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# Effects of Testing Rate on Hydrogen-Assisted Fracture of Ferritic Steels

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# Pipeline Blending CRADA

**Objective - Provide scientific framework that enables blending of hydrogen into NG infrastructure**

4 national laboratories

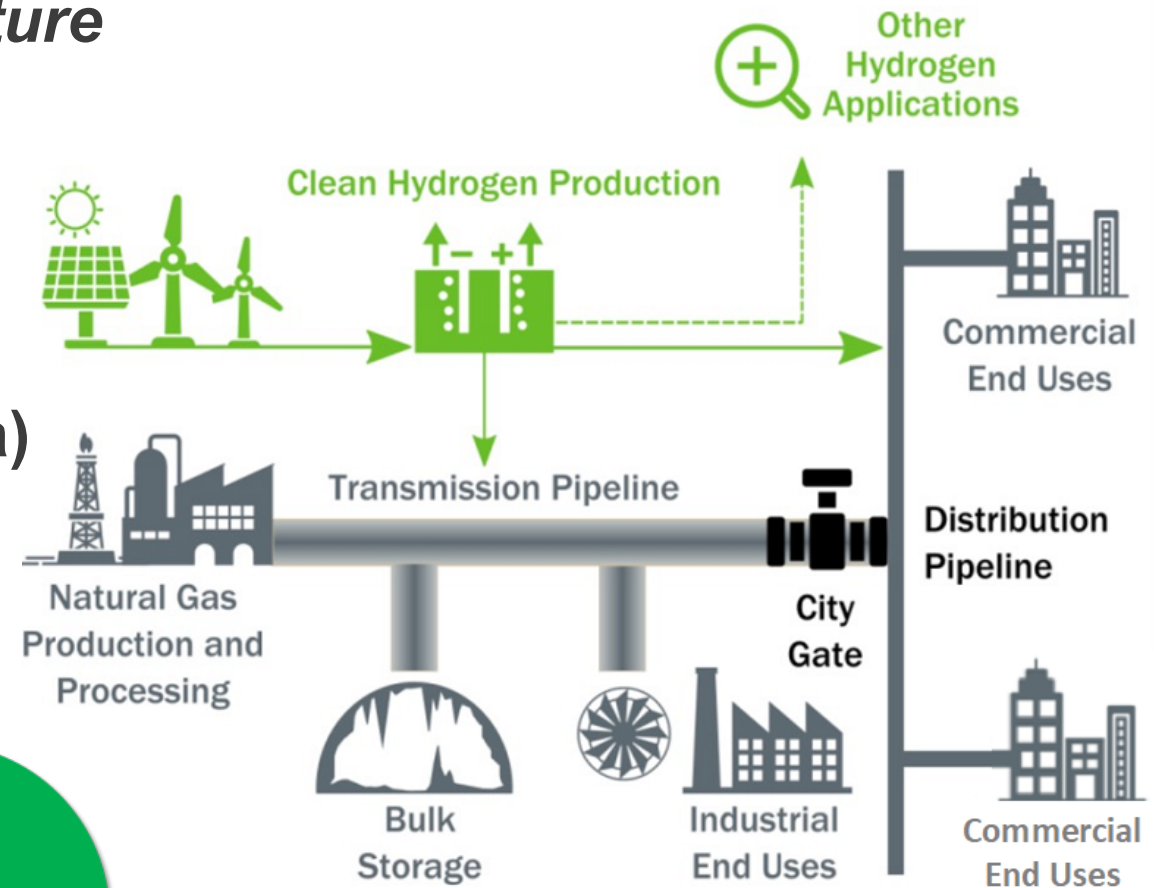
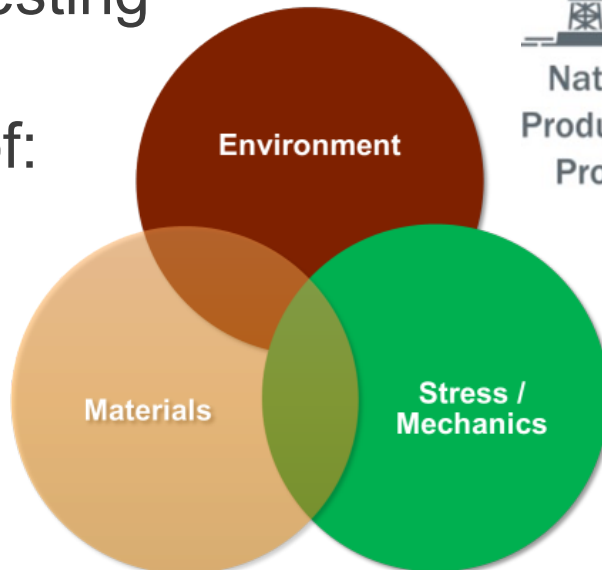
26 total industry, academia, and consortium partners

## Structural Materials Task: Metals (Sandia)

→ Fatigue and Fracture Testing of Vintage pipe / welds

→ Understand influence of:

- Pressure
- Microstructure
- Rate / Frequency
- Strength



Oct 2021 – Sept 2023 (2 yr project)

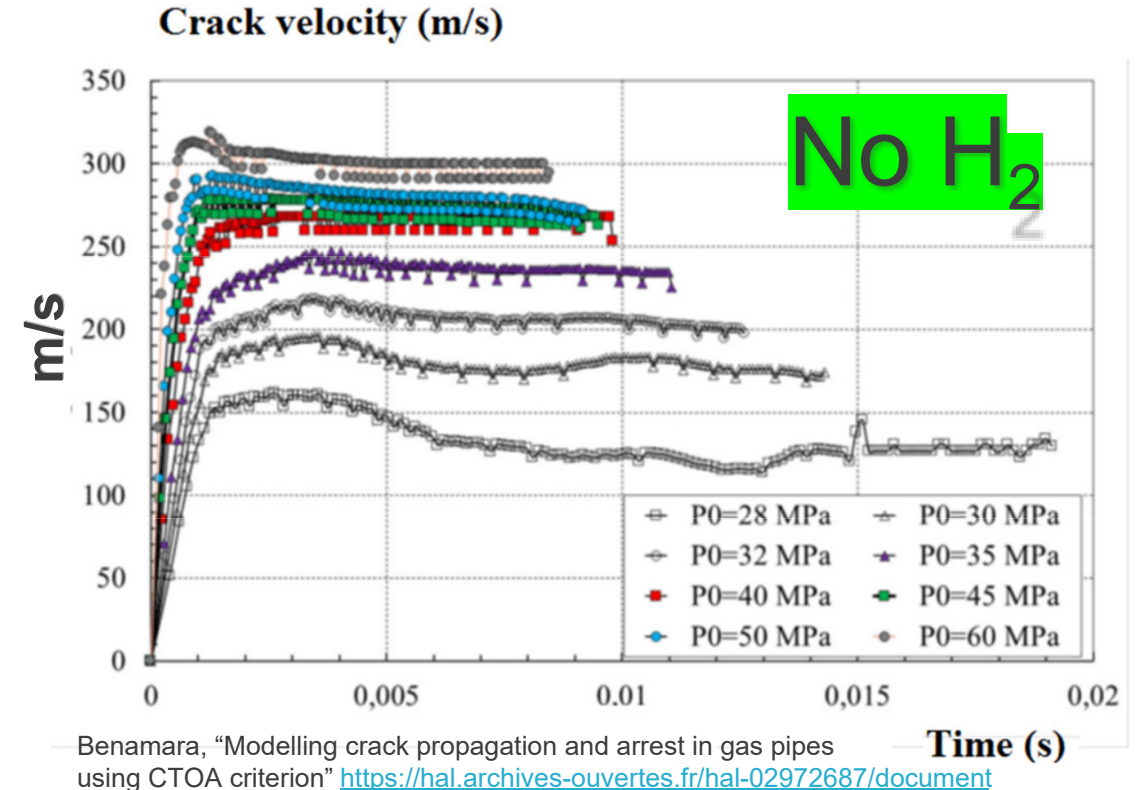


# Research Question: Does hydrogen have an influence on fracture resistance at fast testing rates?

→ Fracture along a seam weld of pipe can be rapid ( $>100$  m/s)



