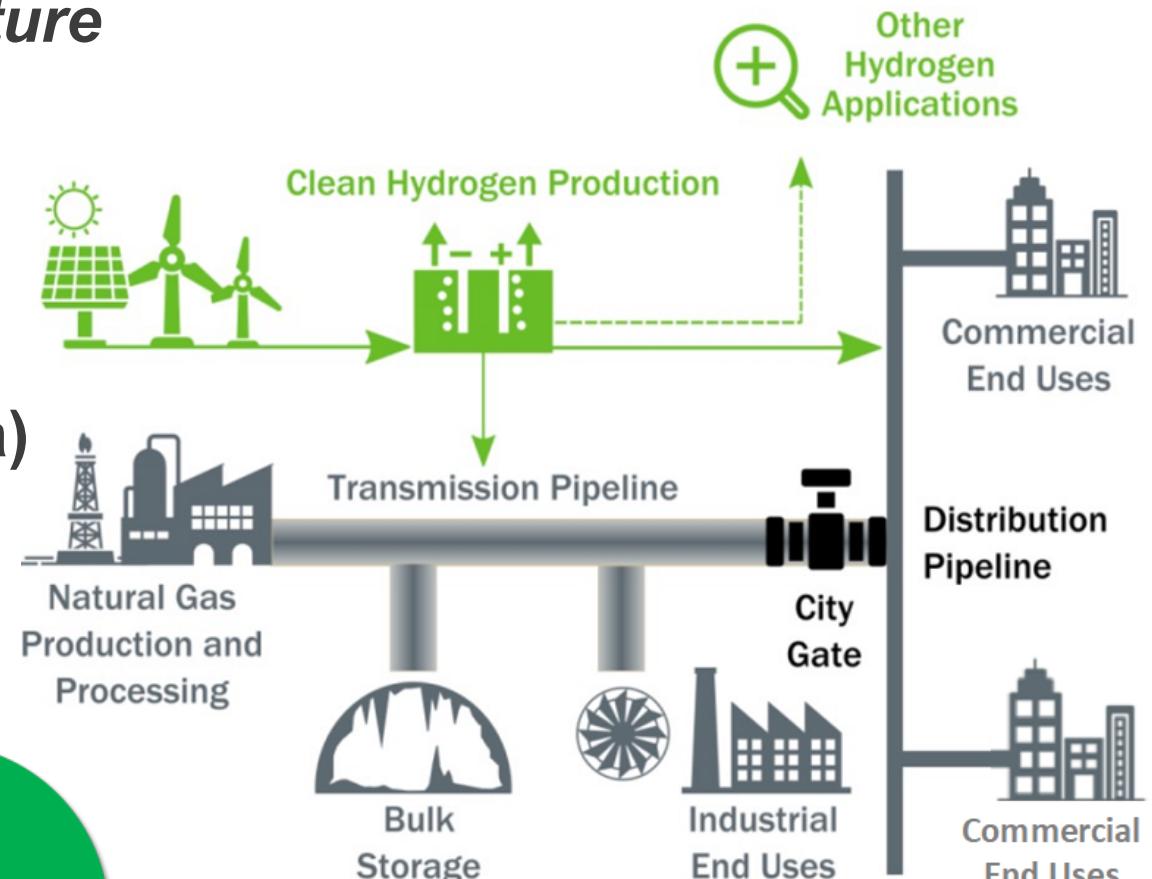
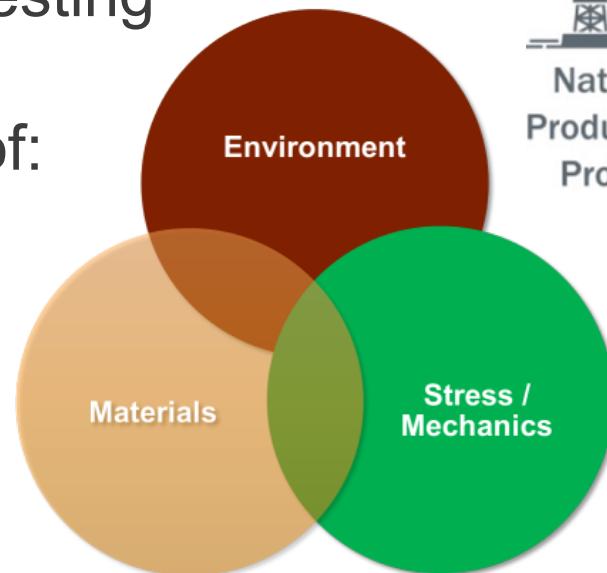
26 total industry, academia, and consortium partners

Structural Materials Task: Metals (Sandia)

→ Fatigue and Fracture Testing
of Vintage pipe / welds

→ Understand influence of:

- Pressure
- Microstructure
- **Rate / Frequency**
- Strength



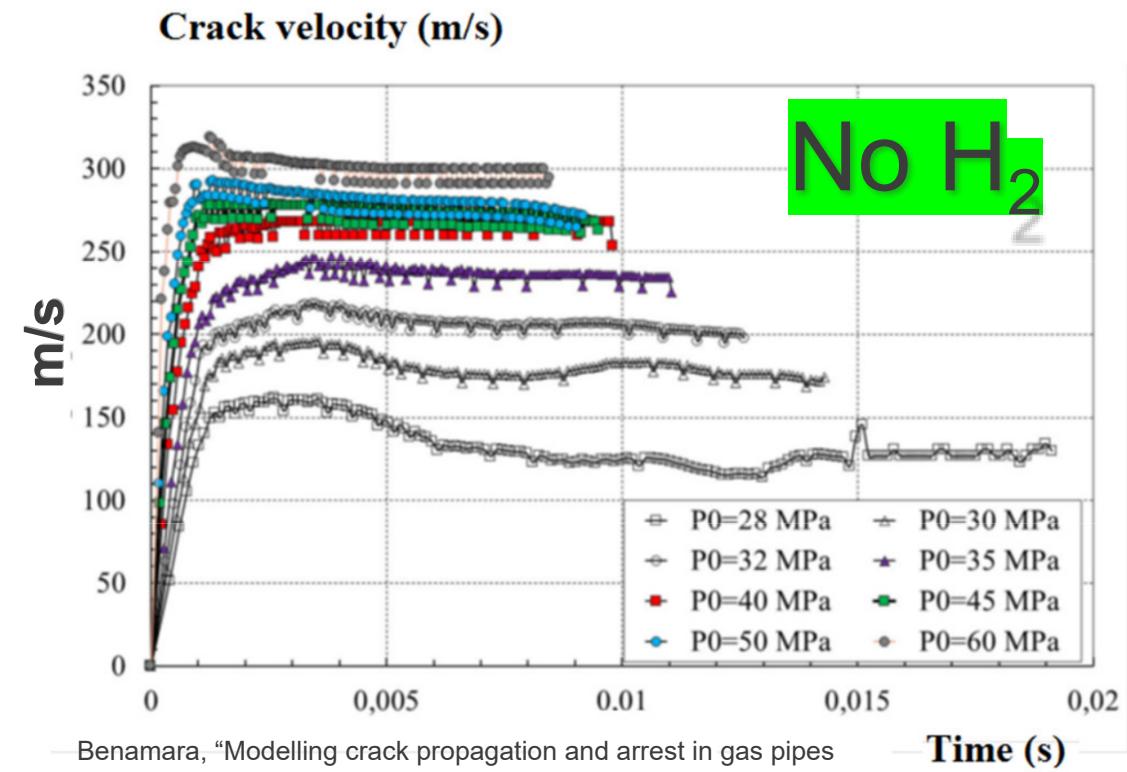
Oct 2021 – Sept 2023 (2 yr project)

Research Question: Does hydrogen have an influence on fracture resistance at fast testing rates?

→ Fracture along a seam weld of pipe can be rapid (>100 m/s)



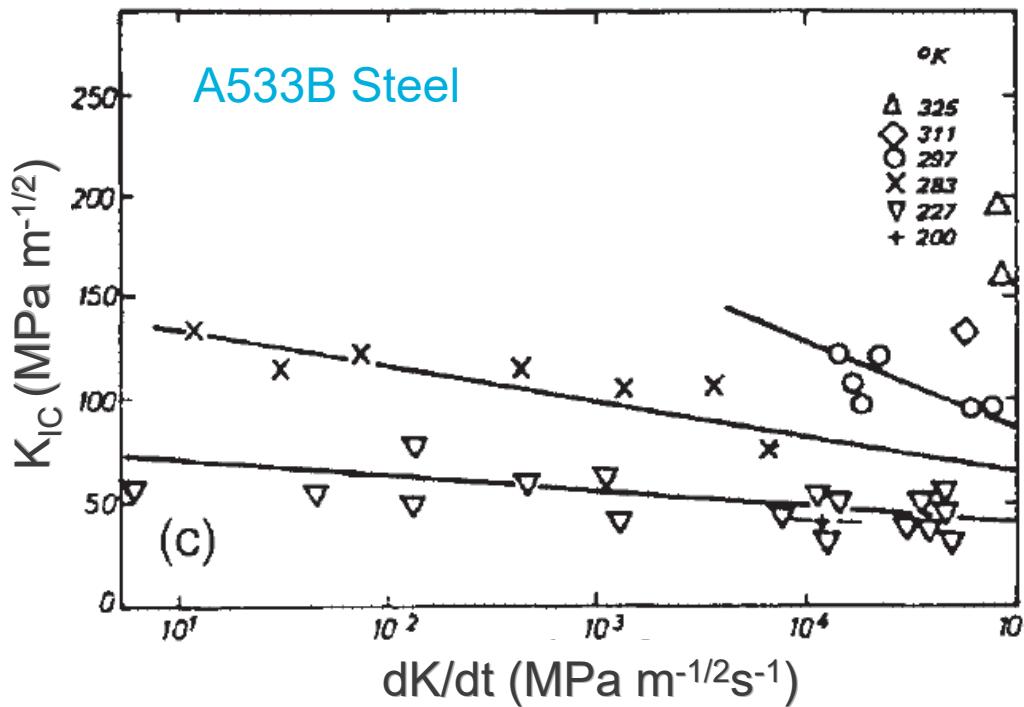
<https://www.ogj.com/general-interest/companies/article/17232192/fullscale-burst-crackarrest-testing-vets-x120-line-pipe>



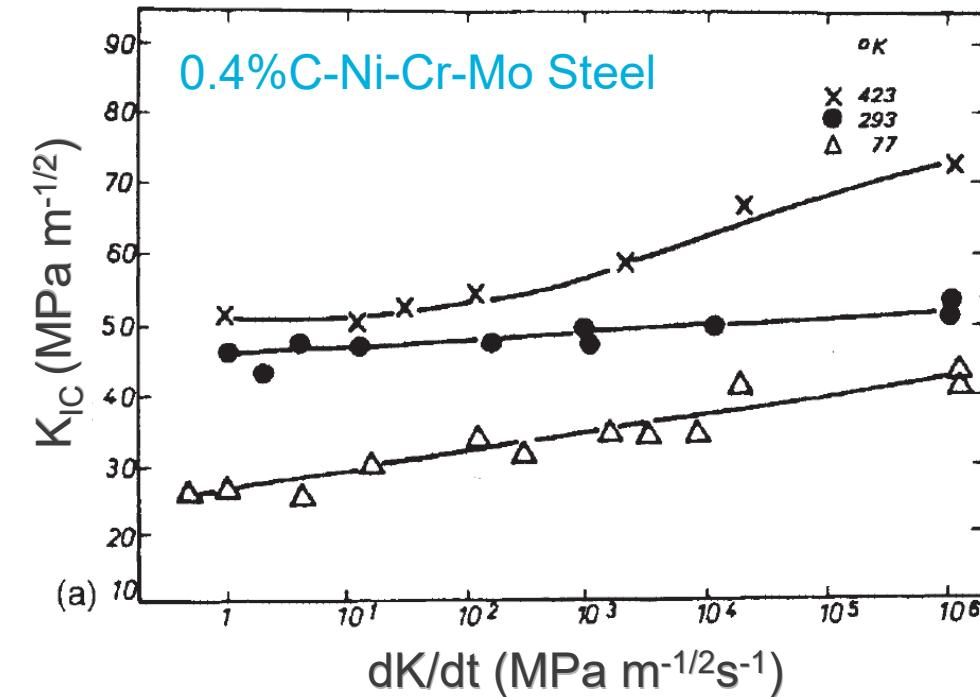
Conventional fracture toughness testing is performed at slow quasi-static rates → Limited data at fast rates in H_2

In absence of H₂, testing rate can influence fracture toughness

K_{IC} can \downarrow as dK/dt \uparrow



K_{IC} can \uparrow as dK/dt \uparrow



Will hydrogen influence this trend?

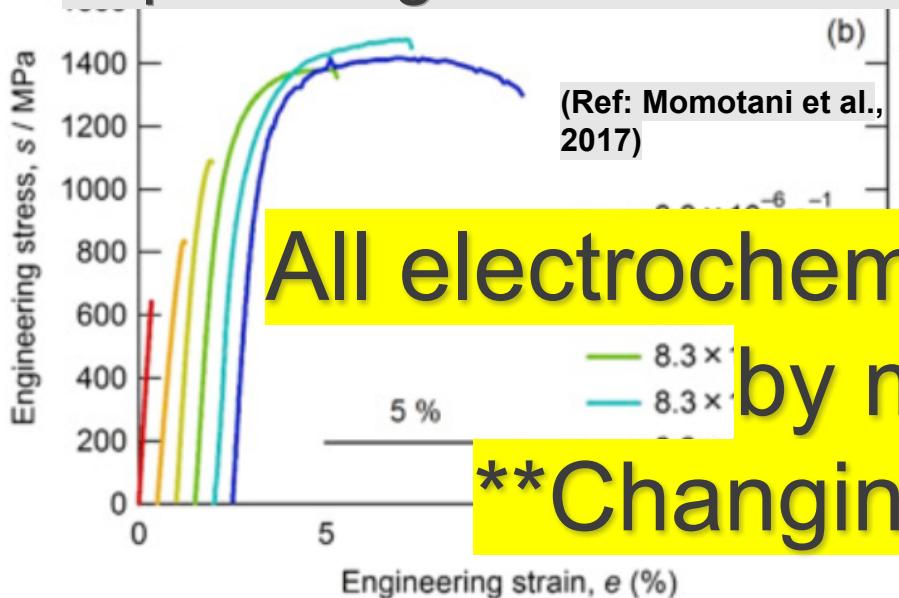
Conventional thinking with H₂...