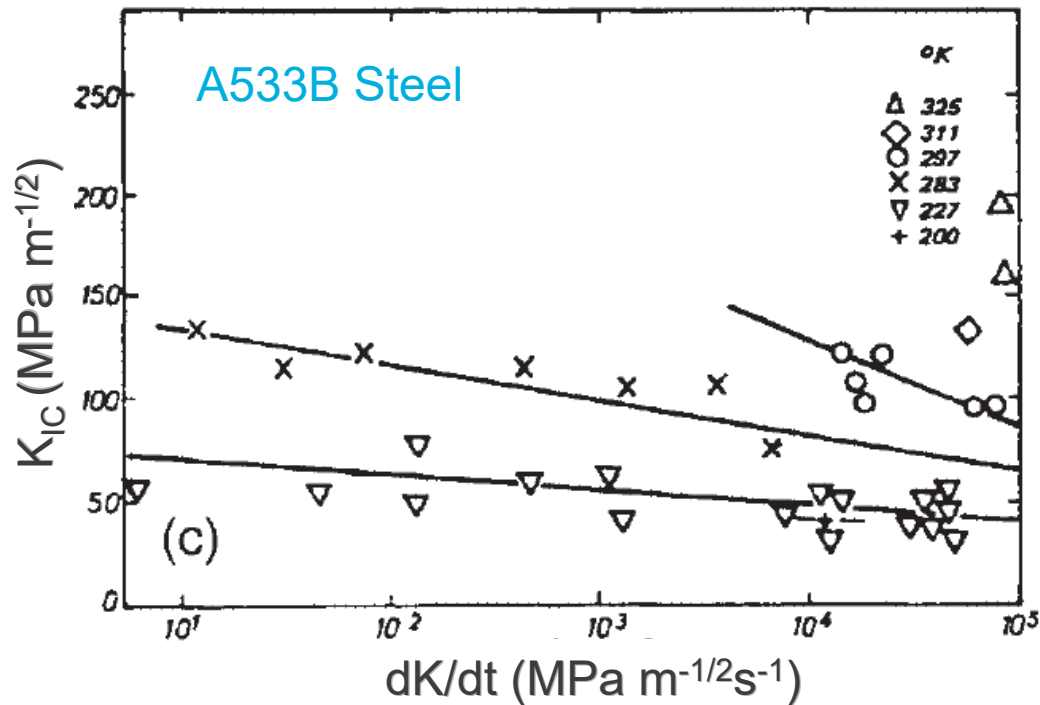
<https://www.ogj.com/general-interest/companies/article/17232192/fullscale-burst-crackarrest-testing-vets-x120-line-pipe>



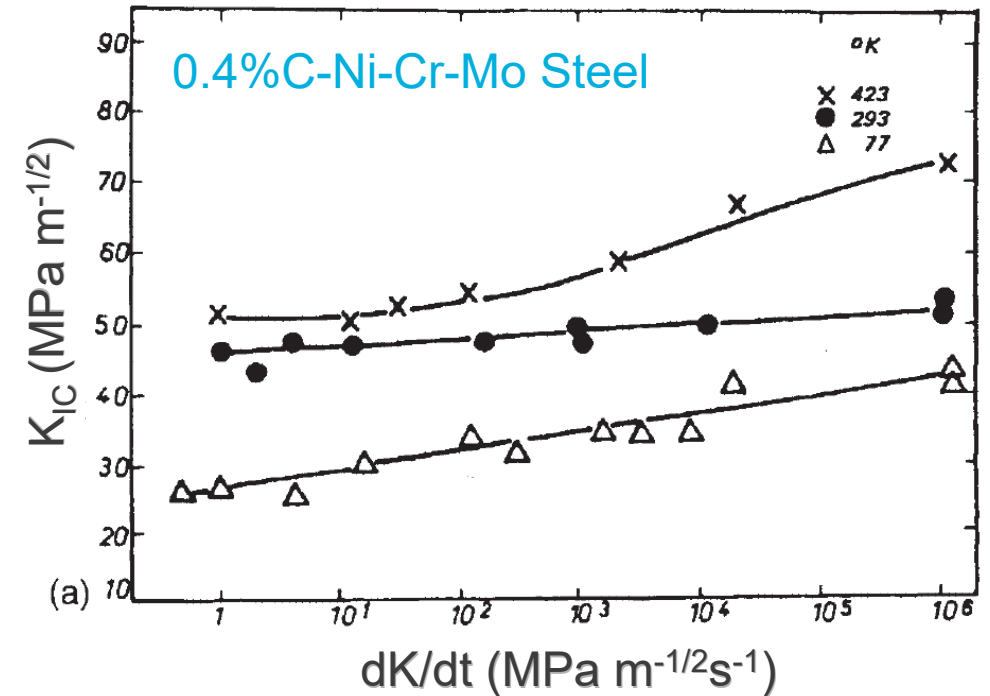
Conventional fracture toughness testing is performed at slow quasi-static rates → Limited data at fast rates in  $H_2$

# In absence of $H_2$ , testing rate can influence fracture toughness

$K_{IC}$  can ↓ as  $dK/dt$  ↑



$K_{IC}$  can ↑ as  $dK/dt$  ↑



Will hydrogen influence this trend?

# Conventional thinking with H<sub>2</sub>...

Faster testing rates

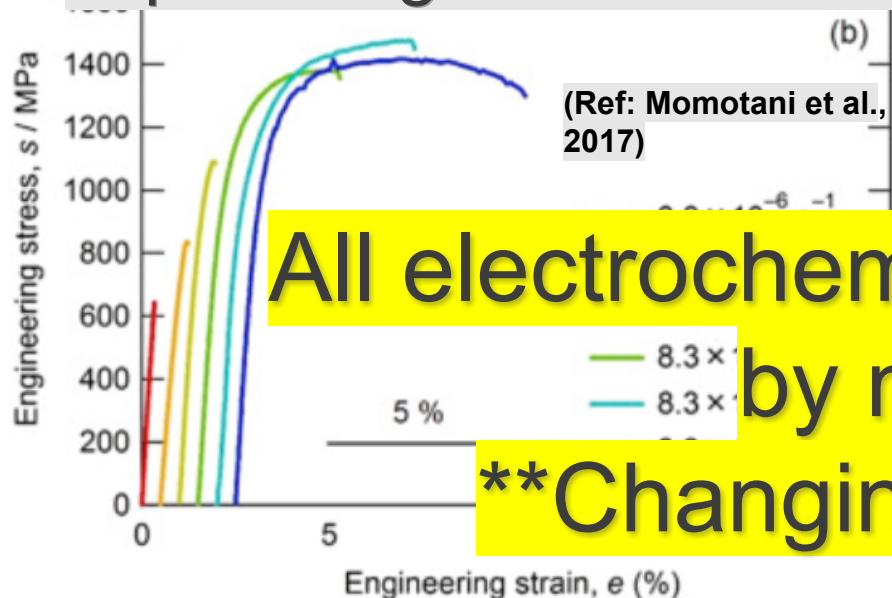


Limited Hydrogen diffusion / accumulation

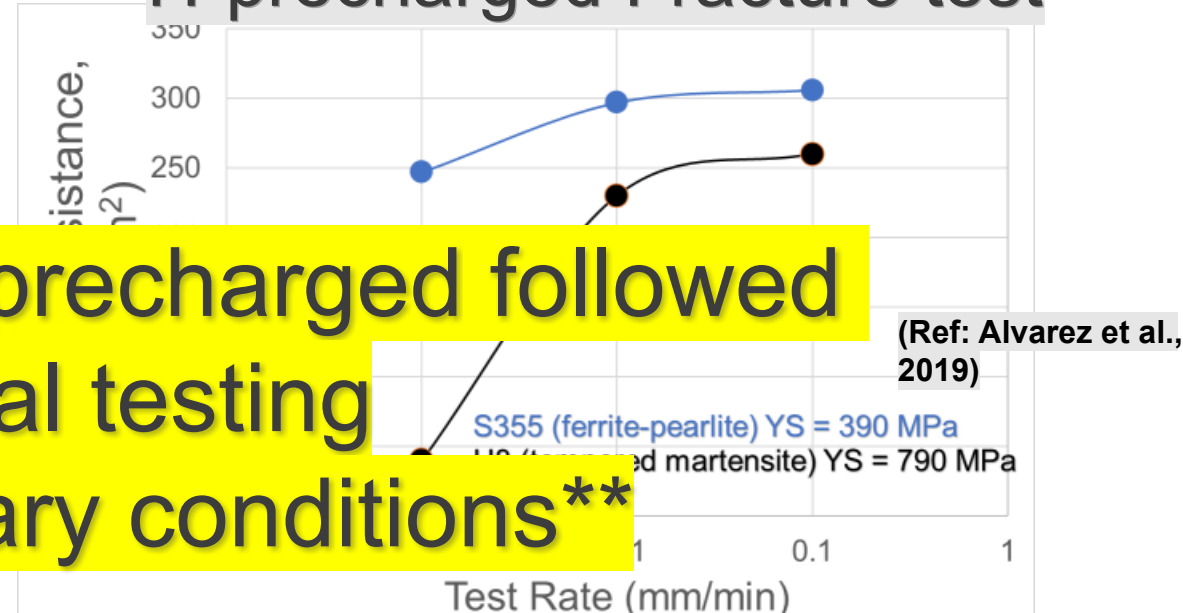


Mitigates / eliminates hydrogen embrittlement

## H-precharged Tensile test



## H-precharged Fracture test



All electrochemically H-precharged followed by mechanical testing

**\*\*Changing boundary conditions\*\***

As strain rate  $\uparrow$  effects of hydrogen  $\downarrow$   
For hydrogen precharged low-carbon martensite

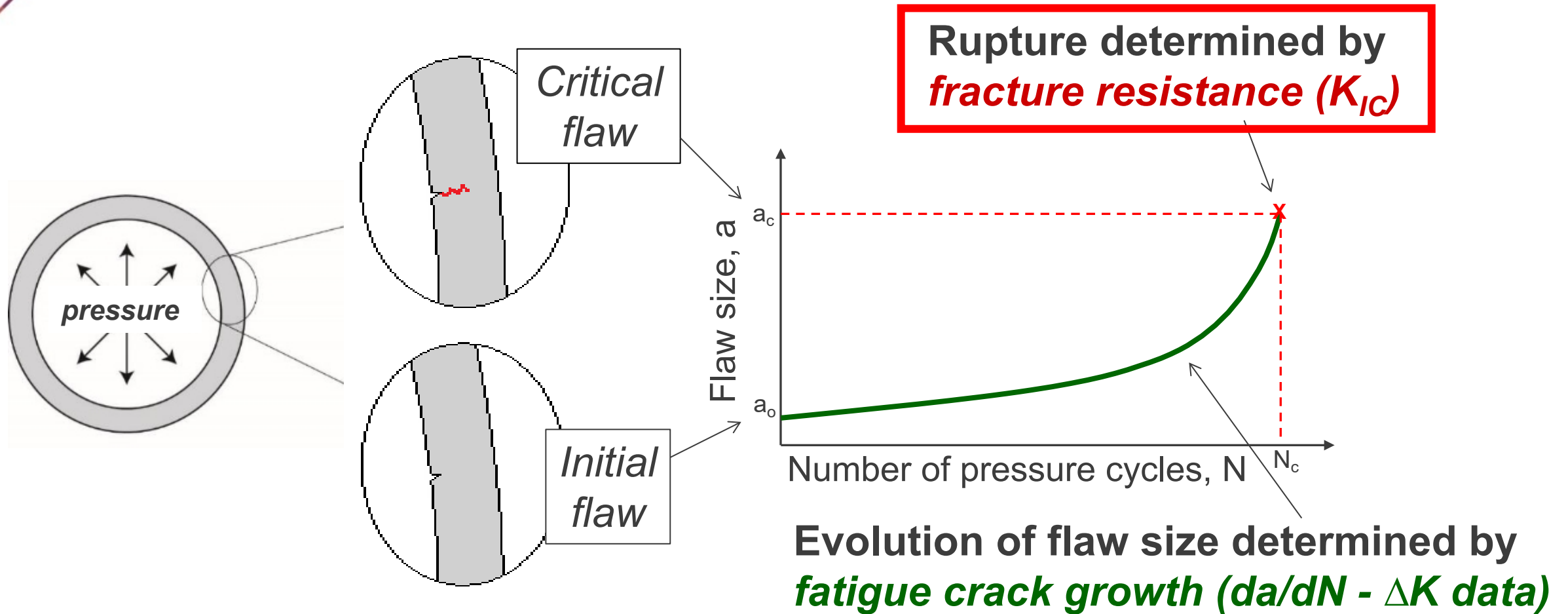
Rate effects still apparent  
 $\rightarrow$  Less rate dependence on low strength steel than high strength steel