Faster testing rates

Limited Hydrogen diffusion / accumulation

Mitigates / eliminates hydrogen embrittlement

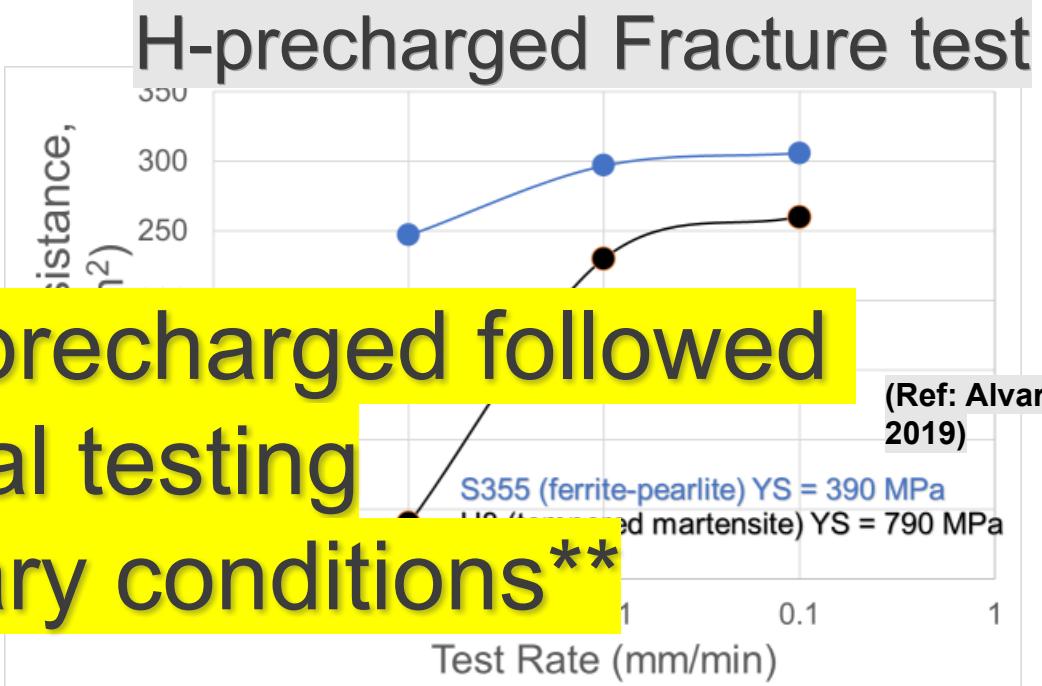
H-precharged Tensile test



All electrochemically H-precharged followed by mechanical testing
Changing boundary conditions

As strain rate \uparrow effects of hydrogen \downarrow
For hydrogen precharged low-carbon martensite

H-precharged Fracture test

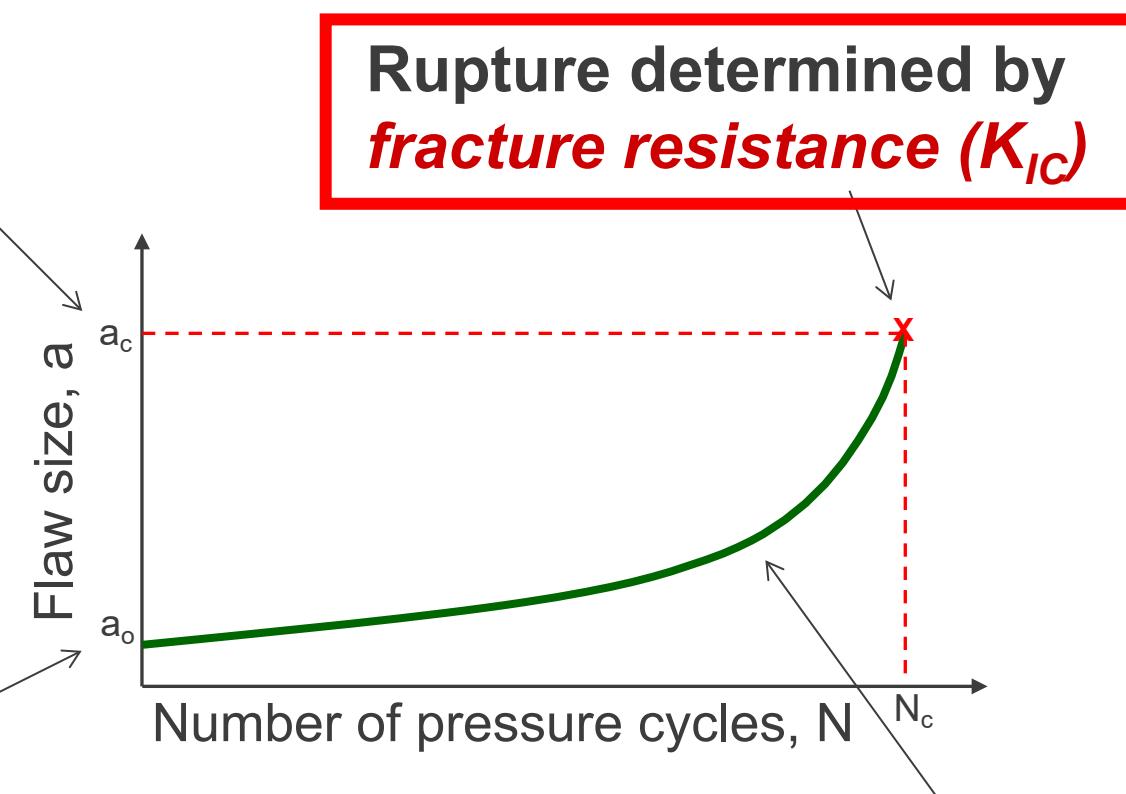
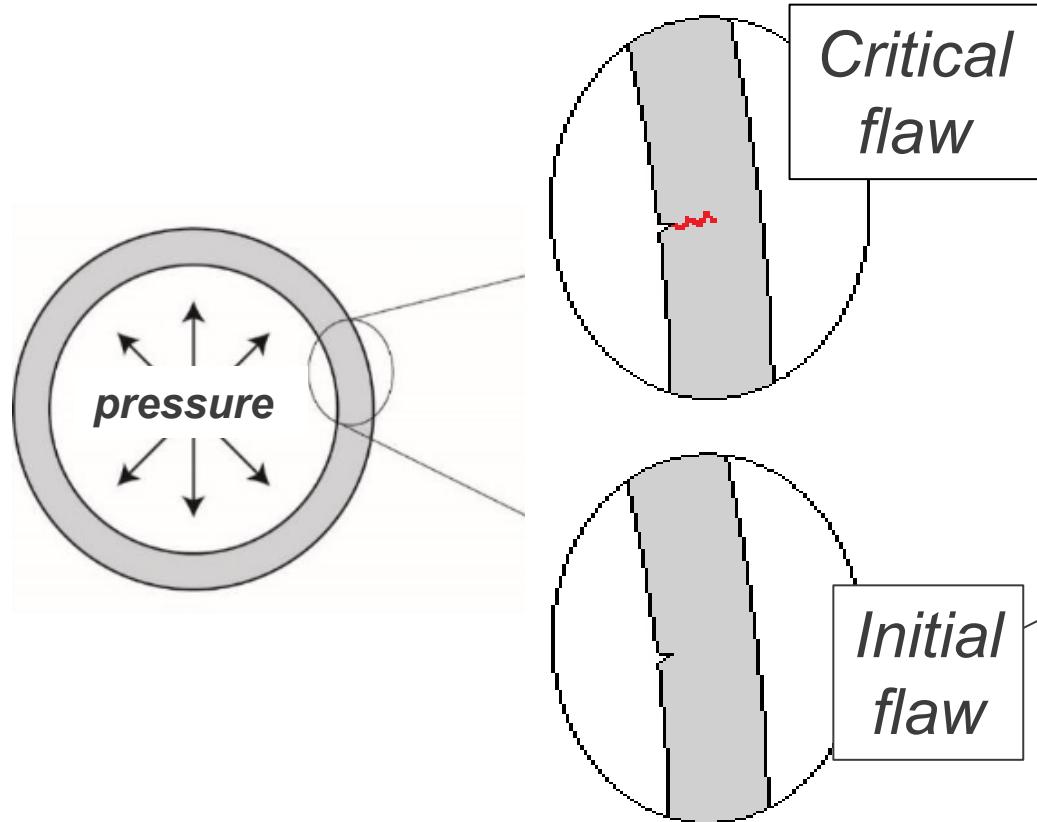


Rate effects still apparent
→ Less rate dependence on low strength steel than high strength steel



Fracture Testing in gaseous H₂

Testing motivation: structural integrity assessment utilizing fracture mechanics-based analysis

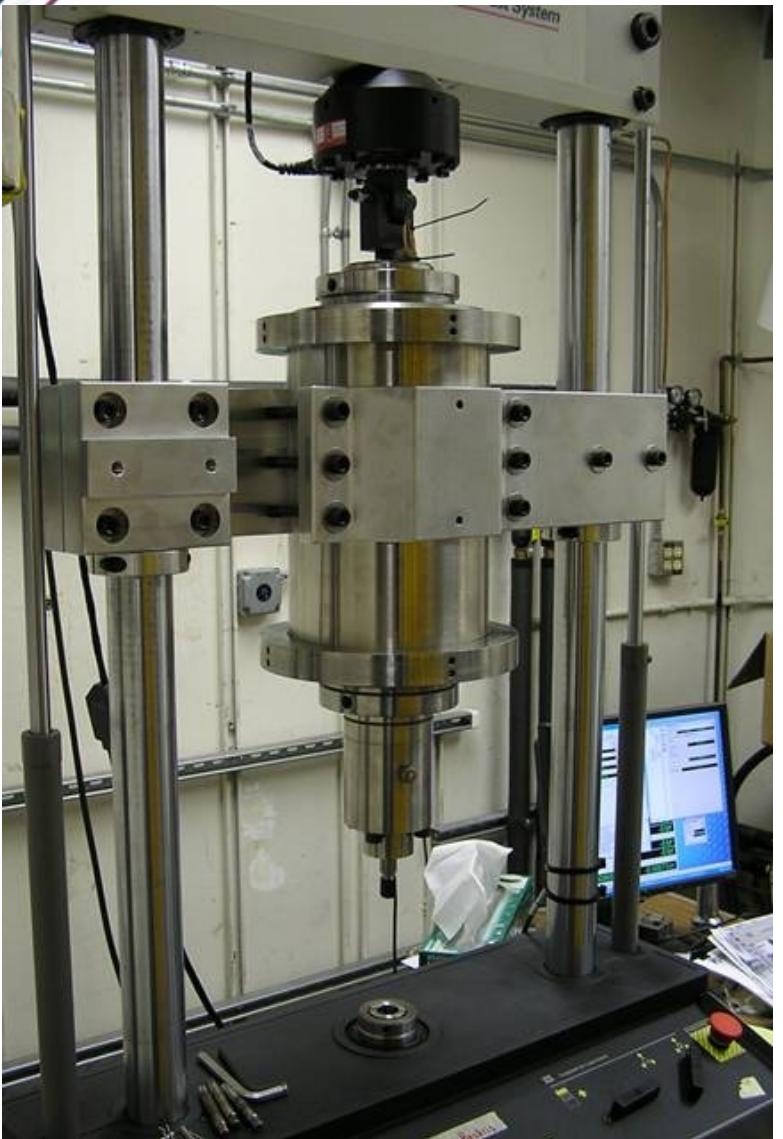


Rupture determined by
fracture resistance (K_{IC})

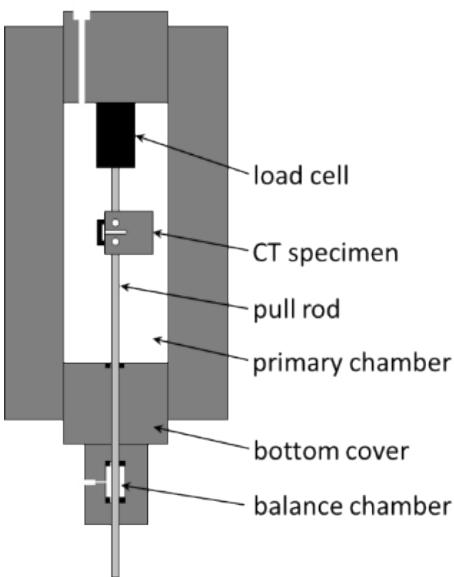
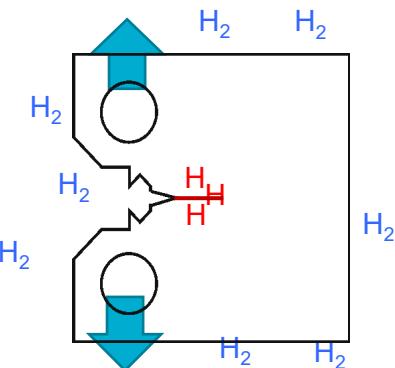
Evolution of flaw size determined by
fatigue crack growth ($da/dN - \Delta K$ data)

ASME B31.12 describes rules for hydrogen pipelines with reference to ASME BPVC Section VIII, Division 3, Article KD-10

Fatigue and Fracture Testing at Hydrogen Effects on Materials Lab



Compact Tension (C(T))



Instrumentation

- Internal Load cell
- Clip gauge
- Direct Current Potential Difference (DCPD)

Fatigue: ASTM E647

- Load ratios (R) 0.1 to 0.8
- Frequency: $0.01 \rightarrow 10$ Hz
- Constant load or K-control

Fracture: ASTM E1820 (Elastic-Plastic)

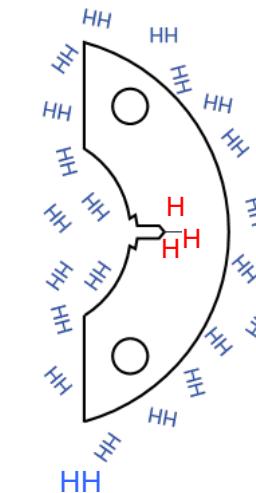
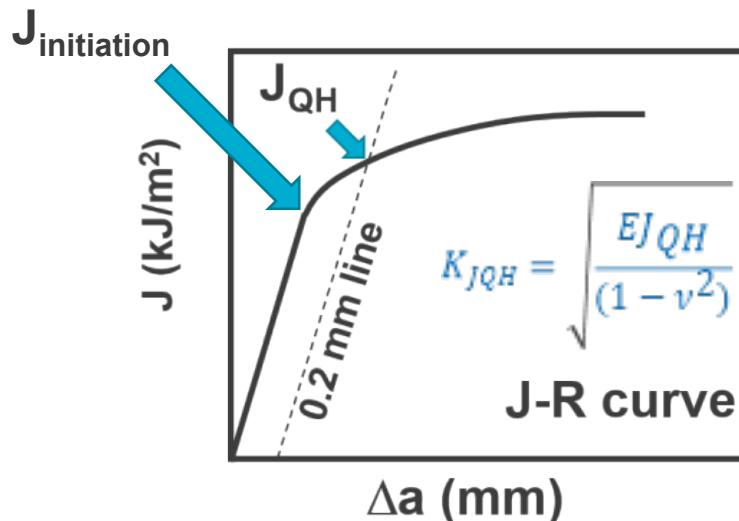
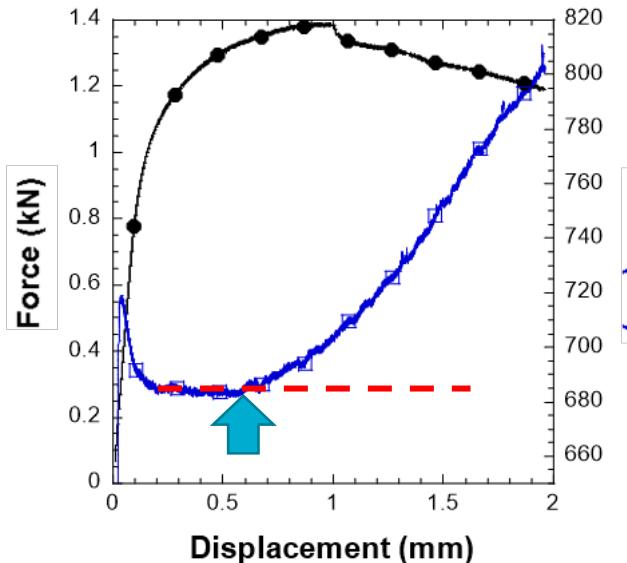
Environment