Fracture  
Testing in  
gaseous H<sub>2</sub>



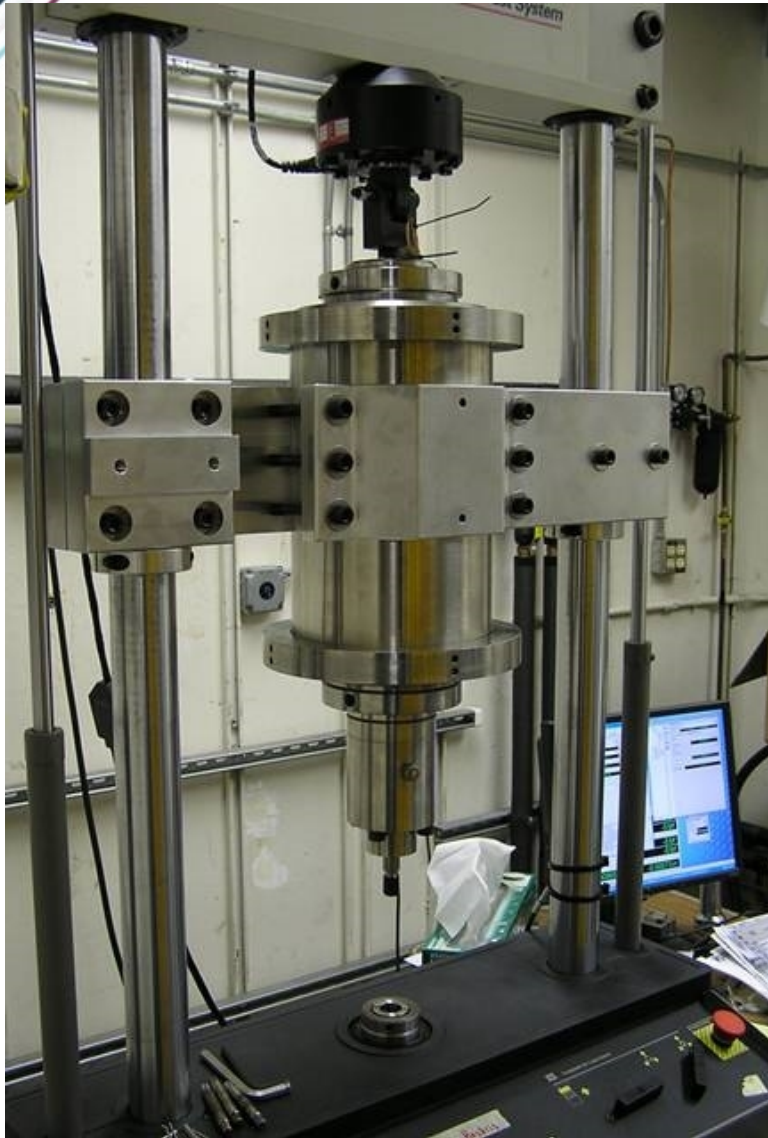
# Testing motivation: structural integrity assessment utilizing fracture mechanics-based analysis



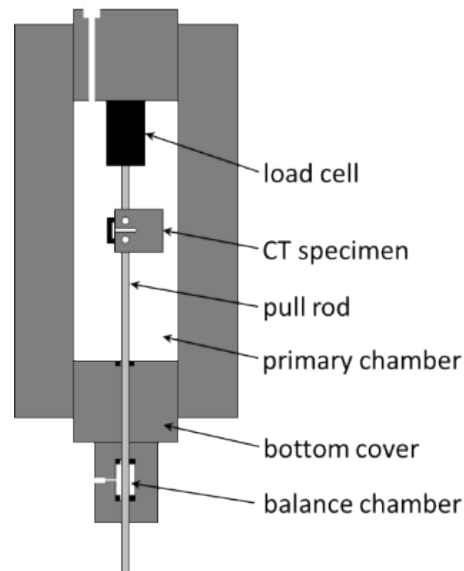
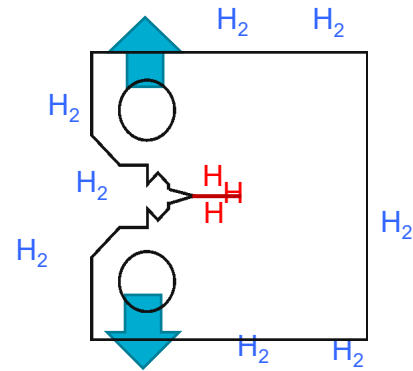
ASME B31.12 describes rules for hydrogen pipelines with reference to ASME BPVC Section VIII, Division 3, Article KD-10



# Fatigue and Fracture Testing at Hydrogen Effects on Materials Lab



## Compact Tension (C(T))



## Instrumentation

- Internal Load cell
- Clip gauge
- Direct Current Potential Difference (DCPD)

## Fatigue: ASTM E647

- Load ratios (R) 0.1 to 0.8
- Frequency: 0.01 → 10 Hz
- Constant load or K-control

## Fracture: ASTM E1820 (Elastic-Plastic)

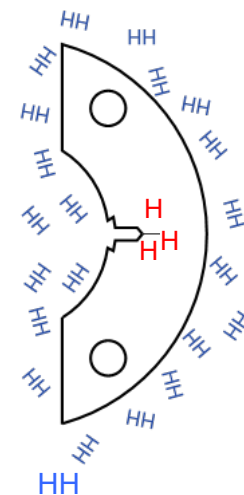
## Environment

- Air
- Pure  $H_2$
- Gas blends, e.g.  $N_2 - 3\%H_2$
- Gas impurity mixtures:  
e.g.  $H_2 + 10-1000 \text{ ppm } O_2$



## Two pipeline materials were examined

Grade	YS (MPa)	Year	Composition in wt. %								
			C	Si	Mn	P	S	V	Nb	Ti	B
X100	910	2000s	0.085	0.26	1.69	0.013	<0.001	-	0.047	0.017	0.0015
X52	490	1962	0.293	0.02	1.17	0.016	0.016	<0.002	<0.005	<0.002	<0.0005

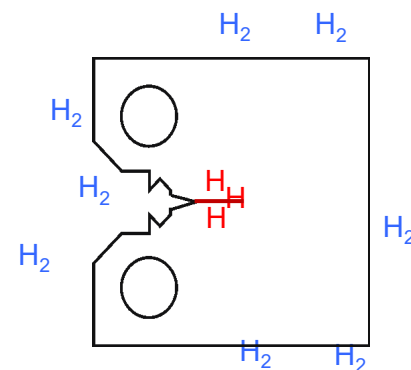
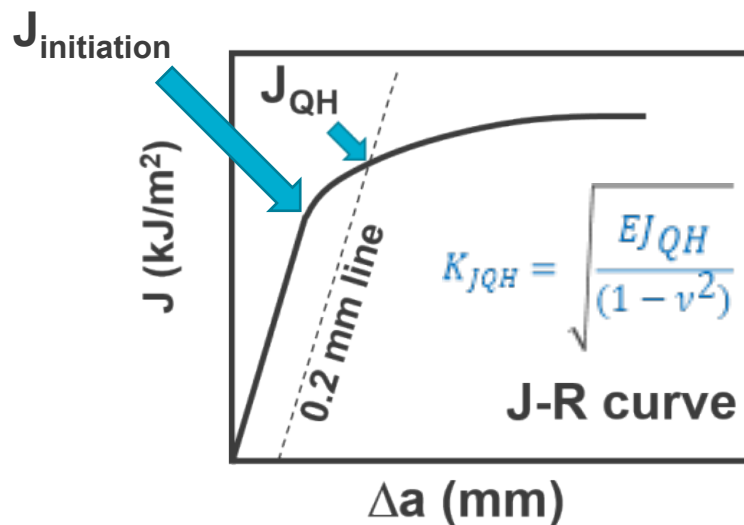
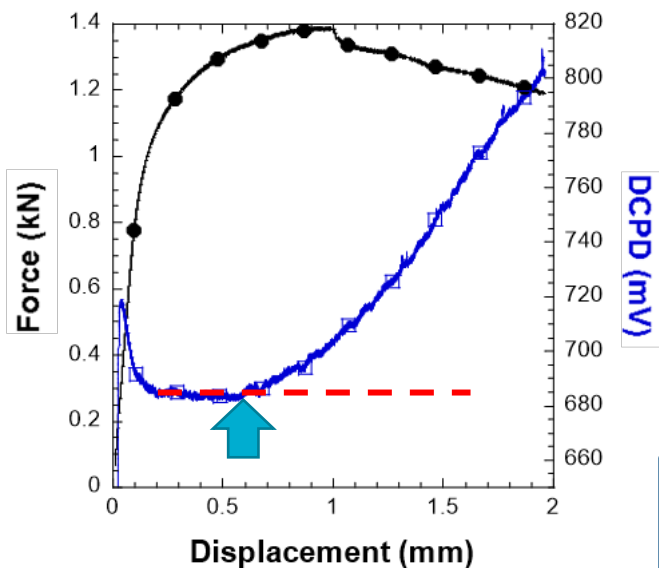