- Air
- Pure H_2
- Gas blends, e.g. $\text{N}_2 - 3\% \text{H}_2$
- Gas impurity mixtures:
e.g. $\text{H}_2 + 10\text{-}1000$ ppm O_2

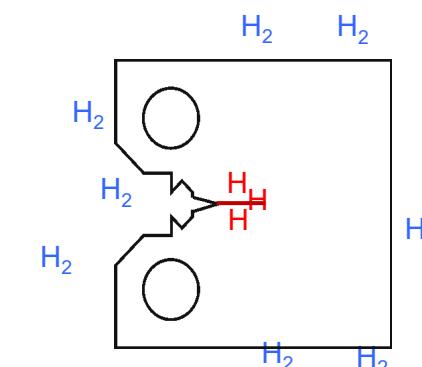
Two pipeline materials were examined

Grade	YS (MPa)	Year	Composition in wt. %								
			C	Si	Mn	P	S	V	Nb	Ti	B
X100	910	2000s	0.085	0.26	1.69	0.013	<0.001	-	0.047	0.017	0.0015
X52	490	1962	0.293	0.02	1.17	0.016	0.016	<0.002	<0.005	<0.002	<0.0005

- ASTM E1820 elastic-plastic fracture test (J-R curve)
- Fracture Displacement Rates:
 - 0.005 → 5 mm/min



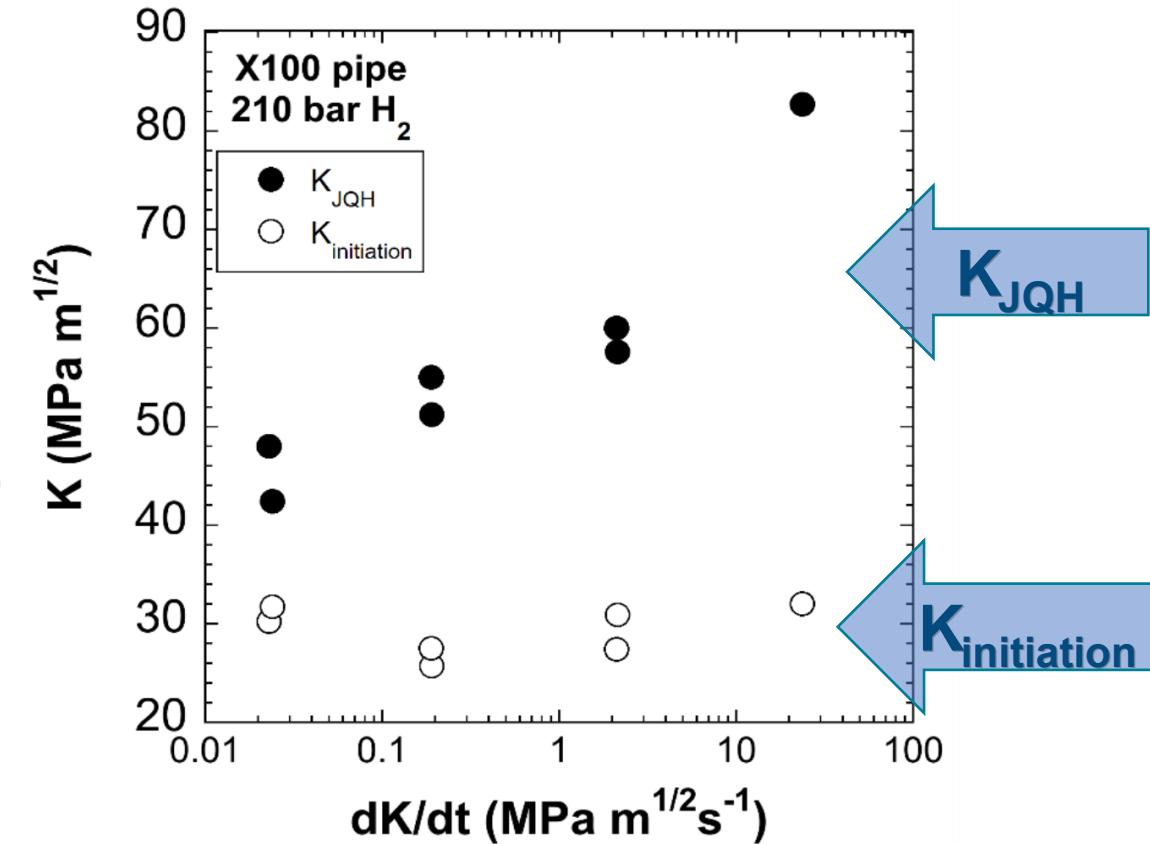
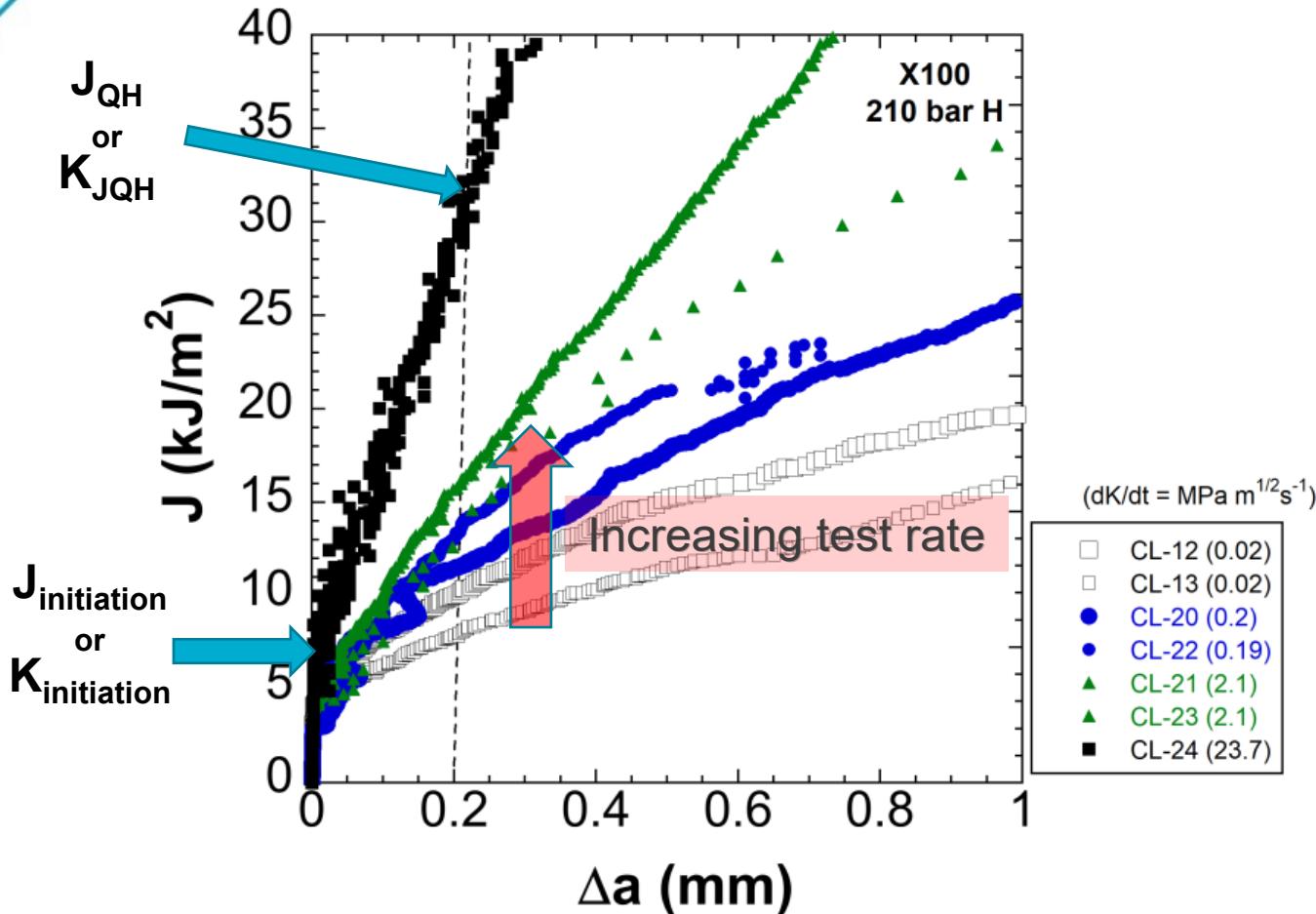
X100
Arc