X100  
Arc

□ ASTM E1820 elastic-plastic fracture test (J-R curve)

□ Fracture Displacement Rates:

- 0.005 → 5 mm/min

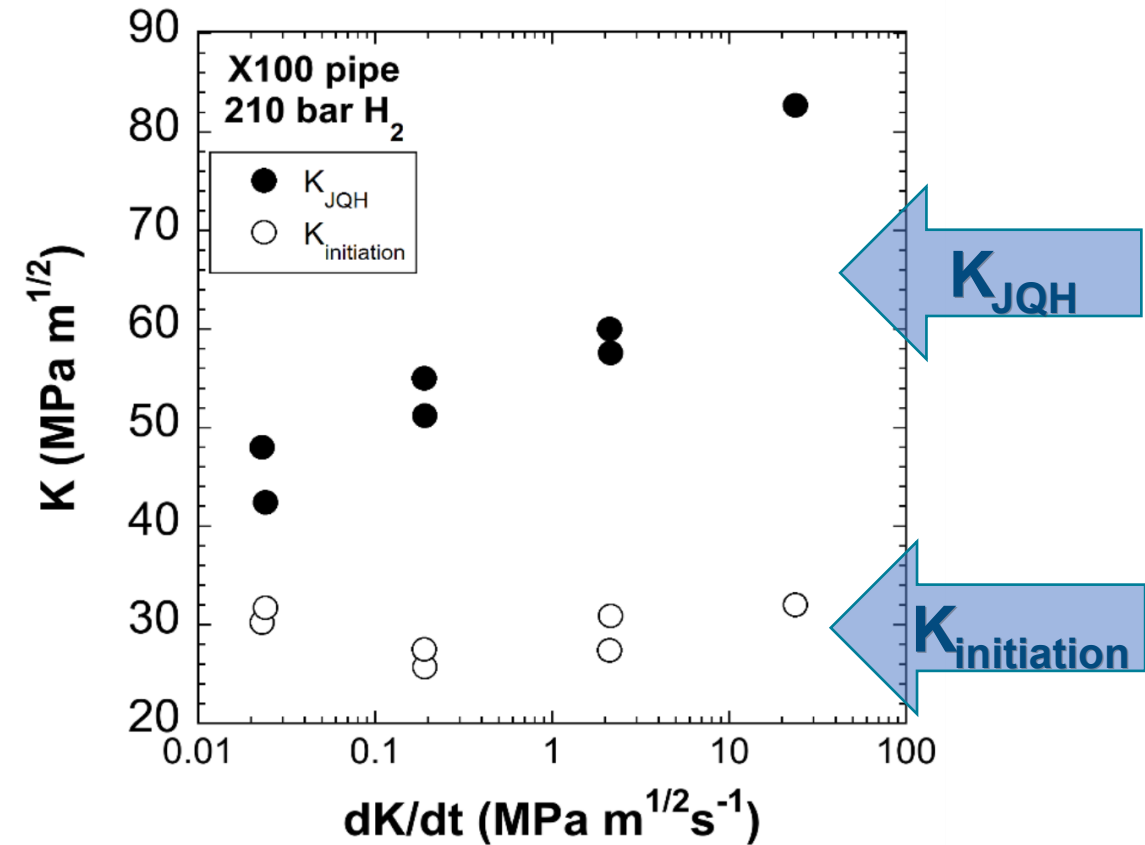
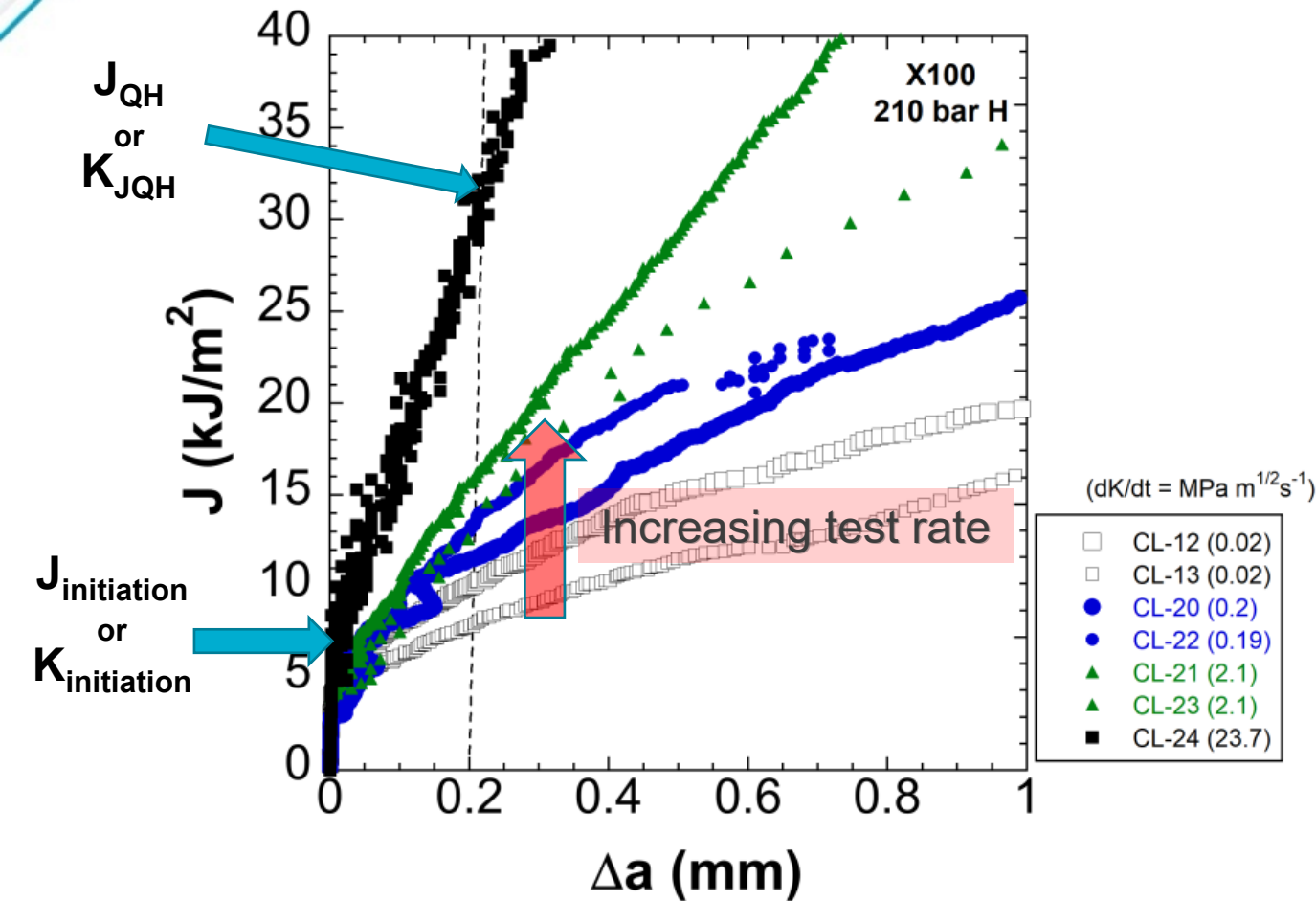