X52
CT

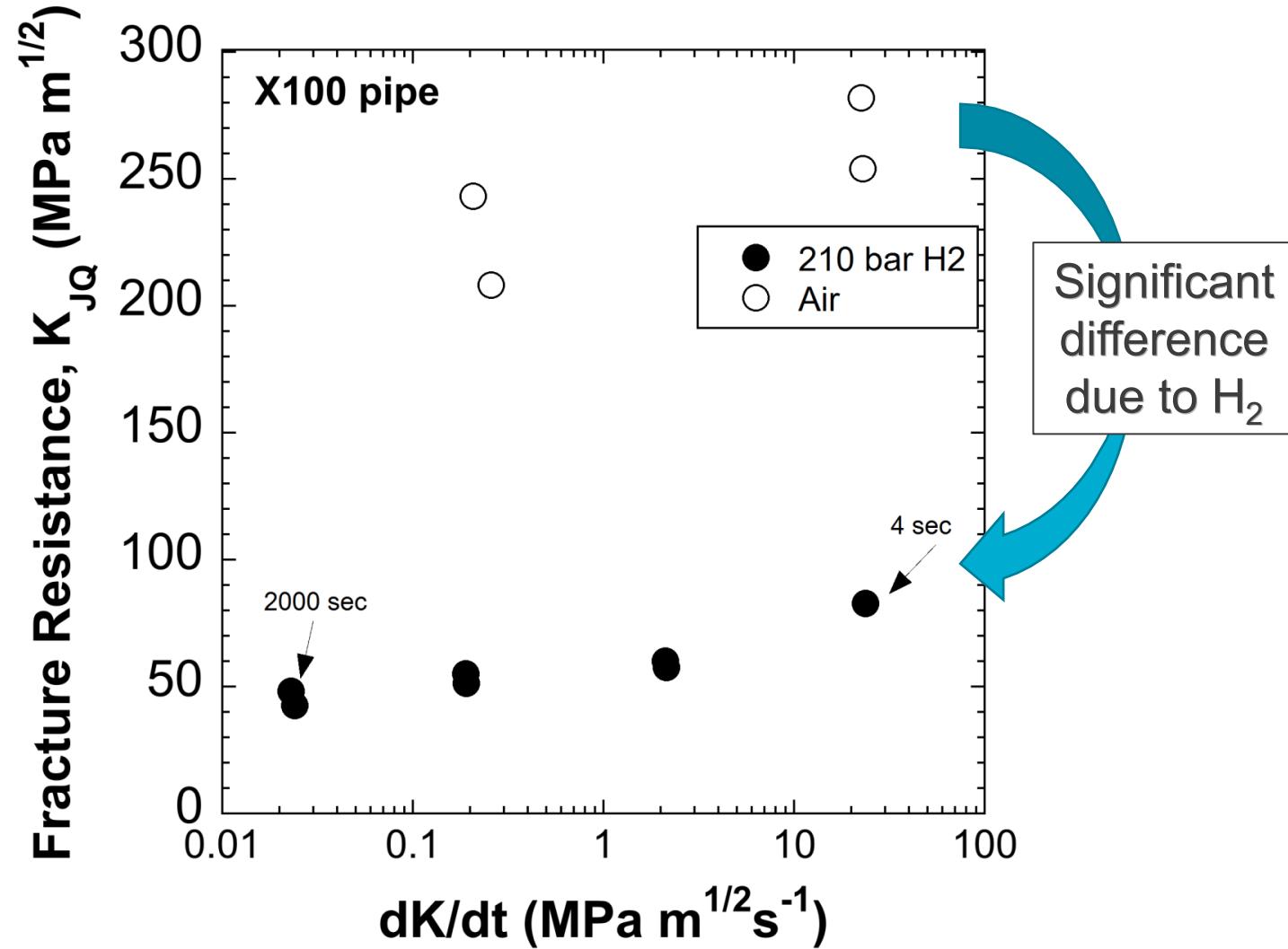
Determined fracture initiation ($J_{\text{initiation}}$) and fracture resistance (J_{QH}) from J-R curves → converted to K

Tearing modulus is clearly influenced by testing rate



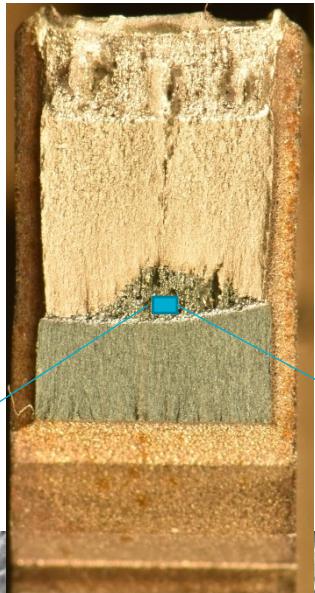
X100 fracture resistance (K_{QH}) was rate-dependent
→ $K_{\text{initiation}}$ was less sensitive to rate

Even at high loading rates, effects of hydrogen cannot be ignored

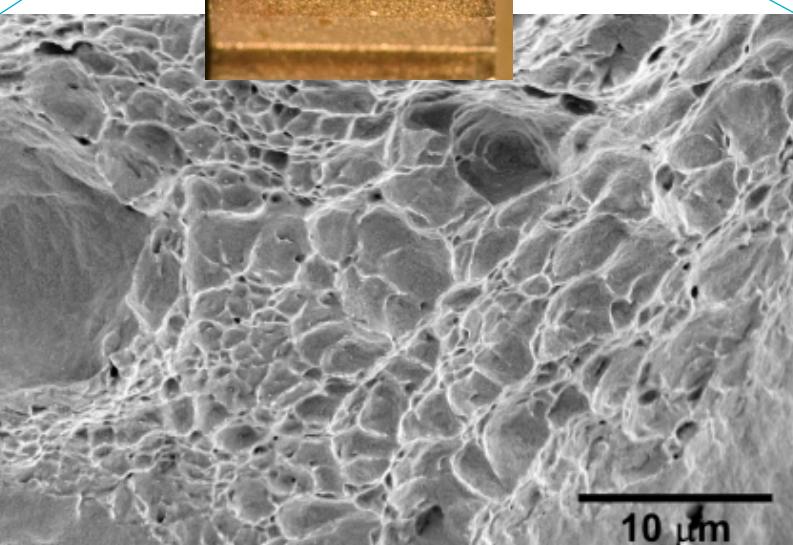


Fracture surfaces still exhibit quasi-cleavage fracture at all rates when tested in gaseous H₂

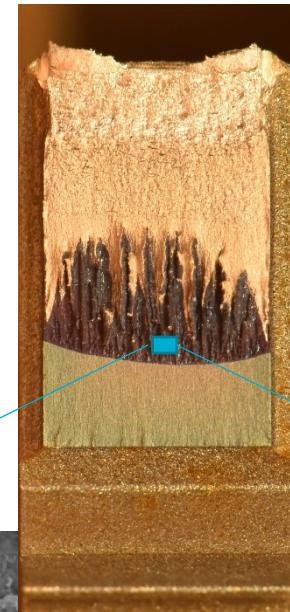
Air (0.05 mm/min)



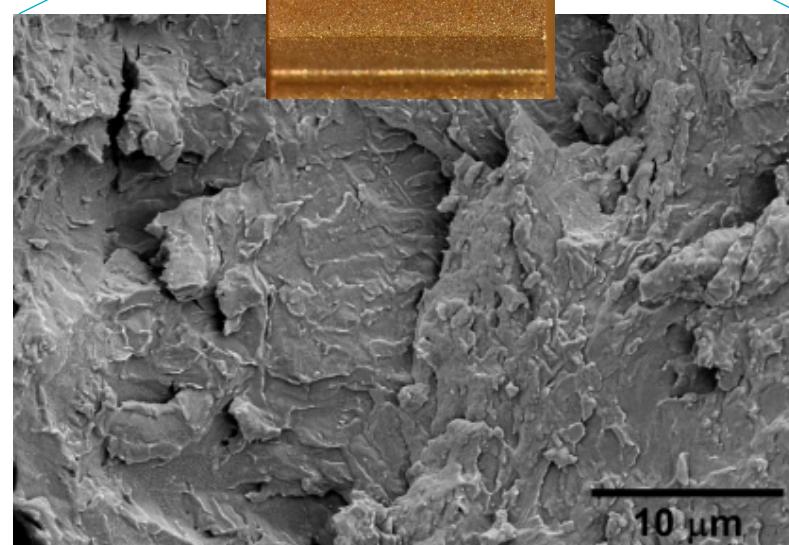
$$K_{JQ} = 208 \text{ MPa m}^{1/2}$$



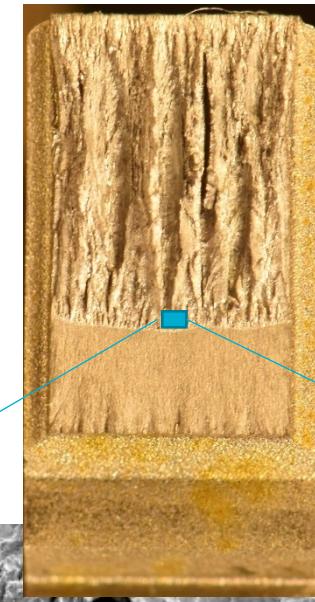
210 bar H₂
(0.005 mm/min)