X52  
CT

Determined fracture initiation ( $J_{\text{initiation}}$ ) and fracture resistance ( $J_{\text{QH}}$ ) from J-R curves → converted to K



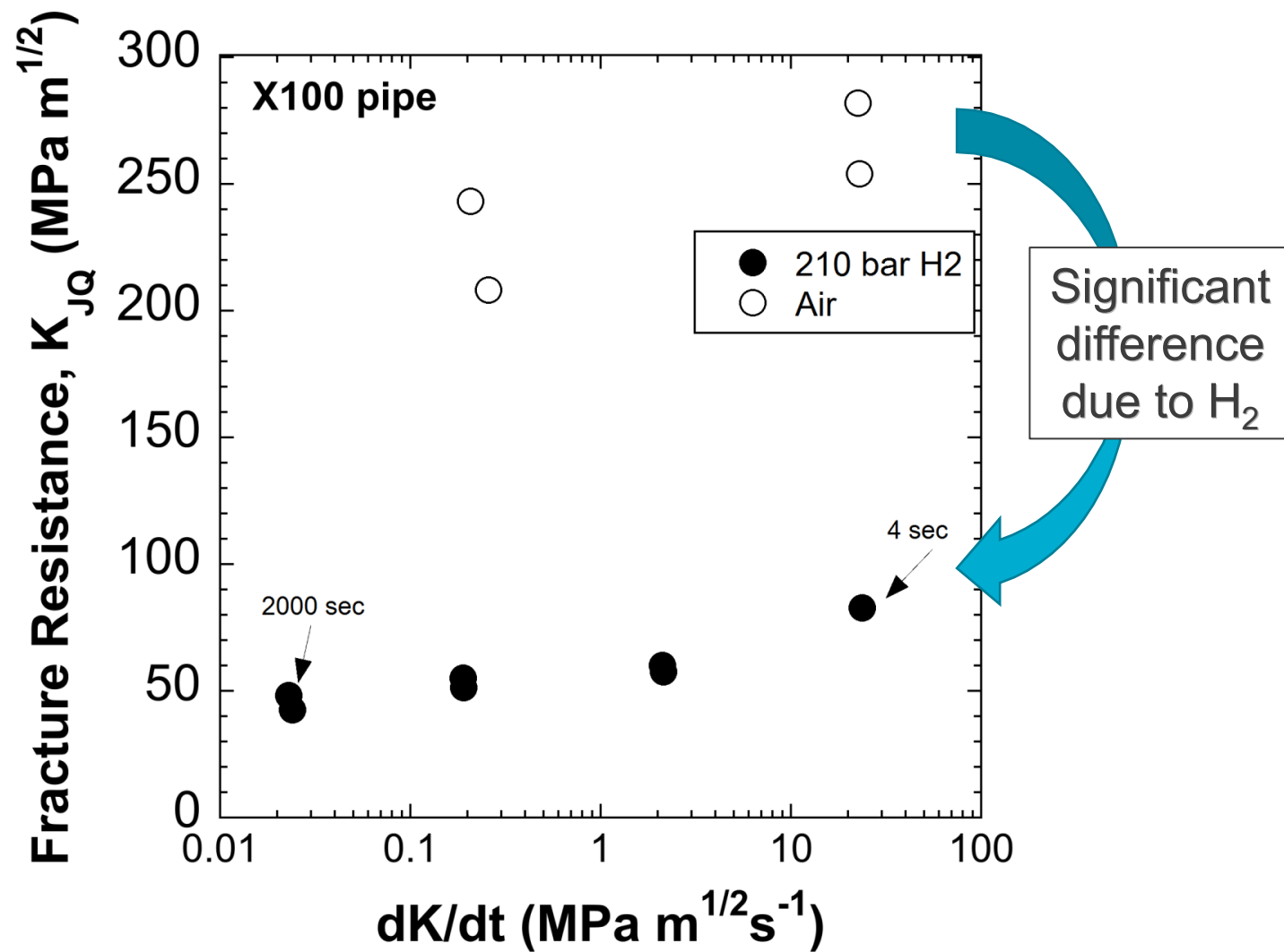
# Tearing modulus is clearly influenced by testing rate



X100 fracture resistance ( $K_{JQH}$ ) was rate-dependent  
→  $K_{initiation}$  was less sensitive to rate



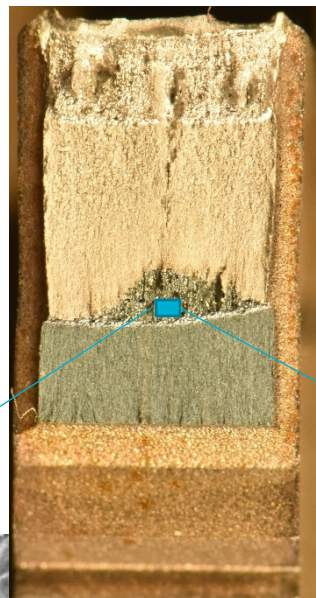
Even at high loading rates, effects of hydrogen cannot be ignored



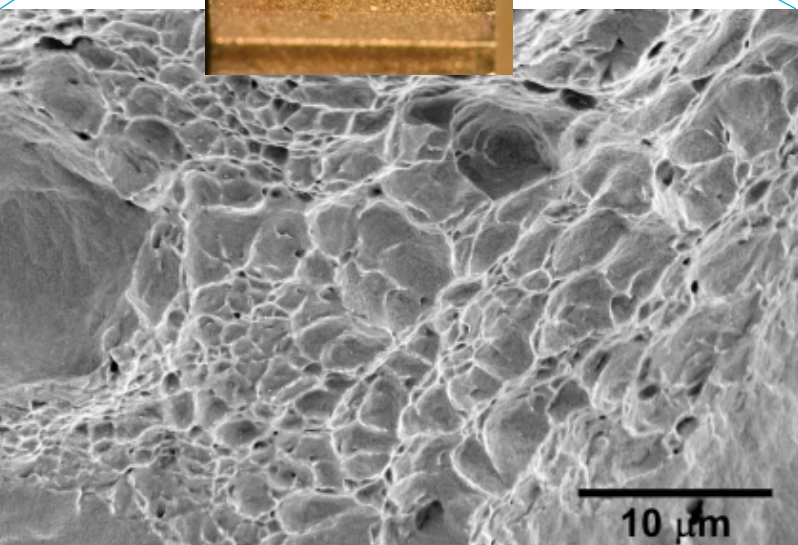


Fracture surfaces still exhibit quasi-cleavage fracture at all rates when tested in gaseous  $H_2$