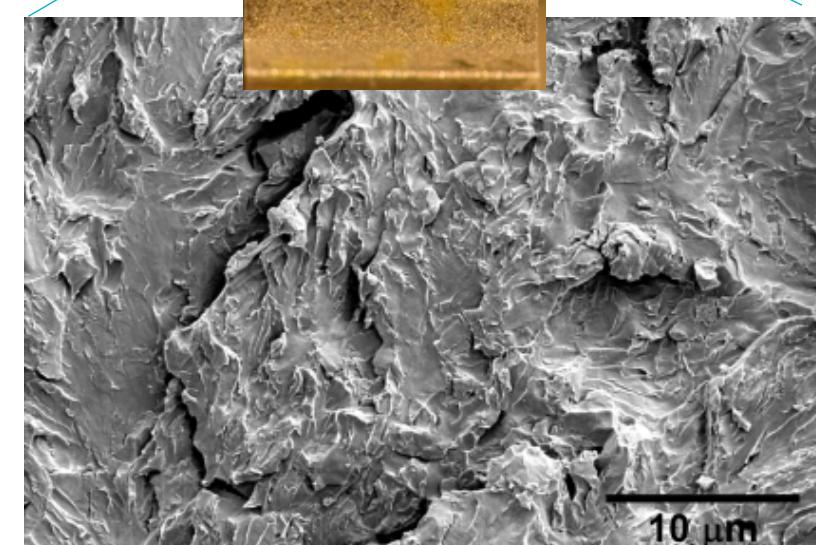
$$K_{JQH} = 42 \text{ MPa m}^{1/2}$$



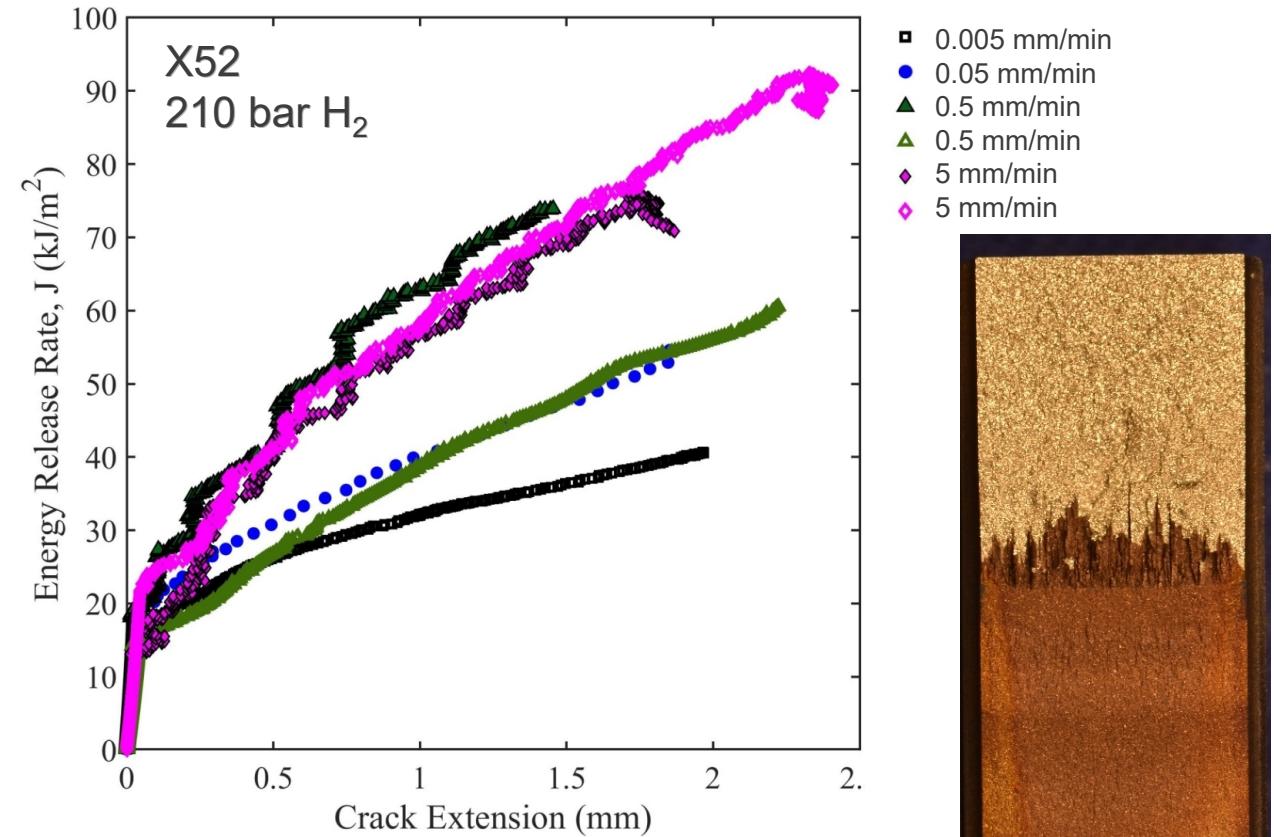
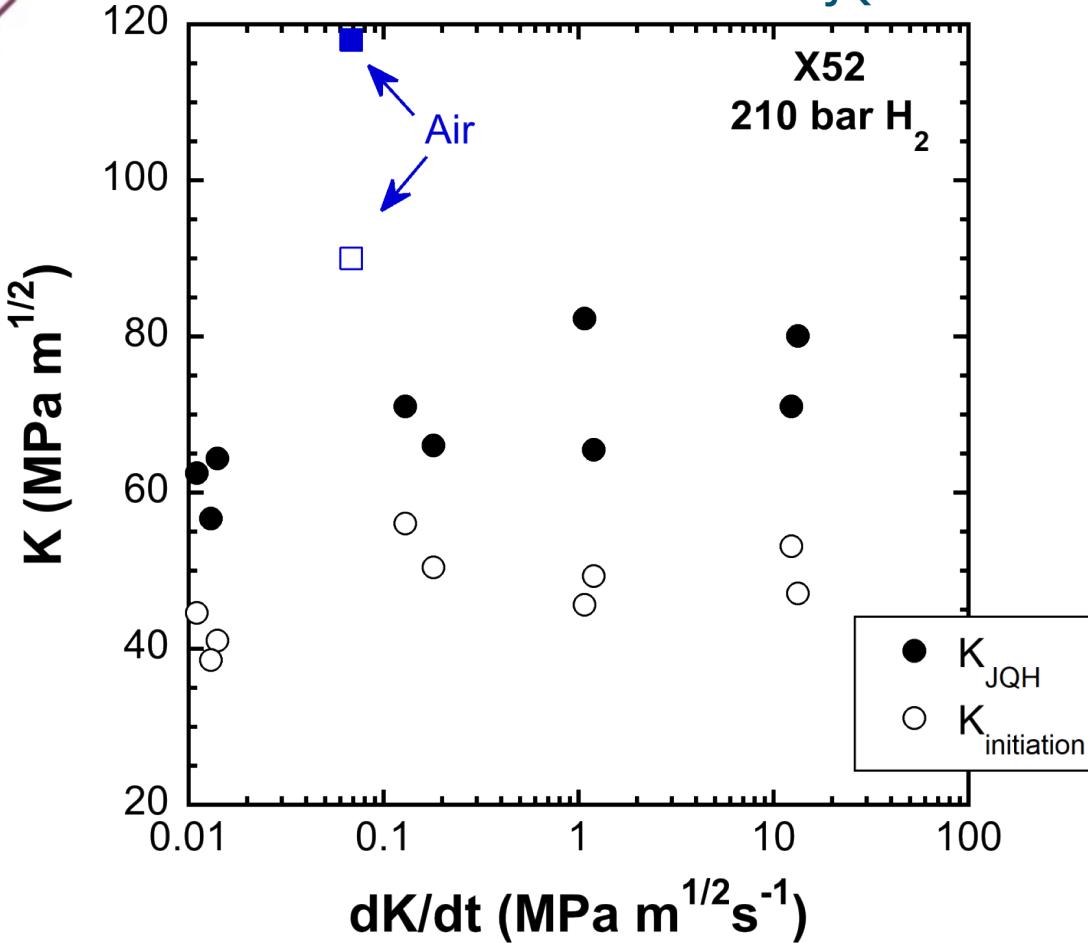
210 bar H₂
(5 mm/min)



$$K_{JQH} = 83 \text{ MPa m}^{1/2}$$



X52 showed more variability for $K_{\text{initiation}}$ and K_{JQH}
 → Small increase in K_{JQH} with dK/dt



Variability might be due to:

→ Inclusions

→ Smaller difference between air and H_2 fracture toughness



Summary

Two pipeline steels (X52 and X100) were subjected to fracture testing in 210 bar H₂ at different testing rates

X100

- Increased K_{JQH} at faster testing rates
- Negligible change in fracture initiation (K_{initiation}) with testing rate

X52

- Small increase in K_{JQH} at faster testing rates
- Fracture initiation (K_{initiation}) exhibited more variability

Hydrogen still influences fracture even at fast testing rates & should not be ignored

Gaps Remaining:

- Influence of delaminations on fracture toughness
- Role of inclusions in crack initiation

Thank you for your attention!

Joe Ronevich

jaronev@sandia.gov

Chris San Marchi

cwsanma@sandia.gov

Milan Agnani

magnani@sandia.gov

Additional HEML Team Members

James McNair

Brendan Davis

Keri McArthur

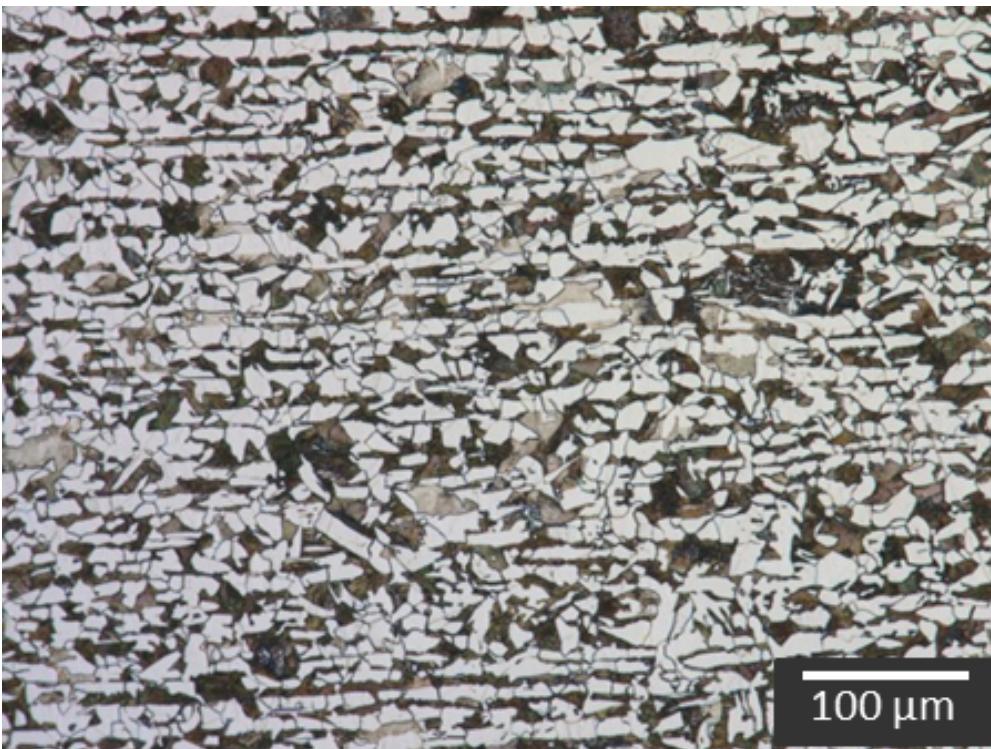
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Microstructures

X52 – Ferrite/Pearlite



X100 – Acicular Ferrite/Bainite