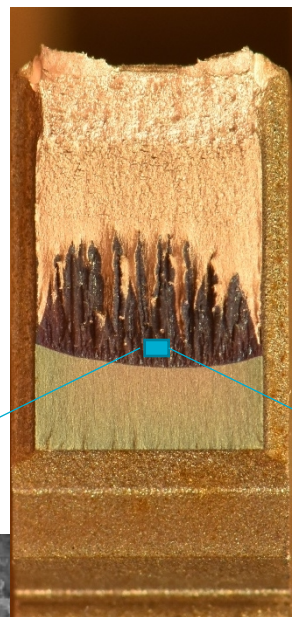
Air (0.05 mm/min)



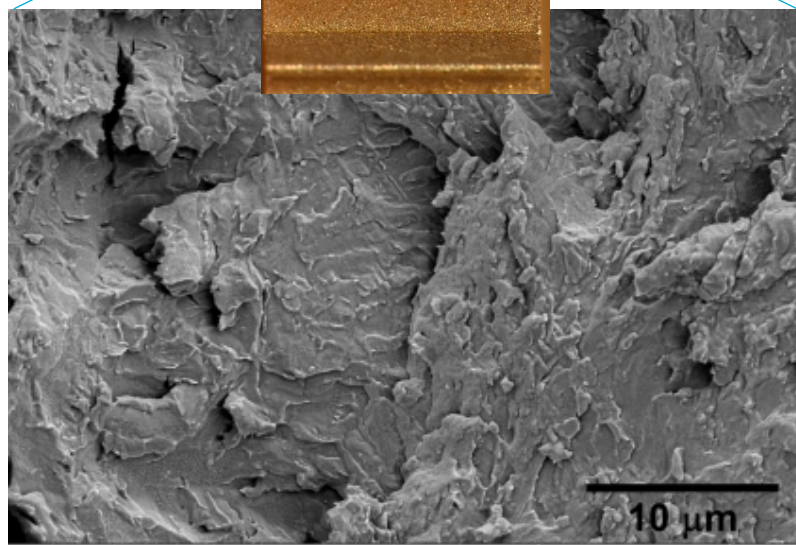
$K_{JQ} = 208 \text{ MPa m}^{1/2}$



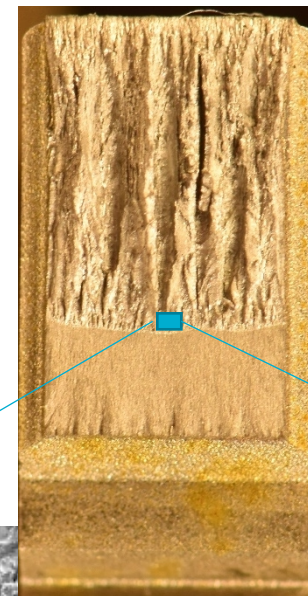
210 bar  $H_2$   
(0.005 mm/min)



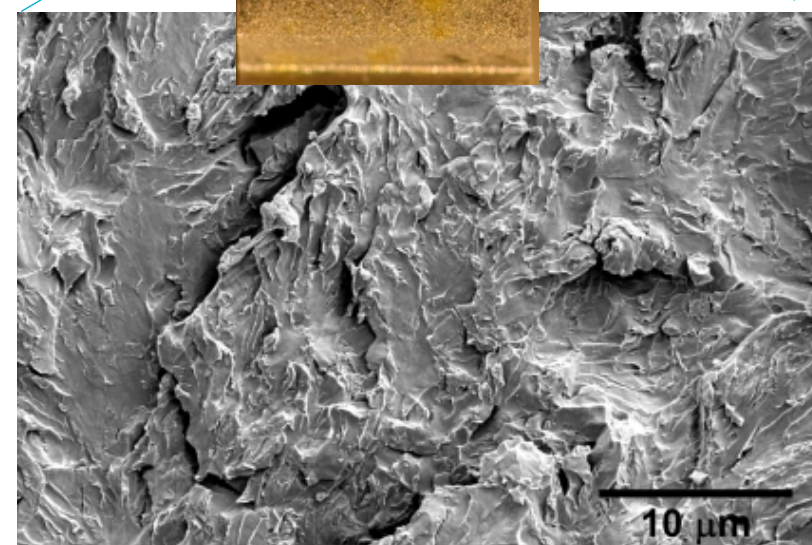
$K_{JQH} = 42 \text{ MPa m}^{1/2}$



210 bar  $H_2$   
(5 mm/min)

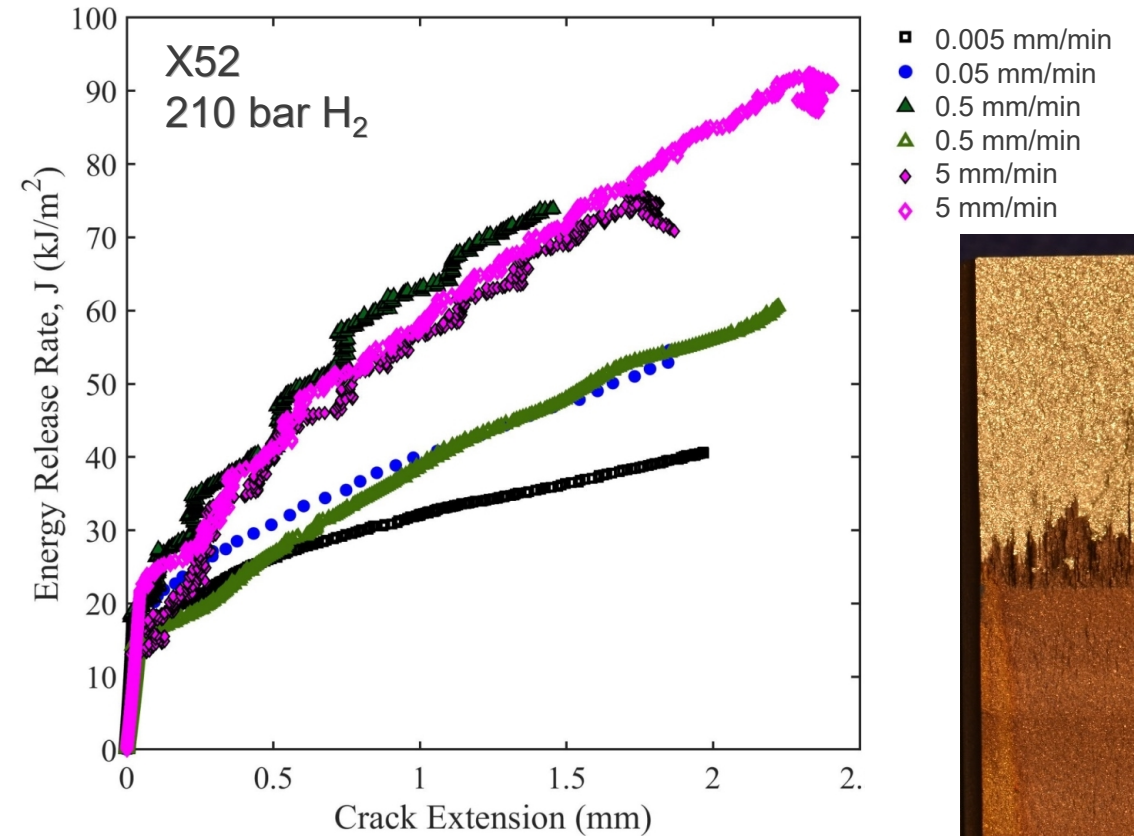
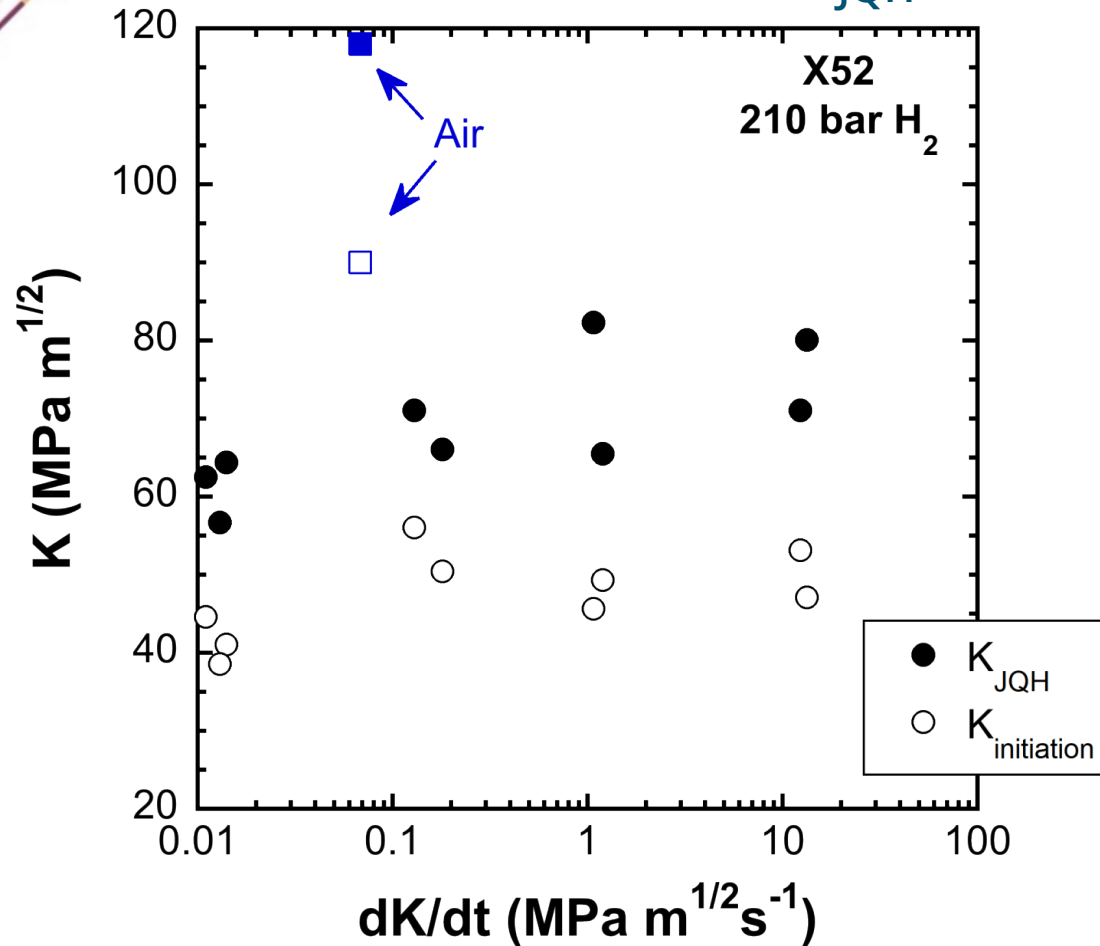


$K_{JQH} = 83 \text{ MPa m}^{1/2}$





X52 showed more variability for  $K_{\text{initiation}}$  and  $K_{\text{JQH}}$   
→ Small increase in  $K_{\text{JQH}}$  with  $dK/dt$



Variability might be due to:

→ Inclusions

→ Smaller difference between air and  $\text{H}_2$  fracture toughness





# Summary

Two pipeline steels (X52 and X100) were subjected to fracture testing in 210 bar  $H_2$  at different testing rates

## X100

- Increased  $K_{JQH}$  at faster testing rates
- Negligible change in fracture initiation ( $K_{initiation}$ ) with testing rate

## X52

- Small increase in  $K_{JQH}$  at faster testing rates
- Fracture initiation ( $K_{initiation}$ ) exhibited more variability

***Hydrogen still influences fracture even at fast testing rates & should not be ignored***

## Gaps Remaining:

- Influence of delaminations on fracture toughness
- Role of inclusions in crack initiation



# Thank you for your attention!

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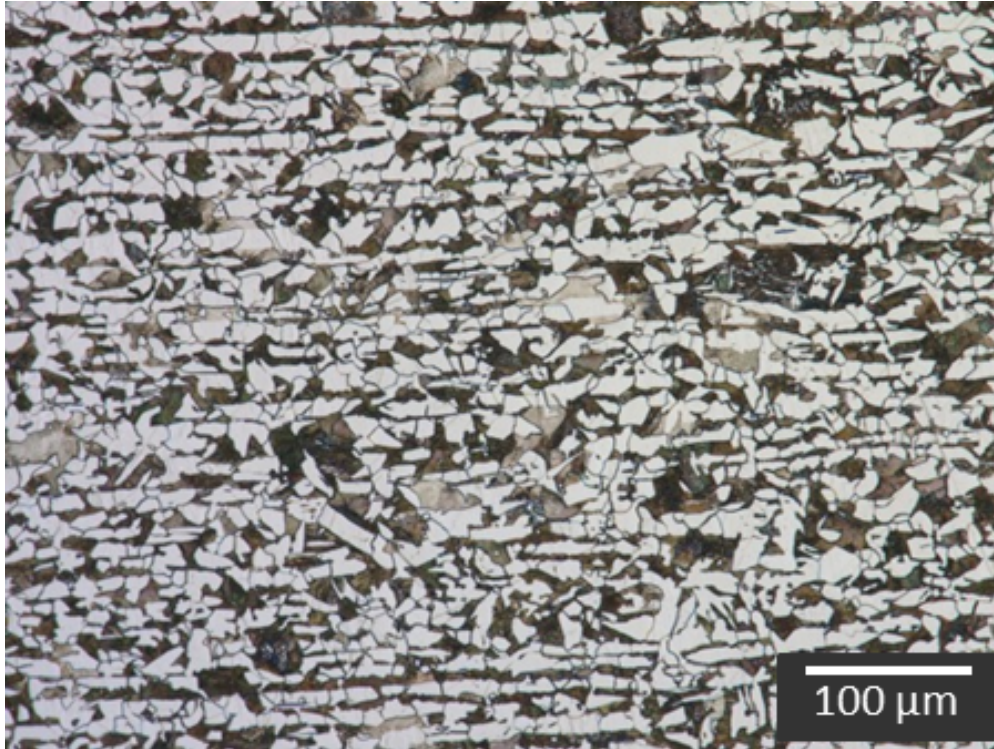
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## Microstructures

X52 – Ferrite/Pearlite



X100 – Acicular Ferrite/Bainite

